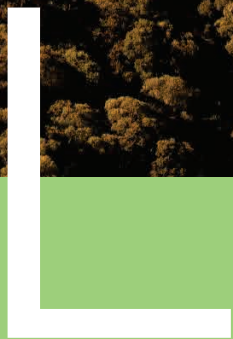




A P P E N D I X



EXCAVATED ROCK PLACEMENT ASSESSMENT

- ANNEXURE C – ENVIRONMENTAL CHARACTERISATIONS OF EXCAVATED ROCKS
- ANNEXURE D – ECOTOXICOLOGY ASSESSMENT OF EXCAVATED ROCK AND
- ANNEXURE E – DISSOLVED ALUMINIUM ASSESSMENT FOR TALBINGO RESERVOIR



Annexure C Environmental Characterisations of Excavated Rocks

Snowy 2.0 Assignment P4: Environmental Categorisation of Excavated Rock Interactions with and Potential Impacts on Reservoir Waters and Sediments

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Foreword and Assignment Summary

CSIRO was requested by Snowy Hydro Limited (SHL) in November 2017 to provide scientific expertise and capability in relation to identifying and assessing the environmental risks associated with the placement of excavated rocks from the development and operations of the proposed Snowy 2.0 scheme. EMM Consulting (EMM) will be preparing the Environmental Impact Statement (EIS) on behalf of SHL, and CSIRO will undertake a series of assignments to provide scientific information for the environmental risk assessment (ERA) associated with the handling of excavated rock materials from the proposed works. In December 2017, CSIRO worked with EMM to develop conceptual models of the proposed works (source, fate and receptors) to provide information to the ERA. As a result, CSIRO was commissioned to undertake an initial series of four assignments.

In March 2018, Haskoning Australia (HKA) was engaged to provide additional capability, specifically to take the role of leading the project entitled: “Engineering Option for Placement of Excavated Rocks”. The draft work assignments that CSIRO had previously provided to SHL and EMM (in late January 2018) were subsequently updated to ensure that they would fulfil the needs of EIS requirements and HKA’s “Engineering Option for Placement of Excavated Rocks” project. These updated assignment(s) have been executed and are providing relevant input into the ERA. This report details the results and findings of Assignment P4: Environmental Categorisation of Excavated Rock Interactions with and Potential Impacts on Reservoir Waters and Sediments.

Disclaimer

This Assignment Subcontract and all documents and information provided by CSIRO to HKA under this Assignment Subcontract are prepared (i) as inputs for further scientific services to be performed for HKA by CSIRO under separate Assignment Subcontracts that has been agreed; and (ii) to assist HKA in its development of a excavated rock disposal and management plan as part of the environmental impact assessment process for the proposed Snowy 2.0 Pumped Hydro Electric Scheme (“Purpose”), and for no other purpose. This Assignment Subcontract does not involve the provision of advice or recommendations in relation to specific risks or mitigations associated with Excavated Rock disposal and management or design and construction of the Snowy 2.0 project however it is understood that the inputs provided by CSIRO are for the Purpose and are based on CSIRO’s professional skill, care and diligence in performing this Assignment Subcontract. In the course of performing this Assignment Subcontract, CSIRO may rely on stated assumptions and/or information provided by HKA or third parties which is not within the control of CSIRO, and this Assignment does not involve CSIRO verifying such assumptions or information except to the extent expressly stated herein. If CSIRO provides any forecasts or projections, CSIRO does not represent that they will be realised as forecast or projected and actual outcomes may vary materially from forecast or projected outcomes. Documents and information provided to HKA under this Assignment Subcontract are to be read as a whole, and if reproduced must be reproduced in full and no part should be read or relied upon out of context. CSIRO does not accept responsibility for, or liability arising from, any error in, or omission in connection with, stated assumptions or third party-supplied information, or reliance on documents or information provided under this Assignment by HKA other than for the Purpose, or by any other person.

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Common Abbreviations/Acronyms

| Abbreviation / Acronym | Description |
|------------------------|--|
| µg | Microgram |
| AEM | Dilute-acid extractable metal (or other element e.g. metalloid) |
| COPC | Contaminant of potential concern |
| CRM | Certified reference material |
| d | Day |
| DGV | Default guideline value |
| DO | Dissolved oxygen |
| DOC | Dissolved organic carbon |
| Eh | Redox potential |
| EIS | Environmental impact statement |
| ERA | Environmental risk assessment |
| GV | Guideline Value, replaces term 'trigger value' (TV) in water quality guidelines (ANZG, 2018) |
| h | Hour |
| kg | Kilogram |
| L | Litre |
| L/S | Liquid/solid ratio |
| LoE | Line of evidence |
| M | Molar = mol per litre (mol/L) |
| mg | Milligram |
| Milli-Q | High purity deionised water |
| mL | millilitre |
| mm | Millimetre |
| NTU | Nephelometric Turbidity Unit |
| PC95(50) | Concentration that is protective of 95% of species (with 50% confidence) |
| QA/QC | Quality assurance/quality control |
| SD | Standard deviation |
| SE | Standard error |
| SQGV | Sediment quality guideline value |
| SOPC | Stressor of potential concern |
| TOC | Total organic carbon |
| TRM | Total recoverable metal (or other element e.g. metalloid) |
| TSS | Total suspended solids |
| WoE | Weight of evidence |
| WQGV | Water quality guideline value |

Chemical symbols and Acronyms

| | | | | | | | |
|-----------------|---|----------------|--------------|------------------------------|------------------|-------------------------------|--------------|
| Ag | Silver | F ⁻ | Fluoride ion | Ni | Nickel | Sn | Tin |
| Al | Aluminium | Fe | Iron | NO ₃ ⁻ | Nitrate ion | SO ₄ ²⁻ | Sulphate ion |
| As | Arsenic | Hg | Mercury | P | Phosphorus | Sr | Strontium |
| Ba | Barium | K | Potassium | Total-P | Total phosphorus | Ti | Titanium |
| Be | Beryllium | Li | Lithium | Pb | Lead | Tl | Thallium |
| Ca | Calcium | Mg | Magnesium | S | Sulphur | Th | Thorium |
| Cd | Cadmium | Mn | Manganese | Total-S | Total sulphur | U | Uranium |
| Cl ⁻ | Chloride | Mo | Molybdenum | Sb | Antimony | V | Vanadium |
| Co | Cobalt | N | Nitrogen | Se | Selenium | Zn | Zinc |
| Cr | Chromium | Na | Sodium | Si | Silicon | | |
| Cu | Copper | | | | | | |
| dAl | Dissolved aluminium (<0.45 µm filtered) | | | | | | |

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Executive summary

Snowy Hydro Limited (SHL) are exploring options for the placement of excavated rock within the two reservoirs Talbingo and Tantangara, as part of a proposed Snowy 2.0 Pumped Hydro Electric Scheme (Snowy 2.0). The excavated rock placement should not compromise, within reasonable parameters, the ecological, chemical, physiochemical, or physical state of the environment in the reservoirs.

CSIRO were engaged by Haskoning Australia (HKA) on behalf of SHL to provide four studies involving tests and data analysis to help inform an Environmental Impact Statement (EIS) for Snowy 2.0. These studies are:

- Assignment P1: Comprehensive Geochemistry Examination;
- Assignment P2: Environmental Risk Categorisation of Rock Materials;
- Assignment P4: Environmental Categorisation of Excavated Rock Interactions with and Potential Impacts on Reservoir Waters and Sediments; and
- Assignment P5: Ecotoxicological Assessment of Excavated Rock Leachates in Water and Excavated Rock-Sediment Mixtures.

This report specifically relates to Assignment P4 - Environmental Categorisation of Excavated Rock Interactions with and Potential Impacts on Reservoir Waters and Sediments.

Assignment P4 provides scientific information to help assess the potential impacts of the excavated rock materials on water and sediment quality within the reservoirs. Rock materials for testing were sourced from seven geological units based on findings from Assignment P2: Environmental Risk Categorisation of Rock Materials (Douglas et al., 2018). Fourteen excavated rock composite materials were prepared to be representative of the possible range of materials being considered for placement in the reservoirs. These comprised two rock composites for each of the seven geological units, for which individual rock materials had been categorised as 'baseline' or 'enriched' based on concentration of sulphur (total S) as described in Assignment P2. The waters and sediments used were from locations where excavated rock placement may potentially occur (Talbingo and Tantangara Reservoirs). A range of exposure scenarios and conditions (i.e. temperature) were evaluated for the interaction of the rock materials with the reservoir waters and sediments, and analyses of changes to water quality associated with the release/attenuation of substances from the rock materials. Here the term 'substances' refers to any elements, ions and chemical compounds that may become classified as contaminants of potential concern (COPCs) or modify water and sediment quality.

Assignment P4 provides information on the lines of evidences (LoEs) relating to stressors of potential concern (SOPCs) that should be considered within the weight of evidence (WoE) assessment framework. The waters of the Talbingo and Tantangara Reservoirs can be classified as having neutral pH (6.9-7.3), low conductivity (26-30 $\mu\text{S}/\text{cm}$), and low turbidity (0.2-0.6 NTU). The background/baseline waters contained no COPCs when compared to Australian national water quality guideline values (ANZG, 2018). Rock materials were available for seven geological units anticipated to be encountered during tunnelling, with fourteen composite samples prepared from <75- μm sized rock materials and used in the majority of the tests. . The reservoir sediments had similar fine particle size. The rock composites and sediments materials contained few metals at concentrations that exceeded the Australian national sediment quality guideline values (SQGVs). For one rock composite material, the concentrations of Ag, Cr, Ni, Pb and Zn exceeded the SQGVs.

During the anticipated period of time the placement of excavated rock will occur within the reservoirs, significant amounts of fine rock material may remain present in the water column, and the finest fractions

may take many days or weeks to settle after the placement activities cease. The release of substances from the rock materials was assessed using a series of elutriate tests that involved mixing and leaching rock materials with reservoir water and covered a wide range of mixing-leaching scenarios and conditions. The tests characterised differences in substance release that may occur due to differences in the concentration of solids in the water (liquid/solid ratio; L/S), time, repeat/successive leaching, rock particle size, temperature, and attenuation of substances released due to interactions with sediments. Substance release was observed to be very similar for rock materials in Talbingo and Tantangara Reservoir waters.

The mixing of excavated rock materials with reservoir waters resulted in increased pH (from approximately pH 7 to 9.5) and conductivity (from approximately 30 to 150 $\mu\text{S}/\text{cm}$). Turbidity was increased in these tests with the $<75\ \mu\text{m}$ rock composites in proportion to the L/S ratio. There were no significant increases in nitrate concentrations and small and variable increases in total-P concentrations. When mixed at high solid concentrations (100 g fine rock/L reservoir water; liquid/solid ratios (L/S) = 10), the concentrations of dissolved ($<0.45\ \mu\text{m}$ filterable) aluminium (Al) exceeded the default guideline value (DGV) for water quality of 55 $\mu\text{g}/\text{L}$. Dissolved As and Cr exceeded DGVs in some L/S=10 tests. Truly dissolved Al ($<0.003\ \mu\text{m}$) rather than colloidal forms comprised the majority of the $<0.45\ \mu\text{m}$ filterable water fraction, with the aluminate ion, $\text{Al}(\text{OH})_4^-$ predicted to be the dominate Al species. Increases in water pH, conductivity and dissolved Al were identified as the primary SOPCs, and were the focus of the subsequent tests. Al was identified as a COPC, where exceeding the DGV may cause toxicity to a range of aquatic organisms.

The concentrations of fine solids in the reservoir waters will be influenced by the properties of the rock (e.g. density, particle size) and the water conditions and the placement procedure. The concentrations of rock materials should decrease with increasing distance from the placement site, with materials of larger particle size settling more rapidly to become sediments, and materials of finer particle size remaining in the reservoir water column for longer and dispersing and becoming diluted with reservoir water (L/S lower in deeper waters and closer to the placement area). The DGV for dissolved Al was exceeded at $\text{L/S} \leq 1000$ ($\geq 1\ \text{g}$ rock solids /L reservoir water, 1 part per thousand) after durations of 18 h, and were exceeded within 0.5 h at a $\text{L/S}=30$. The total-P concentrations were $<10\ \mu\text{g}/\text{L}$ when the reservoir waters contained $<3.3\ \text{g}/\text{L}$ fine rock materials.

The size of the excavated rock material is expected to range from boulder ($>200\ \text{mm}$) to clay ($<0.002\ \text{mm}$). The vast majority of the excavated rock, by mass, will be larger in size than coarse-sand ($>2\ \text{mm}$) and should settle rapidly to form sediments. When mixed with reservoir water, rock materials with particle size $\geq 2\ \text{mm}$ had negligible impact on water quality. For smaller sized rock materials (e.g. $<0.21\ \text{mm}$) mixed with reservoir waters, the pH, conductivity and dissolved Al concentrations increased by a larger extent as the rock particle size decreased, confirming the higher risks of adverse effects to water quality from the finer rock size fractions.

Some portion of the fine rock particles may potentially disperse beyond the target placement area and the release of substances from the solids may continue during this process. Dissolved Al concentrations increased steadily during 1-2 weeks of contact with reservoir water, then decreased and the pH also decreased from pH 9 to 9.5 range (depending on L/S) to nearer pH 8.

The water temperatures of both reservoirs vary between approximately 6°C and 21°C , with significant changes over depth and season. Release of Al from fine rock materials occurred significantly more slowly at 6°C than at 21°C , resulting in fewer elutriate waters exceeding the DGV for dissolved Al.

Greater release of substances may occur from the fine rock materials if they remain in the water column within the placement area or as they disperse away from the placement area. The successive leaches indicated that the Al available for release into solution was not quickly exhausted, with successive leaches often having similar or increased Al concentrations.

Existing benthic sediments in the reservoirs may be resuspended during and following the placement of excavated rock materials in the reservoirs. Tests found that sediments may both release substances and adsorb substances that have been released from the rock materials, with the resuspended sediment concentration and duration of resuspension influencing whether they will act as a sink or a source.

Substance release from excavated rock resulting in stressors of potential concern

The following observations are made with regards to substance release from excavated rock materials in reservoir water that may result in potentially adverse changes to water quality:

- (i) Increases in water pH and conductivity are expected due to rapid release of ions that occur via ion solubility and exchange reactions.
 - Both high pH (e.g. > pH 9) and high conductivity (e.g. >60 $\mu\text{S}/\text{cm}$) may be classified as SOPCs for some sensitive aquatic organisms.
- (ii) Dissolved Al was the only substance consistently identified as a COPC.
 - Dissolved Al concentrations may exceed the DGV.
 - Sustained release of Al may occur from excavated rock materials.
 - Dissolved Al release was negligible for rock materials >2 mm in size.
 - Dissolved Al release increases significantly with decreasing particle size <0.21 mm.
 - Dissolved Al release is markedly lower in waters with temperature of 6°C than at 21°C.
- (iii) Dissolved As and Cr were infrequently identified as COPCs, but only when waters contained >20 g/L fine solids (L/S <50).
- (iv) Resuspension of existing sediments within the reservoirs may buffer the pH closer to that of the reservoir waters, but significant attenuation of dissolved Al was not observed in tests.

Overall, Assignment P4 has identified changes in water pH, conductivity and dissolved Al concentrations as the primary SOPCs in both Talbingo and Tantangara Reservoirs, and that the risk of adverse impacts from these SOPCs will increase as concentrations of fine excavated rock materials increase and the duration the rock materials remaining suspended in the water column increases.

In the summary section of this report, greater discussion is provided on the use of the laboratory-derived data for predicting substance release under excavated rock placement conditions in the field. The technique used for the placement of the excavated rock materials is expected to strongly influence the extent of the potential impacts, and aspects of a range of possible placement techniques are discussed that were outside the scope of the study. Field trials of rock placement techniques at a larger scale would greatly benefit the environmental risk assessment. During field trials, field monitoring should include continuous monitoring of general water quality parameters such as pH, conductivity, temperature and turbidity, and in situ monitoring of dissolved Al to provide time-average concentrations that can be better compared to water quality guidelines when assessing risks.

The summary section also identifies a number of knowledge gaps and provides recommendations for future study to fill knowledge gaps.

1 Introduction

1.1 Background

Snowy Hydro Limited (SHL) are embarking on the development of the landmark Snowy 2.0 Pumped Hydro Electric Scheme (Snowy 2.0). As part of Snowy 2.0, options are being identified and assessed for the management and ultimately disposal of excavated rock as part of an Environmental Impact Statement (EIS) and practical engineering options for its management. There are several challenges that are associated with this expansion and a suitable, extensive but ultimately urgent environmental assessment is necessary. To accomplish Snowy 2.0, SHL will require “drill-out” of 27 km of tunnels between the two reservoirs Talbingo and Tantangara and in the process generate approximately 10 million m³ of excavated rock that will need to be disposed of primarily within these two reservoirs as land-based disposal of significant quantities of excavated rock is not possible within the National Park, nor is it practical to remove it from site.

Haskoning Australia (HKA) have been appointed lead consultant to manage and deliver an Engineering Option Assessment for Excavated Rock Placement for Snowy 2.0. CSIRO has been requested to provide scientific insight into the environmental impacts associated with the excavated rock placement options.

As the subsurface geology was largely unknown, a geological study complemented by a geochemical and mineralogical characterisation was required to determine the composition of the materials to be extracted in the construction phase. The excavated rock will eventually need to be disposed of within the reservoirs, however, initially the excavated rock will be temporarily stockpiled on land and then relocated, along with other materials, into the reservoirs. It is required that the excavated rock be deemed chemically stable now and into the future so the ecological, chemical, physiochemical, and physical state of the environment is not compromised. Further the placement of the excavated rock must:

- not compromise existing reservoir operations during the expansion construction;
- not compromise existing environmental flows;
- ensure extreme and “1 in a 100” year weather events do not impact the long-term stability of the excavated rock placed within either Talbingo or Tantangara Reservoirs, as well as remaining stable under pumping loads of approximately 350 cubic metres per second (cumecs) during expanded hydro operations (intake / outflow); or
- not adversely impact threatened species (both terrestrial and aquatic).

Finally, ensuring all the above, a social licence to operate must be maintained.

1.2 CSIRO work assignments

A series of work assignments were undertaken by CSIRO to inform the EIS:

Assignment P1: Mineralogy and geochemistry characterisation of excavated rock.

Assignment P2: Excavated rock reactivity, leachability, and risk categorisation.

Assignment P4: Environmental characterisation of excavated rock addition to reservoir waters and sediments.

Assignment P5: Effects of excavated rock addition on biota in reservoirs (waters and sediments).

This report relates to Assignment P4 and is provided to HKA to inform their work-programs, considering both the needs of the EIS and the longer-term ecological risk assessment (ERA). Information from baseline

studies (primarily from consultancy firm EMM) and from Assignments P1 and P2 (CSIRO) was used to select a subset of materials (excavated rock, waters and sediments) and exposures.

1.2.1 Context for Assignment P4

For the purpose of Assignment P4, the context for the EIS and ERA was informed by the conceptual site model (CSM) and identification of pathways among pressures, stressors, and likely biological receptors and their responses (Appendix A). In the CSM, placement of excavated rock material was envisaged to occur into deep waters within the reservoirs, possibly via dumping from hopper barges near the water surface that result in rock material dropping through the water column with the intent of depositing within a specific placement depth. The CSM incorporates the services for protection, which, for Snowy 2.0, will include the power assets, ecosystem, and recreational services. The CSM thus enables management aims and goals, community values, and required levels of protection to be defined. The services for protection being considered in Assignment P4 are broadly described as 'water quality', of which sediment quality is a component. The SOPCs may be physical (e.g. suspended solids), physico-chemical (e.g. pH, conductivity, dissolved oxygen (DO)) and chemical (e.g. contaminants released from excavated rock or sediments) and the interactions of these multiple stressors. Based on the CSM and SOPCs, the relevant required LoEs can be determined and the analysis of these LoEs then takes place as part of the monitoring and assessment framework (i.e. considered in the EIS and evaluated in the ERA).

For Snowy 2.0, the assessment issue may be broadly categorised as a 'proposed development in a greenfields (undisturbed) location' or a more general 'development approval' (partly or moderately disturbed). For a greenfields location in advance of future development, the assessment issue relates to the gathering of baseline (pre-disturbance) data and information that enables prediction of potential impacts. Typically, following development of the CSM of existing and future pressures, the assessment should seek to provide an adequate baseline characterisation for defining the water quality and ecological health and potential organism sensitivities (and assessing other baseline pressures). In the case of the EIS, EMM indicated that baseline information on water quality (spatial and temporal) and ecosystem status (i.e. what species and functions require protecting) was being gathered. Establishing the pre-development background conditions is necessary to determine the potential additive effects from additional stressors that might be introduced to the water body as a consequence of the proposed development.

The SOPCs are identified in the CSM (Appendix A). In relation to Snowy 2.0, physical and physico-chemical stressors may be of greater concern (may have a greater impact) than the chemical contaminant stressors (e.g. COPCs for which water and sediment quality guideline values exist). The waters within the reservoirs (in which excavated rock placement may occur) are generally quite clear (low suspended solids), low conductivity (low salts), and have low buffering capacity (low alkalinity). The existing ecosystem will be developed around these conditions, noting that the background studies by EMM will determine and describe these conditions and the existing ecosystem in the EIS. The CSM indicated that important physico-chemical stressors within the Reservoirs waters may include fine crushed rock materials or resuspended sediments, acidity (from potential acid generating rock materials), and salts (that increase water conductivity). Unless significant acidity is generated, it would be unlikely that significant concentrations of COPCs (metals or metalloids) would be released from the excavated rock materials to the reservoir waters.

The quality of the LoEs is an important consideration for the assessment (EIS/ERA), and this is strongly influenced by the type of assessment. In the case of Snowy 2.0 (development approval/greenfield site), use of chemistry and physical stressor data alone may frequently be considered of low quality LoE, and need to be integrated with a biological effects LoE that has been designed to assess potential impacts of stressors on water and sediment biota after development has occurred. For Snowy 2.0, it is unlikely that any baseline toxicity exists at the site(s) (i.e. the baseline ecosystem), but Assignment P5 (Ecotoxicological Assessment of Excavated Rock Leachates in Water and Excavated Rock-Sediment Mixtures) will need to establish the

potential for toxicity at the operating site due to excavated rock placement. This cannot rely on the chemistry and physical stressor information from the baseline and Assignment P4 studies alone, but needs to be supported by site-specific testing to determine the potential sensitivity of the local ecosystem.

Establishing the baseline for the Ecology LoE is important for identifying the key receptors (sensitive species and functions - biodiversity indicators; highlighting key potential sensitivities of the reservoir ecosystem) that should represent the reference/control and potential impact sites (for which risks of adverse effects are to be assessed). This information will assist in identifying classes/types of organisms and habitats that should be considered in more detail during assessment components that seek to predict potential adverse effects from the proposed development (i.e. potential stressors identified in Assignment P4). Thus, the Ecology LoE for the Snowy 2.0 EIS/ERA assists but does not enable a suitable prediction of impacts unless species sensitivity to the stressors has been pre-established. Assignment P5 provides this information through direct assessment of potential effects using toxicity tests on representative and sensitive species/endpoints under conditions (stressor extremes) predicted to potentially exist from Assignment P4. Assignment P5 thus enables a multiple (added) stressor assessment.

Together, information from Assignments P1, P2, P4 and P5, supported by the baseline information is expected to provide the multiple LoEs to enable a WoE assessment to be undertaken (in accordance with current National Water Quality Management Strategy (NWQMS) assessment guidance:

<http://www.waterquality.gov.au/anz-guidelines>). Based on the CSM, an assessment of the potential for elevated bioaccumulation by local organisms seems unlikely to aid the WoE assessment at this stage.

1.3 Environmental characterisation of excavated rock interactions with and potential impacts on reservoir waters and sediments

Assignment P4 intends to address requirements to assess the potential impacts of the excavated rock materials on water and sediment quality within the reservoirs. The project utilises excavated rock materials, and leachates (attenuation study) arising from excavated rock, selected to be representative of the proposed range of excavated rock placement operations. The waters and sediments used for the study will be from locations / depths where excavated rock placement sites may eventually be selected (i.e. most likely locations/sites). This is expected to provide materials suitable for assessing excavated rock/leachate-water-sediment mixing scenarios that cover an adequate range and enable identification of the potential dominant stressors (physical, physico-chemical and chemical).

Within the WoE assessment framework (Appendix A, Figure A3), Assignment P4 will provide information on the LoEs relating to SOPCs. The project will provide information on the potential for the waters and sediments within the reservoir to attenuate (or exacerbate) the stressors (generally indicated by parameter levels or concentration of substances) released from excavated rock material upon mixing with reservoir waters and sediments (i.e. interactions of excavated rock with water alone and with sediments during resuspension and following deposition).

Assignment P4 involved a range of tests designed to provide information on the types, forms, and behaviour of stressors (physical, physico-chemical and chemical) released from excavated rock material upon mixing with reservoir waters and sediments. There were four main work components:

- Physical and chemical characterisation of excavated rock materials.
- Physical and chemical characterisation of waters and sediments used in elutriate tests.
- Substances^a release from excavated rock materials to waters.
- Attenuation of substances released from excavated rock by sediments.

^a Substances include elements, ions and chemical compounds that may become classified as contaminants of potential concern (COPCs) or modify water and sediment quality.

2 Methods

2.1 Waters, sediments and excavated rock materials

The excavated rock samples used in the study were selected based on results from Assignment P2 (Douglas et al., 2018). A total of fourteen composite samples (Appendix B, Tables B1 to B5) were used to represent 'baseline' and 'enriched' materials and seven geological units:

- i. Ravine Group – geology of western portion of the tunnel transect and surge shaft (13 km with (ii));
- ii. Byron/Boraig Group – geology of western portion of the tunnel transect and surge shaft (13 km with (i));
- iii. Shaw Hill Gabbro – in the tunnel transect and constitutes (approximately 1 km);
- iv. Gooandra Volcanics – in the tunnel transect (approximately 5 km);
- v. Peppercorn/Tantangara/Temperance Formations – in the tunnel transect (approximately 9 km). Based on the available information these could not be readily differentiated, but has a mostly similar geology and form a contiguous sequence along the tunnel transect so have been aggregated;
- vi. Kellys Plain Volcanics – in the intake area at the Tantangara Reservoir (approximately 2 km of the tunnel). Note: this material was only available from late in the study and was used in fewer of the tests;
- vii. Felsic/Granite/Gneiss/Ignimbrite – compilation of granitic/extrusive equivalents present at various places along the tunnel transect.

For each of these geological units there were between four and nine individual excavated rock materials available to prepare composites (Table 1). For each sample there were 50 g (<75- μ m) and also core pieces available. The composites for each geological unit were prepared by weighing equal amounts of each individual <75- μ m excavated rock material available for that geological unit and homogenising thoroughly.

Larger pieces of rock (e.g. 3-15 cm length, 2-3 cm thickness) were provided of many of the materials and were used in the laboratory tests investigating the effect of particle size on substance release. Rock samples of varying size categories were prepared using a jaw crusher and sieves to create the following size fractions: 10-25 mm; 2-10 mm, 0.21-2 mm, <0.21 mm. Separate subsamples of rock material were used to also prepare a series of size fractions of 150-210 μ m, 63-150 μ m and <63 μ m.

The reservoir waters (Table 2) and sediments (Table 3) used in the study were provided by HKA and were from locations near the anticipated placement areas for the excavated rock.

Twelve sediment samples (approximately 4 kg each) were collected from 3 sites in the Tantangara Reservoir and 9 sites in Talbingo Reservoir, and transported to CSIRO in Eskys with ice. Seven water samples were collected (approximately 15 L each) in 20-L plastic carboys. For one sample (TAL_PL1B), the carboy was compromised resulting in a leak and it only contained approximately 4 L upon arrival, and was not used for the remainder of the project.

Table 1. Individual <75 µm excavated rock samples used to prepare the composite excavated rock materials.

| Composite name (individual samples in corresponding column) | | | | | | | | | | | |
|---|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 1B | 1E | 2B | 2E | 3B | 3E | 4B | 4E | 5B | 5E | 7B | 7E |
| BH6105 -R-0063 | BH6102 -R-0045 | BH5104 -R-0122 | BH5104 -R-0138 | BH4106 -R-0270 | BH4106 -R-0273 | BH4103 -R-0001 | BH4103 -R-0008 | BH3101 -R-0257 | BH3102 -R-0329 | BH4102 -R-0315 | BH5105 -R-0147 |
| BH4105 -R-0362 | BH7105 -R-0039 | BH5104 -R-0133 | BH5104 -R-0114 | BH4106 -R-0271 | BH4106 -R-0274 | BH4103 -R-0003 | BH3110 -R-0409 | BH3101 -R-0259 | BH3101 -R-0263 | BH4102 -R-0316 | BH5103 -R-0066 |
| BH6105 -R-0061 | BH7105 -R-0396 | BH5101 -R-0055 | BH5104 -R-0109 | BH4106 -R-0272 | BH4106 -R-0276 | BH4103 -R-0011 | BH4103 -R-0026 | BH3101 -R-0261 | BH3102 -R-0331 | BH4102 -R-0318 | BH5103 -R-0080 |
| BH4105 -R-0356 | BH4104 -R-0294 | BH5104 -R-0116 | BH5104 -R-0113 | BH4106 -R-0281 | BH4106 -R-0278 | BH4103 -R-0012 | BH3110 -R-0413 | BH3106 -R-0353 | BH3102 -R-0320 | BH4105 -R-0370 | BH5105 -R-0146 |
| BH4104 -R-0291 | BH4105 -R-0371 | BH5105 -R-0143 | BH8106 -R-0406 | | | BH4103 -R-0014 | BH3110 -R-0407 | BH3104 -R-0395 | BH3102 -R-0322 | BH5104 -R-0115 | |
| BH4105 -R-0363 | BH6101 -R-0226 | BH5104 -R-0120 | BH5104 -R-0110 | | | BH4103 -R-0018 | BH3110 -R-0408 | BH3101 -R-0254 | BH3102 -R-0321 | BH5103 -R-0079 | |
| BH7105 -R-0036 | BH7105 -R-0038 | BH5104 -R-0108 | BH5115 -R-0388 | | | BH4103 -R-0019 | BH3110 -R-0411 | BH3106 -R-0352 | BH3101 -R-0255 | BH7104 -R-0234 | |
| BH6105 -R-0060 | | | | | | BH4102 -R-0312 | BH4103 -R-0017 | BH2102 -R-0345 | BH3102 -R-0319 | | |

Additional details provided in Appendix B, Tables B1 to B5. B = baseline; E = enriched.

For each individual sample, the "R-00XX" identifier tracks the individual samples described in Appendix A7 of Assignment P1.

Table 2. Water samples provided by HKA

| Tantangara Reservoir | | Date | Time |
|----------------------------------|--|-----------|-------|
| TAN-TN2A | | 3/07/2018 | 11:30 |
| TAN-TN3A | | 3/07/2018 | 11:00 |
| TAN-TN1A | | 3/07/2018 | 12:05 |
| Talbingo Reservoir | | Date | Time |
| TAL-PL2A | | 4/07/2018 | 13:50 |
| TAL-PL1A | | 4/07/2018 | 14:00 |
| TAL-PL1B (leaked / contaminated) | | 4/07/2018 | 14:00 |
| TAL-PL2B | | 4/07/2018 | 13:50 |

* Sampling notes and locations in Appendix B

Table 3. Sediment samples provided by HKA

| Tantangara Reservoir | | | |
|----------------------|-----------|-----------|-------|
| Sample I.D. | Depth (m) | Date | Time |
| TN2_P4 | 19 | 3/07/2018 | 11:15 |
| TN1_P4 | 16.5 | 3/07/2018 | 11:45 |
| TN3_P4 | 18.5 | 3/07/2018 | 10:40 |
| Talbingo Reservoir | | | |
| Sample I.D. | Depth (m) | Date | Time |
| RA1_P4 | 31.5 | 4/07/2018 | 10:20 |
| RA2_P4 | 29 | 4/07/2018 | 10:45 |
| RA3_P4 | 28.5 | 4/07/2018 | 11:20 |
| PL1_P4 | 33.5 | 4/07/2018 | 14:20 |
| PL2_P4 | 26.5 | 4/07/2018 | 13:15 |
| PL3_P4 | 27 | 4/07/2018 | 12:35 |
| CA1_P4 | 30 | 5/07/2018 | 11:20 |
| CA2_P4 | 42 | 5/07/2018 | 10:15 |
| CA3_P4 | 48 | 5/07/2018 | 9:45 |

* Sampling notes and locations in Appendix B.

2.2 General analytical procedures

The CSIRO laboratories at Lucas Heights, Sydney, are accredited by the National Association of Testing Authorities (NATA) for all analyses performed for this project. The analysis of trace metals at sub- $\mu\text{g/L}$ concentrations is acknowledged to be technically challenging and necessitates the application of rigorous protocols for container preparation, sample collection and analysis to ensure the accuracy of results. State-of-the-art protocols, as outlined by USEPA (1996) and Angel et al. (2010) were used throughout this work. Plasticware used for metals analyses was either new or acid-washed prior to use with a minimum soak for 24 h in analytical reagent (AR) or Tracepur nitric acid (Merck). Deionised water used was from a Milli-Q system (18 M Ω .cm, Millipore, Australia).

2.2.1 Quality control: general procedures and analysis acceptance criteria

For all analyses, at least three analytical blanks were measured per batch of samples for the determination of mean blank metal concentrations and limits of detection ($3 \times$ standard deviation (3σ)).

For all analyses, at least 10% of the samples had method duplicates analysed to confirm the precision of analytical procedures.

To assess the potential matrix interferences during metals analyses, spike recoveries were performed for at least 10% of the samples.

To confirm the analytical accuracy, aliquots of certified reference materials were analysed with each batch of samples whenever a suitable reference material was available. Reference standards have certified concentrations of elements for a range of sample matrices such as freshwater and sediment, allowing the performance of the analytical procedures to be assessed by a comparison of the results obtained with the certified concentrations. The following reference materials were used: TM-24.4 and TMDA-64.3 waters from Environment and Climate Change Canada), ERM-CC018 (European sandy soil reference material) and OREAS-25a (Australian reference soil).

The general acceptance criteria for the analyses included:

- Method duplicates; relative standard deviation is 100% for concentrations ≤ 5 times limit of detection (LOD), 50% for concentrations between 5 to 10 times the LOD, and 20% for concentrations ≥ 10 times the LOD;
- Spike recoveries; within 85-115%. Spike recoveries are investigated if outside this range. A common cause of poor spike recoveries is the metal spike is low relative to the concentration in the sample (i.e. spike less than a quarter of the measured concentration). For a batch of samples, if spike recoveries are acceptable for all samples other than ones where the spike is low relative to the measured concentration, the poor spike recoveries are treated as not being representative and are ignored; and,
- Certified reference materials (CRMs); within 85-115% of the certified value specified by certifying authority or within the certified concentration range. CRM material recoveries are investigated if outside this range. Common causes of poor CRM recoveries are the concentrations are low and near the LOD, or are not homogenous for particulate matter.

2.3 Waters

2.3.1 Water sample filtration

For the purpose of sample filtration for measurement of dissolved metals and metalloids, acid-washed (10% v/v nitric acid) plastic syringes (Terumo) fitted with 25 mm 0.45- μ m cellulose nitrate capsule filters (Sartorius Minisart) were used (Angel et al., 2015). Before filtering the samples, a 12 mL volume of deionised water followed by 3 mL of sample was passed through each filter to waste to precondition. Then 10-30 mL of sample was filtered into acid-washed polycarbonate filtrate receiving vials. The filtered samples for dissolved metals analysis were preserved by acidifying with 0.2% v/v nitric acid (Merck, Tracepur) immediately after filtration. The samples requiring measurement of anions were not acidified and were placed into a refrigerator to minimise any chemical changes before measurement.

Ultra-filtration of waters to <0.003 μ m

For the test investigating the size fractionation of Al described below (Section 3.4.9), ultrafiltration was used to measure truly dissolved metal concentrations and determine whether the <0.45 μ m fraction comprised a significant concentration of metals are associated with colloidal species. The method used was similar to that described in Angel et al. (2013), and used Macrosep Advance 3K Omega ultrafiltration centrifugal devices (Pall-Gellman, Port Washington, USA) that had a 3 kDa molecular weight cutoff (equivalent to filtration membrane of approximately 0.003 μ m). Each solution added to the devices was centrifuged at 1500 g for 20 min to filter it through the 3 kDa membrane. The ultrafiltration devices were pre-conditioned with 20 mL of Talbingo or Tantangara Reservoir waters (discarded), followed by 20 mL of the treatment solutions. The filtered treatment solutions were subsampled for individual analysis.

In order to verify that the Al did not adsorb to the filter membrane, a dissolved Al control solution (25 μ g/L), prepared by addition of $\text{AlCl}_3 \cdot 6\text{H}_2\text{O}$ to synthetic freshwater (Angel et al., 2013), was subsampled and analysed before and after ultrafiltration ($n=3$). The Al recovery (mean \pm standard deviation) after ultrafiltration of $101 \pm 7\%$ confirmed all of the dissolved Al passed through the ultrafiltration membrane without significant adsorption/loss occurring.

2.3.2 General water quality measurements

The pH, conductivity and DO in waters were measured using an Orion Star A329 meter (Thermo Scientific). The pH was measured using a Thermo Scientific Orion Gel-Filled ROSS pH Ultra Triode Electrode (8107UWMMD) that was calibrated using pH 4.00, 7.00 and 10.00 buffers. The conductivity was measured using a Thermo Scientific Orion Conductivity Cell (013010MD) that was calibrated using potassium chloride (KCl) conductivity standards. The DO was measured using a Thermo Scientific Orion RDO optical DO sensor (087010MD) calibrated with water saturated air within its calibration sleeve.

The alkalinity (as total CaCO_3) of samples was measured via titration of each sample with standardised sulphuric acid to an end point at pH 4.5 (Method 2320B, APHA 2015).

Dissolved ammonia was analysed colourmetrically using an ammonia test kit (API) and a refined method based on the manufacturer's instructions. The sediment porewaters analysed for ammonia were isolated from the sediment by completely filling a 50 mL centrifuge tube with sediment (zero head space) then centrifuging at 1000 g for 3-5 min.

Dissolved concentrations of major and minor anions and cations (including most metal(loid)s and rare earth elements) were quantified using a combination of inductively coupled plasma atomic emission spectrometry (ICP-AES) (Varian730 ES, in-house method C-229) and inductively coupled plasma-mass spectrometry (ICP-MS) (Agilent, 8800, in-house method C-209). Major cations (Ca, K, Mg, Na, Al, Fe, Si) and

Sr were measured by ICPAES. The Ag, As, Ba, Be, Cd, Co, Cr, Cu, Li, Mn, Mo, Ni, Pb, Sb, Se, Sn, Th, Ti, U, V and Zn were measured by ICPMS. The spectrometers were calibrated using matrix-matched standards and operated under the standard operating conditions recommended by the manufacturer.

The major anions Cl^- , F^- , NO_3^- and SO_4^{2-} were measured by suppressed ion chromatography based on APHA Method-4110B using a Shimadzu HPLC system with Merck Sequant Suppressor and conductivity detection. A Shodex IC SI-90 4E column was used with a 12 mM Na carbonate buffer. The HPLC system was calibrated using certified anion standards and samples were diluted (if need) using Milli-Q water to within the linear calibration range. Total-P was analysed by ICPAES, and used to provide an upper limit estimate for reactive phosphate (PO_4^{3-}).

The total organic carbon (TOC) in filtered samples (i.e. dissolved organic carbon (DOC)) was analysed using a Shimadzu TOC-LCSH Total Organic Carbon Analyser following the method APHA 5310B (APHA, 2015). In brief, the total organic carbon (TOC) was calculated from the difference of total carbon (TC) and inorganic carbon (IC) measurements (i.e. TC-IC). The TC was analysed following catalytic oxidation to CO_2 at 680°C, followed by measurement by non-dispersive infrared analysis (NDIR). The IC was analysed by measuring the CO_2 after purging the sample with phosphoric acid to convert carbonates to CO_2 .

2.4 Sediment and rock samples

2.4.1 General analyses

Laser particle size analyses were made using a Malvern Mastersizer 3000, and operating conditions recommended by the manufacturer. In brief, the sediment and excavated rock material were homogenised and approximately 2 g transferred into a 30 mL plastic vial that had been rinsed with deionised water to remove any dust contamination, followed by the addition of approximately 25 mL of deionised water and mixing. A plastic pasteur pipette was then used to draw in and out the sample five times to mix without the addition of air bubbles, after which an aliquot was added to the wet cell of the instrument and sonicated at 100% power for 30 s before measurement of laser diffraction. The international scales are used when referring to particle size (ISO 14688-1:2002): clay (<0.002 mm), fine silt (0.002-0.0063 mm), medium silt (0.0063-0.02 mm), coarse silt (0.02-0.063 mm), fine sand (0.063-0.2 mm), medium sand (0.2-0.63 mm), coarse sand (0.63-2.0 mm), gravel (fine to coarse; 2-63 mm), cobble (63-200 mm), boulder >200 mm).

The moist solid pH was determined using a 1:5 solid/water extract, as described by Rayment and Lyons (2011a). Approximately 10 g of air dried solid was shaken with 50 mL water for one hour and then left to settle for 20 min. The pH was then determined using a Metrohm 815 Robotic Processor and Metrohm 854 glass electrode.

Total carbon was determined by high temperature combustion in an atmosphere of oxygen using a Leco TruMAC (Matejovic, 1997). Carbon was converted to CO_2 and determined by infrared detection. The Inorganic carbon was determined by reacting the sample with acid in a sealed container and measuring the pressure increase (Sherrod et al., 2002; Rayment and Lyons, 2011b). Sufficient finely ground sample to contain no more than 0.8 g CaCO_3 equivalent was weighed into a 250 mL glass bottle, a tube containing 8 mL of 3-M hydrochloric acid (HCl) and 3% Fe(II)Cl_2 was added and the bottle sealed. The contents were mixed intermittently during a 1 h period and the pressure in the bottle measured by piercing the septum with a needle attached to a pressure transducer. Organic carbon content was determined by difference.

The cation exchange capacity (CEC) was determined using ammonium chloride (NH_4Cl) solution at either pH 7.0 or pH 8.5 dependent on solid pH (Rayment and Lyon, 2011c). Non-calcareous solids use extraction solution pH 7.0 and alkaline solids use extraction solution pH 8.5. Samples were pre-treated for soluble salts prior to extraction, and analysed using a Flow Injection Analyser.

2.4.2 Elemental analyses

Total recoverable metals (TRM)

The total recoverable metals (and other elements) in the sediment and rock materials (<75 µm) were extracted within pre-cleaned Teflon digestion vessels using aqua regia in a microwave-assisted reaction system (CEM, MARS). The Teflon vessels were extensively cleaned using in-house method C-226. In brief, the sediments were freeze-dried (Christ Alpha 1-2 LDplus) and ground to a powder using a mortar and pestle before the strong concentrated acid extraction. The sediments and rock samples were weighed into the pre-cleaned MARS Teflon vessels to which 9 mL of concentrated nitric acid (HNO₃, Merck Tracepur) and 3 mL of concentrated hydrochloric acid (HCl, Merck Tracepur) were added. The MARS Teflon vessels were capped and inverted 2-3 times to ensure that all the solid material is contained in the acid. The CEM MARS system was operated at 1600 Watts and the samples were heated to 175±5°C over a ramp time of 12 min. Once the samples reached 175±5°C the samples were held for 4.5 min at this temperature. Following the microwave heating program the vessels were allowed to cool for 30 min in the CEM MARS system and then uncapped to vent the toxic chlorine and nitrogen oxide gases. 40 mL of deionised water was added to each vessel and the vessel stoppered and mixed well by inversion. The digests were left to stand overnight so that the fine solid material settled to the bottom of the vessel. Approximately 20-30 mL of digest was transferred to an acid-washed polycarbonate vial. The digest solutions were subsequently diluted 10-fold using deionised water and analysed using a combination of ICPAES (Varian730 ES) and ICPMS (Agilent 8800 CE) with matrix-matched calibration standards.

Dilute-acid extractable metals (AEM)

Dilute-acid extractable metals (AEM) were determined for each sediment and rock material using an extraction in 1 M HCl (prepared by diluting 36% HCl, 12 M, Merck Tracepur) for 60 min, followed by filtration (<0.45 µm) (in-house method C-241). The extraction treatments (~10 g/L) were shaken for 20 min over the 60 min extraction duration. The 1 M HCl sample extracts were subsequently diluted 10-fold using deionised water and analysed using a combination of ICPAES (Varian730 ES) and ICPMS (Agilent 8800 CE) with matrix-matched calibration standards.

2.5 Substance release from excavated rock materials to waters

Mixing-leaching tests (forms of elutriate tests) were performed on the excavated rock materials to gain an understanding of the release of substances following mixing with reservoir waters. The mixing test methods used were selected following consideration of a range of methods developed in Europe and the USA for the purpose of providing information on the concentrations and potential loads of substances released from the rock materials over time. Leaching for a range of liquid/solid ratios (L/S) were used to develop relationships between the load of substance released and mass of rock (fraction of substance available for leaching). The L/S ratios tested were intended to cover scenarios from worst case (e.g. L/S=10 = 100 g/L) to those representing solids concentration in the water column after sedimentation/settling (e.g. L/S = 3000 = 0.33 g/L). The fraction of a substance released from a rock material generally varies widely between elements, and generally there is a poor correlation between total and potentially leachable concentrations. Replicates were generally performed for 10% of tests.

The leaching kinetics were studied to provide information on changes in dissolved concentrations over time, the release mechanism (ion exchange, dissolution) and available substance load. The effect of rock particle size was investigated to enable relationships to be developed between rock fractions (surface area) and substance load. Successive leaches were undertaken to provide information on available load of the substance being released. The effect of water temperature on substance release was also investigated as the water temperature exhibits substantial variation over seasons and reservoir depth, as well as to provide

information on the substance release mechanism (e.g. dissolution kinetics). Analyses were made of pH and conductivity and dissolved substances (<0.45 µm filterable concentrations of substances). The analyses focussed primarily on inorganic substances (e.g. metals, metalloids and major cations), with alkalinity and anions being analysed in some of the tests. Al was identified early within the testing as the principal substance of interest (COPC) and additional analyses were made to investigate the significance of colloids. The influence of sediments on attenuation of substance released from rock materials was also investigated.

Talbingo Reservoir water was used for most tests as Talbingo Reservoir was anticipated at the time of undertaking the testing to be the location where most of the excavated rock material could be placed (Greg Britton, personal communication).

2.5.1 Elutriate tests

The rock-water elutriate (mixing-leaching) tests were undertaken as bottle-rolling tests, in which a pre-determined amount of the rock material were resuspended in a known volume of test water, after which samples were taken for analyses after set periods of time. Unless otherwise specified, tests were conducted at room temperature (21±2°C) in closed containers (acid-washed polycarbonate (PC) vials or low density polyethylene (LDPE) bottles) and DO measurements indicated that samples remained well oxygenated (e.g. approximately 8 mg/L DO). When considering all the tests, a wide range of mixing-leaching scenarios were investigated and the exact description is provided in the corresponding results section. In brief:

- Liquid to solid ratios (L/S) tested included L/S = 10, 30, 300, 500, 1000, 3000, 5000 and 10000; being equivalent to 100, 33, 3.3, 2, 1, 0.33, 0.2 and 0.1 g/L, respectively, where S = excavated rock.
- Mixing periods prior to measuring substance release generally included times of 0.5, 1, 3, 4, 6, 18, 24, 48 and 120 h, with a longer-term test that investigating substance release being run for 8 weeks.
- The primary rock materials had been milled to <75-µm size as part of Assignment P1. Tests were also conducted on different size fractions of excavated rock materials that had size categories 10-25 mm; 2-10 mm, 0.21-2 mm and <0.21 mm (composite fine material). The core samples received were ground using a jaw crusher plant to create rock materials of size ranges that were then separated using sieves. This plant created a wide range of uneven shapes but were generally more flat than square. The crushed materials were sieved through plastic sieves to create the following size fractions: >10 mm; 2-10 mm, 0.21-2 mm and <0.21 mm (fine material). Owing to the varied shapes, the different size ranges included fractions that were able to pass through the sieve in a single direction but would not pass if perpendicular (e.g. long thin piece could pass). This was considered when selecting fractions for the tests, where the aim was to have pieces that were more 'square' than flat or thin. For a small number of rock materials tests were conducted on a finer particle size range prepared by sieving the <210 µm material to create size categories of 150-210, 63-150 and <63 µm (composite fine material).
- The effect of temperature was investigated by tests undertaken at both 21±2°C and 6±1°C (conducted in a refrigerator).
- Repeated mixing-leaching of rock materials was undertaken, and included three successive leaches lasting time period of 0.5 and 18 h at several L/S ratios.
- The effect of the presence of sediments (PL2) on substance attenuation was investigated using elutriates created at L/S = 500 (2 g rock/L reservoir water) and sediment at L/S = 50 and 500 (20 and 2 g/L, respectively).
- The effect of resuspended sediment concentration on substance attenuation was investigated using an elutriate created by adding 4 g of composites 1B, 2B, 5B, 5E and 7E (i.e. 20 g of solids) to 2

L of Talbingo water and mixing for 24 h. An aliquot of elutriate was mixed with sediments CA3, PL2, RA1 at sediment TSS concentrations of 1, 5 and 25 mg/L for 30 s, and subsampled after 1 and 24 h.

- The effect of deposited sediment (approximately 2 cm on bottom of 50 mL tube) on substance attenuation was investigated using the above elutriate composite and subsampling after 1, 6, 24 and 96 h.

3 Results

For the majority of the tests and analyses undertaken in the project, summaries of what we considered to be key results were reported to HKA and SHL via a series of Memos (13) and Presentations (3) as the results became available. The memos contained preliminary data and some values have been updated in preparing the report sections below. Each Memo is provided in the appendices together with final data summaries.

3.1 Characterisation of Talbingo and Tantangara Reservoir waters

These results were described in Memo 1 (25 September 2018) (Appendix C).

The pH, conductivity, DO, turbidity, alkalinity and DOC measured in the Talbingo and Tantangara Reservoir waters are shown in Table 4. The pH, conductivity, DO and alkalinity were similar in both reservoirs and ranged from 6.93 to 7.27, 26.5 to 29.4 $\mu\text{S}/\text{cm}$, 9.19 to 10.1 mg/L , and 11.5 to 12.5 $\text{mg CaCO}_3/\text{L}$, respectively. The turbidity in the Tantangara Reservoir was in the range 0.51-0.60 NTU, which was relatively low but slightly higher than that measured in Talbingo Reservoir of 0.20-0.34 NTU. The DOC ranged from 1.2-2.3 mg/L , with the Tantangara Reservoir having nearly double the concentration as the Talbingo Reservoir. The hardness of the Talbingo and Tantangara Reservoir waters based on the concentrations of Ca and Mg is shown in Table 5. The hardness was in the range 7.47-8.05 $\text{mg CaCO}_3/\text{L}$, with the Talbingo Reservoir being slightly less hard than the Tantangara Reservoir.

The concentrations of major cations are shown in Table 5. The dissolved Ca, K, Mg and Na were in the range 1.63-1.91, 0.426-0.569, 0.755-0.967 and 1.44-1.57 mg/L , respectively. Talbingo Reservoir had a slightly higher concentration of dissolved Ca, while Tantangara Reservoir had slightly higher concentrations of K and Mg, and Na was of a similar concentration in both reservoirs.

The concentrations of Ag, Al, As, Ba, Cd, Co, Cr, Cu, Fe, Mn, Mo, Ni, Pb, Sb, Se, Sn, Sr, Th, U, V, Zn are shown in Table 6. The concentrations of dissolved Ag, Be, Cd, Li, Mo, Sb, Se, Sn, Sr and Tl were similar in both reservoirs. The concentrations of dissolved Al, As, Ba, Co, Cr, Fe, Mn, Ni, Pb, Th and V were higher in Tantangara Reservoir than Talbingo Reservoir. The dissolved Al, Fe and Mn concentrations were a factor of 6, 15 and 10 times higher in Tantangara Reservoir waters, and were subsequently found to be predominantly comprised of colloidal phases using measurements size fractionation (0.45 μm vs 0.003 μm , Appendix D8). The concentrations of dissolved Ag, Al, As, Ba, Be, Cd, Co, Cr, Fe, Li, Mn, Mo, Ni, Pb, Sb, Se, Sn, Sr, Th, Tl and V exhibited little intra-reservoir variability for the multiple sites sampled in each reservoir, indicating surface waters are well mixed throughout each reservoir. The concentrations of dissolved Cu, U and Zn were generally higher in Talbingo Reservoir than Tantangara Reservoir, however, site TAL-PL1B contained over 5 $\mu\text{g}/\text{L}$ of Cu, attributed to likely contamination during collection and transport; this carboy was damaged and had a leak.

The concentrations were compared to the corresponding guideline values (GVs) for water quality ANZG (2018), representing the 95 and 99% of species protection concentrations Table 6 when values were available. The only exceedance of the default guideline values (DGV) was for Cu in sample TAL-PL1B, and that was attributed to the aforementioned potential contamination. All sites exceeded the 99% guideline value (99% GV) for dissolved Cr, however, it should be noted that the only value available for comparison was for hexavalent Cr being in the hexavalent form, which is unlikely due its' stability. The dissolved Al concentration exceeded the 99% GV in Tantangara Reservoir waters, with approximately 80% of the dissolved (<0.45 μm) speciation subsequently being found to be in colloidal forms (Appendix D8).

Table 4. The pH, alkalinity conductivity, DO, turbidity, and DOC in Talbingo and Tantangara Reservoir waters

| Site Code | Reservoir | pH | Alkalinity (mg CaCO ₃ /L) | Conductivity (µS/cm) | DO (mg/L) | Turbidity (NTU) | DOC ^a (mg/L) |
|-----------|------------|-----|---|-------------------------|--------------|--------------------|----------------------------|
| TAL-PL1A | Talbingo | 7.2 | 12 | 26.5 | 9.7 | 0.20 | 1.3 |
| TAL-PL2A | Talbingo | 6.9 | 12 | 27.3 | 9.6 | 0.34 | 1.2 |
| TAL-PL1B | Talbingo | 7.3 | 12 | 28.9 | 9.5 | 0.26 | 1.3 |
| TAL-PL2B | Talbingo | 7.2 | 12 | 28.3 | 9.5 | 0.22 | 1.3 |
| TAN-TN1A | Talbingo | 7.2 | 13 | 28.4 | 9.2 | 0.51 | 2.2 |
| TAN-TN2A | Tantangara | 7.2 | 12 | 29.4 | 10 | 0.60 | 2.2 |
| TAN-TN3A | Tantangara | 7.1 | 12 | 28.7 | 9.9 | 0.54 | 2.3 |

Table 5. The concentrations of major cations and water hardness in Talbingo and Tantangara Reservoir waters

| Site Code | Hardness (mg CaCO ₃ /L) | Na (mg/L) | K (mg/L) | Mg (mg/L) | Ca (mg/L) |
|-----------|---------------------------------------|--------------|-------------|--------------|--------------|
| TAL-PL1A | 7.5 | 1.51 | 0.43 | 0.81 | 1.88 |
| TAL-PL2A | 7.5 | 1.5 | 0.43 | 0.82 | 1.87 |
| TAL-PL1B | 8.0 | 1.62 | 0.45 | 0.87 | 2.00 |
| TAL-PL2B | 7.5 | 1.51 | 0.43 | 0.82 | 1.87 |
| TAN-TN1A | 8.1 | 1.65 | 0.57 | 1.04 | 1.73 |
| TAN-TN2A | 8.0 | 1.64 | 0.56 | 1.04 | 1.74 |
| TAN-TN3A | 8.0 | 1.63 | 0.57 | 1.04 | 1.72 |

Table 6. The concentrations of metals and metalloids in Talbingo and Tantangara Reservoir waters

| Site Code | Ag (µg/L) | Al (µg/L) | As (µg/L) | Ba (µg/L) | Cd (µg/L) | Co (µg/L) | Cr (µg/L) | Cu (µg/L) | Fe (µg/L) | Mn (µg/L) |
|---------------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| TAL-PL1A | <0.002 | 7 | 0.17 | 4.5 | <0.01 | <0.01 | 0.06 | 0.65 | 24 | 0.3 |
| TAL-PL2A | <0.002 | 8 | 0.18 | 4.5 | <0.01 | <0.01 | 0.06 | 0.63 | 27 | 0.3 |
| TAL-PL1B | <0.002 | 7 | 0.16 | 4.6 | <0.01 | <0.01 | 0.06 | 5.2 | 25 | 0.4 |
| TAL-PL2B | <0.002 | 7 | 0.15 | 4.4 | <0.01 | <0.01 | 0.05 | 0.74 | 26 | 0.3 |
| TAN-TN1A | <0.002 | 43 | 0.31 | 6.2 | <0.01 | 0.03 | 0.10 | 0.48 | 396 | 3.2 |
| TAN-TN2A | <0.002 | 43 | 0.23 | 6.3 | <0.01 | 0.03 | 0.09 | 0.41 | 399 | 3.2 |
| TAN-TN3A | 0.017 | 42 | 0.33 | 6.2 | <0.01 | 0.03 | 0.10 | 0.39 | 394 | 3.3 |
| DVG ^a | 0.05 | 55 | 13 | - | 0.2 | - | 1.0 | 1.4 | - | 1900 |
| 99% GV ^b | 0.02 | 27 | 0.8 | - | 0.06 | - | 0.01 | 1.0 | - | 1200 |

| Site Code | Mo (µg/L) | Ni (µg/L) | Pb (µg/L) | Sb (µg/L) | Se (µg/L) | Sn (µg/L) | Sr (µg/L) | Th (µg/L) | U (µg/L) | V (µg/L) | Zn (µg/L) |
|---------------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|-------------|-------------|--------------|
| TAL-PL1A | <0.1 | 0.08 | <0.01 | 0.01 | 0.03 | <0.02 | 15 | 0.004 | 0.017 | 0.10 | 2.5 |
| TAL-PL2A | <0.1 | 0.10 | <0.01 | <0.01 | 0.02 | <0.02 | 15 | 0.004 | 0.014 | 0.10 | 1.1 |
| TAL-PL1B | <0.1 | 0.11 | 0.03 | 0.01 | 0.02 | <0.02 | 16 | 0.004 | 0.015 | 0.11 | 2.0 |
| TAL-PL2B | <0.1 | 0.12 | <0.01 | 0.01 | 0.02 | <0.02 | 15 | 0.003 | 0.016 | 0.11 | 0.7 |
| TAN-TN1A | <0.1 | 0.19 | 0.08 | 0.01 | 0.02 | <0.02 | 15 | 0.016 | 0.008 | 0.21 | 1.7 |
| TAN-TN2A | <0.1 | 0.20 | 0.06 | <0.01 | 0.02 | <0.02 | 15 | 0.014 | 0.008 | 0.21 | 1.0 |
| TAN-TN3A | <0.1 | 0.18 | 0.05 | <0.01 | 0.03 | <0.02 | 15 | 0.012 | 0.009 | 0.21 | 0.4 |
| DGV ^a | - | 11 | 3.4 | - | 11 | - | - | - | - | - | 8.0 |
| 99% GV ^b | - | 8 | 1.0 | - | 5 | - | - | - | - | - | 2.4 |

^a <http://www.waterquality.gov.au/anz-guidelines/guideline-values/default/water-quality-toxicants/>. DGV = default guideline value (water quality guideline value (WQGV), representing the 95% species protection guideline values (95%GV) for freshwater. ^b 99% species protection guideline values (99%GV) for freshwater. Values for As are for As(V), Cr are for Cr(VI), and tin are for inorganic tin

The concentrations of major anions (Cl^- , F^- , NO_3^- , SO_4^{2-}) and total-P and Si are shown in Table 7. The concentrations of most anions were near the limit of reporting and generally similar for both reservoirs. Nitrate and Si concentrations were higher in the Talbingo Reservoir waters. The C, N, P and Si concentrations are reported due to their potential influence on algal growth (phytoplankton and diatoms). The concentrations of nitrate were greater than the default guideline value of 0.01 mg N/L for NO_x in the Talbingo Reservoir samples. Total-P concentrations were below the DGV (freshwater lakes and reservoirs in south-east Australia).

Table 7. The concentrations of major anions and total-P and Si in Talbingo and Tantangara Reservoir waters

| Site Code | Chloride (mg/L) | Fluoride (mg/L) | Nitrate (mg/L) | Sulphate (mg/L) | Total-P (mg/L) | Si (mg/L) |
|-----------|--------------------|--------------------|-------------------|--------------------|-------------------|--------------|
| TAL-PL1A | <1 | <0.1 | 0.1 | <1 | <0.010 | 2.20 |
| TAL-PL2A | <1 | <0.1 | 0.1 | <1 | <0.010 | 2.20 |
| TAL-PL1B | 1 | <0.1 | 0.2 | <1 | <0.010 | 2.10 |
| TAL-PL2B | <1 | <0.1 | 0.1 | <1 | <0.010 | 2.10 |
| TAN-TN1A | <1 | <0.1 | <0.1 | <1 | <0.010 | 0.64 |
| TAN-TN2A | <1 | <0.1 | <0.1 | <1 | <0.010 | 0.63 |
| TAN-TN3A | <1 | <0.1 | <0.1 | <1 | <0.010 | 0.65 |
| DGV | - | - | 0.01 | - | 0.010 | |

^a <http://www.waterquality.gov.au/anz-guidelines/guideline-values/default/water-quality-toxicants/>.

DGV = default guideline values for nitrate (NO_x as mg N/L) and total-P are for freshwater lakes and reservoirs in south-east Australia.

Reservoir Waters Summary

The reservoir waters had neutral pH (6.9-7.3), low conductivity (26-30 $\mu\text{S}/\text{cm}$), and low turbidity (0.2-0.6 NTU). Most parameters measured in the waters were in a similar concentration range in both reservoirs and there was little variability between sites in each reservoir. The concentrations of dissolved Al, As, Ba, Co, Cr, Fe, Mn, Ni, Pb, Th and V were higher in Tantangara Reservoir than Talbingo Reservoir. Dissolved Al, Fe and Mn concentrations were a factor of 6, 15 and 10 times higher in Tantangara than Talbingo Reservoir, and were subsequently found to be predominantly in colloidal forms (Appendix D8). These colloidal species contribute significantly to the dissolved Al concentration exceeding the 99% GV in the Tantangara waters. In relation to water quality guidelines (ANZG, 2018), the waters contained no contaminants of potential concern (COPCs), i.e. concentrations were less than the corresponding DGV. Nutrient concentrations were generally within acceptable ranges, with care to note that the limit of detection for nitrate analyses was greater than the DGV.

3.2 Characterisation of Talbingo and Tantangara Reservoir sediments

These results were described in Memo 2 (25 September 2018) (Appendix C).

3.2.1 Reservoir sediment pore waters

The pH, conductivity and redox potential of the sediment pore waters in the Talbingo and Tantangara Reservoirs are shown in Table 8. There was little difference in each parameter between the different sites in Talbingo Reservoir. The porewater pH was marginally lower in Talbingo Reservoir than the Tantangara Reservoir, while the conductivity and redox potential were marginally higher. The higher redox potential indicates slightly more oxic conditions prevailed in the Tantangara Reservoir sediment porewaters.

The major anions, total-P and Si and ammonia in the Talbingo and Tantangara Reservoir sediment porewaters are shown in Table 8. The concentration of SO_4^{2-} was variable between sites at the same general location (i.e. CA, PL or RA), whereas, Cl^- , NO_3^- and ammonia concentrations were generally similar between the different sites in the Talbingo Reservoir. The sediment pore water of the Tantangara Reservoir had higher concentrations of ammonia than the Talbingo sites. Total-P concentrations were several orders of magnitude higher in the pore waters than both the reservoir surface waters (Table 7). Total ammonia concentrations were similar within a factor of two, and higher in Tantangara Reservoir sediments than Talbingo Reservoir sediments.

The concentrations of metals, metalloids and major cations in the sediment pore water of Talbingo and Tantangara Reservoir sediments are shown in Table 9. Many of the metals, metalloids and major cations exhibited substantial variability between sites, probably due to differences in micro-environmental parameter conditions, such as redox potential.

When comparing sediment porewater concentrations with the DGVs for surface water (Table 6), the Al and Cu exceeded the corresponding DGV in some pore waters. The dissolved (<0.45 μm filterable) Al was the most variable, probably due to differences in colloidal fractions between sites. Copper is likely to be complexed by organic ligands, resulting in the labile (and potentially bioavailable) concentration being below the DGV. The pore waters of the Talbingo Reservoir sediments from location RA had a dissolved As concentration that exceeded the DGV. It should be noted that the DGVs are designed for risk minimisation in surface waters and the exceedances observed for sediment pore waters may occur naturally for some substances, in which case they are not usually classified as COPCs.

Table 8. pH, redox potential, conductivity, major anions and ammonia of the reservoir sediment pore waters

| Site Code | Reservoir | pH | Redox, Eh (mV) | Conductivity ($\mu\text{S}/\text{cm}$) | Cl^- (mg/L) | NO_3^- (mg/L) | SO_4^{2-} (mg/L) | Total-P (mg/L) | Total Si (mg/L) | Total ammonia (mg NH_3/L) |
|-----------|------------|------|-------------------|---|-------------------------|---------------------------|------------------------------|-------------------|--------------------|---|
| CA1 | Talbingo | 7.30 | -175 | 23.5 | <4 | <0.5 | <3 | 0.34 | 11 | 2.4 |
| CA2 | Talbingo | 7.60 | -180 | 26.5 | <4 | <0.5 | 5 | 0.33 | 10 | 2.8 |
| CA3 | Talbingo | 7.45 | -170 | 19.0 | <4 | 0.7 | <3 | 0.23 | 12 | 2.6 |
| PL1 | Talbingo | 7.05 | -140 | 20.0 | <4 | 0.6 | <3 | 0.50 | 12 | 2.6 |
| PL2 | Talbingo | 7.30 | -125 | 15.7 | <4 | 0.5 | <3 | 0.34 | 10 | 2.3 |
| PL3 | Talbingo | 7.40 | -160 | 18.9 | <4 | 0.6 | <3 | 0.38 | 11 | 2.2 |
| RA1 | Talbingo | 7.25 | -160 | 22.7 | <4 | 0.5 | <3 | 0.08 | 11 | 2.8 |
| RA2 | Talbingo | 7.30 | -185 | 24.0 | <4 | 0.5 | <3 | 0.37 | 14 | 3.3 |
| RA3 | Talbingo | 7.50 | -190 | 21.6 | <4 | <0.5 | <3 | 0.38 | 15 | 4.3 |
| TN1 | Tantangara | 6.70 | -105 | 33.0 | <4 | 0.6 | <3 | 0.14 | 16 | 5.6 |
| TN2 | Tantangara | 7.10 | -140 | 36.0 | 6 | <0.5 | <3 | 0.32 | 14 | 5.7 |
| TN3 | Tantangara | 7.00 | -155 | 36.7 | <4 | <0.5 | <3 | 0.71 | 16 | 7.5 |

Table 9. Concentrations of major ions, metals and metalloids in the reservoir sediment pore waters

| | Na | K | Mg | Ca | Fe | Mn | | Ag | Al | As | Ba | Cd | Co |
|-----------|--------|-------|-------|-------|--------|-------|--------|--------|-------|-------|-------|--------|------|
| Site code | (mg/L) | | | | | | (µg/L) | | | | | | |
| CA1 | 2.9 | 1.0 | 1.84 | 6.08 | 25.9 | 7.3 | | 0.063 | 10 | 6.2 | 68 | <0.021 | 9.2 |
| CA2 | 3.4 | 1.4 | 6.36 | 10.5 | 37.1 | 10.5 | | <0.005 | 8 | 7.9 | 107 | 0.033 | 8.8 |
| CA3 | 2.0 | 1.1 | 1.30 | 5.50 | 17.9 | 15.6 | | <0.005 | 67 | 8.9 | 72 | 0.080 | 7.7 |
| PL1 | 2.9 | 1.2 | 2.01 | 6.10 | 27.5 | 7.4 | | 0.006 | 278 | 11.7 | 75 | <0.021 | 10.5 |
| PL2 | 2.2 | 1.0 | 1.83 | 6.54 | 18.6 | 9.8 | | 0.008 | 600 | 6.7 | 62 | <0.021 | 7.1 |
| PL3 | 2.8 | 1.8 | 3.37 | 7.65 | 36.8 | 12.9 | | 0.007 | 32 | 7.5 | 108 | 0.027 | 11.0 |
| RA1 | 2.1 | 1.1 | 1.23 | 5.40 | 15.6 | 8.1 | | 0.006 | 144 | 10.3 | 89 | <0.021 | 7.0 |
| RA2 | 2.5 | 1.2 | 1.55 | 8.19 | 22.4 | 14.0 | | <0.005 | 51 | 17.7 | 133 | <0.021 | 7.5 |
| RA3 | 2.5 | 1.2 | 2.14 | 13.3 | 30.6 | 28.8 | | <0.005 | 6 | 18.3 | 260 | 0.035 | 9.3 |
| TN1 | 3.6 | 1.4 | 2.26 | 3.66 | 28.1 | 2.7 | | 0.005 | 180 | 4.6 | 107 | <0.021 | 7.2 |
| TN2 | 3.5 | 1.2 | 2.12 | 3.39 | 32.1 | 2.6 | | 0.004 | 179 | 5.1 | 95 | <0.021 | 5.2 |
| TN3 | 1.9 | 0.9 | 1.84 | 3.09 | 37.4 | 3.4 | | <0.005 | 59 | 8.6 | 111 | <0.021 | 5.7 |
| Minimum | 1.92 | 0.917 | 1.230 | 3.09 | 15.6 | 2.56 | | <0.005 | 5.5 | 4.63 | 62.1 | <0.021 | 5.25 |
| Maximum | 3.56 | 1.77 | 6.36 | 13.3 | 37.4 | 28.8 | | 0.063 | 600 | 18.3 | 260 | 0.080 | 11.0 |
| | Cr | Cu | Mo | Ni | Pb | Sb | Se | Sn | Sr | Th | U | V | Zn |
| Site code | (µg/L) | | | | | | | | | | | | |
| CA1 | 0.39 | 0.24 | 0.9 | 1.7 | <0.046 | 0.10 | 0.12 | <0.028 | 51.9 | 0.058 | 0.059 | 1.6 | 1.5 |
| CA2 | 0.57 | 0.31 | 0.8 | 1.7 | <0.046 | 0.10 | 0.14 | <0.028 | 121.7 | 0.080 | 0.096 | 1.9 | 3.5 |
| CA3 | 0.44 | 0.91 | 1.3 | 2.1 | 0.306 | 0.13 | 0.12 | <0.028 | 45.3 | 0.117 | 0.105 | 2.5 | 3.1 |
| PL1 | 0.83 | 1.62 | 0.6 | 2.5 | 0.660 | 0.23 | 0.13 | <0.028 | 47.8 | 0.163 | 0.137 | 2.8 | 2.6 |
| PL2 | 0.68 | 1.39 | 1.3 | 2.1 | 0.622 | 0.20 | 0.10 | <0.028 | 44.8 | 0.149 | 0.137 | 2.6 | 6.2 |
| PL3 | 0.38 | 0.68 | 1.9 | 1.6 | 0.157 | 0.28 | 0.14 | <0.028 | 71.4 | 0.079 | 0.112 | 1.6 | 4.2 |
| RA1 | 0.43 | 1.47 | 1.0 | 2.0 | 0.716 | 0.13 | 0.09 | <0.028 | 35.7 | 0.132 | 0.152 | 1.8 | 4.0 |
| RA2 | 0.45 | 0.46 | 1.2 | 2.4 | 0.134 | 0.06 | 0.12 | <0.028 | 49.9 | 0.093 | 0.105 | 1.9 | 1.9 |
| RA3 | 0.37 | 0.30 | 2.0 | 2.6 | 0.001 | 0.12 | 0.15 | <0.028 | 69.9 | 0.078 | 0.260 | 2.0 | 2.2 |
| TN1 | 0.69 | 0.65 | 0.2 | 1.1 | 0.140 | 0.28 | 0.18 | <0.028 | 36.7 | 0.140 | 0.053 | 3.6 | 1.6 |
| TN2 | 0.73 | 0.53 | 0.2 | 0.8 | 0.150 | 0.28 | 0.17 | <0.028 | 34.8 | 0.133 | 0.035 | 2.9 | 2.2 |
| TN3 | 0.76 | 0.27 | 0.1 | 0.9 | <0.046 | 0.17 | 0.23 | <0.028 | 31.9 | 0.103 | 0.033 | 3.4 | 1.4 |
| Minimum | 0.373 | 0.238 | 0.12 | 0.784 | <0.046 | 0.064 | 0.094 | <0.028 | 31.9 | 0.058 | 0.033 | 1.59 | 1.42 |
| Maximum | 0.835 | 1.62 | 2.03 | 2.62 | 0.716 | 0.283 | 0.235 | 0.013 | 122 | 0.163 | 0.260 | 3.62 | 6.23 |

3.2.2 Reservoir benthic sediments

The particle size distributions of the Talbingo and Tantangara Reservoir sediments are shown in Table 10. Cumulative distribution plots and tables are shown in Appendix C. The mean diameter of the sediments was in the range 23.1 to 77.6 µm. The Dv (50) (50% of particles had lower diameter than this value) were all less than 30 µm, indicating the sediments were predominantly silt and clay. Tantangara Reservoir sediments had a larger particle size-range, which influenced its slightly larger mean particle size.

The total N, total-P, inorganic and organic carbon in benthic reservoir sediments are shown in Table 11. For Talbingo reservoir, the RA sites had lower concentrations of many of the parameters than the CA and PL sites. Tantangara Reservoir sediments had similar or higher concentrations of each parameter than those in Talbingo Reservoir sediments. The concentrations of each parameter varied by approximately two-fold between the different sites in the two reservoirs.

The total Ca, K, Mg, Na, S in the benthic sediments and the sediment cation exchange capacity (CEC) is shown in Table 11. For Talbingo Reservoir sediments, Ca was the only major cation that varied between the sites, with lower concentrations being measured in the RA site sediments than the CA or PL sediments. The concentrations of Ca, Mg, K and Na were generally lower in Tantangara Reservoir sediments than Talbingo

Reservoir sediments. The S concentrations were higher in Tantangara Reservoir sediments and the CEC was similar for both reservoir sediments.

Table 10. Particle size distribution of Talbingo and Tantangara Reservoir benthic sediments

| Site Code | Reservoir | Dv (10) (μm) | Dv (50) (μm) | Dv (90) (μm) | Mean diameter (μm) |
|-----------------|------------|------------------------------|------------------------------|------------------------------|------------------------------------|
| CA1 | Talbingo | 4.40 | 15.7 | 70.6 | 31.2 |
| CA2 | Talbingo | 4.30 | 18.0 | 113 | 45.5 |
| CA3 | Talbingo | 4.36 | 17.2 | 103 | 44.7 |
| PL1 | Talbingo | 4.67 | 18.0 | 81.6 | 36.5 |
| PL1 Dup | Talbingo | 4.73 | 17.4 | 73.9 | 32.7 |
| PL1 mean | Talbingo | 4.70 | 17.7 | 77.8 | 34.6 |
| PL2 | Talbingo | 4.41 | 16.3 | 90.6 | 42.1 |
| PL3 | Talbingo | 4.24 | 16.0 | 103 | 49.6 |
| RA1 | Talbingo | 3.94 | 13.7 | 62.0 | 30.7 |
| RA1 dup | Talbingo | 3.93 | 13.5 | 60.8 | 28.8 |
| RA1 mean | Talbingo | 3.94 | 13.6 | 61.4 | 29.8 |
| RA2 | Talbingo | 3.66 | 11.5 | 43.9 | 23.1 |
| RA3 | Talbingo | 3.75 | 12.0 | 47.7 | 24.2 |
| TN1 | Tantangara | 5.57 | 27.4 | 223 | 77.6 |
| TN2 | Tantangara | 4.84 | 20.1 | 132 | 50.5 |
| TN3 | Tantangara | 4.63 | 20.3 | 133 | 48.7 |

Note: Dv (x) refers to 10, 50 and 90th percentiles of particle diameters (on spherical volume basis).

Table 11. Concentration of total N, total-P, TIC, TOC, Ca, K, Mg, Na, S and CEC of Talbingo and Tantangara Reservoir sediments

| Site Code | Reservoir | Total N (%) | Total-P (mg/kg) | TIC (%) | TOC (%) | Ca | K | Mg (mg/kg) | Na | S | CEC (NH ₄) cmol (+/-)/kg |
|----------------|------------|----------------|--------------------|------------|------------|-------------|--------------|---------------|------------|------------|---|
| CA1 | Talbingo | 0.43 | 1340 | 0.2 | 5.8 | 1900 | 7150 | 5310 | 175 | 475 | 34 |
| CA2 | Talbingo | 0.39 | 1170 | 0.1 | 5.5 | 2080 | 8670 | 6210 | 174 | 432 | 33 |
| CA3 | Talbingo | 0.36 | 1140 | 0.1 | 4.5 | 1790 | 8580 | 7770 | 179 | 395 | 30 |
| PL1 | Talbingo | 0.39 | 1080 | 0.1 | 5.5 | 2450 | 7280 | 6680 | 177 | 436 | 32 |
| PL2 | Talbingo | 0.41 | 1030 | 0.2 | 6.0 | 1900 | 8800 | 6190 | 192 | 409 | 29 |
| PL3 | Talbingo | 0.40 | 1130 | 0.2 | 5.4 | 1620 | 7790 | 6100 | 174 | 448 | 32 |
| RA1 | Talbingo | 0.37 | 945 | 0.1 | 4.4 | 1480 | 8970 | 6630 | 163 | 395 | 27 |
| RA2 | Talbingo | 0.36 | 945 | 0.1 | 4.2 | 1490 | 10230 | 7040 | 175 | 386 | 30 |
| RA3 | Talbingo | 0.32 | 916 | 0.1 | 3.7 | 1450 | 8690 | 6570 | 146 | 338 | 26 |
| TN1 | Tantangara | 0.54 | 1040 | 0.2 | 6.4 | 714 | 6650 | 3320 | 140 | 650 | 34 |
| TN2 | Tantangara | 0.56 | 1500 | 0.2 | 5.7 | 783 | 7700 | 3490 | 150 | 742 | 36 |
| TN3 | Tantangara | 0.54 | 1310 | 0.2 | 5.8 | 653 | 7480 | 3520 | 134 | 773 | 36 |
| Minimum | | 0.32 | 916 | 0.1 | 3.7 | 653 | 6650 | 3320 | 134 | 338 | 26 |
| Maximum | | 0.56 | 1500 | 0.2 | 6.4 | 2450 | 10230 | 7770 | 192 | 773 | 36 |

TIC is total inorganic carbon, TOC is total organic carbon, CEC is cation exchange capacity

The TRM concentrations (total recoverable metal, metalloid, and other major ions) in Talbingo and Tantangara Reservoir sediments are shown in Table 12. There was generally higher concentrations of Ca, Cr, Cu, Fe, K, Mg, Mn, Na, Ni, Sb, Sn, Sr, Th and U in Talbingo Reservoir sediments and a higher concentration of S in Tantangara Reservoir sediments.

These concentrations reflect the background surface sediment concentrations. The concentrations of Ni exceed the corresponding sediment quality guideline value (SQGV) (Simpson et al., 2013; ANZG, 2018) that is considered an overly conservative value (Vangheluwe et al., 2013; Simpson and Batley 2016).

A significant portion of the TRM concentration (extracted using concentrated acids) may release inert (not easily released) fractions of metals that exhibit very low bioavailability to organisms. For most metals, the 'maximum bioavailable concentration' can be estimated by AEM analyses, as commonly achieved by extracting the solid in 1-M HCl for 1 h (Simpson and Batley, 2016). AEM data can also be useful for interpreting the partitioning behaviour of elements between the dissolved and particulate phases, and the potential availability of reactive binding phases.

The AEM concentrations (metal, metalloid, and other major ions) in Talbingo and Tantangara Reservoir sediments are shown in Table 13. There was generally little variation in the AEM concentrations between the different sites in Talbingo Reservoir sediments. However, the K, Mg and V were marginally lower for the RA sites than the CA and PL sites. A comparison between the two reservoirs showed that the AEM concentrations of As, Ba, Ca, Cr, Cu, K, Mg, Mn, Na, Ni, Th and U from Talbingo Reservoir sediments were generally higher than those measured in Tantangara Reservoir, while a higher concentration of S was extracted from Tantangara Reservoir sediments.

No AEM concentrations exceeded their respective SQGVs.

Reservoir Sediment Summary

The concentrations of many of the parameters often differed between the two reservoirs. There were no exceedances of SQGVs for the AEM concentrations, and few based on TRM.

Table 12. Total recoverable concentrations (TRM) metals, metalloids and other elements in Talbingo and Tantangara Reservoir sediments

| Sediment ID | Reservoir | Al | Ag | As | Ba | Cd | Ca | Co | Cr | Cu |
|---------------|------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| | | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) |
| CA1 | Talbingo | 23000 | 0.14 | 9.2 | 250 | 0.24 | 1800 | 30 | 56 | 41 |
| CA2 | Talbingo | 23000 | 0.13 | 8.6 | 270 | 0.17 | 1900 | 23 | 56 | 37 |
| CA3 | Talbingo | 42000 | 0.15 | 12 | 300 | 0.27 | 1900 | 30 | 78 | 51 |
| PL1 | Talbingo | 31000 | 0.11 | 8.8 | 220 | 0.15 | 1800 | 28 | 72 | 46 |
| PL2 | Talbingo | 35000 | 0.14 | 11 | 250 | 0.23 | 2200 | 26 | 61 | 52 |
| PL3 | Talbingo | 36000 | 0.14 | 12 | 240 | 0.26 | 1600 | 30 | 62 | 51 |
| PL3 duplicate | Talbingo | 36000 | 0.15 | 12 | 240 | 0.21 | 1600 | 30 | 61 | 51 |
| PL3 Mean | Talbingo | 36000 | 0.14 | 12 | 240 | 0.23 | 1600 | 30 | 61 | 51 |
| RA1 | Talbingo | 20000 | 0.14 | 10 | 240 | 0.27 | 1400 | 24 | 48 | 46 |
| RA2 | Talbingo | 36000 | 0.16 | 14 | 280 | 0.22 | 1700 | 25 | 59 | 49 |
| RA3 | Talbingo | 26000 | 0.15 | 15 | 320 | 0.23 | 1700 | 25 | 52 | 48 |
| TN1 | Tantangara | 17000 | 0.12 | 5.4 | 180 | 0.27 | 720 | 15 | 27 | 26 |
| TN2 | Tantangara | 31000 | 0.16 | 6.7 | 230 | 0.25 | 840 | 23 | 37 | 28 |
| TN3 | Tantangara | 23750 | 0.15 | 8.2 | 240 | 0.25 | 1150 | 26 | 41 | 32 |
| Minimum | | 17000 | 0.11 | 5.4 | 180 | 0.15 | 720 | 15 | 27 | 26 |
| Maximum | | 42000 | 0.16 | 15 | 320 | 0.28 | 2200 | 30 | 78 | 52 |
| SQGV | | | 1 | 20 | NA | 1.5 | NA | NA | 80 | 65 |

| Sediment ID | Reservoir | Fe | Hg | K | Mg | Mn | Mo | Na | Ni | Pb |
|---------------|------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| | | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) |
| CA1 | Talbingo | 49000 | <0.1 | 2200 | 4400 | 2200 | 0.60 | 58 | 44 | 25 |
| CA2 | Talbingo | 44000 | <0.1 | 3400 | 5400 | 1900 | 0.63 | 51 | 43 | 24 |
| CA3 | Talbingo | 56000 | <0.1 | 6000 | 8000 | 4000 | 0.60 | 120 | 68 | 26 |
| PL1 | Talbingo | 45000 | <0.1 | 3100 | 6400 | 1900 | 0.56 | 83 | 64 | 22 |
| PL2 | Talbingo | 45000 | <0.1 | 3100 | 5700 | 3000 | 0.99 | 100 | 56 | 28 |
| PL3 | Talbingo | 57000 | <0.1 | 3400 | 5900 | 2400 | 0.67 | 120 | 54 | 27 |
| PL3 duplicate | Talbingo | 73000 | <0.1 | 3500 | 5800 | 2500 | 0.65 | 92 | 54 | 27 |
| PL3 Mean | Talbingo | 65000 | <0.1 | 3400 | 5800 | 2400 | 0.66 | 100 | 54 | 27 |
| RA1 | Talbingo | 37000 | <0.1 | 1600 | 5400 | 2100 | 0.49 | 27 | 48 | 28 |
| RA2 | Talbingo | 42000 | <0.1 | 4000 | 6400 | 2800 | 0.40 | 85 | 60 | 32 |
| RA3 | Talbingo | 45000 | <0.1 | 2500 | 6000 | 4000 | 0.39 | 48 | 56 | 30 |
| TN1 | Tantangara | 25000 | <0.1 | 1200 | 2200 | 540 | 0.45 | 44 | 13 | 23 |
| TN2 | Tantangara | 39000 | <0.1 | 2400 | 2600 | 740 | 0.36 | 70 | 19 | 28 |
| TN3 | Tantangara | 41700 | <0.1 | 3180 | 4590 | 2390 | 0.45 | 45 | 27 | 27 |
| Minimum | | 25000 | <0.1 | 1200 | 2200 | 540 | 0.36 | 26 | 13 | 22 |
| Maximum | | 73000 | <0.1 | 6000 | 8000 | 4000 | 0.99 | 120 | 68 | 32 |
| SQGV | | | 0.15 | NA | NA | NA | NA | NA | 21 | 50 |

| Sediment ID | Reservoir | Sb | Se | Sn | Sr | Th | U | V | Zn | P | S |
|---------------|------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| | | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) |
| CA1 | Talbingo | 0.43 | 0.47 | 1.3 | 27 | 12 | 3.8 | 66 | 79 | 1400 | 650 |
| CA2 | Talbingo | 0.47 | 0.44 | 1.4 | 35 | 10 | 3.2 | 63 | 81 | 1300 | 600 |
| CA3 | Talbingo | 0.51 | 0.57 | 1.9 | 33 | 14 | 4.2 | 85 | 109 | 1300 | 550 |
| PL1 | Talbingo | 0.52 | 0.48 | 1.4 | 28 | 11 | 3.2 | 66 | 92 | 1200 | 630 |
| PL2 | Talbingo | 0.56 | 0.58 | 1.7 | 31 | 12 | 4.3 | 65 | 110 | 1100 | 570 |
| PL3 | Talbingo | 0.57 | 0.56 | 1.7 | 29 | 12 | 3.9 | 67 | 99 | 1300 | 630 |
| PL3 duplicate | Talbingo | 0.52 | 0.54 | 1.6 | 29 | 12 | 3.9 | 66 | 99 | 1300 | 640 |
| PL3 Mean | Talbingo | 0.54 | 0.55 | 1.6 | 29 | 12 | 3.9 | 67 | 99 | 1300 | 640 |
| RA1 | Talbingo | 0.62 | 0.47 | 1.2 | 15 | 10 | 3.6 | 47 | 91 | 1000 | 510 |
| RA2 | Talbingo | 0.75 | 0.50 | 1.9 | 22 | 13 | 3.5 | 53 | 113 | 1000 | 510 |
| RA3 | Talbingo | 0.74 | 0.45 | 1.4 | 17 | 12 | 3.0 | 43 | 99 | 1100 | 480 |
| TN1 | Tantangara | 0.28 | 0.43 | 0.83 | 11 | 6.0 | 1.2 | 49 | 85 | 1200 | 880 |
| TN2 | Tantangara | 0.31 | 0.46 | 1.3 | 18 | 9.2 | 1.5 | 59 | 102 | 1700 | 940 |
| TN3 | Tantangara | 0.37 | 0.49 | 1.3 | 17 | 10 | 2.1 | 65 | 104 | 1305 | 762 |
| Minimum | | 0.28 | 0.43 | 0.8 | 11 | 6.0 | 1.2 | 43 | 79 | 1000 | 480 |
| Maximum | | 0.76 | 0.58 | 1.9 | 35 | 14 | 4.3 | 85 | 114 | 1700 | 940 |
| SQGV | | NA | NA | NA | NA | NA | NA | NA | 200 | NA | NA |

SQGV = the sediment quality guideline values (Simpson e al., 2013). Values are bold underline where the default GV is exceeded.

Table 13. Dilute-acid extractable concentrations (AEM) metals, metalloids and other elements in Talbingo and Tantangara Reservoir sediments

| Sediment ID | Reservoir | Ag | Al | As | Ba | Ca | Cd | Co | Cr | Cu | |
|-------------|------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| | | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | |
| CA1 | Talbingo | 0.068 | 4740 | 3.85 | 205 | 1630 | 0.161 | 19.0 | 8.57 | 21.2 | |
| CA2 | Talbingo | 0.046 | 4280 | 3.12 | 208 | 1660 | 0.096 | 13.6 | 7.40 | 18.6 | |
| CA3 | Talbingo | 0.065 | 5020 | 3.82 | 210 | 1420 | 0.194 | 16.7 | 7.89 | 23.3 | |
| PL1 | Talbingo | 0.047 | 4550 | 3.04 | 168 | 1360 | 0.077 | 16.5 | 7.19 | 20.7 | |
| PL2 | Talbingo | 0.071 | 4590 | 3.27 | 174 | 1650 | 0.187 | 15.2 | 6.46 | 24.4 | |
| PL3 | Talbingo | 0.074 | 4600 | 4.45 | 169 | 1160 | 0.187 | 19.0 | 7.08 | 23.0 | |
| RA1 | Talbingo | 0.061 | 4280 | 3.92 | 205 | 1340 | 0.179 | 15.6 | 5.74 | 26.8 | |
| RA2 | Talbingo | 0.045 | 3910 | 4.58 | 213 | 1410 | 0.251 | 16.2 | 6.68 | 24.5 | |
| RA3 | Talbingo | 0.061 | 3460 | 6.60 | 260 | 1520 | 0.215 | 16.8 | 6.04 | 25.2 | |
| TN1 | Tantangara | 0.039 | 3620 | 1.81 | 141 | 661 | 0.192 | 7.19 | 3.05 | 13.0 | |
| TN2 | Tantangara | 0.085 | 3980 | 2.09 | 164 | 760 | 0.229 | 13.3 | 5.84 | 14.3 | |
| TN3 | Tantangara | 0.074 | 4460 | 2.81 | 158 | 649 | 0.310 | 15.6 | 6.30 | 14.8 | |
| Minimum | | 0.039 | 3460 | 1.81 | 141 | 649 | 0.077 | 7.19 | 3.05 | 13 | |
| Maximum | | 0.085 | 5020 | 6.6 | 260 | 1660 | 0.31 | 19 | 8.57 | 26.8 | |
| SQGV | | 1 | NA | 20 | NA | NA | 1.5 | NA | 80 | 65 | |
| Sediment ID | Reservoir | Fe | Hg | K | Mg | Mn | Mo | Na | Ni | Pb | |
| | | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | |
| CA1 | Talbingo | 23500 | <0.008 | 248 | 356 | 1910 | <0.071 | 70.7 | 8.97 | 17.4 | |
| CA2 | Talbingo | 17300 | <0.008 | 389 | 560 | 1630 | <0.071 | 77.2 | 8.01 | 16.0 | |
| CA3 | Talbingo | 16800 | <0.008 | 467 | 488 | 3360 | <0.071 | 58.7 | 10.3 | 17.3 | |
| PL1 | Talbingo | 17000 | <0.008 | 263 | 463 | 1690 | <0.071 | 71.6 | 9.33 | 15.4 | |
| PL2 | Talbingo | 15900 | <0.008 | 245 | 336 | 2490 | 0.084 | 56.6 | 8.50 | 19.4 | |
| PL3 | Talbingo | 25100 | <0.008 | 294 | 384 | 2110 | 0.12 | 68.7 | 7.11 | 17.5 | |
| RA1 | Talbingo | 14400 | <0.008 | 217 | 246 | 1920 | <0.071 | 63.3 | 8.05 | 21.3 | |
| RA2 | Talbingo | 14700 | <0.008 | 209 | 239 | 2540 | <0.071 | 59.5 | 9.33 | 22.1 | |
| RA3 | Talbingo | 17800 | <0.008 | 193 | 201 | 3640 | 0.098 | 76.8 | 8.83 | 21.0 | |
| TN1 | Tantangara | 12400 | <0.008 | 154 | 189 | 470 | <0.071 | 55.8 | 2.40 | 15.0 | |
| TN2 | Tantangara | 20200 | <0.008 | 208 | 195 | 646 | 0.079 | <41.8 | 3.42 | 18.5 | |
| TN3 | Tantangara | 21900 | <0.008 | 163 | 172 | 753 | <0.071 | 47.2 | 3.93 | 19.5 | |
| Minimum | | 12400 | <0.008 | 154 | 172 | 470 | 0.079 | 47.2 | 2.4 | 15 | |
| Maximum | | 25100 | <0.008 | 467 | 560 | 3640 | 0.12 | 77.2 | 10.3 | 22.1 | |
| SQGV | | NA | 0.15 | NA | NA | NA | NA | NA | 21 | 50 | |
| Sediment ID | Reservoir | Sb | Se | Sn | Sr | Th | U | V | Zn | P | S |
| | | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) |
| CA1 | Talbingo | <0.024 | 0.044 | 0.238 | 16.6 | 0.324 | 1.97 | 32.7 | 32.3 | 921 | <43.6 |
| CA2 | Talbingo | <0.024 | 0.034 | 0.209 | 26.3 | 0.165 | 1.27 | 28.5 | 27.4 | 771 | 62.5 |
| CA3 | Talbingo | 0.047 | 0.032 | 0.201 | 12.5 | 0.347 | 2.65 | 29.8 | 34.6 | 708 | 45.5 |
| PL1 | Talbingo | 0.034 | 0.044 | 0.160 | 11.8 | 0.218 | 1.52 | 29.7 | 30.4 | 686 | 43.8 |
| PL2 | Talbingo | 0.039 | 0.043 | 0.089 | 15.1 | 0.250 | 2.35 | 30.7 | 37.3 | 583 | <43.6 |
| PL3 | Talbingo | 0.028 | 0.032 | 0.152 | 13.3 | 0.299 | 2.23 | 28.4 | 33.0 | 705 | <43.6 |
| RA1 | Talbingo | 0.037 | 0.028 | 0.170 | 10.1 | 0.284 | 2.19 | 24.4 | 36.6 | 573 | <43.6 |
| RA2 | Talbingo | 0.034 | 0.034 | 0.191 | 10.9 | 0.160 | 1.20 | 22.2 | 30.9 | 584 | <43.6 |
| RA3 | Talbingo | 0.039 | 0.043 | 0.210 | 10.8 | 0.254 | 1.38 | 19.2 | 28.2 | 638 | <43.6 |
| TN1 | Tantangara | 0.029 | 0.023 | 0.107 | 7.72 | 0.070 | 0.451 | 30.8 | 49.1 | 545 | 76.7 |
| TN2 | Tantangara | <0.024 | 0.033 | 0.282 | 8.43 | 0.057 | 0.688 | 33.4 | 43.4 | 1090 | 104 |
| TN3 | Tantangara | 0.033 | 0.038 | 0.219 | 7.2 | 0.113 | 0.638 | 37.1 | 54.6 | 890 | 124 |
| Minimum | | 0.028 | 0.023 | 0.089 | 7.2 | 0.057 | 0.451 | 19.2 | 27.4 | 545 | 43.8 |
| Maximum | | 0.047 | 0.044 | 0.282 | 26.3 | 0.347 | 2.65 | 37.1 | 54.6 | 1090 | 124 |
| SQGV | | NA | NA | NA | NA | NA | NA | NA | 200 | NA | NA |

SQGV = the sediment quality guideline values (Simpson et al., 2013). Values are bold underline where the default GV is exceeded.

3.3 Characterisation of excavated rock material

These results were described in Memo 3 (28 September 2018) (Appendix C3). Note, the materials 6B and 6E (Kellys Plain Volcanics) were available after the other rock materials and therefore results additional to those presented in Memo 3 are discussed here.

The particle size distribution (PSD), and wet pH and redox potential of the fine excavated rock composites are shown in Table 14. Cumulative distribution plots and tables are shown in Appendix C. The mean diameter of the composites were in the range 21.0 to 41.3 μm . The Dv (10) (10% of particles had lower diameter than this value) had mean \pm SD of 2.6 \pm 0.4 μm , where clay-size is <2 μm . The Dv (50) (50% of particles had lower diameter than this value) were all less than 19 μm (mean \pm SD = 15 \pm 3 μm), indicating the sediments were predominantly silt. The Dv (90) (90% of particles had lower diameter than this value) were between 52 and 110 μm (mean \pm SD = 82 \pm 15 μm), indicating some components of the 75- μm -milled excavated rock samples underwent aggregation and increased above the milled size range or were irregular shaped that affected the PSD reporting of the instrument on a spherical volume basis. In relation to clay and fine silt fractions of the milled material (mean \pm SD), 28 \pm 3% was <6.3 μm (clay and fine silt), 18 \pm 3% was <4 μm , and 6.3 \pm 2% was <2 μm (clay) (Appendix C).

The particle size distribution of the milled excavated rock samples overlapped most of the particle size distribution of Talbingo and Tantangara Reservoir benthic sediments. In order to measure the pH and redox potential of excavated rock material, the samples remaining after the initial 10/1 L/S elutriate test were subsampled (following 48 h mixing of excavated rock material with composite Talbingo Reservoir water and syringe filtration that removed most of the solution (Memo 4) were allowed to stand for ten days, after which the pH and redox potential were measured by inserting probes directly into each wet solid material. The porewater pH after the 10 d was in the range 8.50-9.55, which had decreased from that measured in the elutriate solution following 48 h mixing (shown in brackets in Table 14). The redox potentials indicated that oxic conditions prevailed in the pore waters.

Table 14. Particle size distribution, pH and redox potential of the composite excavated rock material

| Rock ID | Dv (10) (μm) | Dv (50) (μm) | Dv (90) (μm) | Mean diameter (μm) | pH | Redox, Eh (mV) |
|------------------------|------------------------------|------------------------------|------------------------------|------------------------------------|-------------|-------------------|
| 1B composite | 2.71 | 11.6 | 72.2 | 26.4 | 8.75 (9.20) | 180 |
| 1E composite | 2.53 | 18.6 | 97.2 | 41.3 | 8.85 (9.29) | 160 |
| 2B composite | 2.44 | 17.3 | 76.4 | 30.1 | 8.85 (9.33) | 160 |
| 2E composite | 2.43 | 18.3 | 87.3 | 34.0 | 8.55 (8.88) | 115 |
| 3B composite | 2.47 | 12.8 | 80.3 | 28.7 | 8.50 (9.35) | 20 |
| 3E composite | 2.98 | 12.7 | 84.3 | 30.4 | 9.55 (9.58) | 165 |
| 3E composite duplicate | 2.95 | 12.7 | 81.0 | 28.9 | 9.05 (9.81) | 150 |
| 4B composite | 3.72 | 15.0 | 110 | 38.4 | 8.80 (9.67) | 165 |
| 4E composite | 2.87 | 10.6 | 62.9 | 23.7 | 8.61 (9.37) | 180 |
| 5B composite | 2.24 | 12.9 | 52.2 | 21.0 | 8.55 (9.31) | 165 |
| 5E composite | 2.41 | 18.8 | 105 | 39.5 | 8.85 (9.57) | 80 |
| 5E composite duplicate | 2.30 | 16.5 | 93.2 | 33.9 | 8.75 (9.39) | -20 |
| 6B composite | 2.72 | 19.7 | 82.0 | 32.5 | NA | NA |
| 6E composite | 2.45 | 15.7 | 76.3 | 29.3 | NA | NA |
| 7B composite | 2.69 | 14.7 | 80.4 | 29.9 | 9.00 (9.56) | 160 |
| 7E composite | 2.00 | 16.5 | 69.5 | 27.4 | 8.75 (9.38) | 70 |

Note: Dv (x) refers to 10, 50 and 90th percentiles of particle diameters (on spherical volume basis). The pH and Eh values were determined on solids mixed with Talbingo Reservoir water for 48 h and allowed to stand for 10 days. The pH values in brackets is the pH of the elutriate water after 48-h mixing.

The TRM concentrations measured in the milled rock composites are shown in Table 15. The concentrations of most metals were below the corresponding SQGVs. There was one exceedance for Pb and Zn, two exceedances As and Cr, three exceedances for Cu, and eight for Ni. Of the excavated rock composites, 1E had the most SQGV-exceedances; Ag, Cr, Ni, Pb and Zn. It should be noted that the Ni SQGV is considered an overly conservative value and it is not surprising that it exceeded the SQGV for many of the excavated rock composites (Vangheluwe et al., 2013; Simpson and Batley 2016).

As noted above, a significant portion of the TRM may not be bioavailable to organisms, and AEM analyses provide a better estimate of the maximum potentially bioavailable concentration (Simpson and Batley, 2016). The AEM concentrations measured in the milled rock composites are shown in Table 16. The AEM concentrations were found to be below their respective SQGVs (where available) except for Pb in composite 1E.

For most of the excavated rock composites, the percent of total recoverable elements in dilute-acid extractable fraction was generally <30% for Ag, Al, As, Co, Cr, Cu, Fe, Mg, Ni, S, Sb, Sn, U, V and Zn (Appendix C, Memo 3). The percentage of dilute-acid extractable Ba, Pb and Sr was generally >50%.

Excavated Rock Compositions Summary

The fine excavated rock composites used for testing were predominantly silt-sized (<63 µm), with only a small fraction of the samples having diameters larger than this size range. The particle size distributions of the milled excavated rock samples were similar to the Talbingo and Tantangara Reservoir sediments.

The porewater pH of the excavated rock samples mixed with Talbingo Reservoir water and allowed to stand for 10 days was in the range 8.50-9.55 and had decreased from that measured in the elutriate solution following 48 h mixing. This pH range is significantly greater than that of the waters from Talbingo (pH 7.05-7.60) and Tantangara (pH 6.70-7.10) Reservoir.

Composite 1E had the greatest number of metals with TRM concentrations exceeding sediment quality guideline values (SQGVs). When considering the AEM concentrations, there was only one exceedance; lead for composite 1E (197 mg Pb/kg).

Table 15. Total recoverable concentrations (TRM) of metals, metalloids and other elements in the rock composites

| Rock ID | Ag (mg/kg) | Al (mg/kg) | As (µg/g) | Ba (mg/kg) | Ca (mg/kg) | Cd (mg/kg) | Co (mg/kg) | Cr (mg/kg) | Cu (mg/kg) |
|-------------------|---------------|---------------|--------------|---------------|---------------|---------------|---------------|---------------|---------------|
| Composite 1B mean | 0.051 | 16500 | 6.1 | 45 | 7450 | 0.030 | 18 | 65 | 27 |
| Composite 1E | <u>2.4</u> | 24900 | 13 | 82 | 7790 | 1.0 | 21 | <u>113</u> | 51 |
| Composite 2B | 0.13 | 16100 | 5.3 | 97 | 6000 | 0.034 | 12 | 66 | 8.2 |
| Composite 2E | 0.27 | 11200 | 14 | 65 | 11000 | 0.044 | 14 | 29 | 28 |
| Composite 3B | 0.029 | 24600 | 0.93 | 11 | 21100 | 0.031 | 29 | <u>118</u> | 59 |
| Composite 3E | 0.045 | 16800 | 2.2 | 19 | 9980 | 0.019 | 20 | 76 | 62 |
| Composite 4B | 0.072 | 11300 | 5.6 | 32 | 12200 | 0.042 | 8.8 | 13 | 15 |
| Composite 4E | 0.38 | 19200 | <u>39</u> | 66 | 20200 | 0.238 | 21 | 12 | <u>90</u> |
| Composite 5B | 0.052 | 9200 | 3.4 | 53 | 5440 | 0.014 | 6.3 | 20 | 6.1 |
| Composite 5E | 0.20 | 18800 | 12 | 37 | 11200 | 0.121 | 19 | 25 | <u>338</u> |
| Composite 6B | 0.11 | 15500 | 12 | 46.7 | 2010 | 0.007 | 9.3 | 30 | 19 |
| Composite 6E | 0.11 | 18700 | <u>25</u> | 85.4 | 6120 | 0.16 | 15 | 27 | 33 |
| Composite 7B | 0.060 | 11600 | 2.7 | 64 | 13100 | 0.043 | 6.5 | 19 | 11 |
| Composite 7E | 0.18 | 9960 | 6.5 | 2086 | 8080 | 0.025 | 6.3 | 13 | <u>88</u> |
| MIN | 0.029 | 9200 | 0.93 | 10.9 | 5440 | 0.014 | 6.27 | 11.7 | 6.10 |
| MAX | 2.352 | 24900 | 38.5 | 2086 | 21100 | 1.045 | 28.54 | 118 | 338 |
| SQGV | 1 | NA | 20 | NA | NA | 1.5 | NA | 80 | 65 |

| Rock ID | Fe (mg/kg) | Hg (mg/kg) | K (mg/kg) | Mg (mg/kg) | Mn (mg/kg) | Mo (mg/kg) | Na (mg/kg) | Ni (mg/kg) | P (mg/kg) |
|-------------------|---------------|---------------|--------------|---------------|---------------|---------------|---------------|---------------|--------------|
| Composite 1B mean | 29800 | <0.03 | 2240 | 17900 | 638 | 0.14 | 200 | <u>93</u> | 487 |
| Composite 1E | 46400 | <0.03 | 2600 | 22400 | 1316 | 0.21 | 240 | <u>134</u> | 640 |
| Composite 2B | 28600 | <0.03 | 3190 | 8520 | 602 | 0.31 | 160 | <u>28</u> | 423 |
| Composite 2E | 27300 | <0.03 | 3070 | 7110 | 413 | 0.23 | 110 | <u>31</u> | 537 |
| Composite 3B | 39000 | <0.03 | 1840 | 26400 | 727 | 0.10 | 400 | <u>42</u> | 422 |
| Composite 3E | 24900 | <0.03 | 1080 | 15000 | 577 | 0.08 | 330 | <u>39</u> | 459 |
| Composite 4B | 18200 | <0.03 | 1020 | 8020 | 464 | 0.33 | 190 | 13 | 490 |
| Composite 4E | 41800 | <0.03 | 2060 | 10400 | 588 | 1.6 | 310 | 16 | 901 |
| Composite 5B | 15900 | <0.03 | 1880 | 6310 | 336 | 2.1 | 360 | 16 | 516 |
| Composite 5E | 43500 | <0.03 | 1550 | 9680 | 644 | 1.3 | 700 | <u>25</u> | 856 |
| Composite 6B | 19700 | <0.02 | 3910 | 7770 | 269 | 0.49 | 334 | 17 | 414 |
| Composite 6E | 31600 | <0.02 | 4120 | 8660 | 295 | 0.62 | 140 | <u>37</u> | 527 |
| Composite 7B | 18800 | <0.03 | 2760 | 6340 | 525 | 0.13 | 370 | 10 | 378 |
| Composite 7E | 15600 | <0.03 | 3310 | 5500 | 253 | 0.14 | 160 | 11 | 469 |
| MIN | 15600 | <0.03 | 1020 | 5500 | 253 | 0.08 | 110 | 10.0 | 378 |
| MAX | 46400 | <0.03 | 3310 | 26400 | 1316 | 2.11 | 700 | 134 | 901 |
| SQGV | NA | 0.15 | NA | NA | NA | NA | NA | 21 | NA |

| Rock ID | Pb (mg/kg) | S (mg/kg) | Sb (mg/kg) | Se (mg/kg) | Sn (mg/kg) | Sr (mg/kg) | Th (mg/kg) | U (mg/kg) | V (mg/kg) | Zn (mg/kg) |
|-------------------|---------------|--------------|---------------|---------------|---------------|---------------|---------------|--------------|--------------|---------------|
| Composite 1B mean | 10 | 78 | 0.38 | 0.08 | 0.55 | 28 | 10 | 0.86 | 38 | 76 |
| Composite 1E | <u>214</u> | 756 | 0.92 | 0.12 | 0.59 | 33 | 7.9 | 0.75 | 71 | <u>543</u> |
| Composite 2B | 5.2 | 160 | 0.45 | 0.04 | 0.86 | 18 | 10 | 1.2 | 44 | 58 |
| Composite 2E | 11 | 3790 | 2.2 | 0.18 | 0.65 | 48 | 9.1 | 1.1 | 23 | 45 |
| Composite 3B | 0.61 | 15 | 0.03 | 0.02 | 0.35 | 30 | 0.67 | 0.10 | 70 | 66 |
| Composite 3E | 2.3 | 13 | 0.10 | 0.03 | 0.40 | 13 | 5.3 | 0.33 | 34 | 62 |
| Composite 4B | 17 | 17 | 0.17 | 0.04 | 0.55 | 26 | 11 | 0.79 | 14 | 52 |
| Composite 4E | 9.8 | 5410 | 0.63 | 0.30 | 0.41 | 50 | 4.7 | 1.3 | 71 | 104 |
| Composite 5B | 2.7 | 260 | 0.10 | 0.03 | 0.38 | 21 | 7.5 | 0.99 | 22 | 22 |
| Composite 5E | 8.0 | 6050 | 0.21 | 1.0 | 1.0 | 51 | 5.3 | 0.84 | 80 | 76 |
| Composite 6B | 17 | 1070 | 0.31 | 0.032 | 1.6 | 8.24 | 16 | 2.8 | 36 | 44 |
| Composite 6E | 23 | 7530 | 1.3 | 0.18 | 0.62 | 51.5 | 13 | 1.8 | 21 | 109 |
| Composite 7B | 8.8 | 54 | 0.37 | 0.03 | 0.74 | 73 | 11 | 1.4 | 19 | 35 |
| Composite 7E | 8.6 | 1010 | 1.2 | 0.03 | 2.0 | 63 | 8.8 | 1.2 | 14 | 32 |
| MIN | 0.6 | 13 | 0.029 | <0.01 | 0.35 | 13.1 | 0.67 | 0.10 | 13.5 | 79 |
| MAX | 214 | 6050 | 2.17 | 1.03 | 1.98 | 73 | 11.5 | 1.38 | 79.5 | 114 |
| SQGV | 50 | NA | NA | NA | NA | NA | NA | NA | NA | 200 |

Table 16. Dilute-acid extractable concentrations (AEM) of metals, metalloids and other elements in the rock composites

| Rock ID | Ag (mg/kg) | Al (mg/kg) | As (mg/kg) | Ba (mg/kg) | Ca (mg/kg) | Cd (mg/kg) | Co (mg/kg) | Cr (mg/kg) | Cu (mg/kg) | |
|------------------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|--------------|
| Composite 1B mean | 0.015 | 2420 | 2.0 | 31 | 7500 | 0.018 | 2.6 | 6.3 | 3.4 | |
| Composite 1E | 0.085 | 3270 | 2.3 | 57 | 8430 | 0.180 | 2.0 | 12 | 2.3 | |
| Composite 2B | 0.033 | 2960 | 0.63 | 84 | 6620 | 0.015 | 4.3 | 12 | 1.3 | |
| Composite 2E | 0.084 | 2100 | 1.3 | 43 | 11700 | 0.020 | 1.2 | 4.6 | 3.1 | |
| Composite 3B | 0.004 | 2920 | 0.57 | 7.4 | 15100 | 0.013 | 3.4 | 13 | 18 | |
| Composite 3E | 0.017 | 2540 | 1.5 | 12 | 8840 | 0.012 | 2.1 | 8.8 | 21 | |
| Composite 4B | 0.015 | 1160 | 1.6 | 21 | 12400 | 0.029 | 0.40 | 1.9 | 2.9 | |
| Composite 4E | 0.074 | 2750 | 1.9 | 27 | 20100 | 0.079 | 1.2 | 2.8 | 4.9 | |
| Composite 5B | 0.049 | 2800 | 0.76 | 30 | 6570 | 0.026 | 1.1 | 3.8 | 22 | |
| Composite 5E | 0.015 | 1810 | 0.68 | 36 | 5340 | 0.007 | 0.82 | 4.3 | 1.4 | |
| Composite 6B | 0.033 | 1270 | 1.0 | 37 | 1990 | 0.006 | 0.88 | 4.3 | 1.6 | |
| Composite 6E | 0.012 | 2040 | 3.7 | 37 | 6070 | 0.034 | 2.0 | 3.3 | 2.0 | |
| Composite 7B | 0.010 | 1630 | 0.74 | 45 | 14000 | 0.019 | 0.48 | 4.3 | 0.80 | |
| Composite 7E | 0.042 | 2110 | 1.4 | 1836 | 8770 | 0.011 | 0.61 | 2.7 | 4.1 | |
| MIN | 0.004 | 1160 | 0.57 | 7.4 | 5340 | 0.007 | 0.40 | 1.9 | 0.80 | |
| MAX | 0.085 | 3270 | 2.3 | 1836 | 20100 | 0.184 | 4.27 | 13 | 22 | |
| SQGV | 1 | NA | 20 | NA | NA | 1.5 | NA | 80 | 65 | |
| Rock ID | Fe (mg/kg) | Hg (mg/kg) | K (mg/kg) | Mg (mg/kg) | Mn (mg/kg) | Mo (mg/kg) | Na (mg/kg) | Ni (mg/kg) | P (mg/kg) | |
| Composite 1B | 4610 | <0.02 | 1100 | 3060 | 343 | 0.08 | 143 | 8.7 | 523 | |
| Composite 1B duplicate | 4580 | <0.02 | 1130 | 3050 | 345 | 0.06 | 140 | 8.3 | 512 | |
| Composite 1B mean | 4600 | <0.02 | 1120 | 3060 | 344 | 0.07 | 141 | 8.5 | 518 | |
| Composite 1E | 6460 | <0.02 | 1050 | 3510 | 679 | 0.07 | 136 | 13 | 664 | |
| Composite 2B | 5570 | <0.02 | 1100 | 2080 | 514 | 0.08 | 83 | 5.4 | 359 | |
| Composite 2E | 6310 | <0.02 | 1440 | 1400 | 298 | 0.08 | 82 | 3.1 | 545 | |
| Composite 3B | 3830 | <0.02 | 1420 | 3120 | 203 | <0.02 | 189 | 5.3 | 483 | |
| Composite 3E | 2780 | <0.02 | 643 | 1720 | 119 | 0.04 | 220 | 4.3 | 501 | |
| Composite 4B | 1850 | <0.02 | 552 | 674 | 263 | 0.05 | 110 | 0.6 | 519 | |
| Composite 4E | 5470 | <0.02 | 765 | 1260 | 319 | 0.08 | 146 | 1.1 | 952 | |
| Composite 5B | 5820 | <0.02 | 755 | 1330 | 131 | 0.08 | 246 | 1.5 | 919 | |
| Composite 5E | 4250 | <0.02 | 930 | 1400 | 172 | 0.30 | 206 | 1.8 | 546 | |
| Composite 6B | 4970 | 0.085 | 760 | 1050 | 124 | 0.19 | 129 | 1.4 | 401 | |
| Composite 6E | 2820 | 0.063 | 1150 | 632 | 115 | 0.12 | 62.6 | 3.2 | 525 | |
| Composite 7B | 4150 | <0.02 | 1080 | 705 | 452 | 0.05 | 192 | 0.8 | 400 | |
| Composite 7E | 3140 | <0.02 | 1920 | 686 | 198 | 0.07 | 119 | 0.9 | 479 | |
| MIN | 1850 | <0.02 | 552 | 674 | 119 | 0.04 | 82 | 0.6 | 359 | |
| MAX | 6460 | <0.02 | 1920 | 3510 | 679 | 0.30 | 246 | 13 | 952 | |
| SQGV | NA | 0.15 | NA | NA | NA | NA | NA | 21 | NA | |
| Rock ID | Pb (µg/g) | S (µg/g) | Sb (µg/g) | Se (µg/g) | Sn (µg/g) | Sr (µg/g) | Th (µg/g) | U (µg/g) | V (µg/g) | Zn (µg/g) |
| Composite 1B | 7.2 | <30 | 0.10 | <0.01 | 0.17 | 28 | 4.2 | 0.26 | 5.3 | 14 |
| Composite 1B duplicate | 7.3 | <30 | 0.13 | 0.01 | 0.17 | 27 | 4.4 | 0.27 | 5.2 | 14 |
| Composite 1B mean | 7.2 | <30 | 0.12 | 0.01 | 0.17 | 28 | 4.3 | 0.27 | 5.2 | 14 |
| Composite 1E | 197 | 38 | 0.21 | 0.01 | 0.22 | 33 | 3.1 | 0.24 | 9.1 | 86 |
| Composite 2B | 3.7 | <30 | 0.093 | <0.01 | 0.20 | 17 | 2.7 | 0.27 | 8.2 | 15 |
| Composite 2E | 7.1 | <30 | 0.67 | 0.01 | 0.23 | 44 | 3.3 | 0.38 | 4.5 | 8.0 |
| Composite 3B | 0.14 | <30 | 0.005 | <0.01 | 0.03 | 5.8 | 0.17 | 0.01 | 8.3 | 8.9 |
| Composite 3E | 1.1 | <30 | 0.024 | <0.01 | 0.06 | 7.0 | 1.4 | 0.07 | 3.4 | 7.1 |
| Composite 4B | 11 | <30 | 0.030 | <0.01 | 0.09 | 20 | 4.7 | 0.19 | 1.1 | 3.8 |
| Composite 4E | 6.9 | <30 | 0.086 | <0.01 | 0.06 | 44 | 1.5 | 0.28 | 9.7 | 14 |
| Composite 5B | 4.8 | 45 | 0.075 | 0.01 | 0.09 | 13 | 3.0 | 0.19 | 9.4 | 16 |
| Composite 5E | 1.9 | <30 | 0.052 | <0.01 | 0.14 | 13 | 4.5 | 0.29 | 2.9 | 3.8 |
| Composite 6B | 118 | 24.3 | 0.049 | 0.004 | 0.15 | 5.0 | 8.6 | 0.94 | 3.6 | 6.8 |
| Composite 6E | 17 | 137 | 0.77 | 0.018 | 0.14 | 56.4 | 4.1 | 0.39 | 2.3 | 19 |
| Composite 7B | 6.3 | <30 | 0.082 | <0.01 | 0.16 | 71 | 3.9 | 0.26 | 3.0 | 3.7 |
| Composite 7E | 4.4 | 413 | 0.21 | 0.01 | 0.63 | 62 | 2.2 | 0.40 | 2.6 | 6.0 |
| MIN | 0.1 | 38 | 0.005 | <0.01 | 0.03 | 5.8 | 0.17 | 0.01 | 1.1 | 79 |
| MAX | 197 | 413 | 0.67 | 0.01 | 0.63 | 71 | 4.7 | 0.40 | 9.7 | 114 |
| SQGV | 50 | NA | NA | NA | NA | NA | NA | NA | NA | 200 |

3.4 Release of substances from excavated rock materials in reservoir water

This section summarises the results from a large range of tests. The majority of the data is summarised in Appendix D with the accompanying Memo that provided early reporting. The memos also provide further details of the methods. The data included and results discussed here are those considered useful for informing the EIS of potential risk-factors related to the placement of the excavated rock materials in the reservoirs.

3.4.1 Release of substances from <75-µm composite excavated rock materials in reservoir water at low L/S ratio

The vast majority of the excavated rock, by mass, is expected to be larger than sand size and should settle rapidly, whereas the finest fractions (clay to low-silt size range) of the excavated rock materials may remain suspended in the waters in the main disposal area for a considerable period of time. While the placement of excavated rock occurs, considerable amounts of fine rock material may remain present in the waters and not settle for many days after the placement activities cease. Consequently the bottom waters may contain a very high concentration of suspended fine excavated rock material for the duration of the placement activities and potentially for weeks beyond the date placement is deemed complete. Such conditions may allow for prolonged release from those excavated rock materials.

Initial elutriate tests were conducted with the <75-µm composite excavated rock materials at a liquid/solid ratio (L/S) of 10 (100 g/L) over a duration of 48 h with the intention of providing a worst case scenario for concentrations of fine rock materials suspended within the reservoir water column for prolonged periods. These results were described in Memo 4 (28 September 2018) (Appendix D1).

Note: at the time of these test the materials 6B and 6E (Kellys Plain Volcanics) were not available for testing. Results for these materials are provided in later sections at different L/S ratio, after determining more relevant information would be achieved at higher L/S ratios. In general, the magnitude of substance release for 6B and 6E were quite similar to the results for the other 12 materials.

At the end of 48-h L/S=10 tests on the <75-µm rock composites, the pH, conductivity and DO were in the range 8.88-9.81, 107-203 and 7.14-8.49 (Table 17). The pH and conductivity in the elutriate samples were substantially higher than in Talbingo Reservoir water without added rock, while the DO was not affected other than for the lower value measured for composite 5E.

Table 17. Water pH, conductivity and DO for <75-µm rock composites at L/S = 10 after 48 h

| Elutriate | pH | Conductivity (µS/cm) | DO (mg/L) |
|---|------|----------------------|-----------|
| Talbingo composite A (water, no added rock) | 7.12 | 29.1 | 8.26 |
| Talbingo composite B (water, no added rock) | 6.99 | 28.9 | 8.22 |
| Talbingo composite C (water, no added rock) | 7.05 | 29.0 | 8.16 |
| Talbingo composite D (water, no added rock) | 7.03 | 29.0 | 8.19 |
| 1B composite | 9.20 | 154 | 8.21 |
| 1B composite duplicate | 9.29 | 153 | 8.15 |
| 1B composite MEAN | 9.25 | 154 | 8.18 |
| 1E composite | 9.33 | 166 | 8.26 |
| 2B composite | 8.88 | 160 | 8.36 |
| 2E composite | 9.35 | 173 | 8.22 |
| 3B composite | 9.58 | 120 | 8.23 |
| 3E composite | 9.81 | 120 | 8.47 |
| 4B composite | 9.67 | 107 | 8.32 |
| 4E composite | 9.37 | 141 | 8.49 |
| 4E composite duplicate | 9.31 | 143 | 8.35 |
| 4E composite MEAN | 9.34 | 142 | 8.42 |
| 5B composite | 9.57 | 150 | 8.25 |
| 5E composite | 9.39 | 162 | 7.14 |
| 7B composite | 9.56 | 150 | 8.36 |
| 7E composite | 9.38 | 203 | 8.27 |

Note: The Talbingo composites A-D had no added rock materials.

The concentrations of anions released from <75-µm rock composites are shown in Table 18, and major cations, metals and metalloids in Table 19. The concentrations of each parameter were all higher than the corresponding values in the Talbingo Reservoir water except for a few values for SO_4^{2-} which were similar, and NO_3^- which was below the limit of detection.

The metals, metalloids and major cations released from the <75-µm composite rock composites are shown in Table 19. When compared to WQGVs, the main exceedances occurred for Al, As and Cr, where the majority of composites had concentrations of one or more of these elements that exceeded the DGV or 99% species protection concentrations (99% GV). The 95% WQGV for Al was exceeded by the largest factor; over 14-fold higher. There were also six exceedances of DGV for total-P. The inorganic speciation of Al, As and Cr is influenced by anionic complexes at basic pH's and it is likely that higher dilutions (i.e. higher L/S ratios) and/or mixing durations effect solubility. These parameters were investigated in subsequent tests.

Summary for low L/S-elutriate tests on <75-µm composite excavated rock materials

The mixing of the <75-µm composite excavated rock materials in Talbingo Reservoir water (L/S = 10) resulted in an increase in the pH of 2-2.8 pH units, and a 3-7-fold increase in the conductivity.

The Cl^- , F^- , SO_4^{2-} , total-P and total-S increased relative to the original Talbingo Reservoir water, with the total-P being the only parameter that increased above the DGV for water quality.

Most of the metals, metalloids and major cations in the excavated rock elutriates increased relative to the control Talbingo Reservoir water. The As, Cr and, in particular, the Al increased above the DGVs and are identified COPCs.

As described in the introduction, this initial test was performed to assess what we consider to be a worst case scenario for fine excavated rock material remaining in the water column. The results of this test indicate that under such conditions the pH of the waters is likely to increase to levels that result in high concentrations of dissolved Al within the waters. These waters are likely to cause toxicity to a range of aquatic organisms.

The results of this test were used for selection of composites to test in more detail in subsequent tests. Due to the higher concentrations of substances, particularly Al, released from excavated rock composites 1B, 2B, 5B, 5E, and 7E, these materials were often used in these tests.

Table 18. The anions, nitrate, and total-S, -P and -Si released from rock composites in L/S=10 elutriate test

| Elutriate water | F ⁻ (mg/L) | Cl ⁻ (mg/L) | Br ⁻ (mg/L) | SO ₄ ²⁻ (mg/L) | S (mg/L) | Nitrate (mg/L) | Total-P (mg/L) | Total Si (mg/L) |
|----------------------|--------------------------|---------------------------|---------------------------|---|-------------|-------------------|-------------------|--------------------|
| Talbingo composite A | 0.015 | 0.92 | <0.5 | 0.44 | 0.16 | 0.5 | <0.0044 | 2.1 |
| Talbingo composite B | 0.025 | 0.94 | <0.5 | 0.49 | 0.15 | <0.3 | <0.0044 | 2.1 |
| Talbingo composite C | 0.03 | 0.93 | <0.5 | 0.46 | 0.16 | <0.3 | <0.0044 | 2.1 |
| Talbingo composite D | 0.02 | 0.93 | <0.5 | 0.53 | 0.16 | 0.3 | <0.0044 | 2.1 |
| 1B composite | 0.42 | 1.59 | <0.5 | 0.79 | 0.33 | 1.5 | 0.010 | 3.1 |
| 1B duplicate | 0.42 | 1.60 | <0.5 | 0.75 | 0.32 | <0.3 | 0.010 | 3.1 |
| 1B mean | 0.42 | 1.59 | <0.5 | 0.77 | 0.32 | <1 | 0.010 | 3.1 |
| 1E composite | 0.47 | 2.53 | <0.5 | 3.40 | 1.43 | 0.6 | 0.006 | 1.5 |
| 2B composite | 0.45 | 1.95 | <0.5 | 0.96 | 0.45 | 1.0 | 0.039 | 4.1 |
| 2E composite | 0.54 | 1.65 | <0.5 | 9.35 | 5.8 | <0.3 | 0.008 | 2.9 |
| 3B composite | 0.16 | 1.31 | <0.5 | 0.46 | 0.18 | <0.3 | <0.0044 | 2.1 |
| 3E composite | 0.60 | 1.34 | <0.5 | 0.52 | 0.18 | 0.4 | 0.006 | 1.7 |
| 4B composite | 0.48 | 1.56 | <0.5 | 0.69 | 0.29 | 0.4 | 0.005 | 3.0 |
| 4E composite | 0.14 | 2.15 | <0.5 | 5.14 | 3.5 | 0.4 | 0.007 | 1.4 |
| 4E duplicate | 0.16 | 2.12 | <0.5 | 5.08 | 3.5 | <0.3 | <0.0044 | 1.4 |
| 4E mean | 0.15 | 2.13 | <0.5 | 5.11 | 3.5 | 0.3 | 0.006 | 1.4 |
| 5B composite | 0.32 | 2.41 | <0.5 | 1.27 | 0.75 | <0.3 | 0.038 | 4.3 |
| 5E composite | 0.33 | 1.75 | <0.5 | 7.45 | 8.5 | <0.3 | 0.021 | 2.0 |
| 7B composite | 0.72 | 1.51 | <0.5 | 1.10 | 0.52 | <0.3 | 0.005 | 3.8 |
| 7E composite | 0.53 | 1.94 | <0.5 | 11.5 | 4.3 | <0.3 | 0.005 | 4.2 |
| Minimum | 0.14 | 1.31 | <0.5 | 0.46 | 0.18 | | 0.005 | 1.4 |
| Maximum | 0.72 | 2.53 | <0.5 | 11.5 | 8.5 | | 0.039 | 4.3 |
| DGV | | | | | - | 0.010 | 0.010 | |

^a <http://www.waterquality.gov.au/anz-guidelines/guideline-values/default/water-quality-toxicants/>.

DGV = default guideline values for nitrate (NO_x) and total-P are for freshwater lakes and reservoirs in south-east Australia

Table 19. The metals, metalloids and major cations released into the dissolved phase from composite excavated rock materials in L/S=10 elutriate test

| Elutriate water | Na (mg/L) | K (mg/L) | Mg (mg/L) | Ca (mg/L) | Al (µg/L) | Fe (µg/L) | Mn (µg/L) | Ag (µg/L) | As (µg/L) | Ba (µg/L) | Cd (µg/L) | Co (µg/L) |
|----------------------|--------------|-------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| Talbingo composite A | 1.43 | 0.40 | 0.70 | 1.70 | 3.8 | 16 | 0.22 | <0.004 | 0.13 | 4.1 | 0.029 | 0.01 |
| Talbingo composite B | 1.48 | 0.42 | 0.73 | 1.76 | 3.1 | 17 | 0.21 | <0.004 | 0.16 | 4.3 | 0.008 | 0.01 |
| Talbingo composite C | 1.43 | 0.41 | 0.71 | 1.76 | 3.1 | 17 | 0.22 | <0.004 | 0.15 | 4.1 | <0.004 | <0.01 |
| Talbingo composite D | 1.47 | 0.40 | 0.72 | 1.73 | 3.4 | 17 | 0.22 | <0.004 | 0.19 | 4.4 | <0.004 | <0.01 |
| 1B composite | 7.63 | 20.3 | 2.09 | 5.05 | 208 | 0.6 | 1.5 | <0.004 | 15 | 3.6 | <0.004 | 0.03 |
| 1B duplicate | 7.59 | 20.2 | 2.11 | 5.03 | 212 | 0.7 | 1.6 | <0.004 | 15 | 3.6 | <0.004 | 0.02 |
| 1B mean | 7.61 | 20.3 | 2.10 | 5.04 | 210 | 0.6 | 1.5 | <0.004 | 15 | 3.6 | <0.004 | 0.03 |
| 1E composite | 7.72 | 20.7 | 2.51 | 5.61 | 300 | 0.7 | 3.2 | <0.004 | 21 | 20 | <0.004 | 0.06 |
| 2B composite | 4.80 | 13.1 | 6.36 | 6.85 | 73 | 0.3 | 2.3 | <0.004 | 3.8 | 15 | 0.005 | 0.04 |
| 2E composite | 4.33 | 27.8 | 1.52 | 6.75 | 231 | 0.8 | 1.7 | <0.004 | 9.4 | 9.8 | <0.004 | 0.04 |
| 3B composite | 9.33 | 8.60 | 2.59 | 4.17 | 417 | 1.2 | 0.43 | <0.004 | 0.49 | 0.33 | <0.004 | 0.02 |
| 3E composite | 9.71 | 11.1 | 1.90 | 4.64 | 779 | 2.7 | 0.46 | <0.004 | 0.74 | 0.42 | <0.004 | 0.01 |
| 4B composite | 5.90 | 10.6 | 0.89 | 5.30 | 409 | 0.9 | 1.0 | <0.004 | 10 | 1.1 | <0.004 | 0.01 |
| 4E composite | 6.60 | 15.4 | 1.50 | 7.00 | 701 | 3.2 | 1.2 | <0.004 | 10 | 2.1 | <0.004 | 0.02 |
| 4E duplicate | 6.58 | 15.4 | 1.53 | 6.96 | 705 | 3.3 | 1.2 | <0.004 | 10 | 1.9 | <0.004 | 0.02 |
| 4E mean | 6.59 | 15.4 | 1.52 | 6.98 | 703 | 3.3 | 1.2 | <0.004 | 10 | 2.0 | <0.004 | 0.02 |
| 5B composite | 9.48 | 15.5 | 1.39 | 4.62 | 263 | 1.9 | 0.88 | <0.004 | 12 | 4.0 | <0.004 | 0.04 |
| 5E composite | 9.74 | 11.0 | 1.96 | 8.01 | 404 | 1.7 | 1.6 | <0.004 | 2.4 | 6.2 | <0.004 | 0.02 |
| 7B composite | 9.68 | 19.9 | 0.62 | 4.08 | 300 | 1.0 | 3.4 | <0.004 | 5.8 | 6.4 | <0.004 | 0.01 |
| 7E composite | 6.19 | 34.5 | 0.92 | 4.16 | 128 | 1.9 | 0.74 | <0.004 | 24 | 181 | <0.004 | 0.03 |
| MIN elutriate | 4.33 | 8.60 | 0.62 | 4.08 | 73.2 | 0.3 | 0.43 | <0.004 | 0.49 | 0.33 | <0.07 | 0.011 |
| MAX elutriate | 9.74 | 34.50 | 6.36 | 8.01 | 779 | 3.31 | 3.45 | <0.004 | 24.1 | 181 | <0.07 | 0.063 |
| DGV or 95% GV | - | - | - | - | 55 | - | 1900 | 0.05 | 13 | - | 0.2 | - |
| 99% GV | - | - | - | - | 27 | - | 1200 | 0.02 | 0.8 | - | 0.06 | - |

^a <http://www.waterquality.gov.au/anz-guidelines/guideline-values/default/water-quality-toxicants/>.

DGV = default guideline value, representing the 95% species protection guideline values (95%GV) for freshwater.

99% species protection guideline values (99%GV) for freshwater. Values for As are for As(V), Cr are for Cr(VI), and tin are for inorganic tin

Table 19 (continued). The metals, metalloids, and major cations released into the dissolved phase from composite excavated rock materials in L/S=10 elutriate test

| Elutriate water | Cr (µg/L) | Cu (µg/L) | Mo (µg/L) | Ni (µg/L) | Pb (µg/L) | Sb (µg/L) | Se (µg/L) | Sn (µg/L) | Sr (µg/L) | V (µg/L) | Zn (µg/L) |
|----------------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|-------------|--------------|
| Talbingo composite A | <0.04 | 0.542 | 0.02 | 0.085 | <0.01 | <0.02 | 0.02 | <0.02 | 14 | 0.10 | 1.36 |
| Talbingo composite B | <0.04 | 0.578 | 0.03 | 0.078 | 0.01 | <0.02 | 0.02 | <0.02 | 14 | 0.10 | 1.33 |
| Talbingo composite C | 0.04 | 0.554 | 0.03 | 0.068 | <0.01 | <0.02 | 0.02 | <0.02 | 14 | 0.09 | 1.47 |
| Talbingo composite D | 0.05 | 0.567 | 0.03 | 0.233 | <0.01 | <0.02 | 0.02 | <0.02 | 15 | 0.11 | 1.18 |
| 1B composite | <u>0.48</u> | 0.197 | 1.30 | 0.057 | <0.01 | 3.7 | 0.43 | <0.02 | 52 | 14 | 0.115 |
| 1B duplicate | <u>0.48</u> | 0.188 | 1.27 | 0.052 | <0.01 | 3.7 | 0.45 | <0.02 | 52 | 15 | <0.1 |
| 1B mean | <u>0.48</u> | 0.193 | 1.29 | 0.054 | <0.01 | 3.7 | 0.44 | <0.02 | 52 | 15 | <0.1 |
| 1E composite | <0.04 | 0.095 | 1.84 | 0.276 | 0.16 | 11 | 0.54 | <0.02 | 82 | 6.6 | <0.1 |
| 2B composite | <u>1.5</u> | 0.125 | 3.76 | 0.061 | <0.01 | 4.1 | 0.36 | <0.02 | 28 | 6.0 | 0.124 |
| 2E composite | 0.07 | 0.162 | 2.21 | 0.048 | <0.01 | 14 | 0.81 | <0.02 | 36 | 8.6 | 0.129 |
| 3B composite | <u>4.3</u> | 0.369 | 0.116 | 0.032 | <0.01 | 0.07 | 0.02 | <0.02 | 5.7 | 9.1 | <0.1 |
| 3E composite | <u>2.9</u> | 0.691 | 0.125 | 0.032 | <0.01 | 0.20 | 0.05 | <0.02 | 10 | 5.6 | <0.1 |
| 4B composite | 0.07 | 0.586 | 0.250 | 0.045 | <0.01 | 0.49 | 0.12 | <0.02 | 20 | 5.2 | <0.1 |
| 4E composite | 0.07 | 0.342 | 2.49 | 0.072 | <0.01 | 2.1 | 0.66 | <0.02 | 26 | 8.6 | <0.1 |
| 4E duplicate | 0.07 | 0.369 | 2.51 | 0.054 | <0.01 | 2.0 | 0.66 | <0.02 | 25 | 8.6 | <0.1 |
| 4E mean | 0.07 | 0.356 | 2.50 | 0.063 | <0.01 | 2.1 | 0.66 | <0.02 | 25 | 8.6 | <0.1 |
| 5B composite | 0.08 | 0.272 | 15.46 | 0.147 | <0.01 | 0.79 | 0.16 | <0.02 | 19 | 13 | 0.149 |
| 5E composite | 0.05 | 0.983 | 1.45 | 0.026 | <0.01 | 1.6 | 1.4 | <0.02 | 26 | 6.5 | <0.1 |
| 7B composite | 0.06 | 0.318 | 1.24 | 0.057 | <0.01 | 3.1 | 0.22 | <0.02 | 46 | 19 | 0.169 |
| 7E composite | 0.05 | 0.537 | 1.89 | 0.052 | <0.01 | 6.3 | 0.18 | <0.02 | 52 | 15 | 0.227 |
| MIN | <0.04 | 0.095 | 0.116 | 0.026 | <0.01 | 0.068 | 0.020 | <0.02 | 5.66 | 5.23 | <0.1 |
| MAX | 4.30 | 0.983 | 15.5 | 0.276 | 0.160 | 14.0 | 1.39 | <0.02 | 81.9 | 18.7 | 0.227 |
| DVG or 95% GV | 1.0 | 1.4 | - | 11 | 3.4 | - | 11 | - | - | - | 8.0 |
| 99% GV | 0.01 | 1.0 | - | 8 | 1.0 | - | 5 | - | - | - | 2.4 |

3.4.2 Effect of L/S ratio on substance release from <75-µm composite rock materials

The concentrations of fine solids in the water column following placement of excavated rock materials in the reservoirs will be influenced by the properties of the rock (e.g. density, particle size), the water conditions, and the placement procedure. In relation to the suspended concentrations of fine rock materials, the L/S ratios are anticipated to lower in deeper waters (higher concentrations of solids in deeper waters) and expected to increase with increasing distance from the placement site as fine particles disperse and become diluted with reservoir water. As the placement activities will occur over a considerable period of time, fine rock concentrations may be at elevated levels for many days to weeks, and potentially much longer in the bottom waters.

This section describes the results of tests undertaken to characterise the influence of liquid-to-solid (L/S) ratio on substance release from the rock materials. The tests also provide data on the release kinetics that are discussed in Section 3.4.3. Tests were performed on the <75-µm composite rock materials 1B, 2B, 5B, 5E and 7E and reported in Memo 11 (9 November 2018) (Appendix D2). An additional series of tests were performed on the 6B/6E rock materials that were provided later in the project, and these are included in this results section. The primary aim of the tests was to investigate the effect of L/S ratio on pH, conductivity, and the dissolved metal concentrations. The tests were performed at L/S = 30, 300, 1000, 3000 [being 33, 3.3, 1 and 0.33 g/L, respectively] and measurements were made at times of 0.5, 3, 18 and 120 h (Memo 11).

Results

The pH, conductivity and dissolved Al concentrations measured in the elutriate solutions for all composites combined for each L/S ratio over time are shown in Figure 1 (mean±standard error for all results). Appendix D2_Memo 11 provides figures with the data for the individual composites 1B, 2B, 5B, 5E, 6B, 6E and 7E, respectively. For 6B, the conductivity was initially 1.3 mS/cm then dropped to 0.3-0.6 mS/cm range after 3 h, and that data is not shown on the scale of Figure 1 (Figures D2.1 and D2.2 in Appendix D2). In general, the individual composites displayed similar behaviour.

In general, as the L/S ratio decreased (increased solids concentration) the pH and conductivity were higher for leaching times ≤18 h. Note, for the 120 h elutriates there were only two results for L/S =1000 and 3000 tests and no clear relationship was observed between L/S and pH or conductivity. Dissolved Al concentrations increased as the L/S ratio decreased for all leaching times. Dissolved As and Cr concentrations did not exceed DGVs when L/S ≥ 30 (Data in Appendix D2), and would not be categorised as COPCs in reservoir waters containing <33 g/L fine rock (L/S>30). Infrequently, dissolved Zn exceeded the DGV of 8 µg/L and was attributed to contamination owing to the infrequency and difficulties in avoiding low levels zinc contamination arising as part of the test methodology (i.e. not attributed to release from the rock materials).

The initial contact of the solids with the water resulted in a rapid increase in pH and conductivity. The pH generally decreased marginally over the duration of the tests, although increases occurred for 6B and 6E. The pH was nearly always higher for a lower L/S ratio at any given time point, whereas, for the conductivity, this relationship was not quite as clear, with similar values often observed for the 300 and 1000 L/S ratios. Conductivity marginally increased with time, but decreased for 6B L/S=30 tests. Appendix D2 also provides figures with major salt cation concentrations, indicating K > Ca > Na > Mg.

The dissolved Al concentrations were in the range 30-439, 9-445, 6-175, 6.5-42 µg/L for the 30:1 (33 g/L), 300:1 (3.3 g/L), 1000:1 (1 g/L) and 3000:1 (0.33 g/L) L/S ratios, respectively. The dissolved Al concentrations increased over the duration of all tests, with the degree of increase generally being higher for lower L/S ratios. For all composite samples tested except 6B, the dissolved Al exceeded the default guideline value (DGV) of 55 µg/L after 3 h for the 30 and 300 L/S ratios, and exceeded the DGV after 18 h (3 h not tested)

for the 1000 L/S ratio. For 6B the DGV for Al was only exceeded for LS/=30 treatment at 18 h and 120 h. The Al DGV was not exceeded for any composites at the 3000 L/S ratio.

The total-P concentrations decreased with increasing L/S ratio, with mean concentrations (\pm standard deviation, maximum-minimum) of 16 ± 13 (3-44), 7 ± 4 (3-17), and 5 ± 1 (3-7) and 3 ± 1 (3-4) $\mu\text{g total-P/L}$ for the tests with L/S ratio of 30:1 (33 g/L), 300:1 (3.3 g/L), 1000:1 (1 g/L) and 3000:1 (0.33 g/L), respectively (Appendix D2.1). For 3 of the 5 rock composites tested (2B, 5B, 5E) at L/S of 30 (33 g/L) the total-P concentration ranged from 10-44 $\mu\text{g/L}$ (exceeding the DGV of 10 $\mu\text{g/L}$) for measurements made between 0.5 to 120 h. For the same rock composites at L/S of 300 (3.3 g/L), the DGV was exceeded infrequently (4 of 20 measurements), by a lower amount (10-17 $\mu\text{g/L}$). No exceedances of the DGV occurred at L/S of 1000 (1 g/L).

Significant observation from L/S ratio tests

When reservoir waters contain ≥ 1 g/L fine rock (part per thousand), the dissolved Al concentrations are predicted to exceed the DGV for durations of ≥ 18 h. When the reservoir waters contain < 3 g/L fine rock materials, total-P concentrations are predicted to be below the DGV of 10 $\mu\text{g/L}$. Dissolved concentrations of other metals or metalloids (including As and Cr) should not exceed DGVs when reservoir waters contain < 33 g/L fine rock (L/S >30). The water pH and conductivity increased significantly with increasing amount of fine solids (lower L/S), and generally pH > 9 when L/S ≥ 300 and conductivity > 60 $\mu\text{S/cm}$ when L/S ≥ 1000 .

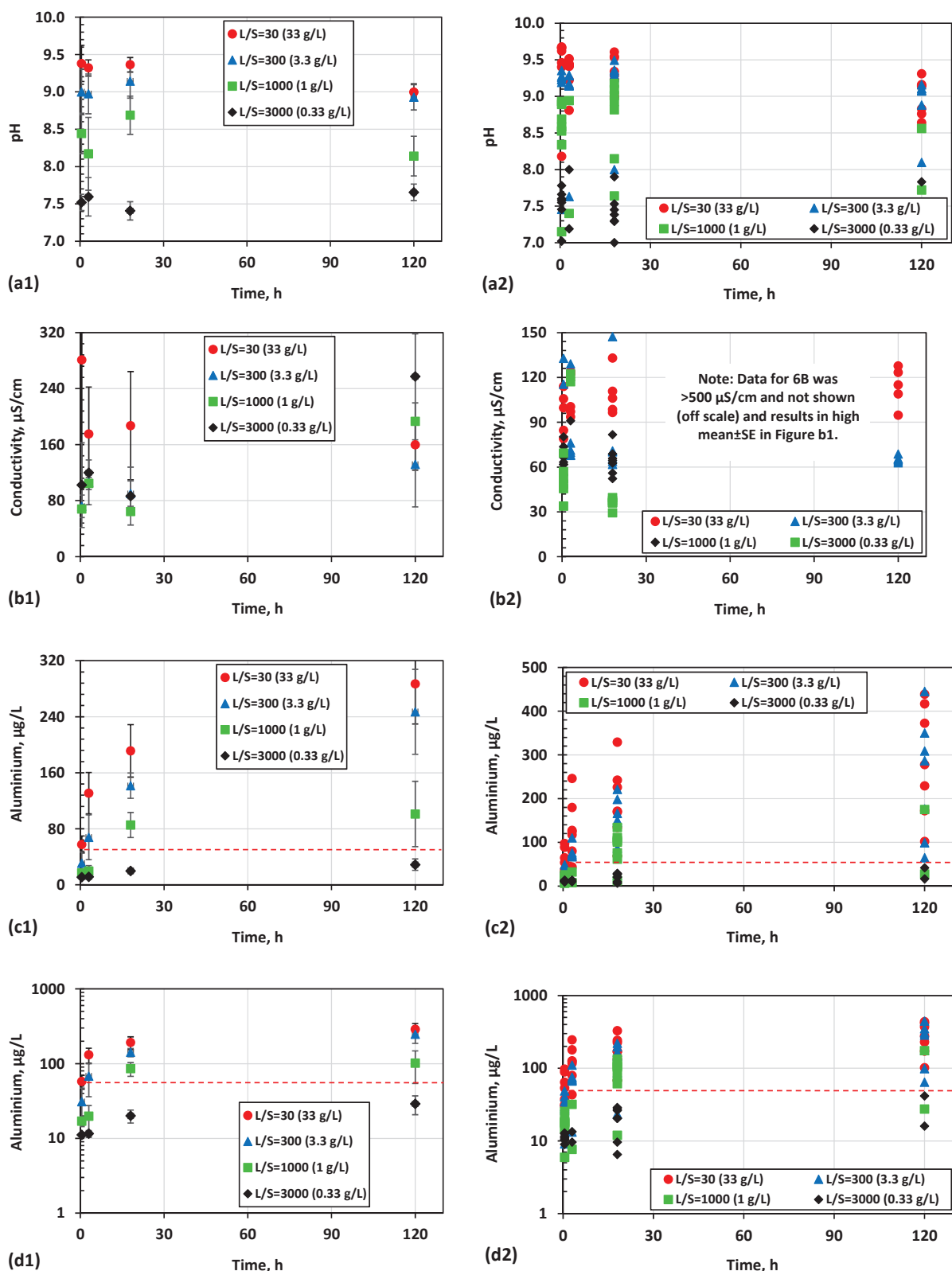


Figure 1. The pH, conductivity and dissolved Al concentration after elutriate times of 0.5, 3, 18 and 120 h for all excavated rock composite samples at liquid to solid ratios (L/S) of 30, 300, 1000 and 3000 (d1, d2 = log scale). The figures on the left (a1-d1) show the mean values (error bars are standard errors), and the figures on the right (a2-d2) show the values measured for each composite material at each duration. A red dashed line at 55 µg/L indicates the DGV for dissolved Al.

3.4.3 Effect of mixing duration on substance release from <75-µm composite rock materials

The time the rock solids spend entrained in the water column before settling as sediments will be influenced by the properties of the rock (e.g. density, particle size), the water conditions (hydrodynamic forces), and the placement procedure. Fine rock particles within the water column may be transported greater distances from the original placement location and may potentially release greater amounts of substances.

This section describes the results of tests undertaken to characterise the influence that the duration the rock materials spend in the water column has on substance release into the water. The tests were performed with those investigating the effect of L/S ratio on substance release (3.4.2). Tests were performed on the <75-µm composite rock material 4E initially (Memo 5, 18 October 2018) to assist in determining the appropriate test conditions/treatment for the other <75-µm composite rock materials (Memo 11, 9 November 2018) (Appendix D3). The primary aim of the test was to investigate the effect of duration on pH, conductivity, and the dissolved Al concentrations. All tests were conducted using the composite Talbingo Reservoir water.

In tests with rock composite 4E, measurements of water quality and substance release were made at times of 0.5, 2, 6 and 24 h for L/S = 100, 1000, and 10000 [being 10, 1 and 0.1 g/L, respectively] (Memo 5). This material was selected owing to the high level of Al release observed in the initial elutriate test (Section 3.4.1).

In tests with rock composites 1B, 2B, 5B, 5E and 7E, measurements of water quality and substance release were made at times of 0.5, 3, 18 and 120 h for L/S = 30, 300, 1000, 3000 [being 33, 3.3, 1 and 0.33 g/L, respectively] (Memo 11).

Also discussed are tests designed specifically to assess changes in water alkalinity (Memo 7, 2 November 2018). These tests were undertaken on eight rock composites (the enriched (E)-samples of 7 geological zones, and also Kelly Plains 6B), measurements of water quality and substance release were made 0.5 and 6 h for L/S = 500 and also for one material (4E) tests were conducted for L/S = 500, 2000, 5000 and 10000 and compared with the alkalinity of the Talbingo Reservoir water.

Results

The initial contact of the <75-µm rock composite 4E solids with the water resulted in a rapid increase in pH and conductivity (Figure 2). Similar observations were made for the subsequent tests with rock composites 1B, 2B, 5B, 5E and 7E (Figure 1). The pH generally decreased marginally over the duration of the tests while the conductivity marginally increased. The pH was nearly always higher for a lower L/S ratio (higher concentrations of solids) at any given time point, whereas, for the conductivity, this relationship was not quite as clear, with similar values often observed at the L/S ratios of 300 and 1000. Appendix D3 also provides figures with major salt cations, shown concentrations $\text{Ca} > \text{K} > \text{Na} > \text{Mg}$ contributing to increased conductivity for this material (Figure D3.1).

The dissolved Al generally exhibited a relatively linear increase as the duration in Talbingo Reservoir water increased. The changes in the dissolved Al concentrations with time indicate dissolution of rock solids is occurring and higher pH promotes continued dissolution through the formation of the highly soluble aluminate ion, $\text{Al}(\text{OH})_4^-$. The degree of increase in dissolved Al concentration was generally higher for lower L/S ratios (greater concentrations of fine solids). As noted in section 3.4.2 (Figures 1c and d), the dissolved Al exceeded the default guideline value (DVG) of 55 µg/L after 3 h for all composite samples tested at L/S of 30 and 300, and after 18 h at a L/S of 1000, but not for a L/S of 3000 over any duration tested. Infrequently, dissolved Zn exceeded the DGV of 8 µg/L (Appendix D7), and was attributed to contamination arising as

part of the methodology as noted in the previous section. No other metal or metalloid concentrations exceeded DGVs.

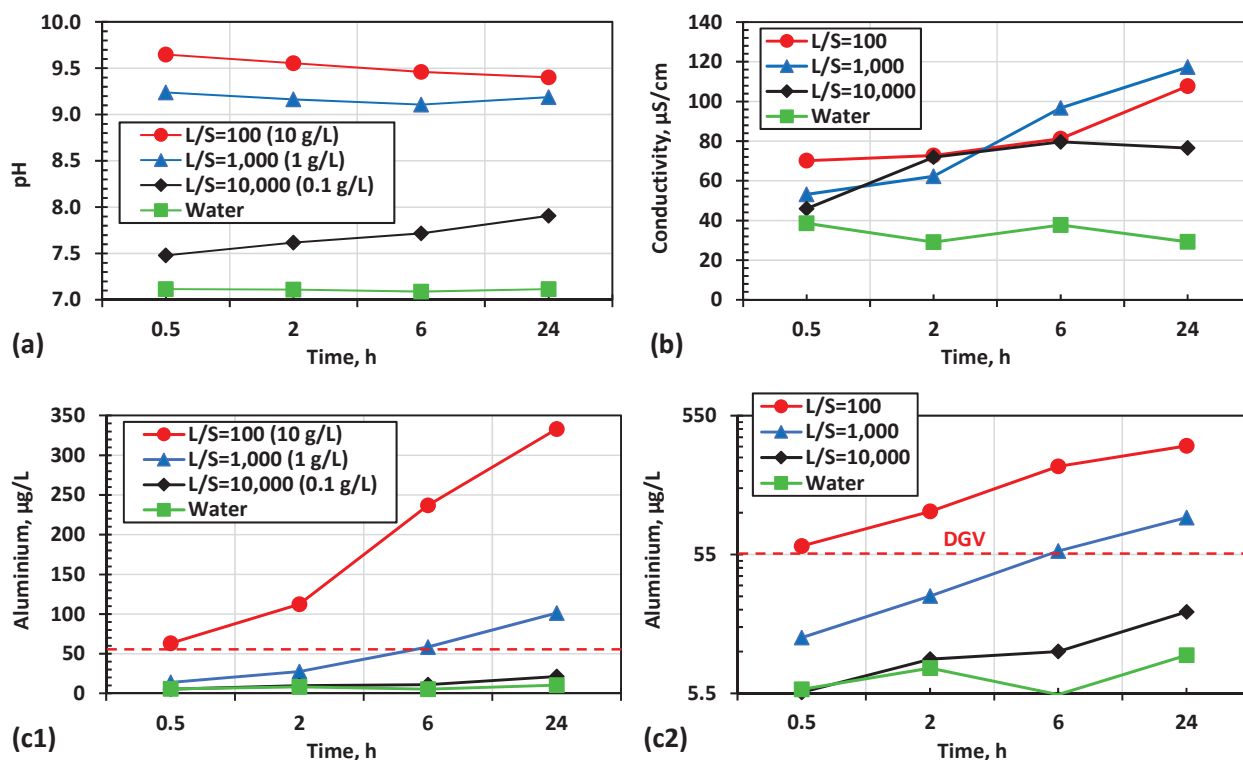


Figure 2. Rock composite material 4E. Elutriate water (a) pH, (b) conductivity and (c1, c2) dissolved Al concentrations. A red dashed line at 55 µg/L indicates the DGV.

Water alkalinity changes

For waters with low pH-buffering capacity, measurements of water pH provide limited information on the acidity or alkalinity changes caused by the addition of the rock materials. For that reason, additional tests were undertaken to characterise changes in alkalinity (Memo 7, Appendix D3). The Talbingo Reservoir water had neutral pH (7.0), low conductivity (25-40 µS/cm) and alkalinity of 13-14 mg CaCO₃/L. The alkalinity of elutriates at L/S of 500 were 50-100% higher than the original Talbingo Reservoir water, and similar after 0.5 and 6 h (Table 20). The increases in pH, conductivity and alkalinity were considerably lower at higher L/S ratios (Table 20).

Significant observations from mixing-duration tests

The kinetics of the changes in pH, conductivity and the dissolved Al concentrations indicate increased dissolution of rock solids occur with time. For Al, the increase with time is consistent with the high pH acting to increase dissolution through formation of the highly soluble aluminate ion, Al(OH)₄⁻.

Both the concentration of fine rock materials and duration within the water column should be considered when predicting the risks posed by dissolved Al. No other released metal concentrations exceeded DGVs.

Increases in alkalinity due to the presence of fine rock materials within the waters were generally modest and are unlikely to result in impacts to aquatic organisms.

Table 20. The pH, conductivity and alkalinity for elutriate test of the fine excavated rock composites

| Test water and fine-rock composite | L/S | Time h | pH | Conductivity ($\mu\text{S}/\text{cm}$) | Alkalinity (mg CaCO_3/L) |
|------------------------------------|----------|-----------|-----|---|--|
| Talbingo water only | ∞ | 0.5 | 7.0 | 39.9 | 14 |
| Talbingo water only | ∞ | 6 | 7.0 | 24.5 | 13 |
| 1E | 500 | 0.5 | 8.4 | 76.9 | 23 |
| 1E | 500 | 6 | 7.1 | 40.4 | 22 |
| 2E | 500 | 0.5 | 9.1 | 78.8 | 25 |
| 2E | 500 | 6 | 8.7 | 48.1 | 25 |
| 3E | 500 | 0.5 | 9.2 | 52.1 | 25 |
| 3E | 500 | 6 | 9.1 | 51.3 | 25 |
| 4E | 500 | 0.5 | 9.2 | 55.6 | 27 |
| 4E | 500 | 6 | 9.1 | 130 | 26 |
| 5E | 500 | 0.5 | 9.2 | 54.6 | 25 |
| 5E | 500 | 6 | 8.9 | 49.0 | 27 |
| 6E | 500 | 0.5 | 8.8 | 58.6 | 21 |
| 6E | 500 | 6 | 8.6 | 47.2 | 24 |
| 7E | 500 | 0.5 | 9.1 | 58.0 | 24 |
| 7E | 500 | 6 | 8.4 | 49.3 | 17 |
| 6B | 500 | 0.5 | 7.4 | 62.0 | 15 |
| 6B | 500 | 6 | 7.5 | 32.0 | 22 |
| Test water and fine-rock composite | L/S | Time h | pH | Conductivity ($\mu\text{S}/\text{cm}$) | Alkalinity as CaCO_3 mg/L |
| Talbingo water only | ∞ | 0.5 | 7.0 | 39.9 | 14 |
| Talbingo water only | ∞ | 6 | 7.0 | 24.5 | 13 |
| 4E | 10,000 | 0.5 | 7.3 | 42.2 | 16 |
| 4E | 10,000 | 6 | 7.4 | 32.5 | 18 |
| 4E | 5,000 | 0.5 | 8.0 | 45.1 | 18 |
| 4E | 5,000 | 6 | 7.7 | 36.4 | 19 |
| 4E | 2,000 | 0.5 | 8.9 | 46.9 | 22 |
| 4E | 2,000 | 6 | 8.7 | 45.2 | 22 |
| 4E | 500 | 0.5 | 9.2 | 55.6 | 27 |
| 4E | 500 | 6 | 9.1 | 130 | 26 |

3.4.4 Effect of rock particle size on substance release

Owing to the greater surface area and therefore reactivity, finer particle size materials are expected to represent the greatest environmental risk with respect to transport and release of substances. The size of the excavated rock material is expected to range from the large boulder to powder size. The vast majority of the excavated rock, by mass, will be larger than sand size and should settle rapidly. While it is important to understand the worst case scenario for impacts to the receiving water, to make realistic calculations of loads of substances that may be released from the rock during placement operations it is important to understand differences in substance release from larger particle size materials that may comprise the majority of the material by mass.

This section describes the results of tests undertaken to characterise the influence of rock particle size on substance release to the reservoir waters. Tests were performed on excavated rock materials that had been mechanically crushed to provide materials with the size categories 10-25 mm; 2-10 mm, 0.21-2 mm and <0.21 mm (composite fine material) (Memo 6, 26 October 2018) (Appendix D4). Elutriate tests were undertaken at L/S of 25 (40 g/L) and measurements made at time periods of 1, 4 and 24 h after mixing then settling in Talbingo Reservoir water. As fine dust was on the surface of large rock pieces, the three larger

rock fraction underwent a 10-s leach (add Talbingo Reservoir water, shake, then decant to waste) immediately before the test water was added.

Following these tests, further investigation was made into the finer particle-size fraction of materials and size categories 150-210, 63-150 and <63 µm (composite fine material) were prepared for three rock materials (1E, 4B, 5E). Elutriate tests were undertaken at a L/S of 1000 (1 g/L) represent a scenario where considerably settling of fine materials has occurred and measurement made 24 h after mixing then settling in Talbingo Reservoir water (Memo 8, 5 November 2018) (Appendix D4). The <210 µm composite was also tested at L/S = 1000 for comparison with previous experiments on the 75-µm rock composites, and these data are provided in Appendix D4.1).

Results

The pH, conductivity and dissolved Al concentrations are shown function of the size of the larger (0.21-25 mm) rock materials in Figure 3 for the 24-h time period. The relationships were similar at 1 and 4 h, and those Figures are provided in Appendix D4 (Memo 6). The concentrations of dissolved major ions (Na, K, Mg, Ca), are provided for 24 h (Figure 4) and for 1 and 4 h in Appendix D4 (Figures D3.3 and D3.4). For different visualisation, the effect of time is shown for individual rock size fractions in Figure 5. The particle size distributions of the <0.21 mm size fractions are provided in Appendix D4. Key observations from tests on the larger size fractions of rock materials include:

- For both pH and conductivity, the values were higher than the Talbingo Reservoir water across the full range of rock material sizes.
- Dissolved Al exceeded the DVG of 55 µg/L by a factor of 4 to 15 within 1 h for the <0.21 mm size fraction, and was below the DGV for the 0.21-2 mm size fraction initially before increasing to exceed the DGV for longer elutriate durations.
- pH kinetics: For the 0.21-2 mm size fraction, pH of 24-h elutriates was significantly lower than 1-h and 4-h elutriates.
- Conductivity varied greatly between different fine rock fractions, and increased with time for the <0.21 mm fraction. Major initial increases (1 h) then variable increases, potentially doubling conductivity over 4 h, with less change through to 24 h.
- The <0.21 mm samples had particle diameters that generally spanned the <0.001-0.21 mm range. Sample 4B (<0.21 mm) was the finest with 50% of the sample being <21.5 µm. The other samples comprised approximately 50% silt i.e. approximately 50% <63 µm.
- For the tests undertaken with L/S = 25 (40 g/L), dissolved As, Cr and/or Zn concentrations frequently exceeded the DGVs (13 µg As(V)/L, 1.0 µg Cr(VI)/L) and 8 µg Zn/L) in elutriates, including elutriates of larger rock fractions over longer durations (Appendix D4). No other metal concentrations exceeded DGVs.

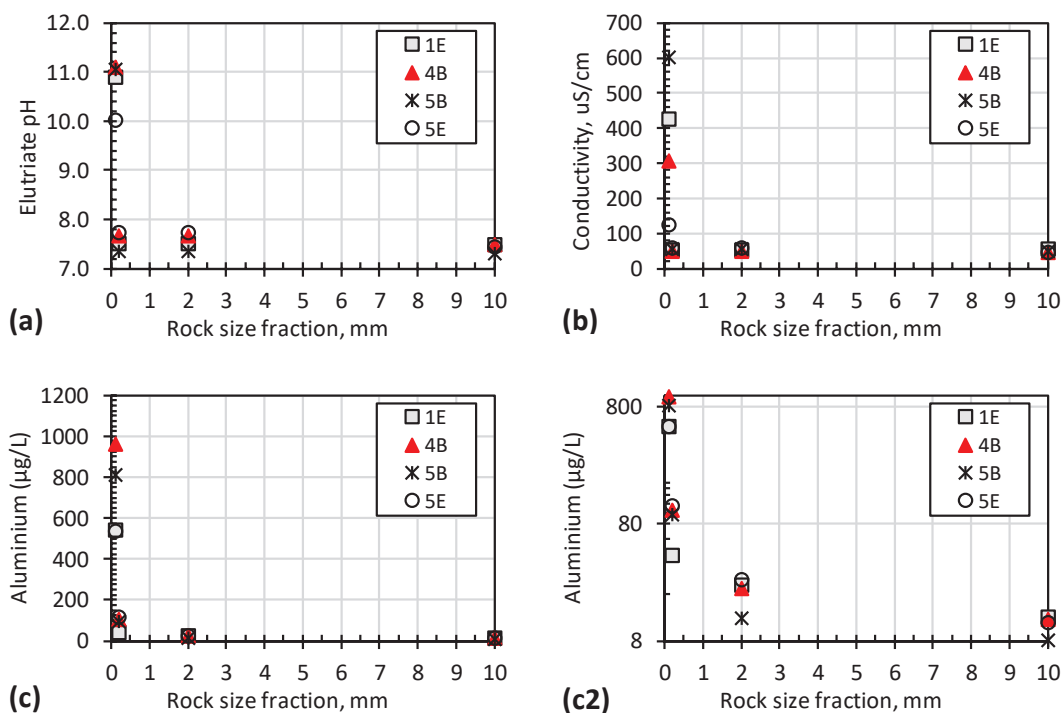


Figure 3. The pH, conductivity and dissolved Al after elutriate time of 24 h (c2 = log scale). Note that the <0.21, 0.21-2, 2-10 and 10-25 mm grain size treatments are plotted on the x-axis of figures at 0.1, 0.21, 2 and 10 mm, respectively.

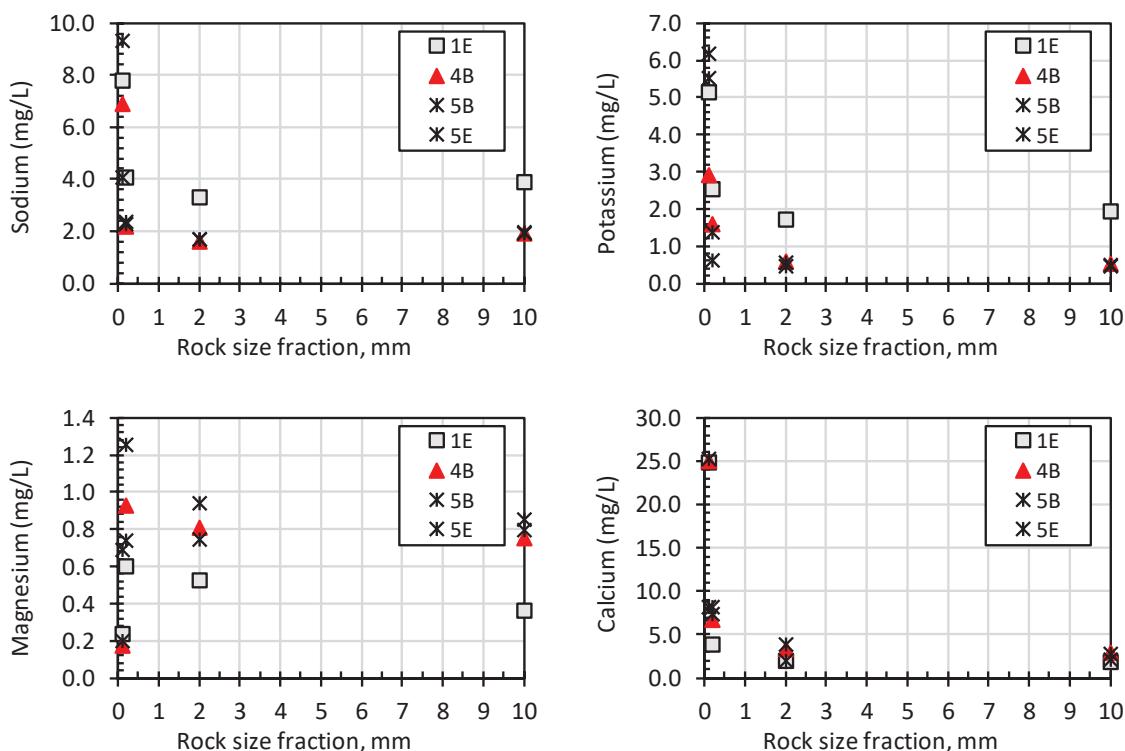


Figure 4. Dissolved major ions (Na, K, Mg, Ca) after elutriate time of 24 h. Note that the <0.21, 0.21-2, 2-10 and 10-25 mm grain size treatments are plotted on the x-axis of figures at 0.1, 0.21, 2 and 10 mm, respectively.

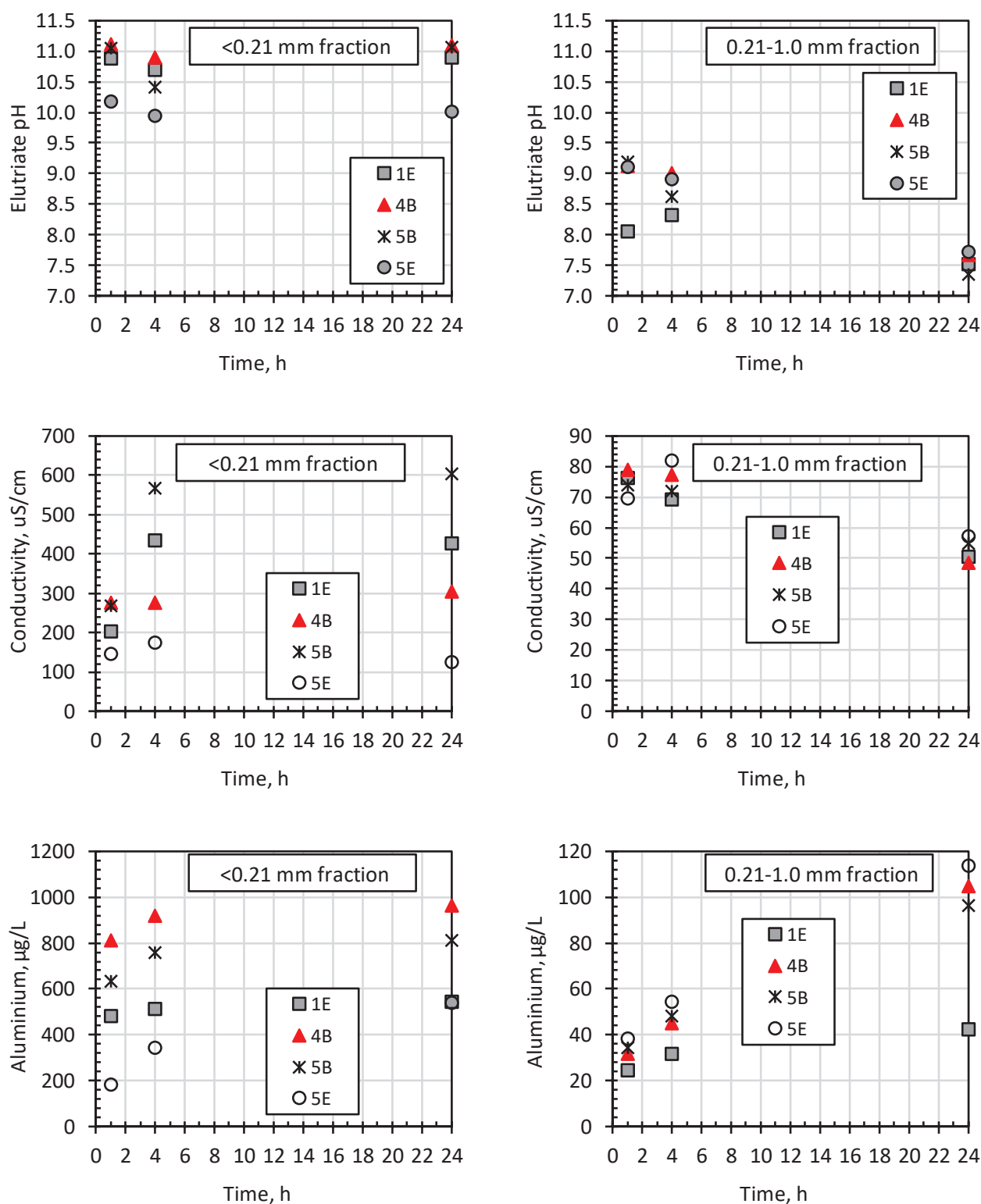


Figure 5. Effect of elutriate time on pH, conductivity and dissolved Al for the two smaller rock size fractions (<0.21 mm and 0.21-2 mm) (L/S=25)

For the <63, 63-150 and 150-210 μm size fractions ($L/S=1000$), the particle size relationships for pH, conductivity and dissolved Al concentrations are in Figure 6 and Figure 7 for major ions (Na, K, Mg, Ca) (24 h elutriates). Key observations from tests on these smaller particle-size rock materials include:

- The dissolved Al exceeded the DVG of 55 $\mu\text{g/L}$ by a factor of 4.2 to 1.1 for the <63 and 63-150 μm size fractions, and was below the DVG for the 150-210 μm size fraction (Figure 7).
- The dissolved Ca and K decreased as the size fraction increased, but the decreases were not as steep as for dissolved Al, while the dissolved Mg and Na were generally similar for the different size fractions (Figure 8).

Significant observations from particle size tests

- Substance release is low, trends towards negligible, for rock materials >2 mm.
- The finer <0.21 mm rock fraction is likely to have an impact on water quality that is an order of magnitude greater than that of rock fractions >2 mm in size.
- For the finer rock materials, pH, conductivity and dissolved Al concentrations decrease as the particle size increases from <63 μm to 150-210 μm , however, the decrease was essentially linear compared to the more exponential decrease observed as size increased for the larger particle size fractions.
- For a L/S of 1000 (1 g/L), the dissolved Al released from the <63 μm size fraction exceeded the DGV after 24 h. For the 63-150 μm , there was a much smaller exceedance of the DGV.
- Dissolved As and/or Cr concentrations frequently exceeded the DGVs in tests with $L/S = 25$ (40 g/L)

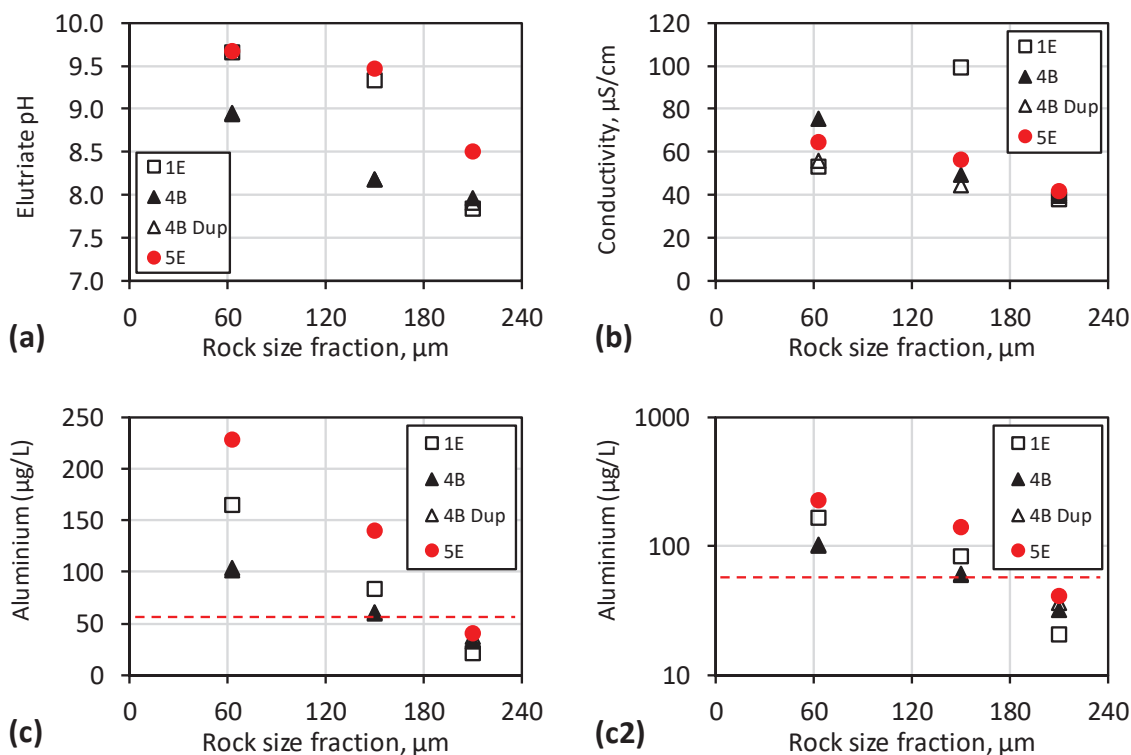


Figure 6. pH (a), conductivity (b) and dissolved Al (c, c2) after an elutriate time of 24 h (c2 = log scale) for <63, 63-150 and 150-210 μm size fractions ($L/S=1000$). A red dashed line at 55 $\mu\text{g/L}$ indicates the DVG. Note that the <63, 63-150, and 150-210 μm grain size treatments are plotted on the x-axis of figures at 63, 150 and 210 μm , respectively.

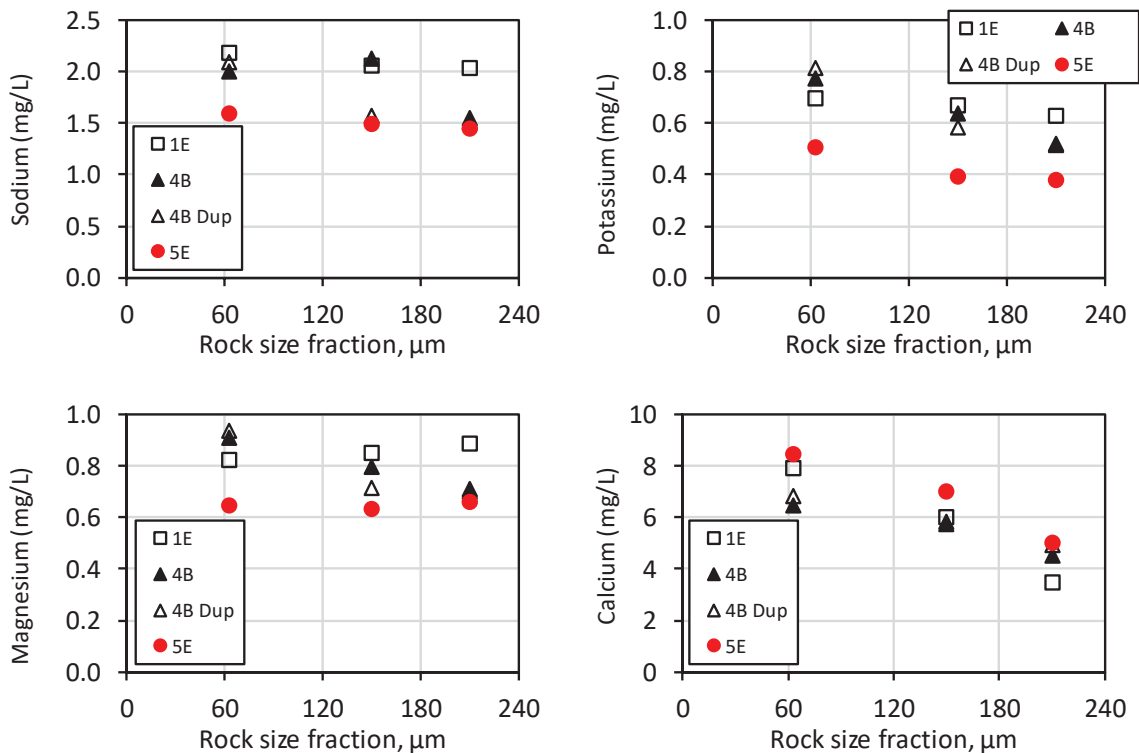


Figure 7. Major ions (Na, K, Mg, Ca) after an elutriate time of 24 h for <63, 63-150 and 150-210 μm size fractions. Note that the <63, 63-150, and 150-210 μm grain size treatments are plotted on the x-axis of figures at 63, 150 and 210 μm, respectively.

3.4.5 Comparison between leaching in Talbingo and Tantangara Reservoir waters

Talbingo Reservoir water was used for most of the elutriate tests as this was anticipated at the time the tests were undertaken to be the location where most of the excavated rock material may be placed (Greg Britton, personal communication). For comparison, elutriate tests were performed in Tantangara Reservoir water and with <75-μm composite rock materials 1B, 2B, 5B, 5E and 7E (Memo 13, 26 November 2018) (Appendix D5). The tests were performed at L/S of 300 and 1000 (3.3 and 1 g/L) with measurements made at 3 and 18 h, enabling comparison with results for Talbingo Reservoir water (Memo 11, Appendix D2). Comparisons of elutriate results for Tantangara and Talbingo Reservoir waters are shown for pH, conductivity and dissolved Al concentrations with composite 2B in Figure 8 and the dissolved Al concentrations for composites 1B, 5B, 5E and 7E are shown in Figure 9, with results for other substances provided in Appendix D5.

For Tantangara Reservoir water treatments, the concentration of dissolved Al was below the DGV of 55 μg/L for the 1000-L/S treatments at 3-h and 18-h, and exceeded the DGV for the 300 L/S treatments at 3 and 18 h. The lower pH of Tantangara 18-h_1000-L/S treatments compared to the corresponding Talbingo treatments indicates the Tantangara Reservoir water had a greater ability to buffer pH increases than the Talbingo Reservoir water. In turn, the lower dissolved Al released from the Tantangara 18-h_1000-L/S treatments than the corresponding Talbingo treatments is likely influenced by the lower pH resulting in slower mineral dissolution and release of Al as the aluminate ion, which is favoured at higher pH values. No other metal or metalloid concentrations exceeded DGVs.

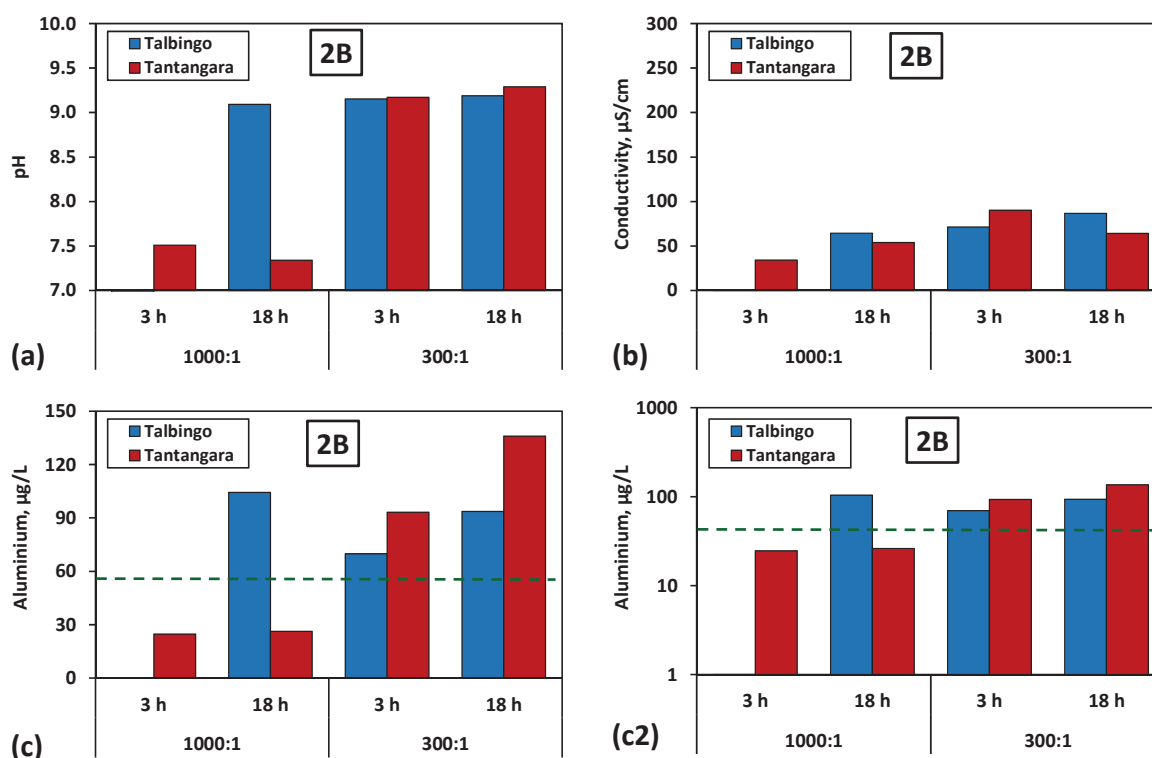


Figure 8. Comparison between the pH, conductivity and dissolved Al concentration measured in Talbingo and Tantangara Reservoir waters following elutriate tests with excavated rock composite 2B (c2 = log scale)

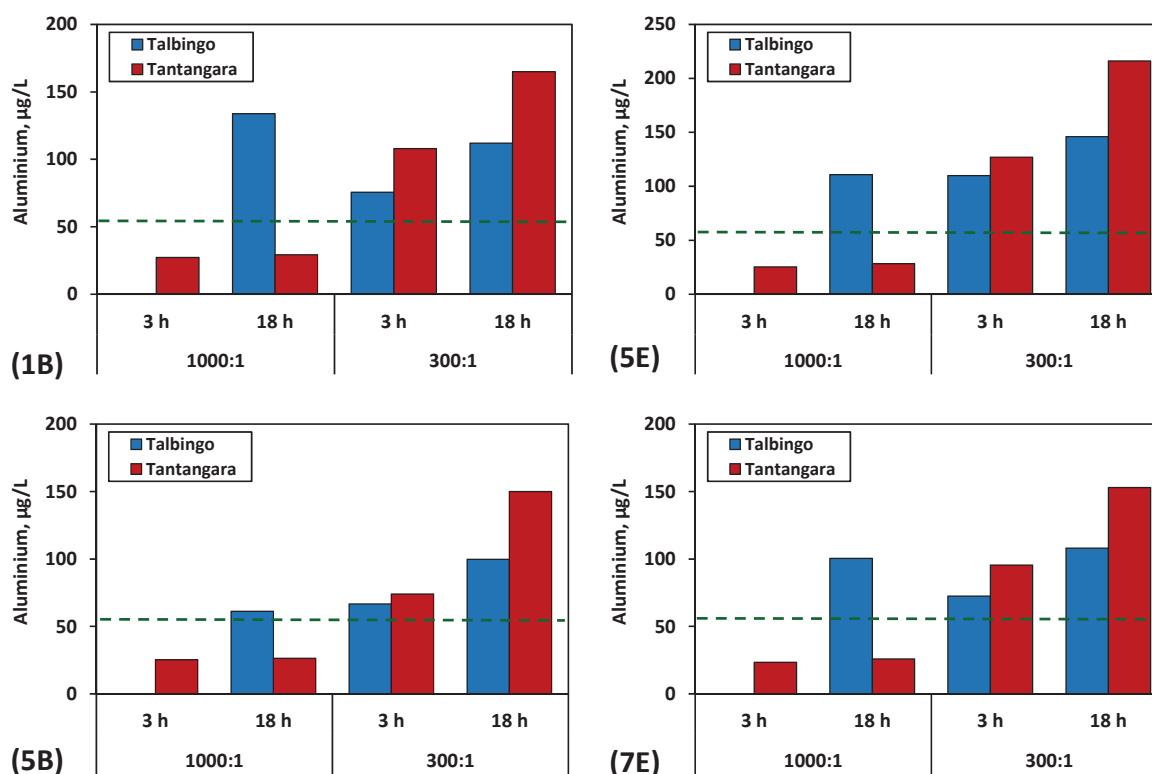


Figure 9. Comparison between the dissolved Al concentration measured in Talbingo and Tantangara Reservoir waters following elutriate tests with excavated rock composites 1B, 5B, 5E and 7E. A green dashed line at 55 µg/L indicates the DGV.

Significant observations from comparison of substance release in Talbingo and Tantangara Reservoir waters

The elutriate water pH was similar in the Tantangara and Talbingo Reservoir water treatments for the 300-L/S tests, but lower in the Tantangara Reservoir treatments for the 1000-L/S_18-h tests, probably due to this water having a greater ability to buffer pH increases. The conductivities were generally in a similar range for the two reservoir waters except for a few Tantangara Reservoir treatments having higher values.

The concentration of dissolved Al was in the range 23.5-216 µg/L in the Tantangara Reservoir elutriate treatments, which was in a similar range to corresponding Talbingo Reservoir treatments conducted in previous tests. Small differences were observed for corresponding treatments, with the Talbingo elutriate treatments having higher concentrations than the Tantangara treatments for the 1000-L/S_18-h tests, and the Tantangara elutriate treatments having higher concentrations than the Talbingo treatments for the 300-L/S_3-h and 300-L/S_18-h tests.

The concentration of dissolved Al in the 1000-L/S Tantangara Reservoir water treatments was below the DGV of 55 µg/L for the 1000-L/S treatments, and exceeded the DGV for the 300-L/S treatments.

3.4.6 Effect of water temperature on substance release

Substance release from solids to waters is usually greater at higher temperatures and to provide a worst-case scenario for substance release the elutriate tests were conducted at a temperature of 21°C. The temperature of the reservoirs varies between approximately 6 and 21°C, with significant changes over depth and season. Lower temperatures may substantially slow the kinetics of reactions that effect the release of pollutants from excavated rock material into the reservoirs.

Elutriate tests (L/S of 300 and 1000) with the <75-µm composite rock materials 1B, 2B, 5B, 5E and 7E were performed at 6°C Memo 9 (7 November 2018) (Appendix D6), and compared with results from corresponding tests performed at 21°C in Talbingo Reservoir water (Memo 11, Appendix D2). The kinetics of substance release at 6 °C was monitored at time periods of 6, 18 and 48 h, while the 21±2°C treatments to which they were compared were sampled after 0.5 and 18 h, with the 3.3 g/L (300/1 L/S) also being sampled after 3 and 120 h. Therefore, the 18-h time point was directly comparable and trends over time were also compared to investigate the effect of temperature on water quality. Comparisons of composite 2B elutriate pH, conductivity and dissolved Al concentrations for water temperatures of 6 °C and 21 °C are shown in Figure 10, and the dissolved Al concentrations for composites 1B, 5B, 5E and 7E are shown in Figure 11. All of the results are provided in Appendix D6, including figures for major cations.

The concentrations of major cations were generally similar for the 1 g/L (1000 L/S) at both temperatures, whereas for the 3.3 g/L (300 L/S), marginally higher concentrations were generally measured for the 21°C than the 6°C (data in Appendix D6).

For the 6°C treatments, only the 3.3 g/L (300 L/S) had dissolved Al concentrations that exceeded the DGV of 55 µg/L (dotted red line in graphs), which occurred for the 48 h sampling time for all but composite 5E, for which the DGV was exceeded for all durations tested. The dissolved Al increased continuously over the 48 h test period for all 6°C treatments and would presumably continue to increase for some time if the test was run longer (i.e. the concentration did not plateau after 48 h). No other metal or metalloid concentrations exceeded DGVs.

A comparison between the 6 and 21°C values for dissolved Al concentrations is shown for all the composite materials together at 18 h in Figure 12. Conductivity was similar for both temperatures (Appendix D6). Water pH and dissolved Al concentrations were mostly higher at 21°C than at 6°C.

Significant observations from comparison of substance release at low water temperature

The release of Al occurred significantly more slowly in the 6°C treatments than the 21°C treatments. As such, after 18 h, the concentration of dissolved Al (and pH) were generally substantially lower for the lower temperature treatment. The dissolved Al continued to increase over the 48-h period of the 6°C test and did not plateau. After 48-h, the dissolved Al exceeded the DGV of 55 µg/L for all 6°C treatments at 3.3 g/L (300 L/S), but did not exceed the DGV for any 1 g/L (1000 L/S) treatments.

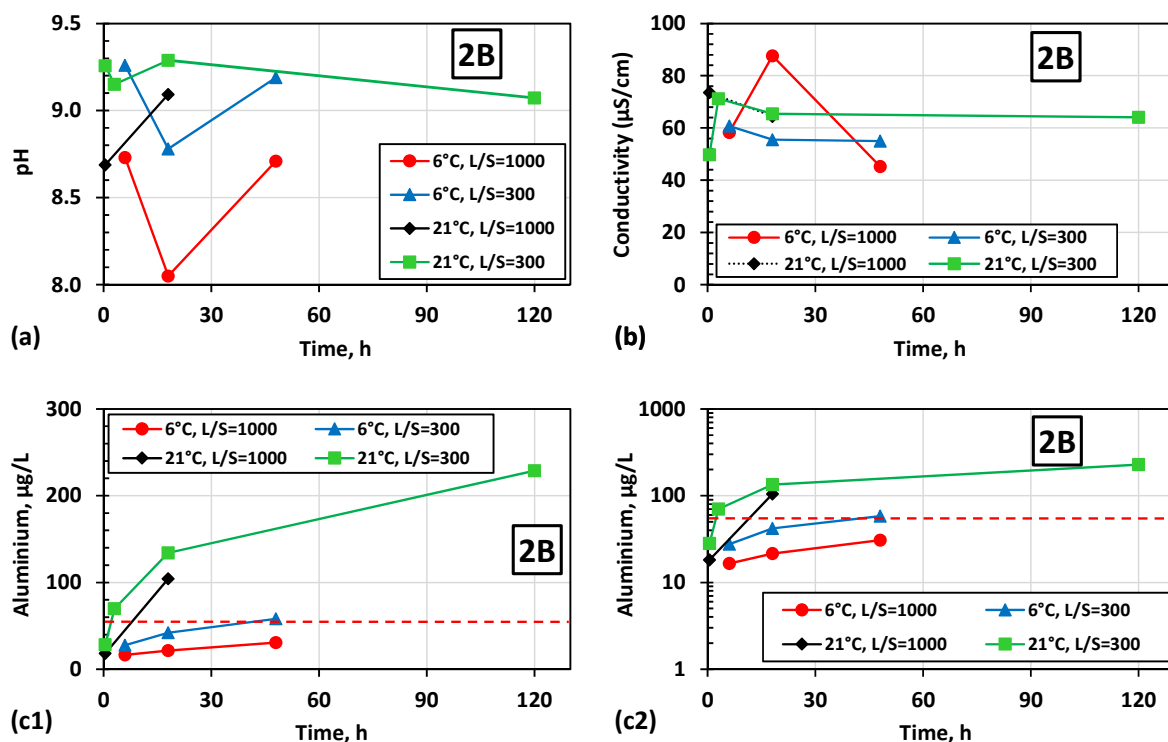


Figure 10. The pH, conductivity and dissolved Al over time for composite 2B (c2 = log scale)

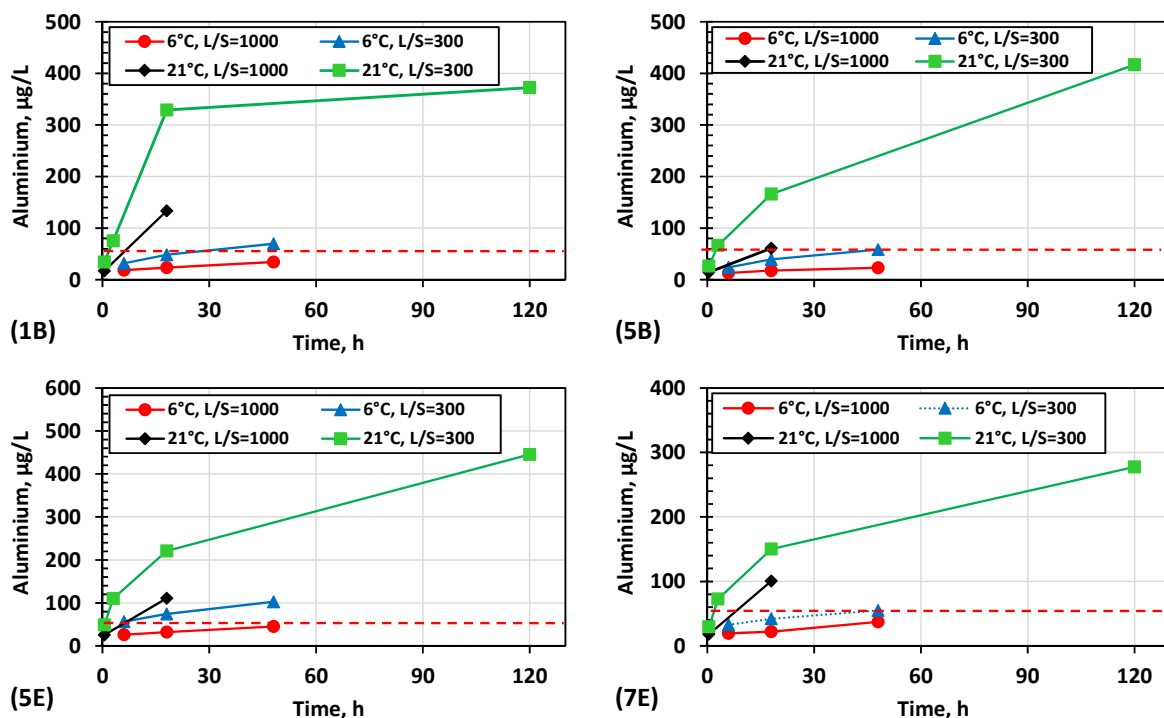


Figure 11. Dissolved Al concentrations at 6°C and 21°C at L/S 300 and 1000 for elutriate tests with excavated rock composites 1B, 5B, 5E and 7E. A red dashed line at 55 µg/L indicates the DGV.

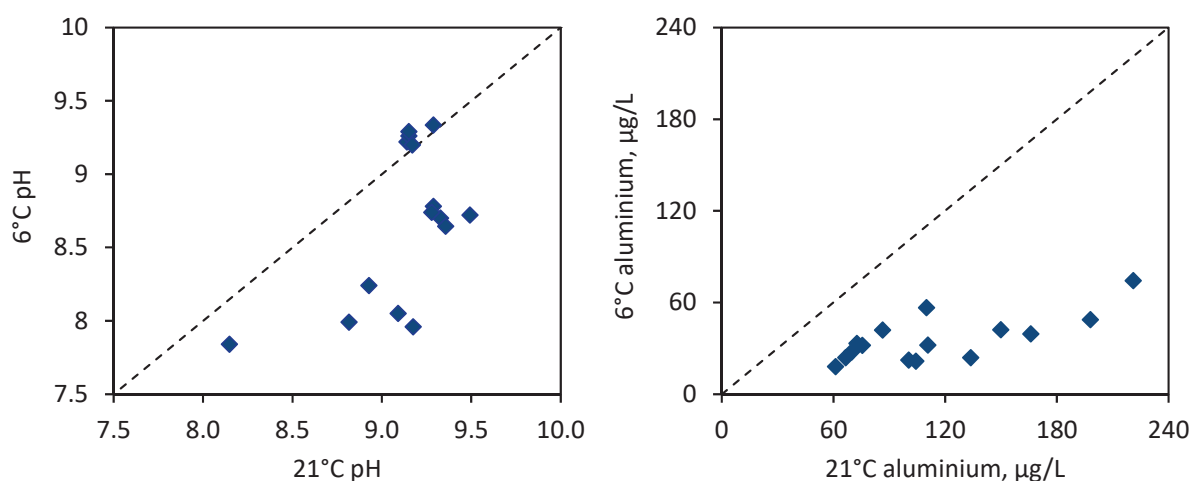


Figure 12. Comparison between temperatures of 6 and 21°C on the pH and dissolved Al for 1B, 2B, 5B, 5E and 7E composites after 18 h in Talbingo Reservoir water. The dotted unity line indicates a 1:1 relationship.

3.4.7 Effect of repeat leaching on substance release

Greater release of substances may occur from the fine rock materials if they remain in the water column, either within the placement area or as they disperse away from the placement area. To assist in predictions of long-term leaching, a series of repeat/successive leach tests was performed on the same rock materials (Memo 12, 26 November 2018) (Appendix D7).

Two series of successive elutriate tests (3 leaches each) were performed on the <75-µm composite rock materials 1B, 2B, 5B, 5E and 7E. The first successive leach test series investigated the effect of two mixing durations (0.5 or 18 h) at L/S of 30 and 300 at 21°C. Key relationships are shown in Figure 13 (pH, conductivity and dissolved Al for 2B) and Figure 14 (dissolved Al concentrations for all other treatments, with other figures provided in Memo 12 and Appendix D7). The second successive leach test series investigated the effect of temperature (6°C and 21°C) for the two L/S (30 and 300) and had a duration of 18 h (further method details are provided in Memo 12). Key relationships shown in Figure 15 (pH, conductivity and dissolved Al for 2B) and Figure 16 (dissolved Al concentrations for all other treatments, with other figures provided in Memo 12 and Appendix D7).

Results from first test series - L/S of 30 or 300, 21°C, 0.5 or 18 h mixing

In the first test series, the pH was generally higher for a lower L/S ratio and longer mixing duration and decreased in each successive leach. The conductivity was more variable than pH, but was generally marginally higher for the lower L/S, and for the L/S=300, was higher for the longer mixing duration. Apart from a few treatments, the conductivity generally decreased in each successive leach. Figures are provided for major cations in Appendix D7.

For all excavated rock samples at each L/S ratio and mixing duration, the concentration of dissolved Al in the leach 1, 2 and 3 solutions were in the range 26.6-329, 26.7-416, and 26.5-512 µg/L, respectively. The concentration of dissolved Al was generally similar or increased over successive leaches, despite the water pH successively decreasing.

The dissolved Al exceeded the default guideline value (DVG) of 55 µg/L for each of the three leaches for each material after a mixing duration of 18 h. The DGV was never exceeded for the L/S=300, 0.5-h treatments, with the dissolved Al remaining at a similar concentration for each successive leach, i.e. the short 0.5-h mixing duration at this L/S was not adequate to either release enough Al to exceed the DGV or exhaust the pool of Al in the samples, so the concentration remained steady. The concentration of dissolved Al released in the L/S=30, 0.5 h treatments always increased over successive leaches, with the

initial leach often being below the DGV and the later leaches being above the DGV. No other metal or metalloid concentrations exceeded DGVs, noting here that a single value of 42 µg/L Zn (exceeding the DGV of 8 µg/L) was attributed to contamination not associated with the rock (Appendix D7).

In the first test series, the pH was generally similar or marginally lower over successive leaches with L/S=30, while for those with L/S=300 the pH was generally similar between the first two leaches then decreased for the third leach. There were no discernible trends for the conductivity in successive leach test series 2, i.e. temperature had no clear effect on conductivity. The conductivity was in the range 35-402 µS/cm.

Results from second test series - L/S of 30 or 300, 6°C and 21°C, 0.5 h mixing and 17.5 h standing in water

For all excavated rock samples at each L/S ratio at 6°C, the concentration of dissolved Al in the leach 1, 2 and 3 solutions were in the range 23.1-109, 27.9-129, and 16.8-137 µg/L, respectively, and at 21°C, the concentration of dissolved Al in the leach 1, 2 and 3 solutions were in the range 93.6-299, 125-403, and 65.0-384 µg/L, respectively. Less Al was released in the 6°C than the 21°C treatments at each L/S ratio, and more Al was released by treatments with a lower L/S ratio. For the 21°C treatments, the dissolved Al was generally steady or decreased over the successive leaches, whereas, for the 6°C treatments the dissolved Al was steady or increased over the successive leaches. The dissolved Al exceeded the default guideline value (DVG) of 55 µg/L for all of the leaches of the 21°C treatments and most leaches of 6°C, L/S=30 treatments, while the DGV was not exceeded by any of the 6°C, L/S=300 treatments.

A comparison of the 21°C treatments that were in contact with the reservoir water for 18 h, 0.5-h mixing (successive leach test series 2) and 18-h mixing (successive leach test series 1) indicated that longer physical mixing often caused an increase in the release of dissolved Al (Figure 17); most evident for the 2nd and 3rd leaches. This is likely to be the cause of the difference in trends over successive leaches between the first and second test series for the 21°C treatments, i.e. generally similar or increased concentrations in test series 1 and generally similar or decreased in test series 2. However, even the short mixing durations (0.5 h) generally resulted in considerable release of dissolved Al when monitored over the same time period, which is a result of the slow settling of the fine rock material (i.e. a considerable portion remain suspended in solution for next 24 h) that are the dominant source of most Al released.

Data were gathered on total-P leaching in these tests and figures are provided in Appendix D7. For successive elutriates at L/S of 30, the total-P concentrations were within the range of 10-40 µg/L (exceeding the DGV of 10 µg/L) for each of the successive elutriates for rock composites 2B, 5B and 5E, but not for rock composites 1B and 7E. Significant observations relating to long term substance release (repeat/successive leaches)

The successive leaches indicated that the Al available for release into solution was not quickly exhausted. Many treatments had similar or increased Al concentrations in the 2nd and 3rd successive leaches. Consistent with results from Section 3.4.6, the lower temperatures resulted in substantially lower concentration of Al being released into reservoir waters. These results suggest a dissolution process is responsible for the release of Al, which is dependent on the duration of contact with water and the temperature. Longer durations of physical mixing also generally increased the release of dissolved Al. The DGV for Al, 55 µg/L, was exceeded by most treatments in the successive leach tests. No other metal or metalloid concentrations exceeded DGVs.

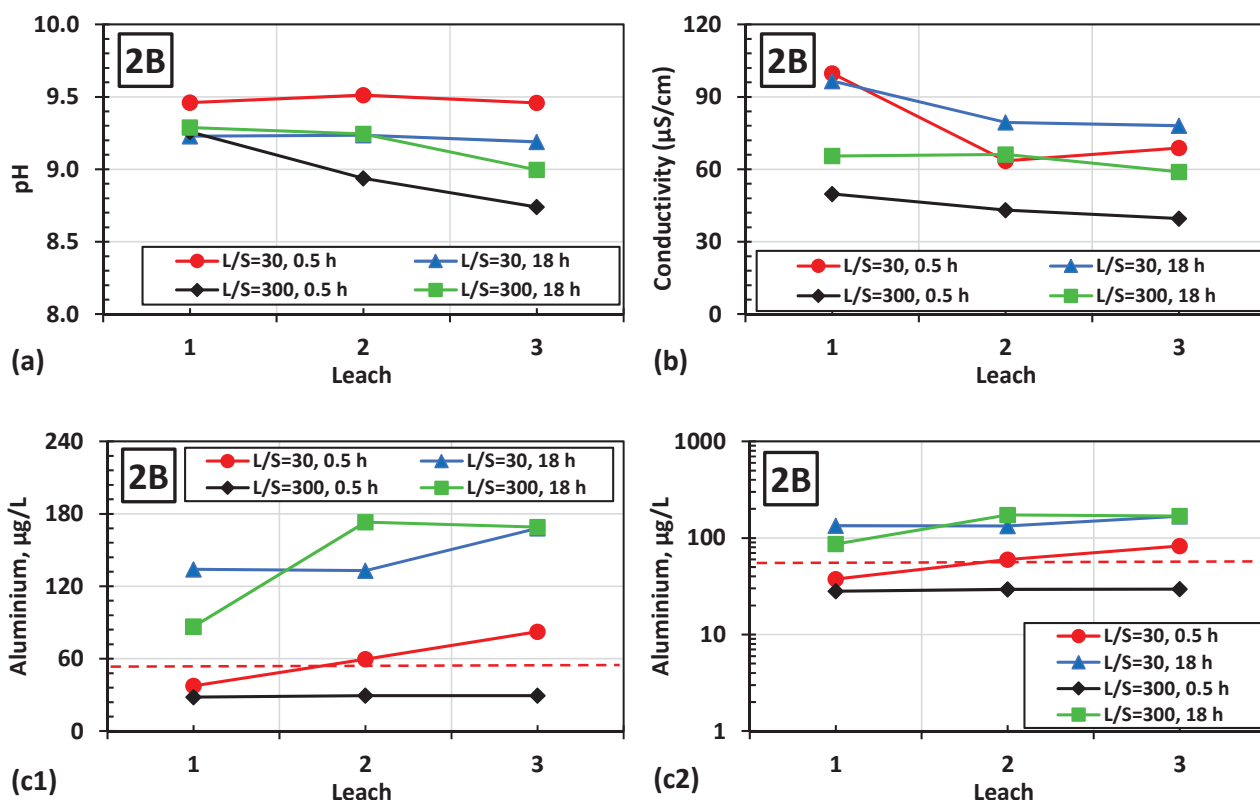


Figure 13. The pH, conductivity and dissolved Al concentration after three successive leach cycles at $21\pm2^{\circ}\text{C}$ for excavated rock sample 2B (successive leach test 1), where the effect of mixing duration and L/S ratio was investigated (c2 = log scale).

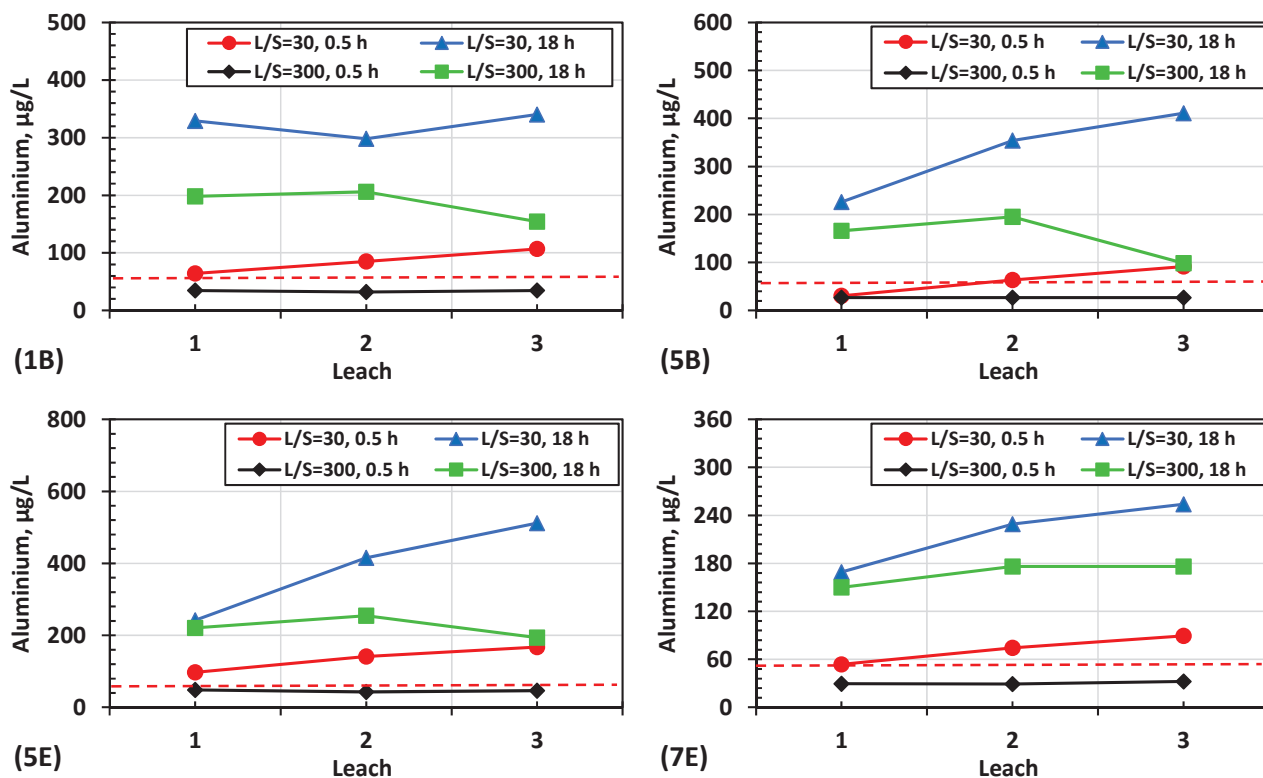


Figure 14. Dissolved Al concentrations for three successive leaches at L/S 30 and 300 after 0.5 h and 18 h for elutriate tests with excavated rock composites 1B, 5B, 5E and 7E. A red dashed line at $55\text{ }\mu\text{g/L}$ indicates the DGV.

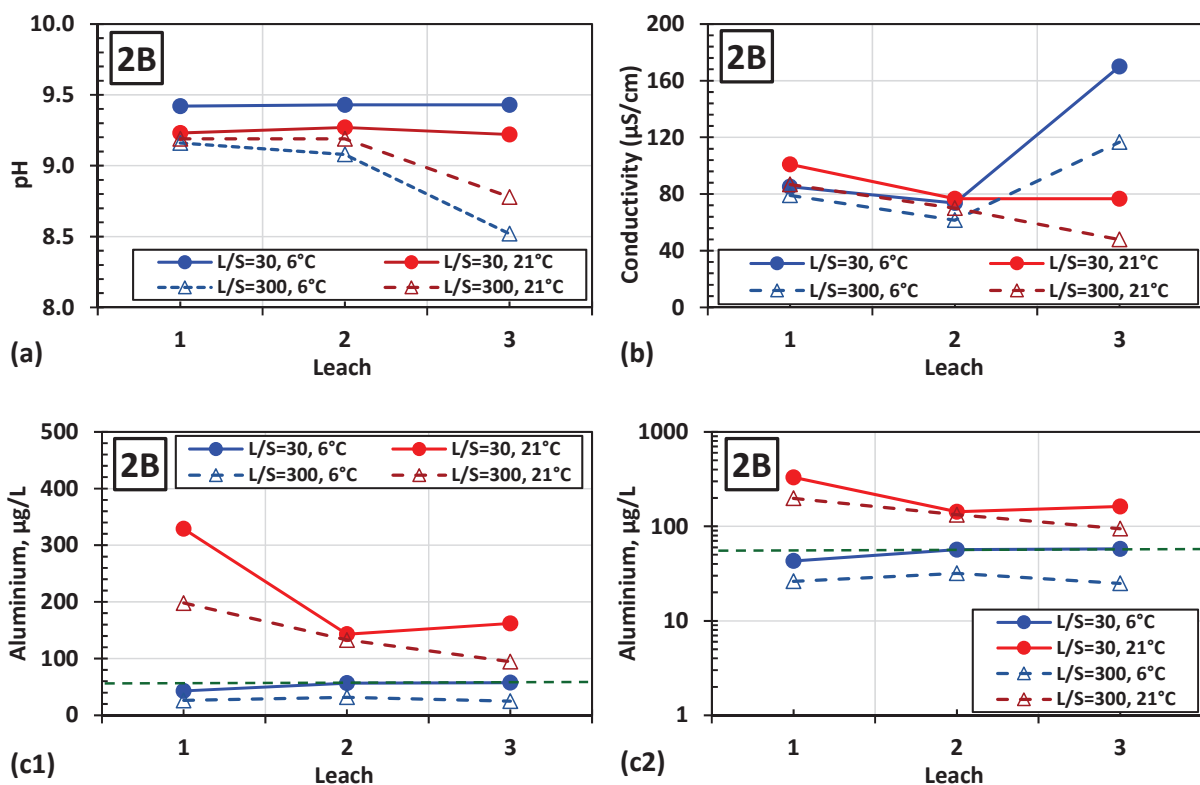


Figure 15. The effect of temperature on the pH, conductivity and dissolved Al concentration after three successive leach cycles at $6\pm1^{\circ}\text{C}$ and $21\pm2^{\circ}\text{C}$ for excavated rock sample 2B (successive leach test 2), (c2 = log scale)

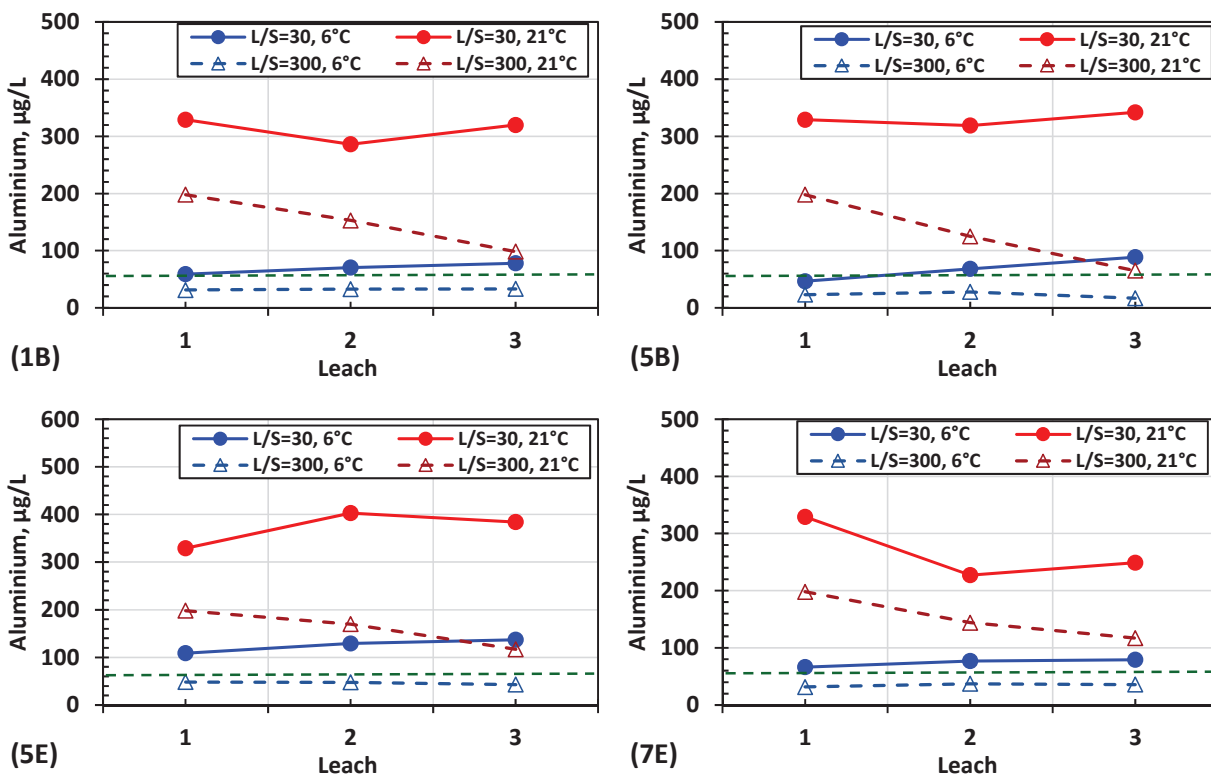


Figure 16. Dissolved Al concentrations for three successive leaches at of 6 and 21°C and L/S 30 and 300 for elutriate tests with excavated rock composites 1B, 5B, 5E and 7E. A green dashed line at $55\text{ }\mu\text{g/L}$ indicates the DGV

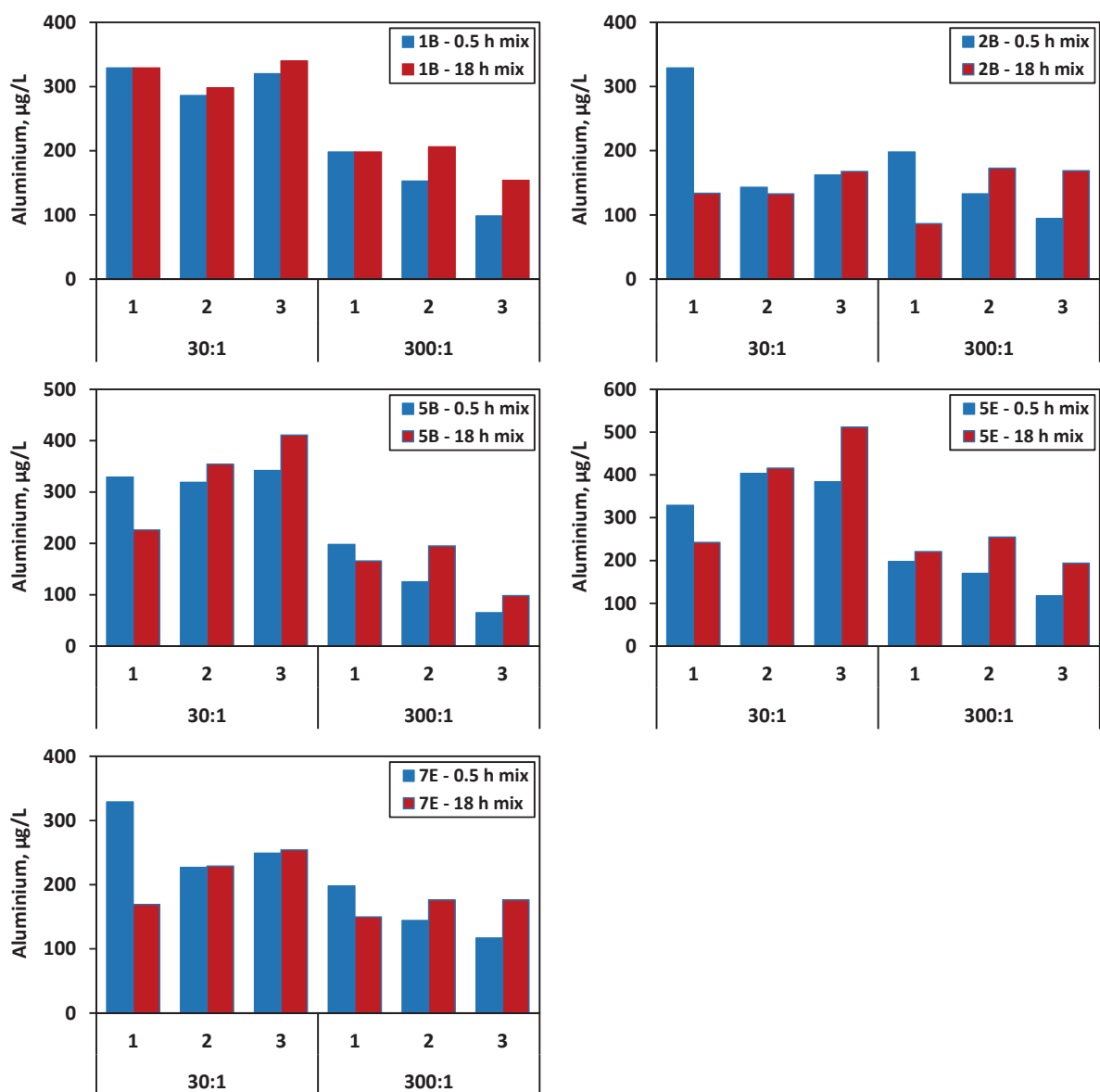


Figure 17. Comparison between the dissolved Al released from excavated rock material at L/S ratios of 30 and 300 in Talbingo Reservoir water after 18 h contact with water between successive leach test 1 (18 h mixing, red bars) and leach test 2 (0.5 h mixing, 17.5 h standing, blue bars) at 21°C to assess the effect of mixing vs standing for each successive leach (1, 2 and 3)

3.4.9 Significance of colloidal forms of Al with <0.45 µm filtered water

A significant portion of Al is often found to exist in colloidal forms in natural waters, and these forms are often predicted to be less bioavailable than truly dissolved forms. It is well recognised that the filtration of waters through a 0.45 µm filter (i.e. the standard filter size) does not completely separate dissolved and colloidal forms of metals (Gundersen and Steinnes, 2003; Wilkinson and Lead, 2007; Simpson et al., 2014). Colloids have sizes in the range of approximately 0.001–1 µm (Wilkinson and Lead, 2007) and may be less bioavailable to some aquatic organisms.

Tests were performed in Talbingo and Tantangara Reservoir waters with <75-µm composite rock materials at L/S of 300 (3.3 g/L) that were filtered (0.45 µm, dissolved and colloidal substances) and ultrafiltered (0.003 µm, dissolved substances) after 18 and 120 h (Appendix D8). The Al concentrations were similar in the <0.45 µm and <0.003 µm fractions of each treatment, and indicated that the <0.45 µm filterable water fraction of the <75-µm composite elutriates contained predominantly dissolved (<0.003 µm) (Figure 18) rather than colloidal forms of aluminium, which is consistent with the dominant aluminium species (ion) in the basic pH waters being the aluminate ion ($\text{Al}(\text{OH})_4^-$).

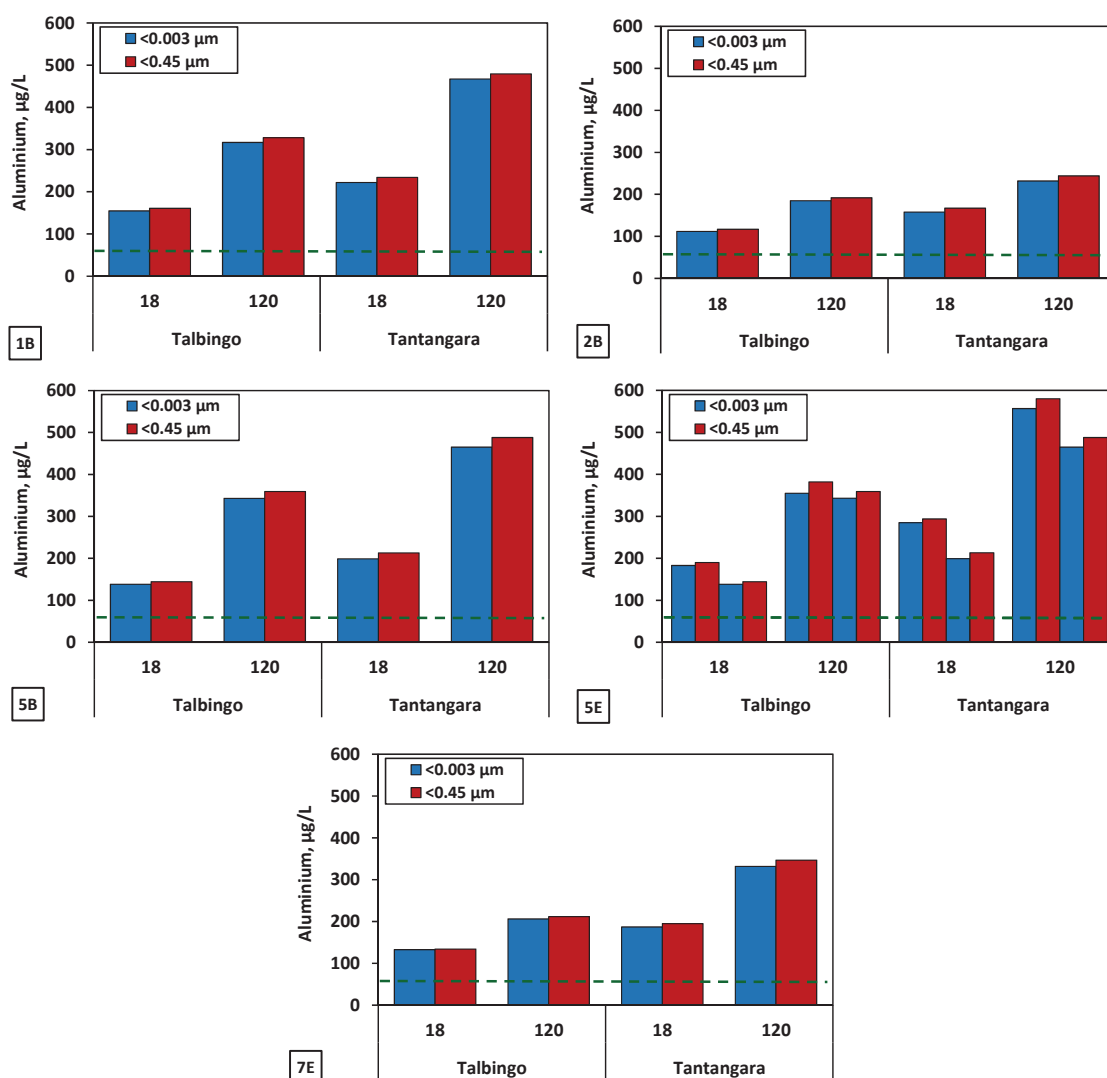


Figure 18. Comparison between the Al concentrations measured in leachate waters generated from a 300 L/S after filtering through 0.45 µm (dissolved and colloidal substances) and 0.003 µm (dissolved substances) filters. 5E has replicate treatments shown.

Significant observations relating to Al colloids

The <0.45 µm filterable elutriates waters prepared with Talbingo Reservoir waters contains predominantly truly dissolved forms of Al, which are predicted to be the aluminate ion, $\text{Al}(\text{OH})_4^-$.

3.4.10 Longer-term substance release

A portion of the finest rock particle size fractions (e.g. clay to fine silt (<2 µm to 6.3 µm)) may remain suspended in the bottom waters for months to years. The hydro-pumping operations of Snowy 2.0 may also generate hydrodynamic forces that result in repeated mixing (resuspension) of rock solids within their vicinity. To investigate long-term changes in water quality, two <75-µm composite rock materials (1B and 5B) were resuspended in Talbingo Reservoir water at L/S of 300 (3.3 g/L) and 1000 (1 g/L) at 6 and 21 °C, and measurements made after durations up to 56 days (Appendix D9). In these tests, each test treatment was initially shaken for 0.5 h to suspend the solids and then allowed to stand at each temperature until next sampled, when they were shaken for 10 s and subsampled for analyses. These longer-duration tests indicated the following (Figure 19):

- Following the initial immediate pH increase to pH 9.5, the pH decreased and exhibited a plateau within the range of pH 7.7-8.2 after approximately 30 days.
- The conductivity increased considerably over the 56 days, although any trends were obscured by variability, with values of 400-600 µS/cm range being reached. In particular, Ca concentrations in the L/S=300 treatments were markedly higher after 14 days (Appendix D9).
- Dissolved Al concentrations generally increased during the first 1-2 weeks then decreased, and indicated potential removal of dissolved Al due to changes in speciation, decreased solubility with decreasing pH, and/or increased adsorption. Over the pH range measured in the treatments of this test, the aluminate ion ($\text{Al}(\text{OH})_4^-$) would remain the dominate dissolved ion in solution.
 - At 21°C, the dissolved Al exceeded the DGV for all rock composite treatments; by a factor of 2-5 for the entire 56 d duration at L/S=300, and by a factor of 1-3 for the entire 56-d duration at L/S=1000, except the initial 18 h duration for 1B.
 - At 6°C, the dissolved Al marginally exceeded the DGV in the mid-duration subsamples of each treatment except the 1000 L/S, 1B treatment that never exceeded the DGV.
- No other metal or metalloid concentrations exceeded DGVs.
- Total-P concentrations remained below the DGV of 10 µg/L over the 56-day period (Appendix D9).

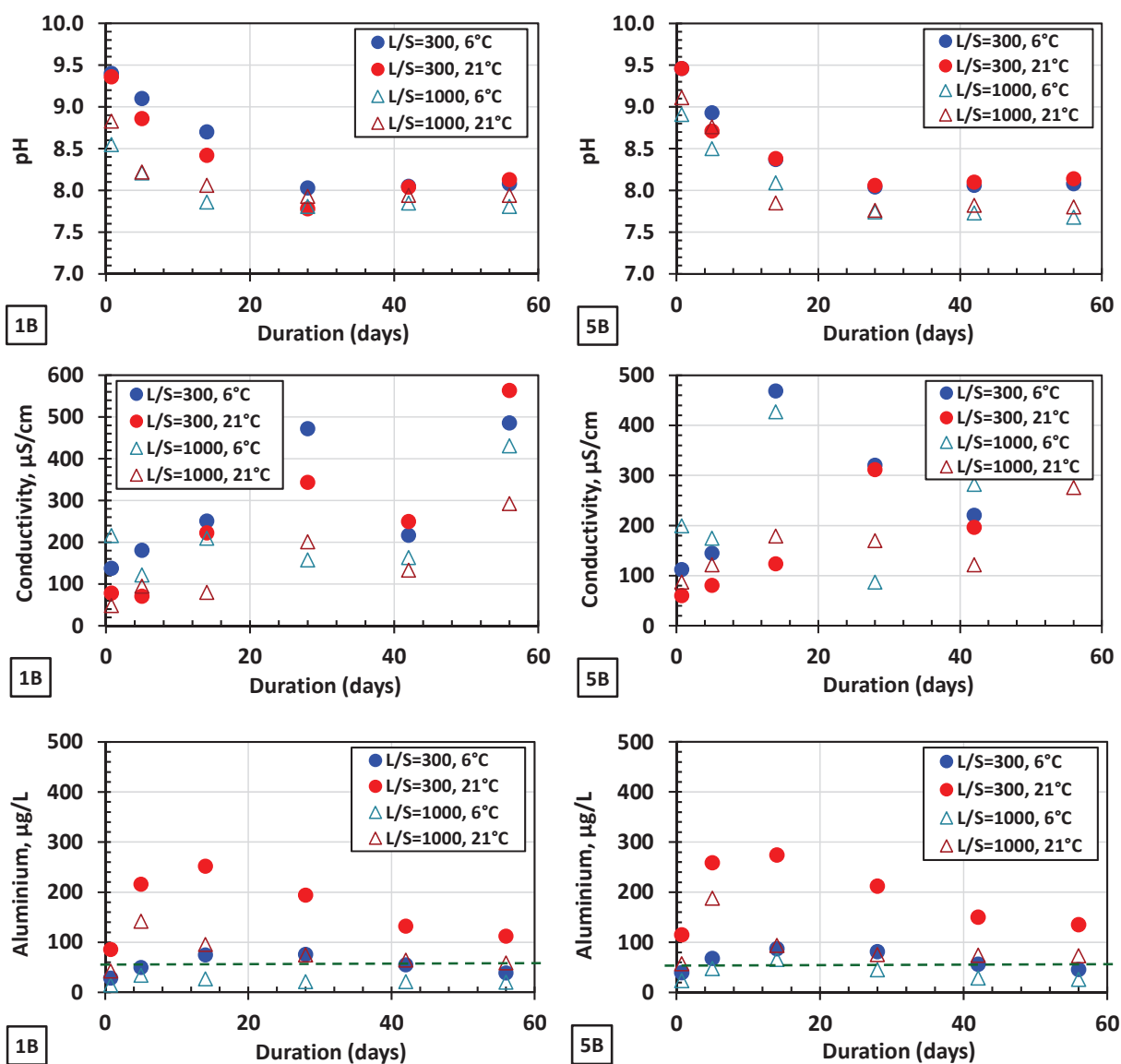


Figure 19. Longer term changes in water quality after water-rock mixing durations of up to 56 days for <75-μm rock composites 1B and 5Bd in Talbingo Reservoir water at L/S of 300 (3.3 g/L) and 1000 (1 g/L) at 6 and 21 °C. A green dashed line at 55 μg/L indicates the DGV.

Significant observations from long term mixing tests

After long durations (56 days) of mixing (suspension) of <75-μm rock composites in Talbingo Reservoir water the pH decreased to plateau, conductivity continued to increase and dissolved Al concentrations decreased, but dissolved Al concentrations remained above the Al DGV in tests performed at 21°C and L/S=300. Total-P concentrations remained below the DGV of 10 μg/L over the 56-day period.

3.4.12 Effect of resuspended sediment in attenuation of substances released from rock materials

Benthic sediments may be resuspended during and following the placement of excavated rock materials in the reservoirs. The sediment may release additional substances or adsorb substances that have been released from the rock materials. Sediment resuspension may attenuate dissolved concentrations of substances, including Al, through adsorption onto these solids. To investigate whether such attenuation reactions occur and the magnitude and rate of any attenuation, a series of tests were undertaken using resuspended and deposited sediments, and the first of these tests was reported in Memo 10 (8 November 2018) (Appendix D10).

First attenuation test – Effect of sediment concentration on attenuation

The first sediment resuspension-attenuation test used the remaining treatment solutions of composites 1E, 2E, 3E, 4E, 5E and 7E after the alkalinity test (Memo 7, 2 November 2018) was completed, and allowed them to equilibrate with the atmosphere for an additional 6 days before the sediment attenuation test was started. These waters had elevated dissolved Al concentrations and were mixed with the Talbingo Reservoir sediment PL2 (Section 3.2) at L/S of 50 and 500 [L-E/Sed=500 and L-E/Sed=50 (L-E=elutriate and Sed=sediment 2 and 20 g/L of PL2, respectively)] and compared with treatments having no added sediment. Each treatment was shaken to disperse the sediment then allowed to settle for 24 h before measurements. The results are compared with treatments containing no added sediment (Figure 20). The pH and conductivity of the elutriate waters decreased with increasing amounts of resuspended sediment. The dissolved Al concentrations in the 2 g/L added sediment treatments were substantially lower than the elutriate treatments with no added sediment, indicating the presence of the sediment contributed to the attenuation of dissolved Al. However, for the 20 g/L added sediment treatments, variable results were observed; the addition of 20 g/L PL2 sediment resulted in lower concentrations of dissolved Al for elutriates 3E and 4E, similar concentrations for elutriate 2E, and higher concentrations for elutriates 1E, 5E and 7E.

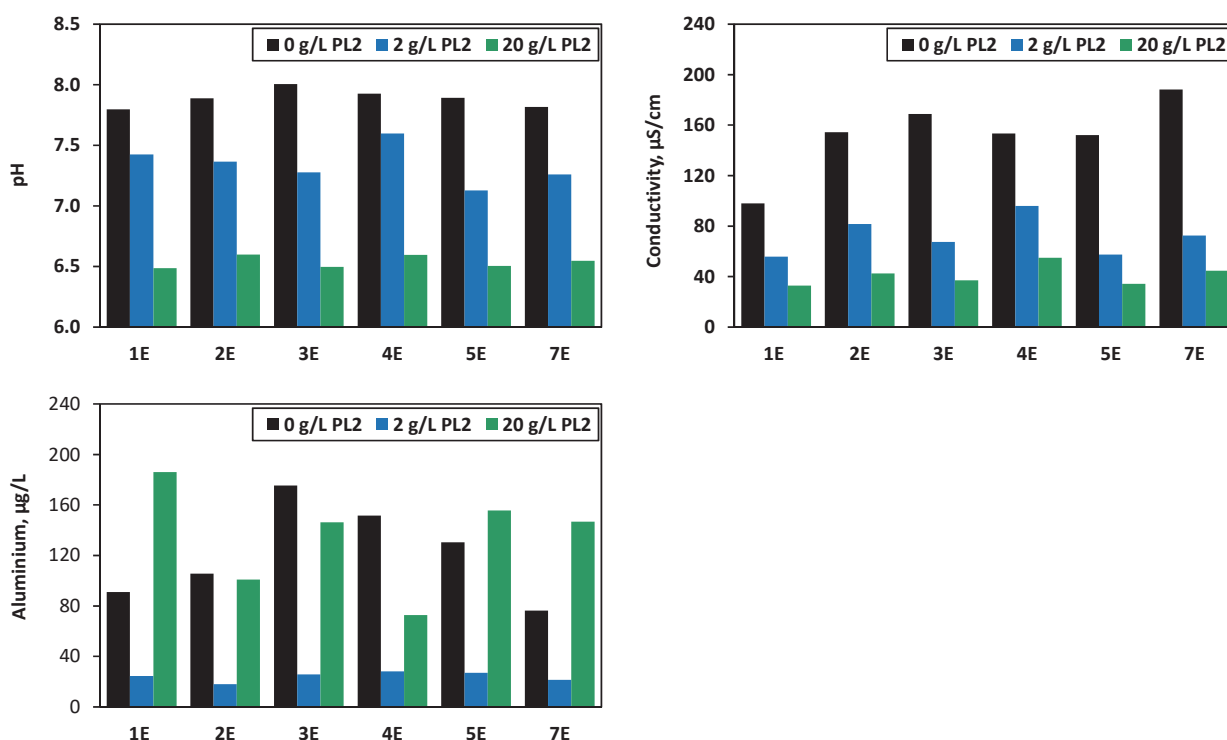


Figure 20. The pH, conductivity and dissolved Al after 0, 2 and 20 g/L of Talbingo Reservoir sediment PL2 was mixed for 10 s with 4-d old composite (1E, 2E, 3E, 4E, 5E and 7E) elutriates then allowed to stand for 24 h before measurement.

The dissolved Al ranges for the L-E/Sed = 500 and 50 sediment resuspension-attenuation tests were 18-28 µg/L and 73-186 µg/L, respectively, compared to the range for the initial waters of 76-176 µg/L, and that of the Talbingo Reservoir water of ca. 5 µg/L.

The PL2 sediment was used for these tests because it had the highest porewater Al concentration of 600 µg/L (Table 13), and should represent a worst case scenario for assessing risks. Based on the mass of sediment and volumes of test solutions, the maximum contribution of porewater Al from the addition of 20 g/L PL2 would be less than 10 µg/L. Increases of up to 100 µg/L dissolved Al were observed in the 20 g/L PL2 treatments, indicating the sediment particulate phase was likely the cause rather than pore water. Significant amounts of colloidal Al may be included in this filterable Al measurement, and the lower pH of 6.5 created by the presence of 20 g/L sediment would favour colloid formation.

Second attenuation test – Effect of resuspended sediment TSS concentration on attenuation

The second and third attenuation tests used a freshly prepared composite bulk elutriate water and Talbingo Reservoir sediments CA3, PL2, RA1, chosen because they had the largest differences in properties such as total organic carbon, particulate Fe etc. The bulk composite elutriate water was prepared by combining <75 µm masses of rock composites 1B, 2B, 5B, 5E and 7E (4 g per composite) to 2 L of Talbingo Reservoir water to achieve a L/S of 100, and was mixed for 24 h before use. This water had a dissolved Al concentration of 150 µg/L and pH 9.52 for attenuation test 2, while for attenuation test 3 that commenced a day later the dissolved Al concentration had decreased to 111 µg/L (same pH). The second attenuation test investigated the effect of resuspended sediment TSS concentration and involved combining an aliquot of elutriate with sediments CA3, PL2, RA1 at sediment TSS concentrations of 1, 5 and 25 mg/L, mixing for 30 min, and subsampling after 1 and 24 h.

These tests indicated that attenuation of dissolved Al concentrations by the presence of such small amounts of suspended sediment was low (<10%) (Figure 21) (Appendix D10.2). For the pH and dissolved Al, there was a general trend of slightly decreasing values as the TSS increased. There was also a general trend of slightly higher pH or concentration of dissolved Al in the 24 h subsamples compared to the 1 h subsamples for any given treatment. The slightly higher dissolved Al in the 24 h than the 1 h subsamples probably indicates release of Al from the suspended sediment. No discernible trend in conductivity was observed for the different parameters tests; TSS concentration, duration, sediment type. There was little difference in the pH, conductivity and concentration of dissolved Al between sediments CA3, PL2 and RA1.

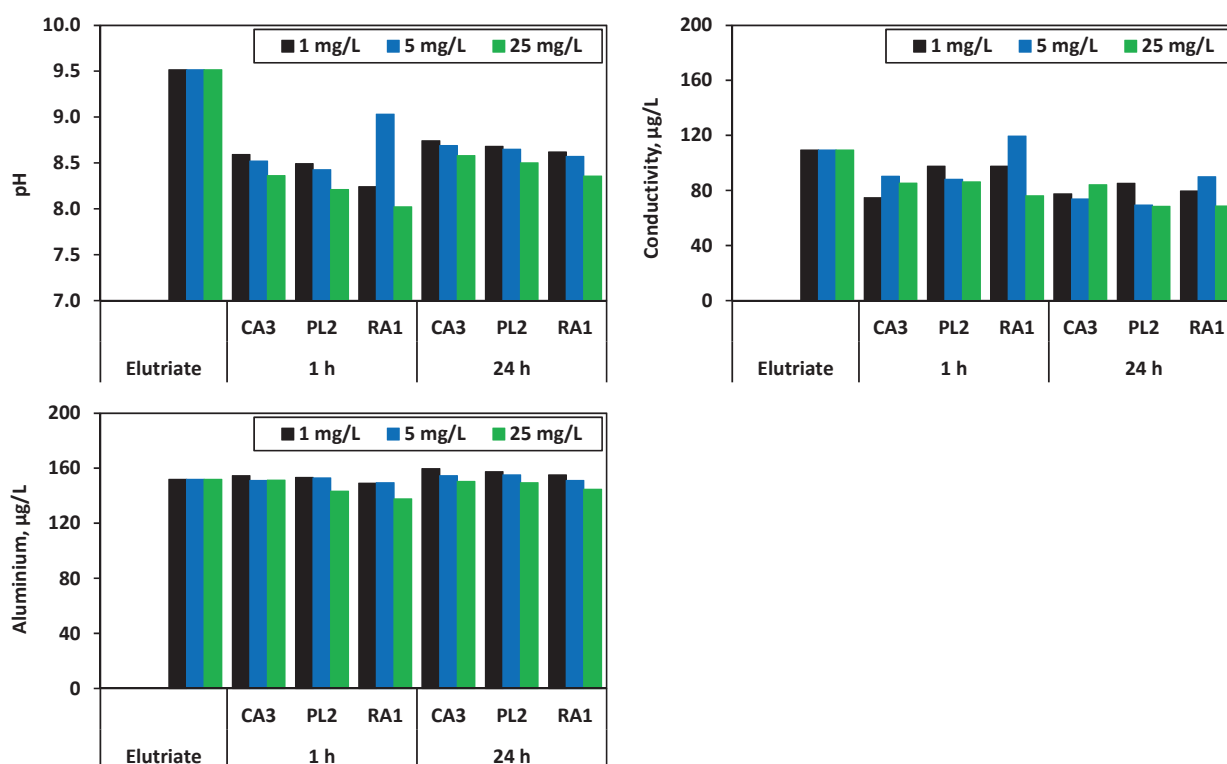


Figure 21. The effect of Talbingo Reservoir sediment TSS concentration on the composite elutriate pH conductivity and dissolved Al

Third attenuation test – Effect of deposited sediment and duration on attenuation

Attenuation test 3 investigated the effect of deposited sediments (CA3, PL2 and RA1) on the attenuation of substances present in the elutriate composite described above in the second attenuation test. Sediment (approximately 2 cm) was deposited on the bottom of 50 mL centrifugation tubes to represent the bottom of the reservoir. An aliquot of the composite elutriate was carefully added to minimise sediment resuspension, and subsamples were taken after 1, 6, 24 and 96 h. Each treatment was performed in duplicate.

The deposited sediments alone (no rock material) released 20-42 µg Al/L to the overlying water after 24 h (Appendix D10.3). In the presence of the deposited sediments the pH and dissolved Al concentration in the overlying elutriates waters decreased over time (Figure 22) to concentrations that were similar to the 24 h control values; the dissolved Al decreased substantially from the initial concentration of 112 µg/L. There was little difference in the attenuation of dissolved Al between the sediments CA3, PL2 and RA1. For each sediment the dissolved Al concentration had decreased below the DGV-dAl after 12 h (Figure 22, Appendix D10.3). No other metal or metalloid concentrations exceeded DGVs. No discernible trend in conductivity was observed for the different parameters tests; TSS concentration, duration, sediment type.

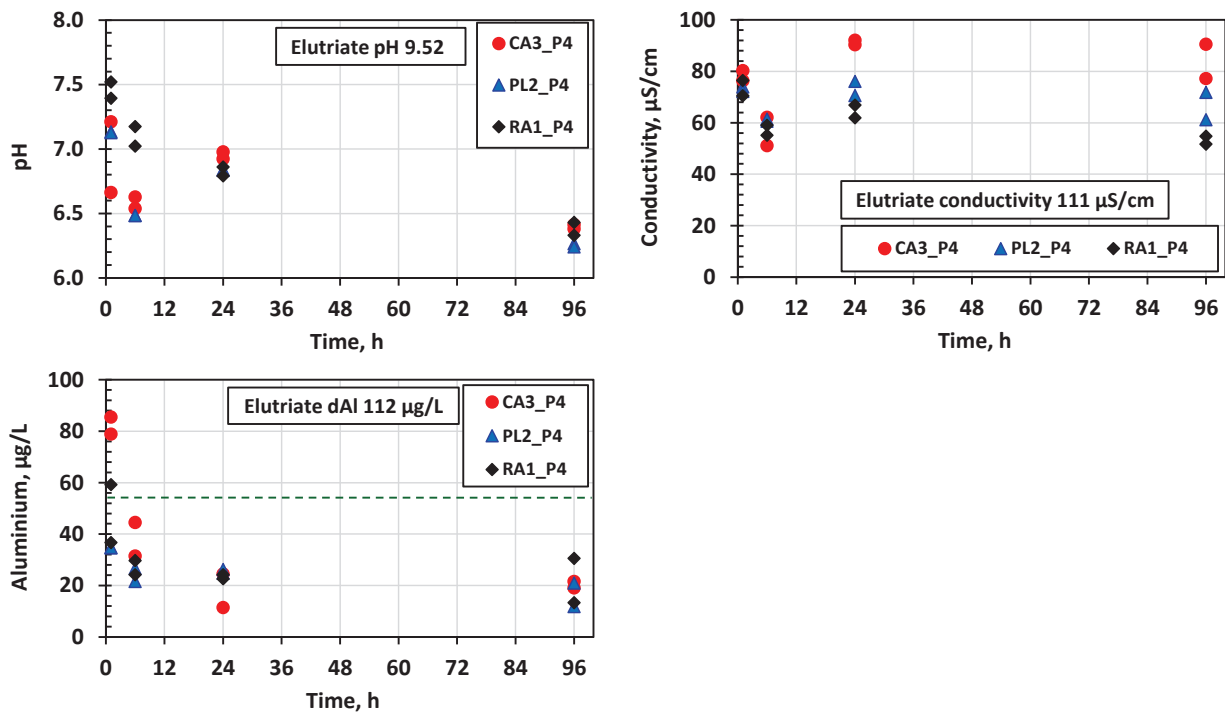


Figure 22. The pH, conductivity and dissolved Al concentrations in elutriate waters (initially pH 8.15, 110 µg Al/L) overlying three Talbingo Reservoir sediments (deposited, not resuspended)

Significant observations relating to sediment resuspension – attenuation tests

The presence of sediments may both lower (attenuate) or increase (release) dissolved substances. For Al, the particulate matter contains adsorption surfaces that decrease the concentration, but also act as a source of Al, possibly in colloidal forms, that can increase the concentration. The pH is also likely to influence the attenuation. Higher pHs (as measured in attenuation test 2) result in greater proportions of the dissolved Al being present as the aluminate ion, which probably has a low affinity for the negatively charged sediment surfaces. As the pH decreases, Al speciation will favour neutral and positively charged Al species (e.g. $\text{Al}(\text{OH})_3$ and $\text{Al}(\text{OH})_2^+$) that probably have a higher adsorptive affinity for sediment surface binding sites.

4 Test Summary and Identification of SOPCs

An intent of Assignment P4 was to provide information on the lines of evidences (LoEs) relating to stressors of potential concern (SOPCs) that should be considered within the WoE assessment framework.

The waters of the Talbingo and Tantangara Reservoirs can be classified as having neutral pH (6.9-7.3), low conductivity (26-30 $\mu\text{S}/\text{cm}$), low turbidity (0.2-0.6 NTU). There was little variability between sites in each reservoir. The concentrations of some dissolved elements were higher in Tantangara Reservoir than Talbingo Reservoir. In relation to water quality GVs (ANZG, 2018), the waters contained no COPCs. Talbingo and Tantangara Reservoir sediments were characterised as being silty (mean particle size 20-20 μm range), with significant amounts of organic matter (3.7-6.4% TOC) and having no COPCs, when considering relevant SQGVs.

Rock composites that had been milled to a size $<75 \mu\text{m}$ were used for the majority of the tests. The rock composites had particle size distributions that were similar to the reservoir sediments. When wet with reservoir water the pH range was 8.5-9.6, which was significantly greater than that of the waters from the reservoir. A large portion of most elements were present in forms considered relatively inert (not easily released) and predicted to exhibit low bioavailability to organisms. The concentrations of most metals were below the corresponding SQGVs, with some exceedances. For the dilute-acid extractable metal concentrations, the SQGVs were only exceeded for lead in one composite.

Release of Substances from Excavated Rock Materials in Reservoir Water

During the period of time the placement of excavated rock occurs within the reservoirs, significant amounts of fine rock material may remain present in the waters, and the finest fractions (e.g. clay to fine silt ($<2 \mu\text{m}$ to $6.3 \mu\text{m}$)) may take many months to years settle after the placement activities cease. The release of substances from the rock materials was assessed using a series of elutriate tests that involved mixing and leaching rock with reservoir water and covered a wide range of mixing-leaching scenarios and conditions. The tests characterised differences in substance release that may occur due to differences in the concentration of solids in the water (liquid/solid ratio; L/S), time (up to 56 days), repeat/successive leaching, rock particle size, temperature, and attenuation of substances released due to interactions with sediments. Substance release was observed to be very similar for rock materials in Talbingo and Tantangara Reservoir waters.

Immediate release of substances and changes in water quality

The vast majority of the excavated rock, by mass, is expected to be larger than sand size and should settle rapidly, whereas the finest fractions of the excavated rock materials may remain suspended in the waters in the main disposal area for a considerable period of time. Consequently the bottom waters may contain very high concentration of suspended fine excavated rock material for the duration of the placement activities and beyond the date that placement is deemed complete.

The initial elutriate test was undertaken to represent a potential worst case scenario for immediate water quality impacts, with waters containing high concentrations of fine solids (100 g/L). The mixing of $<75\text{-}\mu\text{m}$ rock composites with Talbingo Reservoir water at L/S=10 (100 g/L) resulted in the pH and conductivity increasing considerably, e.g. from approximately pH 7 to 9.5 and 30 to 150 $\mu\text{S}/\text{cm}$. There were no significant increases in nitrate concentrations and small and variable increases in total-P concentrations. When mixed at liquid/solid ratios (L/S) of 10, the concentrations of As, Cr and, in particular, the dissolved Al concentration increased to levels that exceeded water quality GVs (default GV, DGVs). Al was identified as

the most significant COPC, and the waters from tests with L/S=10 would be predicted to cause toxicity to a range of aquatic organisms.

As increases in water pH, conductivity and dissolved Al were identified as the primary SOPCs concern, these were the focus of the subsequent tests. The test gathered data on other potential COPCs, but the different test conditions did not reveal any additional stressors. Increases in alkalinity due to the presence of fine rock materials within the waters (from 14 to 25 mg CaCO₃/L at L/S=500) were generally modest and considered unlikely to result in impacts to aquatic organisms. The major ions contributing to the increased conductivity were primarily K and Ca, with lesser contributions from Na and Mg.

Comparison of Talbingo and Tantangara Reservoir elutriate tests

Comparison of elutriate tests performed in Tantangara and Talbingo Reservoir waters indicated that the elutriate water pH was similar in each water for the 300-L/S tests, but lower in Tantangara Reservoir treatments for the 1000-L/S_{18-h} tests, probably due to this water having a greater ability to buffer pH increases. The conductivities were generally in a similar range for the two reservoir waters except for a few Tantangara Reservoir treatments having higher values.

The concentration of dissolved Al was in the range 23.5-216 µg/L in the Tantangara Reservoir elutriate treatments, which was in a similar range to corresponding Talbingo Reservoir treatments. Small differences were observed for corresponding treatments, with the Talbingo elutriate treatments having higher concentrations than the Tantangara treatments for the 1000-L/S_{18-h} tests, and the Tantangara elutriate treatments having higher concentrations than the Talbingo treatments for the 300-L/S_{3-h} and 300-L/S_{18-h} tests. The concentration of dissolved Al in the 1000-L/S Tantangara Reservoir water treatments was below the DGV of 55 µg/L for the 1000-L/S treatments, and exceeded the DGV for the 300-L/S treatments.

Influence of concentration of rock in waters

The concentrations of fine solids in the reservoir waters will be influenced by the properties of the rock (e.g. density, particle size) and the water conditions and the placement procedure. The concentrations of rock materials are anticipated to be greater in deeper waters and should decrease with increasing distance from the placement site as fine particles disperse and become diluted with reservoir water (L/S lower in deeper waters and closer to the placement area).

The <75-µm rock composites were mixed with Talbingo Reservoir water at L/S= 30, 300, 1000, 3000 [33, 3.3, 1 and 0.33 g/L] and monitored for 5 days. The water pH and conductivity increased significantly with increasing amount of fine solids (lower L/S), and generally pH >9 when L/S ≥300 and conductivity >60 µS/cm when L/S ≥1000. The DGV for dissolved Al (DGV-dAl) was exceeded at L/S ≤1000 (≥1 g/L solids, 1 part per thousand) after durations of 18 h, and were exceeded within 0.5 h at a L/S=30. Dissolved concentrations of other metals or metalloids (including As and Cr) should not exceed DGVs when reservoir waters contain <33 g/L fine rock (L/S>30). The total-P concentrations were <10 µg/L when the reservoir waters contained <3.3 g/L fine rock materials.

Influence of water-rock mixing duration

The duration the rock solids will remain suspended in the water column before depositing as sediments will be influenced by the properties of the rock (e.g. density, particle size) and the water conditions (movement) and the placement procedure. Some portion of the fine rock particles may potentially disperse beyond the target placement area and the release of substances from the solids may continue during this process.

Measurements of changes in water quality made over 5 days mixing of the <75-µm rock composites and Talbingo Reservoir water indicated that increased dissolution of rock solids occurs with increased mixing duration. Increases in dissolved Al were consistent with the higher pH (9.1-9.7 range) acting to increase dissolution through formation of the highly soluble aluminate ion, Al(OH)₄⁻.

Over longer durations (56 days) of suspension of <75- μ m rock composites in Talbingo Reservoir water the pH decreased to a plateau within the range of pH 7.7-8.2, while the conductivity continued to increase (400-600 μ S/cm range). Dissolved Al concentrations generally increased during the first 1-2 weeks then decreased, and indicated potential removal of dissolved Al due to changes in speciation, decreased solubility with decreasing pH, and/or increased adsorption. At the warmer water temperature of 21 °C, the Al DGV was exceeded by a factor of 2-5 for the entire 56 day duration for both rock composites at L/S=300, and by a factor of 1-3 for the entire 56 d duration at L/S=1000, except the initial 18 h duration for 1B. At 6 °C, the dissolved Al marginally exceeded the DGV in the mid-duration subsamples of each treatment except the 1000 L/S, 1B treatment, where the DGV was never exceeded. Total-P concentrations remained below the DGV of 10 μ g/L over the 56 day period.

Effect of rock particle size in on substance release

The size of the excavated rock material is expected to range from boulder to clay size. The vast majority of the excavated rock, by mass, will be larger than sand size and should settle rapidly. Rock materials with a smaller particle size are expected to represent the greatest environmental risk with respect to transport and release of substances. The release of substances was characterised for excavated rock materials of seven size categories ranging from 1-2.5 cm to <0.00063 cm (<63 μ m) diameter. Key observations were that substance release is low, trends towards negligible, for rock materials >2 mm. Based on dissolved Al concentrations, the finer <0.21 mm rock fraction is likely to have an impact on water quality that is an order of magnitude greater than that of rock fractions >2 mm in size. For the <210 μ m rock sizes, pH, conductivity and dissolved Al concentrations decrease as size categories increased <63 to <63-150 to 150-210 μ m. Dissolved As and/or Cr concentrations frequently exceeded the DGVs in tests with L/S = 25 (40 g/L)

Effect of water temperature on substance release

Substance release from solids to waters is usually greater at higher temperatures, and warmer water conditions of 21°C were used in most tests to provide a worst-case scenario for substance release. The temperature of the reservoirs varies between approximately 6 and 21°C, with significant changes over depth and season. Test revealed that the release of Al occurs significantly more slowly in the 6°C treatments than the 21°C treatments, resulting in fewer elutriate waters having dissolved Al concentrations that exceed the DGV.

Effect of repeat leaching on substance release

Greater release of substances may occur from the fine rock materials if they remain in the water column within the placement area or as they disperse away from the placement area. To assist in predictions of long-term leaching, a series of repeat/successive leach tests were performed on the same rock materials. The successive leaches indicated that the Al available for release into solution was not quickly exhausted. Many treatments had similar or increased Al concentrations in the second and third successive leaches. The results suggest a dissolution process is responsible for the release of Al, which is dependent on the duration of contact with water and the temperature. Longer durations of physical mixing also generally increased the release of dissolved Al.

Release of dissolved or colloidal forms of Al

A significant portion of Al is often found to exist in colloidal forms in natural waters, and these forms are often predicted to be less bioavailable than truly dissolved forms. It is well recognised that the filtration of waters through a 0.45 μ m filter (i.e. the standard filter size) does not completely separate dissolved and colloidal forms of metals. Filtration through 0.45 μ m (dissolved and colloidal substances) and 0.003 μ m (truly dissolved) membranes was used to distinguish dissolved and colloidal substances. For the <75 μ m composite rock elutriate waters, the concentration of dissolved Al measured in subsamples filtered through the two filter sizes was similar, indicating that the <0.45 μ m filterable water fraction contains

predominantly dissolved ($<0.003\ \mu\text{m}$), rather than colloidal forms of Al. This is consistent with the dominant Al species (ion) being the aluminate ion ($\text{Al}(\text{OH})_4^-$).

Effect of resuspended sediment in attenuation of substances released from rock materials

Benthic sediments may be resuspended during and following the placement of excavated rock materials in the reservoirs. Tests were undertaken to characterise how sediment resuspension may influence dissolved Al concentrations released from rock materials. The pH and conductivity of the elutriate waters decreased with increasing amounts of resuspended sediment. Dissolved Al concentrations decreased in tests with 2 g/L resuspended sediments. At 20 g/L sediment loads the pH decreased to 6.5 and Al concentrations varied greatly between sediments, with several treatments increasing 50-100 $\mu\text{g/L}$ compared to treatments with no sediment. Contributions of colloidal Al forms from the sediment were considered the likely cause of the increased Al concentrations at this pH. When sediments were deposited there was less Al released, indicating that the mixing of sediments increases the release of Al. The dissolved Al also decreased over time in the attenuation test using deposited sediment. In the attenuation test with low (1, 5, 25 mg/L TSS) of resuspended sediment concentrations, there was little attenuation. The water pH is likely to influence the magnitude of attenuation, with water pH 6-8 facilitating greater attenuation via adsorption of Al to sediment binding sites than water with a higher $\text{pH}>8$. The overall finding of the attenuation tests was that sediments may both release substances and adsorb substances that have been released from the rock materials, with the resuspended sediment concentration and duration of resuspension influencing whether they will act as a sink or a source.

Substance Release resulting in Contaminants of Potential Concern

Based on the collective elutriate test results (broad range of conditions-scenarios), the following observations are made with regards to substance release from the excavated rock materials that may result in potentially adverse changes to water quality and/or COPCs being present in the reservoir waters:

- Increases in water pH and conductivity are expected due to rapid release of ions that occur via ion exchange reactions.
 - Water pH was generally $\text{pH}>9$ when $\text{L/S} \geq 300$ (3.3 g fine solids/L)
 - Conductivity was generally $>60\ \mu\text{S/cm}$ when $\text{L/S} \geq 1000$ (1 g fine solids/L).
 - Over a duration of multiple days/weeks the water pH may decrease back to close to that of the original reservoir water as equilibration reactions proceed.
- Al is the only substance consistently identified as a COPC.
 - Sustained release of Al may occur from excavated rock dissolution processes.
 - The rate of Al release may result in dissolved Al concentrations that exceed the default water quality guideline value of 55 $\mu\text{g/L}$ (DGV-dAl).
 - Al release is predicted to be negligible for rock materials $>2\ \text{mm}$ in size, and the rate of Al release may increase proportionally with decreasing particle size $<210\ \mu\text{m}$ (equivalent mass of rock).
 - Al release is markedly lower in waters with temperature of 6°C than at 21°C . The DGV-dAl should not be exceeded when waters at 6°C contain less than 1 g/L of fine excavated rock materials ($<0.21\ \text{mm}$ particle size)
- When predicting the risks posed by dissolved Al released from the excavated rock materials, particular consideration should be given to the concentration of rock materials that are $<210\ \mu\text{m}$ in size, duration within the water column, and water temperature.

- The resuspension of sediments is expected to cause the pH to drop, and potentially result in an increase in the concentration of colloidal Al, through release from the sediments and precipitation and/or adsorption of dissolved Al that had been released from waste rock materials.
- Other potential COPCs
 - Dissolved As and/or Cr concentrations frequently exceeded the DGVs of 13 µg As(V)/L and 1.0 µg/L Cr(VI)/L in elutriates of some rock materials tested with L/S ≤30 (≥33 g/L), including those with larger rock fractions over longer durations.
 - Total-P and nitrate concentrations should not be released at such high rates that they adversely impact water quality. However we cannot discard possible scenarios where concentrations of these substances reach elevated levels if waste rock placement creates regions of shallow waters that do not adequately mix with the greater reservoir.

Overall, Assignment P4 has identified changes in water pH, conductivity and dissolved Al as the primary SOPCs, and that adverse impacts from these SOPCs are predicted when the water contains greater concentrations of the fine excavated rock materials for long durations.

5 Discussion

The tests described in this report were undertaken to provide information to assist in assessing the potential impacts of the placement of excavated rock materials on water and sediment quality within the reservoirs.

The DGV for Al (55 µg/L, applied to water pH >6.5) is classified as moderate reliability (ANZG, 2018). The USEPA uses chronic criterion of 87 µg/L, that is based on no-effect concentrations from a 60-d brook trout study and a 7-d striped bass study (USEPA, 1988). The risk of adverse effects to aquatic organisms from elevated dissolved Al concentrations is influenced by its bioavailability, as well as the exposure paths and sensitivity of the organisms (Gensemer and Playle, 1999). The bioavailability of Al is influenced by its speciation, forms of Al that change with pH, complexation with natural organic matter, and also by concentrations of competing ions (e.g. Ca²⁺, Mg²⁺ - hardness) (Gensemer et al., 2018; Campbell, 1994; Paquin et al., 2002). Based on a review of Al toxicity for freshwater organisms and accompanying data relating to speciation/bioavailability by DeForest et al. (2018), there may be data available that is suitable for developing a site-specific guideline value for dissolved Al that is more appropriate for the assessment of risks of toxicity within the reservoir waters.

There is no DGV for conductivity, however an increasing number of studies indicate that even relatively small increases in water conductivity may impact some freshwater aquatic organisms (Cormier et al., 2011; Cormier et al., 2018; Kefford, 2018). The species present in many freshwater environments may exhibit a wide range of sensitivities to conductivity, and the literature generally indicates that waters with conductivities greater than 300 µS/cm frequently cause adverse effects to a significant number of species, and particularly mayflies.

One of the challenges of using data from the laboratory tests is that the particle size distribution may differ between the laboratory and field. Milled rock materials were used in most tests in this laboratory study, and approximately 50% of the rock particles had size <20 µm (medium silt) and little less than 10% being <2 µm (clay). Excavated rock disposed into reservoirs in the field may have substantially different size distribution. The results from the current study indicate the material with size of medium silt or smaller (<210 µm size fraction in the present study) will be the most important, with the smaller size fractions predicted to release greater amounts of substances into the water (in proportion to mass of the size fraction). The rock fractions ranging in size from fine silt (2-6.3 µm) and clay (<2 µm) may remain entrained in the reservoir waters for months to years, while larger sized material will settle to form sediment more quickly (e.g. minutes to days). Consideration of the proportion of fine silt and clay in the excavated rock relative to the milled rock used in the tests may be important when extrapolating the results from this study to predict substance release from the rock material entrained in reservoir waters during disposal operations. No tests were undertaken on milled rock separated into fractions smaller than <63 µm (coarse silt).

Another difficulty in making predictions of substance release in the field using laboratory test data is that turbidity plumes of disposed rock material fines will comprise a continuous spectrum of material from freshly added to that suspended for days to weeks. Substances released from materials will undergo dilution by reservoir water. Results from this study indicate dissolution will continue over time, so the concentrations of dissolved substances in water such as Al will be controlled by competing processes of dissolution and dilution. Another factor to consider is the pH and how it effects substances release i.e. greater release of Al for higher pH. The pH increases were driven by ion exchange reactions that occurred rapidly. If the disposal results in great enough concentrations of freshly added fine material being

resuspended, the pH may remain as high, or potentially higher, than values measured in this study, which could result in higher concentrations of Al being released from rock material than measured in this study.

Laboratory-based testing programs can be used to simulate processes that may be expected to occur in the field, but cannot match field conditions. Consequently, validation of the observations from this testing program using field tests and measurements is recommended, particularly should the opportunity for a field trial of rock placement occur. Based on the results of this study, we would expect field monitoring to include continuous monitoring of general water quality parameters such as pH, conductivity, temperature and turbidity, and in situ monitoring of dissolved Al to provide time-average concentrations that can be better compared to water quality guidelines when assessing risks.

The technique used for the placement of the excavated rock materials is expected to strongly influence the extent of the potential impacts. The placement scenario considered in the conceptual site model (CSM) (Appendix A), placement of excavated rock material was envisaged to occur into relative deep waters within the reservoirs (e.g. >10 m), possible via dumping from hopper barges that results in rock material dropping through the water column with the intent of depositing below within a specific placement area and remaining at depth (<3 m). During the period of the project, discussions with HKA/SHL (phone conversation with Greg Britton, and during meetings at CSIRO) considered possible changes to the CSM. Based on early results, the possible benefits of using a fall-pipe to release the materials not far above the sediments were discussed. The possible benefits would include minimising surface and subsurface plumes of fine materials within the upper waters than may be more difficult to contain within the target placement area, and also the lower temperatures of the deeper waters reducing dissolved Al release from fine solids.

Later in the project, the possibility was raised of shoreline disposal that created areas that may become beaches, or inter-shoreline zones that may cycle from being above and below the water shoreline as the water intake and outflow processes occur for the Snowy Hydro-electric operation. This scenario was not part of the CSM used in the design tests used in Assignment P4, and tests were not undertaken to assess substance release from the excavated rock materials for this scenario. For inter-shoreline zones of excavated rock material, the assessment would benefit from testing the effect of 'inundation and draining, and 'wetting and drying', that were not evaluated in Assignment P4. Shoreline environments may be occupied by a great range of benthic and aquatic species (fauna and flora), including microalgae that may be stimulated if nutrient releases occur in shallow waters that are not diluted within the broader reservoir environment. The sequential leaching of rock materials within shallow near-shore water environments may also occur with waters that may have already been impacted by previous water-rock interactions, and potentially resulting in successively larger changes in water quality (e.g. higher pH, conductivity and dissolved Al concentrations and possibly other COPCs such as As) than were simulated in the present project (CSM based on placement in deeper waters with dilution and successive leaching with fresh reservoir water).

During the reporting stage of the project, other shoreline placement scenarios were raised in discussions (primarily internal to CSIRO), and included a scenario where placement of excavated rock may be proposed to occur via side-casting from the reservoir bank, and building outwards either new landforms (higher land, beaches or structures extending into the reservoirs such as breakwalls closer to the Snowy 2.0 outfall). Assignment P4 did not undertake tests to evaluate longer-term substance release for side-casting placement scenarios.

Owing to the short timeframe of Assignment P4, a range of possible longer-term tests were not undertaken. Owing to the size of Snowy 2.0, it is envisaged that the excavated rock placement activities may need to occur over a period of several months to years. Assignment P4 primarily assessed placement of rock in new reservoir water, and the concentrations of substances in waters may become significantly higher if the waters in which placement occurs already contain elevated concentrations of fine rock materials and are already impacted by previous cycles of rock placement that have resulted in elevated pH,

conductivity and COPCs. The finest fractions of the excavated rock material (e.g. clay to fine silt size) may remain in the water column for months to years. Assignment P4 did not undertake tests to assess such long-term substance release and impacts to water quality.

5.1 Recommendations

The tests undertaken identified changes in water pH, conductivity and dissolved Al as the primary SOPCs, and that adverse impacts from these SOPCs are predicted in reservoir waters containing higher concentrations of the fine excavated rock materials for prolonged durations. The technique used for the placement of the excavated rock materials is expected to strongly influence the concentrations of fine rock materials within the water column and the extent of substance release. Based on the result of Assignment P4 (Summarised in Section 4) and Discussion (Section 5), recommendations are provided below to fill knowledge gaps that have been identified during the course of this project.

Subject to confirmation of the disposal method and particle size distribution of the excavated rock, the following testing is recommended to fill knowledge gaps:

1. Testing of the longer-term release of substances from the clay to fine silt sized (<2 µm to 6.3 µm) excavated rock materials that are predicted to remain suspended within the reservoir water for periods of many months;
2. Testing of the effects of cycling water exposure to excavated rock materials, representing inundation/draining, and wetting/drying that may occur at shorelines;
3. Testing of longer term effects of water pH on attenuation of dissolved Al release, including potential cycling from dissolved and precipitated forms if pH cycles up and down, and
4. Field trials of rock placement scenarios that may be used, potentially including:
 - placement within deeper waters using a form of fall pipe (expected to minimize duration of high concentrations of fine rock in water column);
 - placement into surface water to deposit through the water column (potentially resulting in elevated concentrations of fine rock in surface waters, and subsurface plumes dispersing);
 - placement from shoreline (fine rock dispersion dependent on method, but subject to surface water cycling processes).

As noted in the discussion, field monitoring should include continuous monitoring of general water quality parameters such as pH, conductivity, temperature and turbidity, and in situ monitoring of dissolved Al to provide time-average concentrations that can be better compared to water quality guidelines when assessing risks.

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Glossary

Alkaline: Description of a substance with a pH greater than 7 when dissolved in or mixed with water.

Anaerobic: Lacking in oxygen.

Anoxic: An environment where oxygen is intrinsically rare or absent.

ANZECC/ARMCANZ: Australian and New Zealand Environment and Conservation Council/Agriculture and Resource Management Council of Australia and New Zealand.

Aquatic environment: The geochemical environment in which dredged material is submerged under water and remains water saturated after disposal is completed.

Aqueous: Composed of or pertaining to water.

Attenuation: A reduction in concentration of a contaminant with increasing distance from the source. Attenuation is specifically used in this document to describe reductions in leachate concentrations as a result of mixing with groundwater, adsorption of contaminants in foundation soils, degradation, volatilisation, and precipitation.

Background: Environmental conditions that commonly occur, or concentration of a substance (ASS or contaminant) that is commonly found, in the local concentration environment at the site being considered.

Buffering capacity: The ability of a mixture or solution to resist pH change – in an ASS context, this may refer to surface or groundwaters, or to the soil solution, or to the soil itself.

COC: Contaminant of concern.

Constituent of potential concern (COPC): A chemical species of interest, which may or may not be regulated, but may be characteristic of release-controlling properties of the sample geochemistry.

Contaminants: Biological or chemical substances or entities, not normally present in a system, capable of producing an adverse effect in a biological system, seriously injuring structure or function

Contaminated: A material (e.g. water or solid) containing chemical substances at concentrations above background concentrations and above the guideline values.

Control: Part of an experimental procedure that is ideally exactly like the treated part except that it is not subject to the test conditions. It is used as a standard of comparison, to check that the outcome of the experiment is a reflection of the test conditions and not of some unknown general factor.

COPC: Contaminant of potential concern.

Detection limit: Method detection limit is the concentration of a substance which, when processed through the complete analytical method, produces a signal that has a 99% probability of being different from the blank.

DGV: Default guideline value; usually the 95% species protection guideline value.

Diffusion: The transport of contaminants by random molecular motion and turbulence, usually from an area of high concentration to an area of low concentration.

Dissolution: In chemistry, the process by which a solid material forms a homogenous mixture with a solvent.

Dissolved solids: The weight of matter, including both organic and inorganic matter, in solution in a stated volume of water. The amount of dissolved solids is usually determined by filtering water through a glass or 0.45 µm pore-diameter micrometer filter, weighing the filtrate residue remaining after the evaporation of the water, and drying the salts to constant weight at 180°C.

DO: Dissolved oxygen.

DOC: Dissolved organic carbon.

Dry-mass equivalent: The mass of “as-tested” (i.e., “wet”) sample that equates to the mass of dry solids plus associated moisture, based on the moisture content of the “as- tested” material. The dry-mass equivalent is typically expressed in mass units of the “as-tested” sample (g).

Effluent: A material, usually a liquid waste, that is emitted by a source.

Eh: Redox potential.

Eluate: The solution collected as an extract from a leaching test that contains the eluent plus constituents leached from the solid phase².

Eluent: The solution used to contact the solid material in a leaching test. The eluent is usually free of COPCs but may contain other species used to control the test conditions of the extraction.

Guideline framework: Narrative statement to support and maintain a designated water use.

Guideline value: Numerical concentration used to assist in identifying risks of adverse effects of water use.

Hydrolysis: The process of splitting the water molecule into separate components of hydrogen ions (H⁺) and hydroxide ions (OH⁻) that often react with other constituents present.

Impact: Environmental change (usually biological) that has occurred as a result of dredging activity. The extent of the change may be considered unacceptable and may require some intervention by regulatory authorities.

Leachate: Water or any other liquid that may contain dissolved (leached) soluble materials, such as organic salts and mineral salts, derived from a solid material.

Level of protection: The acceptable level of change from a defined reference condition.

Liquid-solid partitioning (LSP): The distribution of COPCs between the solid and liquid phases at the conclusion of the extraction.

Liquid-to-solid ratio (L/S): The fraction of the total liquid volume (including the moisture contained in the “as used” solid sample) to the dry mass equivalent of the solid material. L/S is typically expressed in volume units of liquid per dry mass of solid material (mL/g-dry).

Measurement parameter: Any parameter or variable that is measured to find something out about an environment or ecosystem.

Organism: Any living animal or plant; anything capable of carrying on life processes.

Overlying water: The water above the sediment at a collection site or in a test chamber.

pH: The intensity of the acidic or basic character of a solution, defined as the negative logarithm of the hydrogen ion concentration of a solution. Used as a measure of the acidity or alkalinity of a soil or water body on a logarithmic scale of 0 to 14; a pH <7 is acid, pH 7 is neutral, and pH >7 is alkaline. Note that one unit change in pH is a ten-fold change in acidity.

Phase: Distinct state of matter (solid, liquid or gas) which in aquatic systems comprises sediment, water and air.

Pore water: The water that occupies the space between and surrounding individual sediment particles in an aquatic sediment (often called interstitial water).

QA/QC: Quality assurance/quality control.

Quality assurance (QA): The implementation of checks on the success of quality control (e.g. replicate samples, analysis of samples of known concentration).

Quality control (QC): The implementation of procedures to maximise the integrity of monitoring data (e.g. cleaning procedures, contamination avoidance, sample preservation methods).

Redox potential: A measure of the oxidation–reduction potential (ORP) of sediments. The redox potential is often reported as Eh (versus the normal hydrogen electrode).

Redox: Simultaneous (chemical) reduction and oxidation; reduction is the transfer of electrons to an atom or molecule, whereas oxidation is the removal of electrons from an atom or molecule.

Release: The dissolution or partitioning of a constituent of potential concern (COPC) from the solid phase to the aqueous phase during laboratory testing (or under field conditions). In this method, mass release is expressed in units of mg COPC/kg dry solid material.

Risk: A statistical concept defined as the expected frequency or probability of undesirable effects resulting from a specified exposure to known or potential environmental concentrations of a material, organism or condition. A material is considered safe if the risks associated with its exposure are judged to be acceptable. Estimates of risk may be expressed in absolute or relative terms. Absolute risk is the excess risk due to exposure. Relative risk is the ratio of the risk in the exposed population to the risk in the unexposed population.

Salinity: The presence of soluble salts in water or soils.

Soil and sediment: The natural accumulation of unconsolidated mineral particles (derived from weathered rocks) and organic matter that covers much of the earth's surface. The chemical and physical composition varies greatly between soil and sediment types.

Solubility: In chemistry, how easily a substance will dissolve into a homogeneous solution, and also how much of a substance can dissolve into a solvent before saturation is reached. Solubility in water is the most common measurement, and the most relevant to ASS management.

Speciation: Measurement of different chemical forms or species of an element in a solution or solid.

Species: Generally regarded as a group of organisms that resemble each other to a greater degree than members of other groups and that form a reproductively isolated group that will not normally breed with members of another group. (Chemical species are differing compounds of an element.).

Stressors: The physical, chemical or biological factors that can cause an adverse effect on an aquatic ecosystem as measured by the condition indicators.

TOC: Total organic carbon.

Toxicant: A chemical capable of producing an adverse response (effect) in a biological system, seriously injuring structure or function or producing death. Examples include pesticides, heavy metals and biotoxins.

Toxicity: The inherent potential or capacity of a material to cause adverse effects in a living organism.

WQGV: Water quality guideline value. Includes the DVG = default guideline value, representing the 95% species protection guideline values (95%GV). 99% species protection guideline values (99%GV).

Appendix A - Conceptual models [4 pages]

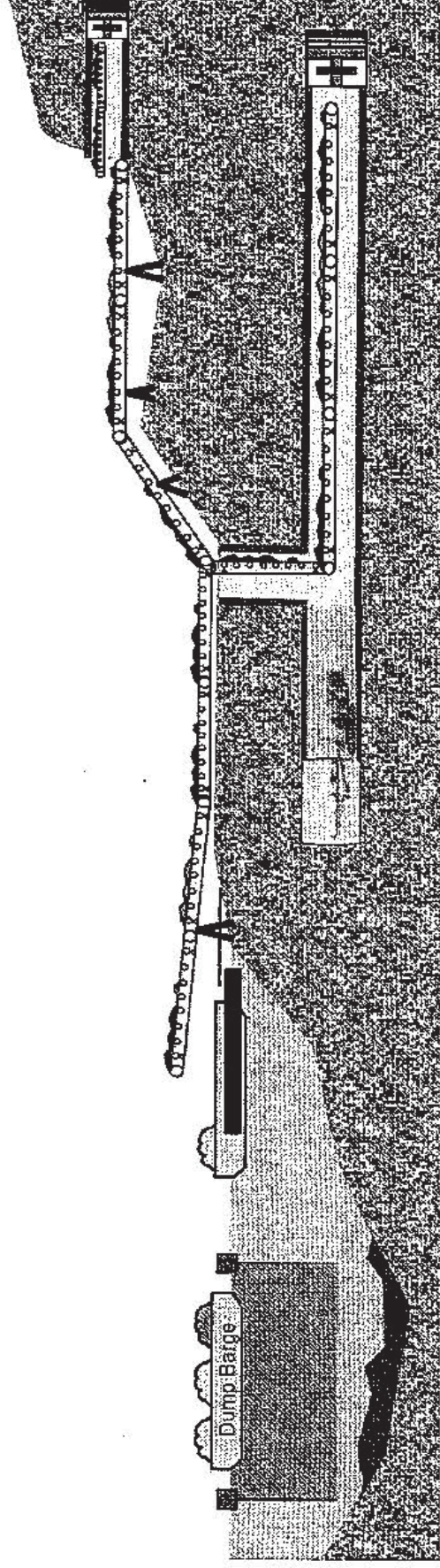


Figure A1. Depiction of excavated rock placement by hopper barge (provided by EMM in early discussions (December 2017))

Table A1. Outline of pressure-stressor-receptor pathways and connections (EMM and CSIRO in December 2017)

| Pathway | Natural | Extreme natural events | Spoil discharge (acute) | Spoil discharge (chronic) |
|---|---------|------------------------|-------------------------|---------------------------|
| Physical paths | | | | |
| Lake water movement - general | Yes | Yes | Yes | Yes |
| Lake water movement - vertical mixing | Yes | Yes | Yes | Yes |
| Lake water movement - storm mixing | ? | ? | ? | ? |
| Rainfall | Yes | Yes | Yes | Yes |
| Evaporation | Yes | Yes | Yes | Yes |
| Stream flow - water | Yes | Yes | Yes | Yes |
| Stream flow - sediments | Yes | Yes | Yes | Yes |
| Snowy Hydro - water release to lake | Yes | Yes | Yes | Yes |
| Snowy Hydro - water take | Yes | Yes | Yes | Yes |
| Dam underflow | Yes | Yes | Yes | Yes |
| Dam spillway | No | Yes | ? | ? |
| Release of spoil water | No | No | Yes | No |
| Particle settling of natural particles | Yes | Yes | Yes | Yes |
| Particle settling of suspended/resuspended spoil | No | No | Yes | Yes |
| Particle settling - initial spoil deposition | No | No | Yes | No |
| Particle resuspension due to water movement | ? | ? | ? | ? |
| Sediment resuspension due to spoil addition | No | ? | Yes | Yes |
| Surface plume formation | ? | ? | ? | ? |
| Sub-surface plume formation | ? | ? | ? | ? |
| Water 'ejected' during spoil consolidation | No | No | Yes | No |
| Smothering of benthos | No | ? | ? | No |
| Bioturbation | Yes | - | - | ? |
| Slumping | ? | ? | ? | ? |
| Chemical paths | | | | |
| Adsorption of contaminants in lake water onto suspended particles | Yes | Yes | Yes | Yes |
| Desorption of contaminants from suspended particles | Yes | Yes | Yes | Yes |
| Adsorption of contaminants from lake water onto spoil particles | No | No | Yes | Yes |
| Desorption of contaminants from spoil particles | No | No | Yes | Yes |
| Diffusion of contaminants from pore water to water column | Yes | Yes | Yes | Yes |
| Adsorption of contaminants in pore water onto natural sediment particles | Yes | Yes | Yes | Yes |
| Desorption of contaminants from natural sediment particles to pore water | Yes | Yes | Yes | Yes |
| Adsorption of contaminants in pore water onto spoil particles | No | No | Yes | Yes |
| Desorption of contaminants from spoil particles to pore water | No | No | Yes | Yes |
| Redox mediated chemical pathways (oxic, sub-oxic and anoxic conditions - spoil and sediments) | No | ? | Yes | Yes |
| Biological paths | | | | |
| Ingestion of suspended particulates | Yes | Yes | Yes | Yes |
| Ingestion of sediment particles on lake bed | Yes | Yes | Yes | Yes |
| Uptake of dissolved contaminants in water column | Yes | Yes | Yes | Yes |
| Uptake of dissolved contaminants in pore water | Yes | Yes | Yes | Yes |
| Ingestion of nekton | Yes | Yes | Yes | Yes |
| Ingestion of benthos | Yes | Yes | Yes | Yes |
| Human ingestion of fish | Yes | Yes | Yes | Yes |
| Human recreational contact | Yes | Yes | Yes | Yes |

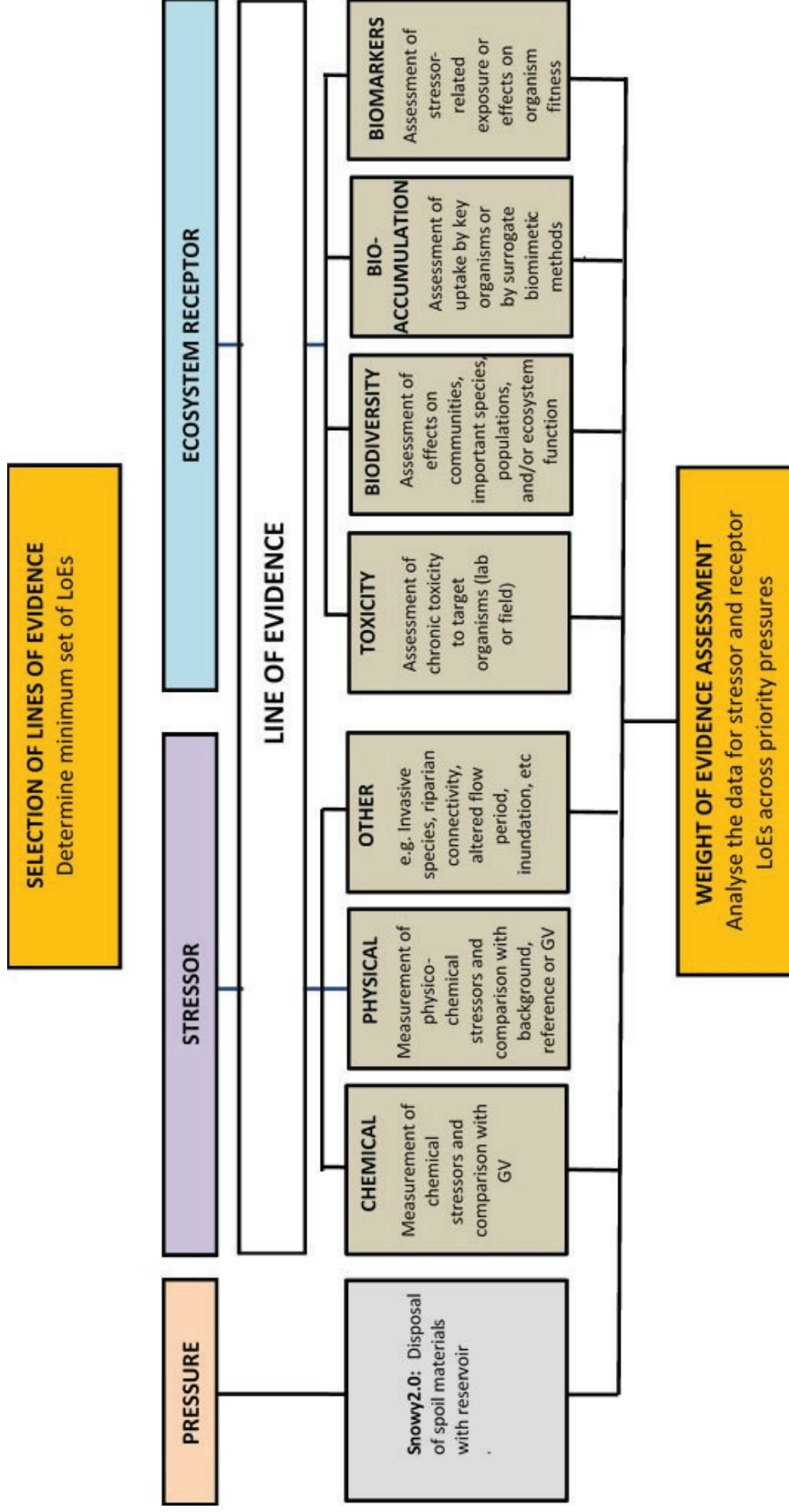


Figure A3. Selection of Lines of Evidence (LoE) in a pressure, stressor, ecosystem receptor within Weight of Evidence (WoE) Assessment framework

Appendix B - Test samples [14 pages]

- Water, Rock and Sediment Materials used in the study.

Table B1. Excavated rock materials - Ravine

| Ravine – Baseline | | | | | | |
|-------------------|-----------|--------|---------------------------------|------------------------------------|------------------|-------------------------------|
| Sample_ID | Depth (m) | | Lithology | Major Geology (Surface)/ Zone | Placement Option | Classification |
| | Top | Bottom | | | | |
| BH6105-R-0063 | 160.57 | 161.00 | Siltstone with a sandstone band | Yarrangobilly Limestone/Palaeozoic | Talbingo | Tunnel/surge shaft/powerhouse |
| BH4105-R-0362 | 200.7 | 201 | Phyllite | Ravine bed | Talbingo | Tunnel/surge shaft/powerhouse |
| BH6105-R-0061 | 177.00 | 177.26 | Siltstone with a chert band | Yarrangobilly Limestone/Palaeozoic | Talbingo | Tunnel/surge shaft/powerhouse |
| BH4105-R-0356 | 18.1 | 18.5 | Siltstone | Ravine bed | Talbingo | Tunnel/surge shaft/powerhouse |
| BH4104-R-0291 | 376.61 | 377 | Siltstone | Yarrangobilly Limestone/Palaeozoic | Talbingo | Tunnel/surge shaft/powerhouse |
| BH4105-R-0363 | 225.7 | 226 | Interbedded phyllite/schist | Ravine bed | Talbingo | Tunnel/surge shaft/powerhouse |
| BH7105-R-0036 | 49.00 | 49.30 | Siltstone | Yarrangobilly Limestone/Palaeozoic | Talbingo | Tunnel/surge shaft/powerhouse |
| BH6105-R-0060 | 147.00 | 147.33 | Siltstone | Yarrangobilly Limestone/Palaeozoic | Talbingo | Tunnel/surge shaft/powerhouse |
| Ravine – Enriched | | | | | | |
| BH6102-R-0045 | 162.00 | 162.15 | Interbedded siltstone/sandstone | Yarrangobilly Limestone/Palaeozoic | Talbingo | Tunnel/surge shaft/powerhouse |
| BH7105-R-0039 | 15.00 | 15.30 | Siltstone | Yarrangobilly Limestone/Palaeozoic | Talbingo | Tunnel/surge shaft/powerhouse |
| BH7105-R-0396 | 23 | 23.25 | Siltstone | Ravine bed | Talbingo | Tunnel/surge shaft/powerhouse |
| BH4104-R-0294 | 871.56 | 871.82 | Siltstone | Yarrangobilly Limestone/Palaeozoic | Talbingo | Tunnel/surge shaft/powerhouse |
| BH4105-R-0371 | 445.7 | 446 | Interbedded phyllite/gneiss | Ravine bed | Talbingo | Tunnel/surge shaft/powerhouse |
| BH6101-R-0226 | 161 | 161.3 | Sandstone/Siltstone | Yarrangobilly Limestone/Palaeozoic | Talbingo | Tunnel/surge shaft/powerhouse |
| BH7105-R-0038 | 25.60 | 26.00 | Conglomerate | Yarrangobilly Limestone/Palaeozoic | Talbingo | Tunnel/surge shaft/powerhouse |

Table B2. Excavated rock - Byron/Boraig and Shaw Hill Gabbro

| Sample_ID | Depth (m) | | Lithology | Major Geology (Surface)/ Zone | Placement Option | Classification |
|-----------------------------|-----------|--------|---------------------------------|---|------------------|---------------------------|
| | Top | Bottom | | | | |
| Byron/Boraig – Baseline | | | | | | |
| BH5104-R-0122 | 472 | 472.3 | Sandstone | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Top of surge shaft |
| BH5104-R-0133 | 727.63 | 727.83 | Sandstone | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Top of surge shaft |
| BH5101-R-0055 | 283.73 | 283.87 | Siltstone | Yarrangobilly Limestone/Palaeozoic | Talbingo | Top of surge shaft |
| BH5104-R-0116 | 282.53 | 282.8 | Felsic ignimbrite | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Top of surge shaft |
| BH5105-R-0143 | 36 | 36 | Sandstone | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Top of surge shaft |
| BH5104-R-0120 | 409 | 409.3 | Conglomerate/sandstone | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Top of surge shaft |
| BH5104-R-0108 | 119.4 | 119.75 | Mudstone | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Top of surge shaft |
| Byron/Boraig - Enriched | | | | | | |
| BH5104-R-0138 | 822.7 | 823 | Siltstone | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Top of surge shaft |
| BH5104-R-0114 | 239.15 | 239.4 | Sandstone | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Top of surge shaft |
| BH5104-R-0109 | 131.1 | 131.35 | Mudstone | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Top of surge shaft |
| BH5104-R-0113 | 227.4 | 227.67 | Conglomerate | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Top of surge shaft |
| BH8106-R-0406 | 640.7 | 641 | Interbedded sandstone/siltstone | Byron range group/ravine bed | Talbingo | Top of surge shaft |
| BH5104-R-0110 | 142.17 | 142.43 | Conglomerate | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Top of surge shaft |
| BH5115-R-0388 | 261.35 | 261.6 | | Byron range group/boraig group/ravine bed | Talbingo | Top of surge shaft |
| Shaw Hill Gabbro - Baseline | | | | | | |
| Sample_ID | Top | Bottom | Lithology | Major Geology (Surface)/ Zone | Placement Option | Classification |
| BH4106-R-0270 | 96.75 | 97 | Schist | Shaw Hill Gabbro | Talbingo | Tunnel alignment/headrace |
| BH4106-R-0271 | 124.75 | 125 | Schist | Shaw Hill Gabbro | Talbingo | Tunnel alignment/headrace |
| BH4106-R-0272 | 162 | 162.2 | Schist | Shaw Hill Gabbro | Talbingo | Tunnel alignment/headrace |
| BH4106-R-0281 | 76.71 | 77 | Schist | Shaw Hill Gabbro | Talbingo | Tunnel alignment/headrace |
| Shaw Hill Gabbro - Enriched | | | | | | |
| BH4106-R-0273 | 198.1 | 198.4 | Diorite | Shaw Hill Gabbro | Talbingo | Tunnel alignment/headrace |
| BH4106-R-0274 | 230.37 | 230.78 | Diorite | Shaw Hill Gabbro | Talbingo | Tunnel alignment/headrace |
| BH4106-R-0276 | 312.42 | 312.72 | Diorite | Shaw Hill Gabbro | Talbingo | Tunnel alignment/headrace |
| BH4106-R-0278 | 383.15 | 383.5 | Diorite | Shaw Hill Gabbro | Talbingo | Tunnel alignment/headrace |

Table B3. Excavated rock - Gooandra Volcanics

| Sample_ID | Depth (m) | | Lithology | Major Geology (Surface)/ Zone | Placement Option | Classification |
|-------------------------------|-----------|--------|---|-------------------------------|------------------|---------------------------|
| | Top | Bottom | | | | |
| Gooandra Volcanics - Baseline | | | | | | |
| BH4103-R-0001 | 360.30 | 360.60 | Greenschist | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |
| BH4103-R-0003 | 76.40 | 76.60 | Schist | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |
| BH4103-R-0011 | 325.00 | 325.40 | Metasiltstone | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |
| BH4103-R-0012 | 246.16 | 246.56 | Metasiltstone | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |
| BH4103-R-0014 | 173.62 | 173.90 | Greenschist | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |
| BH4103-R-0018 | 155.20 | 155.47 | Greenschist | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |
| BH4103-R-0019 | 318.15 | 318.47 | Metasiltstone | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |
| BH4102-R-0312 | 472.25 | 472.55 | Schist | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |
| Gooandra Volcanics - Enriched | | | | | | |
| BH4103-R-0008 | 383.72 | 384.00 | Greenschist | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |
| BH3110-R-0409 | 115.7 | 116 | Metasandstone | Gooandra volcanics | Talbingo | Tunnel alignment/headrace |
| BH4103-R-0026 | 117.65 | 117.93 | Greenschist | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |
| BH3110-R-0413 | 215 | 215.27 | Metasandstone | Gooandra volcanics | Talbingo | Tunnel alignment/headrace |
| BH3110-R-0407 | 64.7 | 65 | Interlaminated metasiltstone/metasandstone | Gooandra volcanics | Talbingo | Tunnel alignment/headrace |
| BH3110-R-0408 | 92 | 92.25 | Metasiltstone | Gooandra volcanics | Talbingo | Tunnel alignment/headrace |
| BH3110-R-0411 | 172.75 | 173 | Metasiltstone | Gooandra volcanics | Talbingo | Tunnel alignment/headrace |
| BH4103-R-0017 | 82.37 | 82.68 | Schist | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |

Table B4. Excavated rock - Peppercorn/Tantangara/Temperance formations

| Sample_ID | Depth (m) | | Lithology | Major Geology (Surface)/ Zone | Placement Option | Classification |
|---|-----------|--------|---------------------------------|-------------------------------|---------------------|---------------------------|
| | Top | Bottom | | | | |
| Peppercorn/Tantangara/Temperance Formations - Baseline | | | | | | |
| BH3101-R-0257 | 110.35 | 110.65 | meta sandstone | Tantangara Formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH3101-R-0259 | 170.3 | 170.6 | Meta Siltstone/Meta Sandstone | Tantangara Formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH3101-R-0261 | 201 | 201.3 | Meta Siltstone/Meta Sandstone | Tantangara Formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH3106-R-0353 | 154 | 154.3 | Interbedded sandstone/siltstone | Tantangara formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH3104-R-0395 | 319 | 319.45 | Siltstone | Tantangara formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH3101-R-0254 | 38 | 38.3 | Meta Siltstone/Meta Sandstone | Tantangara Formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH3106-R-0352 | 129.39 | 129.69 | Interbedded sandstone/siltstone | Tantangara formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH2102-R-0345 | 47.7 | 48 | Interbedded sandstone/siltstone | Tantangara formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| Peppercorn/Tantangara/Temperance Formations - Enriched | | | | | | |
| BH3102-R-0329 | 247.35 | 247.67 | Meta Siltstone/Meta Sandstone | Tantangara Formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH3101-R-0263 | 253 | 253.3 | Meta Siltstone/Meta Sandstone | Tantangara Formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH3102-R-0331 | 268 | 268.3 | Meta Siltstone/Meta Sandstone | Tantangara Formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH3102-R-0320 | 67.6 | 67.9 | meta siltstone | Tantangara Formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH3102-R-0322 | 116 | 116.28 | meta siltstone | Tantangara Formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH3102-R-0321 | 81.7 | 82 | meta siltstone | Tantangara Formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH3101-R-0255 | 61 | 61.3 | Meta Siltstone/Meta Sandstone | Tantangara Formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH3102-R-0319 | 35.25 | 35.55 | meta siltstone | Tantangara Formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| Kellys Plain Volcanics - Not available until late in study testing period | | | | | | |
| BH5102-R-0009, BH5102-R-0011, BH5102-R-0013 | | | | | Tantangara/Talbingo | |
| BH1115-R-0003, BH1116-R-0005, BH1117-R-0007 | | | | | Tantangara/Talbingo | |

Table B5. Excavated rock - Felsics/granitoids/gneiss/ignimbrites

| Sample_ID | Depth (m) | | Lithology | Major Geology (Surface)/ Zone | Placement Option | Classification |
|--|-----------|--------|-------------------|--------------------------------------|------------------|---------------------------|
| | Top | Bottom | | | | |
| Felsics/granitoids/gneiss/ignimbrites - Baseline | | | | | | |
| BH4102-R-0315 | 524 | 524.3 | Gneiss | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |
| BH4102-R-0316 | 546.4 | 546.7 | Gneiss | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |
| BH4102-R-0318 | 599 | 599.3 | Gneiss | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |
| BH4105-R-0370 | 430.7 | 431 | Gneiss | Ravine bed | Talbingo | Tunnel alignment/headrace |
| BH5104-R-0115 | 256 | 256.3 | Felsic ignimbrite | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Tunnel alignment/headrace |
| BH5103-R-0079 | 512.57 | 512.80 | Felsic volcanics | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Tunnel alignment/headrace |
| BH7104-R-0234 | 86.4 | 86.65 | Ignimbrite | Yarrangobilly Limestone/Palaeozoic | Talbingo | Tunnel alignment/headrace |
| Felsics/granitoids/gneiss/ignimbrites - Enriched | | | | | | |
| BH5105-R-0147 | 69 | 69.3 | Ignimbrite | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Tunnel alignment/headrace |
| BH5103-R-0066 | 342.40 | 342.61 | Felsic volcanics | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Tunnel alignment/headrace |
| BH5103-R-0080 | 348.37 | 348.58 | Felsic volcanics | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Tunnel alignment/headrace |
| BH5105-R-0146 | 64.7 | 65 | Ignimbrite | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Tunnel alignment/headrace |
| BH5105-R-0148 | 93.5 | 93.8 | Ignimbrite | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Tunnel alignment/headrace |



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CHAIN OF CUSTODY

| | |
|-----------|-------|
| Batch No: | CE491 |
|-----------|-------|

| Laboratory I.D. No.: | Sample I.D.: | | Date Received: | Date Sampled: | Time: | Sample Preservation | Analyses Requested | Storage Location: | Comments: |
|----------------------|--------------|----------|----------------|---------------|-------|---------------------|--------------------|-------------------|----------------------|
| CE491-1 | 59918111 | TAL-PL2A | 11/07/2018 | 4/07/2018 | 13:50 | | | 2J | 15Litres |
| CE491-2 | 59918111 | TAL-PL1A | | 4/07/2018 | 14:00 | | | | 15Litres |
| CE491-3 | 59918111 | TAN2A | | 3/07/2018 | 11:30 | | | | 15Litres |
| CE491-4 | 59918111 | TN3_A | | 3/07/2018 | 11:00 | | | | 15Litres |
| CE491-5 | 59918111 | TN1_A | | 3/07/2018 | 12:05 | | | | 15Litres |
| CE491-6 | 59918111 | TAL_PL1B | | 4/07/2018 | 14:00 | | | | Estimated as 5Litres |
| CE491-7 | 59918100 | TAL_P22B | | 4/07/2018 | 13:50 | | | | 15Litres |
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|-------------------------|---------------------------|-------------------------------|--------------------------|
| Client: | Cardno | Received By (Print Name): | Chad Jarolimek |
| Client Contact Person: | via Simon Apte/Brad Angel | Date and Time: | 11/07/18 at 15:00 |
| Client Contact Tel/Fax: | | Condition (i.e. Temperature): | Ambient |
| Client Contact Email: | | Signature: | |
| Method of Shipment: | | Comments: | All contained in Carboys |
| Con Note No.: | | NATA Report Required: | |



CSIRO

Centre for Environmental Contaminants Research
CSIRO Land and Water
Locked Bag 2007, Kirrawee, NSW, 2234, Australia
Telephone: (02) 9710 6822
Fax: (02) 9710 6800
Email: Chad.Jarolimek@csiro.au

CHAIN OF CUSTODY

| | |
|-----------|-------|
| Batch No: | CE491 |
|-----------|-------|

| Laboratory I.D. No.: | Sample I.D.: | | Date Received: | Date Sampled: | Time Sampled: | Sample Preservation | Storage Location: | Comments: |
|----------------------|--------------|-------------|----------------|---------------|---------------|---------------------|-------------------|-------------------|
| CE491-8 | TAN_P4 | 19 metres | 11/07/2018 | 3/07/2018 | | Ice in esky | 2J | Blue esky -TAN-P4 |
| CE491-9 | TN1_P4 | 16.5 metres | | 3/07/2018 | | | | Blue esky -TAN-P4 |
| CE491-10 | TN3_P4 | 18.5 metres | | 3/07/2018 | | | | Blue esky -TAN-P4 |
| CE491-11 | CA3_P4 | 48 metres | | 5/07/2018 | 9:45 | | | Red esky -TAL-P4 |
| CE491-12 | RA1_P4 | 31.5 metres | | 4/07/2018 | 10:15 | | | Red esky -TAL-P4 |
| CE491-13 | PL1_P4 | 33.5 metres | | 4/07/2018 | 14:20 | | | Red esky -TAL-P4 |
| CE491-14 | CA1_P4 | 30 metres | | 5/07/2018 | 11:20 | | | Red esky -TAL-P4 |
| CE491-15 | PL3_P4 | 27 metres | | 4/07/2018 | 12:35 | | | Red esky -TAL-P4 |
| CE491-16 | RA3_P4 | 28.5 metres | | 4/07/2018 | 11:20 | | | Red esky -TAL-P4 |
| CE491-17 | PL2_P4 | 26.5 metres | | 4/07/2018 | 13:15 | | | Red esky -TAL-P4 |
| CE491-18 | CA2_P4 | 42 metres | | 5/07/2018 | 10:15 | | | Red esky -TAL-P4 |
| CE491-19 | RA2_P4 | 29 metres | | 4/07/2018 | 10:45 | | | Red esky -TAL-P4 |
| | | | | | | | | |
| | | | | | | | | |

| | | | |
|-------------------------|---------------------------|-------------------------------|---|
| Client: | Cardno | Received By (Print Name): | Chad Jarolimek |
| Client Contact Person: | via Simon Apte/Brad Angel | Date and Time: | 11/07/18 at 15:00 |
| Client Contact Tel/Fax: | | Condition (i.e. Temperature): | Chilled (ice had melted but still cold) |
| Client Contact Email: | | Signature: | |
| Method of Shipment: | | Comments: | All contained in Carboys |
| Con Note No.: | | NATA Report Required: | |

Water and Sediment samples from HKA

From: Ali Watters [<mailto:ali.watters@rhdhv.com>]

Sent: Monday, 9 July 2018 6:05 PM

To: Simpson, Stuart (L&W, Lucas Heights) <Stuart.Simpson@csiro.au>; Adams, Merrin (L&W, Lucas Heights) <Merrin.Adams@csiro.au>; Apte, Simon (L&W, Lucas Heights) <Simon.Apte@csiro.au>; Angel, Brad (L&W, Lucas Heights) <Brad.Angel@csiro.au>; Fraser, Ryan (Mineral Resources, Kensington WA) <Ryan.Fraser@csiro.au>

Cc: Ellen Porter (ellen.porter@snowyhydro.com.au) <ellen.porter@snowyhydro.com.au>; Greg Britton <greg.britton@rhdhv.com>

Subject: RE: CSIRO Project P4 - Water and Sediment samples

Ryan , Simon

The following 10 items have been shipped today and should arrive in Lucas Heights tomorrow (Tuesday) –

Water containers

3 x 15 L Tantangara water – 30 x 30 x 30 cm, 15 kg each, total 45L

4 x 15 L Talbingo Water – 30 x 30 x 30 cm, 15 kg each, total 60L

Eskies with sediment

1 esky 45 x 45 x 30 cm

2 eskies 40 x 60 x 30 cm

The sediment in the eskies comprises the following bagged samples – total 18 kg. Plans showing the sample locations and coordinates are attached.

| Location | Site | Site ID | Sample ID | Sample Wt | No. Bags | Date | Time | Water depth (m) |
|------------|-----------------|---------|-----------|-----------|----------|----------|------|-----------------|
| Tantangara | Placement Area | TN1 | TN1_P4 | 2 kg | 1 bag | 7/3/2018 | 1145 | 16.5 |
| Tantangara | Placement Area | TN2 | TN2_P4 | 2 kg | 1 bag | 7/3/2018 | 1115 | 19 |
| Tantangara | Placement Area | TN3 | TN3_P4 | 2 kg | 1 bag | 7/3/2018 | 1040 | 18.5 |
| Talbingo | Plain Creek Bay | PL1 | PL1_P4 | 2 kg | 1 bag | 7/4/2018 | 1420 | 33.5 |
| Talbingo | Plain Creek Bay | PL2 | PL2_P4 | 2 kg | 1 bag | 7/4/2018 | 1315 | 26.5 |
| Talbingo | Plain Creek Bay | PL3 | PL3_P4 | 2 kg | 1 bag | 7/4/2018 | 1235 | 27 |
| Talbingo | Cascade Bay | CA1 | CA1_P4 | 2 kg | 1 bag | 7/5/2018 | 1115 | 30 |
| Talbingo | Cascade Bay | CA2 | CA2_P4 | 2 kg | 1 bag | 7/5/2018 | 1015 | 42 |
| Talbingo | Cascade Bay | CA3 | CA3_P4 | 2 kg | 1 bag | 7/5/2018 | 945 | 48 |
| Talbingo | Ravine Bay | RA1 | RA1_P4 | 2 kg | 1 bag | 7/4/2018 | 1015 | 30.5 |
| Talbingo | Ravine Bay | RA2 | RA2_P4 | 2 kg | 1 bag | 7/4/2018 | 1045 | 29.5 |
| Talbingo | Ravine Bay | RA3 | RA3_P4 | 2 kg | 1 bag | 7/4/2018 | 1115 | 28.5 |

Please note we asked Cardno to recover bulk sediment samples from three locations within the 3 potential Talbingo placement areas. Similarly 3 bulk samples at the Tantangara placement area. The intention of the three locations within a placement area was to see if any variation within a placement area was observed. This is not expected and we thought it likely that CSIRO Sydney & Adelaide labs will end up compositing their requested volume of sediment from the 3 locations within a placement area into one large bulk sample for use in the P4 & P5 testing.

Regards

Ali

8:15 → LEAVE JIND AIRPORT FOR TALBINGCO.
SPILLWAY AND MIDDLE MICHAMOK (P.D.)

10:20 → PIT STOP IN TALBINGCO.

10:40 → TALBINGCO DAM VIEW POINT NEAR DAM
CAMP. PHOTOS OF SPILLWAY FROM ACROSS DAM.

11:00 → ARRIVED AT TALBINGCO SPILLWAY &
TOOK PHOTOS.

PUT ON WEATHER & COLLECTED ^{APPROX.} 22L OF
RESERVOIR WATER FROM MOST OUTER POINT
WE LEFT PROPOSED WARMER AREA.
WATER TASTE WAS TURPLE RINSED WITH
RESERVOIR WATER.

11:30 → LEFT THE SPILLWAY TO TRY AND ACCESS

MIDDLE BAY AREA.

11:30 → ~~LEAVE~~ ~~WENT~~ ~~HEAD~~ ~~ACCESS~~ ~~WATER~~ ~~AREA~~ ~~TO~~ ~~CP~~.

WARNING: CALLED BY SAFETY OFFICER & WAS
INFORMED OF AIRCRAFT SHOOTING AT LOSS
HOLE AVOID LOSS HOLE (AUGUST ROAD).

NO PILES OF YACANCO BUT PAPER WASTE

AREA.

BRIEF STOP FOR LUNCH.

12:05 → SET OFF FOR TANTAN GARA RESERVOIR.

13:45 → ARRIVED AT TANTAN GARA
AND HAD A LOOK/DIGUE AROUND.

14:15 → COLLECTED APPROX. 20L OF TANTAN GARA
RESERVOIR WATER.
PEOPLE WASHED VESSELS WITH RESERVOIR
WATER.

PNB, JIND AND GOTTEN UP & TANTAN GARA
RESERVOIR WAS FINALLY TURNED OFF. SFE PIES.

THIS MADE IT MORE DIFFICULT TO COLLECT
WATER. (THE WATER WENT OVER THE TOP OF
MY VESSELS & IT WAS COLD.)

14:40 → HEADED BACK TO GOTTEN FROM
TANTAN GARA.

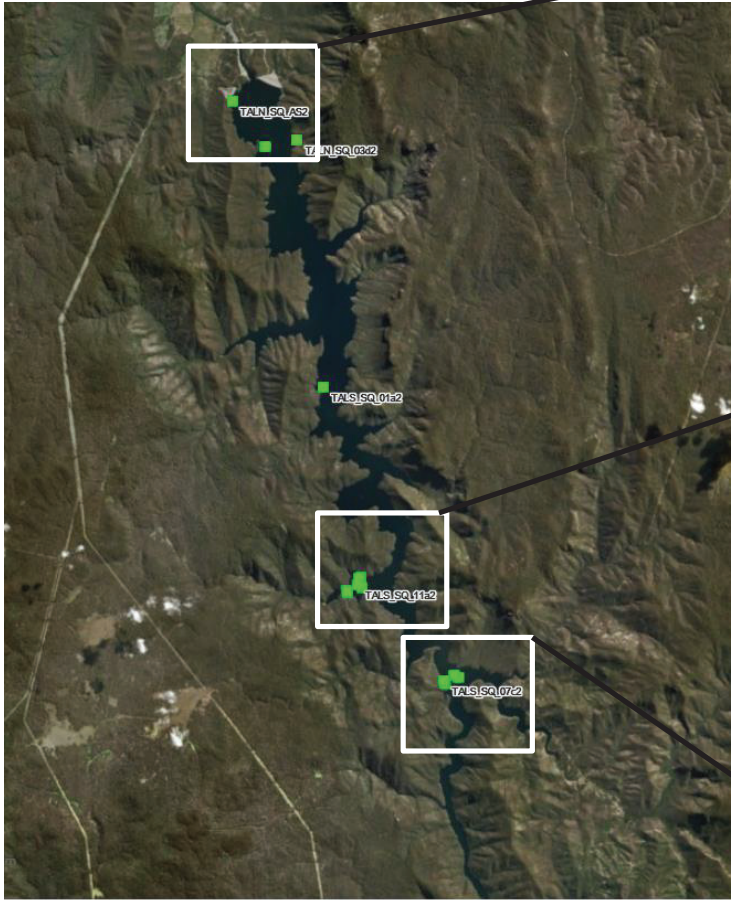
15:00 → ARRIVED GOTTEN IN GOTTEN & FUELED UP.

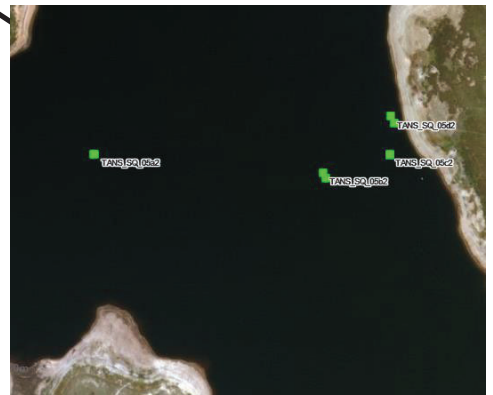
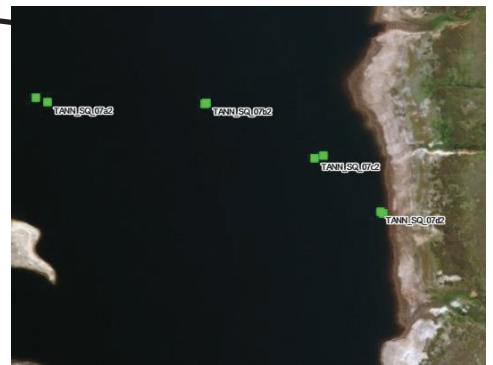
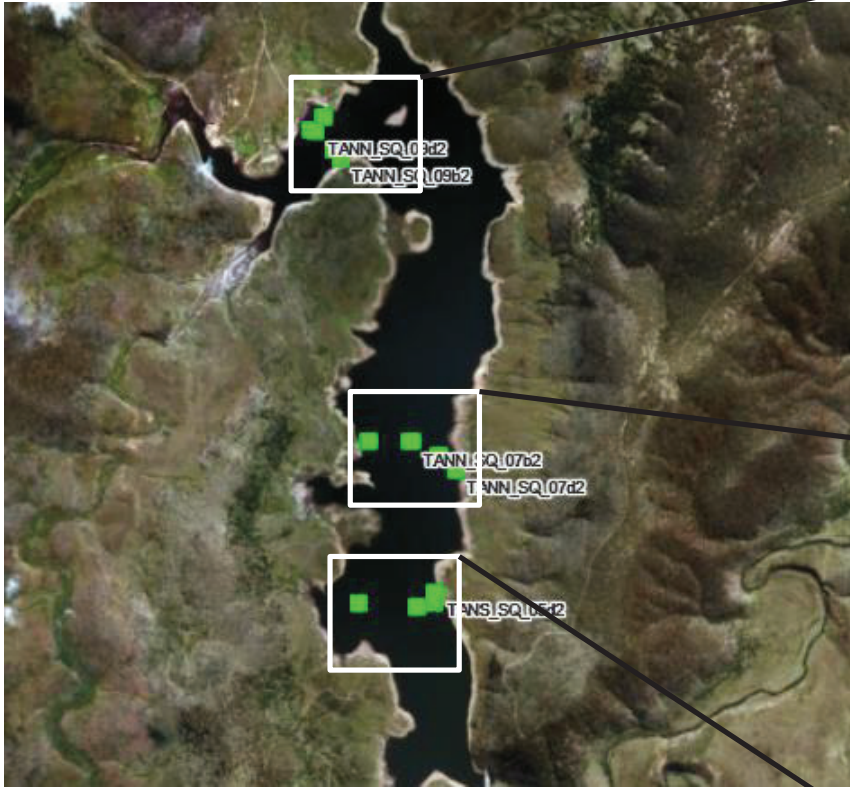
16:10 → ARRIVED BACK AT GOTTEN OFFICE, UNLOADED
& GUARD CAR.



ZParker

14/6/18





TALBINGO - PLACEMENT
CASCADE BAY

| FILL TABLE | | | | |
|------------|----------|----------|------------------------|------------------------|
| No. | Min. (m) | Max. (m) | Area (m ²) | Vol. (m ³) |
| 1 | 0.0 | 5.0 | 60715 | 987951 |
| 2 | 5.0 | 10.0 | 42290 | 718648 |
| 3 | 10.0 | 15.0 | 31653 | 534726 |
| 4 | 15.0 | 20.0 | 21017 | 407150 |
| 5 | 20.0 | 25.0 | 19025 | 305779 |
| 6 | 25.0 | 30.0 | 24204 | 199768 |
| 7 | 30.0 | 35.0 | 25161 | 74050 |
| 8 | 35.0 | 40.0 | 2589 | 9276 |
| TOTAL | | | 226,526 | 3,203,527 |

| SAMPLE COORDINATES TABLE | | |
|--------------------------|-------------|------------|
| Point # | Description | Easting |
| 7 | RA1 | 6041726.97 |
| 8 | RA2 | 6041815.71 |
| 9 | RA3 | 6041667.36 |

KEY PLAN
1:50,000 (A3)

PLAN 3
1:3,000 (A3)

NOTES

- BATHYMETRIC SURVEY DATED 26/02/2018, LEVELS TO AHD.
- FILL TO RL 529mAHD

AUSTRALIAN HEIGHT DATUM

NOT FOR CONSTRUCTION

LEGEND

- FULL SUPPLY LEVEL (FSL) = RL 543.18mAHD
MIN. OPERATING LEVEL (MOL) = RL 534.35mAHD

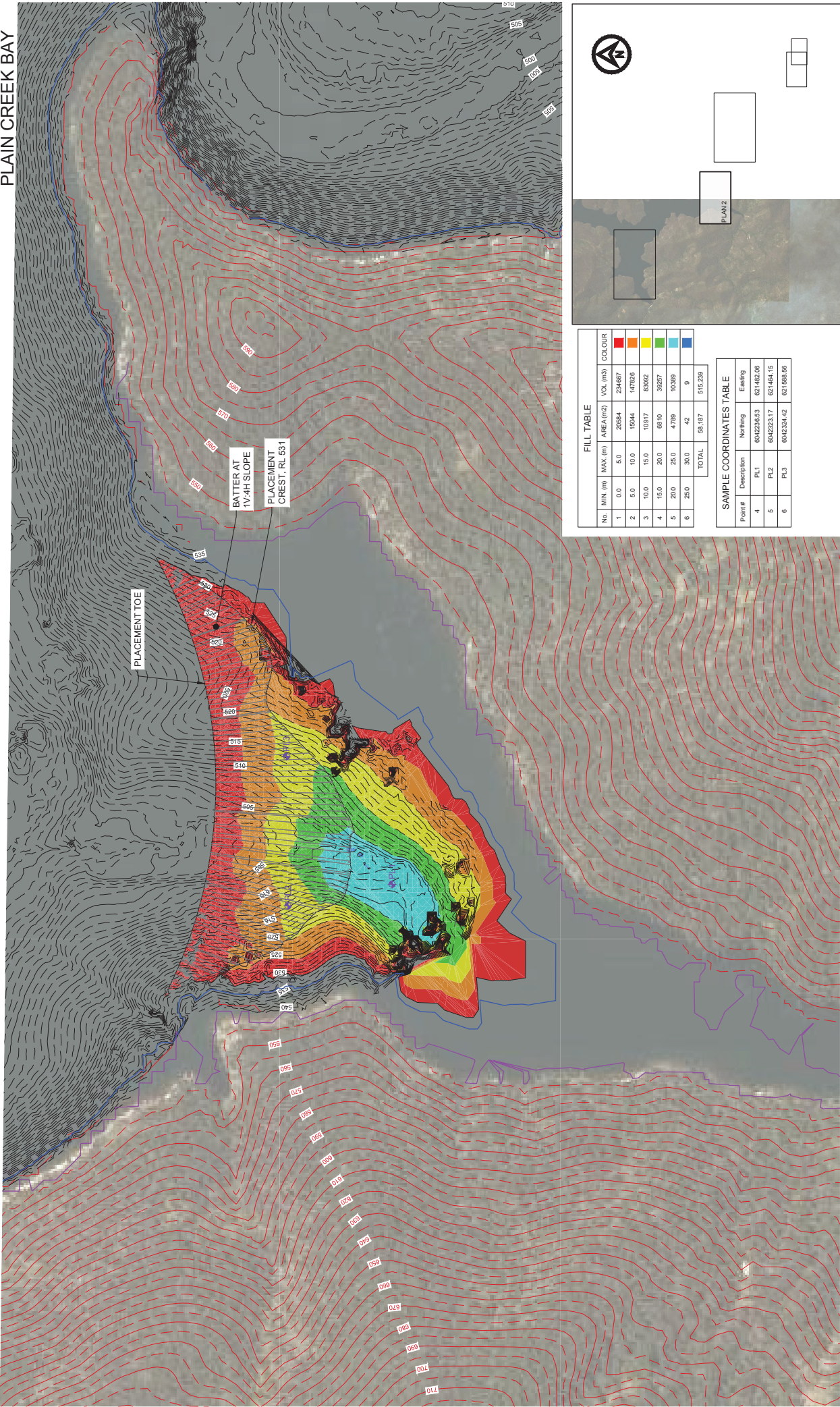
PROPOSED SEDIMENT & WATER SAMPLE

RA1

- LIDAR CONTOUR
HYDRO SURVEY CONTOUR (26/02/2018)



TALBINGO - PLACEMENT
PLAIN CREEK BAY



| FILL TABLE | | | | |
|------------|---------|---------|------------------------|-----------------------|
| No. | MIN (m) | MAX (m) | AREA (m ²) | VOL (m ³) |
| 1 | 0.0 | 5.0 | 20584 | 234667 |
| 2 | 5.0 | 10.0 | 19044 | 147826 |
| 3 | 10.0 | 15.0 | 10977 | 83092 |
| 4 | 15.0 | 20.0 | 6810 | 36627 |
| 5 | 20.0 | 25.0 | 4789 | 10389 |
| 6 | 25.0 | 30.0 | 42 | 9 |
| TOTAL | | | 58187 | 515289 |

| SAMPLE COORDINATES TABLE | | |
|--------------------------|-------------|-----------|
| Point # | Description | Easting |
| 4 | PL1 | 604223.63 |
| 5 | PL2 | 604223.17 |
| 6 | PL3 | 604234.42 |

PLAN 2
1:3000 (A3)

LEGEND

- NOTES
- BATHYMETRIC SURVEY DATED 26/02/2018, LEVELS TO AHD.
 - FILL TO RL 528mAHD.

FULL SUPPLY LEVEL
(FSL) = RL 543.18mAHD

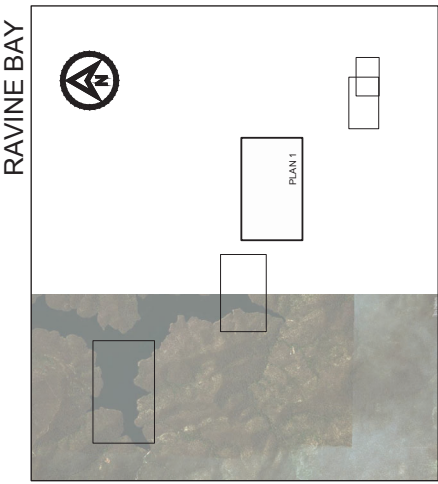
PROPOSED SEDIMENT
& WATER SAMPLE

LIDAR CONTOUR
HYDRO SURVEY
CONTOUR (26/02/2018)

AUSTRALIAN HEIGHT DATUM

NOT FOR CONSTRUCTION

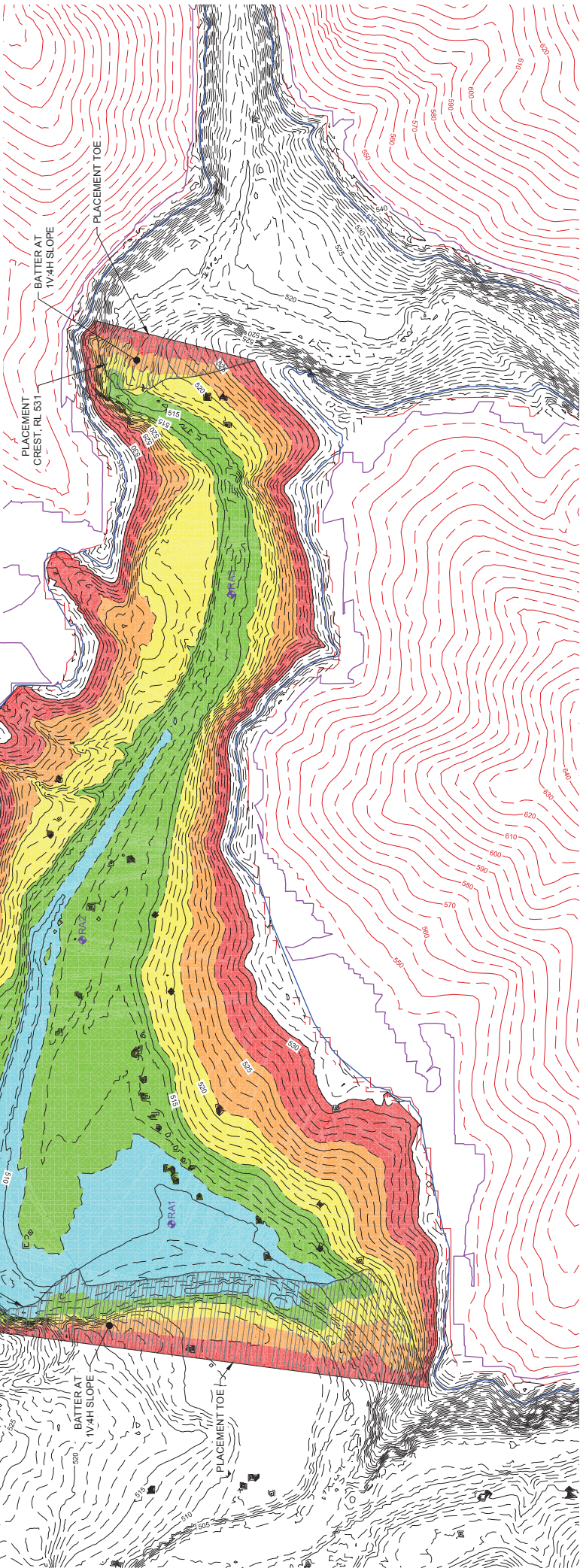
TALBINGO - PLACEMENT
RAVINE BAY



| FILL TABLE | | | | |
|------------|----------|----------|-----------|-----------|
| No. | MIN. (m) | MAX. (m) | AREA (m2) | VOL. (m3) |
| 1 | 0.0 | 5.0 | 55304 | 1383771 |
| 2 | 5.0 | 10.0 | 54863 | 1112881 |
| 3 | 10.0 | 15.0 | 63820 | 833273 |
| 4 | 15.0 | 20.0 | 85220 | 488841 |
| 5 | 20.0 | 25.0 | 45688 | 98859 |
| TOTAL | | | 304,598 | 3,836,994 |

| SAMPLE COORDINATES TABLE | | |
|--------------------------|-------------|-----------|
| Point # | Description | Easting |
| 1 | CA1 | 604046.03 |
| 2 | CA2 | 604167.47 |
| 3 | CA3 | 604169.50 |

KEY PLAN
1:80,000 (A3)



PLAN 1
1:3,000 (A3)

LEGEND

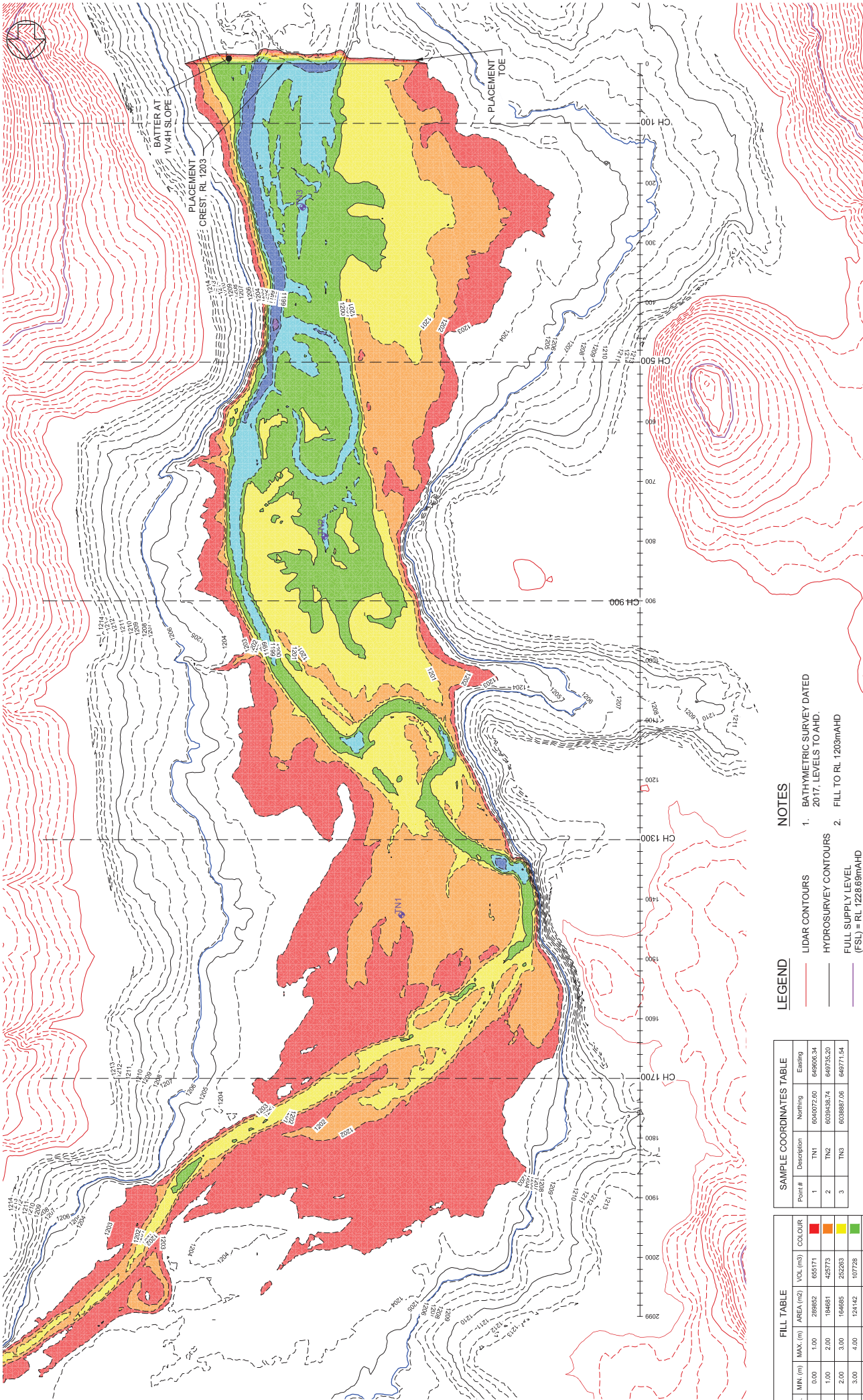
- NOTES
- BATHYMETRIC SURVEY DATED 26/02/2018, LEVELS TO AHD.

- FULL SUPPLY LEVEL (FSL) = RL 543.18mAHD
MIN. OPERATING LEVEL (MOL) = RL 534.35mAHD
- PROPOSED SEDIMENT & WATER SAMPLE

AUSTRALIAN HEIGHT DATUM

NOT FOR CONSTRUCTION





AUSTRALIAN HEIGHT DATUM

NOT FOR CONSTRUCTION

- NOTES**
- BATHYMETRIC SURVEY DATED 2017, LEVELS TO AHD.
 - FILL TO RL 1203m AHD
- LEGEND**
- LIDAR CONTOURS
 - HYDRO SURVEY CONTOURS
 - FULL SUPPLY LEVEL (FSL) = RL 1228.69m AHD
 - MIN. SUPPLY LEVEL (MOL) = RL 1205.88m AHD
 - PROPOSED SEDIMENT & WATER SAMPLE

| SAMPLE COORDINATES TABLE | | | |
|--------------------------|-------------|-----------|-----------|
| Point # | Description | Northing | Easting |
| 1 | TN1 | 604072.60 | 649006.34 |
| 2 | TN2 | 603943.74 | 649735.20 |
| 3 | TN3 | 603887.06 | 649771.54 |

| FILL TABLE | | | |
|------------|---------|---------|----------|
| No. | MIN (m) | MAX (m) | VOL (m3) |
| 1 | 0.00 | 1.00 | 28882 |
| 2 | 1.00 | 2.00 | 19461 |
| 3 | 2.00 | 3.00 | 16485 |
| 4 | 3.00 | 4.00 | 12142 |
| 5 | 4.00 | 5.00 | 39708 |
| 6 | 5.00 | 6.00 | 8777 |
| 7 | 6.00 | 7.00 | 147 |
| TOTAL | | | 146,094 |

Appendix C - Characterisation of the Water, Rock and Sediments [67 pages]

The preliminary results were summarised as Memos 1, 2 and 3, and updated data provided here.

Memo 1 – Reservoir Waters, and data files

Memo 2 - Reservoir Sediments, and data files

Memo 3 – Rock materials, and data files

| | |
|------------------|---|
| Note/Memo | CSIRO P4 Project Investigations |
| To: | Ali Watters (HKA) |
| From: | Brad Angel, Lucas Heights, NSW |
| Date: | 25 September 2018 |
| Copy: | Ryan Fraser, Stuart Simpson and Ellen Porter (SHL) |
| Our reference: | CSIRO P4 – Memo 1 |
| Classification: | Internal use only |
| Subject: | Chemical characterisation of the Talbingo and Tantangara reservoirs |

Chemical formulas and acronyms

| | | | |
|-----------------|--------------------------|-------------------------------|------------|
| Ag | Silver | Mo | Molybdenum |
| Al | Aluminium | Na | Sodium |
| As | Arsenic | Ni | Nickel |
| Ba | Barium | NO ₃ ⁻ | Nitrate |
| Ca | Calcium | Pb | Lead |
| Cd | Cadmium | Sb | Antimony |
| Cl ⁻ | Chloride | Se | Selenium |
| Co | Cobalt | Sn | Tin |
| Cr | Chromium | SO ₄ ²⁻ | Sulfate |
| Cu | Copper | Sr | Strontium |
| DOC | Dissolved organic carbon | Th | Thorium |
| F ⁻ | Fluoride | U | Uranium |
| Fe | Iron | V | Vanadium |
| Mg | Magnesium | Zn | Zinc |
| Mn | Manganese | | |

Background

The CSIRO was engaged by Haskoning Australia Pty Ltd (RHDHV) to undertake an investigation of the pollutant release from excavated rock disposal into the Talbingo and Tantangara reservoirs. The first phase of the work involved chemical characterisation of the reservoir waters.

This technical memo describes the preliminary results.

pH, conductivity, dissolved oxygen, turbidity, alkalinity, DOC and hardness

The pH, electrical conductivity (EC), dissolved oxygen, turbidity, alkalinity and dissolved organic carbon (DOC) measured in the Talbingo and Tantangara reservoir waters are shown in Table 1. The pH, conductivity, dissolved oxygen and alkalinity were similar in both reservoirs and ranged from 6.93 to 7.27, 26.5 to 29.4 $\mu\text{S}/\text{cm}$, 9.19 to 10.1 mg/L, and 11.5 to 12.5 mg CaCO₃/L, respectively. The turbidity in the Tantangara reservoir was in the range 0.51-0.60 NTU, which was relatively low but slightly higher than that measured in Talbingo reservoir of 0.20-0.34 NTU. The DOC ranged from 1.2-2.3 mg/L, with the Tantangara reservoir having nearly double the concentration as the Talbingo reservoir. The hardness of the Talbingo and Tantangara reservoir water based on the concentrations of calcium and magnesium is shown in Table

2. The hardness was in the range 7.47-8.05 mg CaCO₃/L, with the Talbingo water being slightly less hard than the Tantangara water.

Table 1. The pH, conductivity, dissolved oxygen, turbidity and alkalinity of the Talbingo and Tantangara reservoirs

| Sample ID | Reservoir | pH | Conductivity (µS/cm) | Dissolved O ₂ (mg/L) | Turbidity (NTU) | Alkalinity (mg CaCO ₃ /L) | DOC ^a (mg/L) |
|--------------------|------------|------|-------------------------|------------------------------------|--------------------|---|----------------------------|
| TAL-PL1A | Talbingo | 7.20 | 26.5 | 9.71 | 0.20 | 11.9 | 1.3 |
| TAL-PL2A | Talbingo | 6.93 | 27.3 | 9.64 | 0.34 | 11.7 | 1.2 |
| TAL-PL1B | Talbingo | 7.27 | 28.9 | 9.45 | 0.26 | 11.7 | 1.3 |
| TAL-PL2B | Talbingo | 7.18 | 28.3 | 9.65 | 0.22 | 11.5 | 1.3 |
| TAL-PL2B duplicate | Talbingo | 7.16 | 28.3 | 9.41 | 0.21 | - | - |
| TAN-TN1A | Tantangara | 7.20 | 28.4 | 9.19 | 0.51 | 12.5 | 2.2 |
| TAN-TN2A | Tantangara | 7.17 | 29.4 | 10.1 | 0.60 | 12.0 | 2.2 |
| TAN-TN3A | Tantangara | 7.14 | 28.7 | 9.86 | 0.54 | 11.6 | 2.3 |

^a Dissolved organic carbon

Dissolved major cations, metals and metalloids

The concentrations of major cations are shown in Table 2. The dissolved Ca, K, Mg and Na were in the range 1.63-1.91, 0.426-0.569, 0.755-0.967 and 1.44-1.57 mg/L, respectively. The Talbingo reservoir had a slightly higher concentration of dissolved calcium, while the Tantangara reservoir had slightly higher concentrations of potassium and magnesium, and sodium was of a similar concentration in both reservoirs.

The concentrations of Ag, Al, As, Ba, Cd, Co, Cr, Cu, Fe, Mn, Mo, Ni, Pb, Sb, Se, Sn, Sr, Th, U, V, Zn are shown in Table 3. The concentrations of dissolved Ag, Be, Bi, Cd, Li, Mo, Sb, Se, Sn, Sr and Tl were similar in both reservoirs. The concentrations of dissolved Al, As, Ba, Co, Cr, Fe, Mn, Ni, Pb, Th and V were higher in the Tantangara reservoir than the Talbingo reservoir, with the mean dissolved iron having the greatest difference, being over 16 times higher. The concentrations of dissolved Ag, Al, As, Ba, Be, Bi, Cd, Co, Cr, Fe, Li, Mn, Mo, Ni, Pb, Sb, Se, Sn, Sr, Th, Tl and V exhibited little intra-reservoir variability for the multiple sites sampled in each reservoir, indicating surface waters are well mixed throughout each reservoir. The concentrations of dissolved copper, uranium and zinc were generally higher in the Talbingo reservoir than the Tantangara reservoir, however, site TAL-PL1B contained over 5 µg/L of copper and was obviously contaminated, and the dissolved zinc was spotty, probably due to contamination during sampling.

The concentrations were compared to ANZECC / ARMCANZ default water quality guideline values for the protection of 95 and 99% of species in Table 3, when values were available. The only exceedance of the 95% default guideline values (DGV) was for copper in sample TAL-PL1B that had leaked and potentially been contaminated during collection and transport. All sites exceeded the 99% guideline value for dissolved chromium, however, it should be noted that the only value available for comparison was for hexavalent chromium being in the hexavalent form, which is unlikely due its' stability.

Table 2. The concentrations major cations and water hardness in the Talbingo and Tantangara reservoirs

| Sample I.D. | Hardness (mg CaCO ₃ /L) | Ca (mg/L) | K (mg/L) | Mg (mg/L) | Na (mg/L) |
|-------------|---------------------------------------|--------------|-------------|--------------|--------------|
| TAL-PL1A | 7.50 | 1.78 | 0.431 | 0.756 | 1.45 |
| TAL-PL2A | 7.47 | 1.77 | 0.426 | 0.755 | 1.44 |
| TAL-PL1B | 8.03 | 1.91 | 0.451 | 0.807 | 1.57 |
| TAL-PL2B | 7.51 | 1.78 | 0.431 | 0.757 | 1.45 |
| TAN-TN1A | 8.05 | 1.65 | 0.568 | 0.967 | 1.57 |
| TAN-TN2A | 8.00 | 1.64 | 0.563 | 0.962 | 1.55 |
| TAN-TN3A | 7.99 | 1.63 | 0.569 | 0.964 | 1.55 |

Table 3. The concentrations of metals and metalloids in the Talbingo and Tantangara reservoirs

| Client I.D. | Ag (µg/L) | Al (µg/L) | As (µg/L) | Ba (µg/L) | Be (µg/L) | Bi (µg/L) | Cd (µg/L) | Co (µg/L) | Cr (µg/L) | Cu (µg/L) | Li (µg/L) | Fe (µg/L) | Mn (µg/L) |
|---------------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| TAL-PL1A | <0.002 | 3.93 | 0.166 | 4.44 | <0.005 | <0.028 | <0.005 | <0.007 | 0.060 | 0.649 | 0.095 | 23.9 | 0.287 |
| TAL-PL2A | 0.002 | 4.99 | 0.184 | 4.42 | <0.005 | <0.028 | <0.005 | 0.007 | 0.058 | 0.629 | 0.091 | 26.7 | 0.348 |
| TAL-PL1B | <0.002 | 4.86 | 0.16 | 4.52 | <0.005 | <0.028 | <0.005 | <0.007 | 0.064 | 5.22 | 0.116 | 24.9 | 0.386 |
| TAL-PL2B | <0.002 | 4.16 | 0.153 | 4.38 | <0.005 | <0.028 | <0.005 | <0.007 | 0.051 | 0.739 | 0.093 | 26.3 | 0.282 |
| TAN-TN1A | <0.002 | 26.2 | 0.314 | 6.13 | <0.005 | <0.028 | <0.005 | 0.025 | 0.100 | 0.483 | 0.107 | 396 | 2.30 |
| TAN-TN2A | <0.002 | 24.3 | 0.228 | 6.19 | <0.005 | <0.028 | <0.005 | 0.028 | 0.089 | 0.41 | 0.104 | 399 | 2.17 |
| TAN-TN3A | 0.017 | 23.6 | 0.326 | 6.15 | 0.007 | <0.028 | <0.005 | 0.032 | 0.095 | 0.386 | 0.104 | 394 | 2.36 |
| 95% GV ^a | 0.05 | 55 | 13 | - | - | - | 0.2 | - | 0.4 | 1.4 | - | - | 1900 |
| 99% GV ^b | 0.02 | 27 | 0.8 | - | - | - | 0.06 | - | 0.01 | 1.0 | - | - | 1200 |

| Client I.D. | Mo (µg/L) | Ni (µg/L) | Pb (µg/L) | Sb (µg/L) | Se (µg/L) | Sn (µg/L) | Sr (µg/L) | Th (µg/L) | Tl (µg/L) | U (µg/L) | V (µg/L) | Zn (µg/L) |
|-------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|-------------|-------------|--------------|
| TAL-PL1A | <0.073 | 0.078 | <0.02 | 0.012 | 0.026 | <0.021 | 14.7 | 0.0035 | <0.006 | 0.017 | 0.097 | 2.15 |
| TAL-PL2A | <0.073 | 0.102 | <0.02 | 0.007 | 0.020 | <0.021 | 14.7 | 0.0039 | <0.006 | 0.014 | 0.102 | 0.929 |
| TAL-PL1B | <0.073 | 0.111 | 0.033 | 0.01 | 0.015 | <0.021 | 15.1 | 0.0043 | <0.006 | 0.015 | 0.106 | 1.67 |
| TAL-PL2B | <0.073 | 0.117 | <0.02 | 0.01 | 0.024 | <0.021 | 14.8 | 0.0025 | <0.006 | 0.016 | 0.114 | 0.605 |
| TAN-TN1A | <0.073 | 0.188 | 0.079 | 0.012 | 0.024 | <0.021 | 14.7 | 0.0158 | <0.006 | 0.008 | 0.211 | 1.44 |
| TAN-TN2A | <0.073 | 0.205 | 0.06 | 0.007 | 0.022 | <0.021 | 14.6 | 0.0143 | <0.006 | 0.008 | 0.206 | 0.750 |
| TAN-TN3A | <0.073 | 0.179 | 0.04 | 0.009 | 0.029 | <0.021 | 14.8 | 0.0122 | <0.006 | 0.009 | 0.209 | 0.425 |
| 95% GV | - | 11 | 3.4 | - | 11 | - | - | - | - | - | - | 8.0 |
| 99% GV | - | 8 | 1.0 | - | 5 | - | - | - | - | - | - | 2.4 |

* TAL-PL1B sample container had leaked most of its content due to a loose lid or hole in container and sample contamination resulting from this is considered the likely reason for the elevated copper concentration

^a <http://www.waterquality.gov.au/anz-guidelines/guideline-values/default/water-quality-toxicants/>. 95% species protection guideline values (95%GV) for freshwater. Values for Arsenic are for As(V), chromium are for Cr(VI), and tin are for inorganic tin

^b <http://www.waterquality.gov.au/anz-guidelines/guideline-values/default/water-quality-toxicants/>. 99% species protection guideline values (99%GV) for freshwater. Values for Arsenic are for As(V), chromium are for Cr(VI), and tin are for inorganic tin

The concentrations of dissolved organic carbon, major anions and total sulfur

The concentrations of dissolved organic carbon (DOC), fluoride, chloride, nitrate, sulfate and total sulfur measured in the Talbingo and Tantangara reservoir samples are shown in Table 4. There was little intra-site variability in each parameter in each given reservoir. The concentrations of fluoride and chloride were similar in the two reservoirs, whereas nitrate, sulfate and total sulfur were marginally higher in the Talbingo reservoir than the Tantangara reservoir. The concentration of DOC measured in the Tantangara reservoir was nearly double the concentration in the Talbingo reservoir.

Table 4. The concentrations of metals and metalloids in the Talbingo and Tantangara reservoirs.

| Client I.D. | DOC (mg/L) | F ⁻ (mg/L) | Cl ⁻ (mg/L) | NO ₃ ⁻ (mg/L) | SO ₄ ²⁻ (mg/L) | Total S (mg/L) |
|-------------|---------------|--------------------------|---------------------------|--|---|-------------------|
| TAL-PL1A | 1.3 | 0.024 | 0.912 | 0.140 | 0.431 | 0.170 |
| TAL-PL2A | 1.2 | 0.023 | 0.911 | 0.129 | 0.421 | 0.165 |
| TAL-PL1B | 1.3 | 0.032 | 1.154 | 0.151 | 0.513 | 0.192 |
| TAL-PL2B | 1.3 | 0.023 | 0.910 | 0.142 | 0.428 | 0.161 |
| TAN-TN1A | 2.2 | 0.022 | 0.926 | 0.058 | 0.346 | 0.145 |
| TAN-TN2A | 2.2 | 0.025 | 0.910 | 0.039 | 0.343 | 0.155 |
| TAN-TN3A | 2.3 | 0.014 | 0.900 | 0.055 | 0.324 | 0.157 |

* Phosphate to be measured in the near future

Summary

Most parameters measured in the waters were in a similar concentration range in both reservoirs and there was little variability between sites in each reservoir. The concentrations of dissolved Al, As, Ba, Co, Cr, Fe, Mn, Ni, Pb, Th and V were higher in the Tantangara reservoir than the Talbingo reservoir, with the mean dissolved iron having the greatest difference, being over 16 times higher.

Note. For sample collection the containers used were not acid-washed, and the concentrations of metals such as Cu and Zn may also reflect minor contamination owing to the sampling procedures. This is not considered a particular concern for their intended use in later parts of the P4 investigations.

| | |
|------------------|--|
| Note/Memo | CSIRO P4 Project Investigations |
| To: | Ali Watters (HKA) |
| From: | Brad Angel, Lucas Heights, NSW |
| Date: | 25 September 2018 |
| Copy: | Ryan Fraser, Stuart Simpson and Ellen Porter (SHL) |
| Our reference: | CSIRO P4 – Memo 2 |
| Classification: | Internal use only |
| Subject: | Chemical characterisation of Talbingo and Tantangara reservoir sediments |

Chemical formulas and acronyms

| | | | |
|-----------------|--------------------------|-------------------------------|------------|
| Ag | Silver | Mo | Molybdenum |
| Al | Aluminium | Na | Sodium |
| As | Arsenic | Ni | Nickel |
| Ba | Barium | NO ₃ ⁻ | Nitrate |
| Ca | Calcium | Pb | Lead |
| Cd | Cadmium | Sb | Antimony |
| Cl ⁻ | Chloride | Se | Selenium |
| Co | Cobalt | Sn | Tin |
| Cr | Chromium | SO ₄ ²⁻ | Sulfate |
| Cu | Copper | Sr | Strontium |
| DOC | Dissolved organic carbon | Th | Thorium |
| F ⁻ | Fluoride | U | Uranium |
| Fe | Iron | V | Vanadium |
| Mg | Magnesium | Zn | Zinc |
| Mn | Manganese | | |

Background

The CSIRO was engaged by Haskoning Australia Pty Ltd (RHDHV) to undertake an investigation of the pollutant release from excavated rock placed in Talbingo and Tantangara reservoirs (a map of the sample sites will be prepared at a later date for incorporation into an interpretive report). The second phase of the work involved chemical characterisation of the reservoir sediments.

This technical memo describes the preliminary results to date.

Reservoir benthic sediment porewater pH, conductivity and redox potential

The pH and redox potential of the porewaters of the Talbingo and Tantangara reservoir sediments were measured directly in the sediments (not extracted porewater) Table 1. An inadequate volume of porewater was extracted in this initial work for conductivity measurements and instead conductivity was measured on sediment:deionised water suspension (1:10) that had been allowed to equilibrate for two weeks.

Table 1. The pH, conductivity and redox potential of the Talbingo and Tantangara reservoir sediment porewaters.

| Sediment ID | Reservoir | pH | Conductivity ($\mu\text{S}/\text{cm}$) | Redox, Eh (mV) |
|--------------------|------------------|-----------|--|---------------------------|
| CA1 | Talbingo | 7.30 | 23.5 | -175 |
| CA2 | Talbingo | 7.60 | 26.5 | -180 |
| CA3 | Talbingo | 7.45 | 19.0 | -170 |
| PL1 | Talbingo | 7.05 | 20.0 | -140 |
| PL2 | Talbingo | 7.30 | 15.7 | -125 |
| PL3 | Talbingo | 7.40 | 18.9 | -160 |
| RA1 | Talbingo | 7.25 | 22.7 | -160 |
| RA2 | Talbingo | 7.30 | 24.0 | -185 |
| RA3 | Talbingo | 7.50 | 21.6 | -190 |
| TN1 | Tantangara | 6.70 | 33.0 | -105 |
| TN2 | Tantangara | 7.10 | 36.0 | -140 |
| TN3 | Tantangara | 7.00 | 36.7 | -155 |

There was little difference in each parameter between the different sites in the Talbingo reservoir.

The pH was marginally lower in the porewaters from the Talbingo sediments than the Tantangara sediments, while the redox potential were marginally higher. The higher redox potential indicates slightly more oxic conditions prevailed in the Tantangara sediment porewaters.

- The pH of the porewaters was within a similar range to that measured in the reservoir waters (Memo 1), having generally a slightly higher range than the reservoir waters.
- The conductivity of the waters equilibrated with the Talbingo sediments was a little lower than the reservoir water (26-30 $\mu\text{S}/\text{cm}$ range, Memo 1), whereas, the conductivity of the waters equilibrated with the Tantangara sediments was a little higher than the reservoir waters, indicating a minor release of major ions.

Sediment pore water major anions and ammonia

The major anions in the porewater extracted (0.45 μm filtered) from the Talbingo and Tantangara sediments are shown in Table 2. The concentration of sulfate was variable between sites at the same general location (i.e. CA, PL or RA), whereas, chloride, nitrate and ammonia concentrations were generally similar between the different sites in the Talbingo reservoir. The sediment porewater of the Tantangara reservoir had higher concentrations of ammonia than the Talbingo sites.

Table 2. The concentrations of major anions and ammonia in the reservoir sediment porewater.

| Sediment ID | Cl ⁻ (mg/L) | NO ₃ ⁻ (mg/L) | SO ₄ ²⁻ (mg/L) | Total ammonia (mg NH ₃ /L) |
|-------------|---------------------------|--|---|--|
| CA1_P4 | 1.27 | 0.43 | 1.40 | 2.4 |
| CA2_P4 | 1.73 | 0.46 | 5.10 | 2.8 |
| CA3_P4 | 1.74 | 0.73 | 2.55 | 2.6 |
| PL1_P4 | 1.76 | 0.56 | 0.36 | 2.6 |
| PL2_P4 | 1.24 | 0.53 | 1.28 | 2.3 |
| PL3_P4 | 2.49 | 0.63 | 0.89 | 2.2 |
| RA1_P4 | 1.39 | 0.51 | 1.34 | 2.8 |
| RA2_P4 | 1.36 | 0.51 | 0.83 | 3.3 |
| RA3_P4 | 1.69 | 0.48 | 0.39 | 4.3 |
| TN1_P4 | 1.94 | 0.61 | 2.11 | 5.6 |
| TN2_P4 | 5.94 | 0.44 | 2.78 | 5.7 |
| TN3_P4 | 1.89 | 0.49 | 1.75 | 7.5 |

Metals, metalloids and major cations in the porewater of Talbingo and Tantangara reservoirs sediments

The concentrations of metals, metalloids and major cations in the porewater of Talbingo and Tantangara reservoir sediments are shown in Table 3. Many of the metals, metalloids and major cations exhibited substantial variability between sites, probably due to differences in micro-environmental parameter conditions in the porewaters from different sites, such as redox potential.

The default guideline values (DGVs) for water are shown in Table 3, with aluminium and copper exceeding the corresponding DGV in some porewaters. The dissolved (<0.45 μm filterable) aluminium was the most variable, probably due to differences in colloidal fractions between sites. Copper is likely to be complexed

by organic ligands, resulting in the labile concentration being below the DGV. The porewaters of the Talbingo sediments from location RA had arsenic concentration that exceed the DGV.

Table 3. The concentrations of metals and metalloids in the sediment porewaters of the Talbingo and Tantangara reservoirs.

| Sediment ID | Ag (µg/L) | Al (µg/L) | As (µg/L) | Ba (µg/L) | Ca (mg/L) | Cd (µg/L) | Co (µg/L) | Cr (µg/L) | Cu (µg/L) |
|-------------|------------------|--------------|--------------|--------------|--------------|------------------|--------------|--------------|--------------|
| CA1 | 0.063 | 10 | 6.2 | 68 | 6.08 | <0.021 | 9.2 | 0.39 | 0.24 |
| CA2 | <0.005 | 8 | 7.9 | 107 | 10.5 | 0.033 | 8.8 | 0.57 | 0.31 |
| CA3 | <0.005 | 67 | 8.9 | 72 | 5.50 | 0.080 | 7.7 | 0.44 | 0.91 |
| PL1 | 0.006 | 278 | 11.7 | 75 | 6.10 | <0.021 | 10.5 | 0.83 | 1.62 |
| PL2 | 0.008 | 600 | 6.7 | 62 | 6.54 | <0.021 | 7.1 | 0.68 | 1.39 |
| PL3 | 0.007 | 32 | 7.5 | 108 | 7.65 | 0.027 | 11.0 | 0.38 | 0.68 |
| RA1 | 0.006 | 144 | 10.3 | 89 | 5.40 | <0.021 | 7.0 | 0.43 | 1.47 |
| RA2 | <0.005 | 51 | 17.7 | 133 | 8.19 | <0.021 | 7.5 | 0.45 | 0.46 |
| RA3 | <0.005 | 6 | 18.3 | 260 | 13.3 | 0.035 | 9.3 | 0.37 | 0.30 |
| TN1 | 0.005 | 180 | 4.6 | 107 | 3.66 | <0.021 | 7.2 | 0.69 | 0.65 |
| TN2 | 0.004 | 179 | 5.1 | 95 | 3.39 | <0.021 | 5.2 | 0.73 | 0.53 |
| TN3 | <0.005 | 59 | 8.6 | 111 | 3.09 | <0.021 | 5.7 | 0.76 | 0.27 |
| Minimum | <0.005 | 5.5 | 4.63 | 62.1 | 3.09 | <0.021 | 5.25 | 0.373 | 0.238 |
| Maximum | 0.063 | 600 | 18.3 | 260 | 13.3 | 0.080 | 11.0 | 0.835 | 1.62 |
| DGV | 0.05 | 55 | 13 | NA | NA | 0.2 | NA | 0.4 | 1.4 |

| | Fe (mg/L) | K (mg/L) | Mg (mg/L) | Mn (mg/L) | Mo (µg/L) | Na (mg/L) | Ni (µg/L) | Pb (µg/L) | Sb (µg/L) |
|---------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|------------------|--------------|
| CA1 | 25.9 | 1.0 | 1.84 | 7.3 | 0.9 | 2.9 | 1.7 | <0.046 | 0.10 |
| CA2 | 37.1 | 1.4 | 6.36 | 10.5 | 0.8 | 3.4 | 1.7 | <0.046 | 0.10 |
| CA3 | 17.9 | 1.1 | 1.30 | 15.6 | 1.3 | 2.0 | 2.1 | 0.306 | 0.13 |
| PL1 | 27.5 | 1.2 | 2.01 | 7.4 | 0.6 | 2.9 | 2.5 | 0.660 | 0.23 |
| PL2 | 18.6 | 1.0 | 1.83 | 9.8 | 1.3 | 2.2 | 2.1 | 0.622 | 0.20 |
| PL3 | 36.8 | 1.8 | 3.37 | 12.9 | 1.9 | 2.8 | 1.6 | 0.157 | 0.28 |
| RA1 | 15.6 | 1.1 | 1.23 | 8.1 | 1.0 | 2.1 | 2.0 | 0.716 | 0.13 |
| RA2 | 22.4 | 1.2 | 1.55 | 14.0 | 1.2 | 2.5 | 2.4 | 0.134 | 0.06 |
| RA3 | 30.6 | 1.2 | 2.14 | 28.8 | 2.0 | 2.5 | 2.6 | 0.001 | 0.12 |
| TN1 | 28.1 | 1.4 | 2.26 | 2.7 | 0.2 | 3.6 | 1.1 | 0.140 | 0.28 |
| TN2 | 32.1 | 1.2 | 2.12 | 2.6 | 0.2 | 3.5 | 0.8 | 0.150 | 0.28 |
| TN3 | 37.4 | 0.9 | 1.84 | 3.4 | 0.1 | 1.9 | 0.9 | <0.046 | 0.17 |
| Minimum | 15.6 | 0.917 | 1.230 | 2.56 | 0.12 | 1.92 | 0.784 | <0.046 | 0.064 |
| Maximum | 37.4 | 1.77 | 6.36 | 28.8 | 2.03 | 3.56 | 2.62 | 0.716 | 0.283 |
| DGV | NA | NA | NA | 1900 | NA | NA | 11 | 3.4 | NA |

| | Se (µg/L) | Sn (µg/L) | Sr (µg/L) | Th (µg/L) | U (µg/L) | V (µg/L) | Zn (µg/L) |
|---------|--------------|------------------|--------------|--------------|--------------|-------------|--------------|
| CA1 | 0.12 | <0.028 | 51.9 | 0.058 | 0.059 | 1.6 | 1.5 |
| CA2 | 0.14 | <0.028 | 121.7 | 0.080 | 0.096 | 1.9 | 3.5 |
| CA3 | 0.12 | <0.028 | 45.3 | 0.117 | 0.105 | 2.5 | 3.1 |
| PL1 | 0.13 | <0.028 | 47.8 | 0.163 | 0.137 | 2.8 | 2.6 |
| PL2 | 0.10 | <0.028 | 44.8 | 0.149 | 0.137 | 2.6 | 6.2 |
| PL3 | 0.14 | <0.028 | 71.4 | 0.079 | 0.112 | 1.6 | 4.2 |
| RA1 | 0.09 | <0.028 | 35.7 | 0.132 | 0.152 | 1.8 | 4.0 |
| RA2 | 0.12 | <0.028 | 49.9 | 0.093 | 0.105 | 1.9 | 1.9 |
| RA3 | 0.15 | <0.028 | 69.9 | 0.078 | 0.260 | 2.0 | 2.2 |
| TN1 | 0.18 | <0.028 | 36.7 | 0.140 | 0.053 | 3.6 | 1.6 |
| TN2 | 0.17 | <0.028 | 34.8 | 0.133 | 0.035 | 2.9 | 2.2 |
| TN3 | 0.23 | <0.028 | 31.9 | 0.103 | 0.033 | 3.4 | 1.4 |
| Minimum | 0.094 | <0.028 | 31.9 | 0.058 | 0.033 | 1.59 | 1.42 |
| Maximum | 0.235 | 0.013 | 122 | 0.163 | 0.260 | 3.62 | 6.23 |
| DGV | 11 | NA | NA | NA | NA | NA | 8.0 |

DGV = the default guideline value (95% species protection), where GV for arsenic are for As(V), chromium are for Cr(VI), and tin are for inorganic tin. <http://www.waterquality.gov.au/anz-guidelines/guideline-values/default/water-quality-toxicants/>. Values are **bold underline** where the default GV is exceeded

Particle size distribution

The particle size distribution of the Talbingo and Tantangara reservoir sediments are shown in Table 4. The mean diameter of the sediments were in the range 23.1 to 77.6 μm . The Dv (50) (50% of particles had lower diameter than this value) were all less than 30 μm , indicating the sediments were predominantly silt. Tantangara had a larger sediment particle size-range, which influenced its' slightly larger mean particle size.

Table 4. The particle size distribution of benthic sediments collected from Talbingo and Tantangara reservoirs.

| Sediment ID | Reservoir | Dv (10) (μm) | Dv (50) (μm) | Dv (90) (μm) | Mean diameter (μm) |
|-------------|------------|------------------------------|------------------------------|------------------------------|------------------------------------|
| CA1 | Talbingo | 4.40 | 15.7 | 70.6 | 31.2 |
| CA2 | Talbingo | 4.30 | 18.0 | 113 | 45.5 |
| CA3 | Talbingo | 4.36 | 17.2 | 103 | 44.7 |
| PL1 | Talbingo | 4.67 | 18.0 | 81.6 | 36.5 |
| PL1 Dup | Talbingo | 4.73 | 17.4 | 73.9 | 32.7 |
| PL1 | Talbingo | 4.70 | 17.7 | 77.8 | 34.6 |
| PL2 | Talbingo | 4.41 | 16.3 | 90.6 | 42.1 |
| PL3 | Talbingo | 4.24 | 16.0 | 103 | 49.6 |
| RA1 | Talbingo | 3.94 | 13.7 | 62.0 | 30.7 |
| RA1 dup | Talbingo | 3.93 | 13.5 | 60.8 | 28.8 |
| RA1 | Talbingo | 3.94 | 13.6 | 61.4 | 29.8 |
| RA2 | Talbingo | 3.66 | 11.5 | 43.9 | 23.1 |
| RA3 | Talbingo | 3.75 | 12.0 | 47.7 | 24.2 |
| TN1 | Tantangara | 5.57 | 27.4 | 223 | 77.6 |
| TN2 | Tantangara | 4.84 | 20.1 | 132 | 50.5 |
| TN3 | Tantangara | 4.63 | 20.3 | 133 | 48.7 |

Note: Dv (x) refers to 10, 50 and 90th percentiles of particle diameters (on spherical volume basis)

The total nitrogen and phosphorous, inorganic and organic carbon in benthic sediments

The total nitrogen, phosphorous, inorganic and organic carbon in benthic reservoir sediments are shown in Table 5. For the Talbingo reservoir, the RA sites generally had lower concentrations of each parameter than the CA and PL sites. The Tantangara reservoir benthic sediments had similar or higher concentrations of each parameter than those in the Talbingo reservoir. The concentrations of each parameter varied by approximately two-fold between the different sites in the two reservoirs.

The total Ca, K, Mg, Na, S and the cation exchange capacity of benthic sediments

The total Ca, K, Mg, Na, S in the benthic sediments and the sediment cation exchange capacity (CEC) is shown in Table 5. For the Talbingo reservoir sediments, calcium was the only major cation that varied between the sites, with lower concentrations being measured in the RA site sediments than the CA or PL sediments. The concentrations of calcium, magnesium, potassium and sodium were generally lower in the Tantangara reservoir sediments than the Talbingo reservoir sediments. The sulfur was higher in the Tantangara sediments and the CEC was similar for both reservoir sediments.

Table 5. The concentration of N, P, TIC, TOC, Ca, K, Mg, Na, S and CEC in benthic reservoir sediments

| Sediment ID | Reservoir | Total N (%) | Total P (mg/kg) | TIC (%) | TOC (%) | Ca | K | Mg (mg/kg) | Na | S | CEC (NH ₄) cmol (+/-)/kg |
|----------------|------------|----------------|--------------------|------------|------------|-------------|--------------|---------------|------------|------------|--|
| CA1 | Talbingo | 0.43 | 1340 | 0.2 | 5.8 | 1900 | 7150 | 5310 | 175 | 475 | 34 |
| CA2 | Talbingo | 0.39 | 1170 | 0.1 | 5.5 | 2080 | 8670 | 6210 | 174 | 432 | 33 |
| CA3 | Talbingo | 0.36 | 1140 | 0.1 | 4.5 | 1790 | 8580 | 7770 | 179 | 395 | 30 |
| PL1 | Talbingo | 0.39 | 1080 | 0.1 | 5.5 | 2450 | 7280 | 6680 | 177 | 436 | 32 |
| PL2 | Talbingo | 0.41 | 1030 | 0.2 | 6.0 | 1900 | 8800 | 6190 | 192 | 409 | 29 |
| PL3 | Talbingo | 0.40 | 1130 | 0.2 | 5.4 | 1620 | 7790 | 6100 | 174 | 448 | 32 |
| RA1 | Talbingo | 0.37 | 945 | 0.1 | 4.4 | 1480 | 8970 | 6630 | 163 | 395 | 27 |
| RA2 | Talbingo | 0.36 | 945 | 0.1 | 4.2 | 1490 | 10230 | 7040 | 175 | 386 | 30 |
| RA3 | Talbingo | 0.32 | 916 | 0.1 | 3.7 | 1450 | 8690 | 6570 | 146 | 338 | 26 |
| TN1 | Tantangara | 0.54 | 1040 | 0.2 | 6.4 | 714 | 6650 | 3320 | 140 | 650 | 34 |
| TN2 | Tantangara | 0.56 | 1500 | 0.2 | 5.7 | 783 | 7700 | 3490 | 150 | 742 | 36 |
| TN3 | Tantangara | 0.54 | 1310 | 0.2 | 5.8 | 653 | 7480 | 3520 | 134 | 773 | 36 |
| Minimum | | 0.32 | 916 | 0.1 | 3.7 | 653 | 6650 | 3320 | 134 | 338 | 26 |
| Maximum | | 0.56 | 1500 | 0.2 | 6.4 | 2450 | 10230 | 7770 | 192 | 773 | 36 |

Where, TIC is total inorganic carbon, TOC is total organic carbon, CEC is cation exchange capacity ^a C.E.C. = Cation exchange capacity, determined using NH₄Cl solution, as per [Rayment and Lyons \(2011\)](#).

Total recoverable concentrations of metals, metalloid, and major cations in benthic sediments

The total recoverable concentrations of metal, metalloid, and other major ions in Talbingo and Tantangara sediments are shown in Table 6. There was generally higher concentrations of antimony, calcium, chromium, copper, iron, potassium, magnesium, manganese, nickel, sodium, strontium, tin, thallium, and uranium in the Talbingo sediments and a higher concentration of sulfur in the Tantangara sediments.

These concentrations reflect the background surface sediment concentrations, and not surprisingly the concentrations of nickel exceed the corresponding SQGV that is considered an overly conservative value (Vangheluwe et al., 2013; Simpson and Batley 2016).

Dilute-acid extractable concentrations of metals, metalloid, and major cations in benthic sediments

A significant portion of the total element concentration (extracted using concentrated acids) may release inert (not easily released) fractions of metals that exhibit very low bioavailability to organisms. For most metals, the 'maximum bioavailable concentration' can be determined by dilute-acid extractable metal (AEM) analyses, as commonly achieved by extracting the solid in 1 M hydrochloric acid for 1 h (Simpson and Batley 2016). AEM data can also be useful for interpreting the partitioning behaviour of elements between the dissolved and particulate phases, and the availability of reactive binding phases.

The dilute-acid extractable concentrations of metal, metalloid, and other major ions in Talbingo and Tantangara sediments are shown in Table 7. There was generally little variation in the concentrations between the different sites in the Talbingo reservoir. However, the K, Mg and V were marginally lower for the RA sites than the CA and PL sites. A comparison between the two reservoirs showed that the 1 M HCl-extractable concentrations of As, Ba, Ca, Cr, Cu, K, Mg, Mn, Na, Ni, Th and U from the Talbingo reservoir sediments were generally higher than those measured in the Tantangara reservoir, while a higher concentration of sulfur was extracted from the Tantangara reservoir sediments.

No concentrations of diluted acid-extractable metals, metalloids and major cations exceeded their respective SQGV's.

Table 6. Total recoverable concentrations of metals, metalloids, and major ions in the sediments of the Talbingo and Tantangara reservoir waters

| Sediment ID | Reservoir | Al (mg/kg) | Ag (mg/kg) | As (mg/kg) | Ba (mg/kg) | Cd (mg/kg) | Ca (mg/kg) | Co (mg/kg) | Cr (mg/kg) | Cu (mg/kg) | |
|-----------------|-----------------|---------------|----------------|---------------|---------------|---------------|---------------|---------------|------------------|---------------|--------------|
| CA1 | Talbingo | 23000 | 0.14 | 9.2 | 250 | 0.24 | 1800 | 30 | 56 | 41 | |
| CA2 | Talbingo | 23000 | 0.13 | 8.6 | 270 | 0.17 | 1900 | 23 | 56 | 37 | |
| CA3 | Talbingo | 42000 | 0.15 | 12 | 300 | 0.27 | 1900 | 30 | 78 | 51 | |
| PL1 | Talbingo | 31000 | 0.11 | 8.8 | 220 | 0.15 | 1800 | 28 | 72 | 46 | |
| PL2 | Talbingo | 35000 | 0.14 | 11 | 250 | 0.23 | 2200 | 26 | 61 | 52 | |
| PL3 | Talbingo | 36000 | 0.14 | 12 | 240 | 0.26 | 1600 | 30 | 62 | 51 | |
| PL3 duplicate | Talbingo | 36000 | 0.15 | 12 | 240 | 0.21 | 1600 | 30 | 61 | 51 | |
| PL3 Mean | Talbingo | 36000 | 0.14 | 12 | 240 | 0.23 | 1600 | 30 | 61 | 51 | |
| RA1 | Talbingo | 20000 | 0.14 | 10 | 240 | 0.27 | 1400 | 24 | 48 | 46 | |
| RA2 | Talbingo | 36000 | 0.16 | 14 | 280 | 0.22 | 1700 | 25 | 59 | 49 | |
| RA3 | Talbingo | 26000 | 0.15 | 15 | 320 | 0.23 | 1700 | 25 | 52 | 48 | |
| TN1 | Tantangara | 17000 | 0.12 | 5.4 | 180 | 0.27 | 720 | 15 | 27 | 26 | |
| TN2 | Tantangara | 31000 | 0.16 | 6.7 | 230 | 0.25 | 840 | 23 | 37 | 28 | |
| TN3 | Tantangara | 23750 | 0.15 | 8.2 | 240 | 0.25 | 1150 | 26 | 41 | 32 | |
| Minimum | | 17000 | 0.11 | 5.4 | 180 | 0.15 | 720 | 15 | 27 | 26 | |
| Maximum | | 42000 | 0.16 | 15 | 320 | 0.28 | 2200 | 30 | 78 | 52 | |
| SQGV | | | 1 | 20 | NA | 1.5 | NA | NA | 80 | 65 | |
| Sediment ID | Reservoir | Fe (mg/kg) | Hg (mg/kg) | K (mg/kg) | Mg (mg/kg) | Mn (mg/kg) | Mo (mg/kg) | Na (mg/kg) | Ni (mg/kg) | Pb (mg/kg) | |
| CA1 | Talbingo | 49000 | <0.1 | 2200 | 4400 | 2200 | 0.60 | 58 | <u>44</u> | 25 | |
| CA2 | Talbingo | 44000 | <0.1 | 3400 | 5400 | 1900 | 0.63 | 51 | <u>43</u> | 24 | |
| CA3 | Talbingo | 56000 | <0.1 | 6000 | 8000 | 4000 | 0.60 | 120 | <u>68</u> | 26 | |
| PL1 | Talbingo | 45000 | <0.1 | 3100 | 6400 | 1900 | 0.56 | 83 | <u>64</u> | 22 | |
| PL2 | Talbingo | 45000 | <0.1 | 3100 | 5700 | 3000 | 0.99 | 100 | <u>56</u> | 28 | |
| PL3 | Talbingo | 57000 | <0.1 | 3400 | 5900 | 2400 | 0.67 | 120 | <u>54</u> | 27 | |
| PL3 duplicate | Talbingo | 73000 | <0.1 | 3500 | 5800 | 2500 | 0.65 | 92 | <u>54</u> | 27 | |
| PL3 Mean | Talbingo | 65000 | <0.1 | 3400 | 5800 | 2400 | 0.66 | 100 | <u>54</u> | 27 | |
| RA1 | Talbingo | 37000 | <0.1 | 1600 | 5400 | 2100 | 0.49 | 27 | <u>48</u> | 28 | |
| RA2 | Talbingo | 42000 | <0.1 | 4000 | 6400 | 2800 | 0.40 | 85 | <u>60</u> | 32 | |
| RA3 | Talbingo | 45000 | <0.1 | 2500 | 6000 | 4000 | 0.39 | 48 | <u>56</u> | 30 | |
| TN1 | Tantangara | 25000 | <0.1 | 1200 | 2200 | 540 | 0.45 | 44 | 13 | 23 | |
| TN2 | Tantangara | 39000 | <0.1 | 2400 | 2600 | 740 | 0.36 | 70 | 19 | 28 | |
| TN3 | Tantangara | 41700 | <0.1 | 3180 | 4590 | 2390 | 0.45 | 45 | <u>27</u> | 27 | |
| Minimum | | 25000 | <0.1 | 1200 | 2200 | 540 | 0.36 | 26 | 13 | 22 | |
| Maximum | | 73000 | <0.1 | 6000 | 8000 | 4000 | 0.99 | 120 | 68 | 32 | |
| SQGV | | | 0.15 | NA | NA | NA | NA | NA | 21 | 50 | |
| Sediment ID | Reservoir | Sb (mg/kg) | Se (mg/kg) | Sn (mg/kg) | Sr (mg/kg) | Th (mg/kg) | U (mg/kg) | V (mg/kg) | Zn (mg/kg) | P (mg/kg) | S (mg/kg) |
| CA1 | Talbingo | 0.43 | 0.47 | 1.3 | 27 | 12 | 3.8 | 66 | 79 | 1400 | 650 |
| CA2 | Talbingo | 0.47 | 0.44 | 1.4 | 35 | 10 | 3.2 | 63 | 81 | 1300 | 600 |
| CA3 | Talbingo | 0.51 | 0.57 | 1.9 | 33 | 14 | 4.2 | 85 | 109 | 1300 | 550 |
| PL1 | Talbingo | 0.52 | 0.48 | 1.4 | 28 | 11 | 3.2 | 66 | 92 | 1200 | 630 |
| PL2 | Talbingo | 0.56 | 0.58 | 1.7 | 31 | 12 | 4.3 | 65 | 110 | 1100 | 570 |
| PL3 | Talbingo | 0.57 | 0.56 | 1.7 | 29 | 12 | 3.9 | 67 | 99 | 1300 | 630 |
| PL3 duplicate | Talbingo | 0.52 | 0.54 | 1.6 | 29 | 12 | 3.9 | 66 | 99 | 1300 | 640 |
| PL3 Mean | Talbingo | 0.54 | 0.55 | 1.6 | 29 | 12 | 3.9 | 67 | 99 | 1300 | 640 |
| RA1 | Talbingo | 0.62 | 0.47 | 1.2 | 15 | 10 | 3.6 | 47 | 91 | 1000 | 510 |
| RA2 | Talbingo | 0.75 | 0.50 | 1.9 | 22 | 13 | 3.5 | 53 | 113 | 1000 | 510 |
| RA3 | Talbingo | 0.74 | 0.45 | 1.4 | 17 | 12 | 3.0 | 43 | 99 | 1100 | 480 |
| TN1 | Tantangara | 0.28 | 0.43 | 0.83 | 11 | 6.0 | 1.2 | 49 | 85 | 1200 | 880 |
| TN2 | Tantangara | 0.31 | 0.46 | 1.3 | 18 | 9.2 | 1.5 | 59 | 102 | 1700 | 940 |
| TN3 | Tantangara | 0.37 | 0.49 | 1.3 | 17 | 10 | 2.1 | 65 | 104 | 1305 | 762 |
| Minimum | | 0.28 | 0.43 | 0.8 | 11 | 6.0 | 1.2 | 43 | 79 | 1000 | 480 |
| Maximum | | 0.76 | 0.58 | 1.9 | 35 | 14 | 4.3 | 85 | 114 | 1700 | 940 |
| SQGV | | NA | NA | NA | NA | NA | NA | NA | 200 | NA | NA |

SQGV = the sediment quality guideline values (Simpson e al., 2013). Values are bold underline where the default GV is exceeded.

Table 6. Dilute-acid extractable concentrations of metals, metalloids, and major ions in the sediments of the Talbingo and Tantangara reservoir waters

| Sediment ID | Reservoir | Ag (mg/kg) | Al (mg/kg) | As (mg/kg) | Ba (mg/kg) | Ca (mg/kg) | Cd (mg/kg) | Co (mg/kg) | Cr (mg/kg) | Cu (mg/kg) | |
|-------------|------------|---------------|------------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|--------------|
| CA1 | Talbingo | 0.068 | 4740 | 3.85 | 205 | 1630 | 0.161 | 19.0 | 8.57 | 21.2 | |
| CA2 | Talbingo | 0.046 | 4280 | 3.12 | 208 | 1660 | 0.096 | 13.6 | 7.40 | 18.6 | |
| CA3 | Talbingo | 0.065 | 5020 | 3.82 | 210 | 1420 | 0.194 | 16.7 | 7.89 | 23.3 | |
| PL1 | Talbingo | 0.047 | 4550 | 3.04 | 168 | 1360 | 0.077 | 16.5 | 7.19 | 20.7 | |
| PL2 | Talbingo | 0.071 | 4590 | 3.27 | 174 | 1650 | 0.187 | 15.2 | 6.46 | 24.4 | |
| PL3 | Talbingo | 0.074 | 4600 | 4.45 | 169 | 1160 | 0.187 | 19.0 | 7.08 | 23.0 | |
| RA1 | Talbingo | 0.061 | 4280 | 3.92 | 205 | 1340 | 0.179 | 15.6 | 5.74 | 26.8 | |
| RA2 | Talbingo | 0.045 | 3910 | 4.58 | 213 | 1410 | 0.251 | 16.2 | 6.68 | 24.5 | |
| RA3 | Talbingo | 0.061 | 3460 | 6.60 | 260 | 1520 | 0.215 | 16.8 | 6.04 | 25.2 | |
| TN1 | Tantangara | 0.039 | 3620 | 1.81 | 141 | 661 | 0.192 | 7.19 | 3.05 | 13.0 | |
| TN2 | Tantangara | 0.085 | 3980 | 2.09 | 164 | 760 | 0.229 | 13.3 | 5.84 | 14.3 | |
| TN3 | Tantangara | 0.074 | 4460 | 2.81 | 158 | 649 | 0.310 | 15.6 | 6.30 | 14.8 | |
| Minimum | | 0.039 | 3460 | 1.81 | 141 | 649 | 0.077 | 7.19 | 3.05 | 13 | |
| Maximum | | 0.085 | 5020 | 6.6 | 260 | 1660 | 0.31 | 19 | 8.57 | 26.8 | |
| SQGV | | 1 | NA | 20 | NA | NA | 1.5 | NA | 80 | 65 | |
| Sediment ID | Reservoir | Fe (mg/kg) | Hg (mg/kg) | K (mg/kg) | Mg (mg/kg) | Mn (mg/kg) | Mo (mg/kg) | Na (mg/kg) | Ni (mg/kg) | Pb (mg/kg) | |
| CA1 | Talbingo | 23500 | <0.008 | 248 | 356 | 1910 | <0.071 | 70.7 | 8.97 | 17.4 | |
| CA2 | Talbingo | 17300 | <0.008 | 389 | 560 | 1630 | <0.071 | 77.2 | 8.01 | 16.0 | |
| CA3 | Talbingo | 16800 | <0.008 | 467 | 488 | 3360 | <0.071 | 58.7 | 10.3 | 17.3 | |
| PL1 | Talbingo | 17000 | <0.008 | 263 | 463 | 1690 | <0.071 | 71.6 | 9.33 | 15.4 | |
| PL2 | Talbingo | 15900 | <0.008 | 245 | 336 | 2490 | 0.084 | 56.6 | 8.50 | 19.4 | |
| PL3 | Talbingo | 25100 | <0.008 | 294 | 384 | 2110 | 0.12 | 68.7 | 7.11 | 17.5 | |
| RA1 | Talbingo | 14400 | <0.008 | 217 | 246 | 1920 | <0.071 | 63.3 | 8.05 | 21.3 | |
| RA2 | Talbingo | 14700 | <0.008 | 209 | 239 | 2540 | <0.071 | 59.5 | 9.33 | 22.1 | |
| RA3 | Talbingo | 17800 | <0.008 | 193 | 201 | 3640 | 0.098 | 76.8 | 8.83 | 21.0 | |
| TN1 | Tantangara | 12400 | <0.008 | 154 | 189 | 470 | <0.071 | 55.8 | 2.40 | 15.0 | |
| TN2 | Tantangara | 20200 | <0.008 | 208 | 195 | 646 | 0.079 | <41.8 | 3.42 | 18.5 | |
| TN3 | Tantangara | 21900 | <0.008 | 163 | 172 | 753 | <0.071 | 47.2 | 3.93 | 19.5 | |
| Minimum | | 12400 | <0.008 | 154 | 172 | 470 | 0.079 | 47.2 | 2.4 | 15 | |
| Maximum | | 25100 | <0.008 | 467 | 560 | 3640 | 0.12 | 77.2 | 10.3 | 22.1 | |
| SQGV | | NA | 0.15 | NA | NA | NA | NA | NA | 21 | 50 | |
| Sediment ID | Reservoir | Sb (mg/kg) | Se (mg/kg) | Sn (mg/kg) | Sr (mg/kg) | Th (mg/kg) | U (mg/kg) | V (mg/kg) | Zn (mg/kg) | P (mg/kg) | S (mg/kg) |
| CA1 | Talbingo | <0.024 | 0.044 | 0.238 | 16.6 | 0.324 | 1.97 | 32.7 | 32.3 | 921 | <43.6 |
| CA2 | Talbingo | <0.024 | 0.034 | 0.209 | 26.3 | 0.165 | 1.27 | 28.5 | 27.4 | 771 | 62.5 |
| CA3 | Talbingo | 0.047 | 0.032 | 0.201 | 12.5 | 0.347 | 2.65 | 29.8 | 34.6 | 708 | 45.5 |
| PL1 | Talbingo | 0.034 | 0.044 | 0.160 | 11.8 | 0.218 | 1.52 | 29.7 | 30.4 | 686 | 43.8 |
| PL2 | Talbingo | 0.039 | 0.043 | 0.089 | 15.1 | 0.250 | 2.35 | 30.7 | 37.3 | 583 | <43.6 |
| PL3 | Talbingo | 0.028 | 0.032 | 0.152 | 13.3 | 0.299 | 2.23 | 28.4 | 33.0 | 705 | <43.6 |
| RA1 | Talbingo | 0.037 | 0.028 | 0.170 | 10.1 | 0.284 | 2.19 | 24.4 | 36.6 | 573 | <43.6 |
| RA2 | Talbingo | 0.034 | 0.034 | 0.191 | 10.9 | 0.160 | 1.20 | 22.2 | 30.9 | 584 | <43.6 |
| RA3 | Talbingo | 0.039 | 0.043 | 0.210 | 10.8 | 0.254 | 1.38 | 19.2 | 28.2 | 638 | <43.6 |
| TN1 | Tantangara | 0.029 | 0.023 | 0.107 | 7.72 | 0.070 | 0.451 | 30.8 | 49.1 | 545 | 76.7 |
| TN2 | Tantangara | <0.024 | 0.033 | 0.282 | 8.43 | 0.057 | 0.688 | 33.4 | 43.4 | 1090 | 104 |
| TN3 | Tantangara | 0.033 | 0.038 | 0.219 | 7.2 | 0.113 | 0.638 | 37.1 | 54.6 | 890 | 124 |
| Minimum | | 0.028 | 0.023 | 0.089 | 7.2 | 0.057 | 0.451 | 19.2 | 27.4 | 545 | 43.8 |
| Maximum | | 0.047 | 0.044 | 0.282 | 26.3 | 0.347 | 2.65 | 37.1 | 54.6 | 1090 | 124 |
| SQGV | | NA | NA | NA | NA | NA | NA | NA | 200 | NA | NA |

SQGV = the sediment quality guideline values (Simpson e al., 2013). Values are bold underline where the default GV is exceeded.

Summary

The concentrations of many of the parameters often differed between the two reservoirs.

There were no exceedances of diluted-extractable metal, metalloid or major cation concentrations above SQGV's.

References

Rayment, G.E and Lyons, D.J. (2011). Exchangeable bases and CEC (method 15D2). In 'Soil Chemical Methods - Australasia'. (CSIRO publishing, Melbourne). pp 318-321.

Simpson SL and Batley GE (2016) Sediment Quality Assessment: A Practical Guide. CSIRO Publishing, Melbourne, Victoria. 359 p. <https://publications.csiro.au/rpr/download?pid=csiro:EP165955&dsid=DS1>

Vangheluwe MLU, Verdonck FAM, Besser JM, Brumbaugh WG, Ingersoll CG, Schlekot CE, Garman ER (2013) Improving sediment-quality guidelines for nickel: Development and application of predictive bioavailability models to assess chronic toxicity of nickel in freshwater sediments. Environmental Toxicology and Chemistry 32, 2507–2519.

Sediment analyses Total recoverable metals (TRM)

| Sample ID | Sample Description | TRM µg/g | TRM µg/g | TRM µg/g | TRM µg/g | TRM µg/g | TRM µg/g | TRM µg/g | TRM µg/g | TRM µg/g | TRM µg/g | TRM µg/g | TRM µg/g | TRM µg/g | TRM µg/g | TRM µg/g | TRM µg/g |
|------------------|------------------------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|
| | | Sr | Ta | Tb | Te | Th | Ti | Ti | Ti | Tm | U | V | W | Y | Yb | Zn | Zr |
| CE491-8 | TN2_P4 - 19 metres | 18 | 0.003 | 0.84 | 0.03 | 9.2 | 92 | 92 | 0.40 | 0.30 | 1.5 | 59 | 0.079 | 23 | 1.8 | 102 | 12 |
| CE491-9 | TN1_P4 - 16.5 metres | 11 | 0.004 | 0.71 | 0.02 | 6.0 | 40 | 40 | 0.26 | 0.25 | 1.2 | 49 | 0.092 | 20 | 1.5 | 85 | 5.3 |
| CE491-10 | TN3_P4 - 18.5 metres | 12 | 0.003 | 0.81 | 0.02 | 9.0 | 47 | 47 | 0.32 | 0.30 | 1.4 | 57 | 0.10 | 22 | 1.7 | 97 | 9.0 |
| CE491-10 dup | TN3_P4 - 18.5 metres dig dup | 23 | 0.005 | 0.92 | 0.05 | 11 | 416 | 416 | 0.51 | 0.30 | 3.9 | 73 | 0.34 | 23 | 1.7 | 93 | 11 |
| CE491-10 average | TN3_P4 - 18.5 metres avg | 18 | 0.004 | 0.87 | 0.03 | 10 | 232 | 232 | 0.42 | 0.29 | 2.6 | 65 | 0.22 | 23 | 1.7 | 95 | 10 |
| CE491-10 | TN3_P4 - 18.5 metres | 17 | 0.010 | 0.81 | 0.02 | 9.5 | 116 | 116 | 0.39 | 0.28 | 1.6 | 63 | 0.08 | 22 | 1.7 | 110 | 9.9 |
| CE491-10 dup | TN3_P4 - 18.5 metres dig dup | 19 | 0.006 | 0.85 | 0.03 | 10 | 184 | 184 | 0.44 | 0.30 | 1.7 | 67 | 0.08 | 23 | 1.8 | 115 | 12 |
| CE491-10 average | TN3_P4 - 18.5 metres avg | 18 | 0.008 | 0.83 | 0.03 | 9.9 | 150 | 150 | 0.42 | 0.29 | 1.6 | 65 | 0.08 | 22 | 1.7 | 113 | 11 |
| CE491-11 | CA3_P4 - 48 metres | 33 | 0.006 | 1.1 | 0.06 | 14 | 894 | 894 | 0.61 | 0.33 | 4.2 | 85 | 0.17 | 26 | 1.9 | 109 | 17 |
| CE491-12 | RA1_P4 - 31.5 metres | 15 | 0.005 | 0.87 | 0.03 | 10 | 94 | 94 | 0.29 | 0.29 | 3.6 | 47 | 0.39 | 23 | 1.7 | 90 | 8.0 |
| CE491-12 | RA1_P4 - 31.5 metres dli dup | 14 | 0.005 | 0.89 | 0.05 | 10 | 93 | 93 | 0.30 | 0.29 | 3.6 | 46 | 0.37 | 22 | 1.7 | 92 | 8.1 |
| CE491-12 average | RA1_P4 - 31.5 metres avg | 15 | 0.005 | 0.88 | 0.04 | 10 | 94 | 94 | 0.29 | 0.29 | 3.6 | 47 | 0.38 | 22 | 1.7 | 91 | 8.1 |
| CE491-13 | PL1_P4 - 33.5 metres | 28 | 0.003 | 0.83 | 0.03 | 11 | 302 | 302 | 0.36 | 0.27 | 3.2 | 66 | 0.18 | 21 | 1.6 | 92 | 9.2 |
| CE491-14 | CA1_P4 - 30 metres | 27 | 0.008 | 1.0 | 0.03 | 12 | 231 | 231 | 0.37 | 0.34 | 3.8 | 66 | 0.33 | 26 | 2.0 | 79 | 11 |
| CE491-15 | PL3_P4 - 27 metres | 29 | 0.002 | 0.93 | 0.03 | 12 | 279 | 279 | 0.37 | 0.30 | 3.9 | 67 | 0.19 | 23 | 1.7 | 99 | 14 |
| CE491-15 Dup | PL3_P4 - 27 metres dig dup | 29 | 0.003 | 0.92 | 0.02 | 12 | 258 | 258 | 0.37 | 0.30 | 3.9 | 66 | 0.13 | 23 | 1.8 | 99 | 12 |
| CE491-15 average | PL3_P4 - 27 metres avg | 29 | 0.003 | 0.92 | 0.03 | 12 | 268 | 268 | 0.37 | 0.30 | 3.9 | 67 | 0.16 | 23 | 1.8 | 99 | 13 |
| CE491-16 | RA3_P4 - 28.5 metres | 17 | 0.002 | 0.95 | 0.03 | 12 | 159 | 159 | 0.35 | 0.30 | 3.0 | 43 | 0.25 | 23 | 1.8 | 99 | 13 |
| CE491-17 | PL2_P4 - 26.5 metres | 31 | 0.004 | 0.96 | 0.02 | 12 | 262 | 262 | 0.40 | 0.31 | 4.3 | 65 | 0.22 | 24 | 1.8 | 110 | 13 |
| CE491-18 | CA2_P4 - 42 metres | 35 | 0.006 | 0.92 | 0.02 | 10 | 307 | 307 | 0.36 | 0.28 | 3.2 | 63 | 0.31 | 23 | 1.6 | 81 | 10 |
| CE491-19 | RA2_P4 - 29 metres | 22 | 0.003 | 1.0 | 0.02 | 13 | 312 | 312 | 0.47 | 0.34 | 3.4 | 53 | 0.15 | 25 | 2.0 | 112 | 13 |
| CE491-19 | RA2_P4 - 29 metres dli dup | 22 | 0.003 | 1.0 | 0.03 | 13 | 315 | 315 | 0.46 | 0.33 | 3.5 | 53 | 0.15 | 26 | 2.0 | 114 | 13 |
| CE491-19 average | RA2_P4 - 29 metres avg | 22 | 0.003 | 1.0 | 0.03 | 13 | 313 | 313 | 0.46 | 0.34 | 3.5 | 53 | 0.15 | 25 | 2.0 | 113 | 13 |
| LOD 3σ | --- | 0.01 | 0.001 | 0.0001 | 0.01 | 0.002 | 0.2 | 0.004 | 0.0001 | 0.0001 | 0.001 | 0.3 | 0.001 | 0.001 | 0.001 | 1 | 0.01 |
| Method Code: | --- | C-223/C-229 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-229 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-229 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-209 |

Certified Reference Materials

| Sample ID | Sample Description | TRM µg/g | TRM µg/g | TRM µg/g | TRM µg/g | TRM µg/g | TRM µg/g | TRM µg/g | TRM µg/g | TRM µg/g | TRM µg/g | TRM µg/g | TRM µg/g | TRM µg/g | TRM µg/g | TRM µg/g | TRM µg/g |
|-------------------|--------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|------------|----------|----------|----------|----------|----------|
| | | Sr | Ta | Tb | Te | Th | Ti | Ti | Ti | Tm | U | V | W | Y | Yb | Zn | Zr |
| ERM-CC018-1 | | 73 | 0.009 | 0.16 | 0.03 | 15 | 134 | 134 | 0.18 | 0.060 | 0.98 | 15 | 2.0 | 5.9 | 0.37 | 261 | 14 |
| ERM-CC018-1 | ERM-CC018-1 | 72 | 0.008 | 0.16 | 0.02 | 1.92 | 133 | 133 | 0.18 | 0.058 | 0.98 | 15 | 2.0 | 5.7 | 0.37 | 264 | 14 |
| ERM-CC018-2 | ERM-CC018-2 | 74 | 0.007 | 0.16 | 0.03 | 1.95 | 132 | 132 | 0.17 | 0.061 | 0.99 | 15 | 1.9 | 5.8 | 0.38 | 270 | 13 |
| ERM-CC018 average | | 73 | 0.008 | 0.16 | 0.03 | 1.94 | 133 | 133 | 0.18 | 0.060 | 0.99 | 15 | 2.0 | 5.8 | 0.37 | 265 | 14 |
| Certified Value | | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | 19.4 ± 1.0 | --- | --- | --- | 313 ± 13 | --- |
| OREAS-25a-1 | OREAS-25a-1 | 19 | 0.001 | 0.30 | 0.03 | 12.3 | 682 | 682 | 0.28 | 0.084 | 1.55 | 122 | 0.084 | 6.0 | 0.51 | 37 | 36 |
| OREAS-25a-2 | OREAS-25a-2 | 17 | 0.004 | 0.28 | 0.04 | 12.2 | 513 | 513 | 0.25 | 0.075 | 1.51 | 118 | 0.045 | 5.4 | 0.50 | 34 | 34 |
| OREAS-25a average | | 18 | 0.002 | 0.29 | 0.04 | 12.3 | 597 | 597 | 0.27 | 0.080 | 1.53 | 120 | 0.045 | 5.7 | 0.51 | 36 | 35 |
| Certified Value | | 17.3 | --- | --- | --- | 10.7 | --- | --- | 0.20 | --- | 1.49 | 117 | --- | 4.56 | --- | 30.1 | --- |

ERM-CC018 is a European sandy soil reference material

Spike Recoveries

| Sample ID | Sample Description | % | % | % | % | % | % | % | % | % | % | % | % | % | % | % | % |
|-----------|----------------------|----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----|-----|-----|-----|-----|-----|
| | | Sr | Ta | Tb | Te | Th | Ti | Ti | Ti | Tm | U | V | W | Y | Yb | Zn | Zr |
| CE491-12 | RA1_P4 - 31.5 metres | 98 | 111 | 108 | 103 | --- | 102 | 108 | 108 | 108 | 97 | 96 | 105 | 107 | 107 | 113 | 104 |
| CE491-19 | RA2_P4 - 29 metres | 97 | 91 | 107 | 101 | --- | 100 | 105 | 107 | 107 | 104 | 96 | 105 | 106 | 107 | 108 | 102 |

Analyte of interest added to sample prior to analysis

Sediment analyses

Dilute-acid extractable metals (AEM)

| Sample ID | Sample Description | Ca | K | Mg | Na | Ag | Al | As | Au | B | Ba | Be | Bi | Cd | Ce | Co | Cr | Cs | Cu | Dy | Er | Eu | Fe |
|-----------|--------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) |
| CE491-8 | TN2_P4 | 760 | 208 | 195 | <41.8 | 0.085 | 3980 | 2.09 | <0.005 | 1.08 | 164 | 1.16 | 0.273 | 0.229 | 41.9 | 13.3 | 5.84 | 0.149 | 14.3 | 3.61 | 1.86 | 0.911 | 20200 |
| CE491-9 | TN1_P4 | 661 | 154 | 189 | 55.8 | 0.039 | 3620 | 1.81 | <0.005 | <0.816 | 141 | 0.956 | 0.193 | 0.192 | 32.4 | 7.19 | 3.05 | 0.093 | 13 | 2.87 | 1.42 | 0.702 | 12400 |
| CE491-10 | TN3_P4 | 649 | 163 | 172 | 47.2 | 0.074 | 4460 | 2.81 | <0.005 | 0.927 | 158 | 1.18 | 0.267 | 0.31 | 42 | 15.6 | 6.3 | 0.141 | 14.8 | 3.55 | 1.84 | 0.888 | 21900 |
| CE491-11 | CA3_P4 | 1420 | 467 | 488 | 58.7 | 0.065 | 5020 | 3.82 | <0.005 | 1.07 | 210 | 1.25 | 0.339 | 0.194 | 54.3 | 16.7 | 7.89 | 0.502 | 23.3 | 3.77 | 1.87 | 1.05 | 16800 |
| CE491-12 | RA1_P4 | 1340 | 217 | 246 | 63.3 | 0.061 | 4280 | 3.92 | <0.005 | 0.874 | 205 | 1.36 | 0.479 | 0.179 | 46.2 | 15.6 | 5.74 | 0.615 | 26.8 | 3.65 | 1.84 | 0.954 | 14400 |
| CE491-13 | PL1_P4 | 1360 | 263 | 463 | 71.6 | 0.047 | 4550 | 3.04 | 0.01 | 1.24 | 168 | 1.14 | 0.293 | 0.077 | 44.2 | 16.5 | 7.19 | 0.391 | 20.7 | 3.13 | 1.56 | 0.851 | 17000 |
| CE491-14 | CA1_P4 | 1630 | 248 | 356 | 70.7 | 0.068 | 4740 | 3.85 | 0.006 | 1.3 | 205 | 1.41 | 0.327 | 0.161 | 60.8 | 19 | 8.57 | 0.407 | 21.2 | 4.31 | 2.12 | 1.17 | 23500 |
| CE491-15 | PL3_P4 | 1160 | 294 | 384 | 68.7 | 0.074 | 4600 | 4.45 | <0.005 | 1.1 | 169 | 1.26 | 0.363 | 0.187 | 48.2 | 19 | 7.08 | 0.569 | 23 | 3.38 | 1.7 | 0.929 | 25100 |
| CE491-16 | RA3_P4 | 1520 | 193 | 201 | 76.8 | 0.061 | 3460 | 6.6 | <0.005 | 0.961 | 260 | 1.28 | 0.492 | 0.215 | 41.6 | 16.8 | 6.04 | 0.817 | 25.2 | 3.61 | 1.82 | 0.953 | 17800 |
| CE491-17 | PL2_P4 | 1650 | 245 | 336 | 56.6 | 0.071 | 4590 | 3.27 | <0.005 | 0.991 | 174 | 1.34 | 0.375 | 0.187 | 50.8 | 15.2 | 6.46 | 0.509 | 24.4 | 3.6 | 1.8 | 0.956 | 15900 |
| CE491-18 | CA2_P4 | 1660 | 389 | 560 | 77.2 | 0.046 | 4280 | 3.12 | <0.005 | 1.08 | 208 | 1.2 | 0.279 | 0.096 | 47.3 | 13.6 | 7.4 | 0.341 | 18.6 | 3.49 | 1.72 | 0.984 | 17300 |
| CE491-19 | RA2_P4 | 1410 | 209 | 239 | 59.5 | 0.045 | 3910 | 4.58 | <0.005 | 0.945 | 213 | 1.48 | 0.46 | 0.251 | 47.5 | 16.2 | 6.68 | 0.767 | 24.5 | 3.94 | 1.95 | 1.02 | 14700 |

| Lab ID | Client ID | Ca | K | Mg | Na | Ag | Al | As | Au | B | Ba | Be | Bi | Cd | Ce | Co | Cr | Cs | Cu | Dy | Er | Eu | Fe |
|--------------|----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) |
| LOD 3σ | Avg AEM+28 Blk | 2.16 | -0.988 | 2.46 | 13.4 | 0.000 | 1.53 | 0.000 | 0.000 | 0.000 | 0.058 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 1.28 |
| Method Code: | LOD (3 x S.D.) | 7.08 | 16.2 | 13.5 | 41.8 | 0.001 | 2.53 | 0.023 | 0.005 | 0.816 | 0.123 | 0.002 | 0.004 | 0.039 | 0.002 | 0.004 | 0.145 | 0.003 | 0.065 | 0.000 | 0.000 | 0.001 | 2.9 |

Certified Reference Materials

| Lab ID | Client ID | Ca | K | Mg | Na | Ag | Al | As | Au | B | Ba | Be | Bi | Cd | Ce | Co | Cr | Cs | Cu | Dy | Er | Eu | Fe |
|----------------|-----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) |
| ERM-CCO18-1 | | 17900 | 405 | 640 | 85.2 | 1.51 | 2460 | 16.5 | 0.005 | 3.71 | 276 | 0.295 | 1.01 | 5.48 | 8.12 | 2.47 | 41.3 | 0.173 | 62.6 | 0.52 | 0.275 | 0.158 | 3140 |
| ERM-CCO18-2 | | 18000 | 402 | 647 | 88.3 | 1.64 | 2420 | 15.8 | 0.003 | 4.25 | 281 | 0.314 | 1.14 | 5.46 | 8.61 | 2.46 | 41.7 | 0.18 | 61.7 | 0.548 | 0.292 | 0.172 | 3140 |
| ERM-CCO18 Mean | | 17950 | 404 | 644 | 86.8 | 1.57 | 2440 | 16.2 | 0.004 | 3.98 | 279 | 0.304 | 1.07 | 5.47 | 8.37 | 2.47 | 41.5 | 0.177 | 62.2 | 0.534 | 0.284 | 0.165 | 3140 |
| In-house mean | | | | | | 1.446 | 2470 | 17.2 | | | 277 | | | 5.5 | | 2.8 | 44.0 | | 61.8 | | | | 3270 |
| % recovery (%) | | | | | | 109 | 99 | 94 | | | 101 | | | 99 | | 89 | 94 | | 101 | | | | 96 |

Spike Recoveries

| Lab ID | Client ID | Ca | K | Mg | Na | Ag | Al | As | Au | B | Ba | Be | Bi | Cd | Ce | Co | Cr | Cs | Cu | Dy | Er | Eu | Fe |
|---------------|-----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) |
| CE491-12 | RA1_P4 | 104 | 103 | 101 | 103 | 108 | 93 | 108 | 103 | 101 | 98 | 110 | 111 | 108 | 116 | 108 | 107 | 112 | 107 | 110 | 109 | 109 | 71 |
| CE491-19 | RA2_P4 | 100 | 102 | 97 | 99 | 103 | 96 | 107 | 91 | 100 | 99 | 106 | 106 | 106 | 107 | 103 | 104 | 108 | 104 | 105 | 105 | 105 | 77 |
| CE491-10 | TN3_P4 | 612 | 162 | 165 | <41.8 | 0.085 | 4430 | 2.69 | <0.005 | 0.879 | 158 | 1.15 | 0.281 | 0.218 | 42.4 | 15.8 | 6.31 | 0.141 | 15.4 | 3.58 | 1.83 | 0.884 | 21800 |
| CE491-10 Dup | TN3_P4 | 687 | 164 | 179 | 66.1 | 0.064 | 4480 | 2.94 | <0.005 | 0.974 | 159 | 1.21 | 0.252 | 0.402 | 41.6 | 15.4 | 6.3 | 0.141 | 14.3 | 3.52 | 1.85 | 0.892 | 21900 |
| CE491-10 Mean | TN3_P4 | 649 | 163 | 172 | 47.2 | 0.074 | 4460 | 2.81 | <0.005 | 0.927 | 158 | 1.18 | 0.267 | 0.31 | 42 | 15.6 | 6.3 | 0.141 | 14.8 | 3.55 | 1.84 | 0.888 | 21900 |
| CE491-15 | PL3_P4 | 1170 | 303 | 384 | 69.5 | 0.084 | 4610 | 4.65 | <0.005 | 1 | 170 | 1.22 | 0.356 | 0.22 | 48.4 | 19.4 | 7.16 | 0.574 | 23.7 | 3.42 | 1.71 | 0.937 | 25100 |
| CE491-15 Dup | PL3_P4 | 1160 | 284 | 383 | 67.9 | 0.065 | 4590 | 4.25 | <0.005 | 1.2 | 167 | 1.3 | 0.37 | 0.154 | 48 | 18.6 | 7.01 | 0.564 | 22.2 | 3.35 | 1.68 | 0.92 | 25000 |
| CE491-15 Mean | PL3_P4 | 1160 | 294 | 384 | 68.7 | 0.074 | 4600 | 4.45 | <0.005 | 1.1 | 169 | 1.26 | 0.363 | 0.187 | 48.2 | 19 | 7.08 | 0.569 | 23 | 3.38 | 1.7 | 0.929 | 25100 |

Sediment analyses

Dilute-acid extractable metals (AEM)

| Sample ID | Sample Description | Ga | Gd | Ge | Hf | Hg | Ho | In | Ir | La | Li | Lu | Mn | Mo | Nb | Nd | Ni | Os | P | Pb | Pd | Pr | Pt | Rb |
|-----------|--------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) |
| CE491-8 | TN2_P4 | 1.05 | 4.13 | <0.086 | 0.086 | <0.008 | 0.692 | 0.029 | <0.004 | 15.2 | 0.144 | 0.191 | 646 | 0.079 | <0.055 | 17.8 | 3.42 | <0.098 | 1090 | 18.5 | 0.176 | 4.35 | <0.006 | 1.86 |
| CE491-9 | TN1_P4 | 0.897 | 3.24 | <0.086 | 0.044 | <0.008 | 0.544 | 0.018 | <0.004 | 12.1 | 0.118 | 0.14 | 470 | <0.071 | <0.055 | 14 | 2.4 | <0.098 | 545 | 15 | 0.128 | 3.38 | <0.006 | 2.4 |
| CE491-10 | TN3_P4 | 1.26 | 4.03 | <0.086 | 0.078 | <0.008 | 0.686 | 0.021 | <0.004 | 15 | 0.135 | 0.189 | 753 | <0.071 | <0.055 | 17.5 | 3.93 | <0.098 | 890 | 19.5 | 0.185 | 4.23 | <0.006 | 2.35 |
| CE491-11 | CA3_P4 | 1.28 | 4.65 | <0.086 | 0.053 | <0.008 | 0.71 | 0.017 | <0.004 | 22.2 | 0.192 | 0.189 | 3360 | <0.071 | 0.085 | 22.2 | 10.3 | <0.098 | 708 | 17.3 | 0.186 | 5.63 | <0.006 | 4.1 |
| CE491-12 | RA1_P4 | 1.02 | 4.54 | <0.086 | 0.047 | <0.008 | 0.693 | 0.018 | <0.004 | 18.8 | 0.451 | 0.184 | 1920 | <0.071 | <0.055 | 20 | 8.05 | <0.098 | 573 | 21.3 | 0.173 | 4.97 | <0.006 | 2.55 |
| CE491-13 | PL1_P4 | 1.21 | 3.83 | <0.086 | 0.05 | <0.008 | 0.593 | 0.023 | <0.004 | 17.5 | 0.631 | 0.162 | 1690 | <0.071 | <0.055 | 17.7 | 9.33 | <0.098 | 686 | 15.4 | 0.159 | 4.43 | <0.006 | 1.7 |
| CE491-14 | CA1_P4 | 1.18 | 5.24 | <0.086 | 0.052 | <0.008 | 0.805 | 0.02 | <0.004 | 25 | 0.448 | 0.207 | 1910 | <0.071 | 0.09 | 24.9 | 8.97 | <0.098 | 921 | 17.4 | 0.199 | 6.33 | <0.006 | 3.12 |
| CE491-15 | PL3_P4 | 1.11 | 4.16 | <0.086 | 0.054 | <0.008 | 0.635 | 0.017 | <0.004 | 18.7 | 0.496 | 0.17 | 2110 | 0.12 | <0.055 | 19.7 | 7.11 | <0.098 | 705 | 17.5 | 0.162 | 4.85 | <0.006 | 2.82 |
| CE491-16 | RA3_P4 | 0.829 | 4.53 | <0.086 | 0.043 | <0.008 | 0.692 | 0.015 | <0.004 | 17.5 | 0.466 | 0.187 | 3640 | 0.098 | <0.055 | 19.5 | 8.83 | <0.098 | 638 | 21 | 0.157 | 4.78 | <0.006 | 3.53 |
| CE491-17 | PL2_P4 | 1.13 | 4.45 | <0.086 | 0.05 | <0.008 | 0.679 | 0.018 | <0.004 | 19.6 | 0.474 | 0.183 | 2490 | 0.084 | <0.055 | 20.4 | 8.5 | <0.098 | 583 | 19.4 | 0.172 | 5.08 | <0.006 | 3.17 |
| CE491-18 | CA2_P4 | 1.1 | 4.38 | <0.086 | 0.044 | <0.008 | 0.65 | 0.014 | <0.004 | 20.3 | 0.663 | 0.167 | 1630 | <0.071 | 0.078 | 20.5 | 8.01 | <0.098 | 771 | 16 | 0.174 | 5.14 | <0.006 | 3.33 |
| CE491-19 | RA2_P4 | 1.01 | 4.94 | <0.086 | 0.048 | <0.008 | 0.751 | 0.016 | <0.004 | 19.5 | 0.55 | 0.206 | 2540 | <0.071 | 0.056 | 21.5 | 9.33 | <0.098 | 584 | 22.1 | 0.182 | 5.22 | <0.006 | 3.45 |

| Lab ID | Client ID | Ga | Gd | Ge | Hf | Hg | Ho | In | Ir | La | Li | Lu | Mn | Mo | Nb | Nd | Ni | Os | P | Pb | Pd | Pr | Pt | Rb |
|--------------|----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) |
| LOD 3σ | Avg AEM-28 Blk | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.04 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | -0.385 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| Method Code: | LOD (3 x S.D.) | 0.002 | 0.001 | 0.086 | 0.010 | 0.008 | 0.000 | 0.003 | 0.004 | 0.001 | 0.011 | 0.001 | 0.148 | 0.1 | 0.055 | 0.002 | 0.116 | 0.098 | 8.25 | 0.037 | 0.003 | 0.000 | 0.006 | 0.150 |

Certified Reference Materials

| Lab ID | Client ID | Ga | Gd | Ge | Hf | Hg | Ho | In | Ir | La | Li | Lu | Mn | Mo | Nb | Nd | Ni | Os | P | Pb | Pd | Pr | Pt | Rb |
|----------------|-----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) |
| ERM-CCO18-1 | | 0.875 | 0.656 | 0.721 | 0.172 | 0.079 | 0.101 | 0.054 | 0 | 3.62 | 1.82 | 0.031 | 134 | 7.91 | 0.123 | 3.33 | 13.7 | -0.046 | 759 | 289 | 0.058 | 0.845 | 0.001 | 2.03 |
| ERM-CCO18-2 | | 0.853 | 0.718 | 0.617 | 0.19 | 0.085 | 0.108 | 0.053 | 0.002 | 3.85 | 1.93 | 0.035 | 133 | 7.99 | 0.171 | 3.48 | 13.4 | -0.029 | 757 | 308 | 0.059 | 0.898 | 0.003 | 1.8 |
| ERM-CCO18 Mean | | 0.864 | 0.687 | 0.669 | 0.181 | 0.082 | 0.104 | 0.053 | 0.001 | 3.73 | 1.87 | 0.033 | 133 | 7.95 | 0.147 | 3.4 | 13.5 | -0.037 | 758 | 298 | 0.059 | 0.872 | 0.002 | 1.92 |
| In-house mean | | | | | | 0.090 | | | | | | | 137 | 7.8 | | | 13.8 | | | 266.5 | | | | |
| % recovery (%) | | | | | | 92 | | | | | | | 98 | 102 | | | 98 | | | 112 | | | | |

Spike Recoveries

| Lab ID | Client ID | Ga | Gd | Ge | Hf | Hg | Ho | In | Ir | La | Li | Lu | Mn | Mo | Nb | Nd | Ni | Os | P | Pb | Pd | Pr | Pt | Rb |
|---------------|-----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) |
| CE491-12 | RA1_P4 | 113 | 110 | 113 | 110 | - | 112 | 111 | 111 | 113 | 109 | 110 | 90 | 108 | 112 | 110 | 105 | 126 | 100 | 111 | 108 | 113 | 109 | 102 |
| CE491-19 | RA2_P4 | 111 | 104 | 111 | 106 | - | 108 | 105 | 106 | 107 | 105 | 107 | 93 | 105 | 106 | 104 | 100 | 121 | 100 | 104 | 104 | 110 | 104 | 99 |
| CE491-10 | TN3_P4 | 1.25 | 4.05 | <0.086 | 0.08 | <0.008 | 0.687 | 0.02 | <0.004 | 15 | 0.137 | 0.191 | 754 | <0.071 | <0.055 | 17.7 | 4.07 | <0.098 | 889 | 19.6 | 0.176 | 4.24 | <0.006 | 2.45 |
| CE491-10 Dup | TN3_P4 | 1.28 | 4 | <0.086 | 0.075 | <0.008 | 0.685 | 0.023 | <0.004 | 14.9 | 0.133 | 0.187 | 751 | <0.071 | <0.055 | 17.4 | 3.8 | <0.098 | 891 | 19.4 | 0.195 | 4.22 | <0.006 | 2.25 |
| CE491-10 Mean | TN3_P4 | 1.26 | 4.03 | <0.086 | 0.078 | <0.008 | 0.686 | 0.021 | <0.004 | 15 | 0.135 | 0.189 | 753 | <0.071 | <0.055 | 17.5 | 3.93 | <0.098 | 890 | 19.5 | 0.185 | 4.23 | <0.006 | 2.35 |
| CE491-15 | PL3_P4 | 1.13 | 4.18 | <0.086 | 0.06 | <0.008 | 0.637 | 0.018 | <0.004 | 18.9 | 0.487 | 0.171 | 2130 | 0.12 | <0.055 | 19.8 | 7.26 | <0.098 | 705 | 17.3 | 0.165 | 4.85 | <0.006 | 3.15 |
| CE491-15 Dup | PL3_P4 | 1.08 | 4.13 | <0.086 | 0.048 | <0.008 | 0.634 | 0.017 | <0.004 | 18.6 | 0.504 | 0.169 | 2090 | 0.12 | <0.055 | 19.5 | 6.96 | <0.098 | 704 | 17.6 | 0.16 | 4.85 | <0.006 | 2.5 |
| CE491-15 Mean | PL3_P4 | 1.11 | 4.16 | <0.086 | 0.054 | <0.008 | 0.635 | 0.017 | <0.004 | 18.7 | 0.496 | 0.17 | 2110 | 0.12 | <0.055 | 19.7 | 7.11 | <0.098 | 705 | 17.5 | 0.162 | 4.85 | <0.006 | 2.82 |

Sediment analyses

Dilute-acid extractable metals (AEM)

| Sample ID | Sample Description | Re | Rh | Ru | S | Sb | Sc | Se | Sm | Sn | Sr | Ta | Tb | Te | Th | Ti | Tl | Tm | U | V | W | Y | Yb | Zn | Zr |
|-----------|--------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) |
| CE491-8 | TN2_P4 | <0.004 | <0.007 | <0.004 | 104 | <0.024 | 0.854 | 0.033 | 4 | 0.282 | 8.43 | <0.534 | 0.63 | <0.026 | 0.057 | 42.1 | 0.088 | 0.24 | 0.688 | 33.4 | 0.029 | 16.5 | 1.4 | 43.4 | 1.41 |
| CE491-9 | TN1_P4 | <0.004 | <0.007 | <0.004 | 76.7 | 0.029 | 0.482 | 0.023 | 3.07 | 0.107 | 7.72 | <0.534 | 0.497 | <0.026 | 0.07 | 37.5 | 0.054 | 0.185 | 0.451 | 30.8 | <0.015 | 15.2 | 1.04 | 49.1 | 0.869 |
| CE491-10 | TN3_P4 | <0.004 | <0.007 | <0.004 | 124 | 0.033 | 0.852 | 0.038 | 3.9 | 0.219 | 7.2 | <0.534 | 0.619 | <0.026 | 0.113 | 48.1 | 0.07 | 0.234 | 0.638 | 37.1 | 0.042 | 17.5 | 1.38 | 54.6 | 1.42 |
| CE491-11 | CA3_P4 | <0.004 | <0.007 | <0.004 | 45.5 | 0.047 | 1.13 | 0.032 | 4.72 | 0.201 | 12.5 | <0.534 | 0.688 | <0.026 | 0.347 | 122 | 0.126 | 0.24 | 2.65 | 29.8 | 0.133 | 18 | 1.38 | 34.6 | 1.24 |
| CE491-12 | RA1_P4 | <0.004 | <0.007 | <0.004 | <43.6 | 0.037 | 0.706 | 0.028 | 4.42 | 0.17 | 10.1 | <0.534 | 0.663 | <0.026 | 0.284 | 60.2 | 0.091 | 0.23 | 2.19 | 24.4 | 0.139 | 18.8 | 1.36 | 36.6 | 0.974 |
| CE491-13 | PL1_P4 | <0.004 | <0.007 | 0.005 | 43.8 | 0.034 | 0.676 | 0.044 | 3.74 | 0.16 | 11.8 | <0.534 | 0.564 | <0.026 | 0.218 | 88.3 | 0.062 | 0.199 | 1.52 | 29.7 | 0.098 | 15.9 | 1.17 | 30.4 | 0.773 |
| CE491-14 | CA1_P4 | <0.004 | <0.007 | <0.004 | <43.6 | <0.024 | 0.918 | 0.044 | 5.24 | 0.238 | 16.6 | <0.534 | 0.791 | <0.026 | 0.324 | 114 | 0.082 | 0.269 | 1.97 | 32.7 | 0.106 | 20.8 | 1.57 | 32.3 | 1.33 |
| CE491-15 | PL3_P4 | <0.004 | <0.007 | <0.004 | <43.6 | 0.028 | 0.864 | 0.032 | 4.17 | 0.152 | 13.3 | <0.534 | 0.621 | <0.026 | 0.299 | 70.7 | 0.072 | 0.214 | 2.23 | 28.4 | 0.145 | 17.2 | 1.28 | 33 | 1.02 |
| CE491-16 | RA3_P4 | <0.004 | <0.007 | <0.004 | <43.6 | 0.039 | 0.553 | 0.043 | 4.43 | 0.21 | 10.8 | <0.534 | 0.675 | <0.026 | 0.254 | 46.7 | 0.1 | 0.23 | 1.38 | 19.2 | 0.126 | 20 | 1.34 | 28.2 | 0.958 |
| CE491-17 | PL2_P4 | <0.004 | <0.007 | 0.004 | <43.6 | 0.039 | 0.709 | 0.043 | 4.33 | 0.089 | 15.1 | <0.534 | 0.654 | <0.026 | 0.25 | 69.3 | 0.095 | 0.23 | 2.35 | 30.7 | 0.143 | 18.3 | 1.38 | 37.3 | 0.902 |
| CE491-18 | CA2_P4 | <0.004 | <0.007 | 0.008 | 62.5 | <0.024 | 0.541 | 0.034 | 4.29 | 0.209 | 26.3 | <0.534 | 0.644 | <0.026 | 0.165 | 101 | 0.055 | 0.214 | 1.27 | 28.5 | 0.109 | 19.5 | 1.22 | 27.4 | 1.02 |
| CE491-19 | RA2_P4 | <0.004 | 0.008 | 0.004 | <43.6 | 0.034 | 0.387 | 0.034 | 4.78 | 0.191 | 10.9 | <0.534 | 0.722 | <0.026 | 0.16 | 56.9 | 0.088 | 0.255 | 1.2 | 22.2 | 0.133 | 21.3 | 1.45 | 30.9 | 0.816 |

| Lab ID | Client ID | Re | Rh | Ru | S | Sb | Sc | Se | Sm | Sn | Sr | Ta | Tb | Te | Th | Ti | Tl | Tm | U | V | W | Y | Yb | Zn | Zr |
|--------------|----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) |
| LOD 3σ | Avg AEM-28 Blk | 0.000 | 0.000 | 0.000 | 16.8 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.072 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 2.5 | 0.000 |
| Method Code: | LOD (3 x S.D.) | 0.004 | 0.007 | 0.004 | 43.7 | 0.024 | 0.012 | 0.007 | 0.001 | 0.065 | 0.044 | 0.534 | 0.000 | 0.026 | 0.003 | 0.364 | 0.001 | 0.000 | 0.000 | 0.113 | 0.015 | 0.025 | 0.001 | 5.71 | 0.015 |

Certified Reference Materials

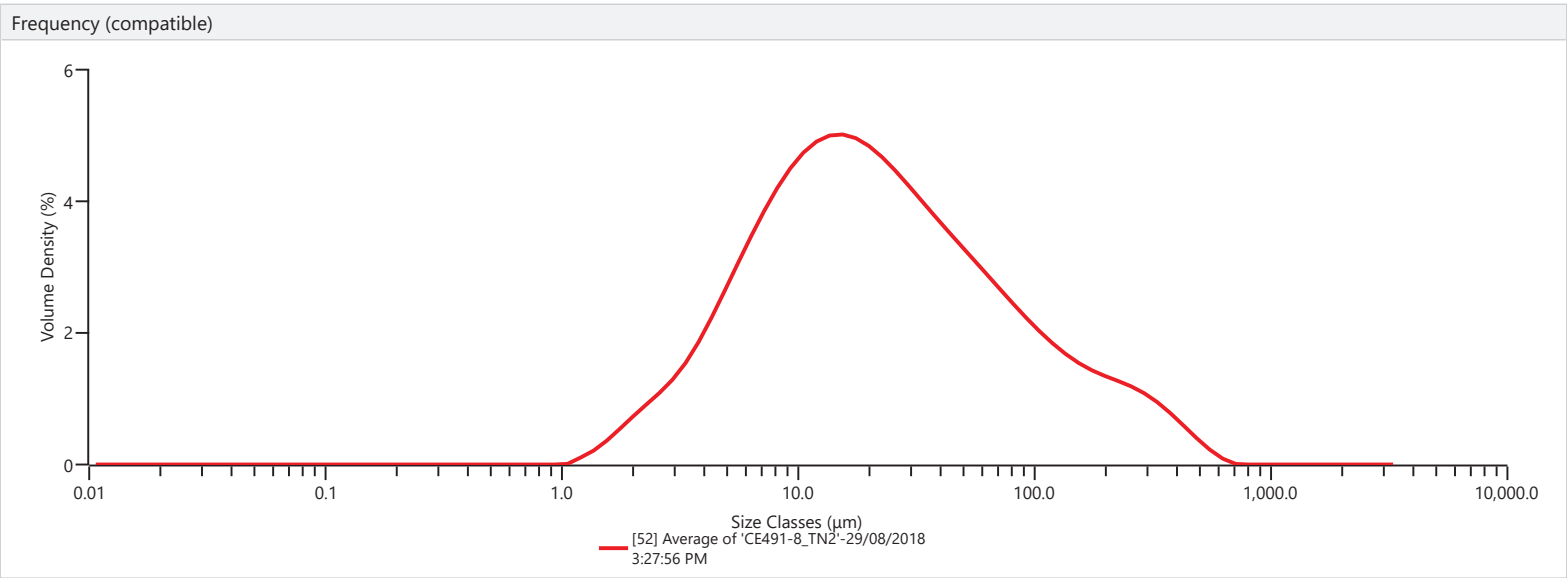
| Lab ID | Client ID | Re | Rh | Ru | S | Sb | Sc | Se | Sm | Sn | Sr | Ta | Tb | Te | Th | Ti | Tl | Tm | U | V | W | Y | Yb | Zn | Zr |
|----------------|-----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) |
| ERM-CCO18-1 | | 0.002 | 0.008 | 0 | 703 | 1.11 | 0.396 | 0.148 | 0.671 | 7.99 | 55.6 | -0.041 | 0.092 | 0.007 | 0.204 | 53.6 | 0.068 | 0.037 | 0.699 | 7.63 | 0.982 | 4.2 | 0.227 | 244 | 6.25 |
| ERM-CCO18-2 | | 0 | 0.011 | 0.001 | 664 | 1.34 | 0.43 | 0.115 | 0.69 | 7.97 | 56.3 | 0.063 | 0.099 | 0.019 | 0.201 | 53.4 | 0.077 | 0.038 | 0.775 | 7.72 | 1.08 | 4.15 | 0.243 | 235 | 6.58 |
| ERM-CCO18 Mean | | 0.001 | 0.009 | 0.001 | 683 | 1.23 | 0.413 | 0.132 | 0.681 | 7.98 | 55.9 | 0.011 | 0.095 | 0.013 | 0.202 | 53.5 | 0.073 | 0.038 | 0.737 | 7.67 | 1.03 | 4.18 | 0.235 | 240 | 6.41 |
| In-house mean | | | | | | 1.199 | | 0.12 | | 7.5 | 57.4 | | | | | 53.1 | 0.065 | | 0.654 | 7.6 | | | 241 | | |
| % recovery (%) | | | | | | 102 | | 113 | | 106 | 97 | | | | | 101 | 111 | | 113 | 100 | | | | 100 | |

Spike Recoveries

| Lab ID | Client ID | Re | Rh | Ru | S | Sb | Sc | Se | Sm | Sn | Sr | Ta | Tb | Te | Th | Ti | Tl | Tm | U | V | W | Y | Yb | Zn | Zr |
|---------------|-----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) |
| CE491-12 | RA1_P4 | 109 | 109 | 110 | 102 | 104 | 110 | 112 | 110 | 108 | 113 | 160 | 113 | 109 | 111 | 102 | 111 | 112 | 110 | 108 | 111 | 111 | 109 | 103 | 110 |
| CE491-19 | RA2_P4 | 105 | 105 | 106 | 99 | 103 | 107 | 110 | 105 | 104 | 106 | 151 | 107 | 104 | 106 | 102 | 106 | 107 | 106 | 102 | 107 | 109 | 105 | 102 | 105 |
| CE491-10 | TN3_P4 | <0.004 | <0.007 | <0.004 | 96.9 | 0.035 | 0.971 | 0.028 | 3.94 | 0.264 | 6.89 | <0.534 | 0.631 | <0.026 | 0.104 | 48.6 | 0.075 | 0.237 | 0.714 | 37 | 0.042 | 17.8 | 1.37 | 56.9 | 1.47 |
| CE491-10 Dup | TN3_P4 | <0.004 | <0.007 | <0.004 | 152 | 0.03 | 0.733 | 0.047 | 3.87 | 0.174 | 7.5 | <0.534 | 0.606 | <0.026 | 0.122 | 47.6 | 0.066 | 0.231 | 0.563 | 37.2 | 0.042 | 17.2 | 1.38 | 52.3 | 1.37 |
| CE491-10 Mean | TN3_P4 | <0.004 | <0.007 | <0.004 | 124 | 0.033 | 0.852 | 0.038 | 3.9 | 0.219 | 7.2 | <0.534 | 0.619 | <0.026 | 0.113 | 48.1 | 0.07 | 0.234 | 0.638 | 37.1 | 0.042 | 17.5 | 1.38 | 54.6 | 1.42 |
| CE491-15 | PL3_P4 | <0.004 | <0.007 | <0.004 | <43.6 | 0.035 | 0.963 | 0.037 | 4.26 | 0.173 | 13.3 | <0.534 | 0.628 | <0.026 | 0.343 | 71.5 | 0.074 | 0.215 | 2.36 | 28.5 | 0.149 | 17.6 | 1.3 | 33.9 | 1.04 |
| CE491-15 Dup | PL3_P4 | <0.004 | <0.007 | 0.004 | <43.6 | <0.024 | 0.765 | 0.027 | 4.07 | 0.131 | 13.3 | <0.534 | 0.615 | <0.026 | 0.255 | 69.9 | 0.07 | 0.212 | 2.11 | 28.2 | 0.141 | 16.9 | 1.27 | 32.1 | 1 |
| CE491-15 Mean | PL3_P4 | <0.004 | <0.007 | <0.004 | <43.65 | 0.028 | 0.864 | 0.032 | 4.17 | 0.152 | 13.3 | <0.534 | 0.621 | <0.026 | 0.299 | 70.7 | 0.072 | 0.214 | 2.23 | 28.4 | 0.145 | 17.2 | 1.28 | 33 | 1.02 |

Analysis

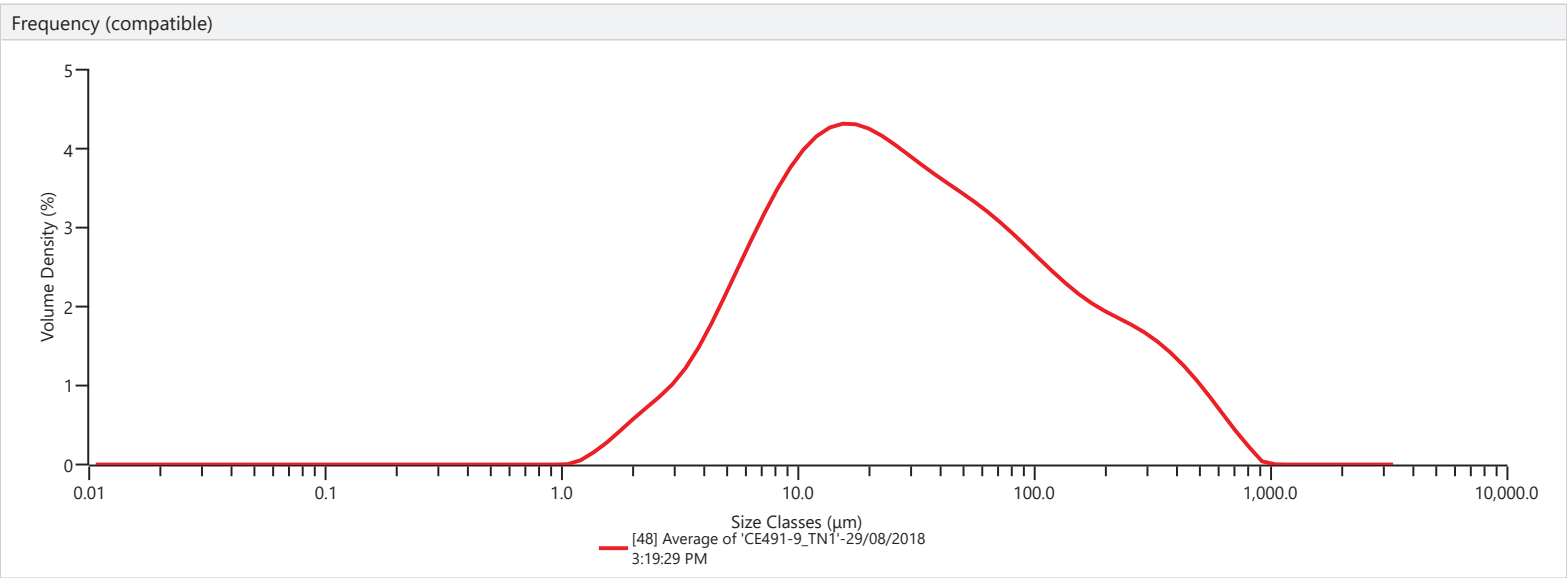
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| Operator Name CSIRO Mastersizer | Analysis Date Time 29/08/2018 3:27:56 PM |
| Sample Name Average of 'CE491-8_TN2' | Measurement Date Time 29/08/2018 3:27:56 PM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0185 % |
| Particle Refractive Index 1.555 | Span 6.363 |
| Particle Absorption Index 0.010 | Uniformity 2.031 |
| Dispersant Name Water | Specific Surface Area 517.0 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 11.6 μm |
| Scattering Model Mie | D [4,3] 50.5 μm |
| Analysis Model General Purpose | Dv (10) 4.84 μm |
| Weighted Residual 0.32 % | Dv (50) 20.1 μm |
| Laser Obscuration 13.08 % | Dv (90) 132 μm |



| Result | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 1.63 | 12.7 | 35.22 | 76.0 | 82.39 | 454 | 99.41 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 2.39 | 14.5 | 39.39 | 86.4 | 84.42 | 516 | 99.74 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 3.29 | 16.4 | 43.58 | 98.1 | 86.28 | 586 | 99.93 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.00 | 3.12 | 4.36 | 18.7 | 47.72 | 111 | 87.97 | 666 | 100.00 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.00 | 3.55 | 5.64 | 21.2 | 51.76 | 127 | 89.51 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.00 | 4.03 | 7.19 | 24.1 | 55.65 | 144 | 90.91 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 0.00 | 4.58 | 9.05 | 27.4 | 59.38 | 163 | 92.19 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 0.00 | 5.21 | 11.25 | 31.1 | 62.92 | 186 | 93.39 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 0.00 | 5.92 | 13.80 | 35.3 | 66.27 | 211 | 94.51 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 0.00 | 6.72 | 16.69 | 40.1 | 69.42 | 240 | 95.57 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 0.09 | 7.64 | 19.90 | 45.6 | 72.38 | 272 | 96.56 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 0.26 | 8.68 | 23.41 | 51.8 | 75.16 | 310 | 97.47 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 0.56 | 9.86 | 27.17 | 58.9 | 77.75 | 352 | 98.26 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 1.02 | 11.2 | 31.12 | 66.9 | 80.16 | 400 | 98.91 | 2390 | 100.00 |

Analysis

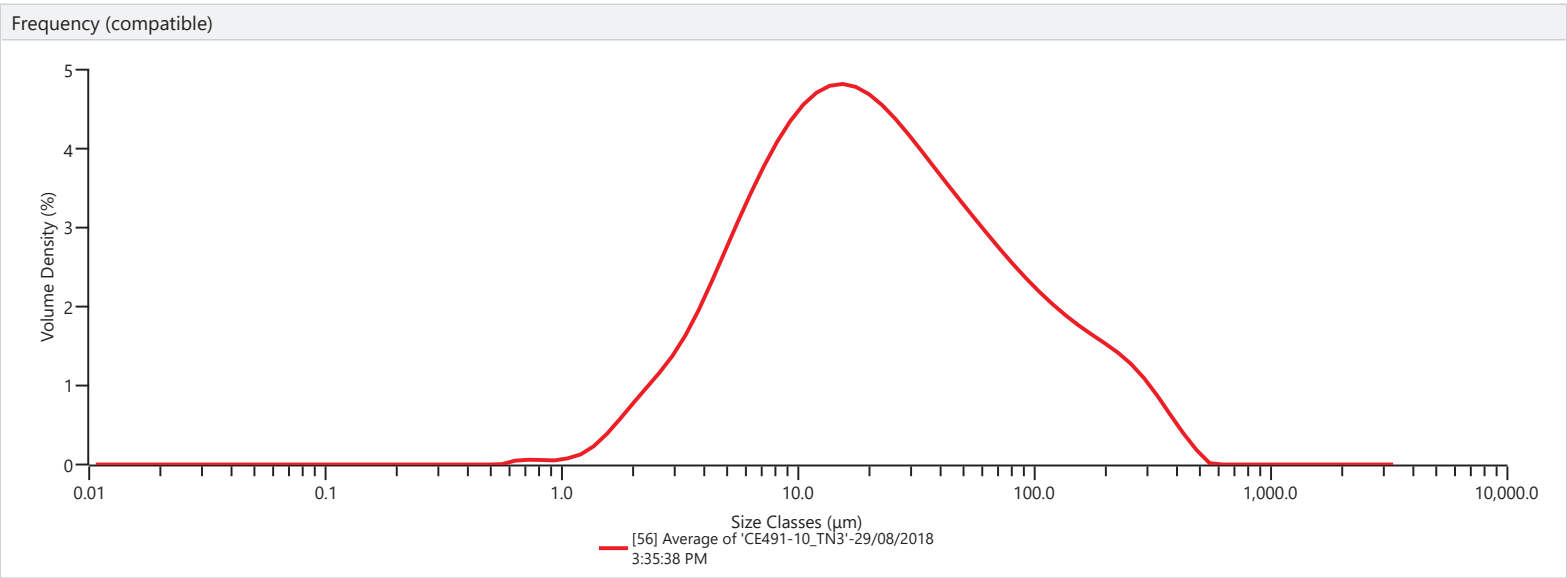
| | |
|--|---|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 29/08/2018 3:19:29 PM |
| Sample Name Average of 'CE491-9_TN1' | Measurement Date Time 29/08/2018 3:19:29 PM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0234 % |
| Particle Refractive Index 1.555 | Span 7.936 |
| Particle Absorption Index 0.010 | Uniformity 2.388 |
| Dispersant Name Water | Specific Surface Area 431.3 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 13.9 μm |
| Scattering Model Mie | D [4,3] 77.6 μm |
| Analysis Model General Purpose | Dv (10) 5.57 μm |
| Weighted Residual 0.26 % | Dv (50) 27.4 μm |
| Laser Obscuration 13.66 % | Dv (90) 223 μm |



| Result | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 1.24 | 12.7 | 28.83 | 76.0 | 73.35 | 454 | 97.30 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 1.83 | 14.5 | 32.39 | 86.4 | 75.79 | 516 | 98.19 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 2.55 | 16.4 | 36.00 | 98.1 | 78.09 | 586 | 98.91 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.00 | 3.12 | 3.39 | 18.7 | 39.59 | 111 | 80.26 | 666 | 99.44 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.00 | 3.55 | 4.40 | 21.2 | 43.14 | 127 | 82.30 | 756 | 99.79 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.00 | 4.03 | 5.63 | 24.1 | 46.61 | 144 | 84.22 | 859 | 99.98 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 0.00 | 4.58 | 7.12 | 27.4 | 49.99 | 163 | 86.02 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 0.00 | 5.21 | 8.90 | 31.1 | 53.26 | 186 | 87.72 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 0.00 | 5.92 | 10.97 | 35.3 | 56.42 | 211 | 89.34 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 0.00 | 6.72 | 13.34 | 40.1 | 59.49 | 240 | 90.88 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 0.04 | 7.64 | 15.99 | 45.6 | 62.46 | 272 | 92.36 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 0.17 | 8.68 | 18.90 | 51.8 | 65.34 | 310 | 93.76 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 0.40 | 9.86 | 22.03 | 58.9 | 68.12 | 352 | 95.06 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 0.76 | 11.2 | 25.36 | 66.9 | 70.79 | 400 | 96.25 | 2390 | 100.00 |

Analysis

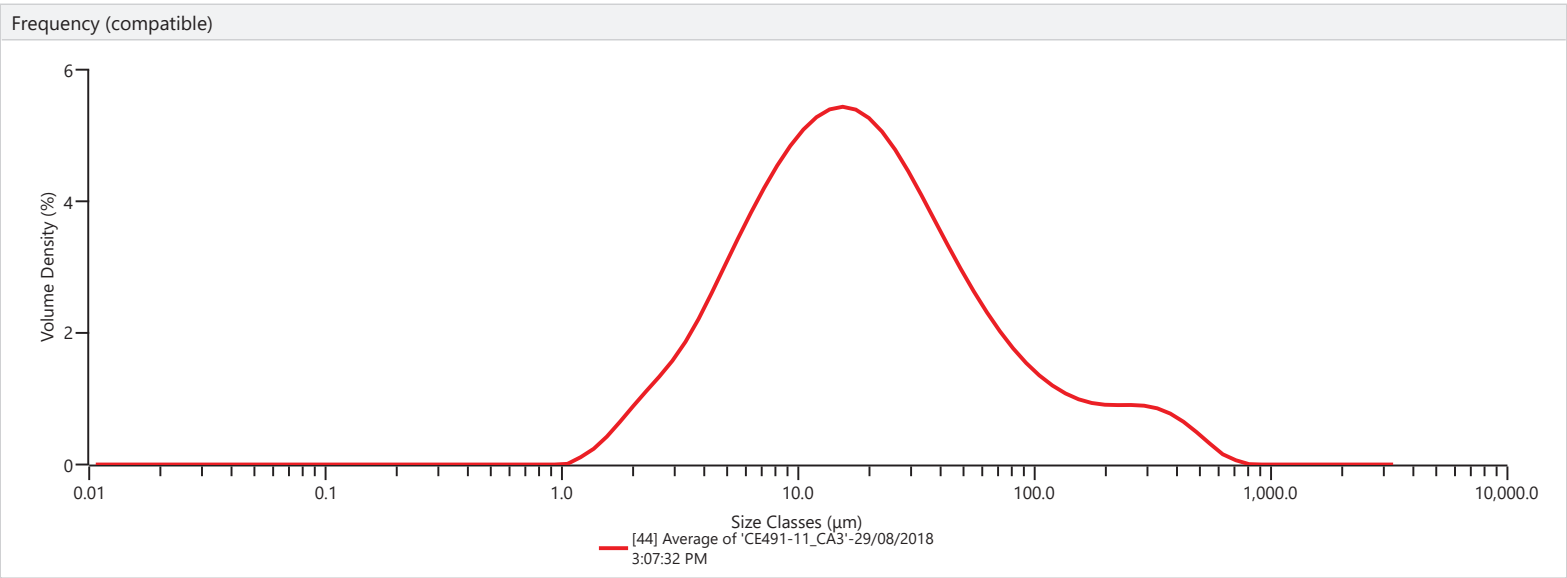
| | |
|--|---|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 29/08/2018 3:35:38 PM |
| Sample Name Average of 'CE491-10_TN3' | Measurement Date Time 29/08/2018 3:35:38 PM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0194 % |
| Particle Refractive Index 1.555 | Span 6.323 |
| Particle Absorption Index 0.010 | Uniformity 1.926 |
| Dispersant Name Water | Specific Surface Area 541.7 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 11.1 μm |
| Scattering Model Mie | D [4,3] 48.7 μm |
| Analysis Model General Purpose | Dv (10) 4.63 μm |
| Weighted Residual 0.36 % | Dv (50) 20.3 μm |
| Laser Obscuration 14.15 % | Dv (90) 133 μm |



| Result | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 1.99 | 12.7 | 35.43 | 76.0 | 81.81 | 454 | 99.85 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 2.79 | 14.5 | 39.44 | 86.4 | 83.93 | 516 | 100.00 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 3.76 | 16.4 | 43.46 | 98.1 | 85.89 | 586 | 100.00 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.00 | 3.12 | 4.90 | 18.7 | 47.45 | 111 | 87.71 | 666 | 100.00 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.00 | 3.55 | 6.26 | 21.2 | 51.36 | 127 | 89.41 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.04 | 4.03 | 7.89 | 24.1 | 55.16 | 144 | 90.98 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 0.10 | 4.58 | 9.82 | 27.4 | 58.81 | 163 | 92.45 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 0.14 | 5.21 | 12.07 | 31.1 | 62.30 | 186 | 93.82 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 0.18 | 5.92 | 14.63 | 35.3 | 65.62 | 211 | 95.10 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 0.25 | 6.72 | 17.50 | 40.1 | 68.75 | 240 | 96.29 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 0.35 | 7.64 | 20.66 | 45.6 | 71.71 | 272 | 97.35 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 0.54 | 8.68 | 24.07 | 51.8 | 74.49 | 310 | 98.27 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 0.86 | 9.86 | 27.70 | 58.9 | 77.10 | 352 | 99.00 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 1.34 | 11.2 | 31.50 | 66.9 | 79.54 | 400 | 99.52 | 2390 | 100.00 |

Analysis

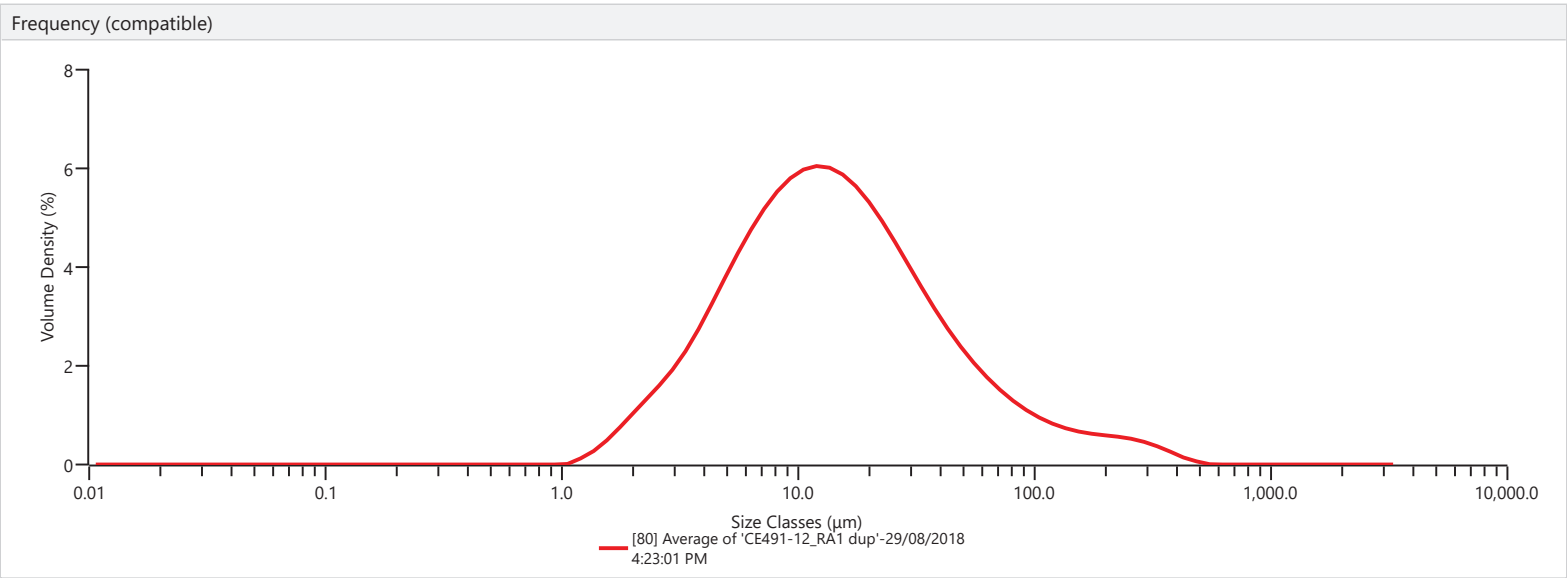
| | |
|--|---|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 29/08/2018 3:07:32 PM |
| Sample Name Average of 'CE491-11_CA3' | Measurement Date Time 29/08/2018 3:07:32 PM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0159 % |
| Particle Refractive Index 1.555 | Span 5.724 |
| Particle Absorption Index 0.010 | Uniformity 2.099 |
| Dispersant Name Water | Specific Surface Area 577.6 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 10.4 μm |
| Scattering Model Mie | D [4,3] 44.7 μm |
| Analysis Model General Purpose | Dv (10) 4.36 μm |
| Weighted Residual 0.35 % | Dv (50) 17.2 μm |
| Laser Obscuration 12.59 % | Dv (90) 103 μm |



| Result | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 1.92 | 12.7 | 39.39 | 76.0 | 86.85 | 454 | 99.14 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 2.85 | 14.5 | 43.90 | 86.4 | 88.32 | 516 | 99.56 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 3.96 | 16.4 | 48.44 | 98.1 | 89.60 | 586 | 99.82 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.00 | 3.12 | 5.27 | 18.7 | 52.94 | 111 | 90.73 | 666 | 99.95 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.00 | 3.55 | 6.82 | 21.2 | 57.33 | 127 | 91.73 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.00 | 4.03 | 8.66 | 24.1 | 61.56 | 144 | 92.62 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 0.00 | 4.58 | 10.83 | 27.4 | 65.55 | 163 | 93.45 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 0.00 | 5.21 | 13.35 | 31.1 | 69.27 | 186 | 94.23 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 0.00 | 5.92 | 16.21 | 35.3 | 72.68 | 211 | 94.98 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 0.00 | 6.72 | 19.41 | 40.1 | 75.78 | 240 | 95.73 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 0.09 | 7.64 | 22.91 | 45.6 | 78.56 | 272 | 96.49 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 0.29 | 8.68 | 26.70 | 51.8 | 81.04 | 310 | 97.24 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 0.64 | 9.86 | 30.74 | 58.9 | 83.24 | 352 | 97.95 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 1.18 | 11.2 | 34.99 | 66.9 | 85.16 | 400 | 98.60 | 2390 | 100.00 |

Analysis

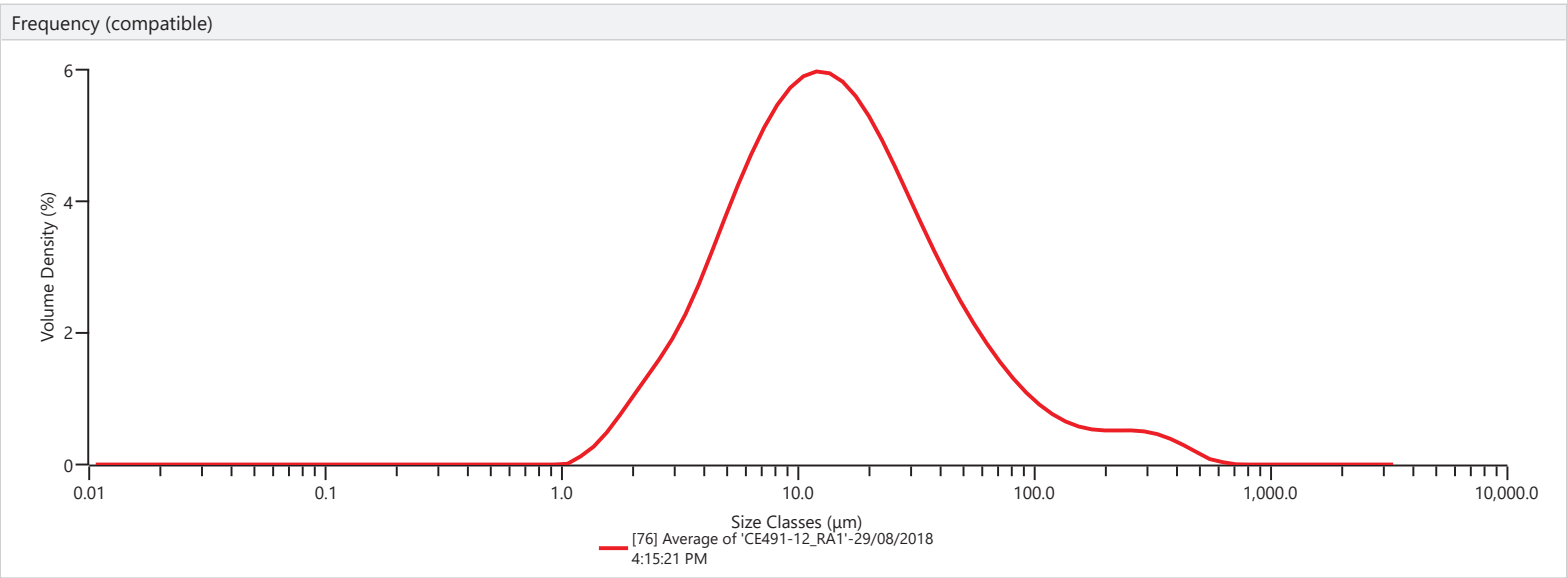
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| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 29/08/2018 4:23:01 PM |
| Sample Name Average of 'CE491-12_RA1 dup' | Measurement Date Time 29/08/2018 4:23:01 PM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0137 % |
| Particle Refractive Index 1.555 | Span 4.213 |
| Particle Absorption Index 0.010 | Uniformity 1.602 |
| Dispersant Name Water | Specific Surface Area 670.3 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 8.95 μm |
| Scattering Model Mie | D [4,3] 28.8 μm |
| Analysis Model General Purpose | Dv (10) 3.93 μm |
| Weighted Residual 0.42 % | Dv (50) 13.5 μm |
| Laser Obscuration 12.62 % | Dv (90) 60.8 μm |



| Result | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 2.23 | 12.7 | 47.67 | 76.0 | 92.36 | 454 | 99.95 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 3.33 | 14.5 | 52.69 | 86.4 | 93.43 | 516 | 100.00 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 4.66 | 16.4 | 57.59 | 98.1 | 94.35 | 586 | 100.00 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.00 | 3.12 | 6.26 | 18.7 | 62.30 | 111 | 95.14 | 666 | 100.00 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.00 | 3.55 | 8.16 | 21.2 | 66.74 | 127 | 95.83 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.00 | 4.03 | 10.45 | 24.1 | 70.86 | 144 | 96.44 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 0.00 | 4.58 | 13.15 | 27.4 | 74.61 | 163 | 97.00 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 0.00 | 5.21 | 16.30 | 31.1 | 77.99 | 186 | 97.52 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 0.00 | 5.92 | 19.88 | 35.3 | 80.99 | 211 | 98.01 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 0.00 | 6.72 | 23.85 | 40.1 | 83.62 | 240 | 98.48 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 0.10 | 7.64 | 28.17 | 45.6 | 85.92 | 272 | 98.92 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 0.33 | 8.68 | 32.79 | 51.8 | 87.91 | 310 | 99.30 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 0.73 | 9.86 | 37.63 | 58.9 | 89.62 | 352 | 99.61 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 1.36 | 11.2 | 42.62 | 66.9 | 91.10 | 400 | 99.83 | 2390 | 100.00 |

Analysis

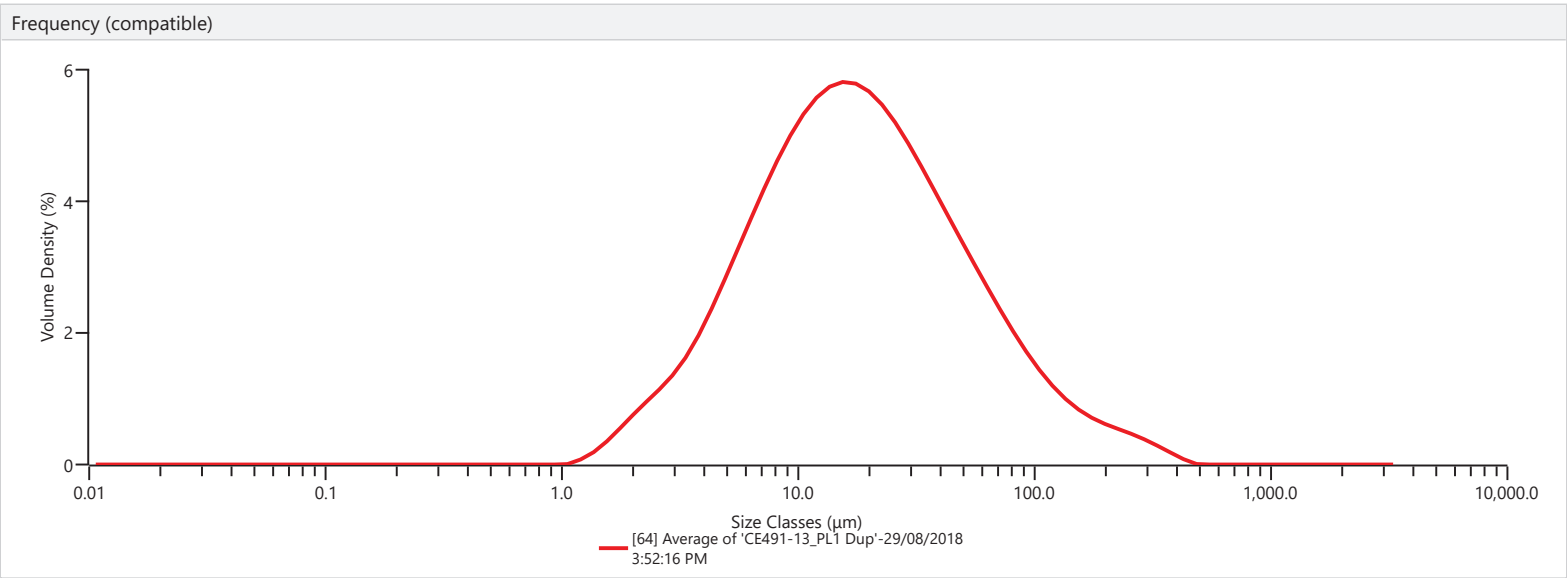
| | |
|--|---|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 29/08/2018 4:15:21 PM |
| Sample Name Average of 'CE491-12_RA1' | Measurement Date Time 29/08/2018 4:15:21 PM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0136 % |
| Particle Refractive Index 1.555 | Span 4.247 |
| Particle Absorption Index 0.010 | Uniformity 1.717 |
| Dispersant Name Water | Specific Surface Area 666.2 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 9.01 μm |
| Scattering Model Mie | D [4,3] 30.7 μm |
| Analysis Model General Purpose | Dv (10) 3.94 μm |
| Weighted Residual 0.38 % | Dv (50) 13.7 μm |
| Laser Obscuration 12.49 % | Dv (90) 62.0 μm |



| | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Result | | | | | | | | | | | | | |
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 2.22 | 12.7 | 47.21 | 76.0 | 92.21 | 454 | 99.75 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 3.32 | 14.5 | 52.18 | 86.4 | 93.30 | 516 | 99.91 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 4.65 | 16.4 | 57.03 | 98.1 | 94.21 | 586 | 99.97 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.00 | 3.12 | 6.24 | 18.7 | 61.70 | 111 | 94.97 | 666 | 100.00 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.00 | 3.55 | 8.14 | 21.2 | 66.12 | 127 | 95.60 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.00 | 4.03 | 10.41 | 24.1 | 70.23 | 144 | 96.15 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 0.00 | 4.58 | 13.10 | 27.4 | 74.01 | 163 | 96.62 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 0.00 | 5.21 | 16.22 | 31.1 | 77.42 | 186 | 97.07 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 0.00 | 5.92 | 19.76 | 35.3 | 80.47 | 211 | 97.50 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 0.00 | 6.72 | 23.69 | 40.1 | 83.16 | 240 | 97.93 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 0.10 | 7.64 | 27.96 | 45.6 | 85.53 | 272 | 98.36 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 0.33 | 8.68 | 32.52 | 51.8 | 87.60 | 310 | 98.79 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 0.73 | 9.86 | 37.30 | 58.9 | 89.38 | 352 | 99.17 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 1.36 | 11.2 | 42.23 | 66.9 | 90.91 | 400 | 99.50 | 2390 | 100.00 |

Analysis

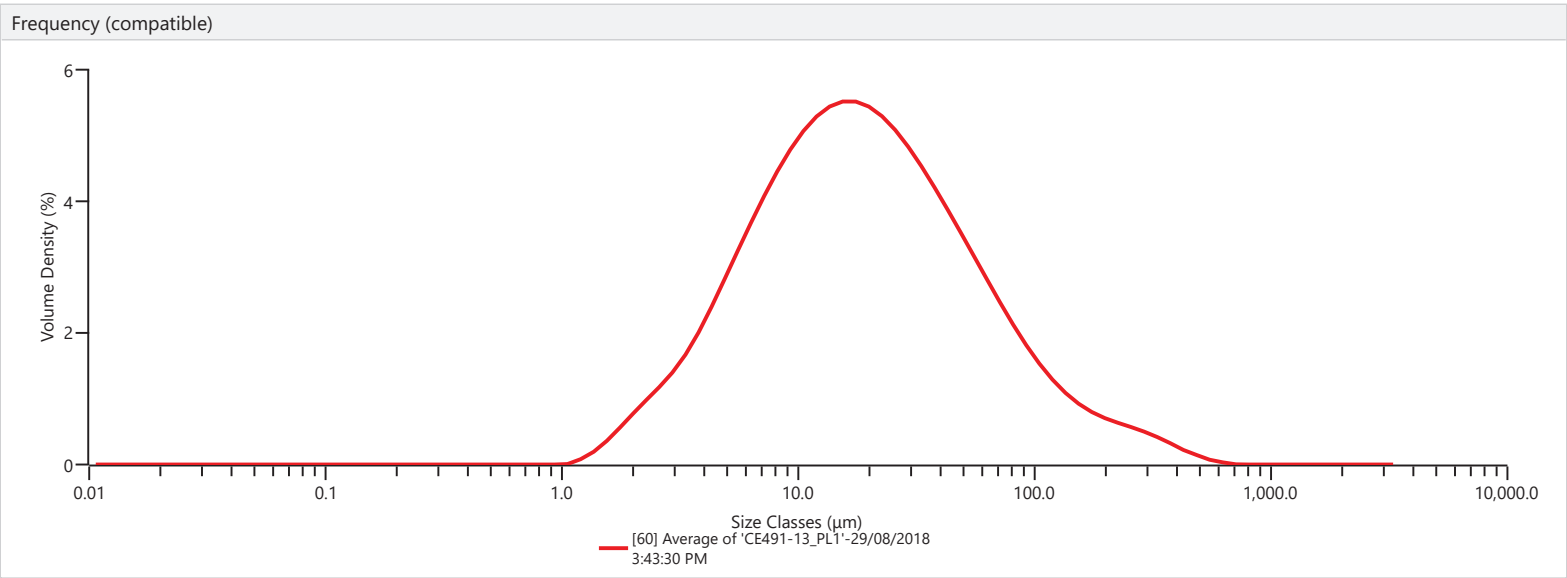
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|--|---|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 29/08/2018 3:52:16 PM |
| Sample Name Average of 'CE491-13_PL1 Dup' | Measurement Date Time 29/08/2018 3:52:16 PM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0162 % |
| Particle Refractive Index 1.555 | Span 3.978 |
| Particle Absorption Index 0.010 | Uniformity 1.365 |
| Dispersant Name Water | Specific Surface Area 554.0 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 10.8 μm |
| Scattering Model Mie | D [4,3] 32.7 μm |
| Analysis Model General Purpose | Dv (10) 4.73 μm |
| Weighted Residual 0.34 % | Dv (50) 17.4 μm |
| Laser Obscuration 12.23 % | Dv (90) 73.9 μm |



| | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Result | | | | | | | | | | | | | |
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 1.59 | 12.7 | 38.22 | 76.0 | 90.44 | 454 | 100.00 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 2.39 | 14.5 | 43.01 | 86.4 | 92.13 | 516 | 100.00 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 3.34 | 16.4 | 47.87 | 98.1 | 93.55 | 586 | 100.00 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.00 | 3.12 | 4.46 | 18.7 | 52.70 | 111 | 94.75 | 666 | 100.00 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.00 | 3.55 | 5.81 | 21.2 | 57.43 | 127 | 95.75 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.00 | 4.03 | 7.44 | 24.1 | 61.99 | 144 | 96.58 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 0.00 | 4.58 | 9.41 | 27.4 | 66.33 | 163 | 97.27 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 0.00 | 5.21 | 11.76 | 31.1 | 70.40 | 186 | 97.86 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 0.00 | 5.92 | 14.49 | 35.3 | 74.18 | 211 | 98.38 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 0.00 | 6.72 | 17.60 | 40.1 | 77.65 | 240 | 98.83 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 0.06 | 7.64 | 21.10 | 45.6 | 80.81 | 272 | 99.22 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 0.22 | 8.68 | 24.95 | 51.8 | 83.67 | 310 | 99.54 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 0.51 | 9.86 | 29.12 | 58.9 | 86.22 | 352 | 99.78 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 0.96 | 11.2 | 33.57 | 66.9 | 88.47 | 400 | 99.93 | 2390 | 100.00 |

Analysis

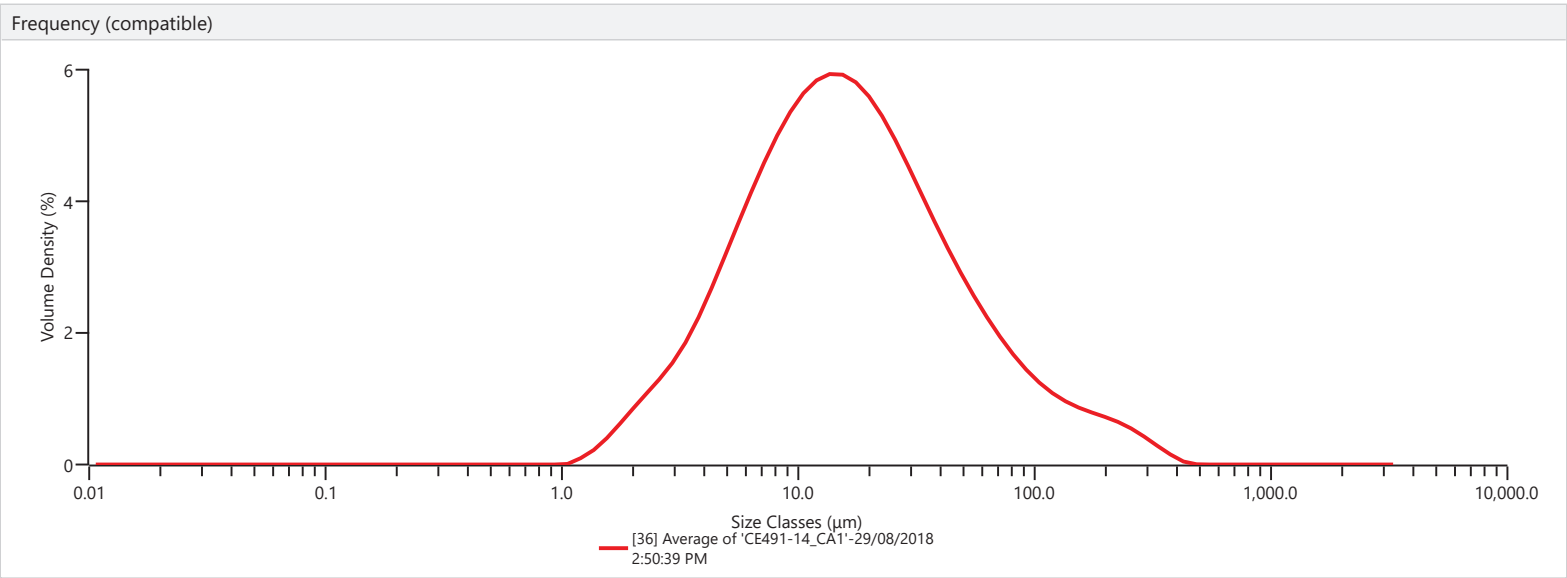
| | |
|--|---|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 29/08/2018 3:43:30 PM |
| Sample Name Average of 'CE491-13_PL1' | Measurement Date Time 29/08/2018 3:43:30 PM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0165 % |
| Particle Refractive Index 1.555 | Span 4.270 |
| Particle Absorption Index 0.010 | Uniformity 1.522 |
| Dispersant Name Water | Specific Surface Area 550.0 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 10.9 μm |
| Scattering Model Mie | D [4,3] 36.5 μm |
| Analysis Model General Purpose | Dv (10) 4.67 μm |
| Weighted Residual 0.34 % | Dv (50) 18.0 μm |
| Laser Obscuration 12.38 % | Dv (90) 81.6 μm |



| Result | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 1.63 | 12.7 | 37.53 | 76.0 | 89.01 | 454 | 99.79 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 2.45 | 14.5 | 42.07 | 86.4 | 90.79 | 516 | 99.91 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 3.43 | 16.4 | 46.67 | 98.1 | 92.30 | 586 | 99.97 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.00 | 3.12 | 4.59 | 18.7 | 51.27 | 111 | 93.57 | 666 | 100.00 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.00 | 3.55 | 5.98 | 21.2 | 55.81 | 127 | 94.65 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.00 | 4.03 | 7.65 | 24.1 | 60.23 | 144 | 95.55 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 0.00 | 4.58 | 9.65 | 27.4 | 64.47 | 163 | 96.32 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 0.00 | 5.21 | 12.00 | 31.1 | 68.50 | 186 | 96.98 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 0.00 | 5.92 | 14.71 | 35.3 | 72.28 | 211 | 97.57 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 0.00 | 6.72 | 17.77 | 40.1 | 75.80 | 240 | 98.10 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 0.07 | 7.64 | 21.18 | 45.6 | 79.03 | 272 | 98.57 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 0.22 | 8.68 | 24.89 | 51.8 | 81.97 | 310 | 98.99 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 0.52 | 9.86 | 28.88 | 58.9 | 84.61 | 352 | 99.34 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 0.99 | 11.2 | 33.11 | 66.9 | 86.96 | 400 | 99.61 | 2390 | 100.00 |

Analysis

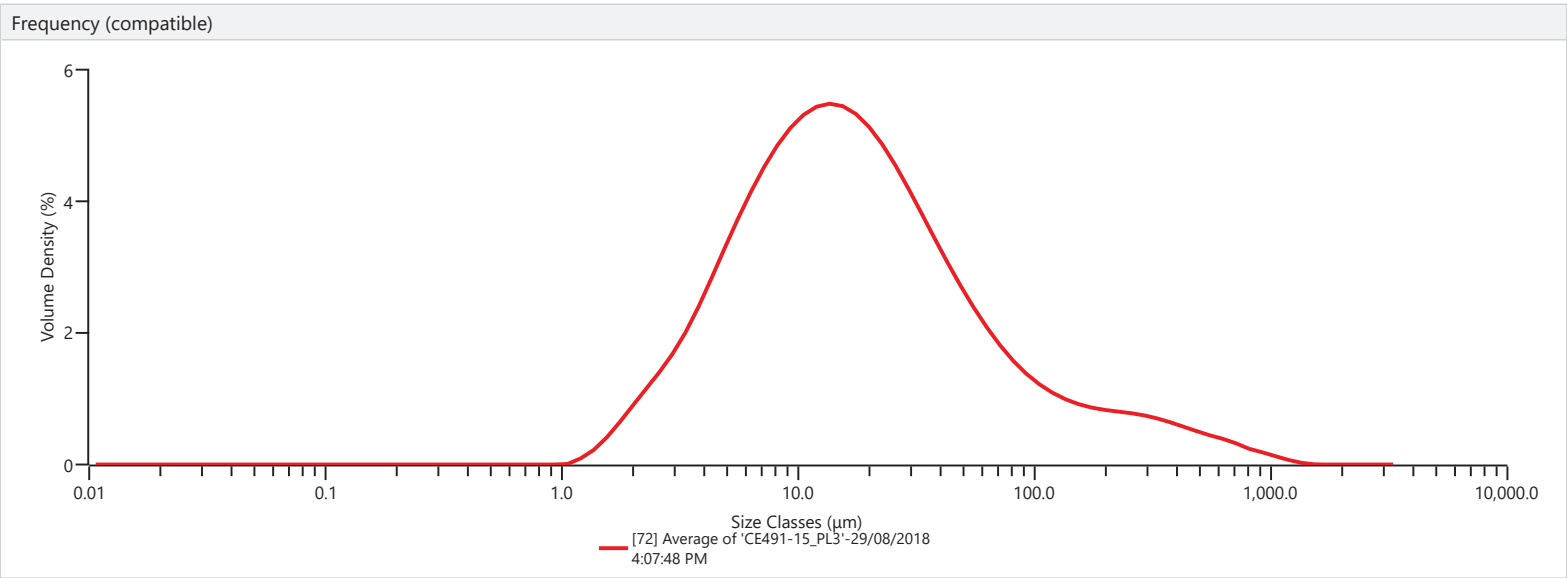
| | |
|--|--|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 29/08/2018 2:50:39 PM |
| Sample Name Average of 'CE491-14_CA1' | Measurement Date Time 29/08/2018 2:50:39 PM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0149 % |
| Particle Refractive Index 1.555 | Span 4.222 |
| Particle Absorption Index 0.010 | Uniformity 1.467 |
| Dispersant Name Water | Specific Surface Area 597.1 m²/kg |
| Dispersant Refractive Index 1.330 | D [3,2] 10.0 µm |
| Scattering Model Mie | D [4,3] 31.2 µm |
| Analysis Model General Purpose | Dv (10) 4.40 µm |
| Weighted Residual 0.41 % | Dv (50) 15.7 µm |
| Laser Obscuration 12.16 % | Dv (90) 70.6 µm |



| | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Result | | | | | | | | | | | | | |
| Size (µm) | % Volume Under | Size (µm) | % Volume Under | Size (µm) | % Volume Under | Size (µm) | % Volume Under | Size (µm) | % Volume Under | Size (µm) | % Volume Under | Size (µm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 1.82 | 12.7 | 41.89 | 76.0 | 90.93 | 454 | 100.00 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 2.71 | 14.5 | 46.84 | 86.4 | 92.33 | 516 | 100.00 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 3.79 | 16.4 | 51.79 | 98.1 | 93.52 | 586 | 100.00 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.00 | 3.12 | 5.07 | 18.7 | 56.64 | 111 | 94.56 | 666 | 100.00 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.00 | 3.55 | 6.61 | 21.2 | 61.31 | 127 | 95.46 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.00 | 4.03 | 8.47 | 24.1 | 65.73 | 144 | 96.26 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 0.00 | 4.58 | 10.71 | 27.4 | 69.85 | 163 | 96.98 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 0.00 | 5.21 | 13.34 | 31.1 | 73.63 | 186 | 97.64 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 0.00 | 5.92 | 16.39 | 35.3 | 77.06 | 211 | 98.25 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 0.00 | 6.72 | 19.84 | 40.1 | 80.14 | 240 | 98.79 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 0.08 | 7.64 | 23.66 | 45.6 | 82.88 | 272 | 99.25 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 0.26 | 8.68 | 27.84 | 51.8 | 85.31 | 310 | 99.60 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 0.59 | 9.86 | 32.31 | 58.9 | 87.45 | 352 | 99.84 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 1.11 | 11.2 | 37.02 | 66.9 | 89.31 | 400 | 99.97 | 2390 | 100.00 |

Analysis

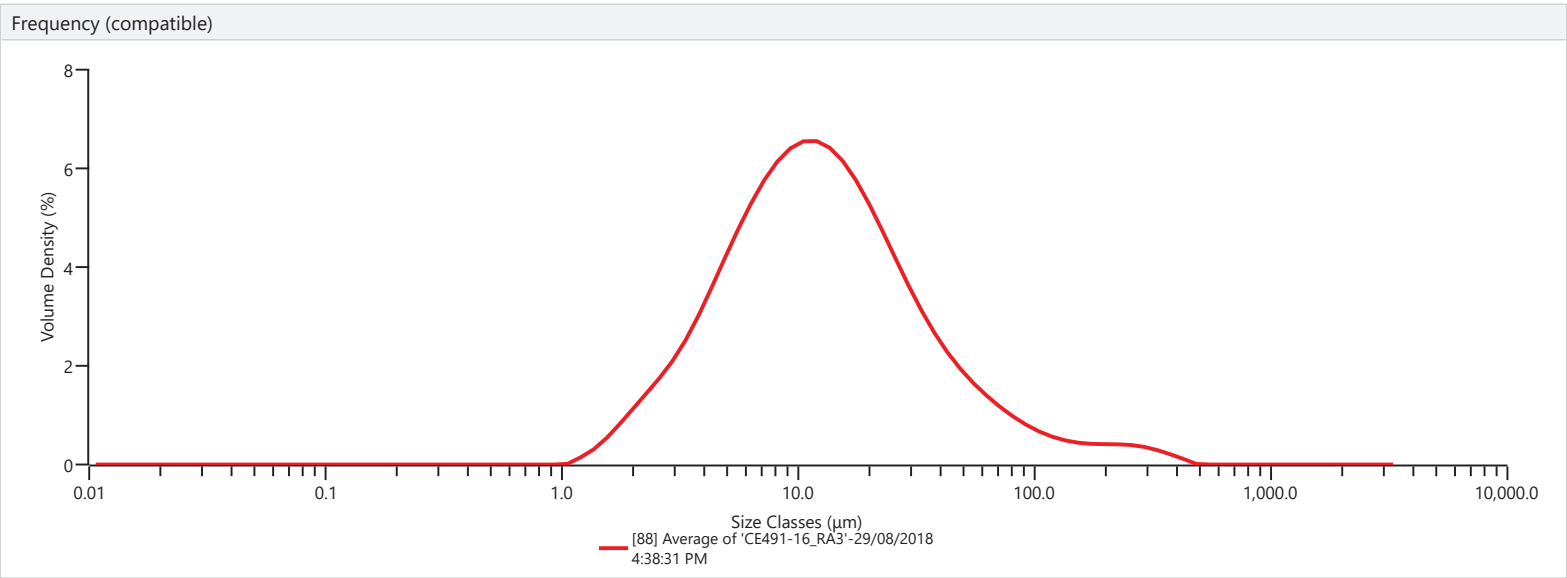
| | |
|--|---|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 29/08/2018 4:07:48 PM |
| Sample Name Average of 'CE491-15_PL3' | Measurement Date Time 29/08/2018 4:07:48 PM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0142 % |
| Particle Refractive Index 1.555 | Span 6.182 |
| Particle Absorption Index 0.010 | Uniformity 2.594 |
| Dispersant Name Water | Specific Surface Area 598.8 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 10.0 μm |
| Scattering Model Mie | D [4,3] 49.6 μm |
| Analysis Model General Purpose | Dv (10) 4.24 μm |
| Weighted Residual 0.35 % | Dv (50) 16.0 μm |
| Laser Obscuration 11.75 % | Dv (90) 103 μm |



| Result | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 1.89 | 12.7 | 41.82 | 76.0 | 87.14 | 454 | 98.07 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 2.85 | 14.5 | 46.39 | 86.4 | 88.45 | 516 | 98.49 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 4.02 | 16.4 | 50.94 | 98.1 | 89.60 | 586 | 98.86 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.00 | 3.12 | 5.41 | 18.7 | 55.39 | 111 | 90.62 | 666 | 99.19 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.00 | 3.55 | 7.08 | 21.2 | 59.67 | 127 | 91.53 | 756 | 99.46 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.00 | 4.03 | 9.08 | 24.1 | 63.73 | 144 | 92.35 | 859 | 99.66 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 0.00 | 4.58 | 11.44 | 27.4 | 67.53 | 163 | 93.11 | 976 | 99.81 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 0.00 | 5.21 | 14.19 | 31.1 | 71.04 | 186 | 93.83 | 1110 | 99.92 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 0.00 | 5.92 | 17.30 | 35.3 | 74.22 | 211 | 94.53 | 1260 | 99.98 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 0.00 | 6.72 | 20.76 | 40.1 | 77.09 | 240 | 95.20 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 0.08 | 7.64 | 24.53 | 45.6 | 79.65 | 272 | 95.85 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 0.26 | 8.68 | 28.58 | 51.8 | 81.91 | 310 | 96.47 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 0.60 | 9.86 | 32.84 | 58.9 | 83.89 | 352 | 97.06 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 1.14 | 11.2 | 37.28 | 66.9 | 85.63 | 400 | 97.59 | 2390 | 100.00 |

Analysis

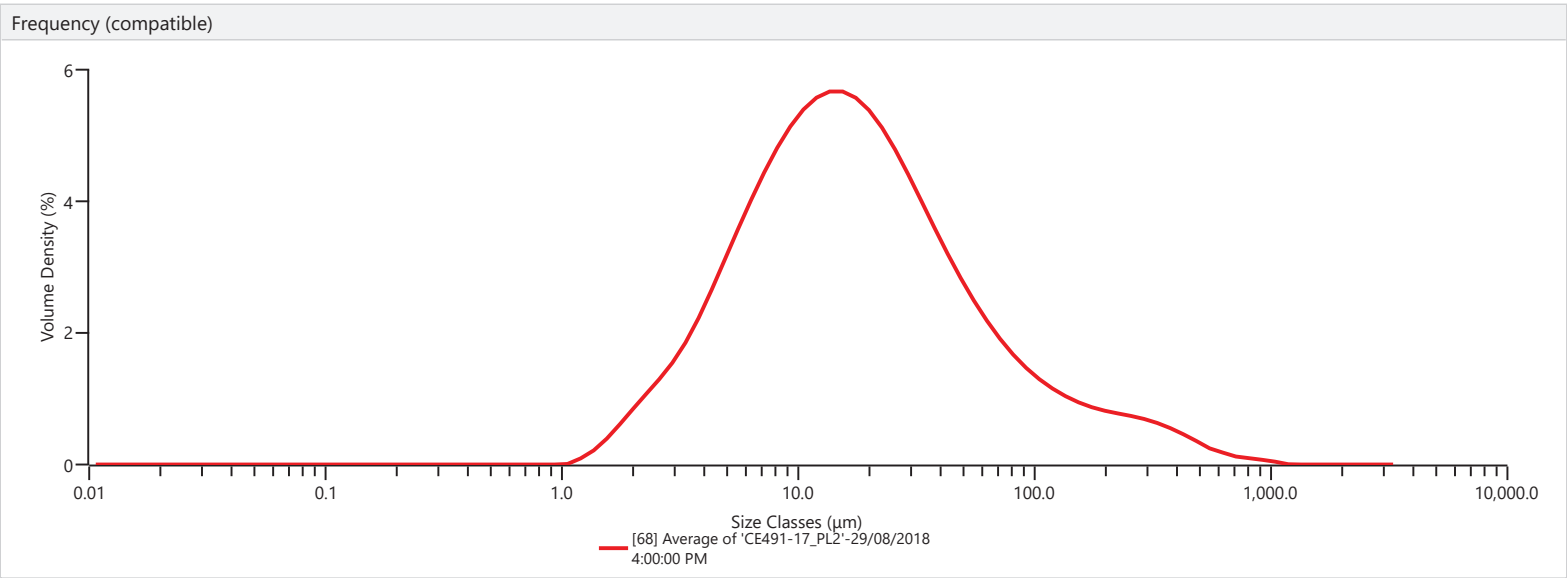
| | |
|--|---|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 29/08/2018 4:38:31 PM |
| Sample Name Average of 'CE491-16_RA3' | Measurement Date Time 29/08/2018 4:38:31 PM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0125 % |
| Particle Refractive Index 1.555 | Span 3.662 |
| Particle Absorption Index 0.010 | Uniformity 1.463 |
| Dispersant Name Water | Specific Surface Area 722.9 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 8.30 μm |
| Scattering Model Mie | D [4,3] 24.2 μm |
| Analysis Model General Purpose | Dv (10) 3.75 μm |
| Weighted Residual 0.39 % | Dv (50) 12.0 μm |
| Laser Obscuration 12.45 % | Dv (90) 47.7 μm |



| Result | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 2.45 | 12.7 | 52.52 | 76.0 | 94.55 | 454 | 100.00 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 3.65 | 14.5 | 57.89 | 86.4 | 95.36 | 516 | 100.00 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 5.10 | 16.4 | 63.02 | 98.1 | 96.03 | 586 | 100.00 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.00 | 3.12 | 6.84 | 18.7 | 67.83 | 111 | 96.58 | 666 | 100.00 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.00 | 3.55 | 8.94 | 21.2 | 72.25 | 127 | 97.05 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.00 | 4.03 | 11.45 | 24.1 | 76.21 | 144 | 97.45 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 0.00 | 4.58 | 14.44 | 27.4 | 79.70 | 163 | 97.82 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 0.00 | 5.21 | 17.92 | 31.1 | 82.73 | 186 | 98.17 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 0.00 | 5.92 | 21.89 | 35.3 | 85.33 | 211 | 98.51 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 0.00 | 6.72 | 26.31 | 40.1 | 87.55 | 240 | 98.85 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 0.12 | 7.64 | 31.11 | 45.6 | 89.44 | 272 | 99.18 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 0.37 | 8.68 | 36.23 | 51.8 | 91.05 | 310 | 99.48 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 0.82 | 9.86 | 41.58 | 58.9 | 92.42 | 352 | 99.73 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 1.51 | 11.2 | 47.05 | 66.9 | 93.57 | 400 | 99.90 | 2390 | 100.00 |

Analysis

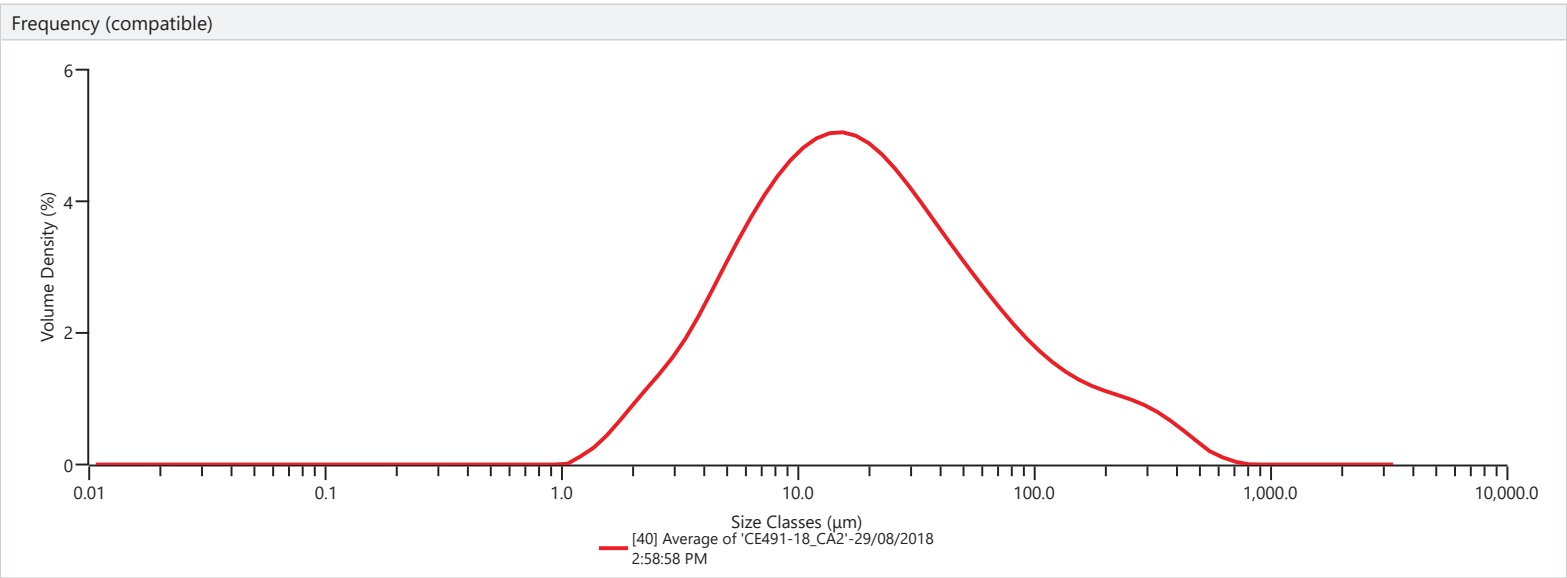
| | |
|--|---|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 29/08/2018 4:00:00 PM |
| Sample Name Average of 'CE491-17_PL2' | Measurement Date Time 29/08/2018 4:00:00 PM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0161 % |
| Particle Refractive Index 1.555 | Span 5.276 |
| Particle Absorption Index 0.010 | Uniformity 2.061 |
| Dispersant Name Water | Specific Surface Area 583.9 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 10.3 μm |
| Scattering Model Mie | D [4,3] 42.1 μm |
| Analysis Model General Purpose | Dv (10) 4.41 μm |
| Weighted Residual 0.33 % | Dv (50) 16.3 μm |
| Laser Obscuration 12.82 % | Dv (90) 90.6 μm |



| Result | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 1.79 | 12.7 | 40.74 | 76.0 | 88.15 | 454 | 99.07 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 2.69 | 14.5 | 45.47 | 86.4 | 89.54 | 516 | 99.37 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 3.77 | 16.4 | 50.20 | 98.1 | 90.76 | 586 | 99.57 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.00 | 3.12 | 5.05 | 18.7 | 54.85 | 111 | 91.84 | 666 | 99.72 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.00 | 3.55 | 6.59 | 21.2 | 59.35 | 127 | 92.80 | 756 | 99.82 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.00 | 4.03 | 8.44 | 24.1 | 63.62 | 144 | 93.67 | 859 | 99.90 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 0.00 | 4.58 | 10.65 | 27.4 | 67.61 | 163 | 94.45 | 976 | 99.96 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 0.00 | 5.21 | 13.25 | 31.1 | 71.29 | 186 | 95.18 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 0.00 | 5.92 | 16.23 | 35.3 | 74.63 | 211 | 95.86 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 0.00 | 6.72 | 19.58 | 40.1 | 77.63 | 240 | 96.51 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 0.08 | 7.64 | 23.28 | 45.6 | 80.30 | 272 | 97.12 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 0.25 | 8.68 | 27.29 | 51.8 | 82.66 | 310 | 97.70 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 0.58 | 9.86 | 31.58 | 58.9 | 84.74 | 352 | 98.23 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 1.09 | 11.2 | 36.08 | 66.9 | 86.56 | 400 | 98.69 | 2390 | 100.00 |

Analysis

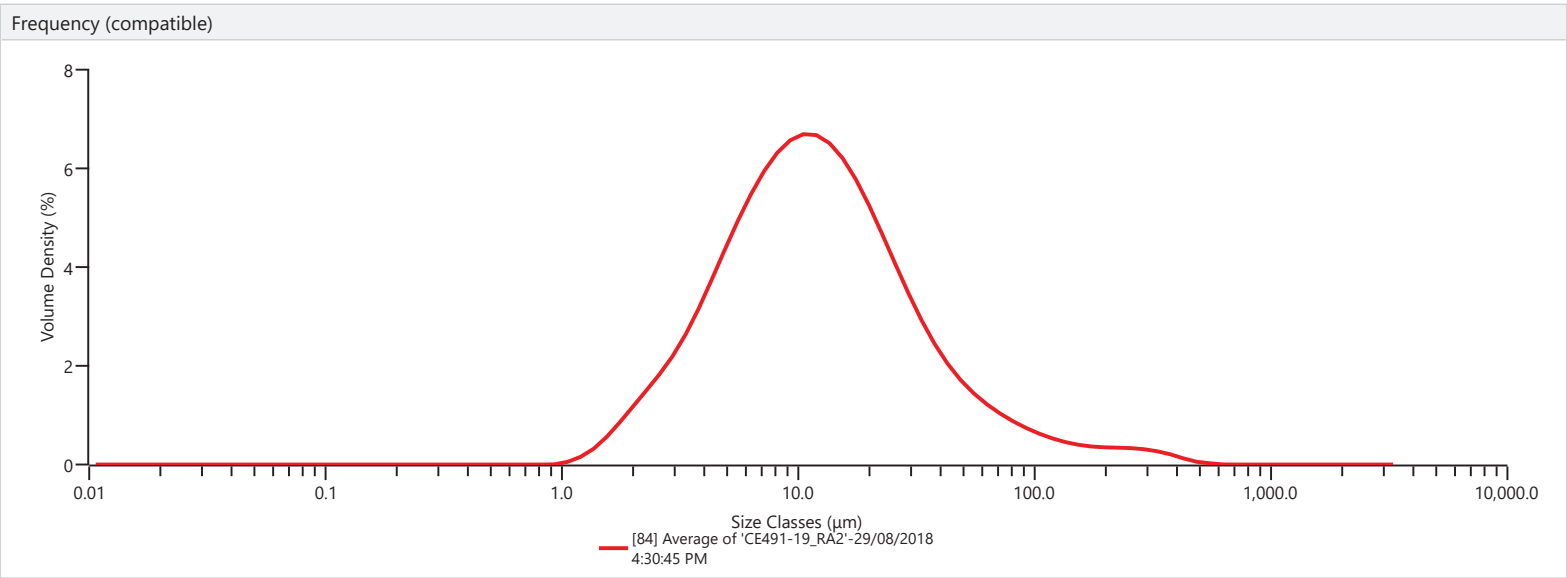
| | |
|--|---|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 29/08/2018 2:58:58 PM |
| Sample Name Average of 'CE491-18_CA2' | Measurement Date Time 29/08/2018 2:58:58 PM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0164 % |
| Particle Refractive Index 1.555 | Span 6.078 |
| Particle Absorption Index 0.010 | Uniformity 2.047 |
| Dispersant Name Water | Specific Surface Area 573.6 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 10.5 μm |
| Scattering Model Mie | D [4,3] 45.5 μm |
| Analysis Model General Purpose | Dv (10) 4.30 μm |
| Weighted Residual 0.36 % | Dv (50) 18.0 μm |
| Laser Obscuration 12.96 % | Dv (90) 113 μm |



| | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Result | | | | | | | | | | | | | |
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 2.00 | 12.7 | 38.68 | 76.0 | 85.00 | 454 | 99.42 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 2.95 | 14.5 | 42.88 | 86.4 | 86.78 | 516 | 99.72 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 4.10 | 16.4 | 47.09 | 98.1 | 88.38 | 586 | 99.88 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.00 | 3.12 | 5.45 | 18.7 | 51.26 | 111 | 89.82 | 666 | 99.97 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.00 | 3.55 | 7.04 | 21.2 | 55.34 | 127 | 91.12 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.00 | 4.03 | 8.92 | 24.1 | 59.27 | 144 | 92.29 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 0.00 | 4.58 | 11.11 | 27.4 | 63.02 | 163 | 93.37 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 0.00 | 5.21 | 13.63 | 31.1 | 66.56 | 186 | 94.36 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 0.00 | 5.92 | 16.47 | 35.3 | 69.87 | 211 | 95.30 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 0.00 | 6.72 | 19.60 | 40.1 | 72.96 | 240 | 96.18 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 0.11 | 7.64 | 23.01 | 45.6 | 75.81 | 272 | 97.00 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 0.31 | 8.68 | 26.66 | 51.8 | 78.43 | 310 | 97.76 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 0.68 | 9.86 | 30.52 | 58.9 | 80.83 | 352 | 98.43 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 1.24 | 11.2 | 34.54 | 66.9 | 83.02 | 400 | 98.98 | 2390 | 100.00 |

Analysis

| | |
|--|---|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 29/08/2018 4:30:45 PM |
| Sample Name Average of 'CE491-19_RA2' | Measurement Date Time 29/08/2018 4:30:45 PM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0127 % |
| Particle Refractive Index 1.555 | Span 3.491 |
| Particle Absorption Index 0.010 | Uniformity 1.449 |
| Dispersant Name Water | Specific Surface Area 745.9 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 8.04 μm |
| Scattering Model Mie | D [4,3] 23.1 μm |
| Analysis Model General Purpose | Dv (10) 3.66 μm |
| Weighted Residual 0.33 % | Dv (50) 11.5 μm |
| Laser Obscuration 13.06 % | Dv (90) 43.9 μm |



| | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Result | | | | | | | | | | | | | |
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 2.59 | 12.7 | 54.32 | 76.0 | 95.00 | 454 | 99.93 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 3.84 | 14.5 | 59.75 | 86.4 | 95.73 | 516 | 99.98 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 5.36 | 16.4 | 64.93 | 98.1 | 96.35 | 586 | 100.00 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.00 | 3.12 | 7.17 | 18.7 | 69.75 | 111 | 96.87 | 666 | 100.00 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.00 | 3.55 | 9.36 | 21.2 | 74.14 | 127 | 97.31 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.00 | 4.03 | 11.99 | 24.1 | 78.04 | 144 | 97.69 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 0.00 | 4.58 | 15.11 | 27.4 | 81.43 | 163 | 98.02 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 0.00 | 5.21 | 18.74 | 31.1 | 84.33 | 186 | 98.32 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 0.00 | 5.92 | 22.86 | 35.3 | 86.77 | 211 | 98.61 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 0.04 | 6.72 | 27.43 | 40.1 | 88.81 | 240 | 98.89 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 0.17 | 7.64 | 32.39 | 45.6 | 90.51 | 272 | 99.17 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 0.43 | 8.68 | 37.66 | 51.8 | 91.93 | 310 | 99.43 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 0.89 | 9.86 | 43.15 | 58.9 | 93.13 | 352 | 99.66 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 1.61 | 11.2 | 48.74 | 66.9 | 94.14 | 400 | 99.83 | 2390 | 100.00 |

| | |
|------------------|---|
| Note/Memo | CSIRO P4 Project Investigations |
| To: | Ali Watters (HKA) |
| From: | Brad Angel, Lucas Heights, NSW |
| Date: | 28 September 2018 |
| Copy: | Ryan Fraser, Stuart Simpson and Ellen Porter (SHL) |
| Our reference: | CSIRO P4 – Memo 3 |
| Classification: | Internal use only |
| Subject: | Chemical characterisation of composite excavated rock samples |

Background

The CSIRO was engaged by Haskoning Australia Pty Ltd (RHDHV) to undertake an investigation of the pollutant release from excavated rock placed in Talbingo and Tantangara reservoirs (a map of the sample sites will be prepared at a later date for incorporation into an interpretive report). The third phase of the work involved chemical characterisation of the composite excavated rock samples.

This technical memo describes the preliminary results to date.

Methodology for preparing excavated rock fine particle composites

The reasoning for the choice of excavated rock materials used to create composites is provided in the accompanying CSIRO study P2. In brief, there were available 50 g quantities of excavated rock materials (rock milled to a fine particle size, <75 µm) from six different geological zones, and for each zone samples were selected to represent baseline and enriched materials. Excavated rock composites were prepared by combining 50 g of each of the samples shown in each column of Table 1 and homogenising thoroughly. Between 4 and 8 individual samples comprised each composite.

Table 1. Individual <75 µm excavated rock samples that comprised each excavated rock composite tested.

| Composite name (individual samples in corresponding column) | | | | | | | | | | | |
|---|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 1B | 1E | 2B | 2E | 3B | 3E | 4B | 4E | 5B | 5E | 7B | 7E |
| BH6105- R-0063 | BH6102- R-0045 | BH5104- R-0122 | BH5104- R-0138 | BH4106- R-0270 | BH4106- R-0273 | BH4103- R-0001 | BH4103- R-0008 | BH3101- R-0257 | BH3102- R-0329 | BH4102- R-0315 | BH5105- R-0147 |
| BH4105- R-0362 | BH7105- R-0039 | BH5104- R-0133 | BH5104- R-0114 | BH4106- R-0271 | BH4106- R-0274 | BH4103- R-0003 | BH4103- R-0409 | BH3101- R-0259 | BH3101- R-0263 | BH4102- R-0316 | BH5103- R-0066 |
| BH6105- R-0061 | BH7105- R-0396 | BH5101- R-0055 | BH5104- R-0109 | BH4106- R-0272 | BH4106- R-0276 | BH4103- R-0011 | BH4103- R-0026 | BH3101- R-0261 | BH3102- R-0331 | BH4102- R-0318 | BH5103- R-0080 |
| BH4105- R-0356 | BH4104- R-0294 | BH5104- R-0116 | BH5104- R-0113 | BH4106- R-0281 | BH4106- R-0278 | BH4103- R-0012 | BH3110- R-0413 | BH3106- R-0353 | BH3102- R-0320 | BH4105- R-0370 | BH5105- R-0146 |
| BH4104- R-0291 | BH4105- R-0371 | BH5105- R-0143 | BH8106- R-0406 | | | BH4103- R-0014 | BH3110- R-0407 | BH3104- R-0395 | BH3102- R-0322 | BH5104- R-0115 | |
| BH4105- R-0363 | BH6101- R-0226 | BH5104- R-0120 | BH5104- R-0110 | | | BH4103- R-0018 | BH3110- R-0408 | BH3101- R-0254 | BH3102- R-0321 | BH5103- R-0079 | |
| BH7105- R-0036 | BH7105- R-0038 | BH5104- R-0108 | BH5115- R-0388 | | | BH4103- R-0019 | BH3110- R-0411 | BH3106- R-0352 | BH3101- R-0255 | BH7104- R-0234 | |
| BH6105- R-0060 | | | | | | BH4102- R-0312 | BH4103- R-0017 | BH2102- R-0345 | BH3102- R-0319 | | |

The particle size distribution of the fine excavated rock composites

The particle size distribution of the fine excavated rock composites are shown in Table 2. Cumulative distribution plots and tables will be provided in the final report (but can be made available earlier if necessary). The mean diameter of the composites were in the range 21.0 to 41.3 μm . The Dv (50) (50% of particles had lower diameter than this value) were all less than 19 μm , indicating the sediments were predominantly silt. The Dv (90) (90% of particles had lower diameter than this value) were between 52 and 110 μm , indicating some components of the 75 μm -milled excavated rock samples underwent aggregation and increased above the milled size range. The particle size distribution of the milled excavated rock samples overlapped most of the particle size distribution of the Talbingo and Tantangara reservoir benthic sediments.

Table 2. The particle size distribution of the milled composite excavated rock samples.

| Sediment ID | Dv (10) (μm) | Dv (50) (μm) | Dv (90) (μm) | Mean diameter (μm) |
|------------------------|------------------------------|------------------------------|------------------------------|------------------------------------|
| 1B composite | 2.71 | 11.6 | 72.2 | 26.4 |
| 1E composite | 2.53 | 18.6 | 97.2 | 41.3 |
| 2B composite | 2.44 | 17.3 | 76.4 | 30.1 |
| 2E composite | 2.43 | 18.3 | 87.3 | 34.0 |
| 3B composite | 2.47 | 12.8 | 80.3 | 28.7 |
| 3E composite | 2.98 | 12.7 | 84.3 | 30.4 |
| 3E composite duplicate | 2.95 | 12.7 | 81.0 | 28.9 |
| 4B composite | 3.72 | 15.0 | 110 | 38.4 |
| 4E composite | 2.87 | 10.6 | 62.9 | 23.7 |
| 5B composite | 2.24 | 12.9 | 52.2 | 21.0 |
| 5E composite | 2.41 | 18.8 | 105 | 39.5 |
| 5E composite duplicate | 2.30 | 16.5 | 93.2 | 33.9 |
| 7B composite | 2.69 | 14.7 | 80.4 | 29.9 |
| 7E composite | 2.00 | 16.5 | 69.5 | 27.4 |

Note: Dv (x) refers to 10, 50 and 90th percentiles of particle diameters (on spherical volume basis)

Excavated rock porewater pH and redox potential (Eh)

In order to measure the excavated rock sample porewater pH and redox potential the composite materials were mixed with a composite mixture of the Talbingo reservoir water for 48 h. The majority of the overlying water was syringe filtered for analysis of dissolved analytes for an initial elutriate test (to be discussed in memo 4). The remaining water and excavated rock composite material was allowed to stand for ten days, after which the pH and redox potential were measured by inserting probes directly into each wet solid material.

The pH and redox potential of the porewaters of the excavated rock materials deposited in Talbingo water is shown in Table 3. The porewater pH was in the range 8.50-9.55 and had decreased from that measured in the elutriate solution following 48 h mixing (shown in brackets in Table 3). The redox potentials were all positive other than composite 5E, indicating oxic conditions prevailed in the porewaters.

Table 3. The pH and redox potential of the composite excavated rock material mixed with Talbingo reservoir water and allowed to stand for 10 days.

| Sample ID | pH ^a | Redox, Eh (mV) |
|--------------|-----------------|----------------|
| 1B | 8.75 (9.20) | 180 |
| 1B duplicate | 8.85 (9.29) | 160 |
| 1E | 8.85 (9.33) | 160 |
| 2B | 8.55 (8.88) | 115 |
| 2E | 8.50 (9.35) | 20 |
| 3B | 9.55 (9.58) | 165 |
| 3E | 9.05 (9.81) | 150 |
| 4B | 8.80 (9.67) | 165 |
| 4E | 8.61 (9.37) | 180 |
| 4E duplicate | 8.55 (9.31) | 165 |
| 5B | 8.85 (9.57) | 80 |
| 5E | 8.75 (9.39) | -20 |
| 7B | 9.00 (9.56) | 160 |
| 7E | 8.75 (9.38) | 70 |

^a Value in brackets is the pH of the elutriate water after 48-h mixing

Total recoverable concentrations of metals, metalloid, and major cations in excavated rock composite

The total recoverable metal, metalloid, and major cation concentrations measured in the excavated rock composites are shown in Table 4. The concentrations of most metals were below the corresponding sediment quality guideline values (SQGVs). There was one exceedance for As, Pb and Zn, two exceedances for Cr, three exceedances for Cu, and nine for nickel. Of the excavated rock composites, 1E had the most SQGV-exceedances; Ag, Cr, Ni, Pb and Zn. It should be noted that the nickel value is considered an overly conservative value and it is not surprising that it exceeded the SQGV for many of the excavated rock composites (Vangheluwe et al., 2013; Simpson and Batley 2016).

Dilute-acid extractable concentrations of elements in the excavated rock composite

A significant portion of the total element concentration (extracted under pressure using hot concentrated acids) may release inert (not easily released) fractions of metals that exhibit very low bioavailability to organisms. For most metals, the ‘maximum bioavailable concentration’ can be determined by dilute-acid extractable metal (AEM) analyses, as commonly achieved by extracting the solid in 1 M hydrochloric acid for 1 h (Simpson and Batley 2016). AEM data can also be useful for interpreting the partitioning behaviour of elements between the dissolved and particulate phases, and the availability of reactive binding phases.

The 1 M HCl-extractable concentrations of metals, metalloids and major cations measured in the excavated rock composites are shown in Table 5. The concentrations of each parameter were all below the corresponding sediment quality guideline values (SQGVs) except for lead in composite 1E.

Table 4. Total recoverable concentrations of metals, metalloids, and major ions in the excavated rock composite

| Sediment ID | Al (mg/kg) | Fe (mg/kg) | Mn (mg/kg) | Na (mg/kg) | K (mg/kg) | Mg (mg/kg) | Ca (mg/kg) | P (mg/kg) | S (mg/kg) | |
|--------------------------|---------------|-----------------|---------------|---------------|---------------|---------------|---------------|-----------------|---------------|---------------|
| Composite 1B | 15600 | 28700 | 636 | 180 | 2040 | 17600 | 7260 | 491 | 80 | |
| Composite 1B duplicate | 17300 | 31000 | 640 | 220 | 2440 | 18300 | 7630 | 483 | 77 | |
| Composite 1B mean | 16500 | 29800 | 638 | 200 | 2240 | 17900 | 7450 | 487 | 78 | |
| Composite 1E | 24900 | 46400 | 1320 | 240 | 2600 | 22400 | 7790 | 640 | 756 | |
| Composite 2B | 16100 | 28600 | 602 | 160 | 3190 | 8520 | 6000 | 423 | 160 | |
| Composite 2E | 11200 | 27300 | 413 | 110 | 3070 | 7110 | 11000 | 537 | 3790 | |
| Composite 3B | 24600 | 39000 | 727 | 400 | 1840 | 26400 | 21100 | 422 | 15 | |
| Composite 3E | 16800 | 24900 | 577 | 330 | 1080 | 15000 | 9980 | 459 | 13 | |
| Composite 4B | 11300 | 18200 | 464 | 190 | 1020 | 8020 | 12200 | 490 | 17 | |
| Composite 4E | 19200 | 41800 | 588 | 310 | 2060 | 10400 | 20200 | 900 | 5410 | |
| Composite 5B | 9200 | 15900 | 336 | 360 | 1880 | 6310 | 5440 | 516 | 260 | |
| Composite 5E | 18800 | 43500 | 644 | 700 | 1550 | 9680 | 11200 | 856 | 6050 | |
| Composite 7B | 11600 | 18800 | 525 | 370 | 2760 | 6340 | 13100 | 378 | 54 | |
| Composite 7E | 9960 | 15600 | 253 | 160 | 3310 | 5500 | 8080 | 469 | 1010 | |
| Minimum | 9200 | 15600 | 253 | 110 | 1020 | 5500 | 5440 | 378 | 13 | |
| Maximum | 24900 | 46400 | 1320 | 700 | 3310 | 26400 | 21100 | 900 | 6050 | |
| SQGV | NA | NA | NA | NA | NA | NA | NA | NA | NA | |
| Sediment ID | Ag (mg/kg) | As (mg/kg) | Ba (mg/kg) | Cd (mg/kg) | Co (mg/kg) | Cr (mg/kg) | Cu (mg/kg) | Hg (mg/kg) | Mo (mg/kg) | |
| Composite 1B | 0.046 | 6.1 | 42 | 0.03 | 18 | 63 | 27 | <0.03 | 0.16 | |
| Composite 1B duplicate | 0.055 | 6.1 | 49 | 0.029 | 18 | 67 | 27 | <0.03 | 0.13 | |
| Composite 1B mean | 0.051 | 6.1 | 45 | 0.03 | 18 | 65 | 27 | <0.03 | 0.14 | |
| Composite 1E | <u>2.4</u> | 13 | 82 | 1 | 21 | <u>113</u> | 51 | <0.03 | 0.21 | |
| Composite 2B | 0.13 | 5.3 | 97 | 0.034 | 12 | 66 | 8.2 | <0.03 | 0.31 | |
| Composite 2E | 0.27 | 14 | 65 | 0.044 | 14 | 29 | 28 | <0.03 | 0.23 | |
| Composite 3B | 0.029 | 0.93 | 11 | 0.031 | 29 | <u>118</u> | 59 | <0.03 | 0.1 | |
| Composite 3E | 0.045 | 2.2 | 19 | 0.019 | 20 | 76 | 62 | <0.03 | 0.08 | |
| Composite 4B | 0.072 | 5.6 | 32 | 0.042 | 8.8 | 13 | 15 | <0.03 | 0.33 | |
| Composite 4E | 0.38 | <u>39</u> | 66 | 0.238 | 21 | 12 | <u>90</u> | <0.03 | 1.6 | |
| Composite 5B | 0.052 | 3.4 | 53 | 0.014 | 6.3 | 20 | 6.1 | <0.03 | 2.1 | |
| Composite 5E | 0.2 | 12 | 37 | 0.121 | 19 | 25 | <u>338</u> | <0.03 | 1.3 | |
| Composite 7B | 0.06 | 2.7 | 64 | 0.043 | 6.5 | 19 | 11 | <0.03 | 0.13 | |
| Composite 7E | 0.18 | 6.5 | 2090 | 0.025 | 6.3 | 13 | <u>88</u> | <0.03 | 0.14 | |
| Minimum | 0.029 | 0.93 | 10.9 | 0.014 | 6.27 | 11.7 | 6.1 | <0.03 | 0.08 | |
| Maximum | 2.4 | 38.5 | 2090 | 1.05 | 28.5 | 118 | 338 | <0.03 | 2.11 | |
| SQGV | 1 | 20 | NA | 1.5 | NA | 80 | 65 | 0.15 | NA | |
| Sediment ID | Ni (mg/kg) | Pb (mg/kg) | Sb (mg/kg) | Se (mg/kg) | Sn (mg/kg) | Sr (mg/kg) | Th (mg/kg) | U (mg/kg) | V (mg/kg) | Zn (mg/kg) |
| Composite 1B | <u>92</u> | 11 | 0.34 | 0.08 | 0.48 | 28 | 9.2 | 0.71 | 36 | 75 |
| Composite 1B duplicate | <u>93</u> | 9.9 | 0.43 | 0.08 | 0.62 | 29 | 11 | 1 | 39 | 76 |
| Composite 1B mean | 93 | 10 | 0.38 | 0.08 | 0.55 | 28 | 10 | 0.86 | 38 | 76 |
| Composite 1E | <u>134</u> | <u>214</u> | 0.92 | 0.12 | 0.59 | 33 | 7.9 | 0.75 | 71 | <u>543</u> |
| Composite 2B | <u>28</u> | 5.2 | 0.45 | 0.04 | 0.86 | 18 | 10 | 1.2 | 44 | 58 |
| Composite 2E | <u>31</u> | 11 | 2.2 | 0.18 | 0.65 | 48 | 9.1 | 1.1 | 23 | 45 |
| Composite 3B | <u>42</u> | 0.61 | 0.03 | 0.02 | 0.35 | 30 | 0.67 | 0.1 | 70 | 66 |
| Composite 3E | <u>39</u> | 2.3 | 0.1 | 0.03 | 0.4 | 13 | 5.3 | 0.33 | 34 | 62 |
| Composite 4B | 0.17 | 0.04 | 0.55 | 26 | 11 | 0.79 | 14 | 52 | 490 | 17 |
| Composite 4E | 0.63 | 0.30 | 0.41 | 50 | 4.7 | 1.3 | 71 | 104 | 900 | 5410 |
| Composite 5B | 0.10 | 0.03 | 0.38 | 21 | 7.5 | 0.99 | 22 | 22 | 516 | 260 |
| Composite 5E | 0.21 | 1.0 | 1.0 | 51 | 5.3 | 0.84 | 80 | 76 | 856 | 6050 |
| Composite 7B | 0.37 | 0.03 | 0.74 | 73 | 11 | 1.4 | 19 | 35 | 378 | 54 |
| Composite 7E | 1.2 | 0.03 | 2.0 | 63 | 8.8 | 1.2 | 14 | 32 | 469 | 1010 |
| Minimum | 0.029 | <0.01 | 0.35 | 13.1 | 0.67 | 0.10 | 13.5 | 79 | 378 | 13 |
| Maximum | 2.17 | 1.03 | 1.98 | 73 | 11.5 | 1.38 | 79.5 | 114 | 900 | 6050 |
| SQGV | NA | NA | NA | NA | NA | NA | NA | 200 | NA | NA |

SQGV = the sediment quality guideline values (Simpson et al., 2013). Values are bold underline where the SQGV is exceeded.

Table 5. Dilute-acid extractable concentrations of metals, metalloids, and major ions in the rock composites.

| Sediment ID | Al (mg/kg) | Fe (mg/kg) | Mn (mg/kg) | Na (mg/kg) | K (mg/kg) | Mg (mg/kg) | Ca (mg/kg) | P (mg/kg) | S (mg/kg) | |
|--------------------------|---------------|---------------|---------------|-----------------|---------------|---------------|---------------|-----------------|---------------|---------------|
| Composite 1B | 2410 | 4610 | 343 | 143 | 1100 | 3060 | 7490 | 523 | <30 | |
| Composite 1B duplicate | 2420 | 4580 | 345 | 140 | 1130 | 3050 | 7510 | 512 | <30 | |
| Composite 1B mean | 2420 | 4600 | 344 | 141 | 1120 | 3060 | 7500 | 518 | <30 | |
| Composite 1E | 3270 | 6460 | 679 | 136 | 1050 | 3510 | 8430 | 664 | 38 | |
| Composite 2B | 2960 | 5570 | 514 | 83 | 1100 | 2080 | 6620 | 359 | <30 | |
| Composite 2E | 2100 | 6310 | 298 | 82 | 1440 | 1400 | 11700 | 545 | <30 | |
| Composite 3B | 2920 | 3830 | 203 | 189 | 1420 | 3120 | 15100 | 483 | <30 | |
| Composite 3E | 2540 | 2780 | 119 | 220 | 643 | 1720 | 8840 | 501 | <30 | |
| Composite 4B | 1160 | 1850 | 263 | 110 | 552 | 674 | 12400 | 519 | <30 | |
| Composite 4E | 2750 | 5470 | 319 | 146 | 765 | 1260 | 20100 | 952 | <30 | |
| Composite 5B | 2800 | 5820 | 131 | 246 | 755 | 1330 | 6570 | 919 | 45 | |
| Composite 5E | 1810 | 4250 | 172 | 206 | 930 | 1400 | 5340 | 546 | <30 | |
| Composite 7B | 1630 | 4150 | 452 | 192 | 1080 | 705 | 14000 | 400 | <30 | |
| Composite 7E | 2110 | 3140 | 198 | 119 | 1920 | 686 | 8770 | 479 | 413 | |
| Minimum | 1160 | 1850 | 119 | 82 | 552 | 674 | 5340 | 359 | 38 | |
| Maximum | 3270 | 6460 | 679 | 246 | 1920 | 3510 | 20100 | 952 | 413 | |
| SQGV | NA | NA | NA | NA | NA | NA | NA | NA | NA | |
| Sediment ID | Ag (mg/kg) | As (mg/kg) | Ba (mg/kg) | Cd (mg/kg) | Co (mg/kg) | Cr (mg/kg) | Cu (mg/kg) | Hg (mg/kg) | Mo (mg/kg) | |
| Composite 1B | 0.016 | 1.9 | 32 | 0.018 | 2.5 | 6.3 | 3.3 | <0.02 | 0.08 | |
| Composite 1B duplicate | 0.015 | 2 | 31 | 0.018 | 2.6 | 6.2 | 3.6 | <0.02 | 0.06 | |
| Composite 1B mean | 0.015 | 2 | 31 | 0.018 | 2.6 | 6.3 | 3.4 | <0.02 | 0.07 | |
| Composite 1E | 0.085 | 2.3 | 57 | 0.18 | 2 | 12 | 2.3 | <0.02 | 0.07 | |
| Composite 2B | 0.033 | 0.63 | 84 | 0.015 | 4.3 | 12 | 1.3 | <0.02 | 0.08 | |
| Composite 2E | 0.084 | 1.3 | 43 | 0.02 | 1.2 | 4.6 | 3.1 | <0.02 | 0.08 | |
| Composite 3B | 0.004 | 0.57 | 7.4 | 0.013 | 3.4 | 13 | 18 | <0.02 | <0.02 | |
| Composite 3E | 0.017 | 1.5 | 12 | 0.012 | 2.1 | 8.8 | 21 | <0.02 | 0.04 | |
| Composite 4B | 0.015 | 1.6 | 21 | 0.029 | 0.4 | 1.9 | 2.9 | <0.02 | 0.05 | |
| Composite 4E | 0.074 | 1.9 | 27 | 0.079 | 1.2 | 2.8 | 4.9 | <0.02 | 0.08 | |
| Composite 5B | 0.049 | 0.76 | 30 | 0.026 | 1.1 | 3.8 | 22 | <0.02 | 0.08 | |
| Composite 5E | 0.015 | 0.68 | 36 | 0.007 | 0.82 | 4.3 | 1.4 | <0.02 | 0.3 | |
| Composite 7B | 0.01 | 0.74 | 45 | 0.019 | 0.48 | 4.3 | 0.8 | <0.02 | 0.05 | |
| Composite 7E | 0.042 | 1.4 | 1840 | 0.011 | 0.61 | 2.7 | 4.1 | <0.02 | 0.07 | |
| Minimum | 0.004 | 0.57 | 7.4 | 0.007 | 0.4 | 1.9 | 0.8 | <0.02 | 0.04 | |
| Maximum | 0.085 | 2.3 | 1840 | 0.184 | 4.27 | 13 | 22 | <0.02 | 0.3 | |
| SQGV | 1 | 20 | NA | 1.5 | NA | 80 | 65 | 0.15 | NA | |
| Sediment ID | Ni (mg/kg) | Pb (mg/kg) | Sb (mg/kg) | Se (mg/kg) | Sn (mg/kg) | Sr (mg/kg) | Th (mg/kg) | U (mg/kg) | V (mg/kg) | Zn (mg/kg) |
| Composite 1B | 8.7 | 7.2 | 0.1 | <0.01 | 0.17 | 28 | 4.2 | 0.26 | 5.3 | 14 |
| Composite 1B duplicate | 8.3 | 7.3 | 0.13 | 0.01 | 0.17 | 27 | 4.4 | 0.27 | 5.2 | 14 |
| Composite 1B mean | 8.5 | 7.2 | 0.12 | 0.01 | 0.17 | 28 | 4.3 | 0.27 | 5.2 | 14 |
| Composite 1E | 13 | 197 | 0.21 | 0.01 | 0.22 | 33 | 3.1 | 0.24 | 9.1 | 86 |
| Composite 2B | 5.4 | 3.7 | 0.093 | <0.01 | 0.2 | 17 | 2.7 | 0.27 | 8.2 | 15 |
| Composite 2E | 3.1 | 7.1 | 0.67 | 0.01 | 0.23 | 44 | 3.3 | 0.38 | 4.5 | 8 |
| Composite 3B | 5.3 | 0.14 | 0.005 | <0.01 | 0.03 | 5.8 | 0.17 | 0.01 | 8.3 | 8.9 |
| Composite 3E | 4.3 | 1.1 | 0.024 | <0.01 | 0.06 | 7 | 1.4 | 0.07 | 3.4 | 7.1 |
| Composite 4B | 0.6 | 11 | 0.03 | <0.01 | 0.09 | 20 | 4.7 | 0.19 | 1.1 | 3.8 |
| Composite 4E | 1.1 | 6.9 | 0.086 | <0.01 | 0.06 | 44 | 1.5 | 0.28 | 9.7 | 14 |
| Composite 5B | 1.5 | 4.8 | 0.075 | 0.01 | 0.09 | 13 | 3 | 0.19 | 9.4 | 16 |
| Composite 5E | 1.8 | 1.9 | 0.052 | <0.01 | 0.14 | 13 | 4.5 | 0.29 | 2.9 | 3.8 |
| Composite 7B | 0.8 | 6.3 | 0.082 | <0.01 | 0.16 | 71 | 3.9 | 0.26 | 3 | 3.7 |
| Composite 7E | 0.9 | 4.4 | 0.21 | 0.01 | 0.63 | 62 | 2.2 | 0.4 | 2.6 | 6 |
| Minimum | 0.6 | 0.1 | 0.005 | <0.01 | 0.03 | 5.8 | 0.17 | 0.01 | 1.1 | 79 |
| Maximum | 13 | 197 | 0.67 | 0.01 | 0.63 | 71 | 4.7 | 0.4 | 9.7 | 114 |
| SQGV | 21 | 50 | NA | NA | NA | NA | NA | NA | NA | 200 |

SQGV = the sediment quality guideline values (Simpson et al., 2013). Values are **bold underline** where the SQGV is exceeded.

Ratio of concentrations: dilute-acid extractable/total recoverable (%).

The elemental ratios of the concentrations measured in dilute-acid extractable and total recoverable forms were calculated and expressed as a percentage in Table 6. As well as providing information on the extractability of the different elements, these calculations serve as a cross check of the analyses undertaken on different subsamples. It is not uncommon for the percentage to be a little greater than 100% when the elements are highly extractable by both methods, but where the percentage is considerably greater than 100% (e.g. >130%) this often reflects heterogeneity (composition or particle size) in the subsamples taken for each separate analysis despite the thorough homogenisation. For example, for Composite 5B the percentage is unexpectedly high for a number of elements.

Table 6. Ratio of concentrations: dilute-acid extractable/total recoverable (%).

| Sediment ID | Al | Fe | Mn | Na | K | Mg | Ca | P | S | |
|------------------------|-----|------|-----|------|-----|------|------|------|-----|-----|
| Composite 1B | 15% | 16% | 54% | 79% | 54% | 17% | 103% | 107% | ND | |
| Composite 1B duplicate | 14% | 15% | 54% | 64% | 46% | 17% | 98% | 106% | ND | |
| Composite 1B mean | 15% | 15% | 54% | 71% | 50% | 17% | 101% | 106% | ND | |
| Composite 1E | 13% | 14% | 51% | 57% | 40% | 16% | 108% | 104% | 5% | |
| Composite 2B | 18% | 19% | 85% | 52% | 34% | 24% | 110% | 85% | ND | |
| Composite 2E | 19% | 23% | 72% | 75% | 47% | 20% | 106% | 101% | ND | |
| Composite 3B | 12% | 10% | 28% | 47% | 77% | 12% | 72% | 114% | ND | |
| Composite 3E | 15% | 11% | 21% | 67% | 60% | 11% | 89% | 109% | ND | |
| Composite 4B | 10% | 10% | 57% | 58% | 54% | 8% | 102% | 106% | ND | |
| Composite 4E | 14% | 13% | 54% | 47% | 37% | 12% | 100% | 106% | ND | |
| Composite 5B | 30% | 37% | 39% | 68% | 40% | 21% | 121% | 178% | 17% | |
| Composite 5E | 10% | 10% | 27% | 29% | 60% | 14% | 48% | 64% | ND | |
| Composite 7B | 14% | 22% | 86% | 52% | 39% | 11% | 107% | 106% | ND | |
| Composite 7E | 21% | 20% | 78% | 74% | 58% | 12% | 109% | 102% | 41% | |
| Sediment ID | Ag | As | Ba | Cd | Co | Cr | Cu | Hg | Mo | |
| Composite 1B | 35% | 31% | 76% | 60% | 14% | 10% | 12% | ND | 50% | |
| Composite 1B duplicate | 27% | 33% | 63% | 62% | 14% | 9% | 13% | ND | 46% | |
| Composite 1B mean | 29% | 33% | 69% | 60% | 14% | 10% | 13% | ND | 50% | |
| Composite 1E | 4% | 18% | 70% | 18% | 10% | 11% | 5% | ND | 33% | |
| Composite 2B | 25% | 12% | 87% | 44% | 36% | 18% | 16% | ND | 26% | |
| Composite 2E | 31% | 9% | 66% | 45% | 9% | 16% | 11% | ND | 35% | |
| Composite 3B | 14% | 61% | 67% | 42% | 12% | 11% | 31% | ND | ND | |
| Composite 3E | 38% | 68% | 63% | 63% | 11% | 12% | 34% | ND | 50% | |
| Composite 4B | 21% | 29% | 66% | 69% | 5% | 15% | 19% | ND | 15% | |
| Composite 4E | 19% | 5% | 41% | 33% | 6% | 23% | 5% | ND | 5% | |
| Composite 5B | 94% | 22% | 57% | 186% | 17% | 19% | 361% | ND | 4% | |
| Composite 5E | 8% | 6% | 97% | 6% | 4% | 17% | 0% | ND | 23% | |
| Composite 7B | 17% | 27% | 70% | 44% | 7% | 23% | 7% | ND | 38% | |
| Composite 7E | 23% | 22% | 88% | 44% | 10% | 21% | 5% | ND | 50% | |
| Sediment ID | Ni | Pb | Sb | Se | Sn | Sr | Th | U | V | Zn |
| Composite 1B | 9% | 65% | 29% | ND | 35% | 100% | 46% | 37% | 15% | 19% |
| Composite 1B duplicate | 9% | 74% | 30% | 13% | 27% | 93% | 40% | 27% | 13% | 18% |
| Composite 1B mean | 9% | 72% | 32% | 13% | 31% | 100% | 43% | 31% | 14% | 18% |
| Composite 1E | 10% | 92% | 23% | 8% | 37% | 100% | 39% | 32% | 13% | 16% |
| Composite 2B | 19% | 71% | 21% | ND | 23% | 94% | 27% | 23% | 19% | 26% |
| Composite 2E | 10% | 65% | 30% | 6% | 35% | 92% | 36% | 35% | 20% | 18% |
| Composite 3B | 13% | 23% | 17% | ND | 9% | 19% | 25% | 10% | 12% | 13% |
| Composite 3E | 11% | 48% | 24% | ND | 15% | 54% | 26% | 21% | 10% | 11% |
| Composite 4B | 5% | 65% | 18% | ND | 16% | 77% | 43% | 24% | 8% | 7% |
| Composite 4E | 7% | 70% | 14% | ND | 15% | 88% | 32% | 22% | 14% | 13% |
| Composite 5B | 9% | 178% | 75% | 33% | 24% | 62% | 40% | 19% | 43% | 73% |
| Composite 5E | 7% | 24% | 25% | ND | 14% | 25% | 85% | 35% | 4% | 5% |
| Composite 7B | 8% | 72% | 22% | ND | 22% | 97% | 35% | 19% | 16% | 11% |
| Composite 7E | 8% | 51% | 18% | 33% | 32% | 98% | 25% | 33% | 19% | 19% |

Not calculated where values were <LOD (e.g. TR-S, TR-Hg), and marked ND.

For most of the excavated rock composites, the percent of total recoverable elements in dilute-acid extractable forms was generally <30% for Ag, Al, As, Co, Cr, Cu, Fe, Mg, Ni, S, Sb, Sn, U, V and Zn. The percentage of dilute-acid extractable Ba, Pb and Sr was generally >50%.

Summary

The fine excavated rock composites used for testing were predominantly silt-sized (<63 µm), with only a small fraction of the samples aggregating to larger diameters than this size range.

The porewater pH of the excavated rock samples mixed with Talbingo water and allowed to stand for 10 days was in the range 8.50-9.55 and had decreased from that measured in the elutriate solution following 48 h mixing. This pH range is significantly greater than that of the waters from Talbingo (7.05-7.60) and Tantangara (6.70-7.10).

Composite 1E had the greatest number of metals with total recoverable concentrations exceeding sediment quality guideline values (SQGVs). When considering the diluted-extractable metal concentrations, there was only one exceedance; lead for composite 1E (197 mg Pb/kg).

References

Simpson SL and Batley GE (2016) Sediment Quality Assessment: A Practical Guide. CSIRO Publishing, Melbourne, Victoria. 359 p. <https://publications.csiro.au/rpr/download?pid=csiro:EP165955&dsid=DS1>

Vangheluwe MLU, Verdonck FAM, Besser JM, Brumbaugh WG, Ingersoll CG, Schlegel CE, Garman ER (2013) Improving sediment-quality guidelines for nickel: Development and application of predictive bioavailability models to assess chronic toxicity of nickel in freshwater sediments. *Environmental Toxicology and Chemistry* 32, 2507–2519.

Rock analyses

Total recoverable metals (TRM)

| Sample ID | Sample Description | Al | Ag | As | Au | B | Ba | Be | Bi | Cd | Ca | Ce | Co | Cr | Cu | Cs | Dy | Er | Eu |
|------------------|---------------------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) |
| CE491-20 | Rock composite 1B | 15600 | 0.046 | 6.1 | <0.001 | 2.0 | 42 | 0.70 | 0.26 | 0.030 | 7260 | 48 | 18 | 63 | 27 | 5.0 | 2.5 | 1.2 | 0.80 |
| CE491-20 dig dup | Rock composite 1B dig dup | 17300 | 0.055 | 6.1 | 0.003 | 2.8 | 49 | 0.77 | 0.26 | 0.029 | 7630 | 62 | 18 | 67 | 27 | 5.5 | 3.0 | 1.4 | 0.99 |
| CE491-20 avg | Rock composite 1B avg | 16500 | 0.051 | 6.1 | 0.002 | 2.4 | 45 | 0.73 | 0.26 | 0.030 | 7450 | 55 | 18 | 65 | 27 | 5.3 | 2.7 | 1.3 | 0.90 |
| CE491-21 | Rock composite 1E | 24900 | 2.4 | 13 | <0.001 | 3.1 | 82 | 0.89 | 0.40 | 1.0 | 7790 | 56 | 21 | 113 | 51 | 4.8 | 2.8 | 1.3 | 1.1 |
| CE491-22 | Rock composite 2B | 16100 | 0.13 | 5.1 | <0.001 | 2.5 | 97 | 0.98 | 0.19 | 0.039 | 6000 | 63 | 12 | 65 | 8.0 | 5.7 | 2.6 | 1.2 | 0.84 |
| CE491-22 dig dup | Rock composite 2B dig dup | 16100 | 0.13 | 5.5 | <0.001 | 2.6 | 97 | 1.0 | 0.18 | 0.029 | 6010 | 63 | 12 | 67 | 8.3 | 5.9 | 2.6 | 1.2 | 0.85 |
| CE491-22 avg | Rock composite 2B avg | 16100 | 0.13 | 5.3 | <0.001 | 2.5 | 97 | 0.99 | 0.18 | 0.034 | 6000 | 63 | 12 | 66 | 8.2 | 5.8 | 2.6 | 1.2 | 0.84 |
| CE491-23 | Rock composite 2E | 11200 | 0.27 | 14 | 0.004 | 2.7 | 65 | 1.1 | 0.63 | 0.044 | 11000 | 48 | 14 | 29 | 28 | 5.8 | 2.4 | 1.0 | 0.82 |
| CE491-24 | Rock composite 3B | 24600 | 0.029 | 0.93 | <0.001 | 0.6 | 11 | 0.22 | 0.004 | 0.031 | 21100 | 4.6 | 29 | 118 | 59 | 0.75 | 1.5 | 1.1 | 0.24 |
| CE491-25 | Rock composite 3E | 16800 | 0.045 | 2.2 | <0.001 | 0.3 | 19 | 0.25 | 0.10 | 0.019 | 9980 | 14 | 20 | 76 | 62 | 0.58 | 1.2 | 0.69 | 0.23 |
| CE491-26 | Rock composite 4B | 11300 | 0.072 | 5.6 | <0.001 | 0.1 | 32 | 0.31 | 0.25 | 0.042 | 12200 | 52 | 8.8 | 13 | 15 | 0.95 | 2.5 | 1.2 | 0.63 |
| CE491-27 | Rock composite 4E | 19200 | 0.38 | 39 | <0.001 | 0.7 | 66 | 0.24 | 0.15 | 0.238 | 20200 | 36 | 21 | 12 | 90 | 0.50 | 2.6 | 1.5 | 0.81 |
| CE491-28 | Rock composite 5B | 9200 | 0.052 | 3.4 | <0.001 | 1.0 | 53 | 0.41 | 0.11 | 0.014 | 5440 | 43 | 6.3 | 20 | 6.1 | 0.94 | 1.9 | 0.93 | 0.61 |
| CE491-29 | Rock composite 5E | 18800 | 0.20 | 12 | <0.001 | 1.7 | 37 | 0.71 | 0.30 | 0.121 | 11200 | 37 | 19 | 25 | 338 | 1.6 | 2.6 | 1.3 | 0.82 |
| CE491-30 | Rock composite 7B | 11600 | 0.060 | 2.7 | <0.001 | 1.4 | 64 | 0.69 | 0.092 | 0.043 | 13100 | 53 | 6.5 | 19 | 11 | 4.0 | 2.9 | 1.5 | 0.72 |
| CE491-31 | Rock composite 7E | 9940 | 0.18 | 6.4 | <0.001 | 1.5 | 2081 | 1.3 | 3.1 | 0.030 | 8060 | 73 | 6.3 | 13 | 88 | 11 | 2.1 | 0.89 | 1.2 |
| CE491-31 dig dup | Rock composite 7E dig dup | 9990 | 0.18 | 6.5 | <0.001 | 1.6 | 2092 | 1.3 | 3.1 | 0.019 | 8110 | 74 | 6.4 | 13 | 88 | 11 | 2.1 | 0.88 | 1.2 |
| CE491-31 avg | Rock composite 7E avg | 9960 | 0.18 | 6.5 | <0.001 | 1.6 | 2086 | 1.3 | 3.1 | 0.025 | 8080 | 74 | 6.3 | 13 | 88 | 11 | 2.1 | 0.89 | 1.2 |
| SED-43 LOD (3σ) | --- | 30 | 0.001 | 0.01 | 0.001 | 0.1 | 0.02 | 0.002 | 0.003 | 0.002 | 3 | 0.002 | 0.001 | 0.02 | 0.02 | 0.001 | 0.001 | 0.001 | 0.001 |
| Method Code | --- | | | | | | | | | | | | | | | | | | |

C-223 Total recoverable metals by Aqua Regia microwave digest

C-209: ICP-MS

C-229: ICP-AES

Certified Reference Materials

| Sample ID | Sample Description | Al | Ag | As | Au | B | Ba | Be | Bi | Cd | Ca | Ce | Co | Cr | Cu | Cs | Dy | Er | Eu |
|-----------------|--------------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) |
| ERM-CC018-1 | --- | 5360 | 2.2 | 22 | 0.036 | 5.9 | 378 | 0.58 | 1.1 | 5.9 | 16500 | 17 | 5.4 | 137 | 82 | 0.91 | 0.98 | 0.51 | 0.31 |
| ERM-CC018-2 | --- | 4670 | 2.2 | 21 | 0.037 | 4.8 | 372 | 0.52 | 1.2 | 6.0 | 16400 | 15 | 4.9 | 133 | 81 | 0.76 | 0.84 | 0.45 | 0.28 |
| ERM-CC018 avg | --- | 5020 | 2.2 | 21 | 0.037 | 5.4 | 375 | 0.55 | 1.2 | 6.0 | 16500 | 16 | 5.1 | 135 | 82 | 0.84 | 0.91 | 0.48 | 0.29 |
| Certified Value | --- | --- | --- | 22.9 ± 1.3 | --- | --- | --- | --- | --- | 5.4 ± 0.5 | --- | --- | 5.9 ± 0.4 | 129 ± 6 | 80 ± 4 | --- | --- | --- | --- |
| OREAS-25a-1 | --- | 52400 | 0.092 | 5.4 | 0.015 | 5.2 | 51 | 0.71 | 0.32 | 0.071 | 1240 | 42 | 6.3 | 90 | 28 | 5.5 | 1.4 | 0.64 | 0.57 |
| OREAS-25a-2 | --- | 65200 | 0.11 | 6.2 | 0.005 | 7.1 | 57 | 0.79 | 0.33 | 0.063 | 1290 | 44 | 7.0 | 95 | 29 | 6.0 | 1.5 | 0.69 | 0.59 |
| OREAS-25a avg | --- | 58800 | 0.099 | 5.8 | 0.010 | 6.1 | 54 | 0.75 | 0.33 | 0.067 | 1260 | 43 | 6.7 | 92 | 29 | 5.8 | 1.5 | 0.66 | 0.58 |
| Certified Value | --- | --- | --- | --- | --- | --- | 56 | --- | 0.30 | --- | 1500 | 33.1 | 5.72 | 73 | 24.9 | 4.45 | --- | --- | --- |

ERM-CC018 is a European sandy soil reference material

OREAS-25a is an Australian reference soil. Certified values reported are for an Aqua Regia Digestion

Spike Recoveries

| Sample ID | Sample Description | Al | Ag | As | Au | B | Ba | Be | Bi | Cd | Ca | Ce | Co | Cr | Cu | Cs | Dy | Er | Eu |
|-----------|--------------------|-----|-----|-----|-----|----|----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| % | % | % | % | % | % | % | % | % | % | % | % | % | % | % | % | % | % | % | % |
| CE491-22 | Rock composite 2B | --- | 104 | 108 | 104 | 91 | 88 | 107 | 107 | 107 | --- | 111 | 108 | 126 | 109 | 110 | 111 | 111 | 110 |
| CE491-31 | Rock composite 7E | 86 | 127 | 113 | 105 | 95 | 96 | 109 | 108 | 108 | 87 | 112 | 109 | 113 | 114 | 114 | 111 | 111 | 111 |

Analyte of interest added to sample prior to analysis

Rock analyses

Total recoverable metals (TRM)

| Sample ID | Sample Description | Fe TRM (µg/g) | Ga TRM (µg/g) | Gd TRM (µg/g) | Ge TRM (µg/g) | Hf TRM (µg/g) | Hg TRM (µg/g) | Ho TRM (µg/g) | In TRM (µg/g) | Ir TRM (µg/g) | K TRM (µg/g) | La TRM (µg/g) | Li TRM (µg/g) | Lu TRM (µg/g) | Mg TRM (µg/g) | Mn TRM (µg/g) | Mo TRM (µg/g) | Na TRM (µg/g) | Nb TRM (µg/g) |
|------------------|---------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|-----------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| CE491-20 | Rock composite 1B | 28700 | 5.6 | 3.9 | 0.15 | 0.38 | <0.03 | 0.43 | 0.021 | <0.002 | 2040 | 23 | 43 | 0.13 | 17600 | 636 | 0.16 | 180 | 0.045 |
| CE491-20 dig dup | Rock composite 1B dig dup | 31000 | 6.2 | 4.7 | 0.16 | 0.53 | <0.03 | 0.54 | 0.024 | <0.002 | 2440 | 30 | 45 | 0.15 | 18300 | 640 | 0.13 | 220 | 0.075 |
| CE491-20 avg | Rock composite 1B avg | 29800 | 5.9 | 4.3 | 0.15 | 0.46 | <0.03 | 0.49 | 0.023 | <0.002 | 2240 | 27 | 44 | 0.14 | 17900 | 638 | 0.14 | 200 | 0.060 |
| CE491-21 | Rock composite 1E | 46400 | 9.8 | 4.5 | 0.16 | 0.43 | <0.03 | 0.51 | 0.075 | <0.002 | 2600 | 28 | 56 | 0.14 | 22400 | 1320 | 0.21 | 240 | 0.021 |
| CE491-22 | Rock composite 2B | 28500 | 5.6 | 4.3 | 0.16 | 0.45 | <0.03 | 0.45 | 0.023 | <0.002 | 3210 | 31 | 28 | 0.14 | 8520 | 602 | 0.31 | 170 | 0.018 |
| CE491-22 dll dup | Rock composite 2B dll dup | 28600 | 5.7 | 4.4 | 0.17 | 0.46 | <0.03 | 0.46 | 0.023 | <0.002 | 3180 | 31 | 28 | 0.15 | 8520 | 603 | 0.31 | 160 | 0.015 |
| CE491-22 avg | Rock composite 2B avg | 28600 | 5.7 | 4.4 | 0.17 | 0.45 | <0.03 | 0.46 | 0.023 | <0.002 | 3190 | 31 | 28 | 0.14 | 8520 | 602 | 0.31 | 160 | 0.017 |
| CE491-23 | Rock composite 3E | 27300 | 4.1 | 3.9 | 0.13 | 0.47 | <0.03 | 0.41 | 0.028 | <0.002 | 3070 | 24 | 19 | 0.11 | 7110 | 413 | 0.23 | 110 | 0.027 |
| CE491-24 | Rock composite 3B | 39000 | 7.0 | 1.1 | 0.10 | 0.36 | <0.03 | 0.35 | 0.010 | <0.002 | 1840 | 2.1 | 14 | 0.11 | 26400 | 727 | 0.10 | 400 | 0.110 |
| CE491-25 | Rock composite 3E | 24900 | 5.2 | 1.3 | 0.07 | 0.27 | <0.03 | 0.24 | 0.006 | <0.002 | 1080 | 6.3 | 31 | 0.074 | 15000 | 577 | 0.08 | 330 | 0.119 |
| CE491-26 | Rock composite 4B | 18200 | 3.7 | 4.0 | 0.12 | 0.44 | <0.03 | 0.44 | 0.010 | <0.002 | 1020 | 25 | 20 | 0.13 | 8020 | 464 | 0.33 | 190 | 0.119 |
| CE491-27 | Rock composite 4E | 41800 | 6.5 | 3.4 | 0.12 | 0.77 | <0.03 | 0.51 | 0.019 | <0.002 | 2060 | 16 | 12 | 0.17 | 10400 | 588 | 1.6 | 310 | 0.121 |
| CE491-28 | Rock composite 5B | 15900 | 3.7 | 3.1 | 0.11 | 0.50 | <0.03 | 0.34 | 0.010 | <0.002 | 1880 | 21 | 5.3 | 0.11 | 6310 | 336 | 2.1 | 360 | 0.094 |
| CE491-29 | Rock composite 5E | 43500 | 8.2 | 3.5 | 0.22 | 0.59 | <0.03 | 0.48 | 0.037 | <0.002 | 1550 | 17 | 8.1 | 0.14 | 9680 | 644 | 1.3 | 700 | 0.154 |
| CE491-30 | Rock composite 7B | 18800 | 4.6 | 4.2 | 0.12 | 0.74 | <0.03 | 0.54 | 0.019 | <0.002 | 2760 | 26 | 19 | 0.18 | 6340 | 525 | 0.13 | 370 | 0.030 |
| CE491-31 | Rock composite 7E | 15600 | 3.4 | 4.5 | 0.11 | 0.69 | <0.03 | 0.35 | 0.071 | <0.002 | 3270 | 36 | 24 | 0.087 | 5480 | 251 | 0.14 | 160 | 0.006 |
| CE491-31 dll dup | Rock composite 7E dll dup | 15600 | 3.5 | 4.5 | 0.12 | 0.68 | <0.03 | 0.35 | 0.071 | <0.002 | 3340 | 36 | 24 | 0.087 | 5530 | 255 | 0.14 | 160 | 0.007 |
| CE491-31 avg | Rock composite 7E avg | 15600 | 3.4 | 4.5 | 0.12 | 0.69 | <0.03 | 0.35 | 0.071 | <0.002 | 3310 | 36 | 24 | 0.087 | 5500 | 253 | 0.14 | 160 | 0.007 |
| SED-43 LOD (3σ) | --- | 1 | 0.002 | 0.001 | 0.01 | 0.001 | 0.03 | 0.001 | 0.002 | 0.002 | 2 | 0.001 | 0.001 | 0.001 | 1 | 0.02 | 0.01 | 30 | 0.004 |
| Method Code | --- | C-223/C-229 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-229 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-229 | C-223/C-229 | C-223/C-209 | C-223/C-229 | C-223/C-209 |

Reference Materials

| Sample ID | Sample Description | Fe TRM (µg/g) | Ga TRM (µg/g) | Gd TRM (µg/g) | Ge TRM (µg/g) | Hf TRM (µg/g) | Hg TRM (µg/g) | Ho TRM (µg/g) | In TRM (µg/g) | Ir TRM (µg/g) | K TRM (µg/g) | La TRM (µg/g) | Li TRM (µg/g) | Lu TRM (µg/g) | Mg TRM (µg/g) | Mn TRM (µg/g) | Mo TRM (µg/g) | Na TRM (µg/g) | Nb TRM (µg/g) | |
|-----------------|--------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|-----------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|-----|
| ERM-CC018-1 | --- | 10100 | 2.9 | 1.3 | 0.84 | 0.26 | 1.4 | 0.19 | 0.075 | <0.002 | 829 | 8.1 | 7.3 | 0.064 | 1180 | 185 | 14 | 210 | 0.801 | |
| ERM-CC018-2 | --- | 9450 | 2.4 | 1.1 | 0.73 | 0.17 | 1.6 | 0.16 | 0.073 | <0.002 | 681 | 6.8 | 6.1 | 0.055 | 1080 | 178 | 14 | 180 | 0.719 | |
| ERM-CC018 avg | --- | 9780 | 2.7 | 1.2 | 0.79 | 0.22 | 1.5 | 0.17 | 0.074 | <0.002 | 755 | 7.5 | 6.7 | 0.060 | 1130 | 182 | 14 | 200 | 0.760 | |
| Certified Value | --- | --- | --- | --- | --- | --- | 1.38 ± 0.06 | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| OREAS-25a-1 | --- | 54500 | 22 | 2.4 | 0.06 | 0.98 | 0.09 | 0.25 | 0.090 | 0.017 | 1280 | 18 | 28 | 0.071 | 1830 | 381 | 1.7 | 300 | 0.305 | |
| OREAS-25a-2 | --- | 64700 | 24 | 2.6 | 0.16 | 1.3 | 0.04 | 0.26 | 0.096 | 0.002 | 1780 | 19 | 33 | 0.077 | 2080 | 402 | 1.9 | 330 | 0.356 | |
| OREAS-25a avg | --- | 59600 | 23 | 2.5 | 0.11 | 1.1 | 0.07 | 0.25 | 0.093 | 0.009 | 1530 | 19 | 31 | 0.074 | 1960 | 392 | 1.8 | 320 | 0.330 | |
| Certified Value | --- | 59900 | --- | --- | --- | --- | --- | --- | --- | --- | 1310 | --- | --- | --- | --- | 420 | --- | --- | --- | --- |

ERM-CC018 is a European sandy soil reference material

ERM-CC018 is a European sandy soil reference material

Spike Recoveries

| Sample ID | Sample Description | Fe % | Ga % | Gd % | Ge % | Hf % | Hg % | Ho % | In % | Ir % | K % | La % | Li % | Lu % | Mg % | Mn % | Mo % | Na % | Nb % |
|-----------|--------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------|---------|---------|---------|---------|---------|---------|---------|---------|
| CE491-22 | Rock composite 2B | --- | 107 | 111 | 104 | 110 | 111 | 111 | 109 | 107 | 129 | 110 | 115 | 111 | --- | 86 | 108 | 104 | 107 |
| CE491-31 | Rock composite 7E | 91 | 108 | 111 | 108 | 111 | 109 | 111 | 109 | 108 | 129 | 111 | 112 | 112 | 92 | 87 | 108 | 103 | 109 |

Analyte of interest added to sample prior to analysis

Analyte of interest added to sample prior to analysis

Rock analyses

Total recoverable metals (TRM)

| Sample ID | Sample Description | Nd | Ni | Os | P | Pb | Pd | Pt | Pr | Rb | Re | Rh | Ru | S | Sb | Sc | Se | Sm | Sn |
|------------------|---------------------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|
| CE491-20 | Rock composite 1B | 22 | 92 | <0.1 | 491 | 11 | 0.18 | 0.003 | 5.6 | 13 | <0.001 | <0.002 | <0.01 | 80 | 0.34 | 5.0 | 0.08 | 4.3 | 0.48 |
| CE491-20 dig dup | Rock composite 1B dig dup | 28 | 93 | <0.1 | 483 | 9.9 | 0.22 | 0.003 | 7.2 | 17 | <0.001 | <0.002 | <0.01 | 77 | 0.43 | 5.5 | 0.08 | 5.4 | 0.62 |
| CE491-20 avg | Rock composite 1B avg | 25 | 93 | <0.1 | 487 | 10 | 0.20 | 0.003 | 6.4 | 15 | <0.001 | <0.002 | <0.01 | 78 | 0.38 | 5.3 | 0.08 | 4.8 | 0.55 |
| CE491-21 | Rock composite 1E | 26 | 134 | <0.1 | 640 | 214 | 0.21 | 0.004 | 6.6 | 17 | <0.001 | 0.004 | <0.01 | 756 | 0.92 | 6.9 | 0.12 | 5.0 | 0.59 |
| CE491-22 | Rock composite 2B | 26 | 28 | <0.1 | 423 | 5.1 | 0.19 | 0.002 | 7.1 | 22 | <0.001 | <0.002 | <0.01 | 159 | 0.45 | 8.6 | 0.04 | 5.0 | 0.84 |
| CE491-22 dli dup | Rock composite 2B dli dup | 27 | 29 | <0.1 | 423 | 5.2 | 0.19 | 0.003 | 7.2 | 24 | <0.001 | <0.002 | <0.01 | 161 | 0.44 | 8.1 | 0.05 | 5.1 | 0.88 |
| CE491-22 avg | Rock composite 2B avg | 27 | 28 | <0.1 | 423 | 5.2 | 0.19 | 0.003 | 7.2 | 23 | <0.001 | <0.002 | <0.01 | 160 | 0.45 | 8.3 | 0.04 | 5.0 | 0.86 |
| CE491-23 | Rock composite 2E | 22 | 31 | 0.2 | 537 | 11 | 0.18 | 0.005 | 5.7 | 24 | <0.001 | 0.002 | <0.01 | 3790 | 2.2 | 3.4 | 0.18 | 4.3 | 0.65 |
| CE491-24 | Rock composite 3B | 2.8 | 42 | <0.1 | 422 | 0.61 | 0.14 | 0.002 | 0.62 | 9.9 | 0.001 | <0.002 | <0.01 | 15 | 0.03 | 6.0 | 0.02 | 0.79 | 0.35 |
| CE491-25 | Rock composite 3E | 6.7 | 39 | <0.1 | 459 | 2.3 | 0.10 | 0.003 | 1.7 | 4.7 | <0.001 | <0.002 | <0.01 | 13 | 0.10 | 2.4 | 0.03 | 1.4 | 0.40 |
| CE491-26 | Rock composite 4B | 23 | 13 | <0.1 | 490 | 17 | 0.17 | 0.003 | 6.0 | 6.3 | <0.001 | <0.002 | <0.01 | 17 | 0.17 | 1.8 | 0.04 | 4.4 | 0.55 |
| CE491-27 | Rock composite 4E | 19 | 16 | <0.1 | 901 | 9.8 | 0.23 | 0.005 | 4.6 | 6.6 | 0.002 | <0.002 | <0.01 | 5410 | 0.63 | 5.8 | 0.30 | 3.8 | 0.41 |
| CE491-28 | Rock composite 5B | 18 | 16 | <0.1 | 516 | 2.7 | 0.14 | 0.003 | 4.9 | 11 | <0.001 | <0.002 | <0.01 | 260 | 0.10 | 1.5 | 0.03 | 3.5 | 0.38 |
| CE491-29 | Rock composite 5E | 19 | 25 | <0.1 | 856 | 8.0 | 0.21 | 0.007 | 4.6 | 11 | 0.005 | <0.002 | <0.01 | 6050 | 0.21 | 6.2 | 1.0 | 3.9 | 1.0 |
| CE491-30 | Rock composite 7B | 23 | 10 | <0.1 | 378 | 8.8 | 0.25 | 0.004 | 6.1 | 20 | <0.001 | <0.002 | <0.01 | 54 | 0.37 | 3.5 | 0.03 | 4.6 | 0.74 |
| CE491-31 | Rock composite 7E | 30 | 11 | <0.1 | 467 | 8.6 | 0.16 | 0.004 | 8.2 | 24 | <0.001 | <0.002 | <0.01 | 1010 | 1.2 | 2.3 | 0.04 | 5.6 | 2.0 |
| CE491-31 dli dup | Rock composite 7E dli dup | 30 | 11 | <0.1 | 472 | 8.6 | 0.17 | 0.004 | 8.2 | 24 | <0.001 | <0.002 | <0.01 | 1010 | 1.2 | 2.6 | 0.03 | 5.6 | 2.0 |
| CE491-31 avg | Rock composite 7E avg | 30 | 11 | <0.1 | 469 | 8.6 | 0.17 | 0.004 | 8.2 | 24 | <0.001 | <0.002 | <0.01 | 1010 | 1.2 | 2.4 | 0.03 | 5.6 | 2.0 |
| SED-43 LOD (3σ) | --- | 0.001 | 0.01 | 0.1 | 4 | 0.01 | 0.002 | 0.001 | 0.003 | 0.01 | 0.001 | 0.002 | 0.01 | 12 | 0.01 | 0.03 | 0.01 | 0.001 | 0.003 |
| Method Code | --- | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-229 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-229 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-209 |

Reference Materials

| Sample ID | Sample Description | Nd | Ni | Os | P | Pb | Pd | Pt | Pr | Rb | Re | Rh | Ru | S | Sb | Sc | Se | Sm | Sn |
|-----------------|--------------------|-----|------------|------|-----|----------|-------|-------|-----|-----|--------|-------|-------|------|------|------|------|-----|-----|
| ERM-CC018-1 | --- | 7.2 | 25 | <0.1 | 830 | 331 | 0.13 | 0.018 | 1.9 | 6.6 | 0.002 | 0.025 | <0.01 | 1010 | 3.0 | 1.8 | 0.56 | 1.4 | 13 |
| ERM-CC018-2 | --- | 6.1 | 24 | <0.1 | 814 | 329 | 0.17 | 0.010 | 1.6 | 5.5 | 0.002 | 0.024 | <0.01 | 987 | 3.0 | 1.3 | 0.54 | 1.2 | 14 |
| ERM-CC018 avg | --- | 6.6 | 25 | <0.1 | 822 | 330 | 0.15 | 0.014 | 1.8 | 6.0 | 0.002 | 0.025 | <0.01 | 1000 | 3.0 | 1.5 | 0.55 | 1.3 | 13 |
| Certified Value | --- | --- | 25.8 ± 1.8 | --- | --- | 289 ± 10 | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| OREAS-25a-1 | --- | 16 | 32 | <0.1 | 354 | 23 | 0.089 | 0.006 | 4.2 | 37 | <0.001 | 0.055 | --- | 431 | 0.22 | 12 | 1.5 | 3.0 | 2.9 |
| OREAS-25a-2 | --- | 17 | 39 | <0.1 | 369 | 24 | 0.093 | 0.006 | 4.5 | 42 | <0.001 | 0.005 | <0.01 | 468 | 0.40 | 12 | 1.8 | 3.2 | 3.2 |
| OREAS-25a avg | --- | 16 | 35 | <0.1 | 361 | 24 | 0.091 | 0.006 | 4.4 | 40 | <0.001 | 0.030 | <0.01 | 450 | 0.31 | 12 | 1.6 | 3.1 | 3.1 |
| Certified Value | --- | --- | 26.9 | --- | 370 | 21 | --- | --- | --- | --- | --- | --- | --- | --- | --- | 8.64 | --- | --- | 2.7 |

ERM-CC018 is a European sandy soil reference material

ERM-CC018 is a European sandy soil reference material

Spike Recoveries

| Sample ID | Sample Description | Nd | Ni | Os | P | Pb | Pd | Pt | Pr | Rb | Re | Rh | Ru | S | Sb | Sc | Se | Sm | Sn |
|-----------|--------------------|-----|-----|-----|----|-----|-----|-----|-----|-----|-----|-----|-----|----|-----|-----|-----|-----|-----|
| CE491-22 | Rock composite 2B | 111 | 110 | 141 | 88 | 107 | 106 | 106 | 113 | 118 | 109 | 106 | 106 | 95 | 108 | 109 | 105 | 110 | 107 |
| CE491-31 | Rock composite 7E | 110 | 111 | 144 | 92 | 108 | 107 | 107 | 116 | 113 | 110 | 108 | 109 | 96 | 109 | 113 | 107 | 112 | 109 |

Analyte of interest added to sample prior to analysis

Analyte of interest added to sample prior to analysis

Rock analyses

Total recoverable metals (TRM)

| Sample ID | Sample Description | Sr | Ta | Tb | Te | Th | Ti | Ti | Ti | Tm | U | V | W | Y | Yb | Zn | Zr |
|------------------|---------------------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|
| TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) |
| CE491-20 | Rock composite 1B | 28 | 0.005 | 0.50 | 0.027 | 9.2 | 219 | 0.09 | 0.15 | 0.13 | 0.71 | 31 | 0.13 | 11 | 0.87 | 75 | 10 |
| CE491-20 dig dup | Rock composite 1B dig dup | 29 | 0.004 | 0.60 | 0.018 | 11 | 440 | 0.11 | 0.18 | 0.13 | 1.0 | 35 | 0.13 | 13 | 1.1 | 76 | 16 |
| CE491-20 avg | Rock composite 1B avg | 28 | 0.005 | 0.55 | 0.022 | 10 | 329 | 0.10 | 0.16 | 0.13 | 0.86 | 33 | 0.13 | 12 | 0.98 | 76 | 13 |
| CE491-21 | Rock composite 1E | 33 | 0.004 | 0.58 | 0.028 | 7.9 | 42 | 0.14 | 0.16 | 0.12 | 0.75 | 61 | 0.12 | 12 | 0.99 | 543 | 10 |
| CE491-22 | Rock composite 2B | 18 | 0.004 | 0.54 | 0.023 | 10 | 21 | 0.11 | 0.15 | 0.084 | 1.2 | 38 | 0.084 | 12 | 0.99 | 57 | 14 |
| CE491-22 dll dup | Rock composite 2B dll dup | 18 | 0.003 | 0.54 | 0.014 | 10 | 21 | 0.11 | 0.16 | 0.086 | 1.2 | 38 | 0.086 | 12 | 0.99 | 60 | 14 |
| CE491-22 avg | Rock composite 2B avg | 18 | 0.004 | 0.54 | 0.018 | 10 | 21 | 0.11 | 0.16 | 0.085 | 1.2 | 38 | 0.085 | 12 | 0.99 | 58 | 14 |
| CE491-23 | Rock composite 2E | 48 | 0.017 | 0.50 | 0.027 | 9.1 | 20 | 0.17 | 0.13 | 0.18 | 1.1 | 20 | 0.18 | 10 | 0.78 | 45 | 13 |
| CE491-24 | Rock composite 3B | 30 | 0.016 | 0.21 | 0.004 | 0.67 | 2210 | 0.064 | 0.16 | 0.077 | 0.10 | 62 | 0.077 | 8.3 | 0.96 | 66 | 8.9 |
| CE491-25 | Rock composite 3E | 13 | 0.012 | 0.20 | 0.029 | 5.3 | 1230 | 0.026 | 0.097 | 0.12 | 0.33 | 30 | 0.12 | 5.7 | 0.59 | 62 | 7.4 |
| CE491-26 | Rock composite 4B | 26 | 0.011 | 0.51 | 0.025 | 11 | 312 | 0.043 | 0.15 | 0.13 | 0.79 | 13 | 0.13 | 10 | 0.95 | 52 | 12 |
| CE491-27 | Rock composite 4E | 50 | 0.014 | 0.47 | 0.011 | 4.7 | 1240 | 0.350 | 0.20 | 0.094 | 1.3 | 62 | 0.094 | 13 | 1.3 | 104 | 24 |
| CE491-28 | Rock composite 5B | 21 | 0.008 | 0.39 | 0.010 | 7.5 | 96 | 0.057 | 0.12 | 0.20 | 0.99 | 19 | 0.20 | 8.5 | 0.76 | 22 | 13 |
| CE491-29 | Rock composite 5E | 51 | 0.010 | 0.47 | 0.097 | 5.3 | 1100 | 0.071 | 0.18 | 0.32 | 0.84 | 67 | 0.32 | 12 | 1.1 | 76 | 16 |
| CE491-30 | Rock composite 7B | 73 | 0.009 | 0.57 | 0.013 | 11 | 37 | 0.11 | 0.20 | 1.4 | 1.4 | 17 | 0.12 | 14 | 1.2 | 35 | 25 |
| CE491-31 | Rock composite 7E | 63 | 0.007 | 0.49 | 0.016 | 8.8 | 7.8 | 0.14 | 0.10 | 0.052 | 1.2 | 12 | 0.052 | 9.0 | 0.61 | 31 | 20 |
| CE491-31 dll dup | Rock composite 7E dll dup | 63 | 0.006 | 0.49 | 0.017 | 8.8 | 8.2 | 0.14 | 0.10 | 0.053 | 1.2 | 12 | 0.053 | 8.9 | 0.61 | 32 | 20 |
| CE491-31 avg | Rock composite 7E avg | 63 | 0.007 | 0.49 | 0.016 | 8.8 | 8.0 | 0.14 | 0.10 | 0.053 | 1.2 | 12 | 0.053 | 8.9 | 0.61 | 32 | 20 |
| SED-43 LOD (3σ) | --- | 0.002 | 0.001 | 0.001 | 0.001 | 0.01 | 0.1 | 0.004 | 0.001 | 0.002 | 0.002 | 0.1 | 0.001 | 0.001 | 0.001 | 1 | 0.01 |
| Method Code | --- | C-223/C-229 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-229 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-229 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-209 | C-223/C-209 |

Reference Materials

| Sample ID | Sample Description | Sr | Ta | Tb | Te | Th | Ti | Ti | Ti | Tm | U | V | W | Y | Yb | Zn | Zr |
|-----------------|--------------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| ERM-CC018-1 | ERM-CC018-1 | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) | TRM (µg/g) |
| ERM-CC018-1 | --- | 73 | 0.015 | 0.18 | 0.028 | 2.5 | 166 | 0.19 | 0.068 | 1.2 | 1.2 | 16 | 2.1 | 6.6 | 0.43 | 307 | 18 |
| ERM-CC018-2 | --- | 71 | 0.016 | 0.16 | 0.031 | 1.9 | 111 | 0.16 | 0.061 | 1.1 | 1.1 | 14 | 2.1 | 5.9 | 0.37 | 299 | 13 |
| ERM-CC018 avg | --- | 72 | 0.015 | 0.17 | 0.029 | 2.2 | 139 | 0.18 | 0.064 | 1.1 | 1.1 | 15 | 2.1 | 6.3 | 0.40 | 303 | 15 |
| Certified Value | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | 19.4 ± 1.0 | --- | --- | --- | 313 ± 13 | --- |
| OREAS-25a-1 | --- | 15 | 0.005 | 0.30 | 0.024 | 13 | 357 | 0.27 | 0.081 | 1.8 | 1.8 | 110 | 0.027 | 5.7 | 0.51 | 36 | 36 |
| OREAS-25a-2 | --- | 17 | 0.004 | 0.33 | 0.041 | 13 | 690 | 0.29 | 0.089 | 1.8 | 1.8 | 117 | 0.038 | 5.9 | 0.54 | 39 | 39 |
| OREAS-25a avg | --- | 16 | 0.005 | 0.31 | 0.033 | 13 | 524 | 0.28 | 0.085 | 1.8 | 1.8 | 113 | 0.032 | 5.8 | 0.53 | 38 | 37 |
| Certified Value | --- | 17.3 | --- | --- | --- | 10.7 | --- | 0.20 | --- | 1.49 | 1.49 | 117 | --- | 4.56 | --- | 30.1 | --- |

ERM-CC018 is a European sandy soil reference material

ERM-CC018 is a European sandy soil reference material

Spike Recoveries

| Sample ID | Sample Description | Sr | Ta | Tb | Te | Th | Ti | Ti | Ti | Tm | U | V | W | Y | Yb | Zn | Zr |
|-----------|--------------------|----|-----|-----|-----|-----|----|-----|-----|-----|-----|----|-----|-----|-----|-----|-----|
| % | % | % | % | % | % | % | % | % | % | % | % | % | % | % | % | % | % |
| CE491-22 | Rock composite 2B | 93 | 112 | 111 | 106 | 112 | 96 | 108 | 111 | 109 | 109 | 91 | 108 | 111 | 110 | 112 | 110 |
| CE491-31 | Rock composite 7E | 95 | 115 | 111 | 107 | 111 | 96 | 109 | 111 | 110 | 110 | 93 | 109 | 114 | 111 | 109 | 112 |

Analyte of interest added to sample prior to analysis

Analyte of interest added to sample prior to analysis

Rock analyses

Dilute-acid extractable metals (AEM)

| Sample ID | Sample Description | Ca (µg/g) | K (µg/g) | Mg (µg/g) | Na (µg/g) | Al (µg/g) | Ag (µg/g) | As (µg/g) | Au (µg/g) | B (µg/g) | Ba (µg/g) | Be (µg/g) | Bi (µg/g) | Cd (µg/g) | Ce (µg/g) | Co (µg/g) | Cr (µg/g) | Cu (µg/g) | Cs (µg/g) | Dy (µg/g) | Er (µg/g) | Eu (µg/g) | Fe (µg/g) | |
|------------------|---------------------------|--------------|-------------|--------------|--------------|--------------|--------------|--------------|--------------|-------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|-------------|
| CE491-20 | Rock composite 1B | 7490 | 1100 | 3060 | 143 | 2410 | 0.016 | 1.9 | <0.01 | 2.5 | 32 | 0.36 | 0.17 | 0.018 | 16 | 2.5 | 6.3 | 3.3 | 1.2 | 1.2 | 1.5 | 0.68 | 0.42 | 4610 |
| CE491-20 Dig Dup | Rock composite 1B dig dup | 7510 | 1130 | 3050 | 140 | 2420 | 0.015 | 2.0 | <0.01 | 1.8 | 31 | 0.37 | 0.18 | 0.018 | 17 | 2.6 | 6.2 | 3.6 | 1.2 | 1.2 | 1.5 | 0.68 | 0.44 | 4580 |
| CE491-20 avg | Rock composite 1B avg | 7500 | 1120 | 3060 | 141 | 2420 | 0.015 | 2.0 | <0.01 | 2.2 | 31 | 0.37 | 0.18 | 0.018 | 17 | 2.6 | 6.3 | 3.4 | 1.2 | 1.2 | 1.5 | 0.68 | 0.43 | 4600 |
| CE491-21 | Rock composite 1E | 8430 | 1050 | 3510 | 136 | 3270 | 0.085 | 2.3 | <0.01 | 2.2 | 57 | 0.49 | 0.26 | 0.18 | 13 | 2.0 | 12 | 2.3 | 0.75 | 2.0 | 0.90 | 0.53 | 6460 | |
| CE491-22 | Rock composite 2B | 6610 | 1090 | 2080 | 83 | 2950 | 0.034 | 0.62 | <0.01 | 0.8 | 84 | 0.44 | 0.10 | 0.014 | 12 | 4.4 | 12 | 1.3 | 0.86 | 1.3 | 0.60 | 0.34 | 5600 | |
| CE491-22 dil dup | Rock composite 2B dil dup | 6620 | 1100 | 2080 | 83 | 2960 | 0.032 | 0.64 | <0.01 | 0.4 | 84 | 0.44 | 0.10 | 0.016 | 12 | 4.1 | 12 | 1.2 | 0.86 | 1.3 | 0.59 | 0.35 | 5540 | |
| CE491-22 avg | Rock composite 2B avg | 6620 | 1100 | 2080 | 83 | 2960 | 0.033 | 0.63 | <0.01 | 0.6 | 84 | 0.44 | 0.10 | 0.015 | 12 | 4.3 | 12 | 1.3 | 0.86 | 1.3 | 0.60 | 0.35 | 5570 | |
| CE491-23 | Rock composite 2E | 11700 | 1440 | 1400 | 82 | 2100 | 0.084 | 1.3 | <0.01 | 1.1 | 43 | 0.60 | 0.32 | 0.020 | 11 | 1.2 | 4.6 | 3.1 | 0.71 | 1.5 | 0.62 | 0.44 | 6310 | |
| CE491-24 | Rock composite 3B | 15100 | 1420 | 3120 | 189 | 2920 | 0.004 | 0.57 | <0.01 | <0.2 | 7.4 | 0.078 | <0.001 | 0.013 | 0.66 | 3.4 | 13 | 18 | 0.47 | 0.14 | 0.10 | 0.026 | 3830 | |
| CE491-25 | Rock composite 3E | 8840 | 643 | 1720 | 220 | 2540 | 0.017 | 1.5 | 0.04 | 5.7 | 12 | 0.13 | 0.027 | 0.012 | 3.4 | 2.1 | 8.8 | 21 | 0.19 | 0.33 | 0.17 | 0.038 | 2780 | |
| CE491-26 | Rock composite 4B | 12400 | 552 | 674 | 110 | 1160 | 0.015 | 1.6 | 0.02 | 1.7 | 21 | 0.15 | 0.096 | 0.029 | 25 | 0.40 | 1.9 | 2.9 | 0.35 | 1.2 | 0.48 | 0.29 | 1850 | |
| CE491-27 | Rock composite 4E | 20100 | 765 | 1260 | 146 | 2750 | 0.074 | 1.9 | 0.01 | 1.4 | 27 | 0.11 | 0.091 | 0.079 | 14 | 1.2 | 2.8 | 4.9 | 0.11 | 0.85 | 0.45 | 0.21 | 5470 | |
| CE491-28 | Rock composite 5B | 6570 | 755 | 1330 | 246 | 2800 | 0.049 | 0.76 | <0.01 | 0.5 | 30 | 0.36 | 0.17 | 0.026 | 8.8 | 1.1 | 3.8 | 22 | 0.23 | 1.00 | 0.46 | 0.26 | 5820 | |
| CE491-29 | Rock composite 5E | 5340 | 930 | 1400 | 206 | 1810 | 0.015 | 0.68 | <0.01 | 0.8 | 36 | 0.23 | 0.062 | 0.007 | 11 | 0.82 | 4.3 | 1.4 | 0.12 | 1.0 | 0.45 | 0.28 | 4250 | |
| CE491-30 | Rock composite 7B | 14000 | 1080 | 705 | 192 | 1630 | 0.010 | 0.74 | <0.01 | 0.3 | 45 | 0.35 | 0.037 | 0.019 | 20 | 0.48 | 4.3 | 0.80 | 0.64 | 1.4 | 0.62 | 0.33 | 4150 | |
| CE491-31 | Rock composite 7E | 8760 | 1930 | 685 | 122 | 2090 | 0.040 | 1.4 | <0.01 | 1.2 | 1836 | 0.83 | 1.3 | 0.011 | 17 | 0.61 | 2.6 | 4.0 | 1.8 | 1.3 | 0.48 | 0.55 | 3190 | |
| CE491-31 dil dup | Rock composite 7E dil dup | 8780 | 1920 | 688 | 117 | 2130 | 0.043 | 1.4 | <0.01 | 1.1 | 1836 | 0.81 | 1.3 | 0.010 | 17 | 0.60 | 2.7 | 4.2 | 1.8 | 1.3 | 0.50 | 0.56 | 3080 | |
| CE491-31 avg | Rock composite 7E avg | 8770 | 1920 | 686 | 119 | 2110 | 0.042 | 1.4 | <0.01 | 1.2 | 1836 | 0.82 | 1.3 | 0.011 | 17 | 0.61 | 2.7 | 4.1 | 1.8 | 1.3 | 0.49 | 0.56 | 3140 | |
| LOD (3σ) | --- | 5 | 2 | 4 | 10 | 30 | 0.001 | 0.03 | 0.01 | 0.2 | 0.1 | 0.002 | 0.001 | 0.001 | 0.001 | 0.01 | 0.1 | 0.3 | 0.003 | 0.001 | 0.001 | 0.001 | 1 | |
| Method Code | --- | C-241/C-229 | | | | C-241/C-229 | | | | C-241/C-209 | | | | C-241/C-209 | | | | C-241/C-209 | | | | C-241/C-229 | | C-241/C-229 |

C-209: ICP-MS C-229: ICP-AES C-241 Dilute Acid Extractable Metals (AEM) 1 M HCl

Certified Reference Materials

| Sample ID | Sample Description | Ca (µg/g) | K (µg/g) | Mg (µg/g) | Na (µg/g) | Al (µg/g) | Ag (µg/g) | As (µg/g) | Au (µg/g) | B (µg/g) | Ba (µg/g) | Be (µg/g) | Bi (µg/g) | Cd (µg/g) | Ce (µg/g) | Co (µg/g) | Cr (µg/g) | Cu (µg/g) | Cs (µg/g) | Dy (µg/g) | Er (µg/g) | Eu (µg/g) | Fe (µg/g) |
|----------------|--------------------|--------------|-------------|--------------|--------------|--------------|--------------|--------------|--------------|-------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| ERM-CC018-1 | --- | 15500 | 348 | 591 | 85 | 2190 | 1.3 | 14 | 0.02 | 7.9 | 226 | 0.30 | 0.98 | 5.0 | 7.2 | 2.2 | 38 | 58 | 0.14 | 0.47 | 0.25 | 0.14 | 2810 |
| ERM-CC018-2 | --- | 16600 | 369 | 617 | 89 | 2300 | 1.5 | 17 | 0.01 | 5.7 | 247 | 0.30 | 0.97 | 5.9 | 8.1 | 2.5 | 41 | 61 | 0.15 | 0.53 | 0.27 | 0.16 | 2990 |
| Avg ERM-CC018 | --- | 16000 | 358 | 604 | 87 | 2240 | 1.4 | 16 | 0.01 | 6.8 | 236 | 0.30 | 0.97 | 5.4 | 7.7 | 2.4 | 40 | 60 | 0.15 | 0.50 | 0.26 | 0.15 | 2900 |
| In-house Value | --- | --- | --- | --- | --- | 2473 | --- | 17 | --- | --- | 278 | --- | --- | 5.5 | --- | 2.8 | 44 | 62 | --- | --- | --- | --- | 3278 |

Spike Recoveries

| Sample ID | Sample Description | Ca % | K % | Mg % | Na % | Al % | Ag % | As % | Au % | B % | Ba % | Be % | Bi % | Cd % | Ce % | Co % | Cr % | Cu % | Cs % | Dy % | Er % | Eu % | Fe % |
|-----------|--------------------|---------|--------|---------|---------|---------|---------|---------|---------|--------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| CE491-22 | Rock composite 2B | 89 | 96 | 95 | 101 | 90 | 38 | 112 | 111 | 119 | 95 | 110 | 113 | 110 | 115 | 107 | 108 | 107 | 112 | 112 | 111 | 113 | 86 |
| CE491-31 | Rock composite 7E | 85 | 96 | 97 | 101 | 94 | 35 | 105 | 102 | 102 | 91 | 105 | 103 | 102 | 102 | 102 | 101 | 105 | 103 | 105 | 105 | 105 | 80 |

Analyte of interest added to sample prior to analysis

Rock analyses

Dilute-acid extractable metals (AEM)

| Sample ID | Sample Description | Ga | Gd | Ge | Hf | Hg | Ho | In | Ir | La | Li | Lu | Mn | Mo | Nb | Nd | Ni | Os | P | Pb | Pd | Pt | Pr |
|------------------|---------------------------|-------------|-------|------|-------|-------------|-------|-------|--------|-------------|-------|-------|-----|-------------|-------|-------|-----|-------------|-----|-------|-------|-------------|-------|
| CE491-20 | Rock composite 1B | 0.72 | 2.1 | 0.11 | 0.092 | <0.02 | 0.26 | 0.010 | <0.001 | 7.0 | 3.4 | 0.073 | 343 | 0.08 | <0.02 | 8.9 | 8.7 | <0.04 | 523 | 7.2 | 0.054 | <0.001 | 2.1 |
| CE491-20 Dig Dup | Rock composite 1B dig dup | 0.72 | 2.2 | 0.13 | 0.11 | <0.02 | 0.27 | 0.010 | <0.001 | 7.4 | 3.4 | 0.077 | 345 | 0.06 | <0.02 | 9.3 | 8.3 | <0.04 | 512 | 7.3 | 0.054 | <0.001 | 2.2 |
| CE491-20 avg | Rock composite 1B avg | 0.72 | 2.1 | 0.12 | 0.099 | <0.02 | 0.27 | 0.010 | <0.001 | 7.2 | 3.4 | 0.075 | 344 | 0.07 | <0.02 | 9.1 | 8.5 | <0.04 | 518 | 7.2 | 0.054 | <0.001 | 2.1 |
| CE491-21 | Rock composite 1E | 1.1 | 2.4 | 0.13 | 0.14 | <0.02 | 0.35 | 0.033 | <0.001 | 5.5 | 5.9 | 0.088 | 679 | 0.07 | <0.02 | 7.7 | 13 | <0.04 | 664 | 197 | 0.074 | <0.001 | 1.7 |
| CE491-22 | Rock composite 2B | 0.86 | 1.8 | 0.12 | 0.080 | <0.02 | 0.23 | 0.010 | <0.001 | 5.1 | 4.5 | 0.067 | 515 | 0.09 | <0.02 | 6.4 | 5.4 | <0.04 | 360 | 3.7 | 0.044 | <0.001 | 1.5 |
| CE491-22 dil dup | Rock composite 2B dil dup | 0.88 | 1.8 | 0.12 | 0.087 | <0.02 | 0.23 | 0.011 | <0.001 | 5.1 | 4.5 | 0.066 | 513 | 0.06 | <0.02 | 6.3 | 5.4 | <0.04 | 358 | 3.7 | 0.048 | <0.001 | 1.5 |
| CE491-22 avg | Rock composite 2B avg | 0.87 | 1.8 | 0.12 | 0.083 | <0.02 | 0.23 | 0.010 | <0.001 | 5.1 | 4.5 | 0.066 | 514 | 0.08 | <0.02 | 6.4 | 5.4 | <0.04 | 359 | 3.7 | 0.046 | <0.001 | 1.5 |
| CE491-23 | Rock composite 2E | 0.62 | 2.1 | 0.16 | 0.15 | <0.02 | 0.26 | 0.015 | <0.001 | 4.7 | 2.4 | 0.063 | 298 | 0.08 | <0.02 | 6.5 | 3.1 | <0.04 | 545 | 7.1 | 0.064 | <0.001 | 1.4 |
| CE491-24 | Rock composite 3B | 0.71 | 0.14 | 0.06 | 0.024 | <0.02 | 0.032 | 0.001 | <0.001 | 0.27 | 1.4 | 0.018 | 203 | <0.02 | <0.02 | 0.42 | 5.3 | <0.04 | 483 | 0.14 | 0.007 | <0.001 | 0.093 |
| CE491-25 | Rock composite 3E | 0.64 | 0.42 | 0.06 | 0.060 | <0.02 | 0.063 | 0.002 | 0.001 | 1.4 | 2.9 | 0.019 | 119 | 0.04 | 0.03 | 1.9 | 4.3 | <0.04 | 501 | 1.1 | 0.014 | <0.001 | 0.45 |
| CE491-26 | Rock composite 4B | 0.33 | 2.0 | 0.16 | 0.087 | <0.02 | 0.19 | 0.003 | <0.001 | 14 | 0.78 | 0.056 | 263 | 0.05 | 0.02 | 13 | 0.6 | <0.04 | 519 | 11 | 0.037 | <0.001 | 3.3 |
| CE491-27 | Rock composite 4E | 0.79 | 1.3 | 0.08 | 0.094 | <0.02 | 0.16 | 0.008 | <0.001 | 6.4 | 0.93 | 0.066 | 319 | 0.08 | <0.02 | 7.5 | 1.1 | <0.04 | 952 | 6.9 | 0.045 | <0.001 | 1.8 |
| CE491-28 | Rock composite 5B | 0.91 | 1.4 | 0.10 | 0.087 | <0.02 | 0.18 | 0.004 | <0.001 | 3.7 | 1.1 | 0.043 | 131 | 0.08 | <0.02 | 5.9 | 1.5 | <0.04 | 919 | 4.8 | 0.038 | <0.001 | 1.2 |
| CE491-29 | Rock composite 5E | 0.54 | 1.5 | 0.12 | 0.14 | <0.02 | 0.18 | 0.006 | <0.001 | 5.0 | 0.67 | 0.047 | 172 | 0.30 | <0.02 | 5.7 | 1.8 | <0.04 | 546 | 1.9 | 0.035 | <0.001 | 1.3 |
| CE491-30 | Rock composite 7B | 0.47 | 2.2 | 0.10 | 0.11 | <0.02 | 0.25 | 0.006 | <0.001 | 9.3 | 1.7 | 0.064 | 452 | 0.05 | <0.02 | 10 | 0.8 | <0.04 | 400 | 6.3 | 0.063 | <0.001 | 2.5 |
| CE491-31 | Rock composite 7E | 0.53 | 2.2 | 0.08 | 0.18 | <0.02 | 0.21 | 0.026 | <0.001 | 7.4 | 2.4 | 0.046 | 198 | 0.07 | <0.02 | 9.2 | 0.9 | <0.04 | 477 | 4.5 | 0.053 | <0.001 | 2.2 |
| CE491-31 dil dup | Rock composite 7E dil dup | 0.53 | 2.2 | 0.08 | 0.18 | <0.02 | 0.21 | 0.025 | <0.001 | 7.3 | 2.3 | 0.044 | 198 | 0.07 | <0.02 | 9.2 | 0.9 | <0.04 | 480 | 4.4 | 0.051 | <0.001 | 2.2 |
| CE491-31 avg | Rock composite 7E avg | 0.53 | 2.2 | 0.08 | 0.18 | <0.02 | 0.21 | 0.025 | <0.001 | 7.3 | 2.3 | 0.045 | 198 | 0.07 | <0.02 | 9.2 | 0.9 | <0.04 | 479 | 4.4 | 0.052 | <0.001 | 2.2 |
| LOD (3σ) | --- | 0.01 | 0.001 | 0.01 | 0.002 | 0.02 | 0.001 | 0.001 | 0.001 | 0.001 | 0.003 | 0.001 | 0.1 | 0.02 | 0.02 | 0.001 | 0.1 | 0.04 | 4 | 0.002 | 0.004 | 0.001 | 0.001 |
| | | C-241/C-209 | | | | C-241/C-209 | | | | C-241/C-209 | | | | C-241/C-209 | | | | C-241/C-209 | | | | C-241/C-209 | |

Certified Reference Materials

| Sample ID | Sample Description | Ga | Gd | Ge | Hf | Hg | Ho | In | Ir | La | Li | Lu | Mn | Mo | Nb | Nd | Ni | Os | P | Pb | Pd | Pt | Pr |
|----------------|--------------------|------|------|------|------|------|-------|-------|-------|-----|-----|-------|-----|-----|------|-----|----|-------|-----|-----|-------|--------|------|
| ERM-CC018-1 | --- | 0.77 | 0.59 | 0.59 | 0.15 | 0.07 | 0.091 | 0.041 | 0.002 | 3.2 | 1.6 | 0.031 | 120 | 7.1 | 0.12 | 2.9 | 13 | <0.04 | 674 | 264 | 0.036 | <0.001 | 0.75 |
| ERM-CC018-2 | --- | 0.82 | 0.65 | 0.67 | 0.16 | 0.08 | 0.10 | 0.044 | 0.002 | 3.6 | 1.7 | 0.035 | 128 | 8.0 | 0.12 | 3.3 | 14 | <0.04 | 728 | 293 | 0.046 | <0.001 | 0.86 |
| Avg ERM-CC018 | --- | 0.79 | 0.62 | 0.63 | 0.15 | 0.08 | 0.096 | 0.043 | 0.002 | 3.4 | 1.7 | 0.033 | 124 | 7.5 | 0.12 | 3.1 | 14 | <0.04 | 701 | 278 | 0.041 | <0.001 | 0.80 |
| In-house Value | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | 137 | 7.8 | --- | --- | 14 | --- | --- | 267 | --- | --- | --- |

Spike Recoveries

| Sample ID | Sample Description | Ga | Gd | Ge | Hf | Hg | Ho | In | Ir | La | Li | Lu | Mn | Mo | Nb | Nd | Ni | Os | P | Pb | Pd | Pt | Pr |
|-----------|--------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----|-----|-----|-----|-----|-----|----|-----|-----|-----|-----|
| CE491-22 | Rock composite 2B | 105 | 113 | 105 | 112 | 108 | 112 | 110 | 111 | 113 | 109 | 112 | 92 | 108 | 124 | 114 | 111 | 146 | 97 | 111 | 109 | 109 | 113 |
| CE491-31 | Rock composite 7E | 100 | 105 | 100 | 105 | 102 | 105 | 104 | 102 | 103 | 102 | 105 | 96 | 107 | 113 | 104 | 107 | 138 | 98 | 103 | 99 | 100 | 103 |

Analyte of interest added to sample prior to analysis

Rock analyses

Dilute-acid extractable metals (AEM)

| Sample ID | | Rb | Re | Rh | Ru | S | Sb | Sc | Se | Sm | Sn | Sr | Ta | Tb | Te | Th | Ti | Ti | Tm | U | V | W | Y | Yb | Zn | Zr |
|--------------------|---------------------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|
| Sample Description | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) |
| CE491-20 | Rock composite 1B | 5.0 | <0.002 | <0.01 | <0.001 | <30 | 0.10 | 2.1 | <0.01 | 2.1 | 0.17 | 28 | <0.3 | 0.29 | <0.02 | 4.2 | 15 | 0.034 | 0.083 | 0.26 | 5.3 | 0.066 | 6.6 | 0.53 | 14 | 2.2 |
| CE491-20 Dig Dup | Rock composite 1B dig dup | 5.6 | <0.002 | <0.01 | <0.001 | <30 | 0.13 | 2.1 | 0.01 | 2.2 | 0.17 | 27 | <0.3 | 0.30 | <0.02 | 4.4 | 16 | 0.032 | 0.085 | 0.27 | 5.2 | 0.072 | 6.4 | 0.52 | 14 | 2.6 |
| CE491-20 avg | Rock composite 1B avg | 5.3 | <0.002 | <0.01 | <0.001 | <30 | 0.12 | 2.1 | 0.01 | 2.2 | 0.17 | 28 | <0.3 | 0.29 | <0.02 | 4.3 | 15 | 0.033 | 0.084 | 0.27 | 5.2 | 0.069 | 6.5 | 0.52 | 14 | 2.4 |
| CE491-21 | Rock composite 1E | 4.9 | <0.002 | <0.01 | <0.001 | 38 | 0.21 | 3.3 | 0.01 | 2.1 | 0.22 | 33 | <0.3 | 0.36 | <0.02 | 3.1 | 13 | 0.043 | 0.11 | 0.24 | 9.1 | 0.085 | 8.6 | 0.65 | 86 | 2.7 |
| CE491-22 | Rock composite 2B | 5.2 | <0.002 | <0.01 | <0.001 | <30 | 0.098 | 2.6 | <0.01 | 1.6 | 0.20 | 17 | <0.3 | 0.26 | <0.02 | 2.7 | 6.5 | 0.022 | 0.075 | 0.28 | 8.3 | 0.021 | 6.1 | 0.47 | 15 | 1.6 |
| CE491-22 dil dup | Rock composite 2B dil dup | 4.6 | <0.002 | <0.01 | <0.001 | <30 | 0.088 | 2.5 | <0.01 | 1.7 | 0.20 | 17 | <0.3 | 0.25 | <0.02 | 2.6 | 6.6 | 0.020 | 0.077 | 0.27 | 8.1 | 0.026 | 5.9 | 0.45 | 14 | 1.6 |
| CE491-22 avg | Rock composite 2B avg | 4.9 | <0.002 | <0.01 | <0.001 | <30 | 0.093 | 2.5 | <0.01 | 1.6 | 0.20 | 17 | <0.3 | 0.25 | <0.02 | 2.7 | 6.5 | 0.021 | 0.076 | 0.27 | 8.2 | 0.024 | 6.0 | 0.46 | 15 | 1.6 |
| CE491-23 | Rock composite 2E | 6.2 | <0.002 | <0.01 | <0.001 | <30 | 0.67 | 1.5 | 0.01 | 1.9 | 0.23 | 44 | <0.3 | 0.30 | <0.02 | 3.3 | 9.8 | 0.041 | 0.074 | 0.38 | 4.5 | 0.082 | 6.7 | 0.43 | 8.0 | 3.4 |
| CE491-24 | Rock composite 3B | 7.3 | <0.002 | <0.01 | <0.001 | <30 | 0.005 | 0.32 | <0.01 | 0.11 | 0.03 | 5.8 | <0.3 | 0.023 | <0.02 | 0.17 | 80 | 0.019 | 0.015 | 0.01 | 8.3 | 0.035 | 0.83 | 0.11 | 8.9 | 0.58 |
| CE491-25 | Rock composite 3E | 2.1 | <0.002 | <0.01 | <0.001 | <30 | 0.024 | 0.36 | <0.01 | 0.41 | 0.06 | 7.0 | <0.3 | 0.057 | <0.02 | 1.4 | 27 | 0.031 | 0.022 | 0.07 | 3.4 | 0.049 | 1.7 | 0.13 | 7.1 | 1.3 |
| CE491-26 | Rock composite 4B | 2.5 | <0.002 | <0.01 | <0.001 | <30 | 0.030 | 0.37 | <0.01 | 2.4 | 0.09 | 20 | <0.3 | 0.24 | <0.02 | 4.7 | 8.3 | 0.029 | 0.059 | 0.19 | 1.1 | 0.070 | 4.7 | 0.37 | 3.8 | 1.7 |
| CE491-27 | Rock composite 4E | 1.5 | <0.002 | <0.01 | <0.001 | <30 | 0.086 | 0.95 | <0.01 | 1.3 | 0.06 | 44 | <0.3 | 0.16 | <0.02 | 1.5 | 19 | 0.050 | 0.058 | 0.28 | 9.7 | 0.062 | 4.1 | 0.37 | 14 | 2.0 |
| CE491-28 | Rock composite 5B | 2.9 | <0.002 | <0.01 | <0.001 | 45 | 0.075 | 0.55 | 0.01 | 1.4 | 0.09 | 13 | <0.3 | 0.19 | <0.02 | 3.0 | 31 | 0.039 | 0.056 | 0.19 | 9.4 | 0.140 | 4.7 | 0.32 | 16 | 2.1 |
| CE491-29 | Rock composite 5E | 3.1 | <0.002 | <0.01 | <0.001 | <30 | 0.052 | 0.42 | <0.01 | 1.4 | 0.14 | 13 | <0.3 | 0.20 | 0.02 | 4.5 | 11 | 0.024 | 0.057 | 0.29 | 2.9 | 0.070 | 4.4 | 0.32 | 3.8 | 2.5 |
| CE491-30 | Rock composite 7B | 4.4 | <0.002 | <0.01 | <0.001 | <30 | 0.082 | 0.82 | <0.01 | 2.2 | 0.16 | 71 | <0.3 | 0.29 | <0.02 | 3.9 | 7.7 | 0.038 | 0.071 | 0.26 | 3.0 | 0.057 | 6.4 | 0.43 | 3.7 | 2.3 |
| CE491-31 | Rock composite 7E | 7.9 | <0.002 | <0.01 | <0.001 | 418 | 0.21 | 0.90 | 0.01 | 2.2 | 0.64 | 62 | <0.3 | 0.27 | <0.02 | 2.2 | 6.9 | 0.040 | 0.056 | 0.40 | 2.6 | 0.028 | 5.6 | 0.31 | 5.7 | 4.0 |
| CE491-31 dil dup | Rock composite 7E dil dup | 7.8 | <0.002 | <0.01 | <0.001 | 409 | 0.20 | 0.93 | 0.01 | 2.2 | 0.63 | 62 | <0.3 | 0.27 | <0.02 | 2.2 | 6.9 | 0.038 | 0.056 | 0.40 | 2.6 | 0.024 | 5.6 | 0.31 | 6.4 | 4.1 |
| CE491-31 avg | Rock composite 7E avg | 7.8 | <0.002 | <0.01 | <0.001 | 413 | 0.21 | 0.91 | 0.01 | 2.2 | 0.63 | 62 | <0.3 | 0.27 | <0.02 | 2.2 | 6.9 | 0.039 | 0.056 | 0.40 | 2.6 | 0.026 | 5.6 | 0.31 | 6.0 | 4.0 |
| LOD (3σ) | --- | 0.03 | 0.002 | 0.01 | 0.001 | 30 | 0.003 | 0.004 | 0.01 | 0.001 | 0.01 | 0.01 | 0.3 | 0.001 | 0.02 | 0.002 | 0.2 | 0.002 | 0.001 | 0.001 | 0.01 | 0.003 | 0.001 | 0.001 | 0.1 | 0.02 |
| | | C-241/C-209 | C-241/C-209 | C-241/C-209 | C-241/C-209 | C-241/C-209 | C-241/C-209 | C-241/C-209 | C-241/C-209 | C-241/C-209 | C-241/C-209 | C-241/C-209 | C-241/C-209 | C-241/C-209 | C-241/C-209 | C-241/C-209 | C-241/C-209 | C-241/C-209 | C-241/C-209 | C-241/C-209 | C-241/C-209 | C-241/C-209 | C-241/C-209 | C-241/C-209 | C-241/C-209 | C-241/C-209 |

Certified Reference Materials

| Sample ID | | Rb | Re | Rh | Ru | S | Sb | Sc | Se | Sm | Sn | Sr | Ta | Tb | Te | Th | Ti | Ti | Tm | U | V | W | Y | Yb | Zn | Zr |
|--------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| Sample Description | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) | (µg/g) |
| ERM-CC018-1 | --- | 1.7 | <0.002 | <0.01 | <0.001 | 579 | 0.96 | 0.20 | 0.11 | 0.58 | 7.1 | 53 | <0.3 | 0.083 | <0.02 | 0.14 | 45 | 0.062 | 0.032 | 0.62 | 7.2 | 0.85 | 3.5 | 0.20 | 218 | 4.7 |
| ERM-CC018-2 | --- | 2.0 | <0.002 | <0.01 | <0.001 | 617 | 1.0 | 0.20 | 0.11 | 0.66 | 7.5 | 56 | <0.3 | 0.097 | <0.02 | 0.15 | 49 | 0.070 | 0.036 | 0.67 | 7.7 | 0.97 | 4.2 | 0.23 | 248 | 5.1 |
| Avg ERM-CC018 | --- | 1.8 | <0.002 | <0.01 | <0.001 | 598 | 1.0 | 0.20 | 0.11 | 0.62 | 7.3 | 54 | <0.3 | 0.090 | <0.02 | 0.14 | 47 | 0.066 | 0.034 | 0.64 | 7.5 | 0.91 | 3.9 | 0.21 | 233 | 4.9 |
| In-house Value | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | 7.6 | 58 | --- | --- | --- | --- | 53 | --- | --- | 0.65 | 7.7 | --- | --- | --- | 241 | --- |

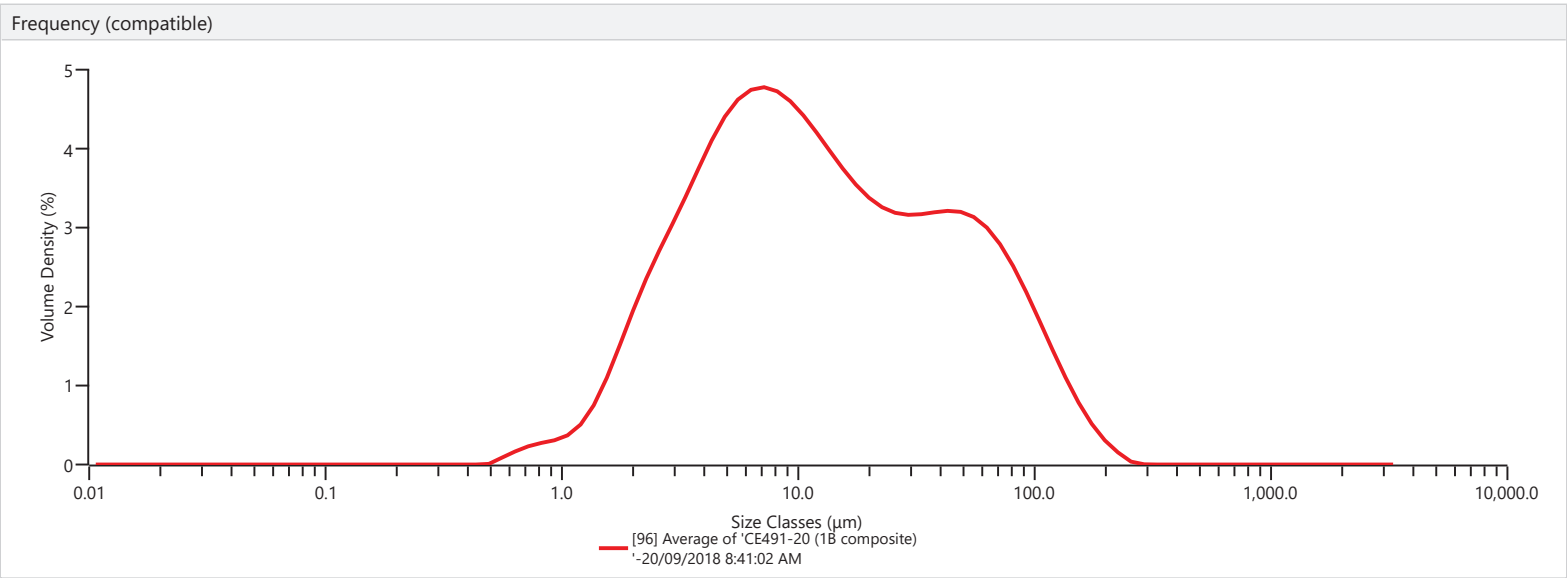
Spike Recoveries

| Sample ID | | Rb | Re | Rh | Ru | S | Sb | Sc | Se | Sm | Sn | Sr | Ta | Tb | Te | Th | Ti | Ti | Tm | U | V | W | Y | Yb | Zn | Zr |
|--------------------|-------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Sample Description | % | % | % | % | % | % | % | % | % | % | % | % | % | % | % | % | % | % | % | % | % | % | % | % | % | % |
| CE491-22 | Rock composite 2B | 116 | 111 | 110 | 112 | 104 | 113 | 110 | 104 | 113 | 111 | 99 | 527 | 112 | 111 | 109 | 100 | 114 | 112 | 107 | 108 | 117 | 111 | 113 | 111 | 114 |
| CE491-31 | Rock composite 7E | 107 | 105 | 100 | 101 | 97 | 104 | 105 | 100 | 104 | 103 | 98 | 522 | 104 | 103 | 104 | 99 | 102 | 105 | 103 | 105 | 109 | 107 | 106 | 104 | 104 |

Analyte of interest added to sample prior to analysis

Analysis

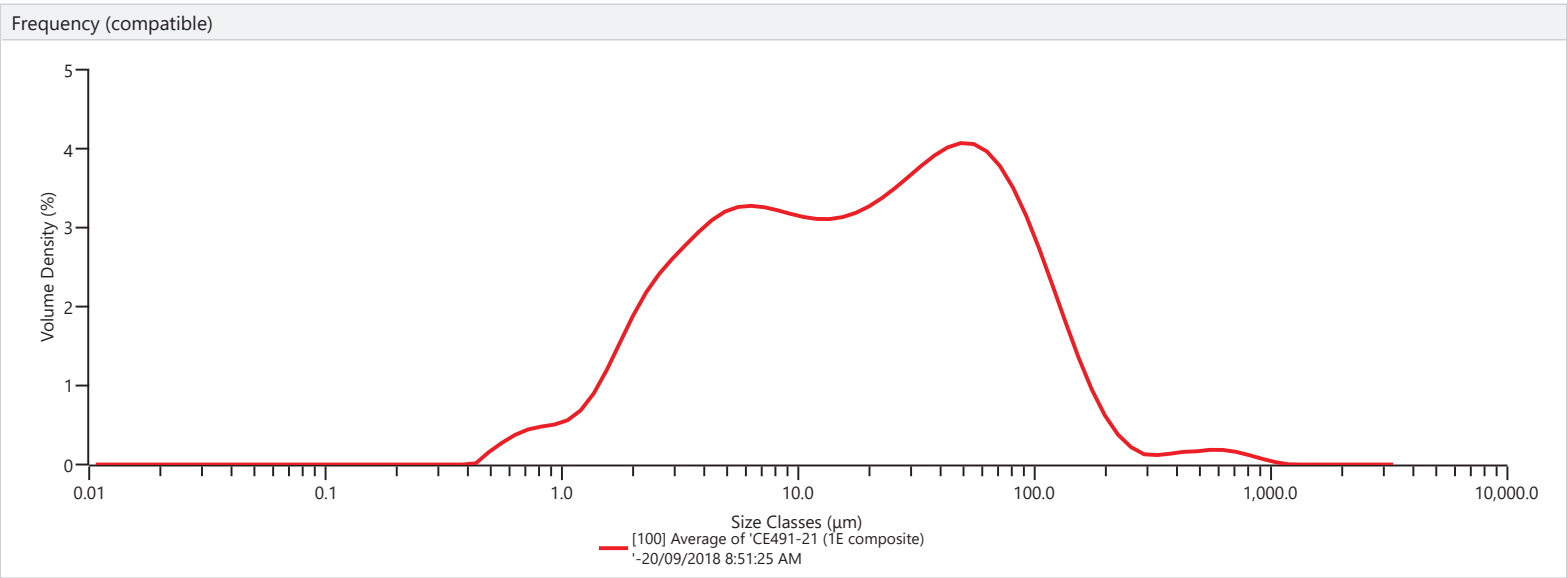
| | |
|--|---|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 20/09/2018 8:41:02 AM |
| Sample Name Average of 'CE491-20 (1B composite) ' | Measurement Date Time 20/09/2018 8:41:02 AM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0098 % |
| Particle Refractive Index 1.555 | Span 6.007 |
| Particle Absorption Index 0.010 | Uniformity 1.808 |
| Dispersant Name Water | Specific Surface Area 910.8 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 6.59 μm |
| Scattering Model Mie | D [4,3] 26.4 μm |
| Analysis Model General Purpose | Dv (10) 2.71 μm |
| Weighted Residual 0.49 % | Dv (50) 11.6 μm |
| Laser Obscuration 12.42 % | Dv (90) 72.2 μm |



| Result | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 6.03 | 12.7 | 52.63 | 76.0 | 90.95 | 454 | 100.00 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 7.99 | 14.5 | 55.94 | 86.4 | 93.05 | 516 | 100.00 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 10.25 | 16.4 | 59.07 | 98.1 | 94.87 | 586 | 100.00 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.00 | 3.12 | 12.79 | 18.7 | 62.02 | 111 | 96.39 | 666 | 100.00 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.07 | 3.55 | 15.61 | 21.2 | 64.83 | 127 | 97.60 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.21 | 4.03 | 18.74 | 24.1 | 67.55 | 144 | 98.52 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 0.41 | 4.58 | 22.16 | 27.4 | 70.20 | 163 | 99.17 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 0.64 | 5.21 | 25.84 | 31.1 | 72.83 | 186 | 99.60 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 0.89 | 5.92 | 29.70 | 35.3 | 75.48 | 211 | 99.85 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 1.19 | 6.72 | 33.66 | 40.1 | 78.14 | 240 | 99.98 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 1.61 | 7.64 | 37.65 | 45.6 | 80.82 | 272 | 100.00 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 2.23 | 8.68 | 41.60 | 51.8 | 83.49 | 310 | 100.00 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 3.14 | 9.86 | 45.44 | 58.9 | 86.11 | 352 | 100.00 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 4.40 | 11.2 | 49.12 | 66.9 | 88.61 | 400 | 100.00 | 2390 | 100.00 |

Analysis

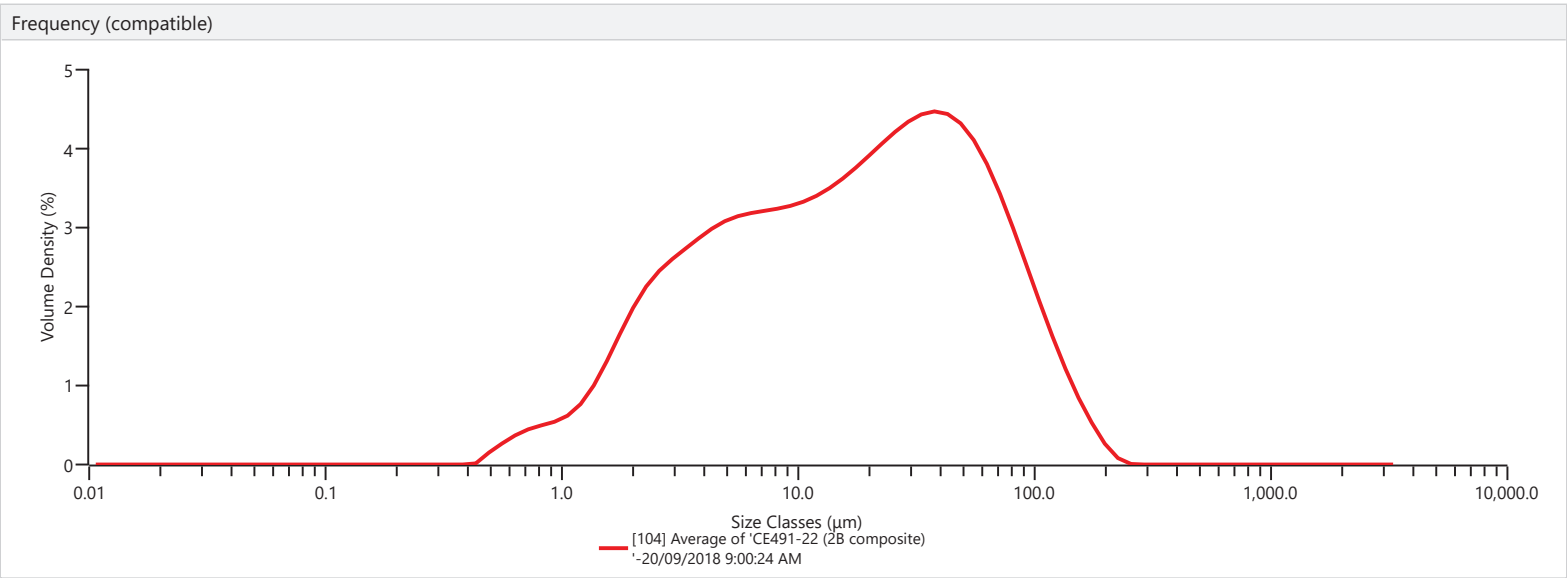
| | |
|--|---|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 20/09/2018 8:51:25 AM |
| Sample Name Average of 'CE491-21 (1E composite) ' | Measurement Date Time 20/09/2018 8:51:25 AM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0106 % |
| Particle Refractive Index 1.555 | Span 5.102 |
| Particle Absorption Index 0.010 | Uniformity 1.853 |
| Dispersant Name Water | Specific Surface Area 905.0 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 6.63 μm |
| Scattering Model Mie | D [4,3] 41.3 μm |
| Analysis Model General Purpose | Dv (10) 2.53 μm |
| Weighted Residual 0.37 % | Dv (50) 18.6 μm |
| Laser Obscuration 12.73 % | Dv (90) 97.2 μm |



| | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Result | | | | | | | | | | | | | |
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 7.51 | 12.7 | 42.25 | 76.0 | 84.63 | 454 | 99.23 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 9.33 | 14.5 | 44.84 | 86.4 | 87.55 | 516 | 99.37 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 11.35 | 16.4 | 47.45 | 98.1 | 90.18 | 586 | 99.52 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.14 | 3.12 | 13.52 | 18.7 | 50.11 | 111 | 92.46 | 666 | 99.68 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.37 | 3.55 | 15.84 | 21.2 | 52.83 | 127 | 94.36 | 756 | 99.81 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.68 | 4.03 | 18.29 | 24.1 | 55.64 | 144 | 95.86 | 859 | 99.91 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 1.06 | 4.58 | 20.87 | 27.4 | 58.56 | 163 | 96.99 | 976 | 99.97 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 1.46 | 5.21 | 23.55 | 31.1 | 61.60 | 186 | 97.78 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 1.88 | 5.92 | 26.27 | 35.3 | 64.75 | 211 | 98.29 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 2.34 | 6.72 | 29.00 | 40.1 | 68.02 | 240 | 98.60 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 2.90 | 7.64 | 31.72 | 45.6 | 71.37 | 272 | 98.78 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 3.65 | 8.68 | 34.40 | 51.8 | 74.77 | 310 | 98.88 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 4.65 | 9.86 | 37.05 | 58.9 | 78.16 | 352 | 98.98 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 5.93 | 11.2 | 39.66 | 66.9 | 81.47 | 400 | 99.09 | 2390 | 100.00 |

Analysis

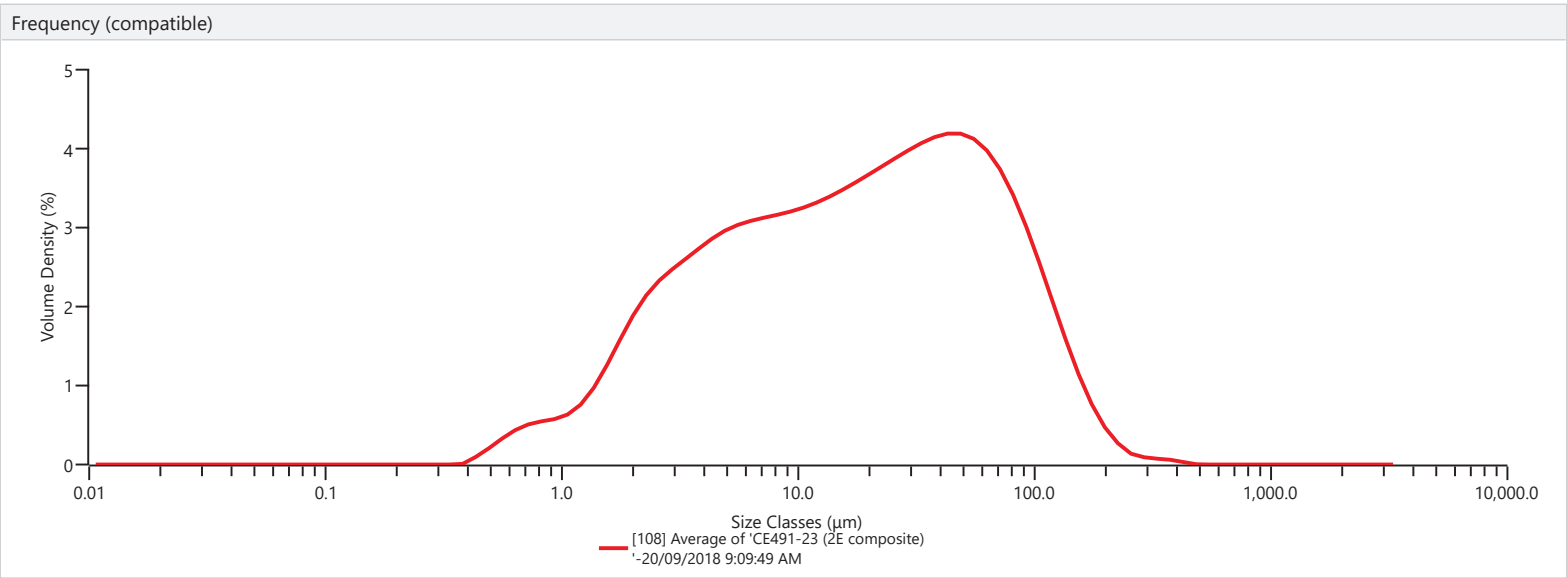
| | |
|--|---|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 20/09/2018 9:00:24 AM |
| Sample Name Average of 'CE491-22 (2B composite) ' | Measurement Date Time 20/09/2018 9:00:24 AM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0109 % |
| Particle Refractive Index 1.555 | Span 4.281 |
| Particle Absorption Index 0.010 | Uniformity 1.354 |
| Dispersant Name Water | Specific Surface Area 933.7 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 6.43 μm |
| Scattering Model Mie | D [4,3] 30.1 μm |
| Analysis Model General Purpose | Dv (10) 2.44 μm |
| Weighted Residual 0.52 % | Dv (50) 17.3 μm |
| Laser Obscuration 13.51 % | Dv (90) 76.4 μm |



| Result | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 8.00 | 12.7 | 42.82 | 76.0 | 89.89 | 454 | 100.00 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 9.88 | 14.5 | 45.74 | 86.4 | 92.39 | 516 | 100.00 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 11.93 | 16.4 | 48.75 | 98.1 | 94.50 | 586 | 100.00 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.13 | 3.12 | 14.10 | 18.7 | 51.89 | 111 | 96.23 | 666 | 100.00 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.35 | 3.55 | 16.38 | 21.2 | 55.15 | 127 | 97.58 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.66 | 4.03 | 18.77 | 24.1 | 58.54 | 144 | 98.59 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 1.03 | 4.58 | 21.26 | 27.4 | 62.05 | 163 | 99.29 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 1.45 | 5.21 | 23.83 | 31.1 | 65.67 | 186 | 99.72 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 1.90 | 5.92 | 26.45 | 35.3 | 69.37 | 211 | 99.94 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 2.41 | 6.72 | 29.11 | 40.1 | 73.11 | 240 | 100.00 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 3.04 | 7.64 | 31.78 | 45.6 | 76.81 | 272 | 100.00 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 3.87 | 8.68 | 34.48 | 51.8 | 80.42 | 310 | 100.00 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 4.96 | 9.86 | 37.21 | 58.9 | 83.85 | 352 | 100.00 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 6.34 | 11.2 | 39.99 | 66.9 | 87.03 | 400 | 100.00 | 2390 | 100.00 |

Analysis

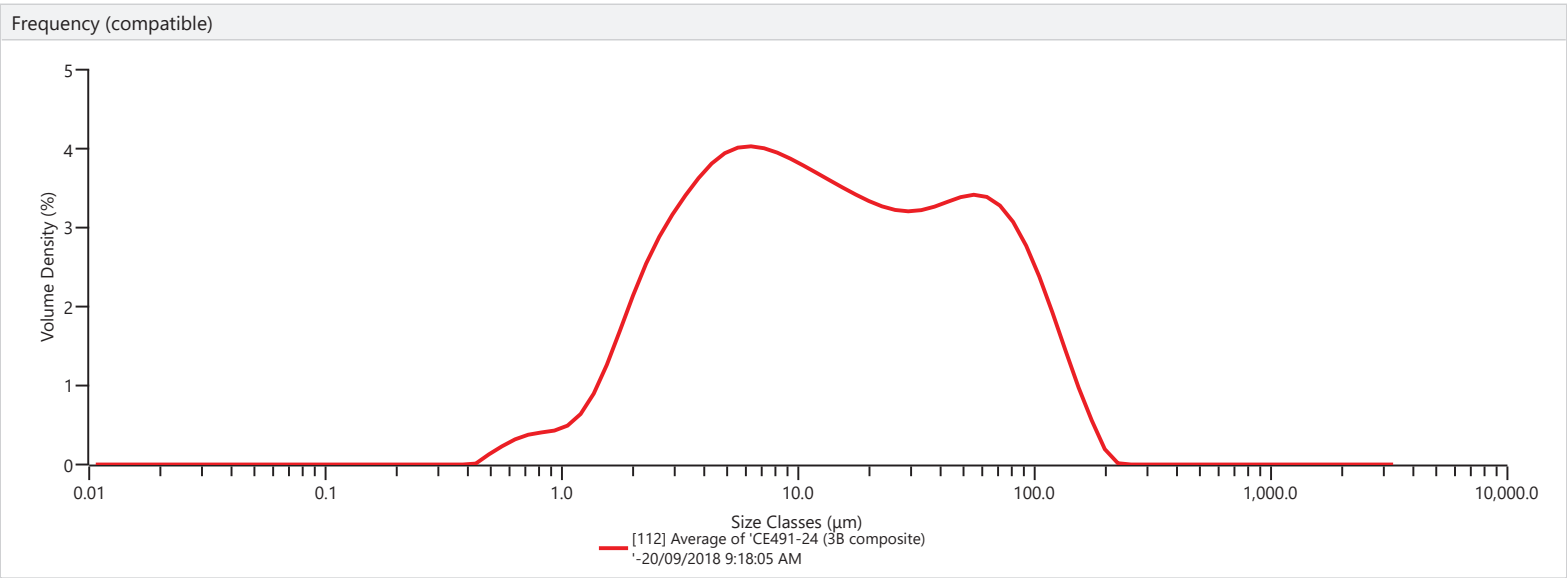
| | |
|--|---|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 20/09/2018 9:09:49 AM |
| Sample Name Average of 'CE491-23 (2E composite) ' | Measurement Date Time 20/09/2018 9:09:49 AM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0102 % |
| Particle Refractive Index 1.555 | Span 4.632 |
| Particle Absorption Index 0.010 | Uniformity 1.478 |
| Dispersant Name Water | Specific Surface Area 942.2 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 6.37 μm |
| Scattering Model Mie | D [4,3] 34.0 μm |
| Analysis Model General Purpose | Dv (10) 2.43 μm |
| Weighted Residual 0.48 % | Dv (50) 18.3 μm |
| Laser Obscuration 12.50 % | Dv (90) 87.3 μm |



| Result | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 8.14 | 12.7 | 41.74 | 76.0 | 86.94 | 454 | 100.00 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 9.93 | 14.5 | 44.56 | 86.4 | 89.79 | 516 | 100.00 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.08 | 2.75 | 11.88 | 16.4 | 47.46 | 98.1 | 92.31 | 586 | 100.00 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.25 | 3.12 | 13.94 | 18.7 | 50.44 | 111 | 94.44 | 666 | 100.00 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.53 | 3.55 | 16.11 | 21.2 | 53.51 | 127 | 96.17 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.89 | 4.03 | 18.39 | 24.1 | 56.65 | 144 | 97.49 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 1.32 | 4.58 | 20.77 | 27.4 | 59.89 | 163 | 98.44 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 1.77 | 5.21 | 23.24 | 31.1 | 63.20 | 186 | 99.07 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 2.25 | 5.92 | 25.78 | 35.3 | 66.60 | 211 | 99.46 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 2.77 | 6.72 | 28.35 | 40.1 | 70.06 | 240 | 99.68 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 3.40 | 7.64 | 30.96 | 45.6 | 73.55 | 272 | 99.79 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 4.20 | 8.68 | 33.59 | 51.8 | 77.05 | 310 | 99.86 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 5.25 | 9.86 | 36.26 | 58.9 | 80.50 | 352 | 99.92 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 6.57 | 11.2 | 38.97 | 66.9 | 83.82 | 400 | 99.97 | 2390 | 100.00 |

Analysis

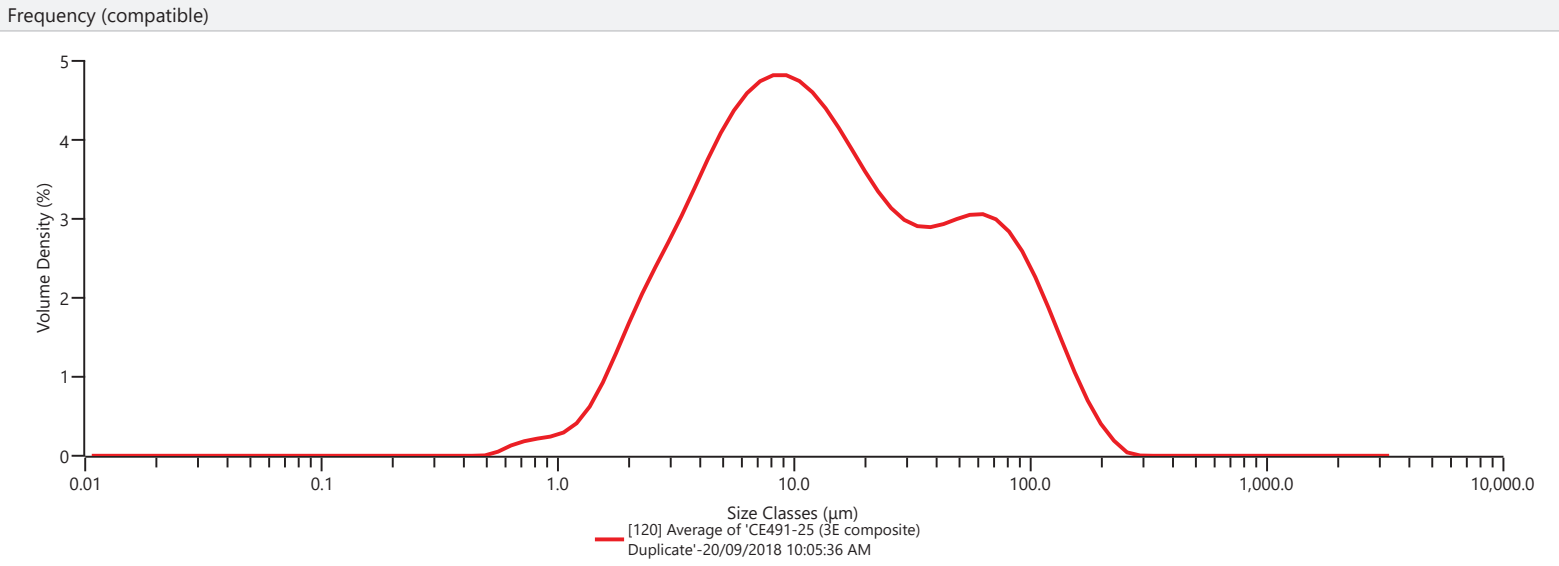
| | |
|--|---|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 20/09/2018 9:18:05 AM |
| Sample Name Average of 'CE491-24 (3B composite) ' | Measurement Date Time 20/09/2018 9:18:05 AM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0098 % |
| Particle Refractive Index 1.555 | Span 6.073 |
| Particle Absorption Index 0.010 | Uniformity 1.810 |
| Dispersant Name Water | Specific Surface Area 976.4 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 6.15 μm |
| Scattering Model Mie | D [4,3] 28.7 μm |
| Analysis Model General Purpose | Dv (10) 2.47 μm |
| Weighted Residual 0.49 % | Dv (50) 12.8 μm |
| Laser Obscuration 12.93 % | Dv (90) 80.3 μm |



| Result | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 7.50 | 12.7 | 49.83 | 76.0 | 88.89 | 454 | 100.00 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 9.63 | 14.5 | 52.83 | 86.4 | 91.46 | 516 | 100.00 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 12.04 | 16.4 | 55.76 | 98.1 | 93.78 | 586 | 100.00 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.11 | 3.12 | 14.68 | 18.7 | 58.61 | 111 | 95.77 | 666 | 100.00 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.30 | 3.55 | 17.52 | 21.2 | 61.39 | 127 | 97.38 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.57 | 4.03 | 20.55 | 24.1 | 64.11 | 144 | 98.58 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 0.89 | 4.58 | 23.73 | 27.4 | 66.80 | 163 | 99.39 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 1.23 | 5.21 | 27.02 | 31.1 | 69.47 | 186 | 99.85 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 1.58 | 5.92 | 30.37 | 35.3 | 72.15 | 211 | 100.00 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 1.99 | 6.72 | 33.73 | 40.1 | 74.87 | 240 | 100.00 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 2.51 | 7.64 | 37.07 | 45.6 | 77.65 | 272 | 100.00 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 3.26 | 8.68 | 40.37 | 51.8 | 80.47 | 310 | 100.00 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 4.30 | 9.86 | 43.60 | 58.9 | 83.32 | 352 | 100.00 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 5.72 | 11.2 | 46.75 | 66.9 | 86.15 | 400 | 100.00 | 2390 | 100.00 |

Analysis

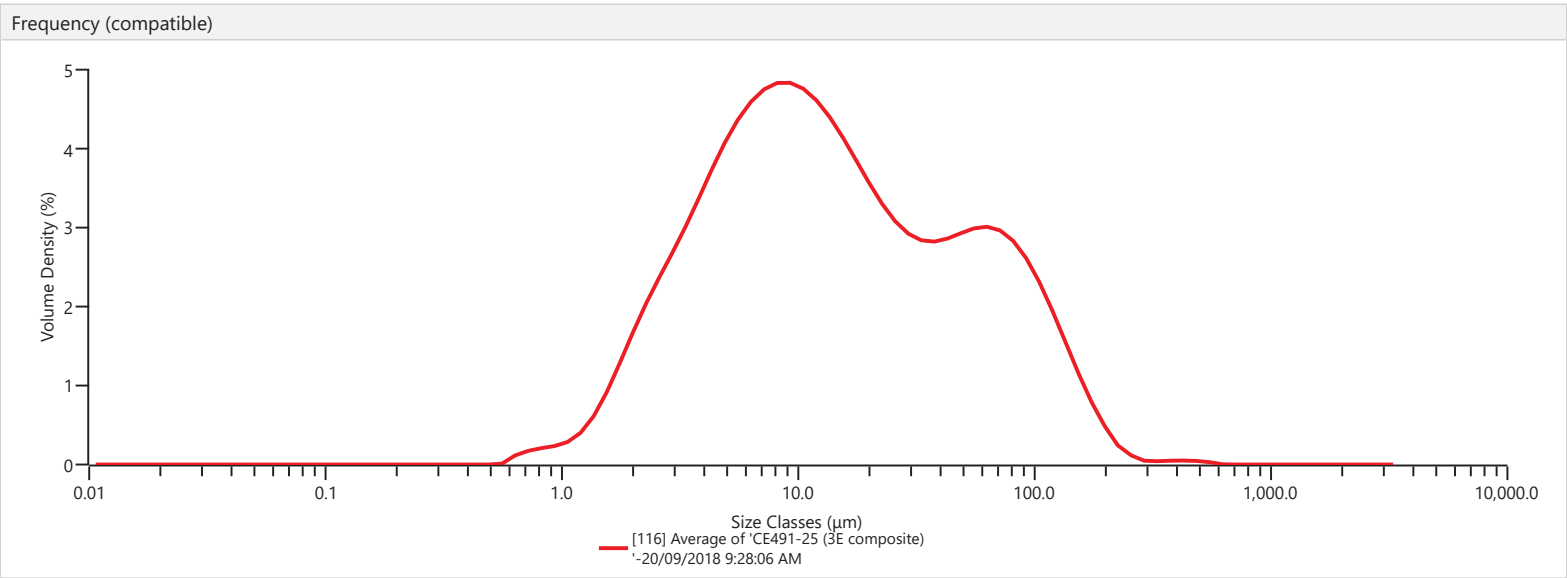
| | |
|--|--|
| Measurement Details | Measurement Details |
| <div><div>Operator Name</div>CSIRO Mastersizer</div> <div><div>Sample Name</div>Average of 'CE491-25 (3E composite) Duplicate'</div> <div><div>SOP File Name</div>Sediment Sonnication_SOP.msop</div> | <div><div>Analysis Date Time</div>20/09/2018 10:05:36 AM</div> <div><div>Measurement Date Time</div>20/09/2018 10:05:36 AM</div> <div><div>Result Source</div>Averaged</div> |
| Analysis | Result |
| <div><div>Particle Name</div>China Clay</div> <div><div>Particle Refractive Index</div>1.555</div> <div><div>Particle Absorption Index</div>0.010</div> <div><div>Dispersant Name</div>Water</div> <div><div>Dispersant Refractive Index</div>1.330</div> <div><div>Scattering Model</div>Mie</div> <div><div>Analysis Model</div>General Purpose</div> <div><div>Weighted Residual</div>0.42 %</div> <div><div>Laser Obscuration</div>16.54 %</div> | <div><div>Concentration</div>0.0147 %</div> <div><div>Span</div>6.171</div> <div><div>Uniformity</div>1.805</div> <div><div>Specific Surface Area</div>833.2 m²/kg</div> <div><div>D [3,2]</div>7.20 μm</div> <div><div>D [4,3]</div>28.9 μm</div> <div><div>Dv (10)</div>2.95 μm</div> <div><div>Dv (50)</div>12.7 μm</div> <div><div>Dv (90)</div>81.0 μm</div> |



| Result | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 5.03 | 12.7 | 50.17 | 76.0 | 88.81 | 454 | 100.00 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 6.75 | 14.5 | 53.85 | 86.4 | 91.18 | 516 | 100.00 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 8.74 | 16.4 | 57.31 | 98.1 | 93.35 | 586 | 100.00 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.00 | 3.12 | 10.99 | 18.7 | 60.55 | 111 | 95.24 | 666 | 100.00 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.04 | 3.55 | 13.52 | 21.2 | 63.55 | 127 | 96.81 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.15 | 4.03 | 16.34 | 24.1 | 66.34 | 144 | 98.03 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 0.31 | 4.58 | 19.47 | 27.4 | 68.95 | 163 | 98.91 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 0.49 | 5.21 | 22.89 | 31.1 | 71.43 | 186 | 99.48 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 0.69 | 5.92 | 26.54 | 35.3 | 73.85 | 211 | 99.82 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 0.93 | 6.72 | 30.37 | 40.1 | 76.26 | 240 | 99.97 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 1.27 | 7.64 | 34.33 | 45.6 | 78.71 | 272 | 100.00 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 1.78 | 8.68 | 38.35 | 51.8 | 81.20 | 310 | 100.00 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 2.55 | 9.86 | 42.37 | 58.9 | 83.75 | 352 | 100.00 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 3.63 | 11.2 | 46.33 | 66.9 | 86.31 | 400 | 100.00 | 2390 | 100.00 |

Analysis

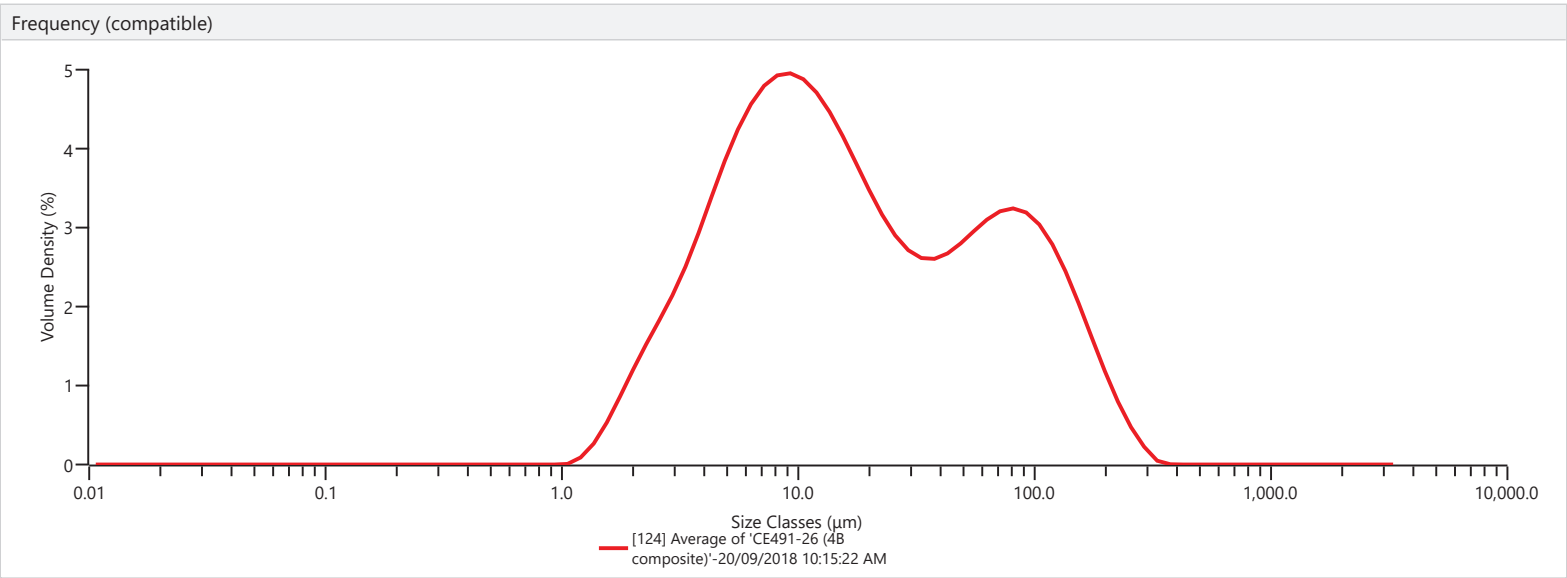
| | |
|--|---|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 20/09/2018 9:28:06 AM |
| Sample Name Average of 'CE491-25 (3E composite) ' | Measurement Date Time 20/09/2018 9:28:06 AM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0116 % |
| Particle Refractive Index 1.555 | Span 6.386 |
| Particle Absorption Index 0.010 | Uniformity 1.911 |
| Dispersant Name Water | Specific Surface Area 821.7 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 7.30 μm |
| Scattering Model Mie | D [4,3] 30.4 μm |
| Analysis Model General Purpose | Dv (10) 2.98 μm |
| Weighted Residual 0.48 % | Dv (50) 12.7 μm |
| Laser Obscuration 13.26 % | Dv (90) 84.3 μm |



| Result | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 4.91 | 12.7 | 49.99 | 76.0 | 88.08 | 454 | 99.93 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 6.62 | 14.5 | 53.66 | 86.4 | 90.45 | 516 | 99.97 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 8.59 | 16.4 | 57.12 | 98.1 | 92.64 | 586 | 100.00 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.00 | 3.12 | 10.83 | 18.7 | 60.34 | 111 | 94.57 | 666 | 100.00 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.00 | 3.55 | 13.34 | 21.2 | 63.31 | 127 | 96.19 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.10 | 4.03 | 16.14 | 24.1 | 66.06 | 144 | 97.48 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 0.25 | 4.58 | 19.26 | 27.4 | 68.63 | 163 | 98.44 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 0.42 | 5.21 | 22.66 | 31.1 | 71.06 | 186 | 99.09 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 0.61 | 5.92 | 26.30 | 35.3 | 73.42 | 211 | 99.49 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 0.85 | 6.72 | 30.14 | 40.1 | 75.77 | 240 | 99.69 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 1.18 | 7.64 | 34.10 | 45.6 | 78.15 | 272 | 99.78 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 1.68 | 8.68 | 38.14 | 51.8 | 80.60 | 310 | 99.82 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 2.44 | 9.86 | 42.17 | 58.9 | 83.09 | 352 | 99.85 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 3.52 | 11.2 | 46.14 | 66.9 | 85.61 | 400 | 99.89 | 2390 | 100.00 |

Analysis

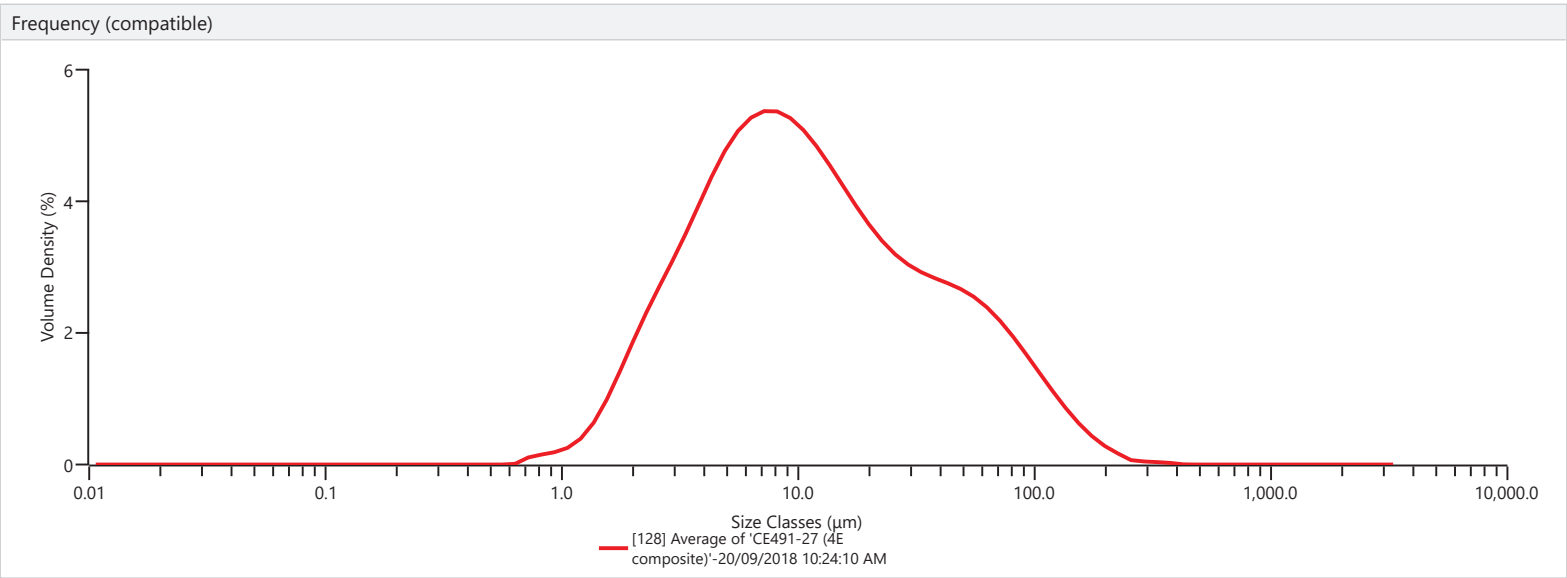
| | |
|---|---|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 20/09/2018 10:15:22 AM |
| Sample Name Average of 'CE491-26 (4B composite)' | Measurement Date Time 20/09/2018 10:15:22 AM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0139 % |
| Particle Refractive Index 1.555 | Span 7.041 |
| Particle Absorption Index 0.010 | Uniformity 2.070 |
| Dispersant Name Water | Specific Surface Area 650.0 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 9.23 μm |
| Scattering Model Mie | D [4,3] 38.4 μm |
| Analysis Model General Purpose | Dv (10) 3.72 μm |
| Weighted Residual 0.54 % | Dv (50) 15.0 μm |
| Laser Obscuration 12.60 % | Dv (90) 110 μm |



| Result | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 2.44 | 12.7 | 45.20 | 76.0 | 82.41 | 454 | 100.00 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 3.71 | 14.5 | 48.93 | 86.4 | 85.12 | 516 | 100.00 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 5.23 | 16.4 | 52.40 | 98.1 | 87.79 | 586 | 100.00 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.00 | 3.12 | 7.01 | 18.7 | 55.58 | 111 | 90.33 | 666 | 100.00 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.00 | 3.55 | 9.10 | 21.2 | 58.48 | 127 | 92.66 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.00 | 4.03 | 11.54 | 24.1 | 61.12 | 144 | 94.71 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 0.00 | 4.58 | 14.37 | 27.4 | 63.53 | 163 | 96.41 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 0.00 | 5.21 | 17.58 | 31.1 | 65.79 | 186 | 97.75 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 0.00 | 5.92 | 21.12 | 35.3 | 67.96 | 211 | 98.74 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 0.00 | 6.72 | 24.93 | 40.1 | 70.13 | 240 | 99.40 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 0.07 | 7.64 | 28.94 | 45.6 | 72.35 | 272 | 99.79 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 0.28 | 8.68 | 33.05 | 51.8 | 74.69 | 310 | 99.97 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 0.72 | 9.86 | 37.19 | 58.9 | 77.15 | 352 | 100.00 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 1.44 | 11.2 | 41.27 | 66.9 | 79.74 | 400 | 100.00 | 2390 | 100.00 |

Analysis

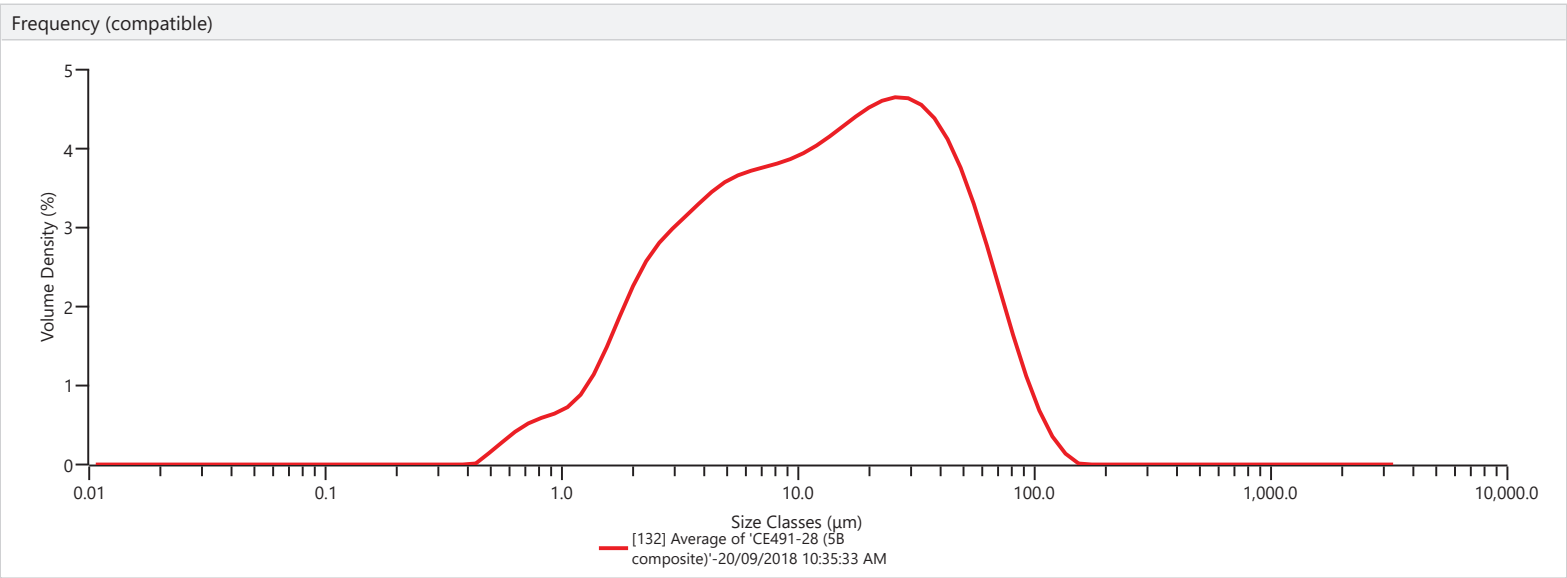
| | |
|---|---|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 20/09/2018 10:24:10 AM |
| Sample Name Average of 'CE491-27 (4E composite)' | Measurement Date Time 20/09/2018 10:24:10 AM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0101 % |
| Particle Refractive Index 1.555 | Span 5.663 |
| Particle Absorption Index 0.010 | Uniformity 1.724 |
| Dispersant Name Water | Specific Surface Area 882.1 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 6.80 μm |
| Scattering Model Mie | D [4,3] 23.7 μm |
| Analysis Model General Purpose | Dv (10) 2.87 μm |
| Weighted Residual 0.44 % | Dv (50) 10.6 μm |
| Laser Obscuration 12.55 % | Dv (90) 62.9 μm |



| Result | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 4.98 | 12.7 | 55.84 | 76.0 | 92.77 | 454 | 100.00 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 6.91 | 14.5 | 59.63 | 86.4 | 94.40 | 516 | 100.00 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 9.16 | 16.4 | 63.17 | 98.1 | 95.79 | 586 | 100.00 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.00 | 3.12 | 11.74 | 18.7 | 66.45 | 111 | 96.96 | 666 | 100.00 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.00 | 3.55 | 14.66 | 21.2 | 69.49 | 127 | 97.89 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.00 | 4.03 | 17.94 | 24.1 | 72.32 | 144 | 98.61 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 0.10 | 4.58 | 21.59 | 27.4 | 74.98 | 163 | 99.13 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 0.22 | 5.21 | 25.57 | 31.1 | 77.51 | 186 | 99.49 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 0.38 | 5.92 | 29.80 | 35.3 | 79.94 | 211 | 99.72 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 0.58 | 6.72 | 34.20 | 40.1 | 82.30 | 240 | 99.86 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 0.90 | 7.64 | 38.68 | 45.6 | 84.60 | 272 | 99.91 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 1.42 | 8.68 | 43.16 | 51.8 | 86.83 | 310 | 99.95 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 2.24 | 9.86 | 47.56 | 58.9 | 88.96 | 352 | 99.98 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 3.42 | 11.2 | 51.80 | 66.9 | 90.95 | 400 | 100.00 | 2390 | 100.00 |

Analysis

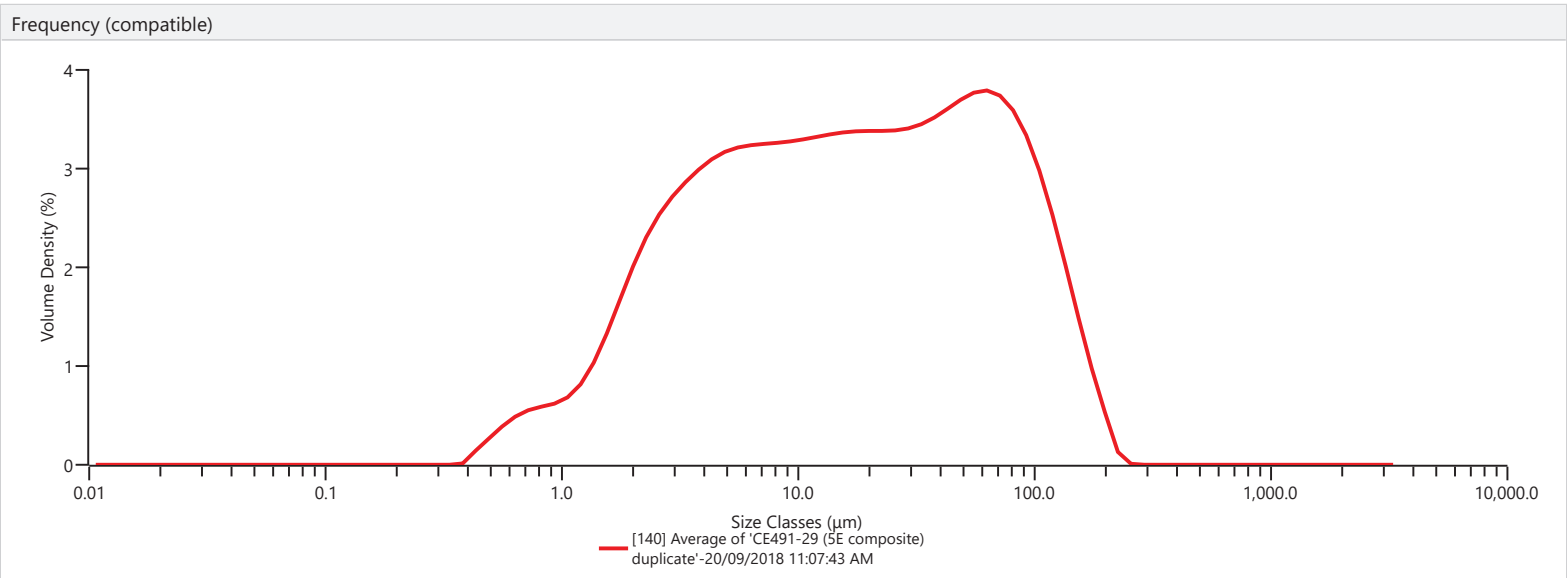
| | |
|---|--|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 20/09/2018 10:35:33 AM |
| Sample Name Average of 'CE491-28 (5B composite)' | Measurement Date Time 20/09/2018 10:35:33 AM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0085 % |
| Particle Refractive Index 1.555 | Span 3.886 |
| Particle Absorption Index 0.010 | Uniformity 1.216 |
| Dispersant Name Water | Specific Surface Area 1060 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 5.66 μm |
| Scattering Model Mie | D [4,3] 21.0 μm |
| Analysis Model General Purpose | Dv (10) 2.24 μm |
| Weighted Residual 0.37 % | Dv (50) 12.9 μm |
| Laser Obscuration 12.12 % | Dv (90) 52.2 μm |



| Result | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 9.14 | 12.7 | 49.71 | 76.0 | 96.74 | 454 | 100.00 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 11.29 | 14.5 | 53.17 | 86.4 | 98.11 | 516 | 100.00 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 13.64 | 16.4 | 56.74 | 98.1 | 99.04 | 586 | 100.00 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.12 | 3.12 | 16.13 | 18.7 | 60.42 | 111 | 99.60 | 666 | 100.00 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.36 | 3.55 | 18.75 | 21.2 | 64.19 | 127 | 99.89 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.70 | 4.03 | 21.50 | 24.1 | 68.03 | 144 | 100.00 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 1.14 | 4.58 | 24.38 | 27.4 | 71.91 | 163 | 100.00 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 1.63 | 5.21 | 27.36 | 31.1 | 75.78 | 186 | 100.00 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 2.17 | 5.92 | 30.42 | 35.3 | 79.59 | 211 | 100.00 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 2.77 | 6.72 | 33.52 | 40.1 | 83.25 | 240 | 100.00 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 3.50 | 7.64 | 36.66 | 45.6 | 86.69 | 272 | 100.00 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 4.44 | 8.68 | 39.84 | 51.8 | 89.83 | 310 | 100.00 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 5.68 | 9.86 | 43.06 | 58.9 | 92.59 | 352 | 100.00 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 7.25 | 11.2 | 46.34 | 66.9 | 94.90 | 400 | 100.00 | 2390 | 100.00 |

Analysis

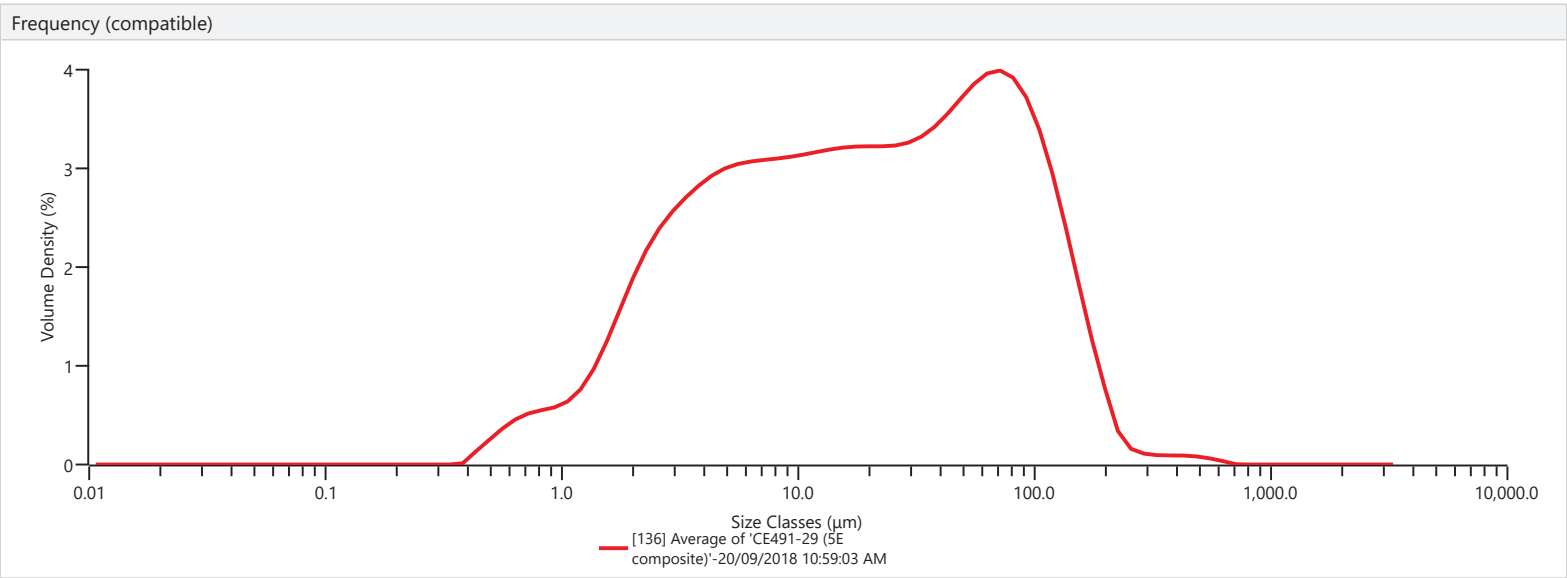
| | |
|---|--|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 20/09/2018 11:07:43 AM |
| Sample Name Average of 'CE491-29 (5E composite) duplicate' | Measurement Date Time 20/09/2018 11:07:43 AM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0102 % |
| Particle Refractive Index 1.555 | Span 5.504 |
| Particle Absorption Index 0.010 | Uniformity 1.676 |
| Dispersant Name Water | Specific Surface Area 1008 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 5.95 μm |
| Scattering Model Mie | D [4,3] 33.9 μm |
| Analysis Model General Purpose | Dv (10) 2.30 μm |
| Weighted Residual 0.44 % | Dv (50) 16.5 μm |
| Laser Obscuration 13.17 % | Dv (90) 93.2 μm |



| Result | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 8.82 | 12.7 | 44.29 | 76.0 | 85.34 | 454 | 100.00 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 10.74 | 14.5 | 47.08 | 86.4 | 88.34 | 516 | 100.00 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.12 | 2.75 | 12.86 | 16.4 | 49.89 | 98.1 | 91.13 | 586 | 100.00 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.34 | 3.12 | 15.13 | 18.7 | 52.71 | 111 | 93.62 | 666 | 100.00 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.67 | 3.55 | 17.52 | 21.2 | 55.52 | 127 | 95.74 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 1.08 | 4.03 | 20.01 | 24.1 | 58.34 | 144 | 97.42 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 1.54 | 4.58 | 22.59 | 27.4 | 61.17 | 163 | 98.66 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 2.03 | 5.21 | 25.23 | 31.1 | 64.00 | 186 | 99.47 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 2.54 | 5.92 | 27.92 | 35.3 | 66.88 | 211 | 99.91 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 3.11 | 6.72 | 30.62 | 40.1 | 69.81 | 240 | 100.00 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 3.78 | 7.64 | 33.33 | 45.6 | 72.82 | 272 | 100.00 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 4.64 | 8.68 | 36.04 | 51.8 | 75.90 | 310 | 100.00 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 5.74 | 9.86 | 38.78 | 58.9 | 79.05 | 352 | 100.00 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 7.14 | 11.2 | 41.52 | 66.9 | 82.21 | 400 | 100.00 | 2390 | 100.00 |

Analysis

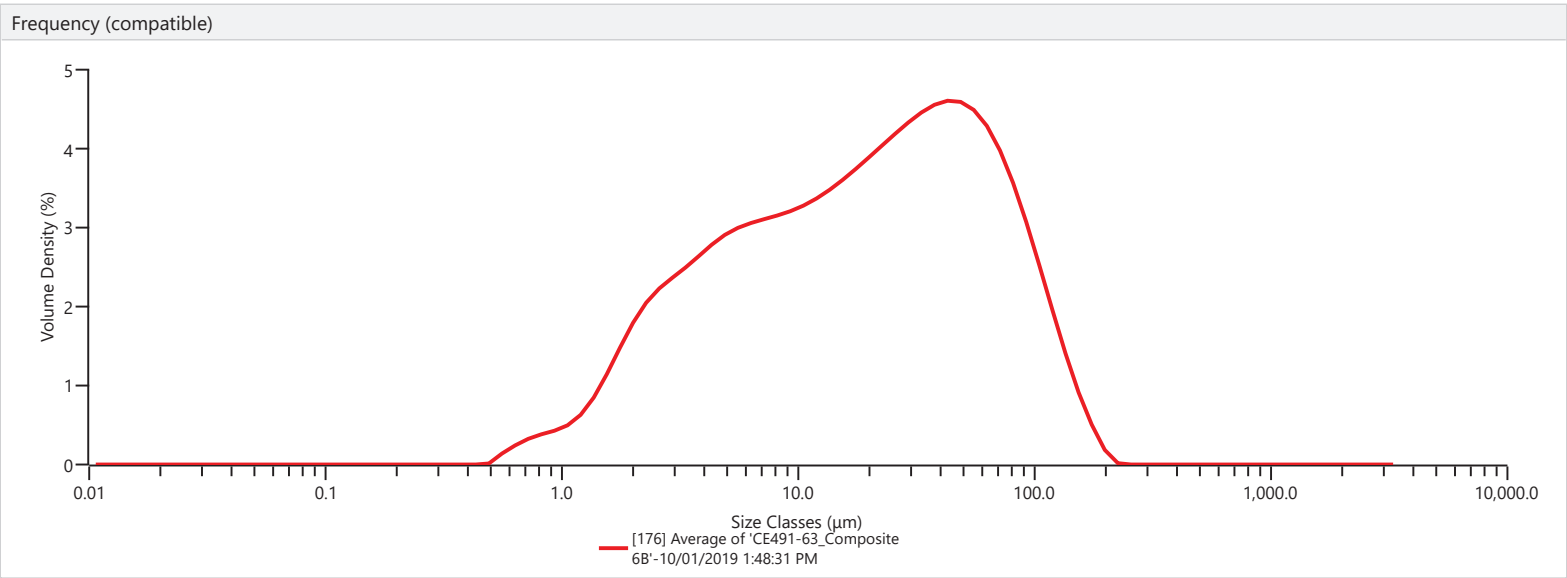
| | |
|---|---|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 20/09/2018 10:59:03 AM |
| Sample Name Average of 'CE491-29 (5E composite)' | Measurement Date Time 20/09/2018 10:59:03 AM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0106 % |
| Particle Refractive Index 1.555 | Span 5.445 |
| Particle Absorption Index 0.010 | Uniformity 1.738 |
| Dispersant Name Water | Specific Surface Area 952.7 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 6.30 μm |
| Scattering Model Mie | D [4,3] 39.5 μm |
| Analysis Model General Purpose | Dv (10) 2.41 μm |
| Weighted Residual 0.55 % | Dv (50) 18.8 μm |
| Laser Obscuration 12.97 % | Dv (90) 105 μm |



| | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Result | | | | | | | | | | | | | |
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 8.26 | 12.7 | 41.87 | 76.0 | 82.20 | 454 | 99.85 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 10.07 | 14.5 | 44.53 | 86.4 | 85.48 | 516 | 99.92 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.11 | 2.75 | 12.07 | 16.4 | 47.21 | 98.1 | 88.59 | 586 | 99.97 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.32 | 3.12 | 14.21 | 18.7 | 49.90 | 111 | 91.43 | 666 | 100.00 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.62 | 3.55 | 16.46 | 21.2 | 52.59 | 127 | 93.89 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 1.00 | 4.03 | 18.82 | 24.1 | 55.27 | 144 | 95.91 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 1.44 | 4.58 | 21.26 | 27.4 | 57.97 | 163 | 97.44 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 1.89 | 5.21 | 23.76 | 31.1 | 60.68 | 186 | 98.49 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 2.38 | 5.92 | 26.30 | 35.3 | 63.45 | 211 | 99.14 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 2.90 | 6.72 | 28.86 | 40.1 | 66.30 | 240 | 99.40 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 3.53 | 7.64 | 31.44 | 45.6 | 69.26 | 272 | 99.53 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 4.33 | 8.68 | 34.02 | 51.8 | 72.35 | 310 | 99.62 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 5.37 | 9.86 | 36.62 | 58.9 | 75.56 | 352 | 99.69 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 6.68 | 11.2 | 39.24 | 66.9 | 78.87 | 400 | 99.77 | 2390 | 100.00 |

Analysis

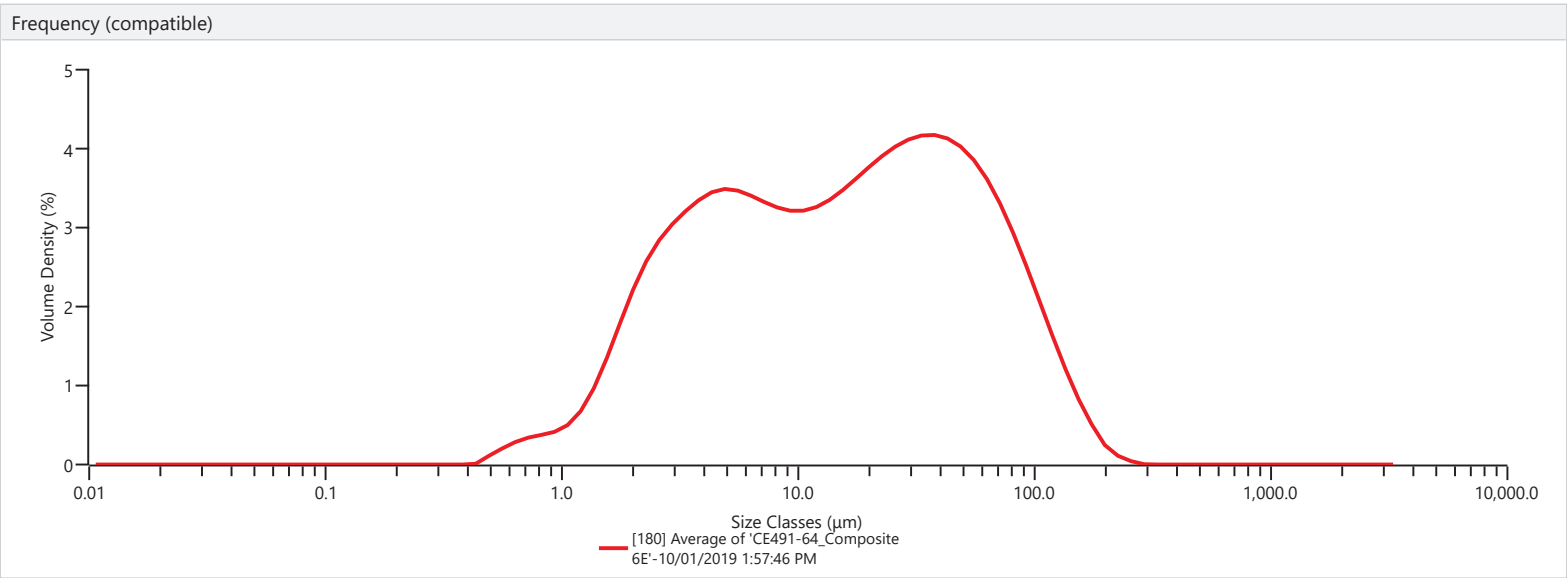
| | |
|---|---|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 10/01/2019 1:48:31 PM |
| Sample Name Average of 'CE491-63_Composite 6B' | Measurement Date Time 10/01/2019 1:48:31 PM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0066 % |
| Particle Refractive Index 1.555 | Span 4.029 |
| Particle Absorption Index 0.010 | Uniformity 1.260 |
| Dispersant Name Water | Specific Surface Area 817.8 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 7.34 μm |
| Scattering Model Mie | D [4,3] 32.5 μm |
| Analysis Model General Purpose | Dv (10) 2.72 μm |
| Weighted Residual 0.52 % | Dv (50) 19.7 μm |
| Laser Obscuration 7.63 % | Dv (90) 82.0 μm |



| Result | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 6.59 | 12.7 | 39.64 | 76.0 | 88.23 | 454 | 100.00 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 8.30 | 14.5 | 42.54 | 86.4 | 91.21 | 516 | 100.00 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 10.16 | 16.4 | 45.54 | 98.1 | 93.78 | 586 | 100.00 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.00 | 3.12 | 12.13 | 18.7 | 48.66 | 111 | 95.88 | 666 | 100.00 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.12 | 3.55 | 14.21 | 21.2 | 51.91 | 127 | 97.51 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.32 | 4.03 | 16.41 | 24.1 | 55.27 | 144 | 98.68 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 0.60 | 4.58 | 18.73 | 27.4 | 58.77 | 163 | 99.44 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 0.92 | 5.21 | 21.16 | 31.1 | 62.38 | 186 | 99.85 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 1.27 | 5.92 | 23.66 | 35.3 | 66.10 | 211 | 100.00 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 1.68 | 6.72 | 26.21 | 40.1 | 69.90 | 240 | 100.00 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 2.20 | 7.64 | 28.80 | 45.6 | 73.74 | 272 | 100.00 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 2.90 | 8.68 | 31.43 | 51.8 | 77.58 | 310 | 100.00 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 3.85 | 9.86 | 34.10 | 58.9 | 81.33 | 352 | 100.00 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 5.09 | 11.2 | 36.83 | 66.9 | 84.91 | 400 | 100.00 | 2390 | 100.00 |

Analysis

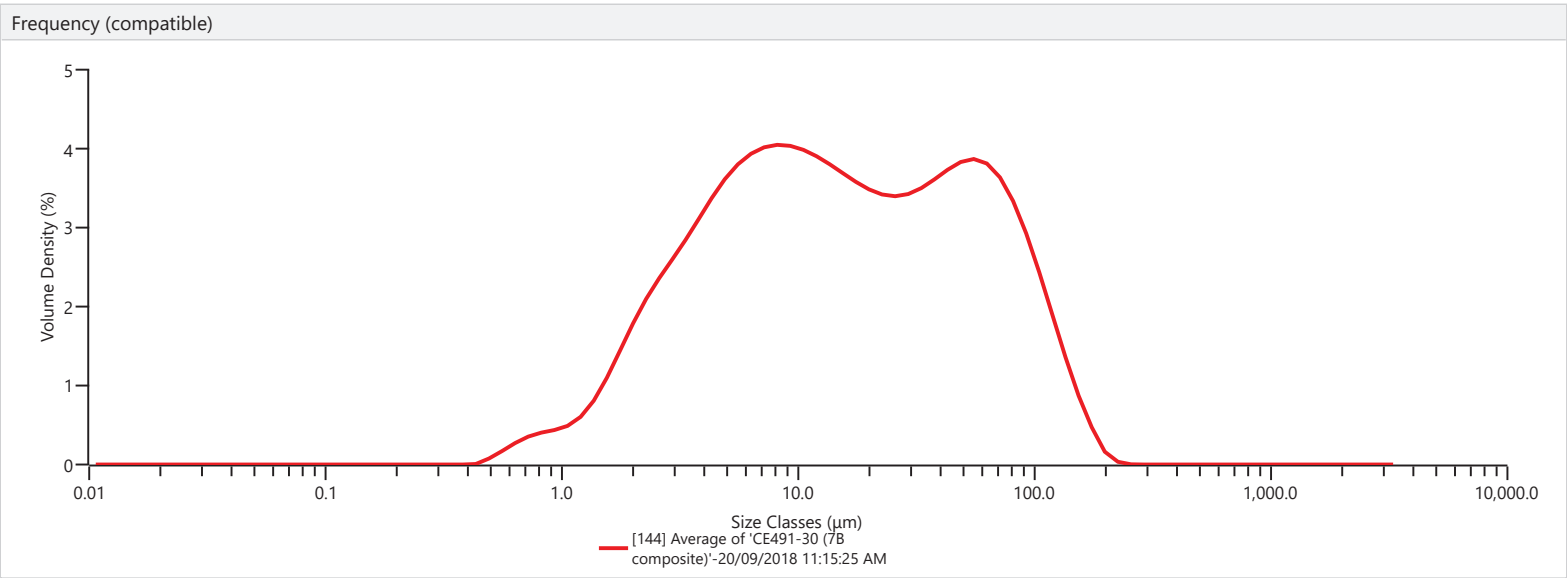
| | |
|---|---|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 10/01/2019 1:57:46 PM |
| Sample Name Average of 'CE491-64_Composite 6E' | Measurement Date Time 10/01/2019 1:57:46 PM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0060 % |
| Particle Refractive Index 1.555 | Span 4.689 |
| Particle Absorption Index 0.010 | Uniformity 1.475 |
| Dispersant Name Water | Specific Surface Area 939.4 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 6.39 μm |
| Scattering Model Mie | D [4,3] 29.3 μm |
| Analysis Model General Purpose | Dv (10) 2.45 μm |
| Weighted Residual 0.52 % | Dv (50) 15.7 μm |
| Laser Obscuration 7.94 % | Dv (90) 76.3 μm |



| Result | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 7.66 | 12.7 | 45.27 | 76.0 | 89.93 | 454 | 100.00 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 9.81 | 14.5 | 48.06 | 86.4 | 92.38 | 516 | 100.00 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 12.19 | 16.4 | 50.96 | 98.1 | 94.48 | 586 | 100.00 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.09 | 3.12 | 14.73 | 18.7 | 53.98 | 111 | 96.21 | 666 | 100.00 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.26 | 3.55 | 17.40 | 21.2 | 57.12 | 127 | 97.57 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.50 | 4.03 | 20.19 | 24.1 | 60.37 | 144 | 98.58 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 0.79 | 4.58 | 23.07 | 27.4 | 63.73 | 163 | 99.26 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 1.10 | 5.21 | 25.99 | 31.1 | 67.16 | 186 | 99.68 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 1.44 | 5.92 | 28.88 | 35.3 | 70.64 | 211 | 99.88 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 1.85 | 6.72 | 31.72 | 40.1 | 74.12 | 240 | 99.97 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 2.40 | 7.64 | 34.49 | 45.6 | 77.57 | 272 | 100.00 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 3.20 | 8.68 | 37.20 | 51.8 | 80.93 | 310 | 100.00 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 4.32 | 9.86 | 39.88 | 58.9 | 84.15 | 352 | 100.00 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 5.81 | 11.2 | 42.56 | 66.9 | 87.17 | 400 | 100.00 | 2390 | 100.00 |

Analysis

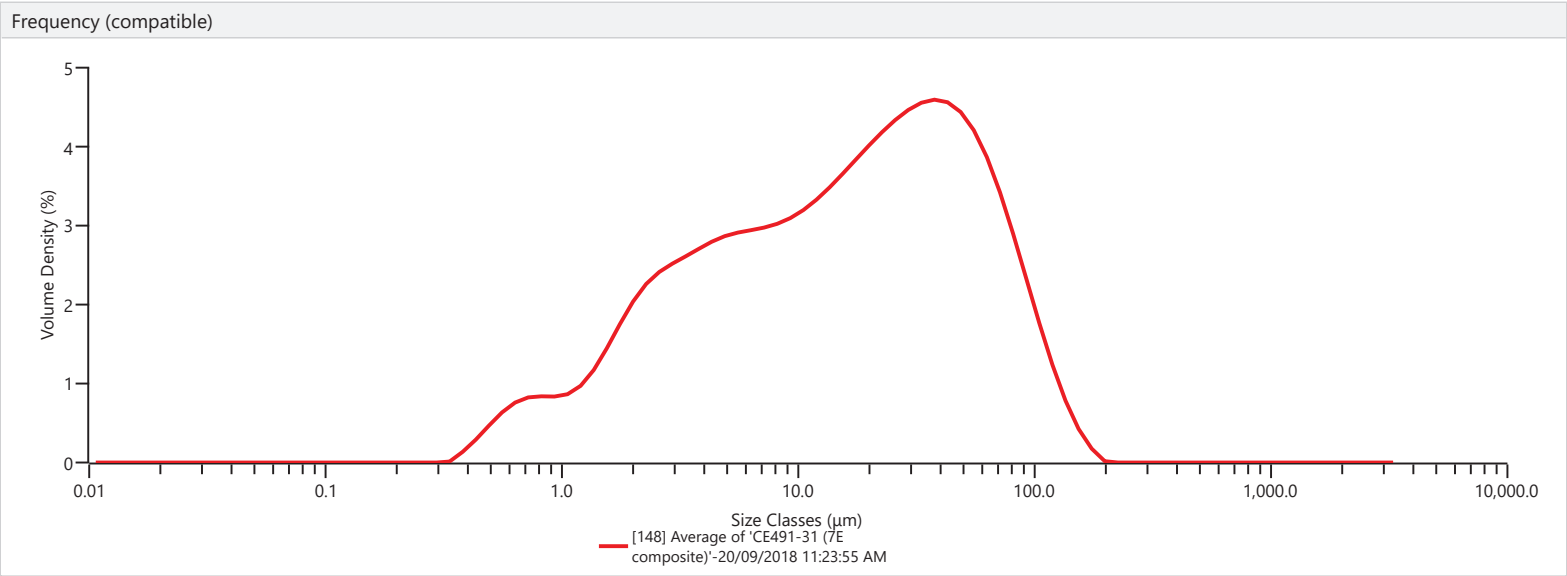
| | |
|---|---|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 20/09/2018 11:15:25 AM |
| Sample Name Average of 'CE491-30 (7B composite)' | Measurement Date Time 20/09/2018 11:15:25 AM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0100 % |
| Particle Refractive Index 1.555 | Span 5.283 |
| Particle Absorption Index 0.010 | Uniformity 1.607 |
| Dispersant Name Water | Specific Surface Area 886.9 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 6.77 μm |
| Scattering Model Mie | D [4,3] 29.9 μm |
| Analysis Model General Purpose | Dv (10) 2.69 μm |
| Weighted Residual 0.48 % | Dv (50) 14.7 μm |
| Laser Obscuration 12.06 % | Dv (90) 80.4 μm |



| | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Result | | | | | | | | | | | | | |
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 6.60 | 12.7 | 46.41 | 76.0 | 88.77 | 454 | 100.00 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 8.35 | 14.5 | 49.58 | 86.4 | 91.56 | 516 | 100.00 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 10.32 | 16.4 | 52.66 | 98.1 | 94.01 | 586 | 100.00 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.06 | 3.12 | 12.49 | 18.7 | 55.64 | 111 | 96.04 | 666 | 100.00 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.20 | 3.55 | 14.86 | 21.2 | 58.55 | 127 | 97.62 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.43 | 4.03 | 17.45 | 24.1 | 61.39 | 144 | 98.75 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 0.73 | 4.58 | 20.26 | 27.4 | 64.22 | 163 | 99.47 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 1.07 | 5.21 | 23.28 | 31.1 | 67.08 | 186 | 99.86 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 1.43 | 5.92 | 26.45 | 35.3 | 69.99 | 211 | 99.98 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 1.83 | 6.72 | 29.73 | 40.1 | 73.00 | 240 | 100.00 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 2.33 | 7.64 | 33.09 | 45.6 | 76.11 | 272 | 100.00 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 3.00 | 8.68 | 36.46 | 51.8 | 79.31 | 310 | 100.00 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 3.91 | 9.86 | 39.83 | 58.9 | 82.54 | 352 | 100.00 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 5.11 | 11.2 | 43.16 | 66.9 | 85.73 | 400 | 100.00 | 2390 | 100.00 |

Analysis

| | |
|---|--|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 20/09/2018 11:23:55 AM |
| Sample Name Average of 'CE491-31 (7E composite)' | Measurement Date Time 20/09/2018 11:23:55 AM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0089 % |
| Particle Refractive Index 1.555 | Span 4.087 |
| Particle Absorption Index 0.010 | Uniformity 1.286 |
| Dispersant Name Water | Specific Surface Area 1161 m ² /kg |
| Dispersant Refractive Index 1.330 | D [3,2] 5.17 μm |
| Scattering Model Mie | D [4,3] 27.4 μm |
| Analysis Model General Purpose | Dv (10) 2.00 μm |
| Weighted Residual 0.41 % | Dv (50) 16.5 μm |
| Laser Obscuration 12.35 % | Dv (90) 69.5 μm |



| Result | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under | Size (μm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 10.86 | 12.7 | 43.91 | 76.0 | 92.00 | 454 | 100.00 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.11 | 2.42 | 12.75 | 14.5 | 46.82 | 86.4 | 94.42 | 516 | 100.00 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.35 | 2.75 | 14.76 | 16.4 | 49.86 | 98.1 | 96.37 | 586 | 100.00 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.74 | 3.12 | 16.86 | 18.7 | 53.06 | 111 | 97.84 | 666 | 100.00 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 1.27 | 3.55 | 19.04 | 21.2 | 56.41 | 127 | 98.86 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 1.91 | 4.03 | 21.29 | 24.1 | 59.90 | 144 | 99.51 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 2.60 | 4.58 | 23.63 | 27.4 | 63.52 | 163 | 99.86 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 3.30 | 5.21 | 26.02 | 31.1 | 67.24 | 186 | 100.00 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 4.00 | 5.92 | 28.45 | 35.3 | 71.04 | 211 | 100.00 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 4.71 | 6.72 | 30.90 | 40.1 | 74.88 | 240 | 100.00 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 5.52 | 7.64 | 33.38 | 45.6 | 78.69 | 272 | 100.00 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 6.49 | 8.68 | 35.90 | 51.8 | 82.40 | 310 | 100.00 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 7.69 | 9.86 | 38.48 | 58.9 | 85.91 | 352 | 100.00 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 9.16 | 11.2 | 41.14 | 66.9 | 89.14 | 400 | 100.00 | 2390 | 100.00 |

Appendix D - Release of substances excavated rock materials in reservoir water [100 pages]

Appendix D1. Release of substances from <75 µm composite excavated rock materials in reservoir water at low L/S ratio

| | |
|------------------|--|
| Note/Memo | CSIRO P4 Project Investigations |
| To: | Ali Watters (HKA) |
| From: | Brad Angel, Lucas Heights, NSW |
| Date: | 28 September 2018 |
| Copy: | Ryan Fraser, Stuart Simpson and Ellen Porter (SHL) |
| Our reference: | CSIRO P4 – Memo 4 |
| Classification: | Internal use only |
| Subject: | Pollutant release from excavated rock composites |

Chemical formulas and acronyms

| | | | | | |
|-----------------|--------------------------|------------------------------|-------------------------|-------------------------------|--------------------|
| Ag | Silver | F ⁻ | Fluoride | Sb | Antimony |
| Al | Aluminium | Fe | Iron | Se | Selenium |
| As | Arsenic | Mg | Magnesium | Sn | Tin |
| Ba | Barium | Mn | Manganese | SO ₄ ²⁻ | Sulfate |
| Ca | Calcium | Mo | Molybdenum | Sr | Strontium |
| Cd | Cadmium | Na | Sodium | Th | Thorium |
| Cl ⁻ | Chloride | Ni | Nickel | U | Uranium |
| Co | Cobalt | NO ₃ ⁻ | Nitrate | V | Vanadium |
| Cr | Chromium | Pb | Lead | Zn | Zinc |
| Cu | Copper | | | | |
| DOC | Dissolved organic carbon | DGV | Default guideline value | L/S | Liquid/solid ratio |
| | | | | | |

Background - Introduction

The CSIRO was engaged by Haskoning Australia Pty Ltd (RHDHV) to undertake an investigation of the pollutant release from excavated rock disposal into Talbingo and Tantangara reservoirs. This phase of the work involved investigating the release of pollutants from composite excavated rock samples in an initial elutriate test that had a liquid to solid (L/S) ratio of 10/1 and was run for 48 h. With respect to placement scenarios for the excavated rock, these tests were intended to assess a worst case scenario for impacts to the receiving water. It is envisaged that the design of the excavated rock placement will result in fast deposition of the majority of the excavated rock, and concentrations of fine materials within the waters will be managed to achieve considerably lower concentrations of suspended solids. The vast majority of the excavated rock, by mass, will be larger than sand size and should settle rapidly. The scenario assessed here is to represent predominantly fine excavated rock materials remaining suspended in the waters in the main disposal area. Daily excavated rock-placement activities at the site may potentially result in this material being disturbed and remaining in suspension for considerably longer than would occur without disturbance. Consequently the bottom waters may contain very high concentration of suspended fine excavated rock material for days, allowing for prolonged release from those excavated rock materials.

Further tests will evaluate scenarios of pollutant release for excavated rock materials at much higher L/S ratios (e.g. 100/1, 1000/1) and the release occurring over shorter durations to represent the scenario of more rapid settling and release within waters beyond the main placement area (where some fine material may potentially disperse to).

This technical memo describes the preliminary results.

pH, conductivity and dissolved oxygen

The final pH, conductivity and dissolved oxygen concentrations of the elutriates from the 12 excavated rock composites in Talbingo water (composite of four waters) are shown in Table 1 (liquid/solid (L/S) ratio = 10, 48 h).

Table 1. The pH, conductivity and dissolved oxygen in 48 h elutriate test of excavated rock composites @ L/S=10.

| Sample ID | pH | Conductivity ($\mu\text{S}/\text{cm}$) | Dissolved oxygen (mg/L) |
|---|-------------|---|----------------------------|
| Talbingo water (composite), replicate 1 | 7.12 | 29.1 | 8.26 |
| Talbingo water, replicate 2 | 6.99 | 28.9 | 8.22 |
| Talbingo water, replicate 3 | 7.05 | 29.0 | 8.16 |
| Talbingo water, replicate 4 | 7.03 | 29.0 | 8.19 |
| 1B composite | 9.20 | 154 | 8.21 |
| 1B composite duplicate | 9.29 | 153 | 8.15 |
| 1B composite MEAN | 9.25 | 154 | 8.18 |
| 1E composite | 9.33 | 166 | 8.26 |
| 2B composite | 8.88 | 160 | 8.36 |
| 2E composite | 9.35 | 173 | 8.22 |
| 3B composite | 9.58 | 120 | 8.23 |
| 3E composite | 9.81 | 120 | 8.47 |
| 4B composite | 9.67 | 107 | 8.32 |
| 4E composite | 9.37 | 141 | 8.49 |
| 4E composite duplicate | 9.31 | 143 | 8.35 |
| 4E composite MEAN | 9.34 | 142 | 8.42 |
| 5B composite | 9.57 | 150 | 8.25 |
| 5E composite | 9.39 | 162 | 7.14 |
| 7B composite | 9.56 | 150 | 8.36 |
| 7E composite | 9.38 | 203 | 8.27 |

The pH, conductivity and dissolved oxygen concentrations were in the ranges 8.88-9.81, 107-203 $\mu\text{S}/\text{cm}$ and 7.14-8.49 mg/L. The pH and conductivity values were substantially higher than in the Talbingo composite water used in the tests (pH 7-7.1, 29 $\mu\text{S}/\text{cm}$), while the dissolved oxygen was not affected other than for the lower value measured for composite 5E.

The release of anions from excavated rock composites

The anions (mg/L), and total P and S (µg/L) released from excavated rock in elutriate test 1 is shown in Table 2. The concentrations of each parameter were all higher than the corresponding values in the Talbingo elutriate control water except for a few values for sulfate which were similar, and nitrate which was below the limit of detection.

Table 2. The anions, P and S released from excavated rock composites in elutriate test 1.^a

| Client I.D. | F ⁻ (mg/L) | Cl ⁻ (mg/L) | Br ⁻ (mg/L) | SO ₄ ²⁻ (mg/L) | P (µg/L) | S (µg/L) |
|----------------------------------|--------------------------|---------------------------|---------------------------|---|-------------|-------------|
| Talbingo water composite A | 0.015 | 0.92 | <0.5 | 0.44 | <4.4 | 156 |
| Talbingo water composite B | 0.025 | 0.94 | <0.5 | 0.49 | <4.4 | 154 |
| Talbingo water composite C | 0.03 | 0.93 | <0.5 | 0.46 | <4.4 | 156 |
| Talbingo water composite D | 0.02 | 0.93 | <0.5 | 0.53 | <4.4 | 161 |
| Initial elutriate 1B | 0.42 | 1.59 | <0.5 | 0.79 | 10.1 | 327 |
| Initial elutriate 1B duplicate | 0.42 | 1.60 | <0.5 | 0.75 | 9.5 | 320 |
| Initial elutriate 1B mean | 0.42 | 1.59 | <0.5 | 0.77 | 9.8 | 324 |
| Initial elutriate 1E | 0.47 | 2.53 | <0.5 | 3.40 | 5.7 | 1430 |
| Initial elutriate 2B | 0.45 | 1.95 | <0.5 | 0.96 | 38.9 | 452 |
| Initial elutriate 2E | 0.54 | 1.65 | <0.5 | 9.35 | 8 | 5780 |
| Initial elutriate 3B | 0.16 | 1.31 | <0.5 | 0.46 | <4.4 | 177 |
| Initial elutriate 3E | 0.60 | 1.34 | <0.5 | 0.52 | 6.2 | 180 |
| Initial elutriate 4B | 0.48 | 1.56 | <0.5 | 0.69 | 5 | 289 |
| Initial elutriate 4E | 0.14 | 2.15 | <0.5 | 5.14 | 6.6 | 3510 |
| Initial elutriate 4E duplicate | 0.16 | 2.12 | <0.5 | 5.08 | <4.4 | 3540 |
| Initial elutriate 4E mean | 0.15 | 2.13 | <0.5 | 5.11 | 5.5 | 3525 |
| Initial elutriate 5B | 0.32 | 2.41 | <0.5 | 1.27 | 38 | 752 |
| Initial elutriate 5E | 0.33 | 1.75 | <0.5 | 7.45 | 21 | 8510 |
| Initial elutriate 7B | 0.72 | 1.51 | <0.5 | 1.10 | 4.8 | 516 |
| Initial elutriate 7E | 0.53 | 1.94 | <0.5 | 11.5 | 5.1 | 4280 |
| Minimum rock composite | 0.14 | 1.31 | <0.5 | 0.46 | 4.8 | 177 |
| Maximum rock composite | 0.72 | 2.53 | <0.5 | 11.5 | 38.9 | 8510 |
| DGVB^b | | 3 | | | 10 | |

^a liquid/solid (L/S) ratio = 10, 48 h

^b <http://www.waterquality.gov.au/anz-guidelines/guideline-values/default/water-quality-toxicants/>. 95% species protection guideline values (95%GV) for freshwater. Values for Arsenic are for As(V), chromium are for Cr(VI), and tin are for inorganic tin

The release of metals, metalloids and major cations from composite excavated rock samples in an initial elutriate test

The metals, metalloids and major cations released from the composite rock composites in elutriate test 1 are shown in Tables 3-5. When compared to water quality guideline values (WQGVs), the main exceedances occurred for aluminium, arsenic and chromium, where the majority of composites exceeded the 95% or 99% species protection WQGVs. The 95% WQGV for aluminium was exceeded by the largest factor; over 14-fold higher. There were also six exceedances of the total phosphorous WQGV. The inorganic speciation of Al, As and Cr is influenced by anionic complexes at basic pH's and it is likely that higher dilutions (i.e. higher L/S ratios) and/or mixing durations effect solubility. These parameters will be investigated in future tests.

Table 3. The Al, Fe, Mn and major cations released into the dissolved phase from excavated rocks in test 1.^a

| Site code | Al (µg/L) | Fe (µg/L) | Mn (µg/L) | Na (µg/L) | K (µg/L) | Mg (µg/L) | Ca (µg/L) |
|----------------------------------|--------------|--------------|--------------|--------------|-------------|--------------|--------------|
| Talbingo water composite A | 4.5 | 16 | 0.25 | 1640 | 402 | 704 | 1700 |
| Talbingo water composite B | 4.4 | 15.8 | 0.25 | 1660 | 417 | 725 | 1760 |
| Talbingo water composite C | 4.7 | 16.7 | 0.24 | 1660 | 414 | 711 | 1760 |
| Talbingo water composite D | 4.9 | 16.7 | 0.28 | 1660 | 404 | 724 | 1730 |
| Initial elutriate 1B | 249 | <0.6 | 1.51 | 7680 | 20300 | 2090 | 5050 |
| Initial elutriate 1B duplicate | 252 | <0.6 | 1.51 | 7680 | 20200 | 2110 | 5030 |
| Initial elutriate 1B mean | 251 | <0.6 | 1.51 | 7680 | 20250 | 2100 | 5040 |
| Initial elutriate 1E | 286 | <0.6 | 2.96 | 6390 | 20700 | 2510 | 5610 |
| Initial elutriate 2B | 85.3 | <0.6 | 2.14 | 4930 | 13100 | 6360 | 6850 |
| Initial elutriate 2E | 274 | <0.6 | 1.58 | 4520 | 27800 | 1520 | 6750 |
| Initial elutriate 3B | 467 | 0.8 | 0.4 | 9290 | 8600 | 2590 | 4170 |
| Initial elutriate 3E | 783 | 2.4 | 0.46 | 9540 | 11100 | 1900 | 4640 |
| Initial elutriate 4B | 457 | <0.6 | 1.01 | 5930 | 10600 | 893 | 5300 |
| Initial elutriate 4E | 712 | 2.9 | 1.13 | 6620 | 15400 | 1500 | 7000 |
| Initial elutriate 4E duplicate | 719 | 2.9 | 1.17 | 6550 | 15400 | 1530 | 6960 |
| Initial elutriate 4E mean | 716 | 2.9 | 1.15 | 6585 | 15400 | 1515 | 6980 |
| Initial elutriate 5B | 304 | 1.6 | 0.86 | 9300 | 15500 | 1390 | 4620 |
| Initial elutriate 5E | 445 | 1.3 | 1.56 | 9470 | 11000 | 1960 | 8010 |
| Initial elutriate 7B | 343 | 0.7 | 3.2 | 9620 | 19900 | 617 | 4080 |
| Initial elutriate 7E | 149 | 1.2 | 0.68 | 6220 | 34500 | 917 | 4160 |
| MIN | 85 | 0.7 | 0.4 | 4520 | 8600 | 617 | 4080 |
| MAX | 783 | 2.93 | 3.2 | 9620 | 34500 | 6360 | 8010 |
| 95% DGV^b | 55 | 700 | 1900 | - | - | - | - |
| 99% DGV^c | 27 | 400 | 1200 | - | - | - | - |

^a liquid/solid (L/S) ratio = 10, 48 h. ^b <http://www.waterquality.gov.au/anz-guidelines/guideline-values/default/water-quality-toxicants/>.

95% species protection guideline values (95%GV) for freshwater. ^c 99% species protection guideline values (99%GV) for freshwater.

Values for iron are from the final draft revision document, and are not expected to change before release in 2018.

Table 4. The metals and metalloids released into the dissolved phase from excavated rocks in test 1.^a

| Site code | Ag (µg/L) | As (µg/L) | Ba (µg/L) | Cd (µg/L) | Co (µg/L) | Cr (µg/L) | Cu (µg/L) | Mo (µg/L) |
|----------------------------------|-----------------|----------------|--------------|-----------------|----------------|----------------|----------------|--------------|
| Talbingo water composite A | <0.36 | <0.5 | 4.0 | <0.07 | <1.4 | <0.4 | <1.1 | <1.5 |
| Talbingo water composite B | <0.36 | <0.5 | 4.0 | <0.07 | <1.4 | <0.4 | <1.1 | <1.5 |
| Talbingo water composite C | <0.36 | <0.5 | 4.1 | <0.07 | <1.4 | <0.4 | 1.2 | <1.5 |
| Talbingo water composite D | <0.36 | <0.5 | 4.1 | <0.07 | <1.4 | <0.4 | <1.1 | <1.5 |
| Initial elutriate 1B | <0.36 | 14.9 | 3.2 | <0.07 | <1.4 | 0.5 | <1.1 | <1.5 |
| Initial elutriate 1B duplicate | <0.36 | 14.8 | 3.3 | <0.07 | <1.4 | <0.4 | <1.1 | <1.5 |
| Initial elutriate 1B mean | <0.36 | 14.9 | 3.2 | <0.07 | <1.4 | <0.4 | <1.1 | <1.5 |
| Initial elutriate 1E | <0.36 | 17.4 | 16.6 | <0.07 | <1.4 | <0.4 | <1.1 | <1.5 |
| Initial elutriate 2B | <0.36 | 4.1 | 15.1 | <0.07 | <1.4 | 1.3 | <1.1 | 3.9 |
| Initial elutriate 2E | <0.36 | 8.5 | 9.2 | <0.07 | <1.4 | <0.4 | <1.1 | 2.0 |
| Initial elutriate 3B | <0.36 | <0.5 | 0.2 | <0.07 | <1.4 | 4.1 | <1.1 | <1.5 |
| Initial elutriate 3E | <0.36 | 1.1 | 0.2 | <0.07 | <1.4 | 2.9 | <1.1 | <1.5 |
| Initial elutriate 4B | <0.36 | 12.2 | 1.1 | <0.07 | <1.4 | <0.4 | <1.1 | <1.5 |
| Initial elutriate 4E | <0.36 | 10.8 | 1.9 | <0.07 | <1.4 | <0.4 | <1.1 | 2.5 |
| Initial elutriate 4E duplicate | <0.36 | 11.4 | 1.9 | <0.07 | <1.4 | <0.4 | <1.1 | 2.1 |
| Initial elutriate 4E mean | <0.36 | 11.1 | 1.9 | <0.07 | <1.4 | <0.4 | <1.1 | 2.3 |
| Initial elutriate 5B | <0.36 | 13.4 | 3.8 | <0.07 | <1.4 | <0.4 | <1.1 | 14.5 |
| Initial elutriate 5E | <0.36 | 2.8 | 5.8 | <0.07 | <1.4 | <0.4 | <1.1 | 1.7 |
| Initial elutriate 7B | <0.36 | 5.8 | 6.0 | <0.07 | <1.4 | <0.4 | <1.1 | <1.5 |
| Initial elutriate 7E | <0.36 | 25.2 | 166 | <0.07 | <1.4 | <0.4 | <1.1 | 1.7 |
| MIN | <0.36 | <0.5 | 0.2 | <0.07 | <1.4 | <0.4 | <1.1 | 1.7 |
| MAX | <0.36 | 25.2 | 166 | <0.07 | <1.4 | 4.30 | <1.1 | 14.5 |
| 95% DGV^b | 0.05 | 13 | - | 0.2 | - | 0.4 | 1.4 | - |
| 99% DGV^c | 0.02 | 0.8 | - | 0.06 | - | 0.01 | 1.0 | - |

^a liquid/solid (L/S) ratio = 10, 48 h. ^b <http://www.waterquality.gov.au/anz-guidelines/guideline-values/default/water-quality-toxicants/>. 95% species protection guideline values (95%GV) for freshwater. ^c 99% species protection guideline values (99%GV) for freshwater. Values for Arsenic are for As(V) and chromium are for Cr(VI).

Table 5. The metals and metalloids released into the dissolved phase from excavated rocks in test 1.^a

| Site code | Ni (µg/L) | Pb (µg/L) | Sb (µg/L) | Sn (µg/L) | Sr (µg/L) | V (µg/L) | Zn (µg/L) |
|----------------------------------|-----------------|------------------|---------------|----------------|--------------|-------------|----------------|
| Talbingo water composite | <0.37 | 2.3 | <50 | <1.1 | 18 | <0.3 | 1.0 |
| Talbingo water composite | <0.37 | 5.2 | <50 | <1.1 | 18 | <0.3 | 0.9 |
| Talbingo water composite | <0.37 | 2.8 | <50 | <1.1 | 18 | <0.3 | 1.2 |
| Talbingo water composite | <0.37 | 3.3 | <50 | <1.1 | 18 | <0.3 | <0.9 |
| Initial elutriate 1B | <0.37 | <2.3 | 70 | <1.1 | 58 | 14.0 | <0.9 |
| Initial elutriate 1B duplicate | <0.37 | <2.3 | <50 | <1.1 | 57 | 13.8 | <0.9 |
| Initial elutriate 1B mean | <0.37 | <2.3 | ~60 | <1.1 | 57 | 13.9 | <0.9 |
| Initial elutriate 1E | <0.37 | 3.8 | <50 | <1.1 | 82 | 5.0 | <0.9 |
| Initial elutriate 2B | <0.37 | 6 | <50 | <1.1 | 33 | 5.9 | <0.9 |
| Initial elutriate 2E | <0.37 | 3.5 | <50 | <1.1 | 41 | 8.1 | <0.9 |
| Initial elutriate 3B | <0.37 | 4.7 | <50 | <1.1 | 6.3 | 8.2 | <0.9 |
| Initial elutriate 3E | <0.37 | <2.3 | <50 | <1.1 | 12 | 5.3 | <0.9 |
| Initial elutriate 4B | <0.37 | 4.5 | <50 | <1.1 | 24 | 4.8 | <0.9 |
| Initial elutriate 4E | <0.37 | <2.3 | <50 | <1.1 | 30 | 8.3 | <0.9 |
| Initial elutriate 4E duplicate | <0.37 | <2.3 | <50 | <1.1 | 30 | 8.5 | <0.9 |
| Initial elutriate 4E mean | <0.37 | <2.3 | <50 | <1.1 | 30 | 8.4 | <0.9 |
| Initial elutriate 5B | <0.37 | 3.5 | <50 | <1.1 | 23 | 12.2 | <0.9 |
| Initial elutriate 5E | <0.37 | <2.3 | <50 | <1.1 | 31 | 5.8 | <0.9 |
| Initial elutriate 7B | <0.37 | 4.5 | <50 | <1.1 | 52 | 18.4 | <0.9 |
| Initial elutriate 7E | <0.37 | 3.2 | <50 | <1.1 | 58 | 14.0 | <0.9 |
| MIN | <0.37 | <0.2.3 | <50 | <1.1 | 6 | 4.8 | <0.9 |
| MAX | <0.37 | 6 | 70 | <1.1 | 82 | 18.4 | <0.9 |
| 95% DGV^b | 11 | 3.4 | - | - | - | - | 8.0 |
| 99% DGV^c | 8 | 1.0 | - | - | - | - | 2.4 |

^a liquid/solid (L/S) ratio = 10, 48 h. ^b <http://www.waterquality.gov.au/anz-guidelines/guideline-values/default/water-quality-toxicants/>. 95% species protection guideline values (95%GV) for freshwater. ^c .99% species protection guideline values (99%GV) for freshwater. Value for tin is for inorganic tin.

Summary

The elutriate test with a solid to liquid (L/S) ratio of 10 undertaken to maintain the resuspension of materials for a duration of 48 h resulted in an increase in the pH of 2-2.8 pH units, and a 3-7-fold increase in the conductivity above that in the Talbingo control water.

The chloride, fluoride, sulfate, total phosphorous and sulfur increased relative to the control water, with the total phosphorous being the only parameter that increased above the 95% species protection water quality guideline value (WQGV).

Most of the metals, metalloids and major cations in the excavated rock elutriates increased relative to the control Talbingo water. The arsenic, chromium and, in particular, the aluminium increased above the DGVs.

As described in the introduction, this initial test was performed to assess what we consider to be a worst case scenario for fine excavated rock material remaining in the water column. The tests indicate that under such conditions the pH of the waters may increase to levels that result in high concentration of dissolved aluminium within the waters. These waters would be predicted to cause toxicity to a range of aquatic organisms.

Tests now underway (to be reported in future Memos) are evaluating scenarios of pollutant release for excavated rock materials at much higher L/S ratios (e.g. 100/1, 1000/1) and the release occurring over shorter durations to represent the scenario of more rapid settling and release within waters beyond the main placement area (where some fine material may potentially disperse to).

Successive leaching tests will be used to provide information on substance release from excavated rock materials transported within the water column.

Leach tests on composite materials of large particle sizes will provide information on how leaching from those materials compares to the fine solids.

Appendix D1. Release of substances from <75 µm composite excavated rock materials in reservoir water at low L/S ratio
Memo 4 (28 September 2018) (Appendix D1).

Combination of ICP-MS and AES data. Not all data available when original (initial) Memo provided to HKA/SHL.

Notes

Composite Talbingo reservoir water used as leachate solution

L/S of 10/1 tested i.e. 5 g solid and 50 mL Talbingo composite solution

QA/QC.

| Sample Labels | Treatment | Al (µg/L) | Fe (µg/L) | Mn (µg/L) | | Na (µg/L) | K (µg/L) | Mg (µg/L) | Ca (µg/L) | | P (µg/L) | S (µg/L) |
|---------------------|-----------------------|--------------|--------------|--------------|--|--------------|-------------|--------------|--------------|--|-------------|-------------|
| LOD (3 x 5.d.) | | 0.2 | 0.1 | 0.01 | | 15.0 | 15.9 | 42.6 | 20 | | 5 | 10 |
| TM24.4 | | 34.5 | 16.3 | 8.51 | | --- | --- | --- | --- | | --- | --- |
| Certified TM24.4 | | 32.9 ± 4.5 | 16.0 ± 2.3 | 8.24 ± 0.73 | | --- | --- | --- | --- | | --- | --- |
| % recovery (TM24.4) | | 105 | 102 | 103 | | --- | --- | --- | --- | | --- | --- |
| CE491-21+spike | 10/1 L/S composite 1E | 103 | - | - | | 112 | 129 | 106 | 111 | | - | - |
| CE491-37+spike | Initial elutriate 3B | - | 99 | 100 | | - | - | - | - | | - | - |
| CE491-38+spike | 10/1 L/S composite 3E | - | - | - | | - | - | - | - | | 96 | 89 |
| CE491-39+spike | 10/1 L/S composite 4B | - | - | - | | - | - | - | - | | 100 | 94 |
| CE491-40+spike | Initial elutriate 4E | - | 103 | 103 | | - | - | - | - | | - | - |
| CE491-31+spike | 10/1 L/S composite 7E | 104 | - | - | | 109 | 113 | 104 | 109 | | - | - |

QA/QC.

| Sample Labels | Treatment | Ag (µg/L) | As (µg/L) | B (µg/L) | Ba (µg/L) | Be (µg/L) | Cd (µg/L) | Ce (µg/L) | Co (µg/L) | Cr (µg/L) | Cu (µg/L) | Li (µg/L) | Mo (µg/L) | Ni (µg/L) | Pb (µg/L) | Sb (µg/L) | Se (µg/L) | Sn (µg/L) | Sr (µg/L) | Th (µg/L) | Ti (µg/L) | Ti (µg/L) | U (µg/L) | V (µg/L) | Zn (µg/L) |
|---------------------|-----------------------|--------------|--------------|-------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|-------------|-------------|--------------|
| LOD (3 x 5.d.) | | 0.004 | 0.01 | 0.664 | 0.003 | 0.004 | 0.004 | 0.42 | 0.01 | 0.04 | 0.02 | 0.01 | 0.02 | 0.01 | 0.01 | 0.02 | 0.01 | 0.02 | 0.03 | 0.004 | 0.037 | 0.01 | 0.003 | 0.01 | 0.1 |
| TM24.4 | | 8.74 | 5.16 | 10.2 | 15.3 | 1.98 | 3.97 | <0.42 | 6.46 | 5.00 | 6.40 | 4.82 | 6.48 | 4.93 | 5.51 | 3.47 | 3.43 | 3.52 | 114 | 0.21 | 7.5 | 5.31 | 4.91 | 7.11 | 26.2 |
| Certified TM24.4 | | --- | 5.30 ± 0.53 | --- | 15.0 ± 1.0 | 2.06 ± 0.24 | 3.96 ± 0.34 | --- | 6.27 ± 0.57 | 5.00 ± 0.59 | 6.31 ± 0.60 | 4.95 ± 0.42 | 6.30 ± 0.56 | 5.03 ± 0.53 | 5.60 ± 0.52 | --- | 3.56 ± 0.58 | 3.72 ± 0.39 | 113 ± 8 | --- | --- | --- | 4.20 ± 0.34 | 4.24 ± 0.34 | 7.00 ± 0.58 |
| % recovery (TM24.4) | | --- | 97 | --- | 102 | 96 | 100 | --- | 103 | 100 | 101 | 97 | 103 | 98 | 98 | --- | 96 | 94 | 101 | --- | --- | 126 | 116 | 102 | --- |
| CE491-21+spike | 10/1 L/S composite 1E | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 98 | - | - | - |
| CE491-37+spike | Initial elutriate 3B | 93 | 97 | - | 103 | 100 | 94 | - | 103 | 105 | 101 | 99 | 100 | 100 | 97 | 101 | 95 | 98 | 106 | 128 | - | 117 | 107 | 108 | 96 |
| CE491-38+spike | 10/1 L/S composite 3E | 99 | - | 95 | - | - | - | 99 | - | - | - | - | - | - | - | - | - | - | - | - | 103 | - | - | - | - |
| CE491-39+spike | 10/1 L/S composite 4B | 99 | - | 98 | - | - | - | 101 | - | - | - | - | - | - | - | - | - | - | - | - | 106 | - | - | - | - |
| CE491-40+spike | Initial elutriate 4E | 72 | 98 | - | 100 | 89 | 97 | - | 100 | 98 | 98 | 90 | 102 | 97 | 93 | 97 | 95 | 90 | 104 | 135 | - | 111 | 109 | 103 | 97 |
| CE491-31+spike | 10/1 L/S composite 7E | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 103 | - | - | - |

Appendix D2. Effect of L/S ratio on substance release from <75 µm composite rock materials

| | |
|------------------|--|
| Note/Memo | CSIRO P4 Project Investigations |
| To: | Ali Watters (HKA) |
| From: | Brad Angel, Lucas Heights, NSW |
| Date: | 9 November 2018 |
| Copy: | Ryan Fraser, Stuart Simpson and Ellen Porter (SHL) |
| Our reference: | CSIRO P4 – Memo 11 |
| Classification: | Internal use only |
| Subject: | Pollutant release from excavated rock composites: effect of L/S and kinetics |

Chemical formulas and acronyms

| | | | | | |
|-----|--------------|-----|-------------------------|-----|--------------------|
| Al | Aluminium | DGV | Default guideline value | L/S | Liquid/solid ratio |
| SEC | Conductivity | | | | |

Background - Introduction

The CSIRO was engaged by Haskoning Australia Pty Ltd (RHDHV) to undertake an investigation of the pollutant release from excavated rock disposal into Talbingo and Tantangara reservoirs. Previous elutriate tests (Memo 4, 5, 6) investigating the release of pollutants from composite excavated rock samples have observed significant changes in water quality with respect to pH, conductivity (SEC) and the dissolved aluminium concentrations. The results in memo 5 for composite 4E detailed how the water quality is affected by the liquid to solid (L/S) ratio and duration of contact between the composite material and reservoir water.

This technical memo describes results of elutriate tests performed on excavated rock composites 1B, 2B, 5B, 5E and 7E investigating the effect of liquid- to-solid (L/S) ratio and duration of contact with Talbingo reservoir water on pH, conductivity (SEC), and the dissolved aluminium concentration. The tests were performed using the following conditions:

- L/S = 30, 300, 1000, 3000
 - [being 33, 3.3, 1 and 0.33 g/L, respectively]
- Measurements at times of 0.5, 3, 18 and 120 h
- Solids mixed in composite Talbingo control water for 0.5 h then allowed to stand for durations tested
- Tests performed at 21±2°C

Results

The pH, conductivity and dissolved aluminium concentrations measured in the elutriate solutions for all composites combined for each L/S ratio over time are shown in Figure 1. Figures 2, 3, 4, 5 and 6 show the pH, conductivity and dissolved aluminium concentrations for the individual composites 1B, 2B, 5B, 5E and 7E, respectively. There were generally higher pH, conductivity and concentrations of dissolved aluminium at each time as the L/S ratio increased.

The pH was in the range 8.76-9.67, 9.07-9.49, 8.15-9.18, 7.00-7.87 for the 30:1 (33 g/L), 300:1 (3.3 g/L), 1000:1 (1 g/L) and 3000:1 (0.33 g/L) L/S ratios, respectively.

The conductivity was in the range 78.9-133, 49.6-76.0, 52.2-81.7, 29.3-56.9 $\mu\text{S}/\text{cm}$ for the 30:1 (33 g/L), 300:1 (3.3 g/L), 1000:1 (1 g/L) and 3000:1 (0.33 g/L) L/S ratios, respectively.

The dissolved aluminium concentrations were in the range 30.4-439, 26.6-445, 14.6-134, 6.5-28.9 $\mu\text{g}/\text{L}$ for the 30:1 (33 g/L), 300:1 (3.3 g/L), 1000:1 (1 g/L) and 3000:1 (0.33 g/L) L/S ratios, respectively.

The initial contact of the solids with the water resulted in a rapid increase in pH and conductivity. The pH generally decreased marginally over the duration of the tests while the conductivity marginally increased. The pH was nearly always higher for a lower L/S ratio at any given time point, whereas, for the conductivity, this relationship was not quite as clear, with similar values often observed for the 300 and 1000 L/S ratios.

The dissolved aluminium increased over the duration of the tests, with the degree of increase generally being higher for lower L/S ratios. For all composite samples tested, the dissolved aluminium exceeded the default guideline value (DVG) of 55 $\mu\text{g}/\text{L}$ after 3 h for the 30 and 300 L/S ratios, and exceeded the DGV after 18 h (3 h not tested) for the 1000 L/S ratio. The aluminium DGV was not exceeded for any composites at the 3000 L/S ratio.

Summary

The kinetics of the changes in pH, conductivity and the dissolved aluminium concentrations indicate increased dissolution of rock solids occur with time. For aluminium the increase with time is consistent with the high pH acting to increase dissolution through formation of the highly soluble aluminate ion, $\text{Al}(\text{OH})_4^-$.

The aluminium DGV was exceeded for L/S ratios ≤ 1000 (i.e. ≥ 1 g/L) after composite durations of ≤ 18 h in Talbingo reservoir water.

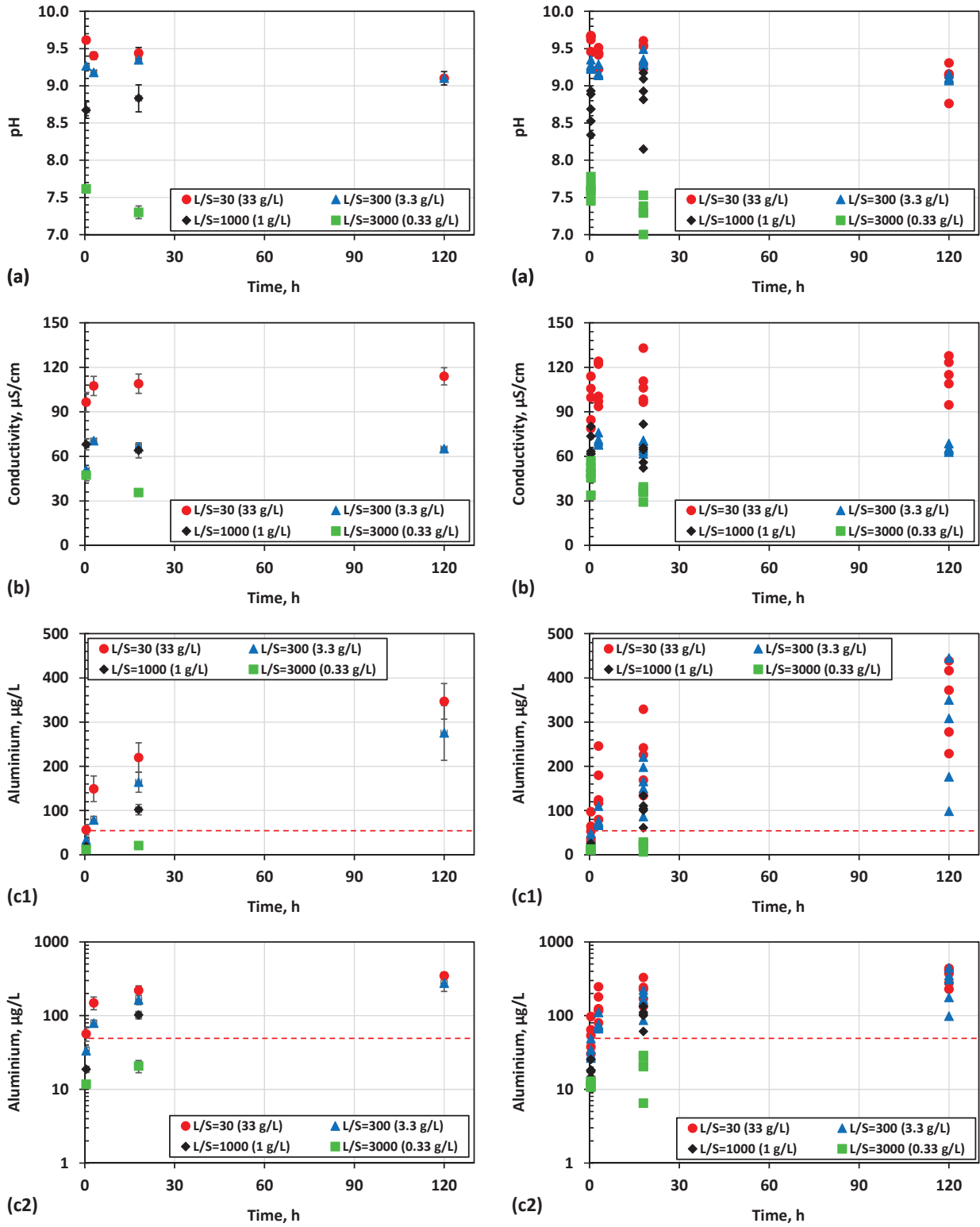


Figure 1. The pH, conductivity and dissolved aluminium concentration after elutriate times of 0.5, 3, 18 and 120 h for all excavated rock composite samples at liquid to solid ratios (L/S) of 30, 300, 1000 and 3000 (c2 = log scale). The figures on the left show the mean values (error bars are standard errors), and the figures on the right show the values measured for each composite materials at each duration.

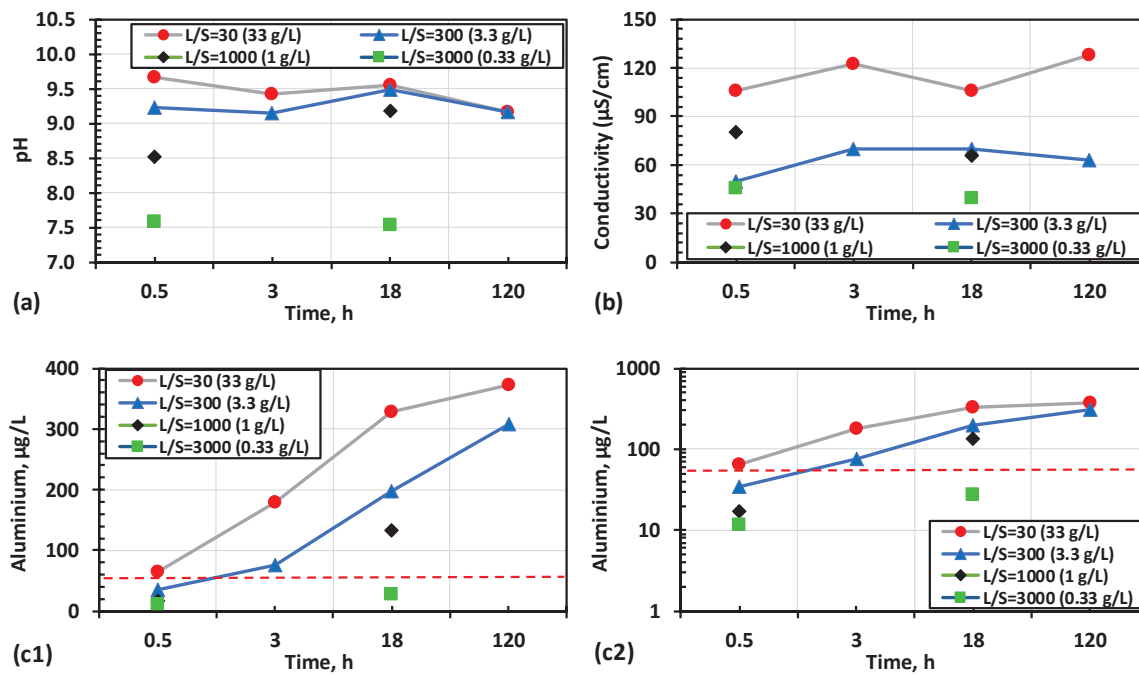


Figure 2. The pH, conductivity and dissolved aluminium concentration of composite 1B elutriate tests after times of 0.5, 3, 18 and 120 h for liquid to solid ratios (L/S) of 30, 300, 1000 and 3000 (c2 = log scale).

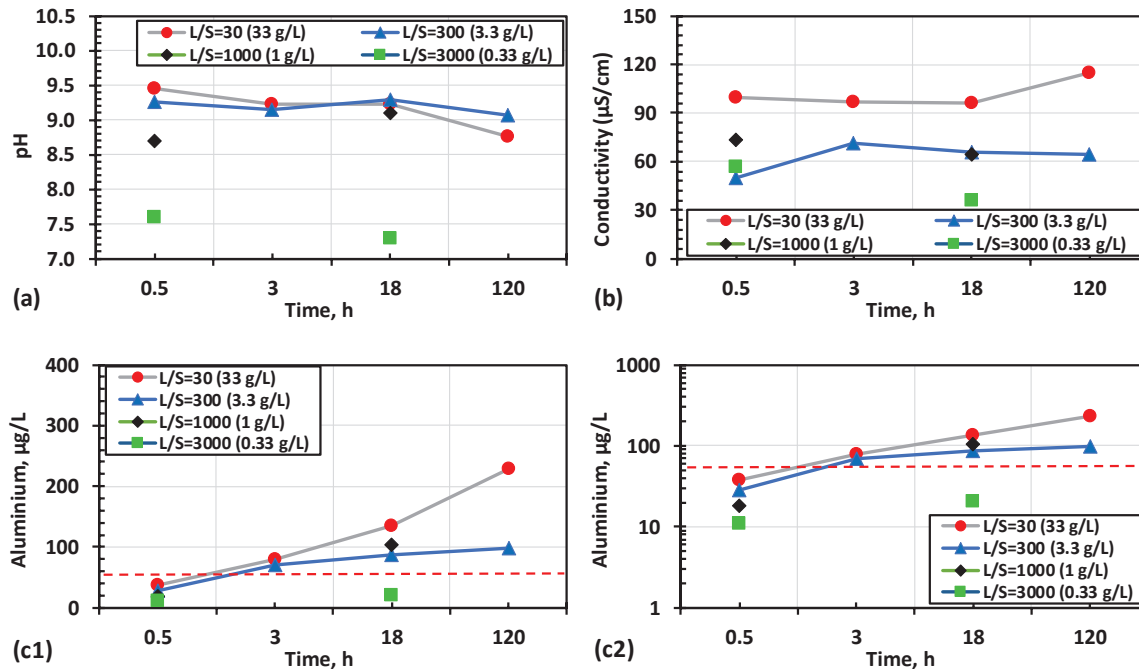


Figure 3. The pH, conductivity and dissolved aluminium concentration of composite 2B elutriate tests after times of 0.5, 3, 18 and 120 h for liquid to solid ratios (L/S) of 30, 300, 1000 and 3000 (c2 = log scale).

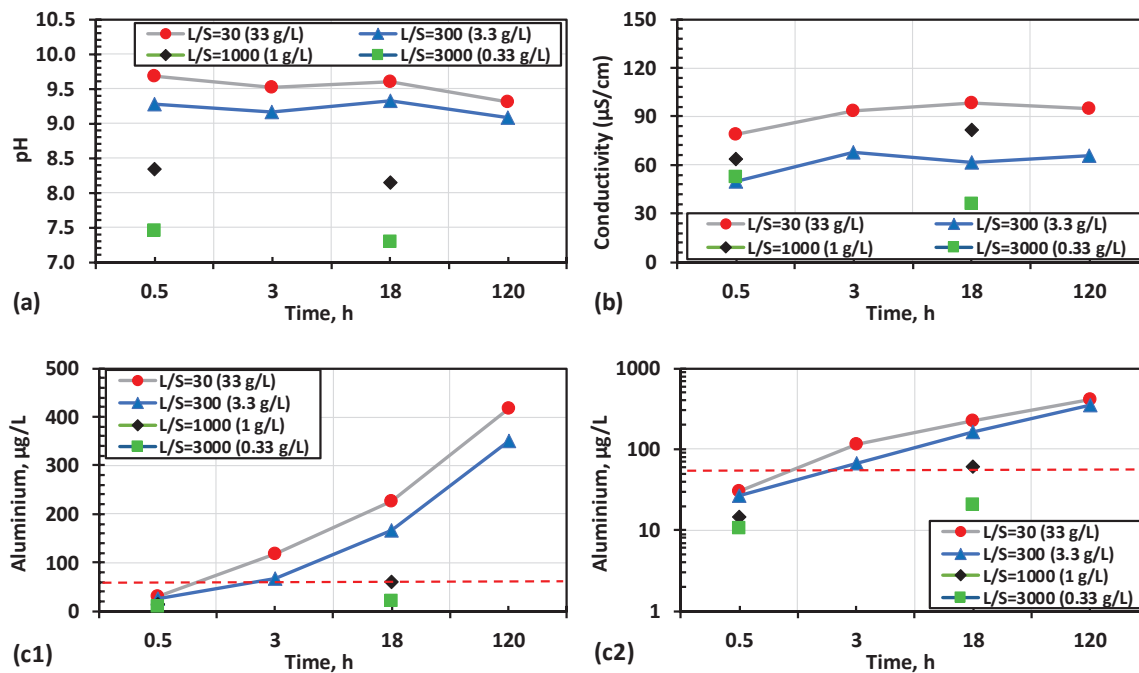


Figure 4. The pH, conductivity and dissolved aluminium concentration of composite 5B elutriate tests after times of 0.5, 3, 18 and 120 h for liquid to solid ratios (L/S) of 30, 300, 1000 and 3000 (c2 = log scale).

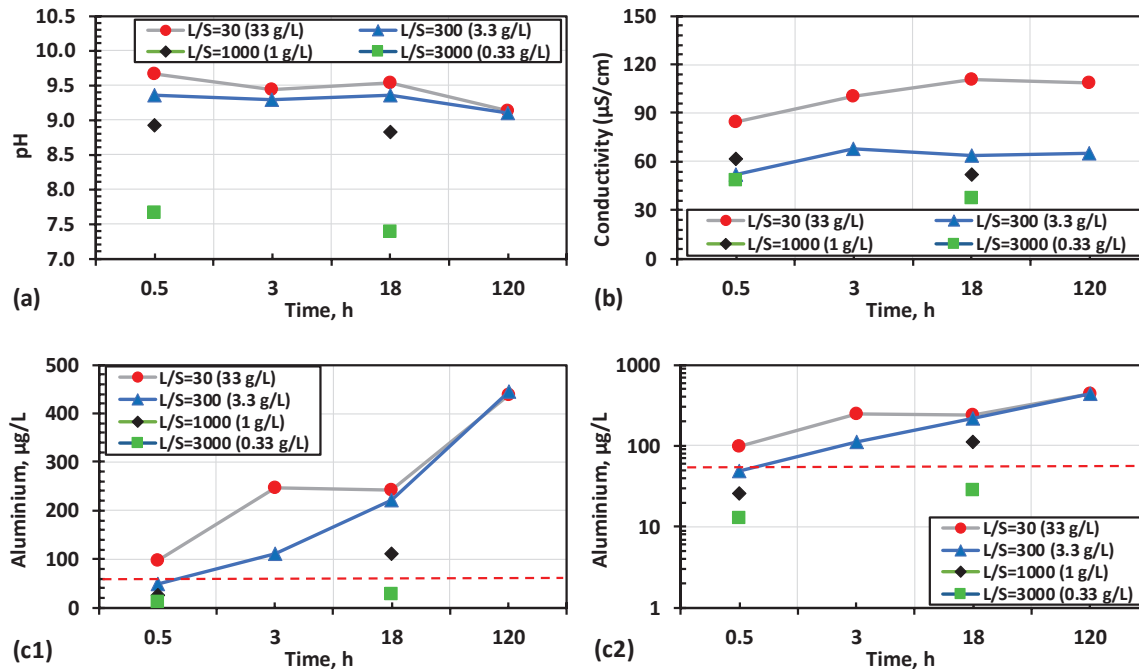


Figure 5. The pH, conductivity and dissolved aluminium concentration of composite 5E elutriate tests after times of 0.5, 3, 18 and 120 h for liquid to solid ratios (L/S) of 30, 300, 1000 and 3000 (c2 = log scale).

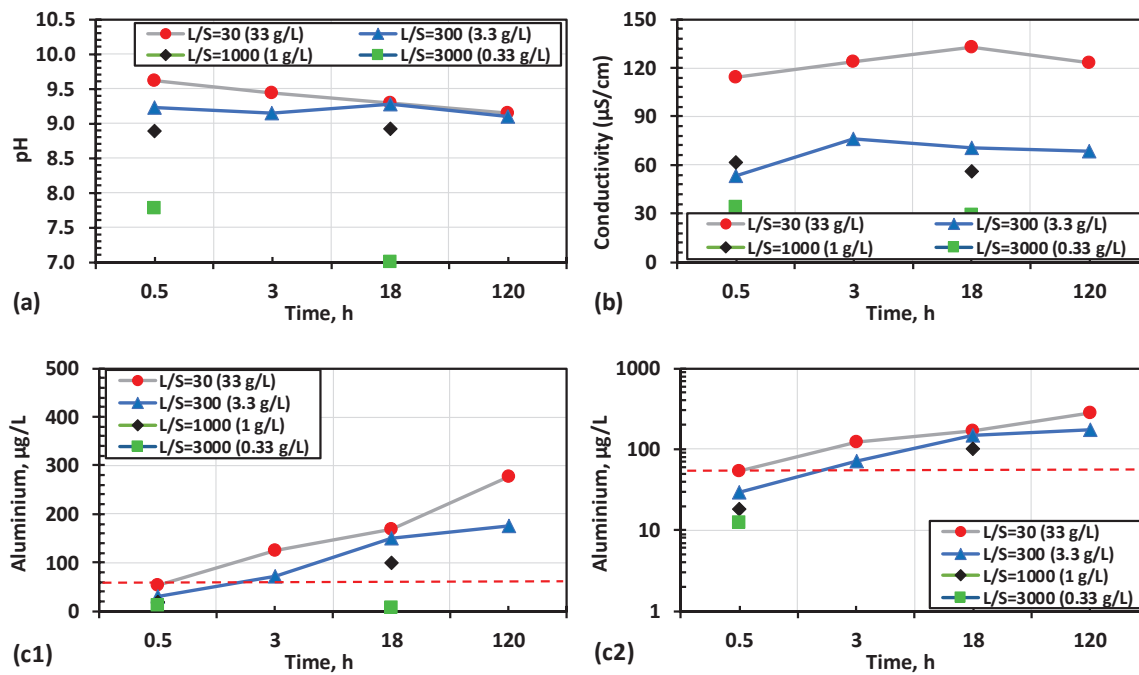


Figure 6. The pH, conductivity and dissolved aluminium concentration of composite 7E elutriate tests after times of 0.5, 3, 18 and 120 h for liquid to solid ratios (L/S) of 30, 300, 1000 and 3000 (c2 = log scale).

Samples re-analysed without dilution to provide different level of detection/reporting. New data for P (phosphorous) S (sulfur) and Si (silicon)

| Sample Labels | Sample name | L/S ratio | Duration (h) | P (µg/L) | S (µg/L) | Si (µg/L) | Ag (µg/L) | Al (µg/L) | As (µg/L) | B (µg/L) | Ba (µg/L) | Be (µg/L) | Ca (µg/L) | Cd (µg/L) | Ce (µg/L) | Co (µg/L) | Cr (µg/L) | Cu (µg/L) | Fe (µg/L) | K (µg/L) | Li (µg/L) | Mg (µg/L) | Mn (µg/L) | Mo (µg/L) | Na (µg/L) | Ni (µg/L) | P (µg/L) | Pb (µg/L) | S (µg/L) | Sn (µg/L) | Sr (µg/L) | Ti (µg/L) | V (µg/L) | Zn (µg/L) | | |
|---------------------|-------------|-----------|--------------|----------|----------|-----------|---------------|-----------|-----------|----------|-----------|-----------|-----------|-----------|---------------|---------------|-----------|-----------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|-----------|----------|-----------|-----------|-----------|----------|-----------|------|--|
| Mean blank | | | | 2.1 | 3.1 | -1.8 | 0.0 | 0.0 | -1.2 | -1.3 | 0.0 | 0.0 | -4.6 | 0.0 | 0.6 | -0.7 | 0.0 | 0.3 | -0.1 | 0.7 | -0.1 | -1 | 0.0 | 0.0 | 0.0 | -3 | -0.1 | 2.1 | -0.1 | 3.1 | 0.0 | 0.0 | 0.0 | -0.1 | -0.6 | |
| LOD (3 x S.d.) | | | | 3.4 | 8.1 | 1.2 | 0.5 | 0.1 | 0.6 | 0.7 | 0.0 | 0.0 | 0.2 | 0.1 | 1.2 | 1.3 | 0.0 | 0.6 | 0.2 | 0.8 | 0.1 | 4 | 0.0 | 0.3 | 0 | 0.6 | 3.4 | 1.3 | 8 | 0.4 | 0.0 | 0.0 | 0.2 | 0.2 | 0.2 | |
| Mean blank | | | | 3.7 | -6.2 | -4.2 | 0.1 | 0.3 | -0.1 | -3.4 | 0.0 | 0.0 | -2 | 0.0 | 1.3 | 0.0 | 0.0 | -0.4 | 0.0 | 0.3 | -0.1 | -1 | 0.0 | 0.0 | -1 | -0.2 | 3.7 | -0.2 | -6 | 0.4 | 0.0 | 0.0 | 0.0 | -0.2 | -0.2 | |
| LOD (3 x S.d.) | | | | 4.7 | 8.9 | 0.2 | 0.5 | 0.2 | 0.6 | 0.9 | 0.0 | 0.0 | 1 | 0.1 | 4.1 | 1.3 | 0.2 | 1.4 | 0.3 | 0.7 | 0.3 | 1 | 0.0 | 0.1 | 0 | 0.4 | 4.7 | 0.1 | 9 | 1.6 | 0.0 | 0.0 | 0.3 | 0.1 | 0.1 | |
| TM24-4 | | | | -2 | 5802 | 352 | 9 | 33 | 6 | 16 | 15 | 2 | | 4 | -1 | 7 | 5 | 7 | 16 | 1123 | 0 | 5409 | 8 | 6 | 9298 | 5 | -2 | 7 | 5802 | 4 | 115 | 7 | 7 | 29 | | |
| Certified TM24.4 | | | | | | | 32.9 ± 5.30 ± | | | | 15.0 ± | | | 3.96 ± | 6.27 ± 5.00 ± | 6.31 ± 16.0 ± | | | | 4.95 ± | | | | | | 5.03 ± | | 5.60 ± | | 113 ± | | 7.00 ± | | | | |
| % recovery (TM24.4) | | | | | | | 8.92 | 4.5 | 0.53 | | 1.0 | | | 0.34 | 0.57 | 0.59 | 0.60 | 2.3 | | 0.42 | | | | | | 0.53 | | 0.52 | | 8 | | 0.58 | | | | |
| | | | | 102 | 101 | 113 | | | | | 97 | | | 102 | 111 | 104 | 110 | 98 | | 4 | | | | | | 103 | | 116 | | 101 | | 102 | | | | |
| TM24-64.3 | | | | 3 | 5701 | 376 | 12 | 298 | 160 | 277 | 275 | 161 | | 269 | 241 | 292 | 263 | 297 | 1169 | 126 | 5404 | 295 | 285 | 9538 | 262 | 3 | 286 | 5701 | 278 | 671 | 129 | 285 | 327 | | | |
| Certified TM63.4 | | | | | | | 12.6 ± 291 ± | 164 ± | | | 287 ± | | | 258 ± | 250 ± 283 ± | 261 ± 298 ± | | | | 143 ± | | | | | | 252 ± | | 280 ± | | 628 ± | | 279 ± | 320 ± | | | |
| % recovery (TM24.4) | | | | | | | 99 | 102 | 97 | | 96 | | | 104 | 96 | 103 | 101 | 100 | | 88 | | | | | | 104 | | 102 | | 107 | | 102 | | 102 | 102 | |
| TM24-4 | | | | 0.6 | 5864 | 351 | 8.9 | 32.7 | 4.5 | 16 | 15 | 2.2 | | 4.2 | 1.3 | 7.0 | 5.1 | 7.2 | 162 | 1113 | 0.3 | 5408 | 8.2 | 6.0 | 9044 | 5.3 | 0.6 | 5.7 | 5864 | 3.6 | 115 | 7.4 | 7.2 | 29 | | |
| Certified TM24.4 | | | | | | | 32.9 ± 5.30 ± | | | | 15.0 ± | | | 3.96 ± | 6.27 ± 5.00 ± | 6.31 ± 16.0 ± | | | | 4.95 ± | | | | | | 5.03 ± | | 5.60 ± | | 113 ± | | 7.00 ± | | | | |
| % recovery (TM24.4) | | | | | | | 8.92 | 4.5 | 0.53 | | 1.0 | | | 0.34 | 0.57 | 0.59 | 0.60 | 2.3 | | 0.42 | | | | | | 0.53 | | 0.52 | | 8 | | 0.58 | | | | |
| | | | | 100 | 100 | 84 | | | | | 97 | | | 105 | 111 | 103 | 114 | 102 | | 6 | | | | | | 105 | | 101 | | 102 | | 102 | | 103 | | |
| TM24-64.3 | | | | -1.6 | 5741 | 375 | 12.3 | 293 | 160 | 281 | 275 | 165 | | 267 | 257 | 288 | 264 | 299 | 1180 | 127 | 5396 | 290 | 285 | 9241 | 261 | -1.6 | 286 | 5741 | 278 | 670 | 131 | 286 | 329 | | | |
| Certified TM63.4 | | | | | | | 12.6 ± 291 ± | 164 ± | | | 287 ± | | | 258 ± | 250 ± 283 ± | 261 ± 298 ± | | | | 143 ± | | | | | | 252 ± | | 280 ± | | 628 ± | | 279 ± | 320 ± | | | |
| % recovery (TM24.4) | | | | | | | 1.3 | 23 | 15 | | 18 | | | 21 | 16 | 17 | 18 | 21 | | 15 | | | | | 18 | | 22 | | 34 | | 18 | 23 | | | | |
| | | | | 98 | 101 | 98 | | | | | 96 | | | 104 | 103 | 102 | 101 | 100 | | 89 | | | | | | 103 | | 102 | | 107 | | 103 | 103 | 103 | | |
| T5-10 + Spike | | | | 97 | 93 | | 97 | 96 | 97 | 97 | 96 | 96 | | 95 | 97 | 93 | 96 | 98 | 96 | 101 | 92 | 84 | 95 | 99 | 95 | 96 | 97 | 95 | 93 | 100 | 96 | 97 | 97 | 95 | | |
| T5-20 + Spike | | | | 95 | 94 | | 96 | 95 | 97 | 98 | 96 | 95 | | 95 | 97 | 95 | 96 | 98 | 96 | 99 | 93 | 82 | 95 | 99 | 96 | 96 | 95 | 95 | 94 | 99 | 96 | 97 | 97 | 95 | | |
| T3-10 + Spike | | | | 97 | 74 | | 95 | 91 | 97 | 97 | 95 | 96 | | 94 | 94 | 94 | 96 | 97 | 95 | 97 | 90 | 77 | 95 | 98 | 81 | 94 | 97 | 94 | 74 | 99 | 95 | 97 | 97 | 95 | | |
| T3-20 + Spike | | | | 100 | 92 | | 97 | 96 | 99 | 97 | 96 | 99 | | 99 | 98 | 97 | 98 | 98 | 97 | 60 | 94 | 59 | 97 | 98 | 99 | 96 | 100 | 95 | 92 | 98 | 97 | 99 | 99 | 97 | | |
| T3-30 + Spike | | | | 100 | 92 | | 99 | ? | 99 | 97 | 97 | 100 | | 98 | 99 | 96 | 98 | 99 | 98 | 90 | 95 | 86 | 98 | 99 | 96 | 98 | 100 | 98 | 92 | 99 | 98 | 99 | 99 | 98 | | |
| T3-40 + Spike | | | | 99 | 95 | | 98 | 97 | 99 | 97 | 98 | 100 | | 99 | 99 | 98 | 99 | 99 | 98 | 101 | 96 | 87 | 99 | 100 | 96 | 98 | 99 | 97 | 95 | 99 | 98 | 99 | 100 | 99 | | |

QUALITY CONTROL SUMMARY of Test 11: Investigation of Kelly's Plains L/S and kinetics effects of metal release and water quality

| Sample Labels | Rock Spoil sample | L/S ratio | Mixing duration | Duration in water | Na (mg/L) | K (mg/L) | Mg (mg/L) | Ca (mg/L) | Ag (µg/L) | Al (µg/L) | As (µg/L) | B (µg/L) | Ba (µg/L) | Be (µg/L) | Cd (µg/L) | Ce (µg/L) | Co (µg/L) | Cr (µg/L) | Cu (µg/L) | Fe (µg/L) | Li (µg/L) | Mn (µg/L) | Mo (µg/L) | Ni (µg/L) | P (µg/L) | Pb (µg/L) | S (µg/L) | Sn (µg/L) | Sr (µg/L) | Ti (µg/L) | Ti (µg/L) | V (µg/L) | Zn (µg/L) | |
|------------------------|-------------------|-----------|-----------------|-------------------|-----------|----------|-----------|-----------|-----------|-----------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|-----------|----------|-----------|-----------|-----------|-----------|----------|-----------|-----|
| Mean blank | | | | | -0.02 | -0.03 | 0.02 | 0.00 | 0.4 | -0.1 | 0.6 | 27.6 | 0.0 | 0.0 | 0.1 | -0.6 | 0.1 | 0.0 | 0.1 | -0.3 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 1.4 | 0.2 | 11.5 | 0.5 | 0.0 | 0.0 | 1.7 | -0.2 | 0.1 |
| LOD (3 x S.d.) | | | | | 0.01 | 0.04 | 0.06 | 0.01 | 0.2 | 0.4 | 1.1 | 12.0 | 0.0 | 0.0 | 0.1 | 0.8 | 1.2 | 0.3 | 0.2 | 0.5 | 0.0 | 0.0 | 0.0 | 0.4 | 0.9 | 5.9 | 1.8 | 11.9 | 1.6 | 0.0 | 0.0 | 2.5 | 0.1 | 0.0 |
| TM24.4 | | | | | 9.0 | 1.0 | 5.2 | 25 | 9.2 | 39 | 5.7 | 3.4 | 17 | 2.3 | 4.3 | -0.3 | 6.9 | 5.6 | 7.1 | 17 | 5.9 | 8.7 | 6.2 | 5.2 | 5.7 | 3.4 | 5.9 | | 115 | 7.6 | 4.1 | 7.5 | 34 | |
| Certified TM24.4 | | | | | | | | 15.0 ± | 32.9 ± | 5.30 ± | | | | | 3.96 ± | | 6.27 ± | 5.00 ± | 6.31 ± | 16.0 ± | 4.95 ± | 8.24 ± | | 5.03 ± | | 5.60 ± | | | | 113 ± | | 7.00 ± | | |
| % recovery (TM24.4) | | | | | | | | 1.0 | 8.92 | 4.5 | 0.53 | | | | 0.34 | | 0.57 | 0.59 | 0.60 | 2.3 | 0.42 | 0.73 | | 0.53 | | 0.52 | | | 8 | | | 0.58 | | |
| | | | | | | | | | 103 | 117 | 108 | 110 | 111 | 112 | 109 | 111 | 112 | 112 | 108 | 119 | 105 | 105 | 103 | 103 | 105 | 105 | 105 | 105 | 102 | 102 | 103 | 107 | 107 | 107 |
| TM24.4.3 | | | | | 9.4 | 1.1 | 5.3 | 24 | 12 | 299 | 165 | 255 | 306 | 166 | 272 | -2 | 259 | 298 | 273 | 305 | 162 | 290 | 287 | 265 | 1 | 290 | 282 | 647 | 130 | 147 | 288 | 338 | | |
| Certified TM63.4 | | | | | | | | 287 ± | 12.6 ± | 291 ± | 164 ± | | | | 258 ± | | 250 ± | 283 ± | 298 ± | 143 ± | 292 ± | | 252 ± | | 280 ± | | | | 628 ± | | 279 ± | 320 ± | | |
| % recovery (TM24.63.4) | | | | | | | | 18 | 1.3 | 23 | 15 | | | | 21 | | 16 | 17 | 21 | 21 | 15 | 17 | 18 | 18 | 22 | 22 | 34 | | 34 | | | 18 | 23 | |
| | | | | | | | | 107 | 96 | 103 | 101 | 107 | 107 | 100 | 105 | 103 | 103 | 105 | 92 | 102 | 113 | 99 | 105 | 105 | 104 | 104 | 103 | 103 | 100 | 99 | 100 | 103 | 106 | 106 |
| CE491_T11-1+spike | | | | - | - | - | - | - | 99 | 97 | 100 | 97 | 98 | 100 | 99 | 98 | 99 | 98 | 101 | 97 | 102 | 99 | 99 | 98 | 99 | 98 | 98 | 93 | 99 | 98 | 99 | 97 | 99 | 100 |
| CE491_T11-10+spike | | | | 99 | 99 | 99 | 99 | 99 | 100 | 99 | 101 | 104 | 100 | 100 | 100 | 100 | 101 | 100 | 101 | 100 | 103 | 100 | 100 | 99 | 100 | 100 | 100 | 94 | 101 | 101 | 100 | 99 | 101 | 101 |
| CE491_T11-20+spike | | | | 97 | 97 | 97 | 97 | 97 | 100 | 99 | 101 | 105 | 100 | 101 | 100 | 100 | 102 | 100 | 100 | 100 | 103 | 101 | 101 | 99 | 100 | 100 | 100 | 97 | 101 | 100 | 100 | 100 | 101 | 101 |
| CE491_T11-30+spike | | | | 97 | 97 | 97 | 97 | 97 | 99 | 99 | 101 | 107 | 99 | 101 | 100 | 99 | 100 | 100 | 100 | 99 | 104 | 100 | 101 | 99 | 100 | 100 | 100 | 97 | 100 | 99 | 100 | 100 | 101 | 100 |
| CE491_T11-40+spike | | | | 99 | 99 | 99 | 99 | 99 | 101 | 99 | 101 | 107 | 100 | 102 | 100 | 100 | 101 | 100 | 102 | 99 | 103 | 102 | 101 | 99 | 101 | 99 | 101 | 99 | 101 | 100 | 100 | 99 | 100 | 100 |

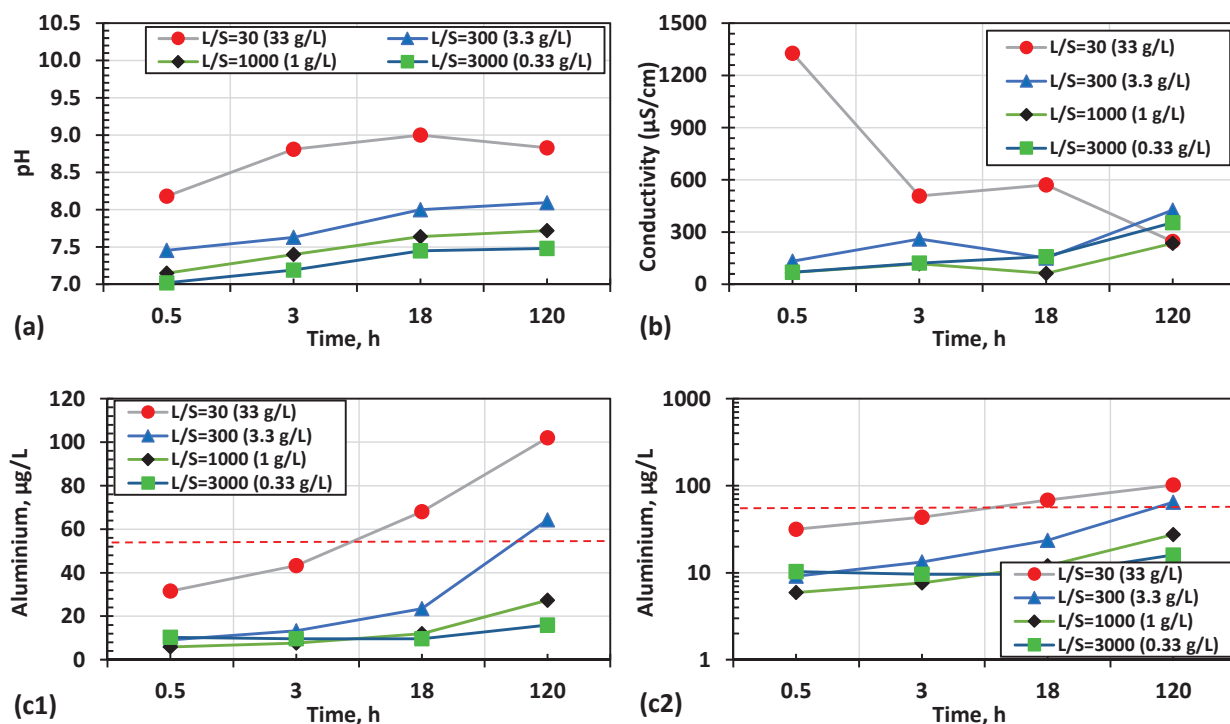


Figure D2.1 The pH, conductivity and dissolved Al concentration of composite 6B elutriate tests after times of 0.5, 3, 18 and 120 h for liquid to solid ratios (L/S) of 30, 300, 1000 and 3000 (c2 = log scale)

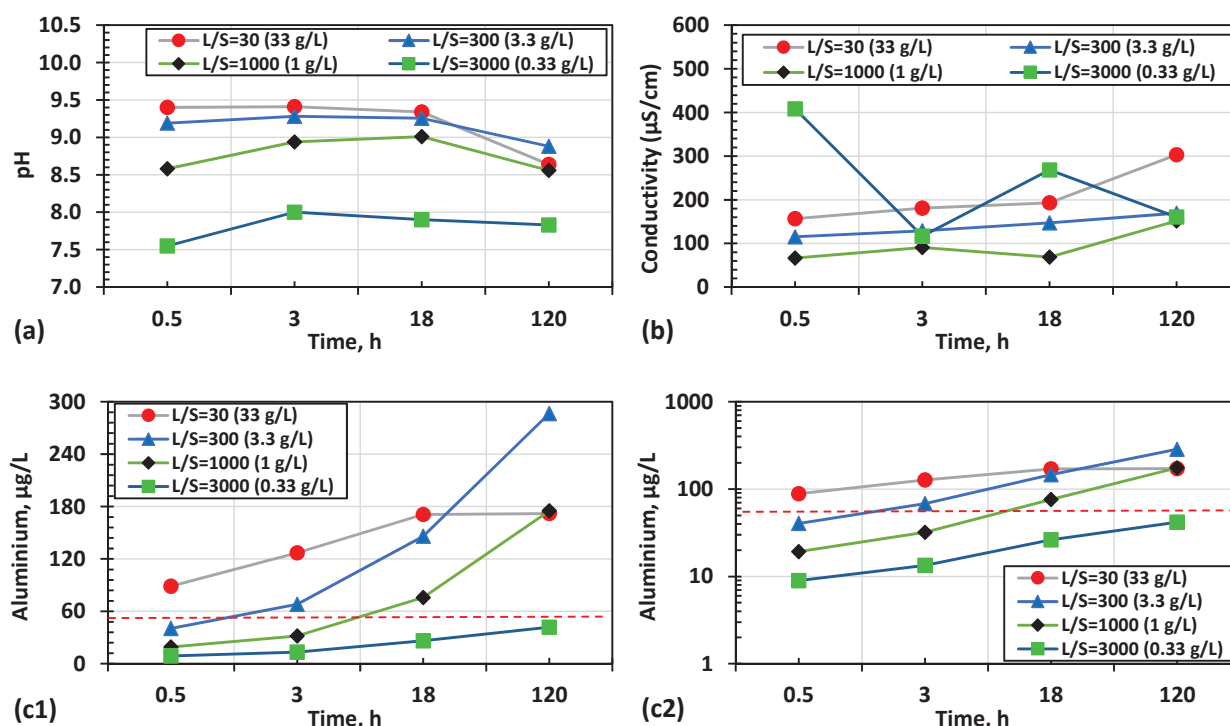


Figure D2.2 The pH, conductivity and dissolved Al concentration of composite 6E elutriate tests after times of 0.5, 3, 18 and 120 h for liquid to solid ratios (L/S) of 30, 300, 1000 and 3000 (c2 = log scale)

Figures for major cations from Memo 11 and 6B/6E tests

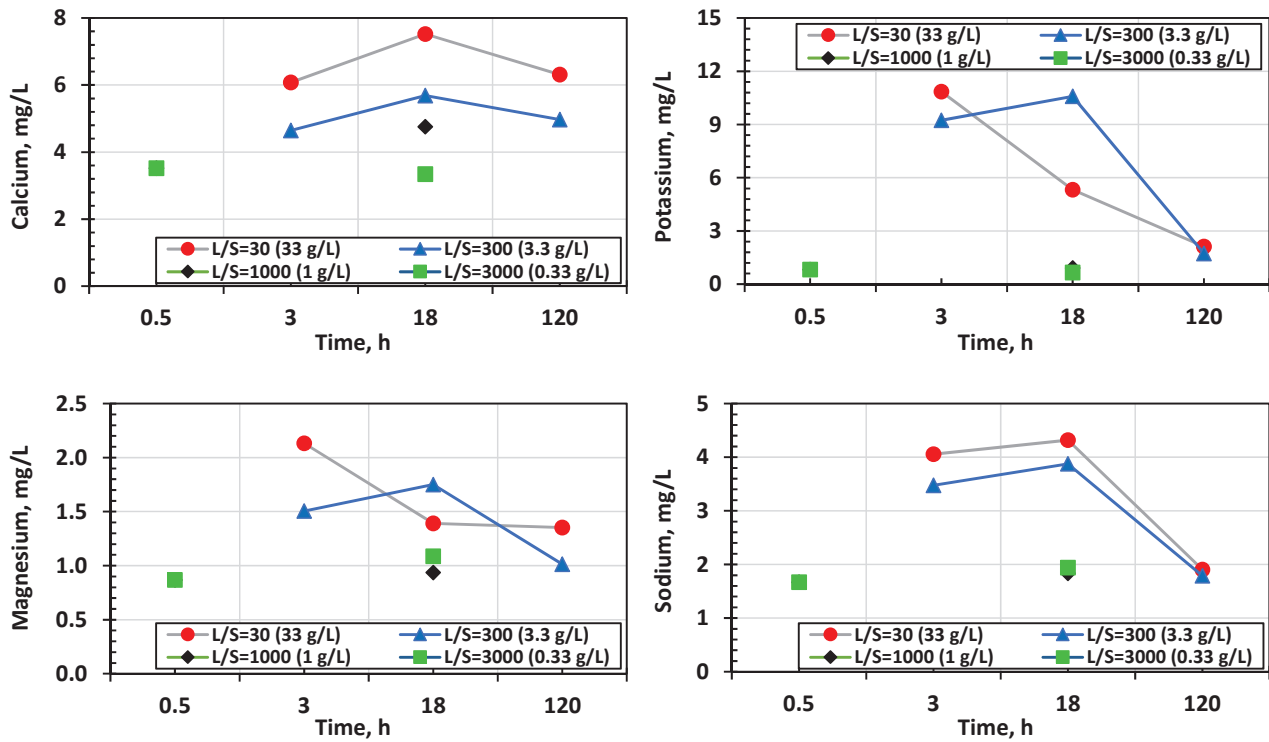


Figure D2.3 Dissolved major ions (Na, K, Mg, Ca) for composite 1B elutriate tests after times of 0.5, 3, 18 and 120 h for liquid to solid ratios (L/S) of 30, 300, 1000 and 3000

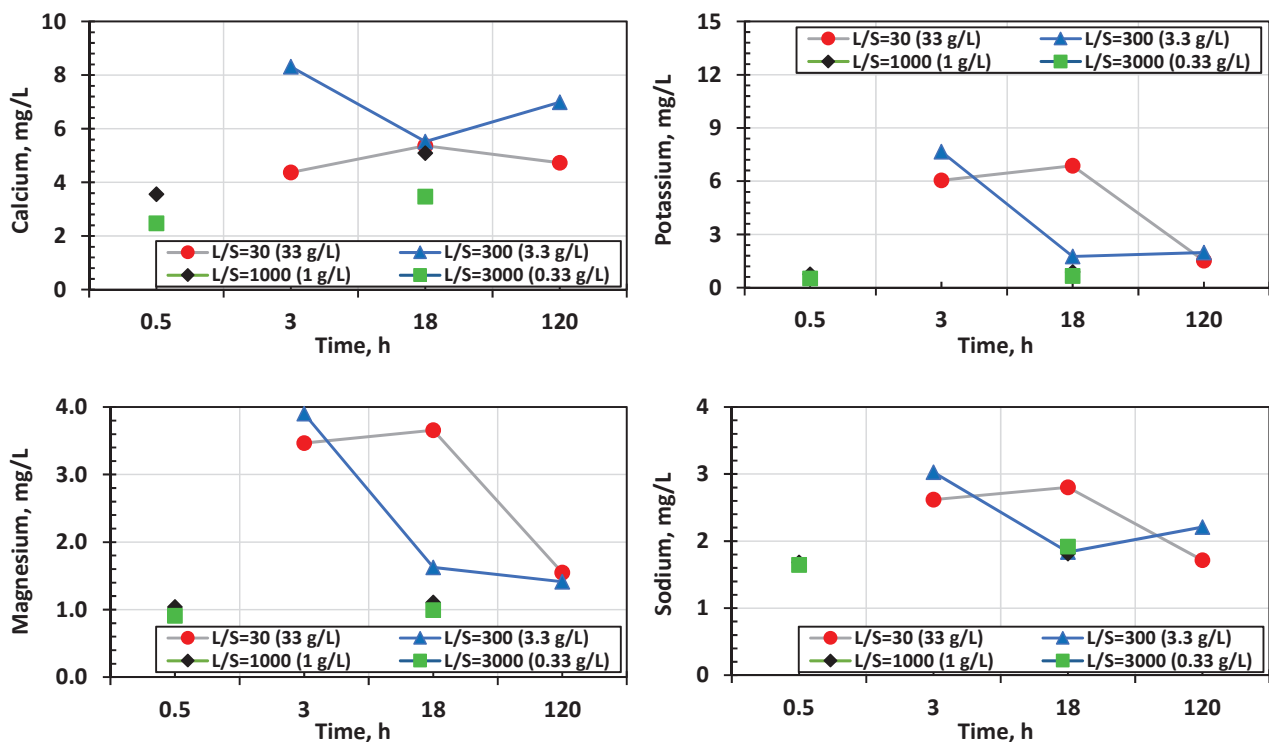


Figure D2.4 Dissolved major ions (Na, K, Mg, Ca) for composite 2B elutriate tests after times of 0.5, 3, 18 and 120 h for liquid to solid ratios (L/S) of 30, 300, 1000 and 3000

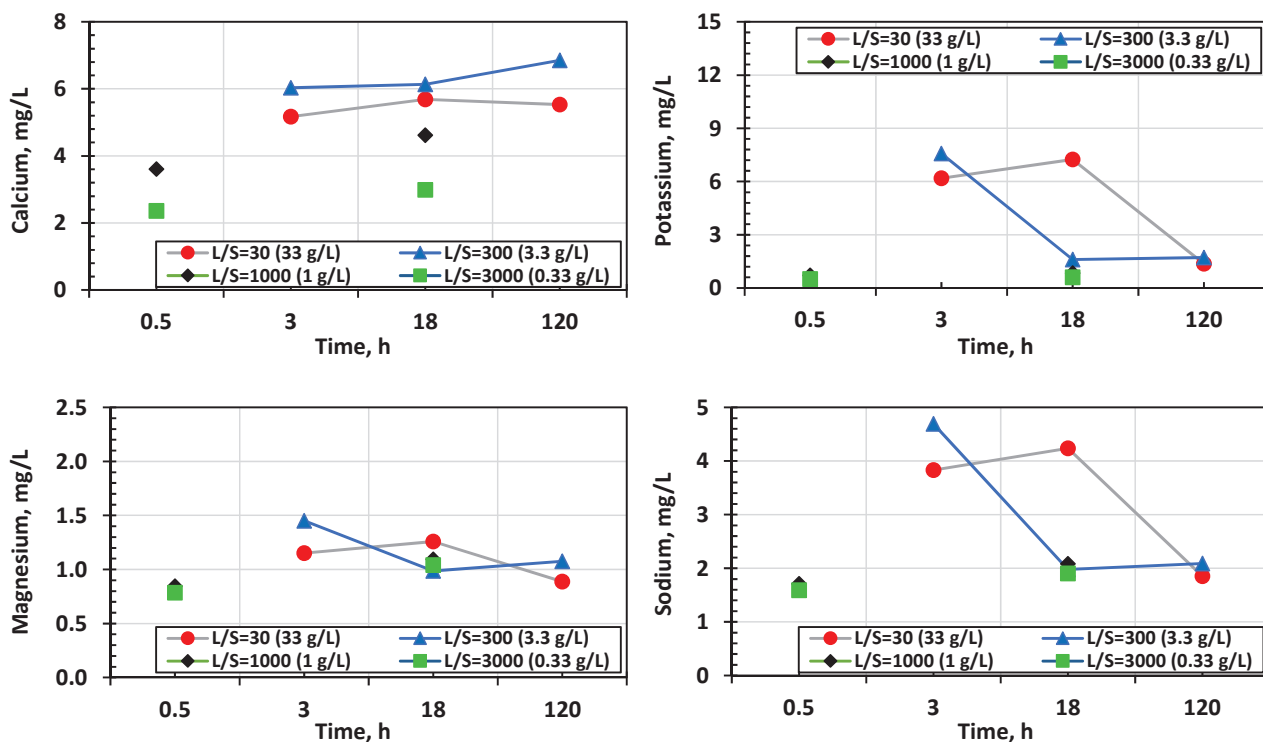


Figure D2.5 Dissolved major ions (Na, K, Mg, Ca) for of composite 5B elutriate tests after times of 0.5, 3, 18 and 120 h for liquid to solid ratios (L/S) of 30, 300, 1000 and 3000

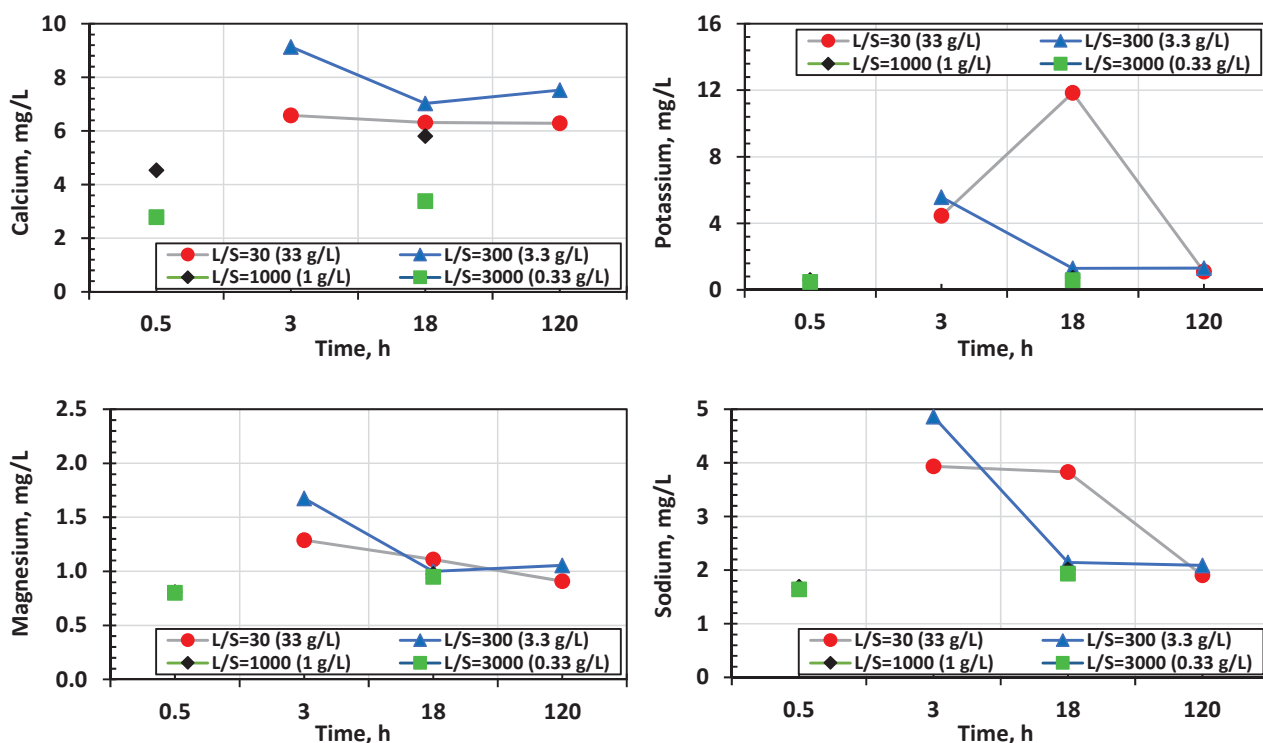


Figure D2.6 Dissolved major ions (Na, K, Mg, Ca) for composite 5E elutriate tests after times of 0.5, 3, 18 and 120 h for liquid to solid ratios (L/S) of 30, 300, 1000 and 3000

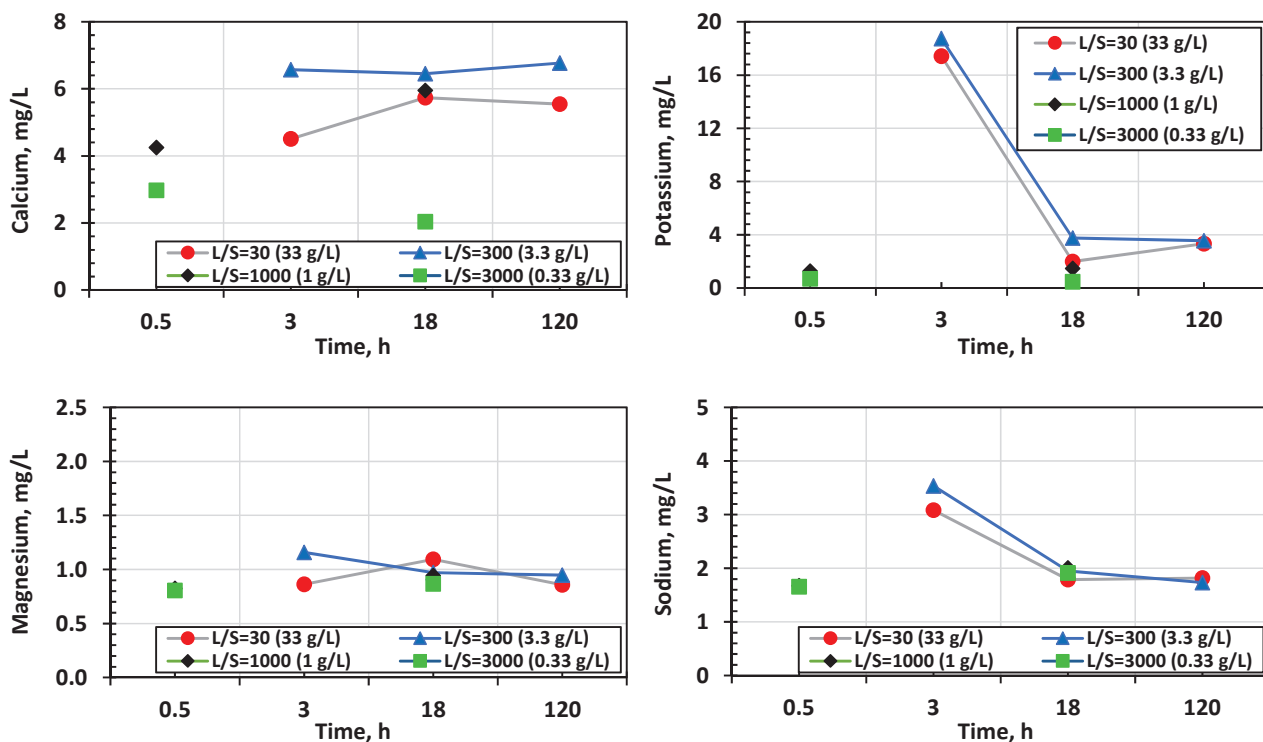


Figure D2.7 Dissolved major ions (Na, K, Mg, Ca) for composite 7E elutriate tests after times of 0.5, 3, 18 and 120 h for liquid to solid ratios (L/S) of 30, 300, 1000 and 3000

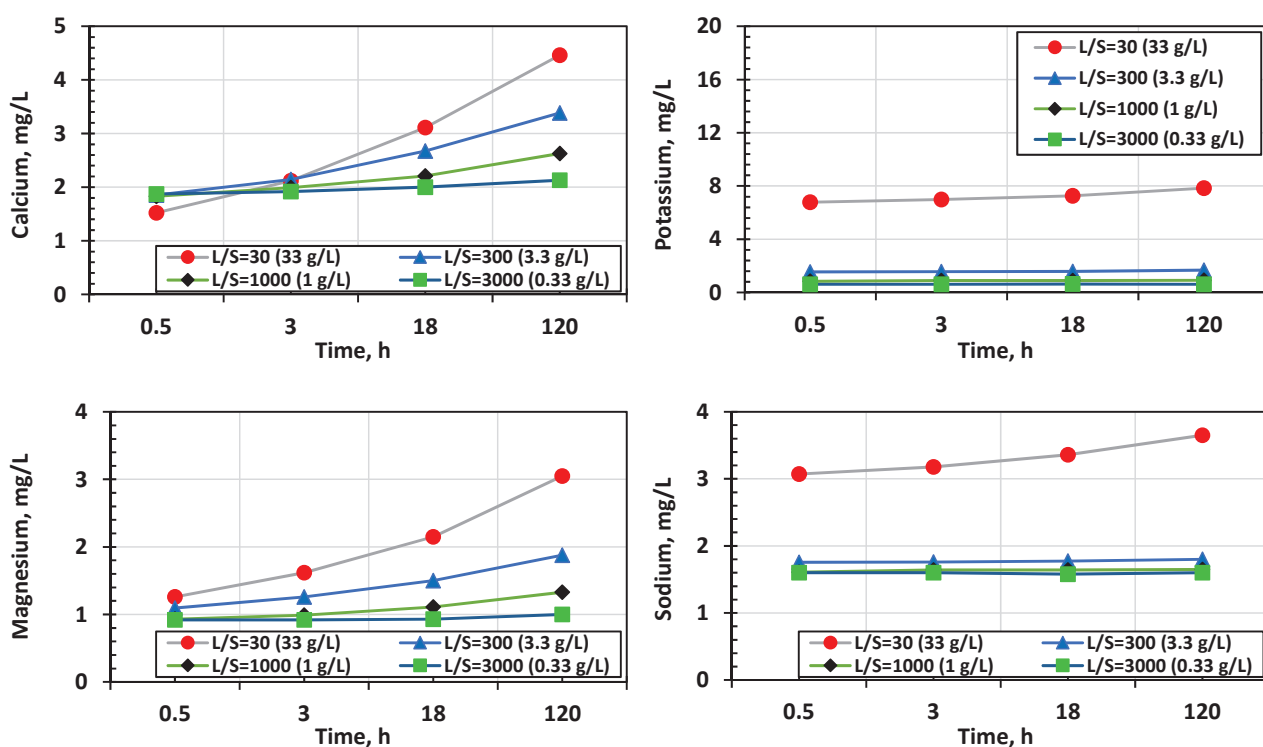


Figure D2.8 Dissolved major ions (Na, K, Mg, Ca) for composite 6B elutriate tests after times of 0.5, 3, 18 and 120 h for liquid to solid ratios (L/S) of 30, 300, 1000 and 3000

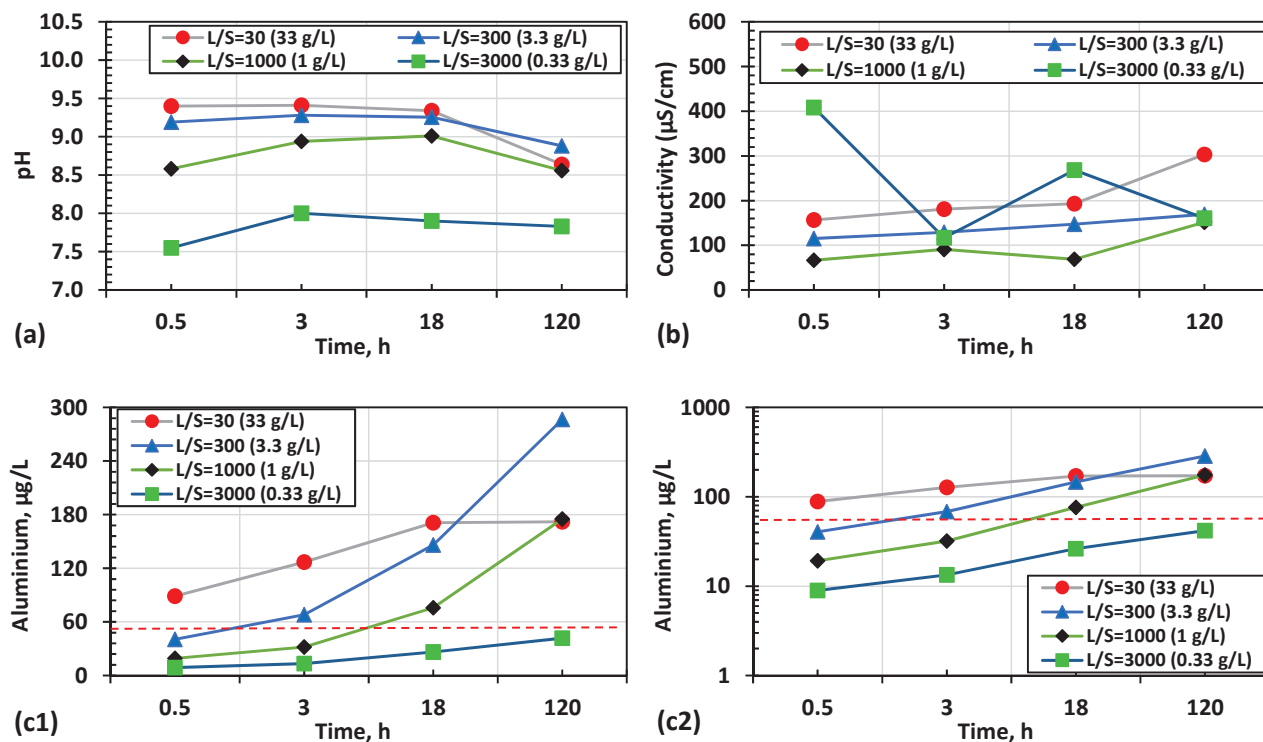


Figure D2.9 Dissolved major ions (Na, K, Mg, Ca) for composite 6E elutriate tests after times of 0.5, 3, 18 and 120 h for liquid to solid ratios (L/S) of 30, 300, 1000 and 3000 (c2 = log scale)

Appendix D3. Effect of mixing duration on substance release from <75 µm composite rock materials

| | |
|------------------|--|
| Note/Memo | CSIRO P4 Project Investigations |
| To: | Ali Watters (HKA) |
| From: | Brad Angel, Lucas Heights, NSW |
| Date: | 18 October 2018 |
| Copy: | Ryan Fraser, Stuart Simpson and Ellen Porter (SHL) |
| Our reference: | CSIRO P4 – Memo 5 |
| Classification: | Internal use only |
| Subject: | Pollutant release from excavated rock composites – Effect of liquid to solid ratio and duration in reservoir water |

Chemical formulas and acronyms

| | | | | | |
|-----|--------------|-----|-------------------------|-----|--------------------|
| Al | Aluminium | dAl | Dissolved aluminium | | |
| SEC | conductivity | DGV | Default guideline value | L/S | Liquid/solid ratio |

Background - Introduction

The CSIRO was engaged by Haskoning Australia Pty Ltd (RHDHV) to undertake an investigation of the pollutant release from excavated rock disposal into Talbingo and Tantangara reservoirs.

The initial elutriate tests (Memo 4) investigating the release of pollutants from composite excavated rock samples (L/S = 10, 48 h) observed some significant changes in water quality with respect to pH, conductivity (SEC) the dissolved aluminium concentrations:

- pH increased from 7.0-7.1 to 8.9-9.8 range
- SEC increased from 29 $\mu\text{S}/\text{cm}$ to 110-200 $\mu\text{S}/\text{cm}$ range, and
- dissolved Al ($<0.45 \mu\text{m}$ filterable) increased from $<4 \mu\text{g}/\text{L}$ (ppb) to 200-800 $\mu\text{g}/\text{L}$ range.

The conditions of those elutriate tests, L/S = 10, 48 h, were designed to assess a severe / worst case scenario for impacts to the receiving water in which large amounts of fine excavated rock materials may remain suspended in the waters in the main disposal area.

This technical memo describes results of elutriate tests performed on a single fine excavated rock composite material, 4E, in which the kinetics of the changes in pH, conductivity the dissolved aluminium concentrations were investigated over a range of Liquid/solid ratios (Figure 1):

- L/S = 100, 1000, 10000, and Reservoir water only (Talbingo)
 - [being 10 g/L, 1.0 g/L, 0.1 g/L and 0 g/L respectively]
- Measurements at times of 0.5, 2, 6 and 24 h
- Solids mixed in composite Talbingo control water for 30 s then allowed to stand for durations tested

Kinetics of pH, conductivity and dissolved aluminium

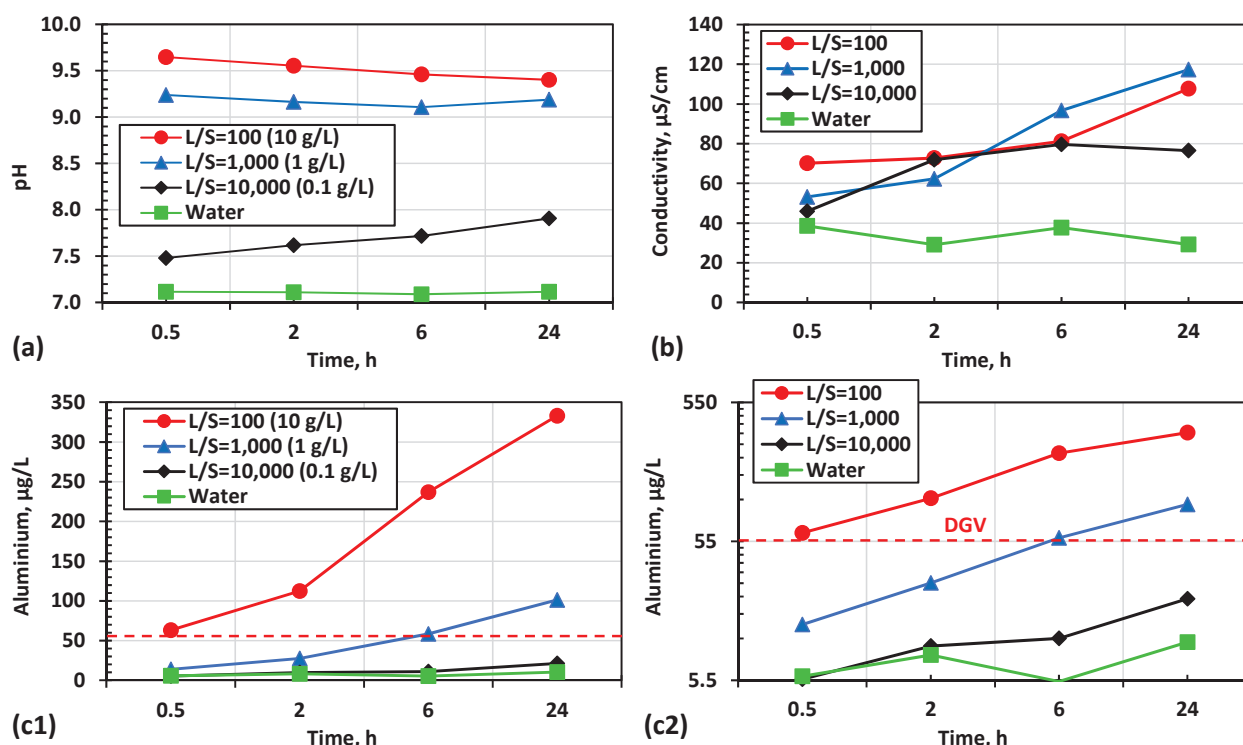


Figure 1. Water (Talbingo) (a) pH, (b) conductivity and (c1, c2) dissolved aluminium concentrations for elutriates of fine excavated rock composite material 4E. DGV represents the default guideline value (95% species protection for freshwater) of 55 $\mu\text{g Al/L}$, where the 99% species protection concentration is 27 $\mu\text{g/L}$.

Summary

The initial contact of the solids with the water resulted in a rapid increase in pH and conductivity.

Higher solids concentrations (lower L/S) resulted in greater initial pH, conductivity and dissolved aluminium concentrations.

Risks of adverse effect to aquatic organisms are predicted to occur due to:

- high pH (within 30 min) for Talbingo water containing ≥ 1 g 4E-fine_solids/L (L/S=1,000), pH >8.5 water likely occurring within 0.2-1 g/L 4E-fine_solids concentration range.
- high dissolved aluminium concentrations (dAl) after 6 h for Talbingo water containing 1 g 4E-fine_solids/L, or after 30 min for Talbingo water containing 10 g 4E-fine_solids/L (L/S=100)

The kinetics of the changes in pH, conductivity and the dissolved aluminium concentrations indicate increased dissolution of rock solids occur with time. For aluminium the increase with time is consistent with the high pH acting to increase dissolution through formation of the highly soluble aluminate ion, $\text{Al}(\text{OH})_4^-$.

The rock composite 4E was selected owing to the high level of aluminium release observed in the initial elutriate test (Memo 4).

In tests now underway a greater range of rock composites are being investigated using a similar test design (1B, 1B, 5B, 5E, 7E), and across a wider range of L/S ratios (30, 3000, 1000, 3000). These tests are expected to provide a more representative assessment of potential changes in pH, conductivity and dissolved aluminium, along with other parameters.

| | |
|------------------|---|
| Note/Memo | CSIRO P4 Project Investigations |
| To: | Ali Watters (HKA) |
| From: | Brad Angel, Lucas Heights, NSW |
| Date: | 2 November 2018 |
| Copy: | Ryan Fraser, Stuart Simpson and Ellen Porter (SHL) |
| Our reference: | CSIRO P4 – Memo 7 |
| Classification: | Internal use only |
| Subject: | Pollutant release from excavated rock composites – Alkalinity |

Chemical formulas and acronyms

| | | | | | |
|-----|--------------------|-----|--------------|--|--|
| L/S | Liquid/solid ratio | SEC | Conductivity | | |
|-----|--------------------|-----|--------------|--|--|

Background - Introduction

The CSIRO was engaged by Haskoning Australia Pty Ltd (RHDHV) to undertake an investigation of pollutant release from excavated rock disposal into Talbingo and Tantangara reservoirs.

The elutriate tests investigating the release of pollutants from composite excavated rock samples observed some significant changes in water quality with respect to water pH, with increases from 7.0-7.1 in Reservoir waters to 8.9-11 range in elutriates (L/S = 10 – 1,000).

This technical memo describes results of elutriate tests performed on eight fine (<75 µm) excavated rock composite materials (7 geological zones, including Kelly Plains 6B and 6E), for which the pH, conductivity, and alkalinity were measured after 30 min and 6 h. The tests were conducted at a liquid/solid ratio (L/S) of 500, and for one material (4E) tests were conducted for L/S = 500, 2000, 5000 and 10000 and compared with the alkalinity of the Talbingo Reservoir water.

Note, that these tests included for the first time the previously unavailable Kelly Plains materials – an additional ‘geological zone’ referred to as composite 6.

Water alkalinity

The pH, SEC and alkalinity after 0.5 h and 6 h settling of the Talbingo water and elutriate test performed on eight fine-rock composites at L/S=500 are shown in Table 1 and for the 4E fine-rock composite over a range of L/S in Table 2.

Similar to that reported in the initial result (Memo 1), the Talbingo water had neutral pH (7.0) and low conductivity (25-40 µS/cm). The alkalinity of the Talbingo water was 13-14 mg CaCO₃/L. For the L/S=500 elutriates the pH and conductivity were both higher after 0.5 h than after 6 h, and remained higher than the Talbingo water (Table 1). The 6 h result for 4E is an outlier with regards to this. For the L/S=500 elutriates the alkalinity was similar for measurements after 0.5 and 6 h, and was 50-100% higher than the original Talbingo water.

The increase in pH, SEC and alkalinity was much lower at higher L/S ratios (Table 2), where L/S 10,000 = (0.1 g fine-rock solids/L reservoir water) and L/S 500 = 2 g/L.

Summary

Overall the increases in alkalinity observed in the elutriate solutions were significant and will result in increased pH-buffering at the higher pH. However, the increases in alkalinity were generally modest and are unlikely to result in impacts to aquatic organisms.

Table 1. The pH, conductivity and alkalinity for elutriate test of the fine excavated rock composites.

| Test water and fine-rock composite | L/S | Time h | pH | Conductivity ($\mu\text{S}/\text{cm}$) | Alkalinity (mg CaCO_3/L) |
|------------------------------------|----------|-----------|-----|---|--|
| Talbingo water only | ∞ | 0.5 | 7.0 | 39.9 | 14 |
| Talbingo water only | ∞ | 6 | 7.0 | 24.5 | 13 |
| 1E | 500 | 0.5 | 8.4 | 76.9 | 23 |
| 1E | 500 | 6 | 7.1 | 40.4 | 22 |
| 2E | 500 | 0.5 | 9.1 | 78.8 | 25 |
| 2E | 500 | 6 | 8.7 | 48.1 | 25 |
| 3E | 500 | 0.5 | 9.2 | 52.1 | 25 |
| 3E | 500 | 6 | 9.1 | 51.3 | 25 |
| 4E | 500 | 0.5 | 9.2 | 55.6 | 27 |
| 4E | 500 | 6 | 9.1 | 130 | 26 |
| 5E | 500 | 0.5 | 9.2 | 54.6 | 25 |
| 5E | 500 | 6 | 8.9 | 49.0 | 27 |
| 6E | 500 | 0.5 | 8.8 | 58.6 | 21 |
| 6E | 500 | 6 | 8.6 | 47.2 | 24 |
| 7E | 500 | 0.5 | 9.1 | 58.0 | 24 |
| 7E | 500 | 6 | 8.4 | 49.3 | 17 |
| 6B | 500 | 0.5 | 7.4 | 62.0 | 15 |
| 6B | 500 | 6 | 7.5 | 32.0 | 22 |

Table 2. Influence of L/S on pH, conductivity and alkalinity for elutriate test of the fine-rock composites 4E

| Test water and fine-rock composite | L/S | Time h | pH | Conductivity ($\mu\text{S}/\text{cm}$) | Alkalinity as CaCO_3 mg/L |
|------------------------------------|----------|-----------|-----|---|---------------------------------------|
| Talbingo water only | ∞ | 0.5 | 7.0 | 39.9 | 14 |
| Talbingo water only | ∞ | 6 | 7.0 | 24.5 | 13 |
| 4E | 10,000 | 0.5 | 7.3 | 42.2 | 16 |
| 4E | 10,000 | 6 | 7.4 | 32.5 | 18 |
| 4E | 5,000 | 0.5 | 8.0 | 45.1 | 18 |
| 4E | 5,000 | 6 | 7.7 | 36.4 | 19 |
| 4E | 2,000 | 0.5 | 8.9 | 46.9 | 22 |
| 4E | 2,000 | 6 | 8.7 | 45.2 | 22 |
| 4E | 500 | 0.5 | 9.2 | 55.6 | 27 |
| 4E | 500 | 6 | 9.1 | 130 | 26 |

Figures for major cations from Memo 4 (4B)

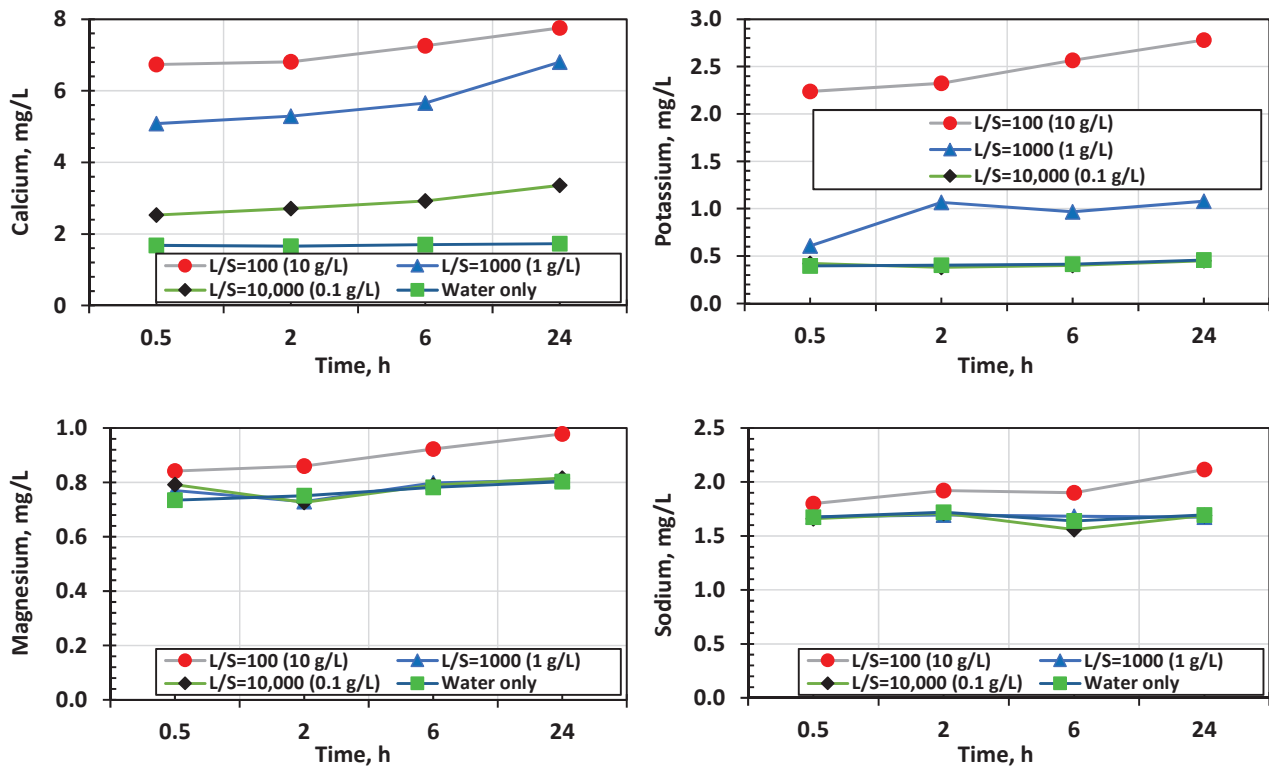


Figure D3.1. Major cation concentration of composite 4E elutriate tests after times of 0.5, 2, 6 and 24 h for liquid to solid ratios (L/S) of 100, 1000, and 10,000.

Appendix D4. Effect of rock material size on substance

| | |
|------------------|--|
| Note/Memo | CSIRO P4 Project Investigations |
| To: | Ali Watters (HKA) |
| From: | Brad Angel, Lucas Heights, NSW |
| Date: | 26 October 2018 |
| Copy: | Ryan Fraser, Stuart Simpson and Ellen Porter (SHL) |
| Our reference: | CSIRO P4 – Memo 6 |
| Classification: | Internal use only |
| Subject: | Pollutant release from excavated rock composites |

Chemical formulas and acronyms

| | | | | | |
|-----------------|--------------------------|------------------------------|-------------------------|-------------------------------|--------------------|
| Ag | Silver | F ⁻ | Fluoride | Sb | Antimony |
| Al | Aluminium | Fe | Iron | Se | Selenium |
| As | Arsenic | Mg | Magnesium | Sn | Tin |
| Ba | Barium | Mn | Manganese | SO ₄ ²⁻ | Sulfate |
| Ca | Calcium | Mo | Molybdenum | Sr | Strontium |
| Cd | Cadmium | Na | Sodium | Th | Thorium |
| Cl ⁻ | Chloride | Ni | Nickel | U | Uranium |
| Co | Cobalt | NO ₃ ⁻ | Nitrate | V | Vanadium |
| Cr | Chromium | Pb | Lead | Zn | Zinc |
| Cu | Copper | | | | |
| DOC | Dissolved organic carbon | DGV | Default guideline value | L/S | Liquid/solid ratio |
| SEC | Conductivity | | | | |

Background - Introduction

The CSIRO was engaged by Haskoning Australia Pty Ltd (RHDHV) to undertake an investigation of the pollutant release from excavated rock disposal into Talbingo and Tantangara reservoirs. This phase of the work involved investigating the release of pollutants from composite excavated rock samples in an initial elutriate test that had a liquid to solid (L/S) ratio of 10/1 and was run for 48 h. With respect to placement scenarios for the excavated rock, these tests were intended to assess a worst case scenario for impacts to the receiving water. It is envisaged that the design of the excavated rock placement will result in fast deposition of the majority of the excavated rock, and concentrations of fine materials within the waters will be managed to achieve considerably lower concentrations of suspended solids. The vast majority of the excavated rock, by mass, will be larger than sand size and should settle rapidly.

The materials with finer particle size are expected to represent the greatest environmental risk with respect to transport and release of pollutants. Materials with a larger particle size are expected to settle rapidly and release smaller amounts of pollutants to the reservoir waters.

This technical memo describes results of elutriate tests performed on four different excavated rock materials that had been mechanically crushed to provide materials with the size categories 10-25 mm; 2-10 mm, 0.21-2 mm and <0.21 mm (composite fine material). The kinetics of substance release was monitored at time periods of 1, 4 and 24 h after resuspension then settling in Talbingo reservoir water.

Preparation of rock materials in different size ranges

For each core material rock pieces larger than ~2 cm were passed through a jaw crusher plant. This process created a wide range of uneven shapes but were generally more flat than square. The crushed materials

were sieved through plastic sieves to create the following size fractions: >10 mm; 2-10 mm, 0.21-2 mm and <0.21 mm (fine material). Owing to the varied shapes, the different size ranges included fractions that were able to pass through the sieve in a single direction but would not pass if perpendicular (e.g. long thin piece could pass). This was considered when selecting fractions for the tests, where the aim was to have pieces that were more 'square' than flat or thin.

The rock materials tested included 1E (Ravine), 4B (Gooandra Volcanics), 5B and 5E (Peppercorn/Tantangara/Temperance Formations). For each test, the liquid to solid ratio (L/S, weight/weight) was 25, resulting in a greater number of pieces of rock for the tests with smaller L/S. For the 10-25 mm size range, a single piece of rock was selected, for the 2-10 mm size range 4-6 pieces were selected, with the finer size fractions prepared from homogenised samples. The tests were undertaken in volumes of 250 mL water for the two larger size fractions, 125 mL for the 0.21-2 mm fraction and 50 mL for the <0.21 mm size fraction. Each test was undertaken in triplicate, unless there was insufficient material, and this enabled variability across shapes to be incorporated. Talbingo reservoir water was used for all tests, comprising an equal volume composite from three buck waters. As fine dust was on the surface of large rock pieces, the three larger rock fraction underwent a 10-s leach (add, shake, then decant to waste) immediately before the test water was added.

For the elutriate tests, the materials (rock and water) were shaken briefly and then rolled for 30 min on a purpose built bottle roller (~50 rpm) to continually mix the water and solids of that period. The containers were then placed upright to allow the materials to settle until the time of the measurements. Subsamples were taken 1 h, 4 h, 24 h for measurement of pH, conductivity and dissolved analytes (filtered <0.45 µm). The containers were not shaken between time points.

The <0.21 mm fraction of the materials was analysed by laser diffraction to provide information on the particle size distribution and give an idea of the fine material that is likely to be the major source of pollutant release.

Results - Influence of rock material size (and time) on elutriate pH, conductivity and dissolved analytes

The pH, conductivity and dissolved analyte concentrations of the elutriates from the four size fractions of each excavated rock sample in Talbingo water were determined for elutriate tests lasting 1 h, 4 h, and 24 h at L/S = 25. Data has been generated from these tests for a range of other analytes, but results shown in this memo focus on dissolved aluminium owing to the concentrations exceeding the default guideline value (DVG) of 55 µg/L.

The pH, conductivity and dissolved aluminium for each elutriate time period as a function of the size of the rock materials are shown in Figures 1, 2, 3. The concentrations of dissolved major ions (Na, K, Mg, Ca) for each elutriate time period as a function of the size of the rock materials are shown in Figures 4, 5 and 6. The effect of the elutriate duration is clearer in Figure 7. The particle size distribution of the <0.21 mm size fraction is shown in Table 1 and Figure 8.

Points to note:

- pH range of 9.9 to 11.1 for the <25 mm rock materials was notably higher than the range from the initial elutriates (8.8 to 9.8) generated from the fine solids (<75 µm) at L/S=10 (Memo 4). The higher pH is expected to result in higher concentrations of the aluminate ion, $\text{Al}(\text{OH})_4^-$.
- Conductivity range of 125 to 600 µS/cm, was notably higher than the range (110-200 µS/cm) from the initial elutriates generated from the fine solids (<75 µm) at L/S=10 (Memo 4). The pattern is consistent with Ca, followed by Na and K being the major contributors to the increased water conductivity (Figure 7).
- For both pH and conductivity, the high values were observed across the full range of rock material sizes, with conductivity increasing with time. Noting here that the rock materials that were crushed were a

range of different pieces and differences to the initial elutriates may reflect heterogeneity within the rocks material used in the studies.

- Dissolved aluminium exceeded the DVG of 55 µg/L by factor of 4 to 15 within 1 h for <0.21 mm size fraction, and below DGV for 0.21-2 mm size fraction initially then increasing to exceed the DGV for longer elutriate durations.
- pH kinetics: For the 0.21-2 mm size fraction, pH of 24 h elutriates was significantly lower than 1 h and 4 h elutriates.
- Conductivity kinetics: Major initial increases (1 h) then variable increases, potentially doubling conductivity over 4 h, with less change through to 24 h.
- Particle size distribution of <0.21 mm size fraction: The <0.21 mm samples had particle diameters that generally spanned the 0-0.21 mm range. Sample 4B (<0.21 mm) was the finest with 50% of the sample being <21.5 µm. The other samples comprised approximately 50% silt i.e. approximately 50% <63 µm.

Summary

Pollutant release is low, trends towards negligible, for rock materials >2 mm.

The finer <0.21 mm rock fraction is likely to have an impact on water quality that is an order of magnitude greater than that of rock fractions >2 mm in size.

The relationships between L/S, kinetics and water pH, conductivity and dissolved aluminium concentrations are becoming clearer.

Tests underway are investigating release from solids with TSS in 0.1 to 1 mg/L range, as this appears important for defining the transition to having dissolved aluminium concentrations above the DGV.

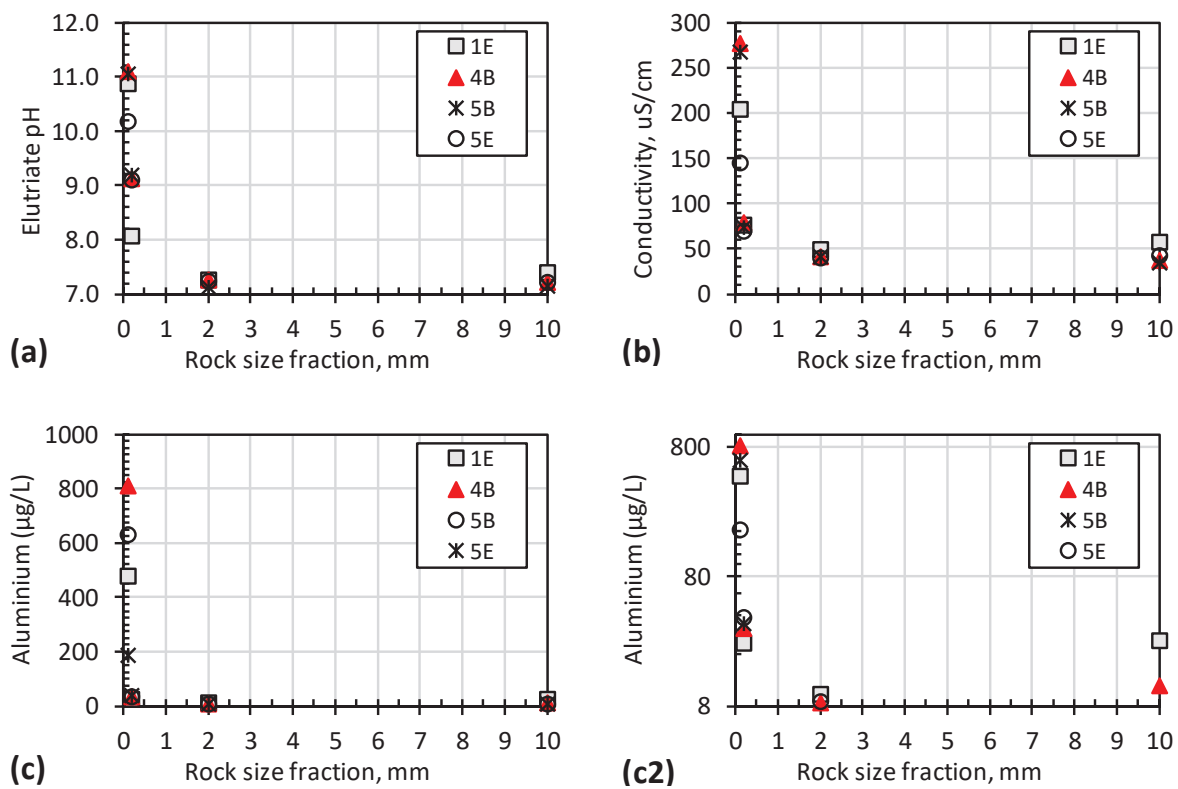


Figure 1. The pH, conductivity and dissolved aluminium after elutriate time of 1 h (c2 = log scale).

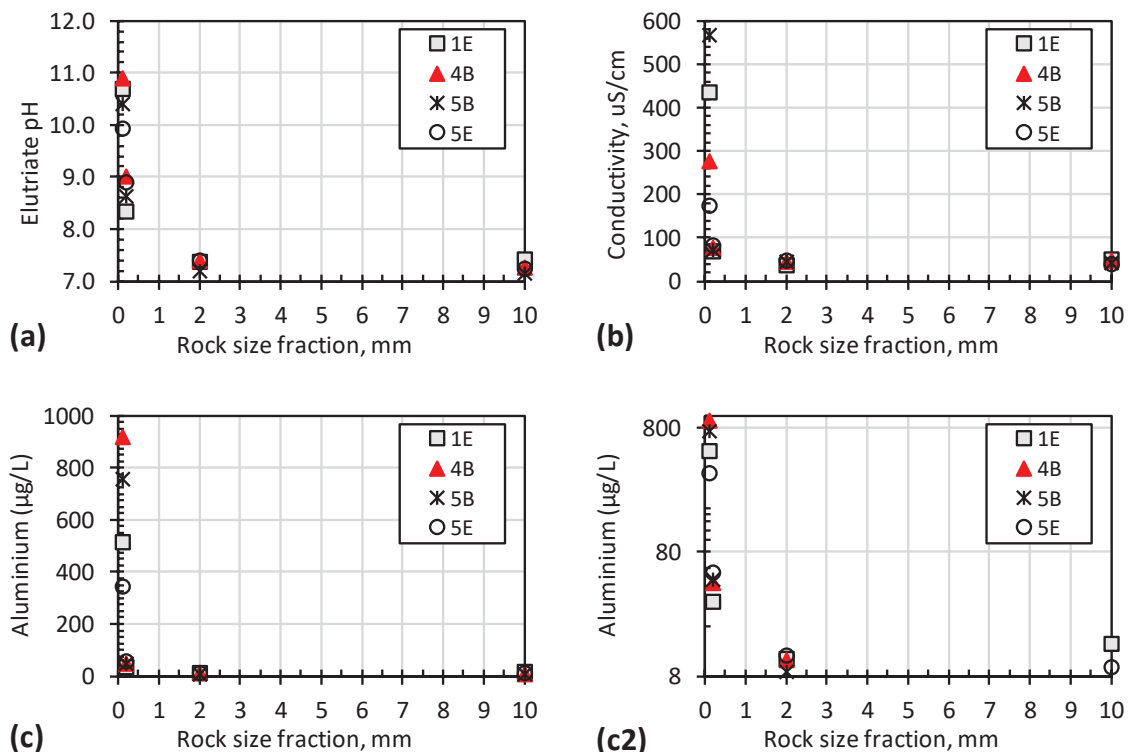


Figure 2. The pH, conductivity and dissolved aluminium after elutriate time of 4 h (c2 = log scale).

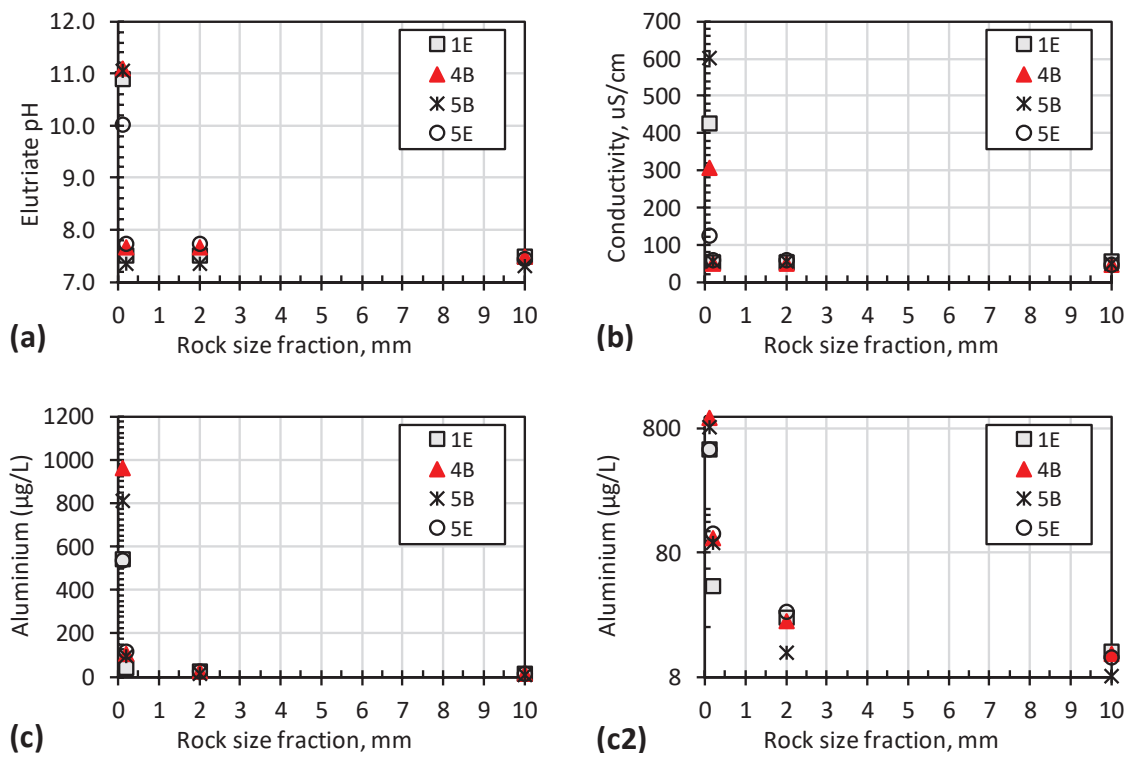


Figure 3. The pH, conductivity and dissolved aluminium after elutriate time of 24 h (c2 = log scale).

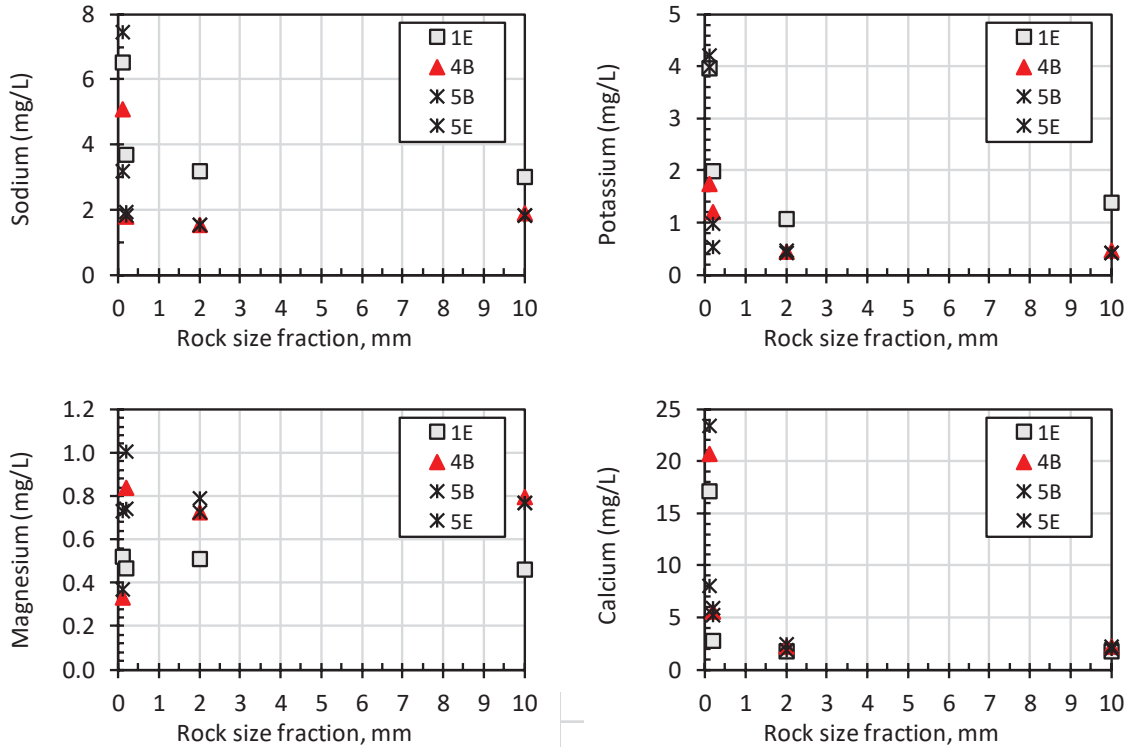


Figure 4. Dissolved major ions (Na, K, Mg, Ca) after elutriate time of 1 h.

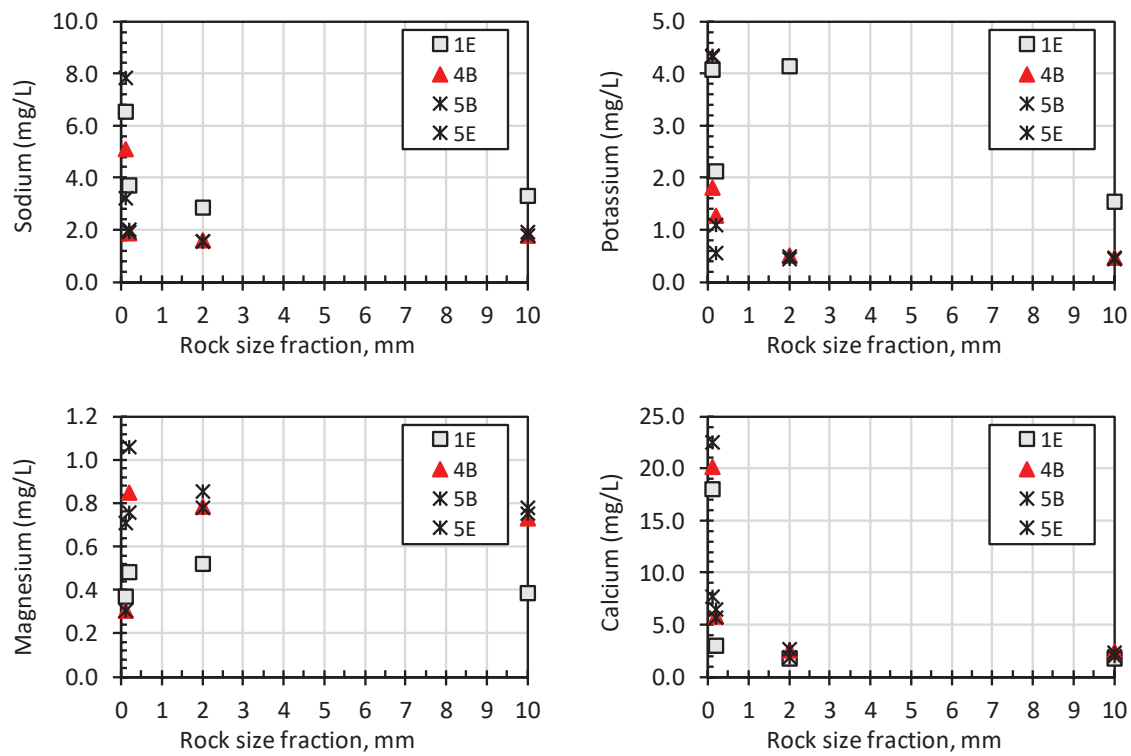


Figure 5. Dissolved major ions (Na, K, Mg, Ca) after elutriate time of 4 h.

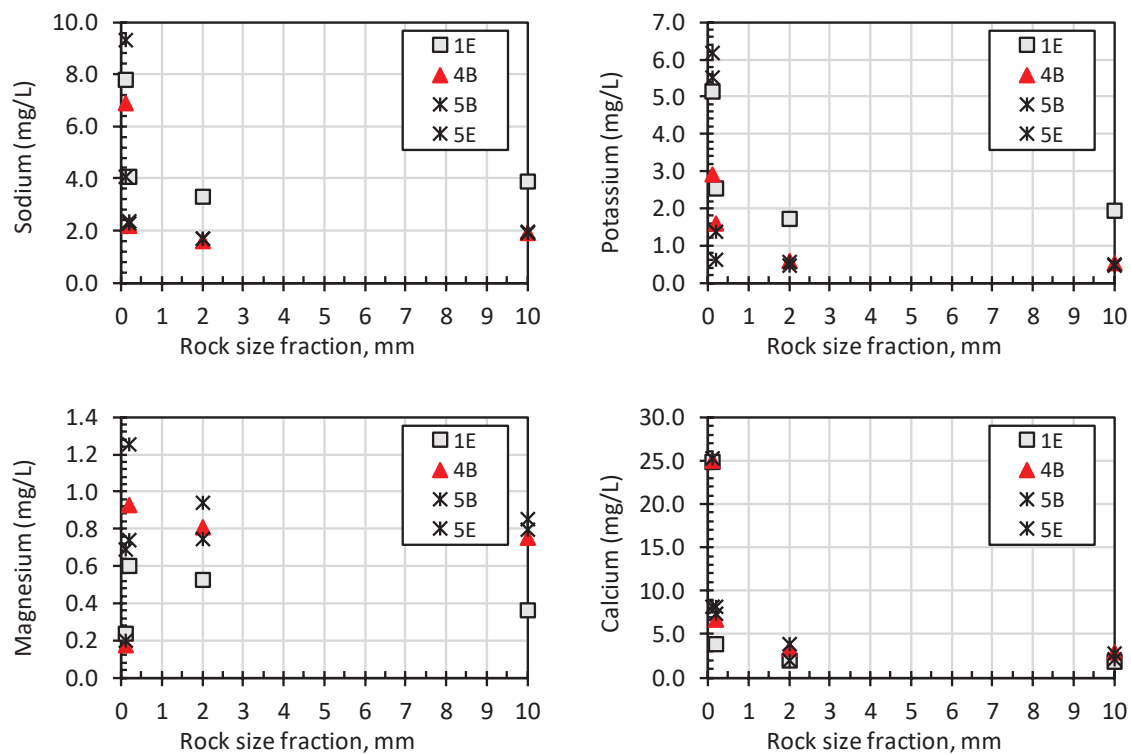


Figure 6. Dissolved major ions (Na, K, Mg, Ca) after elutriate time of 24 h.

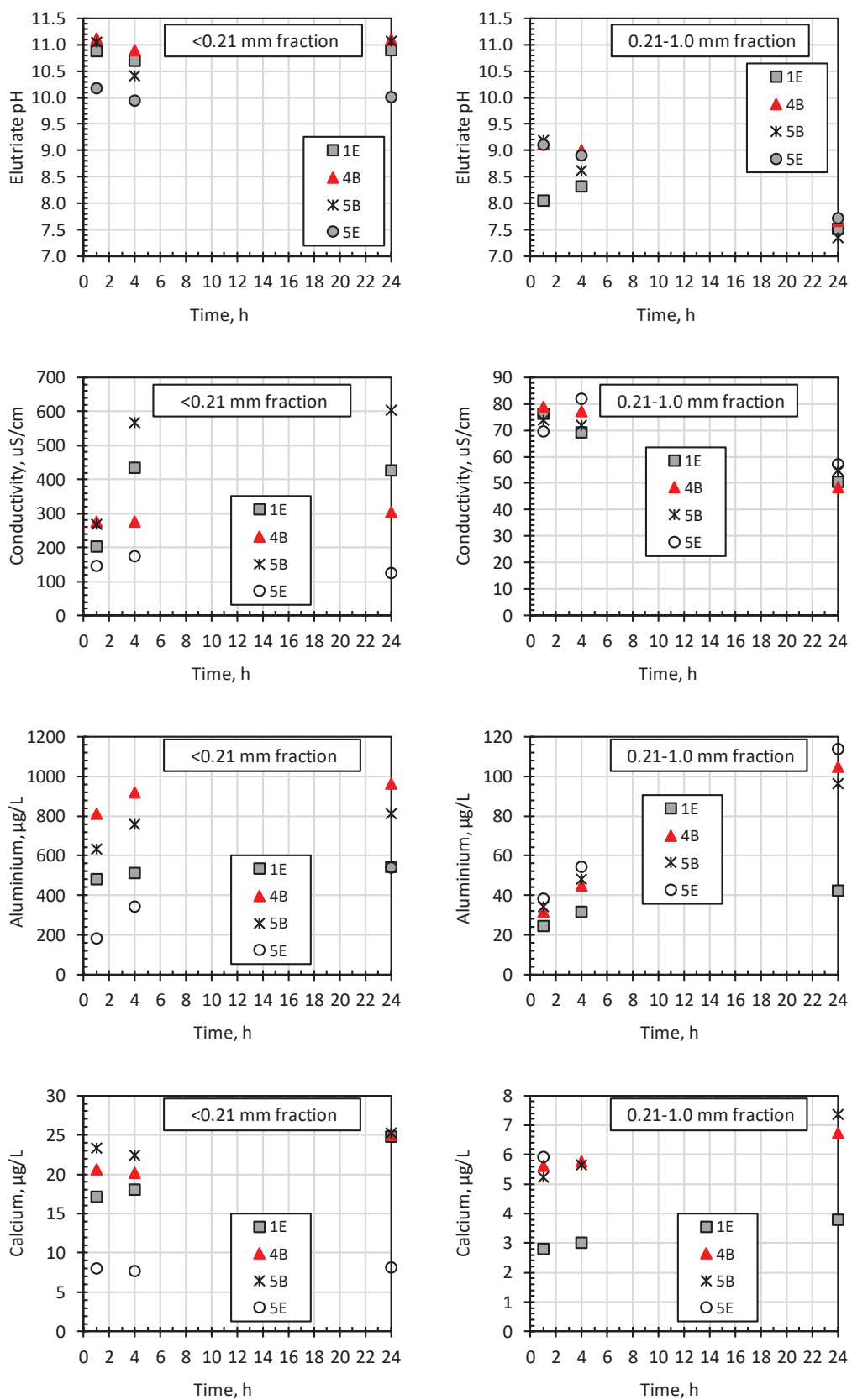


Figure 7. Effect of elutriate time on pH, conductivity and dissolved aluminium and calcium for the two smaller rock size fractions (<0.21 mm and 0.21-2 mm).

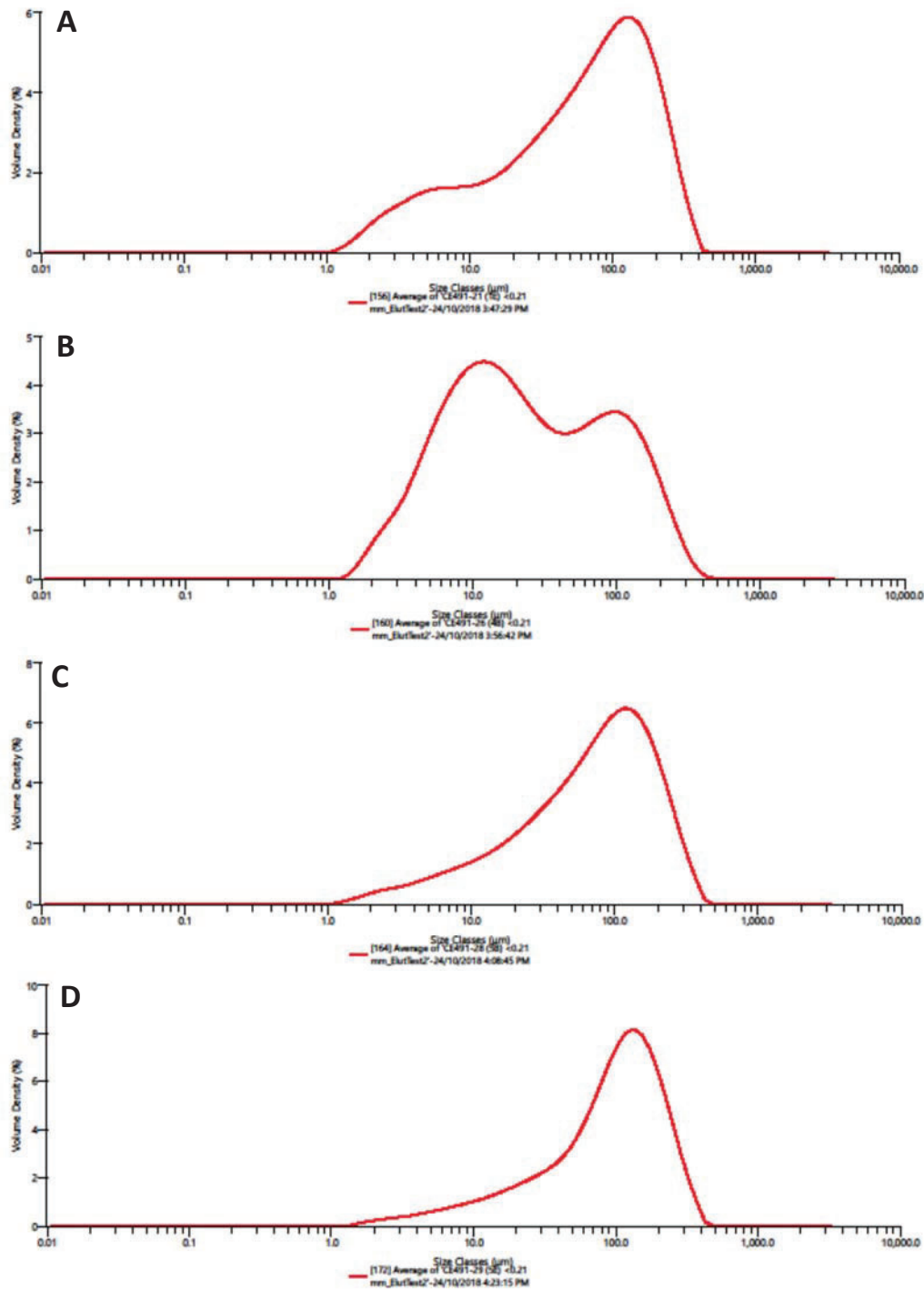


Figure 8. The particle size distribution of the <0.21 mm sieved fraction of samples 1E (A), 4B (B), 5B (C) and 5E (D).

Table 1. The particle size distribution of the <0.21 mm fraction used in grain size test

| Sample Name | Dv (10) (μm) | Dv (50) (μm) | Dv (90) (μm) | Mean diameter (μm) |
|--------------------|---|---|---|---|
| 1E, <0.21 mm | 5.93 | 66.3 | 206 | 88.3 |
| 4B, <0.21 mm | 4.71 | 21.5 | 140 | 50.3 |
| 5B, <0.21 mm | 10.7 | 75.6 | 210 | 95.3 |
| 5E, <0.21 mm | 16 | 99.6 | 228 | 113 |

Note: Dv (x) refers to 10, 50 and 90th percentiles of particle diameters (on spherical volume basis)

| | |
|------------------|---|
| Note/Memo | CSIRO P4 Project Investigations |
| To: | Ali Watters (HKA) |
| From: | Brad Angel, Lucas Heights, NSW |
| Date: | 5 November 2018 |
| Copy: | Ryan Fraser, Stuart Simpson and Ellen Porter (SHL) |
| Our reference: | CSIRO P4 – Memo 8 |
| Classification: | Internal use only |
| Subject: | Pollutant release from excavated rock composites – fine grain size effect |

Chemical formulas and acronyms

| | | | | | |
|-----------------|--------------------------|------------------------------|-------------------------|-------------------------------|--------------------|
| Ag | Silver | F ⁻ | Fluoride | Sb | Antimony |
| Al | Aluminium | Fe | Iron | Se | Selenium |
| As | Arsenic | Mg | Magnesium | Sn | Tin |
| Ba | Barium | Mn | Manganese | SO ₄ ²⁻ | Sulfate |
| Ca | Calcium | Mo | Molybdenum | Sr | Strontium |
| Cd | Cadmium | Na | Sodium | Th | Thorium |
| Cl ⁻ | Chloride | Ni | Nickel | U | Uranium |
| Co | Cobalt | NO ₃ ⁻ | Nitrate | V | Vanadium |
| Cr | Chromium | Pb | Lead | Zn | Zinc |
| Cu | Copper | | | | |
| DOC | Dissolved organic carbon | DGV | Default guideline value | L/S | Liquid/solid ratio |
| SEC | Conductivity | | | | |

Background - Introduction

The CSIRO was engaged by Haskoning Australia Pty Ltd (RHDHV) to undertake an investigation of the pollutant release from excavated rock disposal into Talbingo and Tantangara reservoirs. Previous elutriate testing that investigated the effect of excavated rock grain size; >10,000 µm, 2,000-10,000 µm, 210-2,000 µm and <210 µm (referred to as >10 mm; 2-10 mm, 0.21-2 mm and <0.21 mm in Memo 6) found the finer <210 µm rock fraction is likely to have an impact on water quality that is an order of magnitude greater than that of rock fractions >2000 µm in size. This testing was conducted at a liquid to solid ratio of 25 (i.e. 40 g/L). It is envisaged that the design of the excavated rock placement will result in fast deposition of the majority of the excavated rock, and concentrations of fine materials within the waters will be managed to achieve considerably lower concentrations of suspended solids. However, due to the much larger effect of the <210 µm rock fraction on water pH, conductivity and dissolved aluminium concentrations and the likelihood of fine material requiring special handling / treatment, an additional investigation of the effect of finer (sub 210 µm) excavated rock fractions on water quality was performed.

This technical memo describes results of elutriate tests performed on three different excavated rock materials that had been mechanically crushed and sieved to provide materials with the size categories 150-210, 63-150 and <63 µm (composite fine material). The tests were performed by resuspending sieved fractions of composites 1B, 4B and 5E in Talbingo water at a liquid to solid ratio of 1000.

Preparation of rock materials in different size ranges

For the elutriate tests, the 1B, 4B and 5E sieved materials (rock and water) were shaken briefly and then rolled for 30 min on a purpose built bottle roller (~50 rpm) to continually mix the water and solids of that

period. The containers were then placed upright to allow the materials to settle until the time that measurements were performed; measurement of pH, conductivity and dissolved analytes (filtered <0.45 µm) 24 h after water initially added.

Results - Influence of rock material size (and time) on elutriate pH, conductivity and dissolved analytes

The pH, conductivity and dissolved analyte concentrations measured in the elutriate solutions generated from the three size fractions of each excavated rock sample in Talbingo water for elutriate tests lasting 24 h at L/S = 1000 are shown in Figure 1. The concentrations of dissolved major ions (Na, K, Mg, Ca) for each as a function of the size of the rock materials are shown in Figure 2. Data has been generated from these tests for a range of other analytes, but results shown in this memo focus on dissolved aluminium owing to the concentrations exceeding the default guideline value (DVG) of 55 µg/L.

The particle size distribution of the <210 µm size fraction (previously shown in memo 6) is shown in Figure 3 and Table 1 for the purpose of interpreting the importance of the findings for this test.

The pH, conductivity and dissolved aluminium all decreased as the size fraction increased. However, the pH, conductivity and dissolved aluminium exhibited linear decreases as the particle size increased rather than exponential, as observed for sizes between >10,000 µm to <210 µm (Memo 6).

Points to note:

- pH range of 7.84 to 9.68 was similar to most previous results when considering the liquid to solid ratio of 1000, and not as high as for some treatments in memo 6.
- Conductivity range of 38 to 99 µS/cm, was similar to most previous results when considering the liquid to solid ratio of 1000. The pattern is consistent with Ca, followed by Na being the major contributors to the increased water conductivity, with K and Mg contributing less (Figure 1).
- The dissolved aluminium exceeded the DVG of 55 µg/L by a factor of 4.2 to 1.1 for the <63 and 63-150 µm size fractions, and was below the DVG for the 150-210 µm size fraction (Figure 1).
- The dissolved calcium and potassium decreased as the size fraction increased, but the decreases were not as steep as for dissolved aluminium, while the dissolved magnesium and sodium were generally similar for the different size fractions (Figure 2).
- Particle size distribution of <210 µm size fraction: The <210 µm samples had particle diameters that generally spanned the 0-210 µm range. Sample 4B (<210 µm) was the finest with 50% of the sample being <21.5 µm. The other samples comprised approximately 50% silt, i.e. approximately 50% <63 µm.

Summary

The pH, conductivity and dissolved aluminium decreased as the particle size increased from <63 µm to 150-210 µm, however, the decrease was essentially linear rather than exponential, as observed for 210 µm to >10,000 µm fractions in memo 6.

For a liquid to solid ratio of 1000, the dissolved aluminium released from the <63 µm size fraction exceeded the DVG after 24 h. For the 63-150 µm, there was a much smaller exceedance of the DVG.

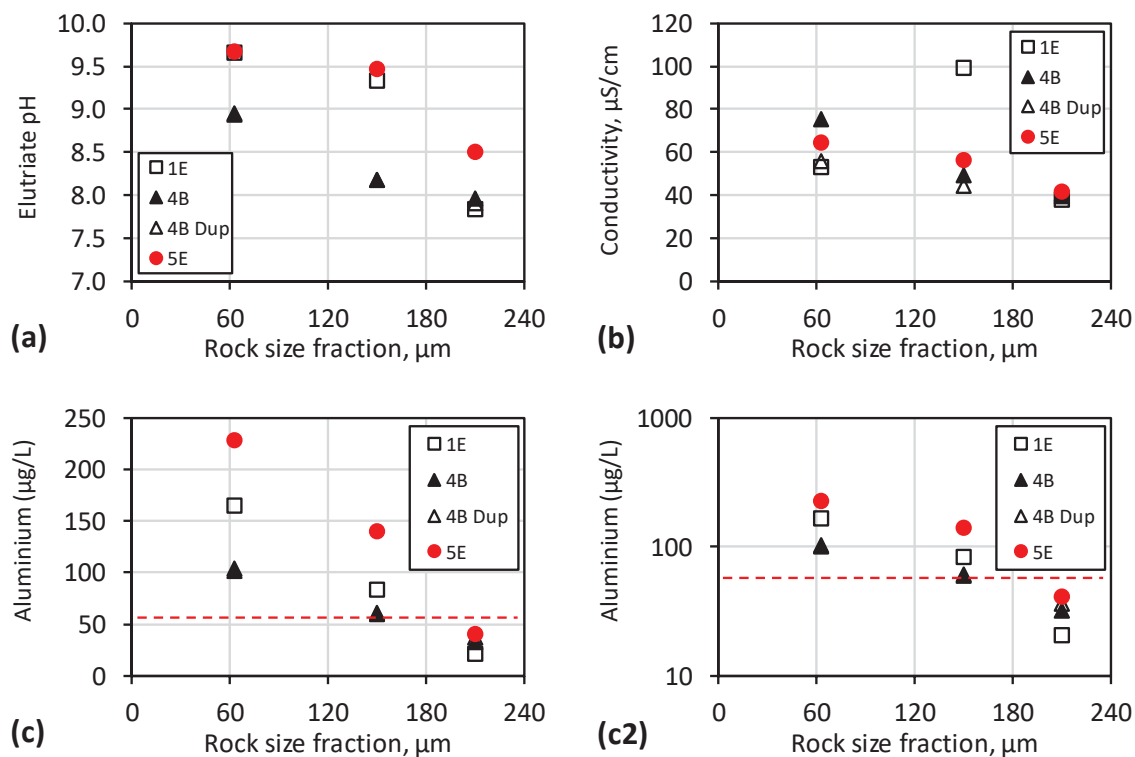


Figure 1. The pH (a), conductivity (b) and dissolved aluminium (c, c2) after an elutriate time of 24 h (c2 = log scale) for <63, 63-150 and 150-210 μm size fractions.

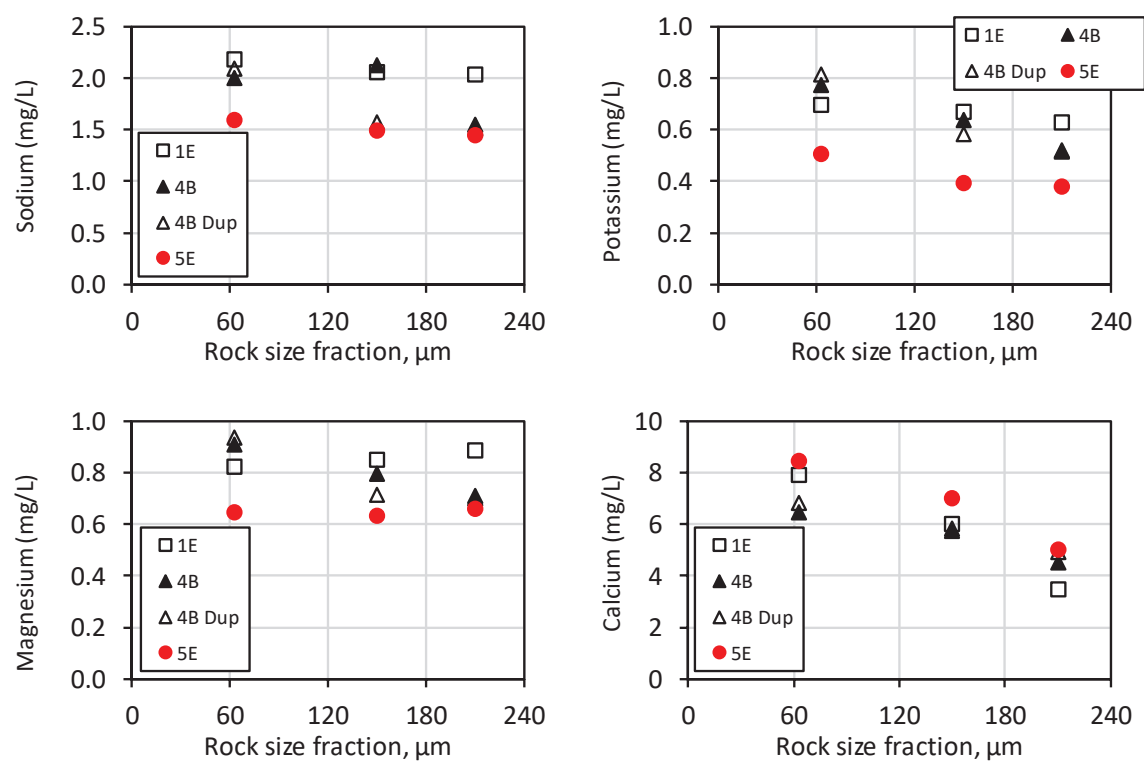


Figure 2. Dissolved major ions (Na, K, Mg, Ca) after an elutriate time of 24 h for <63, 63-150 and 150-210 μm size fractions.

Table 1. The particle size distribution of the <210 μm fraction used in grain size test

| Sample Name | Dv (10) (μm) | Dv (50) (μm) | Dv (90) (μm) | Mean diameter (μm) |
|------------------------|------------------------------|------------------------------|------------------------------|------------------------------------|
| 1E, <210 μm | 5.93 | 66.3 | 206 | 88.3 |
| 4B, <210 μm | 4.71 | 21.5 | 140 | 50.3 |
| 5B, <210 μm | 10.7 | 75.6 | 210 | 95.3 |
| 5E, <210 μm | 16 | 99.6 | 228 | 113 |

Note: Dv (x) refers to 10, 50 and 90th percentiles of particle diameters (on spherical volume basis)

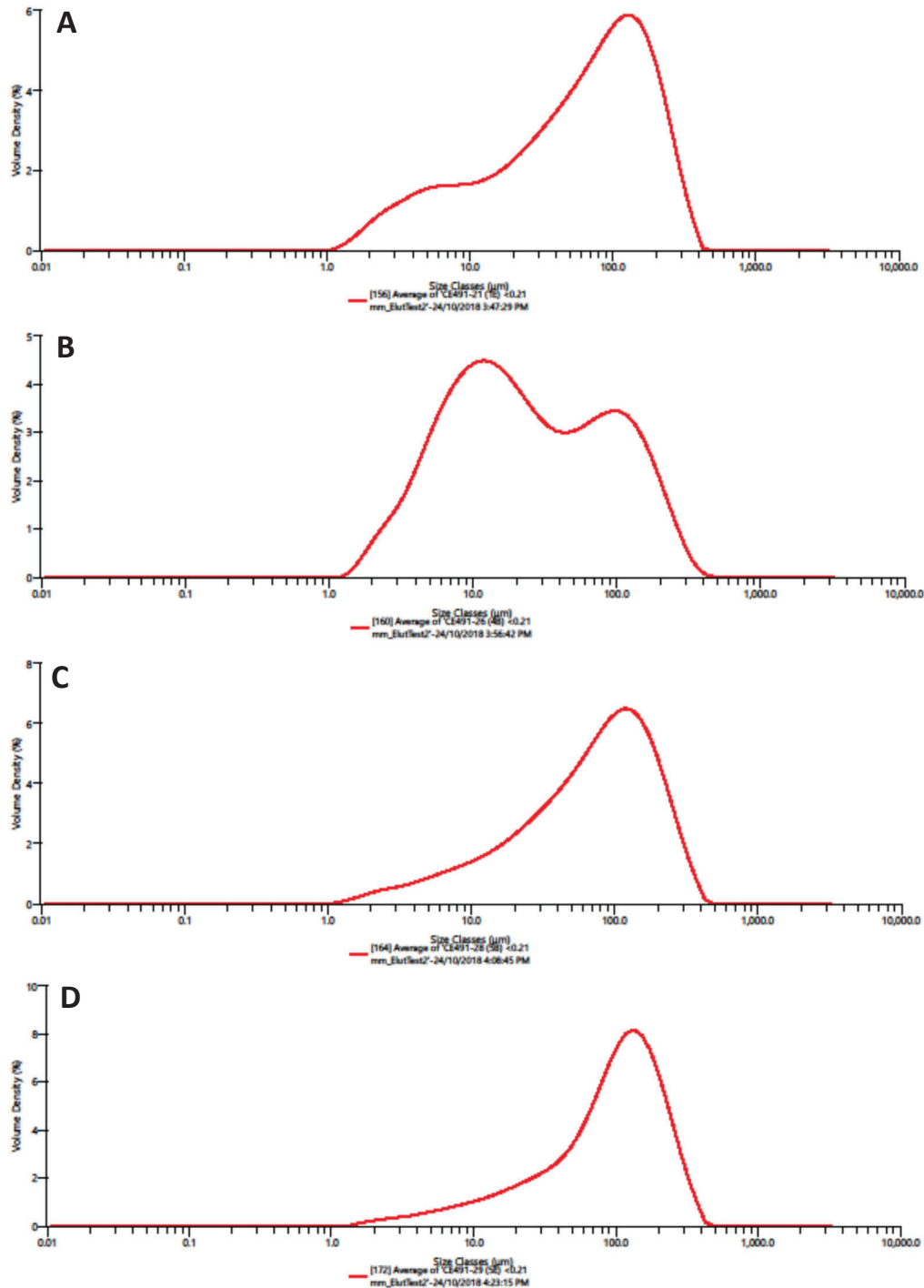


Figure 3. The particle size distribution of the <210 μm sieved fraction of samples 1E (A), 4B (B), 5B (C) and 5E (D).

Appendix D4. Effect of rock particle size in on substance release
Memo 6 (26 October 2018).

Spike Recoveries

| Sample Name | Sample ID | Sample Desc. | Particle Size | Time | | | | Ag | Al | As | Ba | Ca | Cd | Co | Cr | Cu | Fe | K | Mg | Mn | Mo | Na | Ni | Pb | Sb | Se | Sn | Sr | Th | U | V | Zn |
|-------------|----------------|--------------|---------------|-------|-----|-----|-----|-----|-----|-----|----|-----|-----|----|----|-----|-----|-----|-----|-----|-----|-----|----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| T1-10 | CE491-29 rep-1 | 5E rep-1 | >10 mm | 1 hr | --- | --- | --- | 96 | 102 | 99 | 99 | 112 | 102 | 99 | 99 | 100 | 101 | 100 | 99 | 101 | 97 | 101 | 99 | 99 | 96 | 101 | 97 | 103 | 104 | 100 | 100 | 102 |
| T1-20 | CE491-28 rep-2 | 5B rep-2 | >10 mm | 4 hr | --- | --- | --- | 95 | 95 | 94 | 98 | 112 | 96 | 97 | 96 | 97 | 95 | 99 | 97 | 97 | 98 | 95 | 97 | 99 | 97 | 94 | 98 | 101 | 104 | 99 | 99 | 101 |
| T1-30 | CE491-26 rep-3 | 4B rep-3 | >10 mm | 24 hr | --- | --- | --- | 94 | 99 | 94 | 95 | 114 | 101 | 93 | 96 | 95 | 100 | 100 | 101 | 101 | 98 | 103 | 95 | 98 | 95 | 101 | 98 | 98 | 101 | 98 | 94 | 96 |
| T1-40 | CE491-26 rep-1 | 4B rep-1 | 2-10 mm | 1 hr | --- | --- | --- | 93 | 91 | 95 | 99 | 108 | 92 | 98 | 96 | 97 | 92 | 103 | 102 | 92 | 95 | 104 | 99 | 96 | 94 | 91 | 94 | 99 | 99 | 96 | 96 | 95 |
| T1-50 | CE491-21 rep-2 | 1E rep-2 | 2-10 mm | 4 hr | --- | --- | --- | 95 | 97 | 96 | 92 | 85 | 96 | 93 | 93 | 95 | 95 | 88 | 84 | 96 | 98 | 84 | 94 | 98 | 96 | 93 | 98 | 96 | 102 | 98 | 92 | 93 |
| T1-60 | CE491-29 rep-3 | 5E rep-3 | 2-10 mm | 4 hr | --- | --- | --- | 96 | 95 | 96 | 97 | 101 | 96 | 97 | 95 | 97 | 96 | 98 | 99 | 96 | 97 | 104 | 97 | 99 | 97 | 93 | 100 | 99 | 103 | 97 | 94 | 94 |
| T1-70 | CE491-29 rep-1 | 5E rep-1 | 2-10 mm | 24 hr | --- | --- | --- | 95 | 96 | 97 | 97 | 104 | 96 | 98 | 97 | 97 | 96 | 98 | 101 | 97 | 99 | 103 | 96 | 98 | 96 | 94 | 99 | 101 | 101 | 96 | 96 | 100 |
| T1-80 | CE491-28 rep-2 | 5B rep-2 | 0.25 - 2 mm | 1 hr | --- | --- | --- | 95 | 99 | 97 | 98 | 102 | 99 | 97 | 97 | 98 | 100 | 97 | 98 | 99 | 99 | 102 | 96 | 98 | 96 | 96 | 99 | 99 | 99 | 96 | 95 | 95 |
| T1-84 | CE491-29 rep-3 | 5E rep-3 | 0.25 - 2 mm | 1 hr | --- | --- | --- | 95 | 96 | 100 | 98 | 103 | 97 | 98 | 98 | 99 | 97 | 100 | 99 | 97 | 100 | 101 | 97 | 98 | 95 | 95 | 98 | 100 | 101 | 98 | 97 | 95 |
| T1-90 | CE491-28 rep-1 | 5B rep-1 | 0.25 - 2 mm | 4 hr | --- | --- | --- | 94 | 94 | 95 | 99 | 97 | 95 | 97 | 96 | 99 | 96 | 100 | 96 | 96 | 98 | 101 | 96 | 98 | 95 | 93 | 98 | 101 | 101 | 97 | 98 | 87 |
| T1-109 | CE491-21 rep-2 | 1E rep-2 | <0.21 mm | 1 hr | --- | --- | --- | 103 | 103 | 92 | 96 | 115 | 94 | 95 | 95 | 94 | 94 | 103 | 100 | 94 | 96 | 105 | 93 | 107 | 105 | 90 | 107 | 94 | 110 | 109 | 95 | 92 |
| T1-106 | CE491-29 rep-2 | 5E rep-2 | 0.25 - 2 mm | 24 hr | --- | --- | --- | 95 | 93 | 96 | 97 | 103 | 97 | 97 | 98 | 100 | 96 | 101 | 99 | 95 | 99 | 100 | 97 | 98 | 96 | 95 | 99 | 104 | 103 | 98 | 97 | 99 |
| T1-124 | CE491-26 rep-2 | 4B rep-2 | <0.21 mm | 4 hr | --- | --- | --- | 91 | 89 | 88 | 95 | 126 | 92 | 94 | 94 | 95 | 94 | 103 | 102 | 93 | 94 | 110 | 93 | 94 | 92 | 90 | 97 | 98 | 99 | 95 | 95 | 94 |

Certified Reference Materials

| Sample Name | | | | | Ag | Al | As | Ba | Ca | Cd | Co | Cr | Cu | Fe | K | Mg | Mn | Mo | Na | Ni | Pb | Sb | Se | Sn | Sr | Th | U | V | Zn | |
|-----------------|-----|-----|-----|-----|------|------------|-------------|------------|----------|-------------|-------------|-------------|-------------|------------|-----|-----|-------------|-------------|-----|-------------|-------------|----------|-------------|-------------|----------|-------------|-------------|----------|----------|-----|
| TM24.4 (n=3) | --- | --- | --- | --- | --- | 32.7 | 4.96 | 14.7 | --- | 3.83 | 6.54 | 4.98 | 6.65 | 15.2 | --- | --- | 7.99 | 6.13 | --- | 5.16 | 5.70 | --- | 3.39 | 3.72 | 116 | --- | 4.23 | 6.91 | --- | --- |
| Certified Value | | | | | | 32.9 ± 4.5 | 5.30 ± 0.53 | 15.0 ± 1.0 | | 3.96 ± 0.34 | 6.27 ± 0.57 | 5.00 ± 0.59 | 6.31 ± 0.60 | 16.0 ± 2.3 | | | 8.24 ± 0.73 | 6.30 ± 0.56 | | 5.03 ± 0.53 | 5.60 ± 0.52 | | 3.56 ± 0.58 | 3.72 ± 0.39 | | 4.24 ± 0.34 | 7.00 ± 0.58 | | --- | |
| Recovery (%) | | | | | | --- | 99 | 94 | 98 | 97 | 104 | 100 | 105 | 95 | --- | --- | 97 | 97 | --- | 103 | 102 | --- | 95 | 100 | 103 | --- | 100 | 99 | --- | --- |
| TM-DA64.3 (n=3) | --- | --- | --- | --- | 11.9 | 291 | 156 | 281 | --- | 247 | 247 | 274 | 257 | 281 | --- | --- | 276 | 279 | --- | 245 | 276 | 121 | 142 | 267 | 633 | --- | 131 | 273 | 324 | |
| Certified Value | | | | | | 12.6 ± 1.3 | 291 ± 23 | 164 ± 15 | 287 ± 18 | 258 ± 21 | 250 ± 16 | 283 ± 17 | 261 ± 18 | 298 ± 21 | | | 292 ± 17 | 286 ± 21 | | 252 ± 18 | 280 ± 22 | 124 ± 11 | 154 ± 2.2 | 281 ± 25 | 628 ± 34 | | 135 ± 11 | 279 ± 18 | 320 ± 23 | |
| Recovery (%) | | | | | | 94 | 100 | 95 | 98 | 96 | 99 | 97 | 99 | 94 | --- | --- | 95 | 97 | --- | 97 | 99 | 98 | 92 | 95 | 101 | --- | 97 | 98 | 101 | |

Method Codes:

C-209: ICP-MS

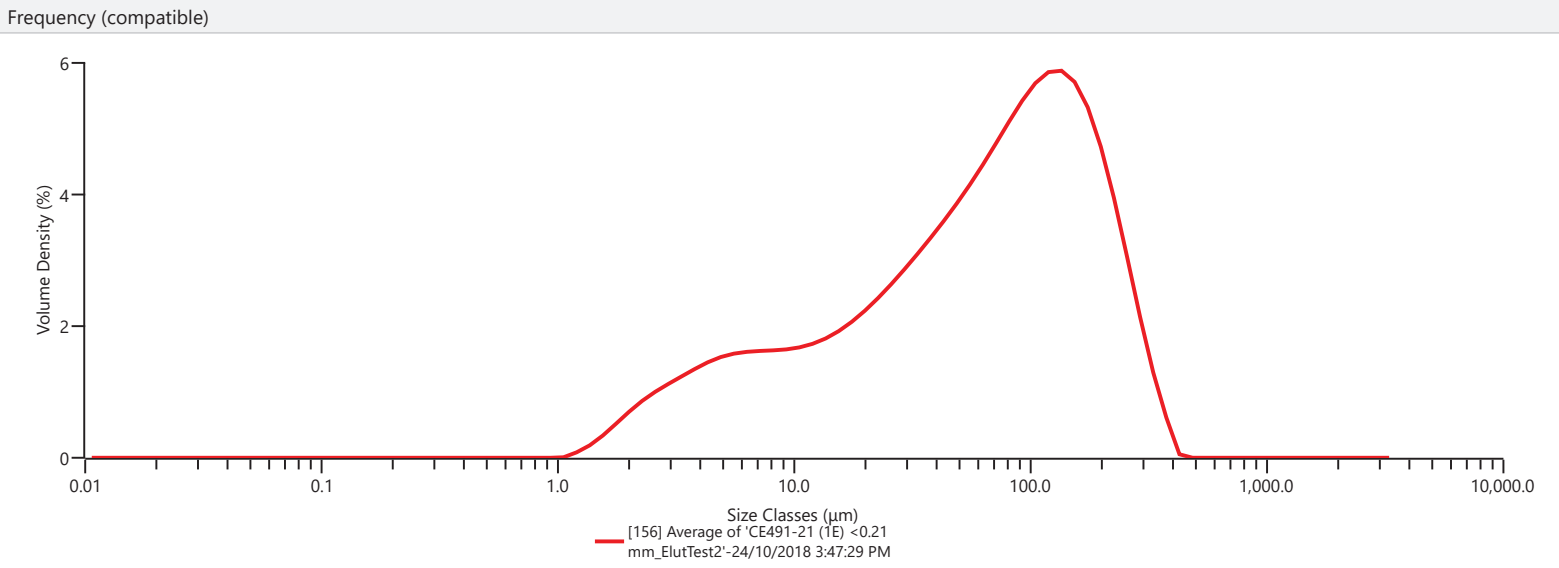
C-229: ICP-AES

C-240: Determination of pH

C-255: Conductivity

Analysis

| | |
|--|--|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 24/10/2018 3:47:29 PM |
| Sample Name Average of 'CE491-21 (1E) <0.21 mm_ElutTest2' | Measurement Date Time 24/10/2018 3:47:29 PM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0221 % |
| Particle Refractive Index 1.555 | Span 3.015 |
| Particle Absorption Index 0.010 | Uniformity 0.947 |
| Dispersant Name Water | Specific Surface Area 340.4 m²/kg |
| Dispersant Refractive Index 1.330 | D [3,2] 17.6 µm |
| Scattering Model Mie | D [4,3] 88.3 µm |
| Analysis Model General Purpose | Dv (10) 5.93 µm |
| Weighted Residual 0.35 % | Dv (50) 66.3 µm |
| Laser Obscuration 10.65 % | Dv (90) 206 µm |



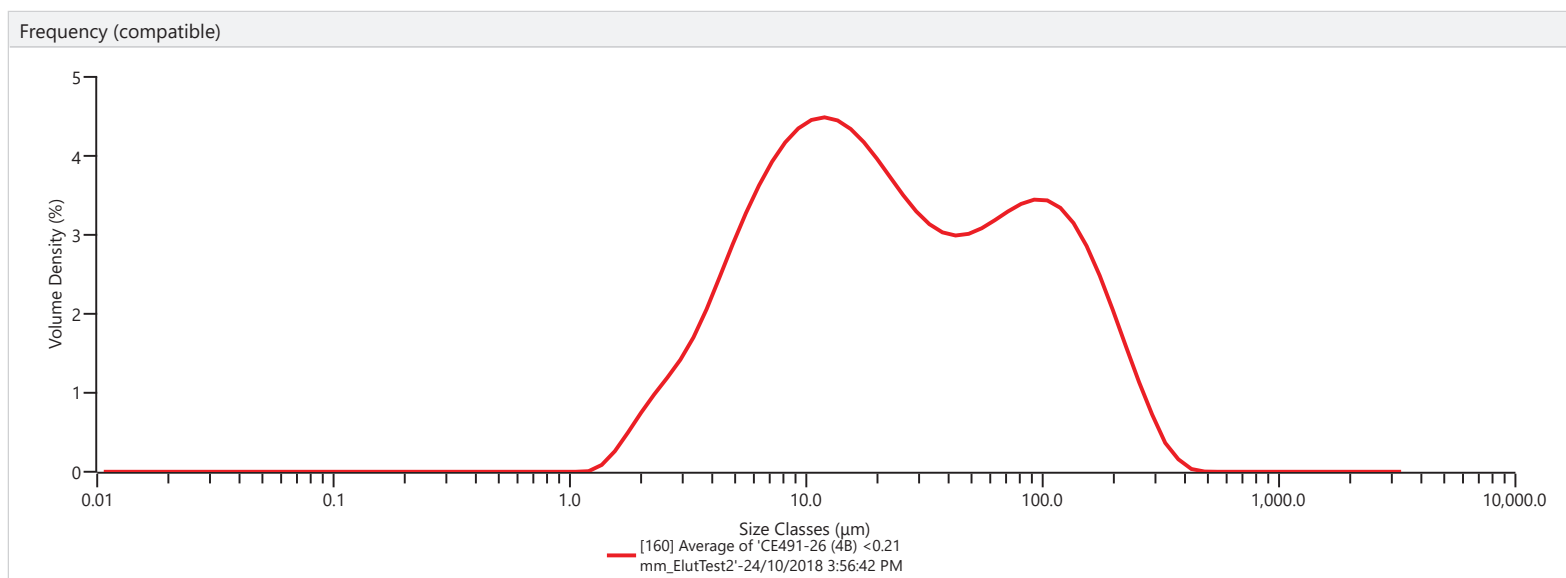
| Result | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Size (µm) | % Volume Under | Size (µm) | % Volume Under | Size (µm) | % Volume Under | Size (µm) | % Volume Under | Size (µm) | % Volume Under | Size (µm) | % Volume Under | Size (µm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 1.52 | 12.7 | 18.24 | 76.0 | 54.26 | 454 | 100.00 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 2.24 | 14.5 | 19.75 | 86.4 | 58.52 | 516 | 100.00 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 3.08 | 16.4 | 21.35 | 98.1 | 63.05 | 586 | 100.00 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.00 | 3.12 | 4.01 | 18.7 | 23.07 | 111 | 67.80 | 666 | 100.00 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.00 | 3.55 | 5.04 | 21.2 | 24.93 | 127 | 72.69 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.00 | 4.03 | 6.16 | 24.1 | 26.95 | 144 | 77.61 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 0.00 | 4.58 | 7.37 | 27.4 | 29.15 | 163 | 82.39 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 0.00 | 5.21 | 8.65 | 31.1 | 31.54 | 186 | 86.84 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 0.00 | 5.92 | 9.97 | 35.3 | 34.11 | 211 | 90.80 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 0.00 | 6.72 | 11.32 | 40.1 | 36.90 | 240 | 94.10 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 0.07 | 7.64 | 12.67 | 45.6 | 39.89 | 272 | 96.65 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 0.22 | 8.68 | 14.03 | 51.8 | 43.11 | 310 | 98.42 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 0.50 | 9.86 | 15.40 | 58.9 | 46.57 | 352 | 99.49 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 0.93 | 11.2 | 16.80 | 66.9 | 50.28 | 400 | 100.00 | 2390 | 100.00 |

| Measurement Details | |
|----------------------|---|
| Operator Name | CSIRO Mastersizer |
| Sample Name | Average of 'CE491-26 (4B) <0.21 mm_ElutTest2' |
| SOP File Name | Sediment Sonnication_SOP.msop |

| Measurement Details | |
|------------------------------|-----------------------|
| Analysis Date Time | 24/10/2018 3:56:42 PM |
| Measurement Date Time | 24/10/2018 3:56:42 PM |
| Result Source | Averaged |

| Analysis | |
|-----------------------------|-----------------|
| Particle Name | China Clay |
| Particle Refractive Index | 1.555 |
| Particle Absorption Index | 0.010 |
| Dispersant Name | Water |
| Dispersant Refractive Index | 1.330 |
| Scattering Model | Mie |
| Analysis Model | General Purpose |
| Weighted Residual | 0.49 % |
| Laser Obscuration | 8.43 % |

| Result |
|---|
| Concentration 0.0120 % |
| Span 6.300 |
| Uniformity 1.886 |
| Specific Surface Area 505.9 m ² /kg |
| D [3,2] 11.9 μm |
| D [4,3] 50.3 μm |
| Dv (10) 4.71 μm |
| Dv (50) 21.5 μm |
| Dv (90) 140 μm |



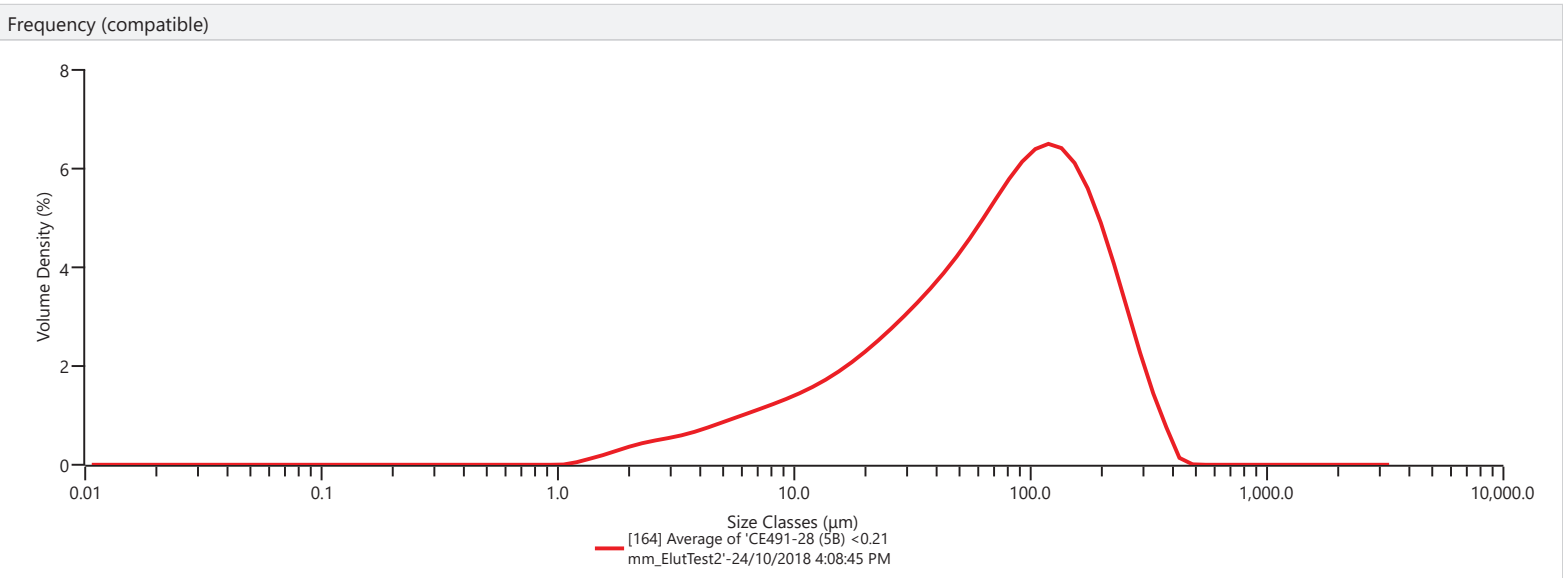
Analysis

| |
|--|
| Measurement Details |
| Operator Name CSIRO Mastersizer |
| Sample Name Average of 'CE491-28 (5B) <0.21 mm_ElutTest2' |
| SOP File Name Sediment Sonnication_SOP.msop |

| |
|--|
| Analysis |
| Particle Name China Clay |
| Particle Refractive Index 1.555 |
| Particle Absorption Index 0.010 |
| Dispersant Name Water |
| Dispersant Refractive Index 1.330 |
| Scattering Model Mie |
| Analysis Model General Purpose |
| Weighted Residual 0.37 % |
| Laser Obscuration 5.94 % |

| |
|--|
| Measurement Details |
| Analysis Date Time 24/10/2018 4:08:45 PM |
| Measurement Date Time 24/10/2018 4:08:45 PM |
| Result Source Averaged |

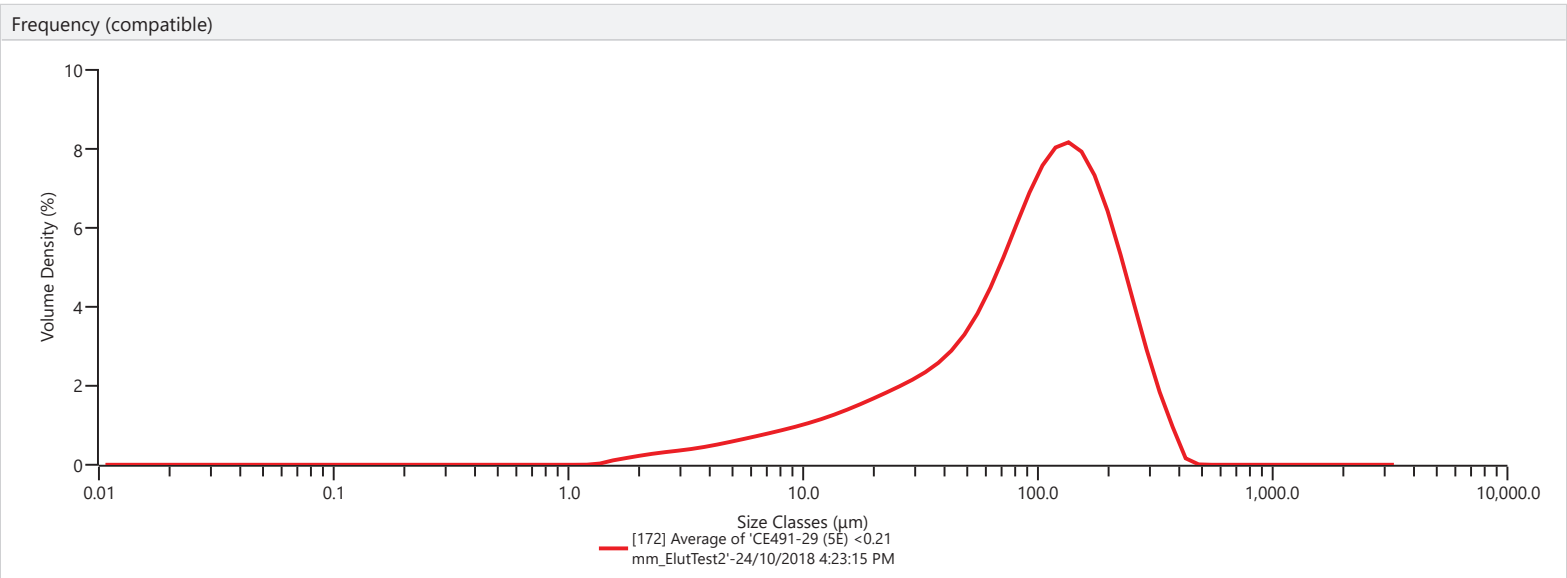
| |
|--|
| Result |
| Concentration 0.0176 % |
| Span 2.634 |
| Uniformity 0.821 |
| Specific Surface Area 239.3 m²/kg |
| D [3,2] 25.1 µm |
| D [4,3] 95.3 µm |
| Dv (10) 10.7 µm |
| Dv (50) 75.6 µm |
| Dv (90) 210 µm |



| | | | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Result | | | | | | | | | | | | | |
| Size (µm) | % Volume Under | Size (µm) | % Volume Under | Size (µm) | % Volume Under | Size (µm) | % Volume Under | Size (µm) | % Volume Under | Size (µm) | % Volume Under | Size (µm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 0.84 | 12.7 | 11.70 | 76.0 | 50.18 | 454 | 100.00 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 1.21 | 14.5 | 13.14 | 86.4 | 55.01 | 516 | 100.00 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 1.62 | 16.4 | 14.71 | 98.1 | 60.14 | 586 | 100.00 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.00 | 3.12 | 2.07 | 18.7 | 16.44 | 111 | 65.48 | 666 | 100.00 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.00 | 3.55 | 2.57 | 21.2 | 18.35 | 127 | 70.92 | 756 | 100.00 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.00 | 4.03 | 3.12 | 24.1 | 20.45 | 144 | 76.28 | 859 | 100.00 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 0.00 | 4.58 | 3.75 | 27.4 | 22.74 | 163 | 81.39 | 976 | 100.00 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 0.00 | 5.21 | 4.46 | 31.1 | 25.26 | 186 | 86.07 | 1110 | 100.00 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 0.00 | 5.92 | 5.24 | 35.3 | 27.99 | 211 | 90.17 | 1260 | 100.00 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 0.00 | 6.72 | 6.11 | 40.1 | 30.97 | 240 | 93.57 | 1430 | 100.00 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 0.04 | 7.64 | 7.05 | 45.6 | 34.20 | 272 | 96.21 | 1630 | 100.00 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 0.14 | 8.68 | 8.07 | 51.8 | 37.72 | 310 | 98.10 | 1850 | 100.00 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 0.30 | 9.86 | 9.19 | 58.9 | 41.54 | 352 | 99.29 | 2100 | 100.00 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 0.54 | 11.2 | 10.39 | 66.9 | 45.69 | 400 | 99.92 | 2390 | 100.00 |

Analysis

| | |
|--|--|
| Measurement Details | Measurement Details |
| Operator Name CSIRO Mastersizer | Analysis Date Time 24/10/2018 4:23:15 PM |
| Sample Name Average of 'CE491-29 (5E) <0.21 mm_ElutTest2' | Measurement Date Time 24/10/2018 4:23:15 PM |
| SOP File Name Sediment Sonnication_SOP.msop | Result Source Averaged |
| Analysis | Result |
| Particle Name China Clay | Concentration 0.0307 % |
| Particle Refractive Index 1.555 | Span 2.130 |
| Particle Absorption Index 0.010 | Uniformity 0.652 |
| Dispersant Name Water | Specific Surface Area 175.6 m²/kg |
| Dispersant Refractive Index 1.330 | D [3,2] 34.2 µm |
| Scattering Model Mie | D [4,3] 113 µm |
| Analysis Model General Purpose | Dv (10) 16.0 µm |
| Weighted Residual 0.49 % | Dv (50) 99.6 µm |
| Laser Obscuration 7.40 % | Dv (90) 228 µm |



| Result | | | | | | | | | | | |
|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|-----------|----------------|
| Size (µm) | % Volume Under | Size (µm) | % Volume Under | Size (µm) | % Volume Under | Size (µm) | % Volume Under | Size (µm) | % Volume Under | Size (µm) | % Volume Under |
| 0.0100 | 0.00 | 0.0597 | 0.00 | 0.357 | 0.00 | 2.13 | 0.45 | 12.7 | 8.04 | 76.0 | 38.44 |
| 0.0114 | 0.00 | 0.0679 | 0.00 | 0.405 | 0.00 | 2.42 | 0.68 | 14.5 | 9.10 | 86.4 | 43.52 |
| 0.0129 | 0.00 | 0.0771 | 0.00 | 0.460 | 0.00 | 2.75 | 0.95 | 16.4 | 10.26 | 98.1 | 49.27 |
| 0.0147 | 0.00 | 0.0876 | 0.00 | 0.523 | 0.00 | 3.12 | 1.24 | 18.7 | 11.54 | 111 | 55.61 |
| 0.0167 | 0.00 | 0.0995 | 0.00 | 0.594 | 0.00 | 3.55 | 1.57 | 21.2 | 12.94 | 127 | 62.33 |
| 0.0189 | 0.00 | 0.113 | 0.00 | 0.675 | 0.00 | 4.03 | 1.95 | 24.1 | 14.46 | 144 | 69.16 |
| 0.0215 | 0.00 | 0.128 | 0.00 | 0.767 | 0.00 | 4.58 | 2.37 | 27.4 | 16.12 | 163 | 75.80 |
| 0.0244 | 0.00 | 0.146 | 0.00 | 0.872 | 0.00 | 5.21 | 2.86 | 31.1 | 17.91 | 186 | 81.93 |
| 0.0278 | 0.00 | 0.166 | 0.00 | 0.991 | 0.00 | 5.92 | 3.40 | 35.3 | 19.86 | 211 | 87.31 |
| 0.0315 | 0.00 | 0.188 | 0.00 | 1.13 | 0.00 | 6.72 | 4.00 | 40.1 | 22.01 | 240 | 91.75 |
| 0.0358 | 0.00 | 0.214 | 0.00 | 1.28 | 0.00 | 7.64 | 4.67 | 45.6 | 24.41 | 272 | 95.17 |
| 0.0407 | 0.00 | 0.243 | 0.00 | 1.45 | 0.02 | 8.68 | 5.40 | 51.8 | 27.15 | 310 | 97.59 |
| 0.0463 | 0.00 | 0.276 | 0.00 | 1.65 | 0.12 | 9.86 | 6.20 | 58.9 | 30.33 | 352 | 99.12 |
| 0.0526 | 0.00 | 0.314 | 0.00 | 1.88 | 0.26 | 11.2 | 7.08 | 66.9 | 34.07 | 400 | 99.92 |

Appendix D5. Comparison between leaching in Talbingo and Tantangara waters

| | |
|------------------|--|
| Note/Memo | CSIRO P4 Project Investigations |
| To: | Ali Watters (HKA) |
| From: | Brad Angel, Lucas Heights, NSW |
| Date: | 26 November 2018 |
| Copy: | Ryan Fraser, Stuart Simpson and Ellen Porter (SHL) |
| Our reference: | CSIRO P4 – Memo 13 |
| Classification: | Internal use only |
| Subject: | Elutriate test with Tantangara reservoir water investigating effect on water quality and pollutant release |

Chemical formulas and acronyms

| | | | | | |
|-----|--------------|-----|-------------------------|-----|--------------------|
| Al | Aluminium | DGV | Default guideline value | L/S | Liquid/solid ratio |
| SEC | Conductivity | | | | |

Background - Introduction

The CSIRO was engaged by Haskoning Australia Pty Ltd (RHDHV) to undertake an investigation of the effect on water quality of excavated rock disposal into the Talbingo and Tantangara reservoirs. Previous elutriate tests performed to date for this assessment have utilised Talbingo reservoir water, and have observed significant changes in water quality with respect to pH, conductivity (SEC) and the dissolved aluminium concentrations.

This technical memo describes results of elutriate tests performed in Tantangara reservoir water with five different excavated rock composite materials that had been milled to <75 µm. Comparison is made with results for matching tests performed using Talbingo reservoir water.

Test methodology

The 75-µm milled composites 1B, 2B, 5B, 5E and 7E characterised in Memo 3 were used in the elutriate tests in Tantangara reservoir water. The tests were performed at liquid to solid (L/S) ratios of 300 and 1000, which were equivalent to 3.3 and 1 g/L, respectively. The material was weighed into plastic vials to which Tantangara water at 21°C was added. The treatments were shaken (50 rpm) for 30 mins then allowed to stand at 21±2°C for the remaining duration so that they were in water for 3 and 18 h. The Tantangara reservoir elutriate treatments in this test were compared with Talbingo treatments from previous tests at the same L/S ratio and duration to assess if different reservoir waters cause differences in effects on water quality and pollutant release.

Results

A comparison of the pH, conductivity and dissolved aluminium for composites 1B, 2B, 5B, 5E and 7E in the Tantangara waters measured in this test with values in Talbingo water from previous tests are shown in Figures 1, 2, 3, 4 and 5, respectively. The pH varied between 7.27 and 9.35 in the elutriate tests with Tantangara reservoir water, compared to 7.36 in the Tantangara test control water and 8.15 to 9.29 in Talbingo reservoir treatments with the same L/S and durations. The main difference in pH between the different reservoir waters was observed for the 1000 L/S, with the Tantangara elutriate treatments having a

lower pH than the corresponding Talbingo elutriate treatments after 18 h. No elutriate treatments with 3-h duration were undertaken at 1000 L/S in the Talbingo reservoir water so that comparison was not possible.

The conductivity varied between 34 and 282 $\mu\text{S}/\text{cm}$ in the Tantangara reservoir elutriate treatments, compared to 36 $\mu\text{S}/\text{cm}$ in the Tantangara test control water and 52 and 87 $\mu\text{S}/\text{cm}$ for the corresponding Talbingo reservoir elutriate treatments. The conductivity was in a similar range in each corresponding Tantangara and Talbingo reservoir elutriate treatment except for higher values measured in the Tantangara 300-L/S_3-h and 1000-L/S_18-h treatments with excavated rock composites 1B and 7E, respectively.

For the dissolved aluminium, the Talbingo elutriate treatments had higher concentrations than the Tantangara treatments for the 1000-L/S_18-h tests, whereas, the Tantangara elutriate treatments had higher concentrations than the Talbingo treatments for the 300 L/S_3- and 300-L/S_-h tests. However, the concentration of dissolved aluminium was in the same general range in the different reservoir treatments; 23.5-216 $\mu\text{g}/\text{L}$ and 61.2-146 $\mu\text{g}/\text{L}$ in the Tantangara and Talbingo reservoir water treatments, respectively. The Tantangara test control water had a dissolved aluminium concentration of 25.3 $\mu\text{g}/\text{L}$.

For the Tantangara reservoir water treatments, the concentration of dissolved aluminium was below the DGV of 55 $\mu\text{g}/\text{L}$ for the 1000-L/S treatments at 3-h and 18-h, and exceeded the DGV for the 300 L/S treatments at 3 and 18 h.

The lower pH of the Tantangara 18-h_1000-L/S treatments than the corresponding Talbingo treatments indicates the Tantangara reservoir water had a greater ability to buffer pH increases than the Talbingo reservoir water. In turn, the lower dissolved aluminium released from the Tantangara 18-h_1000-L/S treatments than the corresponding Talbingo treatments is likely influenced by the lower pH resulting in slower mineral dissolution and release of aluminium as the aluminate ion, which is favoured at higher pH's.

The higher concentrations of dissolved aluminium in the 300-L/S Tantangara reservoir treatments may be the result of greater aluminium colloid formation in this water, as this reservoir water has higher concentrations of dissolved organic carbon (DOC) and dissolved (<0.45 μm) iron than the Talbingo reservoir water (Memo 1), which are often associated with colloids.

Summary

The elutriate water pH was similar in the Tantangara and Talbingo reservoir water treatments for the 300-L/S tests, but lower in the Tantangara reservoir treatments for the 1000-L/S_18-h tests, probably due to this water having a greater ability to buffer pH increases.

The conductivities were generally in a similar range for the two reservoir waters except for a few Tantangara reservoir treatments having higher values.

The concentration of dissolved aluminium was in the range 23.5-216 $\mu\text{g}/\text{L}$ in the Tantangara reservoir elutriate treatments, which was in a similar range to corresponding Talbingo reservoir treatments conducted in previous tests. Small differences were observed for corresponding treatments, with the Talbingo elutriate treatments having higher concentrations than the Tantangara treatments for the 1000-L/S_18-h tests, and the Tantangara elutriate treatments having higher concentrations than the Talbingo treatments for the 300-L/S_3-h and 300-L/S_18-h tests.

The concentration of dissolved aluminium in the 1000-L/S Tantangara reservoir water treatments was below the DGV of 55 $\mu\text{g}/\text{L}$ for the 1000-L/S treatments, and exceeded the DGV for the 300-L/S treatments.

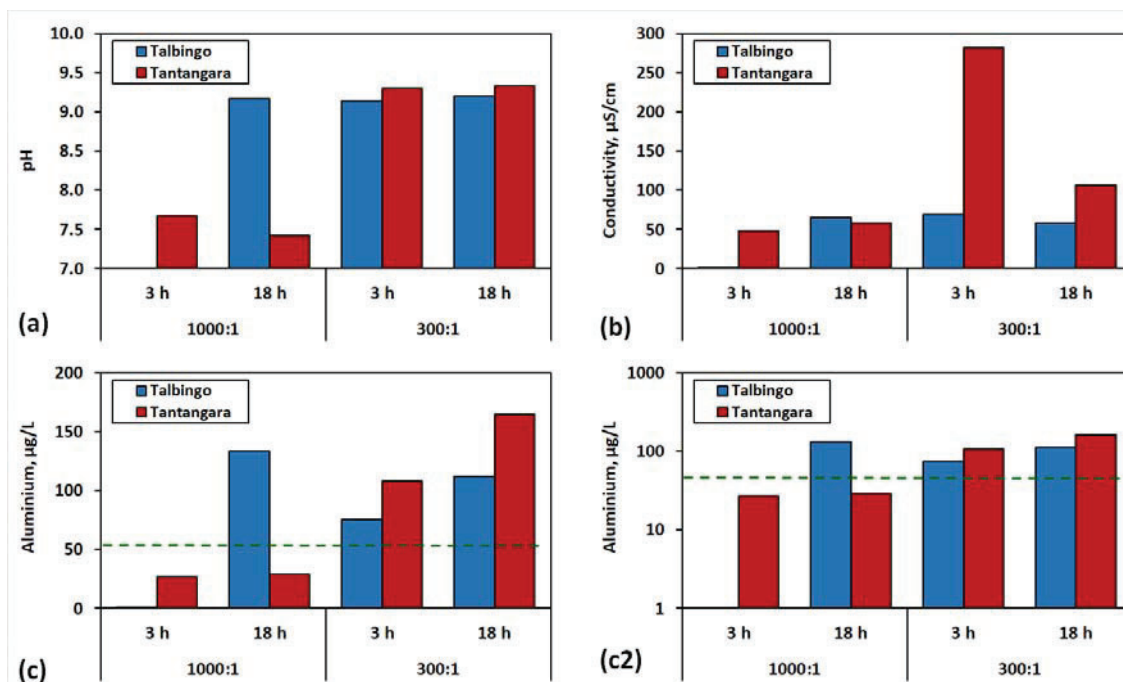


Figure 1. Comparison between the pH, conductivity and dissolved aluminium concentration measured in Talbingo and Tantangara reservoir waters following elutriate tests with excavated rock composite 1B (c_2 = log scale). The dotted green line is the DGV for 95% species protection in freshwater of 55 µg/L.

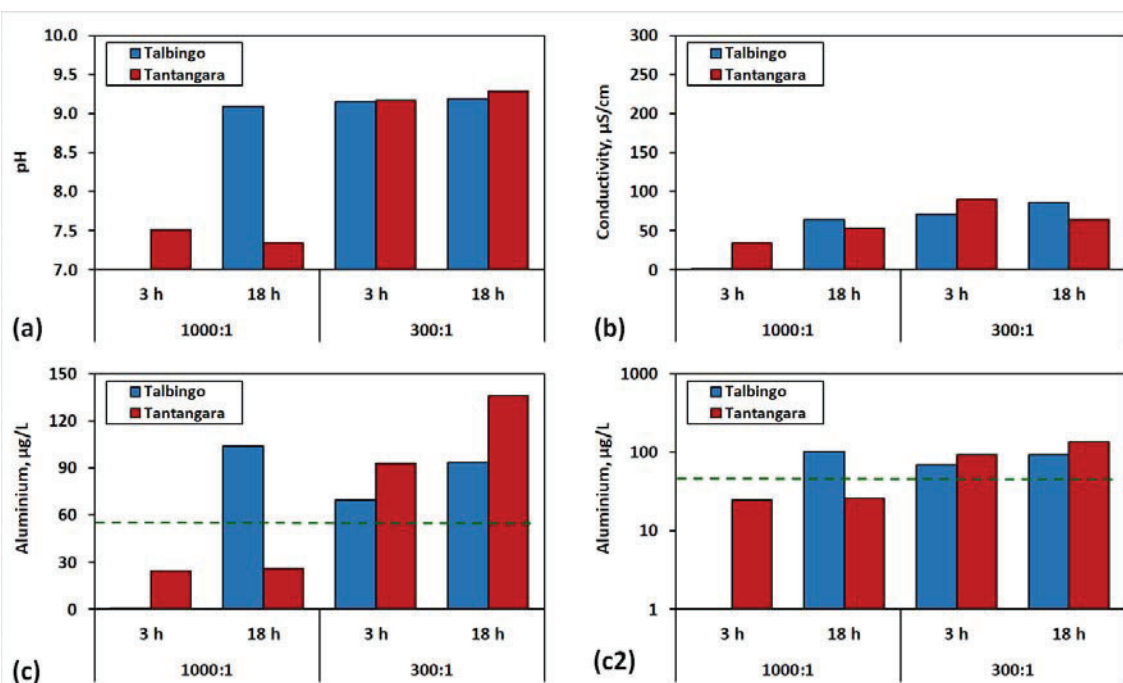


Figure 2. Comparison between the pH, conductivity and dissolved aluminium concentration measured in Talbingo and Tantangara reservoir waters following elutriate tests with excavated rock composite 2B (c_2 = log scale). The dotted green line is the DGV for 95% species protection in freshwater of 55 µg/L.

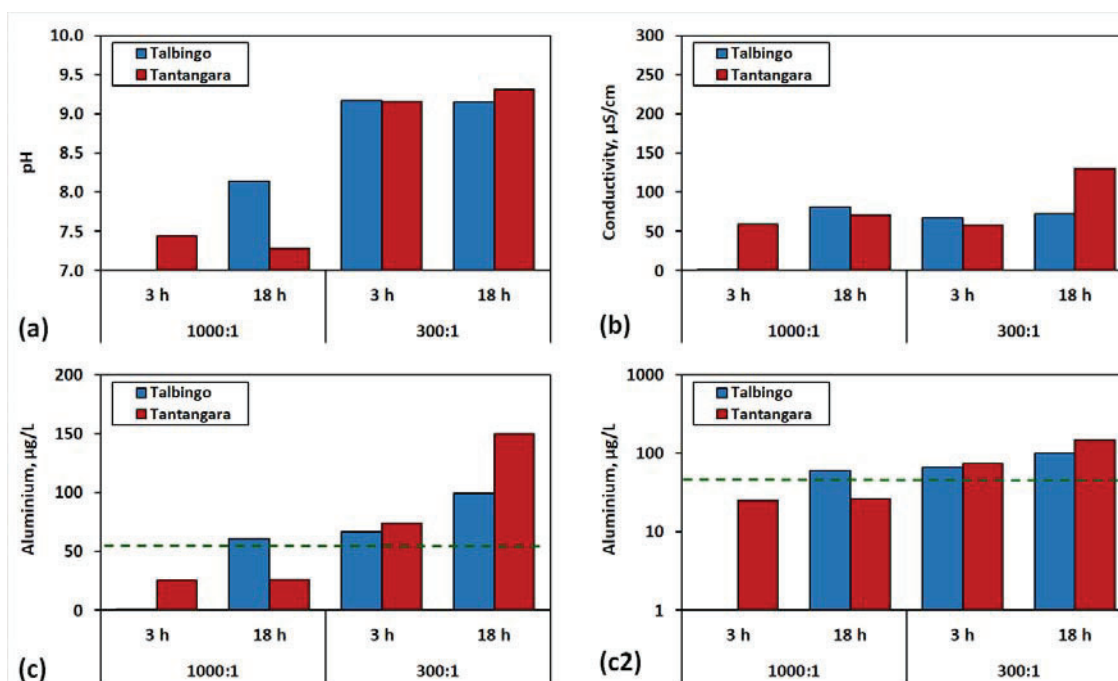


Figure 3. Comparison between the pH, conductivity and dissolved aluminium concentration measured in Talbingo and Tantangara reservoir waters following elutriate tests with excavated rock composite 5B (c2 = log scale). The dotted green line is the DGV for 95% species protection in freshwater of 55 µg/L.

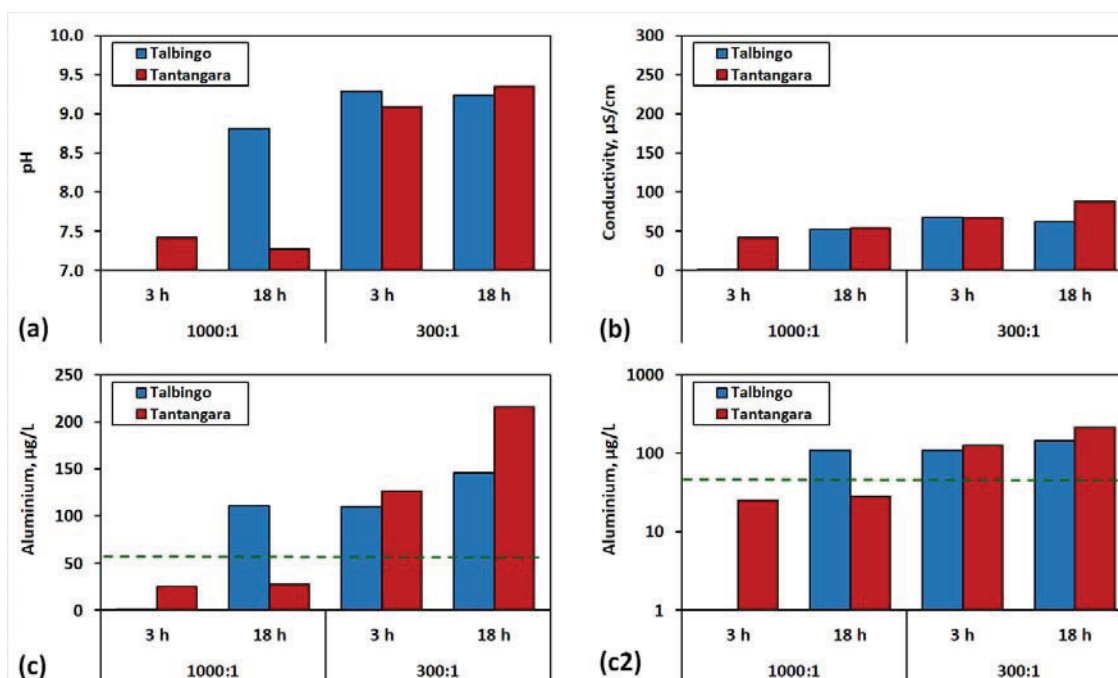


Figure 4. Comparison between the pH, conductivity and dissolved aluminium concentration measured in Talbingo and Tantangara reservoir waters following elutriate tests with excavated rock composite 5E (c2 = log scale). The dotted green line is the DGV for 95% species protection in freshwater of 55 µg/L.

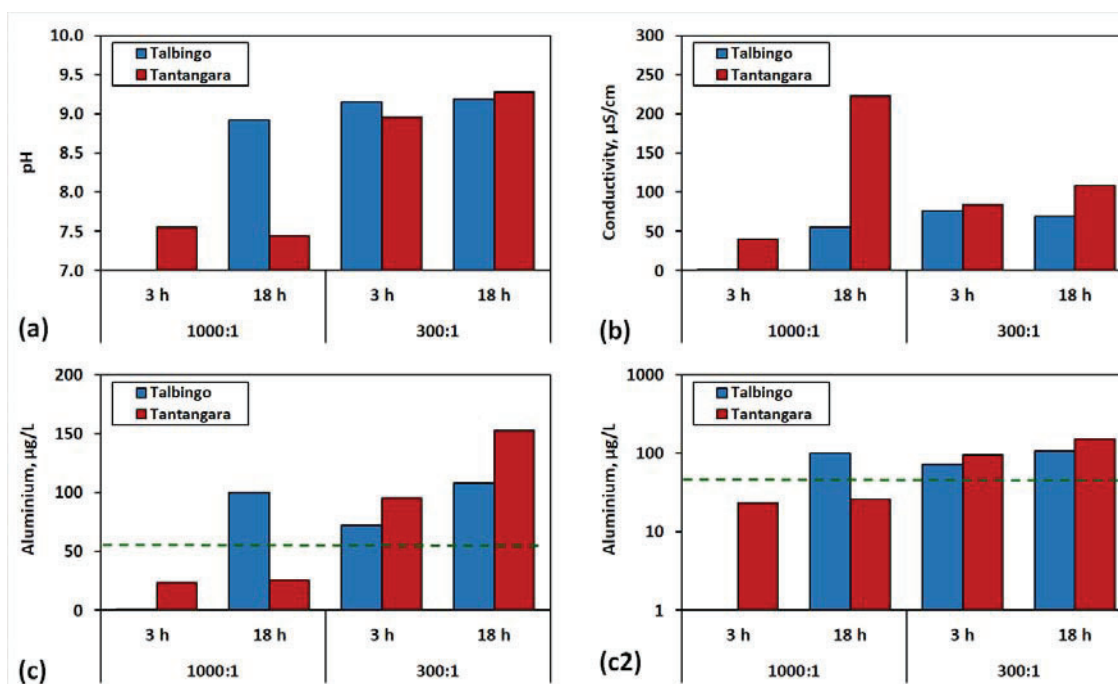


Figure 5. Comparison between the pH, conductivity and dissolved aluminium concentration measured in Talbingo and Tantangara reservoir waters following elutriate tests with excavated rock composite 7E (c2 = log scale). The dotted green line is the DGV for 95% species protection in freshwater of 55 µg/L.

Appendix D6. Effect of water temperature on substance

| | |
|------------------|---|
| Note/Memo | CSIRO P4 Project Investigations |
| To: | Ali Watters (HKA) |
| From: | Brad Angel, Lucas Heights, NSW |
| Date: | 7 November 2018 |
| Copy: | Ryan Fraser, Stuart Simpson and Ellen Porter (SHL) |
| Our reference: | CSIRO P4 – Memo 9 |
| Classification: | Internal use only |
| Subject: | Effect of temperature on pollutant release from excavated rock composites |

Chemical formulas and acronyms

| | | | | | |
|-----------------|--------------------------|------------------------------|-------------------------|-------------------------------|--------------------|
| Ag | Silver | F ⁻ | Fluoride | Sb | Antimony |
| Al | Aluminium | Fe | Iron | Se | Selenium |
| As | Arsenic | Mg | Magnesium | Sn | Tin |
| Ba | Barium | Mn | Manganese | SO ₄ ²⁻ | Sulfate |
| Ca | Calcium | Mo | Molybdenum | Sr | Strontium |
| Cd | Cadmium | Na | Sodium | Th | Thorium |
| Cl ⁻ | Chloride | Ni | Nickel | U | Uranium |
| Co | Cobalt | NO ₃ ⁻ | Nitrate | V | Vanadium |
| Cr | Chromium | Pb | Lead | Zn | Zinc |
| Cu | Copper | | | | |
| DOC | Dissolved organic carbon | DGV | Default guideline value | L/S | Liquid/solid ratio |
| SEC | Conductivity | | | | |

Background - Introduction

The CSIRO was engaged by Haskoning Australia Pty Ltd (RHDHV) to undertake an investigation of the effect on water quality of excavated rock disposal into the Talbingo and Tantangara reservoirs. Previous elutriate tests performed to date to assess the release of pollutants into reservoir waters have been conducted at a temperature of 21°C. The temperature of the reservoirs varies between approximately 6 and 21°C, with significant changes over depth and season. Lower temperatures may substantially slow the kinetics of reactions that effect the release of pollutants from excavated rock material into the reservoirs

This technical memo describes results of elutriate tests performed on five different excavated rock composite materials that had been milled to <75 µm. The kinetics of substance release was monitored at time periods of 6, 18 and 48 h after resuspension then settling in Talbingo reservoir water at 6°C. The results were compared to data generated from the same liquid to solid ratio and duration in water at 21°C (full details of results from the 21°C tests will be reported in a future memo).

Test methodology

The 75 µm milled composites 1B, 2B, 5B, 5E and 7E characterised in memo 3 were used in the elutriate tests investigating the effect of temperature. The tests were performed at liquid to solid ratios of 300 and 1000, which were equivalent to 3.3 and 1 g/L, respectively. The material was weighed into plastic vials to which Talbingo water at 6°C was added. The treatments were shaken (50 rpm) for 30 mins then allowed to stand at 6±1°C for the remaining duration so that they were in water for 6, 18 and 48 h. The 21±2°C treatments to which they were compared were sampled after 0.5 and 18 h, with the 3.3 g/L (300/1 L/S) also

being sampled after 3 and 120 h. Therefore, the 18-h time point was directly comparable and trends over time were also compared to investigate the effect of temperature on water quality.

Results - Influence of rock material size (and time) on elutriate pH, conductivity and dissolved analytes

The pH, conductivity and dissolved aluminium for composites 1B, 2B, 5B, 5E and 7E are shown in Figures 1, 2, 3, 4 and 5, respectively. For the 6°C treatments, the pH varied between 7.84 and 9.34 and the conductivity varied between 40 and 88 µS/cm. The pH and conductivity generally decreased marginally between the 6 and 48-h measurements.

For the 6°C treatments, only the 3.3 g/L (300 L/S) had dissolved aluminium that exceeded the DGV of 55 µg/L (dotted red line in graphs), which occurred for the 48 h sampling time for all but composite 5E, for which the DGV was exceeded for all durations tested. The dissolved aluminium increased continuously over the 48 h test period for all 6°C treatments and would presumably continue to increase for some time if the test was run longer (i.e. the concentration did not plateau after 48 h).

For the dissolved major cation concentrations, the excavated rock material affected the calcium most followed by magnesium, with the concentrations increasing rapidly, followed by either a slow increase or being steady over the 48 h duration for the 6°C treatments (data not shown). The dissolved magnesium and sodium were only marginally higher in composite treatments than reservoir control water.

A comparison between the 6 and 21°C values for pH and dissolved aluminium is shown for different treatments in Figures 1 to 5 for each composite material and for all treatments at 18 h in Figure 6. Conductivity was similar for both temperatures. It can be seen that the pH and dissolved aluminium are mostly higher at 21°C than at 6°C.

The concentrations of major cations were generally similar for the 1 g/L (1000 L/S) at both temperatures, whereas for the 3.3 g/L (300 L/S), marginally higher concentrations were generally measured for the 21°C than the 6°C (data not shown).

Summary

The release of aluminium occurred significantly more slowly in the 6°C treatments than the 21°C treatments. As such, after 18 h, the concentration of dissolved aluminium (and pH) were generally substantially lower for the lower temperature treatment. The dissolved aluminium continued to increase over the 48-h period of the 6°C test and did not plateau. After 48-h, the dissolved aluminium exceeded the DGV of 55 µg/L for all 6°C treatments at 3.3 g/L (300 L/S), but did not exceed the DGV for any 1 g/L (1000 L/S) treatments.

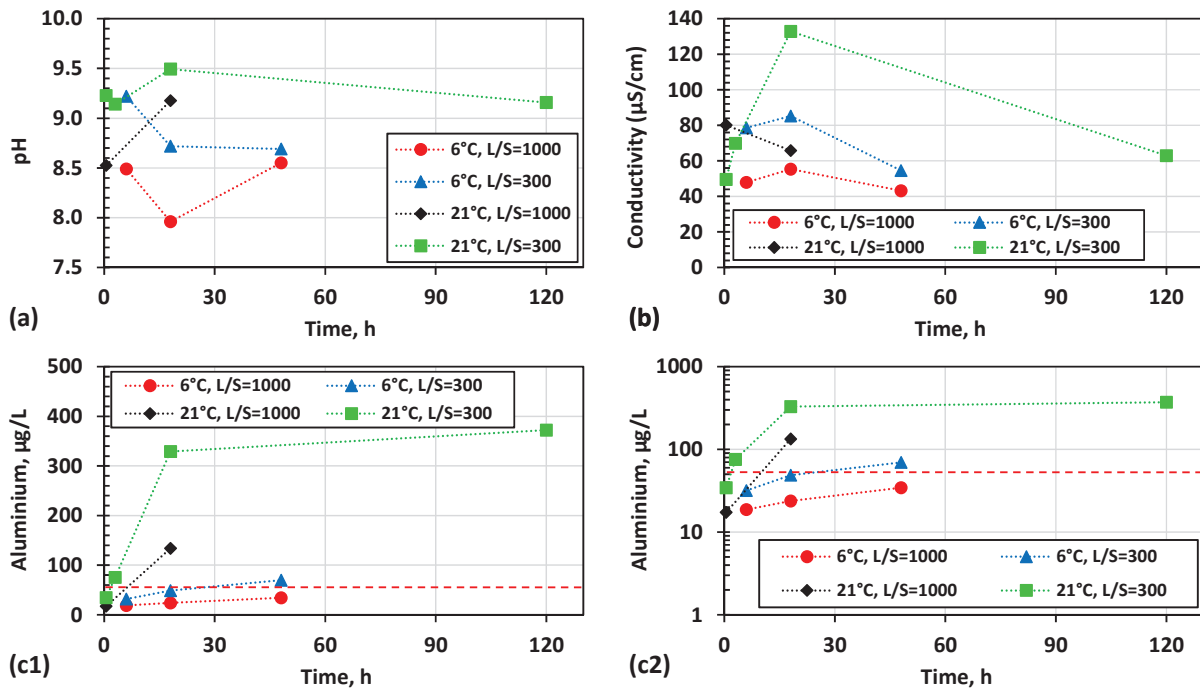


Figure 1. The pH, conductivity and dissolved aluminium over time for composite 1B ($c_2 = \log$ scale). The dotted red line is the DGV for 95% species protection in freshwater of 55 $\mu\text{g}/\text{L}$.

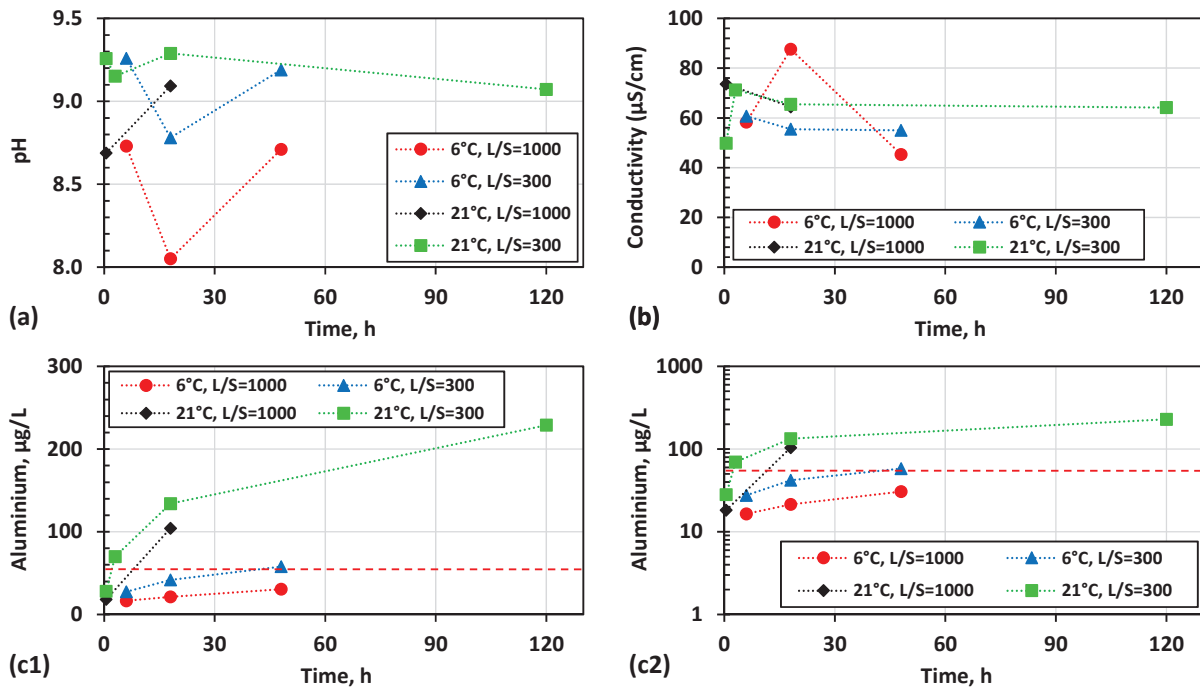


Figure 2. The pH, conductivity and dissolved aluminium over time for composite 2B ($c_2 = \log$ scale). The dotted red line is the DGV for 95% species protection in freshwater of 55 $\mu\text{g}/\text{L}$.

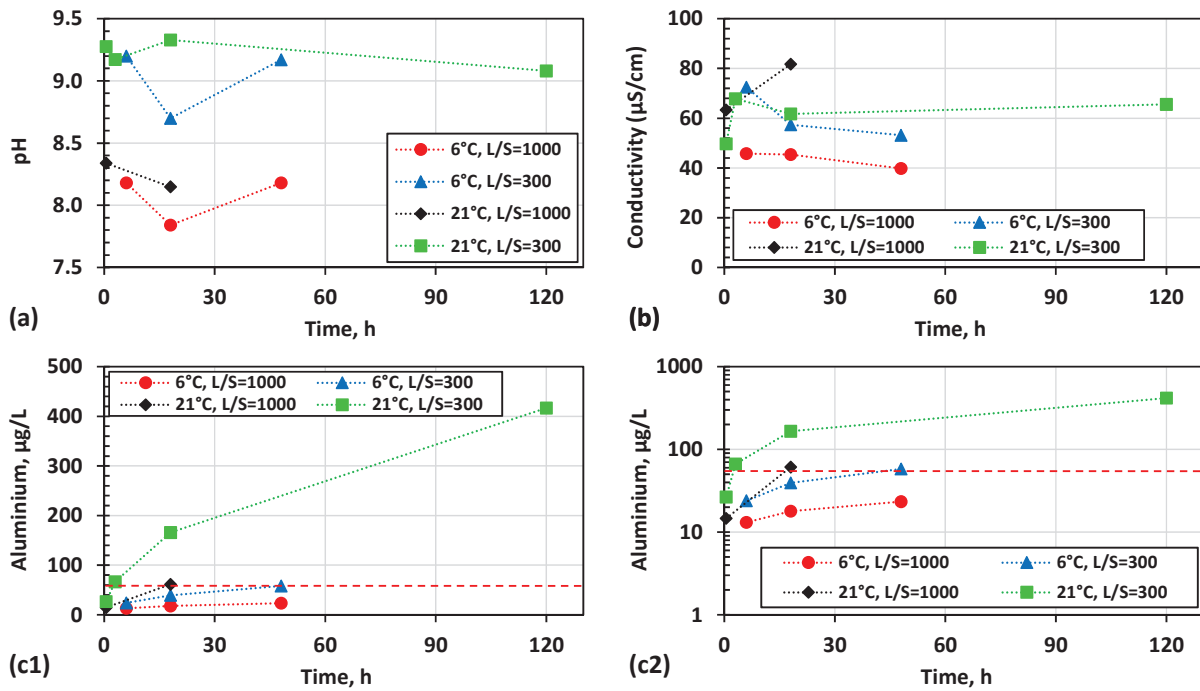


Figure 3. The pH, conductivity and dissolved aluminium over time for composite 5B (c2 = log scale). The dotted red line is the DGV for 95% species protection in freshwater of 55 µg/L.

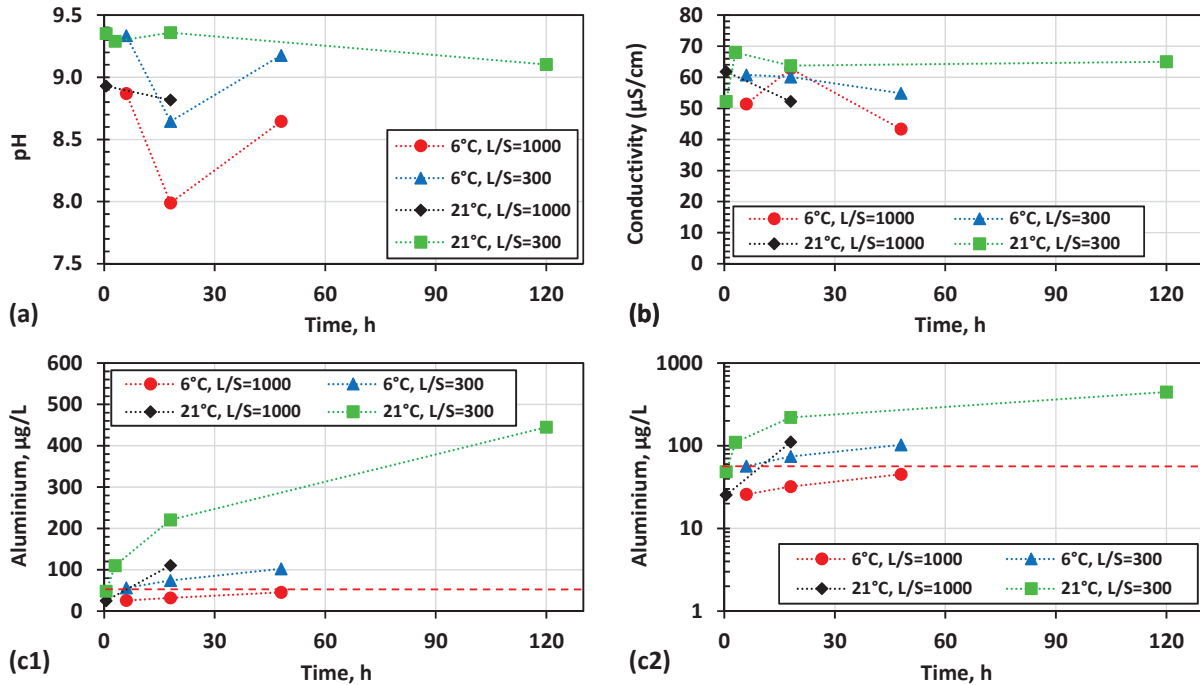


Figure 4. The pH, conductivity and dissolved aluminium over time for composite 5E (c2 = log scale). The dotted red line is the DGV for 95% species protection in freshwater of 55 µg/L.

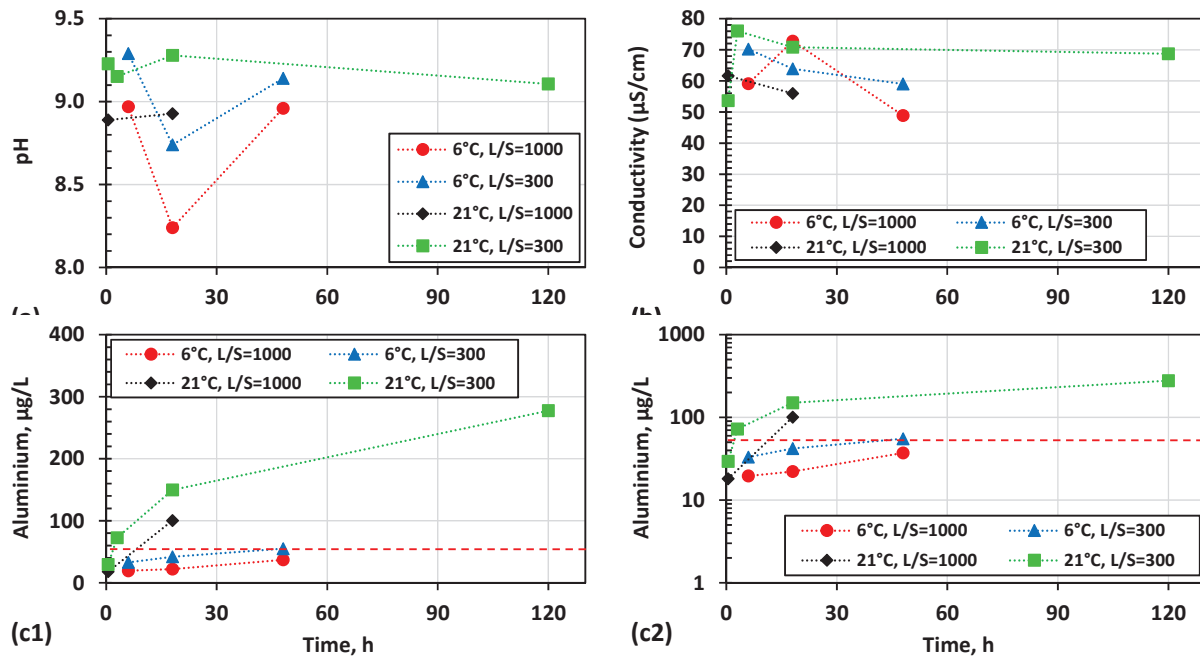


Figure 5. The pH, conductivity and dissolved aluminium over time for composite 5E (c2 = log scale). The dotted red line is the DGV for 95% species protection in freshwater of 55 µg/L.

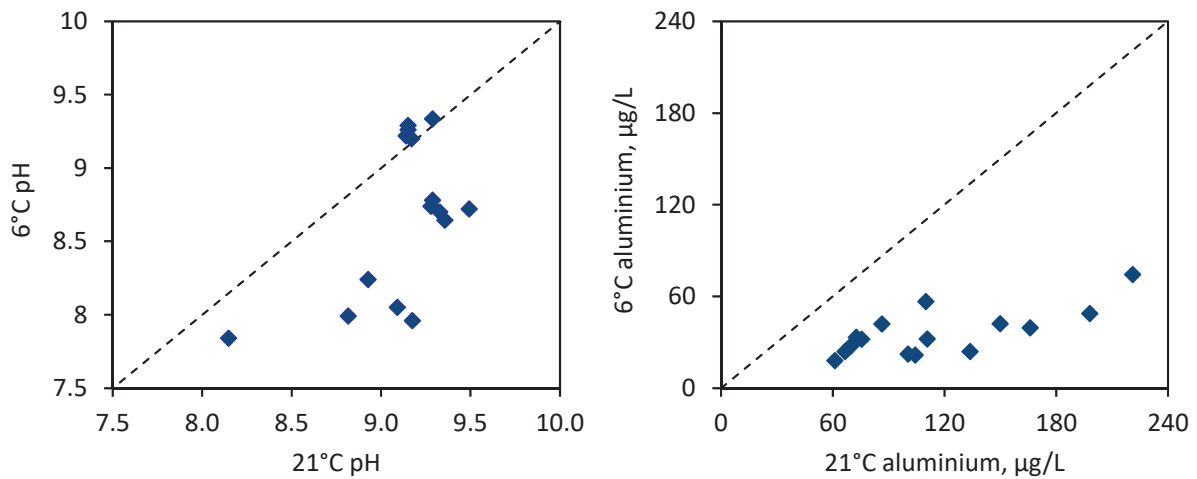


Figure 6. Comparison between temperatures of 6 and 21°C on the pH and dissolved aluminium for 1B, 2B, 5B, 5E and 7E composites after 18 h in Talbingo reservoir water. The dotted unity line indicates a 1:1 relationship.

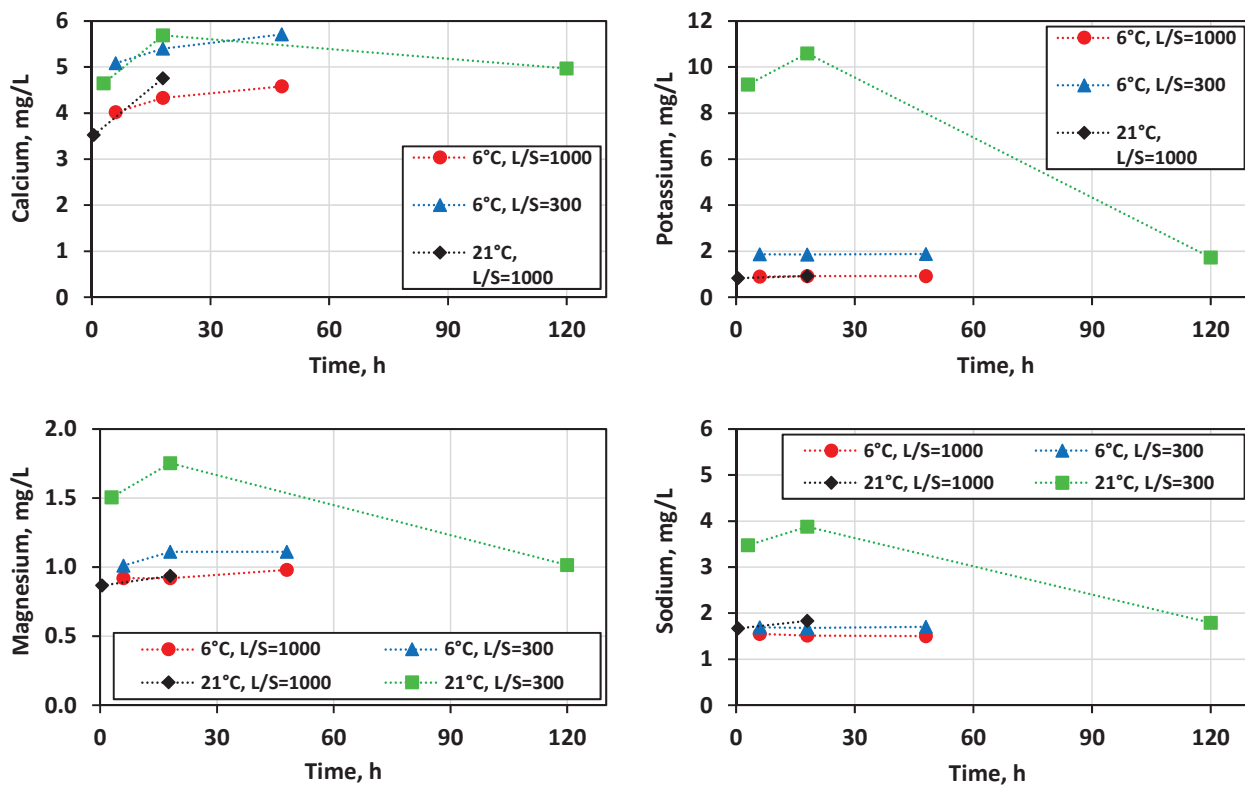


Figure D6.1. Major cation concentration of composite 1B elutriate tests undertaken at 6°C and 21°C

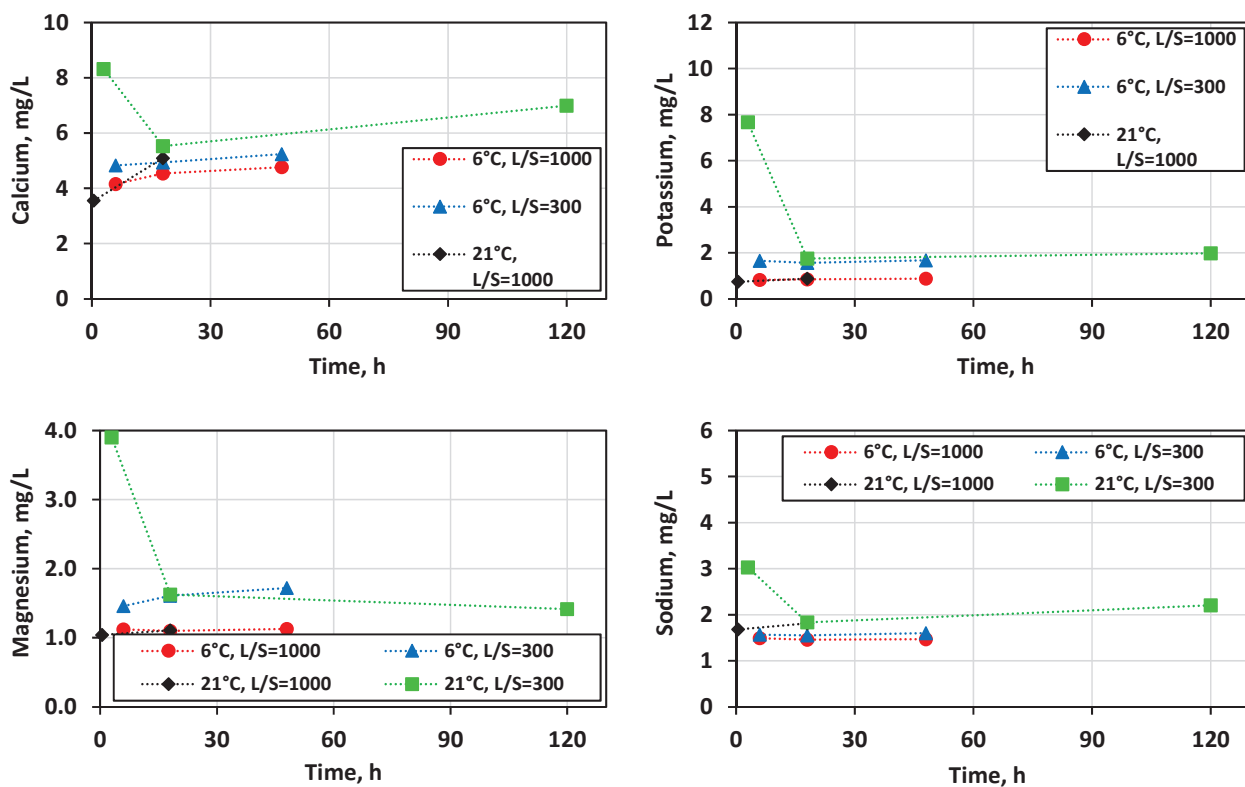


Figure D6.2. Major cation concentration of composite 2B elutriate tests undertaken at 6°C and 21°C

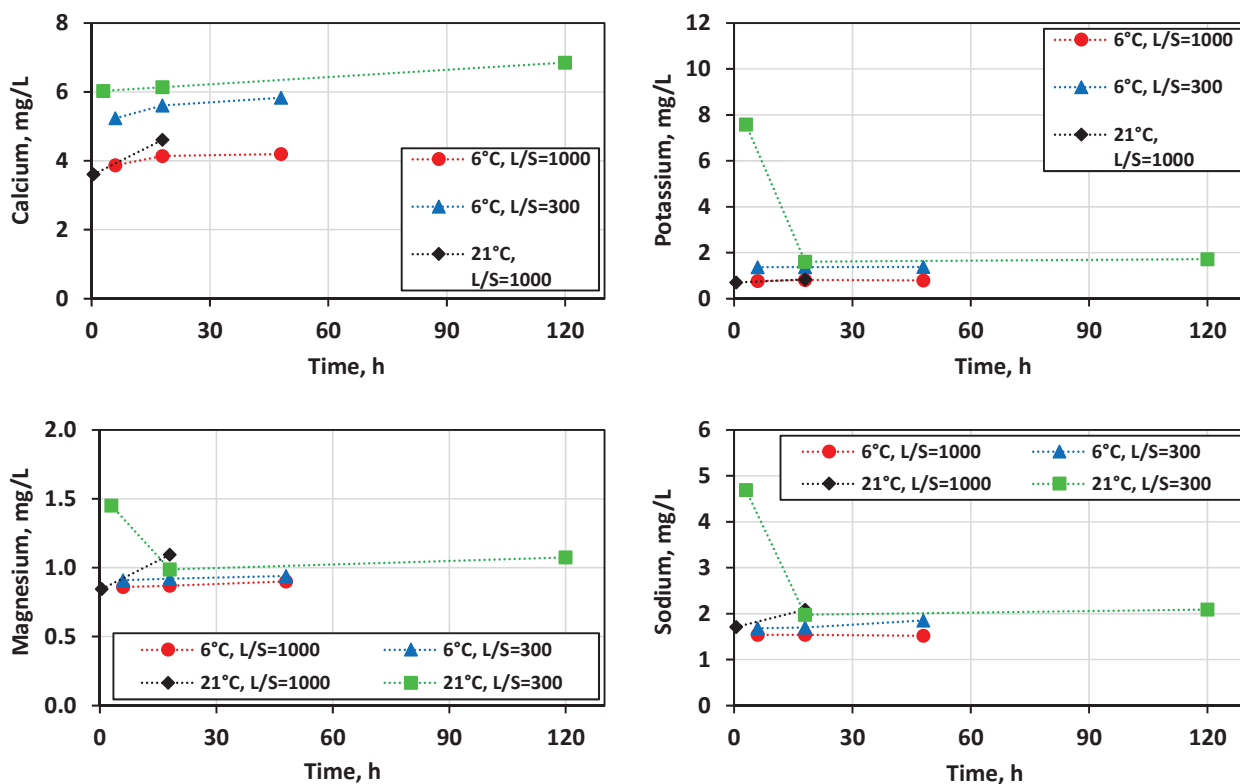


Figure D6.3. Major cation concentration of composite 5B elutriate tests undertaken at 6°C and 21°C

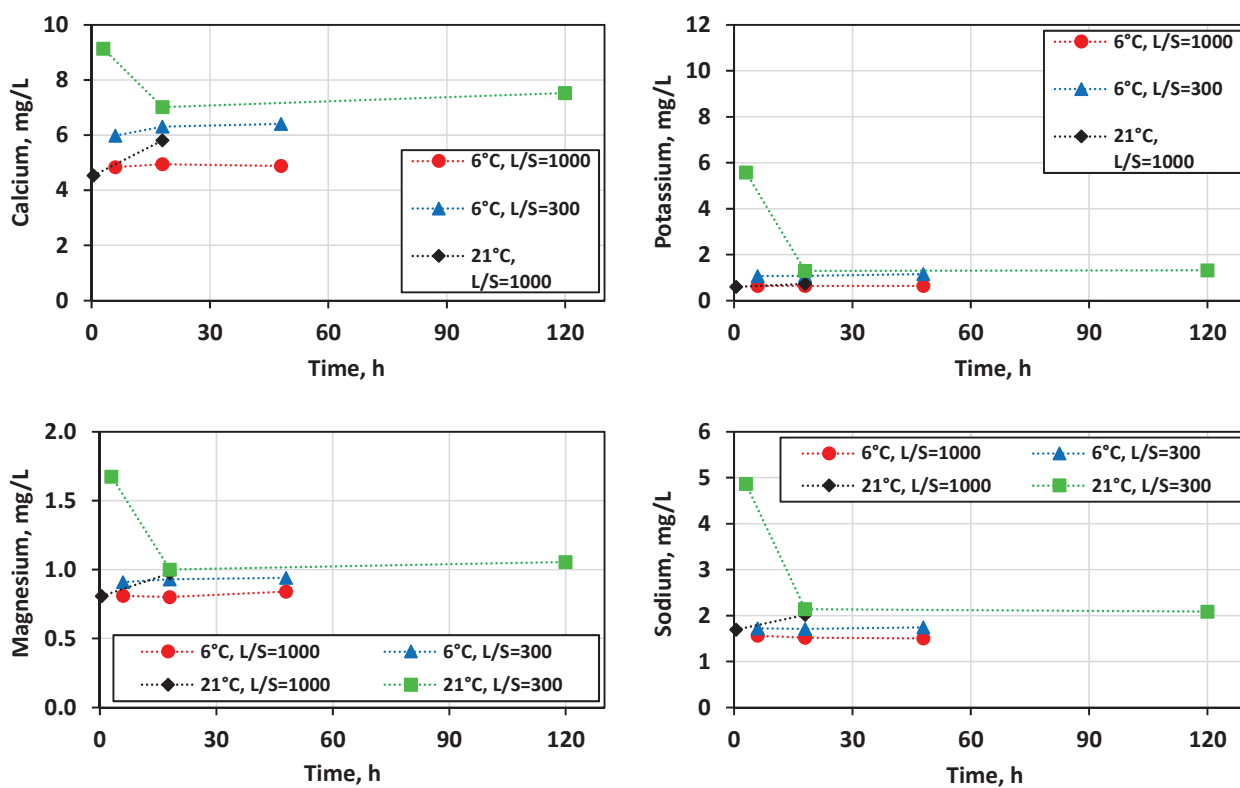


Figure D6.4. Major cation concentration of composite 5E elutriate tests undertaken at 6°C and 21°C

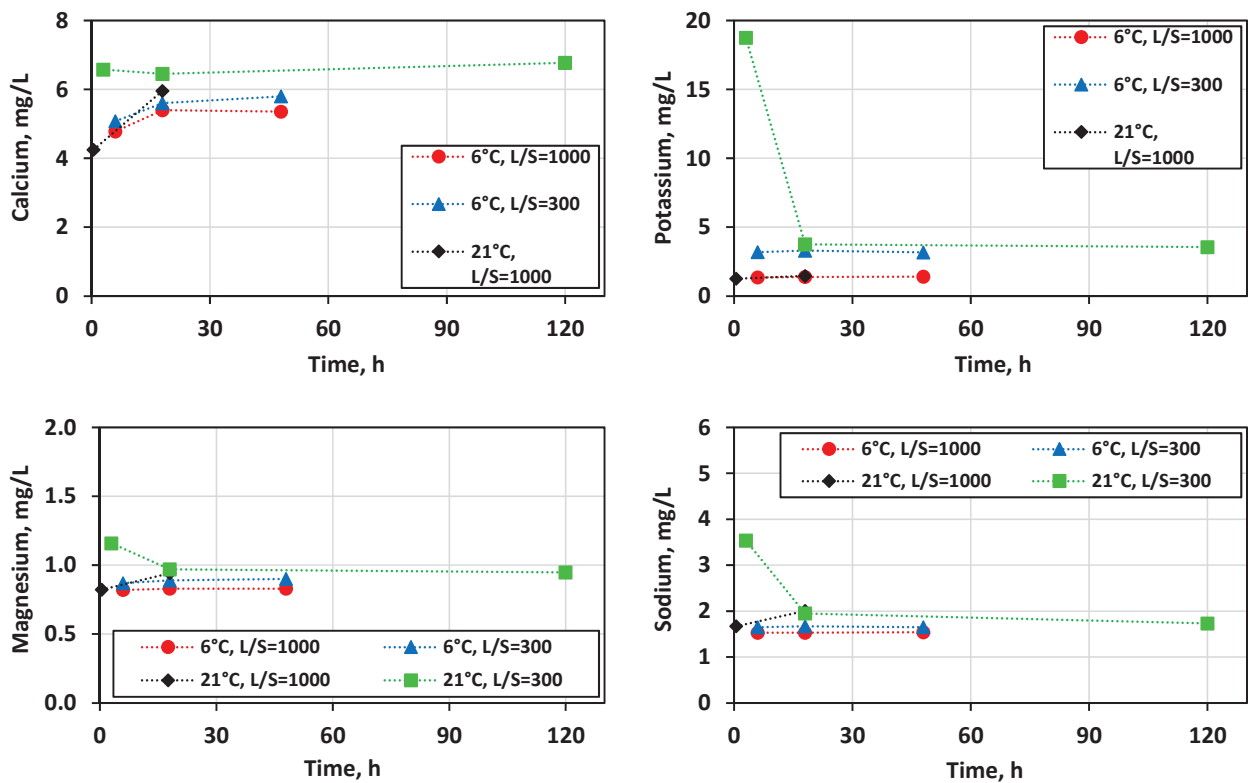


Figure D6.5. Major cation concentration of composite 7E elutriate tests undertaken at 6°C and 21°C

Appendix D7. Effect of repeat leaching on substance release

| | |
|------------------|---|
| Note/Memo | CSIRO P4 Project Investigations |
| To: | Ali Watters (HKA) |
| From: | Brad Angel, Lucas Heights, NSW |
| Date: | 23 November 2018 |
| Copy: | Ryan Fraser, Stuart Simpson and Ellen Porter (SHL) |
| Our reference: | CSIRO P4 – Memo 12 |
| Classification: | Internal use only |
| Subject: | Pollutant release from excavated rock composites: effect of successive leaches and temperature on water quality and pollutant release |

Chemical formulas and acronyms

| | | | | | |
|-----|--------------|-----|-------------------------|-----|--------------------|
| Al | Aluminium | DGV | Default guideline value | L/S | Liquid/solid ratio |
| SEC | Conductivity | | | | |

Background - Introduction

The CSIRO was engaged by Haskoning Australia Pty Ltd (RHDHV) to undertake an investigation of the pollutant release from excavated rock disposal into Talbingo and Tantangara reservoirs. Previous elutriate tests (e.g. Memos 4, 5, 6) investigating the release of pollutants from composite excavated rock samples have observed significant changes in water quality with respect to pH, conductivity (SEC) and the dissolved aluminium concentrations. The temperature of elutriate solutions was also shown to have a strong effect on water quality and aluminium concentrations (Memo 9).

This technical memo describes results of two series of successive elutriate tests (3 leaches each) performed to investigate the effect of excavated rock composites 1B, 2B, 5B, 5E and 7E in Talbingo reservoir water on pH, conductivity (SEC), and the dissolved aluminium concentration. The first successive leach test series investigated the effect of two mixing durations for two liquid to solid (L/S) ratios at 21°C. The second successive leach test series investigated the effect of temperature (6°C and 21°C) for the two L/S ratios. The tests were performed using the following conditions:

- Successive leach test series 1
 - L/S = 30 and 300 i.e. 33 and 3.3 g/L, respectively
 - Mixing durations for each successive leach of either 0.5 or 18 h
 - Talbingo reservoir water at 21±2°C
- Successive leach test series 2
 - L/S = 30 and 300 i.e. 33 and 3.3 g/L, respectively
 - Mixing durations for each successive leach of 18 h
 - Talbingo reservoir water at 6±1°C and 21±2°C

Test methodology

The 75 µm milled composites 1B, 2B, 5B, 5E and 7E characterised in memo 3 were used in the successive leach tests. The desired mass of each sample was weighed into 50 mL acid washed polyethylene tubes, to which 50 mL of composite Talbingo (TAL-PL1A, TAL-PL2A and TAL-PL2B) reservoir water was added. The water was adjusted to 6°C and 21°C before addition. For successive leach test series 1, the treatments were shaken (50 rpm) at 21°C for either 0.5 or 18 h for each cycle. For successive leach test series 2, the treatments were shaken for 0.5 h, then stood in temperature controlled rooms (6±1°C and 21±2°C) for another 17.5 h so that they were in contact with the water for 18 h for each leach cycle. This allowed an additional comparison of the effect of mixing vs standing for the 18 h, 21±2°C treatments in tests series 1 and 2.

After each leach cycle, the tubes were centrifuged (2000 g, 5 mins) followed by subsampling for measurement of pH, SEC, and dissolved (0.45 µm) metals analyses. The remaining supernatant was decanted and 50 mL fresh composite Talbingo reservoir water of the desired temperature added. The tube and its' contents were weighed before adding fresh reservoir water to check on the residual water carried over from one leach to the next; this was 2-4% by volume and considered negligible. The process was repeated so that each treatment received three leaches in total.

Results

Test series 1 (0.5 h or 18 h mixing, 21°C):

The pH, conductivity and dissolved aluminium concentrations measured in successive leach test series 1 (21°C treatments) with excavated rock composites 1B, 2B, 5B, 5E and 7E are shown in Figures 1, 2, 3, 4 and 5, respectively.

For all excavated rock samples at each L/S ratio and mixing duration, the pH of the leach 1, 2 and 3 solutions were in the range 9.23-9.67, 8.83-9.57, and 7.89-9.51, respectively. The pH was generally higher for a lower L/S ratio and longer mixing duration and decreased in each successive leach.

For all excavated rock samples at each L/S ratio and mixing duration, the conductivity of the leach 1, 2 and 3 solutions were in the range 50-133, 40-89, and 33-117 µS/cm, respectively. The conductivity was more variable than pH, but was generally marginally higher for the lower L/S, and for the 300 L/S ratio, was higher for the longer mixing duration. Apart from a few treatments, the conductivity generally decreased in each successive leach.

For all excavated rock samples at each L/S ratio and mixing duration, the concentration of dissolved aluminium in the leach 1, 2 and 3 solutions were in the range 26.6-329, 26.7-416, and 26.5-512 µg/L, respectively. The concentration of dissolved aluminium was generally similar or increased over successive leaches, despite the water pH successively decreasing. The exception was the 300 L/S, 18 h mixing duration treatments, where the aluminium concentration of leach 2 was similar or higher than leach 1, but often decreased for leach 3. Figures 1-5 also show that mixing duration (i.e. leach contact time) was more important than the L/S ratio, as the 0.5 h treatments for each L/S ratio also had lower concentrations of dissolved aluminium than the 18 h treatments.

The dissolved aluminium exceeded the default guideline value (DVG) of 55 µg/L for three leaches of each material for the 18 h mixing duration. The DGV was never exceeded for the 300 L/S, 0.5 h treatments, with the dissolved aluminium remaining at a similar concentration for each successive leach, i.e. the short 0.5 h mixing duration at this L/S was not adequate to either release enough aluminium to exceed the DGV or exhaust the pool of aluminium in the samples, so the concentration remained steady. The concentration of dissolved aluminium released in the 30 L/S, 0.5 h treatments always increased over successive leaches, with the initial leach often being below the DGV and the later leaches being above the DGV.

Test series 2 (0.5 h mixing, 17.5 h standing, 6°C or 21°C):

The pH, conductivity and dissolved aluminium concentrations measured in successive leach test series 2 (6°C and 21°C treatments) with excavated rock composites 1B, 2B, 5B, 5E and 7E are shown in Figures 6, 7, 8, 9 and 10, respectively.

The pH was higher for a lower L/S ratio, but temperature generally had little effect on pH. The pH was generally similar or marginally lower over successive leaches for the 30 L/S ratio, while for the 300 L/S ratio the pH was generally similar between the first two leaches then decreased for the third leach.

There were no discernible trends for the conductivity in successive leach test series 2, i.e. temperature had no clear effect on conductivity. The conductivity was in the range 35-402 $\mu\text{S}/\text{cm}$.

For all excavated rock samples at each L/S ratio at 6°C, the concentration of dissolved aluminium in the leach 1, 2 and 3 solutions were in the range 23.1-109, 27.9-129, and 16.8-137 $\mu\text{g}/\text{L}$, respectively, and at 21°C, the concentration of dissolved aluminium in the leach 1, 2 and 3 solutions were in the range 93.6-299, 125-403, and 65.0-384 $\mu\text{g}/\text{L}$, respectively. Less aluminium was released in the lower temperature treatments for each L/S ratio, and more aluminium was released by treatments with a lower L/S ratio. For the 21°C treatments the dissolved aluminium was generally steady or decreased over the successive leaches, whereas, for the 6°C treatments the dissolved aluminium was steady or increased over the successive leaches. The dissolved aluminium exceeded the default guideline value (DVG) of 55 $\mu\text{g}/\text{L}$ for all of the leaches of the 21°C treatments and most leaches of 6°C, 30 L/S treatments, while the DVG was not exceeded by any of the 6°C, 300 L/S treatments.

A comparison of the 21°C treatments that were in contact with the reservoir water for 18 h, 0.5 h mixing (successive leach test series 2) and 18 h mixing (successive leach test series 1) indicated that longer physical mixing often caused an increase in the release of dissolved aluminium (Figure 11); most evident for the 2nd and 3rd leaches. This is likely to be the cause of the difference in trends over successive leaches between the tests for the 21°C treatments i.e. generally steady or increased in test series 1 and generally steady or decreased in test series 2.

Discussion

The lack of an effect of temperature on the conductivity and pH indicates the increase in pH occurs due to a rapid release of ions that increase the alkalinity, and this release likely occurs via ion exchange reactions. This is supported by measurements of rapid pH increase in previous tests of kinetics (Memos 6 and 11).

The results of the successive leach tests showing sustained release of aluminium over successive leaches is evidence of a dissolution process controlling the release of aluminium. This process continues while the excavated rock particles are in contact with the reservoir water and contain aluminium in forms that can be released. This process occurs more slowly at a lower temperature, so the pool of available aluminium is drawn down more slowly resulting in a greater pool available in successive leaches for the lower temperature treatments. In other words, the aluminium available for dissolution is depleted more slowly at a lower temperature.

The increased release for successive leaches and longer mixing times may be influenced by water taking time to fully encompass / contact all of the surfaces of rock particles (i.e. porosity), or particles disaggregating over time, particularly for longer mixing durations, leading to more surfaces being available for dissolution reactions to occur.

Summary

Successive leaches of excavated rock samples with Talbingo reservoir water did not rapidly exhaust the aluminium available for release into solution. To the contrary, many treatments had similar or increased aluminium concentrations in the 2nd and 3rd successive leaches. The lower temperature substantially decreased the concentration of aluminium released into reservoir waters. These results suggest a dissolution process is responsible for the release of aluminium, which is dependent on the duration of contact with water and the temperature. Longer durations of physical mixing also generally increased the release of dissolved aluminium.

The DGV for aluminium, 55 µg/L, was exceeded by most treatments in the successive leach tests.

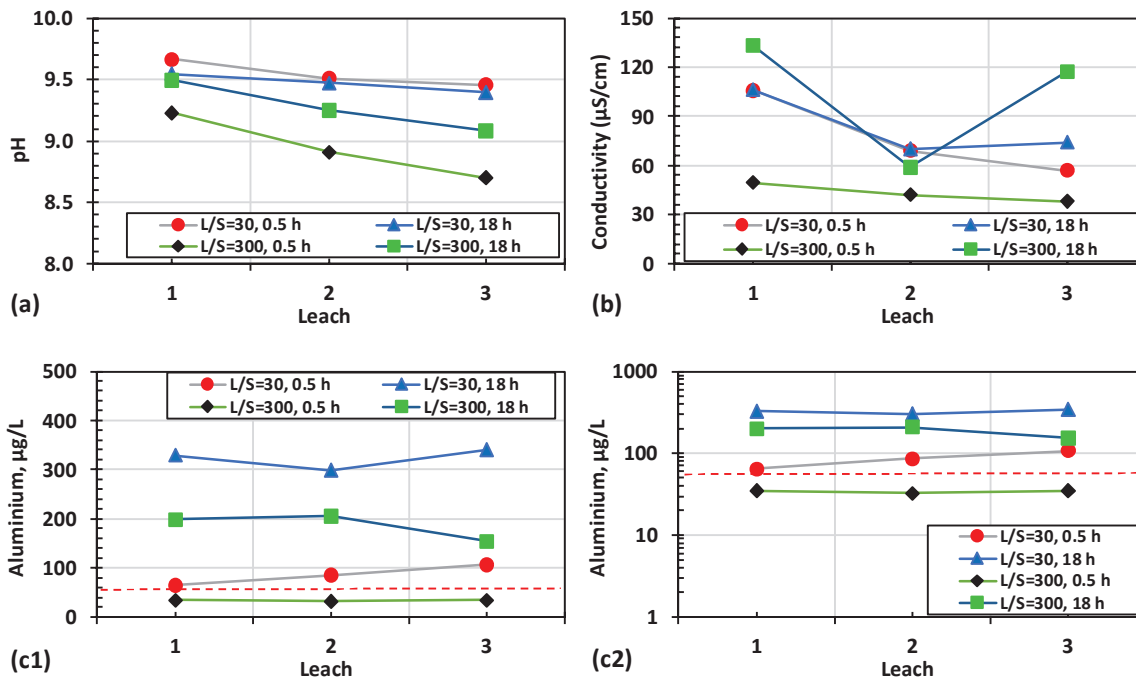


Figure 1. The pH, conductivity and dissolved aluminium concentration after three successive leach cycles at $21\pm 2^{\circ}\text{C}$ for excavated rock sample 1B (successive leach test 1), where the effect of mixing duration and L/S ratio was investigated (c2 = log scale). The 95% species protection default guideline value for dissolved aluminium is shown by the red dotted line.

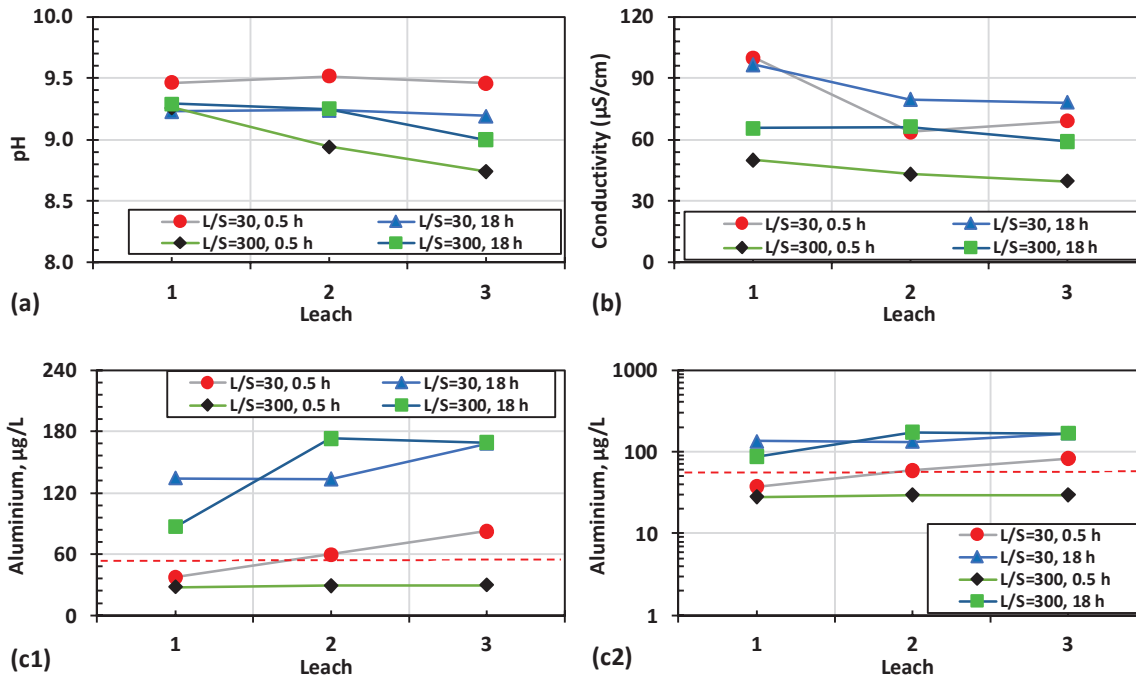


Figure 2. The pH, conductivity and dissolved aluminium concentration after three successive leach cycles at $21\pm 2^{\circ}\text{C}$ for excavated rock sample 2B (successive leach test 1), where the effect of mixing duration and L/S ratio was investigated (c2 = log scale). The 95% species protection default guideline value for dissolved aluminium is shown by the red dotted line.

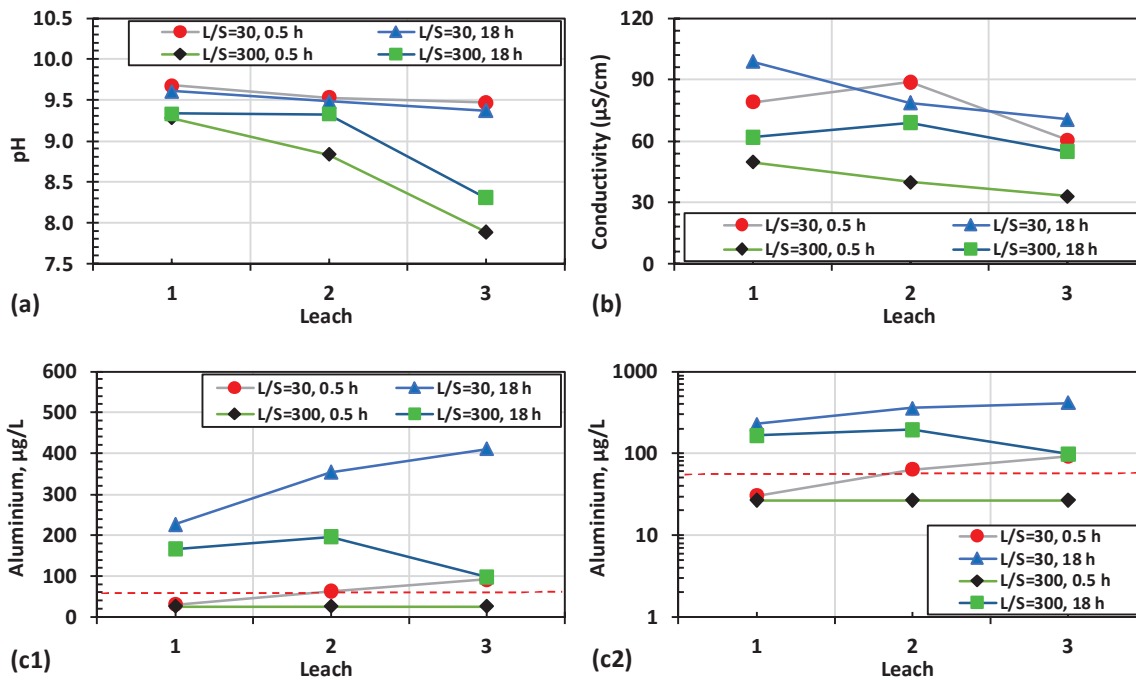


Figure 3. The pH, conductivity and dissolved aluminium concentration after three successive leach cycles at $21\pm 2^\circ\text{C}$ for excavated rock sample 5B (successive leach test 1), where the effect of mixing duration and L/S ratio was investigated (c2 = log scale). The 95% species protection default guideline value for dissolved aluminium is shown by the red dotted line.

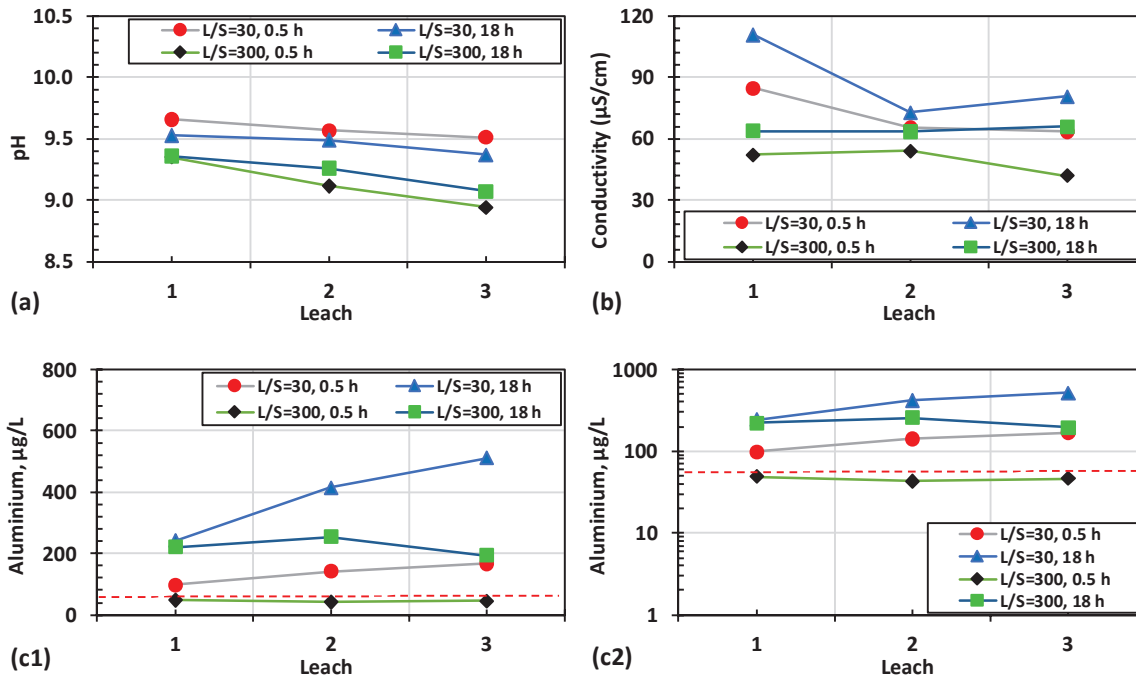


Figure 4. The pH, conductivity and dissolved aluminium concentration after three successive leach cycles at $21\pm 2^\circ\text{C}$ for excavated rock sample 5E (successive leach test 1), where the effect of mixing duration and L/S ratio was investigated (c2 = log scale). The 95% species protection default guideline value for dissolved aluminium is shown by the red dotted line.

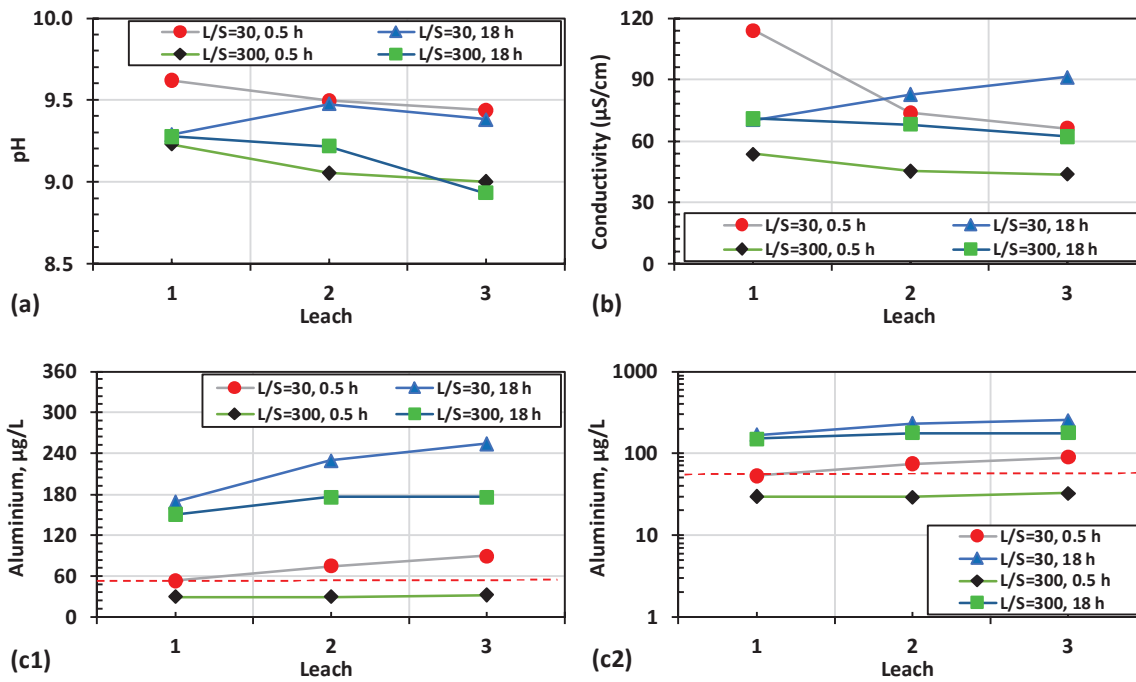


Figure 5. The pH, conductivity and dissolved aluminium concentration after three successive leach cycles at $21 \pm 2^\circ\text{C}$ for excavated rock sample 7E (successive leach test 1), where the effect of mixing duration and L/S ratio was investigated (c2 = log scale). The 95% species protection default guideline value for dissolved aluminium is shown by the red dotted line.

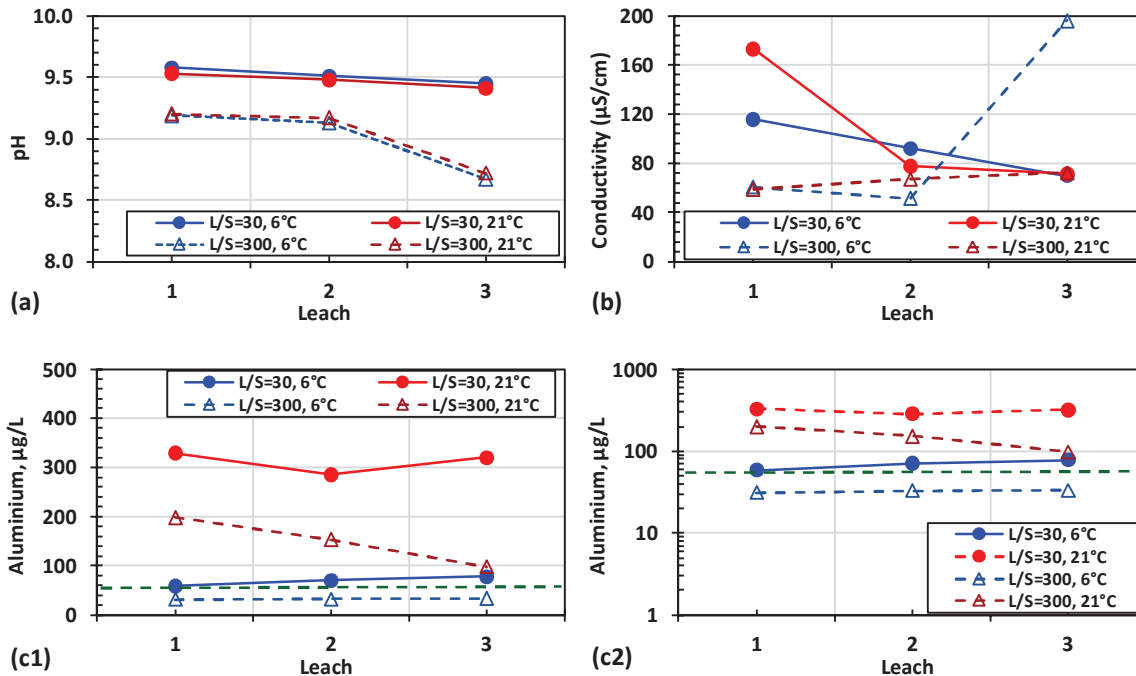


Figure 6. The effect of temperature on the pH, conductivity and dissolved aluminium concentration after three successive leach cycles at $6 \pm 1^\circ\text{C}$ and $21 \pm 2^\circ\text{C}$ for excavated rock sample 1B (successive leach test 2), (c2 = log scale). The 95% species protection default guideline value for dissolved aluminium is shown by the green dotted line.

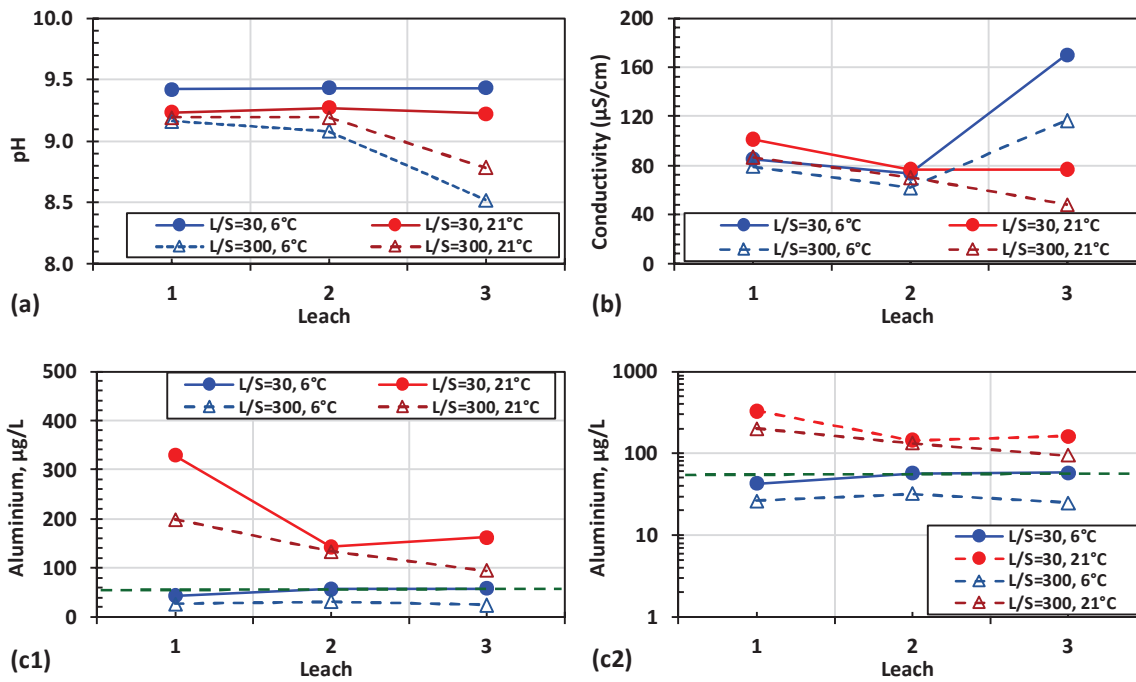


Figure 7. The effect of temperature on the pH, conductivity and dissolved aluminium concentration after three successive leach cycles at $6\pm1^{\circ}\text{C}$ and $21\pm2^{\circ}\text{C}$ for excavated rock sample 2B (successive leach test 2), (c2 = log scale). The 95% species protection default guideline value for dissolved aluminium is shown by the green dotted line.

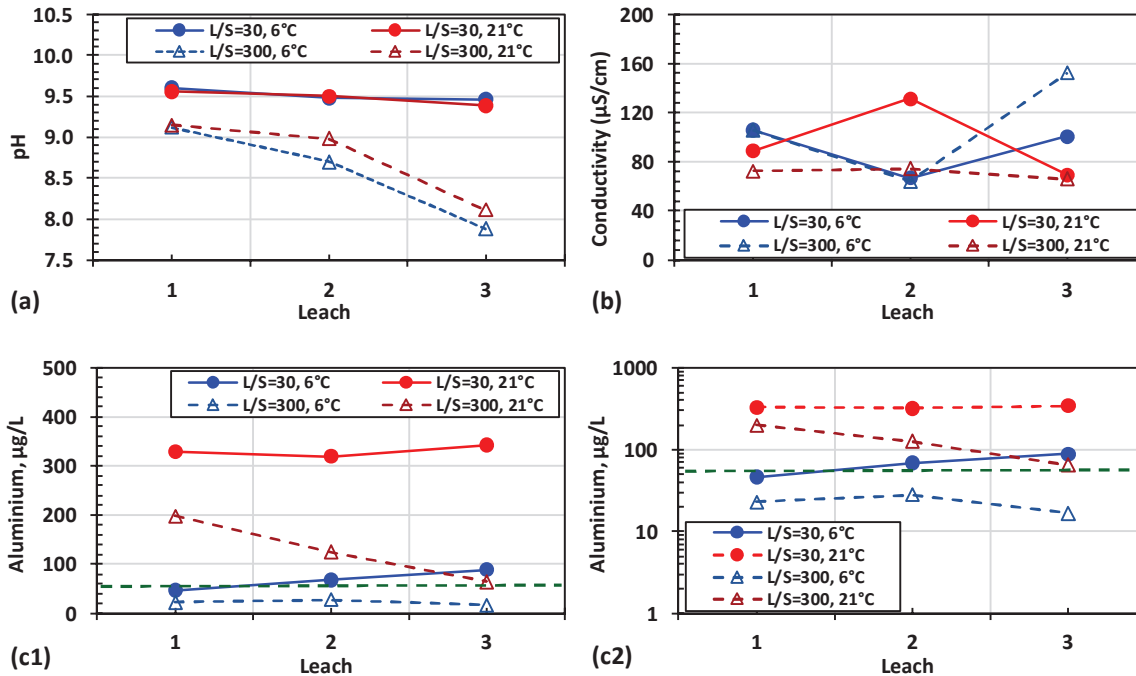


Figure 8. The effect of temperature on the pH, conductivity and dissolved aluminium concentration after three successive leach cycles at $6\pm1^{\circ}\text{C}$ and $21\pm2^{\circ}\text{C}$ for excavated rock sample 5B (successive leach test 2), (c2 = log scale). The 95% species protection default guideline value for dissolved aluminium is shown by the green dotted line.

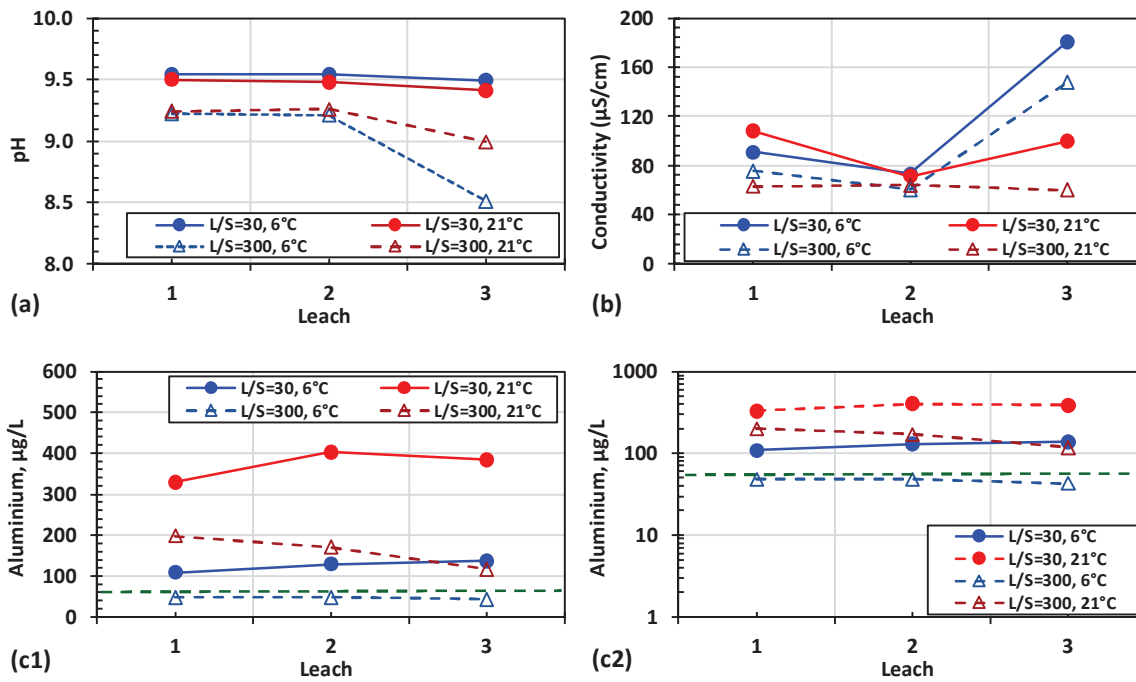


Figure 9. The effect of temperature on the pH, conductivity and dissolved aluminium concentration after three successive leach cycles at $6\pm 1^\circ\text{C}$ and $21\pm 2^\circ\text{C}$ for excavated rock sample 5E (successive leach test 2), (c2 = log scale). The 95% species protection default guideline value for dissolved aluminium is shown by the green dotted line.

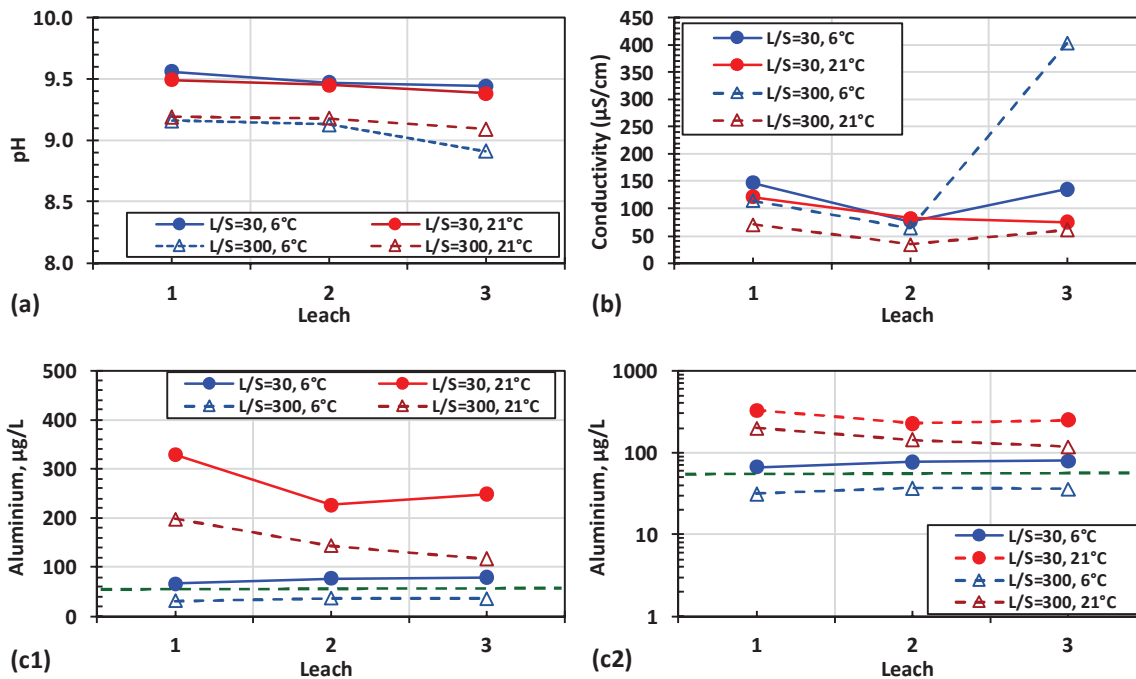


Figure 10. The effect of temperature on the pH, conductivity and dissolved aluminium concentration after three successive leach cycles at $6\pm 1^\circ\text{C}$ and $21\pm 2^\circ\text{C}$ for excavated rock sample 7E (successive leach test 2), (c2 = log scale). The 95% species protection default guideline value for dissolved aluminium is shown by the green dotted line.

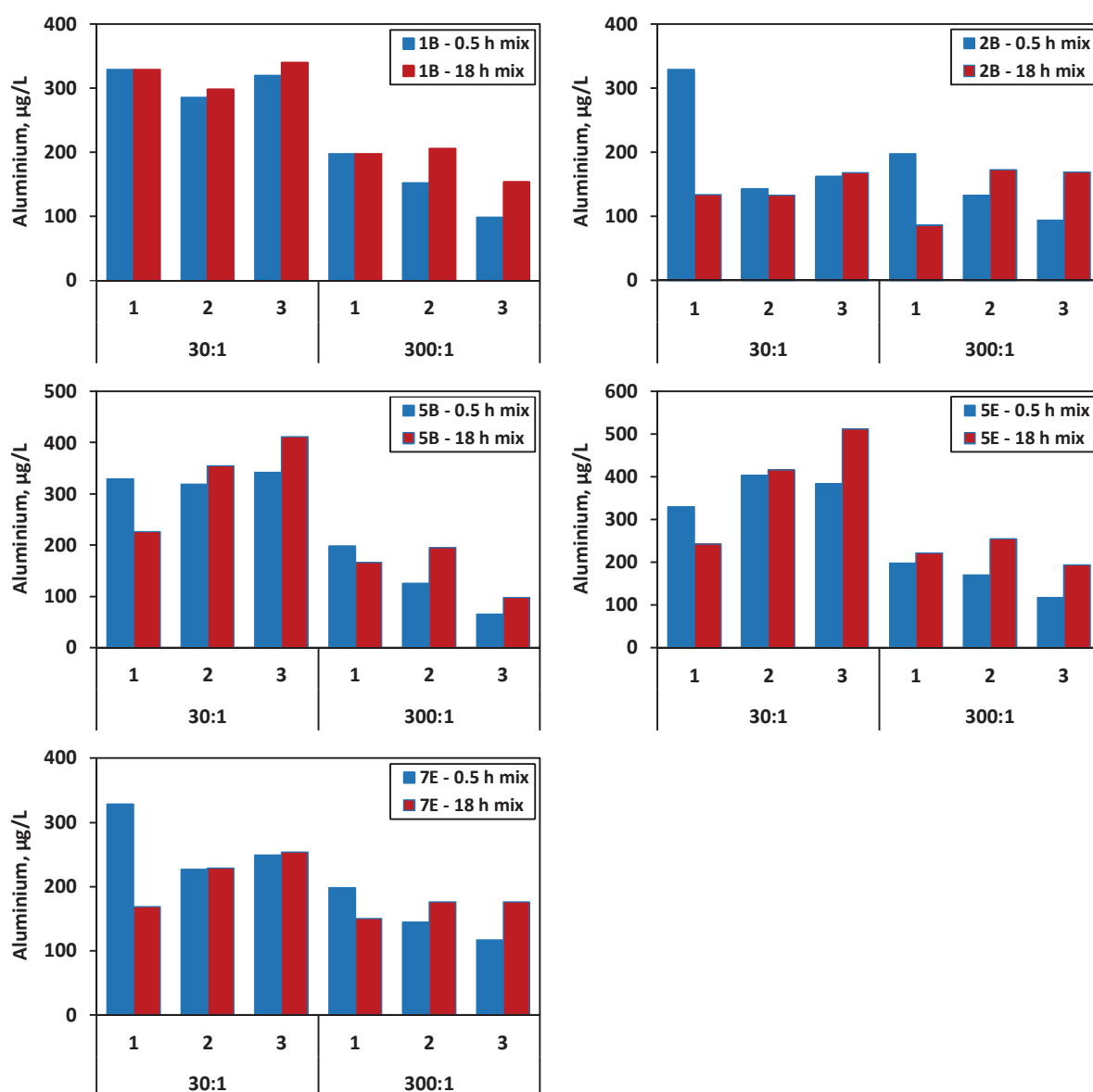


Figure 11. Comparison between the dissolved aluminium released from excavated rock material at L/S ratios of 30 and 300 in Talbingo reservoir water after 18 h contact with water between successive leach test 1 (18 h mixing, red bars) and leach test 2 (0.5 h mixing, 17.5 h standing, blue bars) at 21°C to assess the effect of mixing vs standing for each successive leach (1, 2 and 3).

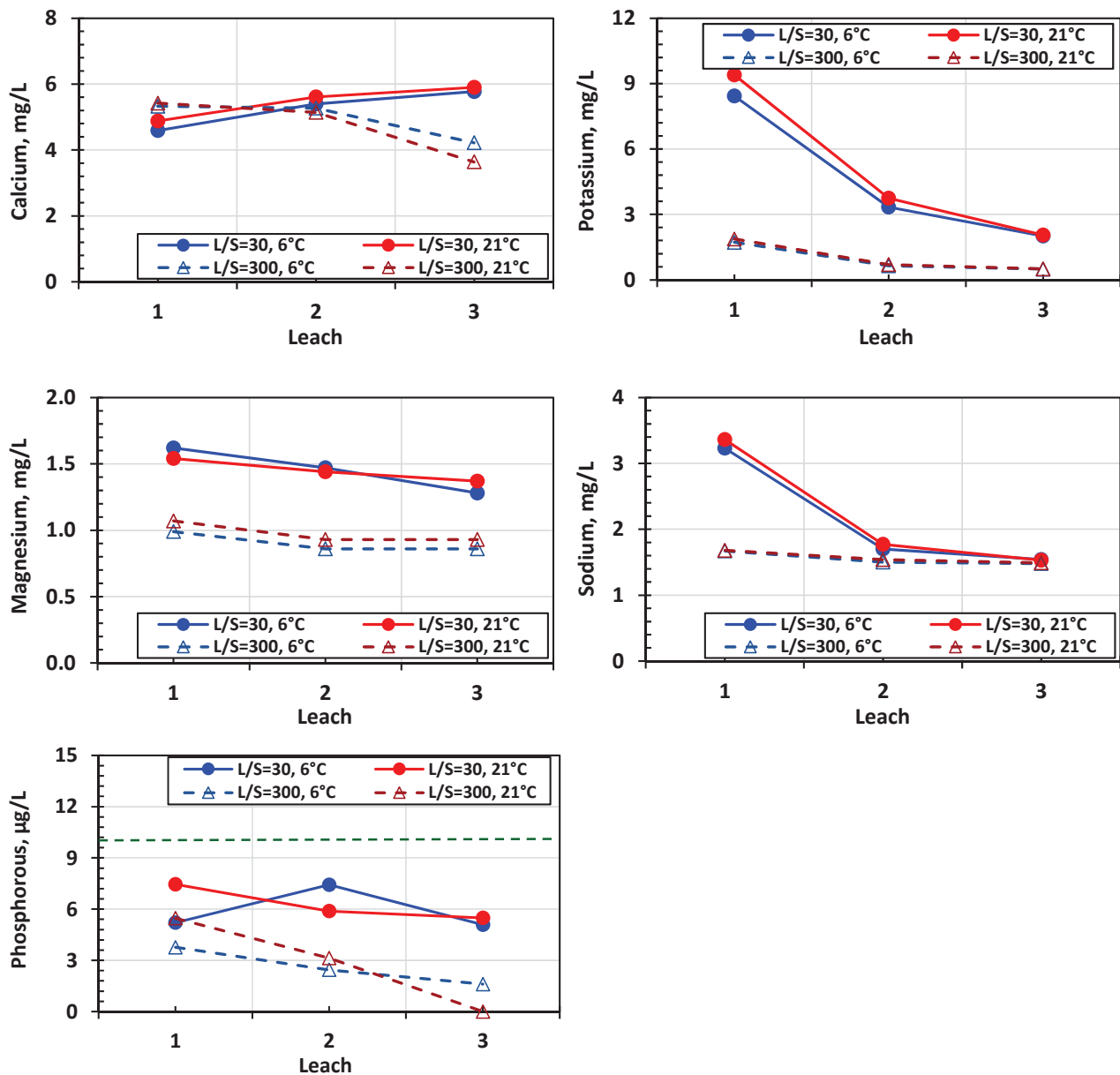


Figure D7.1. Major cation and total-P concentrations for successive elutriates at 6°C and 21 °C of composite 1B at L/S of 30 and 300.

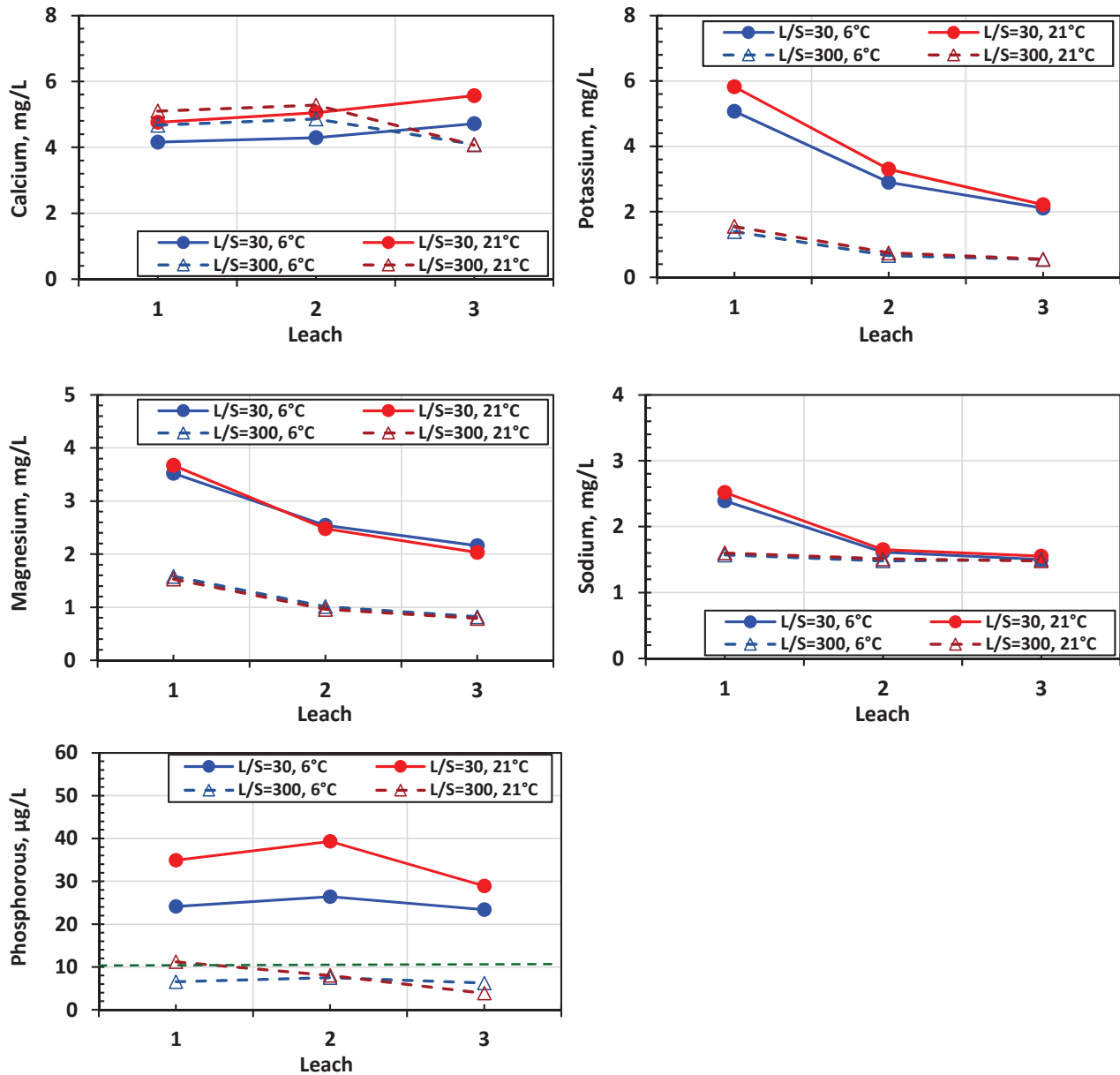


Figure D7.2 Major cation and total-P concentrations for successive elutriates at 6°C and 21 °C of composite 2B at L/S of 30 and 300.

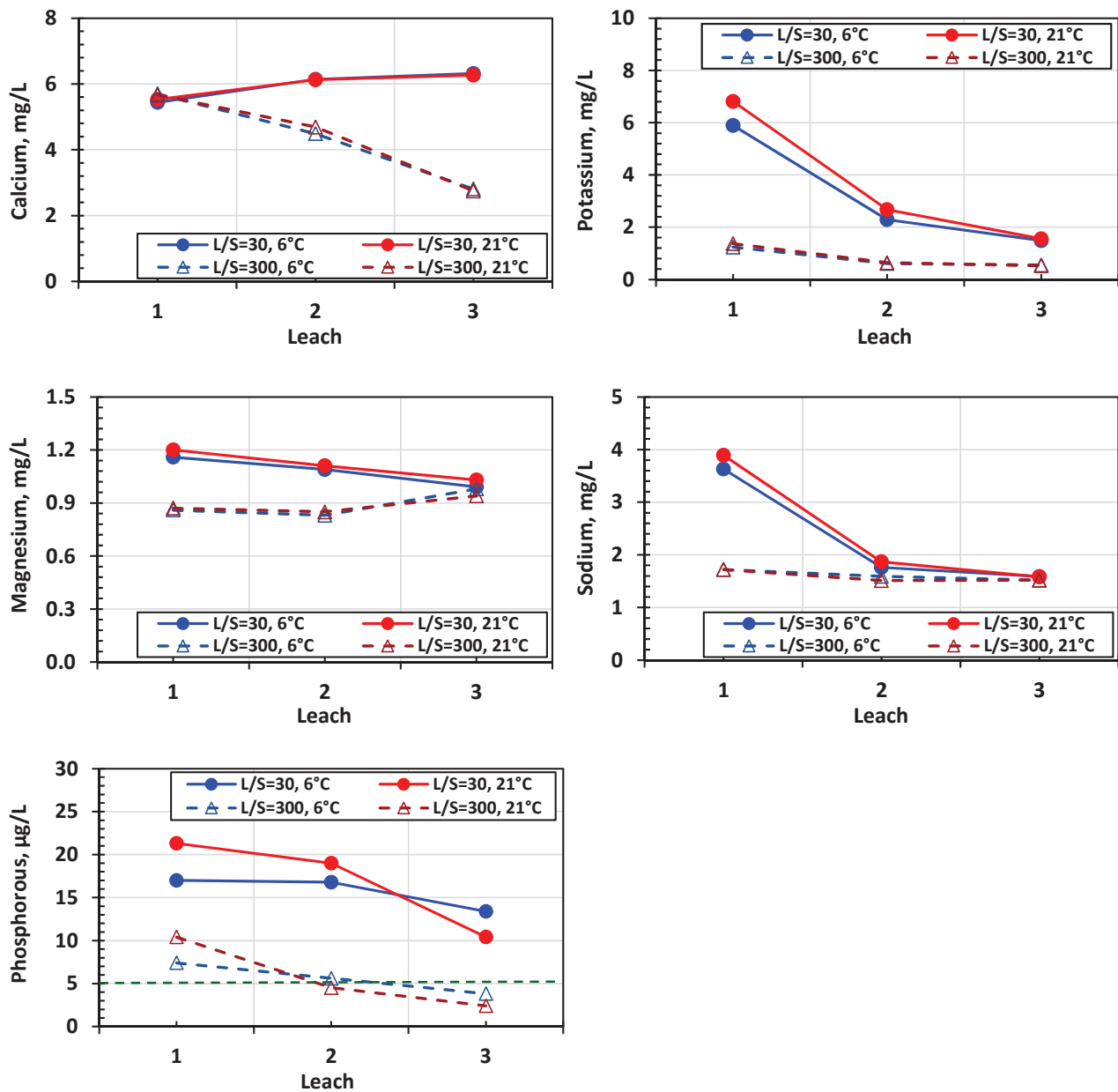


Figure D7.3. Major cation and total-P concentrations for successive elutriates at 6°C and 21 °C of composite 5B at L/S of 30 and 300.

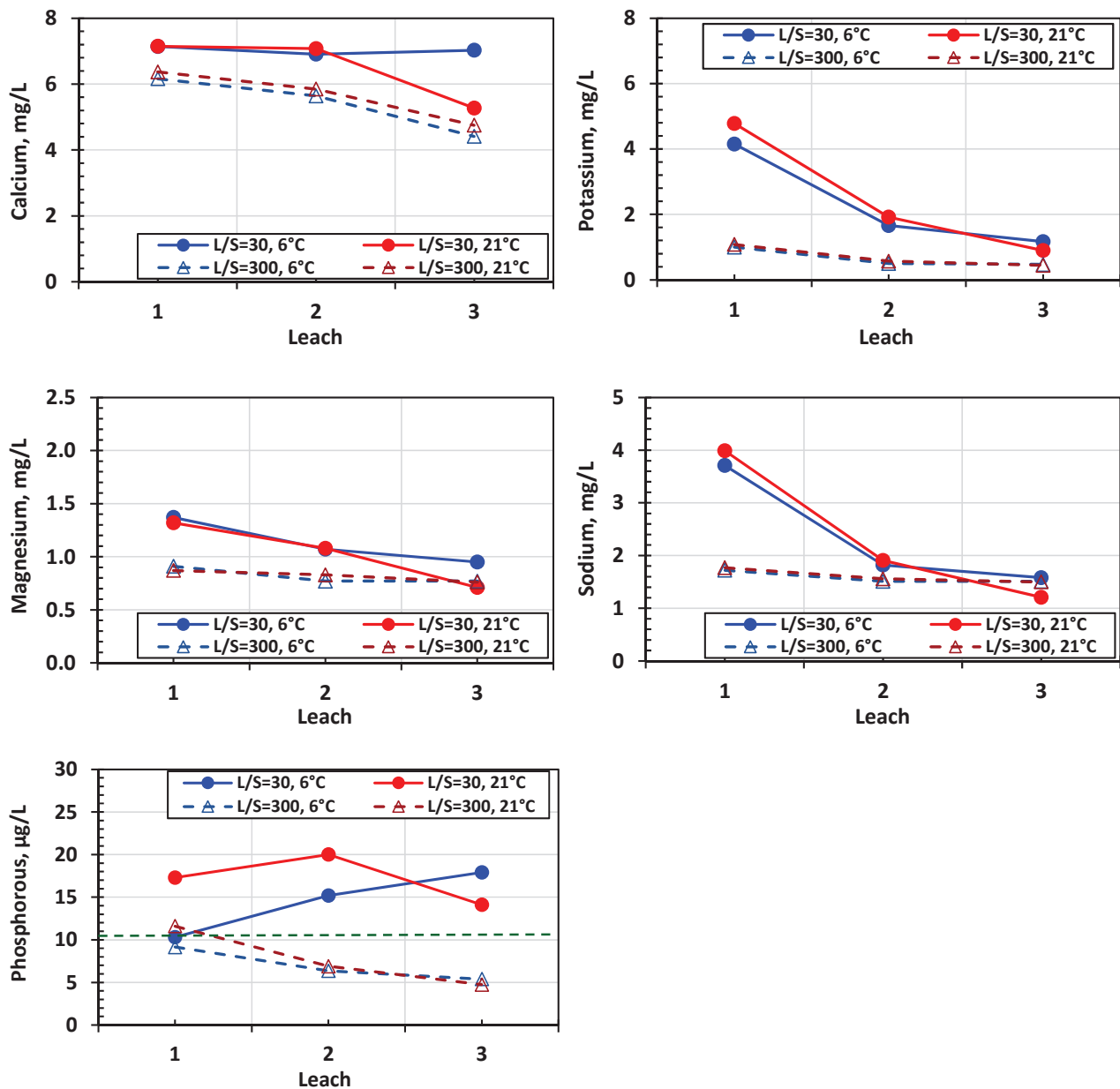


Figure D7.4. Major cation and total-P concentrations for successive elutriates at 6°C and 21 °C of composite 5E at L/S of 30 and 300.

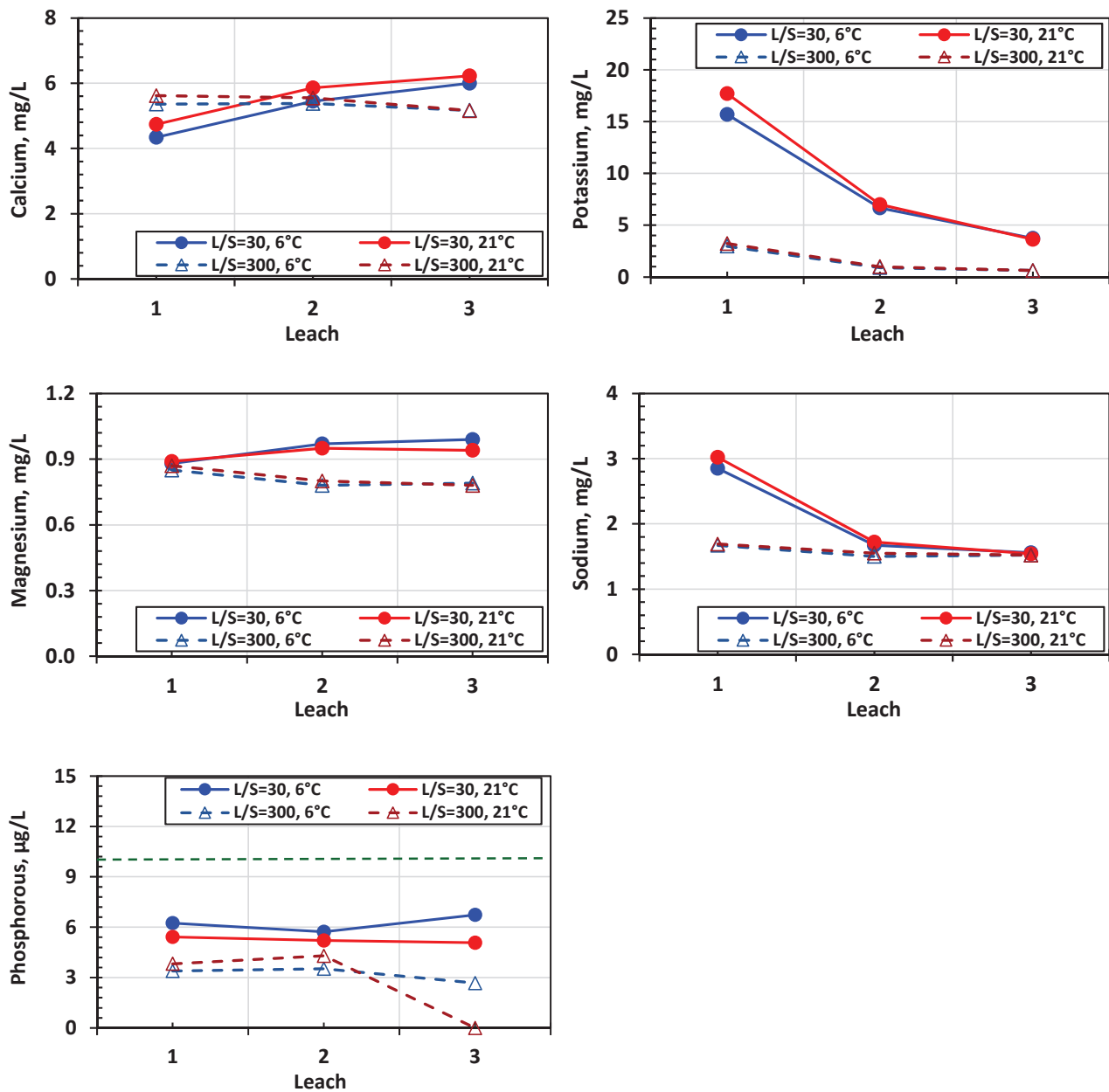


Figure D7.5. Major cation and total-P concentrations for successive elutriates at 6°C and 21 °C of composite 7E at L/S of 30 and 300.

Appendix D8. Colloidal forms of Al with <0.45 µm filtered water

| | |
|------------------|---|
| Note/Memo | CSIRO P4 Project Investigations |
| To: | Ali Watters (HKA) |
| From: | Brad Angel, Lucas Heights, NSW |
| Date: | 23 November 2018 |
| Copy: | Ryan Fraser, Stuart Simpson and Ellen Porter (SHL) |
| Our reference: | CSIRO P4 – Memo 12 |
| Classification: | Internal use only |
| Subject: | Pollutant release from excavated rock composites: effect of successive leaches and temperature on water quality and pollutant release |

Chemical formulas and acronyms

| | | | | | |
|-----|--------------|-----|-------------------------|-----|--------------------|
| Al | Aluminium | DGV | Default guideline value | L/S | Liquid/solid ratio |
| SEC | Conductivity | | | | |

Background - Introduction

The CSIRO was engaged by Haskoning Australia Pty Ltd (RHDHV) to undertake an investigation of the pollutant release from excavated rock disposal into Talbingo and Tantangara reservoirs. Previous elutriate tests (e.g. Memos 4, 5, 6) investigating the release of pollutants from composite excavated rock samples have observed significant changes in water quality with respect to pH, conductivity (SEC) and the dissolved aluminium concentrations. The temperature of elutriate solutions was also shown to have a strong effect on water quality and aluminium concentrations (Memo 9).

This technical memo describes results of two series of successive elutriate tests (3 leaches each) performed to investigate the effect of excavated rock composites 1B, 2B, 5B, 5E and 7E in Talbingo reservoir water on pH, conductivity (SEC), and the dissolved aluminium concentration. The first successive leach test series investigated the effect of two mixing durations for two liquid to solid (L/S) ratios at 21°C. The second successive leach test series investigated the effect of temperature (6°C and 21°C) for the two L/S ratios. The tests were performed using the following conditions:

- Successive leach test series 1
 - L/S = 30 and 300 i.e. 33 and 3.3 g/L, respectively
 - Mixing durations for each successive leach of either 0.5 or 18 h
 - Talbingo reservoir water at 21±2°C
- Successive leach test series 2
 - L/S = 30 and 300 i.e. 33 and 3.3 g/L, respectively
 - Mixing durations for each successive leach of 18 h
 - Talbingo reservoir water at 6±1°C and 21±2°C

Test methodology

The 75 µm milled composites 1B, 2B, 5B, 5E and 7E characterised in memo 3 were used in the successive leach tests. The desired mass of each sample was weighed into 50 mL acid washed polyethylene tubes, to which 50 mL of composite Talbingo (TAL-PL1A, TAL-PL2A and TAL-PL2B) reservoir water was added. The water was adjusted to 6°C and 21°C before addition. For successive leach test series 1, the treatments were shaken (50 rpm) at 21°C for either 0.5 or 18 h for each cycle. For successive leach test series 2, the treatments were shaken for 0.5 h, then stood in temperature controlled rooms (6±1°C and 21±2°C) for another 17.5 h so that they were in contact with the water for 18 h for each leach cycle. This allowed an additional comparison of the effect of mixing vs standing for the 18 h, 21±2°C treatments in tests series 1 and 2.

After each leach cycle, the tubes were centrifuged (2000 g, 5 mins) followed by subsampling for measurement of pH, SEC, and dissolved (0.45 µm) metals analyses. The remaining supernatant was decanted and 50 mL fresh composite Talbingo reservoir water of the desired temperature added. The tube and its' contents were weighed before adding fresh reservoir water to check on the residual water carried over from one leach to the next; this was 2-4% by volume and considered negligible. The process was repeated so that each treatment received three leaches in total.

Results

Test series 1 (0.5 h or 18 h mixing, 21°C):

The pH, conductivity and dissolved aluminium concentrations measured in successive leach test series 1 (21°C treatments) with excavated rock composites 1B, 2B, 5B, 5E and 7E are shown in Figures 1, 2, 3, 4 and 5, respectively.

For all excavated rock samples at each L/S ratio and mixing duration, the pH of the leach 1, 2 and 3 solutions were in the range 9.23-9.67, 8.83-9.57, and 7.89-9.51, respectively. The pH was generally higher for a lower L/S ratio and longer mixing duration and decreased in each successive leach.

For all excavated rock samples at each L/S ratio and mixing duration, the conductivity of the leach 1, 2 and 3 solutions were in the range 50-133, 40-89, and 33-117 µS/cm, respectively. The conductivity was more variable than pH, but was generally marginally higher for the lower L/S, and for the 300 L/S ratio, was higher for the longer mixing duration. Apart from a few treatments, the conductivity generally decreased in each successive leach.

For all excavated rock samples at each L/S ratio and mixing duration, the concentration of dissolved aluminium in the leach 1, 2 and 3 solutions were in the range 26.6-329, 26.7-416, and 26.5-512 µg/L, respectively. The concentration of dissolved aluminium was generally similar or increased over successive leaches, despite the water pH successively decreasing. The exception was the 300 L/S, 18 h mixing duration treatments, where the aluminium concentration of leach 2 was similar or higher than leach 1, but often decreased for leach 3. Figures 1-5 also show that mixing duration (i.e. leach contact time) was more important than the L/S ratio, as the 0.5 h treatments for each L/S ratio also had lower concentrations of dissolved aluminium than the 18 h treatments.

The dissolved aluminium exceeded the default guideline value (DVG) of 55 µg/L for three leaches of each material for the 18 h mixing duration. The DGV was never exceeded for the 300 L/S, 0.5 h treatments, with the dissolved aluminium remaining at a similar concentration for each successive leach, i.e. the short 0.5 h mixing duration at this L/S was not adequate to either release enough aluminium to exceed the DGV or exhaust the pool of aluminium in the samples, so the concentration remained steady. The concentration of dissolved aluminium released in the 30 L/S, 0.5 h treatments always increased over successive leaches, with the initial leach often being below the DGV and the later leaches being above the DGV.

Test series 2 (0.5 h mixing, 17.5 h standing, 6°C or 21°C):

The pH, conductivity and dissolved aluminium concentrations measured in successive leach test series 2 (6°C and 21°C treatments) with excavated rock composites 1B, 2B, 5B, 5E and 7E are shown in Figures 6, 7, 8, 9 and 10, respectively.

The pH was higher for a lower L/S ratio, but temperature generally had little effect on pH. The pH was generally similar or marginally lower over successive leaches for the 30 L/S ratio, while for the 300 L/S ratio the pH was generally similar between the first two leaches then decreased for the third leach.

There were no discernible trends for the conductivity in successive leach test series 2, i.e. temperature had no clear effect on conductivity. The conductivity was in the range 35-402 $\mu\text{S}/\text{cm}$.

For all excavated rock samples at each L/S ratio at 6°C, the concentration of dissolved aluminium in the leach 1, 2 and 3 solutions were in the range 23.1-109, 27.9-129, and 16.8-137 $\mu\text{g}/\text{L}$, respectively, and at 21°C, the concentration of dissolved aluminium in the leach 1, 2 and 3 solutions were in the range 93.6-299, 125-403, and 65.0-384 $\mu\text{g}/\text{L}$, respectively. Less aluminium was released in the lower temperature treatments for each L/S ratio, and more aluminium was released by treatments with a lower L/S ratio. For the 21°C treatments the dissolved aluminium was generally steady or decreased over the successive leaches, whereas, for the 6°C treatments the dissolved aluminium was steady or increased over the successive leaches. The dissolved aluminium exceeded the default guideline value (DVG) of 55 $\mu\text{g}/\text{L}$ for all of the leaches of the 21°C treatments and most leaches of 6°C, 30 L/S treatments, while the DGV was not exceeded by any of the 6°C, 300 L/S treatments.

A comparison of the 21°C treatments that were in contact with the reservoir water for 18 h, 0.5 h mixing (successive leach test series 2) and 18 h mixing (successive leach test series 1) indicated that longer physical mixing often caused an increase in the release of dissolved aluminium (Figure 11); most evident for the 2nd and 3rd leaches. This is likely to be the cause of the difference in trends over successive leaches between the tests for the 21°C treatments i.e. generally steady or increased in test series 1 and generally steady or decreased in test series 2.

Discussion

The lack of an effect of temperature on the conductivity and pH indicates the increase in pH occurs due to a rapid release of ions that increase the alkalinity, and this release likely occurs via ion exchange reactions. This is supported by measurements of rapid pH increase in previous tests of kinetics (Memos 6 and 11).

The results of the successive leach tests showing sustained release of aluminium over successive leaches is evidence of a dissolution process controlling the release of aluminium. This process continues while the excavated rock particles are in contact with the reservoir water and contain aluminium in forms that can be released. This process occurs more slowly at a lower temperature, so the pool of available aluminium is drawn down more slowly resulting in a greater pool available in successive leaches for the lower temperature treatments. In other words, the aluminium available for dissolution is depleted more slowly at a lower temperature.

The increased release for successive leaches and longer mixing times may be influenced by water taking time to fully encompass / contact all of the surfaces of rock particles (i.e. porosity), or particles disaggregating over time, particularly for longer mixing durations, leading to more surfaces being available for dissolution reactions to occur.

Summary

Successive leaches of excavated rock samples with Talbingo reservoir water did not rapidly exhaust the aluminium available for release into solution. To the contrary, many treatments had similar or increased aluminium concentrations in the 2nd and 3rd successive leaches. The lower temperature substantially decreased the concentration of aluminium released into reservoir waters. These results suggest a dissolution process is responsible for the release of aluminium, which is dependent on the duration of contact with water and the temperature. Longer durations of physical mixing also generally increased the release of dissolved aluminium.

The DGV for aluminium, 55 µg/L, was exceeded by most treatments in the successive leach tests.

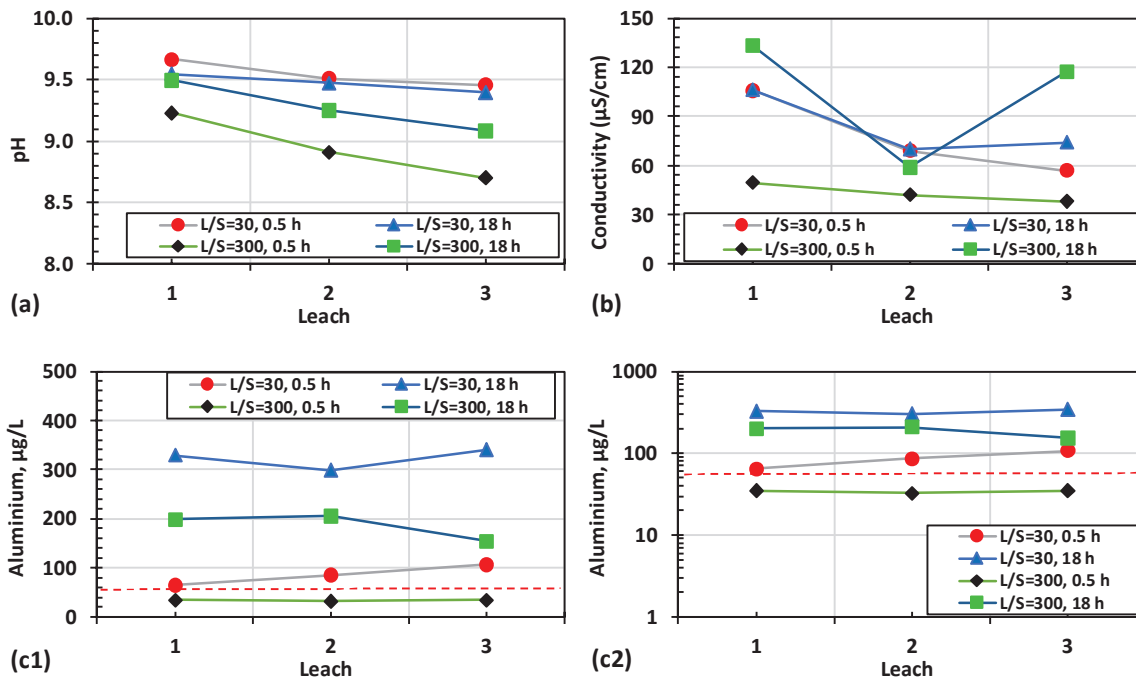


Figure 1. The pH, conductivity and dissolved aluminium concentration after three successive leach cycles at $21\pm 2^\circ\text{C}$ for excavated rock sample 1B (successive leach test 1), where the effect of mixing duration and L/S ratio was investigated (c2 = log scale). The 95% species protection default guideline value for dissolved aluminium is shown by the red dotted line.

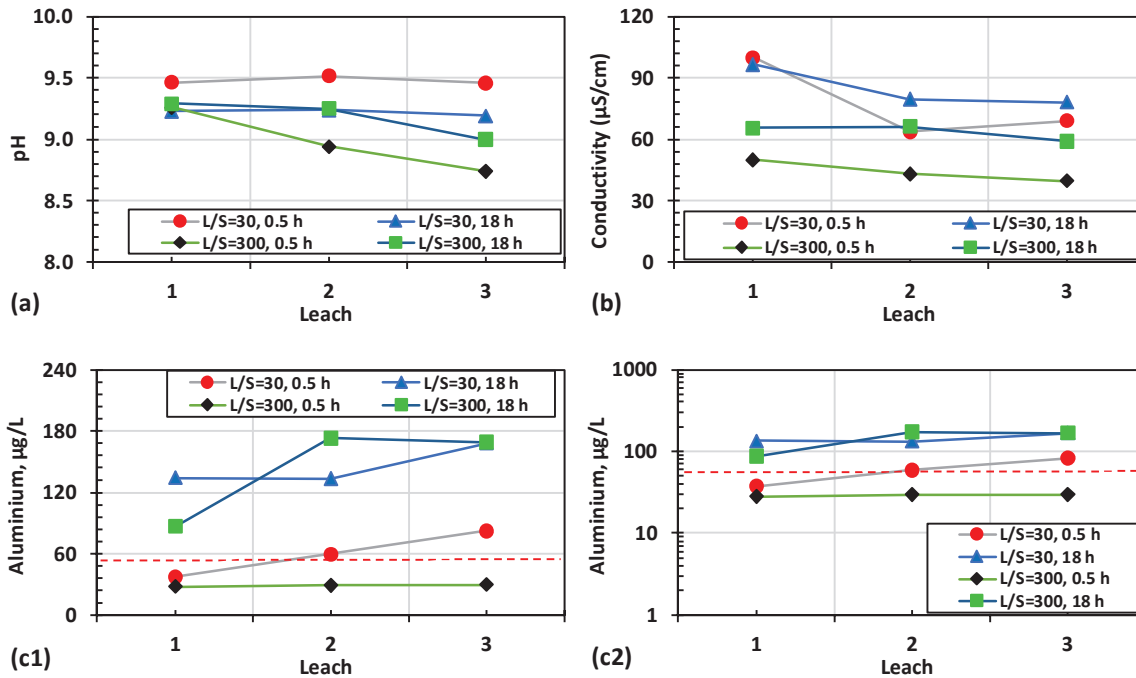


Figure 2. The pH, conductivity and dissolved aluminium concentration after three successive leach cycles at $21\pm 2^\circ\text{C}$ for excavated rock sample 2B (successive leach test 1), where the effect of mixing duration and L/S ratio was investigated (c2 = log scale). The 95% species protection default guideline value for dissolved aluminium is shown by the red dotted line.

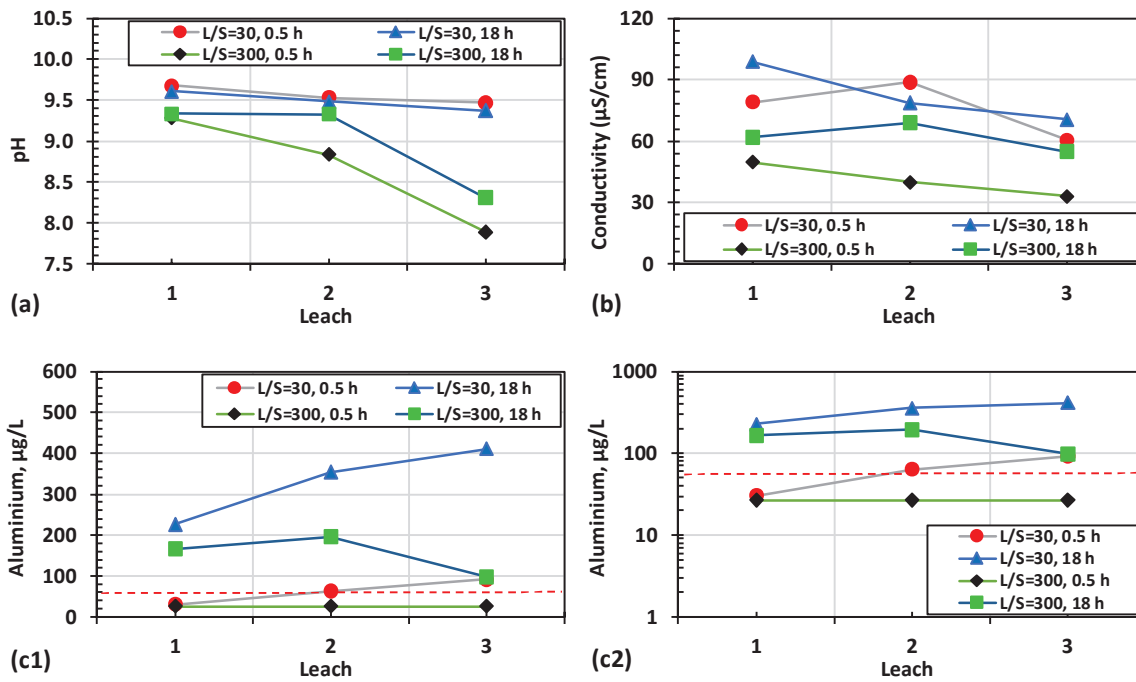


Figure 3. The pH, conductivity and dissolved aluminium concentration after three successive leach cycles at $21\pm 2^\circ\text{C}$ for excavated rock sample 5B (successive leach test 1), where the effect of mixing duration and L/S ratio was investigated (c2 = log scale). The 95% species protection default guideline value for dissolved aluminium is shown by the red dotted line.

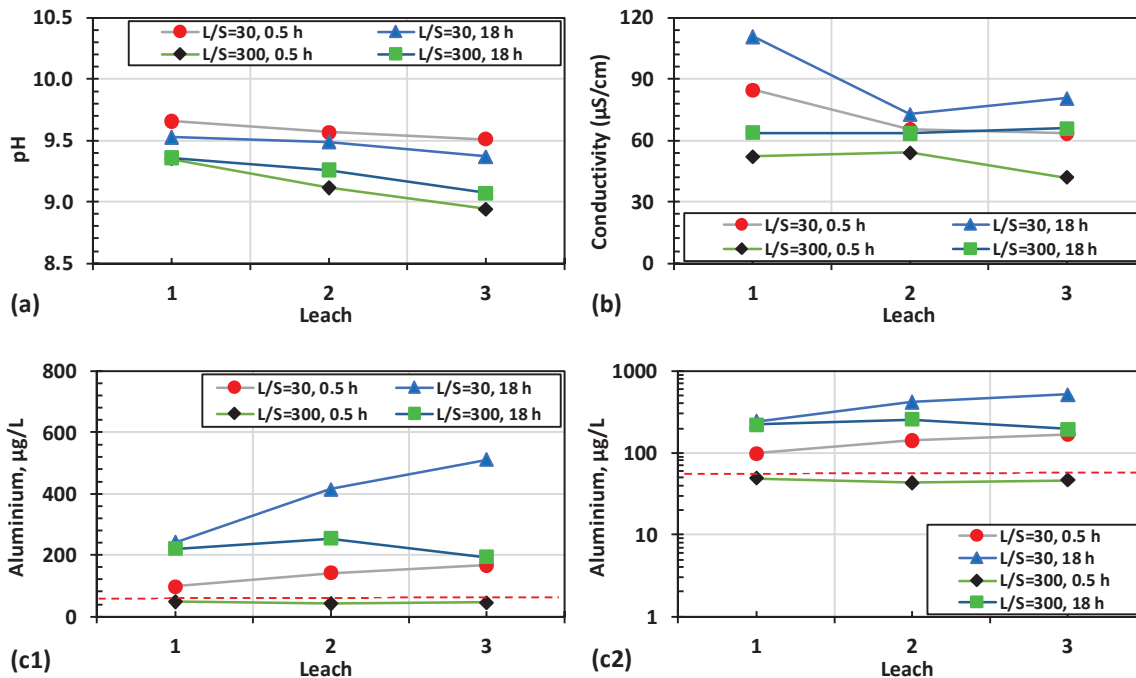


Figure 4. The pH, conductivity and dissolved aluminium concentration after three successive leach cycles at $21\pm 2^\circ\text{C}$ for excavated rock sample 5E (successive leach test 1), where the effect of mixing duration and L/S ratio was investigated (c2 = log scale). The 95% species protection default guideline value for dissolved aluminium is shown by the red dotted line.

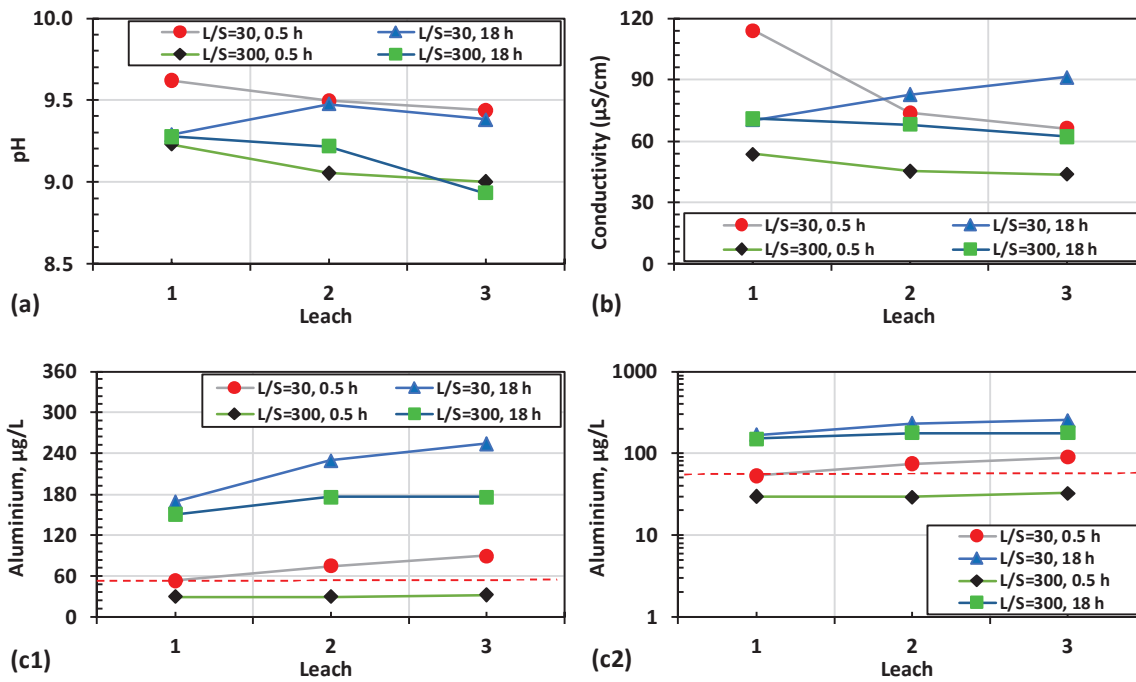


Figure 5. The pH, conductivity and dissolved aluminium concentration after three successive leach cycles at $21 \pm 2^\circ\text{C}$ for excavated rock sample 7E (successive leach test 1), where the effect of mixing duration and L/S ratio was investigated (c2 = log scale). The 95% species protection default guideline value for dissolved aluminium is shown by the red dotted line.

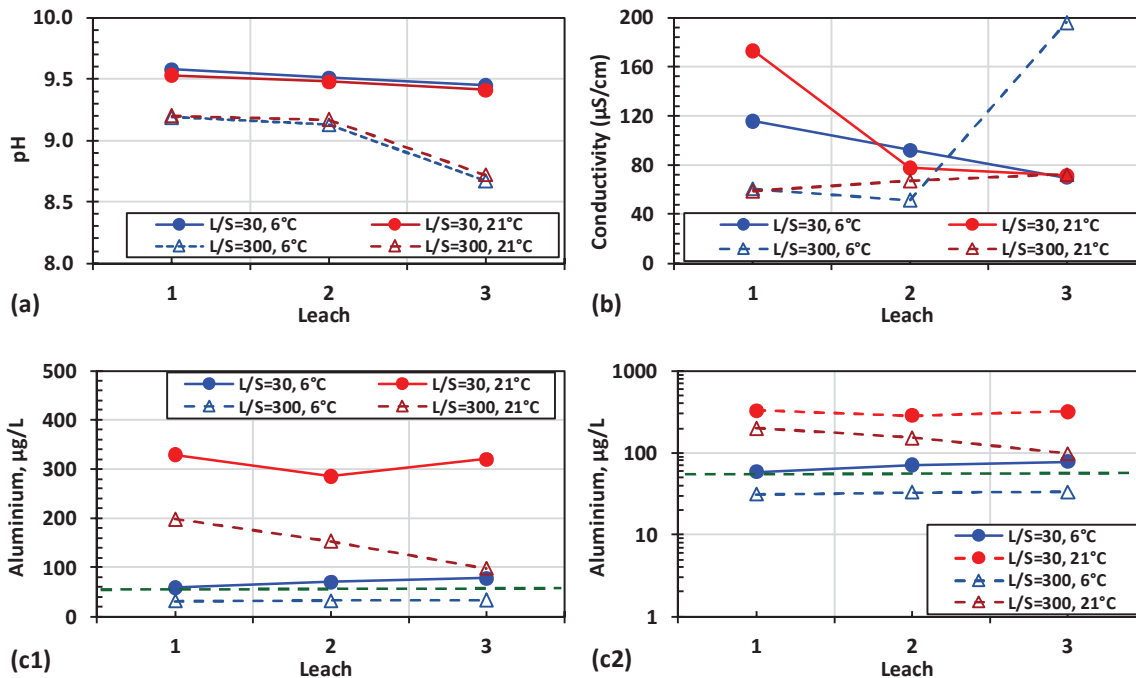


Figure 6. The effect of temperature on the pH, conductivity and dissolved aluminium concentration after three successive leach cycles at $6 \pm 1^\circ\text{C}$ and $21 \pm 2^\circ\text{C}$ for excavated rock sample 1B (successive leach test 2), (c2 = log scale). The 95% species protection default guideline value for dissolved aluminium is shown by the green dotted line.

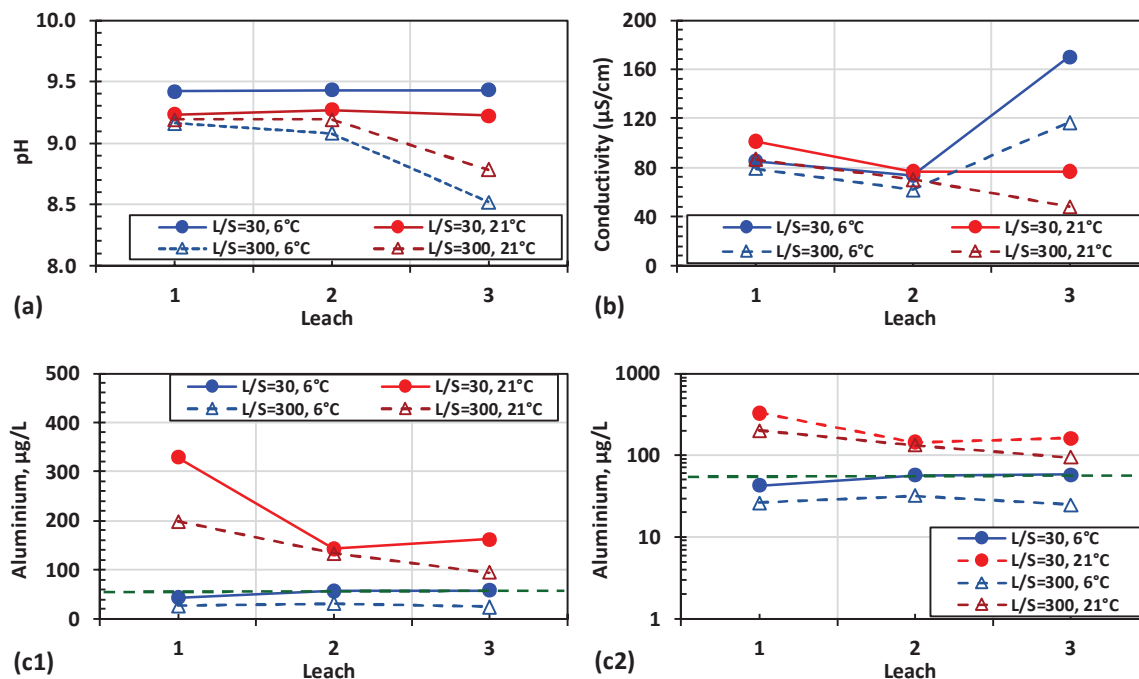


Figure 7. The effect of temperature on the pH, conductivity and dissolved aluminium concentration after three successive leach cycles at $6\pm1^{\circ}\text{C}$ and $21\pm2^{\circ}\text{C}$ for excavated rock sample 2B (successive leach test 2), (c2 = log scale). The 95% species protection default guideline value for dissolved aluminium is shown by the green dotted line.

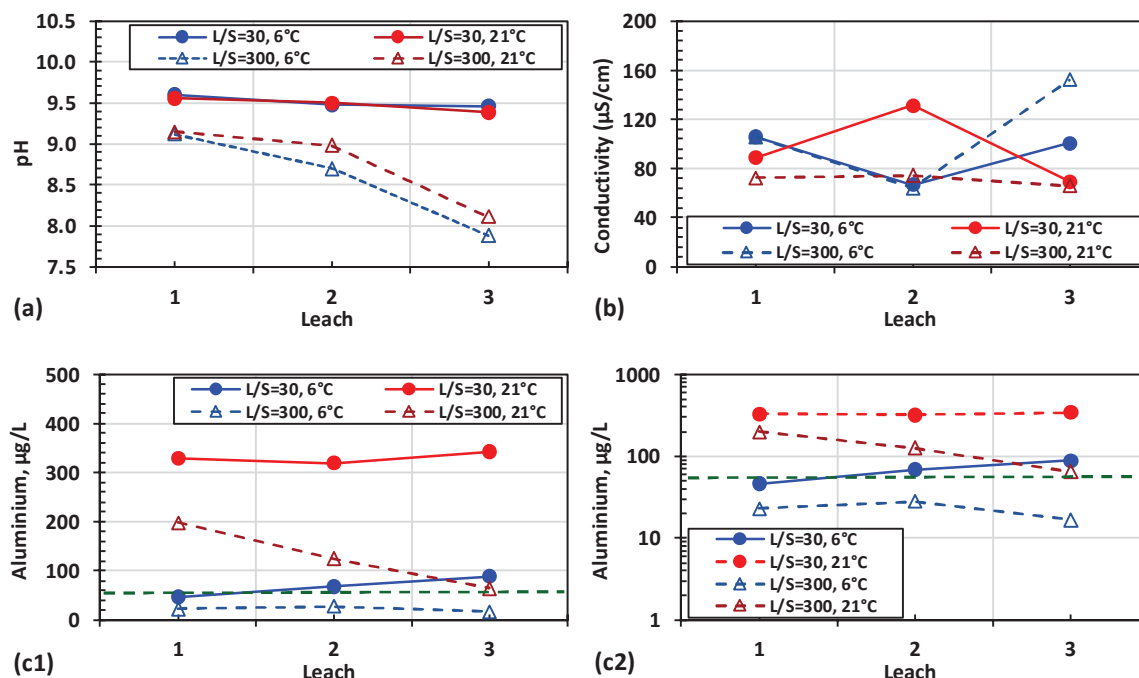


Figure 8. The effect of temperature on the pH, conductivity and dissolved aluminium concentration after three successive leach cycles at $6\pm1^{\circ}\text{C}$ and $21\pm2^{\circ}\text{C}$ for excavated rock sample 5B (successive leach test 2), (c2 = log scale). The 95% species protection default guideline value for dissolved aluminium is shown by the green dotted line.

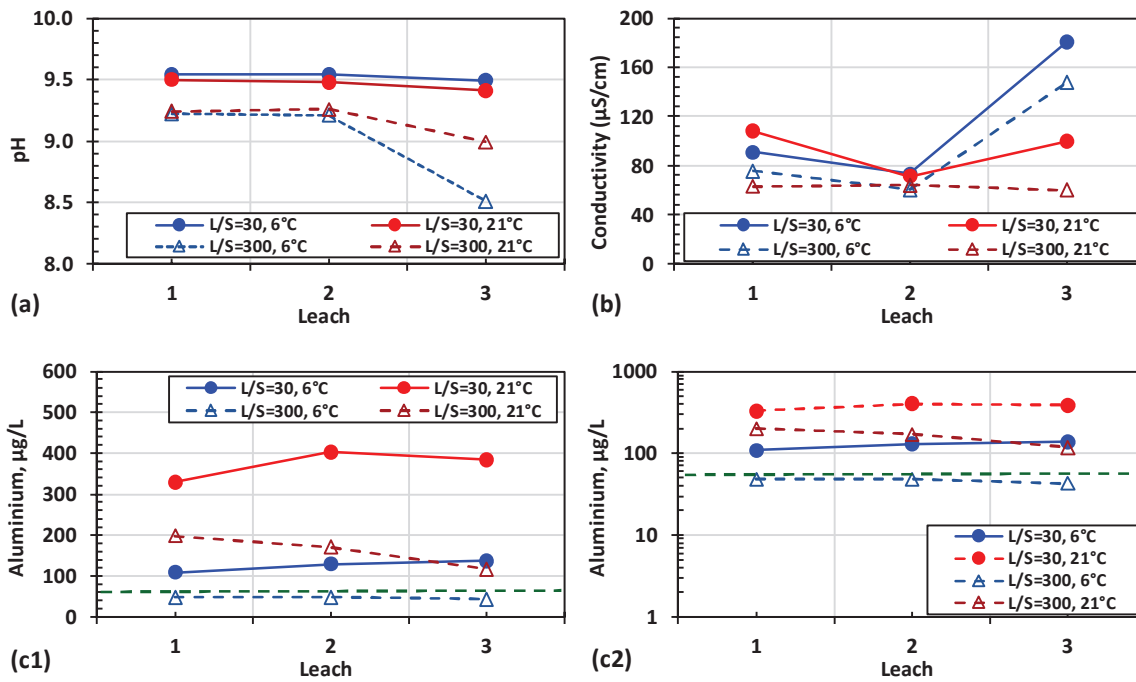


Figure 9. The effect of temperature on the pH, conductivity and dissolved aluminium concentration after three successive leach cycles at $6\pm1^{\circ}\text{C}$ and $21\pm2^{\circ}\text{C}$ for excavated rock sample 5E (successive leach test 2), (c2 = log scale). The 95% species protection default guideline value for dissolved aluminium is shown by the green dotted line.

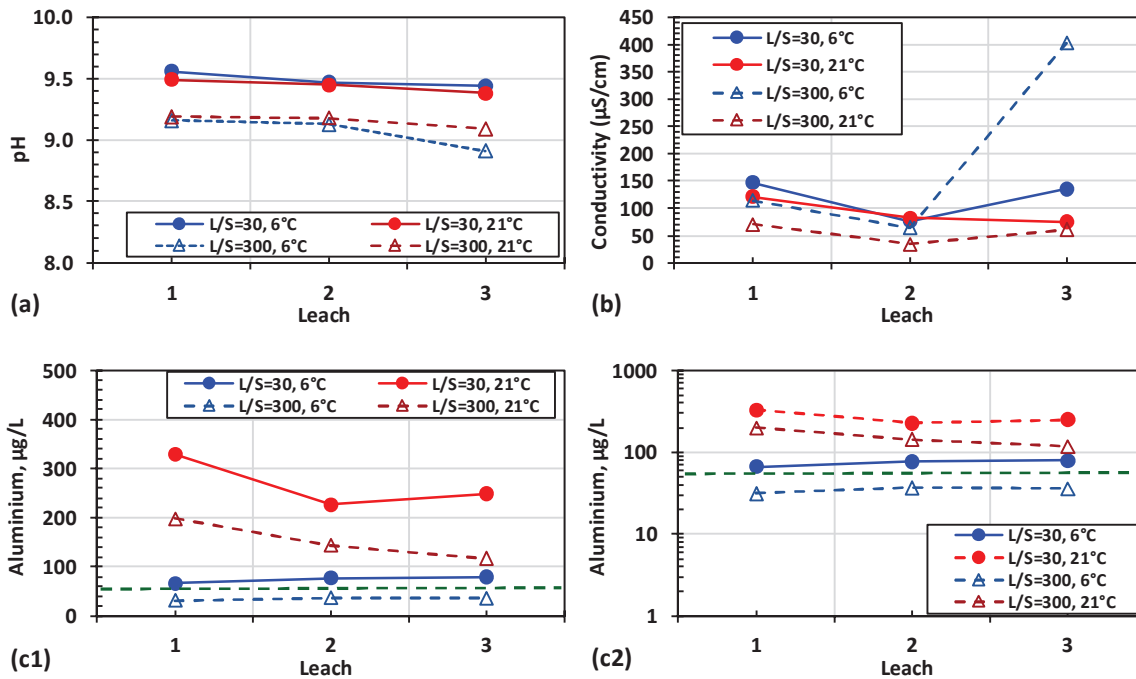


Figure 10. The effect of temperature on the pH, conductivity and dissolved aluminium concentration after three successive leach cycles at $6\pm1^{\circ}\text{C}$ and $21\pm2^{\circ}\text{C}$ for excavated rock sample 7E (successive leach test 2), (c2 = log scale). The 95% species protection default guideline value for dissolved aluminium is shown by the green dotted line.

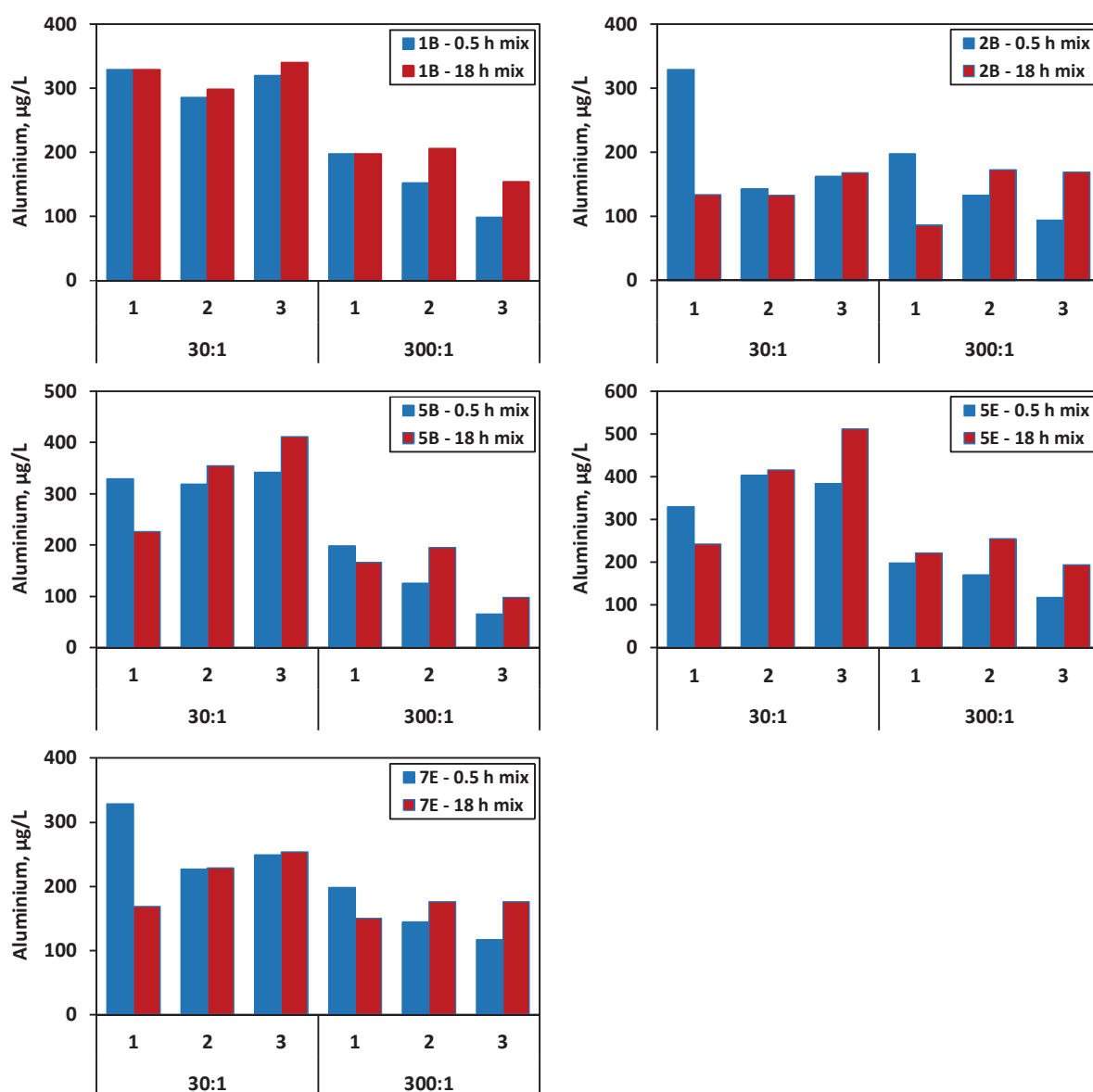


Figure 11. Comparison between the dissolved aluminium released from excavated rock material at L/S ratios of 30 and 300 in Talbingo reservoir water after 18 h contact with water between successive leach test 1 (18 h mixing, red bars) and leach test 2 (0.5 h mixing, 17.5 h standing, blue bars) at 21°C to assess the effect of mixing vs standing for each successive leach (1, 2 and 3).

Appendix D9. Longer term substance release

Appendix D10. Effect of resuspended sediment in attenuation of substances released from rock materials

| | |
|------------------|---|
| Note/Memo | CSIRO P4 Project Investigations |
| To: | Ali Watters (HKA) |
| From: | Brad Angel, Lucas Heights, NSW |
| Date: | 8 November 2018 |
| Copy: | Ryan Fraser, Stuart Simpson and Ellen Porter (SHL) |
| Our reference: | CSIRO P4 – Memo 10 |
| Classification: | Internal use only |
| Subject: | Pollutant release from excavated rock composites – Attenuation Test 1 |

Chemical formulas and acronyms

| | | | | | |
|-----|--------------|-----|-------------------------|--|--|
| Al | Aluminium | dAl | Dissolved aluminium | | |
| SEC | Conductivity | L/S | Liquid/solid ratio | | |
| | | DGV | Default guideline value | | |

Background - Introduction

The CSIRO was engaged by Haskoning Australia Pty Ltd (RHDHV) to undertake an investigation of the pollutant release from excavated rock disposal into Talbingo and Tantangara reservoirs.

The initial elutriate tests (Memo 4) investigating the release of pollutants from composite excavated rock samples (L/S = 10, 48 h) observed some significant changes in water quality with respect to pH, conductivity (SEC) and the dissolved aluminium concentrations:

- pH increased from 7.0-7.1 to 8.9-9.8 range
- SEC increased from 29 $\mu\text{S}/\text{cm}$ to 110-200 $\mu\text{S}/\text{cm}$ range, and
- Dissolved Al (<0.45 μm filterable) increased from <4 $\mu\text{g}/\text{L}$ (ppb) to 200-800 $\mu\text{g}/\text{L}$ range.

The conditions of those elutriate tests, L/S = 10, 48 h, were designed to assess a severe / worst case scenario for impacts to the receiving water in which large amounts of fine excavated rock materials may remain suspended in the waters in the main disposal area.

Following release of substances from the fine-rock materials, a series of attenuation processes may occur, such as adsorption of dissolved aluminium onto particulate matter. A series of tests are underway to determine the magnitude and rate of attenuation that occurs in the presence of resuspended and deposited sediments.

This technical memo describes results of the initial attenuation test performed using elutriate waters from six fine-rock composites (liquid to solid ratio (L/S) of 500) created during the 'Alkalinity' tests 4 days earlier (Memo 7). Attenuation of pollutants in these elutriate solutions was investigated using a single sediment (PL2) material resuspended at L/S=500 and L/S=50, where L=elutriate and S=sediment. The sediment-elutriate was shaken to mix for 10 sec, and then left to settle for 24 h, after which, the pH, SEC and dissolved metals were measured. This is referred to as a sediment resuspension-attenuation test.

Changes in elutriate water composition with time

While it was not the intent of this test to investigate this, some interesting observations were made.

The pH and conductivity of the elutriate waters that were used in the tests (2nd row for each material in Table 1) differed from that of the original elutriate water (1st row for each material) that had been prepared four days earlier and allowed to sit overlying the small amount of fine-rock composition it was prepared from (i.e. 2 g fine-rock/1 L Talbingo water). Except for 1E, generally the pH was approximately one unit lower – potentially due to equilibration with air (increased carbon dioxide dissolving into the waters). All of the elutriate waters used had a higher conductivity than the original elutriate water – consistent with some further dissolution of salts from the solids that remained wet during the 4 day period before the attenuation test was performed.

Attenuation

The effect of 2 and 20 g/L of PL2 sediment compared to no added sediment on the pH, conductivity and dissolved aluminium in the elutriate solutions is shown in Figure 1. The pH and conductivity of the elutriate waters decreased with increasing amounts of resuspended sediment, as measured 24 h after the sediment resuspension occurring. The dissolved aluminium concentrations in the 2 g/L added sediment treatments were substantially lower than the elutriate treatments with no added sediment, indicating the sediment attenuated the aluminium. However, for the 20 g/L added sediment treatments, variable results were observed; the addition of 20 g/L PL2 sediment resulted in lower concentrations of dissolved aluminium for elutriates 3E and 4E, similar concentrations for elutriate 2E, and higher concentrations for elutriates 1E, 5E and 7E. These results indicate that competing processes occur upon the addition of sediment to the elutriate solutions; the dissolved aluminium may decrease via adsorption onto particulate matter, but the sediment may also act as a source of aluminium and increase its' concentration, possibly in colloidal form.

Points to note:

- The pH ranges for the L/S = 500 and 50 sediment resuspension-attenuation tests were 7.1-7.6 and 6.5-6.6, respectively compared to the pH range for the initial waters of 7.8-8.0, and that of the Talbingo Reservoir water of pH 7.0.
- The conductivity ranges for the L/S = 500 and 50 sediment resuspension-attenuation tests were 56-96 $\mu\text{S}/\text{cm}$ and 33-55 $\mu\text{S}/\text{cm}$ respectively compared to the conductivity range for the initial waters of 98-188 $\mu\text{S}/\text{cm}$, and that of the Talbingo Reservoir water of 25-40 $\mu\text{S}/\text{cm}$.
- The dissolved aluminium ranges for the L/S = 500 and 50 sediment resuspension-attenuation tests were 18-28 $\mu\text{g}/\text{L}$ and 73-186 $\mu\text{g}/\text{L}$, respectively compared to the range for the initial waters of 76-176 $\mu\text{g}/\text{L}$, and that of the Talbingo Reservoir water of ca. 5 $\mu\text{g}/\text{L}$.
- The dissolved aluminium in the porewater of the PL2 sediment was 600 $\mu\text{g}/\text{L}$ (reported in memo 2 and shown in Table 2 below). Based on the mass of sediment and volumes of test solutions, the maximum contribution of porewater aluminium from the addition of 20 g/L PL2 would be less than 10 $\mu\text{g}/\text{L}$. Therefore, significant aluminium is contributed by the particulate phase of the PL2 sediment. Additional information on the sediment contribution of aluminium and its' increase over time will be reported for other attenuation tests that have been performed in a future memo.

Summary

The interaction of the elutriate water with the reservoir sediment resulted in pH and conductivity decreasing to levels similar to the original reservoir water. The dissolved aluminium concentrations decreased in the presence of 2 g/L of PL2 sediment, but were variable in the presence of 20 g/L PL2 sediment; lower for 3E and 4E, similar 2E, and higher for 1E, 5E and 7E. The results indicate sediments may decrease dissolved aluminium via adsorption, but also contribute aluminium when resuspended.

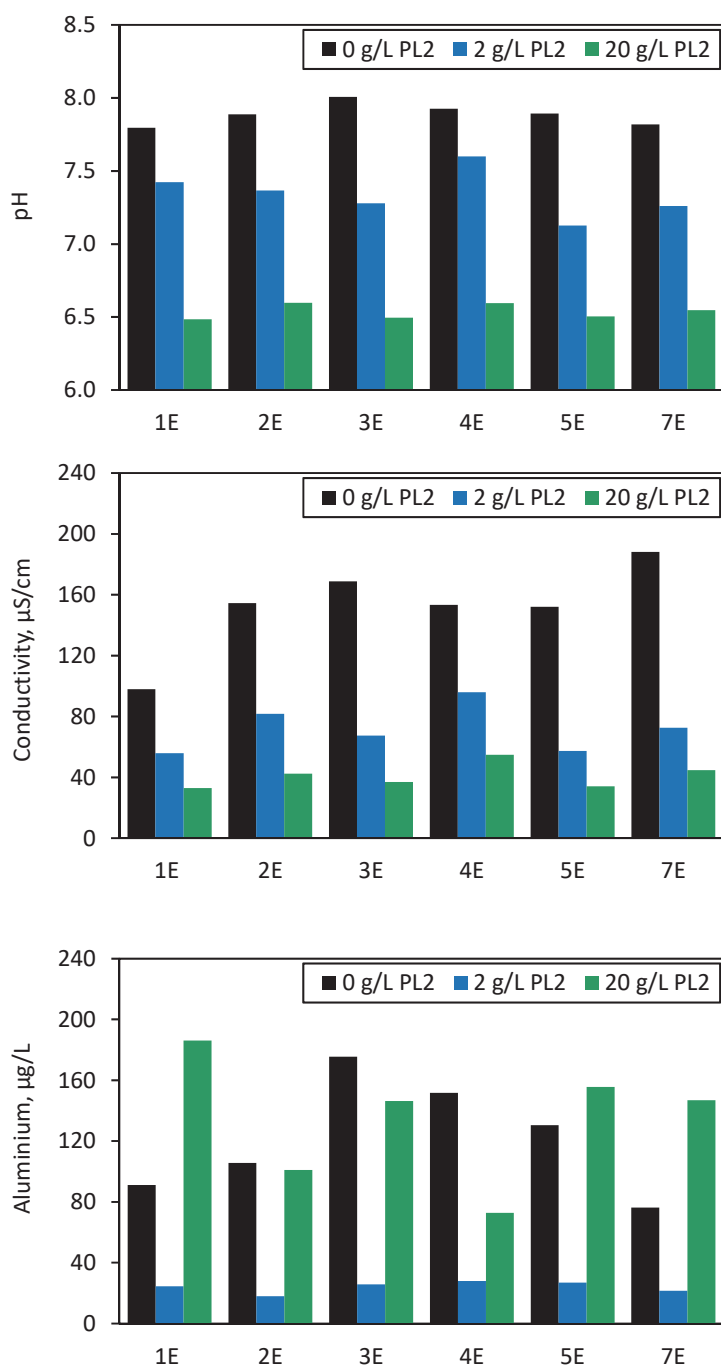


Figure 1. The pH, conductivity and dissolved aluminium after 0, 2 and 20 g/L of PL2 sediment was mixed for 10 s with 4-d old composite (1E, 2E, 3E, 4E, 5E and 7E) elutriates then allowed to stand for 24 h before measurement.

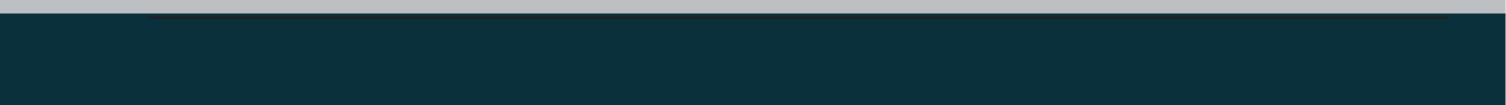
Table 1. The pH, conductivity and dissolved aluminium for sediment-resuspension attenuation Test 1.

| Sample | L/S, where L= elutriate, S=sediment | Time h | pH | Conductivity μS/cm | dAL μg/L |
|-----------------------|--|-----------|-----|-----------------------|-------------|
| 1E original elutriate | Prepared 4 days earlier | | 7.8 | 60 | NM |
| 1E elutriate used | ∞ | 24 h | 7.8 | 98 | <u>91</u> |
| 1E | 500 [2 g sediment/L elutriate] | 24 h | 7.4 | 56 | 24 |
| 1E | 50 [20 g sediment/L elutriate] | 24 h | 6.5 | 33 | <u>186</u> |
| 2E original elutriate | Prepared 4 days earlier | | 8.8 | 45 | NM |
| 2E elutriate used | ∞ | 24 h | 7.9 | 155 | <u>106</u> |
| 2E | 500 | 24 h | 7.4 | 82 | 18 |
| 2E | 50 | 24 h | 6.6 | 43 | <u>101</u> |
| 3E original elutriate | Prepared 4 days earlier | | 9.1 | 51 | NM |
| 3E elutriate used | ∞ | 24 h | 8.0 | 170 | <u>176</u> |
| 3E | 500 | 24 h | 7.3 | 67 | 26 |
| 3E | 50 | 24 h | 6.5 | 37 | <u>146</u> |
| 4E original elutriate | Prepared 4 days earlier | | 9.1 | 90 | NM |
| 4E elutriate used | ∞ | 24 h | 7.9 | 150 | <u>152</u> |
| 4E | 500 | 24 h | 7.6 | 96 | 28 |
| 4E | 50 | 24 h | 6.6 | 55 | <u>73</u> |
| 5E original elutriate | Prepared 4 days earlier | | 9.0 | 52 | NM |
| 5E elutriate used | ∞ | 24 h | 7.9 | 150 | <u>130</u> |
| 5E | 500 | 24 h | 7.1 | 57 | 27 |
| 5E | 50 | 24 h | 6.5 | 34 | <u>156</u> |
| 7E original elutriate | Prepared 4 days earlier | | 8.8 | 54 | NM |
| 7E elutriate used | ∞ | 24 h | 7.8 | 190 | <u>76</u> |
| 7E | 500 | 24 h | 7.3 | 73 | 22 |
| 7E | 50 | 24 h | 6.5 | 45 | <u>147</u> |
| DGV | | | - | - | 55 |

Elutriate used differs from original elutriate in that it was prepared 4 days earlier. NM = not measured.

Table 2. The pH, conductivity, redox potential and dissolved aluminium measured in sediment porewaters reported in memo 2.

| Sediment ID | pH | Conductivity (μS/cm) | Redox, Eh (mV) | Al (μg/L) |
|----------------|------|-------------------------|-------------------|--------------|
| CA1 | 7.30 | 23.5 | -175 | 10 |
| CA2 | 7.60 | 26.5 | -180 | 8 |
| CA3 | 7.45 | 19.0 | -170 | <u>67</u> |
| PL1 | 7.05 | 20.0 | -140 | <u>278</u> |
| PL2 | 7.30 | 15.7 | -125 | <u>600</u> |
| PL3 | 7.40 | 18.9 | -160 | 32 |
| RA1 | 7.25 | 22.7 | -160 | <u>144</u> |
| RA2 | 7.30 | 24.0 | -185 | 51 |
| RA3 | 7.50 | 21.6 | -190 | 6 |
| TN1 | 6.70 | 33.0 | -105 | <u>180</u> |
| TN2 | 7.10 | 36.0 | -140 | <u>179</u> |
| TN3 | 7.00 | 36.7 | -155 | <u>59</u> |
| Minimum | 6.70 | 15.7 | -190 | 5.5 |
| Maximum | 7.60 | 36.7 | -105 | 600 |
| DGV | - | - | - | 55 |



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Annexure D Ecotoxicology Assessment of Excavated Rock

Ecotoxicological Assessment of Excavated Rock Leachates in Water and Excavated Rock-Sediment Mixtures

Snowy 2.0, CSIRO Assignment P5

Anu Kumar, Merrin Adams, Adrienne Gregg, Bhanu Nidumolu, Andrea Ramirez Sepulveda and Angel Rea

27th June 2019

Prepared for Haskoning Australia (HKA) on behalf of Snowy Hydro Limited (SHL)

Report number: EP191174

[Commercial-in-confidence]

Citation

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Total 143 pages in the Final Report and three appendices prepared as supplementary information (Appendix B, Appendix I and Appendix J).

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Foreword and Assignment Summary

CSIRO was requested by Snowy Hydro Limited (SHL) in November 2017 to provide scientific expertise and capability in relation to identifying and assessing the environmental risks associated with the placement of excavated rocks from the development and operations of the proposed Snowy 2.0 Project. EMM Consulting (EMM) is preparing the Environmental Impact Statement (EIS) on behalf of SHL, and CSIRO's role was to develop and undertake a series of assignments to provide information to inform handling of excavated rock materials from the proposed works. In December 2017, CSIRO worked with EMM to develop conceptual models to provide information for the environmental risk assessment (ERA). As a result, CSIRO agreed to undertake an initial series of five assignments.

In March 2018, Haskoning Australia (HKA) was engaged to provide additional capability, specifically to lead the project entitled: "Engineering Option for Placement of Excavated Rocks". The draft work assignments that CSIRO had previously provided to SHL and EMM (in late January 2018) were subsequently updated to ensure that they would fulfil the needs of the EIS requirements and HKA's "Engineering Option for placement of Excavated Rocks" project. These updated assignments have been executed and are providing relevant input into the ERA.

This report details the results of Assignment P5. *Ecotoxicological Assessment of Excavated Rock Leachates in Water and Excavated Rock-Sediment Mixtures*

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Abbreviations/Acronyms

| Abbreviation / Acronym | Description |
|------------------------|--|
| µg | microgram |
| AEM | Dilute-acid extractable metal (or other element) |
| CRM | Certified reference material |
| d | day |
| DGV | Default guideline value |
| DO | Dissolved oxygen |
| DOC | Dissolved organic carbon |
| EC | Electrical conductivity |
| Eh | Redox potential |
| EIS | Environmental impact statement |
| GV | Guideline Value, replaces term 'trigger value' (TV) in water quality guidelines (ANZG, 2018) |
| h | hour |
| kg | kilogram |
| L | litre |
| L/S | Liquid/solid ratio |
| LoE | Line of evidence |
| M | mol per litre |
| mg | milligram |
| Milli-Q | High purity deionised water |
| mL | millilitre |
| mm | millimetre |
| PC95(50) | concentration that is protective of 95% of species (with 50% confidence) |
| PC99(50) | concentration that is protective of 99% of species (with 50% confidence) |
| PSU | Practical salinity units |
| QA/QC | Quality assurance/quality control |
| SD | standard deviation |
| SE | standard error |
| SEM | Scanning electron microscope |
| SQGV | Sediment quality guideline value |
| TOC | Total organic carbon |
| TRM | Total recoverable metal (or other element) |
| TSS | Total suspended solids |
| WOE | Weight of evidence |
| WQGV | Water quality guideline value (ANZECC/ARMCANZ, 2000) |

Chemical symbols and Acronyms

| | | | | | |
|-----------------|---|------------------------------|------------|-------------------------------|-----------|
| Ag | Silver | F ⁻ | Fluoride | Sb | Antimony |
| Al | Aluminium | Fe | Iron | Se | Selenium |
| As | Arsenic | Mg | Magnesium | Sn | Tin |
| Ba | Barium | Mn | Manganese | SO ₄ ²⁻ | Sulphate |
| Ca | Calcium | Mo | Molybdenum | Sr | Strontium |
| Cd | Cadmium | Na | Sodium | Th | Thorium |
| Cl ⁻ | Chloride | Ni | Nickel | U | Uranium |
| Co | Cobalt | NO ₃ ⁻ | Nitrate | V | Vanadium |
| Cr | Chromium | Pb | Lead | Zn | Zinc |
| Cu | Copper | | | | |
| dAl | Dissolved Aluminium (<0.45 µm filtered) | | | | |
| | | | | | |

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Executive Summary

Snowy Hydro Limited (SHL) is exploring options for the placement of “excavated rock” within two reservoirs (Talbingo and Tantangara) as part of a proposed expansion of their operations known as Snowy 2.0 Pumped Hydro Electric Scheme (Snowy 2.0). The excavated rock placement should not compromise, within reasonable parameters, the ecological, chemical, physiochemical, or physical state of the environment in the reservoirs.

CSIRO was engaged by Haskoning Australia (HKA) on behalf of SHL to provide four studies involving tests and data analysis to help inform an Environmental Impact Statement (EIS) for Snowy 2.0. These studies are:

- Assignment P1: Comprehensive Geochemistry Examination;
- Assignment P2: Environmental Risk Categorisation of Rock Materials;
- Assignment P4: Environmental Categorisation of Excavated Rock Interactions with and Potential Impacts on Reservoir Waters and Sediments; and
- Assignment P5: Ecotoxicological Assessment of Excavated Rock Leachates in Water and Excavated Rock-Sediment Mixtures.

This report relates to the ecotoxicological assessment of excavated rock addition to reservoir waters and sediments, and is an output of Assignment P5.

Assignment P5 - Ecotoxicological Assessment of Excavated Rock Leachates in Water and Excavated Rock-Sediment Mixtures provides information on the potential toxicity of leachates of excavated rock and excavated rock-sediment mixtures. These potential toxicities were used to assess the potential impacts of the excavated rock materials on water and sediment quality within the two reservoirs. Fourteen excavated rock materials were selected to represent the possible range of materials that may be placed in the reservoirs; they comprised ‘Baseline’ and ‘Enriched’ rock composites for seven of nine geological units likely to be intercepted during construction of the 27 km of tunnel (refer to the Assignment P2 report for detailed descriptions). The waters and sediments used in the testing were collected from locations where excavated rock placement may potentially occur. The toxicity to microalgae and three invertebrate species under various interactions of the rock materials and reservoir waters/sediments was evaluated, so as to generate results relevant to a range of scenarios and environmental conditions.

The water samples from the Talbingo and Tantangara Reservoirs exhibited no acute toxicity to water fleas, midge larvae and blackworms. In relation to water quality guidelines (ANZG, 2018), the concentrations of contaminants of potential concern (COPCs) in waters were less than the corresponding guideline values (GVs), i.e. they represented no impediment to preserving the ecological status. Few of the metals present in rock materials were present at concentrations in excess of the sediment quality GV.

During the period that excavated rock placement within the reservoirs occurs, significant amounts of fine rock material may remain present in the waters, and the finest fractions may take many weeks or months to settle after placement activities cease. The properties of substances released from submerged rock materials was assessed using a series of tests that involved mixing and

leaching rock with reservoir water. Leachates from excavated rock and water with ratios from 1 to 10 were used. Toxicity tests (chronic and acute) with representatives of four groups of aquatic life (a microalga, a water flea, a midge and blackworm) were carried out on leachates of excavated rock material prepared with water from Talbingo or Tantangara Reservoirs. Leachates of excavated rock had high levels of suspended solids (turbidity) that did not completely settle out of solution after 24 h. Therefore, the toxicity of leachates was assessed with water fleas, midges and blackworms on raw and/or after 12-day settling and/or filtered leachates. Microalgae were only tested with filtered leachates.

Toxicity tests (chronic) with midges and blackworms were carried out on excavated rock material under varying scenarios of mixing and layering. Benthic sediment scenarios ranged from predominantly excavated rock becoming the substrate, to excavated rock mixing with sediments to form a smaller fraction of the substrate, and also thin layers of excavated rock that may spread and deposit at locations away from the main placement area. Measurements of dominant stressors (e.g. dissolved metals, pH, electrical conductivity (EC) and suspended solids) in toxicity tests provided information to link the ecotoxicology effects to stressors.

The waters within the reservoirs (in which excavated rock placement may occur) are generally quite clear (low suspended solids), have low EC, and have low buffering capacity (low alkalinity). Based on an integrated ranking system as given below in Table E1, the raw leachates from enriched excavated rock materials from Ravine, Byron and Shaw zones exhibited high toxicity. The toxicity tests using raw leachates are the 'worst case' scenarios unlikely to be encountered during placement activities. Settling of some leachates at 4°C for 12 days reduced turbidity but fine colloidal particles were still found to be suspended in the leachate. 12-day settled leachates from the Kellys (Enriched) and Byron (Baseline) zones exhibited moderate toxicity. Turbidity in the range of 50-200 NTU due to suspension of particulate material from excavated rock can also harm fish and other aquatic life during chronic long-term exposures by reducing food supplies, degrading spawning beds, and affecting gill function.

Macroinvertebrates including midge and blackworms are present in the Talbingo and Tantangara Reservoirs and were used as test organisms in this study to assess impacts associated with sedimentation of excavated material. Sediments mixed with excavated rock or top of reservoir sediments generally showed no toxicity to low toxicity during 7-day exposures to midge larvae and 28-day exposure to blackworms. Exposures to neat Enriched excavated rock material from all zones as a worst-case scenario exhibited moderate toxicity to high toxicity. As an integrated toxicity assessment, Shaw (Enriched and Baseline), Volcanics (Enriched) and Peppercorn (Baseline) excavated material exhibited low to moderate level toxicity to blackworms and midge larvae when exposed as mixtures of sediment and excavated rock material mixtures.

Increase in turbidity and metals and metalloids such Al that might be introduced to the water body as a consequence of suspended sediments from the excavated rock and/or due to sedimentation. These multistressors could result in low level of toxicological, physiological or physical impacts on fish and macroinvertebrates. Suggestions for collection of further biological assessment data for Talbingo and Tantangara reservoirs, including ecotoxicological effects and an ongoing in-situ monitoring program based on sufficient baseline data are provided.

Table E1. Integrated toxicological assessment as toxic units (TU) and colour coding based on the acute and chronic tests conducted in this study. 100% raw leachate and neat excavated rock material exposures are the worst-case scenarios and are not expected during the excavated rock placement within the reservoirs. Higher the toxic unit (TU) greater the toxicity (e.g. TU 2.0-2.2 represent high toxicity and TU 0.0 – 0.3 represent no toxicity).

| | | Leachates | | | Sediments | | |
|------------|---|-----------|---------|----------|-----------|-------|------|
| Scenarios | | Raw | Settled | Filtered | Top | Mixed | Rock |
| Ravine | B | 1.3 | 0.3 | 0.7 | 0.7 | 0.0 | 0.0 |
| | E | 2.0 | 0.3 | 0.3 | 0.0 | 0.0 | 2.0 |
| Byron | B | 1.3 | 1.0 | 0.7 | 0.0 | 0.0 | 0.0 |
| | E | 2.0 | 0.3 | 0.7 | 0.0 | 0.0 | 2.3 |
| Shaw | B | 1.3 | 0.0 | 0.3 | 1.7 | 1.0 | 2.0 |
| | E | 2.0 | 0.3 | 1.0 | 0.7 | 0.0 | 1.0 |
| Volcanics | B | 1.3 | 0.7 | 0.7 | 0.0 | 0.0 | 2.0 |
| | E | 1.7 | 0.7 | 1.3 | 1.0 | 1.7 | 1.0 |
| Peppercorn | B | 1.3 | 0.3 | 0.3 | 1.7 | 0.7 | 2.0 |
| | E | 1.3 | 0.0 | 0.3 | 0.3 | 0.7 | 2.0 |
| Kellys | E | NA | NA | 0.0 | NA | NA | NA |
| | B | 1.0 | 1.0 | 1.0 | 0.0 | 0.0 | 0.0 |
| Felsic | B | 1.3 | 0.7 | 0.3 | 0.0 | 0.0 | 2.0 |
| | E | 1.0 | 0.3 | 0.7 | 0.7 | 0.0 | 1.0 |

1 Introduction

1.1 Background

Snowy Hydro Limited (SHL) is embarking on the development of the landmark Snowy 2.0 Pumped Hydro Electric Scheme (Snowy 2.0). As part of Snowy 2.0, options are being sought for the management and ultimate placement of excavated rock as part of an Environmental Impact Statement (EIS) and practical engineering options for its management. There are several challenges associated with this expansion and an extensive environmental assessment is necessary. To accomplish Snowy 2.0, a 27 km tunnel will be excavated between the Talbingo and Tantangara Reservoirs. This process will remove approximately 9 million m³ of excavated rock (bulked) that will need to be disposed of primarily within these two reservoirs. Land-based placement of significant quantities of excavated rock not possible within the National Park, nor is it practicable to remove it from the project area.

Haskoning Australia (HKA) have been appointed lead consultant to manage and deliver an Engineering Option Assessment for Excavated Rock Placement for Snowy 2.0. CSIRO has been requested to provide scientific insight into the environmental impacts associated with the excavated rock placement options.

As the subsurface geology was largely unknown, a geological study complemented by a geochemical and mineralogical characterisation was required to determine the composition of the materials to be extracted in the construction phase. Before its placement within the reservoirs, the excavated rock will be temporarily stockpiled on land and then relocated, along with other materials, into the reservoirs. It is required that the excavated rock be deemed physically and chemically stable now and into the future so the ecological, chemical, physiochemical, and physical state of the environment is not compromised. Further, the placement of the excavated rock (to the extent possible) must:

- not compromise existing reservoir operations during the expansion construction;
- not compromise existing environmental flows;
- ensure extreme and “1 in 100” year weather events do not impact the long-term stability of the excavated rock placed within either Talbingo or Tantangara Reservoirs;
- remain stable under maximum generation loads of approximately 350 cumecs (maximum pumping loads will be less) during expanded hydro operations (intake and outflow); and
- not adversely impact threatened species (both terrestrial and aquatic) located in, around and downstream of the reservoirs.

Finally, ensuring all the above, a social licence to operate must be maintained.

1.2 CSIRO work assignments

A series of work assignments were undertaken by CSIRO to inform the EIS:

- Assignment P1: Comprehensive Geochemistry Examination, i.e. mineralogy and geochemistry characterisation of excavated rock.
- Assignment P2: Environmental Risk Categorisation of Rock Materials, i.e. identifying the reactivity of the rock and its risk category;
- Assignment P4: Environmental Categorisation of Excavated Rock Interactions and Potential Impacts on Reservoir Waters and Sediments, i.e. categorising excavated rock impacts on reservoir water and sediments
- Assignment P5: Ecotoxicological Assessment of Excavated Rock Leachates in Water and Excavated Rock-Sediment Mixtures, i.e. assessing the ecotoxicological impact of placement of the excavated rocks within the reservoirs

This report relates to Assignment P5 and is provided to HKA to inform their work programs, considering both the needs of the EIS and the longer-term ecological risk assessment (ERA). Information from baseline studies (primarily from consultancy firm EMM) and from Assignments P1 and P2 (CSIRO) was used to select a subset of materials (excavated rock, waters and sediments) and conditions for use in Assignments P4 and P5.

1.3 Context of Assignment P5: Ecotoxicology

The context for the assessment is informed by the conceptual site model (CSM, Appendix A) and identification of pathways among pressures, stressors, and likely biological receptors and their responses. Although the likely placement method has since evolved, at the time of developing this assessment, the placement of excavated rock material was assumed to be in deep waters within the reservoirs, possibly via placement methods that result in rock material dropping through the water column with the intent of depositing them within a specific range of placement depths. In the CSM, the placement of excavated rock material was assumed to be in deep waters within the reservoirs, possibly via placement methods that result in rock material dropping through the water column with the intent of depositing them within a specific range of placement depths. The CSM incorporates the services for protection, which, for Snowy 2.0, will include the power assets, ecosystem, and recreational services. The CSM enables management aims, community values, management goals, and required levels of protection to be defined.

For Snowy 2.0, the assessment issue may be broadly categorised as a 'proposed development in a greenfields (undisturbed) location' or a more general 'development approval' (partly or moderately disturbed). For a greenfields location in advance of future development, the assessment issue relates to the gathering of baseline (pre-disturbance) data and information that enables prediction of potential impacts. Typically, following development of the CSM of existing and future pressures, the assessment should seek to provide an adequate baseline characterisation for defining the water quality and ecological health and potential organism sensitivities (and assessing other baseline pressures). In the case of the EIS, EMM has indicated that it is gathering baseline information on water quality (spatial and temporal) and ecosystem

status (i.e. what species and functions require protecting). Establishing the pre-development background conditions is necessary to determine the potential additive effects from additional stressors that might be introduced to the water body as a consequence of the proposed development.

The services for protection being considered in Assignment P4 (stressors) and Assignment P5 (ecosystem receptors) are broadly described as 'water quality', of which sediment quality is a component. The waters within the reservoirs (in which excavated rock placement may occur) are generally quite clear (low suspended solids), have low EC and have low buffering capacity (low alkalinity). In relation to Snowy 2.0 and Assignment P4, the stressors of potential concern (SOPCs) include physical and physico-chemical characteristics, such as suspended solids/sediment and benthic flocs of fine crushed material along with chemical contaminant stressors (e.g. traditional COPCs for which water and sediment quality guideline values exist) and the interactions of these multiple stressors. Multiple stressors may contribute complex and variable effects within ecosystems, and for many individual stressors, no guidelines exist. Furthermore, the interactions of different stressors and how these interactions influence aquatic organisms, is poorly understood.

The quality of the lines of evidence (LoE) is an important consideration for the assessment (EIS/ERA), and this is strongly influenced by the type of assessment. For Snowy 2.0 (development approval/greenfield site), use of chemistry and physical stressor data alone (Assignment P4) may frequently be considered as a low quality LoE. LoE assessments require integration with ecosystem receptors (biological effects). For Snowy 2.0, it is unlikely that any baseline ecosystem information exists to determine the potential sensitivity of the local ecosystem. Ecosystem receptors, or biological effects, include the assessment of toxicity to organisms, biodiversity (ecology and/or ecosystem function), bioaccumulation of substances by organisms and biomarkers (indicator of exposure to stressors).

Establishing the baseline for the biodiversity (ecology) LoE is important for: (i) identifying the key receptors (sensitive species and functions - biodiversity indicators) which can highlight the key potential sensitivities of the reservoir ecosystem, and (ii) selecting locations to represent the reference/control and potential impact sites (for which risks of adverse effects are to be assessed). This information will assist in identifying those classes/types of organisms and habitats that should be considered in more detail during assessment components that seek to predict potential adverse effects from the proposed development (i.e. potential stressors identified in P4). Thus, the ecology LoE for the Snowy 2.0 EIS/ERA assist but cannot enable a suitable prediction of impacts unless species' sensitivity to the stressors has been pre-established based on ecotoxicological approaches. The thresholds/tolerance limits of each stressor such as turbidity for key species present in the receiving environment (the two reservoirs) needs to be determined. Assignment P5 provides stressor sensitivities through direct assessment of potential effects using toxicity tests on representative and sensitive species (and endpoints) under conditions (stressor extremes and multiple stressors) predicted to potentially exist from Assignment P4.

Based on the present CSM, assessment of the potential for elevated bioaccumulation by local organisms seems unlikely to aid the weight of evidence (WoE) assessment. Biomarkers are limited in their interpretability because, without a direct known adverse outcome pathway connecting the

biomarker response to a population-based ecological outcome, biomarkers tend to indicate exposure to stressors, not necessarily biological effects.

Together, information from Assignments P1, P2, P4 and P5, supported by the baseline information is expected to provide the multiple LoEs to enable a WoE assessment to be undertaken (in accordance with current National Water Quality Management Strategy (NWQMS) assessment guidance, ANZG (2018): <http://www.waterquality.gov.au/anz-guidelines>).

1.4 Assignment P5: Ecotoxicology assessment of excavated rock leachates in water and excavated rock-sediment mixtures

Assignment P5 addresses the potential impacts of the excavated rock materials on water and sediment quality within the reservoirs to predict the risks of effects of potential management options for disposing the excavated rock material. It provides an ecosystem response (effect) using the ecotoxicology LoE and links with the stressor exposure LoE provided by P4. Like P4, this project uses excavated rock material, and leachates of excavated rock, considered representative of the proposed range of excavated rock placement operations. The reservoir waters and sediments used in this study were collected from locations where excavated rock placement sites/locations may eventually be chosen.

The ecotoxicity of reservoir waters and sediment before and after addition of excavated rock material provides information on the potential for the excavated rock to cause toxicity to organisms that inhabit the water column and sediments at the proposed placement sites. The project uses standardised bioassays with sensitive species to assess the acute and chronic effects that occur due to leachates of excavated rocks within waters (effects on water-column species) and excavated rock-sediment mixtures (effects on benthic species).

1.4.1 Potential impact pathways associated with placement of excavated material

Fine suspended sediments in water column may results in:

1. Reduced light penetration inhibiting growth of aquatic plants and algae with profound 'bottom-up' ecological impacts;
2. Damage to zooplankton such as waterfleas by clogging their filter feeding apparatus and digestive organs;
3. Reduced food quality of organic suspended matter for filter-feeders by 'dilution' with fine mineral sediment;
4. Toxicity mainly due to leaching of dissolved metals and other potential contaminants; and
5. Damage to respiratory structures such as irritation and clogging of the gills of fish.

Sediment particles are capable of adversely affecting benthic macroinvertebrates such as midge larvae and blackworms and could exhibit behavioural, physiological, or toxicological responses. The potential impact pathways can include:

1. Direct smothering of organisms inhabiting the stream bed;
2. Clogging of feeding apparatus in filter-feeding taxa causing stress or mortality;
3. Reducing the effectiveness of oxygen exchange organs such as gills through clogging;
4. Altering habitat, for example by filling the interstices of the substrate;

5. Bioavailability of sediment bound contaminants resulting in adverse effects;
6. Behavioural responses, such as increased invertebrate drift as an avoidance response to increased SPM levels;
7. Influencing both the decomposition and availability of detrital material, with consequent impacts on the availability of food for many macroinvertebrates;

In the present study, midge and blackworm were exposed to combination of excavated rock and reservoir sediments to assess impact pathways 1-5 as listed above.

1.4.2 Ecotoxicological assessment of excavated rock material

In the present study, the acute and chronic toxicity of contaminants (inorganics including metals) and physico-chemical stressors such as pH, EC, DO and turbidity released from excavated rock materials was assessed. A suite of standardised ecotoxicological bioassays under two different experimental set-ups were conducted with the following objectives:

1. Assess toxicity to aquatic organisms due to fine **suspended sediments** from excavated rock material interacting with the reservoir water and;
2. Assess toxicity to benthic organisms due to fine **deposited sediments** from excavated rock material interacting with the reservoir sediments.

Chronic toxicity tests have durations of weeks to months, and were used to provide an appropriate level of confidence for predicting the risks of toxicity. An exception was the chronic toxicity test with microalgae – which tested for population growth rate inhibition over three days. Acute toxicity tests (with test durations of up to two days) were also incorporated into the study to screen the water/leachate samples for toxicity prior to initiating long-term chronic toxicity tests. Toxicity tests with an aquatic microalga and a water flea, benthic midge and blackworms were selected for use in this project because they either represent sensitive species or are known to be present in the reservoirs. The test endpoints (e.g. growth rate, reproduction) measured during toxicity testing have well-established quality assurance (QA) and quality control (QC) criteria.

Excavated rock leachate testing

In the present study, the leachates from excavated rock and reservoir water with ratios of 1 to 10 were used for ecotoxicological assessment. The 1:10 mass/mass, sample to water ratio, is double the projected volume of rock spoil (5%) to be deposited in Lakes Talbingo and Tantangara. This assessment intentionally represents worse-case scenarios. The effect of various concentrations of suspended solids in the leachates was also assessed to indicate how the risk might change over time following a placement event (e.g. following settling of solids after a period of time, and filtration. Leachate toxicity tests were carried out with one microalga and three macroinvertebrates (waterfleas, midge and blackworms).

Water/leachate toxicity tests included:

- Chronic single-celled microalgal population growth rate inhibition with the freshwater temperate species *Raphidocelis subcapitata* (previously known as *Pseudokirchneriella subcapitata* and as *Selenastrum capricornutum*) over 72 h.
- Acute (48-h immobilisation) and chronic (7-d reproduction) toxicity tests with the cladoceran water flea *Ceriodaphnia dubia*.

- Acute toxicity tests with the midge *Chironomus tepperi* measuring immobilisation/survival after 48 h.
- Acute toxicity tests with the blackworm *Lumbriculus variegatus* measuring immobilisation after 48 h.

The macroinvertebrate tests were conducted using the following three scenarios to determine if any toxicity associated with excavated material was due to contaminants (such as metals/ions) and/or the presence of suspended sediments:

- Raw scenario: 24 h settled leachates were tested to determine a combination of the contaminants and turbidity impacts. This represented the 'worst case' scenarios unlikely to be encountered during placement activities;
- 12-day settled scenario: to determine impacts due to contaminants and reduced turbidity after 12-day settling of leachates; and
- Filtered scenario: leachates were filtered through 0.45 µm filter to minimise suspended sediments in the leachates and to examine toxicity associated with dissolved metals.

Excavated rock-sediment mixtures testing

Under the different benthic sediment scenarios, the substrate composition varied from predominantly excavated rock, to excavated rock mixed with sediments and also thin layers of excavated rock that may spread and deposit at locations away from the main placement area.

Sediment/excavated rock toxicity tests were carried out with two benthic species (midge and blackworms) and covered three excavated-rock and sediment mixture scenarios:

- Top scenario: thin layers of excavated rock material covering natural sediments (spreading and being deposited at locations away from the main placement area);
- Mixed scenario: excavated rock mixing with sediments to form a smaller fraction of the substrate; and
- Rock scenario: excavated rock becoming the dominant substrate in an area. This represented the 'worst case' scenarios unlikely to be encountered during placement activities.

Toxicity tests included:

- Chronic toxicity tests with the midge *C. tepperi* measuring survival and growth (length) over 7 days.
- Chronic toxicity tests with the blackworm *L. variegatus* measuring reproduction and biomass over 28 days. Endobenthic aquatic oligochaetes such as *L. variegatus* burrow in the sediment, and ingest sediment particles below the sediment surface. This ensures exposure to the test substance via all possible uptake routes (e.g. contact with and ingestion of contaminated sediment particles; via pore water; via overlying water).

Measurements of the dominant stressors (e.g. dissolved metals, pH, EC and suspended solids) in toxicity tests provided information to link the ecotoxicology effects to those stressors. In Assignment P5, the ecotoxicological assessment was based on specific scenarios testing under laboratory conditions. Following this project, modelling and refinement of the proposed

excavated rock placement methods will be undertaken to determine how likely the tested experimental scenarios will be to conditions experienced within the reservoirs.

A total of 14 excavated rock materials assessed in this project represented seven of nine geological zones that will likely be encountered during tunnel construction, each with a classification of Baseline and Enriched materials. The samples were informed from Assignments P2 (Douglas et al., 2018) and were the same as those used in Assignment P4 (Simpson et al., 2019). Douglas and co-workers used a classification based on a comparison to the Post-Archean Australian Shale, an average upper crustal composition, to assist in the selection of Baseline and Enriched Groups for each of the seven geological zones. The most common attribute of the Enriched Group being elevated S and trace element (metal and metalloids) concentrations over the Baseline Group. Further details are given in Section 2.1.

This project can be used to categorise the potential environmental risk to organisms that inhabit the waters and surface sediments of the reservoirs following addition of excavated rock material. It will contribute towards better management and mitigation strategies (e.g. excavated rock placement, containment, and remediation) to reduce environmental impacts of the placement of excavated rock material.

2 Methodology

2.1 Waters, sediments and excavated rock materials

2.1.1 Samples

The excavated rock samples used in the study were selected based on results from Assignment P2 (Douglas et al., 2018). A total of fourteen composite samples were used to represent Baseline and Enriched materials from seven geological zones (Table 1).

Table 1. Geographical units for the excavated rock materials

| Zone | Geographical Unit | Description | Abbreviation used |
|------|---|--|-------------------|
| i | Ravine Group | geology of western portion of the tunnel transect and surge shaft (13 km with (ii)) | Ravine (R) |
| ii | Byron/Boraig Group | geology of western portion of the tunnel transect and surge shaft (13 km with (i)) | Byron (B) |
| iii | Shaw Hill Gabbro | in the tunnel transect and constitutes (~1 km) | Shaw Gabbro (S) |
| iv | Gooandra Volcanics | in the tunnel transect (~5 km) | Volcanics (V) |
| v | Peppercorn/Tantaranga/Temperance Formations | in the tunnel transect (~ 9 km); based on the available information these could not be readily differentiated, but has a mostly similar geology and form a contiguous sequence along the tunnel transect so have been aggregated | Peppercorn (P) |
| vi | Kellys Plain Volcanics | in the intake area at the Tantaranga Reservoir (~2 km of the tunnel); Note that this material was only made available from late in the study | Kellys Plain (K) |
| vii | Felsic/Granite/Gneiss/Ignimbrite | compilation of granitic/extrusive equivalents present at various places along the tunnel transect | Felsic (F) |

For each of these geological units, composite material was prepared from between four and nine individual excavated rock sources, which are described more fully in the Assignment P4 report (Simpson et al., 2019 and Appendix B). The composites for each geological unit were prepared by weighing equal amounts of each individual excavated rock materials (<75 µm) available for that geological unit and homogenising them thoroughly.

The samples of reservoir waters (Table 2) and sediments (Table 3) used in the study were provided by HKA and were from locations near proposed placement areas for the excavated rock. Seven water samples were collected (~15 L each) in 20-L plastic carboys. Twelve sediment samples (~4 kg each) were collected from three sites in Tantaranga Reservoir and nine sites in Talbingo Reservoir, and transported to CSIRO in Eskys with ice and were stored at 4°C until further testing. For one sub-sample of reservoir water received at CSIRO Lucas Heights (TAL_PL1B) there appeared to have been a leak because it contained only approximately 4 L. Chemical analysis confirmed that this sample had an elevated dissolved copper concentration and hence this reservoir water sub-sample was not used in this study.

Excavated rock material for each baseline and enriched geographical unit, along with water and sediment samples received by CSIRO Adelaide, were used in the water flea, midge and blackworm toxicity tests. The microalgal toxicity tests were carried out with excavated rock material and reservoir water samples received by CSIRO Lucas Heights, and the same as those used in Assignment P4.

Table 2. Reservoir water samples used for ecotoxicological testing

| Reservoir* | CSIRO Laboratory Received | Sample I.D. | Date received | Time received |
|------------|---------------------------|----------------------------------|---------------|---------------|
| Tantangara | Lucas Heights | TAN-TN2A | 3/07/2018 | 11:30 |
| | | TAN-TN3A | 3/07/2018 | 11:00 |
| | | TAN-TN1A | 3/07/2018 | 12:05 |
| | Adelaide | TN1-B | 12/07/2018 | 14:30 |
| | | TN2-B | 12/07/2018 | 14:30 |
| | | TN3-B | 12/07/2018 | 14:30 |
| Talbingo | Lucas Heights | TAL-PL2A | 4/07/2018 | 13:50 |
| | | TAL-PL1A | 4/07/2018 | 14:00 |
| | | TAL-PL1B (leaked / contaminated) | 4/07/2018 | 14:00 |
| | | TAL-PL2B | 4/07/2018 | 13:50 |
| | Adelaide | TAL-PL1C | 12/07/2018 | 14:30 |
| | | TAL-PL2C | 12/07/2018 | 14:30 |
| | | TAL-PL1D | 12/07/2018 | 14:30 |
| | | TAL-PL2D | 12/07/2018 | 14:30 |

* Refer to Assignment P4 (Simpson et al., 2019, Appendix B) for sampling notes and locations.

Table 3. Reservoir sediment samples used for ecotoxicological testing

| Reservoir* | CSIRO Laboratory Received | Sample I.D. | Date | Time |
|------------|---------------------------|-------------|-----------|-------|
| Tantangara | Lucas Heights | TN2_P4 | 3/07/2018 | 11.15 |
| | | TN1_P4 | 3/07/2018 | 11.45 |
| | | TN3_P4 | 3/07/2018 | 10.40 |
| | Adelaide** | TN1_P5 | 7/3/2018 | 1150 |
| | | TN2_P5 | 7/3/2018 | 1120 |
| | | TN3_P5 | 7/3/2018 | 1050 |
| Talbingo | Lucas Heights | RA1_P4 | 4/07/2018 | 10.20 |
| | | RA2_P4 | 4/07/2018 | 10:45 |
| | | RA3_P4 | 4/07/2018 | 11:20 |
| | | PL1_P4 | 4/07/2018 | 14:20 |
| | | PL2_P4 | 4/07/2018 | 13:15 |
| | | PL3_P4 | 4/07/2018 | 12:35 |
| | | CA1_P4 | 5/07/2018 | 11:20 |
| | | CA2_P4 | 5/07/2018 | 10:15 |
| | | CA3_P4 | 5/07/2018 | 9:45 |
| | Adelaide** | PL1_P5 | 7/4/2018 | 1430 |
| | | PL2_P5 | 7/4/2018 | 1325 |
| | | PL3_P5 | 7/4/2018 | 1245 |
| | | CA1_P5 | 7/5/2018 | 1130 |
| | | CA2_P5 | 7/5/2018 | 1025 |
| | | CA3_P5 | 7/5/2018 | 945 |
| | | RA1_P5 | 7/4/2018 | 1020 |
| | | RA2_P5 | 7/4/2018 | 1050 |
| | | RA3_P5 | 7/4/2018 | 1130 |

* Refer to Assignment P4 (Simpson et al., 2019, Appendix B) for sampling notes and locations. **dates and time refer to the days and time the sediment samples were collected by Cardno.

2.1.2 Preparation of leachates of excavated rock

Toxicity tests with microalgae, water fleas, midges and blackworms were carried out on leachates of composite excavated rock material (milled to $<75\ \mu\text{m}$, Appendix B) with a liquid:solid ratio of 10 (L:S = 10, equivalent to 100 g/L).

For microalgal toxicity tests, 20 g of each sample of excavated rock and 200 mL of Talbingo Reservoir water were added to a 250-mL high-density polyethylene bottle. Reservoir water control treatment was prepared by combining equal volumes of three sub-samples of water from Talbingo Reservoir (TAL-PL1A, TAL-PL2A and TAL-PL2B). The bottles were capped (double bagged in zip-locked bags) and mixed end-on-end for 18 h at 32 rpm. A procedural method blank (MB) consisted of reservoir water control treatment that was prepared in parallel with the leachates (i.e. rotated for 18 h and filtered). After 18 h, leachates were collected and filtered through an acid-washed 47-mm diameter, $0.45\ \mu\text{m}$ filter (cellulose acetate membrane, Sartorius) using an acid-washed polycarbonate filter unit (Sartorius). [Filtration was required to remove the solids and microalgae present in the samples, precluding them from interfering with the subsequent measurement of the test species.] Leachates were tested within 3 h of filtration.

Leachate preparation for toxicity tests with water fleas (acute and chronic tests), midges (acute tests) and blackworms (acute tests) were prepared by adding 4 g excavated rock and 40 mL of reservoir water to a 50-mL plastic tube with a screw cap. The particular reservoir water used to prepare leachates was based on the likely placement site (Appendix B). Talbingo Reservoir water was used to prepare leachates of Ravine, Byron, Shaw Gabbro, Volcanics and Felsic excavated rock, and Tantangara Reservoir water for Peppercorn and Kellys Plain, respectively. Approximately 70 tubes were prepared for each excavated rock sample, comprising in total approximately 2.5 L of leachate for toxicity testing. The tubes were mixed overnight (18 h) using a mechanical shaker and then placed upright in a fridge ($\sim 4^{\circ}\text{C}$) for 24 h to allow some settling of suspended solids at the bottom of the tubes.

Three types of leachate: 'raw', 12-d 'settling' and 'filtered' were prepared and used in the acute toxicity test with water fleas, midges and blackworms. The supernatant (liquid fraction above the settled suspended solids) of each leachate sample was collected in glass jars. This fraction was termed the 'raw' leachate and contained a relatively large amount of suspended solids that did not settle out of solution within the 24-h settling time. Raw leachates were kept in 1 L glass jars for 12 days to allow additional settling of suspended solids prior to testing, producing 'settling' leachates. In addition, a third treatment consisted of filtering ($0.45\ \mu\text{m}$ polyvinylidene fluoride membrane) raw leachate to obtain a 'filtered' leachate sample that was devoid of the majority of the suspended solids.

2.1.3 Preparation of excavated rock-sediment mixtures for toxicity testing

The toxicity of 13 excavated rock materials (excluding Kellys Plain Baseline) was assessed using benthic organisms (midges and blackworms). Similar to the reservoir water analyses, three scenarios were prepared and tested, each using excavated rock material sieved to $425\ \mu\text{m}$ and reservoir sediments. Reservoir sediments with no excavated rock material were used as controls and tested concurrently with every geological zone testing and reservoir water was used as overlying water for each testing regime.

Scenarios for blackworm toxicity tests included:

1. Excavated rock becoming the dominant substrate in an area. This was prepared by adding 75 g of neat excavated rock material to each test vial.
2. Excavated rock mixed with sediments to form a smaller fraction of the substrate. This was prepared by adding 75 g reservoir sediment to 20 g excavated rock material to each vial and mixing thoroughly prior to testing.
3. Thin layers of excavated rock material covering natural sediments. This scenario represents the spreading and deposition of excavated rock at locations away from the main placement area. This was prepared by adding 75 g reservoir sediment to each test vial followed by 20 g of excavated rock material on to the surface of the reservoir sediment.

Scenarios for midge toxicity tests included:

1. Excavated rock becoming the dominant substrate in an area. This was prepared by adding 140 g of neat excavated rock material to each test chamber.
2. Excavated rock mixed with sediments to form a smaller fraction of the substrate. This was prepared by adding 140 g reservoir sediment to 20 g excavated rock material to each test chamber and mixing thoroughly prior to testing.
3. Thin layers of excavated rock material covering natural sediments. This scenario represents the spreading and deposition of excavated rock at locations away from the main placement area. This was prepared by adding 140 g reservoir sediment to each test chamber followed by 20 g of excavated rock material on to the surface of the reservoir sediment.

2.1.4 Physico-chemical and chemical analysis

Water pH, EC, dissolved oxygen (DO) and temperature measurements were made using either Thermo Orion (VersaStar Pro-series) or Hanna (HI9819X-series) meters and probes that were calibrated as per the manufacturer's instructions. Turbidity was measured using a TN-100 Turbidimeter (Eutech Instruments).

Excavated rock, leachates, reservoir waters and sediments were measured for total and/or dissolved (0.45 µm filtered) metals. If not already filtered to 0.45 µm during sample preparation (section 2.2.1), samples for dissolved metals analysis were filtered through acid-washed 0.45-µm syringe filters (Sartorius, Australia) with the first ~3 mL of sample pre-conditioning the filter and discarded to waste, before collecting the filtrate in an acid-washed polycarbonate vial. All samples were acidified with concentrated nitric acid (Tracepur, Merck) to 0.2 % (v/v) prior to analysis.

Concentrations of metals and major ions were determined by inductively coupled plasma atomic emission spectrometry (ICP-AES) (CSIRO Method C-229), inductively coupled plasma mass spectrometry (ICP-MS) (CSIRO Method C-209) or aqua regia digestion for total recoverable metals (TRM, CSIRO Method C-223) and dilute-acid extractable metal (AEM, CSIRO Method C-241).

Analysis of samples from the microalgal toxicity tests were carried out at CSIRO Lucas Heights. Analysis of samples from the water flea, midge and blackworm toxicity tests were carried out at CSIRO Adelaide. Metal and metalloids analysed included: aluminium (Al), arsenic (As), boron (B), barium (Ba), calcium (Ca), cadmium (Cd), cobalt (Co), chromium (Cr), copper (Cu), iron (Fe), potassium (K), magnesium (Mg), manganese (Mn), molybdenum (Mo), sodium (Na), nickel (Ni), lead (Pb), antimony (Sb), selenium (Se), silicon (Si), tin (Sn), strontium (Sr), thorium (Th), uranium (U), vanadium (V), zinc (Zn), mercury (Hg), sulphur (S) and phosphorus (P).

The composition of the 'raw' leachate samples were also analysed by scanning electron microscopy (SEM) (for imagery and to provide energy dispersive X-ray) and X-ray power diffraction (XRD) spectrometry (carried out at CSIRO Adelaide; refer to Appendix I and J, respectively, for methods).

The total recoverable metals (and other elements) in the sediments and rock samples (<75 µm) were extracted based on the methods validated and described in Assignment P4 (Simpson et al., 2019). Sediments and excavated rock samples were extracted within pre-cleaned Teflon digestion vessels using aqua regia digestions in a microwave-assisted reaction system (MARS). The Teflon vessels were extensively cleaned as per CSIRO Method C-223. The sediments were freeze-dried (Christ Alpha 1-2 LDplus) and ground to a powder using a mortar and pestle before digestion.

The sediments and rock samples were weighed into the pre-cleaned MARS Teflon vessels to which 9 mL of concentrated nitric acid (Merck Tracepur) and 3 mL of concentrated hydrochloric acid (Merck Tracepur) were added. The digestion vessels were heated at high pressure in a MARS digestion system for 90 minutes (CSIRO Method C-223). Once cool, digests were diluted to a final volume of 40 mL with deionised water. The digest solutions were subsequently diluted 10-fold using deionised water and analysed using a combination of ICPAES (Varian730 ES) and ICPMS (Agilent 8800 CE) with matrix-matched calibration standards.

Dilute-acid-extractable metals (AEM) were determined for each solid using an extraction in 1 M HCl (84 mL of 36% HCl/L) for 60 min, followed by filtration (<0.45 µm). The extraction treatments were shaken each 20 min over the 60 min extraction duration. The 1 M HCl sample extracts were subsequently diluted 10-fold using deionised water and analysed using a combination of ICPAES (Varian730 ES) and ICPMS (Agilent 8800 CE), with matrix-matched calibration standards.

2.2 Ecotoxicity testing - overview

Toxicity tests (chronic and acute) with microalgae, water fleas, midges and blackworms were carried out on leachates of excavated rock material prepared with water from Talbingo or Tantangara Reservoirs. Toxicity tests (chronic) with midges and blackworms were carried out on excavated rock material under varying scenarios of mixing and layering (Table 4).

Leachates of excavated rock had high levels of suspended solids (turbidity), which had not completely settled out of solution after 24 h. Therefore, the toxicity of leachates was assessed with water fleas, midge and blackworms on raw and/or after settling (12 d) and/or 0.45 µm filtered leachates based on the decision tree in Figure 1.

Table 4. Summary of toxicity tests and material tested

| Species | Endpoint (acute or chronic) | Exposure (d) | Material tested |
|---|--|--------------|--|
| Water (leachate) tests | | | |
| Microalga, <i>Raphidocelis subcapitata</i> | Population growth rate inhibition (chronic) | 3 | (i) Reservoir water (0.45 µm filtered) (ii) Leachates of excavated rock representing 7 geological units (each with a Baseline and Enriched composite) prepared with reservoir water (and filtered to 0.45 µm prior to toxicity testing) |
| Water flea (cladoceran), <i>Ceriodaphnia dubia</i> | (i) Survival (acute) | 2 | (i) Reservoir water (ii) Leachates of excavated rock representing 7 geological units (each with a Baseline and Enriched composite) prepared with reservoir water representing three treatments a) Raw leachate as a worst-case scenario a) 12-day settled leachate b) Filtered leachate |
| Water flea (cladoceran), <i>Ceriodaphnia dubia</i> | Reproduction (chronic) | 8 | (i) Reservoir water (ii) Leachates of excavated rock representing 6 geological units (each with a 0.45 µm filtered Enriched composite) prepared with reservoir water |
| Midge <i>Chironomus tepperi</i> | Immobilisation (acute) | 2 | (i) Reservoir water (ii) Leachates of excavated rock representing 7 geological units (each with a Baseline and Enriched composite) prepared with reservoir water representing three treatments based on decision tree given in Figure 1 |
| Blackworm, <i>Lumbriculus variegatus</i> | Immobilisation (acute) | 2 | As above |
| Sediment (excavated rock) tests | | | |
| Midge larvae, <i>Chironomus tepperi</i> | (i) Survival (chronic) (ii) Growth (length) (chronic) | 7 | (i) Reservoir sediment (ii) Reservoir water as overlying water (ii) Excavated rock representing 7 geological units (each with a Baseline and Enriched composite) b) mixed with reservoir sediment c) as a surface layer on top of reservoir sediment d) 100% Enriched excavated rock as a worst-case scenario |
| Blackworm, <i>Lumbriculus variegatus</i> | (i) Reproduction (chronic) (ii) Biomass (chronic) | 28 | As above |

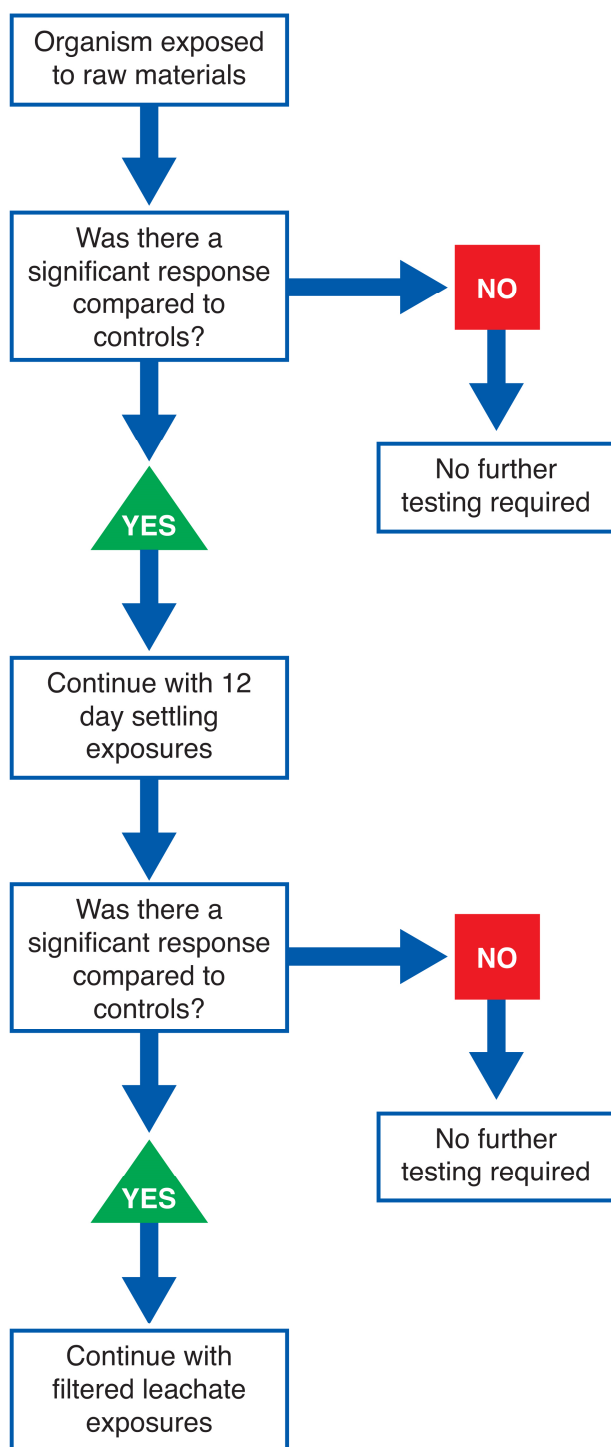


Figure 1. Decision tree for toxicity testing of raw, settling and filtered (0.45 µm) leachates with water fleas, midges and blackworms.

2.3 Toxicity testing of leachates of excavated rock material

2.3.1 Microalgal toxicity testing

Chronic toxicity to the temperate freshwater microalga *Raphidocelis subcapitata* (strain CS-327 CSIRO National Algal Culture Collection) was tested in this project, based on Test Guideline 201 (2002), Organisation for Economic Co-operation and Development (OECD). Toxicity was measured as an inhibition in population growth rate over 72 h. Toxicity tests with *R. subcapitata* are summarised in Table 5 and described in Stauber et al. (2005).

Toxicity tests were carried out on filtered (0.45 µm) reservoir waters to remove the natural phytoplankton present in the samples, as it interferes with the measurement of microalgal cell densities (and hence microalgal growth rates) of the inoculated test species (refer to Appendix C, Test report 1). Leachate water was also tested after filtration (0.45 µm) to remove particulates from the leachate that can potentially interfere with the determination of algal cell densities. Reservoir waters and leachates (14 samples) were screened for toxicity by testing undiluted water (100%). Leachates of Gooandra Baseline and Gooandra Enriched were tested further by diluting each leachate with filtered reservoir water (1 in 2) to achieve six leachate concentrations of 6.3%, 13%, 25%, 50%, 75% and 100%.

Cultured algal cells in their exponential growth phase (5-6 d) were washed by centrifugation to remove culture media and cell exudates (potential sources of metal ligands) before being added to each minivial glass test vessel ($1-2 \times 10^3$ cells/mL) along with essential nutrients (USEPA nutrients, without EDTA, Stauber et al., 2005). Control treatments consisting of reservoir water, leachate MB and USEPA media were also prepared. All treatments were prepared at least in triplicate as a minimum. All treatments were incubated at 24°C under a 24-h light cycle. Cell densities in each vial were then determined daily for three days using a FACSCalibur flow cytometer (BD Bioscience) and the microalgal cell division rates were calculated (Stauber et al., 2005). For quality control purposes, a reference toxicant (copper) was also tested to ensure that the microalgae were responding to a known toxicant in a reproducible way. Additional toxicity test conditions are summarised in Table 5.

The pH and EC of each treatment was measured at the beginning of the test and pH was measured at the end of the test. Temperature was monitored throughout the test. Selected chemical analyses included dissolved metals at the beginning of the test (Section 2.3.3).

Significant differences ($p \leq 0.05$) in the microalgal growth rates measured between different treatments were tested using the Homoscedastic t-test following tests for normality (Shapiro-Wilk's test) and variance (F-test). Where a concentration-response relationship was observed (e.g. for the reference toxicant), the toxicity was expressed as the concentration of sample that causes a 10% or 50% inhibition in algal growth rate relative to the control (IC₁₀ and IC₅₀ values, respectively) derived through linear interpolation. The lower the IC₁₀ or IC₅₀, the more toxic the sample. The lowest observable effect (LOEC) and no observable effect (NOEC) concentrations were calculated using the Dunnett's Test. All statistical tests were carried out using ToxCalc Version 5.0.23 (Tidepool Software).

Table 5. Summary of the test protocol for growth inhibition tests with the temperate microalga *Raphidocelis subcapitata*

| Parameter | Test condition |
|---|--|
| Test type | Static, non-renewal |
| Temperature | 24 ± 2°C |
| Light quality | Cool white fluorescent daylight lighting |
| Light intensity | 65 µmol photons/m ² /s |
| Photoperiod | 24 h light |
| Test chamber size | 20 mL |
| Test solution volume | 6 mL |
| Renewal of test solutions | None |
| Age of test organisms | 5-6 days |
| Initial cell density in test chambers | 1-2 x 10 ³ cells/mL |
| No. of replicate chambers/concentration | 3 (minimum) |
| Shaking rate | Twice daily by hand |
| Dilution water | USEPA media |
| Sample (leachate) concentrations | Screening tests: 1 (undiluted, 100%) Concentration-response curve: 6 (minimum) |
| Dilution factor | Screening tests: not applicable Concentration-response curve: 1 in 2 (minimum) |
| Test duration | 72 h |
| Endpoint | Cell division rate (growth rate) |
| Test acceptability | <ul style="list-style-type: none"> • Cell division rate in control within Cusum chart limits (2.2–2.6 doublings per day) • Variability in the controls <20% • Reference toxicant, copper, IC50 within Cusum chart limits (9–21 µg/L) |

2.3.2 Cladoceran immobilisation (acute) and reproduction (chronic) tests

Toxicity tests with *Ceriodaphnia dubia* employed the endpoints of immobilisation and reproduction for the acute and chronic tests, respectively. Cultures of *C. dubia* were sourced from CSIRO Lucas Heights and maintained at CSIRO Adelaide throughout the project.

Cladoceran 48-h acute immobilisation test

The acute toxicity test measures immobilisation of *C. dubia* over 48 h and follows the OECD guideline 202 (OECD, 2004) with minor modifications (Table 6). For each leachate sample, 25 mL was dispensed into 50 mL beakers, with control treatments of 25 mL moderately hard water (MHW; US EPA, 2002) and reservoir water. All treatments were prepared with four replicates. Five *C. dubia* neonates (aged <24 h) were added to each test vessel and the vessels incubated at 25 ± 1°C under a 16:8 h light: dark cycle. After 48 h, the number of surviving (mobile) and non-surviving (immobile) neonates were observed and counted under a stereomicroscope. Surviving cladocerans were identified by signs of movement. Test solutions were not renewed during the 48 h exposure. A control consisting of MHW containing a reference toxicant of copper, was tested for quality assurance purposes.

Table 6. Summary of the cladoceran acute (48-h immobilisation) and chronic (8-d reproduction) test

| Parameter | Acute test condition | Chronic test condition |
|-----------------------------------|---|--|
| Test type | Static, non-renewal | Semi-static |
| Test duration | 48 h | 8 d |
| Temperature | 25 ± 1°C | 25 ± 1°C |
| Light quality | Cool white fluorescent tube lighting | Cool white fluorescent tube lighting |
| Light intensity | 800 ± 160 Lux | 800 ± 160 Lux |
| Photoperiod | 16 h light : 8 h dark | 16 h light : 8 h dark |
| Test chamber size | 50 mL vial | 50 mL |
| Test solution volume | 25 mL | 25 mL |
| Renewal of test solution | None | 48 h |
| Age of test organisms | ≤24 h (neonate) | ≤24 h (neonate) |
| No. of organisms per replicate | 5 | 1 |
| No. of replicates per treatment | 4 | 10 |
| No. of organisms per treatment | 20 | 10 |
| Feeding regime | None | <i>R. subcapitata</i> and <i>Dunaliella salina</i> daily |
| Dilution water/control treatments | reservoir water | Moderately hard water (MHW) and reservoir water |
| Sample (leachate) concentrations | Screening tests: 1 (undiluted, 100%) | 1 (undiluted, 100%) |
| Dilution factor | Screening tests: not applicable Concentration-response curve: 1 in 2 (minimum) | Not applicable |
| Endpoint | Immobilisation | Total number of neonates (over three broods for the control treatment) |
| Test acceptability criteria | ≥90% survival in controls Reference toxicant, copper, EC50 within Cusum chart control limits | ≥80% survival in controls Reference toxicant, copper, 48-h acute EC50 within Cusum chart control limits |

Cladoceran 8-d chronic reproduction test

Reproduction of *C. dubia* was assessed over 8 days with a method based on the OECD Test Guideline 211 (1984 and 2012) for *Daphnia magna* (Table 6). Tests were carried out in 50 mL beakers each containing 25 mL of test solution. Control treatments were also prepared with MHW and reservoir water, with each treatment consisting of ten replicates. One neonate (<24-h old) was added to each beaker and incubated at 25 ± 1°C with a photoperiod of 16:8 h light: dark cycle. *C. dubia* were fed a microalgal mixture of *R. subcapitata* and *Dunaliella salina* on a daily basis. During the 8-d toxicity test, test solutions were renewed every 48 h using the originally prepared leachate. After 8 days, the number of surviving *C. dubia* and the total number of young generated over three broods were counted. The pH, DO, EC and temperature were measured at the beginning and end of the bioassay and when test solutions were renewed.

2.3.3 Midge survival (acute) tests

The acute toxicity test measures immobilisation of *C. tepperi* over 48 h. For each leachate, 25 mL was dispensed into 50 mL beakers, with control treatments of 25 mL MHW (US EPA, 2002) and reservoir water. All treatments were prepared with four replicates. Five 2nd instar larvae were added to each test vessel and the vessels incubated at 25 ± 1°C under a 16:8 h light: dark cycle.

After 48 h, the number of surviving (mobile based on gentle prodding) and non-surviving (immobile) larvae were counted under a stereo microscope. Test solutions were not renewed during the 48 h exposure (Table 7). A control consisting of MHW containing a reference toxicant of copper, was tested for quality assurance purposes.

Table 7. Summary of the acute (48-h survival) midge test

| Parameter | Acute test condition (waters) |
|---------------------------------|---|
| Test type | Static, non-renewal |
| Test duration | 48 h |
| Temperature | 21 ± 1°C |
| Light quality | Cool-white fluorescent tube lighting |
| Light intensity | 800 ± 160 Lux |
| Photoperiod | 16 h light : 8 h dark |
| Test chamber size | 50 mL vial |
| Test solution volume | 25 mL |
| Age of test organisms | Similar sizes |
| No. of organisms per replicate | 5 |
| No. of replicates per treatment | 4 |
| No. of organisms per treatment | 20 |
| Feeding regime | None |
| Dilution water | Reservoir water |
| Test concentrations | 4 + 1 Control (if 100% sample shows toxicity) |
| Control treatments | Moderately hard water (MHW) and Reservoir water |
| Endpoint | Survival (Immobilisation) |
| Test acceptability criterion | ≥90% survival in the controls Reference toxicant, copper, EC50 within Cusum chart limits |

2.3.4 Blackworm survival (acute) tests

The acute toxicity test measures immobilisation of *L. variegatus* over 48 adult blackworms of similar physiological development (synchronised) were exposed to leachates of excavated rock material prepared in reservoir water. Test vessels with reservoir water were used as the control treatments. For each leachate, 25 mL was dispensed into 50 mL beakers, with control treatments of 25 mL MHW (US EPA, 2002) and reservoir water. All treatments were prepared with four replicates. After 48 h, the number of surviving (mobile based on gentle prodding) and non-surviving (immobile) adult blackworms were counted under a stereomicroscope. Test solutions were not renewed during the 48 h exposure (Table 8). A control consisting of MHW containing a reference toxicant of copper, was tested for quality assurance purposes.

Table 8. Summary of the acute (48-h survival) blackworm test

| Parameter | Acute test condition (waters) |
|---------------------------------|---|
| Test type | Static, non-renewal |
| Test duration | 48 h |
| Temperature | 21 ± 1°C |
| Light quality | Cool white fluorescent tube lighting |
| Light intensity | 800 ± 160 Lux |
| Photoperiod | 16 h light : 8 h dark |
| Test chamber size | 50 mL vial |
| Test solution volume | 25 mL |
| Age of test organisms | Similar sizes (physiological synchronised) |
| No. of organisms per replicate | 5 |
| No. of replicates per treatment | 4 |
| No. of organisms per treatment | 20 |
| Feeding regime | None |
| Dilution water | Reservoir water |
| Test concentrations | 4 + 1 Control (if 100% sample shows toxicity) |
| Control treatments | Moderately hard water (MHW) and Reservoir water |
| Endpoint | Survival (immobilisation) |
| Test acceptability criterion | ≥90% survival in controls Reference toxicant, copper, EC50 within Cusum chart control limits |

2.4 Toxicity testing of excavated rock-sediment mixtures

2.4.1 Midge survival and growth (chronic) tests

The chronic toxicity of excavated rock mixtures with sediment were assessed using *C. tepperi* larvae. The survival and growth of midge larvae was measured after 7 days based on methods described by Simpson and Kumar (2016) and summarised in Table 9.

For the sediment and excavated rock midge bioassay, ten 5-day old midge larvae were added to beakers containing 140 g (wet weight) of 425 µm sieved sediment and 250 mL of reservoir water (4 replicates per site, Figure 2). The beakers were incubated for 7 days at 21 ± 1°C (16:8 h light: dark). After 7 days, and prior to pupation, larvae from each replicate were removed, pooled and their wet weights recorded. Individual midge larvae lengths were measured using image analysing software. Survival of the midge larvae was also determined.

The pH, EC, DO and temperature of the overlying water was measured at the beginning and end of the test, and on Day 3 and 5 when overlying water of the test chambers were renewed.

Table 9. Summary of the chronic (7-d survival and growth) midge test

| Parameter | Chronic test condition (sediments) |
|--|--|
| Test type | Semi-static with aeration |
| Test duration | 7 d |
| Temperature | 21 ± 1°C |
| Light quality | Cool-white fluorescent tube lighting |
| Light intensity | 800 ± 160 Lux |
| Photoperiod | 16 h light : 8 h dark |
| Test chamber size | 400 mL beaker |
| Test solution volume (overlying water) | 250 mL |
| Sediment and excavated rock | Three treatments (1) 140 g (wet weight) of 425 µm sieved sediment and 20 g excavated rock material on top of sediments (2) 140 g (wet weight) of 425 µm sieved sediment and 20 g excavated rock material mixed with sediments (3) 160 g (wet weight) of 425 µm excavated rock material |
| Age of test organisms | 2 nd instar larvae (5 day old larvae after collecting egg sacs) |
| No. of organisms per replicate | 10 |
| No. of replicates per treatment | 4 |
| No. of organisms per treatment | 40 |
| Feeding regime | 1.5 mL food added on alternate days (3 times during the test) |
| Dilution water | Reservoir water |
| Control treatments | Reservoir sediment |
| Endpoint | Survival and growth |
| Test acceptability criterion | ≥80% survival in controls. The oxygen concentration in the overlying water should not be <80% of air saturation value at test temperature at the end of the test. Copper reference test for 48 hours –water only exposures |

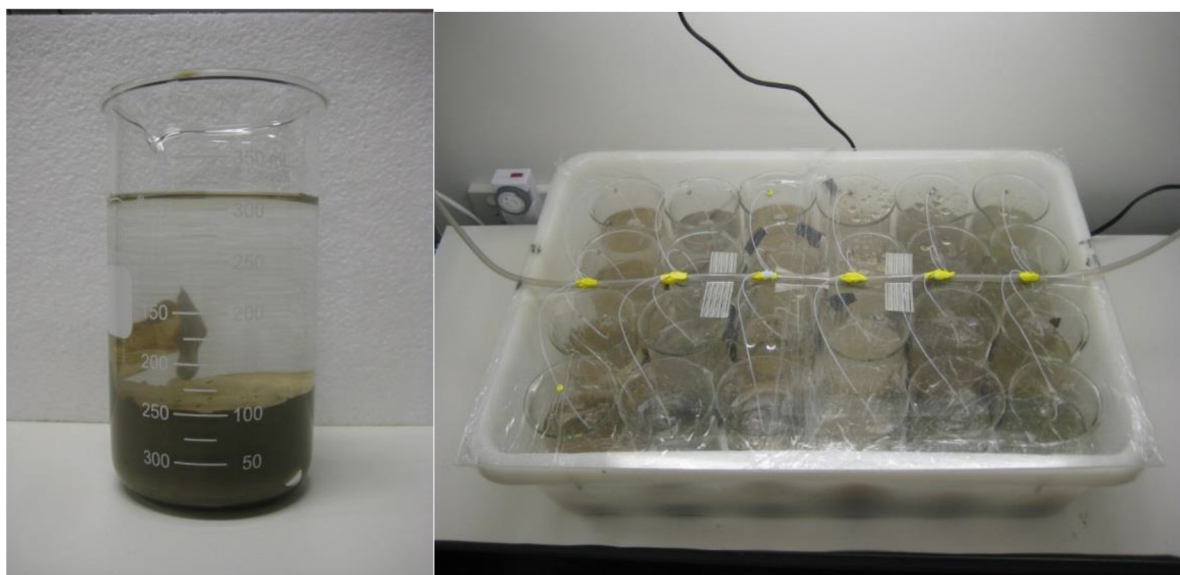


Figure 2. Midge whole sediment toxicity test set up

2.4.2 Blackworm reproduction and biomass (chronic) tests

This test determines effects on the reproduction and the biomass of the blackworm *L. variegatus* and follows the OECD guideline 225 (OECD, 2007). The chronic measured biological parameters are the total number of surviving worms and the biomass (dry weight) at the end of the exposure. Acute toxicity of leachates of excavated rock material was also assessed as a screening tool prior to initiating long-term chronic toxicity tests by measuring survival of *L. variegatus* over 48 h (Section 2.3.4). A summary of the chronic toxicity tests is described in Table 10.

Blackworms were exposed to the reservoir sediment- excavated material for 28 days.

Table 10. Summary of the chronic (28-d survival and growth) blackworm test

| Parameter | Chronic test condition (sediments) |
|---------------------------------|--|
| Test type | Static with aeration (overlying water topped up on Day 14 of test) |
| Test duration | 28 d |
| Temperature | 20 ± 2°C |
| Light quality | Cool white fluorescent tube lighting |
| Light intensity | 800 ± 160 Lux |
| Photoperiod | 16 h light : 8 h dark |
| Test chamber size | 400 mL beaker |
| Test solution volume | 250 mL (overlying water to be topped-up on Day 14) |
| Sediment and excavated rock | Three treatments (1) 75 g (wet weight) of 425µm sieved sediment and 20 g excavated rock on top of sediments and (2) 75 g sediments and 20 g excavated rock mixed well and (3) last treatment of neat excavated rock material of 75 grams. |
| Age of test organisms | Smallest BW used in the test should not be less than half the size of the largest BW used in the test. |
| No. of organisms per replicate | 10 |
| No. of replicates per treatment | 4 |
| No. of organisms per treatment | 40 |
| Feeding regime | Food added to the sediment prior to testing. Add 100 mg spirulina crushed tablet and 100 mg sera-micron powder to sediment or excavated rock materials. No additional feeding required during 28 days test. |
| Dilution water | Reservoir water |
| Control treatments | Reservoir sediment |
| Endpoint | Survival and growth |
| Test acceptability criterion | The average number of living worms per replicate in the controls should have increased by a factor of at least 1.8 at the end of exposure compared to the number of worms per replicate at the start of exposure. The oxygen concentration in the overlying water should not be <30% of air saturation Value at test temperature at the end of the test. |

Adult worms of similar physiological development (synchronised) were exposed to a combination of treatments of excavated-rock mixtures with sediment collected from the proposed placement sites. Talbingo Reservoir water was used as overlying water for Ravine, Byron, Shaw Gabbro, Volcanics and Felsic excavated rock-sediment testing scenarios. And Tantangara Reservoir water was used as overlying water for Peppercorn and Kellys Plain excavated rock-sediment testing scenarios. Test vessels with reservoir water and sediment, without the addition of the excavated rock material were used as the control treatments. Blackworms were exposed to the sediment-water treatments for 28 days. To ensure that there was sufficient organic matter to allow the worms to grow over 28 days, the organic content of the control sediment was supplemented by mixing in 0.75 g of flaked tropical fish food.

The pH, EC, DO and temperature of the surface waters were measured at the beginning and end of the test, and every day in which surface waters were renewed.

3 Results

3.1 Introduction

Each of the acute and chronic toxicity tests with waters/leachates and excavated-rock sediment mixtures met their respective QA/QC criteria (refer to Appendices C–H).

Detailed toxicity test results for chronic microalgal tests, acute and chronic cladoceran tests, acute midge tests and acute blackworm tests with excavated rock leachates are presented in Appendices C, D, E and F respectively. Detailed test reports for chronic midge tests and chronic blackworm tests are detailed in Appendices G and H respectively.

3.2 Toxicity of leachates of excavated rock to microalgae

3.2.1 Reservoir water (baseline, pre-placement)

The conductivities of waters from Tantangara Reservoir and Talbingo Reservoir were low (26.0–26.3 and 24.3–24.9 $\mu\text{S}/\text{cm}$ respectively) and the pH was near neutral (7.21–7.25 and 7.18–7.29 respectively) (Appendix C, Test Report 3). For Tantangara, concentrations of dissolved aluminium exceeded the GV for 99% species protection (Simpson et al., 2019).

Toxicity tests with microalgae are generally carried out in waters with higher EC and the low EC of the reservoir water may have affected the growth rate of microalgae. Initial toxicity testing with *C. vulgaris* indicated that while this microalgae achieved good growth rates at low conductivities (16 $\mu\text{S}/\text{cm}$) in synthetic soft water, microalgal growth was lower in Tantangara Reservoir (59–69% inhibition) than in Talbingo Reservoir (15–24% inhibition) waters suggesting that some other unknown characteristic(s) of the reservoir water suppressed *C. vulgaris* growth rates (refer to Appendix C, Test Report 2). Therefore, without further investigation, *C. vulgaris* was considered an unsuitable test species for this project and an alternative temperate freshwater species was selected: *R. subcapitata*. The toxicity test with *R. subcapitata* is an internationally standardised toxicity test protocol and has been used worldwide for the assessment of chemicals and waters for more than 30 years.

Toxicity test protocols for *R. subcapitata* require the addition of a range of nutrients (USEPA nutrients, Stauber et al., 2005) to each test solution. While this ensures an acceptable microalgal growth rate is achieved, it also alters the water quality parameters of the solutions being tested. For example, following additional of USEPA nutrients, the Tantangara Reservoir and Talbingo Reservoir waters increased in EC to 117–119 and 113–118 $\mu\text{S}/\text{cm}$ respectively and pH of 7.53–7.61 and 7.50–7.59 respectively (similar to the EC and pH of the standard control treatment (USEPA media, 93 $\mu\text{S}/\text{cm}$ and pH of 7.37, Appendix C, Test Report 3).

Where water characteristics have altered, care should be taken when interpreting the toxicity data. Overall, following addition of the USEPA nutrients to lake waters the pH increased by 0.3 units, conductivity increased by 93 $\mu\text{S}/\text{cm}$ and the hardness increased by a factor of 2 (from 11 to 22 mg CaCO_3/L , calculated from Mg and Ca concentrations) and still considered soft water (<30

mg CaCO₃/L (ANZG, 2019). Interpretation of these results with supporting information (chemical measurements and toxicity to other species) strengthens the overall toxicity assessment of lake water and leachates of excavated rock.

Water from Tantangara Reservoir (three locations) and Talbingo Reservoir (three locations) did not inhibit microalga *R. subcapitata* population growth rate (i.e. they were not toxic) with growth rates of 2.24–2.32 and 2.29–2.38 doublings/day, respectively, and similar to the standard control treatment (USEPA media, 2.28 doublings/day). This may be an artefact of the addition of USEPA nutrients to each test solution which resulted in the EC and pH of the reservoir waters to be similar to the standard control treatment (additional details are provided in Appendix C, Test Report 3).

3.2.2 Leachates of excavated rock

The effect of suspended solids on microalgal growth is difficult to assess because they interfere with microalgal cell density measurements (and hence microalgal growth rate), and the solids can shade microalgae from light that is essential for photosynthesis and cell division. Hence, leachates tested in this study were filtered to 0.45 µm prior to testing, but some leachate samples were visibly cloudy indicating that suspended solids/colloids (<0.45 µm) were also likely to be present in the leachate samples that were tested. Reduction in microalgal growth rates due to a potential of blocking of light in the toxicity tests on the elutriates in this study was not expected. For example, Volcanics Enriched sample was the cloudiest, but was not the most toxic elutriate to the microalgae.

Concentrations of dissolved metals and major ions in leachates used in the microalgal toxicity tests were measured before and after the addition of microalgal nutrients (+ N, i.e. the leachate sample tested for toxicity) (Table 11 and Table 12). The most toxic leachate (Gooandra Enriched, 47% inhibition in algal growth rate) did not have the highest concentrations of dissolved metals (aluminium, arsenic, zinc) but it did have the highest concentration of copper (7 µg/L; Table 11 and Table 12). The dissolved aluminium concentrations exceeded the 95% GV for all leachates tested (88 to >2000 µg/L) and highest concentrations were observed for Felsic Enriched (1847 and >2000 µg/L). Felsic Enriched also had the highest concentrations of dissolved arsenic and zinc, exceeding the respective 95% GVs. Other notable 95% GV exceedances include arsenic for Ravine Enriched and Kellys Plain Enriched samples.

The addition of USEPA nutrients to the leachates (immediately prior to toxicity testing) did not alter (in general) the concentration of dissolved aluminium (86 to 109% of the original leachate); the exception was for Kellys Plain Enriched, whose dissolved aluminium concentrations decreased by 55% after addition of the microalgal nutrients (590 to 265 µg/L) and Felsic Enriched (>2000 to 1847 µg/L). For Felsic Enriched, zinc, copper and iron concentrations also decreased by 47%, 62% and 60% respectively. For Kellys Plain Enriched, arsenic and iron concentrations also decreased (by 59% and 66% respectively).

The addition of the microalgal nutrients to the leachates can increase concentrations of dissolved metals and major ions (e.g. iron, manganese, sodium, calcium and magnesium) or, decrease concentrations of dissolved metals by complexation (potentially making them less bioavailable). Microalgal test solutions with simpler nutrient addition (e.g. nitrate and phosphate only) is likely

to minimise these changes to the original composition and speciation of the leachates being tested.

Leachates of excavated rock material prepared with Tantangara Reservoir water (S/L ratio of 10, 18 h mixing, 0.45 µm filtration) did not inhibit *R. subcapitata* growth rate (that is, they were not toxic) for Baseline samples of Ravine, Byron, Gooandra, Kellys Plain and Felsic, and Enriched samples of Kellys Plain (Figure 3). However, Baseline samples of Shaw Gabbro and Peppercorn, and Enriched samples of Ravine, Byron, Shaw Gabbro, Peppercorn and Felsic significantly inhibited microalgal growth by $\geq 18\%$. The Enriched Gooandra sample inhibited microalgal growth to the greatest extent (47% inhibition, compared to the control).

Serial dilution of Gooandra Baseline and Enriched samples (the latter being the most toxic leachate sample) indicated that a dilution of 1 in 2 (i.e. 50% leachate) was sufficient to remove the toxicity of the leachate to *R. subcapitata* (Figure 4).

There were no clear trends between the dissolved metal concentrations in the leachates and the toxicity observed. The leachate with the highest concentrations of metals (Al, As and Zn), Felsic Enriched, was the third most toxic leachate sample (total of 14 leachates) and of similar toxicity to other leachates.

Table 11. Concentrations of dissolved (0.45 µm) major ions, pH and EC in leachates of excavated rock material (18 h mixing)*

| Sample Name | pH | EC (µS/cm) | Ca | K | Mg | Na | | | | |
|----------------------------------|------|------------|------|-------|------|------|------|--------|------|-------|
| Ravine, Baseline | 9.27 | 133 | 4800 | 19000 | 2100 | 7100 | | | | |
| Ravine, Baseline + N | | | | | 8.94 | 216 | 6100 | 19000 | 5100 | 18000 |
| Ravine, Enriched | | | | | 9.16 | 139 | 5400 | 19000 | 2300 | 7100 |
| Ravine, Enriched + N | | | | | 8.81 | 222 | 6600 | 19000 | 5200 | 18000 |
| Byron, Baseline | | | | | 8.74 | 132 | 6300 | 11000 | 5900 | 4800 |
| Byron, Baseline + N | | | | | 8.45 | 219 | 7500 | 12000 | 8800 | 16000 |
| Byron, Enriched | | | | | 9.07 | 146 | 6100 | 25000 | 1400 | 4400 |
| Byron, Enriched + N | | | | | 8.72 | 232 | 7200 | 26000 | 4200 | 16000 |
| Shaw Gabbro, Baseline | | | | | 9.31 | 109 | 4800 | 9800 | 1700 | 8600 |
| Shaw Gabbro, Baseline + N | | | | | 8.95 | 197 | 6100 | 10000 | 4600 | 21000 |
| Shaw Gabbro, Enriched | | | | | 9.39 | 107 | 4600 | 7900 | 2300 | 8700 |
| Shaw Gabbro, Enriched + N | | | | | 8.99 | 188 | 5800 | 8300 | 5300 | 20000 |
| Volcanics, Baseline | | | | | 8.87 | 93 | 5500 | 10000 | 860 | 6000 |
| Volcanics, Baseline + N | | | | | 8.76 | 180 | 7300 | 12000 | 4100 | 19000 |
| Volcanics, Enriched | | | | | 8.98 | 115 | 6500 | 14000 | 1300 | 6300 |
| Volcanics, Enriched + N | | | | | 8.83 | 203 | 8100 | 15000 | 4400 | 18000 |
| Peppercorn, Baseline | | | | | 9.38 | 118 | 4700 | 14000 | 1400 | 8600 |
| Peppercorn, Baseline + N | | | | | 8.96 | 202 | 6000 | 15000 | 4300 | 20000 |
| Peppercorn, Enriched | | | | | 9.16 | 125 | 7200 | 10000 | 1700 | 8800 |
| Peppercorn, Enriched + N | | | | | 8.71 | 208 | 8300 | 10000 | 4600 | 20000 |
| Kellys Plain, Baseline | | | | | 8.41 | 114 | 3000 | 11000 | 2300 | 6500 |
| Kellys Plain, Baseline + N | | | | | 8.46 | 199 | 4100 | 11000 | 4900 | 16000 |
| | | | | | | | 1900 | >25,00 | | |
| Kellys Plain, Enriched | | | | | 8.43 | 179 | 0 | 0 | 4500 | 8100 |
| | | | | | | | 1100 | | | |
| Kellys Plain, Enriched + N | | | | | 8.48 | 263 | 0 | 16000 | 4900 | 14000 |
| Felsic, Baseline | | | | | 9.40 | 125 | 4300 | 18000 | 680 | 8700 |
| Felsic, Baseline + N | | | | | 8.98 | 209 | 5400 | 19000 | 3500 | 21000 |
| | | | | | | | | >25,00 | | |
| Felsic, Enriched | | | | | 7.99 | 181 | 6500 | 0 | 3000 | 6500 |
| | | | | | | | | >25,00 | | |
| Felsic, Enriched + N | | | | | 8.06 | 262 | 6400 | 0 | 5000 | 18000 |
| Volcanics, Baseline 6% + N | | | | | 7.84 | 118 | 3300 | 1500 | 3700 | 12000 |
| Volcanics, Baseline 75% + N | | | | | 8.63 | 163 | 5700 | 8600 | 3700 | 16000 |
| Volcanics, Baseline + N | | | | | 8.76 | 180 | 7300 | 12000 | 4100 | 19000 |
| Volcanics, Enriched 6% + N | | | | | 7.91 | 118 | 3300 | 1700 | 3600 | 12000 |
| Volcanics, Enriched 75% + N | | | | | 8.57 | 179 | 6600 | 11000 | 4000 | 16000 |
| Volcanics, Enriched + N | | | | | 8.83 | 203 | 8100 | 15000 | 4400 | 18000 |
| DGV or 95% GV^a | | | | | - | - | - | - | - | - |

* Analytes reported are based on the major analytes detected in Assignment P4 (Simpson et al., 2019)

^a <http://www.waterquality.gov.au/anz-guidelines/guideline-values/default/water-quality-toxicants/>

DGV = default guideline value, representing the 95% species protection guideline values (95% GV) for freshwater.

Table 12. Concentrations of dissolved (0.45 µm) metals (µg/L) in leachates of excavated rock material (18 h mixing)*

| Sample Name | Al | As | Cu | Fe | Mn | Ni | P | Zn |
|----------------------------------|-----------|------------|------------|----------|----------|-----------|----------|------------|
| Ravine, Baseline | 340 | 11 | 0.9 | 250 | 5.4 | <5.9 | 11 | 0.6 |
| Ravine, Baseline + N | 350 | 11 | <0.7 | 290 | 120 | <5.9 | 150 | 2.4 |
| Ravine, Enriched | 280 | 16 | <0.7 | 93 | 5.2 | <5.9 | 7.7 | 1.0 |
| Ravine, Enriched + N | 280 | 15 | <0.7 | 120 | 120 | <5.9 | 150 | 2.8 |
| Byron, Baseline | 89 | <8.3 | <0.7 | 33 | 2.5 | <5.9 | 36 | <0.2 |
| Byron, Baseline + N | 88 | <8.3 | <0.7 | 62 | 120 | <5.9 | 180 | 1.6 |
| Byron, Enriched | 270 | 11 | <0.7 | 130 | 2.7 | <5.9 | 14 | 0.3 |
| Byron, Enriched + N | 270 | 9.7 | <0.7 | 160 | 120 | <5.9 | 150 | 1.6 |
| Shaw Gabbro, Baseline | 510 | <8.3 | <0.7 | 46 | 1.7 | <5.9 | 2.2 | 0.5 |
| Shaw Gabbro, Baseline + N | 480 | <8.3 | <0.7 | 77 | 110 | <5.9 | 140 | 2.0 |
| Shaw Gabbro, Enriched | 300 | <8.3 | 1.5 | 10 | 0.7 | <5.9 | 8.0 | <0.2 |
| Shaw Gabbro, Enriched + N | 290 | <8.3 | 0.7 | 41 | 110 | <5.9 | 130 | 1.7 |
| Volcanics, Baseline | 270 | 11 | 0.9 | <0.8 | 1.2 | <5.9 | <1.0 | <0.2 |
| Volcanics, Baseline + N | 230 | <8.3 | <7 | <8 | 130 | <5.9 | 140 | <2 |
| Volcanics, Enriched | 480 | 8.5 | <0.7 | 1.7 | 1.4 | <5.9 | 2.5 | <0.2 |
| Volcanics, Enriched + N | 440 | <8.3 | 7.0 | <8 | 120 | <5.9 | 80 | <2 |
| Peppercorn, Baseline | 260 | 11 | <0.7 | 110 | 2.8 | <5.9 | 37 | <0.2 |
| Peppercorn, Baseline + N | 260 | 8.6 | 1.0 | 140 | 120 | <5.9 | 180 | 1.8 |
| Peppercorn, Enriched | 360 | <8.3 | <0.7 | 91 | 2.8 | <5.9 | 21 | <0.2 |
| Peppercorn, Enriched + N | 340 | <8.3 | 0.7 | 110 | 110 | <5.9 | 160 | 1.6 |
| Kellys Plain, Baseline | 180 | <5.2 | <1.1 | 95 | 4 | NR | 22 | 0.9 |
| Kellys Plain, Baseline + N | 190 | 5.7 | <1.1 | 160 | 110 | NR | 170 | 2.5 |
| Kellys Plain, Enriched | 590 | 27 | <1.1 | 370 | 10 | NR | 23 | 1.7 |
| Kellys Plain, Enriched + N | 270 | 11 | <1.1 | 130 | 110 | NR | 150 | 2.1 |
| Felsic, Baseline | 270 | <8.3 | <0.7 | 69 | 4.7 | <5.9 | 7.8 | 0.2 |
| Felsic, Baseline + N | 280 | <8.3 | <0.7 | 99 | 110 | <5.9 | 150 | 1.9 |
| Felsic, Enriched | >2,000 | 19 | 2.7 | 2300 | 34 | <5.9 | 27 | 360 |
| Felsic, Enriched + N | 1800 | 20 | 1.0 | 940 | 130 | <5.9 | 160 | 190 |
| Volcanics, Baseline 6% + N | 20 | <8.3 | <0.7 | 25 | 110 | <5.9 | 140 | 7.5 |
| Volcanics, Baseline 75% + N | 180 | <8.3 | <7 | <8 | 100 | <5.9 | 120 | 2.1 |
| Volcanics, Baseline + N | 230 | <8.3 | <7 | <8 | 130 | <5.9 | 140 | <2 |
| Volcanics, Enriched 6% + N | 32 | <8.3 | 0.7 | 22 | 110 | <5.9 | 140 | 2.6 |
| Volcanics, Enriched 75% + N | 290 | <8.3 | <7 | 8.5 | 110 | <5.9 | 91 | <2 |
| Volcanics, Enriched + N | 440 | <8.3 | 7.0 | <8 | 120 | <5.9 | 80 | <2 |
| DGW or 95% GV^a | 55 | 13 | 1.4 | – | – | 11 | – | 8.0 |
| 99% GV^b | 27 | 0.8 | 1.0 | – | – | 8 | – | 2.4 |

* Analytes reported are based on the major analytes detected in Assignment P4 (Simpson et al., 2019)

^a <http://www.waterquality.gov.au/anz-guidelines/guideline-values/default/water-quality-toxicants/>

DVG = default guideline value, representing the 95% species protection guideline values (95% GV) for freshwater.

^b 99% species protection guideline values (99% GV) for freshwater. Values for Arsenic are for As(V)

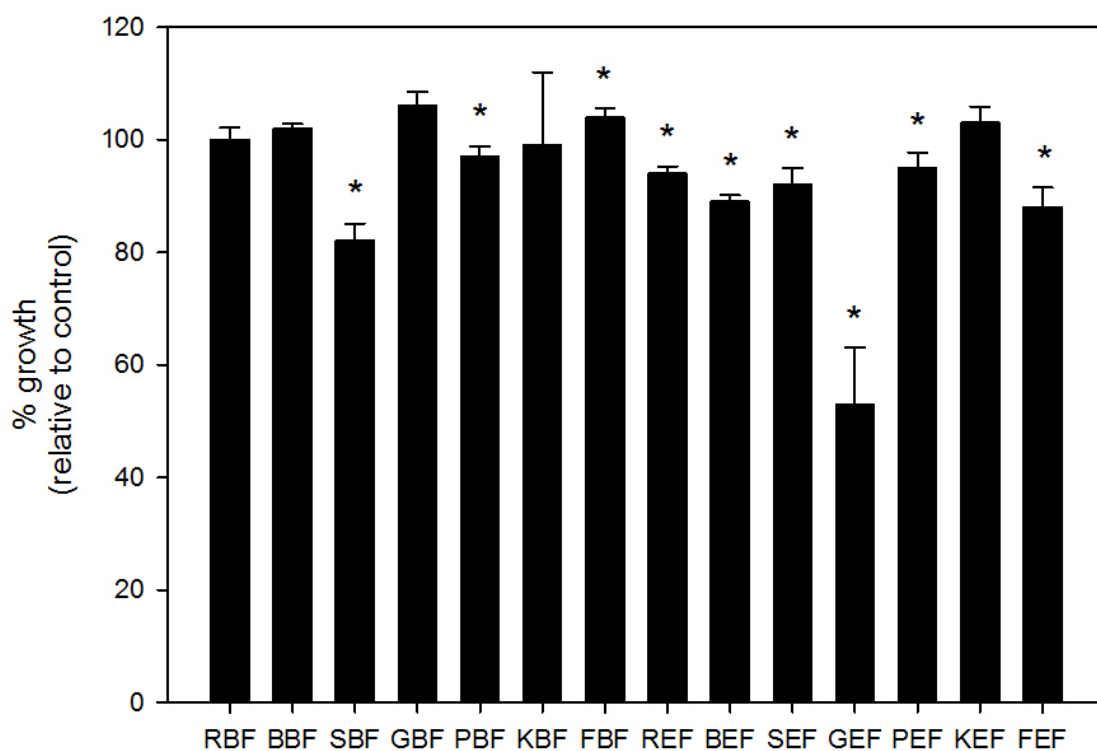


Figure 3. Toxicity of leachates of excavated rock material (prepared in Talbingo Reservoir water) to the microalga *Raphidocelis subcapitata*. Microalgal population growth (72 h) is expressed as % of control treatment (algal growth rate in the Method Blank control (Talbingo Reservoir water)). The lower the column, the more toxic the sample. The x-axis labels consist of three letters; first letter represents the geological zone Ravine (R), Byron (B), Shaw Gabbro (S), Gooandra Volcanics (G), Peppercorn (P), Kellys Plain (K) and Felsic (F); second letter represents Baseline (B) or Enriched (E) excavated rock. All leachates were filtered (0.45 μ m). Error bars represent 1 standard deviation. * indicates treatment is significantly different to the control treatment ($p \leq 0.05$). FBF is significantly greater than the control (i.e. stimulation in response)

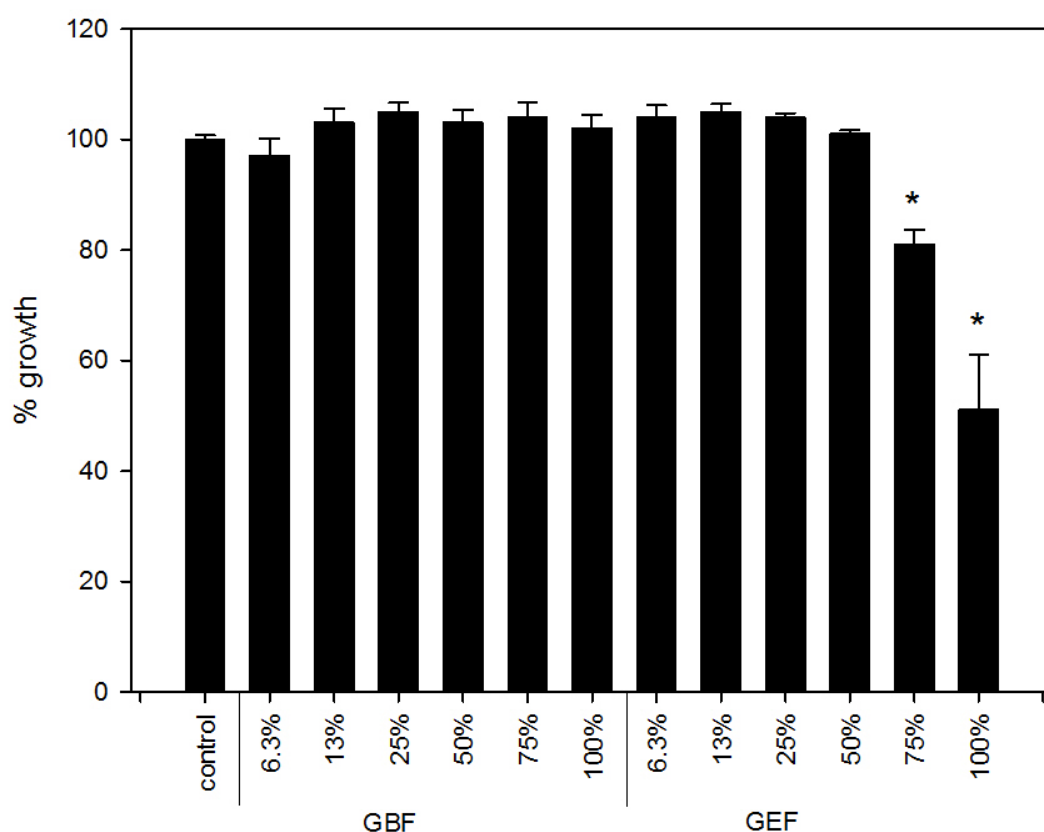


Figure 4. Toxicity of Gooandra Baseline (GBF) and Gooandra Enriched (GEF) leachates of excavated rock material (prepared in Talbingo Reservoir water) to the microalga *Raphidocelis subcapitata* (72 h population growth rate). Leachates were serially diluted 1 in 2 with control water (USEPA media). Microalgal growth is expressed as % of control treatment (algal growth rate in the USEPA media). The lower the column, the more toxic the sample. * indicates treatment is significant different to the control treatment ($p \leq 0.05$)

The most toxic leachate (Gooandra Enriched, 47% inhibition in algal growth rate) did not have the highest concentrations of dissolved metals (aluminium, arsenic, zinc) but it did have the highest concentration of copper (7 $\mu\text{g/L}$). It is unclear if the toxicity was due to truly dissolved metals and/or, suspended solids/precipitated metals of $<0.45 \mu\text{m}$.

3.3 Characterisation of reservoir water used for baseline toxicity assessment using macroinvertebrates

The pH, EC, DO and turbidity measured in the Talbingo and Tantangara Reservoir waters are shown in Table 13. The pH, EC, DO and turbidity were similar in both reservoirs and ranged from 7.58 to 8.0, 30 to 33 $\mu\text{S}/\text{cm}$, 104-108% DO, and 0.5 to 2.55 NTU, respectively. The concentrations of metal and metalloid elements are shown in Table 14. The concentrations of dissolved Ag, Be, Cd, Li, Mo, Sb, Se, Sn, Sr and Tl were similar in both reservoirs. The concentrations of dissolved Al, As, Ba, Co, Cr, Fe, Mn, Ni, Pb, Th and V were higher in the Tantangara Reservoir than the Talbingo Reservoir waters.

The dissolved metal concentrations were compared to the corresponding GVs for water quality (ANZG, 2018), representing the 95 and 99% of species protection concentrations, when values were available (Table 14). Tantangara Reservoir and Talbingo Reservoir waters exceeded the 99% guideline value (99% GV) for dissolved Al and Fe.

3.4 Characterisation of leachates used for determining toxicity using macroinvertebrates

The vast majority of the excavated rock, by mass, is expected to be larger than sand size and should settle rapidly, whereas the finest fractions (clay to low-silt size range) of the excavated rock materials may remain suspended in the waters in the main disposal area for a considerable period of time and not settle for many weeks or months after the placement activities cease. Consequently the bottom waters may contain a high concentration of suspended fine excavated rock material for the duration of the placement activities and potentially for weeks beyond the date placement is deemed complete.

Characterisation of leachate samples is given in Table 15, Table 16 and Table 17. Al, Fe, Cr, Cu, As, Pb were above the GVs in raw and 12-day settled leachates. Raw leachates had the highest concentration of metals and there was >50% reduction in metal concentrations in the 12-day settled corresponding leachates. Filtered leachates had the lowest concentrations of metals and only aluminium and chromium were still reported to be higher than the GVs. However, Al was also exceeding the 99% GV value (27 $\mu\text{g}/\text{L}$) in the Tantangara Reservoir water samples.

Table 13. The pH, EC, dissolved oxygen, turbidity, major cations, sulphur and phosphorus in background water samples from Talbingo and Tantangara Reservoirs

| Sample | pH | DO % Saturation | EC µs/cm | Turbidity NTU | Ca mg/L | K mg/L | Mg mg/L | Na mg/L | S mg/L | P mg/L |
|---------------------|------|--------------------|-------------|------------------|------------|-----------|------------|------------|-----------|-----------|
| TN1-B | 7.84 | 104.5 | 31.0 | 0.51 | 1.4 | 0.6 | 0.9 | 1.6 | <0.2 | 0.2 |
| TN2-B | 7.87 | 105.5 | 31.4 | 1.06 | 1.4 | 0.6 | 0.9 | 1.7 | <0.2 | 0.1 |
| TN3-B | 8.00 | 108.5 | 32.1 | 0.79 | 1.4 | 0.6 | 0.9 | 1.7 | <0.2 | 0.2 |
| TAL-PL1C | 7.71 | 107.1 | 30.4 | 1.81 | 1.6 | 0.4 | 0.7 | 1.6 | <0.2 | 0.2 |
| TAL-PL2C | 7.76 | 104.3 | 30.1 | 2.55 | 1.6 | 0.4 | 0.7 | 1.6 | <0.2 | 0.2 |
| TAL-PL1D | 7.58 | 106.2 | 33.0 | 1.83 | 1.6 | 0.4 | 0.7 | 1.5 | <0.2 | 0.2 |
| TAL-PL2D | 7.67 | 104.6 | 30.3 | 0.77 | 1.6 | 0.4 | 0.7 | 1.5 | <0.2 | 0.2 |
| Min | 7.58 | 104.3 | 30.1 | 0.51 | 1.4 | 0.4 | 0.7 | 1.5 | <0.2 | 0.1 |
| Max | 8.0 | 108.5 | 33.0 | 2.55 | 1.6 | 0.6 | 0.9 | 1.7 | <0.2 | 0.2 |
| 95% GV ^a | - | - | - | - | - | - | - | - | 0.39 | 8.51 |
| 99% GV ^a | - | - | - | - | - | - | - | - | 0.01 | - |

<http://www.waterquality.gov.au/anz-guidelines/guideline-values/default/water-quality-toxicants/>

^a GV guideline value represents the 95% (95% GV) and 99% (99% GV) species protection guideline values for freshwater. Values highlighted in red and blue is where default guideline value is exceeded.

Table 14. The concentrations of metals and metalloids in background water samples from Talbingo and Tantangara Reservoirs

| Sample | Al µg/L | As µg/L | B mg/L | Ba µg/L | Cd µg/L | Co µg/L | Cr µg/L | Cu µg/L | Fe µg/L | Hg µg/L | Mn µg/L | Mo µg/L |
|---------------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| TN1-B | 45 | <0.5 | <0.05 | 4.1 | <0.1 | <0.1 | <1 | <0.5 | 304 | <0.5 | 3 | <0.1 |
| TN2-B | 50 | <0.5 | <0.05 | 4.0 | <0.1 | <0.1 | <1 | <0.5 | 306 | <0.5 | 3 | <0.1 |
| TN3-B | 50 | <0.5 | <0.05 | 2.9 | <0.1 | <0.1 | <1 | <0.5 | 309 | <0.5 | 2 | <0.1 |
| TAL-PL1C | 7 | <0.5 | <0.05 | 2.8 | <0.1 | <0.1 | <1 | <0.5 | 13 | <0.5 | <1 | <0.1 |
| TAL-PL2C | 7 | <0.5 | <0.05 | 3.0 | <0.1 | <0.1 | <1 | <0.5 | 14 | <0.5 | <1 | <0.1 |
| TAL-PL1D | 2 | <0.5 | <0.05 | 1.2 | <0.1 | <0.1 | <1 | <0.5 | 8 | <0.5 | <1 | <0.1 |
| TAL-PL2D | 4 | <0.5 | <0.05 | 1.2 | <0.1 | <0.1 | <1 | <0.5 | 8 | <0.5 | <1 | <0.1 |
| Min | 2 | <0.5 | <0.05 | 1.2 | <0.1 | <0.1 | <1 | <0.5 | 8 | <0.5 | <1 | <0.1 |
| Max | 50 | <0.5 | <0.05 | 4.1 | <0.1 | <0.1 | <1 | <0.5 | 309 | <0.5 | 3 | <0.1 |
| 95% GV ^a | 55 | 13 | 0.37 | - | 0.2 | - | 0.4 | 1.4 | 700 | - | 1900 | - |
| 99% GV ^a | 27 | 0.8 | 0.09 | - | 0.06 | - | 0.01 | 1 | 400 | - | 1200 | - |
| Sample | Ni µg/L | Pb µg/L | Sb µg/L | Se µg/L | Si mg/L | Sn µg/L | Sr µg/L | Th µg/L | U µg/L | V µg/L | Zn µg/L | |
| TN1-B | <0.5 | <0.1 | <0.5 | 0.5 | 0.4 | <0.5 | 11.2 | <0.1 | <0.05 | 0.2 | 0.8 | |
| TN2-B | <0.5 | <0.1 | <0.5 | 0.6 | 0.4 | <0.5 | 10.9 | <0.1 | <0.05 | 0.2 | <0.5 | |
| TN3-B | <0.5 | <0.1 | <0.5 | 0.8 | 0.5 | <0.5 | 9.7 | <0.1 | <0.05 | 0.2 | <0.5 | |
| TAL-PL1C | <0.5 | <0.1 | <0.5 | 2.0 | 0.6 | <0.5 | 12.2 | <0.1 | <0.05 | <0.1 | <0.5 | |
| TAL-PL2C | <0.5 | <0.1 | <0.5 | 2.0 | 0.7 | <0.5 | 11.3 | <0.1 | <0.05 | <0.1 | <0.5 | |
| TAL-PL1D | <0.5 | <0.1 | <0.5 | 2.0 | 0.3 | <0.5 | 6.3 | <0.1 | <0.05 | <0.1 | <0.5 | |
| TAL-PL2D | <0.5 | <0.1 | <0.5 | 2.0 | 0.5 | <0.5 | 7.6 | <0.1 | <0.05 | <0.1 | <0.5 | |
| Min | <0.5 | <0.1 | <0.5 | 0.55 | 0.30 | <0.5 | 6.30 | <0.1 | <0.05 | <0.1 | <0.5 | |
| Max | <0.5 | <0.1 | <0.5 | 2.01 | 0.70 | <0.5 | 12.20 | <0.1 | <0.05 | 0.2 | 0.8 | |
| 95% GV ^a | 11 | 3.4 | - | 11 | - | - | - | - | - | - | 8 | |
| 99% GV ^a | 8 | 1 | - | 5 | - | - | - | - | - | - | 2.4 | |

<http://www.waterquality.gov.au/anz-guidelines/guideline-values/default/water-quality-toxicants/>

^a GV guideline value represents the 95% (95% GV) and 99% (99% GV) species protection guideline values for freshwater. Values highlighted in red and blue is where default guideline value is exceeded. Values for arsenic are for As(V), chromium are for Cr(VI), and tin are for inorganic tin

Table 15. The pH, EC, dissolved oxygen, turbidity, major cations, sulphur and phosphorus in leachates of excavated rock from seven geological zones

| Sample | | | pH | DO % Saturation | EC µs/cm | Turbidity NTU | Ca mg/L | K mg/L | Mg mg/L | Na mg/L | S mg/L | P mg/L |
|-------------|----------|---------------------|------|--------------------|-------------|------------------|------------|-----------|------------|------------|-----------|-----------|
| Ravine | Baseline | Raw | 7.91 | 81.3 | 121.4 | 4390 | 5.9 | 12 | 22 | 6 | <1 | <1 |
| | | Settling | 7.59 | 93.9 | 119.3 | 150 | 4.4 | 8.9 | 11 | 5.1 | <1 | <1 |
| | | Filtered | 7.55 | 90.7 | 103.6 | 1.49 | 4.2 | 6.7 | 2.1 | 7.3 | 0.3 | <0.2 |
| | Enriched | Raw | 7.86 | 88.4 | 160.0 | 8370 | 5 | 16 | 26 | <5 | <5 | <5 |
| | | Settling | 7.79 | 93.1 | 143.7 | 99.7 | 5.4 | 7.3 | 8.2 | 4.9 | 1.1 | <1 |
| | | Filtered | 7.86 | 92.6 | 146.5 | 2.62 | 4.1 | 11 | 3.3 | 4.9 | 1.3 | <0.2 |
| | Baseline | Raw | 7.83 | 83.3 | 192.1 | 7810 | 9.9 | 85 | 19 | 5 | <1 | <1 |
| | | Settling | 7.23 | 93.6 | 149.8 | 570 | 6.4 | 45 | 8.1 | 4.3 | 0.4 | <1 |
| | | Filtered | 7.50 | 89.2 | 148.9 | 4.23 | 2.6 | 24 | 0.7 | 5.5 | 0.9 | <0.2 |
| Byron | Enriched | Raw | 7.93 | 84.7 | 250.0 | 6890 | 7 | 42 | 10 | <5 | <5 | <5 |
| | | Settling | 7.68 | 95.3 | 196.1 | 53.1 | 9.0 | 17 | 2.8 | 4.2 | 3.0 | <1 |
| | | Filtered | 7.93 | 93.6 | 198.0 | 2.14 | 4.3 | 27 | 1.3 | 3.8 | 2.9 | <0.2 |
| | Baseline | Raw | 7.98 | 84.4 | 154.6 | 1750 | 5.1 | 5 | 4.6 | 8 | <1 | <1 |
| | | Settling | 7.67 | 93.7 | 135.4 | 7.02 | 5.2 | 5.2 | 1.9 | 6.7 | <1 | <1 |
| | | Filtered | 7.64 | 90.8 | 110.3 | 0.46 | 3.2 | 8.2 | 2.0 | 10 | 0.2 | <0.2 |
| | Enriched | Raw | 7.82 | 87.7 | 147.7 | 824 | 8 | 9 | 6 | <5 | <5 | <5 |
| | | Settling | 7.82 | 93.4 | 111.1 | 30.7 | 6.6 | 3.4 | 1.9 | 3.9 | <1 | <1 |
| | | Filtered | 7.86 | 93.0 | 114.4 | 6.38 | 4.0 | 7.3 | 1.0 | 4.5 | 0.3 | <0.2 |
| Shaw Gabbro | Baseline | Raw | 8.04 | 80.6 | 160.8 | 2930 | 7.0 | 15 | 6.1 | 8 | <1 | <1 |
| | | Settling | 7.73 | 93.7 | 133.9 | 61.4 | 4.9 | 9.3 | 1.5 | 5.6 | <1 | <1 |
| | | Filtered | 7.67 | 90.0 | 114.3 | 4.92 | 5.2 | 13 | 0.9 | 7.7 | 0.3 | <0.2 |
| | Enriched | Raw | 7.83 | 91.1 | 123.4 | 436.8 | 8 | <5 | <3 | <5 | <5 | <5 |
| | | Settling | 7.80 | 93.8 | 122.4 | 2.06 | 7.8 | 2.4 | 0.9 | 3.1 | 1.1 | <1 |
| | | Filtered | 7.82 | 92.8 | 132.7 | 3.37 | 7.8 | 8.4 | 1.3 | 5.0 | 3.3 | <0.2 |
| | Baseline | Raw | 7.97 | 80.6 | 131.6 | 3340 | 8.7 | 16 | 11 | 7 | <1 | <1 |
| | | Settling | 7.50 | 94.1 | 111.7 | 155 | 5.9 | 9.0 | 4.1 | 5.4 | <1 | <1 |
| | | Filtered | 7.53 | 90.1 | 93.7 | 3.14 | 5.5 | 6.3 | 1.5 | 6.6 | 0.4 | <0.2 |
| Peppercorn | Enriched | Raw | 7.81 | 88.1 | 168.1 | 436.8 | 9 | 16 | 9 | <5 | <5 | <5 |
| | | Settling | 7.71 | 93.6 | 138.5 | 103 | 8.8 | 7.5 | 4.0 | 5.5 | 2.8 | <1 |
| | | Filtered | 7.83 | 92.7 | 143.8 | 3.42 | 5.3 | 8.3 | 1.8 | 5.3 | 3.9 | <0.2 |
| | Baseline | Raw | 7.89 | 88.7 | 144.6 | 6660 | 5 | 31 | 17 | <5 | <5 | <5 |
| | | Settling | 7.74 | 93.8 | 126.3 | 196 | 4.4 | 11 | 8.1 | 4.6 | 2.1 | <1 |
| | | Filtered | 7.84 | 93.2 | 139.9 | 1.75 | 2.6 | 7.4 | 3.9 | 4.4 | 3.1 | <0.2 |
| | Enriched | Raw | 7.96 | 81.4 | 152.2 | 6290 | 8.7 | 20 | 11 | 7 | <1 | <1 |
| | | Settling | 7.43 | 94.3 | 125.2 | 153 | 6.0 | 10 | 3.0 | 6.3 | <1 | <1 |
| | | Filtered | 7.53 | 90.2 | 105.8 | 1.71 | 5.4 | 8.4 | 1.1 | 8.1 | 0.2 | <0.2 |
| Felsic | Enriched | Raw | 8.05 | 87.6 | 203.8 | 6920 | 11 | 115 | 32 | <5 | <5 | <5 |
| | | Settling | 7.74 | 95.4 | 159.4 | 531 | 9.9 | 48 | 12 | 4.9 | 1.1 | <1 |
| | | Filtered | 7.90 | 93.0 | 165.8 | 6.69 | 3.3 | 18 | 1.1 | 5.1 | 1.4 | <0.2 |
| | Baseline | Min | 7.23 | 80.6 | 93.7 | 0.46 | 2.6 | 2.4 | 0.7 | 3.1 | 0.2 | <0.2 |
| | | Max | 8.05 | 95.4 | 250.0 | 8370 | 10.5 | 115.1 | 32.4 | 10.3 | 3.9 | <5 |
| | | 95% GV ^a | - | - | - | - | - | - | - | - | 0.39 | 8.51 |
| | | 99% GV ^a | - | - | - | - | - | - | - | - | 0.01 | - |

<http://www.waterquality.gov.au/anz-guidelines/guideline-values/default/water-quality-toxicants/>

^a GV guideline value represents the 95% (95% GV) and 99% (99% GV) species protection guideline values for freshwater. Values highlighted in red and blue is where default guideline value is exceeded. Values for arsenic are for As(V), chromium are for Cr(VI), and tin are for inorganic tin

Table 16. The concentrations of metals and metalloids in leachates of excavated rock from seven geological zones (part A)

| Sample ID | | | Al µg/L | As µg/L | B mg/L | Ba µg/L | Cd µg/L | Co µg/L | Cr µg/L | Cu µg/L | Fe µg/L | Hg µg/L | Mn µg/L | Mo µg/L |
|---------------|----------|---------------------|------------|------------|-----------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| Ravine | Baseline | Raw | 39011 | 19 | <0.2 | 220 | <0.5 | 17.4 | 112 | 39 | 29236 | <3 | 625 | <2 |
| | | Settling | 17794 | 11 | <0.2 | 119 | <0.5 | 6.9 | 77 | 8 | 14437 | <3 | 208 | <2 |
| | | Filtered | 181 | 5.7 | <0.05 | 2.0 | <0.1 | 0.08 | 0.6 | 0.4 | 79 | <0.5 | 1.4 | <0.4 |
| | Enriched | Raw | 35794 | <10 | <1 | 286 | <3 | 16 | 148 | <5 | 30402 | <10 | 759 | <10 |
| | | Settling | 9561 | <2 | <0.2 | 111 | <0.5 | 3.5 | 58 | 8 | 8292 | <3 | 205 | <2 |
| | | Filtered | 131 | 2.9 | <0.05 | 17.9 | <0.1 | <0.05 | <0.4 | <0.2 | 59 | <0.5 | 3.8 | 1.1 |
| Byron | Baseline | Raw | 186110 | 20 | <0.2 | 1061 | <0.5 | 10.7 | 74 | 10 | 14764 | <3 | 358 | 9 |
| | | Settling | 84476 | 15 | <0.2 | 482 | <0.5 | 3.6 | 51 | 3 | 13616 | <3 | 113 | 3 |
| | | Filtered | 400 | 12.2 | <0.05 | 5.3 | <0.1 | <0.05 | 2.1 | <0.2 | 60 | <0.5 | 0.9 | 3.2 |
| | Enriched | Raw | 59828 | 11 | <1 | 437 | <3 | 9 | 88 | <5 | 17998 | <10 | 135 | 32 |
| | | Settling | 7683 | 6 | <0.2 | 56 | <0.5 | 1.3 | 35 | 8 | 2075 | <3 | 23 | 5 |
| | | Filtered | 52 | 7.6 | <0.05 | 2.6 | <0.1 | <0.05 | <0.4 | <0.2 | 3 | <0.5 | 0.6 | 9.0 |
| Shaw Gabbro | Baseline | Raw | 2491 | <2 | <0.2 | 3 | <0.5 | 4.1 | 33 | 4 | 2191 | <3 | 49 | <2 |
| | | Settling | 483 | <2 | <0.2 | 3 | <0.5 | 1.0 | 38 | 3 | 310 | <3 | 10 | <2 |
| | | Filtered | 214 | 0.7 | <0.05 | <0.4 | <0.1 | 0.05 | 8.0 | 0.3 | 4 | <0.5 | <0.4 | <0.4 |
| | Enriched | Raw | 19904 | <10 | <1 | 172 | <3 | 9 | 54 | 9 | 8516 | <10 | 245 | <10 |
| | | Settling | 5093 | 2 | <0.2 | 41 | <0.5 | 1.7 | 36 | 5 | 2150 | <3 | 64 | <2 |
| | | Filtered | 144 | 2.4 | <0.05 | 5.3 | <0.1 | <0.05 | 0.5 | 0.6 | 34 | <0.5 | 1.8 | <0.4 |
| Volcanics | Baseline | Raw | 27611 | 18 | <0.2 | 269 | <0.5 | 4.9 | 29 | 8 | 9555 | <3 | 169 | <2 |
| | | Settling | 5849 | 18 | <0.2 | 61 | <0.5 | 1.3 | 36 | 3 | 1812 | <3 | 29 | 2 |
| | | Filtered | 465 | 16.8 | <0.05 | 2.0 | <0.1 | 0.05 | 0.5 | 0.4 | 25 | <0.5 | 1.6 | <0.4 |
| | Enriched | Raw | 2273 | 15 | <1 | 25 | <3 | 6 | 31 | 71 | 876 | <10 | 16 | <10 |
| | | Settling | 235 | 12 | <0.2 | 7 | <0.5 | 0.7 | 30 | 4 | 57 | <3 | 12 | <2 |
| | | Filtered | 108 | 15.0 | <0.05 | 1.1 | <0.1 | <0.05 | <0.4 | 0.3 | 16 | <0.5 | 1.5 | 1.1 |
| Peppercorn | Baseline | Raw | 37918 | 7 | <0.2 | 381 | <0.5 | 7.1 | 67 | 5 | 16079 | <3 | 292 | 4 |
| | | Settling | 17509 | 6 | <0.2 | 188 | <0.5 | 2.9 | 59 | 6 | 6491 | <3 | 92 | 4 |
| | | Filtered | 241 | 4.9 | <0.05 | 3.9 | <0.1 | 0.07 | 0.6 | 0.3 | 60 | <0.5 | 1.4 | 3.0 |
| | Enriched | Raw | 37547 | <10 | <1 | 890 | <3 | 9 | 70 | 31 | 15624 | <10 | 237 | <10 |
| | | Settling | 13769 | 3 | <0.2 | 435 | <0.5 | 2.3 | 44 | 14 | 6106 | <3 | 92 | <2 |
| | | Filtered | 545 | 2.6 | <0.05 | 83.9 | <0.1 | 0.10 | 0.7 | 1.2 | 275 | <0.5 | 5.8 | 1.7 |
| Kelly's Plain | Enriched | Raw | 91102 | <10 | <1 | 270 | <3 | 13 | 123 | 6 | 22727 | <10 | 251 | 17 |
| | | Settling | 35343 | 2 | <0.2 | 107 | 3.1 | 3.2 | 58 | 10 | 8715 | <3 | 76 | 14 |
| | | Filtered | 369 | 1.7 | <0.05 | 8.0 | <0.1 | <0.05 | 0.5 | <0.2 | 93 | <0.5 | 3.3 | 12.1 |
| Felsic | Baseline | Raw | 47513 | 3 | <0.2 | 314 | <0.5 | 7.6 | 72 | 6 | 18782 | <3 | 187 | <2 |
| | | Settling | 14523 | 2 | <0.2 | 107 | <0.5 | 2.1 | 44 | 5 | 5629 | <3 | 65 | <2 |
| | | Filtered | 218 | 2.1 | <0.05 | 3.3 | <0.1 | 0.06 | <0.4 | 0.2 | 37 | <0.5 | 1.1 | 0.7 |
| | Enriched | Raw | 204275 | 22 | <1 | 2063 | <3 | 15 | 167 | 17 | 46306 | <10 | 243 | <10 |
| | | Settling | 97202 | 20 | <0.2 | 960 | <0.5 | 5.0 | 89 | 11 | 19816 | <3 | 121 | 2 |
| | | Filtered | 709 | 19.4 | <0.05 | 25.0 | <0.1 | 0.06 | 0.6 | 1.9 | 122 | <0.5 | 1.2 | 2.3 |
| | | Min | 52 | 1 | <0.05 | 1 | 3 | <0.05 | 1 | 0 | 3 | <0.5 | 1 | 1 |
| | | Max | 204275 | 22 | <1 | 2063 | 3 | 17 | 167 | 71 | 46306 | <10 | 759 | 32 |
| | | 95% GV ^a | 55 | 13 | 0.37 | - | 0.2 | - | 0.4 | 1.4 | 700 | - | 1900 | - |
| | | 99% GV ^a | 27 | 0.8 | 0.09 | - | 0.06 | - | 0.01 | 1 | 400 | - | 1200 | - |

<http://www.waterquality.gov.au/anz-guidelines/guideline-values/default/water-quality-toxicants/>

^a GV guideline value represents the 95% (95% GV) and 99% (99% GV) species protection guideline values for freshwater. Values highlighted in red and blue is where default guideline value is exceeded. Values for arsenic are for As(V), chromium are for Cr(VI), and tin are for inorganic tin

Table 17. The concentrations of metals and metalloids in leachates of excavated rock from seven geological zones (part B)

| Sample ID | | | Ni µg/L | Pb µg/L | Sb µg/L | Se µg/L | Si mg/L | Sn µg/L | Sr µg/L | Th µg/L | U µg/L | V µg/L | Zn µg/L | |
|---------------|----------|---------------------|---------------------|------------|------------|------------|------------|------------|------------|------------|-----------|-----------|------------|------|
| Ravine | Baseline | Raw | 93 | 16 | <3 | 4 | 45 | 5 | 84 | 10.9 | 2.2 | 93 | 86 | |
| | | Settling | 45 | 4 | 2 | 4 | 24 | 3.7 | 73 | 4.0 | 0.9 | 43 | 28 | |
| | | Filtered | 0.3 | <0.4 | 1.0 | 0.5 | 2.7 | 1.0 | 33.8 | <0.1 | <0.1 | 3.6 | <0.5 | |
| | Enriched | Raw | 111 | 137 | <10 | <10 | 40 | 15 | 71 | <3 | <3 | 113 | 115 | |
| | | Settling | 26 | 43 | 8 | 4 | 13 | 3.0 | 95 | 0.6 | <0.5 | 26 | 37 | |
| | | Filtered | 0.3 | <0.4 | 8.4 | <0.5 | 1.8 | <0.1 | 31.9 | <0.1 | <0.1 | 3.5 | <0.5 | |
| Byron | Baseline | Raw | 32 | 12 | 7 | 33 | 27 | 26 | 55 | 32.1 | 7.2 | 152 | 47 | |
| | | Settling | 11 | 4 | 7 | 3 | 51 | 11.0 | 34 | 8.5 | 3.3 | 67 | 15 | |
| | | Filtered | 0.2 | <0.4 | 6.5 | 0.7 | 3.7 | 0.9 | 9.0 | <0.1 | 0.2 | 5.7 | <0.5 | |
| | Enriched | Raw | 17 | 12 | 33 | <10 | 54 | 38 | 49 | 12 | <3 | 107 | 20 | |
| | | Settling | 3 | <2 | 14 | 4 | 9.9 | 3.9 | 78 | 0.6 | 1.4 | 13 | 8 | |
| | | Filtered | <0.2 | <0.4 | 15.4 | 1.1 | 1.7 | <0.1 | 18.9 | <0.1 | <0.1 | 5.7 | <0.5 | |
| Shaw Gabbro | Baseline | Raw | 5 | <2 | <3 | <3 | 5 | 4 | 5 | <0.5 | <0.5 | 15 | 6 | |
| | | Settling | 1 | <2 | <2 | 4 | 2.3 | 1.3 | 5 | <0.5 | <0.5 | 11 | 4 | |
| | | Filtered | <0.2 | <0.4 | <0.5 | <0.5 | 2.1 | 0.8 | 2.5 | <0.1 | <0.1 | 8.1 | <0.5 | |
| | Enriched | Raw | 14 | <10 | <10 | <10 | 23 | 13 | 32 | 14 | <3 | 41 | 22 | |
| | | Settling | 3 | 2 | <2 | 3 | 8.6 | 2.9 | 28 | 3.6 | 0.9 | 13 | 8 | |
| | | Filtered | <0.2 | <0.4 | <0.5 | <0.5 | 2.1 | <0.1 | 6.7 | <0.1 | 0.2 | 5.4 | <0.5 | |
| Volcanics | Baseline | Raw | 7 | 14 | <3 | 4 | 30 | 4 | 47 | 11.9 | 1.7 | 35 | 23 | |
| | | Settling | 2 | 3 | <2 | 4 | 8.2 | 2.5 | 22 | 2.2 | 0.8 | 11 | 6 | |
| | | Filtered | <0.2 | <0.4 | 0.7 | <0.5 | 2.3 | <0.4 | 9.5 | <0.1 | 0.1 | 4.4 | <0.5 | |
| | Enriched | Raw | 108 | <10 | <10 | <10 | <5 | 11 | 15 | <3 | <3 | 16 | 428 | |
| | | Settling | 1 | <2 | 2 | <3 | 1.1 | 1.6 | 21 | <0.5 | <0.5 | 9 | <3 | |
| | | Filtered | <0.2 | <0.4 | 2.5 | <0.5 | 1.2 | <0.1 | 14.1 | <0.1 | 0.2 | 6.5 | <0.5 | |
| Peppercorn | Baseline | Raw | 17 | 4 | <3 | 5 | 47 | 7 | 60 | 12.4 | 3.0 | 74 | 27 | |
| | | Settling | 7 | <2 | <2 | <3 | 24 | 3.7 | 41 | 3.9 | 1.6 | 34 | 13 | |
| | | Filtered | <0.2 | <0.4 | <0.5 | <0.5 | 3.3 | 0.7 | 17.6 | <0.1 | 0.2 | 3.9 | <0.5 | |
| | Enriched | Raw | 26 | <10 | <10 | <10 | 34 | 16 | 32 | 4 | <3 | 69 | 49 | |
| | | Settling | 10 | 4 | <2 | 5 | 18 | 3.6 | 44 | 1.2 | 0.6 | 23 | 16 | |
| | | Filtered | 0.7 | <0.4 | 1.4 | <0.5 | 2.2 | 0.2 | 16.3 | <0.1 | 0.1 | 3.9 | <0.5 | |
| Kelly's Plain | Enriched | Raw | 18 | 35 | <10 | <10 | 56 | 26 | 23 | 15 | 6 | 207 | 53 | |
| | | Settling | 7 | 7 | <2 | 5 | 39 | 7.5 | 18 | 3.5 | 2.1 | 61 | 19 | |
| | | Filtered | 0.2 | <0.4 | 0.6 | <0.5 | 3.5 | 0.6 | 4.2 | <0.1 | 0.1 | 3.0 | 1.0 | |
| Felsic | Baseline | Raw | 13 | 5 | 4 | 3 | 54 | 7 | 113 | 8.6 | 1.7 | 109 | 21 | |
| | | Settling | 4 | <2 | 3 | 4 | 21 | 3.0 | 82 | 2.4 | 0.9 | 37 | 8 | |
| | | Filtered | <0.2 | <0.4 | 1.8 | 0.5 | 2.6 | 0.4 | 42.2 | <0.1 | <0.1 | 8.7 | <0.5 | |
| | Enriched | Raw | 22 | 15 | 12 | <10 | 33 | 74 | 101 | 21 | 6 | 410 | 66 | |
| | | Settling | 8 | 8 | 6 | 4 | 45 | 22.6 | 123 | 5.5 | 3.8 | 157 | 26 | |
| | | Filtered | <0.2 | <0.4 | 5.9 | <0.5 | 3.8 | 0.6 | 19.4 | <0.1 | 0.4 | 10.4 | 6.2 | |
| | | | Min | <0.2 | <0.4 | 0.6 | <0.5 | 1.1 | <0.1 | 2.5 | <0.1 | <0.1 | 3.0 | <0.5 |
| | | | Max | 111 | 137 | 33 | 33 | 56 | 74 | 123 | 32 | 7 | 410 | 428 |
| | | | 95% GV ^a | 11 | 3.4 | - | 11 | - | - | - | - | - | - | 8 |
| | | 99% GV ^a | 8 | 1 | - | 5 | - | - | - | - | - | - | 2.4 | |

<http://www.waterquality.gov.au/anz-guidelines/guideline-values/default/water-quality-toxicants/>

^a GV guideline value represents the 95% (95% GV) and 99% (99% GV) species protection guideline values for freshwater. Values highlighted in red and blue is where default guideline value is exceeded. Values for arsenic are for As(V), chromium are for Cr(VI), and tin are for inorganic tin

3.5 Toxicity of leachates of excavated rock to macroinvertebrates

3.5.1 Leachate toxicity to the water flea (*Ceriodaphnia dubia*)

Acute toxicity

Results on acute toxicity of raw (Scenario 1), 12-day settled (Scenario 2), and filtered (Scenario 3) leachates of excavated rock to water fleas over 48 h exposure are given below:

- Reservoir water samples (Tantangara Reservoir from three locations; Talbingo Reservoir from three locations, and pooled reservoir water samples) and QA control treatments exhibited >95% survival of water fleas over 48-h exposures, and thus did not exhibit any adverse effects (Appendix D, Table D3 and Table D4).
- Toxicity tests with water fleas are generally carried out in waters with higher EC and the low EC of the reservoir water may affect the survival of waterfleas during 48-h acute exposures. Acute toxicity testing using dilutions of moderately hard water (MHW) at EC between 30-300 $\mu\text{S}/\text{cm}$ did not demonstrate significant mortality in the exposed water flea (*C. dubia*, Appendix D, Table D5).
- Water fleas exhibited 100% mortality during 48-h exposures to all 1:10 raw leachates of Baseline and Enriched excavated rock samples, except the Baseline Volcanics sample (70% mortality (Figure 5);
- Raw leachates (Scenario 1) demonstrated very high turbidity. Values were 427-774 NTU in 1:10 Enriched leachates from Peppercorn, Volcanics and Shaw Gabbo zones. Higher turbidities (666-837 NTU) were present in 1:100 leachates for Byron, Felsic, Kelly Plains and Ravine zones.
- 12-day settled leachates (Scenario 2) from Byron, Volcanics and Felsics exhibited toxicity to water fleas with turbidity of 570, 61 and 153, respectively (Table 15). All Enriched 12-day settled leachates did not exhibit toxicity to waterfleas and the measured turbidity in these samples varied between 2-200 NTU.
- All filtered leachate samples (1:10) of Baseline and Enriched excavated rock samples (Scenario 3) showed >90% survival in water fleas (Figure 5) and the turbidity all filtered leachates varied between 0.5-6 NTU (Table 15).
- Acute toxicity to water fleas was completely removed after filtration of raw leachates. This confirms that the high content of the suspended sediments in the raw leachates was the major contributor to the high mortality observed in water fleas during 48 h exposures.
- There were no clear trends between the dissolved metal concentrations in the leachates and the toxicity observed.

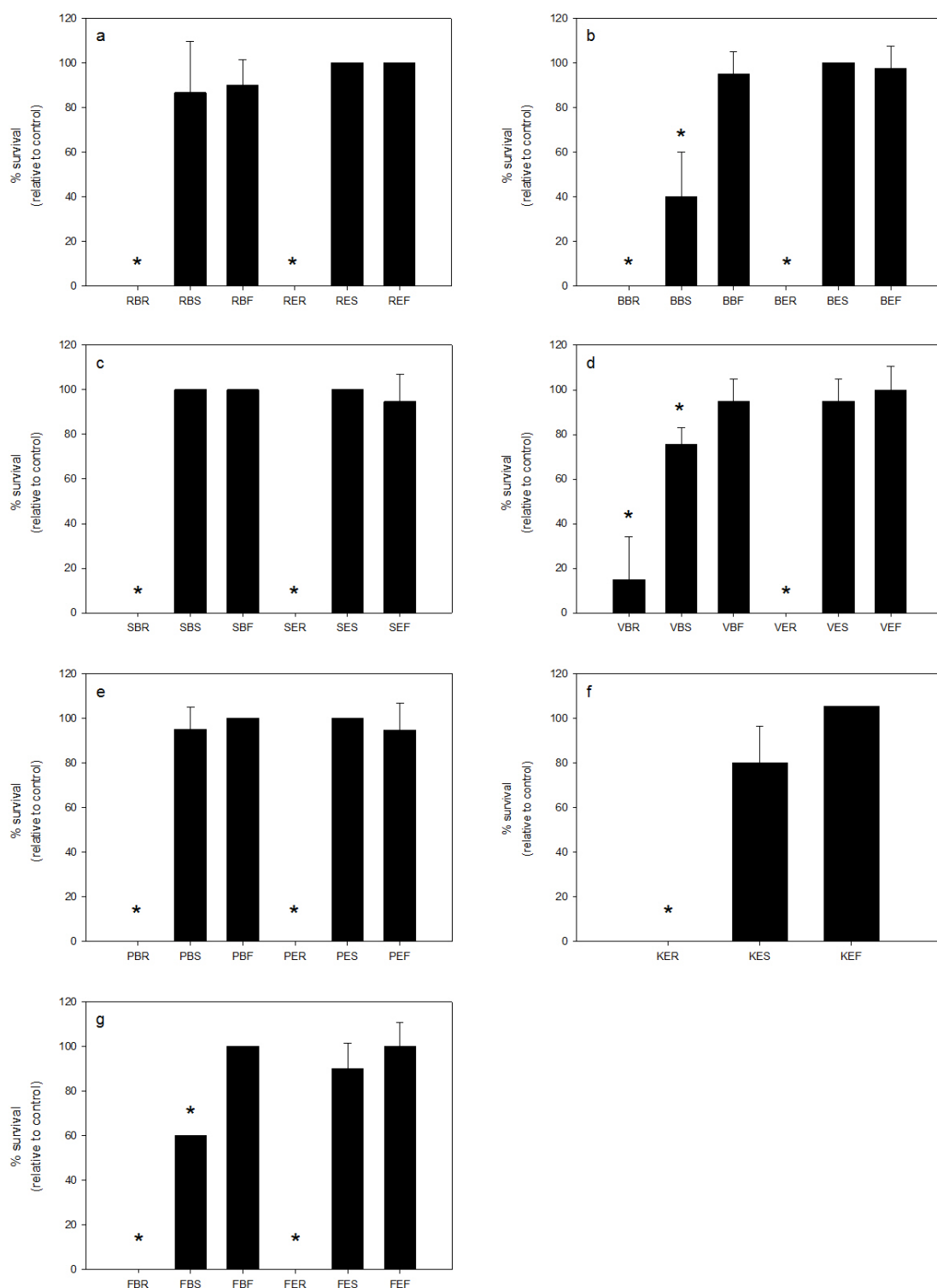


Figure 5. Acute toxicity of leachates of excavated rock to water fleas *Ceriodaphnia dubia* (48-h immobilisation/survival). Data expressed as percent survival. Geological units are (a) Ravine, (b) Byron, (c) Shaw Gabbro, (d) Volcanics, (e) Peppercorn, (f) Kellys Plain and (g) Felsic. The x-axis labels consist of three letters; first letter represents the geological zone R, B, S, V, P, K and F respectively; second letter represents Baseline (B) or Enriched (E) excavated rock; third letter represents raw (R), after 24 h settling (S) and filtered (F) fraction of leachate. Error bars represent 1 standard deviation. * indicates treatment is significant different to the control treatment ($p \leq 0.05$).

Acute toxicity of Byron baseline leachates to water fleas

A preliminary toxicity assessment of the dilutions of raw leachate (after 24 h settling) from a Byron Baseline sample was conducted. The toxicity was expressed as the dilution series of the leachate (1:10) and also expressed as turbidity. A 12.5% dilution of the leachate, corresponding to 1640 NTU, exhibited toxicity to water fleas with only 50% survival during 48-h exposures (Figure 6 and Figure 7). The undiluted raw leachate (100%) and its 50 % dilution (representing 6400 and 20,608 NTU turbidity, respectively) resulted in 100% mortality of waterfleas during 48 h exposures (Figures 6 and 7).

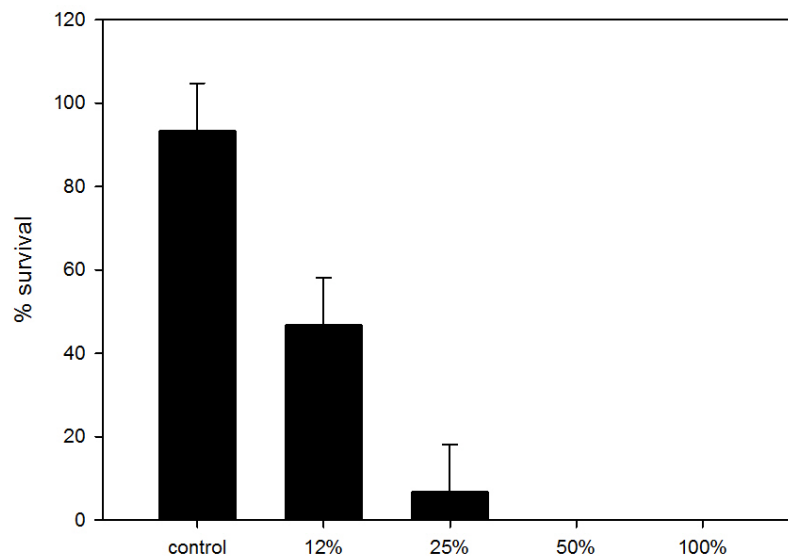


Figure 6. Acute toxicity (48 h) response of the raw leachate for Byron Baseline excavated rock, controls represent reservoir water (n=20/treatment). 50 and 100% treatments resulted in 100% mortality of exposed waterfleas.

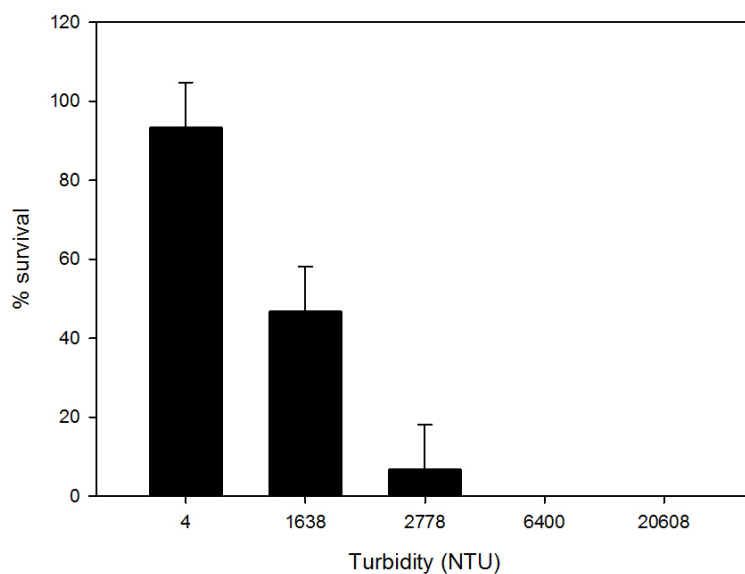


Figure 7. Acute toxicity (48 h) response of the Byron Baseline excavated rock leachate dilutions expressed as turbidity units. 3.8 NTU represents turbidity of reservoir water. 6400 and 20608 NTU resulted in 100% mortality of exposed waterfleas.

Chronic toxicity to water fleas

Chronic toxicity assessment to water fleas was conducted using 0.45 µm filtered Enriched samples only. The tests conducted were based on survival and reproduction endpoints. The undiluted filtered leachate (100%) from Kelly's Plain Enriched excavated rock sample exhibited a significant effect on reproduction success of water fleas, with the number of neonates produced in three broods over 8 days (Mean 9.6 ± 4.7 ; $n=10$) suppressed in comparison to the control treatment (Mean: 16.3 ± 2.1 , $n=10$; Figure 8; Appendix D). In addition, 20% water flea mortality was exhibited in Volcanics undiluted filtered leachate and 10% in both Kelly's Plain and Ravine undiluted filtered samples but these effects were non-significant. The undiluted filtered leachates representing Ravine, Byron, Shaw Gabbro, Volcanics, Peppercorn and Felsic zones did not exhibit any chronic toxicity to waterfleas during 8-day exposure.

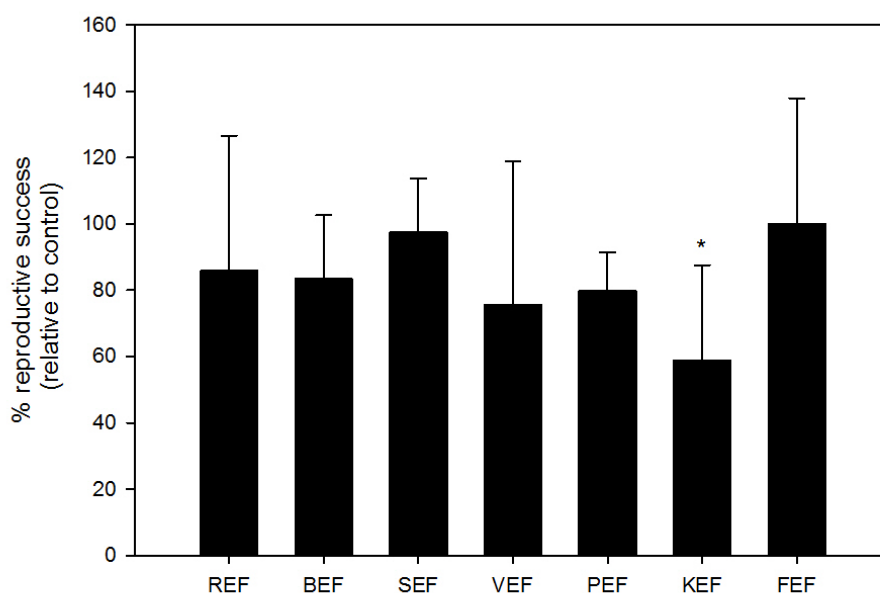


Figure 8.. Chronic toxicity of leachates of excavated rock material to the water flea *Ceriodaphnia dubia* (8-d reproduction). Data expressed as relative to reservoir water control (as a percentage of the reservoir water control). Geological units are (a), (b) Byron, (c) Shaw Gabbro, (d) Volcanics, (e) Peppercorn, (f) Kellys Plain and (g) Felsic. The x-axis labels consist of three letters; first letter represents the geological zone Ravine (R), Byron (B), Shaw Gabbro (S), Volcanics (V), Peppercorn (P), Kellys Plain (K) and Felsic (F); second letter represents Enriched (E) excavated rock material; third letter represents the filtered (F) fraction of leachate tested. Error bars represent 1 standard deviation, $n=10$ per treatment. * indicates treatment is significant different to the control treatment ($p \leq 0.05$).

3.5.2 Leachate toxicity to midge larvae

- Water from Tantangara Reservoir (three locations) and Talbingo Reservoir (three locations) did not exhibit acute toxicity to midge larvae over 48 h exposures (Appendix E, Table E3).
- Toxicity tests with midge are generally carried out in waters with higher EC (~ 270-320 $\mu\text{S}/\text{cm}$) and the low EC of the reservoir water may have affected the survival of midge larvae during 48-h acute exposures. Acute toxicity testing using dilutions of MHW at EC between 30-300 $\mu\text{S}/\text{cm}$ and sodium chloride (125-2000mg/L) did not demonstrate significant mortality in the exposed midge larvae (*C. tepperi*, Appendix E, Table E4 and Table E5). This confirmed the use of reservoir water as controls for leachate testing.
- Baseline raw leachates (1:10) did not indicate toxicity to midge larvae during 48-h acute exposures (Figure 9) with turbidity measured in the range of (Table ---)
- Midge larvae exhibited significant toxicity to raw Enriched leachates from Byron, Ravine, Shaw and Volcanics during 48-h exposures (Figure 9) with turbidity of 4390, 7810, 1750 and 436 NTU, respectively (Table 15).
- Further midge testing using Enriched 12-day settled leachates showed toxicity only in Kelly's Plain Enriched sample with turbidity of 196 NTU.
- There were no clear trends between the turbidity and dissolved metal concentrations in the leachates and the toxicity observed in the midge larvae.

3.5.3 Leachate toxicity to blackworms

- Water from Tantangara Reservoir (three locations) and Talbingo Reservoir (three locations) did not exhibit toxicity to blackworms (Appendix F, Table F3).
- Toxicity tests with blackworms are generally carried out in waters with higher EC and the low EC of the reservoir water may have affected the survival of blackworms during 48-h acute exposures. Acute toxicity testing using dilutions of moderately hard water (MHW) at EC between 30-300 $\mu\text{S}/\text{cm}$ did not demonstrate significant mortality in the exposed midge larvae (*L. variegatus*, Appendix F, Table F4).
- Blackworms exhibited no acute toxicity (with 100% survival) when exposed to Baseline and Enriched raw leachates (1:10) under Scenario 1. (Figure 10).
- No further toxicity testing was conducted with 12-day settled and filtered leachates representing Scenarios 2 and 3.

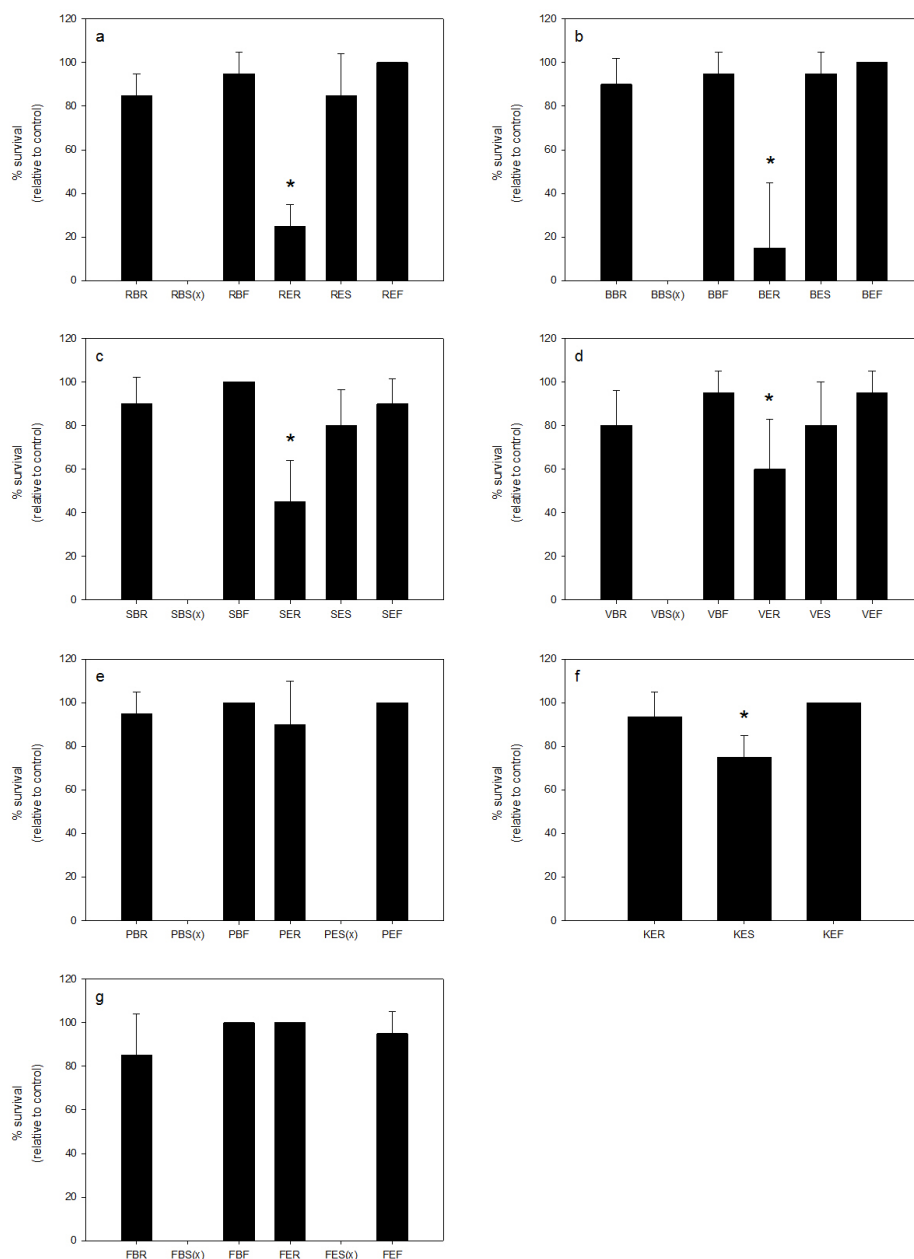


Figure 9. Acute toxicity of leachates of excavated rock to the midge *Chironomus tepperi* (48-h survival). Data expressed as percent survival. Geological units are (a) Ravine, (b) Byron, (c) Shaw Gabbro, (d) Volcanics, (e) Peppercorn, (f) Kellys Plain and (g) Felsic. The x-axis labels consist of three letters; first letter represents the geological zone R, B, S, V, P, K and F respectively; second letter represents Baseline (B) or Enriched (E) excavated rock; third letter represents raw (R), after 24 h settling (S) and filtered (F) fraction of leachates. Error bars represent 1 standard deviation. * indicates treatment is significant different to the control treatment ($p \leq 0.05$).

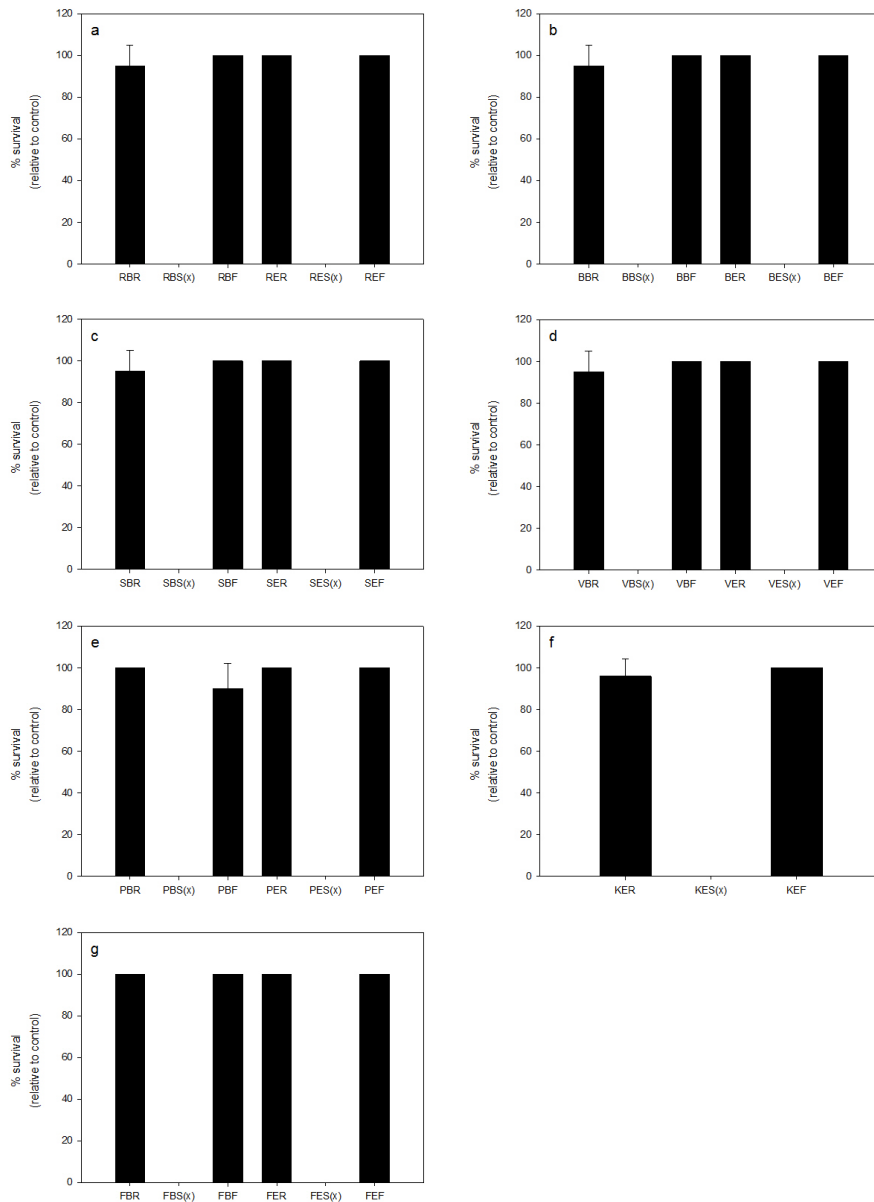


Figure 10. Acute toxicity of leachates of excavated rock to blackworm *Lumbriculus variegatus* (48-h survival). Data expressed as percent survival. Geological units are (a) Ravine, (b) Byron, (c) Shaw Gabbro, (d) Volcanics, (e) Peppercorn, (f) Kellys Plain and (g) Felsic. The x-axis labels consist of three letters; first letter represents the geological zone R, B, S, V, P, K and F respectively; second letter represents Baseline (B) or Enriched (E) excavated rock; third letter represents raw (R) and filtered (F) fraction of leachate. Error bars represent 1 standard deviation. * indicates treatment is significant different to the control treatment ($p \leq 0.05$).

3.6 Characterisation of reservoir sediments used for determining toxicity to macroinvertebrates

The total nitrogen, phosphorus, inorganic and organic carbon in the benthic reservoir sediments are shown in Table 18. Spatial variation of sediment quality was evident. For Talbingo Reservoir, the Ravine Bay sites had lower concentrations of many parameters than the Cascade Bay and Plain Creek Bay sites. The Tantangara Reservoir sediments had similar or higher concentrations of each parameter than those in Talbingo Reservoir, with concentrations of varying approximately two-fold between the different sites in the two reservoirs. There were generally higher concentrations of Sb, Ca, Cr, Cu, Fe, K, Mg, Mn, Ni, Na, Sr, Sn, Ti, and U in the Talbingo sediments and a higher concentration of sulphur in the Tantangara sediments (Table 18).

These concentrations reflect the background surface sediment concentrations with the concentrations of nickel exceeding the corresponding sediment quality guideline value (SQGV) (Simpson et al., 2013; ANZG, 2018), which some consider an overly conservative value (Vangheluwe et al., 2013; Simpson and Batley, 2016).

A significant portion of the total element concentration (extracted using concentrated acids) may release inert (not easily released) fractions of metals of very low bioavailability. For most metals, the 'maximum bioavailable concentration' can be determined by dilute-acid-extractable metal (AEM) analyses, as commonly achieved by extracting the solid in 1-M hydrochloric acid for 1 h (Simpson and Batley, 2016). AEM data can also be useful for interpreting the partitioning of elements between the dissolved and particulate phases, and the availability of reactive binding phases.

There was generally little variation in the dilute-acid-extractable concentrations of metal, metalloid, and other major ions between the different sites in Talbingo Reservoir (Table 19). No concentrations of dilute-acid-extractable metals, metalloids and major cations exceeded their respective SQGVs.

Table 18. Concentrations of carbon, nitrogen, total recoverable metals, metalloids and other elements in reservoir sediments

| Sample | C (Total) | N (Total) | Ca | K | Mg | Na | S | P | Al | As | B | Cd |
|-------------------------|--------------|--------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|------------|------------|
| Reservoir sediments | % | % | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg |
| PL1 | 5.7 | 0.50 | 1500 | 4200 | 4700 | 120 | 440 | 1100 | 42000 | 9 | 5 | <4 |
| PL2 | 5.6 | 0.41 | 1700 | 4700 | 4900 | 130 | 450 | 1100 | 46000 | 9 | 6 | <4 |
| RPL1 | 3.9 | 0.29 | 1300 | 4200 | 4500 | 90 | 260 | 620 | 31000 | 6 | 5 | <4 |
| RPL2 | 3.8 | 0.27 | 1300 | 4500 | 4600 | 90 | 270 | 630 | 33000 | 6 | 7 | <4 |
| TN1 | 5.8 | 0.48 | 600 | 4500 | 2900 | 110 | 650 | 1200 | 47000 | 6 | 6 | <4 |
| TN2 | 5.8 | 0.53 | 600 | 4500 | 3000 | 110 | 660 | 1200 | 47000 | 6 | 5 | <4 |
| RA1 | 4.1 | 0.34 | 1300 | 4900 | 5500 | 110 | 350 | 930 | 41000 | 11 | 7 | <4 |
| RA2 | 4.0 | 0.34 | 1300 | 5300 | 5600 | 120 | 350 | 920 | 43000 | 10 | 8 | <4 |
| PL-TN & RA1 | 4.9 | 0.42 | 1200 | 4900 | 4600 | 120 | 460 | 1000 | 44000 | 9 | 7 | <4 |
| PL-TN & RA2 | 5.0 | 0.43 | 1000 | 3900 | 4000 | 110 | 450 | 1000 | 38000 | 9 | 4 | <4 |
| Min | 3.8 | 0 | 600 | 3900 | 2900 | 90 | 260 | 620 | 31000 | 6 | 4 | <4 |
| Max | 5.8 | 1 | 1700 | 5300 | 5600 | 130 | 660 | 1200 | 47000 | 11 | 8 | <4 |
| SQGV^a | NA | NA | NA | NA | NA | NA | NA | NA | NA | 20 | NA | 1.5 |
| Sample | Co | Cr | Cu | Fe | Mn | Mo | Ni | Pb | Sb | Se | Zn | |
| Reservoir sediments | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | |
| PL1 | 27 | 66 | 46 | 47000 | 1900 | <4 | 56 | 15 | <8 | <4 | 85 | |
| PL2 | 28 | 70 | 47 | 50000 | 1900 | <4 | 57 | 16 | <8 | <4 | 89 | |
| RPL1 | 14 | 44 | 31 | 28000 | 900 | <4 | 38 | 17 | <8 | <4 | 80 | |
| RPL2 | 14 | 46 | 32 | 28000 | 910 | <4 | 38 | 18 | <8 | <4 | 81 | |
| TN1 | 19 | 39 | 27 | 37000 | 660 | <4 | 21 | 20 | <8 | <4 | 99 | |
| TN2 | 20 | 39 | 28 | 38000 | 670 | <4 | 22 | 21 | <8 | <4 | 100 | |
| RA1 | 21 | 57 | 46 | 40000 | 2400 | <4 | 51 | 20 | <8 | <4 | 95 | |
| RA2 | 21 | 58 | 46 | 41000 | 2400 | <4 | 52 | 21 | <8 | <4 | 96 | |
| PL-TN & RA1 | 22 | 55 | 42 | 42000 | 1800 | <4 | 45 | 19 | <8 | <4 | 95 | |
| PL-TN & RA2 | 21 | 51 | 40 | 39000 | 1700 | <4 | 42 | 19 | <8 | <4 | 90 | |
| Min | 14 | 39 | 27 | 28000 | 660 | <4 | 21 | 15 | <8 | <4 | 80 | |
| Max | 28 | 70 | 47 | 50000 | 2400 | <4 | 57 | 21 | <8 | <4 | 100 | |
| SQGV^a | NA | 80 | 65 | NA | NA | NA | 21 | 50 | NA | NA | 200 | |

Table 19. Concentrations of dilute acid-extractable metals, metalloids and other elements in reservoir sediments

| Sample | Ca | K | Mg | Na | S | P | Al | As | B | Cd |
|---------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Reservoir sediments | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg |
| PL1 | 1200 | 290 | 390 | 46 | 70 | 670 | 4300 | 4 | <3 | <3 |
| PL2 | 1100 | 300 | 400 | 36 | 65 | 660 | 4300 | 4 | <3 | <3 |
| RPL1 | 1200 | 300 | 250 | 21 | 43 | 320 | 2600 | <3 | <3 | <3 |
| RPL2 | 1200 | 300 | 250 | 23 | 44 | 330 | 2600 | <3 | <3 | <3 |
| TN1 | 600 | 190 | 170 | 23 | 110 | 760 | 4100 | <3 | <3 | <3 |
| TN2 | 610 | 190 | 180 | 26 | 110 | 770 | 4200 | <3 | <3 | <3 |
| RA1 | 1400 | 220 | 250 | 25 | 37 | 560 | 3500 | 4 | <3 | <3 |
| RA2 | 1400 | 220 | 240 | 22 | 36 | 550 | 3500 | 5 | <3 | <3 |
| PL-TN &RA1 | 1100 | 220 | 270 | 25 | 61 | 640 | 3900 | 4 | <3 | <3 |
| PL-TN &RA2 | 1100 | 230 | 280 | 30 | 65 | 660 | 4000 | 4 | <3 | <3 |
| Min | 600 | 190 | 170 | 21 | 36 | 320 | 2600 | <3 | <3 | <3 |
| Max | 1400 | 300 | 400 | 46 | 110 | 770 | 4300 | 5 | <3 | <3 |
| SQGV ^a | NA | NA | NA | NA | NA | NA | NA | 20 | NA | 1.5 |

| Sample | Co | Cr | Cu | Fe | Mn | Mo | Ni | Pb | Sb | Se | Zn |
|---------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Reservoir sediments | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg |
| PL1 | 15 | 6 | 24 | 23000 | 1800 | 29 | 8 | 13 | <6 | <3 | 33 |
| PL2 | 15 | 6 | 24 | 23000 | 1800 | <3 | 8 | 13 | <6 | <3 | 64 |
| RPL1 | 6 | <3 | 17 | 7700 | 770 | <3 | 4 | 15 | <6 | <3 | 50 |
| RPL2 | 6 | <3 | 17 | 8100 | 770 | <3 | 4 | 15 | <6 | <3 | 46 |
| TN1 | 14 | 5 | 15 | 21000 | 610 | <3 | 4 | 14 | <6 | <3 | 68 |
| TN2 | 14 | 5 | 15 | 21000 | 620 | <3 | 4 | 14 | <6 | <3 | 69 |
| RA1 | 11 | 5 | 26 | 17000 | 2300 | <3 | 7 | 18 | <6 | <3 | 48 |
| RA2 | 11 | 5 | 26 | 16000 | 2300 | <3 | 7 | 18 | <6 | <3 | 47 |
| PL-TN &RA1 | 13 | 5 | 23 | 19000 | 1800 | <3 | 6 | 16 | <6 | <3 | 52 |
| PL-TN &RA2 | 13 | 5 | 23 | 20000 | 1700 | <3 | 7 | 15 | <6 | <3 | 52 |
| Min | 6 | 5 | 15 | 7700 | 610 | <3 | 4 | 13 | <6 | <3 | 33 |
| Max | 15 | 6 | 26 | 23000 | 2300 | 29 | 8 | 18 | <6 | <3 | 69 |
| SQGV ^a | NA | 80 | 65 | NA | NA | NA | 21 | 50 | NA | NA | 200 |

^a SQGV: The sediment quality guideline values (Simpson et al., 2013). Values highlighted in red is where default guideline value exceeded. NA-not available. For cadmium, the detection limit was higher than the sediment quality guideline value. However the concentrations were expected to be below the sediment quality guideline value based on cadmium concentrations reported in Simpson et al. (2019) (excavated rock material ≤1 mg/kg and reservoir water sediments ≤0.27 mg/kg)

3.7 Characterisation of excavated rocks used for sediment toxicity assessment

The total recoverable metal, metalloid, and major cation concentrations measured in the milled rock composites are shown in Table 20. The concentrations of all metals were below the corresponding SQGVs.

The AEM concentrations (see Section 3.6) of metals, metalloids and major cations measured in the milled rock composites are shown in Table 21. The concentrations of each parameter were all below their respective SQGVs.

Table 20. Concentrations of total recoverable metals, metalloids and other elements excavated rock material

| Sample | C (Total) | N (Total) | Ca | K | Mg | Na | S | P | Al | As | B | Cd |
|-------------------------|--------------|--------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|------------|------------|
| Excavated rock | % | % | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/K g |
| Ravine Baseline | 0.38 | 0.04 | 6600 | 4400 | 18000 | 160 | 90 | 520 | 26000 | 8 | 9 | <4 |
| Ravine Enriched | 0.28 | 0.04 | 5500 | 5500 | 20000 | 130 | 790 | 610 | 32000 | 7 | 10 | <4 |
| Byron Baseline | 0.25 | 0.12 | 5600 | 9200 | 4400 | 200 | 130 | 340 | 24000 | <4 | 12 | <4 |
| Byron Enriched | 0.35 | 0.03 | 8600 | 8400 | 6900 | 170 | 3900 | 520 | 25000 | 11 | 13 | <4 |
| Shaw Gabbro Baseline | 0.60 | 0.03 | 37000 | 2500 | 22000 | 430 | <16 | 340 | 38000 | <4 | <4 | <4 |
| Shaw Gabbro Enriched | 0.16 | 0.02 | 14000 | 1400 | 10000 | 240 | <16 | 380 | 21000 | <4 | <4 | <4 |
| Volcanics Baseline | 0.36 | 0.04 | 12000 | 5300 | 7000 | 560 | <16 | 460 | 23000 | <4 | <4 | <4 |
| Volcanics Enriched | 0.46 | 0.02 | 15000 | 2800 | 6800 | 210 | 5800 | 1100 | 20000 | 63 | <4 | <4 |
| Peppercorn Baseline | 0.21 | 0.00 | 6400 | 3000 | 6000 | 190 | 150 | 500 | 14000 | <4 | <4 | <4 |
| Peppercorn Enriched | 0.21 | 0.01 | 13000 | 4100 | 10000 | 350 | 3400 | 750 | 27000 | 7 | 5 | <4 |
| Kelly's Plain Enriched | 0.21 | 0.01 | 1500 | 3700 | 8100 | 190 | 650 | 360 | 17000 | 5 | <4 | <4 |
| Felsics Baseline | 0.86 | 0.04 | 26000 | 5000 | 11000 | 160 | <16 | 430 | 22000 | <4 | 6 | <4 |
| Felsics Enriched | 0.17 | 0.03 | 9600 | 10000 | 6600 | 130 | 610 | 470 | 27000 | 6 | 12 | <4 |
| Min | 0.2 | 0.00 | 1500 | 1400 | 4400 | 130 | <16 | 340 | 14000 | <4 | <4 | <4 |
| Max | 0.9 | 0.12 | 37000 | 10000 | 22000 | 560 | 5800 | 1100 | 38000 | 63 | 13 | <4 |
| SQGV^a | NA | NA | NA | NA | NA | NA | NA | NA | NA | 20 | NA | 1.5 |
| Sample | Co | Cr | Cu | Fe | Mn | Mo | Ni | Pb | Sb | Se | Zn | |
| Excavated rock | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | |
| Ravine Baseline | 19 | 83 | 32 | 45000 | 750 | <4 | 96 | 7 | <8 | <4 | 90 | |
| Ravine Enriched | 19 | 110 | 33 | 52000 | 1100 | <4 | 116 | 410 | <8 | <4 | 550 | |
| Byron Baseline | 4 | 20 | 7 | 20000 | 290 | <4 | 14 | <4 | <8 | <4 | 21 | |
| Byron Enriched | 9 | 48 | 14 | 34000 | 380 | <4 | 28 | 5 | <8 | <4 | 28 | |
| Shaw Gabbro Baseline | 24 | 160 | 59 | 42000 | 660 | <4 | 40 | <4 | <8 | <4 | 42 | |
| Shaw Gabbro Enriched | 12 | 44 | 23 | 27000 | 520 | <4 | 19 | 6 | <8 | <4 | 47 | |
| Volcanics Baseline | 8 | 14 | 15 | 22000 | 490 | <4 | 9 | 17 | <8 | <4 | 39 | |
| Volcanics Enriched | 17 | 6 | 110 | 47000 | 430 | <4 | 10 | 7 | <8 | <4 | 79 | |
| Peppercorn Baseline | 6 | 20 | 5 | 19000 | 340 | <4 | 13 | <4 | <8 | <4 | 19 | |
| Peppercorn Enriched | 15 | 43 | 270 | 49000 | 700 | <4 | 25 | 6 | <8 | <4 | 76 | |
| Kelly's Plain Enriched | 8 | 26 | 13 | 29000 | 310 | <4 | 14 | 9 | <8 | <4 | 56 | |
| Felsics Baseline | 9 | 52 | 7 | 34000 | 740 | <4 | 18 | <4 | <8 | <4 | 31 | |
| Felsics Enriched | 6 | 21 | 82 | 21000 | 250 | <4 | 10 | 8 | <8 | <4 | 27 | |
| Min | 4 | 6 | 5 | 19000 | 250 | <4 | 9 | <4 | <8 | <4 | 19 | |
| Max | 24 | 160 | 270 | 52000 | 1100 | <4 | 116 | 410 | <8 | <4 | 550 | |
| SQGV^a | NA | 80 | 65 | NA | NA | NA | 21 | 50 | NA | NA | 200 | |

^a SQGV: The sediment quality guideline values (Simpson et al., 2013). Values highlighted in red is where default guideline value exceeded. .N A-not available. For cadmium, the detection limit was higher than the sediment quality guideline value. However the concentrations were expected to be below the sediment quality guideline value based on cadmium concentrations reported in Simpson et al. (2019) (excavated rock material ≤1 mg/kg and reservoir water sediments ≤0.27 mg/kg)

Table 21. Concentrations of dilute acid-extractable metals, metalloids and other elements in excavated rock material

| Sample | Ca | K | Mg | Na | S | P | Al | As | B | Cd |
|------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Excavated rock | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg |
| Ravine Baseline | 5700 | 470 | 2300 | 83 | <12 | 500 | 1100 | <3 | <3 | <3 |
| Ravine Enriched | 7100 | 410 | 1900 | 47 | 130 | 580 | 1200 | <3 | <3 | <3 |
| Byron Baseline | 6900 | 1300 | 780 | 81 | <12 | 360 | 1900 | <3 | <3 | <3 |
| Byron Enriched | 8700 | 1400 | 1200 | 79 | 22 | 570 | 2000 | <3 | <3 | <3 |
| Shaw Gabbro Baseline | 18000 | 2000 | 3400 | 180 | <12 | 380 | 3400 | <3 | <3 | <3 |
| Shaw Gabbro Enriched | 6200 | 250 | 530 | 94 | <12 | 450 | 900 | <3 | <3 | <3 |
| Volcanics Baseline | 11000 | 790 | 610 | 140 | <12 | 510 | 1700 | <3 | <3 | <3 |
| Volcanics Enriched | 18000 | 350 | 640 | 76 | 33 | 1200 | 1300 | <3 | <3 | <3 |
| Peppercorn Baseline | 6000 | 320 | 890 | 81 | <12 | 530 | 670 | <3 | <3 | <3 |
| Peppercorn Enriched | 7800 | 500 | 1100 | 110 | 380 | 790 | 1600 | <3 | <3 | <3 |
| Kelly's Plain Enriched | 2000 | 370 | 1000 | 66 | 17 | 390 | 720 | <3 | <3 | <3 |
| Felsics Baseline | 23000 | 500 | 920 | 92 | <12 | 440 | 870 | <3 | <3 | <3 |
| Felsics Enriched | 10000 | 1100 | 510 | 61 | <12 | 480 | 1100 | <3 | <3 | <3 |
| Min | 2000 | 250 | 510 | 47 | <12 | 360 | 670 | <3 | <3 | <3 |
| Max | 23000 | 2000 | 3400 | 180 | 380 | 1200 | 3400 | <3 | <3 | <3 |
| SQGV ^a | NA | NA | NA | NA | NA | NA | NA | 20 | NA | 1.5 |

| Sample | Co | Cr | Cu | Fe | Mn | Mo | Ni | Pb | Sb | Se | Zn |
|------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Excavated rock | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg |
| Ravine Baseline | <3 | 3 | <3 | 5100 | 370 | <3 | 5 | 6 | <6 | <3 | 15 |
| Ravine Enriched | <3 | 4 | <3 | 3700 | 350 | <3 | 5 | 190 | <6 | <3 | 45 |
| Byron Baseline | <3 | <3 | <3 | 4700 | 190 | <3 | 3 | <3 | <6 | <3 | 7 |
| Byron Enriched | <3 | 4 | <3 | 6300 | 270 | <3 | 3 | 4 | <6 | <3 | 7 |
| Shaw Gabbro Baseline | 4 | 22 | 23 | 5400 | 200 | <3 | 8 | <3 | <6 | <3 | 11 |
| Shaw Gabbro Enriched | <3 | <3 | 6 | 1900 | 69 | <3 | <3 | <3 | <6 | <3 | 6 |
| Volcanics Baseline | <3 | <3 | 6 | 2200 | 240 | <3 | <3 | 12 | <6 | <3 | 6 |
| Volcanics Enriched | <3 | <3 | 4 | 3300 | 150 | <3 | <3 | 5 | <6 | <3 | 11 |
| Peppercorn Baseline | <3 | <3 | <3 | 2300 | 120 | <3 | <3 | <3 | <6 | <3 | 4 |
| Peppercorn Enriched | <3 | 6 | 10 | 4400 | 100 | <3 | <3 | 7 | <6 | <3 | 14 |
| Kelly's Plain Enriched | <3 | <3 | <3 | 6600 | 120 | <3 | <3 | 7 | <6 | <3 | 16 |
| Felsics Baseline | <3 | <3 | <3 | 3100 | 610 | <3 | <3 | <3 | <6 | <3 | 4 |
| Felsics Enriched | <3 | <3 | 3 | 2300 | 190 | <3 | <3 | 5 | <6 | <3 | 4 |
| Min | <3 | <3 | <3 | 1900 | 69 | <3 | <3 | <3 | <6 | <3 | 4 |
| Max | 4 | 22 | 23 | 6600 | 610 | <3 | 8 | 190 | <6 | <3 | 45 |
| SQGV ^a | NA | 80 | 65 | NA | NA | NA | 21 | 50 | NA | NA | 200 |

^a SQGV: The sediment quality guideline values (Simpson et al., 2013). Values highlighted in red is where default guideline value exceeded. . NA-not available. For cadmium, the detection limit was higher than the sediment quality guideline value. However the concentrations were expected to be below the sediment quality guideline value based on cadmium concentrations reported in Simpson et al. (2019) (excavated rock material ≤1 mg/kg and reservoir water sediments ≤0.27 mg/kg)

3.8 Toxicity of excavated rock and excavated rock-sediment mixtures

3.8.1 Toxicity to midge larvae

Excavated rocks from each geological zone were tested using three scenarios and a control treatment of reservoir sediment was also included with each batch of tests:

- (1) 140 g (wet weight) of 425- μ m sieved sediment with 20 g Excavated rock on top of sediments - both Enriched and Baseline from each zone.
- (2) 140 g sediments and 20 g Excavated rock mixed well - both Enriched and Baseline from each zone.
- (3) 160 g excavated rock material only (Enriched Excavated rock from each zone).

Key results are given below:

- Reservoir sediments (as listed in Table 3) were used as control treatments with each batch of sediment and excavated testing scenarios. Exposure of midge larvae to these control reservoir sediments over 7 days resulted in greater than 90% survival. All experimental data was expressed as % of control response (Figures 11 and 12).
- In general, excavated rock material (both Enriched and Baseline) on top of sediments (Scenario 1) and mixed with sediments (Scenario 2) did not exhibit significant toxicity, with all treatments exhibiting >80% survival.
- Midge larvae showed reduced survival (30-65%) when exposed to Shaw Gabbro, Volcanics and Felsics Enriched excavated rock under Scenario 3. However, midge larvae survival was not affected over 7 days exposure to Enriched Ravine, Byron, Peppercorn and Kellys rock material under Scenario 3 (Figure 11 and Figure 12).
- Growth of midge larvae was not significantly affected in all scenarios of excavated rock and reservoir sediments except for Byron Enriched under Scenario 3 (Figure 11 and Figure 12).
- In the chronic toxicity tests, nickel concentrations (ranging from 28-64 mg/kg) were above the sediments guideline values (SGVs) in all combinations of sediment and excavated rock materials (Table 22). Nickel in the reservoir sediments were below the SGVs as reported in Table 21.

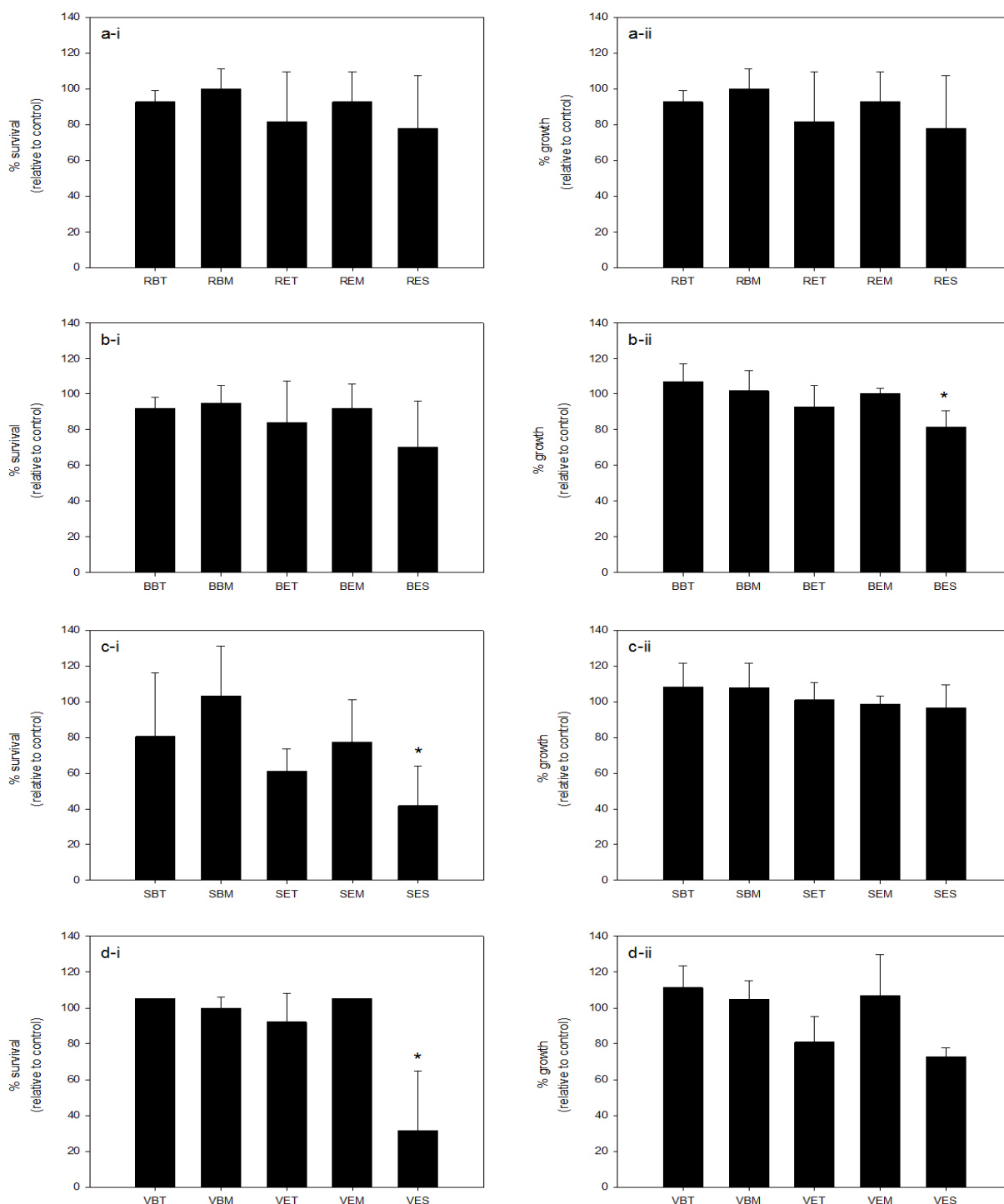


Figure 11. Chronic toxicity of excavated rock and sediment mixtures to the midge *Chironomus tepperi* (7-d survival and growth) Part 1. Data expressed as percent survival. Geological units are (a) Ravine, (b) Byron, (c) Shaw Gabbro, (d) Volcanics with test endpoint of (i) survival and (ii) growth (as length). The x-axis labels consist of three letters; first letter represents the geological zone R, B, S and V respectively; second letter represents Baseline (B) or Enriched (E) excavated rock; third letter represents excavated rock as a surface layer on sediment (T), excavated rock mixed with sediment (M) and excavated rock (S) scenario. Error bars represent 1 standard deviation. * indicates treatment is significantly different to the control treatment ($p \leq 0.05$).

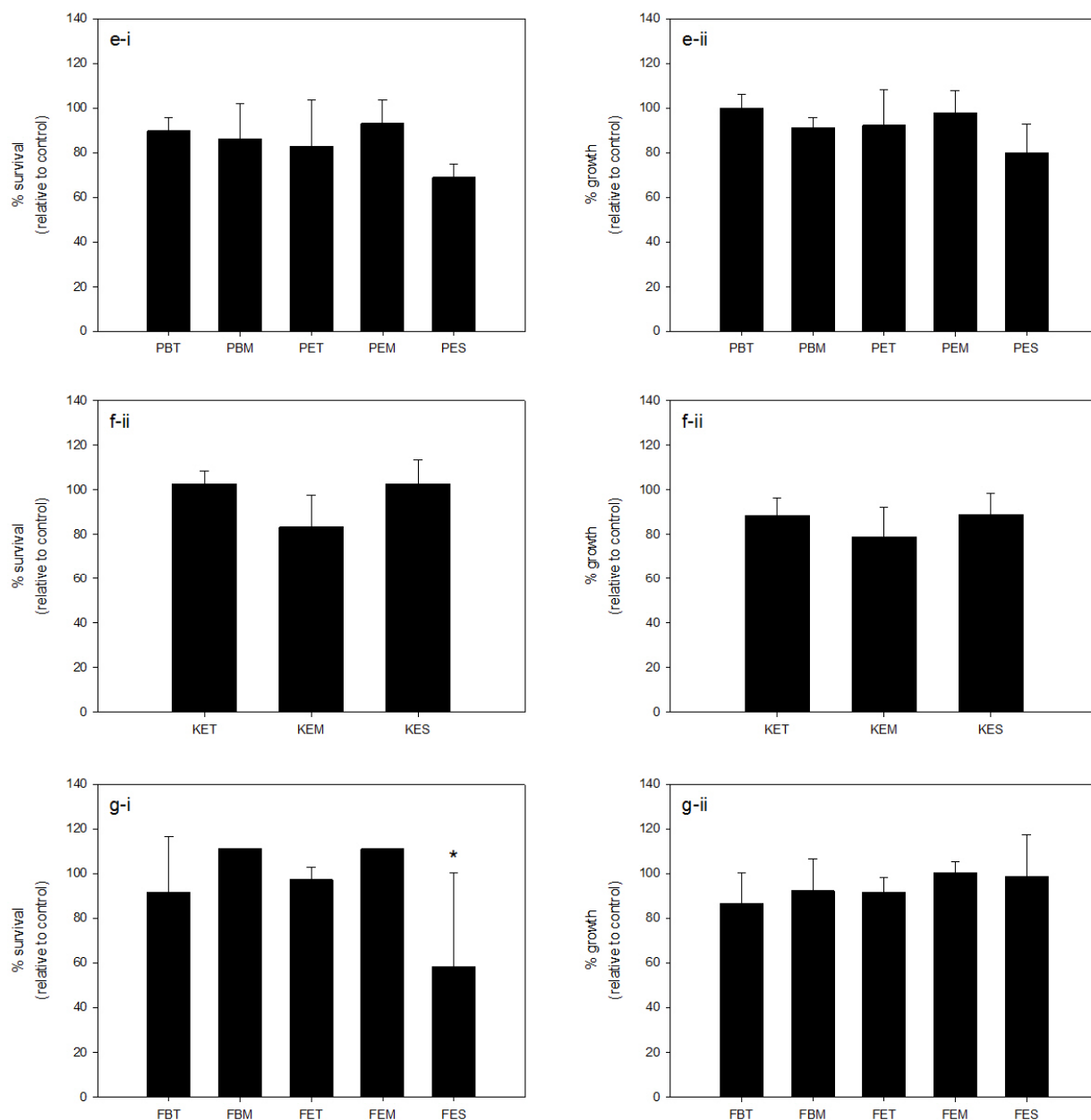


Figure 12. Chronic toxicity of excavated rock and sediment mixtures to the midge *Chironomus tepperi* (7-d survival and growth) Part 2. Data expressed as percent survival. Geological units are (e) Peppercorn, (f) Kellys Plain and (g) Felsic with test endpoint of (i) survival and (ii) growth (as length). The x-axis labels consist of three letters; first letter represents the geological zone P, K, and F respectively; second letter represents Baseline (B) or Enriched (E) excavated rock; third letter represents excavated rock as a surface layer on sediment (T), excavated rock mixed with sediment (M) and excavated rock (S) scenario. Error bars represent 1 standard deviation. * indicates treatment is significant different to the control treatment ($p \leq 0.05$).

Table 22. Concentrations of total recoverable metals, metalloids and other elements excavated rock material in the midge chronic toxicity tests

| Sample | C (Total) | N (Total) | Ca | K | Mg | Na | S | P | Al | As | B | Cd |
|------------------------|-----------|-----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Midge test | % | % | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg |
| Ravine Baseline | 3.1 | 0.16 | 2800 | 2800 | 10000 | 120 | 310 | 830 | 30000 | 9 | <4 | <4 |
| Ravine Enriched | 3.2 | 0.17 | 3500 | 2900 | 7900 | 90 | 540 | 820 | 30000 | 8 | <4 | <4 |
| Byron Baseline | 3.1 | 0.26 | 2800 | 3300 | 4500 | 120 | 330 | 760 | 26000 | 6 | 4 | <4 |
| Byron Enriched | 3.1 | 0.16 | 3400 | 3700 | 5000 | 120 | 1600 | 810 | 26000 | 9 | <4 | <4 |
| Shaw Gabbro Baseline | 3.2 | 0.26 | 16000 | 5500 | 13000 | 290 | 270 | 790 | 47000 | 6 | 7 | <4 |
| Shaw Gabbro Enriched | 3.0 | 0.26 | 5700 | 5300 | 7700 | 220 | 270 | 790 | 41000 | 6 | 7 | <4 |
| Volcanics Baseline | 3.0 | 0.15 | 4800 | 3200 | 6700 | 210 | 280 | 790 | 29000 | 8 | <4 | <4 |
| Volcanics Enriched | 3.3 | 0.16 | 7500 | 2300 | 7100 | 120 | 2200 | 920 | 29000 | 16 | <4 | <4 |
| Peppercorn Baseline | 2.9 | 0.24 | 2800 | 2300 | 4500 | 120 | 330 | 800 | 24000 | 6 | <4 | <4 |
| Peppercorn Enriched | 3.1 | 0.26 | 4000 | 2500 | 5800 | 190 | 1600 | 900 | 28000 | 8 | <4 | <4 |
| Kelly's Plain Enriched | 3.0 | 0.14 | 1200 | 2500 | 5400 | 130 | 500 | 770 | 25000 | 7 | <4 | <4 |
| Felsics Baseline | 3.2 | 0.15 | 8100 | 2900 | 6500 | 110 | 280 | 770 | 27000 | 6 | <4 | <4 |
| Felsics Enriched | 3.1 | 0.16 | 3600 | 9000 | 5400 | 160 | 520 | 820 | 42000 | 7 | 11 | <4 |
| Min | 2.9 | 0.14 | 1200 | 2300 | 4500 | 90 | 270 | 760 | 24000 | 6 | <4 | <4 |
| Max | 3.3 | 0.26 | 16000 | 9000 | 13000 | 290 | 2200 | 920 | 47000 | 16 | 11 | <4 |
| SQGV ^a | NA | NA | NA | NA | NA | NA | NA | NA | NA | 20 | NA | 1.5 |

| Sample | Co | Cr | Cu | Fe | Mn | Mo | Ni | Pb | Sb | Se | Zn |
|------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Midge test | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg |
| Ravine Baseline | 21 | 59 | 38 | 40000 | 1400 | <4 | 64 | 14 | <8 | <4 | 92 |
| Ravine Enriched | 19 | 51 | 39 | 40000 | 1300 | <4 | 52 | 57 | <8 | <4 | 150 |
| Byron Baseline | 15 | 35 | 27 | 32000 | 1200 | <4 | 31 | 12 | <8 | <4 | 63 |
| Byron Enriched | 16 | 43 | 29 | 35000 | 1200 | <4 | 34 | 12 | <8 | <4 | 63 |
| Shaw Gabbro Baseline | 24 | 100 | 48 | 40000 | 1300 | <4 | 42 | 10 | <8 | <4 | 68 |
| Shaw Gabbro Enriched | 18 | 54 | 34 | 34000 | 1200 | <4 | 33 | 13 | <8 | <4 | 71 |
| Volcanics Baseline | 17 | 36 | 30 | 34000 | 1300 | <4 | 30 | 15 | <8 | <4 | 74 |
| Volcanics Enriched | 22 | 31 | 48 | 43000 | 1300 | <4 | 28 | 12 | <8 | <4 | 78 |
| Peppercorn Baseline | 15 | 35 | 25 | 31000 | 1200 | <4 | 30 | 11 | <8 | <4 | 60 |
| Peppercorn Enriched | 18 | 40 | 130 | 40000 | 1300 | <4 | 33 | 15 | <8 | <4 | 82 |
| Kelly's Plain Enriched | 16 | 39 | 31 | 35000 | 1200 | <4 | 30 | 13 | <8 | <4 | 77 |
| Felsics Baseline | 16 | 46 | 27 | 34000 | 1300 | <4 | 31 | 11 | <8 | <4 | 61 |
| Felsics Enriched | 15 | 44 | 61 | 32000 | 1100 | <4 | 30 | 14 | <8 | <4 | 66 |
| Min | 15 | 31 | 25 | 31000 | 1100 | <4 | 28 | 10 | <8 | <4 | 60 |
| Max | 24 | 100 | 130 | 43000 | 1400 | <4 | 64 | 57 | <8 | <4 | 150 |
| SQGV ^a | NA | 80 | 65 | NA | NA | NA | 21 | 50 | NA | NA | 200 |

^a SQGV: The sediment quality guideline values (Simpson et al., 2013). Values highlighted in red is where default guideline value exceeded. For Cd the detection limit was higher than the sediment quality guideline value. However the concentrations were expected to be below the sediment quality guideline value based on cadmium concentrations reported in Simpson et al. (2019) (excavated rock material ≤1 mg/kg and reservoir water sediments ≤0.27 mg/kg)

Table 23. Concentrations of dilute acid-extractable metals, metalloids and other elements in excavated rock material in the midge chronic toxicity tests

| Sample | Ca | K | Mg | Na | S | P | Al | As | B | Cd |
|-------------------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|------------|
| Midge test | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg |
| Ravine Baseline | 2900 | 310 | 1100 | 46 | 41 | 590 | 2800 | 3 | <3 | <3 |
| Ravine Enriched | 4200 | 300 | 570 | 29 | 43 | 580 | 2800 | <3 | <3 | <3 |
| Byron Baseline | 3500 | 640 | 440 | 43 | 39 | 540 | 3000 | <3 | <3 | <3 |
| Byron Enriched | 4300 | 700 | 630 | 46 | 57 | 620 | 3200 | <3 | <3 | <3 |
| Shaw Gabbro Baseline | 8000 | 960 | 1700 | 85 | 25 | 550 | 3900 | <3 | <3 | <3 |
| Shaw Gabbro Enriched | 2900 | 230 | 350 | 52 | 40 | 570 | 2700 | <3 | <3 | <3 |
| Volcanics Baseline | 5000 | 490 | 530 | 70 | 35 | 600 | 3200 | 3 | <3 | <3 |
| Volcanics Enriched | 8800 | 250 | 400 | 40 | 33 | 770 | 2900 | 3 | <3 | <3 |
| Peppercorn Baseline | 3100 | 250 | 510 | 47 | 39 | 590 | 2500 | <3 | <3 | <3 |
| Peppercorn Enriched | 3400 | 330 | 530 | 57 | 71 | 700 | 3000 | <3 | <3 | <3 |
| Kelly's Plain Enriched | 1400 | 300 | 530 | 47 | 46 | 550 | 2600 | <3 | <3 | <3 |
| Felsics Baseline | 10000 | 330 | 500 | 49 | 28 | 550 | 2700 | <3 | <3 | <3 |
| Felsics Enriched | 4500 | 580 | 360 | 39 | 40 | 590 | 2900 | <3 | <3 | <3 |
| Min | 1400 | 230 | 350 | 29 | 25 | 540 | 2500 | <3 | <3 | <3 |
| Max | 10000 | 960 | 1700 | 85 | 71 | 770 | 3900 | <3 | <3 | <3 |
| SQGV^a | NA | NA | NA | NA | NA | NA | NA | 20 | NA | 1.5 |

| Sample | Co | Cr | Cu | Fe | Mn | Mo | Ni | Pb | Sb | Se | Zn |
|-------------------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|------------|
| Midge test | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg |
| Ravine Baseline | 9 | 4 | 14 | 13000 | 1100 | <3 | 6 | 11 | <6 | <3 | 38 |
| Ravine Enriched | 8 | 4 | 13 | 13000 | 1100 | <3 | 5 | 45 | <6 | <3 | 38 |
| Byron Baseline | 8 | 4 | 14 | 14000 | 1100 | <3 | 5 | 10 | <6 | <3 | 36 |
| Byron Enriched | 9 | 5 | 15 | 14000 | 1100 | <3 | 5 | 11 | <6 | <3 | 36 |
| Shaw Gabbro Baseline | 10 | 12 | 22 | 14000 | 1000 | <3 | 7 | 9 | <6 | <3 | 25 |
| Shaw Gabbro Enriched | 8 | 4 | 16 | 12000 | 1000 | <3 | 4 | 10 | <6 | <3 | 23 |
| Volcanics Baseline | 8 | 4 | 14 | 12000 | 1100 | <3 | 5 | 12 | <6 | <3 | 37 |
| Volcanics Enriched | 8 | 4 | 14 | 13000 | 1100 | <3 | 4 | 11 | <6 | <3 | 36 |
| Peppercorn Baseline | 8 | 3 | 13 | 12000 | 970 | <3 | 4 | 9 | <6 | <3 | 34 |
| Peppercorn Enriched | 8 | 6 | 17 | 13000 | 1000 | <3 | 5 | 12 | <6 | <3 | 38 |
| Kelly's Plain Enriched | 8 | 4 | 13 | 13000 | 1000 | <3 | 4 | 12 | <6 | <3 | 37 |
| Felsics Baseline | 8 | 4 | 13 | 12000 | 1200 | <3 | 4 | 10 | <6 | <3 | 21 |
| Felsics Enriched | 8 | 4 | 15 | 13000 | 1100 | <3 | 4 | 11 | <6 | <3 | 23 |
| Min | 8 | 3 | 13 | 12000 | 970 | <3 | 4 | 9 | <6 | <3 | 21 |
| Max | 10 | 12 | 22 | 14000 | 1200 | <3 | 7 | 45 | <6 | <3 | 38 |
| SQGV^a | NA | 80 | 65 | NA | NA | NA | 21 | 50 | NA | NA | 200 |

^a SQGV: The sediment quality guideline values (Simpson et al., 2013). Values highlighted in red is where default guideline value exceeded. For Cd the detection limit was higher than the sediment quality guideline value. However the concentrations were expected to be below the sediment quality guideline value based on cadmium concentrations reported in Simpson et al. (2019) (excavated rock material ≤1 mg/kg and reservoir water sediments ≤0.27 mg/kg)

3.8.2 Toxicity to blackworms

Excavated rocks from each geological zone were tested using three scenarios as given below and a control treatment was also included with each geological zone excavated rock and sediment mixture tests.

- (1) 75 g (wet weight) of 425-µm sieved sediment with 20 g Excavated rock on top of sediments - both Enriched and Baseline from each zone.
- (2) 75 g sediments and 20 g Excavated rock mixed well - both Enriched and Baseline from each zone.
- (3) 75 g excavated rock material only (Enriched Excavated rock from each zone).

Key results were:

- There was no significant difference in the reproductive success of blackworms in comparison to controls under Scenario 1 or 2 exposures (Figure 13; Figure 14).
- Exposure Scenarios 1 and 2 of Enriched Shaw Gabbro and Baseline Peppercorn resulted in significant reduction of the reproductive success in blackworms than in comparison to the reservoir sediment control treatments.
- Exposure to 100% Enriched excavated rock (Scenario 3) for 28 days caused 100% mortality of blackworms resulting in reproduction failure and zero biomass (Figure 13; Figure 14).
- The biomass of blackworms was significantly reduced in half of the combinations of excavated rock and reservoir sediments (indicated by * in Figure 13 and Figure 14) with Peppercorn Baseline and Enriched, Shaw Gabbro and Kellys Plain Enriched samples exhibiting significant effects in Scenarios 1 and 2.
- Biomass in blackworms was also affected when exposed to Byron and Volcanics Baseline excavated rock material as Scenario 1 and Ravine Baselines rock material when exposed as Scenario 2.
- In the blackworm chronic toxicity tests, Ni concentration (ranging from 26-91 mg/kg) was above the SQGV in all combinations of sediment and excavated rock materials (Table 24).
- As acid-extractable metal concentrations, lead was above the SQGV in Ravine Enriched excavated rock material in the chronic tests (Table 25).

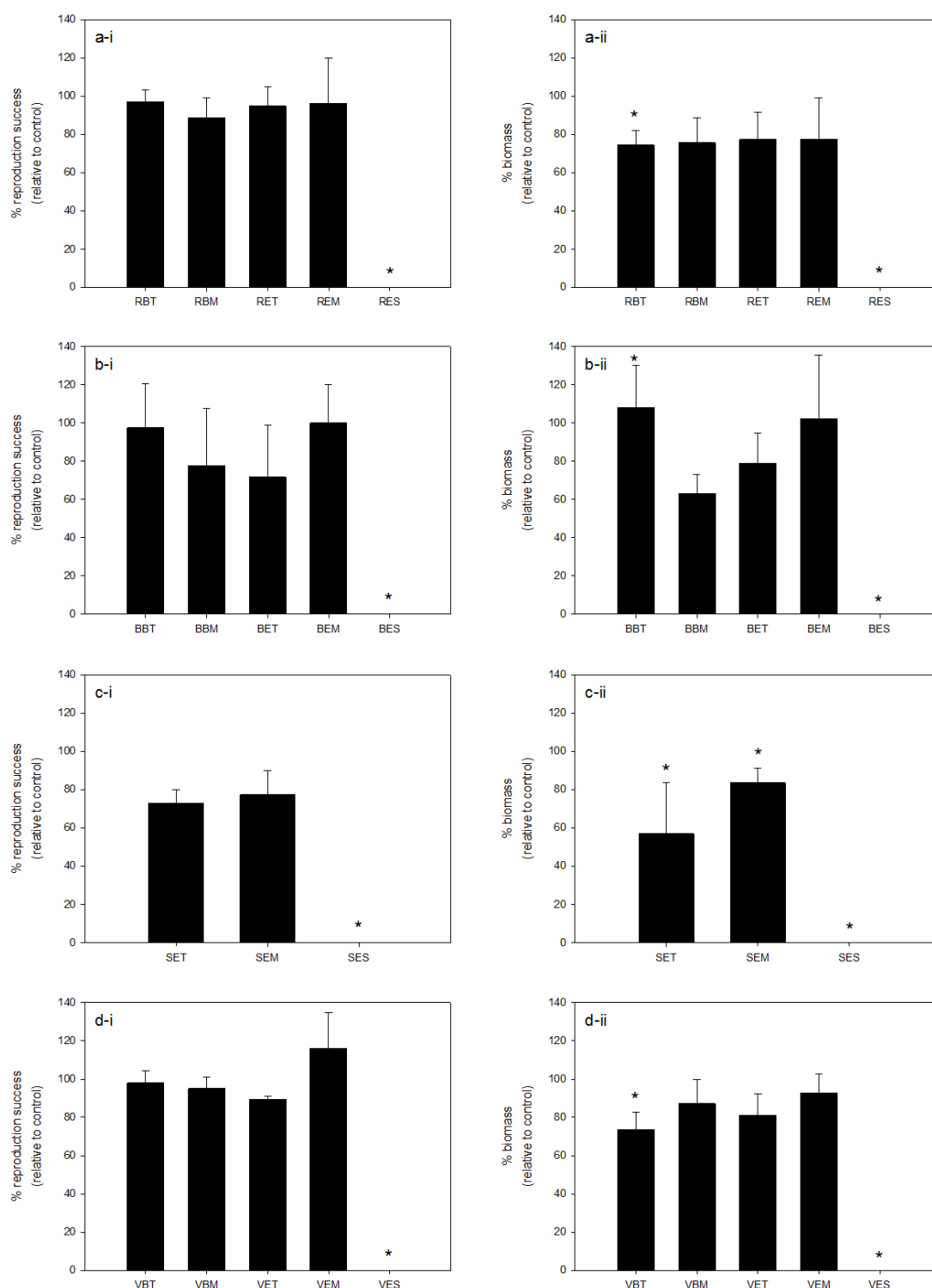


Figure 13. Chronic toxicity of excavated rock and sediment mixtures to the blackworm *Lumbriculus variegatus* (28-d reproduction and biomass) Geological units are (a) Ravine, (b) Byron, (c) Shaw Gabbro, (d) with test endpoint of (i) average number of juveniles and (ii) Biomass. The x-axis labels consist of three letters; first letter represents the geological zone R, B, S and V respectively; second letter represents Baseline (B) or Enriched (E) excavated rock; third letter represents excavated rock as a surface layer on sediment (T), excavated rock mixed with sediment (M) and excavated rock (S) scenario. Error bars represent 1 standard deviation. * indicates treatment is significant different to the control treatment ($p \leq 0.05$).

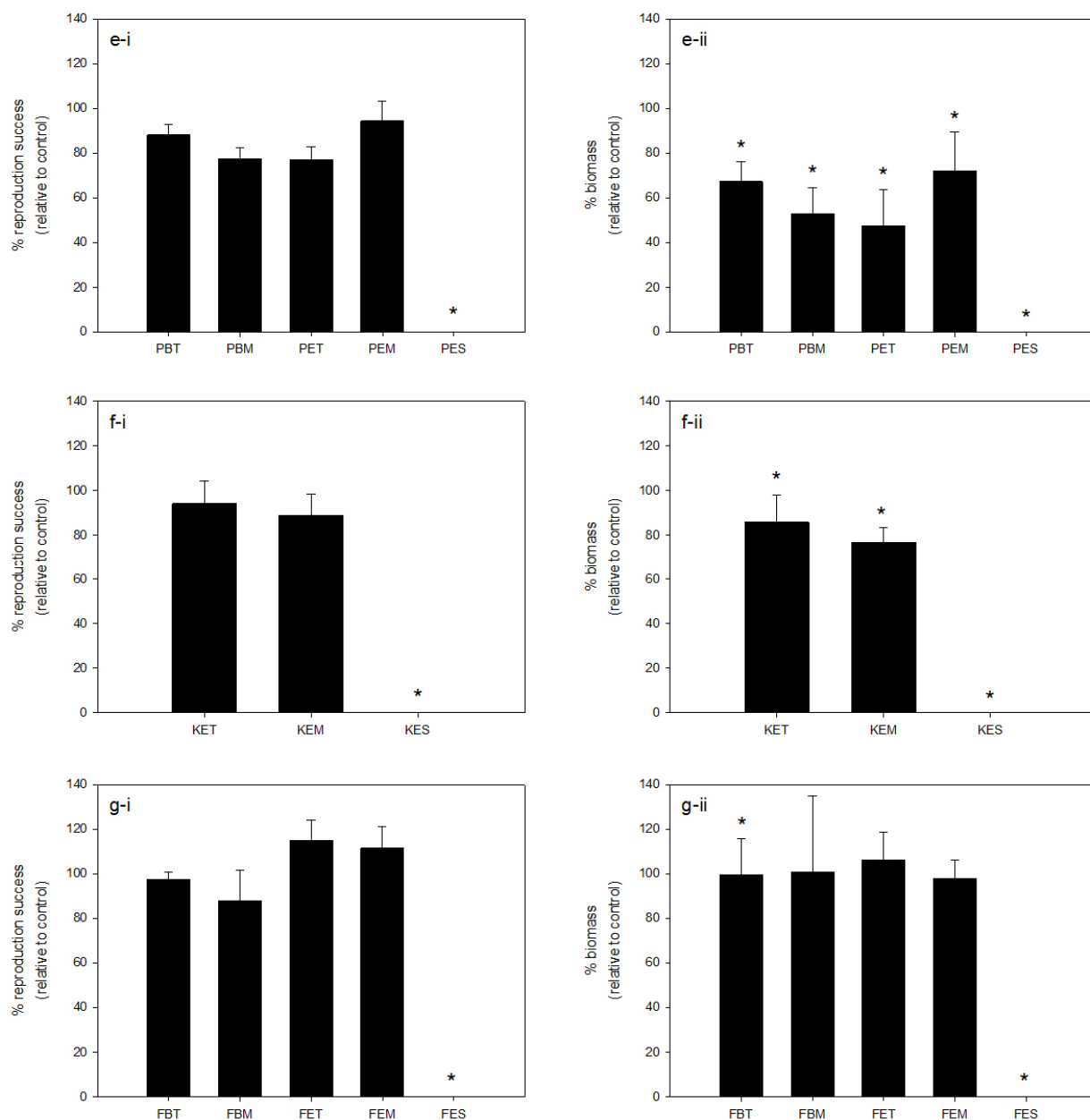


Figure 14. Chronic toxicity of excavated rock and sediment mixtures to the blackworm *Lumbriculus variegatus* (28-d reproduction and biomass) Data expressed as percent survival. Geological units are (e) Peppercorn, (f) Kellys Plain and (g) Felsic with test endpoint of (i) Average number of juveniles and (ii) Biomass. The x-axis labels consist of three letters; first letter represents the geological zone P, K, and F respectively; second letter represents Baseline (B) or Enriched (E) excavated rock; third letter represents excavated rock as a surface layer on sediment (T), excavated rock mixed with sediment (M) and excavated rock (S) scenario. Error bars represent 1 standard deviation. * indicates treatment is significant different to the control treatment ($p \leq 0.05$).

Table 24. Concentrations of total recoverable metals, metalloids and other elements excavated rock material in the blackworm chronic toxicity tests

| Sample | C(Total) | N(Total) | Ca | K | Mg | Na | S | P | Al | As | B | Cd |
|-------------------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|------------|------------|
| Blackworm test | % | % | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg |
| Ravine Baseline | 2.8 | 0.25 | 3000 | 3800 | 12000 | 140 | 280 | 770 | 33000 | 8 | 6 | <4 |
| Ravine Enriched | 2.6 | 0.24 | 2800 | 4100 | 15000 | 120 | 490 | 820 | 37000 | 8 | 6 | <4 |
| Byron Baseline | 2.6 | 0.24 | 3100 | 5500 | 4500 | 150 | 300 | 680 | 31000 | 6 | 8 | <4 |
| Byron Enriched | 2.6 | 0.24 | 3500 | 6100 | 5500 | 150 | 2450 | 770 | 32000 | 10 | 7 | <4 |
| Shaw Gabbro Baseline | 2.9 | 0.23 | 14000 | 3400 | 12000 | 250 | 230 | 690 | 35000 | 5 | <4 | <4 |
| Shaw Gabbro Enriched | 2.7 | 0.23 | 4900 | 2700 | 7200 | 190 | 250 | 720 | 29000 | 6 | <4 | <4 |
| Volcanics Baseline | 2.7 | 0.24 | 6200 | 3900 | 7500 | 240 | 250 | 770 | 32000 | 8 | 4 | <4 |
| Volcanics Enriched | 2.9 | 0.23 | 11000 | 2900 | 9600 | 130 | 1990 | 880 | 33000 | 10 | <4 | <4 |
| Peppercorn Baseline | 2.6 | 0.23 | 3400 | 3200 | 5400 | 150 | 300 | 780 | 27000 | 6 | 4 | <4 |
| Peppercorn Enriched | 2.6 | 0.23 | 5700 | 3700 | 6600 | 240 | 1900 | 880 | 33000 | 8 | 5 | <4 |
| Kelly's Plain Enriched | 2.6 | 0.22 | 1300 | 3400 | 5800 | 140 | 530 | 690 | 28000 | 7 | 4 | <4 |
| Felsics Baseline | 2.8 | 0.19 | 11000 | 4300 | 7300 | 140 | 240 | 700 | 31000 | 5 | 5 | <4 |
| Felsics Enriched | 2.8 | 0.24 | 4200 | 5500 | 5000 | 120 | 520 | 730 | 30000 | 7 | 7 | <4 |
| Min | 2.6 | 0.19 | 1300 | 2700 | 4500 | 120 | 230 | 680 | 27000 | 5 | <4 | <4 |
| Max | 2.9 | 0.25 | 14000 | 6100 | 15000 | 250 | 2450 | 880 | 37000 | 10 | 8 | <4 |
| SQGV^a | NA | NA | NA | NA | NA | NA | NA | NA | NA | 20 | NA | 1.5 |
| Sample | Co | Cr | Cu | Fe | Mn | Mo | Ni | Pb | Sb | Se | Zn | |
| Blackworm test | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | |
| Ravine Baseline | 20 | 63 | 37 | 39000 | 1200 | <4 | 67 | 13 | <8 | <4 | 87 | |
| Ravine Enriched | 21 | 84 | 41 | 46000 | 1500 | <4 | 91 | 150 | <8 | <4 | 390 | |
| Byron Baseline | 13 | 35 | 24 | 30000 | 1000 | <4 | 29 | 10 | <8 | <4 | 55 | |
| Byron Enriched | 16 | 46 | 30 | 35000 | 1000 | <4 | 34 | 13 | <8 | <4 | 57 | |
| Shaw Gabbro Baseline | 23 | 97 | 47 | 36000 | 1100 | <4 | 40 | 9 | <8 | <4 | 64 | |
| Shaw Gabbro Enriched | 18 | 47 | 33 | 32000 | 1200 | <4 | 32 | 12 | <8 | <4 | 70 | |
| Volcanics Baseline | 17 | 36 | 31 | 35000 | 1200 | <4 | 29 | 15 | <8 | <4 | 72 | |
| Volcanics Enriched | 21 | 30 | 39 | 48000 | 1300 | <4 | 26 | 9 | <8 | <4 | 74 | |
| Peppercorn Baseline | 14 | 35 | 23 | 30000 | 1000 | <4 | 29 | 10 | <8 | <4 | 55 | |
| Peppercorn Enriched | 18 | 44 | 160 | 42000 | 1200 | <4 | 36 | 13 | <8 | <4 | 85 | |
| Kelly's Plain Enriched | 15 | 39 | 30 | 35000 | 1000 | <4 | 29 | 13 | <8 | <4 | 75 | |
| Felsics Baseline | 15 | 50 | 24 | 34000 | 1200 | <4 | 29 | 10 | <8 | <4 | 58 | |
| Felsics Enriched | 14 | 34 | 64 | 29000 | 1000 | <4 | 26 | 13 | <8 | <4 | 58 | |
| Min | 13 | 30 | 23 | 29000 | 1000 | <4 | 26 | 9 | <8 | <4 | 55 | |
| Max | 23 | 97 | 160 | 48000 | 1500 | <4 | 91 | 150 | <8 | <4 | 390 | |
| SQGV^a | NA | 80 | 65 | NA | NA | NA | 21 | 50 | NA | NA | 200 | |

^a SQGV: The sediment quality guideline values (Simpson et al., 2013). Values highlighted in red is where default guideline value exceeded. For cadmium, the detection limit was higher than the sediment quality guideline value. However the concentrations were expected to be below the sediment quality guideline value based on cadmium concentrations reported in Simpson et al. (2019) (excavated rock material ≤1 mg/kg and reservoir water sediments ≤0.27 mg/kg)

Table 25. Concentrations of dilute-acid-extractable metals, metalloids and other elements in excavated rock material in the blackworm chronic toxicity tests

| Sample | Ca | K | Mg | Na | S | P | Al | As | B | Cd |
|------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Blackworm test | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg |
| Ravine Baseline | 3500 | 330 | 1300 | 54 | 33 | 580 | 2600 | 3 | <3 | <3 |
| Ravine Enriched | 3300 | 320 | 1100 | 43 | 37 | 660 | 2600 | <3 | <3 | <3 |
| Byron Baseline | 4000 | 750 | 480 | 52 | 34 | 520 | 2900 | <3 | <3 | <3 |
| Byron Enriched | 4400 | 830 | 650 | 47 | 53 | 600 | 3000 | <3 | <3 | <3 |
| Shaw Gabbro Baseline | 9400 | 1000 | 1900 | 92 | 19 | 520 | 3700 | <3 | <3 | <3 |
| Shaw Gabbro Enriched | 3300 | 260 | 380 | 65 | 35 | 570 | 2600 | <3 | <3 | <3 |
| Volcanics Baseline | 5500 | 510 | 510 | 76 | 29 | 600 | 3100 | <3 | <3 | <3 |
| Volcanics Enriched | 12000 | 240 | 460 | 46 | 16 | 760 | 2700 | <3 | <3 | <3 |
| Peppercorn Baseline | 3400 | 250 | 570 | 49 | 33 | 580 | 2200 | <3 | <3 | <3 |
| Peppercorn Enriched | 3800 | 340 | 550 | 62 | 70 | 690 | 2700 | <3 | <3 | <3 |
| Kelly's Plain Enriched | 1400 | 290 | 530 | 47 | 44 | 510 | 2200 | <3 | <3 | <3 |
| Felsics Baseline | 13000 | 350 | 560 | 58 | 8 | 530 | 2400 | <3 | <3 | <3 |
| Felsics Enriched | 5300 | 650 | 370 | 40 | 32 | 580 | 2500 | <3 | <3 | <3 |
| Min | 1400 | 240 | 370 | 40 | 8 | 510 | 2200 | <3 | <3 | <3 |
| Max | 13000 | 1000 | 1900 | 92 | 70 | 760 | 3700 | <3 | <3 | <3 |
| SQGV ^a | NA | NA | NA | NA | NA | NA | NA | 20 | NA | 1.5 |

| Sample | Co | Cr | Cu | Fe | Mn | Mo | Ni | Pb | Sb | Se | Zn |
|------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Blackworm test | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg | mg/kg |
| Ravine Baseline | 8 | 4 | 13 | 12000 | 1000 | <3 | 6 | 11 | <6 | <3 | 39 |
| Ravine Enriched | 7 | 5 | 12 | 12000 | 1000 | <3 | 6 | 120 | <6 | <3 | 43 |
| Byron Baseline | 7 | 4 | 13 | 12000 | 920 | <3 | 5 | 9 | <6 | <3 | 37 |
| Byron Enriched | 7 | 5 | 13 | 13000 | 930 | <3 | 5 | 10 | <6 | <3 | 36 |
| Shaw Gabbro Baseline | 9 | 13 | 22 | 13000 | 920 | <3 | 7 | 8 | <6 | <3 | 35 |
| Shaw Gabbro Enriched | 7 | 4 | 15 | 12000 | 910 | <3 | 4 | 9 | <6 | <3 | 35 |
| Volcanics Baseline | 7 | 4 | 13 | 12000 | 990 | <3 | 4 | 12 | <6 | <3 | 35 |
| Volcanics Enriched | 7 | 3 | 13 | 11000 | 970 | <3 | 4 | 9 | <6 | <3 | 33 |
| Peppercorn Baseline | 7 | 3 | 11 | 10000 | 850 | <3 | 4 | 8 | <6 | <3 | 32 |
| Peppercorn Enriched | 7 | 5 | 16 | 11000 | 860 | <3 | 4 | 11 | <6 | <3 | 35 |
| Kelly's Plain Enriched | 7 | 3 | 11 | 12000 | 860 | <3 | 4 | 11 | <6 | <3 | 35 |
| Felsics Baseline | 6 | 4 | 12 | 11000 | 1100 | <3 | 4 | 9 | <6 | <3 | 31 |
| Felsics Enriched | 7 | 3 | 13 | 11000 | 900 | <3 | 4 | 10 | <6 | <3 | 32 |
| Min | 6 | 3 | 11 | 10000 | 850 | <3 | 4 | 8 | <6 | <3 | 31 |
| Max | 9 | 13 | 22 | 13000 | 1100 | <3 | 7 | 120 | <6 | <3 | 43 |
| SQGV ^a | NA | 80 | 65 | NA | NA | NA | 21 | 50 | NA | NA | 200 |

^a SQGV: The sediment quality guideline values (Simpson et al., 2013). Values highlighted in red is where default guideline value exceeded. For cadmium, the detection limit was higher than the sediment quality guideline value. However the concentrations were expected to be below the sediment quality guideline value based on cadmium concentrations reported in Simpson et al. (2019) (excavated rock material ≤1 mg/kg and reservoir water sediments ≤0.27 mg/kg)

4 Fine suspended and deposited sediment associated adverse effects

Turbidity is a measure of suspended particulate matter (SPM) concentrations and is a non-toxic direct-effect stressor (ANZG, 2018). The SPM may have a deleterious influence on aquatic ecosystems while in suspension and then a further effect when it settles out of suspension as sediment. Measurements of suspended sediments are typically reported in either turbidity levels (Nephelometric Turbidity Units or NTU) or suspended sediment concentrations (mg/L) and is a direct measure of the mass of sediments suspended in a water sample. Turbidity can also be influenced by suspended particles other than inorganic sediment (e.g. organic matter, algal cells). Thus it is possible to have high turbidity without high suspended sediments concentrations (Bilotta & Brazier 2008). Furthermore, turbidity is also influenced by the physical and optical properties of the suspended particles (e.g. particle size, shape, mineral composition) and the amount of dissolved colour (e.g. humic substances), which can vary widely between waterways and within a waterway over time (Davies-Colley & Smith 2001; Bilotta & Brazier 2008).

The default turbidity GV for ecosystem protection for slightly disturbed ecosystems in south-eastern Australia are 2-25 NTU for upland rivers and 1-20 NTU for lakes and reservoirs (ANZG, 2018). Filtered excavated rock leachates from all geological and the reservoir water were well below this range (0.5-6.5 NTU).

In the present study, turbidity of the raw leachates (after 24 h settling period, Scenario 1) of excavated rock material was above 400 NTU for all geological zones. Ravine Enriched zone leachate showed the highest turbidity of 8100 NTU and 12-day settling reduced this high turbidity significantly to 100 NTU, whereas the 12-day settled leachates from Byron Baseline and Felsic Enriched zones remained around 520 NTU (Figure 15).

Both the scientific literature and international water quality guidelines relating to SS are dominated by the implicit assumption that the concentration-response model applies to SS effects on aquatic biota (i.e. increase in SS = increase in effect on aquatic biota) (Newcombe and MacDonald 1991). Indeed, numerous authors have reported that the magnitude of the effects of SS on aquatic organisms generally increases with their concentration. However, other factors such as the duration of exposure, particle-size distribution and chemical composition of the SS, and the presence of other contaminants on the solids, also appear to have an important control over the effect of SS on aquatic biota. These additional factors complicate the relationship between the magnitude of effect of SS and the concentration, making it difficult to predict the effect of SS on an organism merely by considering just the concentration.

The geochemical composition of the suspended load in a waterbody is an important factor in determining its effect on aquatic organisms. The geochemical composition will influence both the physical characteristics of the solids (including the shape, angularity and particle-size of the SS) and the chemical characteristics of the solids, including the likelihood of any chemical alterations in the receiving waters (e.g. pH, salinity, dissolved oxygen, phosphorus concentration, and toxicity).

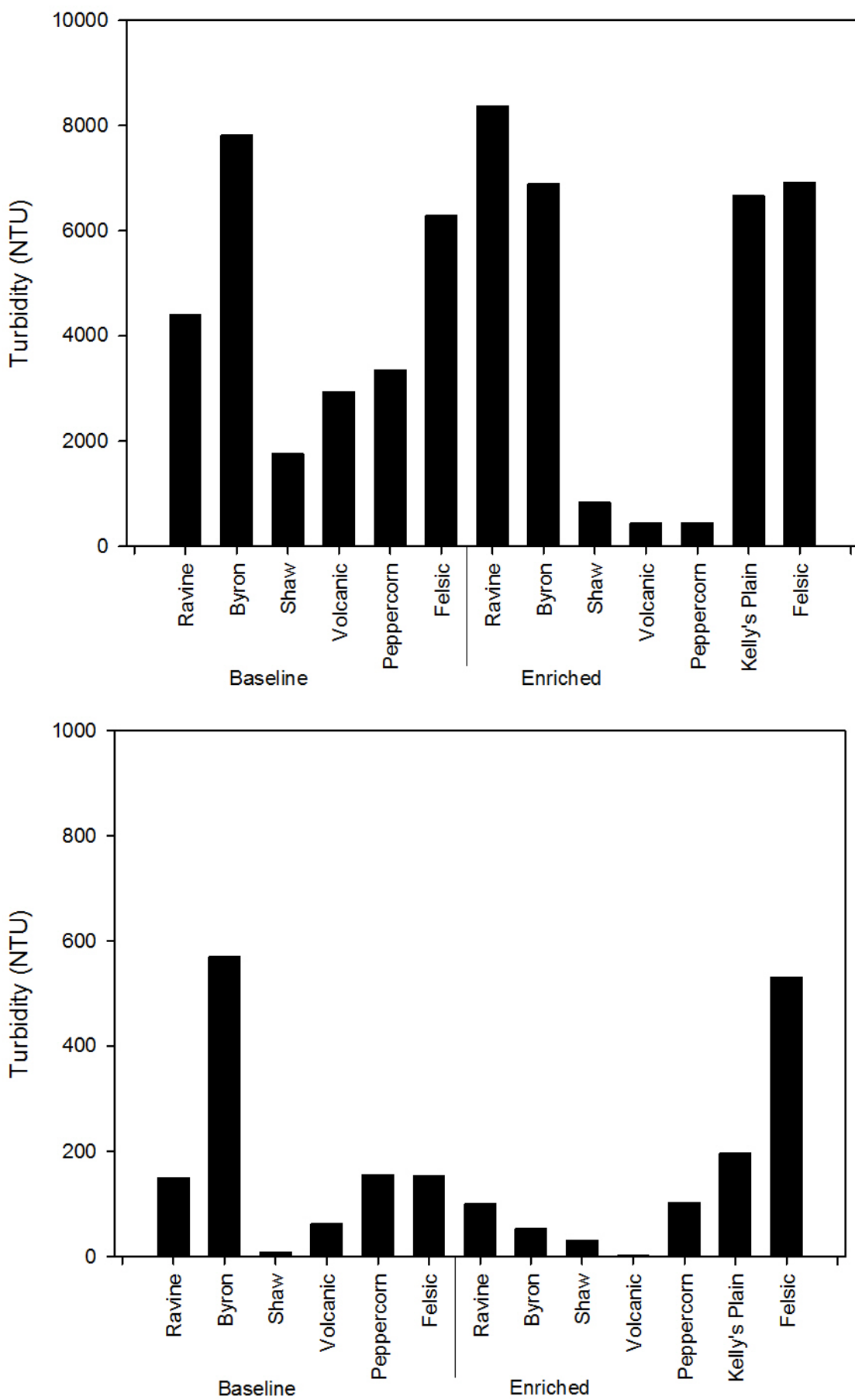


Figure 15. Turbidity (NTU) of raw and 12-day settled leachates of Baseline and Enriched excavated rocks

The detailed literature review “Adverse effects of fine sediments on aquatic organisms” has been submitted to SHL as a separate task. Some of the key points are discussed below.

Sub-aqueous excavated rock placement could degrade crucial life cycle processes among microflora (diatoms, green algae, cyanobacteria, and fungi), protozoa, microcrustacea and macroinvertebrates due to increased sedimentation at the placement locations. Often, these ecosystem elements drive the cascades of change that indirectly limit the productivity, food web relationships, health and survivorship of fish and crayfish. Increased or excessive suspended sediments can reduce productivity by (1) inhibiting photosynthesis, due to decreased light penetration; (2) physically smothering benthic communities; (3) removing periphyton by scouring; and (4) affecting community composition (Singleton, 1985). Notwithstanding these general patterns, temporary resuspension (e.g. dredging and logging) of sediments and nutrients in the water column can temporarily augment algal productivity (Bilby and Bisson, 1992).

Sediment particles are capable of adversely affecting benthic macroinvertebrates in several ways. These include:

- 1) direct smothering of benthic organisms (Hogg and Norris, 1991);
- 2) clogging of feeding apparatus in filter-feeding taxa causing stress or mortality (Newcombe and MacDonald, 1991; Metzeling et al., 1995);
- 3) reducing the effectiveness of oxygen exchange organs such as gills through clogging;
- 4) behavioural responses, such as increased invertebrate drift as an avoidance response to increased SPM levels (Doeg and Milledge, 1991; Richardson, 1985); and
- 5) influencing both the decomposition and availability of detrital material, with consequent impacts on the availability of food for many macroinvertebrates (Metzeling et al., 1995).

Potential impact pathway 4 listed above is not relevant to a reservoir environment and impact pathway 6 listed above was not investigated in the present study.

Excessive amounts of suspended sediment can harm fisheries ecosystems in any of six ways (Newcombe, 2003) by:

1. acting directly on free-swimming fish;
2. preventing the successful development of fish eggs and larvae;
3. modifying the natural movements and migrations of fish;
4. reducing the abundance of food available to the fish;
5. altering habitat; and
6. reducing catch per unit effort.

In the present study, toxicity of excavated rock material to fish was not carried out and all investigation were based on microalga and the invertebrate species.

There have been numerous studies on the effects of SPM on fish, with most focused on the effects on northern hemisphere salmonoid species in riverine environments (Lloyd, 1987). Impact types for fish range from direct mortality, to stress, (resulting in increased incidence of disease and reduced growth rates), to behavioural responses such as avoidance and altered feeding patterns, and adverse effects on reproduction. SPM has been shown to directly affect fish by clogging or coating gills, which can lead to death if concentrations are high enough. Indirectly, turbid water may impair feeding behaviour, particularly for species that use visual cues for foraging (Wenger et

al., 2017). Alternatively, diets may be altered by changes in populations of prey species (Garmen and Moring, 1993). Reproduction may also be affected, with SPM likely to cause impaired respiration and development, or in severe cases smothering, of eggs (Lloyd 1987).

While the above effects are particularly well known for salmonid species, the relevance of these overseas data to fish populations in Australian and New Zealand ecosystems is not well understood (Stowar, 1997). For example, Ryan (1991) has noted that the biological effects of SPM will depend upon many factors, including the nature of the SPM, the dissolved oxygen concentration, water temperature, natural SPM levels, and the species of fish in question, and this makes it difficult to extrapolate overseas data to aquatic Australian ecosystems. It is also important to note that mobile species will have the ability to move away and avoid the disturbance area.

There have been few Australian or New Zealand studies on the effects of SPM on fish populations (Campbell and Doeg, 1989). New Zealand studies have shown that turbidity levels over 25 NTU resulted in reduced feeding rates and avoidance behaviour in banded kokopu (*Galaxias fasciatus*) (Boubee et al., 1997; Rowe and Dean, 1998; Richardson et al., 2001). Richardson (1985) found that logging activities in NSW resulted in reduced abundance of the common jollytail (*Galaxias maculatus*). In these studies, it is difficult to disassociate the individual effects of SPM, sedimentation and habitat alteration. A laboratory study reportedly showed increased mortalities of river blackfish (*Gadopsis marmoratus*) and common galaxias (*Galaxias maculatus*) when exposed to increased levels of SPM, but unfortunately no data were presented (Koehn and O'Connor, unpublished data reported by Metzeling et al. (1995)).

Recent literature suggests silt-clay particles are most likely responsible for suffocating salmonid eggs. Decreased embryo survival was related to a change in fine sediment ($<0.074\text{mm}$) from less than 0.5% to 1.5% (Louhi et al., 2011). Fine sediment infilling may not be well correlated to % cover; instead suspended sediment (analogous to the deposited re-suspendable fraction in the silt-clay range) is likely to be the most appropriate attribute (Collins et al., 2011). Very fine sediment is likely to be more damaging than sand-sized material.

Wenger et al. (2017) note that, in line with the precautionary principle, management plans for sediment should consider both direct and indirect impacts to fish, as there can also be significant indirect effects of habitat loss, which can compound the direct effects of lethal and sub lethal toxicity, leading to further impacts.

However, indirect effects on fish through loss of prey, changes to biochemical processes and habitat loss may also occur. As the primary energy source, disruptions to the dynamics of light can fundamentally influence biogeochemistry. A reduction in light penetration will result in a net decrease in photochemical processes including the breakdown of contaminants by photolysis. This may reduce the capacity for waters to naturally degrade contaminants (Dunlop et al. 2005). Further, cloudier water traps more heat energy than the equivalent volume of clear water; the consequent increase in temperature decreases the absolute solubility of oxygen, and may contribute to depletion of this essential gas in ecosystems. The risk of increased temperature related low DO in the reservoirs of the size of Talbingo and Tantnagara could be low.

Carefully controlled experiments, subjecting organisms to different conditions, are rare. The variability and uncertainty in response of aquatic biota to concentrations of SS is such that although the effect of SPM is related to the concentration of SS in the water column, it also

depends on the type/species of organism, the stage that the organism is at within its life cycle, the duration and seasonal timing of exposure to the SS. Suggestions for further work to refine the understanding of likely impacts on other species include: Laboratory ecotoxicology bioassays using fish (including early life stages) and other invertebrates and/or follow-up *in-situ* caging studies (using yabbys, shrimp and fish) at different water depths during placement of rocks. This will help in validating the laboratory results under field conditions.

5 Conclusions

In the present study, the acute and chronic toxicity of contaminants (inorganics including metals) and physico-chemical stressors such as pH, EC, DO and turbidity released from excavated rock materials was assessed. A suite of standardised ecotoxicological bioassays under two different experimental set-ups were conducted with the following objectives:

3. Assess toxicity to aquatic organisms due to fine **suspended sediments** from excavated rock material interacting with the reservoir water and;
4. Assess toxicity to benthic organisms due to fine **deposited sediments** from excavated rock material interacting with the reservoir sediments.

In the first set of experiments, leachates from excavated rock and water with ratios from 1 to 10 were used for ecotoxicological assessment. Acute and chronic toxicity tests with representatives of four groups of aquatic life (a microalga, a water flea, a midge and blackworm) were carried out on leachates of excavated rock material prepared with water from Talbingo or Tantangara Reservoirs. Leachates of excavated rock had high levels of suspended solids (turbidity) that did not completely settle out of solution after 24 h. Therefore, the toxicity of leachates was assessed with water fleas, midges and blackworms on 'raw leachate' after 24 h settling and/or after '12-day settling' and/or 'filtered leachates'. Microalgae were only tested with filtered leachates. The toxicity tests using raw leachates were the 'worst case' scenarios unlikely to be encountered during placement activities.

In the second set of experiments, Sediment/excavated rock toxicity tests were carried out with two benthic species (midge and blackworms) and covered three excavated-rock and sediment mixture scenarios. 'Rock scenario' represented excavated rock as the dominant substrate in an area. 'Mixed scenario' indicated excavated rock mixing with sediments to form a smaller fraction of the substrate; and "Top scenario" specified thin layers of excavated rock material covering natural sediments to examine the effects of sedimentation on aquatic biota.

The acute and chronic toxicity data generated using one microalgae and three macroinvertebrate species was summarised by using the following ranking system:

| | |
|--|-------------------|
| Response NOT significantly different from Control and $p > 0.05$ | No toxicity |
| Significant difference and $\geq 80\%$ response relative to Control | Low toxicity |
| Significant difference and 79-60% response relative to Control | Moderate toxicity |
| Significant difference and $\leq 59\%$ response relative to Control | High toxicity |

5.1 Leachate toxicity

The key results from leachate toxicity testing under different scenarios are summarised below.

5.1.1 Acute toxicity

- Among invertebrates, water fleas were the most sensitive test organisms during 48-h leachate exposures, as compared to midges and blackworms.
- Water fleas exhibited high toxicity with 100% mortality when exposed to raw leachates of all Baseline and Enriched samples representing seven geological zones (Table 26).
- 12-day settled leachates from Byron Baseline exhibited high toxicity whereas Felsic Baseline and Volcanic Baseline leachates indicated moderate toxicity.
- No toxicity was observed when water fleas were exposed to 12-day settled leachates from Ravine Enriched, Byron Enriched, Peppercorn Enriched and Shaw Baseline and Enriched samples (Table 26 A)
- In addition, water fleas showed low to no acute toxicity when exposed to filtered leachates from all seven zone (Table 26A).
- During 48 h exposure, midge larvae exhibited high acute toxicity to raw Enriched leachates from Byron, Ravine and Shaw and moderate toxicity to Volcanic Enriched leachate (Table 26 B).
- Blackworms did not exhibit any toxicity, expressing 100% survival when exposed to raw, 12-day settled and filtered leachates from all seven geological zones (Table 26 C).
- Raw leachates demonstrated very high turbidity. Values were 427-774 NTU in 1:10 Enriched leachates from Peppercorn, Volcanics and Shaw Gabbo zones. Higher turbidities (666-837 NTU) were present in 1:100 leachates for Byron, Felsic, Kelly Plains and Ravine zones

5.1.2 Chronic toxicity

Chronic toxicity of filtered leachates representing Scenario 3 was evaluated using a microalga and a water flea. The results are summarised below:

- Baseline filtered leachates of Shaw Gabbro and Peppercorn and Enriched samples of Ravine, Byron, Shaw Gabbro, Peppercorn and Felsic demonstrated low chronic toxicity by significantly inhibiting microalgal growth by $\leq 18\%$. The Enriched Volcanics sample showed high toxicity and inhibited microalgal growth to the greatest extent (47% inhibition, compared to the control, Table 26 D).
- Baseline filtered leachates from Ravine, Byron, Volcanics, Peppercorn and enriched filtered leachates representing Peppercorn and Kelly's zones did exhibit toxicity to microalga.
- Chronic water flea testing was conducted using only Enriched undiluted filtered leachates from seven geological zones. Leachate from Kelly's Plain Enriched excavated sample resulted in high toxicity due to significant suppression of water flea reproduction. Leachates from other six geological zones (Ravine, Byron, Shaw, Volcanics, Peppercorn and Felsic) did not exhibit any chronic toxicity to water fleas (Table 26 D).

The dissolved aluminium concentrations exceeded the 95% GV for all leachates tested and highest concentrations were observed for Felsic Enriched. Felsic Enriched leachates also had dissolved As, Cr, Cu and Zn exceeding 95% GVs. Volcanics baseline leachate measured three dissolved metals (Al, As and Cr) above DGVs. Based on integrated ranking, the leachates from Shaw Gabbro, Volcanics, Byron and Kelly's Plain excavated rock material exhibited the highest toxicity to invertebrates and microalgae.

Based on an integrated ranking system, the raw leachates from enriched excavated rock materials from Ravine, Byron and Shaw zones exhibited high toxicity. Settling of some leachates at 4°C for 12 days reduced turbidity but fine colloidal particles were still found to be suspended in the leachate after this time. 12-day settled leachates from the Kellys (Enriched) and Byron (Baseline) zones exhibited moderate toxicity. This high turbidity of excavated rock material (between 200-500 NTU) and slow settling of the excavated rock materials in the placement area could exhibit acute toxicity to fish and macroinvertebrates inhabiting the reservoirs. Turbidity in the range of 50-200 NTU due to suspension of particulate material from excavated rock can also harm fish and other aquatic life during chronic long-term exposures by reducing food supplies, degrading spawning beds, and affecting gill function.

In Assignment P5, the ecotoxicological assessment was based on specific scenarios testing under laboratory conditions. The potential source of toxicity observed in aquatic and benthic biota during the tow experimental set-ups was associated with multistressors such as concentrations of metals, changes in water quality, elevated turbidity, and or elevated concentrations of suspended sediment. Following this project, modelling and refinement of the proposed excavated rock placement methods will be undertaken to determine how likely the tested experimental scenarios will be to conditions experienced within the reservoirs.

Table 26. Summary of ecotoxicological assessment of Baseline and Enriched leachates as three scenarios to water fleas (A), midges (B) and blackworms (C) and chronic toxicity to microalgae and water fleas (D). Three scenarios were tested (1) Raw –24 h settled leachate (2) settled-12-day settled leachate (3) Filtered – 0.45 µm filtered leachate. NT-No toxicity, LT-Low toxicity, MT Moderate toxicity, HT High toxicity and NA- not analysed.

| A. Acute toxicity of leachates to waterfleas | | | | | B. Acute toxicity of leachates to midge larvae | | | | |
|--|---|-----|---------|----------|--|---|-----|---------|----------|
| Scenarios | | Raw | Settled | Filtered | Scenarios | | Raw | Settled | Filtered |
| Ravine | B | HT | LT | LT | Ravine | B | LT | NA | LT |
| | E | HT | NT | NT | | E | HT | LT | NT |
| Byron | B | HT | HT | LT | Byron | B | LT | NA | LT |
| | E | HT | NT | LT | | E | HT | LT | NT |
| Shaw | B | HT | NT | NT | Shaw | B | LT | NA | NT |
| | E | HT | NT | LT | | E | HT | LT | LT |
| Volcanics | B | HT | MT | LT | Volcanics | B | LT | NA | LT |
| | E | HT | LT | NT | | E | MT | LT | LT |
| Peppercorn | B | HT | LT | NT | Peppercorn | B | LT | NA | NT |
| | E | HT | NT | LT | | E | LT | NA | NT |
| Kellys | E | HT | LT | NT | Kellys | E | NT | MT | NT |
| Felsic | B | HT | MT | NT | Felsic | B | LT | NA | NT |
| | E | HT | LT | HT | | E | NT | NA | LT |

| C. Acute toxicity of leachates to blackworms | | | | | D. Chronic toxicity of filtered leachates | | | |
|--|---|-----|---------|----------|---|---|------------|-------------|
| Scenarios | | Raw | Settled | Filtered | Scenarios | | Microalgae | Water fleas |
| Ravine | B | NT | NA | NT | Ravine | B | NT | NA |
| | E | NT | NA | NT | | E | LT | NT |
| Byron | B | NT | NA | NT | Byron | B | NT | NA |
| | E | NT | NA | NT | | E | LT | NT |
| Shaw | B | NT | NA | NT | Shaw | B | LT | NA |
| | E | NT | NA | NT | | E | LT | NT |
| Volcanics | B | NT | NA | NT | Volcanics | B | NT | NA |
| | E | NT | NA | NT | | E | HT | NT |
| Peppercorn | B | NT | NA | NT | Peppercorn | B | LT | NA |
| | E | NT | NA | NT | | E | NT | NT |
| Kellys | E | NT | NA | NT | Kellys | B | NT | NA |
| | E | NT | NA | NT | | E | NT | HT |
| Felsic | B | NT | NA | NT | Felsic | B | LT | NA |
| | E | NT | NA | NT | | E | LT | NT |

5.2 Sediment and excavated rock combination toxicity

Ecotoxicological observations from excavated rock and reservoir sediment under three different scenarios can be summarised as follows:

- In general, excavated rock material (both Enriched and Baseline) mixed with sediments or on top of sediments did not affect survival of midge larvae, with all treatments exhibiting >80% survival (Table 27 A).
- Midge larvae exhibited high toxicity with significant reduced survival (30-60% relative of control) when exposed to 100% Enriched excavated rock (referred as Scenario 3) from Shaw Gabbro, Volcanics and Felsic zones over 7-day exposure (Table 27A).
- Blackworm biomass was the most sensitive indicator to detect toxicological responses after 28 days exposure to excavated rock and sediment in three different scenarios. .
- Exposure Scenarios 1 and 2 of Enriched Shaw Gabbo and Baseline Peppercorn resulted in significant reduction of the reproductive success in blackworms than in comparison to the reservoir sediment control treatments.
- Exposure to 100% Enriched excavated rock (Scenario 3) for 28 days caused 100% mortality of blackworms resulting in reproduction failure and zero biomass (Table 28).
- The biomass of blackworms was significantly reduced in half of the combinations of excavated rock and reservoir sediments (Table 28) with Peppercorn Baseline and Enriched, Shaw Gabbro and Kellys Plain Enriched samples exhibiting significant effects in Scenarios 1 and 2.
- Biomass in blackworms was also affected when exposed to Byron and Volcanics Baseline excavated rock material as Scenario1 and Ravine Baselines rock material when exposed as Scenario 2 (Table 28).
- In the blackworm chronic toxicity tests, nickel concentrations (ranging from 26-91 mg/kg) were above the sediment guideline levels in all combinations of sediment and excavated rock materials.
- Peppercorn, Shaw Gabbro and Volcanics excavated rock material exhibited the highest toxicity to the benthic macroinvertebrates tested in this study.

Macroinvertebrates such as midge and blackworms are present in the Talbingo and Tantangara Reservoirs and were used as test organisms in this study. Sediments mixed with excavated rock or top of reservoir sediments generally showed no toxicity to low toxicity during 7-day exposures to midge larvae and 28-day exposure to blackworms. Exposures to neat Enriched excavated rock material from all zones as a worst-case scenario with very low probability exhibited moderate toxicity to high toxicity. As an integrated toxicity assessment, Shaw (Enriched and Baseline), Volcanics (Enriched) and Peppercorn (Baseline) excavated material exhibited low to moderate level toxicity to blackworms and midge larvae when exposed as mixtures of sediment and excavated rock material mixtures.

100% raw leachates as suspended sediments in the reservoir and neat excavated rock material as sedimentation represent worst-case exposure scenarios tested in the present study. Increase in turbidity and metals and metalloids such as Al that might be introduced to the water body as a consequence of suspended sediments from the excavated rock and/or due to sedimentation. These multistressors could result in low level of toxicological, physiological or physical impacts on fish and macroinvertebrates. Suggestions for collection of further biological assessment data for Talbingo and Tantangara reservoirs, including ecotoxicological effects and an ongoing in-situ monitoring program based on sufficient baseline data are provided.

Table 27. Summary of ecotoxicological assessment of Baseline and Enriched samples for midge larvae survival (A) and growth (B). Three scenarios were tested (1) Top –as a surface layer on top of reservoir sediment (2) Mixed – mixed with reservoir sediment (3) Rock - 100% Enriched excavated rock. NT-No toxicity, LT-Low toxicity, MT Moderate toxicity, HT High toxicity and NA- not analysed

| A. Midge Survival | | | | | B. Midge Growth | | |
|-------------------|---|-----|-------|------|-----------------|-------|------|
| Scenarios | | Top | Mixed | Rock | Top | Mixed | Rock |
| Ravine | B | NT | NT | NA | NT | NT | NA |
| | E | NT | NT | NT | NT | NT | NT |
| Byron | B | NT | NT | NA | NT | NT | NA |
| | E | NT | NT | NT | NT | NT | LT |
| Shaw | B | NT | NT | NA | NT | NT | NA |
| | E | NT | NT | HT | NT | NT | NT |
| Volcanics | B | NT | NT | NA | NT | NT | NA |
| | E | NT | HT | HT | NT | NT | NT |
| Peppercorn | B | NT | NT | NA | NT | NT | NA |
| | E | NT | NT | NT | NT | NT | NT |
| Kellys | E | NT | NT | NT | NT | NT | NT |
| Felsic | B | NT | NT | NA | NT | NT | NA |
| | E | NT | NT | HT | NT | NT | NT |

Table 28 Summary of ecotoxicological assessment of Baseline and Enriched samples for blackworm total biomass (A) and reproduction success (B). Three scenarios were tested (1) Top –as a surface layer on top of reservoir sediment (2) Mixed –mixed with reservoir sediment (3) Rock - 100% Enriched excavated rock. NT-No toxicity, LT- Low toxicity, MT Moderate toxicity, HT High toxicity and NA- not analysed

| A. Blackworm reproduction success | | | | | B. Blackworm biomass | | |
|-----------------------------------|---|-----|-------|------|----------------------|-------|------|
| Scenarios | | Top | Mixed | Rock | Top | Mixed | Rock |
| Ravine | B | NT | NT | NA | MT | NT | NA |
| | E | NT | NT | HT | NT | NT | HT |
| Byron | B | NT | NT | NA | NT | NT | NA |
| | E | NT | NT | HT | NT | NT | HT |
| Shaw | B | MT | MT | HT | HT | LT | NT |
| | E | NT | NT | NA | MT | NT | NA |
| Volcanics | B | NT | NT | HT | NT | NT | HT |
| | E | LT | MT | NA | MT | HT | NA |
| Peppercorn | B | MT | NT | HT | HT | MT | HT |
| | E | NT | NT | HT | LT | MT | HT |
| Kellys | E | NT | NT | NA | NT | NT | NA |
| Felsic | B | NT | NT | HT | NT | NT | HT |
| | E | NT | NT | NA | MT | NT | NA |

6 Suggestions for further work

Suggestions for future study to fill knowledge gaps are dependent on the final excavated rock placement methodology but include:

1. High turbidity and/or suspended sediment of the rock material could also exhibit mortality in the early life stages of fish preventing successful development of fish eggs and larvae. This could be further investigated by conducting laboratory and field investigations using fish larvae (such as Murray cod and golden perch).
2. Lethal and sub-lethal impact of turbidity to adult fish (such as flathead gudgeon) could be investigated under variable concentration and duration of exposures.
3. Determining the turbidity tolerance limit for invertebrates such as shrimp, yabbies, and snails, with species relevant to the study area.
4. The turbidity tolerance limit for microalgae could be examined to understand indirect effects due to low food availability for fish and invertebrates.
5. Longer-term releases of substances from very fine excavated rock materials are predicted to remain suspended within the reservoir water for periods of many months (e.g. <4 µm particle size fraction). Long term *in-situ* toxicity testing on fish and macroinvertebrates inhabiting Tantangara/Talbingo reservoirs would add value to this assessment. In addition, monitoring of general water quality parameters such as pH, EC, temperature and turbidity, and in situ monitoring of dissolved aluminium should also be considered if field trials occur.
6. Testing of longer-term effects of dissolved aluminium release, including potential cycling from dissolved and precipitated forms if pH cycles up and down could also be investigated.

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Appendix A Conceptual model and lines of evidence

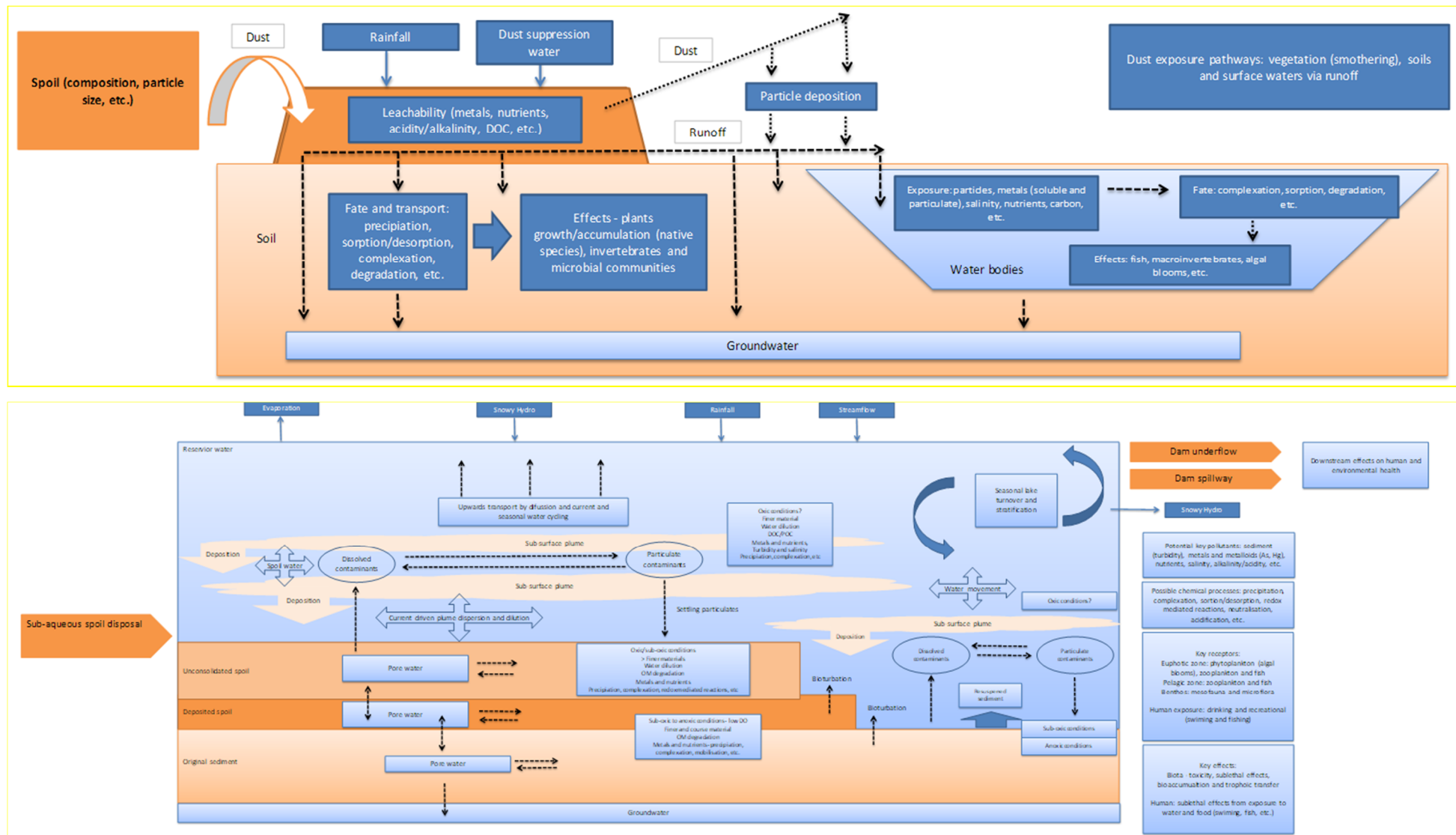


Figure A1. Two figures outlining the pressure-stressor-receptor pathways and connections developed by EMM and CSIRO (December 2017).

Table A1. Pressure-stressors-receptor pathways

| Pathway | Natural | Extreme natural events | Spoil discharge (acute) | Spoil discharge (chronic) |
|---|---------|------------------------|-------------------------|---------------------------|
| Physical paths | | | | |
| Lake water movement - general | Yes | Yes | Yes | Yes |
| Lake water movement - vertical mixing | Yes | Yes | Yes | Yes |
| Lake water movement - storm mixing | ? | ? | ? | ? |
| Rainfall | Yes | Yes | Yes | Yes |
| Evaporation | Yes | Yes | Yes | Yes |
| Stream flow - water | Yes | Yes | Yes | Yes |
| Stream flow - sediments | Yes | Yes | Yes | Yes |
| Snowy Hydro - water release to lake | Yes | Yes | Yes | Yes |
| Snowy Hydro - water take | Yes | Yes | Yes | Yes |
| Dam underflow | Yes | Yes | Yes | Yes |
| Dam spillway | No | Yes | ? | ? |
| Release of spoil water | No | No | Yes | No |
| Particle settling of natural particles | Yes | Yes | Yes | Yes |
| Particle settling of suspended/resuspended spoil | No | No | Yes | Yes |
| Particle settling - initial spoil deposition | No | No | Yes | No |
| Particle resuspension due to water movement | ? | ? | ? | ? |
| Sediment resuspension due to spoil addition | No | ? | Yes | Yes |
| Surface plume formation | ? | ? | ? | ? |
| Sub-surface plume formation | ? | ? | ? | ? |
| Water 'ejected' during spoil consolidation | No | No | Yes | No |
| Smothering of benthos | No | ? | ? | No |
| Bioturbation | Yes | - | - | ? |
| Slumping | ? | ? | ? | ? |
| Chemical paths | | | | |
| Adsorption of contaminants in lake water onto suspended particles | Yes | Yes | Yes | Yes |
| Desorption of contaminants from suspended particles | Yes | Yes | Yes | Yes |
| Adsorption of contaminants from lake water onto spoil particles | No | No | Yes | Yes |
| Desorption of contaminants from spoil particles | No | No | Yes | Yes |
| Diffusion of contaminants from pore water to water column | Yes | Yes | Yes | Yes |
| Adsorption of contaminants in pore water onto natural sediment particles | Yes | Yes | Yes | Yes |
| Desorption of contaminants from natural sediment particles to pore water | Yes | Yes | Yes | Yes |
| Adsorption of contaminants in pore water onto spoil particles | No | No | Yes | Yes |
| Desorption of contaminants from spoil particles to pore water | No | No | Yes | Yes |
| Redox mediated chemical pathways (oxic, sub-oxic and anoxic conditions - spoil and sediments) | No | ? | Yes | Yes |
| Biological paths | | | | |
| Ingestion of suspended particulates | Yes | Yes | Yes | Yes |
| Ingestion of sediment particles on lake bed | Yes | Yes | Yes | Yes |
| Uptake of dissolved contaminants in water column | Yes | Yes | Yes | Yes |
| Uptake of dissolved contaminants in pore water | Yes | Yes | Yes | Yes |
| Ingestion of nekton | Yes | Yes | Yes | Yes |
| Ingestion of benthos | Yes | Yes | Yes | Yes |
| Human ingestion of fish | Yes | Yes | Yes | Yes |
| Human recreational contact | Yes | Yes | Yes | Yes |

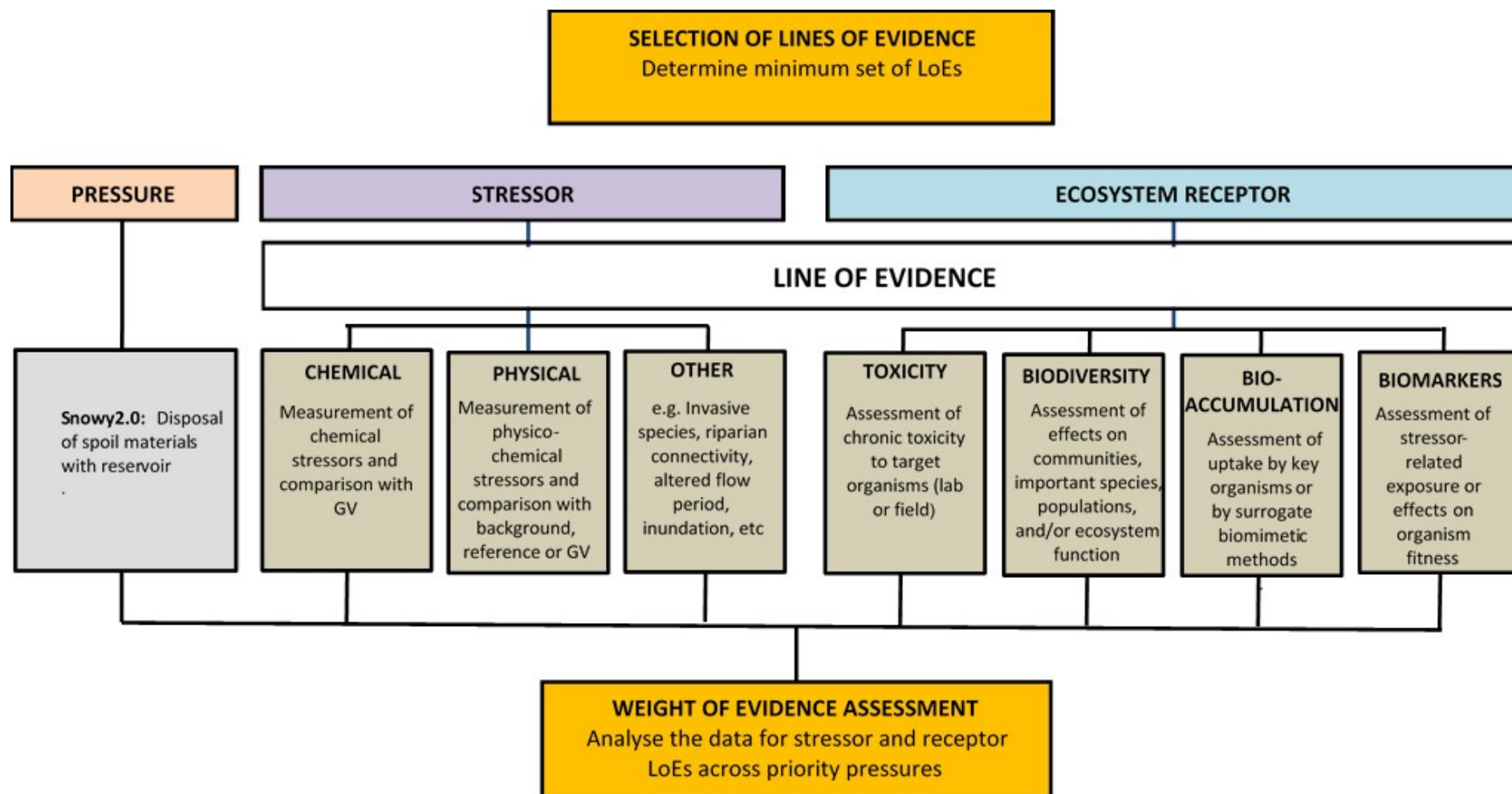


Figure A2. Lines of evidence used in water quality weight-of-evidence assessments

Appendix B Composition of excavated rock material

Table B1. Excavated rock materials - Ravine

| Ravine – Baseline | | | | | | |
|----------------------|---------------|---------------|---------------------------------|---|------------------|--------------------------------------|
| Sample_ID | Depth (m) | | Lithology | Major Geology (Surface)/ Zone | Placement Option | Classification |
| | Top | Bottom | | | | |
| BH6105-R-0063 | 160.57 | 161.00 | Siltstone with a sandstone band | Yarrangobilly Limestone/Palaeozoic | Talbingo | Tunnel/surge shaft/powerhouse |
| BH4105-R-0362 | 200.7 | 201 | Phyllite | Ravine bed | Talbingo | Tunnel/surge shaft/powerhouse |
| BH6105-R-0061 | 177.00 | 177.26 | Siltstone with a chert band | Yarrangobilly Limestone/Palaeozoic | Talbingo | Tunnel/surge shaft/powerhouse |
| BH4105-R-0356 | 18.1 | 18.5 | Siltstone | Ravine bed | Talbingo | Tunnel/surge shaft/powerhouse |
| BH4104-R-0291 | 376.61 | 377 | Siltstone | Yarrangobilly Limestone/Palaeozoic | Talbingo | Tunnel/surge shaft/powerhouse |
| BH4105-R-0363 | 225.7 | 226 | Interbedded phyllite/schist | Ravine bed | Talbingo | Tunnel/surge shaft/powerhouse |
| BH7105-R-0036 | 49.00 | 49.30 | Siltstone | Yarrangobilly Limestone/Palaeozoic | Talbingo | Tunnel/surge shaft/powerhouse |
| <i>BH6105-R-0060</i> | <i>147.00</i> | <i>147.33</i> | <i>Siltstone</i> | <i>Yarrangobilly Limestone/Palaeozoic</i> | <i>Talbingo</i> | <i>Tunnel/surge shaft/powerhouse</i> |
| Ravine – Enriched | | | | | | |
| BH6102-R-0045 | 162.00 | 162.15 | Interbedded siltstone/sandstone | Yarrangobilly Limestone/Palaeozoic | Talbingo | Tunnel/surge shaft/powerhouse |
| BH7105-R-0039 | 15.00 | 15.30 | Siltstone | Yarrangobilly Limestone/Palaeozoic | Talbingo | Tunnel/surge shaft/powerhouse |
| BH7105-R-0396 | 23 | 23.25 | Siltstone | Ravine bed | Talbingo | Tunnel/surge shaft/powerhouse |
| BH4104-R-0294 | 871.56 | 871.82 | Siltstone | Yarrangobilly Limestone/Palaeozoic | Talbingo | Tunnel/surge shaft/powerhouse |
| BH4105-R-0371 | 445.7 | 446 | Interbedded phyllite/gneiss | Ravine bed | Talbingo | Tunnel/surge shaft/powerhouse |
| BH6101-R-0226 | 161 | 161.3 | Sandstone/Siltstone | Yarrangobilly Limestone/Palaeozoic | Talbingo | Tunnel/surge shaft/powerhouse |
| <i>BH7105-R-0038</i> | <i>25.60</i> | <i>26.00</i> | <i>Conglomerate</i> | <i>Yarrangobilly Limestone/Palaeozoic</i> | <i>Talbingo</i> | <i>Tunnel/surge shaft/powerhouse</i> |

Table B2. Excavated rock - Byron/Boraig and Shaw Hill Gabbro

| Sample_ID | Depth (m) | | Lithology | Major Geology (Surface)/ Zone | Placement Option | Classification |
|-----------------------------|--------------|--------------|---------------------------------|---|------------------|---------------------------|
| | Top | Bottom | | | | |
| Byron/Boraig – Baseline | | | | | | |
| BH5104-R-0122 | 472 | 472.3 | Sandstone | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Top of surge shaft |
| BH5104-R-0133 | 727.63 | 727.83 | Sandstone | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Top of surge shaft |
| BH5101-R-0055 | 283.73 | 283.87 | Siltstone | Yarrangobilly Limestone/Palaeozoic | Talbingo | Top of surge shaft |
| BH5104-R-0116 | 282.53 | 282.8 | Felsic ignimbrite | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Top of surge shaft |
| BH5105-R-0143 | 36 | 36 | Sandstone | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Top of surge shaft |
| BH5104-R-0120 | 409 | 409.3 | Conglomerate/sandstone | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Top of surge shaft |
| BH5104-R-0108 | 119.4 | 119.75 | Mudstone | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Top of surge shaft |
| Byron/Boraig – Enriched | | | | | | |
| BH5104-R-0138 | 822.7 | 823 | Siltstone | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Top of surge shaft |
| BH5104-R-0114 | 239.15 | 239.4 | Sandstone | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Top of surge shaft |
| BH5104-R-0109 | 131.1 | 131.35 | Mudstone | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Top of surge shaft |
| BH5104-R-0113 | 227.4 | 227.67 | Conglomerate | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Top of surge shaft |
| BH8106-R-0406 | 640.7 | 641 | Interbedded sandstone/siltstone | Byron range group/ravine bed | Talbingo | Top of surge shaft |
| BH5104-R-0110 | 142.17 | 142.43 | Conglomerate | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Top of surge shaft |
| BH5115-R-0388 | 261.35 | 261.6 | | Byron range group/boraig group/ravine bed | Talbingo | Top of surge shaft |
| Shaw Hill Gabbro – Baseline | | | | | | |
| Sample_ID | Depth fr (m) | Depth to (m) | Lithology | Major Geology (Surface)/ Zone | Placement Option | Classification |
| BH4106-R-0270 | 96.75 | 97 | Schist | Shaw Hill Gabbro | Talbingo | Tunnel alignment/headrace |
| BH4106-R-0271 | 124.75 | 125 | Schist | Shaw Hill Gabbro | Talbingo | Tunnel alignment/headrace |
| BH4106-R-0272 | 162 | 162.2 | Schist | Shaw Hill Gabbro | Talbingo | Tunnel alignment/headrace |
| BH4106-R-0281 | 76.71 | 77 | Schist | Shaw Hill Gabbro | Talbingo | Tunnel alignment/headrace |
| Shaw Hill Gabbro – Enriched | | | | | | |
| BH4106-R-0273 | 198.1 | 198.4 | Diorite | Shaw Hill Gabbro | Talbingo | Tunnel alignment/headrace |
| BH4106-R-0274 | 230.37 | 230.78 | Diorite | Shaw Hill Gabbro | Talbingo | Tunnel alignment/headrace |
| BH4106-R-0276 | 312.42 | 312.72 | Diorite | Shaw Hill Gabbro | Talbingo | Tunnel alignment/headrace |
| BH4106-R-0278 | 383.15 | 383.5 | Diorite | Shaw Hill Gabbro | Talbingo | Tunnel alignment/headrace |

Table B3. Excavated rock - Gooandra Volcanics

| Sample_ID | Depth (m) | | Lithology | Major Geology (Surface)/ Zone | Placement Option | Classification |
|-------------------------------|-----------|--------|---|-------------------------------|------------------|------------------------------|
| | Top | Bottom | | | | |
| Gooandra Volcanics – Baseline | | | | | | |
| BH4103-R-0001 | 360.30 | 360.60 | Greenschist | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |
| BH4103-R-0003 | 76.40 | 76.60 | Schist | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |
| BH4103-R-0011 | 325.00 | 325.40 | Metasiltstone | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |
| BH4103-R-0012 | 246.16 | 246.56 | Metasiltstone | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |
| BH4103-R-0014 | 173.62 | 173.90 | Greenschist | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |
| BH4103-R-0018 | 155.20 | 155.47 | Greenschist | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |
| BH4103-R-0019 | 318.15 | 318.47 | Metasiltstone | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |
| BH4102-R-0312 | 472.25 | 472.55 | Schist | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |
| Gooandra Volcanics – Enriched | | | | | | |
| BH4103-R-0008 | 383.72 | 384.00 | Greenschist | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |
| BH3110-R-0409 | 115.7 | 116 | Metasandstone | Gooandra volcanics | Talbingo | Tunnel alignment/headrace |
| BH4103-R-0026 | 117.65 | 117.93 | Greenschist | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |
| BH3110-R-0413 | 215 | 215.27 | Metasandstone | Gooandra volcanics | Talbingo | Tunnel alignment/headrace |
| BH3110-R-0407 | 64.7 | 65 | Interlaminated metasiltstone/metasandstone | Gooandra volcanics | Talbingo | Tunnel alignment/headrace |
| BH3110-R-0408 | 92 | 92.25 | Metasiltstone | Gooandra volcanics | Talbingo | Tunnel alignment/headrace |
| BH3110-R-0411 | 172.75 | 173 | Metasiltstone | Gooandra volcanics | Talbingo | Tunnel alignment/headrace |
| BH4103-R-0017 | 82.37 | 82.68 | Schist | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |

Table B4. Excavated rock - Peppercorn/Tantangara/Temperance formations

| Sample_ID | Depth (m) | | Lithology | Major Geology (Surface)/ Zone | Placement Option | Classification |
|---|-----------|--------|---------------------------------|-------------------------------|---------------------|---------------------------|
| | Top | Bottom | | | | |
| Peppercorn/Tantangara/Temperance Formations - Baseline | | | | | | |
| BH3101-R-0257 | 110.35 | 110.65 | meta sandstone | Tantangara Formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH3101-R-0259 | 170.3 | 170.6 | Meta Siltstone/Meta Sandstone | Tantangara Formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH3101-R-0261 | 201 | 201.3 | Meta Siltstone/Meta Sandstone | Tantangara Formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH3106-R-0353 | 154 | 154.3 | Interbedded sandstone/siltstone | Tantangara formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH3104-R-0395 | 319 | 319.45 | Siltstone | Tantangara formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH3101-R-0254 | 38 | 38.3 | Meta Siltstone/Meta Sandstone | Tantangara Formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH3106-R-0352 | 129.39 | 129.69 | Interbedded sandstone/siltstone | Tantangara formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH2102-R-0345 | 47.7 | 48 | Interbedded sandstone/siltstone | Tantangara formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| Peppercorn/Tantangara/Temperance Formations - Enriched | | | | | | |
| BH3102-R-0329 | 247.35 | 247.67 | Meta Siltstone/Meta Sandstone | Tantangara Formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH3101-R-0263 | 253 | 253.3 | Meta Siltstone/Meta Sandstone | Tantangara Formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH3102-R-0331 | 268 | 268.3 | Meta Siltstone/Meta Sandstone | Tantangara Formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH3102-R-0320 | 67.6 | 67.9 | meta siltstone | Tantangara Formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH3102-R-0322 | 116 | 116.28 | meta siltstone | Tantangara Formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH3102-R-0321 | 81.7 | 82 | meta siltstone | Tantangara Formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH3101-R-0255 | 61 | 61.3 | Meta Siltstone/Meta Sandstone | Tantangara Formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| BH3102-R-0319 | 35.25 | 35.55 | meta siltstone | Tantangara Formation | Tantangara/Talbingo | Tunnel alignment/Headrace |
| Kellys Plain Volcanics - Not available until late in study testing period | | | | | | |
| BH5102-R-0009, BH5102-R-0011, BH5102-R-0013 | | | | | Tantangara/Talbingo | |
| BH1115-R-0003, BH1116-R-0005, BH1117-R-0007 | | | | | Tantangara/Talbingo | |

Table B5. Excavated rock - Felsics/granitoids/gniess/ignimbrites

| Sample_ID | Depth (m) | | Lithology | Major Geology (Surface)/ Zone | Placement Option | Classification |
|--|-----------|--------|-------------------|--------------------------------------|------------------|------------------------------|
| | Top | Bottom | | | | |
| Felsics/granitoids/gniess/ignimbrites – Baseline | | | | | | |
| BH4102-R-0315 | 524 | 524.3 | Gneiss | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |
| BH4102-R-0316 | 546.4 | 546.7 | Gneiss | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |
| BH4102-R-0318 | 599 | 599.3 | Gneiss | Gooandra Volcanics | Talbingo | Tunnel alignment/headrace |
| BH4105-R-0370 | 430.7 | 431 | Gneiss | Ravine bed | Talbingo | Tunnel alignment/headrace |
| BH5104-R-0115 | 256 | 256.3 | Felsic ignimbrite | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Tunnel alignment/headrace |
| BH5103-R-0079 | 512.57 | 512.80 | Felsic volcanics | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Tunnel alignment/headrace |
| BH7104-R-0234 | 86.4 | 86.65 | Ignimbrite | Yarrangobilly Limestone/Palaeozoic | Talbingo | Tunnel alignment/headrace |
| Felsics/granitoids/gniess/ignimbrites – Enriched | | | | | | |
| BH5105-R-0147 | 69 | 69.3 | Ignimbrite | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Tunnel alignment/headrace |
| BH5103-R-0066 | 342.40 | 342.61 | Felsic volcanics | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Tunnel alignment/headrace |
| BH5103-R-0080 | 348.37 | 348.58 | Felsic volcanics | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Tunnel alignment/headrace |
| BH5105-R-0146 | 64.7 | 65 | Ignimbrite | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Tunnel alignment/headrace |
| BH5105-R-0148 | 93.5 | 93.8 | Ignimbrite | Sandstone/Shale/Limestone/Palaeozoic | Talbingo | Tunnel alignment/headrace |

Appendix C Leachates of excavated rock material: microalgal toxicity test reports

Provided as supplementary information

Appendix D Leachates of excavated rock material: Supplementary information for the water flea (*Ceriodaphnia dubia*) acute and chronic toxicity tests

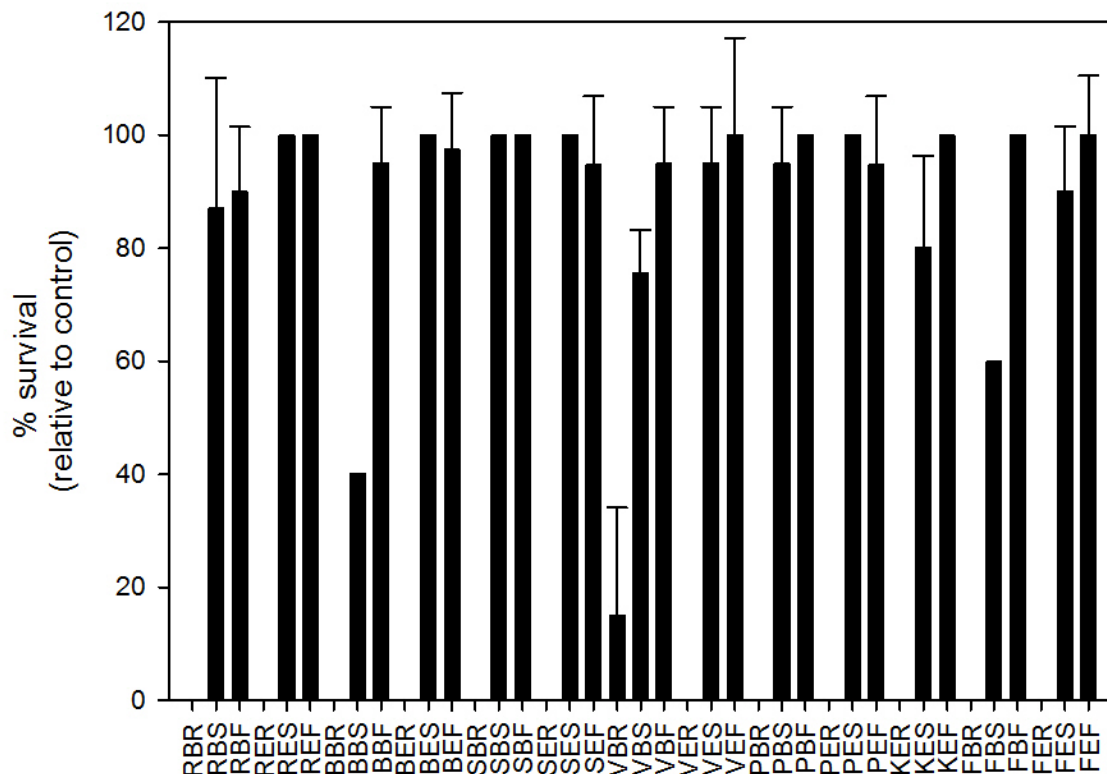


Figure D1. Summary data on the survival (acute toxicity) of water fleas (*Ceriodaphnia dubia*) for all leachates. Data expressed as relative to Reservoir water control. First letter represents the geological zone Ravine (R), Byron (B), Shaw Gabbro (S), Volcanics (V), Peppercorn (P), Kellys Plain (K) and Felsic (F) respectively; Second letter represents Baseline (B) or Enriched (E) excavated rock; Third letter represents raw (R), after 24 h settling (S) and filtered (F) fraction of leachate.

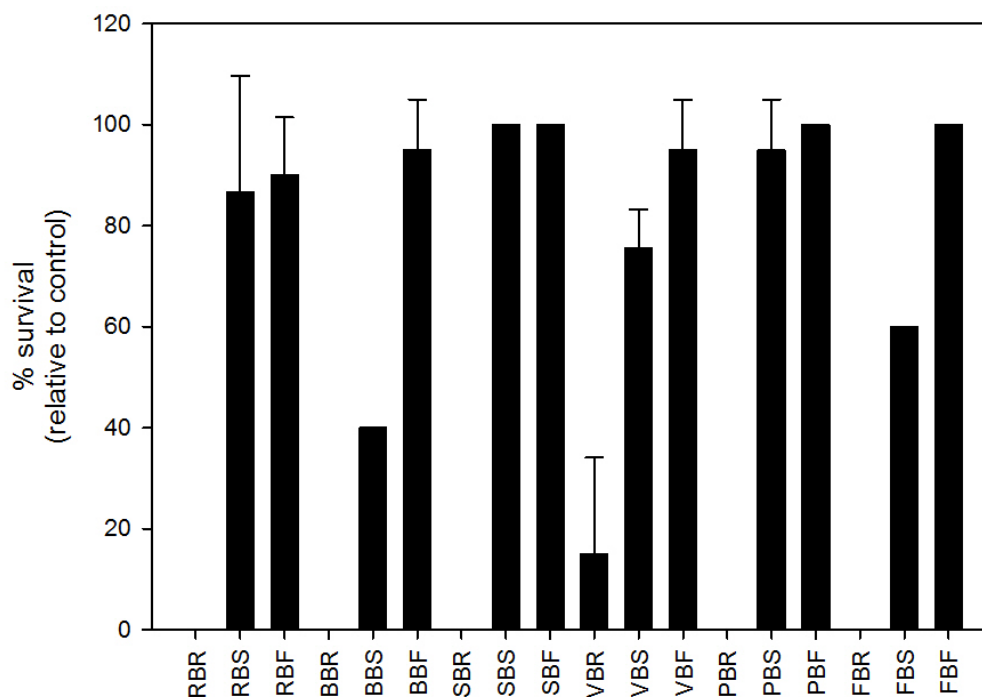


Figure D2. Summary data on survival (acute toxicity) of water fleas (*Ceriodaphnia dubia*) to leachates of Baseline material. Data expressed as relative to reservoir water control. . First letter represents the geological zone Ravine (R), Byron (B), Shaw Gabbro (S), Volcanics (V), Peppercorn (P), Kellys Plain (K) and Felsic (F) respectively; Second letter represents Baseline (B) excavated rock; Third letter represents raw (R), after 24 h settling (S) and filtered (F) fraction of leachate

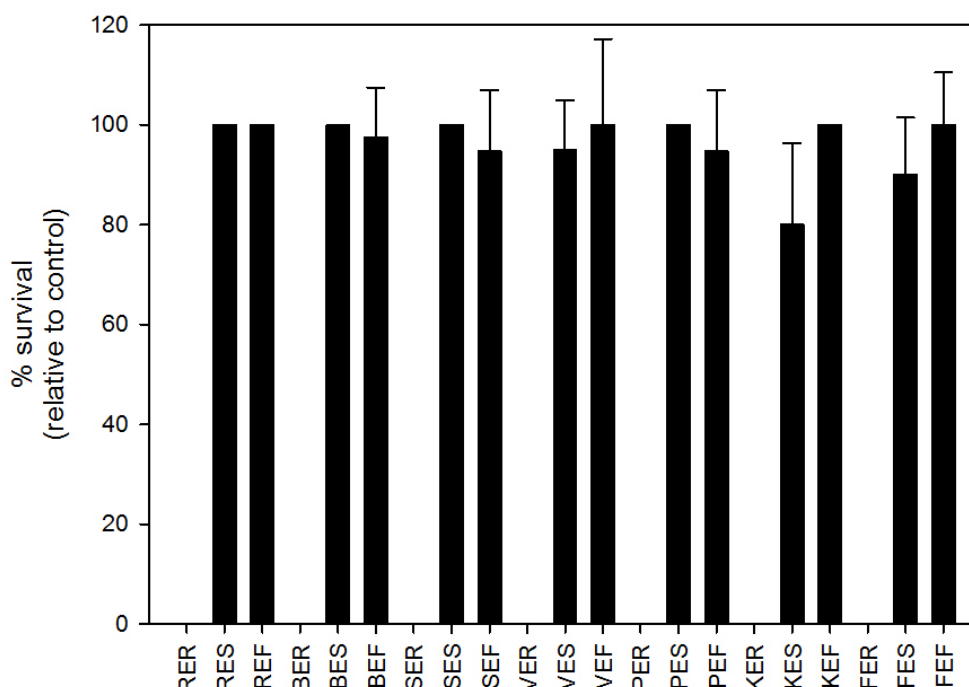


Figure D3. Summary data on survival (acute toxicity) of water fleas (*Ceriodaphnia dubia*) to leachates of Enriched material. Data expressed as relative to reservoir water control. . First letter represents the geological zone Ravine (R), Byron (B), Shaw Gabbro (S), Volcanics (V), Peppercorn (P), Kellys Plain (K) and Felsic (F) respectively; Second letter represents Enriched (E) excavated rock; Third letter represents raw (R), after 24 h settling (S) and filtered (F) fraction of leachate

Table D1. Supplementary data on survival (acute toxicity) of water fleas (*Ceriodaphnia dubia*) for toxicity test data for all leachates. NA indicates sample not analysed. First letter represents the geological zone Ravine (R), Byron (B), Shaw Gabbro (S), Volcanics (V), Peppercorn (P), Kellys Plain (K) and Felsic (F) respectively; Second letter represents Baseline (B) or Enriched (E) excavated rock; Third letter represents raw (R), after 24 h settling (S) and filtered (F) fraction of leachate

| Total survival out of 5 after 48 hrs | | | | | | | |
|--------------------------------------|---|---|----|---|------|-----|---------|
| | A | B | C | D | Avg. | SD | p-value |
| Control | 5 | 5 | 5 | 5 | 5 | 0 | |
| RBR | 0 | 0 | NA | | 0.0 | 0.0 | <0.001 |
| RBS | 0 | 4 | 5 | 5 | 3.5 | 2.4 | |
| RBF | 5 | 4 | 5 | 4 | 4.5 | 0.6 | |
| RER | 0 | 0 | NA | | 0.0 | 0.0 | <0.001 |
| RES | 5 | 5 | 5 | 5 | 5.0 | 0.0 | |
| REF | 5 | 5 | 5 | 5 | 5.0 | 0.0 | |
| BBR | 0 | 0 | NA | | 0.0 | 0.0 | <0.001 |
| BBS | 4 | 4 | 5 | 2 | 3.8 | 1.3 | 0.02 |
| BBF | 5 | 5 | 5 | 4 | 4.8 | 0.5 | |
| BER | 0 | 0 | NA | | 0.0 | 0.0 | <0.001 |
| BES | 5 | 5 | 5 | 5 | 5.0 | 0.0 | |
| BEF | 5 | 5 | 5 | 5 | 5.0 | 0.0 | |
| SBR | 0 | 0 | NA | | 0.0 | 0.0 | <0.001 |
| SBS | 2 | 5 | 5 | 5 | 4.3 | 1.5 | |
| SBF | 5 | 5 | 5 | 5 | 5.0 | 0.0 | |
| SER | 0 | 0 | NA | | 0.0 | 0.0 | <0.001 |
| SES | 5 | 5 | 5 | 5 | 5.0 | 0.0 | |
| SEF | 5 | 4 | 5 | 4 | 4.5 | 0.6 | |
| VBR | 0 | 0 | NA | | 0.0 | 0.0 | <0.001 |
| VBS | 4 | 3 | 4 | 4 | 3.8 | 0.5 | 0.001 |
| VBF | 4 | 5 | 5 | 5 | 4.8 | 0.5 | |
| VER | 0 | 0 | NA | | 0.0 | 0.0 | <0.001 |
| VES | 5 | 5 | 4 | 5 | 4.8 | 0.5 | |
| VEF | 5 | 5 | 5 | 4 | 4.8 | 0.5 | |
| PBR | 0 | 0 | NA | | 0.0 | 0.0 | <0.001 |
| PBS | 5 | 4 | 5 | 5 | 4.8 | 0.5 | |
| PBF | 5 | 5 | 5 | 5 | 5.0 | 0.0 | |
| PER | 0 | 0 | NA | | 0.0 | 0.0 | <0.001 |
| PES | 5 | 5 | 5 | 5 | 5.0 | 0.0 | |
| PEF | 4 | 4 | 5 | 5 | 4.5 | 0.6 | |
| KER | 0 | 0 | NA | | 0.0 | 0.0 | <0.001 |
| KES | 4 | 3 | 5 | 4 | 4.0 | 0.8 | |
| KEF | 5 | 5 | 5 | 5 | 5.0 | 0.0 | |
| FBR | 0 | 0 | NA | | 0.0 | 0.0 | <0.001 |
| FBS | 4 | 3 | 3 | 3 | 3.3 | 0.5 | <0.001 |
| FBF | 5 | 4 | 5 | 5 | 4.8 | 0.5 | |
| FER | 0 | 0 | NA | | 0.0 | 0.0 | <0.001 |
| FES | 4 | 4 | 5 | 5 | 4.5 | 0.6 | |
| FEF | 5 | 5 | 4 | 5 | 4.8 | 0.5 | |

Table D2. Supplementary water quality data for the acute (survival) toxicity tests with the water flea (*Ceriodaphnia dubia*).

| Treatment | Water Quality at test completion | | | |
|-----------|----------------------------------|----------------|---|----------------------|
| | pH | DO (% sat.) | Conductivity ($\mu\text{S}/\text{cm}$) | Temperature (° C) |
| RBR | 7.8 | 92.8 | 102.4 | 24.0 |
| RBS | 7.6 | 93.9 | 119.3 | 24.0 |
| RBF | 7.8 | 93.0 | 95.1 | 24.0 |
| RER | 8.1 | 87.5 | 133.4 | 24.0 |
| RES | 7.8 | 93.1 | 143.7 | 24.0 |
| REF | 8.0 | 92.7 | 115.3 | 24.0 |
| BBR | 7.7 | 91.6 | 165.5 | 24.0 |
| BBS | 7.2 | 93.6 | 149.8 | 24.0 |
| BBF | 7.9 | 92.9 | 136.9 | 24.0 |
| BER | 8.0 | 88.1 | 203.6 | 24.0 |
| BES | 7.7 | 95.3 | 196.1 | 24.0 |
| BEF | 8.1 | 92.3 | 162.1 | 24.0 |
| SBR | 7.8 | 93.2 | 127.3 | 24.0 |
| SBS | 7.7 | 93.7 | 135.4 | 24.0 |
| SBF | 7.9 | 93.5 | 108.7 | 24.0 |
| SER | 8.1 | 90.0 | 101.8 | 24.0 |
| SES | 7.8 | 93.4 | 111.1 | 24.0 |
| SEF | 8.0 | 92.8 | 90.1 | 24.0 |
| VBR | 7.8 | 92.6 | 117.0 | 24.0 |
| VBS | 7.7 | 93.7 | 133.9 | 24.0 |
| VBF | 7.9 | 93.6 | 119.9 | 24.0 |
| VER | 8.0 | 90.9 | 113.3 | 24.0 |
| VES | 7.8 | 93.8 | 122.4 | 24.0 |
| VEF | 8.0 | 92.4 | 106.0 | 24.0 |
| PBR | 7.8 | 92.3 | 106.6 | 24.0 |
| PBS | 7.5 | 94.1 | 111.7 | 24.0 |
| PBF | 7.8 | 93.0 | 87.4 | 24.0 |
| PER | 8.0 | 88.8 | 124.4 | 24.0 |
| PES | 7.7 | 93.6 | 138.5 | 24.0 |
| PEF | 8.0 | 92.4 | 113.1 | 24.0 |
| KER | 8.0 | 88.5 | 113.9 | 24.0 |
| KES | 7.7 | 93.8 | 126.3 | 24.0 |
| KEF | 8.0 | 91.8 | 101.0 | 24.0 |
| FBR | 7.8 | 91.8 | 124.0 | 24.0 |
| FBS | 7.4 | 94.3 | 125.2 | 24.0 |
| FBF | 7.9 | 92.9 | 97.0 | 24.0 |
| FER | 8.1 | 85.8 | 157.4 | 24.0 |
| FES | 7.7 | 95.4 | 159.4 | 24.0 |
| FEF | 8.1 | 92.9 | 126.1 | 24.0 |

Ravine (R), Byron (B), Shaw Gabbro (S), Volcanics (V), Peppercorn (P), Kellys Plain (K) and Felsic (F); Baseline (B) or Enriched (E) excavated rock; raw (R), after 24 h settling (S) and filtered (F) fraction of leachate.

Table D3. Acute toxicity of Tantangara and Talbingo Reservoir water samples to the water flea, *Ceriodaphnia dubia*

| | Total survival out of 5 after 48 hrs | | | | | | Water Quality at test completion | | | |
|----------|--------------------------------------|---|---|---|------|---------|----------------------------------|-------------|----------------------|-------------------|
| | A | B | C | D | Avg. | SD | pH | DO (% sat.) | Conductivity (µS/cm) | Temperature (° C) |
| TN3 | 5 | 5 | 5 | 5 | 5 | 0 | 8.0 | 108.5 | 32.1 | 24.0 |
| TN2 | 5 | 4 | 5 | 5 | 4.75 | 0.5 | 7.9 | 105.5 | 31.4 | 24.0 |
| TN1 | 3 | 5 | 5 | 5 | 4.5 | 1 | 7.8 | 104.5 | 31.0 | 24.0 |
| TAL-PL2C | 5 | 5 | 4 | 5 | 4.75 | 0.5 | 7.8 | 104.3 | 30.1 | 24.0 |
| TAL-PL1C | 4 | 5 | 5 | 5 | 4.75 | 0.5 | 7.7 | 107.1 | 30.4 | 24.0 |
| TAL-PL2D | 5 | 4 | 5 | 5 | 4.75 | 0.5 | 7.7 | 104.6 | 30.3 | 24.0 |
| TAL-PL1D | 4 | 5 | 5 | 4 | 4.5 | 0.57735 | 7.6 | 106.2 | 33.0 | 24.0 |

Table D4. Acute toxicity of pooled reservoir water samples to the water flea, *Ceriodaphnia dubia* and corresponding copper reference toxicity test results.

| Treatment | After 24 hours | | | | After 48 hours | | | |
|-----------|----------------|---|---|---|----------------|---|---|---|
| | # Alive | | | | # Alive | | | |
| | A | B | C | D | A | B | C | D |
| MHW | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 4 |
| TAL | 4 | 4 | 5 | 5 | 4 | 4 | 5 | 5 |
| TN | 4 | 5 | 4 | 5 | 4 | 5 | 4 | 5 |
| Cu-5µg/l | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| Cu-10µg/l | 5 | 5 | 5 | 5 | 4 | 4 | 5 | 5 |
| Cu-20µg/l | 3 | 3 | 2 | 0 | 0 | 0 | 0 | 0 |

Table D5. Low electrical conductivity (EC) related acute toxicity to the water flea, *Ceriodaphnia dubia*

| | Total survival out of 5 after 48 hrs | | | | | | Water Quality at test completion | | | |
|--------|--------------------------------------|---|---|---|------|------|----------------------------------|-------------|----------------------|-------------------|
| | A | B | C | D | Avg. | SD | pH | DO (% sat.) | Conductivity (µS/cm) | Temperature (° C) |
| MHW | 5 | 5 | 5 | 4 | 4.75 | 0.5 | 8.09 | 107.8 | 321 | 24.0 |
| EC 20 | 5 | 5 | 4 | 4 | 4.5 | 0.58 | 7.38 | 109 | 28.9 | 24.0 |
| EC 40 | 5 | 5 | 5 | 5 | 5 | 0 | 7.31 | 109 | 49.2 | 24.0 |
| EC 60 | 5 | 5 | 5 | 4 | 4.75 | 0.5 | 7.23 | 109 | 69.2 | 24.0 |
| EC 80 | 5 | 5 | 5 | 4 | 4.75 | 0.5 | 7.25 | 109 | 89.7 | 24.0 |
| EC 120 | 5 | 5 | 5 | 5 | 5 | 0 | 7.36 | 108 | 132.7 | 24.0 |
| EC 160 | 5 | 5 | 5 | 5 | 5 | 0 | 7.42 | 108 | 167.3 | 24.0 |
| EC 240 | 5 | 5 | 5 | 4 | 4.75 | 0.5 | 7.51 | 110 | 264 | 24.0 |

Table D6. Copper reference toxicity tests and the effective concentration (EC in µg/L) of copper at 50%, 10% and 20% for the water flea (*Ceriodaphnia dubia*) during acute toxicity tests with leachates.

| Treatment | After 24 hours | | | | After 48 hours | | | |
|-----------|----------------|---|---|---|----------------|---|---|---|
| | # Alive | | | | # Alive | | | |
| | A | B | C | D | A | B | C | D |
| MHW | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 4 |
| TAL | 4 | 4 | 5 | 5 | 4 | 4 | 5 | 5 |
| TN | 4 | 5 | 4 | 5 | 4 | 5 | 4 | 5 |
| Cu-5µg/l | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| Cu-10µg/l | 5 | 5 | 5 | 5 | 4 | 4 | 5 | 5 |
| Cu-20µg/l | 3 | 3 | 2 | 0 | 0 | 0 | 0 | 0 |

| Treatment | After 48 hours | | | | | |
|-----------|----------------|---|---|--------|---|---|
| | # Alive | | | # Dead | | |
| MHW | 5 | 5 | 4 | 0 | 0 | 1 |
| TAL | 5 | 5 | 4 | 0 | 0 | 1 |
| Cu-5µg/l | 5 | 4 | 5 | 0 | 1 | 0 |
| Cu-10µg/l | 3 | 2 | 3 | 2 | 3 | 2 |
| Cu-20µg/l | 0 | 0 | 0 | 5 | 5 | 5 |

| Treatment | After 24 hours | | | | After 48 hours | | | |
|-----------|----------------|---|---|---|----------------|---|---|---|
| | # Alive | | | | # Alive | | | |
| | A | B | C | D | A | B | C | D |
| MHW | 5 | 5 | 5 | 5 | 4 | 5 | 5 | 5 |
| TAL | 5 | 5 | 5 | 5 | 5 | 5 | 4 | 4 |
| Cu-5µg/l | 5 | 5 | 5 | 5 | 3 | 5 | 5 | 5 |
| Cu-10µg/l | 6 | 5 | 4 | 5 | 4 | 2 | 2 | 3 |
| Cu-20µg/l | 3 | 1 | 0 | 1 | 1 | 1 | 0 | 0 |

| Copper reference test | EC50(µg/l) | 95% Conf. intervals For EC50 | | EC10(µg/l) | 95% Conf. intervals For EC10 | |
|--------------------------|------------|---------------------------------|-------|------------|---------------------------------|---------|
| | | | | | | |
| Test 1 | 11.56 | #N/A | #N/A | 10.00 | #N/A | #N/A |
| Test 2 | 11.56 | #N/A | #N/A | 2.14 | #N/A | #N/A |
| Test 3 | 18.99 | 4.40 | 82.03 | 16.92 | 0.15 | 1927.73 |

Table D7. Reproduction (chronic toxicity) of water flea (*Ceriodaphnia dubia*) to leachates (filtered) of Enriched material. Control represents moderately hard water (MHW) treatment and TAL and TN are Talbingo and Tantangara Reservoir waters. First letter represents the geological zone Ravine (R), Byron (B), Shaw Gabbro (S), Volcanics (V), Peppercorn (P), Kellys Plain (K) and Felsic (F) respectively; Second letter Enriched (E) excavated rock; Third letter represents filtered (F) fraction of leachate.

| Total number of juveniles | | | | | | | | | | | Avg. | SD | p-value |
|---------------------------|----|----|----|----|----|----|----|----|----|----|------|----------|---------|
| | A | B | C | D | E | F | G | H | I | J | | | |
| MHW | 14 | 21 | 16 | 17 | 14 | 15 | 18 | 16 | 15 | 17 | 16.3 | 2.110819 | |
| TAL | 13 | 13 | 19 | 14 | 18 | 8 | 13 | 10 | 10 | 4 | 12.2 | 4.467164 | |
| TN | 11 | 14 | 16 | 17 | 17 | 17 | 18 | 16 | 12 | 12 | 15 | 2.538591 | |
| REF | 12 | 24 | 16 | 15 | 15 | 17 | 21 | 10 | 10 | 0 | 14 | 6.6 | |
| BEF | 18 | 12 | 17 | 10 | 10 | 18 | 14 | 14 | 12 | 11 | 13.6 | 3.1 | |
| SEF | 16 | 17 | 15 | 15 | 19 | 19 | 12 | 12 | 15 | 19 | 15.9 | 2.6 | |
| VEF | 14 | 22 | 18 | 14 | 15 | 0 | 0 | 12 | 13 | 15 | 12.3 | 7.1 | |
| PEF | 16 | 13 | 9 | 14 | 12 | 15 | 13 | 12 | 13 | 13 | 13 | 1.9 | |
| KEF | 12 | 10 | 0 | 18 | 9 | 13 | 10 | 10 | 6 | 8 | 9.6 | 4.7 | 0.01 |
| FEF | 15 | 14 | 9 | 16 | 9 | 14 | 20 | 15 | 30 | 21 | 16.3 | 6.2 | |

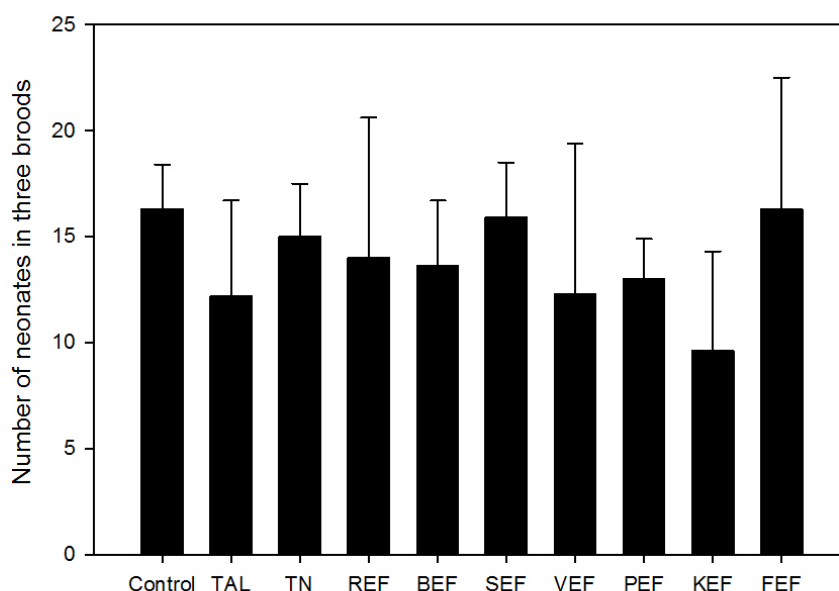


Figure D4. Reproduction (chronic toxicity) of the water flea (*Ceriodaphnia dubia*) to Enriched Filtered leachates. Control represents moderately hard water (MHW) treatment and TAL and TN are Talbingo and Tantangara Reservoir waters. First letter represents the geological zone Ravine (R), Byron (B), Shaw Gabbro (S), Volcanics (V), Peppercorn (P), Kellys Plain (K) and Felsic (F) respectively; Second letter represents Enriched (E) excavated rock; Third letter represents filtered (F) fraction of leachate.

Table D8. Copper test run with water flea (*Ceriodaphnia dubia*) during chronic toxicity tests.

| Treatment | After 24 hours | | | | After 48 hours | | | |
|-------------|----------------|---|---|---|----------------|---|---|---|
| | # Alive | | | | # Alive | | | |
| MHW Control | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| TAL | 5 | 5 | 5 | 4 | 5 | 5 | 5 | 4 |
| TN | 5 | 5 | 5 | 4 | 5 | 5 | 5 | 5 |
| Cu-5µg/l | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| Cu-10µg/l | 5 | 5 | 5 | 5 | 4 | 3 | 3 | 4 |
| Cu-20µg/l | 4 | 5 | 4 | 3 | 1 | 3 | 0 | 2 |

Table D9. The effective concentration (µg/L) of copper at 50%, 10% and 20% for cladocerans (*Ceriodaphnia dubia*) during chronic toxicity tests.

| | µg/l | 95% Conf. intervals | |
|------|-------|---------------------|-------|
| EC50 | 14.32 | 11.34 | 18.09 |
| EC10 | 6.40 | 3.90 | 10.52 |
| EC20 | 8.62 | 5.96 | 12.47 |

Table D10. Water quality data for the chronic (reproduction) toxicity tests with the water flea (*Ceriodaphnia dubia*). Control represents moderately hard water (MHW) treatment and TAL and TN are Talbingo and Tantangara Reservoir waters. Renewal of test solutions was done every second day.

| Water Quality at test completion | | | | | |
|----------------------------------|-----------|------|-------------|----------------------|------------------|
| Day | Treatment | pH | DO (% sat.) | Conductivity (µS/cm) | Temperature (°C) |
| 0 | MHW | 7.67 | 96 | 309 | 24.0 |
| | TAL | 7.39 | 104.1 | 25.4 | 24.0 |
| | TN | 7.62 | 102.5 | 28.1 | 24.0 |
| 2 | MHW | 7.64 | 95.5 | 319 | 24.0 |
| | TAL | 7.91 | 96.4 | 38 | 24.0 |
| | TN | 8.02 | 95.9 | 41.2 | 24.0 |
| 4 | MHW | 7.93 | 96.9 | 360 | 24.0 |
| | TAL | 7.98 | 97.8 | 35 | 24.0 |
| | TN | 7.98 | 97.3 | 36.9 | 24.0 |
| 6 | MHW | 7.67 | 96 | 309 | 24.0 |
| | TAL | 7.84 | 95.4 | 33.3 | 24.0 |
| | TN | 7.71 | 95.9 | 36.5 | 24.0 |
| 8 | MHW | 7.9 | 99.4 | 376 | 24.0 |
| | TAL | 7.23 | 99.8 | 39.6 | 24.0 |
| | TN | 7.27 | 100.9 | 61 | 24.0 |

Table D11. Water quality data for the chronic (reproduction) toxicity tests with the water flea (*Ceriodaphnia dubia*). Leachates (filtered) of Enriched material (renewal of test solution every second day). First letter represents the geological zone Ravine (R), Byron (B), Shaw Gabbro (S), Volcanics (V), Peppercorn (P), Kellys Plain (K) and Felsic (F) respectively; Second letter represents Enriched (E) excavated rock; Third letter represents filtered (F) fraction of leachate

| Day | Treatment | Water Quality | | | |
|-----|-----------|---------------|----------------|-------------------------|----------------------|
| | | pH | DO (% sat.) | Conductivity (µS/cm) | Temperature (° C) |
| 0 | REF | 7.9 | 96.1 | 109.4 | 24.0 |
| | BEF | 8.2 | 92.2 | 148.8 | 24.0 |
| | SEF | 8.1 | 97.8 | 85.1 | 24.0 |
| | VEF | 8.4 | 97.9 | 106.8 | 24.0 |
| | PEF | 7.9 | 94.5 | 104.9 | 24.0 |
| | KEF | 7.9 | 91.5 | 90.8 | 24.0 |
| | FEF | 8.0 | 91.2 | 115.8 | 24.0 |
| 2 | REF | 8.6 | 102.9 | 126.5 | 24.0 |
| | BEF | 8.7 | 106 | 163.6 | 24.0 |
| | SEF | 8.3 | 98.1 | 103.1 | 24.0 |
| | VEF | 8.5 | 98.6 | 122.7 | 24.0 |
| | PEF | 8.2 | 97.9 | 121.1 | 24.0 |
| | KEF | 8.7 | 104.5 | 111.3 | 24.0 |
| | FEF | 8.7 | 106.6 | 131.7 | 24.0 |
| 4 | REF | 8.4 | 98.6 | 122.5 | 24.0 |
| | BEF | 8.4 | 99 | 162.7 | 24 |
| | SEF | 8.3 | 96.1 | 94.9 | 24.0 |
| | VEF | 8.2 | 95.1 | 118.7 | 24.0 |
| | PEF | 8.3 | 98.4 | 117.1 | 24.0 |
| | KEF | 8.4 | 98.1 | 105.5 | 24.0 |
| | FEF | 8.2 | 99.6 | 131.8 | 24.0 |
| 6 | REF | 7.9 | 92.6 | 141.3 | 24.0 |
| | BEF | 7.2 | 93.3 | 191.4 | 24.0 |
| | SEF | 7.8 | 91.2 | 119.1 | 24.0 |
| | VEF | 7.5 | 91.8 | 146.7 | 24.0 |
| | PEF | 7.7 | 90.9 | 151.2 | 24.0 |
| | KEF | 7.7 | 92.2 | 122.6 | 24.0 |
| | FEF | 8.0 | 92.3 | 158.9 | 24.0 |
| 8 | REF | 7.8 | 106.8 | 151.5 | 24.0 |
| | BEF | 7.9 | 108.5 | 193.1 | 24.0 |
| | SEF | 7.8 | 107.6 | 134 | 24.0 |
| | VEF | 7.8 | 106.9 | 156.6 | 24.0 |
| | PEF | 7.9 | 107.3 | 169.2 | 24.0 |
| | KEF | 7.8 | 106.4 | 137.5 | 24.0 |
| | FEF | 7.9 | 106 | 188.5 | 24.0 |

Appendix E Leachates of excavated rock material: Supplementary information for the midge (*Chironomus tepperi dubia*) acute toxicity tests

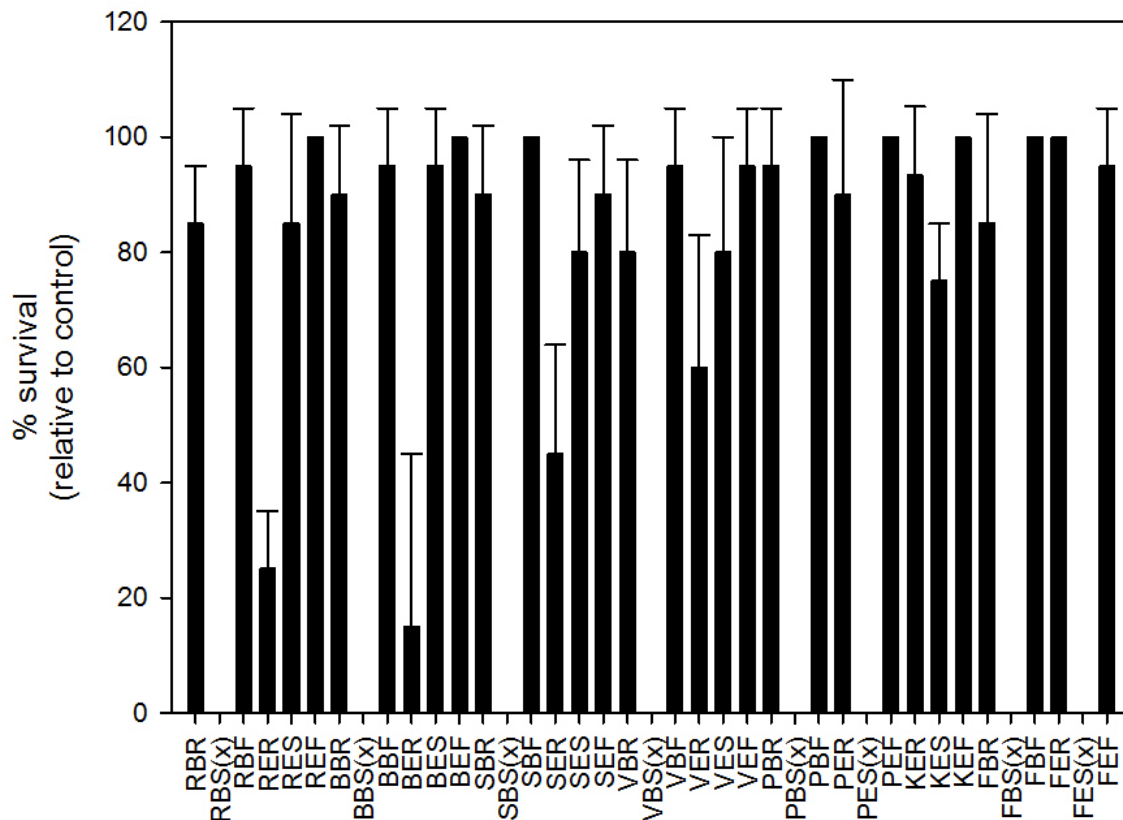


Figure E1. Summary data on survival (acute toxicity) of midges (*Chironomus tepperi*) for all leachates. Data expressed as relative to reservoir water control. (x) indicates sample was not tested. First letter represents the geological zone Ravine (R), Byron (B), Shaw Gabbro (S), Volcanics (V), Peppercorn (P), Kellys Plain (K) and Felsic (F) respectively; Second letter represents Baseline (B) or Enriched (E) excavated rock; Third letter represents raw (R), after 24 h settling (S) and filtered (F) fraction of leachate

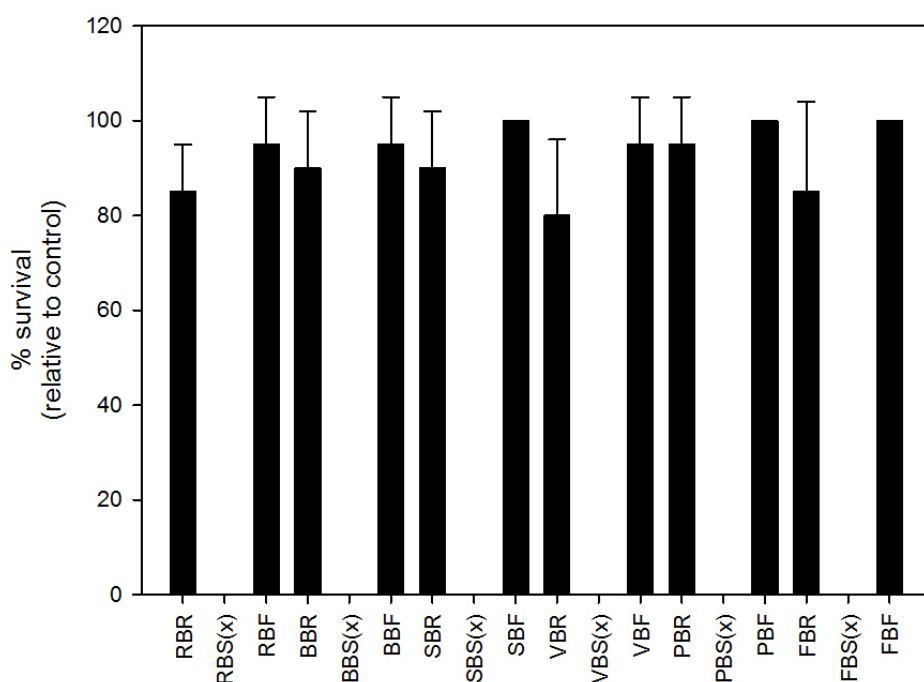


Figure E2. Summary data on survival (acute toxicity) of midges (*Chironomus tepperi*) for leachates of Baseline material. Data expressed as relative to reservoir water control. (x) indicates sample was not tested. First letter represents the geological zone Ravine (R), Byron (B), Shaw Gabbro (S), Volcanics (V), Peppercorn (P), Kellys Plain (K) and Felsic (F) respectively; Second letter represents Baseline (B) excavated rock; Third letter represents raw (R), after 24 h settling (S) and filtered (F) fraction of leachate

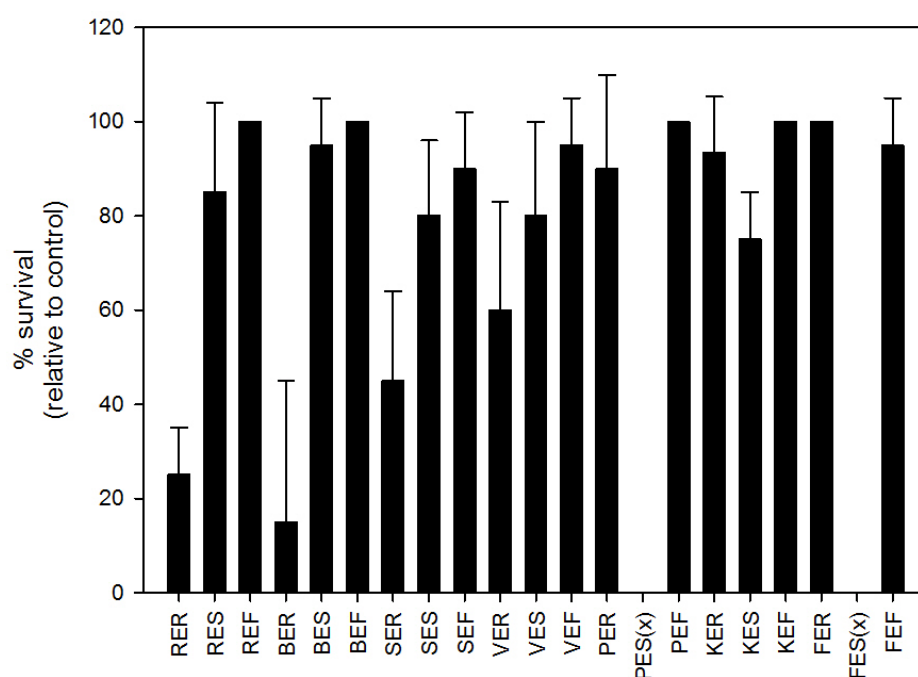


Figure E3. Summary data on survival (acute toxicity) of midges (*Chironomus tepperi*) for leachates of Enriched material. Data expressed as relative to reservoir water control. (x) indicates sample was not tested. First letter represents the geological zone Ravine (R), Byron (B), Shaw Gabbro (S), Volcanics (V), Peppercorn (P), Kellys Plain (K) and Felsic (F) respectively; Second letter Enriched (E) excavated rock; Third letter represents raw (R), after 24 h settling (S) and filtered (F) fraction of leachate

Table E1. Supplementary survival data (acute toxicity) data for midges (*Chironomus tepperi*) toxicity tests for all leachates. NA sample not analysed. First letter represents the geological zone Ravine (R), Byron (B), Shaw Gabbro (S), Volcanics (V), Peppercorn (P), Kellys Plain (K) and Felsic (F) respectively; Second letter represents Baseline (B) or Enriched (E) excavated rock; Third letter represents raw (R), after 24 h settling (S) and filtered (F) fraction of leachate

| Total survival out of 5 after 48 hrs | | | | | | | |
|--------------------------------------|----|---|---|---|------|-----|---------|
| | A | B | C | D | Avg. | SD | p-value |
| Control | 5 | 5 | 5 | 5 | 5.0 | 0.0 | |
| RBR | 5 | 4 | 4 | 4 | 4.3 | 0.5 | |
| RBS | NA | | | | | | |
| RBF | 5 | 4 | 5 | 5 | 4.8 | 0.5 | |
| RER | 1 | 1 | 1 | 2 | 1.3 | 0.5 | <0.001 |
| RES | 3 | 5 | 5 | 4 | 4.3 | 1.0 | |
| REF | 5 | 5 | 5 | 5 | 5.0 | 0.0 | |
| BBR | 5 | 4 | 4 | 5 | 4.5 | 0.6 | |
| BBS | NA | | | | | | |
| BBF | 4 | 5 | 5 | 5 | 4.8 | 0.5 | |
| BER | 0 | 0 | 3 | 0 | 0.8 | 1.5 | <0.001 |
| BES | 5 | 5 | 5 | 4 | 4.8 | 0.5 | |
| BEF | 5 | 5 | 5 | 5 | 5.0 | 0.0 | |
| SBR | 5 | 4 | 4 | 5 | 4.5 | 0.6 | |
| SBS | NA | | | | | | |
| SBF | 5 | 5 | 5 | 5 | 5.0 | 0.0 | |
| SER | 1 | 3 | 3 | 2 | 2.3 | 1.0 | <0.001 |
| SES | 4 | 3 | 5 | 4 | 4.0 | 0.8 | |
| SEF | 4 | 5 | 4 | 5 | 4.5 | 0.6 | |
| VBR | 4 | 5 | 4 | 3 | 4.0 | 0.8 | |
| VBS | NA | | | | | | |
| VBF | 4 | 5 | 5 | 5 | 4.8 | 0.5 | |
| VER | 4 | 2 | 2 | 4 | 3.0 | 1.2 | <0.001 |
| VES | 2 | 5 | 4 | 3 | 3.5 | 1.3 | |
| VEF | 5 | 4 | 5 | 5 | 4.8 | 0.5 | |
| PBR | 4 | 5 | 5 | 5 | 4.8 | 0.5 | |
| PBS | NA | | | | | | |
| PBF | 5 | 5 | 5 | 5 | 5.0 | 0.0 | |
| PER | 5 | 3 | 5 | 5 | 4.5 | 1.0 | |
| PES | NA | | | | | | |
| PEF | 5 | 5 | 5 | 5 | 5.0 | 0.0 | |
| KER | 5 | 5 | 4 | 5 | 4.8 | 0.5 | |
| KES | 4 | 4 | 3 | 4 | 3.8 | 0.5 | 0.001 |
| KEF | 5 | 5 | 5 | 5 | 5.0 | 0.0 | |
| FBR | 5 | 4 | 5 | 3 | 4.3 | 1.0 | |
| FBS | NA | | | | | | |
| FBF | 5 | 5 | 5 | 5 | 5.0 | 0.0 | |
| FER | 5 | 5 | 5 | 5 | 5.0 | 0.0 | |
| FES | NA | | | | | | |
| FEF | 5 | 5 | 5 | 4 | 4.8 | 0.5 | |

Table E2. Supplementary water quality data for the acute (survival) toxicity tests with the midge (*Chironomus tepperi*). NA indicates sample not analysed. First letter represents the geological zone Ravine (R), Byron (B), Shaw Gabbro (S), Volcanics (V), Peppercorn (P), Kellys Plain (K) and Felsic (F) respectively; Second letter represents Baseline (B) or Enriched (E) excavated rock; Third letter represents raw (R), after 24 h settling (S) and filtered (F) fraction of leachate

| Treatment | Water Quality at test completion | | | |
|-----------|----------------------------------|----------------|---|---------------------------------------|
| | pH | DO (% sat.) | Conductivity ($\mu\text{S}/\text{cm}$) | Temperature ($^{\circ}\text{C}$) |
| RBR | 8.1 | 85.2 | 120.9 | 24.0 |
| RBS | NA | | | |
| RBF | 7.9 | 90.1 | 93.3 | 24.0 |
| RER | 7.9 | 86.1 | 157.2 | 24.0 |
| RES | 7.8 | 95.3 | 152.4 | 24.0 |
| REF | 7.9 | 91.4 | 148.7 | 24.0 |
| BBR | 8.0 | 85.2 | 192.5 | 24.0 |
| BBS | NA | | | |
| BBF | 7.9 | 91.1 | 135.2 | 24.0 |
| BER | 7.8 | 84.0 | 244.0 | 24.0 |
| BES | 7.8 | 94.1 | 218.3 | 24.0 |
| BEF | 8.0 | 92.2 | 189.6 | 24.0 |
| SBR | 7.7 | 93.0 | 170.3 | 24.0 |
| SBS | NA | | | |
| SBF | 7.9 | 90.0 | 102.8 | 24.0 |
| SER | 7.9 | 86.8 | 144.2 | 24.0 |
| SES | 7.8 | 95.6 | 122.8 | 24.0 |
| SEF | 7.9 | 91.8 | 120.3 | 24.0 |
| VBR | 8.2 | 86.6 | 158.0 | 24.0 |
| VBS | NA | | | |
| VBF | 7.9 | 90.5 | 109.0 | 24.0 |
| VER | 7.9 | 89.6 | 120.2 | 24.0 |
| VES | 7.8 | 94.5 | 134.4 | 24.0 |
| VEF | 7.9 | 91.7 | 132.7 | 24.0 |
| PBR | 7.4 | 89.9 | 165.0 | 24.0 |
| PBS | NA | | | |
| PBF | 7.9 | 90.3 | 85.1 | 24.0 |
| PER | 7.9 | 85.4 | 164.2 | 24.0 |
| PES | NA | | | |
| PEF | 7.9 | 91.7 | 144.5 | 24.0 |
| KER | 7.7 | 93.0 | 144.7 | 24.0 |
| KES | 7.8 | 94.9 | 138.4 | 24.0 |
| KEF | 7.9 | 92.1 | 130.9 | 24.0 |
| FBR | 8.1 | 85.8 | 148.8 | 24.0 |
| FBS | NA | | | |
| FBF | 7.9 | 91.6 | 100.0 | 24.0 |
| FER | 8.0 | 85.9 | 191.8 | 24.0 |
| FES | NA | | | |
| FEF | 8.0 | 91.9 | 152.9 | 24.0 |

Table E3. Acute toxicity of reservoir water samples to the midge, *Chironomus tepperi*

| | Total survival out of 5 after 48 hrs | | | | | | Water Quality at test completion | | | |
|----------|--------------------------------------|---|---|---|------|------|----------------------------------|-------------|----------------------|-------------------|
| | A | B | C | D | Avg. | SD | pH | DO (% sat.) | Conductivity (µS/cm) | Temperature (° C) |
| TN3 | 5 | 5 | 5 | 5 | 5 | 0 | 7.7 | 87.8 | 40.5 | 21 |
| TN2 | 5 | 5 | 5 | 3 | 4.5 | 1.00 | 7.6 | 87.0 | 40.5 | 21 |
| TN1 | 4 | 4 | 4 | 5 | 4.25 | 0.50 | 7.7 | 87.2 | 40.2 | 21 |
| TAL-PL2C | 4 | 5 | 4 | 5 | 4.5 | 0.58 | 7.7 | 87.6 | 41.7 | 21 |
| TAL-PL1C | 4 | 4 | 4 | 5 | 4.25 | 0.50 | 7.8 | 87.2 | 37.9 | 21 |
| TAL-PL2D | 5 | 5 | 4 | 5 | 4.75 | 0.50 | 7.9 | 87.4 | 34.3 | 21 |
| TAL-PL1D | 5 | 4 | 4 | 5 | 4.5 | 0.58 | 7.7 | 87.0 | 42.9 | 21 |

Table E4. Low electrical conductivity (EC) related acute toxicity to the midge, *Chironomus tepperi*

| | Total survival out of 5 after 48 hrs | | | | | | Water Quality at test completion | | | |
|-----------|--------------------------------------|---|---|---|------|------|----------------------------------|-------------|----------------------|-------------------|
| | A | B | C | D | Avg. | SD | pH | DO (% sat.) | Conductivity (µS/cm) | Temperature (° C) |
| MHW | 5 | 5 | 5 | 4 | 4.75 | 0.5 | 7.59 | 88.8 | 312 | 21 |
| 6.25% MHW | 5 | 5 | 4 | 4 | 4.5 | 0.58 | 7.8 | 89.8 | 35.3 | 21 |
| 12.5% MHW | 5 | 5 | 5 | 5 | 5 | 0 | 7.78 | 88.8 | 59 | 21 |
| 25% MHW | 5 | 5 | 5 | 4 | 4.75 | 0.5 | 7.81 | 87.8 | 97.5 | 21 |
| 50% MHW | 5 | 5 | 5 | 4 | 4.75 | 0.5 | 7.76 | 87.2 | 172.8 | 21 |
| 75% MHW | 5 | 5 | 5 | 5 | 5 | 0 | 7.72 | 87.4 | 241 | 21 |
| 100% MHW | 5 | 5 | 5 | 5 | 5 | 0 | 7.59 | 88.8 | 312 | 21 |

Table E5. Low electrical conductivity (EC) as sodium chloride related acute toxicity to the midge, *Chironomus tepperi*

| Concentration of NaCl | After 48 hours # Alive | | | | | | Water Quality at test completion | | | |
|-----------------------|------------------------|---|---|---|------|-----|----------------------------------|-------|----------------------|-------------------|
| | A | B | C | D | Avg. | SD | pH | DO | Conductivity (µS/cm) | Temperature (° C) |
| MHW | 5 | 5 | 5 | 5 | 5 | 0 | 7.79 | 117.3 | 321 | 21 |
| 125mg/l | 5 | 5 | 5 | 5 | 5 | 0 | 7.53 | 89.5 | 55.7 | 21 |
| 250mg/l | 5 | 5 | 5 | 4 | 4.75 | 0.5 | 7.62 | 89.4 | 79.0 | 21 |
| 500mg/l | 5 | 5 | 5 | 4 | 4.75 | 0.5 | 7.73 | 89.7 | 127.3 | 21 |
| 1000mg/l | 5 | 5 | 5 | 5 | 5 | 0 | 7.79 | 89.7 | 238.0 | 21 |
| 2000mg/l | 5 | 4 | 5 | 5 | 4.75 | 0.5 | 7.75 | 90.8 | 468.0 | 21 |

Table E6. Copper test run with the midge (*Chironomus tepperi*) during acute toxicity tests with leachates.

| | After 24 hours | | | After 48 hours | | |
|--------------|----------------|---|---|----------------|---|---|
| | # Alive | | | # Alive | | |
| MHW | 5 | 5 | 5 | 4 | 5 | 5 |
| TAL | 4 | 3 | 4 | 4 | 3 | 4 |
| Cu-31.25µg/l | 5 | 5 | 5 | 5 | 5 | 5 |
| Cu-62.5µg/l | 6 | 5 | 4 | 5 | 4 | 3 |
| Cu-125µg/l | 3 | 4 | 5 | 2 | 1 | 1 |
| Cu-250µg/l | 5 | 4 | 3 | 3 | 0 | 1 |
| Cu-500µg/l | 4 | 2 | 2 | 1 | 0 | 0 |

Table E7. The effective concentration (µg/L) of copper at 50%, 10% and 20% for the midge (*Chironomus tepperi*) during acute toxicity tests with leachates.

| | µg/l | 95% Conf. intervals | |
|------|--------|---------------------|--------|
| EC50 | 102.66 | 71.81 | 146.77 |
| EC10 | 38.12 | 17.62 | 82.45 |
| EC20 | 54.94 | 31.76 | 95.05 |

Appendix F Leachates of excavated rock material: Supplementary information for blackworm (*Lumbriculus variegatus*) acute tests

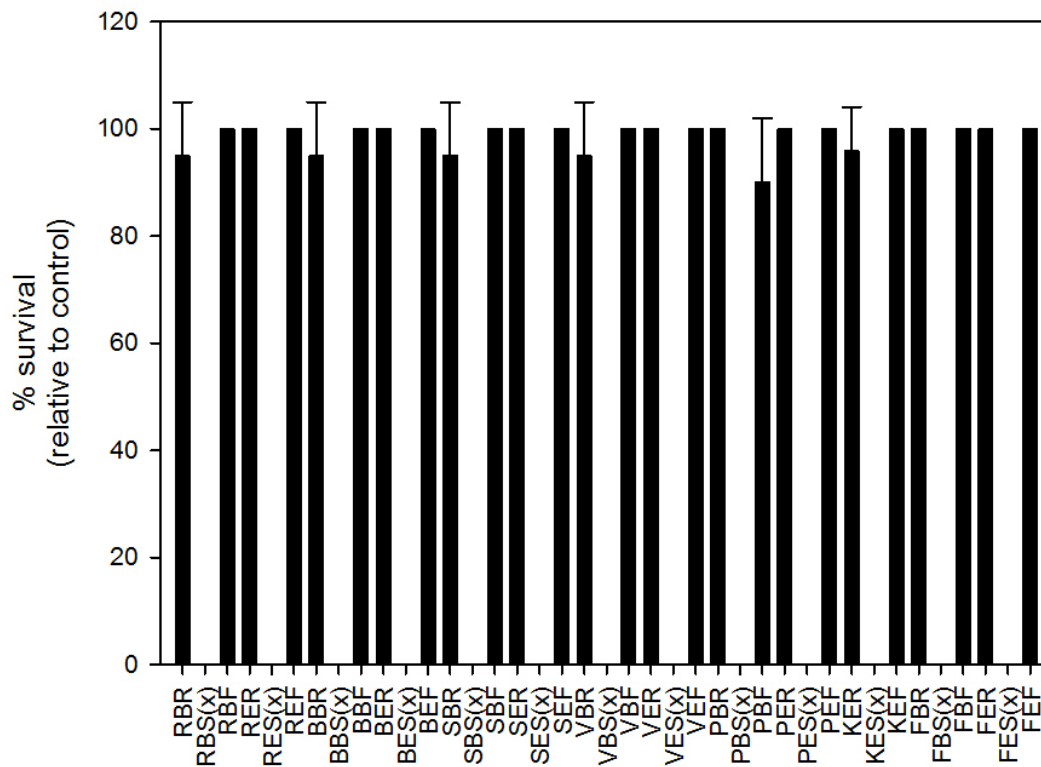


Figure F1. Summary data on survival (acute toxicity) of the blackworm (*Lumbriculus variegatus*) for all leachates. Data expressed as relative to reservoir water control. (x) indicates sample was not tested.. First letter represents the geological zone Ravine (R), Byron (B), Shaw Gabbro (S), Volcanics (V), Peppercorn (P), Kellys Plain (K) and Felsic (F) respectively; Second letter represents Baseline (B) or Enriched (E) excavated rock; Third letter represents raw (R), after 24 h settling (S) and filtered (F) fraction of leachate

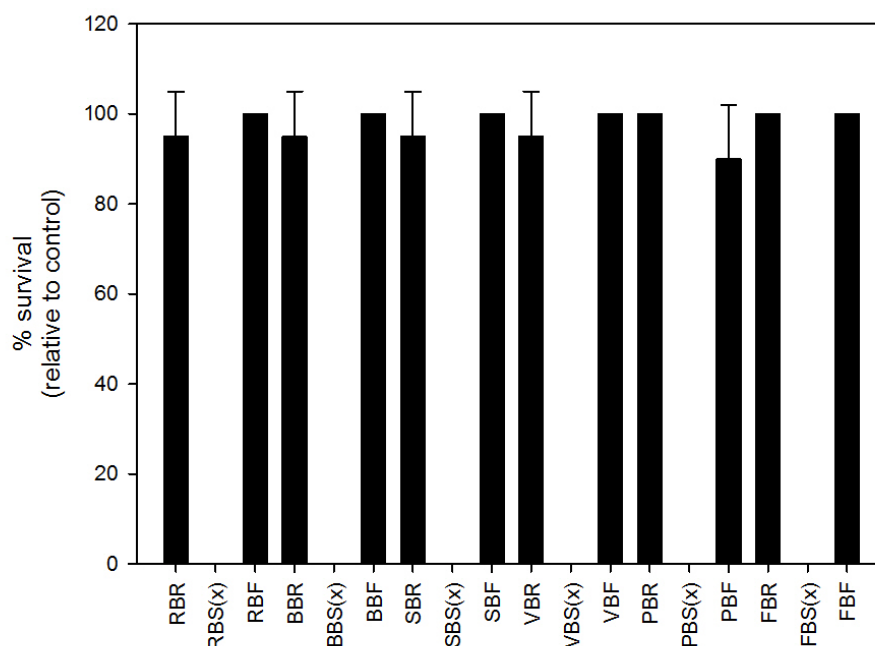


Figure F2. Summary data on survival (acute toxicity) of blackworm (*Lumbriculus variegatus*) for leachates of Baseline material. Data expressed as relative to reservoir water control. (x) indicates sample was not tested. First letter represents the geological zone Ravine (R), Byron (B), Shaw Gabbro (S), Volcanics (V), Peppercorn (P), Kellys Plain (K) and Felsic (F) respectively; Second letter represents Baseline (B) excavated rock; Third letter represents raw (R), after 24 h settling (S) and filtered (F) fraction of leachate

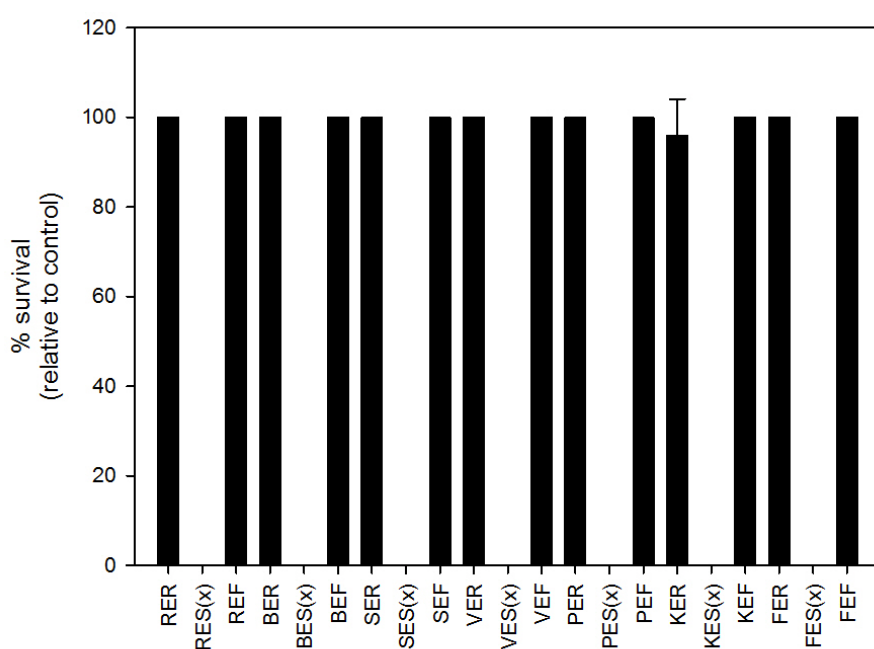


Figure F3. Summary data on survival (acute toxicity) of blackworm (*Lumbriculus variegatus*) for leachates of Enriched material. Data expressed as relative to reservoir water control. (x) indicates sample was not tested. First letter represents the geological zone Ravine (R), Byron (B), Shaw Gabbro (S), Volcanics (V), Peppercorn (P), Kellys Plain (K) and Felsic (F) respectively; Second letter represents Enriched (E) excavated rock; Third letter represents raw (R), after 24 h settling (S) and filtered (F) fraction of leachate

Table F1. Summary of survival (acute toxicity) data for blackworm (*Lumbriculus variegatus*) toxicity tests for all leachates. NA indicates sample not analysed.. First letter represents the geological zone Ravine (R), Byron (B), Shaw Gabbro (S), Volcanics (V), Peppercorn (P), Kellys Plain (K) and Felsic (F) respectively; Second letter represents Baseline (B) or Enriched (E) excavated rock; Third letter represents raw (R), after 24 h settling (S) and filtered (F) fraction of leachate

| Total survival out of 5 after 48 hrs | | | | | | | p-value |
|--------------------------------------|----|---|---|---|------|-----|---------|
| | A | B | C | D | Avg. | SD | |
| Control | 5 | 5 | 5 | 5 | 5 | 0 | |
| RBR | 5 | 5 | 5 | 5 | 5 | 0 | |
| RBS | NA | | | | | | |
| RBF | 5 | 5 | 5 | 5 | 5 | 0 | |
| RER | 5 | 5 | 5 | 5 | 5 | 0 | |
| RES | NA | | | | | | |
| REF | 5 | 5 | 5 | 5 | 5 | 0 | |
| BBR | 5 | 5 | 4 | 5 | 4.75 | 0.5 | |
| BBS | NA | | | | | | |
| BBF | 5 | 5 | 5 | 5 | 5 | 0 | |
| BER | 5 | 5 | 5 | 5 | 5 | 0 | |
| BES | NA | | | | | | |
| BEF | 5 | 5 | 5 | 5 | 5 | 0 | |
| SBR | 5 | 4 | 5 | 5 | 4.75 | 0.5 | |
| SBS | NA | | | | | | |
| SBF | 5 | 5 | 5 | 5 | 5 | 0 | |
| SER | 5 | 5 | 5 | 5 | 5 | 0 | |
| SES | NA | | | | | | |
| SEF | 5 | 5 | 5 | 5 | 5 | 0 | |
| VBR | 5 | 5 | 4 | 5 | 4.75 | 0.5 | |
| VBS | NA | | | | | | |
| VBF | 5 | 5 | 5 | 5 | 5 | 0 | |
| VER | 5 | 5 | 5 | 5 | 5 | 0 | |
| VES | NA | | | | | | |
| VEF | 5 | 5 | 5 | 5 | 5 | 0 | |
| PBR | 5 | 5 | 5 | 5 | 5 | 0 | |
| PBS | NA | | | | | | |
| PBF | 5 | 4 | 4 | 5 | 4.5 | 0.6 | |
| PER | 5 | 5 | 5 | 5 | 5 | 0 | |
| PES | NA | | | | | | |
| PEF | 5 | 5 | 5 | 5 | 5 | 0 | |
| KER | 5 | 5 | 5 | 5 | 5 | 0 | |
| KES | NA | | | | | | |
| KEF | 5 | 5 | 5 | | 5 | 0 | |
| FBR | 5 | 5 | 5 | 5 | 5 | 0 | |
| FBS | NA | | | | | | |
| FBF | 5 | 5 | 5 | 5 | 5 | 0 | |
| FER | 5 | 5 | 5 | 5 | 5 | 0 | |
| FES | NA | | | | | | |
| FEF | 5 | 5 | 5 | 5 | 5 | 0 | |

Table F2. Supplementary water quality data for the acute (survival) toxicity tests with the blackworm (*Lumbriculus variegatus*). NA indicates sample not analysed. First letter represents the geological zone Ravine (R), Byron (B), Shaw Gabbro (S), Volcanics (V), Peppercorn (P), Kellys Plain (K) and Felsic (F) respectively; Second letter represents Baseline (B) or Enriched (E) excavated rock; Third letter represents raw (R), after 24 h settling (S) and filtered (F) fraction of leachate.

| Treatment | Water Quality at test completion | | | |
|-----------|----------------------------------|----------------|-------------------------------|----------------------|
| | pH | DO (% sat.) | Conductivity (μ S/cm) | Temperature (° C) |
| RBR | 7.7 | 77.4 | 121.8 | 24.0 |
| RBS | NA | | | |
| RBF | 7.2 | 91.3 | 113.8 | 24.0 |
| RER | 7.8 | 90.7 | 162.7 | 24.0 |
| RES | NA | | | |
| REF | 7.8 | 93.7 | 144.2 | 24.0 |
| BBR | 7.6 | 81.3 | 191.6 | 24.0 |
| BBS | NA | | | |
| BBF | 7.1 | 87.2 | 162.5 | 24.0 |
| BER | 8.1 | 85.3 | 256.0 | 24.0 |
| BES | NA | | | |
| BEF | 7.9 | 95.0 | 206.3 | 24.0 |
| SBR | 7.9 | 81.4 | 158.2 | 24.0 |
| SBS | NA | | | |
| SBF | 7.4 | 91.6 | 117.7 | 24.0 |
| SER | 7.7 | 88.6 | 151.2 | 24.0 |
| SES | NA | | | |
| SEF | 7.8 | 94.1 | 108.5 | 24.0 |
| VBR | 7.9 | 74.6 | 163.5 | 24.0 |
| VBS | NA | | | |
| VBF | 7.4 | 89.5 | 119.5 | 24.0 |
| VER | 7.8 | 92.5 | 126.6 | 24.0 |
| VES | NA | | | |
| VEF | 7.7 | 93.8 | 132.6 | 24.0 |
| PBR | 7.8 | 76.4 | 132.5 | 24.0 |
| PBS | NA | | | |
| PBF | 7.2 | 89.9 | 102.3 | 24.0 |
| PER | 7.7 | 90.7 | 172.0 | 24.0 |
| PES | NA | | | |
| PEF | 7.8 | 93.7 | 143.0 | 24.0 |
| KER | 7.9 | 92.0 | 150.6 | 24.0 |
| KES | NA | | | |
| KEF | 7.8 | 94.3 | 148.8 | 24.0 |
| FBR | 7.8 | 77.0 | 155.5 | 24.0 |
| FBS | NA | | | |
| FBF | 7.2 | 88.7 | 111.5 | 24.0 |
| FER | 8.1 | 89.3 | 215.7 | 24.0 |
| FES | NA | | | |
| FEF | 7.8 | 94.1 | 178.7 | 24.0 |

Table F3. Acute toxicity of Tantangara and Talbingo Reservoir water samples to the blackworm, *Lumbriculus variegatus*.

| | Total survival out of 5 after 48 hrs | | | | | | Water Quality at test completion | | | |
|----------|--------------------------------------|---|---|---|------|----|----------------------------------|----------------|-------------------------------|----------------------|
| | A | B | C | D | Avg. | SD | pH | DO (% sat.) | Conductivity (μ S/cm) | Temperature (° C) |
| TN3 | 5 | 5 | 5 | 5 | 5 | 0 | 7.26 | 83.8 | 52.6 | 21 |
| TN2 | 5 | 5 | 5 | 5 | 5 | 0 | 7.22 | 82.0 | 56.2 | 21 |
| TN1 | 5 | 5 | 5 | 5 | 5 | 0 | 7.19 | 83.8 | 55.1 | 21 |
| TAL-PL2C | 5 | 5 | 3 | 5 | 4.5 | 1 | 7.16 | 81.8 | 48.4 | 21 |
| TAL-PL1C | 5 | 5 | 5 | 5 | 5 | 0 | 7.15 | 81.2 | 59.1 | 21 |
| TAL-PL2D | 5 | 5 | 5 | 5 | 5 | 0 | 7.17 | 81.3 | 51.7 | 21 |
| TAL-PL1D | 5 | 5 | 5 | 5 | 5 | 0 | 7.15 | 81.8 | 57.2 | 21 |

Table F4. Low electrical conductivity (EC) related acute toxicity to the blackworm, *Lumbriculus variegatus*.

| | A | B | C | Avg. | SD | pH | DO (% sat.) | Conductivity (μ S/cm) | Temperature (° C) |
|-----------|---|---|---|------|----|------|----------------|-------------------------------|----------------------|
| MHW | 5 | 5 | 5 | 5 | 0 | 7.47 | 88.8 | 323 | 21 |
| 0.78% MHW | 5 | 5 | 5 | 5 | 0 | 7.21 | 91.5 | 15.98 | 21 |
| 1.56%MHW | 5 | 5 | 5 | 5 | 0 | 6.96 | 88.1 | 20.02 | 21 |
| 6.25% MHW | 5 | 5 | 5 | 5 | 0 | 6.87 | 87.3 | 26.2 | 21 |
| 12.5% MHW | 5 | 5 | 5 | 5 | 0 | 6.89 | 87.5 | 37.1 | 21 |
| 25% MHW | 5 | 5 | 5 | 5 | 0 | 7.06 | 86 | 62.6 | 21 |
| 50% MHW | 5 | 5 | 5 | 5 | 0 | 7.07 | 84.5 | 101 | 21 |
| 75% MHW | 5 | 5 | 5 | 5 | 0 | 7.22 | 86 | 172.8 | 21 |
| 100% MHW | 5 | 5 | 5 | 5 | 0 | 7.46 | 87.3 | 324 | 21 |

Table F5. Copper reference toxicity tests with the blackworm (*Lumbriculus variegatus*) during acute toxicity tests with leachates.

| Treatment | After 24 hours | | | After 48 hours | | |
|--------------|----------------|---|---|----------------|---|---|
| | # Alive | | | # Alive | | |
| MHW | 5 | 5 | 5 | 5 | 5 | 5 |
| TAL | 5 | 5 | 5 | 5 | 5 | 5 |
| Cu125-µg/l | 5 | 5 | 5 | 5 | 4 | 5 |
| Cu 250-µg/l | 5 | 4 | 4 | 3 | 4 | 2 |
| Cu 500-µg/l | 1 | 0 | 0 | 1 | 1 | 1 |
| Cu 1000-µg/l | 0 | 0 | 0 | 0 | 0 | 0 |
| Cu 2000-µg/l | 0 | 0 | 0 | 0 | 0 | 0 |

Table F6. The effective concentration (µg/l) of copper at 50%, 10% and 20% for blackworm (*Lumbriculus variegatus*) during acute toxicity tests with leachates.

| | µg/l | 95% Conf. intervals | |
|------|--------|---------------------|--------|
| EC50 | 293.81 | 250.78 | 344.23 |
| EC10 | 135.63 | 97.10 | 189.44 |
| EC20 | 180.41 | 140.22 | 232.10 |

Appendix G Excavated rock material in sediments: Supplimentary information on midge (*Chironomus tepperi*) toxicity tests

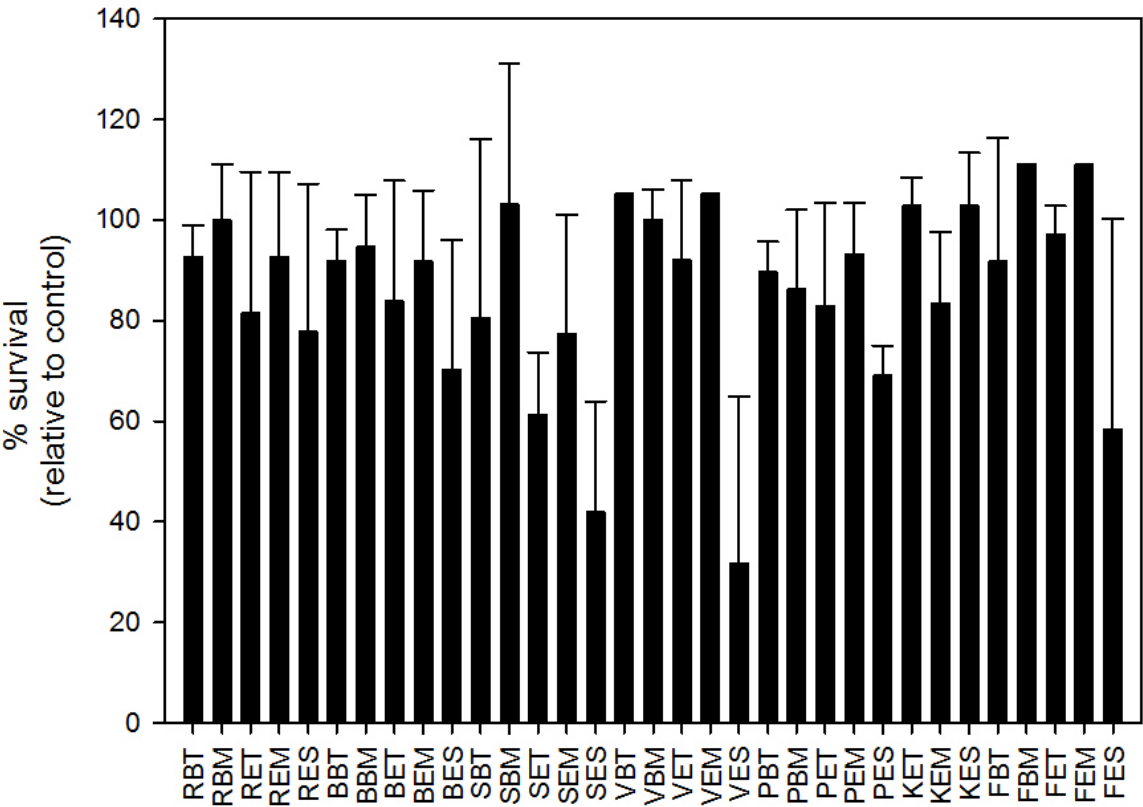


Figure G1. % Survival of midges (*Chironomus tepperi*) after 7-day exposure to excavated rock from seven geological zones (Abbreviations for treatments in Table G1)

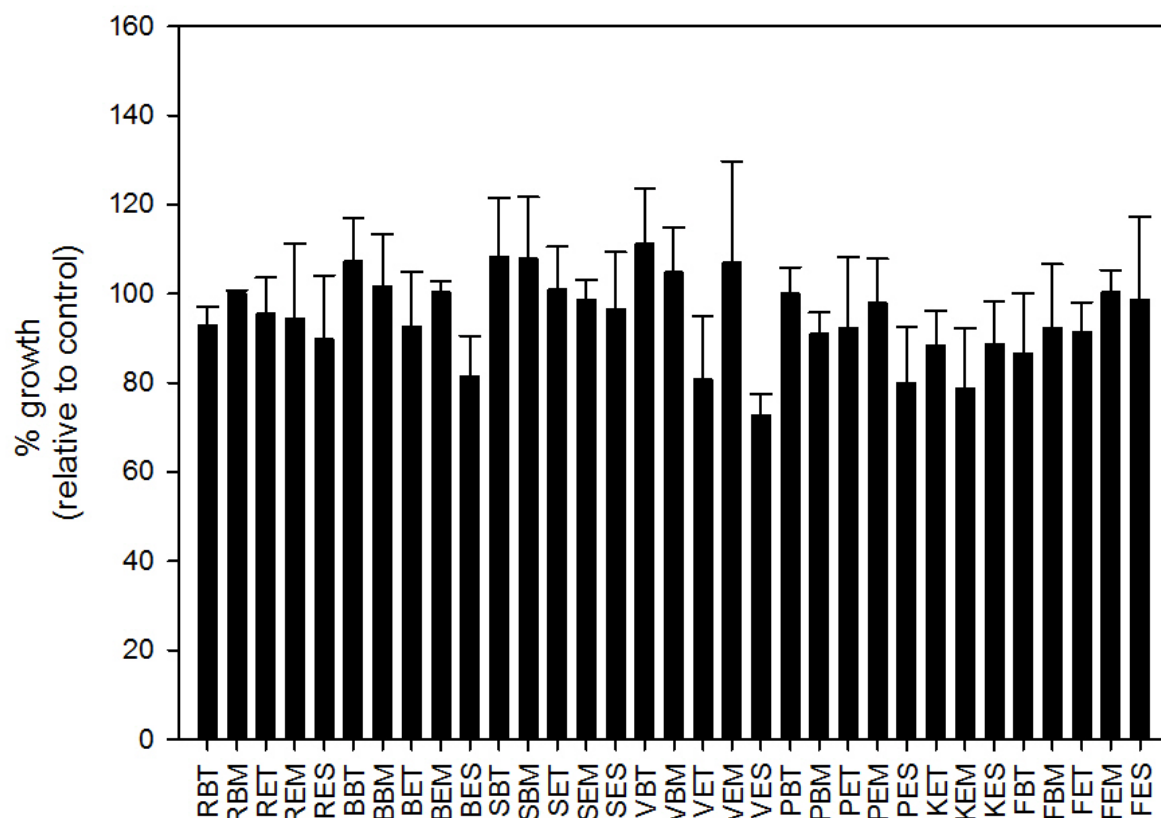


Figure G2. % Growth of midges (*Chironomus tepperi*) after 7-day exposure to excavated rock from seven geological zones (Abbreviations for treatments in Table G1)

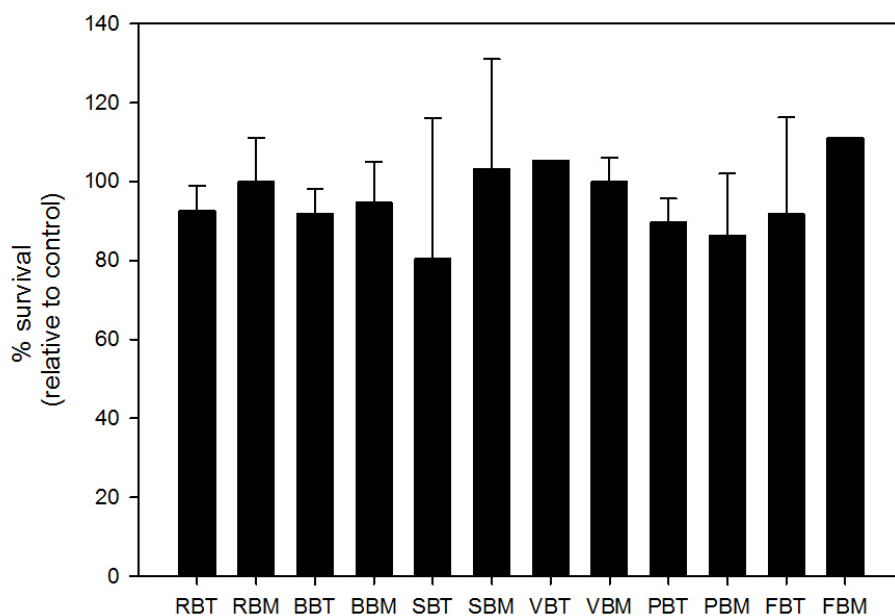


Figure G3. % Survival of midges (*Chironomus tepperi*) after 7-day exposure to Baseline excavated rock from seven geological zones (Abbreviations for treatments in Table G1)

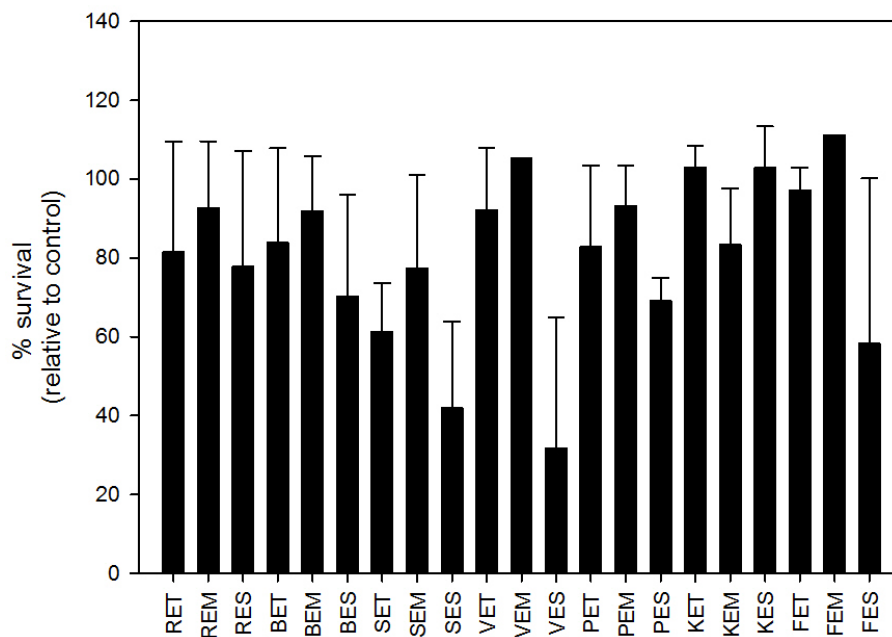


Figure G4. % Survival of midges (*Chironomus tepperi*) after 7-day exposure to Enriched excavated rock from seven geological zones (Abbreviations for treatments in Table G1)

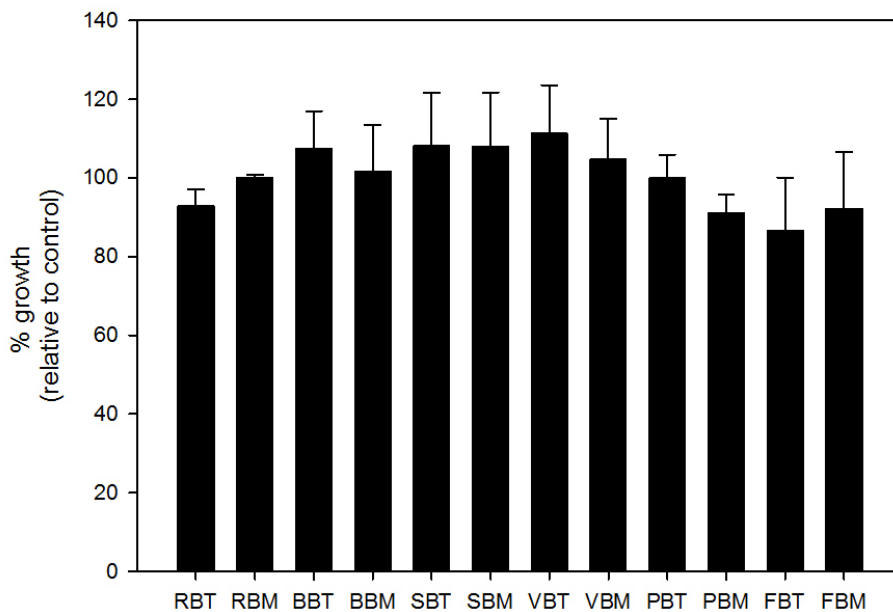


Figure G5. % Growth of midges (*Chironomus tepperi*) after 7-day exposure to Baseline excavated rock from seven geological zones (Abbreviations for treatments in Table G1)

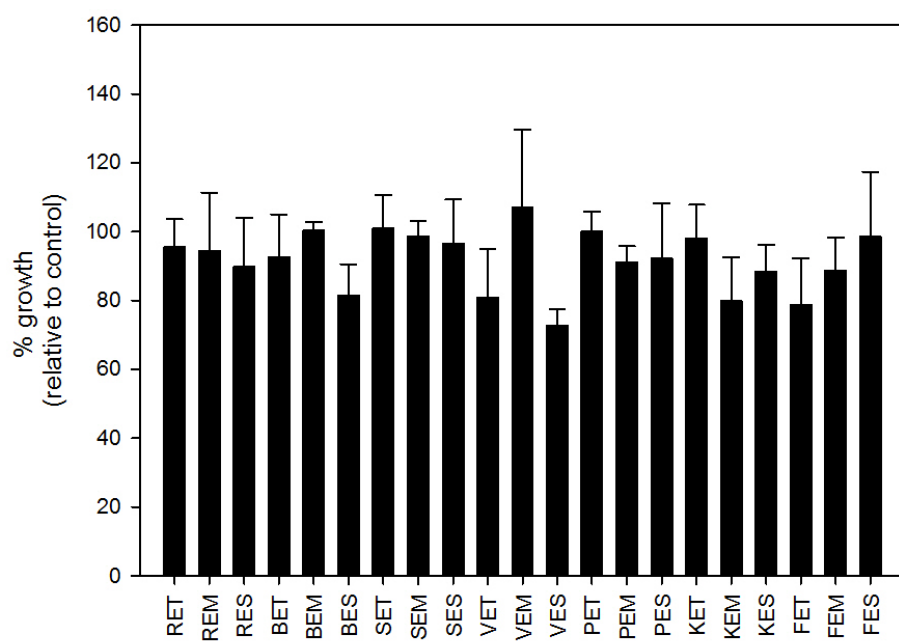


Figure G6. % Growth of midges (*Chironomus tepperi*) after 7-day exposure to Enriched excavated rock from seven geological zones (Abbreviations for treatments in Table G1)

Table G1. Supplementary survival data from midge sediment-excavated rock tests for seven geological zones.

| Total survival out of 10 after 7 days | | | | | | | | | |
|---------------------------------------|---------|----|----|----|-------------|------|--------|---|---------|
| | # Alive | | | | Total Alive | Avg | St.Dev | n | p-value |
| | A | B | C | D | | | | | |
| CONTROL | 10 | 7 | 10 | - | 27 | 9.0 | 1.7 | 3 | |
| RBT | 9 | 8 | 8 | - | 25 | 8.3 | 0.6 | 3 | |
| RBM | 9 | 10 | 8 | - | 27 | 9.0 | 1.0 | 3 | |
| RET | 10 | 5 | 7 | - | 22 | 7.3 | 2.5 | 3 | |
| REM | 8 | 7 | 10 | - | 25 | 8.3 | 1.5 | 3 | |
| RES | 9 | 4 | 8 | - | 21 | 7.0 | 2.6 | 3 | |
| CONTROL | 10 | 7 | 10 | 10 | 37 | 9.3 | 1.5 | 4 | |
| BBT | 9 | 8 | 8 | 9 | 34 | 8.5 | 0.6 | 4 | |
| BBM | 9 | 10 | 8 | 8 | 35 | 8.8 | 1.0 | 4 | |
| BET | 10 | 5 | 7 | 9 | 31 | 7.8 | 2.2 | 4 | |
| BEM | 8 | 7 | 10 | 9 | 34 | 8.5 | 1.3 | 4 | |
| BES | 9 | 4 | 8 | 5 | 26 | 6.5 | 2.4 | 4 | |
| CONTROL | 7 | 7 | 7 | 10 | 31 | 7.8 | 1.5 | 4 | |
| SBT | 9 | 3 | 8 | 5 | 25 | 6.3 | 2.8 | 4 | |
| SBM | 8 | 9 | 5 | 10 | 32 | 8.0 | 2.2 | 4 | |
| SET | 6 | 4 | 5 | 4 | 19 | 4.8 | 1.0 | 4 | |
| SEM | 7 | 8 | 4 | 5 | 24 | 6.0 | 1.8 | 4 | |
| SES | 3 | 5 | 4 | 1 | 13 | 3.3 | 1.7 | 4 | 0.015 |
| CONTROL | 10 | 10 | 10 | 8 | 38 | 9.5 | 1.0 | 4 | |
| VBT | 10 | 10 | 10 | 10 | 40 | 10.0 | 0.0 | 4 | |
| VBM | 9 | 9 | 10 | 10 | 38 | 9.5 | 0.6 | 4 | |
| VET | 7 | 8 | 10 | 10 | 35 | 8.8 | 1.5 | 4 | |
| VEM | 10 | 10 | 10 | 10 | 40 | 10.0 | 0.0 | 4 | |
| VES | 7 | 4 | 1 | 0 | 12 | 3.0 | 3.2 | 4 | <0.001 |
| CONTROL | 10 | 9 | 10 | - | 29 | 9.7 | 0.6 | 3 | |
| PBT | 9 | 9 | 8 | - | 26 | 8.7 | 0.6 | 3 | |
| PBM | 10 | 7 | 8 | - | 25 | 8.3 | 1.5 | 3 | |
| PET | 10 | 6 | 8 | - | 24 | 8.0 | 2.0 | 3 | |
| PEM | 10 | 9 | 8 | - | 27 | 9.0 | 1.0 | 3 | |
| PES | 7 | 7 | 6 | - | 20 | 6.7 | 0.6 | 3 | |
| CONTROL | 8 | 10 | 9 | 9 | 36 | 9.0 | 0.8 | 4 | |
| KET | 9 | 9 | 9 | 10 | 37 | 9.3 | 0.5 | 4 | |
| KEM | 9 | 6 | 8 | 7 | 30 | 7.5 | 1.3 | 4 | |
| KES | 8 | 10 | 9 | 10 | 37 | 9.3 | 1.0 | 4 | |
| CONTROL | 9 | 9 | 8 | 10 | 36 | 9.0 | 0.8 | 4 | |
| FBT | 9 | 9 | 5 | 10 | 33 | 8.3 | 2.2 | 4 | |
| FBM | 10 | 10 | 10 | 10 | 40 | 10.0 | 0.0 | 4 | |
| FET | 9 | 8 | 9 | 9 | 35 | 8.8 | 0.5 | 4 | |
| FEM | 10 | 10 | 10 | 10 | 40 | 10.0 | 0.0 | 4 | |
| FES | 6 | 9 | 6 | 0 | 21 | 5.3 | 3.8 | 4 | 0.038 |

Table G2. Supplementary growth data from midge sediment-excavated rock tests for seven geological zones

| | Length(mm) | | | | Avg Length | Std Dev | n | p value |
|---------|------------|-------|-------|-------|------------|---------|---|---------|
| | A | B | C | D | | | | |
| CONTROL | 15.21 | 14.56 | 14.53 | - | 14.77 | 0.39 | 3 | |
| RBT | 14.09 | 14.08 | 12.99 | - | 13.72 | 0.63 | 3 | |
| RBM | 14.66 | 14.88 | 14.81 | - | 14.78 | 0.11 | 3 | |
| RET | 15.24 | 12.90 | 14.22 | - | 14.12 | 1.18 | 3 | |
| REM | 16.20 | 14.40 | 11.23 | - | 13.94 | 2.52 | 3 | |
| RES | 11.08 | 15.31 | 13.38 | - | 13.26 | 2.12 | 3 | |
| CONTROL | 15.90 | 15.07 | 13.99 | 15.09 | 15.01 | 0.78 | 4 | |
| BBT | 15.02 | 17.78 | 17.18 | 14.43 | 16.10 | 1.62 | 4 | |
| BBM | 14.95 | 12.98 | 16.50 | 16.65 | 15.27 | 1.71 | 4 | |
| BET | 14.82 | 11.32 | 14.15 | 15.32 | 13.90 | 1.79 | 4 | |
| BEM | 15.58 | 15.34 | 14.82 | 14.48 | 15.05 | 0.50 | 4 | |
| BES | 10.79 | 11.97 | 13.55 | 12.59 | 12.23 | 1.15 | 4 | 0.037 |
| CONTROL | 10.95 | 13.68 | 9.94 | 14.90 | 12.37 | 2.31 | 4 | |
| SBT | 11.81 | 14.70 | 11.95 | 15.12 | 13.39 | 1.76 | 4 | |
| SBM | 13.45 | 15.57 | 12.19 | 12.16 | 13.34 | 1.60 | 4 | |
| SET | 12.91 | 13.33 | 11.07 | 12.59 | 12.48 | 0.98 | 4 | |
| SEM | 11.72 | 12.55 | 12.80 | 11.67 | 12.18 | 0.58 | 4 | |
| SES | 11.83 | 12.83 | 14.91 | 8.23 | 11.95 | 2.79 | 4 | |
| CONTROL | 12.83 | 13.96 | 12.93 | 14.52 | 13.56 | 0.82 | 4 | |
| VBT | 16.94 | 14.63 | 13.71 | 0.00 | 11.32 | 7.67 | 4 | |
| VBM | 14.58 | 12.50 | 15.12 | 14.67 | 14.22 | 1.17 | 4 | |
| VET | 8.31 | 12.08 | 10.75 | 12.72 | 10.97 | 1.95 | 4 | |
| VEM | 18.00 | 14.30 | 11.89 | 13.86 | 14.51 | 2.55 | 4 | |
| VES | 9.14 | 10.24 | 10.25 | 0.00 | 9.88 | 4.97 | 4 | |
| CONTROL | 15.46 | 10.26 | 14.39 | - | 13.37 | 2.75 | 3 | |
| PBT | 15.40 | 13.79 | 14.12 | - | 14.44 | 0.85 | 3 | |
| PBM | 12.84 | 14.11 | 13.97 | - | 13.64 | 0.70 | 3 | |
| PET | 14.54 | 15.76 | 11.11 | - | 13.80 | 2.41 | 3 | |
| PEM | 16.33 | 14.17 | 13.48 | - | 14.66 | 1.49 | 3 | |
| PES | 13.31 | 12.82 | 9.82 | - | 11.98 | 1.89 | 3 | |
| CONTROL | 15.94 | 13.23 | 16.25 | 16.52 | 15.49 | 1.52 | 4 | |
| KET | 14.04 | 15.19 | 13.13 | 12.39 | 13.69 | 1.21 | 4 | |
| KEM | 14.25 | 9.39 | 13.06 | 12.09 | 12.20 | 2.07 | 4 | |
| KES | 11.74 | 14.34 | 15.22 | 13.73 | 13.76 | 1.48 | 4 | |
| CONTROL | 16.85 | 13.35 | 14.41 | 14.18 | 14.70 | 1.51 | 4 | |
| FBT | 12.02 | 14.73 | 10.86 | 13.31 | 12.73 | 1.67 | 4 | |
| FBM | 16.10 | 11.99 | 13.10 | 13.00 | 13.55 | 1.77 | 4 | |
| FET | 14.00 | 12.81 | 14.56 | 12.98 | 13.59 | 0.83 | 4 | |
| FEM | 14.82 | 13.93 | 14.96 | 15.36 | 14.77 | 0.60 | 4 | |
| FES | 13.17 | 16.45 | 12.54 | 0.00 | 10.54 | 7.23 | 4 | |

Table G3. Water quality data for of the midge sediment-excavated rock toxicity tests for the seven geological zones

| Treatment | Replicate | Water Quality at Day 1 | | | | Water Quality at test completion | | | |
|-----------|-----------|------------------------|----------------------|-------------------------|-----------------------|----------------------------------|----------------------|-------------------------|-----------------------|
| | | pH | DO (% saturation) | Conductivity (µS/cm) | Temperature (° C) | pH | DO (% saturation) | Conductivity (µS/cm) | Temperature (° C) |
| Control | A | 7.52 | 89 | 218 | 21 | 7.98 | 90.3 | 170 | 21 |
| | B | 7.54 | 89 | 217 | 21 | 7.41 | 89.2 | 160 | 21 |
| | C | 7.53 | 90.2 | 216 | 21 | 7.57 | 90.3 | 172 | 21 |
| RBT | A | 7.37 | 92.4 | 291 | 21 | 7.66 | 89.0 | 270 | 21 |
| | B | 7.82 | 92.4 | 317 | 21 | 7.58 | 90.1 | 239 | 21 |
| | C | 8.05 | 92.4 | 323 | 21 | 7.62 | 93.2 | 269 | 21 |
| RBM | A | 7.77 | 92.3 | 321 | 21 | 8.04 | 71 | 417 | 21 |
| | B | 7.62 | 89.9 | 237 | 21 | 8.01 | 75.5 | 418 | 21 |
| | C | 7.57 | 89.4 | 213 | 21 | 8.06 | 77.6 | 407 | 21 |
| RET | A | 7.86 | 90.2 | 240 | 21 | 8.09 | 82.1 | 410 | 21 |
| | B | 7.91 | 90.1 | 295 | 21 | 8.15 | 80.4 | 440 | 21 |
| | C | 8.05 | 91 | 298 | 21 | 7.91 | 54.6 | 465 | 21 |
| REM | A | 7.78 | 88.6 | 231 | 21 | 7.98 | 79 | 383 | 21 |
| | B | 7.68 | 89.1 | 223 | 21 | 7.96 | 72.8 | 402 | 21 |
| | C | 7.54 | 89.6 | 220 | 21 | 8.01 | 77 | 395 | 21 |
| RES | A | 8.05 | 91.5 | 323 | 21 | 8.21 | 8.21 | 457 | 21 |
| | B | 8.14 | 91.1 | 325 | 21 | 8.32 | 8.32 | 495 | 21 |
| | C | 8.17 | 91.7 | 325 | 21 | 8.3 | 8.3 | 505 | 21 |

| Treatment | Replicate | Water Quality at Day 1 | | | | Water Quality at test completion | | | |
|-----------|-----------|------------------------|----------------------|-------------------------|-----------------------|----------------------------------|----------------------|-------------------------|-----------------------|
| | | pH | DO (% saturation) | Conductivity (µS/cm) | Temperature (° C) | pH | DO (% saturation) | Conductivity (µS/cm) | Temperature (° C) |
| Control | A | 7.77 | 110.5 | 246 | 21 | 7.66 | 77.4 | 314 | 21 |
| | B | 7.79 | 107.9 | 224 | 21 | 7.64 | 77.8 | 305 | 21 |
| | C | 7.78 | 104.4 | 218 | 21 | 7.66 | 80.2 | 298 | 21 |
| | D | 7.69 | 103.2 | 234 | 21 | 7.43 | 74.9 | 316 | 21 |
| BBT | A | 8.09 | 110.9 | 350 | 21 | 7.88 | 72.7 | 371 | 21 |
| | B | 8.07 | 101.6 | 332 | 21 | 7.89 | 74.7 | 365 | 21 |
| | C | 8.07 | 103.4 | 346 | 21 | 7.79 | 78.6 | 371 | 21 |
| | D | 8.08 | 106.8 | 360 | 21 | 7.47 | 28 | 375 | 21 |
| BBM | A | 7.87 | 113.3 | 300 | 21 | 7.54 | 72.7 | 348 | 21 |
| | B | 7.84 | 110.5 | 286 | 21 | 7.45 | 68.3 | 364 | 21 |
| | C | 7.85 | 110.1 | 283 | 21 | 7.53 | 79 | 345 | 21 |
| | D | 7.86 | 109.9 | 303 | 21 | 7.43 | 72.7 | 344 | 21 |
| BET | A | 8.07 | 104.5 | 350 | 21 | 7.84 | 72.9 | 368 | 21 |
| | B | 8.09 | 98.9 | 350 | 21 | 7.61 | 65.6 | 369 | 21 |
| | C | 8.07 | 95.7 | 334 | 21 | 7.55 | 83 | 357 | 21 |
| | D | 8.08 | 101.9 | 346 | 21 | 7.88 | 78.3 | 359 | 21 |
| BEM | A | 7.95 | 114.3 | 275 | 21 | 7.69 | 70.8 | 338 | 21 |
| | B | 7.84 | 108.8 | 284 | 21 | 7.73 | 75.7 | 337 | 21 |
| | C | 7.86 | 109.3 | 278 | 21 | 7.68 | 78.3 | 330 | 21 |
| | D | 7.81 | 108.6 | 270 | 21 | 7.72 | 72 | 331 | 21 |
| BES | A | 8.28 | 88.6 | 469 | 21 | 7.97 | 63.5 | 578 | 21 |
| | B | 8.3 | 89.1 | 445 | 21 | 7.97 | 56.9 | 581 | 21 |
| | C | 8.37 | 88.5 | 445 | 21 | 8.09 | 69.8 | 569 | 21 |
| | D | 8.35 | 88.9 | 444 | 21 | 7.6 | 70.6 | 573 | 21 |

| Treatment | Replicate | Water Quality at Day 1 | | | | Water Quality at test completion | | | |
|-----------|-----------|------------------------|----------------------|-------------------------|-----------------------|----------------------------------|----------------------|-------------------------|-----------------------|
| | | pH | DO (% saturation) | Conductivity (µS/cm) | Temperature (° C) | pH | DO (% saturation) | Conductivity (µS/cm) | Temperature (° C) |
| Control | A | 7.77 | 110.5 | 246 | 21 | 7.66 | 77.4 | 314 | 21 |
| | B | 7.79 | 107.9 | 224 | 21 | 7.64 | 77.8 | 305 | 21 |
| | C | 7.78 | 104.4 | 218 | 21 | 7.66 | 80.2 | 298 | 21 |
| | D | 7.69 | 103.2 | 234 | 21 | 7.43 | 74.9 | 316 | 21 |
| SBT | A | 8.25 | 91.5 | 328 | 21 | 7.79 | 81.9 | 512 | 21 |
| | B | 8.28 | 90.8 | 320 | 21 | 7.93 | 79.4 | 532 | 21 |
| | C | 8.31 | 91.7 | 328 | 21 | 7.88 | 79.4 | 493 | 21 |
| | D | 8.36 | 92.4 | 330 | 21 | 7.68 | 53.5 | 531 | 21 |
| SBM | A | 8 | 85.2 | 353 | 21 | 7.74 | 74.2 | 470 | 21 |
| | B | 8.02 | 86.1 | 353 | 21 | 7.89 | 77.6 | 473 | 21 |
| | C | 7.85 | 86.8 | 340 | 21 | 7.87 | 78.2 | 459 | 21 |
| | D | 8.08 | 86.9 | 344 | 21 | 7.9 | 69.1 | 434 | 21 |
| SET | A | 7.89 | 88 | 324 | 21 | 7.88 | 81.4 | 416 | 21 |
| | B | 7.54 | 91 | 327 | 21 | 7.52 | 69.7 | 445 | 21 |
| | C | 8.04 | 91.6 | 325 | 21 | 7.6 | 46.6 | 482 | 21 |
| | D | 8.75 | 91.5 | 325 | 21 | 7.58 | 54.5 | 476 | 21 |
| SEM | A | 8.04 | 89.6 | 271 | 21 | 7.65 | 67.4 | 449 | 21 |
| | B | 7.8 | 89 | 262 | 21 | 7.7 | 57.8 | 431 | 21 |
| | C | 7.74 | 89.7 | 265 | 21 | 7.54 | 52.1 | 442 | 21 |
| | D | 7.82 | 88.5 | 255 | 21 | 7.37 | 48.8 | 433 | 21 |
| SES | A | 7.47 | 91.9 | 329 | 21 | 7.66 | 36 | 576 | 21 |
| | B | 7.84 | 91.6 | 329 | 21 | 7.78 | 59.7 | 545 | 21 |
| | C | 8 | 91.4 | 331 | 21 | 7.72 | 54.6 | 544 | 21 |
| | D | 8.09 | 92.1 | 331 | 21 | 7.69 | 55.8 | 565 | 21 |

| Treatment | Replicate | Water Quality at Day 1 | | | | Water Quality at test completion | | | |
|-----------|-----------|------------------------|----------------------|-------------------------|-----------------------|----------------------------------|----------------------|-------------------------|-----------------------|
| | | pH | DO (% saturation) | Conductivity (µS/cm) | Temperature (° C) | pH | DO (% saturation) | Conductivity (µS/cm) | Temperature (° C) |
| Control | A | 7.35 | 90.8 | 293 | 21 | 7.78 | 72.9 | 334 | 21 |
| | B | 7.25 | 84.7 | 255 | 21 | 7.80 | 77.4 | 307 | 21 |
| | C | 7.46 | 93 | 288 | 21 | 7.78 | 69.9 | 322 | 21 |
| | D | 7.45 | 92.9 | 297 | 21 | 7.80 | 69.7 | 326 | 21 |
| VBT | A | 7.48 | 90.2 | 311 | 21 | 7.92 | 77.1 | 401 | 21 |
| | B | 7.53 | 93.6 | 309 | 21 | 7.93 | 75.6 | 418 | 21 |
| | C | 7.67 | 92.5 | 303 | 21 | 7.98 | 80.2 | 386 | 21 |
| | D | 7.72 | 91.7 | 306 | 21 | 7.96 | 76.3 | 381 | 21 |
| VBM | A | 7.32 | 92 | 287 | 21 | 7.51 | 76.4 | 360 | 21 |
| | B | 7.47 | 92.1 | 285 | 21 | 7.68 | 73.6 | 350 | 21 |
| | C | 7.34 | 90.8 | 277 | 21 | 7.69 | 65.6 | 356 | 21 |
| | D | 7.64 | 89 | 274 | 21 | 7.76 | 74.9 | 336 | 21 |
| VET | A | 7.54 | 93.3 | 306 | 21 | 7.59 | 58.2 | 401 | 21 |
| | B | 7.69 | 93 | 305 | 21 | 7.66 | 56.4 | 418 | 21 |
| | C | 7.46 | 90.5 | 296 | 21 | 7.5 | 57.3 | 386 | 21 |
| | D | 7.49 | 92.2 | 316 | 21 | 7.8 | 70 | 381 | 21 |
| VEM | A | 7.44 | 88.5 | 272 | 21 | 7.78 | 75.5 | 382 | 21 |
| | B | 7.36 | 86.3 | 271 | 21 | 7.75 | 69.9 | 338 | 21 |
| | C | 7.4 | 89.3 | 271 | 21 | 7.75 | 67.7 | 355 | 21 |
| | D | 7.4 | 89.8 | 275 | 21 | 7.78 | 72.5 | 346 | 21 |
| VES | A | 8.07 | 89.4 | 395 | 21 | 7.7 | 59 | 620 | 21 |
| | B | 8.2 | 87.8 | 392 | 21 | 7.71 | 60.3 | 615 | 21 |
| | C | 8.13 | 89 | 391 | 21 | 7.72 | 66.9 | 631 | 21 |
| | D | 8.15 | 89.6 | 375 | 21 | 7.91 | 60.8 | 603 | 21 |

| Treatment | Replicate | Water Quality at Day 1 | | | | Water Quality at test completion | | | |
|-----------|-----------|------------------------|----------------------|-------------------------------|--------------------------------|----------------------------------|----------------------|-------------------------------|--------------------------------|
| | | pH | DO (% saturation) | Conductivity (μ S/cm) | Temperature ($^{\circ}$ C) | pH | DO (% saturation) | Conductivity (μ S/cm) | Temperature ($^{\circ}$ C) |
| Control | A | 7.75 | 92.5 | 228 | 21 | 8.02 | 77.4 | 391 | 21 |
| | B | 7.66 | 92.3 | 220 | 21 | 8.09 | 80.1 | 407 | 21 |
| | C | 7.60 | 93.1 | 219 | 21 | 7.87 | 70.2 | 373 | 21 |
| PBT | A | 7.63 | 93.7 | 323 | 21 | 7.90 | 80.3 | 450 | 21 |
| | B | 7.92 | 93.9 | 343 | 21 | 8.15 | 83.6 | 445 | 21 |
| | C | 8.07 | 94.3 | 340 | 21 | 8.23 | 84.0 | 443 | 21 |
| PBM | A | 7.88 | 93 | 282 | 21 | 8.07 | 73.5 | 452 | 21 |
| | B | 7.84 | 92 | 288 | 21 | 8.09 | 78.9 | 448 | 21 |
| | C | 7.86 | 93.2 | 279 | 21 | 8.15 | 77 | 467 | 21 |
| PET | A | 8.09 | 93.5 | 352 | 21 | 8.23 | 79.2 | 477 | 21 |
| | B | 8.15 | 93.8 | 354 | 21 | 8.22 | 80.3 | 467 | 21 |
| | C | 8.15 | 93.7 | 352 | 21 | 8.07 | 62 | 492 | 21 |
| PEM | A | 7.91 | 91.4 | 251 | 21 | 8.09 | 73 | 446 | 21 |
| | B | 7.87 | 92.7 | 271 | 21 | 7.91 | 61.6 | 526 | 21 |
| | C | 7.85 | 91.8 | 275 | 21 | 8.08 | 76.6 | 452 | 21 |
| PES | A | 8.25 | 90.2 | 369 | 21 | 7.93 | 49.1 | 607 | 21 |
| | B | 8.21 | 88.5 | 367 | 21 | 7.8 | 2.9 | 666 | 21 |
| | C | 8.19 | 89.1 | 373 | 21 | 7.93 | 51.2 | 577 | 21 |

| Treatment | Replicate | Water Quality at Day 1 | | | | Water Quality at test completion | | | |
|-----------|-----------|------------------------|----------------------|-------------------------------|--------------------------------|----------------------------------|----------------------|-------------------------------|--------------------------------|
| | | pH | DO (% saturation) | Conductivity (μ S/cm) | Temperature ($^{\circ}$ C) | pH | DO (% saturation) | Conductivity (μ S/cm) | Temperature ($^{\circ}$ C) |
| Control | A | 7.39 | 91 | 218 | 21 | 7.54 | 84.8 | 425 | 21 |
| | B | 7.37 | 91.1 | 221 | 21 | 8.02 | 49.5 | 458 | 21 |
| | C | 7.40 | 91.8 | 212 | 21 | 8.08 | 85.2 | 449 | 21 |
| | D | 7.44 | 91.1 | 222 | 21 | 8.12 | 86.2 | 424 | 21 |
| KET | A | 7.56 | 94.1 | 308 | 21 | 7.47 | 81.8 | 414 | 21 |
| | B | 7.82 | 93.9 | 302 | 21 | 7.87 | 84.2 | 410 | 21 |
| | C | 7.86 | 93.7 | 302 | 21 | 7.71 | 88 | 395 | 21 |
| | D | 7.92 | 93.5 | 294 | 21 | 7.75 | 74.4 | 388 | 21 |
| KEM | A | 7.39 | 92.4 | 213 | 21 | 7.9 | 86.3 | 377 | 21 |
| | B | 7.36 | 91.6 | 207 | 21 | 7.69 | 81.7 | 386 | 21 |
| | C | 7.39 | 91.8 | 207 | 21 | 7.8 | 87.2 | 366 | 21 |
| | D | 7.42 | 93 | 216 | 21 | 7.86 | 85 | 355 | 21 |
| KES | A | 7.94 | 92.4 | 333 | 21 | 7.82 | 85.6 | 378 | 21 |
| | B | 8.09 | 93 | 328 | 21 | 7.55 | 87.1 | 374 | 21 |
| | C | 8.11 | 92.7 | 332 | 21 | 7.54 | 86.9 | 383 | 21 |
| | D | 8.14 | 93 | 329 | 21 | 7.35 | 87.7 | 368 | 21 |

| Treatment | Replicate | Water Quality at Day 1 | | | | Water Quality at test completion | | | |
|-----------|-----------|------------------------|----------------------|-------------------------------|--------------------------------|----------------------------------|----------------------|-------------------------------|--------------------------------|
| | | pH | DO (% saturation) | Conductivity (μ S/cm) | Temperature ($^{\circ}$ C) | pH | DO (% saturation) | Conductivity (μ S/cm) | Temperature ($^{\circ}$ C) |
| Control | A | 7.64 | 85.5 | 236 | 21 | 7.76 | 69.9 | 367 | 21 |
| | B | 7.59 | 86.7 | 239 | 21 | 7.65 | 59.5 | 380 | 21 |
| | C | 7.52 | 85 | 226 | 21 | 7.71 | 67.6 | 392 | 21 |
| | D | 7.47 | 84.8 | 236 | 21 | 7.71 | 66.8 | 383 | 21 |
| FBT | A | 7.40 | 87.5 | 338 | 21 | 7.68 | 72.4 | 468 | 21 |
| | B | 7.59 | 90 | 340 | 21 | 7.77 | 70.6 | 450 | 21 |
| | C | 7.65 | 92.2 | 346 | 21 | 7.89 | 76.4 | 445 | 21 |
| | D | 7.79 | 89.8 | 341 | 21 | 7.93 | 73.9 | 466 | 21 |
| FBM | A | 7.55 | 81.1 | 341 | 21 | 7.82 | 66.1 | 437 | 21 |
| | B | 7.59 | 85.7 | 342 | 21 | 7.66 | 78.7 | 426 | 21 |
| | C | 7.52 | 81.1 | 329 | 21 | 7.6 | 55.7 | 435 | 21 |
| | D | 7.56 | 82.7 | 334 | 21 | 7.72 | 61.5 | 433 | 21 |
| FET | A | 7.82 | 86 | 342 | 21 | 7.83 | 74.3 | 437 | 21 |
| | B | 7.81 | 86.9 | 334 | 21 | 7.88 | 71.3 | 438 | 21 |
| | C | 7.93 | 89.2 | 349 | 21 | 7.88 | 68.4 | 453 | 21 |
| | D | 8.04 | 88.9 | 351 | 21 | 7.93 | 70.8 | 463 | 21 |
| FEM | A | 7.78 | 83.6 | 306 | 21 | 7.65 | 74 | 424 | 21 |
| | B | 7.71 | 84.2 | 317 | 21 | 7.68 | 55.4 | 424 | 21 |
| | C | 7.75 | 85.9 | 329 | 21 | 7.83 | 67.7 | 440 | 21 |
| | D | 7.68 | 85 | 315 | 21 | 7.82 | 67.4 | 426 | 21 |
| FES | A | 8.02 | 90.9 | 369 | 21 | 7.74 | 32.8 | 553 | 21 |
| | B | 7.88 | 90.5 | 369 | 21 | 8.01 | 73 | 531 | 21 |
| | C | 7.59 | 89.8 | 365 | 21 | 7.99 | 57.8 | 578 | 21 |
| | D | 8.25 | 90.1 | 366 | 21 | 7.36 | 71.7 | 606 | 21 |

Table G4. Abbreviations used in blackworm and midge sediment toxicity tests

| | |
|-----|--|
| RBT | Ravine Baseline excavated rock on Top of reservoir sediment |
| RBM | Ravine Baseline excavated rock mixed with reservoir sediment |
| RET | Ravine Enriched excavated rock on Top of reservoir sediment |
| REM | Ravine Enriched excavated rock mixed with reservoir sediment |
| RES | Ravine Enriched Excavated rock |
| BBT | Byron Baseline excavated rock on Top of reservoir sediment |
| BBM | Byron Baseline excavated rock mixed with reservoir sediment |
| BET | Byron Enriched excavated rock on Top of reservoir sediment |
| BEM | Byron Enriched excavated rock mixed with reservoir sediment |
| BES | Byron Enriched Excavated rock |
| SET | Shaw Gabbro Enriched excavated rock on Top of reservoir sediment |
| SEM | Shaw Gabbro Enriched excavated rock mixed with reservoir sediment |
| SES | Shaw Gabbro Enriched Excavated rock |
| VBT | Volcanics Baseline excavated rock on Top of reservoir sediment |
| VBM | Volcanics Baseline excavated rock mixed with reservoir sediment |
| VET | Volcanics Enriched excavated rock on Top of reservoir sediment |
| VEM | Volcanics Enriched excavated rock mixed with reservoir sediment |
| VES | Volcanics Enriched Excavated rock |
| PBT | Peppercorn Baseline excavated rock on Top of reservoir sediment |
| PBM | Peppercorn Baseline excavated rock mixed with reservoir sediment |
| PET | Peppercorn Enriched excavated rock on Top of reservoir sediment |
| PEM | Peppercorn Enriched excavated rock mixed with reservoir sediment |
| PES | Peppercorn Enriched Excavated rock |
| KET | Kelly's Plains Enriched excavated rock on Top of reservoir sediment |
| KEM | Kelly's Plains Enriched excavated rock mixed with reservoir sediment |
| KES | Kelly's Plains Enriched Excavated rock |
| FBT | Felsics Baseline excavated rock on Top of reservoir sediment |
| FBM | Felsics Baseline excavated rock mixed with reservoir sediment |
| FET | Felsics Enriched excavated rock on Top of reservoir sediment |
| FEM | Felsics Enriched excavated rock mixed with reservoir sediment |
| FES | Felsics Enriched Excavated rock |

Table G5. Copper reference toxicity tests with the midge (*Chironomus tepperi*) during chronic toxicity tests.

| Treatment | After 24 hours | | | | After 48 hours | | | |
|-----------|----------------|---|---|---|----------------|---|---|---|
| | # Alive | | | | # Alive | | | |
| | A | B | C | D | A | B | C | D |
| MHW | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| 31.25µg/l | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| 62.5µg/l | 4 | 3 | 5 | 3 | 5 | 5 | 5 | 5 |
| 125µg/l | 5 | 3 | 4 | 4 | 4 | 3 | 3 | 3 |
| 250µg/l | 1 | 3 | 4 | 4 | 1 | 0 | 2 | 1 |
| 500µg/l | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 |

| Treatment | After 48 hours | | | | | | | |
|-----------|----------------|---|---|---|--------|---|---|---|
| | # Alive | | | | # Dead | | | |
| | A | B | C | D | A | B | C | D |
| MHW | 5 | 4 | 5 | 5 | 0 | 1 | 0 | 0 |
| 31.25µg/l | 4 | 5 | 5 | 4 | 1 | 0 | 0 | 1 |
| 62.5µg/l | 3 | 3 | 4 | 4 | 2 | 2 | 1 | 1 |
| 125µg/l | 2 | 1 | 1 | 2 | 3 | 4 | 4 | 3 |
| 250µg/l | 1 | 1 | 1 | 0 | 4 | 4 | 4 | 5 |
| 500µg/l | 0 | 0 | 0 | 0 | 5 | 5 | 5 | 5 |

| Treatment | After 48 hours | | | | | |
|-----------|----------------|---|---|--------|---|---|
| | # Alive | | | # Dead | | |
| | A | B | C | A | B | C |
| MHW | 5 | 5 | 5 | 0 | 0 | 0 |
| 31.25µg/l | 5 | 5 | 5 | 0 | 0 | 0 |
| 62.5µg/l | 4 | 5 | 4 | 1 | 0 | 1 |
| 125µg/l | 2 | 2 | 3 | 3 | 3 | 2 |
| 250µg/l | 2 | 0 | 2 | 3 | 5 | 3 |
| 500µg/l | 0 | 0 | 0 | 5 | 5 | 5 |

Table G6. The effective concentration (µg/L) of copper at 50%, 10% and 20% for the midge (*Chironomus tepperi*) during chronic toxicity tests.

| Copper reference test | EC50(µg/l) | 95% Conf. intervals For EC50 | | EC10(µg/l) | 95% Conf. intervals For EC10 | |
|-----------------------|------------|------------------------------|--------|------------|------------------------------|-------|
| Test 1 | 96.51 | #N/A | #N/A | 36.23 | #N/A | #N/A |
| Test 2 | 94.22 | 78.66 | 112.86 | 35.55 | 23.69 | 53.34 |
| Test 3 | 130.97 | 102.96 | 166.60 | 48.64 | 29.83 | 79.30 |

Appendix H Excavated rock material in sediments: Supplementary information on blackworm (*Lumbriculus variegatus*) toxicity tests

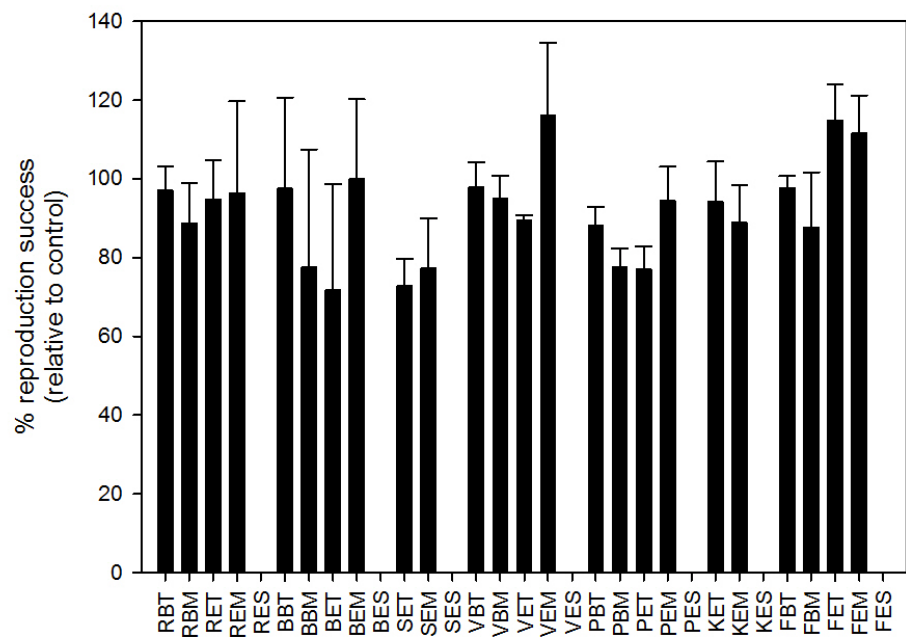


Figure H1. Reproduction success in the blackworm (*Lumbriculus variegatus*) after 28-day exposure to excavated rock from seven geological zones (Abbreviations for treatments in Table H4)

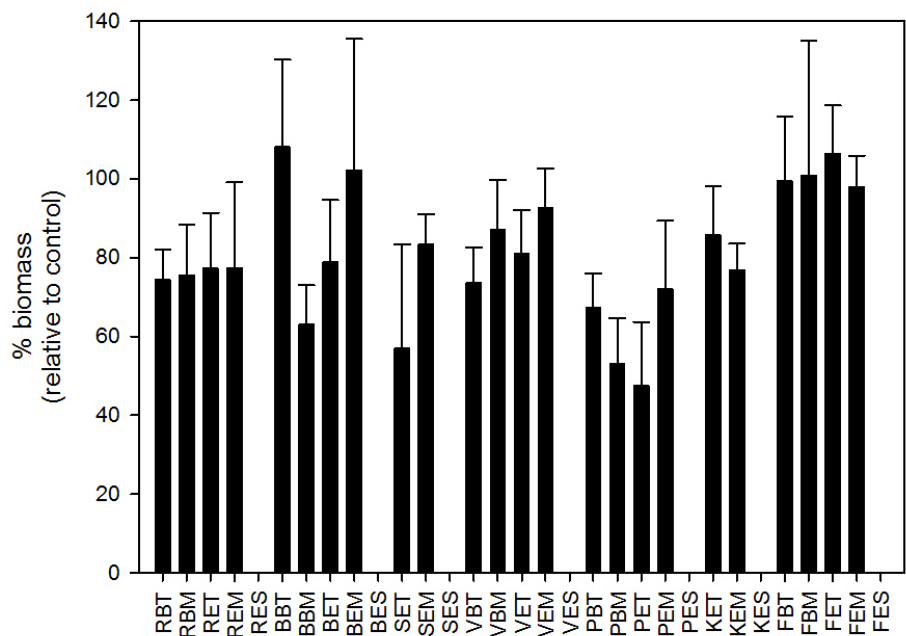


Figure H2. Total biomass of the blackworm (*Lumbriculus variegatus*) after 28-day exposure to excavated rock from seven geological zones (Abbreviations for treatments in Table H4)

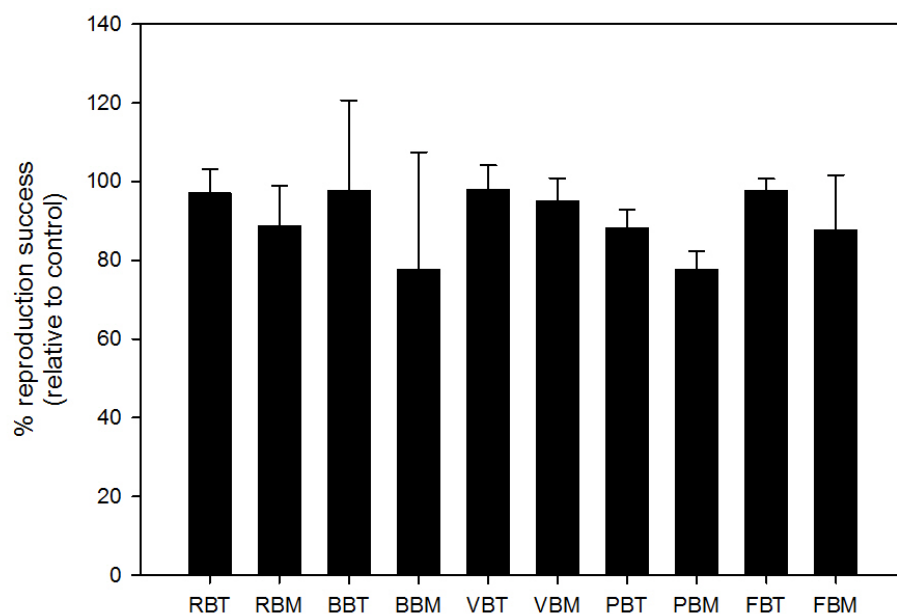


Figure H3: Reproduction success in the blackworm (*Lumbriculus variegatus*) after 28-day exposure to Baseline excavated rock from seven geological zones (Abbreviations for treatments in Table H4)

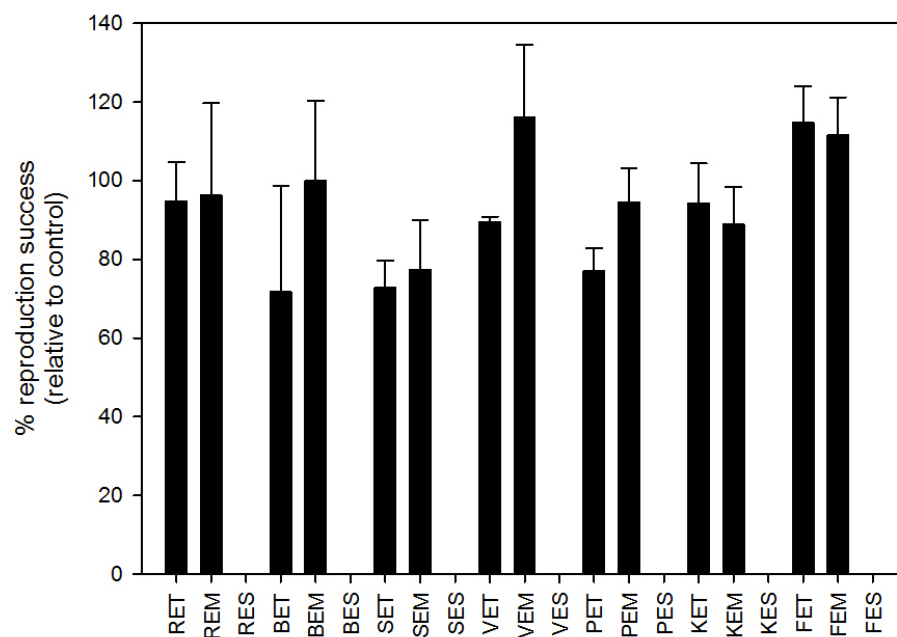


Figure H4: Reproduction success in the blackworm (*Lumbriculus variegatus*) after 28-day exposure to Enriched excavated rock from seven geological zones (Abbreviations for treatments in Table H4)

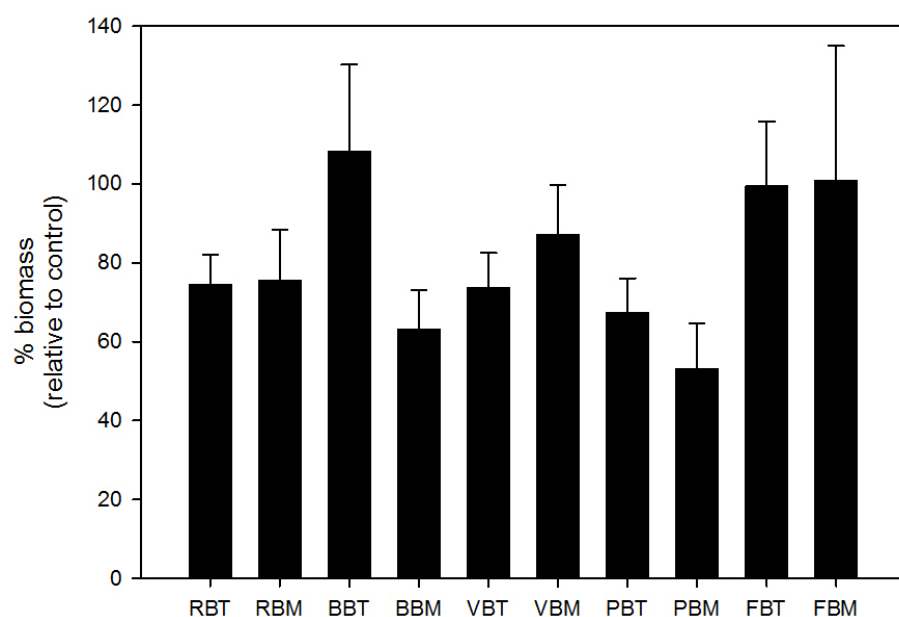


Figure H5: Total biomass of the blackworm (*Lumbriculus variegatus*) after 28-day exposure to Baseline excavated rock from seven geological zones (Abbreviations for treatments in Table H4)

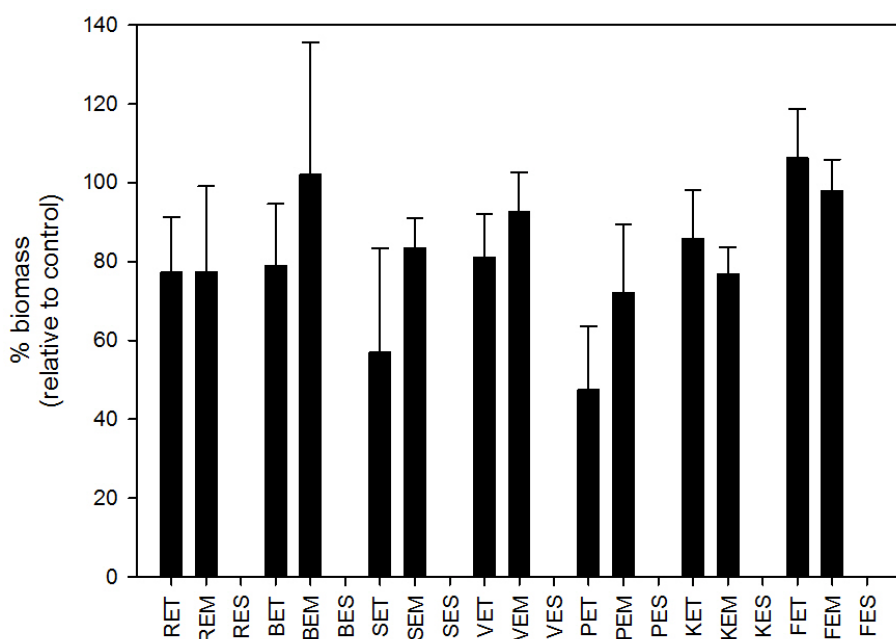


Figure H6: Total biomass of the blackworm (*Lumbriculus variegatus*) after 28-day exposure to Enriched excavated rock from seven geological zones (Abbreviations for treatments in Table H4)

Table H1. Supplementary data on the reproduction success in the blackworm (*Lumbriculus variegatus*) during 28-day sediment-excavated rock tests for seven geological zones.

| Number of blackworms after 28d | | | | | Avg | STd Dev | p-Value |
|--------------------------------|-----|-----|-----|-----|------|---------|---------|
| | A | B | C | D | | | |
| Control | 30 | 35 | 34 | 34 | 33.3 | 2.2 | |
| RBT | 30 | 31 | 34 | 34 | 32.3 | 2.1 | |
| RBM | 29 | 25 | 33 | 31 | 29.5 | 3.4 | |
| RET | 32 | 35 | 32 | 27 | 31.5 | 3.3 | |
| REM | 37 | 32 | 21 | 38 | 32.0 | 7.8 | |
| RES | 0 | 0 | 0 | 0 | 0.0 | 0.0 | <0.001 |
| Control | 31 | 29 | 30 | 30 | 30.0 | 0.8 | |
| BBT | 37 | 25 | 33 | 22 | 29.3 | 6.9 | |
| BBM | 34 | 23 | 12 | 24 | 23.3 | 9.0 | |
| BET | 23 | 13 | 18 | 32 | 21.5 | 8.1 | |
| BEM | 37 | 24 | 33 | 26 | 30.0 | 6.1 | |
| BES | 0 | 0 | 0 | 0 | 0.0 | 0.0 | <0.001 |
| Control | 29 | 38 | 32 | 37 | 34.0 | 4.2 | |
| SBT | n/a | n/a | n/a | n/a | | | |
| SBM | n/a | n/a | n/a | n/a | | | |
| SET | 23 | 23 | 28 | 25 | 24.8 | 2.4 | 0.005 |
| SEM | 32 | 27 | 24 | 22 | 26.3 | 4.3 | 0.015 |
| SES | 0 | 0 | 0 | 0 | 0.0 | 0.0 | <0.001 |
| Control | 35 | 37 | 32 | 38 | 35.5 | 2.6 | |
| VBT | 36 | 37 | 34 | 32 | 34.8 | 2.2 | |
| VBM | 35 | 36 | 32 | 32 | 33.8 | 2.1 | |
| VET | 32 | 32 | 31 | 32 | 31.8 | 0.5 | |
| VEM | 42 | 35 | 50 | 38 | 41.3 | 6.5 | |
| VES | 0 | 0 | 0 | 0 | 0.0 | 0.0 | <0.001 |
| Control | 38 | 34 | 35 | 35 | 35.5 | 1.7 | |
| PBT | 29 | 32 | 31 | 33 | 31.3 | 1.7 | 0.027 |
| PBM | 29 | 26 | 26 | 29 | 27.5 | 1.7 | <0.001 |
| PET | 20 | 28 | 25 | 29 | 25.5 | 4.0 | <0.001 |
| PEM | 37 | 35 | 30 | 32 | 33.5 | 3.1 | |
| PES | 0 | 0 | 0 | 0 | 0.0 | 0.0 | <0.001 |
| Control | 36 | 35 | 42 | 40 | 38.3 | 3.3 | |
| KBT | n/a | n/a | n/a | n/a | | | |
| KBM | n/a | n/a | n/a | n/a | | | |
| KET | 41 | 37 | 34 | 32 | 36.0 | 3.9 | |
| KEM | 32 | 36 | 38 | 30 | 34.0 | 3.7 | |
| KES | 0 | 0 | 0 | 0 | 0.0 | 0.0 | <0.001 |
| Control | 33 | 31 | 21 | 37 | 30.5 | 6.8 | |
| FBT | 29 | 30 | 29 | 31 | 29.8 | 1.0 | |
| FBM | 26 | 21 | 30 | 30 | 26.8 | 4.3 | |
| FET | 35 | 31 | 37 | 37 | 35.0 | 2.8 | |
| FEM | 38 | 34 | 33 | 31 | 34.0 | 2.9 | |
| FES | 0 | 0 | 0 | 0 | 0.0 | 0.0 | <0.001 |

Table H2. Supplementary data on the biomass of the Blackworm (*Lumbriculus variegatus*) during 28-day sediment-excavated rock tests for seven geological zones.

| Total Bioamass(mg) after 28d | | | | | | | |
|------------------------------|------|------|------|------|------|---------|---------|
| | A | B | C | D | Avg | STd Dev | p-Value |
| Control | 64.9 | 70 | 59.1 | 70.1 | 66.0 | 5.2 | |
| RBT | 45.2 | 54.3 | 44.2 | 52.6 | 49.1 | 5.1 | 0.040 |
| RBM | 40 | 47.7 | 60.5 | 51.3 | 49.9 | 8.5 | |
| RET | 48 | 61.9 | 54.2 | 39.9 | 51.0 | 9.3 | |
| REM | 55.7 | 53.4 | 30.8 | 64.5 | 51.1 | 14.4 | |
| RES | 0 | 0 | 0 | 0 | 0.0 | 0.0 | <0.001 |
| Control | 45.7 | 55.2 | 68 | 54.8 | 55.9 | 9.2 | |
| BBT | 70.8 | 53 | 71.1 | 46.8 | 60.4 | 12.4 | 0.007 |
| BBM | 39.1 | 36.3 | 27 | 38.6 | 35.3 | 5.6 | |
| BET | 43.8 | 31.8 | 50.2 | 50.7 | 44.1 | 8.8 | |
| BEM | 80.9 | 40.2 | 63 | 44.4 | 57.1 | 18.7 | |
| BES | 0 | 0 | 0 | 0 | 0.0 | 0.0 | <0.001 |
| Control | 45.9 | 50.3 | 50.9 | 47.5 | 48.7 | 2.4 | |
| SBT | n/a | n/a | n/a | n/a | | | |
| SBM | n/a | n/a | n/a | n/a | | | |
| SET | 7.4* | 17.2 | 23.7 | 42.1 | 27.7 | 12.9 | 0.046 |
| SEM | 40.2 | 45.8 | 37.3 | 39.1 | 40.6 | 3.7 | 0.002 |
| SES | 0 | 0 | 0 | 0 | 0.0 | 0.0 | <0.001 |
| Control | 66.9 | 73 | 54.2 | 60.2 | 63.6 | 8.1 | |
| VBT | 43 | 44 | 44.8 | 55.2 | 46.8 | 5.7 | 0.007 |
| VBM | 56.2 | 66.1 | 47.3 | 52 | 55.4 | 8.0 | |
| VET | 60.2 | 50 | 52.7 | 43.1 | 51.5 | 7.1 | |
| VEM | 52 | 59.3 | 67.2 | 57.2 | 58.9 | 6.3 | |
| VES | 0 | 0 | 0 | 0 | 0.0 | 0.0 | <0.001 |
| Control | 59.9 | 61.3 | 60.9 | 56.1 | 59.6 | 2.4 | |
| PBT | 43.2 | 32.2 | 41.9 | 42.9 | 40.1 | 5.3 | 0.003 |
| PBM | 35 | 21.8 | 31.6 | 37.7 | 31.5 | 6.9 | <0.001 |
| PET | 11.4 | 31.9 | 17.4 | 35.6 | 24.1 | 11.5 | <0.001 |
| PEM | 46.8 | 54.4 | 29.9 | 40.5 | 42.9 | 10.4 | 0.011 |
| PES | 0 | 0 | 0 | 0 | 0.0 | 0.0 | <0.001 |
| Control | 69.5 | 67 | 74.1 | 73.4 | 71.0 | 3.3 | |
| KBT | n/a | n/a | n/a | n/a | | | |
| KBM | n/a | n/a | n/a | n/a | | | |
| KET | 73.6 | 59.5 | 56.8 | 53.6 | 60.9 | 8.8 | 0.046 |
| KEM | 54.2 | 51.1 | 61.4 | 51.7 | 54.6 | 4.7 | 0.002 |
| KES | 0 | 0 | 0 | 0 | 0.0 | 0.0 | <0.001 |
| Control | 39.9 | 35.8 | 21 | 38.9 | 33.9 | 8.8 | |
| FBT | 39.9 | 36.9 | 28.8 | 29.1 | 33.7 | 5.6 | 0.007 |
| FBM | 18.8 | 44.4 | 31.6 | 41.8 | 34.2 | 11.6 | |
| FET | 38.7 | 30.6 | 34.9 | 39.9 | 36.0 | 4.2 | |
| FEM | 35.6 | 33.7 | 29.4 | 34.2 | 33.2 | 2.7 | |
| FES | 0 | 0 | 0 | 0 | 0.0 | 0.0 | <0.001 |

Table H3. Water quality data for 28-d blackworm sediment toxicity test

| Treatment | Replicate | Water Quality at Day 1 | | | | Water Quality at test completion | | | |
|-----------|-----------|------------------------|----------------------|---|---------------------------------------|----------------------------------|----------------------|---|---------------------------------------|
| | | pH | DO (% saturation) | Conductivity ($\mu\text{S}/\text{cm}$) | Temperature ($^{\circ}\text{C}$) | pH | DO (% saturation) | Conductivity ($\mu\text{S}/\text{cm}$) | Temperature ($^{\circ}\text{C}$) |
| Control | A | 7.39 | 89 | 289 | 21 | 7.98 | 90.3 | 170 | 21 |
| | B | 7.30 | 89 | 274 | 21 | 7.41 | 89.2 | 160 | 21 |
| | C | 7.26 | 90.2 | 285 | 21 | 7.57 | 90.3 | 172 | 21 |
| | D | 7.30 | 90.6 | 280 | 21 | 7.38 | 87.0 | 213 | 21 |
| RBT | A | 7.62 | 92.4 | 388 | 21 | 7.66 | 89.0 | 270 | 21 |
| | B | 7.71 | 92.4 | 382 | 21 | 7.58 | 90.1 | 239 | 21 |
| | C | 7.73 | 92.4 | 404 | 21 | 7.62 | 93.2 | 269 | 21 |
| | D | 7.80 | 92.4 | 398 | 21 | 7.4 | 91.3 | 271 | 21 |
| RBM | A | 7.74 | 92.3 | 304 | 21 | 7.68 | 76.9 | 187 | 21 |
| | B | 7.58 | 89.9 | 275 | 21 | 7.64 | 75.7 | 191 | 21 |
| | C | 7.52 | 89.4 | 294 | 21 | 7.51 | 77.9 | 169 | 21 |
| | D | 7.55 | 90.2 | 294 | 21 | 7.6 | 83.7 | 174 | 21 |
| RET | A | 7.71 | 90.2 | 378 | 21 | 7.64 | 80.7 | 275 | 21 |
| | B | 7.67 | 90.1 | 351 | 21 | 7.66 | 79.2 | 262 | 21 |
| | C | 7.65 | 91 | 375 | 21 | 7.62 | 82.6 | 246 | 21 |
| | D | 7.67 | 91.3 | 374 | 21 | 7.75 | 86.9 | 262 | 21 |
| REM | A | 7.58 | 88.6 | 303 | 21 | 7.66 | 73.7 | 210 | 21 |
| | B | 7.53 | 89.1 | 300 | 21 | 7.64 | 64.4 | 187 | 21 |
| | C | 7.53 | 89.6 | 299 | 21 | 7.71 | 81.9 | 223 | 21 |
| | D | 7.46 | 90.1 | 298 | 21 | 7.7 | 79.2 | 194 | 21 |
| RES | A | 7.47 | 91.5 | 500 | 21 | 8.72 | 106.6 | 754 | 21 |
| | B | 7.48 | 91.1 | 484 | 21 | 8.8 | 103.5 | 792 | 21 |
| | C | 7.65 | 91.7 | 507 | 21 | 8.87 | 113 | 699 | 21 |
| | D | 7.6 | 91.6 | 492 | 21 | 8.84 | 104.8 | 759 | 21 |
| | | | | | | | | | |
| Treatment | Replicate | Water Quality at Day 1 | | | | Water Quality at test completion | | | |
| | | pH | DO (% saturation) | Conductivity ($\mu\text{S}/\text{cm}$) | Temperature ($^{\circ}\text{C}$) | pH | DO (% saturation) | Conductivity ($\mu\text{S}/\text{cm}$) | Temperature ($^{\circ}\text{C}$) |
| Control | A | 7.51 | 110.5 | 339 | 21 | 5.91 | 90.4 | 182 | 21 |
| | B | 7.36 | 107.9 | 351 | 21 | 6.03 | 90.3 | 190 | 21 |
| | C | 7.40 | 104.4 | 346 | 21 | 5.83 | 91.0 | 186 | 21 |
| | D | 7.33 | 103.2 | 362 | 21 | 6.65 | 88.7 | 171 | 21 |
| BBT | A | 7.79 | 95.9 | 527 | 21 | 7.98 | 88.7 | 316 | 21 |
| | B | 7.90 | 110.9 | 584 | 21 | 7.95 | 88.0 | 371 | 21 |
| | C | 7.95 | 101.6 | 531 | 21 | 7.98 | 86.9 | 312 | 21 |
| | D | 7.84 | 103.4 | 560 | 21 | 7.88 | 77.5 | 326 | 21 |
| BBM | A | 7.83 | 106.8 | 535 | 21 | 8.06 | 91.4 | 315 | 21 |
| | B | 7.8 | 113.3 | 503 | 21 | 8.05 | 91.2 | 318 | 21 |
| | C | 7.23 | 110.5 | 615 | 21 | 8.07 | 90.1 | 307 | 21 |
| | D | 7.48 | 110.1 | 568 | 21 | 8.09 | 90.3 | 296 | 21 |
| BET | A | 7.66 | 109.9 | 526 | 21 | 7.94 | 89.3 | 326 | 21 |
| | B | 7.82 | 104.5 | 570 | 21 | 8.03 | 90.1 | 347 | 21 |
| | C | 7.8 | 98.9 | 561 | 21 | 8.02 | 86.9 | 300 | 21 |
| | D | 7.99 | 95.7 | 542 | 21 | 7.97 | 87.7 | 314 | 21 |
| BEM | A | 7.63 | 101.9 | 536 | 21 | 8.31 | 89.6 | 311 | 21 |
| | B | 7.87 | 114.3 | 511 | 21 | 8.19 | 92.4 | 319 | 21 |
| | C | 7.64 | 108.8 | 584 | 21 | 8.12 | 92 | 318 | 21 |
| | D | 7.75 | 109.3 | 491 | 21 | 7.96 | 71.4 | 307 | 21 |
| BES | A | 8.22 | 88.6 | 670 | 21 | 8.49 | 88.5 | 888 | 21 |
| | B | 8.3 | 89.1 | 678 | 21 | 8.65 | 89.8 | 872 | 21 |
| | C | 8.32 | 88.5 | 683 | 21 | 8.65 | 88.9 | 880 | 21 |
| | D | 8.28 | 85.2 | 704 | 21 | 8.59 | 87.8 | 868 | 21 |

| Treatment | Replicate | Water Quality at Day 1 | | | | Water Quality at test completion | | | |
|-----------|-----------|------------------------|----------------------|-------------------------|-----------------------|----------------------------------|----------------------|-------------------------|-----------------------|
| | | pH | DO (% saturation) | Conductivity (µS/cm) | Temperature (° C) | pH | DO (% saturation) | Conductivity (µS/cm) | Temperature (° C) |
| Control | A | 7.82 | 78.7 | 311 | 21 | 8.20 | 93.2 | 168 | 21 |
| | B | 7.74 | 67.4 | 319 | 21 | 8.35 | 96.0 | 185 | 21 |
| | C | 7.76 | 82.7 | 306 | 21 | 8.13 | 92.3 | 203 | 21 |
| | D | 7.71 | 79.5 | 325 | 21 | 8.55 | 101.6 | 177 | 21 |
| SET | A | 7.65 | 90.1 | 426 | 21 | 8.28 | 93.9 | 285 | 21 |
| | B | 7.98 | 90.2 | 416 | 21 | 8.73 | 100.6 | 255 | 21 |
| | C | 8.06 | 89.6 | 426 | 21 | 8.7 | 97 | 265 | 21 |
| | D | 8.14 | 89.3 | 436 | 21 | 8.59 | 95.4 | 288 | 21 |
| SEM | A | 8.09 | 91.6 | 351 | 21 | 8.55 | 92.2 | 248 | 21 |
| | B | 8.11 | 89.1 | 389 | 21 | 8.55 | 92.9 | 249 | 21 |
| | C | 8.1 | 86.1 | 391 | 21 | 8.54 | 92 | 235 | 21 |
| | D | 8.18 | 89 | 375 | 21 | 8.52 | 92.4 | 241 | 21 |
| SES | A | 8.13 | 72.9 | 511 | 21 | 8.74 | 87.7 | 641 | 21 |
| | B | 8.12 | 61.7 | 499 | 21 | 8.75 | 80.1 | 661 | 21 |
| | C | 8.09 | 76 | 504 | 21 | 8.69 | 87 | 641 | 21 |
| | D | 8 | 66.4 | 502 | 21 | 8.7 | 81.9 | 658 | 21 |
| | | | | | | | | | |
| Treatment | Replicate | Water Quality at Day 1 | | | | Water Quality at test completion | | | |
| | | pH | DO (% saturation) | Conductivity (µS/cm) | Temperature (° C) | pH | DO (% saturation) | Conductivity (µS/cm) | Temperature (° C) |
| Control | A | 7.29 | 90.8 | 306 | 21 | 8.33 | 83.0 | 175 | 21 |
| | B | 7.23 | 84.7 | 320 | 21 | 8.02 | 78.4 | 176 | 21 |
| | C | 7.11 | 93 | 298 | 21 | 7.77 | 80.6 | 169 | 21 |
| | D | 7.13 | 92.9 | 295 | 21 | 7.67 | 83.6 | 171 | 21 |
| VBT | A | 7.84 | 90.2 | 373 | 21 | 7.15 | 86.8 | 328 | 21 |
| | B | 7.82 | 93.6 | 378 | 21 | 7.22 | 67.5 | 358 | 21 |
| | C | 7.76 | 92.5 | 367 | 21 | 7.40 | 80.5 | 309 | 21 |
| | D | 7.68 | 91.7 | 385 | 21 | 7.49 | 84.3 | 370 | 21 |
| VBM | A | 7.65 | 92 | 356 | 21 | 7.42 | 71.2 | 324 | 21 |
| | B | 7.62 | 92.1 | 329 | 21 | 7.57 | 79.5 | 293 | 21 |
| | C | 7.51 | 90.8 | 354 | 21 | 7.49 | 62.2 | 300 | 21 |
| | D | 7.55 | 89 | 361 | 21 | 7.63 | 75.6 | 302 | 21 |
| VET | A | 7.59 | 93.3 | 376 | 21 | 7.58 | 85.2 | 297 | 21 |
| | B | 7.68 | 93 | 361 | 21 | 7.64 | 85.3 | 285 | 21 |
| | C | 7.63 | 90.5 | 378 | 21 | 7.69 | 85.6 | 311 | 21 |
| | D | 7.68 | 92.2 | 366 | 21 | 7.71 | 85.9 | 302 | 21 |
| VEM | A | 7.45 | 88.5 | 351 | 21 | 7.77 | 86.3 | 290 | 21 |
| | B | 7.46 | 86.3 | 367 | 21 | 7.65 | 72.2 | 287 | 21 |
| | C | 7.51 | 89.3 | 353 | 21 | 7.62 | 72.9 | 291 | 21 |
| | D | 7.58 | 89.8 | 363 | 21 | 7.66 | 73.9 | 278 | 21 |
| VES | A | 7.18 | 89.4 | 510 | 21 | 8.39 | 74.1 | 891 | 21 |
| | B | 7.19 | 87.8 | 547 | 21 | 7.52 | 77.9 | 810 | 21 |
| | C | 7.27 | 89 | 518 | 21 | 7.51 | 81 | 696 | 21 |
| | D | 7.28 | 89.6 | 515 | 21 | 7.48 | 81.8 | 806 | 21 |

| Treatment | Replicate | Water Quality at Day 1 | | | | Water Quality at test completion | | | |
|-----------|-----------|------------------------|----------------------|-------------------------|-----------------------|----------------------------------|----------------------|-------------------------|-----------------------|
| | | pH | DO (% saturation) | Conductivity (µS/cm) | Temperature (° C) | pH | DO (% saturation) | Conductivity (µS/cm) | Temperature (° C) |
| Control | A | 6.71 | 63.9 | 273 | 21 | 7.63 | 92.3 | 257 | 21 |
| | B | 6.79 | 71.4 | 272 | 21 | 7.66 | 89.3 | 242 | 21 |
| | C | 7.19 | 69.9 | 278 | 21 | 7.84 | 92.8 | 246 | 21 |
| | D | 7.20 | 71.2 | 286 | 21 | 7.89 | 92.4 | 259 | 21 |
| PBT | A | 7.65 | 85.5 | 361 | 21 | 7.89 | 92.2 | 200 | 21 |
| | B | 7.70 | 87.5 | 373 | 21 | 7.81 | 91.3 | 193 | 21 |
| | C | 7.70 | 88.4 | 360 | 21 | 7.82 | 90.4 | 198 | 21 |
| | D | 7.72 | 86.8 | 368 | 21 | 7.8 | 90.1 | 197 | 21 |
| PBM | A | 7.64 | 81.8 | 317 | 21 | 8.04 | 91.3 | 328 | 21 |
| | B | 7.55 | 80.4 | 323 | 21 | 8.17 | 89.3 | 321 | 21 |
| | C | 7.58 | 81 | 329 | 21 | 8.26 | 90.8 | 334 | 21 |
| | D | 7.57 | 77.9 | 310 | 21 | 8.24 | 90.5 | 332 | 21 |
| PET | A | 7.78 | 85.4 | 413 | 21 | 8.17 | 87.9 | 252 | 21 |
| | B | 7.84 | 84.2 | 390 | 21 | 8.03 | 85.3 | 262 | 21 |
| | C | 7.85 | 86.4 | 422 | 21 | 8.04 | 87.4 | 271 | 21 |
| | D | 7.89 | 86.1 | 419 | 21 | 8.1 | 88.7 | 260 | 21 |
| PEM | A | 7.59 | 71.6 | 372 | 21 | 7.3 | 54.7 | 151 | 21 |
| | B | 7.63 | 77.3 | 366 | 21 | 7.12 | 82.6 | 144 | 21 |
| | C | 7.66 | 78.5 | 372 | 21 | 6.99 | 83 | 145 | 21 |
| | D | 7.68 | 71.4 | 372 | 21 | 6.69 | 84.1 | 156 | 21 |
| PES | A | 7.46 | 53.1 | 607 | 21 | 8.48 | 68.2 | 908 | 21 |
| | B | 7.58 | 69.8 | 514 | 21 | 8.76 | 81.3 | 895 | 21 |
| | C | 7.53 | 66.3 | 463 | 21 | 8.76 | 78.6 | 880 | 21 |
| | D | 7.56 | 55.4 | 498 | 21 | 8.79 | 89.5 | 909 | 21 |
| | | | | | | | | | |
| | | | | | | | | | |
| Treatment | Replicate | Water Quality at Day 1 | | | | Water Quality at test completion | | | |
| | | pH | DO (% saturation) | Conductivity (µS/cm) | Temperature (° C) | pH | DO (% saturation) | Conductivity (µS/cm) | Temperature (° C) |
| Control | A | 6.71 | 75.1 | 296 | 21 | 6.86 | 93.1 | 221.0 | 21 |
| | B | 6.81 | 80.3 | 294 | 21 | 7.25 | 92.2 | 219.6 | 21 |
| | C | 7.01 | 86.7 | 281 | 21 | 7.22 | 91.8 | 210.0 | 21 |
| | D | 7.03 | 79.0 | 303 | 21 | 7.15 | 91.6 | 252.0 | 21 |
| KET | A | 7.37 | 88.9 | 367 | 21 | 7.39 | 91.1 | 247 | 21 |
| | B | 7.48 | 88.8 | 371 | 21 | 7.62 | 89.8 | 264 | 21 |
| | C | 7.59 | 89.6 | 371 | 21 | 7.52 | 90.5 | 249 | 21 |
| | D | 7.65 | 90.6 | 380 | 21 | 7.57 | 91.3 | 278 | 21 |
| KEM | A | 7.57 | 85.2 | 303 | 21 | 7.52 | 91.5 | 276 | 21 |
| | B | 7.42 | 81.9 | 303 | 21 | 7.54 | 92.8 | 188.8 | 21 |
| | C | 7.44 | 87.4 | 286 | 21 | 7.55 | 91.2 | 184.2 | 21 |
| | D | 7.43 | 83.5 | 299 | 21 | 7.45 | 93.6 | 213.6 | 21 |
| KES | A | 7.53 | 92.4 | 492 | 21 | 8.8 | 107.4 | 548 | 21 |
| | B | 7.49 | 93 | 491 | 21 | 8.82 | 99.2 | 598 | 21 |
| | C | 7.3 | 92.7 | 470 | 21 | 8.51 | 91.2 | 586 | 21 |
| | D | 7.39 | 93 | 504 | 21 | 8.51 | 94.8 | 488 | 21 |

| Treatment | Replicate | Water Quality at Day 1 | | | | Water Quality at test completion | | | |
|-----------|-----------|------------------------|----------------------|-------------------------------|--------------------------------|----------------------------------|----------------------|-------------------------------|--------------------------------|
| | | pH | DO (% saturation) | Conductivity (μ S/cm) | Temperature ($^{\circ}$ C) | pH | DO (% saturation) | Conductivity (μ S/cm) | Temperature ($^{\circ}$ C) |
| Control | A | 7.61 | 85.5 | 270 | 21 | 7.27 | 82.4 | 171 | 21 |
| | B | 7.36 | 86.7 | 291 | 21 | 6.86 | 87.4 | 156 | 21 |
| | C | 7.30 | 85 | 275 | 21 | 7.65 | 97.3 | 143 | 21 |
| | D | 7.27 | 84.8 | 223 | 21 | 7.29 | 78.5 | 148 | 21 |
| FBT | A | 7.40 | 95.9 | 434 | 21 | 8.13 | 113.1 | 367 | 21 |
| | B | 7.57 | 87.5 | 425 | 21 | 8.27 | 101.0 | 350 | 21 |
| | C | 7.62 | 90 | 408 | 21 | 8.14 | 89.2 | 383 | 21 |
| | D | 7.65 | 92.2 | 427 | 21 | 8.29 | 99.2 | 380 | 21 |
| FBM | A | 7.64 | 89.8 | 468 | 21 | 7.85 | 105.7 | 318 | 21 |
| | B | 7.61 | 81.1 | 453 | 21 | 8.06 | 105.2 | 307 | 21 |
| | C | 7.76 | 85.7 | 443 | 21 | 8.04 | 95.8 | 312 | 21 |
| | D | 7.75 | 81.1 | 454 | 21 | 8.07 | 94.2 | 302 | 21 |
| FET | A | 7.82 | 82.7 | 441 | 21 | 8.15 | 111.2 | 288 | 21 |
| | B | 7.81 | 86 | 440 | 21 | 8.28 | 117 | 308 | 21 |
| | C | 7.72 | 86.9 | 407 | 21 | 8.17 | 93 | 330 | 21 |
| | D | 7.84 | 89.2 | 411 | 21 | 8.13 | 98.3 | 312 | 21 |
| FEM | A | 7.72 | 88.9 | 391 | 21 | 8.67 | 118.2 | 257 | 21 |
| | B | 7.69 | 83.6 | 394 | 21 | 8.35 | 97.3 | 279 | 21 |
| | C | 7.7 | 84.2 | 390 | 21 | 8.19 | 98.1 | 290 | 21 |
| | D | 7.69 | 85.9 | 403 | 21 | 8.11 | 93 | 321 | 21 |
| FES | A | 7.38 | 85 | 549 | 21 | 9.3 | 110.2 | 603 | 21 |
| | B | 7.42 | 83.6 | 550 | 21 | 9.2 | 112.2 | 621 | 21 |
| | C | 7.44 | 86.9 | 542 | 21 | 8.83 | 118.6 | 681 | 21 |

Table H4. Abbreviations used in blackworm and midge sediment toxicity tests

| | |
|-----|--|
| RBT | Ravine Baseline excavated rock on Top of reservoir sediment |
| RBM | Ravine Baseline excavated rock mixed with reservoir sediment |
| RET | Ravine Enriched excavated rock on Top of reservoir sediment |
| REM | Ravine Enriched excavated rock mixed with reservoir sediment |
| RES | Ravine Enriched Excavated rock |
| BBT | Byron Baseline excavated rock on Top of reservoir sediment |
| BBM | Byron Baseline excavated rock mixed with reservoir sediment |
| BET | Byron Enriched excavated rock on Top of reservoir sediment |
| BEM | Byron Enriched excavated rock mixed with reservoir sediment |
| BES | Byron Enriched Excavated rock |
| SET | Shaw Gabbro Enriched excavated rock on Top of reservoir sediment |
| SEM | Shaw Gabbro Enriched excavated rock mixed with reservoir sediment |
| SES | Shaw Gabbro Enriched Excavated rock |
| VBT | Volcanics Baseline excavated rock on Top of reservoir sediment |
| VBM | Volcanics Baseline excavated rock mixed with reservoir sediment |
| VET | Volcanics Enriched excavated rock on Top of reservoir sediment |
| VEM | Volcanics Enriched excavated rock mixed with reservoir sediment |
| VES | Volcanics Enriched Excavated rock |
| PBT | Peppercorn Baseline excavated rock on Top of reservoir sediment |
| PBM | Peppercorn Baseline excavated rock mixed with reservoir sediment |
| PET | Peppercorn Enriched excavated rock on Top of reservoir sediment |
| PEM | Peppercorn Enriched excavated rock mixed with reservoir sediment |
| PES | Peppercorn Enriched Excavated rock |
| KET | Kelly's Plains Enriched excavated rock on Top of reservoir sediment |
| KEM | Kelly's Plains Enriched excavated rock mixed with reservoir sediment |
| KES | Kelly's Plains Enriched Excavated rock |
| FBT | Felsics Baseline excavated rock on Top of reservoir sediment |
| FBM | Felsics Baseline excavated rock mixed with reservoir sediment |
| FET | Felsics Enriched excavated rock on Top of reservoir sediment |
| FEM | Felsics Enriched excavated rock mixed with reservoir sediment |
| FES | Felsics Enriched Excavated rock |

Table H5. Copper reference toxicity tests with the blackworm (*Lumbriculus variegatus*) during sediment and excavated rock chronic toxicity tests.

| Treatment | After 48 hours | | | | | | | |
|--------------|----------------|---|---|---|--------|---|---|---|
| | # Alive | | | | # Dead | | | |
| | A | B | C | D | A | B | C | D |
| MHW | 5 | 5 | 5 | 5 | 0 | 0 | 0 | 0 |
| TAL | 5 | 5 | 5 | 5 | 0 | 0 | 0 | 0 |
| Cu 31.25µg/l | 5 | 5 | 5 | 5 | 0 | 0 | 0 | 0 |
| Cu 62.5µg/l | 4 | 5 | 5 | 4 | 1 | 0 | 0 | 1 |
| Cu125µg/l | 4 | 5 | 5 | 4 | 1 | 0 | 0 | 1 |
| Cu 250µg/l | 3 | 2 | 3 | 2 | 2 | 3 | 2 | 3 |
| Cu 500µg/l | 3 | 2 | 3 | 2 | 2 | 3 | 2 | 3 |
| Cu 1000µg/l | 0 | 0 | 0 | 0 | 5 | 5 | 5 | 5 |
| Cu 2000µg/l | 0 | 0 | 0 | 0 | 5 | 5 | 5 | 5 |

| Treatment | After 48 hours | | | | | | | |
|--------------|----------------|---|---|---|--------|---|---|---|
| | # Alive | | | | # Dead | | | |
| | A | B | C | D | A | B | C | D |
| MHW | 5 | 5 | 5 | 5 | 0 | 0 | 0 | 0 |
| TAL | 5 | 5 | 5 | 5 | 0 | 0 | 0 | 0 |
| Cu 31.25µg/l | 5 | 5 | 5 | 5 | 0 | 0 | 0 | 0 |
| Cu 62.5µg/l | 4 | 5 | 5 | 4 | 1 | 0 | 0 | 1 |
| Cu125µg/l | 5 | 4 | 3 | 5 | 0 | 1 | 2 | 0 |
| Cu 250µg/l | 2 | 3 | 3 | 3 | 3 | 2 | 2 | 2 |
| Cu 500µg/l | 3 | 3 | 3 | 2 | 2 | 2 | 2 | 3 |
| Cu 1000µg/l | 0 | 2 | 3 | 0 | 5 | 3 | 2 | 5 |
| Cu 2000µg/l | 0 | 0 | 0 | 0 | 5 | 5 | 5 | 5 |

| Treatment | After 48 hours | | | | | |
|--------------|----------------|---|---|--------|---|---|
| | # Alive | | | # Dead | | |
| | A | B | C | A | B | C |
| MHW | 5 | 5 | 5 | 0 | 0 | 0 |
| TAL | 5 | 5 | 5 | 0 | 0 | 0 |
| Cu 31.25µg/l | 5 | 5 | 5 | 0 | 0 | 0 |
| Cu 62.5µg/l | 4 | 5 | 4 | 1 | 0 | 1 |
| Cu125µg/l | 4 | 4 | 3 | 1 | 1 | 2 |
| Cu 250µg/l | 2 | 3 | 0 | 3 | 2 | 5 |
| Cu 500µg/l | 0 | 2 | 0 | 5 | 3 | 5 |
| Cu 1000µg/l | 1 | 0 | 0 | 4 | 5 | 5 |
| Cu 2000µg/l | 0 | 0 | 0 | 5 | 5 | 5 |

Table G6. The effective concentration (µg/L) of copper at 50%, 10% and 20% for blackworms (*Lumbriculus variegatus*) during chronic toxicity tests

| Copper reference test | EC50(µg/l) | 95% Conf. intervals For EC50 | | EC10(µg/l) | 95% Conf. intervals For EC10 | |
|-----------------------|------------|------------------------------|--------|------------|------------------------------|--------|
| | | | | | | |
| Test 1 | 332.82 | 258.01 | 429.33 | 94.26 | 54.75 | 162.26 |
| Test 2 | 376.37 | 249.67 | 567.38 | 66.64 | 26.17 | 169.69 |
| Test 3 | 189.34 | 141.17 | 253.93 | 63.70 | 31.20 | 130.06 |

Appendix I SEM analyses of excavated rock

Provided as supplementary information

Appendix J XRD analyses of Baseline and Enriched excavated rock

Provided as supplementary information

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Annexure E Dissolved Aluminium assessment for Talbingo Reservoir



Australia's National
Science Agency

Dissolved aluminium assessment for Talbingo Reservoir

Stuart L. Simpson

August 2019

Prepared for Haskoning Australia (HKA) on behalf of Snowy Hydro Limited (SHL)

Report number: EP195920 [Commercial-in-confidence]

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Foreword

In November 2017, CSIRO was requested by Snowy Hydro Limited (SHL) to provide scientific expertise and capability in relation to identifying and assessing the environmental risks associated with the placement of excavated rocks from the development and operations of the proposed Snowy 2.0 scheme into Talbingo Reservoir and Tantangara Reservoir. EMM Consulting (EMM) was to prepare the Environmental Impact Statement (EIS) on behalf of SHL, and CSIRO would undertake a series of assignments to provide scientific information for the environmental risk assessment (ERA) associated with the handling of excavated rock materials from the proposed works. In December 2017, CSIRO worked with EMM to develop conceptual models of the proposed works (source, fate and receptors) to provide information to the ERA. As a result, CSIRO was commissioned to undertake an initial series of four assignments. In March 2018, Haskoning Australia (HKA) was engaged to provide additional capability, specifically to lead the project entitled: “Engineering Option for Placement of Excavated Rocks”. The draft work assignments that CSIRO had previously provided to SHL and EMM (in late January 2018) were subsequently updated to ensure that they would fulfil the needs of EIS requirements and of this project. These updated assignment(s) have now been completed. In August 2019, CSIRO were engaged to undertake a desktop assessment to estimate where and after how much time in Talbingo Reservoir would aluminium concentrations return to below default guideline values and to baseline concentrations. This report details the results and findings of that assessment.

Disclaimer

This Assignment Subcontract and all documents and information provided by CSIRO to HKA under this Assignment Subcontract are prepared: (i) as inputs for further scientific services to be performed for HKA by CSIRO under separate Assignment Subcontracts that has been agreed; and (ii) to assist HKA in its development of an excavated rock disposal and management plan as part of the environmental impact assessment process for the proposed Snowy 2.0 Pumped Hydro Electric Scheme (“Purpose”), and for no other purpose. This Assignment Subcontract does not involve the provision of advice or recommendations in relation to specific risks or mitigations associated with Excavated Rock disposal and management or design and construction of the Snowy 2.0 project, however, it is understood that the inputs provided by CSIRO are for the Purpose and are based on CSIRO’s professional skill, care and diligence in performing this Assignment Subcontract. In the course of performing this Assignment Subcontract, CSIRO may rely on stated assumptions and/or information provided by HKA or third parties which is not within the control of CSIRO, and this Assignment does not involve CSIRO verifying such assumptions or information except to the extent expressly stated herein. If CSIRO provides any forecasts or projections, CSIRO does not represent that they will be realised as forecast or projected and actual outcomes may vary materially from forecast or projected outcomes. Documents and information provided to HKA under this Assignment Subcontract are to be read as a whole, and if reproduced must be reproduced in full and no part should be read or relied upon out of context. CSIRO does not accept responsibility for, or liability arising from, any error in, or omission in connection with, stated assumptions or third party-supplied information, or reliance on documents or information provided under this Assignment by HKA other than for the Purpose, or by any other person.

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Acknowledgments

CSIRO would like to acknowledge the support from Haskoning Australia (HKA) and Snowy Hydro Limited (SHL) in acquiring information for this report. We thank Greg Britton and Arjen Overduin of HKA for discussions and provision of information on the hydrodynamic model for Talbingo Reservoir. We thank Graeme Batley and Brad Angel (CSIRO) for an internal review of the report.

Executive summary

Snowy Hydro Limited (SHL) are exploring options for the placement of excavated rock within the two reservoirs Talbingo and Tantangara, as part of a proposed Snowy 2.0 Pumped Hydro Electric Scheme (Snowy 2.0). The excavated rock placement should not compromise, within reasonable parameters, the ecological, chemical, physiochemical, or physical state of the environment in the reservoirs. Previously, CSIRO were engaged by Haskoning Australia (HKA) on behalf of SHL to provide a series of studies involving tests and data analysis to help inform an Environmental Impact Statement (EIS) for Snowy 2.0. CSIRO study Assignment P4, 'Environmental Categorisation of Excavated Rock Interactions with and Potential Impacts on Reservoir Waters and Sediments', identified that changes in water pH, conductivity and dissolved aluminium concentrations may occur in both Talbingo and Tantangara Reservoirs as a result of increases in concentrations of fine excavated rock materials.

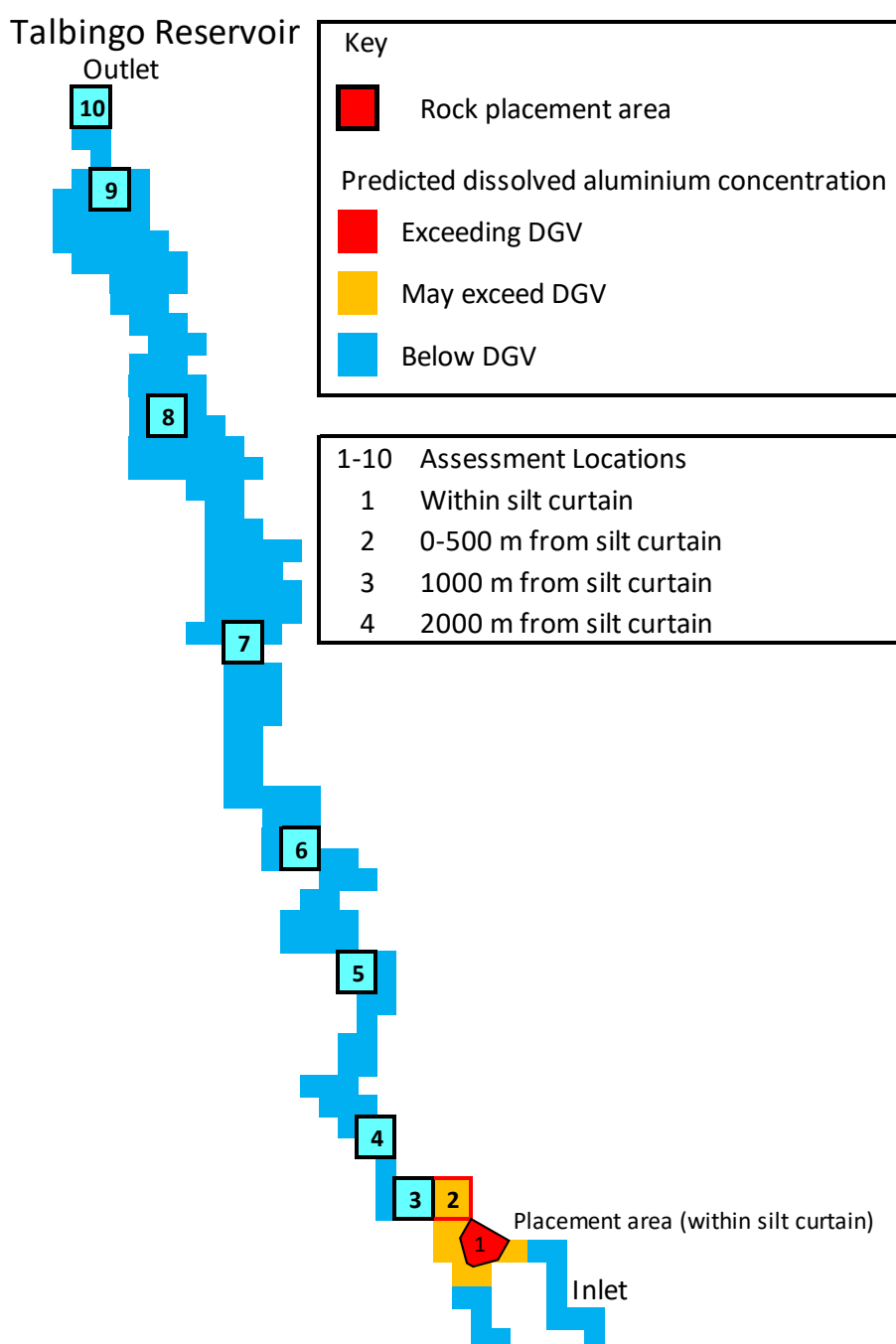
Here, CSIRO have been engaged to undertake a desktop assessment to estimate where and after how much time in Talbingo Reservoir aluminium concentrations would return to below default guideline values (GVs) and baseline concentrations. For the task, data from CSIRO Assignment P4 (Simpson et al., 2019) were summarised and used to develop relationships between the concentration of fine excavated rock materials suspended in Talbingo Reservoir water (mg/L) and concentrations of dissolved aluminium ($\mu\text{g/L}$). The relationships considered the water temperature and duration that the excavated rock materials were suspended within the water. Using these relationships, the hydrodynamic model for Talbingo Reservoir was used to predict total suspended solids concentrations (TSS, mg/L) of excavated rock within surface, middle and bottom waters at ten locations within the reservoir. The predictions were made for the 2-year duration of the proposed works (rock placement) and for 1-year following their completion, and considered the seasonal heating/cooling periods.

The assessment indicates that dissolved aluminium concentrations may exceed the default GV (DGV) of 55 $\mu\text{g/L}$ within the placement area contained by the silt curtain (Location 1). Outside the silt curtain, a gradient (mixing zone) is expected to develop, along which dissolved aluminium released in Location 1 will dilute and some further aluminium release from particles will occur. In the 500 m space between Location 1 and Location 2, the dissolved aluminium concentrations may also exceed the DGV. Beyond Location 2, the dissolved aluminium concentrations are predicted to remain below the DGV, and within a factor of 2-3 of the background aluminium concentrations of 5-10 $\mu\text{g/L}$.

Significant uncertainty exists with the predictions on both the high side (higher dissolved aluminium) and low side (lower dissolved aluminium). CSIRO Assignment P4 (Simpson et al., 2019) describes a number of data/knowledge gaps that influence this uncertainty. Higher TSS concentrations and higher water pH are considered the primary drivers for higher dissolved aluminium concentrations. Lower water temperatures will result in lower dissolved aluminium concentrations. At Location 1 (placement area), should the pH not rise as high in the field environment as it did in the laboratory tests (CSIRO Assignment P4), then the dissolved aluminium concentrations in the field may be considerably lower within Location 1 than those predicted here.

Greater rates of water dilution will also lower dissolved aluminium concentrations in Location 1, and the export of the aluminium to locations further down the reservoir may not substantially increase the predicted concentrations at those locations. While difficult to estimate, the predictions may have 50% uncertainty on both the high or low sides for Location 1 and 2. At Locations 2-10, attenuation reactions that result in lower water pH may result in substantially lower aluminium release from TSS at locations further from the placement area. The dilutions may also be greater than those estimated for these predictions, resulting in lower dissolved aluminium concentrations. For the locations beyond Location 2, the predictions will have even greater uncertainty, but dissolved aluminium concentrations seem likely to be within a factor of 2-3 of the background concentrations.

Assessment summary: Depiction of area where dissolved aluminium may exceed the water quality default guideline value (DGV) of 55 µg/L.



1 Introduction

1.1 Background

Snowy Hydro Limited (SHL) are embarking on the development of the landmark Snowy 2.0 Pumped Hydro Electric Scheme (Snowy 2.0). To accomplish Snowy 2.0, SHL will require “drill-out” of 27 km of tunnels between the two reservoirs Talbingo and Tantangara. It is proposed that a large quantity of the excavated rock that is generated from this activity be placed in the Talbingo Reservoir. As part of an Environmental Impact Statement (EIS), the engineering options chosen for the management and disposal of the excavated rock should result in minimal adverse effects on the reservoir environment.

Haskoning Australia (HKA) were appointed lead consultant to manage and deliver an Engineering Option Assessment for Excavated Rock Placement for Snowy 2.0. CSIRO has been requested to provide scientific insight into the environmental impacts associated with the placement of excavated rock in Talbingo Reservoir.

CSIRO Assignment P4 (Simpson et al., 2019) determined the waters of this reservoir to have neutral pH (6.9-7.3), low conductivity (26-29 $\mu\text{S}/\text{cm}$), low turbidity (0.2-0.5 NTU), and dissolved aluminium concentrations of $<10 \mu\text{g}/\text{L}$ ($<0.45 \mu\text{m}$ filterable). Assignment P4 determined that the mixing of excavated rock materials ($<75 \mu\text{m}$) with the Talbingo Reservoir waters resulted in concentrations of dissolved aluminium frequently exceeding the Australian national DGV for freshwaters of $55 \mu\text{g}/\text{L}$ (ANZG, 2018), accompanied by an increased pH (from approximately pH 7 to 9.5) and conductivity (from approximately 30 to $150 \mu\text{S}/\text{cm}$). Those studies investigated the influence of a range of rock-water mixing-leaching scenarios and conditions on dissolved aluminium release.

The CSIRO tests characterised differences in dissolved aluminium release that may occur due to differences in the concentration of solids in the water (liquid/solid ratio; L/S), time, repeat/successive leaching, rock particle size, temperature, and attenuation of substances released due to interactions with sediments. Without re-summarising those results, the more important observations were that dissolved aluminium release from fine rock into Talbingo water was lower at 6°C than at 21°C and greater with increased mixing duration, indicating ongoing release.

In this subsequent assignment, CSIRO has been requested to undertake a desktop assessment to estimate where and after how much time in Talbingo Reservoir aluminium concentrations return to below the DGV and baseline concentrations.

1.2 Methodology

Data used to construct relationships between the concentration of fine excavated rock materials suspended in Talbingo Reservoir water (mg/L) and concentrations of dissolved Al ($\mu\text{g/L}$) were taken entirely from Assignment P4 report (Simpson et al., 2019).

The hydrodynamic model for Talbingo Reservoir was used to predict total suspended solids concentrations (TSS, mg/L) of excavated rock within surface, middle and bottom waters at ten locations within the reservoir (data provided by HKA) (Figure 1). The particle size distribution of the TSS in the model was 12-15% clay ($<4\ \mu\text{m}$) and 85-88% silt ($4\text{-}63\ \mu\text{m}$).

Location 1 is within the placement area and separated by a silt curtain from Location 2 that was approximately 500 m down the reservoir (towards the outlet). In the hydrodynamic model, the silt curtain extended from the water surface to a depth of 15 m. The curtain should be impervious to rock material of all sizes (i.e. including clays) and was treated as impervious to water, although some water may pass through at a slowed flow rate. Significant amounts of TSS are predicted to pass below the silt curtain and some of this TSS is transported to Locations 2 to 10. Locations 3 and 4 were approximately 1000 and 2000 m beyond the silt curtain heading towards the reservoir outlet. Locations 5-9 continued towards to reservoir outlet, and the final Location 10 was nearest the reservoir outlet.

The CSIRO relationships and model predictions were then brought together to make predictions of concentrations of dissolved aluminium within the reservoir at the designated locations.

The quality of the CSIRO data and the hydrodynamic model, and associated assumptions influence the predicted dissolved aluminium concentrations. CSIRO Assignment P4 identified a number of data gaps, limited aluminium release data for fine excavated rock TSS concentrations $<500\ \text{mg/L}$, aluminium release over longer durations, and potentially successively larger changes in water quality (e.g. increasing higher pH leading to higher dissolved aluminium concentrations) that may occur in the placement area if mixing of the waters where aluminium release first occurs with the broader reservoir waters is constrained (naturally or by the presence of the silt curtain). There may also be longer-term attenuation processes (reducing dissolved aluminium concentrations) that have not yet been adequately characterised, and were not included in this assessment.

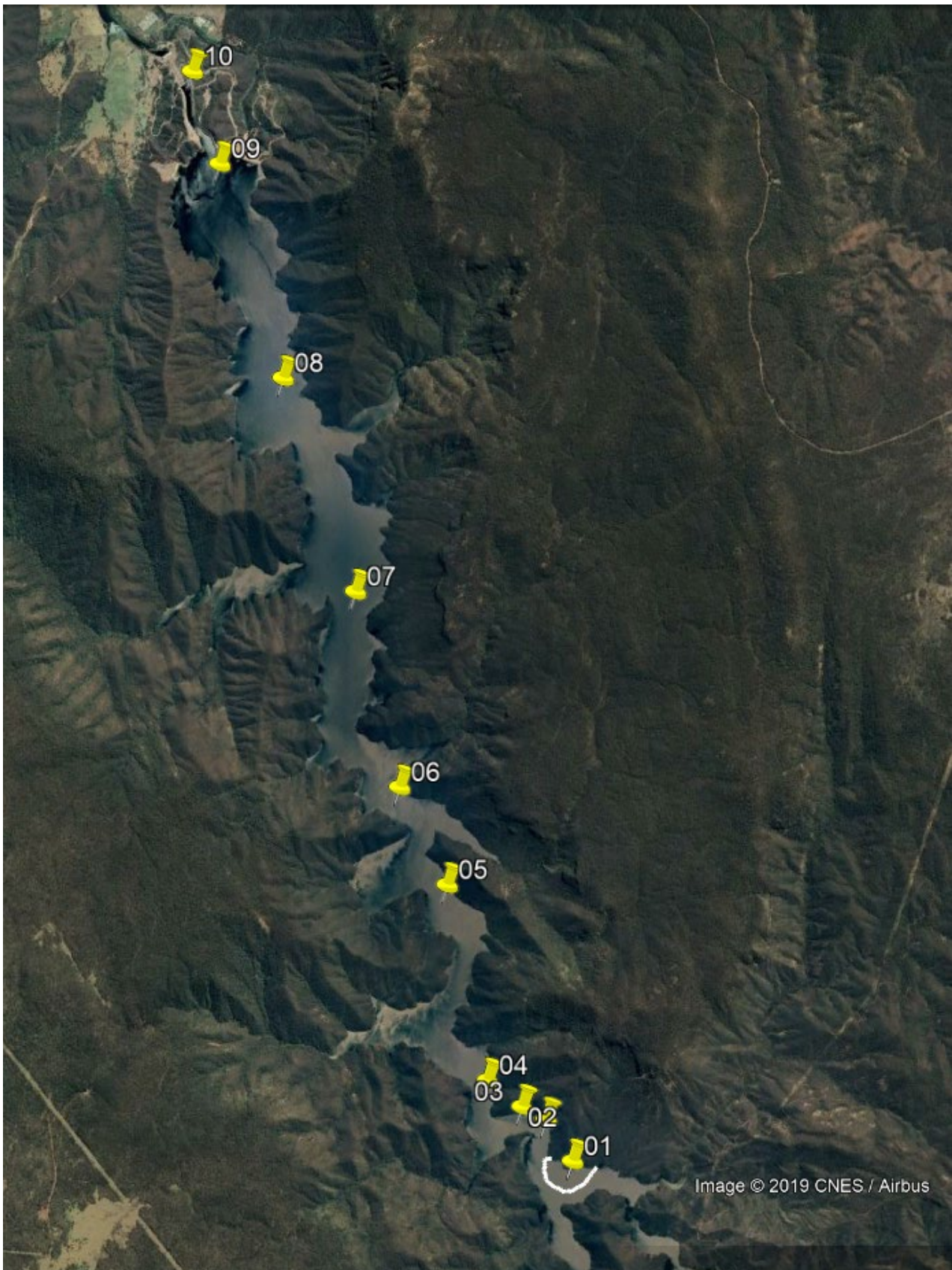


Figure 1. Locations with Talbingo Reservoir used in the study. The yellow pins indicate the locations used in the assessment, with Location 1 being closest to the reservoir inlet and Location 10 closest to the reservoir outlet. The white line depicts the location of a silt curtain.

1.2.1 Hydrodynamic model

In this report, we do not describe or discuss in detail any assumptions or possible limitations of the hydrodynamic model, but these may include factors such as changes in bathymetry (the placement area becoming shallower as rock is added resulting in warmer water temperatures), the rate and magnitude of dilution of waters within the placement area (through displacement from inflows of water or excavated rock, or dispersion throughout the reservoir), and the expected transmission of some water through the silt curtain (treated as impervious in the model).

Following release of aluminium from TSS (rock materials), a portion of the dissolved aluminium and fine rock will be dispersed and transported out from the placement area (Location 1), and then through the reservoir with the net flux towards the reservoir outlet (Location 10). The volume of water designated as the placement area (Location 1, within the silt curtain) is estimated to be 5,400,000 m³ (5,400,000,000 Litre (L). HKA, personal communication). The hydrodynamic model output provided to CSIRO had TSS data at 6-h time intervals throughout the 2-year placement and 1-year post-placement periods. The model had 'placement rate' of TSS constant for 6-month periods, being 2.75, 1.5, 2.1, 1.1, 0.0, 0.0 kg/s, respectively. This data was converted to kg/d, then kg/6-h, and finally mg/6-h time interval in order to calculate TSS added in mg/L. During each 6-h interval, a portion of the TSS and dissolved aluminium is exported to the next location. To estimate this a simple model was created with %-retained/6-h as a variable and fitted to the TSS-time data predicted in the hydrodynamic model. For %-retained in Location 1, a value of 9% per day (or 97.75%/6-h) estimated from a conservative tracer modelling run by HKA (Figure 2) was used for the CSIRO predictions.

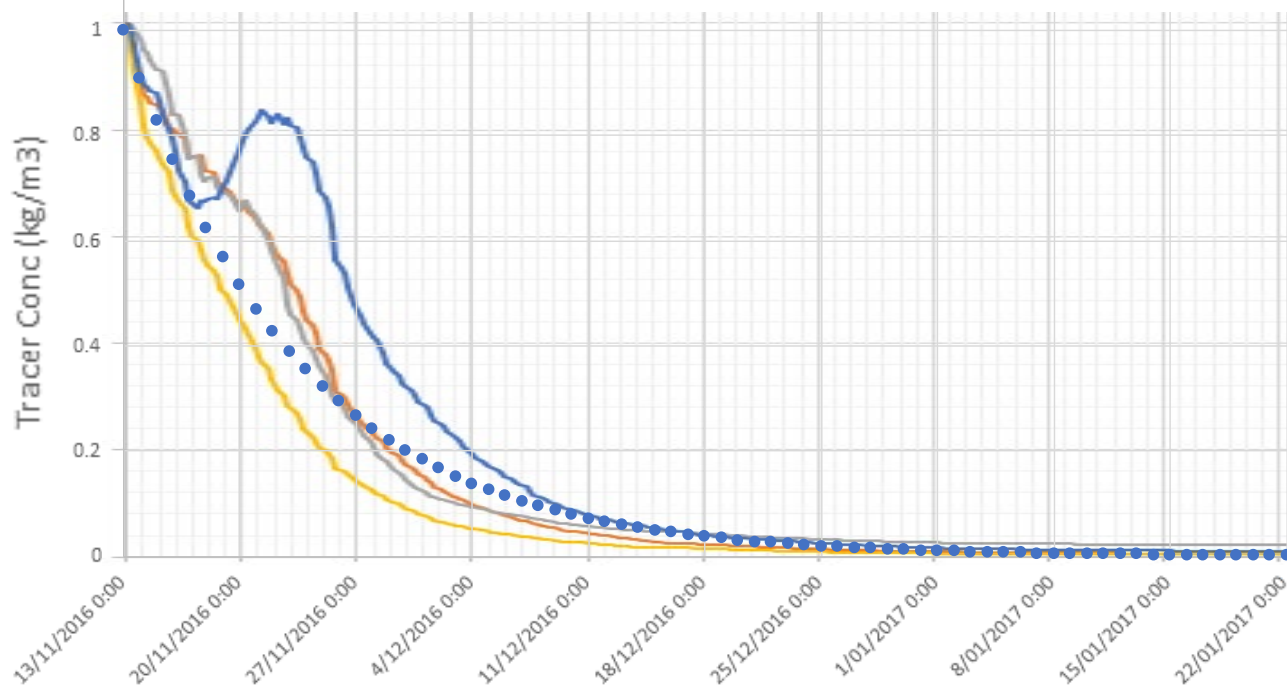


Figure 2. Rate of loss of tracer (normalised to 100% start) from Location 1. The four lines represent individual hydrodynamic model predictions of losses following ceasing of input (Background figure provided by HKA) at four different points within Location 1. The different position and shape of these lines reflects the variability of TSS within the water column. The dotted line is calculated as a loss of 9% of tracer/day (overlaid). Note: The start and end dates in this figure and later figures do not relate to proposed operations, but the duration is important.

Along the reservoir towards the outlet the values used were 15%/6-h for Location 2, 25%/6-h for Locations 3 and 4, and 40%/6-h for the remaining locations to the reservoir outlet (Figure 3).

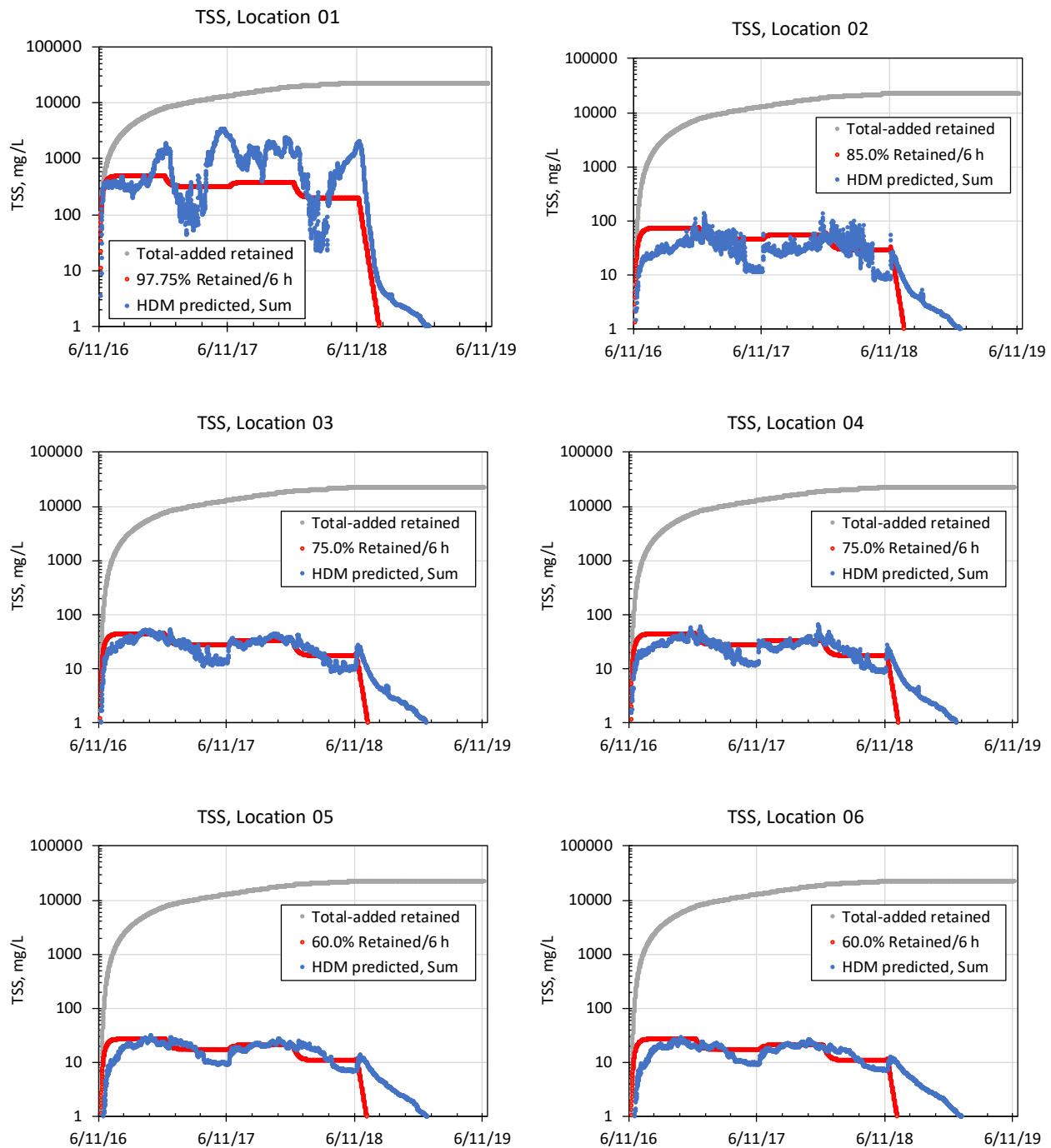


Figure 3. Total suspended solids (TSS) concentrations predicted from: (i) hydrodynamic model (HDM, sum of TSS in surface, middle and bottom waters), (ii) total added based on location placement rates and Location 01 volume or transfer to next locations (2, 3, 4, 5, ...), and (iii) retention factor (incremental changes derived from CSIRO model).

1.2.2 Effect of water temperature

The majority of the CSIRO data for aluminium release were from experiments conducted at a water temperature of 21°C, and a fewer number of tests were conducted at 6°C (none at intermediate temperatures). Based on water temperature profiles (Figure 4, Appendix A), the surface water temperatures may range from 16 to 25°C in summer (heating), and 6 to 8°C in winter (cooling). The waters are cooler at greater depth, with summer water temperature being 10-16°C at mid-depth and 6-8°C at the bottom.

For the purpose of this desktop assessment, the data were analysed separately to create two models for aluminium release at 21°C (5 months heating; Dec 1-April 30) and 6°C (5 months cooling; June 1-Oct 30), respectively (Figure 4). Only with aluminium release predicted from the 21°C and 6°C models, release at intermediate temperatures was predicted using mixtures of the 21°C and 6°C model outputs. For the mixed temperature predictions, during the heating period aluminium release was predicted from the 21°C model in surface waters, as 50:50 of 21°C- and 6°C-models in middle waters, and 20:80 of 21°C and 6°C models in bottom waters. During the cooling period, the aluminium release was predicted as 20:80 of 21°C- and 6°C-models in surface and middle waters and by the 6°C models in bottom waters. There were two intermediate months, indicated by the step transitions in temperature in Figure 3. In May (1 month, as the waters were predicted began to cool rapidly, Figure 4) aluminium was predicted from the 80:20 of 21°C and 6°C models in surface waters, 30:70 of 21°C- and 6°C-models in middle waters, and 20:80 of 21°C and 6°C models in bottom waters. In November (1 month, as the waters warmed rapidly), the aluminium release was predicted from the 50:50 of 21°C and 6°C models in surface waters, 30:70 of 21°C and 6°C models in middle waters, and 20:80 of 21°C and 6°C models in bottom waters. These mixed models are expected to provide a better estimate of the possible aluminium release than the individual models.

1.2.3 Effect of duration

Lower amounts of aluminium release were observed for mixing durations <6 h than for longer durations, and some attenuation (low net aluminium release) may have been occurring at durations ≥336 h (2 weeks). However, the data set was not large enough to enable a wide range of mixing durations to be analysed separately across an adequate range of excavated rock concentrations. With the purpose of simulating mid- to longer-term aluminium releases within the immediate placement area (within the curtain), the data set comprised results from experiments with durations ranging from 24 to 336 h. A second data set was created with results from experiments with durations ≤18 h, and while the overlap of these two data sets is not ideal, it was necessary to construct meaningful relationships at both 21°C and 6°C.

For the predictions, the model derived from the longer durations (24 to 336 h) was used for predicting aluminium release within the waters behind the silt curtain (Location 1). For the other locations (2 to 10), a model derived from the shorter durations (≤18 h) was used for predicting aluminium release because the rock particles are predicted to be dispersing and being diluted at a greater rate at these locations (i.e. most particles will move beyond this location within 18 h).

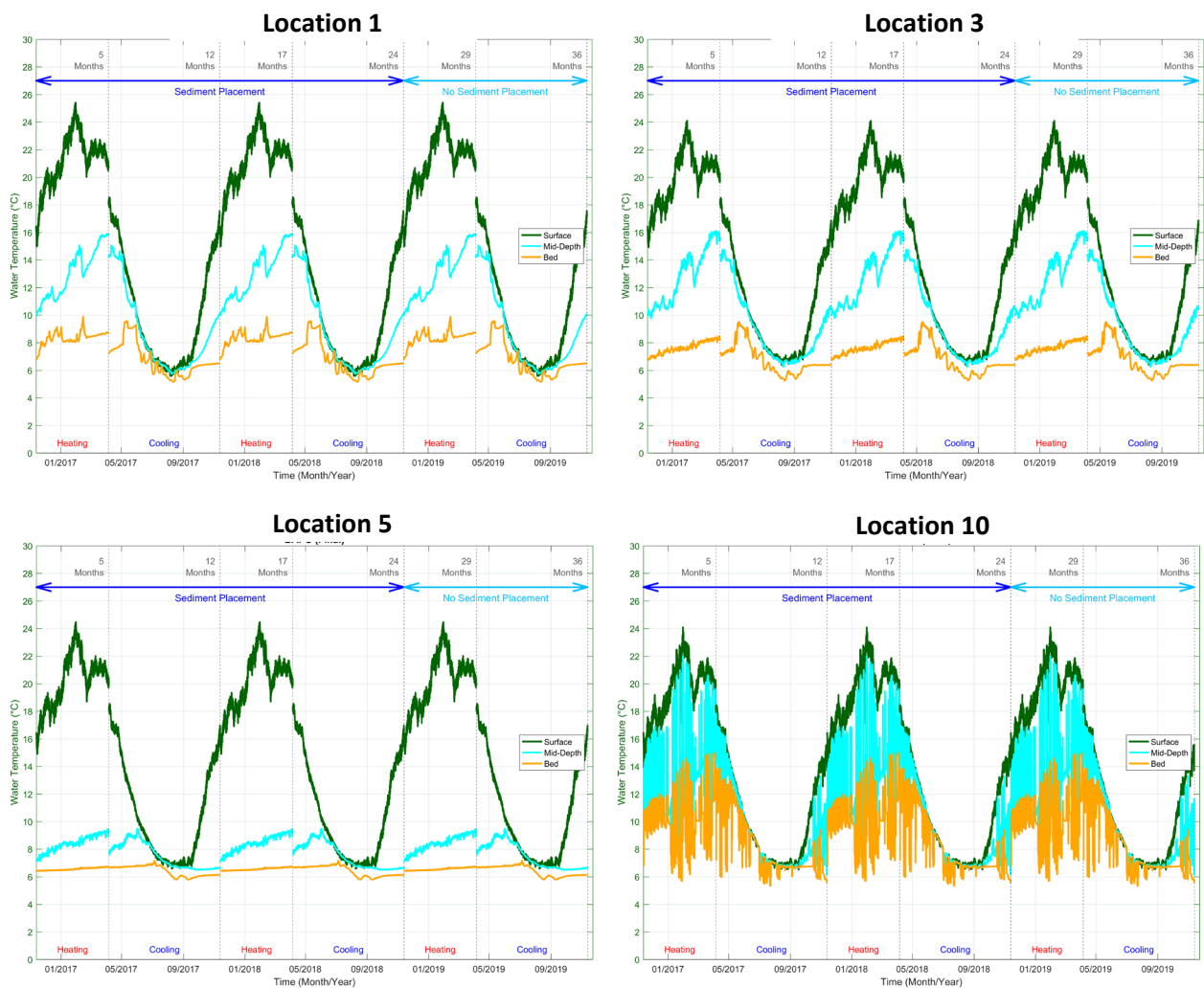


Figure 4. Temperature profiles for Talbingo Reservoir used in the hydrodynamic model and aluminium assessment at Locations 1, 3, 5 and 10 (Reservoir outlet). Larger images of profiles for all locations are shown in Appendix A.

1.2.4 Other factors

All of the rock materials were used in this assessment, although greater portions of those from the geological units designated as Ravine and Boraig may comprise the majority of the rock materials destined for placement in Talbingo Reservoir. The majority of CSIRO tests were conducted using rock material of particle size $<75\ \mu\text{m}$, and the aluminium release data from these materials were considered a suitable estimate of what may occur from the TSS-rock material, whose concentrations were predicted by the hydrodynamic model. The $<75\ \mu\text{m}$ materials comprised $28\pm3\%$ that was $<6.3\ \mu\text{m}$ (clay and fine silt), $18\pm3\%$ that was $<4\ \mu\text{m}$, and $6.3\pm2\%$ that was $<2\ \mu\text{m}$ (clay). Dissolved aluminium release was negligible for rock materials $>2\ \text{mm}$ in size.

The aluminium release appeared to be controlled by dissolution from rock materials to form the highly soluble aluminate ion, $\text{Al}(\text{OH})_4^-$. Consequently, waters with higher pH release aluminium faster and higher equilibrium concentrations are possible. In this desktop study, the water pH was not considered explicitly, and aluminium concentrations may be greater if the pH was to rise higher than that observed in the CSIRO tests due to sustained placement of fine rock materials without dilution and neutralisation, or aluminium concentrations may be lower if the pH remained lower.

2 Results

2.1 Excavated rock -dissolved aluminium relationships

There exists a high degree of variability in the dissolved aluminium concentrations across the excavated rock TSS concentrations, and the dissolved aluminium concentration range was greater for the tests conducted at 21°C than those at 6°C (Figure 5). The variability in the measured dissolved aluminium concentration at each TSS concentration is due to the combination of data sets with different rock types and test durations (Simpson et al., 2019). For neither of these variables was there sufficient data to develop individual models, beyond the test duration data sets described here. All tests were with materials of <75 µm particle size.

The lines in Figure 5 are the models calculated by curve-fitting (NCSS version 07.1.13, NCSS.COM) and are described further in Appendix B. The data enabled separate analysis and curve-fitting for experimental duration ranges of (i) 6-336 h (mid to long-term release), and (ii) ≤18 h (shorter-term release) at both 21°C and 6°C. For both of these data sets, it was possible to calculate the mean and upper confidence limit (95% Student's-t UCL, using NCSS) and run the curve-fitting with these data sets (Appendix B). A range of additional figures, including those for UCLs that were not significantly different to those for means are shown in Appendix B. The fit of the different curves was strongly influenced by the number of test data points at each TSS concentration. There was considerably greater aluminium release for TSS concentrations of 3.3 and 33 g/L. The data sets were not large enough to analyse relationships separately for individual times or rock types (i.e. there were not a sufficient number of pairs of TSS and dissolved aluminium concentrations for each variable). The curve-fitting was repeated for the 24-336-h data set (removing the overlapping 18-h data), which was eventually selected as better for predicting the mid to long-term aluminium release (Location 1) (Figure 5).

A visual comparison of the different curve fits shown in Figure 5 were an important consideration for which to use for predicting dissolved aluminium during the placement operations. There were also considerably fewer data at TSS concentrations <1 g/L, and that resulted in greater uncertainty for these lower TSS concentrations. For the final aluminium release predictions, the calculations used the predictions from two TSS-dissolved aluminium relationships: (i) the 24-336-h model (dashed purple line) and 6-336 UCL model (full red line) (comparing two models) for Location 1 (within the silt curtain) that generally had a TSS range of 200-2000 mg/L, (ii) the ≤18 h curve (solid green line) for the other locations (<100 mg/L TSS range). Considering the overall spread of the data and the uncertainty at the lower TSS concentrations, the actual dissolved aluminium concentrations may be within a factor of two of the predictions (higher or lower).

The curve-fits influence the predictions. For the mid to long-term release relationships with the 21°C data, the differences in curve-fits through the TSS data ranges of 50-500 mg/L and 1000-2000 mg/L have a particularly significant influence on the predicted dissolved aluminium concentrations. These fits are strongly influenced by data distributions, noting there was very limited data available at TSS concentration <1000 mg/L. For the shorter-term release relationships, the 24-336-h model (UCLs could not be calculated) provides a suitably conservative prediction of dissolved aluminium release.

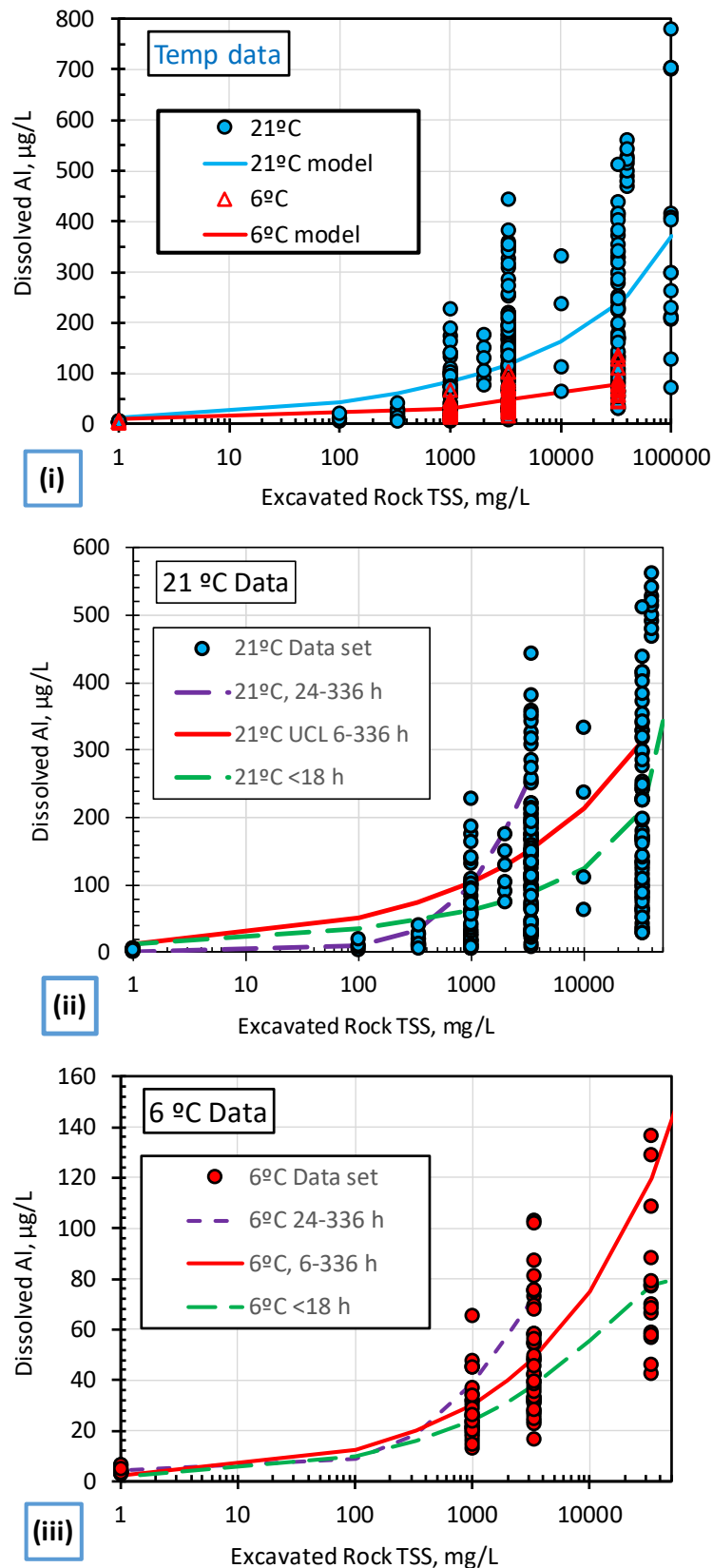


Figure 5. Relationship between excavated rock TSS concentration (mg/L) and dissolved Al (µg/L). (i) Comparison of models for the full data sets at 21°C and 6°C, respectively. For the **aluminium** release predictions the calculations used the predictions from (ii) the 24-336 h model (dashed purple line) and 6-336 UCL (full red line) for Location 1 (within the silt curtain) that generally had 200-2000 mg/L TSS range, (iii) the ≤18-h model (solid green line) for the other locations (<100 mg/L TSS range). Figures for mean and 95th percentiles (UCLs) are provided in Appendix B.

2.2 TSS (hydrodynamic model)-dissolved aluminium relationship

The TSS outputs from the hydrodynamic model are shown in Figure 6 and Appendix C. These profiles depict TSS concentration increases as a result of rock placement then decreasing when the placement ceases after 24 months. TSS concentration increases in the surface waters and mid-depth waters during the summer months owing to the warmer waters nearer the surface, and at some locations increased in deeper waters during the winter period owing to TSS settling out.

Using the predicted TSS concentrations to represent the concentrations of fine excavated rock, and models derived in Section 2.1 (excavated rock (mg/L)-dissolved Al ($\mu\text{g/L}$) relationships), dissolved aluminium concentration profiles were constructed for each location. Note here that the relationships represent the aluminium release due to rock placement and do not include any background aluminium that already existed in the reservoir waters (5-10 $\mu\text{g/L}$).

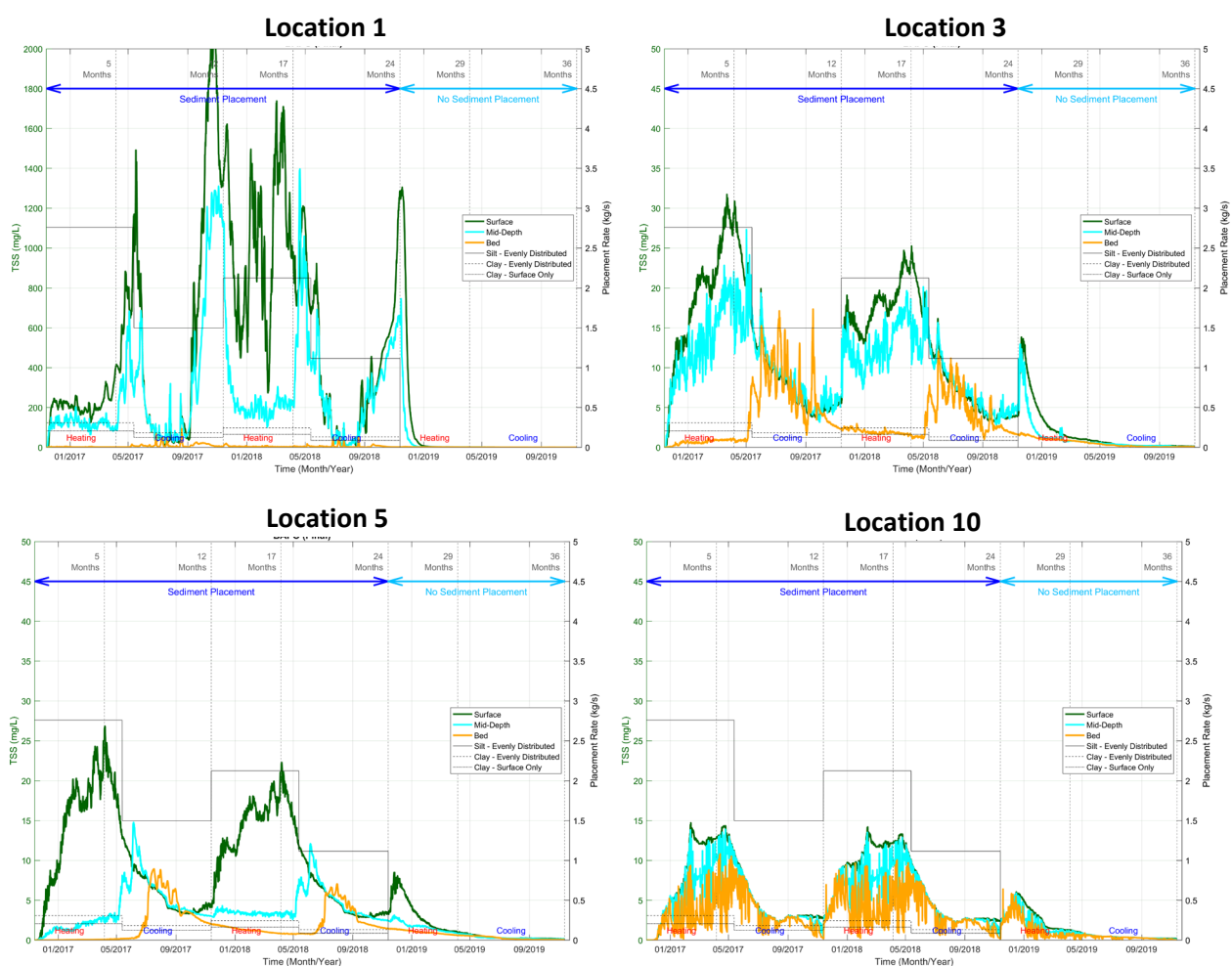


Figure 6. TSS profiles for Talbingo Reservoir used in the hydrodynamic model and aluminium assessment at Locations 1, 3, 5 and 10 (Reservoir outlet). Larger images of profiles for all locations are shown in Appendix C.

2.3.1 Predicted dissolved aluminium concentrations in Talbingo Reservoir

2.2.1 Predicted dissolved aluminium in the placement area (Location 1)

In Figure 7, the predicted dissolved aluminium concentrations are shown during (24 months) and following (12 months) for the rock placement period for Location 1. For this location, predictions based on two relationships for mid-long-term release were compared:

(i) 24-336-h relationship (dashed purple line), and (ii) 6-336-h UCL relationship (full red line) in Figure 5(ii). In addition, two scenarios are described:

- (A) Aluminium release is predicted using the two relationships for mid to long-term release, representing a simple equilibrium-partitioning between TSS and dissolved aluminium.
- (B) Ongoing additions of excavated rock result in higher dissolved aluminium due to release occurring into waters that already contain dissolved aluminium that has not yet been transported beyond the silt curtain (Location 1). For this scenario, 91%/day of the aluminium release accumulates in the waters within the silt curtain, and 9%/day of the dissolved aluminium is exported to Location 2, and additional release occurs from newly added rock materials (predicted using the two relationships for mid to long-term release).

A range of other scenarios were tested, and several of those are illustrated in Appendix D. Each has different assumptions and uncertainties. The greatest uncertainty relates to water pH. If the pH was to rise to and be maintained at pH 9.5-10.5 within Location 1, the rate of aluminium release may be significantly greater (note, recommendations had been made to undertake such tests to fill this data/knowledge gap). Under such a scenario, the peak dissolved aluminium concentrations may be in the 300-420 µg/L range at Location 1 (Figure D2), and 40-90 µg/L range at Location 2 (Figure D3). Alternatively, if water inputs and dispersion results in the pH <9 (e.g. pH 8-9), then the aluminium release may be lower.

Based on the available data and for both relationships (i) and (ii), Scenario B represents the higher range of the aluminium release predictions for Location 1. Both Scenarios A and B, using both relationships, predict dissolved aluminium in the surface and middle depth waters to exceed the DGV of 55 µg/L during periods of higher water temperatures (close to summer months).

Relationship (i) predicts steeper increases in dissolved aluminium concentrations and higher peak concentrations, compared to relationship (ii) that indicated higher average aluminium concentrations but lower peak concentrations.

Both relationships and scenarios predict that dissolved aluminium concentrations in the deeper waters should generally remain close to background concentrations (<10 µg/L), however, here we note that the hydrodynamic model predicts very low TSS concentrations in the bottom waters (Figure 6), which seem counterintuitive if the rock placement materials are depositing. Within the placement area, the formation of a dense layer of fine rock materials might be expected that is being disturbed and resuspended throughout the duration of the rock placement activities.

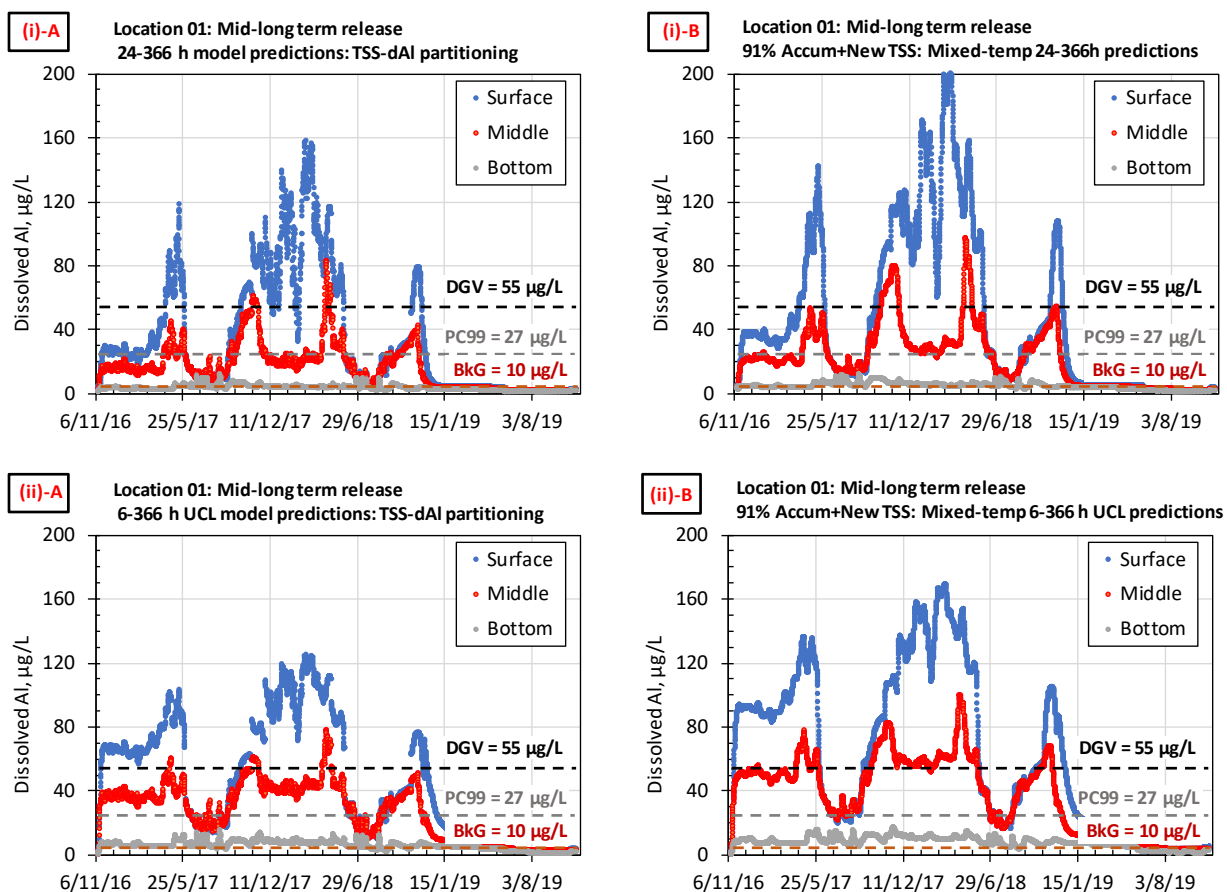


Figure 7. Predicted dissolved aluminium concentrations ($\mu\text{g/L}$) at Location 1 (J-Placement) during the rock placement period (24 months of placement and 12 months following placement): Mid to long-term release relationship (i) (24-336-h data) was used for the top figures and relationship (ii) (6-336 UCL data) for the bottom figure. Figures (iii) and (iv) Mixed-temperature model $t=6-336$ UCL data. Scenarios A (left figures) Aluminium release is predicted using the 'basic relationship', representing a simple equilibrium-partitioning between TSS and dissolved aluminium. Scenario B Ongoing additions of excavated rock result in higher dissolved aluminium due to release occurring into waters that already contain dissolved aluminium that has not yet been transported beyond the silt curtain.

2.2.2 Predicted dissolved aluminium concentrations at locations beyond the placement area (Locations 2, 3, 4, 5, 6 and 10)

For predictions of dissolved aluminium concentrations at locations beyond the placement area, the following two scenarios examined are:

- (A) Aluminium release occurs from rock materials that are present as TSS (predicted using model for short-term release (≤ 18 -h relationship, as most particles will move beyond this location within 18 h), and dilution occurs according to estimates from the hydrodynamic model (e.g. 15%/day dissolved aluminium is exported from Location 2 to Location 3).
- (B) A portion of aluminium released from the previous location is transported to the new location (e.g. 9%/day of dissolved aluminium is exported from Location 1 to Location 2), and this dissolved aluminium is added to that predicted based on release from TSS and ongoing dilutions.

This approach to predicting dissolved aluminium was followed for Locations 2, 3 and 4 (Figure 8), and then Locations 5, 6 and then Location 10 (near reservoir outlet) (Figure 9). These predictions

indicate that dissolved aluminium concentrations should not exceed the DGV at or beyond Location 2. Between Locations 1 and 2, there is expected to be a gradient in dissolved aluminium concentrations, and the DGV may be exceeded within this gradient (mixing zone). The predictions indicated that the dissolved aluminium released in the placement area and from particles transported through the reservoir should not contribute more than the existing background dissolved aluminium concentrations beyond Location 5.

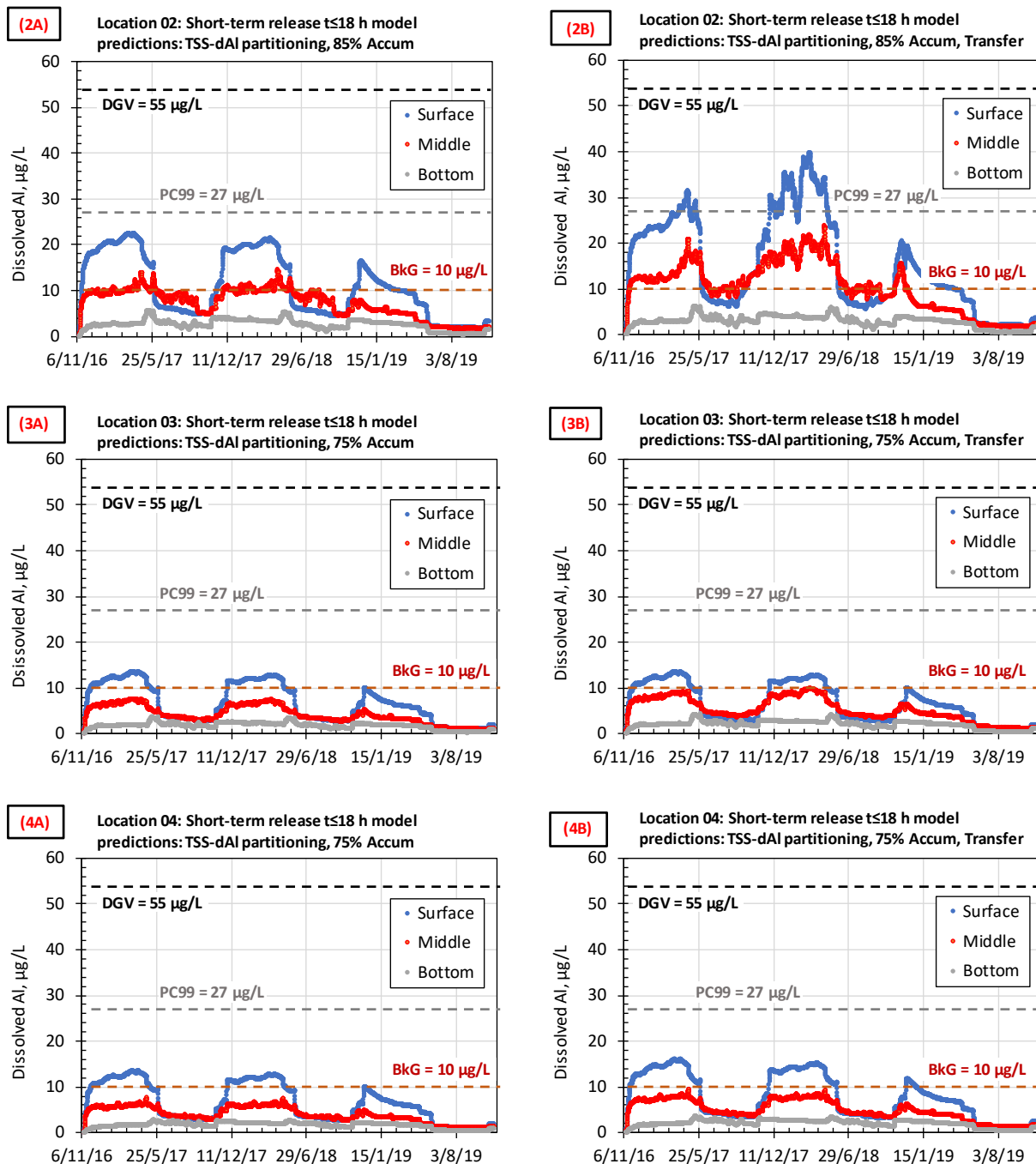


Figure 8. Predicted dissolved aluminium concentrations (µg/L) during the rock placement period (24 months of placement and 12 months following placement): Locations 2, 3 and 4. Mixed-temperature model $t \leq 18$ -h data. Scenarios A and B described in text using short term release relationships (≤ 18 -h model), and dilution occurs according to estimates from the hydrodynamic model (e.g. 15%/day of aluminium is exported from Location 2 to 3).

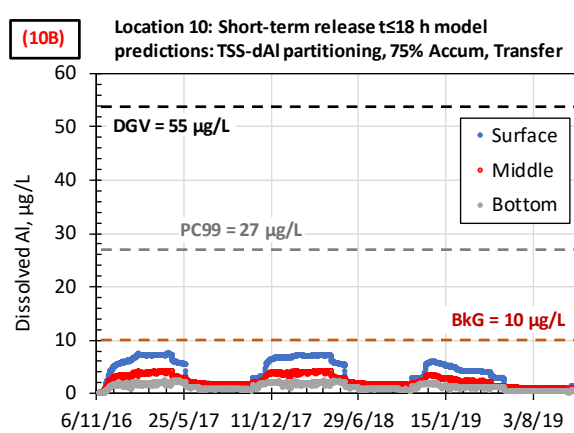
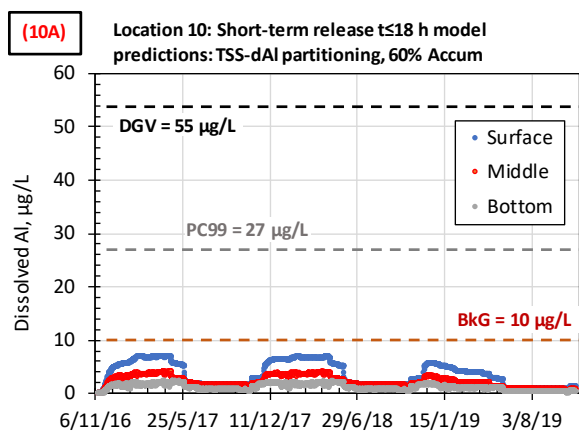
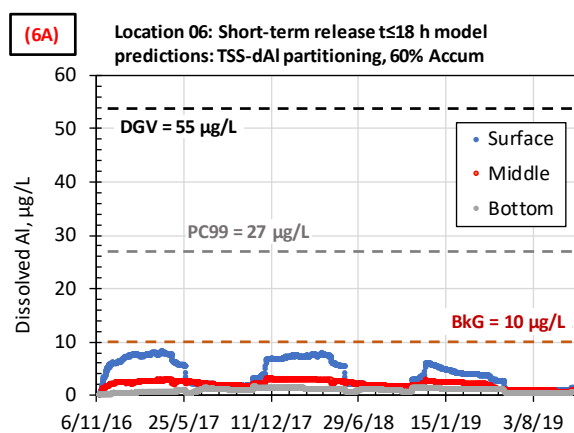
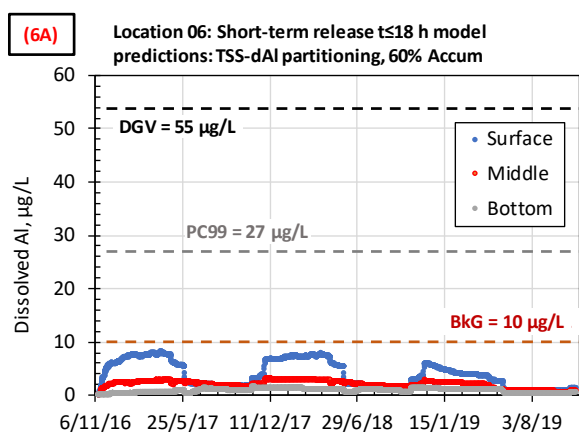
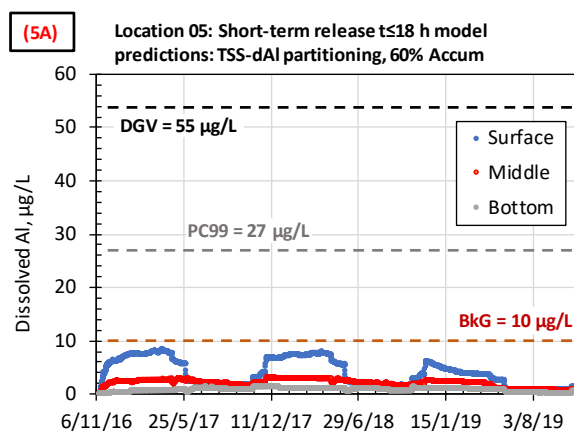
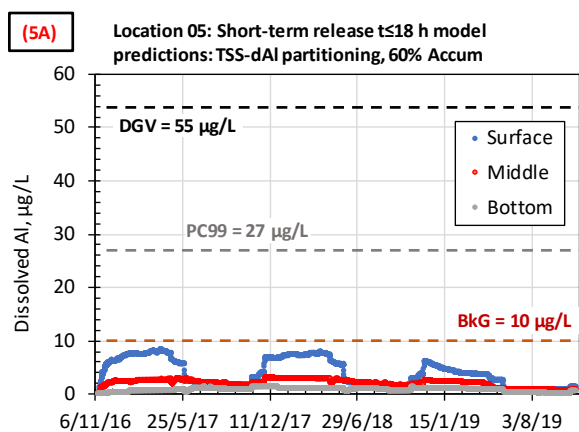


Figure 9. Predicted dissolved aluminium concentrations ($\mu\text{g/L}$) during the rock placement period (24 months of placement and 12 months following placement): Locations 5, 6, and 10 (Reservoir outlet). A and B described in Figure 8.

3 Dissolved aluminium summary

The assessment indicates that dissolved aluminium concentrations are likely to exceed the default GV (DGV) of 55 µg/L within the placement area contained by the silt curtain (Location 1). Outside the silt curtain, a gradient (mixing zone) is expected to develop, along which dissolved aluminium released in Location 1 will be diluted and further aluminium release from particles will occur. From Location 1 to Location 2, 500 m away, dissolved aluminium concentrations may also exceed the DGV. Beyond Location 2 the dissolved aluminium concentrations are predicted to remain below the DGV.

Significant uncertainty exists with the predictions on both the high side (higher dissolved aluminium) and low side (lower dissolved aluminium). CSIRO Assignment P4 (Simpson et al., 2019) described a number of data/knowledge gaps that influence this uncertainty. Higher TSS concentrations and higher water pH are considered the primary drivers for higher dissolved aluminium concentrations. Lower water temperatures will result in lower dissolved aluminium concentrations.

The great source of uncertainty for aluminium release relates to water pH. If the pH was to rise to and be maintained at pH 9.5-10.5 within Location 1, the rate of aluminium release may be significantly greater and peak dissolved aluminium concentrations of 300-420 µg/L may be reached at Location 1, and 40-90 µg/L at Location 2. Alternatively, if water inputs and dispersion results in the pH <9 (e.g. pH 8-9), then the aluminium releases may be lower than those predicted here. Greater rates of water dilution will also lower dissolved aluminium concentrations in Location 1, and the export of the aluminium to locations further down the reservoir may not substantially increase the predicted concentrations at those locations. While difficult to estimate, the predictions may have 50% uncertainty on both the high or low sides for Location 1 and 2.

The hydrodynamic model predicted low TSS in the bottom waters, and while this seems counterintuitive (gravity), the presence in the cooler bottom waters may not have a large influence on the predictions.

At Locations 3 to 10, attenuation reactions that result in lower water pH may result in substantially lower aluminium release from TSS at locations further from the placement area. The dilutions may also be greater than those estimated for these predictions, resulting in lower dissolved aluminium concentrations. For the locations beyond the silt curtain, the predictions will have even greater uncertainty, but dissolved aluminium concentrations seem likely to be within a factor of 2-3 of the background concentrations.

4 References

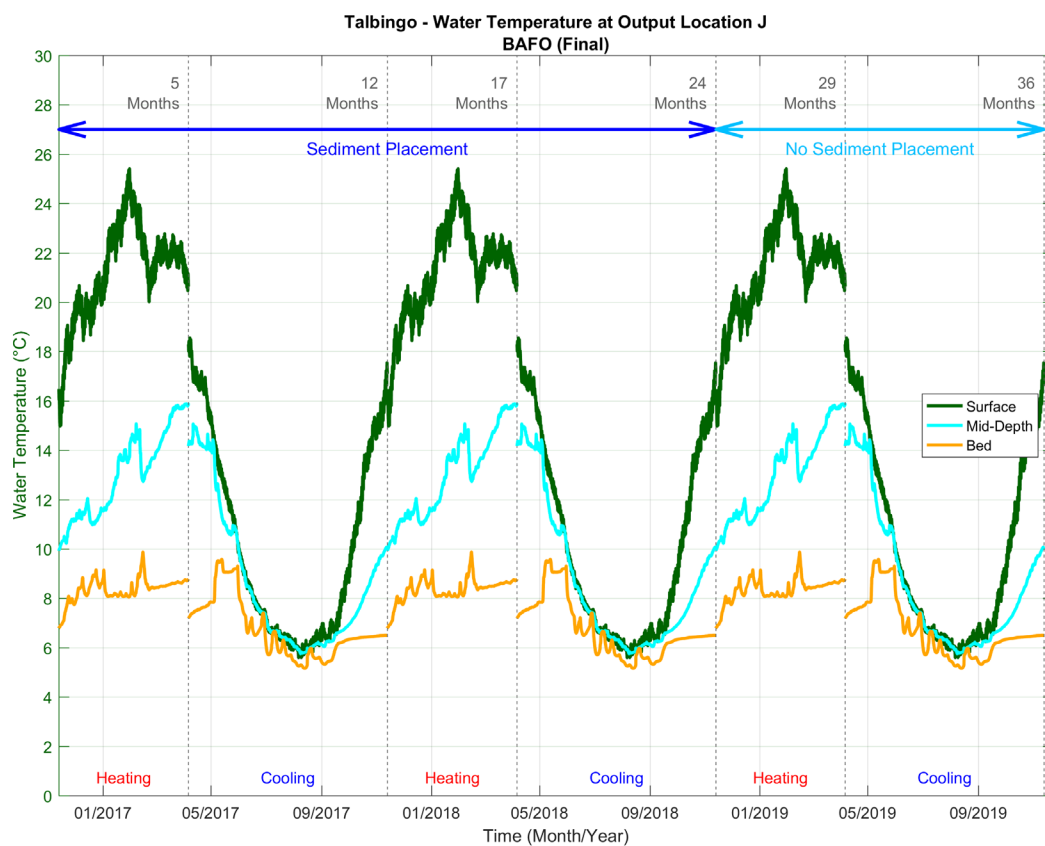
Simpson SL, Angel BM, Mudaliar P, King JJ, and Jarolimek CV (2019). Snowy 2.0 P4: Environmental Categorisation of Excavated Rock Interactions with and Potential Impacts on Reservoir Waters and Sediments. CSIRO Land and Water Report EP19176, Lucas Heights, NSW, Australia.

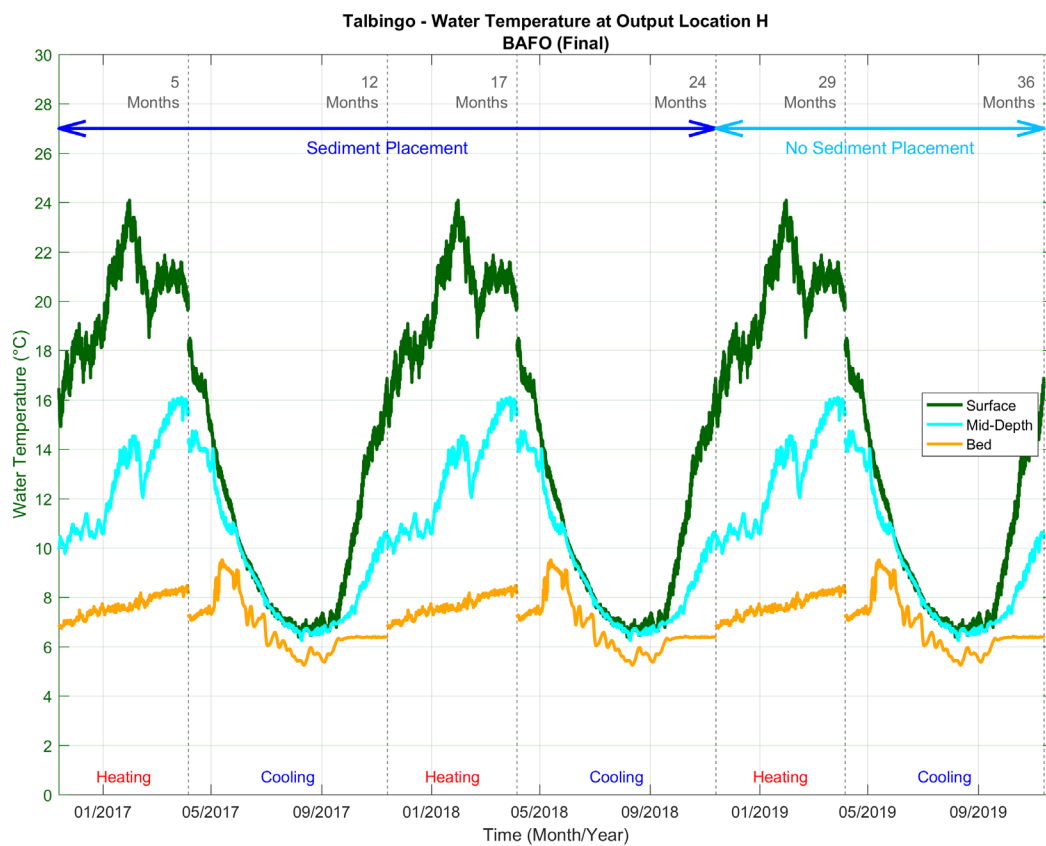
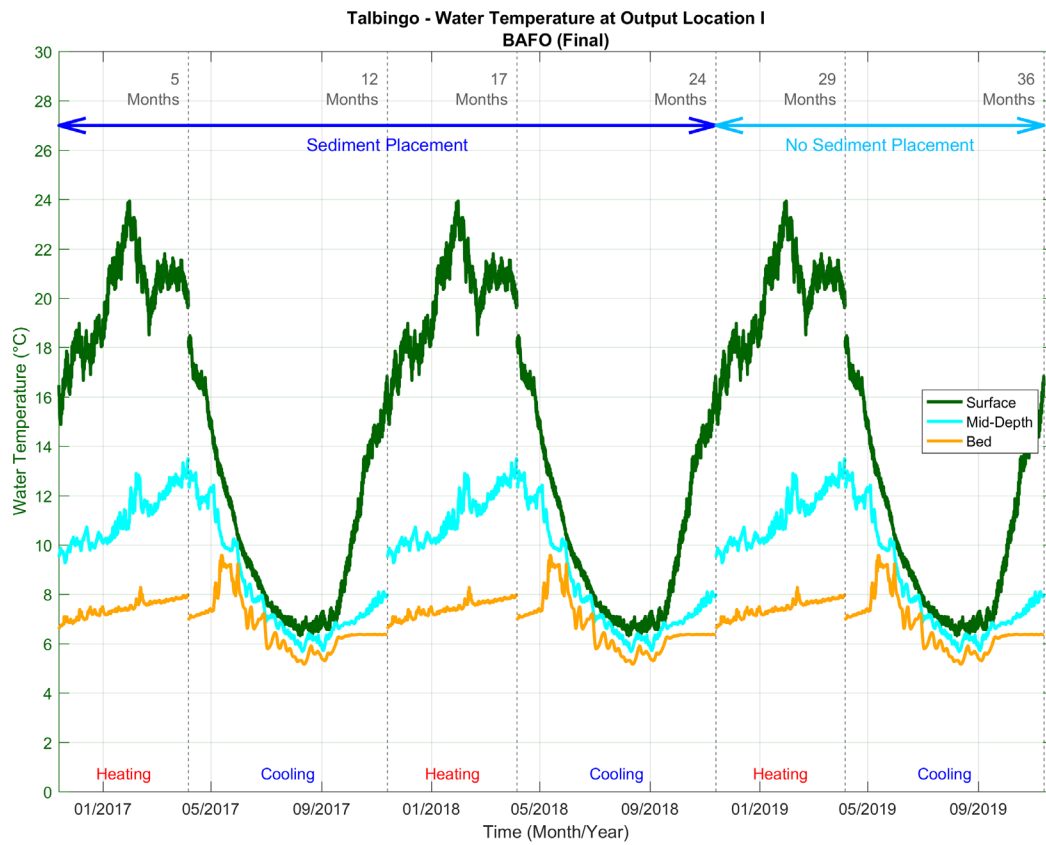
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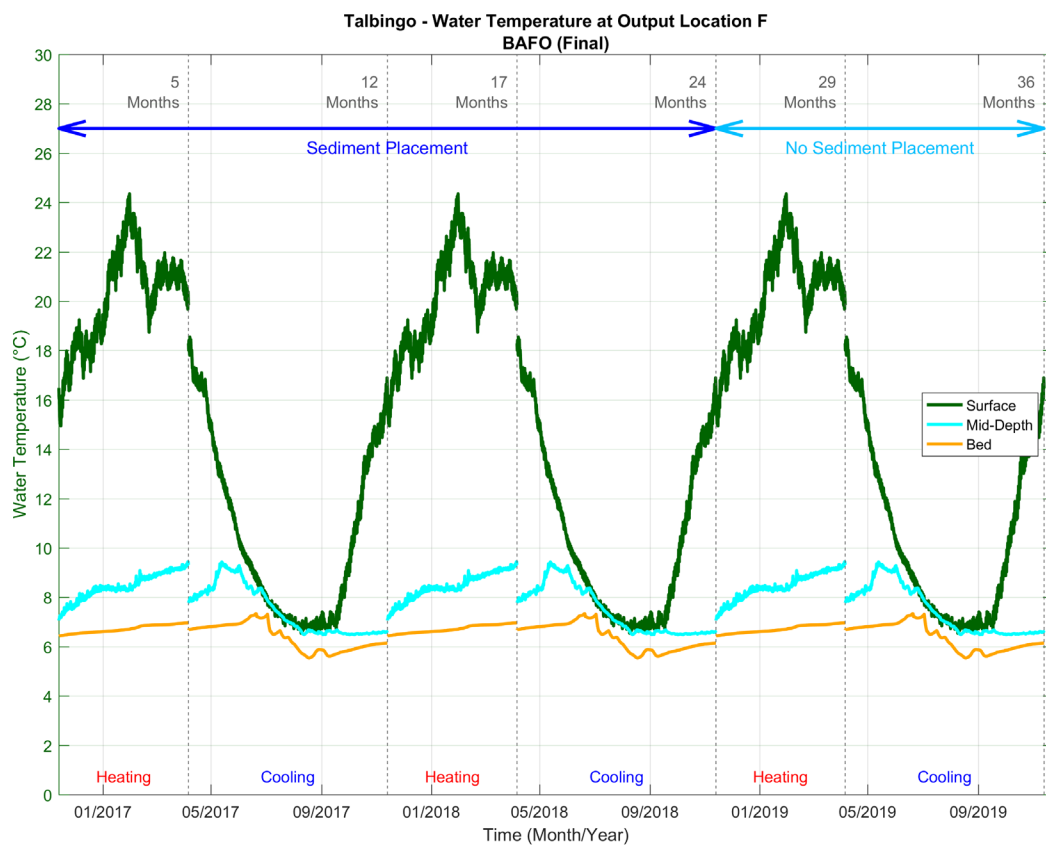
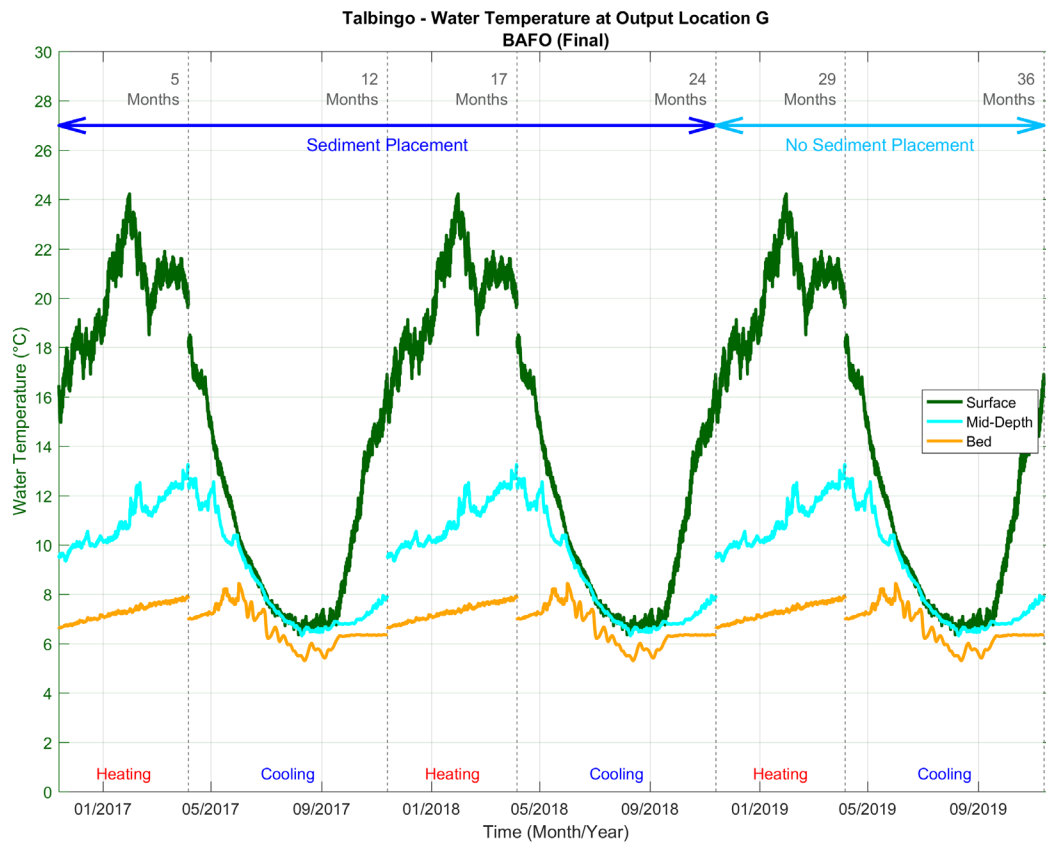
ANZG (2018). Australian and New Zealand Guidelines for Fresh and Marine Water Quality. Australian and New Zealand Governments and Australian state and territory governments, Canberra ACT, Australia. Available at www.waterquality.gov.au/anz-guidelines.

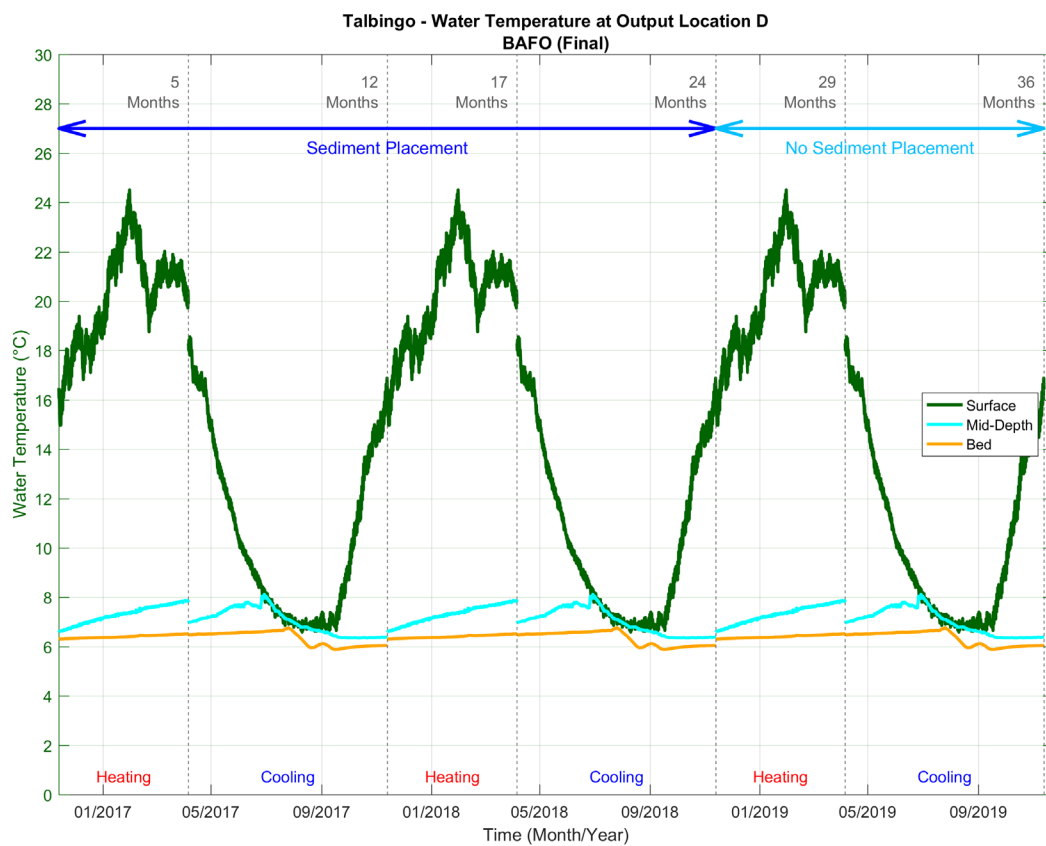
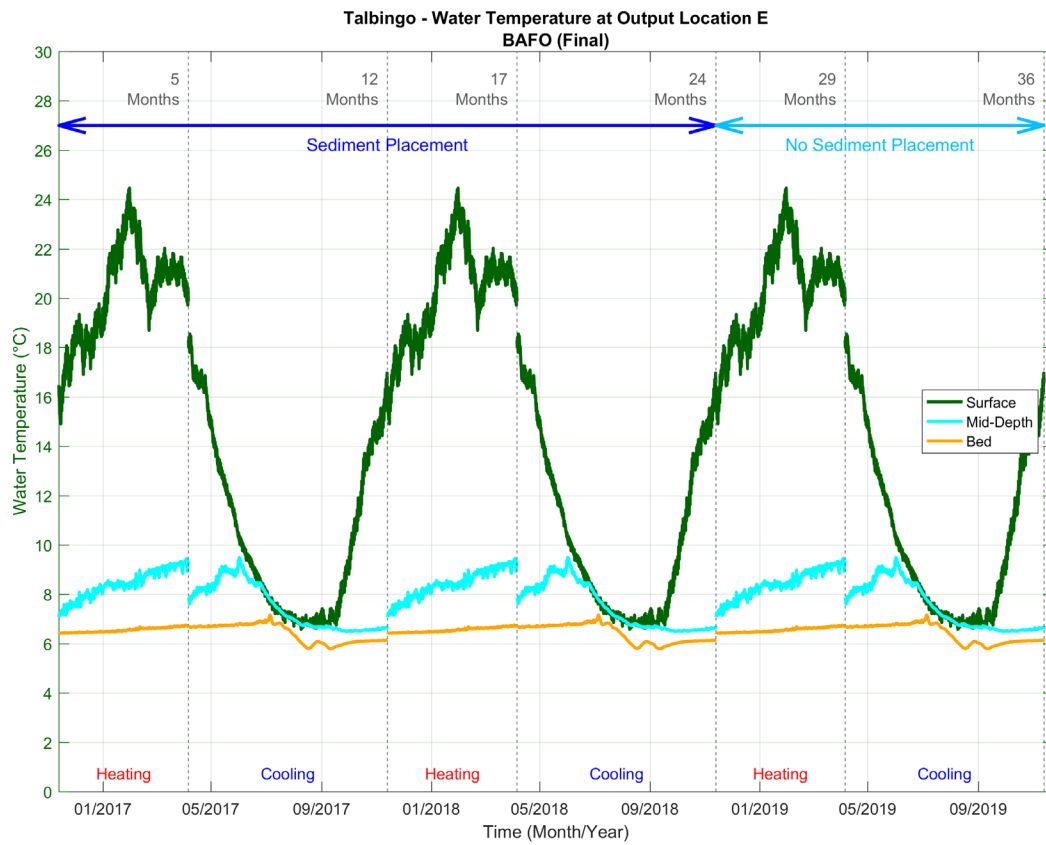
Appendix A Water temperature profiles for Talbingo Reservoir used in the hydrodynamic model and aluminium assessment

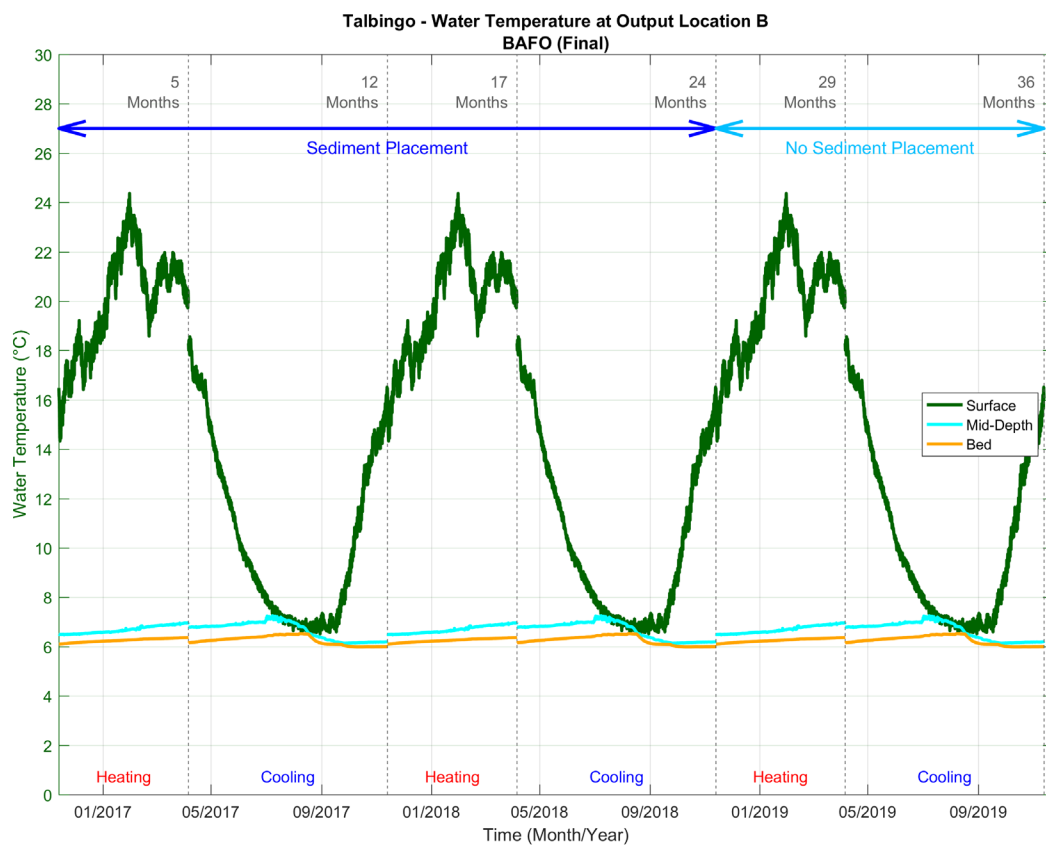
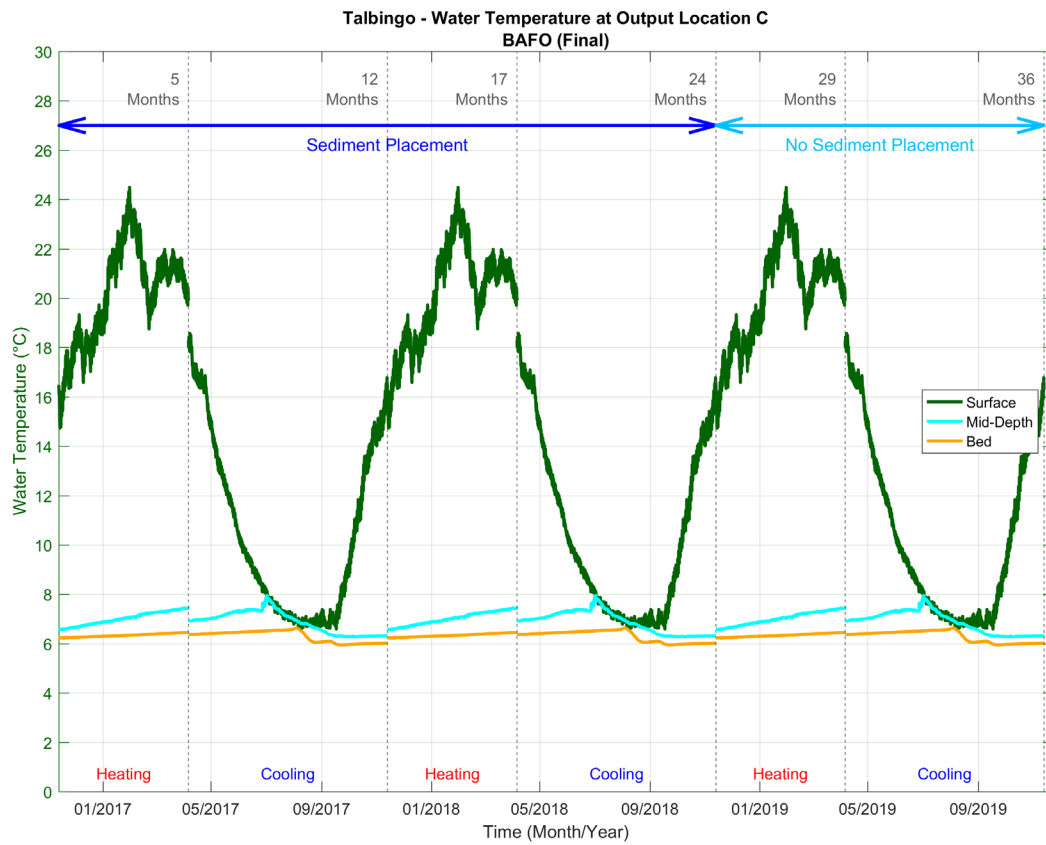
Note in the figures shown here the location names are in alphabetical order (J to A), being Location J = 1 (Placement area) to Location A = 10 (Reservoir outlet)

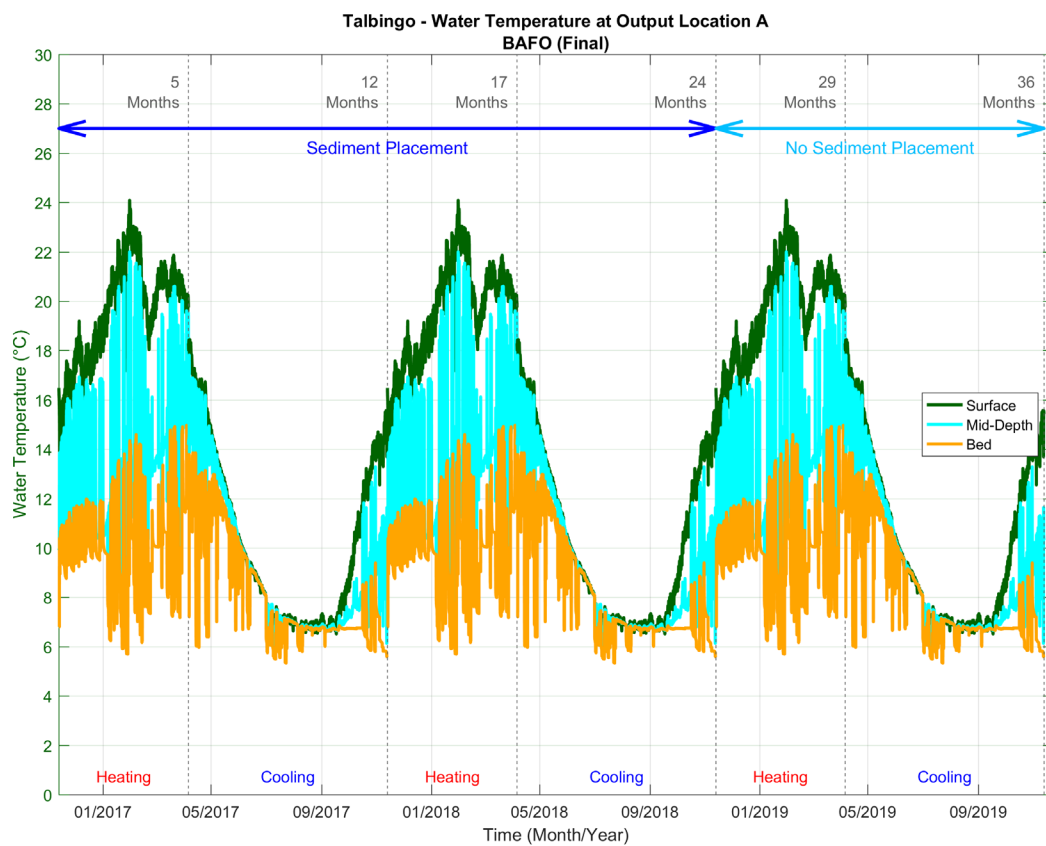












Appendix B Relationship between released dissolved aluminium and total suspended sediments

Relationships between released dissolved aluminium and TSS were calculated using curve-fitting (NCSS version 07.1.13, NCSS.COM), with the more suitable being either exponential Type-1 [$\text{Dissolved-Al}(\mu\text{g/L}) = A * (\text{TSS}(\text{mg/L})^B) * \text{EXP}(-C * (\text{TSS}(\text{mg/L})))$] or PolyRatio(1,1) [$\text{Dissolved-Al}(\mu\text{g/L}) = (A + B * (\text{TSS}(\text{mg/L}))) / (1 + C * (\text{TSS}(\text{mg/L})))$].

There exists a high degree of variability in the dissolved aluminium concentrations across the excavated rock TSS concentrations, and the dissolved aluminium concentration range was greater for the tests conducted at 21 °C than those at 6 °C (Figure B1).

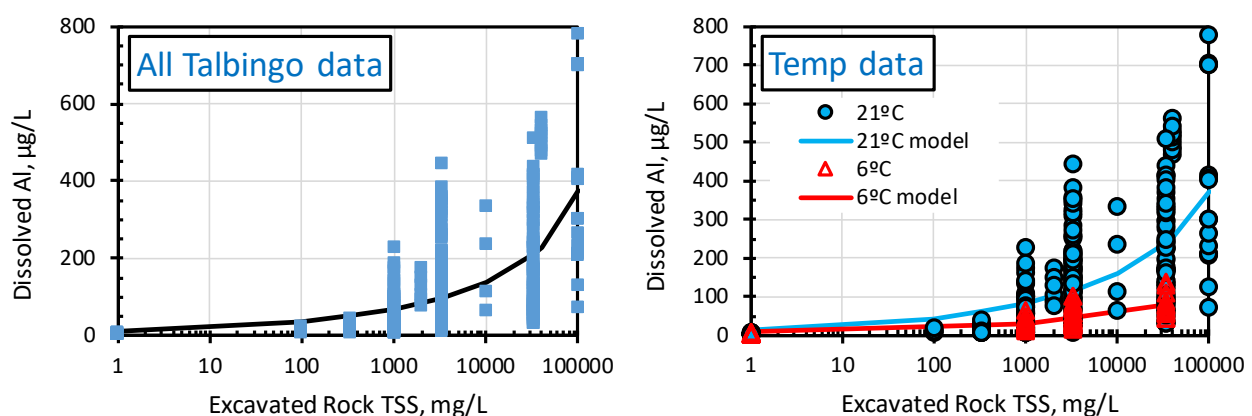


Figure B1. Relationship between excavated rock TSS concentration (mg/L) and dissolved Al (µg/L):
(i) All data for Talbingo Reservoir, and (ii) data separated into tests at 21°C and 6°C respectively. The lines shown here are from curve-fitting through the entire data set, being a little lower than the mean and UCL shown in next figures.

The data enabled separate analysis and release prediction for experiments with durations (i) ranging from 6 to 336 h (mid to long-term release), and (ii) ≤18 h (shorter-term release) at both 21°C and 6°C (Figure B2). For both data sets, it was possible to calculate the mean and upper confidence limit (95% Student's-t UCL, using NCSS) and run the curve-fitting with these data sets (Figure B2).

The fit of the different curves was strongly influenced by the number of test data points at each TSS concentration. There were considerably greater aluminium release data for TSS concentrations of 3.3 and 33 mg/L. The data sets were not large enough to analyse relationships separately for individual times or rock types (i.e. there was not a sufficient number of pairs of TSS and dissolved aluminium for each variable). The 6-336-h time range provided the larger data set and the relatively similar mean and UCL for dissolved aluminium shown in Figure B2). While a considerable number of data points have dissolved aluminium concentrations above the mean and

UCL lines, it is expected that the mean should provide a reasonable estimate of dissolved aluminium release over the long duration of the rock placement, noting that comparison against GV's is recommended to involve using the 95th percentile of the test distribution. Similar points can be made about the relationships derived from the ≤ 18 -h data, with a note that this was a smaller data set. The curve-fitting was repeated for the 24- to 336-h data set (removing the overlapping 18-h data), which was eventually selected as better for predicting the mid to long-term aluminium release (Location 1).

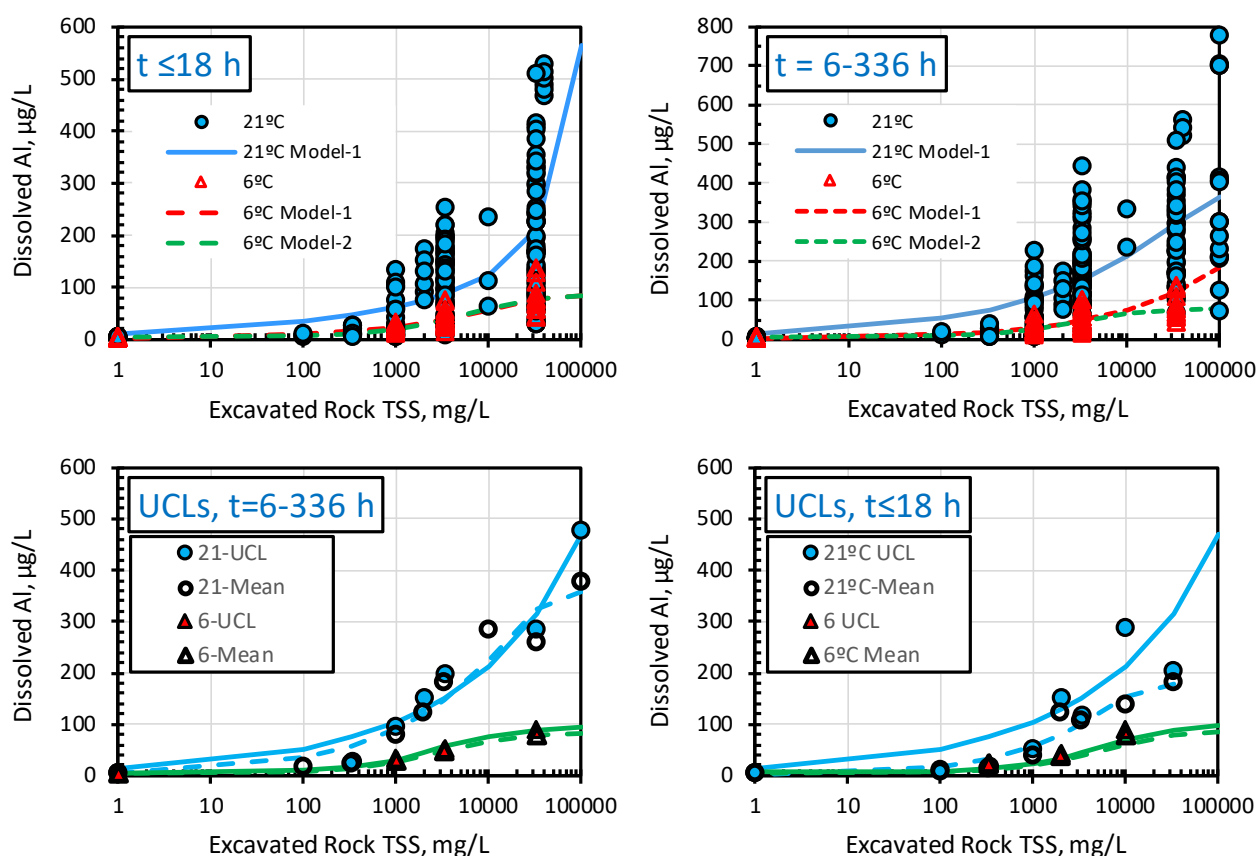


Figure B2. Relationship between excavated rock TSS concentration (mg/L) and dissolved Al (µg/L):

(i) Data for Talbingo Reservoir separated as (i) 6 to 336 h (mid to long-term release), and (ii) ≤ 18 h, showing all data in top two figures and mean (curve fits = dashed lines) and UCLs (solid lines).

Data set purpose: mid to long-term release in main ER disposal area

| 21°C Talbingo t=6-336 h | | | | | 6°C Talbingo t=6-336 h | | | | | |
|-------------------------|---------------------------|-----|------|---------|------------------------|---------------------------|---------|------|------|---------|
| | Model-1 | UCL | Mean | SE-Mean | | Model-1 | Model-2 | UCL | Mean | SE-Mean |
| ER TSS, mg/L | Dissolved aluminium, µg/L | | | | ER TSS, mg/L | Dissolved aluminium, µg/L | | | | |
| 100000 | 364 | 477 | 378 | 57 | 100000 | 184 | 80 | | | |
| 33300 | 294 | 285 | 259 | 16 | 33300 | 120 | 77 | 90.4 | 78 | 7.2 |
| 10000 | 213 | | 285 | | 10000 | 75 | 66 | | | |
| 3330 | 154 | 198 | 181 | 10 | 3330 | 49 | 48 | 52.9 | 47 | 3.4 |
| 2000 | 132 | 153 | 122 | 16 | 2000 | 40 | 39 | | | |
| 1000 | 107 | 96 | 79 | 10 | 1000 | 30 | 27 | 33.5 | 29 | 2.5 |
| 333 | 77 | 29 | 22 | 3.6 | 333 | 20 | 14 | | | |
| 100 | 53 | | 16 | | 100 | 12 | 8 | | | |
| 1 | 13 | 4.6 | 4.2 | 0.2 | 1 | 2 | 5 | 4.6 | 4.2 | 0.2 |

Data set purpose: 24-336 h mid to long-term release in main ER disposal area

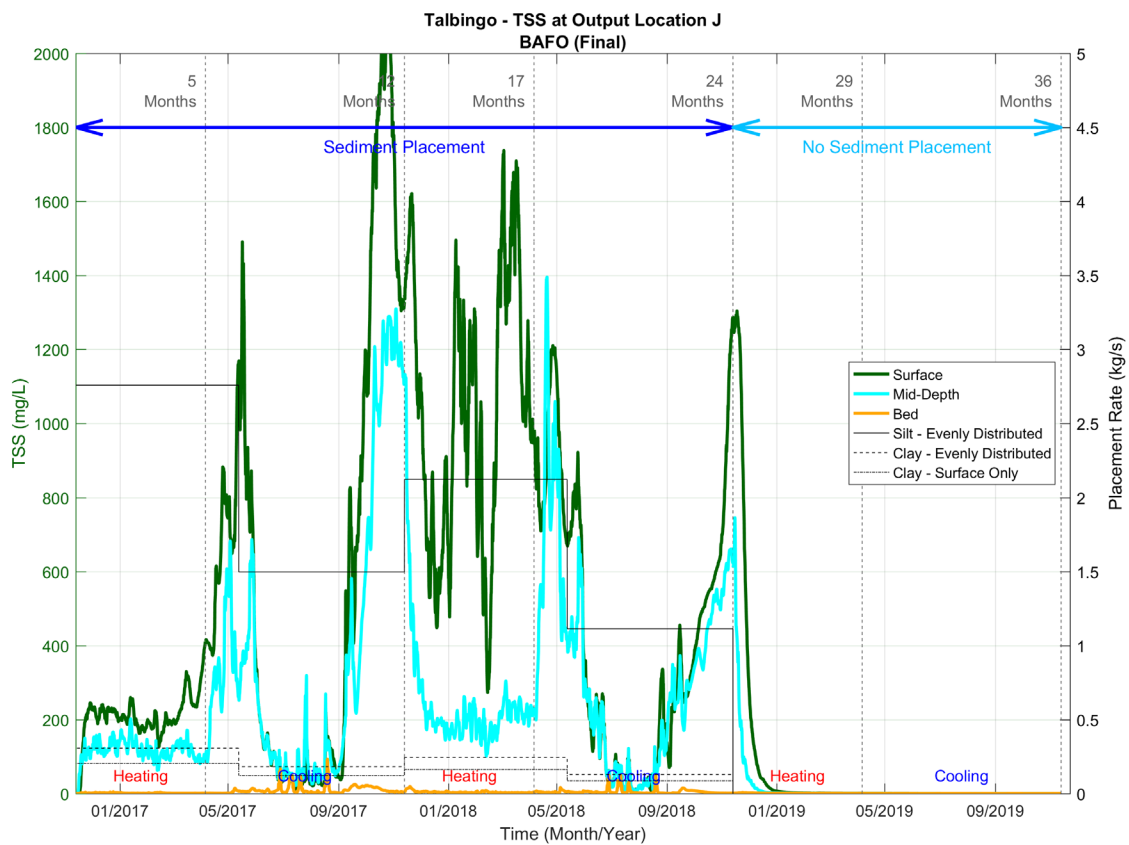
| 21°C Talbingo t=24-336 h | | | | | 6°C Talbingo t=24-336 h | | | | | |
|--------------------------|---------------------------|---------|--|--|-------------------------|---------------------------|-----------|--|--|--|
| | Model-1 | Model 2 | | | | Model-1 | Model-2 | | | |
| ER TSS, mg/L | Dissolved aluminium, µg/L | | | | ER TSS, mg/L | Dissolved aluminium, µg/L | | | | |
| 100000 | | 870 | | | 100000 | | | | | |
| 33300 | | 748 | | | 33300 | | | | | |
| 10000 | | 502 | | | 10000 | | | | | |
| 3330 | 260 | 260 | | | 3330 | | 73 | | | |
| 2000 | 181 | 176 | | | 2000 | | 58 | | | |
| 1000 | 99 | 99 | | | 1000 | | 39 | | | |
| 333 | 34 | 38 | | | 333 | | 19 | | | |
| 100 | 10 | 14 | | | 100 | | 9 | | | |
| 1 | 0 | 4 | | | 1 | | 4 | | | |

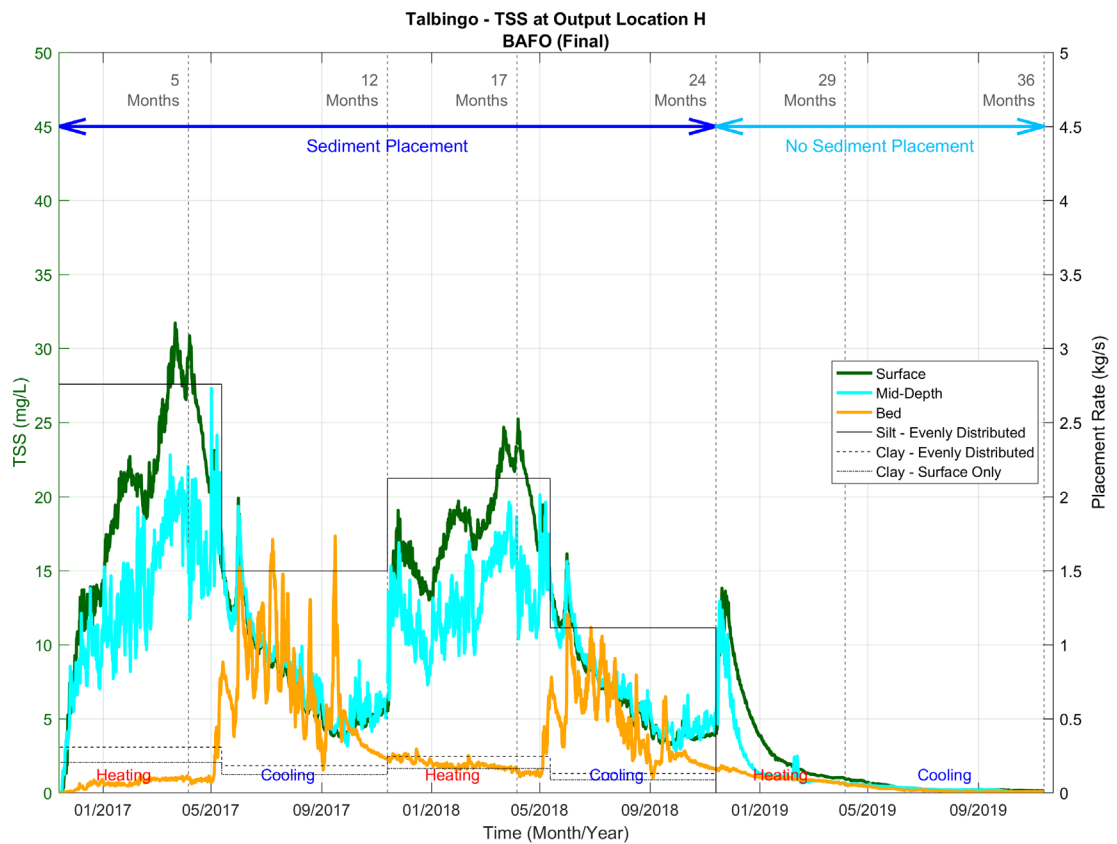
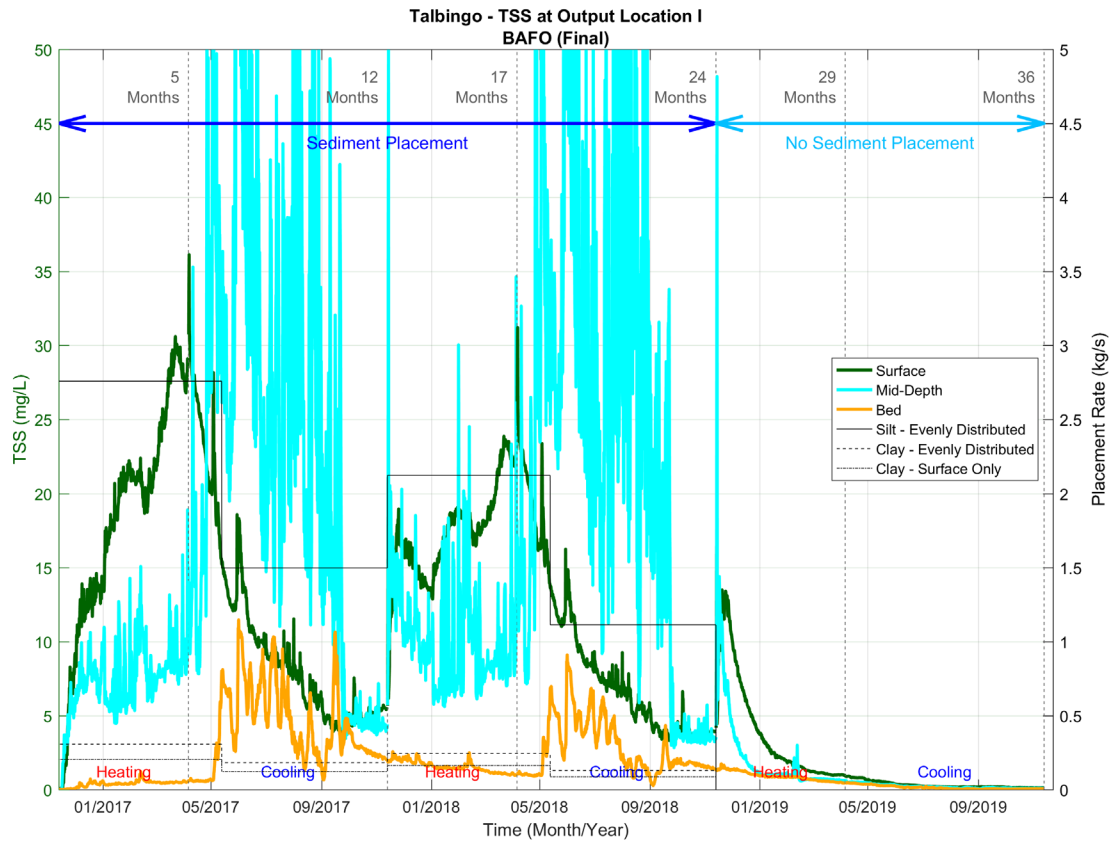
Data set purpose: ≤18 h short-term, reoccurring release, and representing release further from ER disposal area

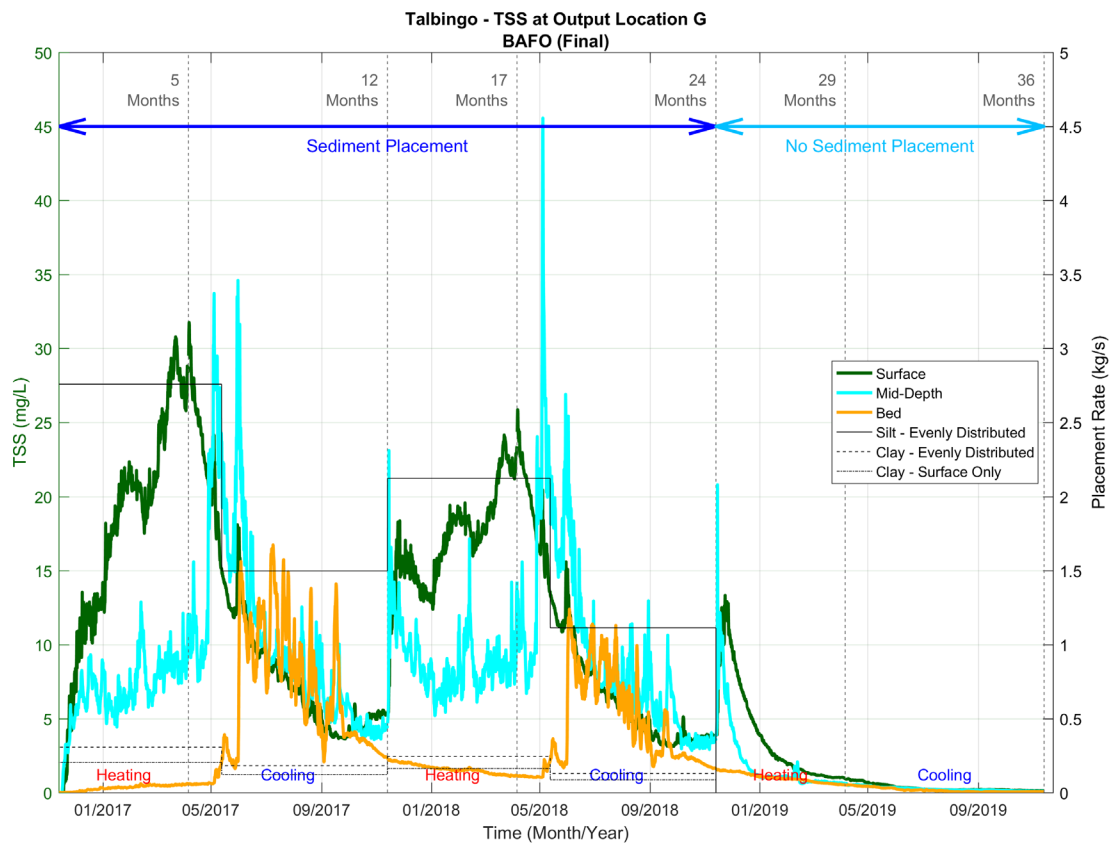
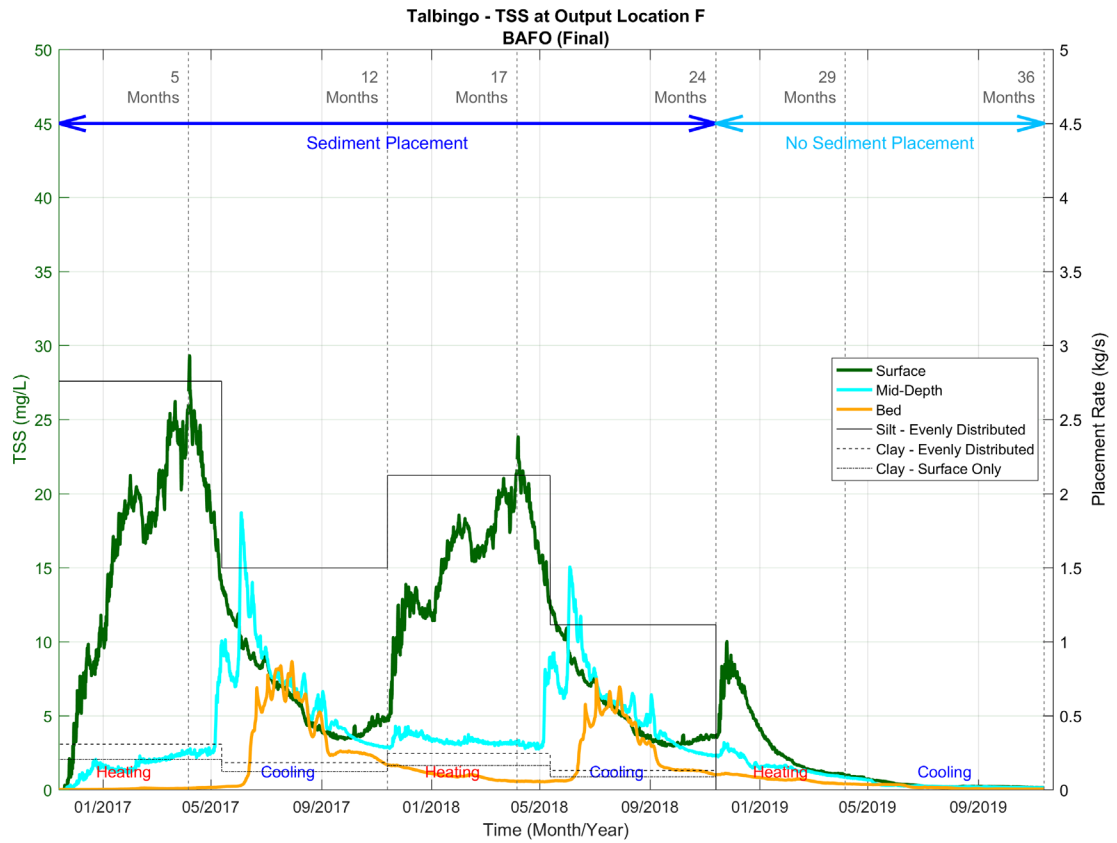
| 21°C Talbingo t ≤18 h | | | | | 6°C Talbingo t ≤18 h | | | | | |
|-----------------------|---------------------------|-----|------|---------|----------------------|---------------------------|---------|-----|------|---------|
| | Model-1 | UCL | Mean | SE-Mean | | Model-1 | Model-2 | UCL | Mean | SE-Mean |
| ER TSS, mg/L | Dissolved aluminium, µg/L | | | | ER TSS, mg/L | Dissolved aluminium, µg/L | | | | |
| 100000 | 564 | | | | 100000 | 83 | 84 | | | |
| 33300 | 212 | 205 | 181 | 14 | 33300 | 78 | 77 | 90 | 78 | 7.2 |
| 10000 | 124 | 150 | 137 | 52 | 10000 | 55 | 61 | | | |
| 3330 | 88 | 118 | 106 | 7.2 | 3330 | 38 | 39 | 43 | 38 | 2.6 |
| 2000 | 77 | 85 | 122 | 16 | 2000 | 31 | 29 | | | |
| 1000 | 64 | 51 | 39 | 7.4 | 1000 | 24 | 19 | 25 | 22 | 1.5 |
| 333 | 48 | 18 | 15 | 1.8 | 333 | 16 | 10 | | | |
| 100 | 36 | 13 | 9 | 1.5 | 100 | 10 | 7 | | | |
| 1 | 12 | 4.6 | 4.2 | 0.2 | 1 | 2 | 5 | 4.6 | 4.2 | 0.2 |

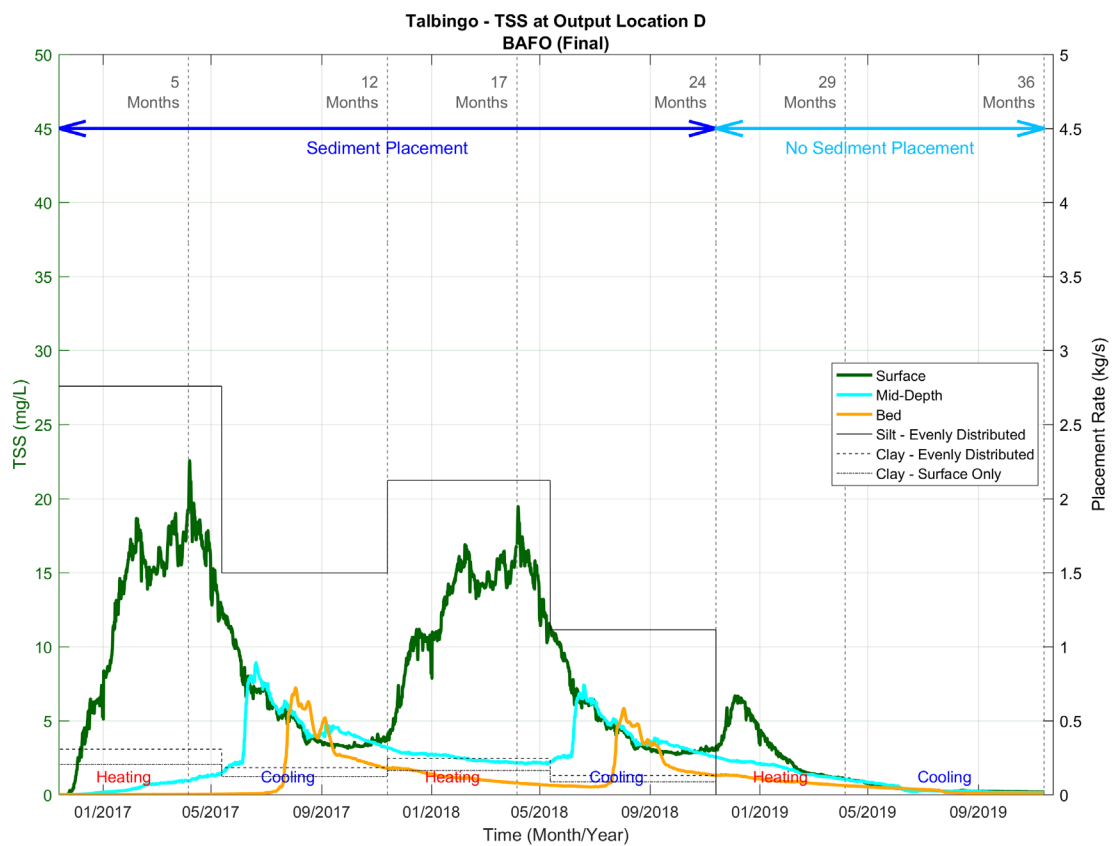
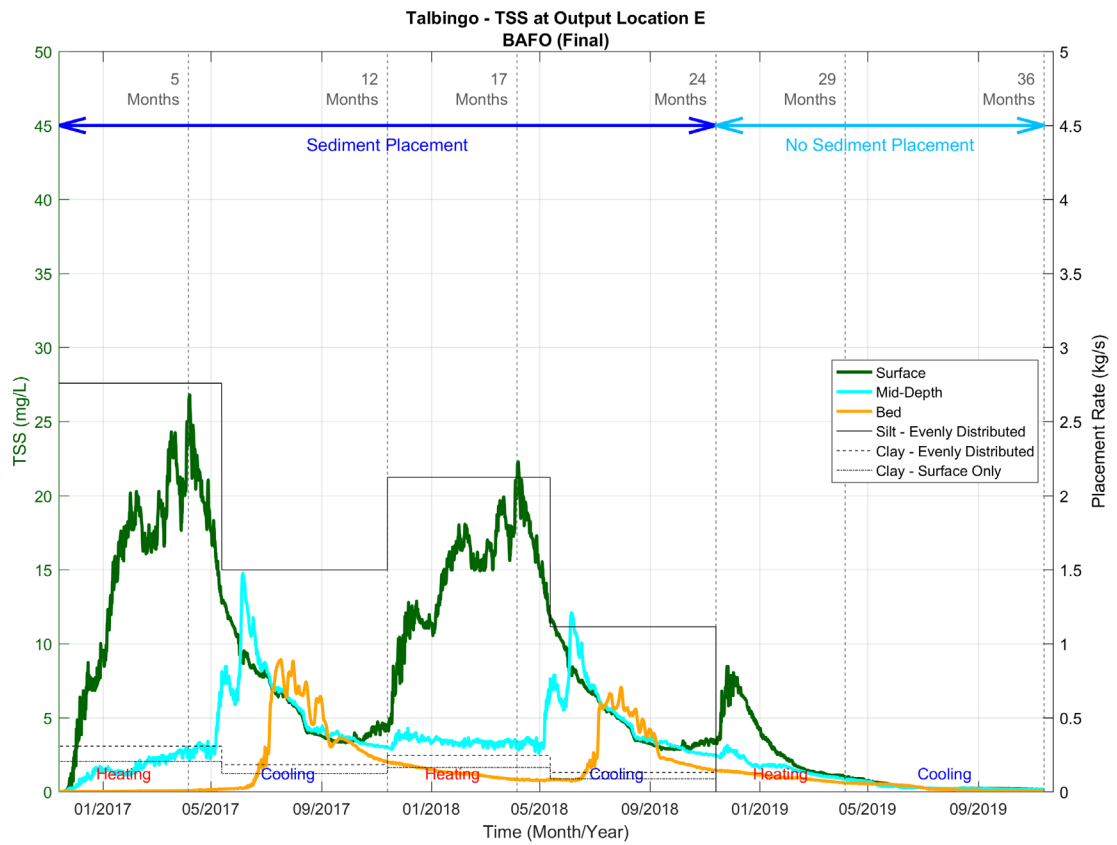
Appendix C TSS profiles for Talbingo Reservoir used in the hydrodynamic model and aluminium assessment

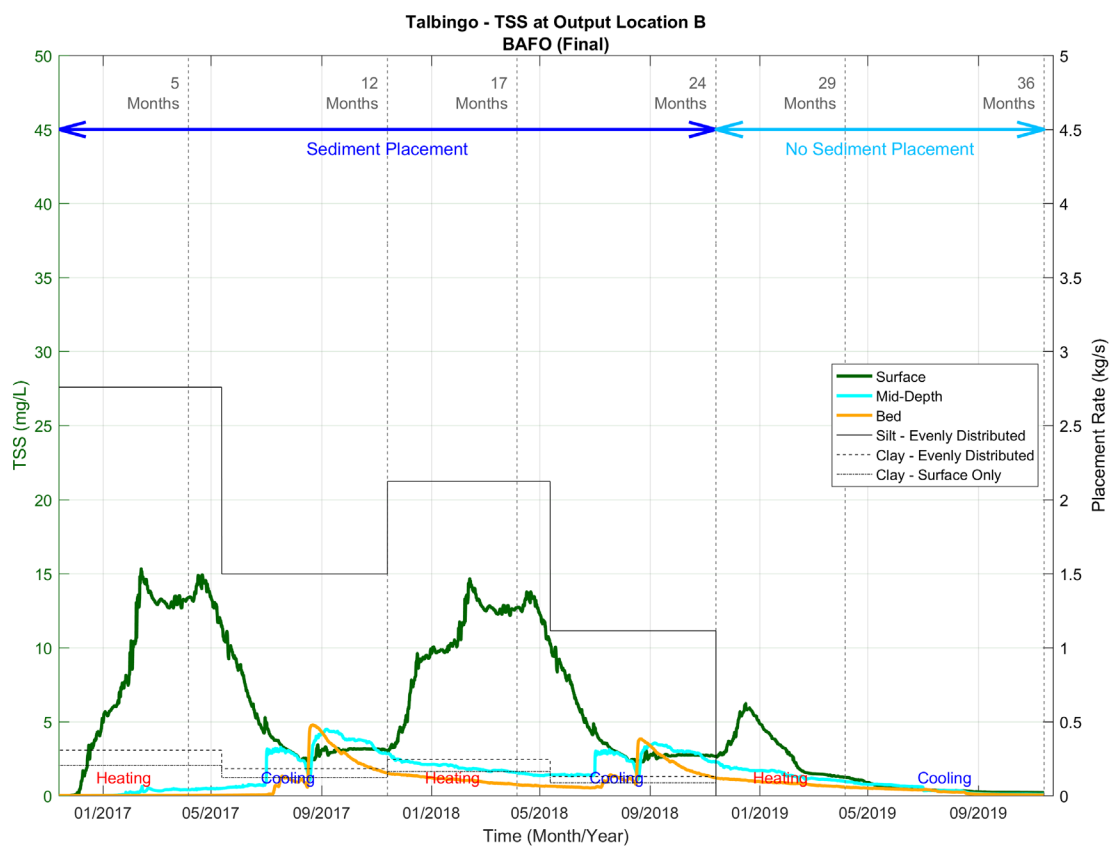
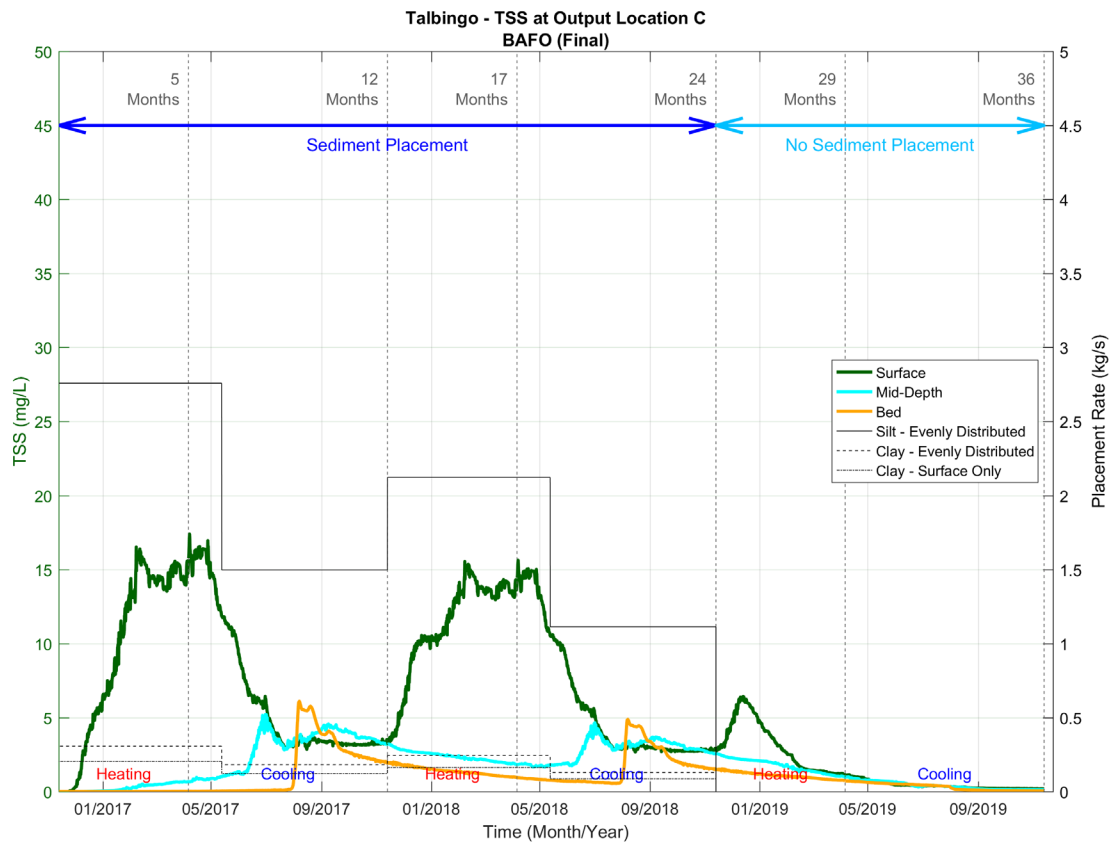
Note in the figures shown here the location names are alphabetical (J to A), being Location J = 1 (Placement area) to Location A = 10 (Reservoir outlet)

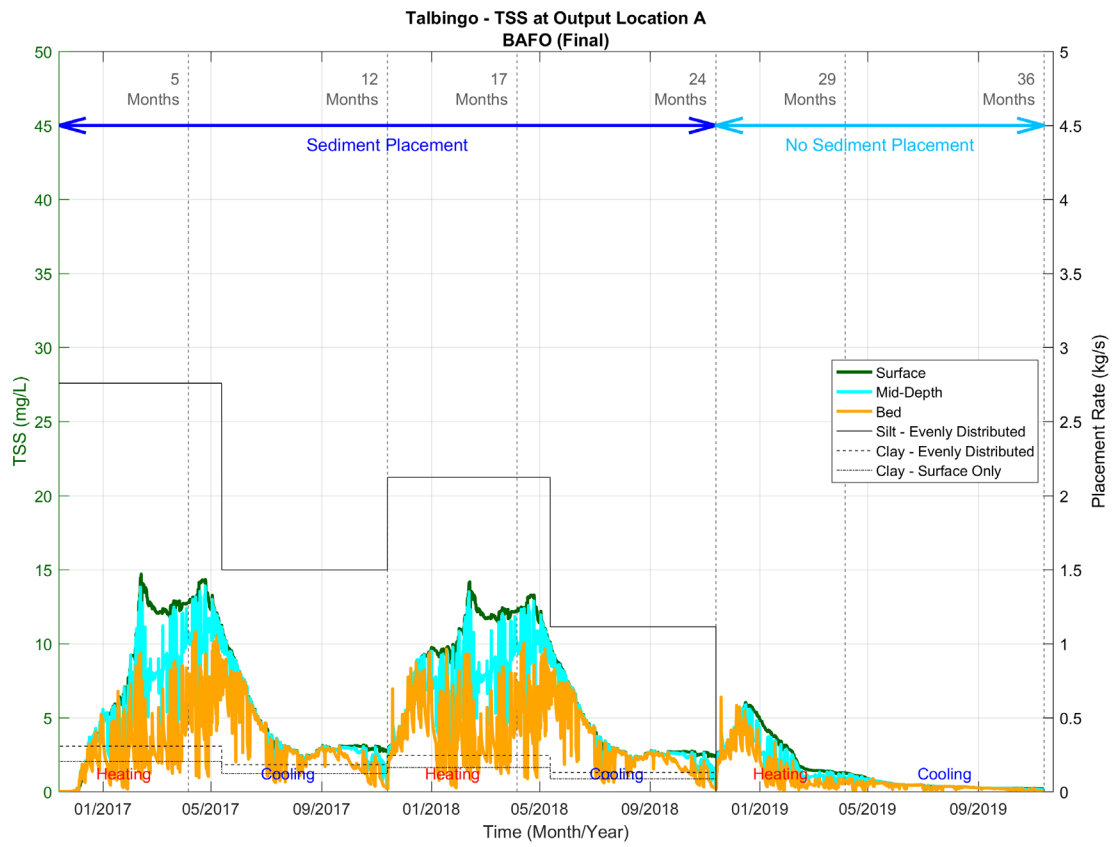












Appendix D Additional figures

Influence of water temperature

- The figures below illustrate the predicted lower dissolved aluminium concentrations that may occur at Location 1 if all of the fine rock material (TSS) was in cooler waters (6°C), compared to all being in warmer waters (21°C).

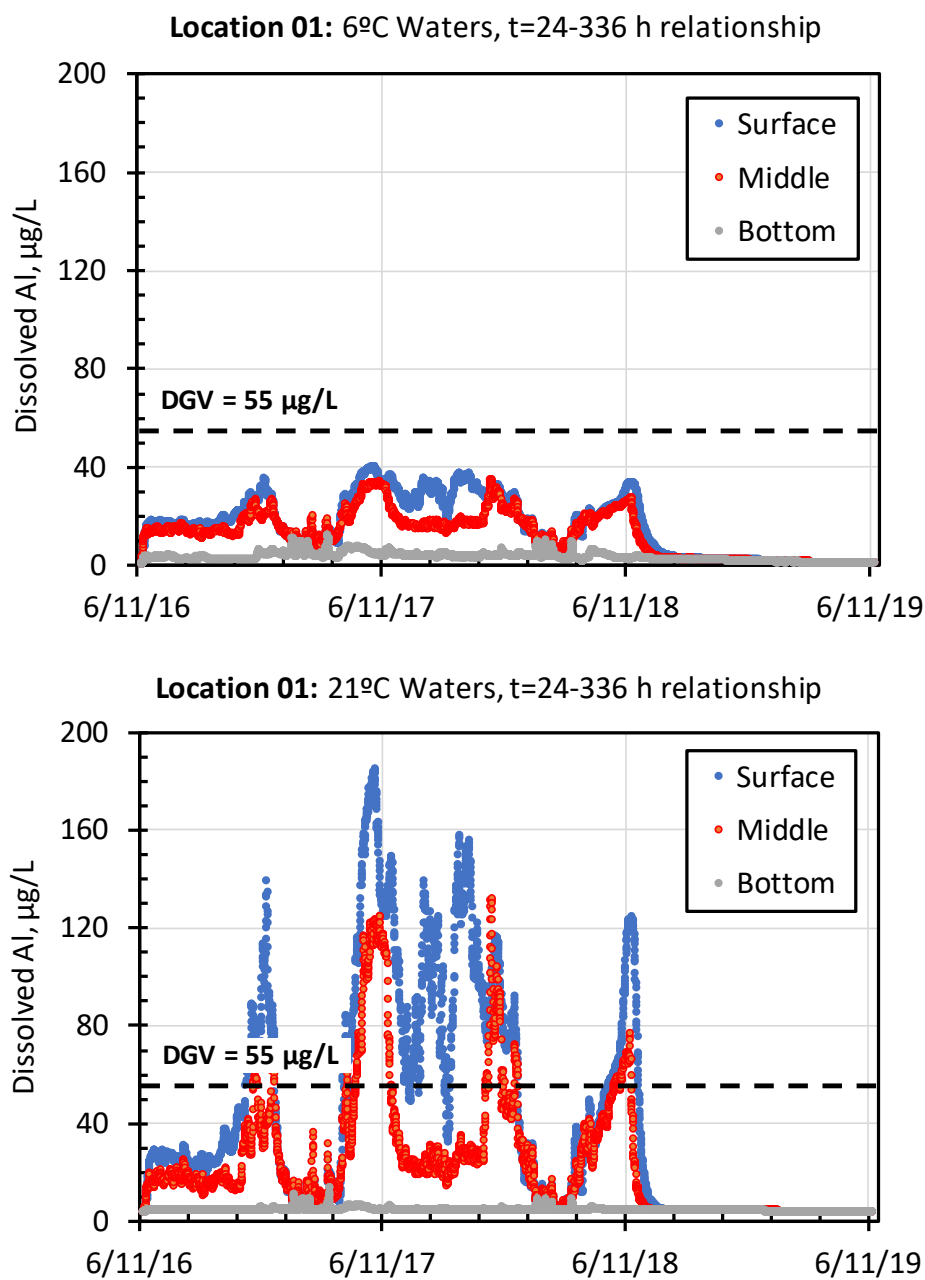


Figure D1. Predictions of dissolved aluminium concentrations at for Location 1 for waters at all depths being 21°C and 6°C, respectively.

Influence of higher levels of aluminium release at Locations 1 and 2

- This provides an indication of how higher amounts of dissolved aluminium release may influence dissolved aluminium concentrations at Locations 1 and 2. The rate of release per 6-h period is twice that shown in the main text.
- This scenario might exist if the continuous addition of fine rock material results in higher water pH being maintained within these two regions.

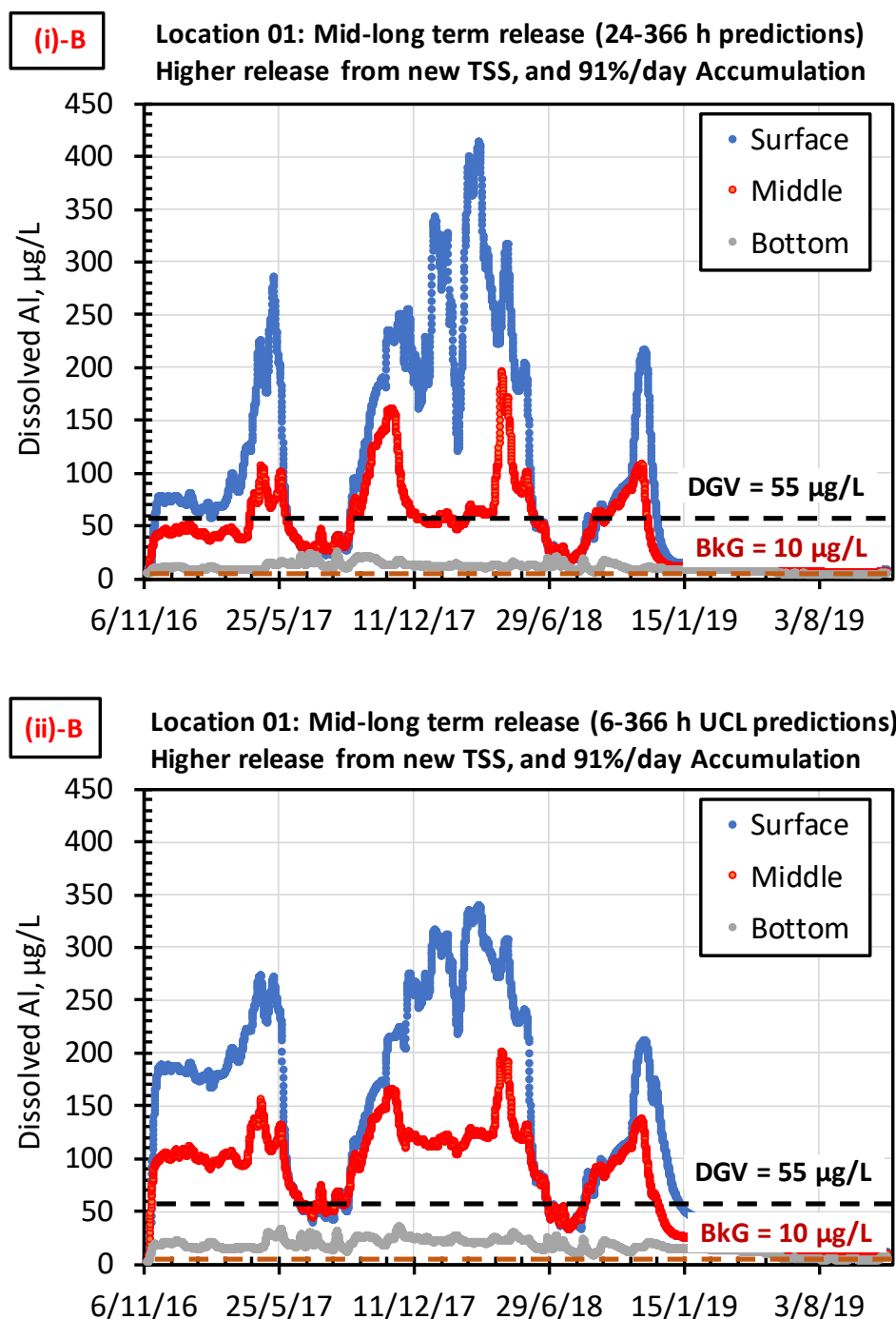
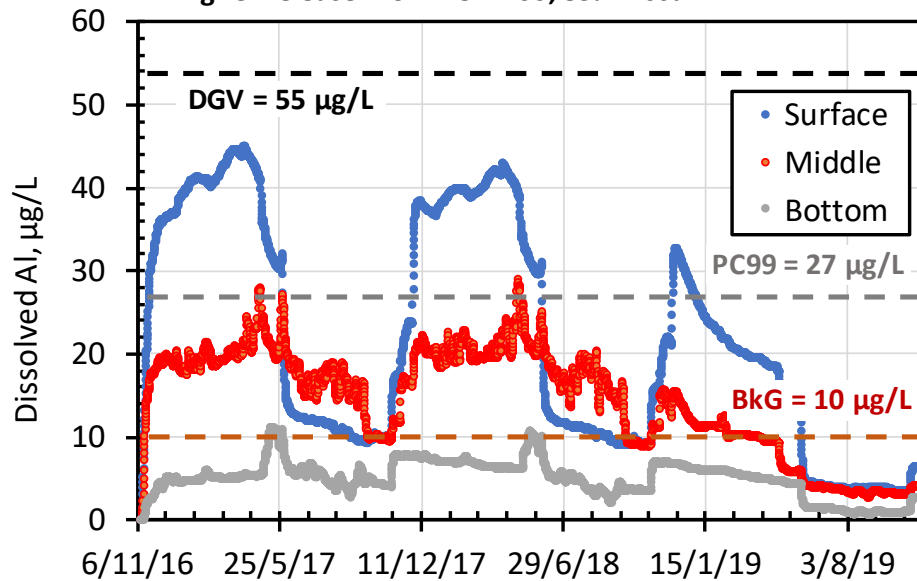


Figure D2. Predictions of dissolved aluminium concentrations at for Location 1 when factoring in a rate of aluminium release that is twice that used in Figure 7 predictions

(2A)

Location 02: Short-term release $t \leq 18$ h predictions:
Higher release from new TSS, 85% Accum



a

(2B)

Location 02: Short-term release $t \leq 18$ h model predictions:
Higher release from new TSS, 85% Accum, Transfer from 01

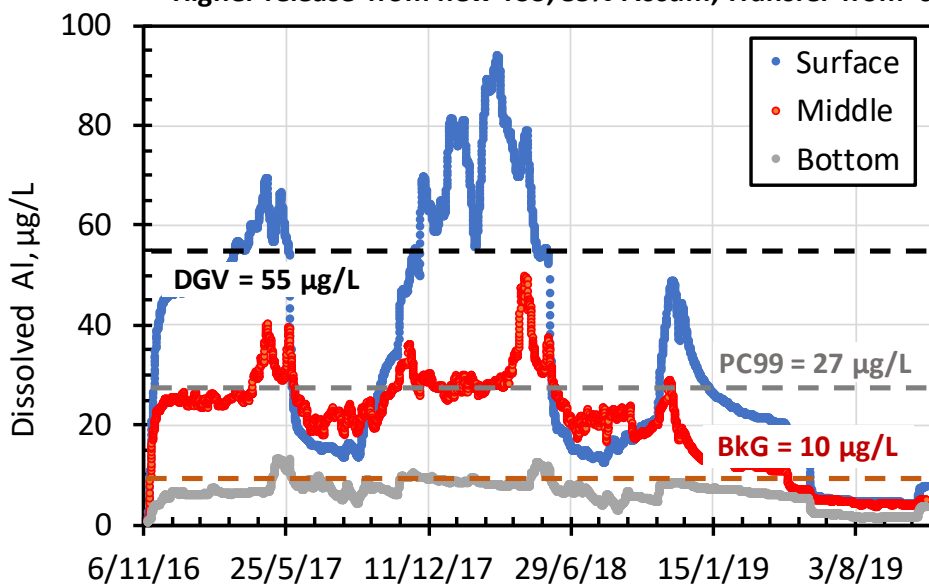


Figure D3. Predictions of dissolved aluminium concentrations at for Location 2 when factoring in a rate of aluminium release that is twice that used in Figure 8 predictions.

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