

Final Report

Wind Tunnel Test for: **MARTIN PLACE OVERSTATION** Sydney, Australia

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EXECUTIVE SUMMARY

A wind tunnel study of the proposed Martin Place Overstation development, to be located in Sydney, was conducted to assess pedestrian wind comfort at ground level. A massing model of the envelope of the project was fabricated to a 1:400 length scale and centred on a turntable in the wind tunnel. Replicas of surrounding buildings within a 570 m radius were constructed and placed on the turntable. The testing was conducted in a configuration including tower setbacks of 8 m as per the City of Sydney (2012) DCP, and with the amended building envelope for the South Site sought under the Stage 1 Amending DA. The results are compared with the wind conditions in the existing configuration on the site and the approved Stage 1 DA envelopes.

The wind tunnel testing was performed in the natural boundary layer wind tunnel of Cermak Peterka Petersen Pty. Ltd., St. Peters. Approach boundary layers, representative of the environment surrounding the proposed development, were established in the test section of the wind tunnel. The approach wind flow had appropriate turbulence characteristics corresponding to a suburban approach, as defined in Standards Australia (2011).

Measurements of winds likely to be experienced by pedestrians were made with a hot-film anemometer at 29 locations for 16 wind directions each. These points were tested around the development in the proposed and the LEP/DCP compliant configurations, focusing on access routes, doorways, and outdoor seating areas. The measurements were combined with site specific wind statistics to produce results of wind speed versus the percentage of time that wind speed is exceeded for each location. All locations were also tested in the existing configuration for comparison.

The wind environment around the development was found to be generally suitable for pedestrian standing and walking activities from a comfort perspective with reference to the Lawson criteria. All locations passed the Lawson distress criteria with the exception of two locations exposed to winds from the south-east over the exposed Hyde Park. The conditions in these two locations are not degraded by the proposed development. The tested wind conditions on the ground plane were found to be similar to the existing conditions in most areas. Some areas to the immediate north and east of the proposed buildings are affected by increased downwash off the northern façades of the proposed buildings, but still satisfy the required comfort and safety criteria.

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LIST OF SYMBOLS

D	Characteristic dimension (building height, width, etc.) (m)
n	Mean velocity profile power law exponent
T_u	Turbulence intensity, $U_{\rm stdev}/U$
U	Local mean velocity (m/s)
$U_{ m ref}$	Reference velocity at reference height z_{ref} (m/s)
$U_{ m pk}$	Peak wind speed in pedestrian studies (m/s)
$U_{ m stdev}$	Standard deviation of fluctuating velocity (m/s)
Z	Height above surface (m)
ν	Kinematic viscosity of approach flow (m ² /s)
σ()	Standard deviation of (),=()' _{rms}
ρ	Density of approach flow (kg/m ³)
() _{max}	Maximum value during data record
() _{min}	Minimum value during data record
()mean	Mean value during data record
() _{stdev}	Standard deviation

1. CLIENT PROVIDED PROJECT BACKGROUND

1.1 Introduction

This report supports a State Significant Development (SSD) Development Application (DA) submitted to the Minister for Planning (Minister) pursuant to Part 4 of the Environmental Planning and Assessment Act 1979 (EP&A Act) on behalf of Macquarie Corporate Holdings Pty Limited (Macquarie), who is seeking to create a world class transport and employment precinct at Martin Place, Sydney.

The SSD DA seeks approval for an amended Concept Proposal (otherwise known as a Stage 1 DA) relating to the Martin Place Metro Station Precinct ('the Precinct'). An existing development consent (SSD 17_8351) for a Concept Proposal is in place for the Precinct, which approved the concept for two Over Station Development (OSD) commercial towers above the northern (North Site) and southern (South Site) entrances of Martin Place Metro Station. The Concept Proposal approved building envelopes, land uses, Gross Floor Areas (GFA) and Design Guidelines with which the detailed design (otherwise known as a Stage 2 DA) must be consistent.

This Stage 1 Amending DA is a concept development application made under Section 4.22 of the EP&A Act. It seeks to align the approved South Site building envelope with the new planning controls established for the precinct as a result of a site specific amendment to Sydney LEP 2012. The new controls permit greater building height (over a portion of the South Site only) and additional floor space (North Site and South Site).

Whilst the approved Concept Proposal related to the entire Precinct, this Amending DA relates principally to the building envelope of the South Site, in terms of amending the approved height and floor space

Accordingly, this report presents the results of wind tunnel testing of the pedestrian level wind environment around the proposed development as reported for the previous Stage 1 DA configurations in CPP (2017).

1.2 Context

The New South Wales (NSW) Government is implementing Sydney's Rail Future (Transport for NSW, 2012), a plan to transform and modernise Sydney's rail network so that it can grow with the city's population and meet the needs of customers in the future.

Sydney Metro is a new standalone rail network identified in Sydney's Rail Future. The Sydney Metro network consists of Sydney Metro Northwest (Stage 1) and Sydney Metro City & Southwest (Stage 2).

Stage 2 of the Metro entails the construction and operation of a new Metro rail line from Chatswood, under Sydney Harbour through Sydney's CBD to Sydenham and onto Bankstown through the conversion of the existing line to Metro standards. The project also involves the delivery of seven (7) new Metro stations, including Martin Place.

This step-change piece of public transport infrastructure once complete will have the capacity for 30 trains an hour (one every two minutes) through the CBD in each direction catering for an extra 100,000 customers per hour across the Sydney CBD rail lines.

On 9 January 2017 the Minister approved the Stage 2 (Chatswood to Sydenham) Metro application lodged by Transport for NSW (TfNSW) as a Critical State Significant Infrastructure (CSSI) project (reference SSI 15_7400). Work is well underway under this approval, including demolition of buildings at Martin Place.

The OSD development is subject to separate applications to be lodged under the relevant provisions of the EP&A Act.

1.3 Site Description

The Sydney Metro Martin Place Station Precinct project relates to the following properties (refer to Figure 1):

- 50 Martin Place, 9 19 Elizabeth Street, 8 12 Castlereagh Street, 5 Elizabeth Street, 7 Elizabeth Street, and 55 Hunter Street (North Site);
- 39-49 Martin Place (South Site); and
- Martin Place (that part bound by Elizabeth Street and Castlereagh Street).

This Stage 1 Amending DA relates principally to the building envelope of the South Site, being land at 39 - 49 Martin Place, Sydney (refer to Figure 2).



Land not subject to this application

Figure 1: Location map of the Precinct (Google maps and JBA, 2017)



Figure 2: Aerial photo of the North and South Site (Nearmap and JBA, 2017)

1.4 Background

Sydney Metro Stage 2 Approval (SSI 15_7400)

On 9 January 2017, the Minister approved Stage 2 of the Sydney Metro project, involving the construction and operation of a metro rail line between Chatswood and Sydenham, including the construction of a tunnel under Sydney Harbour, links with the existing rail network, seven metro stations (including a station at Martin Place), and associated ancillary infrastructure. The project approves the demolition of existing buildings at Martin Place, excavation and construction of the new station (above and below ground) along with construction of below and above ground structural and other components of the future OSD, although the fit-out and use of such areas are the subject of separate development approval processes.

Modification 3 to the Sydney Metro approval enabled the inclusion of Macquarie-owned land at 50 Martin Place and 9-19 Elizabeth Street within the Martin Place Station footprint, and other associated changes (including retention of existing MLC pedestrian link).

Planning Proposal (PP 2017 SYDNE 007 00) - Amendment to Sydney LEP 2012

The Planning Proposal (PP_2017_SYDNE_007_00) sought to amend the development standards applying to the Sydney Metro Martin Place Station Precinct through the inclusion of a site-specific provision in the Sydney LEP 2012. This site-specific provision reduced the portion of the South Site that was subject to a 55 metre height limit from 25 metres from the boundary to Martin Place, to 8 metres, and applies the Hyde Park North Sun Access Plane to the remainder of the South Site, forming the height limit of the tower. It also permitted a revised FSR of 22:1 on the South Site and 18.5:1 on the North Site (resulting in a combined permissible overall GFA of 153,141m²). These amendments were gazetted within Sydney LEP 2012 and reflect the new planning controls applying to the precinct.

Concept Proposal (SSD 17_8351)

In early 2018, the Minister approved a Concept Proposal (SSD 17_8351) for the Precinct. The Concept Proposal established the planning and development framework through which to assess the detailed Stage 2 applications.

The approved Concept Proposal specifically encompassed:

- building envelopes for OSD towers on the North Site and South Site (see Figure 3) comprising:
 - 28+ storey building on the South Site, with a 25m setback to Martin Place above 55m in height, and a 40+ storey building on the North Site.

- Concept approval to integrate the North Site with the existing/retained 50 Martin Place building (the former Government Savings Bank of NSW).
- predominantly commercial land uses on both sites, comprising office, business and retail premises;
- a maximum total GFA of 125,437m² across both sites;
- consolidated Design Guidelines to guide the built form and design of the future development.
- a framework for achieving design excellence.
- strategies for utilities and services provision, managing drainage and flooding, and achieving ecological sustainable development.
- conceptual OSD areas in the approved Martin Place Metro Station structure, above and below ground level.

The Concept Proposal was prepared and determined prior to the site specific Sydney LEP 2012 amendment being gazetted and was developed based on the height development standards that applied to the South Site at the time. As a result, the approved Concept Proposal allows for a tower on the South Site that is now inconsistent with the building envelope envisaged through the Sydney LEP 2012.



Figure 3: North Site and South Site Approved OSD Building Envelopes (JBA, 2018)

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1.5 Overview of the Proposed Development

The Stage 1 Amending DA seeks approval for an amended Concept Proposal for the Martin Place Metro Station Precinct, specifically a larger building envelope for the South Site compared to the building envelope approved by the Minister through SSD 17_8351. The amended South Tower envelope will reflect a building envelope that aligns with the new controls applying to the precinct under Sydney LEP 2012, including increased height and FSR limits. It is proposed to amend the South Tower building envelope, through:

• a tower setback to Martin Place of 8 metres above the 55m podium height (reduced from 25 metres as approved within the Concept Proposal);

• a tower height that is consistent with the Hyde Park North Sun Access Plane beyond the 8m setback to Martin Place (constituting a generally taller tower than approved within Concept Proposal); and

• an increase in GFA/FSR for the South Site from approximately 23,700m² (12.5:1) up to approximately 41,700m² (22:1) - inclusive of all CSSI Station components.

Figure 4 below illustrates these proposed amendments to the South Site building envelope.

It is proposed that a condition be imposed on the Stage 1 Amending DA development consent pursuant to Section 4.17(1)(b) of the EP&A Act, requiring the modification of the original consent (SSD 17_8351) upon the commencement of the Stage 1 Amending DA Consent, in accordance with the procedures under Clause 97 of the *Environment Planning and Assessment Regulation 2000* (EP&A Regulation). This condition would address any inconsistency between the approved Concept Proposal and the Stage 1 Amending DA (and any subsequent detailed consents, i.e. the Stage 2 South Site DA).

1.6 Planning Approvals Strategy

The *State Environmental Planning Policy (State and Regional Development) 2011* (SEPP SRD) identifies development which is declared to be State Significant. Under Schedule 1 and Clause 19(2) of SEPP SRD, development within a railway corridor or associated with railway infrastructure that has a capital investment value of more than \$30 million and involves commercial premises is declared to be State Significant Development (SSD) for the purposes of the EP&A Act.

The proposed amendment (involving commercial development that is both located within a rail corridor and associated with rail infrastructure) is therefore SSD.

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Approved South Site Building Envelope

Proposed Amended South Site OSD Envelope (aligning with site specific amendment to Sydney LEP 2012)

Figure 4: Relationship between the approved and proposed amended South Site building envelope (JBA, 2018)

Submitted separately to this SSD DA are detailed proposals for the South Site (Stage 2 South Site DA) and North Site (Stage 2 North Site DA), which follow the approval of the Concept Proposal for the Precinct under Section 4.22 of the EP&A Act (formerly Section 83B). The Stage 2 detailed DA for the South Tower includes a design which is consistent with the envelope envisaged with this subject Stage 1 Amending DA and where it must only be determined following approval of the subject Stage 1 Amending DA.

Figure 5 below is a diagrammatic representation of the suite of key planning applications undertaken or proposed by Macquarie and their relationship to the subject application (the subject of this report).

The Department of Planning and Environment have provided Secretary's Environmental Assessment Requirements (SEARs) to the applicant for the preparation of an Environmental Impact Statement for the proposed development. This report has been prepared having regard to the SEARs as relevant.

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Figure 5: Relationship of key planning applications to the Stage 1 Amending DA (this application) (JBA,

2018)

2. INTRODUCTION

Pedestrian acceptability of footpaths, entrances, plazas, and terraces is often an important design parameter of interest to the development approvals body, building owner, and architect. Assessment of the acceptability of the pedestrian level wind environment is desirable during the project design phase so that modifications can be made, if necessary, to create wind conditions suitable for the intended use of the space.

Analytical methods such as computational fluid dynamics (CFD) are not capable, except in very simple geometries, to estimate wind pressures, frame loads, or windiness in pedestrian areas.

Techniques have been developed which permit boundary layer wind tunnel modelling of buildings to determine wind velocities in pedestrian areas. This report includes wind tunnel test procedures, test results, and a discussion of results. Table 1 summarises the model configurations, test methods, and data acquisition parameters used. All the data collection was performed in accordance with Australasian Wind Engineering Society (2001), and American Society of Civil Engineers (1999, 2010).

General Information							
Model length scale	1:400						
Surrounding model radius (full-scale)	570 m						
Reference height (full-scale)	200 m above ground level						
Approach Terrain Category	Suburban approach, Terrain Category 3						
Test C	Configuration Specifications						
Configuration A: Existing	Existing development with surrounding buildings and						
(Locations denoted XX)	landscape, as shown in Figure 8 and Figure 9.						
	Pedestrian winds measured at 29 locations for 16 wind directions at 22.5° increments from 0° (north)						
Configuration B: LEP/DCP compliant	LEP compliant envelope with DCP (8 m tower) setbacks						
(Locations denoted XX.1)	on both towers, as shown in Figure 11.						
	Pedestrian winds measured at 29 locations.						
Configuration C: Stage 1 DA approved envelopes (25 m tower	Envelopes of the Stage 1 Concept Proposal (SSD 8351), as shown in Figure 12.						
setback to Martin Place – South Site)	Pedestrian winds measured at 29 locations.						
(Locations denoted XX.2)							
Configuration D: Stage 1 Amending DA envelopes (8 m tower setback to Martin Place – South Site)	Envelope of the proposed Martin Place Overstation development, the subject of the Amending Stage 1 DA, as shown in Figure 10 and Figure 13.						
(Locations denoted XX.3)	Pedestrian winds measured at 29 locations.						

Table 1:	Configura	ations for	data a	acquisition

3. THE WIND TUNNEL TEST

Modelling of the aerodynamic flow around structures requires special consideration of flow conditions to obtain similitude between the model and the prototype. A detailed discussion of the similarity requirements and their wind tunnel implementation can be found in Cermak (1971, 1975, 1976). In general, the requirements are that the model and prototype be geometrically similar, that the approach mean velocity and turbulence characteristics at the model building site have a vertical profile shape similar to the full-scale flow, and that the Reynolds number for the model and prototype be equal. Due to modelling constraints, the Reynolds number cannot be made equal and Australasian Wind Engineering Society Quality Assurance Manual (2001) suggests a minimum Reynolds number of 50,000, based on representative model width and wind velocity at the top of the model; in this study the modelled Reynolds number was over 50,000.

The wind tunnel test was performed in the boundary layer wind tunnel shown in Figure 6. The wind tunnel test section is 3.0 m wide, by 2.4 m high with a porous slatted roof for passive blockage correction. This wind tunnel has a 21 m long test section, the floor of which is covered with roughness elements, preceded by a vorticity generating fence and spires. The spires, barrier, and roughness elements were designed to provide a modelled atmospheric boundary layer approximately 1.2 m thick with a mean velocity and turbulence intensity profile similar to that expected to occur in the region approaching the modelled area. The approach wind characteristics used for the model test are shown in Figure 7 and are explained more fully in Section 5.1.1.



Figure 6: Schematic of the closed-circuit wind tunnel

A massing model of the proposed development and surrounds to a radius of 570 m was constructed at a length scale of 1:400, which was consistent with the modelled atmospheric flow, and permitted a reasonable test model size with an adequate portion of the adjoining environment to be included in a proximity model that was within wind tunnel blockage limitations. The model was mounted on the turntable located near the downstream end of the wind tunnel test section, Figure 9. The turntable permitted rotation of the modelled area for examination of velocities from any approach wind direction.



Figure 7: Mean velocity and turbulence profiles approaching the model, terrain category 3

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Figure 8: Turntable layout with existing buildings



Figure 9: Photograph of the existing configuration model in the CPP wind tunnel viewed from the east

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Figure 10: Turntable layout with proposed buildings



Figure 11: Close-up photograph of the wind tunnel model for Configuration B (LEP/DCP compliant envelopes) viewed from the north-east



Figure 12: Close-up photograph of the wind tunnel model for Configuration C (Stage 1 DA approved envelopes) viewed from the north-east



Figure 13: Close-up photograph of the wind tunnel model for Configuration D (Amending Stage 1 DA envelopes) viewed from the north-east

4. ENVIRONMENTAL WIND CRITERIA

Over the years, a number of researchers have added to the knowledge of wind effects on pedestrians by suggesting criteria for comfort and safety. Because pedestrians will tolerate higher wind speeds for a smaller period of time than for lower wind speeds, these criteria provide a means of evaluating the overall acceptability of a pedestrian location. A location can further be evaluated for its intended use, such as for an outdoor café or a footpath. One of the most widely accepted set of criteria was developed by Lawson (1990), which is described in Table 2.

Table 2: The Lawson co	omfort criteria
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Comfort (m	Comfort (maximum of mean or gust equivalent mean (GEM ⁺) wind speed exceeded 5% of the time)							
< 4 m/s	Pedestrian Sitting (considered to be of long duration)							
4 - 6 m/s	Pedestrian Standing (or sitting for a short time or exposure)							
6 - 8 m/s	Pedestrian Walking							
8 - 10 m/s	Business Walking (objective walking from A to B or for cycling)							
> 10 m/s	Uncomfortable							
Distress (ma	aximum of mean or GEM wind speed exceeded 0.022% of the time)							
<15 m/s	not to be exceeded more than two times per year (or one time per season) for general							
<15 m/s access area								
<20 m/s	not to be exceeded more than two times per year (or one time per season) where only							
able bodied people would be expected; frail or cyclists would not be expected								
Note: ^{+.} The gu	st equivalent mean (GEM) is the peak 3 s gust wind speed divided by 1.85.							

Lawson's criteria have categories for comfort, based on wind speeds exceeded five percent of the time, allowing planners to judge the usability of locations for various intended purposes ranging from "business walking" to "pedestrian sitting". The level and severity of these comfort categories can vary based on individual preference, so calibration to the local wind environment is recommended when evaluating the Lawson ratings. The criteria also include a distress rating, for safety assessment, which is based on occasional (once or twice per year) wind speeds. In both cases, the wind speed used is the larger of a mean or gust equivalent-mean (GEM) wind speed¹. The GEM is defined as the peak gust wind speed divided by 1.85; this is intended to account for locations where the gustiness is the dominant characteristic of the wind. Assessment using the Lawson criteria provides a similar classification as using the once per annum gust, which was the basis of the City of Sydney (2011) DCP, however provides additional information regarding the serviceability wind climate. The current City of Sydney (2012) DCP specifies wind effects not to exceed 16 m/s, and 10 m/s for 'active frontages'. The draft amendments of the DCP require a wind speed of 8 m/s not to be exceeded for more than 5% of the time

¹ The rating of "uncomfortable" in Table 2 is the word of the acceptance criteria author and may not apply directly to any particular project. High wind areas are certainly not uncomfortable all the time, just on windier days. The word uncomfortable, in our understanding, refers to acceptability of the site by pedestrians for typical pedestrian use; i.e., on the windiest days, pedestrians will not find the areas "acceptable" for walking and will tend to avoid such areas if possible. The distress rating fail indicates some unspecified potential for causing injury to a less stable individual who might be blown over. The likelihood of such events is not well described in the literature and is likely to be strongly affected by individual differences, presence of water, blowing dust or particulates, and other variables in addition to the wind speed.

between 6 am and 10 pm, aligning with the pedestrian walking criterion by Lawson. The safety criterion of the draft amendments requires an annual maximum peak 0.5 second gust wind speed not to be exceeded, which aligns with the Lawson criterion of a GEM wind speed of 15 m/s for a 3 second gust. In the vicinity of the Martin Place Overstation development Martin Place, Hunter Street, and parts of Castlereagh Street are classified as active frontages, while Elizabeth Street is not. There are few locations in Sydney that would meet the current DCP criteria without shielding to improve the wind conditions. From discussions with Council the current DCP criterion wind speed is a once per annum gust wind speed similar to the 2004 DCP, but is meant to be interpreted as a comfort level criterion to promote outdoor café style activities and is not a distress requirement.

The once per annum gust wind speed criterion is based on the work of Melbourne (1978), and the 16 m/s level is classified as acceptable for pedestrian walking along a main accessway, and 10 m/s level is classified as generally acceptable for use for pedestrian sitting. This criterion gives the once per annum (actually 0.1% of the time) gust wind speed, and uses this as an estimator of the general wind conditions at a site. To combat this limitation, this study is based upon the criteria of Lawson (1990), which are described above. Assessment using the Lawson criteria provides a similar comfort classification as using the once per annum gust criteria, which is the basis of the City of Sydney (2012) DCP; however, it also provides significantly more information regarding the serviceability wind climate. The Lawson criteria align with the draft amendments of the City of Sydney DCP.

5. DATA ACQUISITION AND RESULTS

5.1 Velocities

Velocity profile measurements were taken to verify that appropriate boundary layer flow approaching the site was established and to determine the likely pedestrian level wind climate around the test site. Pedestrian wind measurements and analysis are described in Section 5.1.2. All velocity measurements were made with hot-film anemometers, which were calibrated against a Pitot-static tube in the wind tunnel. The calibration data were described by a King's Law relationship (King, 1914).

5.1.1 Velocity Profiles

Mean velocity and turbulence intensity profiles for the boundary layer flow approaching the model are shown in Figure 7. Turbulence intensities are related to the local mean wind speed. These profiles have the form as derived from Standards Australia (2011) and are appropriate for the approach conditions.

5.1.2 Pedestrian Winds

The proposed development is situated in the Sydney CBD between Castlereagh and Elizabeth Streets with the proposed towers being located north and south of the existing 50 Martin Place building, Figure 15. The site is surrounded by high-rise buildings of the Sydney CBD. The site is in the centre of the CBD and consequently receives some shielding from all wind directions.

Wind speed measurements were recorded at 29 locations to evaluate pedestrian comfort in and around the project site, Figure 15 to Figure 17. These locations were tested in a full envelope configuration of the proposed development and a configuration with a LEP/DCP compliant envelope on both towers, as well as in the existing building configuration for comparative purposes. Wind speed measurements were made at the model scale equivalent of 1.5 to 2.1 m above the surface for 16 wind directions at 22.5° intervals. Locations were chosen to determine pedestrian comfort at the building corners where relatively severe conditions are frequently found, near building entrances, on adjacent pavements with heavy pedestrian traffic, and in areas potentially intended for use as upper level outdoor terraces.

The hot-film signal was sampled for a period corresponding to one hour in prototype. All wind speed data were digitally filtered to obtain the two to three second running mean wind speed at each point; this is the minimum size of a gust affecting a pedestrian and the gust duration on which the wind criteria are based.

These local wind speeds, U, were normalised by the tunnel reference velocity, U_{ref} . Mean and turbulence statistics were calculated and used to calculate the normalised effective peak gust using

$$\frac{U_{\rm pk}}{U_{\rm ref}} = \frac{U + 3 \cdot \sigma_{\rm U}}{U_{\rm ref}}$$

The mean and gust equivalent mean velocities relative to the free stream wind tunnel reference velocity at a full-scale elevation of 200 m are plotted in polar form in Appendix 1. The graphs show velocity magnitude and the approach wind direction for which that velocity was measured. The polar plots aid in visualisation of the effects of the nearby structures or topography, the relative significance of various wind azimuths, and whether the mean or gust wind speed is of greater importance.

To enable a quantitative assessment of the wind environment, the wind tunnel data were combined with wind frequency and direction information measured by the Bureau of Meteorology (BoM) at a standard height of 10 m at Sydney Airport from 1995 to 2015, Figure 14. From these data, directional criterion lines for the Lawson rating wind speeds have been calculated and included on the polar plots in Appendix 1; this gives additional information regarding directional sensitivity at each location.

The criteria of Lawson consider the integration of the velocity measurements with local wind climate statistical data summarized in Figure 14 to rate each location. From the cumulative wind speed distributions for each location, the percentage of time each of the Lawson comfort rating wind speeds are exceeded are presented in tabular form under the polar plots in Appendix 1. In addition to the rating wind speeds, the percentage of time that 2 m/s is exceeded is also reported. This has been provided as it has been found that the limiting wind speed for long-term stationary activities such as fine outdoor dining should be about 2 to 2.5 m/s rather than 4 m/s.

Interpretation of these wind levels can be aided by the description of the effects of wind of various magnitudes on people. The earliest quantitative description of wind effects was established by Sir Francis Beaufort in 1806, for use at sea; the Beaufort scale is reproduced in Table 3 including qualitative descriptions of wind effects.

The tables in Appendix 1 additionally provide the wind speed exceeded 5% and 0.022% of the time for direct comparison with the Lawson comfort and distress criteria and the associated Lawson ratings for both mean and GEM wind speeds. A colour coded summary assessment of pedestrian comfort and safety with respect to the Lawson criteria is presented in Figure 15 to Figure 17 for each test location. The implications of the results are discussed in Section 6.



Figure 14: Wind rose of direction and speed for Sydney Airport

Description	Beaufort Number	Speed (m/s)	Effects
Calm, light air	0, 1	0–2	Calm, no noticeable wind.
Light breeze	2	2-3	Wind felt on face.
Gentle breeze	3	3–5	Wind extends light flag. Hair is disturbed. Clothing flaps
Moderate breeze	4	5-8	Raises dust, dry soil, and loose paper. Hair disarranged.
Fresh breeze 5 8–11		8-11	Force of wind felt on body. Drifting snow becomes airborne.
			Limit of agreeable wind on land.
Strong breeze	6	11-14	Umbrellas used with difficulty. Hair blown straight. Difficult to
			walk steadily. Wind noise on ears unpleasant. Windborne snow
			above head height (blizzard).
Near gale	7	14–17	Inconvenience felt when walking.
Gale	8	17-21	Generally impedes progress. Great difficulty with balance in
			gusts.
Strong gale	9	21–24	People blown over by gusts.

Table 3: Summary of wind effects on people, Penwarden (1973)

6. **DISCUSSION**

The wind climatology chart of Figure 14 indicates that the most frequent strong winds are from the south, and to a lesser extent, the west and north-east. The development is located in a central area of the city leading to some shielding effects from all wind directions. The topography and surrounding building layout relative to the prevailing strong wind directions influence the local wind flow in and around the development. Individual locations around the development are more susceptible to winds from different directions, depending on the relative location of the point tested to the geometry of the surrounding buildings. The influence of wind direction on the suitability of a location for an intended purpose can be ascertained from the polar plots in Appendix 1.

A high-level summary of the wind tunnel results including the Lawson comfort and safety ratings is provided in Table 4. The target criteria are based on the intended use of the space for each pedestrian level measurement location. It is evident that all ground plane locations meet the intended use of the space from a comfort perspective and pass the safety criterion, with the exception of locations 26 and 29. Both of these locations are unaffected by the proposed development and experience similar conditions in all configurations including the existing configuration.

More detailed conclusions of the pedestrian study can be understood by reviewing the colour coded images in Figure 15 to Figure 17, which present the locations selected for investigation of pedestrian wind comfort in and around the site along with the Lawson criteria rating for both comfort and distress. The central colour indicates the comfort rating for the location, and the colour of the outer ring indicates whether the location passes the distress criterion.

Note that testing was performed without planned trees, or other plantings to provide a worst case assessment; heavy streetscape planting typically reduces the wind speeds by less than 10%. Mitigation measures are likely to be required for red and orange locations, and may be necessary for other locations depending on the intended use of the space. Although conditions may be classified as acceptable there may be certain wind directions that cause regular strong events, these can be determined by an inspection of the plots in Appendix 1.

		Target		Wind Tunnel Results											
		_				Stage 1 DA approved envelopes (25m Amending Stage 1 DA envelopes (8n							envelopes (8m		
Description / Location			Existing			LEP/DCP Con	LEP/DCP Compliant Configuration			tower setback to MP - South Site)			tower setback to MP - South Site)		
		Comfort rating, 5% exceedance wind speed (m/s)	Comfort rating, 5% exceedance wind speed (m/s)	Meets target Y/N	Safety rating, 0.022% exceedance wind speed (m/s)	Comfort rating, 5% exceedance wind speed (m/s)	Meets target Y/N	Safety rating, 0.022% exceedance wind speed (m/s)	Comfort rating, 5% exceedance wind speed (m/s)	Meets target Y/N	Safety rating, 0.022% exceedance wind speed (m/s)	Comfort rating, 5% exceedance wind speed (m/s)	Meets target Y/N	Safety rating, 0.022% exceedance wind speed (m/s)	
	1	>6 to 8	3.7	Y	7.1	4.0	Y	8.0	4.0	Y	7.8	4.2	Y	8.3	
	2	>6 to 8	4.1	Y	8.0	4.2	Y	7.8	4.1	Y	8.0	4.0	Y	7.4	
	3	>6 to 8	4.8	Y	9.2	4.6	Y	8.9	5.9	Y	11.6	4.8	Y	10.2	
	4	>6 to 8	5.8	Y	11.8	6.3	Y	11.6	6.3	Y	12.6	6.3	Y	12.6	
	5	>6 to 8	4.8	Y	9.2	6.2	Y	12.1	6.4	Y	11.9	6.8	Y	13.0	
	6	>6 to 8	5.0	Y	10.7	4.8	Y	11.0	4.2	Y	10.2	4.4	Y	10.3	
	7	>6 to 8	6.2	Y	12.1	5.8	Y	10.9	6.0	Y	11.7	5.9	Y	12.2	
	8	>6 to 8	3.2	Y	6.3	3.3	Y	6.2	4.0	Y	7.5	4.0	Y	7.4	
	9	>6 to 8	2.2	Y	4.3	3.4	Y	6.6	3.8	Y	7.3	3.7	Y	7.7	
	10	>6 to 8	3.8	Y	7.5	3.9	Y	7.8	3.9	Y	8.0	4.0	Y	8.1	
	11	>6 to 8	2.5	Y	5.1	2.2	Y	4.8	2.4	Y	5.0	2.4	Y	4.9	
	12	>6 to 8	5.8	Y	10.6	5.7	Y	11.2	5.8	Y	11.1	5.9	Y	11.6	
Plane	13	>6 to 8	4.0	Y	8.1	4.9	Y	10.0	4.8	Y	9.9	5.5	Y	11.1	
Pla	14	>6 to 8	6.3	Y	12.0	6.3	Y	11.6	6.0	Y	11.0	6.1	Y	11.3	
Ground	15	>6 to 8	3.8	Y	7.5	4.2	Y	8.3	4.5	Y	9.3	4.0	Y	8.0	
rou	16	>6 to 8	4.5	Y	9.3	5.6	Y	11.1	5.1	Y	9.6	5.7	Y	11.4	
0	17	>6 to 8	4.5	Y	9.3	6.3	Y	12.8	4.6	Y	9.2	5.9	Y	11.7	
	18	>6 to 8	4.7	Y	10.6	6.2	Y	12.7	5.7	Y	11.6	6.8	Y	13.1	
	19	>6 to 8	4.7	Y	8.7	6.6	Y	12.1	6.2	Y	11.5	6.9	Y	13.4	
	20	>6 to 8	6.4	Y	11.6	6.4	Y	12.0	6.4	Y	12.0	6.5	Y	11.8	
	21	>6 to 8	6.9	Y	13.4	6.8	Y	13.1	6.9	Y	13.4	6.8	Y	13.0	
	22	>6 to 8	5.9	Y	10.9	5.6	Y	10.2	5.7	Y	10.7	5.6	Y	10.5	
	23	>6 to 8	5.2	Y	10.7	4.1	Y	8.6	3.1	Y	6.3	3.8	Y	7.7	
	24	>6 to 8	4.7	Y	9.3	4.7	Y	9.8	4.6	Y	9.3	4.8	Y	9.8	
	25	>6 to 8	5.0	Y	9.5	6.2	Y	12.1	5.4	Y	10.2	6.0	Y	11.4	
	26	>6 to 8	7.5	Y	15.6	7.5	Y	15.5	7.3	Y	15.1	7.4	Y	15.3	
	27	>6 to 8	4.6	Y	8.3	4.3	Y	8.1	4.4	Y	9.1	4.5	Y	8.2	
	28	>6 to 8	5.2	Y	10.3	5.2	Y	9.6	4.7	Y	9.3	5.5	Y	10.6	
	29	>6 to 8	7.7	Y	16.3	7.3	Y	15.7	7.2	Y	15.3	7.3	Y	15.7	

Table 1: Summary	of target criteria	and wind tunnel results
Table 4: Summary	of target criteria	and wind tunnel results



6.1.1 – Existing development with existing surroundings

In the surrounding area of the proposed development, the wind conditions at pedestrian level in the existing configuration are generally classified as suitable for pedestrian standing and walking with some specific locations meeting the sitting criterion, refer to Table 4 and Figure 15.



Figure 15: Pedestrian wind speed measurement locations with comfort/distress ratings – Configuration A, existing buildings

Wind conditions to the north of the northern tower site, Locations 1 to 7 along Hunter Street, are generally rated as suitable for pedestrian standing from a comfort perspective with the exception of Location 1, which is at the border between pedestrian sitting and standing, and Location 7, which slightly exceeds the pedestrian standing threshold and is rated as suitable for pedestrian walking. This area is generally affected by winds from the north-east quadrant, in the form of channelled flow along

Philip and Hunter Streets augmented by downwash from the north façade of the existing buildings along these streets such as Chifley Tower, 8 Chifley Square, and 126 Philip Street.

Areas to the north of Martin Place along Castlereagh and Elizabeth Streets are relatively calm, with Locations 8-15 rated as suitable for pedestrian sitting or standing, with the exception of Location 14 which is slightly above the border between pedestrian standing and walking. The test locations along Martin Place, Locations 16-22 are all rated as suitable for pedestrian standing except for Locations 20 and 21, which are rated as suitable for pedestrian walking.

Conditions to the south of Martin Place along Castlereagh and Elizabeth Street are mostly suitable for pedestrian standing. The exception is Location 26, which is rated as suitable for pedestrian walking and fails the Lawson distress criterion with a classification as suitable for able bodied pedestrians only. Location 26 experiences windy conditions for winds from the south-east quadrant approaching over the exposed Hyde Park area and channelling up Elizabeth Street.

Location 29, remote from the site at the southern end of Philip Street is classified as suitable for pedestrian walking from a comfort perspective and fails the Lawson distress criterion being classified as suitable for able bodied pedestrians. This location is similarly affected by strong winds from the south-east quadrant, which approach over the exposed area of Hyde Park.

All locations except Locations 26 and 29 pass the distress criterion.

6.1.2 – Proposed development with existing surroundings and DCP compliant setbacks

With the inclusion of the proposed buildings with DCP compliant setbacks, i.e. tower setbacks of 8 m to street frontages, wind conditions at ground level are generally similar to the existing conditions, with most locations being classified as suitable for pedestrian standing or sitting, refer to Figure 16. An increased number of locations were found suitable for pedestrian walking relative to the existing case, however conditions in many areas are near the threshold between standing and walking categories and any increases in wind speeds are relatively minor.

Conditions to the north and east of the development sites are slightly degraded by the addition of the two towers. Locations 4.1, 5.1, 17.1 to 19.1, and 25.1 are classified as suitable for pedestrian walking in this configuration. These areas are most strongly affected by winds from the east. The proposed towers are significantly taller than the existing buildings, and will therefore produce stronger downwash at the ground plane. Areas along Castlereagh Street are largely unaffected by the addition of the proposed development.

Wind conditions along Martin Place to the east and west of the proposed development, Locations 16.1, and 20.1-22.1, are almost unchanged compared with the existing conditions.

Wind conditions to the south of the site on Elizabeth Street, Location 26.1-28.1 remain similar to the existing conditions. This area remains suitable for pedestrian walking from a comfort perspective, and fails the distress criterion in Location 26.1 as in the existing configuration.

Further away from the site, on Philip Street, Location 29.1 is classified as suitable for pedestrian walking and fails the distress criterion with an able-bodied rating. The strong wind conditions at this location are not caused by the proposed development and are similar to the existing configuration.



Figure 16: Pedestrian wind speed measurement locations with comfort/distress ratings - Configuration B,

LEP/DCP compliant envelope of proposed buildings

6.1.3 – Stage 1 DA approved envelopes with existing surroundings

Conditions in Configuration C generally remain similar to Configuration B, Figure 17. Location 8.2 shows a degradation in comfort category, however it should be noted that the measured 5% exceedance wind speeds at this location is close to the boundary between two comfort categories, and the quantifiable difference in condition between Configurations B and C is minor. Similarly, though Locations 17.2-18.2, 23.2, and 25.2 are shown to improve in terms of their respective comfort categories relative to the previous configuration, the difference in wind conditions is insignificant. Overall, wind conditions in this configuration are largely the same as the LEP/DCP-compliant configuration, with wind speeds slightly increasing at some locations and slightly decreasing at others.

Locations 26.2 and 29.2 fail the distress criterion, as in the existing and LEP/DCP-compliant configuration.



Figure 17: Pedestrian wind speed measurement locations with comfort/distress ratings – Configuration C, Stage 1 DA approved envelopes (25 m tower setback to Martin Place on South Site)

6.1.4 – Amending Stage 1 DA envelopes with existing surroundings

Conditions in Configuration D generally remain similar to Configurations B and C, refer to Figure 17. Locations 18.3 and 25.3 show a degradation in comfort category compared to the larger setback on the south tower towards Martin Place in the Stage 1 DA approved envelope, however these comfort ratings are identical to those in the LEP/DCP envelopes (Configuration B). Location 2.3 is shown to improve in terms of the comfort category relative to the previous configurations, however the difference in wind conditions is insignificant. Overall, wind conditions in this configuration are largely the same as the LEP/DCP-compliant configuration and the Stage 1 DA approved envelope, with wind speeds slightly increasing at some locations and slightly decreasing at others.

Locations 26.3 and 29.3 fail the distress criterion, as in all other configurations.



Figure 18: Pedestrian wind speed measurement locations with comfort/distress ratings – Configuration D, Amending Stage 1 DA envelopes (8 m tower setback to Martin Place on South Site)

7. CONCLUSIONS

A wind tunnel investigation of the pedestrian level wind environment in and around the proposed Martin Place Overstation development has been conducted. At street level, the existing wind environment near the development site is generally suitable for pedestrian standing and walking. Some areas on Elizabeth and Philip Street to the south of the site are windy and currently exceed the distress criterion, due to being exposed to unimpeded winds flowing over Hyde Park from the south-east quadrant.

The addition of the LEP/DCP-compliant scheme creates some changes to wind flow patterns in the area, causing some areas to be windier and providing shelter for others. In general, conditions at the ground plane remain similar to the existing.

The modification to the building setbacks in Configurations C and D has a relatively minor impact on wind amenity at the ground plane, with a small improvement in wind conditions at some locations and slight degradation at others. Excluding locations where existing conditions exceed target levels already, all areas are assessed as suitable for the intended use of space in this section of the city.



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Appendix 1: Directional Wind Results



Configuration A – Existing



July 2018


















Configuration B – DCP compliant































































Configuration D – Full envelope of proposed buildings (8 m setback)

























