# TRAFFIC AND PARKING IMPACT ASSESSMENT OF SAINTS PETER AND PAUL ASSYRIAN PRIMARY SCHOOL 

## AT 17-19 KOSOVICH PLACE, CECIL PARK



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## 1 INTRODUCTION

$M^{C}$ Laren Traffic Engineering (MTE) was commissioned by PMDL to provide a Traffic and Parking Impact Assessment of the Saints Peter and Paul Assyrian Primary School at 17 19 Kosovich Place, Cecil Park as shown in Annexure A for reference. This report is to accompany the State Significant Development Application (SSDA) for stage one of the overall masterplan and provides an assessment of the traffic and parking impacts for both the first stage and final masterplan form of development proposed.

### 1.1 Description and Scale of Development

The proposed Saints Peter and Paul Primary School will be constructed and populated in multiple stages and includes the following characteristics relevant to traffic and parking impacts:

- Stage One:
- Total of 210 students $(\mathrm{K}-6)$;
- Total of 12 staff;
- 39 off-street car parking spaces for staff, including two disabled spaces;
- Formalised internal kiss and ride facility for parents.
- Final Development:
- Total of 630 students $(\mathrm{K}-6)$;
- Total of 35 school staff;
- 39 off-street car parking spaces for staff, including two disabled spaces;
- Formalised internal kiss and ride facility for parents.

In addition to the construction of the school, some public works are proposed to improve Kosovich Place and the surrounding road network including the following:

- Widening of Kosovich Place to provide sufficient width for bus access;
- Construction of a footpath along the frontage of the site to provide for a bus stop;
- Improvements to the Kosovich Place/Wallgrove Road intersection;
- Improvements to the Wallgrove Road/Elizabeth Drive intersection if required;
- Removal and reconstruction of two vehicular crossings on Kosovich Place.


### 1.2 State Environmental Planning Policy (Infrastructure) 2007

The proposed development does qualify as a development with relevant size and/or capacity under Clause 104 of the SEPP (Infrastructure) 2007 being an 'Educational Establishment' of 50 or more students. Accordingly, formal referral to the Roads and Maritime Services (RMS) is necessary.

### 1.3 Site Description

The subject site is located within the Fairfield City Council Local Government Area and has a single street frontage to Kosovich Place. Wallgrove Road, a State Classified Road, is nearby approximately 280 m to the east of the site.
The school is zoned RU4 - Primary Production Small Lots under the Fairfield City Council Local Environmental Plan 2013 and is generally surrounded by rural properties and lowdensity residential dwellings.

### 1.4 Site Context

The location of the site is shown on aerial imagery and a map in Figure 1 \& Figure 2 respectively.


Site Location
FIGURE 1: SITE CONTEXT - AERIAL IMAGE


Site Location
FIGURE 2: SITE CONTEXT - MAP

## 2 EXISTING SITE \& SURROUNDING CONDITIONS

### 2.1 Road Hierarchy

The relevant characteristics of the road network servicing the site are summarised below.

### 2.1.1 Wallgrove Road

- Classified State Main Road No. 515;
- Approximately 11.5 m in width facilitating one traffic and one parking lane in each direction;
- Signposted $80 \mathrm{~km} / \mathrm{h}$ carriageway;
- Unrestricted kerbside parking generally permitted along both sides of the road in linemarked shoulders.


### 2.1.2 Elizabeth Drive

- Classified State Main Road No. 535;
- Approximately 21.5 m in width to the east of Wallgrove Road, facilitating two traffic lanes in each direction and a 6 m wide median;
- Approximately 13 m wide to the west of Wallgrove Road, facilitating one traffic lane and one parking lane in each direction;
- Signposted $70 \mathrm{~km} / \mathrm{h}$ carriageway;
- No parking permitted to the east of Wallgrove Road, unrestricted parking generally permitted along both sides of the road to the west of Wallgrove Road in line-marked shoulders.


### 2.1.3 The Horsley Drive

- Classified State Main Road No. 609;
- Approximately 13 m wide to the east of Wallgrove Road, facilitating one traffic lane eastbound and two traffic lanes westbound and a $2 m$ wide median;
- Approximately 11 m wide to the west of Wallgrove Road, facilitating one traffic lane and a formalised shoulder in either direction;
- Signposted $70 \mathrm{~km} / \mathrm{h}$ carriageway to the east of Wallgrove Road, $50 \mathrm{~km} / \mathrm{h}$ to the west of Wallgrove Road;
- No parking permitted to the east of Wallgrove Road, unrestricted parking generally permitted along both sides of the road to the west of Wallgrove Road in line-marked shoulders.


### 2.1.4 Kosovich Place

- Unclassified Local Road;
- Approximately 6.5 m in width, providing for two-way passing of traffic;
- $50 \mathrm{~km} / \mathrm{h}$ speed limit applies;
- No kerbs are provided and some informal parking may occur on either side of the road, partially using the verge.


### 2.2 Existing Traffic Management

- Signalised intersection of Wallgrove Road/Elizabeth Drive;
- Signalised intersection of Wallgrove Road/The Horsley Drive;
- "GIVE WAY" controlled intersection of Kosovich Place/Wallgrove Road;
- Roundabout controlled intersection at Wallgrove Road/Villiers Road.


### 2.3 Existing Traffic Environment

### 2.3.1 Turning Movement Counts

Turning movement counts were completed on Thursday 26 and Friday 27 July 2018 between the times of 7:00 am - 9:30 am and 2:00 pm - 4:30 pm to capture the key school peak times at the intersections of:

- Elizabeth Drive/Wallgrove Road;
- The Horsley Drive/Wallgrove Road;
- Kosovich Place/Wallgrove Road.

Detailed results from these surveys are provided in Annexure B for reference.

Growth rates have been provided by the Roads and Maritime Servicesfor the roads and intersections in the surrounds of the site, as reproduced in Annexure C. The growth rates for each intersection have been applied to the existing traffic counts to produce predicted turning movement counts for 2028.

### 2.3.2 Intersection Performances

Existing (2018) and future (2028) intersection performances have been assessed using SIDRA INTERSECTION 8. The results of the analysis are summarised in Table 1. The SIDRA output summaries are provided in Annexure D.

TABLE 1: INTERSECTION PERFORMANCES (SIDRA INTERSECTION 7)

| Intersection | Peak Hour | Degree of Saturation ${ }^{(1)}$ | Average Delay ${ }^{(2)}$ <br> (sec/veh) | Level of Service ${ }^{(3)}$ | Control Type | Worst Movement | 95th Percentile Queue |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| EXISTING PERFORMANCE |  |  |  |  |  |  |  |
| M7 Exit / Elizabeth Drive | AM | 0.93 | 37.2 | C | Signals | RT from Wallgrove Road (N) | 33.2 veh (248.2m) <br> Elizabeth Drive (W) |
|  | PM | 0.90 | 46.9 | D |  | $\begin{aligned} & \text { LT from M7 } \\ & \text { Exit (S) } \end{aligned}$ | 34.2 veh (259.7m) <br> Elizabeth Drive (W) |
| Wallgrove Road / The Horsely Drive | AM | 0.80 | 40 | C | Signals | LT from The Horsely Drive (W) | $18.7 \text { veh (139m) }$ <br> Wallgrove Road (S) |
|  | PM | 0.82 | 36.2 | C |  | LT from The Horsely Drive (E) | 21.9 veh (160.9m) <br> Wallgrove Road (N) |
| Wallgrove Road/ Kosovich Place | AM | 0.49 | $\begin{gathered} 0.1 \\ \text { (Worst: } \\ \text { 17.3) } \\ \hline \end{gathered}$ | NA <br> (Worst: B) | Give Way | RT from Kosovich Place (E) | 0 veh ( 0.2 m ) <br> Wallgrove Road (S) |
|  | PM | 0.51 |  | NA <br> (Worst: B) |  | RT from Kosovich Place (E) | 0 veh ( 0.3 m ) <br> Wallgrove Road (S) |
| Wallgrove Road / Villiers Road | AM | 0.54 | $4.1$ <br> (Worst: 10.8) | A <br> (Worst: A) | Roundabout | UT from Wallgrove Road (S) | 1.1 veh ( 8.5 m ) <br> Wallgrove Road (N) |
|  | PM | 0.56 |  | A <br> (Worst: A) |  | UT from Wallgrove Road (S) | 4.9 veh ( 36.1 m ) <br> Wallgrove Road (N) |

NOTES:
(1) Degree of Saturation is the ratio of demand to capacity for the most disadvantaged movement.
(2) The average delay is the delay experienced on average by all vehicles. The value in brackets represents the delay to the most disadvantaged movement.
(3) The level of Service is a qualitative measure of performance describing operational conditions. There are six levels of service, designated from $A$ to $F$, with $A$ representing the best operational condition and level of service $F$ the worst. The LoS of the intersection is shown in bold, and the LoS of the most disadvantaged movement is shown in brackets.

As shown above, other than the intersection of Elizabeth Drive and Wallgrove Road, the surrounding intersections are operating satisfactorily at Level of Service (LoS) C or better during the morning and afternoon peak periods. This represents adequate performance.

The intersection of Elizabeth Drive and Wallgrove Road is nearing its existing capacity in the weekday PM peak, with a Level of Service of D reflected, which indicates that the intersection is operating near to its capacity.

### 2.4 Public Transport

The subject site is poorly served by existing public transport and is not within walking distance of any bus stops or other public transport facilities. It is intended that a school bus service be established to provide transport to and from the finished school and consultation has been undertaken with the local operator, Transit Systems, to achieve this outcome.

### 2.5 Future Road and Infrastructure Upgrades

From the Fairfield Council Development Application tracker and website, it appears that there are no future planned road or public transport changes that will affect traffic conditions within the immediate vicinity of the subject site.

From a review of the Roads and Maritime Services Sydney West projects register, there are two proposed upgrades that may affect the traffic conditions surrounding the proposed school including the upgrade to the Horsley Drive and the M12 Motorway.

The upgrades to the Horsley Drive will include an upgrade of the Wallgrove Road/The Horsley Drive intersection, with the future geometry of the intersection depicted in Figure 3. As shown, a lane will be added to the eastern approach to the intersection. The upgraded layout of the intersection has been considered in the modelling of the 10 year scenarios in Section 4.3 of this report.

The RMS has been contacted to provide comment on the impacts of the M12 Motorway on Wallgrove Road and the intersection of Elizabeth Drive and Wallgrove Road, but to date no response has been received.


FIGURE 3: THE HORSLEY DRIVE/WALLGROVE ROAD UPGRADED GEOMETRY

## 3 PARKING IMPACT ASSESSMENT

### 3.1 Council Parking Requirement

Reference is made to the Fairfield Council Development Control Plan (2015) which provides the following parking requirements relevant to the subject development:

## Educational Establishment

## Schools

1 space per employee plus 1 space per 10 students in Year 12 (where applicable)

The resulting parking requirement is provided in Table 2.
TABLE 2: DCP PARKING REQUIREMENTS

| Land Use | Type | Scale | Rate | Spaces Required |
| :---: | :---: | :---: | :---: | :---: |
| STAGE 1 |  |  |  |  |
| School | Staff | 12 | 1 space per staff member | 12 |
| Total for Stage 1 |  |  |  | $\mathbf{1 2}$ |
| FINAL DEVELOPMENT |  |  |  |  |
| School | Staff | 35 | 1 space per staff member | 35 |
| Future Total |  |  |  | $\mathbf{3 5}$ |

As shown, under the requirements of the Fairfield City Council DCP the site requires a total of 12 parking spaces for staff for the first stage of development, with a final projected parking requirement of 35 spaces for staff for the final development scale.

School parking is proposed to be accommodated completely on-site in both Stage 1 and the final form of development. The parking and kiss and drop facility will be completed for the opening of the first Stage of the development and will incorporate:

- 30 kiss and drop spaces;
- 39 parking spaces for staff and disabled visitors;
- Internal queueing areas for up to 44 additional vehicles without affecting the efficacy of the kiss and drop operations of the site.

Figure 4 illustrates the function of the proposed parking and kiss and drop areas on the site.


FIGURE 4: KISS AND DROP OPERATIONS

### 3.2 Parent Pick-Up Queue Analysis

Surveys of the associated St Hermizd Primary School have been undertaken to ascertain the characteristics of schools operated by the applicant. These surveys reflect that on average, 1.85 children are enrolled by each family at the St Hermizd Primary School.

The potential queue lengths for both the Stage 1 and completed school have been considered based on the following assumptions:

- Stage 1:
- $100 \%$ of children travel from school by private car;
- Car occupancy rate of 1.85 children per car;
- Picking up operations take an average of 4 minutes;
- Parents begin to arrive 15 minutes prior to bell times.
- Completed school:
- $80 \%$ of children travel from school by private car, $20 \%$ by bus;
- Car occupancy rate of 1.85 children per car;
- Picking up operations take an average of 4 minutes;
- Parents begin to arrive 15 minutes prior to bell times.

Considering that a total of 30 kiss and drop spaces are proposed, on average the service rate of this system will be one vehicle every 8 seconds.

Typically for primary schools the afternoon pick-up operation has the highest demand for parking and occurs in two phases:
a) Prior to school pick-up, with parents arriving approximately 15 minutes prior to the bell ringing;
b) During the pick up period after the bell has rung.

The greatest queue length can occur in either of the above phases depending on the efficiency of the kiss and drop operations. Table 3 provides a simplistic estimate for the maximum queue predicted in each phase.

TABLE 3: QUEUEING ANALYSIS - SIMPLE CASE

| Phase | Vehicle <br> Arrival Rate <br> (vehicles per <br> minute) | Vehicle <br> Service Rate <br> (vehicles per <br> minute) | Duration | Estimated <br> Vehicles in <br> Kiss and Drop <br> Spaces | Estimated <br> Queued <br> Vehicles |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Development Stage 1 (210 Children) |  |  |  |  |  |
| Prior to Pick <br> Up | 2.35 | 0 | 15 Minutes | 30 | 5 |
| During Pick <br> Up | 2.35 | 7.5 | 45 Minutes | 3 | 0 |
|  | Final Development Stage (630 Children) |  |  |  |  |
| Prior to Pick <br> Up | 4.53 | 0 | 15 Minutes | 30 | 36 |
| During Pick <br> Up | 4.53 | 7.5 | 45 Minutes | 7 | 0 |

The results in Table 3 indicate that the proposed design will completely contain the parking demands of the development but do not provide an assessment of the interaction between the two phases. An Aimsun microsimulation model has been used to simulate the operation of this kiss and drop system, resulting in a maximum queue of 35 vehicles for the final stage of development, all of which can be accommodated within the site.

The design of the kiss and drop facilities is therefore sufficient to completely accommodate the demands of the final 630 student population of the school. In the experience of McLaren Traffic Engineering it is extremely unusual for a primary school to be provided with a kiss and drop facility of this capacity and this should be considered favourably during the assessment of the development on the whole.

### 3.3 Management of Kiss and Drop Operations

To ensure that the proposed kiss and drop facilities operate with high levels of both efficiency and safety, some management practices will be implemented, including:

- Traffic control by school staff at internal pedestrian crossing locations;
- Traffic control by school staff to direct queued vehicles into vacant kiss and drop spaces;
- Organisation of students into general kiss and drop areas by year-group to speed pick-up operations;
- Assistance of school staff to load vehicles with children and bags.


### 3.4 Bicycle \& Motorcycle Parking Requirements

The Fairfield City Council DCP does not provide a rate for the provision of bicycle storage facilities, stating the following:

To encourage the use of bicycles, new developments should incorporate appropriate bicycle parking/storage facilities.

Bicycle racks can be placed around the perimeter of a building in areas where they will not act as obstructions. Bicycle parking is often in high demand at educational or recreation facilities, corner shops and civic buildings

The New South Wales Educational Facilities Standards and Guidelines (EFSG) provide rates of suggested bicycle storage provision for Primary Schools, as shown in Figure 5.

| School size - Core (No. Home Bases) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Room | Room | Measur | Sq |  |  |  |  |  |  |  |
| ID | name | asure | M | $1$ (1) | $\underline{3}$ <br> (2-4) | $\begin{aligned} & 7 \\ & (5-10) \end{aligned}$ | $14$ $(11-17)$ | 21 <br> (18-24) | $28$ <br> (25-30) | $\begin{aligned} & \frac{35}{(31-40)} \end{aligned}$ |
| PS609.41 | Bicycle <br> Storage <br> Area | No of Bicycle | - | - | - | 12 | 24 | 36 | - |  |

FIGURE 5: EFSG BICYCLE PARKING RECOMMENDATION

The proposed school will include some 630 students in 21 home bases when complete, corresponding to a bicycle storage provision of 36 spaces. Considering the lack of bicycle facilities surrounding the school and the considerable distance from the school to residential centres, there is likely to be a very low or no use of bicycles to travel to and from the site and the omission of bicycle storage from the site would be acceptable.

The Fairfield City Council DCP does not require that schools provide motorcycle parking spaces and the nil provision is considered to be acceptable. Any staff who travel to and from work using motorcycles can utilise the car parking spaces provided.

### 3.5 Servicing \& Loading

The Fairfield City Council DCP does not provide requirements for loading facilities for schools and the provision of on-site loading and servicing facilities has been based on the typical requirements of a Primary School. Appropriate access and loading facilities are proposed for vehicles up to a 12.5 m length Heavy Rigid Vehicle, such that a large vehicle can undertake deliveries to the school. The access from Kosovich Place will also connect to an emergency access path through the school to outdoor play areas for ambulance use if required. A dedicated Emergency Vehicle parking space has also been provided. Swept path testing has been undertaken to demonstrate that the design can accommodate the forward entry and exit of a Heavy Rigid Vehicle and is provided in Annexure E.

Garbage collection will occur within the site outside of peak school hours, usually once or twice per week.

### 3.6 Disabled Parking

The Building Code of Australia (BCA) classifies the assembly hall of a school as a 9b building and provides the following disabled parking requirement:

Class 9b
an assembly building, including a trade workshop, laboratory or the like in a primary or secondary school, but excluding any other parts of the building that are of another Class
(a) School 1 space for every 100 carparking spaces or part thereof.

The design proposes two (2) disabled parking spaces. This provision exceeds the single space required by the BCA.

### 3.7 Car Park Design \& Compliance

The car parking areas, both on and off-street, have been designed to meet or exceed the requirements of the relevant standards, being AS2890.1 and AS2890.6. The car parking design includes the following features:

- Minimum car parking aisle widths of 6.5 m ;
- Parallel kiss and drop spaces of 6.3 m length and 2.1 m width;
- $90^{\circ}$ car parking spaces for staff of 5.4 m length and 2.4 m width;
- Circulating aisles of minimum 6.5 m width and turning radii sufficient to satisfy the requirements of NSW Rural Fire Service’ Planning for Bushfire Protection document;
- Two-way, median separated driveway to Kosovich Place;
- Disabled $90^{\circ}$ parking spaces of minimum 5.4 m length and 2.4 m width, with appropriately dimensioned shared area to satisfy the objectives of AS2890.6;
- Compliant driveway and circulation roadway gradients throughout the site.


## 4 TRAFFIC ASSESSMENT

The impact of the expected traffic generation levels associated with the subject proposal is discussed in the following sub-sections.

### 4.1 Traffic Generation

Considering the location of the school and the poor access to public transport, it is assumed that all students and staff in Stage 1 will drive to and from school. Based on surveys of the associated St Hermizd Assyrian Primary School families in the community have 1.85 children on average, which can be conservatively assumed as the average vehicle occupancy.

In addition to the above assumptions, a conservative $80 \%$ student private vehicle use rate has been assumed for the completed school (at which time it is expected a bus service will be in operation). The resulting estimated AM and PM peak hourly traffic generations are provided in Table 4 and Table 5 respectively.

TABLE 4: ESTIMATED TRAFFIC GENERATION (AM)

| Type | Scale | Rate | Trips | Direction |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| STAGE 1 |  |  |  |  |  |  |
| Staff | 12 | 1 per staff | 12 | 12 IN, 0 OUT |  |  |
| Student | 210 | 0.54 two-way trips per student ${ }^{(1)}$ | 227 | 113 IN, 113 OUT |  |  |
| Total |  | FINAL DEVELOPMENT $^{\|c\|}$ |  |  |  |  |
| 125 IN, 113 OUT |  |  |  |  |  |  |
| Staff | 35 | 1 per staff | 35 | 35 IN, 0 OUT |  |  |
| Student | 630 | 0.43 two-way trips per student ${ }^{(2)}$ | 544 | 272 IN, 272 OUT |  |  |
| Total |  | $\mathbf{5 7 9}$ | $\mathbf{3 0 7}$ IN / 272 OUT |  |  |  |

Notes:
(1) Based on 1.85 children per vehicle;
(2) Based on 1.85 children per vehicle, and a $20 \%$ use of public transport.

TABLE 5: ESTIMATED TRAFFIC GENERATION (PM)

| Type | Scale | Rate | Trips | Direction |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| STAGE 1 |  |  |  |  |  |  |
| Staff | 12 | 1 per staff | 12 | 0 IN, 12 OUT |  |  |
| Student | 210 | 0.54 two-way trips per student ${ }^{(1)}$ | 227 | 113 IN, 113 OUT |  |  |
| Total |  | FINAL DEVELOPMENT |  |  |  |  |
|  |  |  |  |  |  |  |
| Staff | 35 | 1 per staff | 35 | 0 IN, 35 OUT |  |  |
| Student | 630 | 0.53 two-way trips per student ${ }^{(2)}$ | 544 | 272 IN, 272 OUT |  |  |
| Total |  | 579 | $\mathbf{2 7 2}$ IN / 307 OUT |  |  |  |

Notes:
(1) Based on 1.85 children per vehicle;
(2) Based on 1.85 children per vehicle, and a $20 \%$ use of public transport.

As shown, the traffic generation has been estimated at some 239 trips for Stage 1 and 579 trips for the final development scale. The AM peak hour has, for the purposes of traffic modelling, been assumed to be similar to the PM with the direction of staff travel reversed. The PM peak is a worst case as students will typically arrive for school over a longer period of time than when departing in the afternoon.

### 4.2 Traffic Assignment

The surrounding road network, the routes to and from the site, school catchment areas (reproduced in Annexure F) and Journey to Work data as provided by the NSW Bureau of Transport Statistics have been examined and the following trip assignment assumed:

### 4.2.1 AM Traffic to the Site

- $30 \%$ from the north via The Horsley Drive:
- $20 \%$ from the east;
- $10 \%$ from the west.
- $70 \%$ from the south via Elizabeth Drive:
- $50 \%$ from the east;
- $10 \%$ from the west;
- $10 \%$ from the south (via the M7 exit).


### 4.2.2 AM Traffic from the Site

- $40 \%$ to the north:
- $35 \%$ to the east at The Horsley Drive;
- $5 \%$ to the west at The Horsley Drive.
- $60 \%$ to the south
- $55 \%$ to the east at Elizabeth Drive;
- $5 \%$ to the west at Elizabeth Drive.

The above distribution is reversed in the PM when parents will typically be returning from their place of work to collect their child and then driving home.

### 4.3 Traffic Impact

The traffic generation estimated previously in Section 4.1 has been distributed into the existing traffic volumes as per the traffic assignment provided in Section 4.2 and assessed using SIDRA Intersection 7.0. The results of this assessment are summarised in the subsections below.

### 4.3.1 Stage 1 Development - School for 210 Students

The impacts of Stage 1 of the development on the surrounding road network have been assessed using the existing traffic volumes. The results of the SIDRA Intersection analysis are summarised in Table 6.

TABLE 6: INTERSECTION PERFORMANCES (SIDRA INTERSECTION 8) DEVELOPMENT STAGE 1

| Intersection | Peak Hour | Degree of Saturation ${ }^{(1)}$ | Average Delay ${ }^{(2)}$ (sec/veh) | Level of Service ${ }^{(3)}$ | Control Type | Worst Movement | 95th Percentile Queue |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| EXISTING VOLUMES |  |  |  |  |  |  |  |
| M7 Exit / <br> Elizabeth Drive | AM | 0.93 | 37.2 | C | Signals | RT from Wallgrove Road (N) | $\begin{aligned} & \hline 33.2 \text { veh }(248.2 \mathrm{~m}) \\ & \text { Elizabeth Drive (W) } \\ & \hline \end{aligned}$ |
|  | PM | 0.90 | 46.9 | D |  | LT from M7 Exit (S) | $\begin{aligned} & \hline 34.2 \text { veh ( } 259.7 \mathrm{~m} \text { ) } \\ & \text { Elizabeth Drive (W) } \end{aligned}$ |
| Wallgrove Road / The Horsely Drive | AM | 0.80 | 40 | C | Signals | LT from The Horsely Drive (W) | $\begin{gathered} 18.7 \text { veh (139m) } \\ \text { Wallgrove Road (S) } \end{gathered}$ |
|  | PM | 0.82 | 36.2 | C |  | LT from The Horsely Drive (E) | $\begin{gathered} 21.9 \text { veh (160.9m) } \\ \text { Wallgrove Road (N) } \end{gathered}$ |
| Wallgrove Road / Kosovich Place | AM | 0.49 | 0.1 <br> (Worst: 17.3) | NA <br> (Worst: B) | Give Way | RT from Kosovich Place (E) | 0 veh ( 0.2 m ) <br> Wallgrove Road (S) |
|  | PM | 0.51 | 0.1 <br> (Worst: 19.4) | NA <br> (Worst: B) |  | RT from Kosovich Place (E) | 0 veh (0.3m) <br> Wallgrove Road (S) |
| Wallgrove Road / Villiers Road | AM | 0.54 | 4.1 (Worst: 10.8 ) | A (Worst: A) | Roundabout | UT from Wallgrove Road (S) | $\begin{gathered} 1.1 \text { veh (8.5m) } \\ \text { Wallgrove Road (N) } \end{gathered}$ |
|  | PM | 0.56 | 4.2 (Worst: 10.8) | A (Worst: A) |  | UT from Wallgrove Road (S) | 4.9 veh (36.1m) <br> Wallgrove Road (N) |
| EXISTING VOLUMES + STAGE 1 GENERATION |  |  |  |  |  |  |  |
| M7 Exit / <br> Elizabeth Drive | AM | 0.99 | 40.7 | C | Signals | LT from M7 Exit (S) | $\begin{aligned} & 36.7 \text { veh }(274.6 \mathrm{~m}) \\ & \text { Elizabeth Drive }(\mathrm{W}) \\ & \hline \end{aligned}$ |
|  | PM | 0.98 | 55.3 | D |  | LT from M7 Exit (S) | $\begin{gathered} \hline 38.2 \text { veh (276.9m) } \\ \text { Wallgrove Road (N) } \end{gathered}$ |
| Wallgrove Road / The Horsley Drive | AM | 0.80 | 39.2 | C | Signals | LT from The Horsley Drive (W) | 18.7 veh (139m) <br> Wallgrove Road (S) |
|  | PM | 0.91 | 36.3 | C |  | LT from The Horsley Drive (E) | $\begin{gathered} 25.4 \text { veh (196m) } \\ \text { Wallgrove Road (N) } \end{gathered}$ |
| Wallgrove Road / Kosovich Place | AM | 0.55 | 1.9 <br> (Worst: 13.6) | NA <br> (Worst: A) | Give Way | RT from Wallgrove Road (N) | $1.1 \text { veh (7.6m) }$ <br> Kosovich Place (E) |
|  | PM | 0.57 | 1.1 <br> (Worst: 7.2) | NA (Worst: A) |  | RT from Wallgrove Road (N) | 0.5 veh (3.8m) <br> Kosovich Place (E) |
| Wallgrove Road / Villiers Road | AM | 0.62 | $4.7$ <br> (Worst: 10.8) | A <br> (Worst: A) | Roundabout | UT from Wallgrove Road (S) | 2 veh (15.4m) <br> Wallgrove Road (N) |
|  | PM | 0.77 | 5.5 (Worst: 10.8) | A (Worst: A) |  | UT from Wallgrove Road (S) | 9.7 veh (72.3m) <br> Wallgrove Road (N) |

NOTES:
(1) Degree of Saturation is the ratio of demand to capacity for the most disadvantaged movement.
(2) The average delay is the delay experienced on average by all vehicles. The value in brackets represents the delay to the most disadvantaged movement.
(3) The level of Service is a qualitative measure of performance describing operational conditions. There are six levels of service, designated from A to F, with A representing the best operational condition and level of service F the worst. The LoS of the intersection is shown in bold, and the LoS of the most disadvantaged movement is shown in brackets.

As shown, there is a minor increase to approach delays at each of the intersections modelled, but no change in Level of Service (LoS) is predicted as a result of the traffic generation of Stage 1 of development.

It should be noted that this modelling has been completed with the assumption of a "No Right Turn" restriction at the intersection of Kosovich Place/Wallgrove Road, as is discussed in Section 5 of this report.

### 4.3.2 Final Development - Completed School for 630 Students

The impacts of the final stage of development on the surrounding road network have been assessed using 10-year projected traffic volumes. The growth on each of the roads and intersections surrounding the site were provided by the Roads and Maritime Services and were used to scale the existing traffic volumes to reflect the predicted volumes for 2028. For the purposes of the 2028 modelling the upgraded layout of the intersection of the Horsley Drive/Wallgrove Road has been used for both the 2028 and 2028 plus development scenarios. The results of this modelling are summarised in Table 7.

As shown, the traffic associated with the proposed school will not substantially change the operation of the intersections surrounding the site and all intersections will remain at their present Level of Service other than the intersection of Elizabeth Drive/Wallgrove Road in the PM peak hour, which is predicted to operate with a Level of Service of E.

As discussed in Section 5 of this report, the modification of the intersection to include a high angle left turn slip lane would provide additional capacity at the intersection. Further analysis of the PM peak hour traffic has been undertaken to examine the impact of the addition of a left turn slip lane on the performance of the intersection. The results of this analysis are summarised in Table 8.

As shown, with the addition of a left turn slip lane on the northern approach to the intersection, the Level of Service of the intersection will be $D$ in both peak hours, a decrease in average delays when compared to the predicted operation of the intersection in 2028 (without the proposed school).

Based on the data received to date from the RMS, it is therefore suggested that such an upgrade should be performed to the intersection prior to the opening of the completed school. However, analysis should be undertaken with the latest traffic volumes and projections nearer to the time of construction of the final stage of the school to confirm that such an upgrade is necessary, as there may be significant reductions in the traffic using the Elizabeth Drive/Wallgrove Road intersection after the construction of the M12 Motorway.

TABLE 7: INTERSECTION PERFORMANCES (SIDRA INTERSECTION 8) FINAL DEVELOPMENT

| Intersection | Peak Hour | Degree of Saturation ${ }^{(1)}$ | Average Delay ${ }^{(2)}$ (sec/veh) | Level of Service ${ }^{(3)}$ |  | Control Type | Worst Movement | 95th Percentile Queue |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| EXISTING PERFORMANCE + 10 YEARS GROWTH |  |  |  |  |  |  |  |  |
| M7 Exit / Elizabeth Drive |  | AM | 0.91 | 32.9 | C | Signals | LT from M7 Exit (S) | 37.3 veh (278.9m) <br> Elizabeth Drive (W) |
|  |  | PM | 1.00 | 60.4 | E |  | LT from M7 <br> Exit (S) | 55.2 veh (419.7m) <br> Elizabeth Drive (W) |
| Wallgrove Road / The Horsley Drive |  | AM | 0.81 | 38.6 | C | Signals | LT from The Horsley Drive (W) | 19.1 veh (141.4m) <br> Wallgrove Road (S) |
|  |  | PM | 1.00 | 46 | D |  | T from The Horsley Drive (E) | 32.5 veh (251m) <br> The Horsley Drive (E) |
| Wallgrove Road / Kosovich Place |  | AM | 0.48 | $0.1$ <br> (Worst: 17.2) | NA <br> (Worst: B) | Give Way | RT from Kosovich Place (E) | 0 veh ( 0.2 m ) <br> Wallgrove Road (S) |
|  |  | PM | 0.52 | $0.1$ <br> (Worst: 20.6) | NA <br> (Worst: <br> B) |  | RT from Kosovich Place (E) | 0 veh ( 0.3 m ) <br> Wallgrove Road (S) |
| Wallgrove Road / Villiers Road |  | AM | 0.53 | 4.1 (Worst: 10.8) | A <br> (Worst: <br> A) | Roundabout | UT from <br> Wallgrove <br> Road (S) | 1.1 veh (8.5m) Wallgrove Road (N) |
|  |  | PM | 0.57 | 4.2 (Worst: 10.8) | A <br> (Worst: <br> A) |  | UT from Wallgrove Road (S) | 5.1 veh (37.6m) <br> Wallgrove Road (N) |
| EXISTING VOLUMES + 10 YEARS GROWTH + FINAL DEVELOPMENT GENERATION |  |  |  |  |  |  |  |  |
| M7 Exit / Elizabeth Drive |  | AM | 1.00 | 48.7 | D | Signals | T from Elizabeth Drive (W) | 56.8 veh (425.2m) <br> Elizabeth Drive (W) |
|  |  | PM | 1.10 | 99.3 | F |  | $\begin{aligned} & \text { LT from M7 } \\ & \text { Exit (S) } \end{aligned}$ | 84.4 veh (611.4m) <br> Wallgrove Road (N) |
| Wallgrove Road / The Horsley Drive |  | AM | 0.77 | 37.6 | C | Signals | T from Wallgrove Road (N) | $15.8 \text { veh (117m) }$ <br> Wallgrove Road (S) |
|  |  | PM | 1.00 | 45.6 | D |  | T from The Horsley Drive (E) | 32.5 veh ( 251 m ) <br> The Horsley Drive (E) |
| Wallgrove Road / Kosovich Place |  | AM | 0.60 | $\begin{gathered} 3.4 \\ \text { (Worst: } \\ 17.5 \text { ) } \\ \hline \end{gathered}$ | NA (Worst: B) | Give Way | RT from Wallgrove Road (N) | 2.7 veh (18.8m) <br> Kosovich Place (E) |
|  |  | PM | 0.64 | 1.8 <br> (Worst: <br> 7.9) | NA <br> (Worst: <br> A) |  | RT from Wallgrove Road (N) | 1.2 veh ( 8.5 m ) <br> Kosovich Place (E) |
| Wallgrove Road / Villiers Road |  | AM | 0.67 | 5.1 <br> (Worst: <br> 10.7 ) <br> 10.4 |  | Roundabout | UT from Wallgrove Road (S) | 2.8 veh (21.3m) <br> Wallgrove Road (N) |
|  |  | PM | 0.91 | $\begin{gathered} \hline 10.4 \\ \text { (Worst: } \\ 12.9 \text { ) } \end{gathered}$ | A <br> (Worst: <br> A) |  | T from Wallgrove Road (N) | 22.9 veh (160.3m) <br> Wallgrove Road (N) |

## NOTES:

(1) Degree of Saturation is the ratio of demand to capacity for the most disadvantaged movement.
(2) The average delay is the delay experienced on average by all vehicles. The value in brackets represents the delay to the most disadvantaged movement.
(3) The level of Service is a qualitative measure of performance describing operational conditions. There are six levels of service, designated from $A$ to $F$, with A representing the best operational condition and level of service F the worst. The LoS of the intersection is shown in bold, and the LoS of the most disadvantaged movement is shown in brackets.

TABLE 8: INTERSECTION PERFORMANCES (SIDRA INTERSECTION 8)
FINAL DEVELOPMENT W/ LEFT SLIP LANE

| Intersection | Peak Hour | Degree of Saturation ${ }^{(1)}$ | Average Delay ${ }^{(2)}$ <br> (sec/veh) | Level of Service ${ }^{(3)}$ | Control Type | Worst Movement | 95th Percentile Queue |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| EXISTING PERFORMANCE + 10 YEARS GROWTH |  |  |  |  |  |  |  |
| M7 Exit / Elizabeth Drive | AM | 1.05 | 43.4 | D | Signals | RT from <br> Wallgrove <br> Road (N) | 44.9 veh (336.1m) <br> Elizabeth Drive (W) |
|  | PM | 0.96 | 47.3 | D |  | $\begin{gathered} \text { LT from M7 } \\ \text { Exit (S) } \end{gathered}$ | $52.3 \text { veh (378.8m) }$ <br> Wallgrove Road (N) |

## 5 PROPOSED INFRASTRUCTURE WORKS

The provide suitable facilities and capacity within the road network, a number of improvements are proposed. Each proposed improvement is outlined below and illustrated in Annexure G for reference.

### 5.1 Road Width

The 6.5 m width of Kosovich Place is insufficient to accommodate the standing of buses and two-way passing of traffic. The implementation of a bus zone should be accompanied by the widening of Kosovich Place to 7.0 m width from the intersection of Wallgrove Road to the boundary of the site and 10 m from the driveway to the termination of the street. This road widening will enable bus access and provide sufficient width for up to four buses to pick up or drop off passengers without interrupting traffic flow along the street. It has been advised by the bus operator, Transit Systems, that the existing turning bulb is sufficient to facilitate U-turns by buses.

### 5.2 Pedestrian Facilities

Pedestrian footpaths will be constructed along the frontage of the site to Kosovich Place to provide safe passage for pedestrians to and from the bus zone. Considering that all parent kiss and drop operations will be undertaken on-site, no formal footpath is necessary other than along the frontage of the site.

### 5.3 Parking Restrictions

The following parking restrictions should be implemented to ensure parking does not occur in locations that will compromise traffic flow:

- "Bus Zone" signage, which acts as a "No Stopping" restriction with buses excluded;
- "No Stopping" signage around the circumference of the turning bulb;
- "No Stopping - 8:00 AM - 9:30 AM \& 2:30 PM - 4:00 PM" signage is proposed along the southern side of Kosovich Place to ensure that two-way passing will be maintained at all school drop-off and pick-up times.


### 5.4 Intersection Works

### 5.4.1 Kosovich Place/Wallgrove Road

Whilst the traffic modelling completed does not indicate that the intersection of Kosovich Place/Wallgrove Road will be pushed to capacity by the traffic associated with the site, the Austroads Guide to Road Design suggests that a CHR treatment is appropriate for an intersection with the traffic volumes that are proposed. Consequently, it is proposed that the intersection be adjusted to include a CHR treatment. The traffic modelling outlined in Section 4 of this report demonstrates that the intersection will perform satisfactorily with the proposed layout.

### 5.4.2 Wallgrove Road/Elizabeth Drive

The traffic modelling indicates that the completed school may cause a significant increase in delays at the intersection of Wallgrove Road/Elizabeth Drive, depending on the future traffic flows along Elizabeth Drive and Wallgrove Road. To relieve these delays, a high-angle slip lane could be added to the northern approach of the intersection. The necessity of this treatment should be confirmed prior to the issue of a construction certificate for the final stage of the school, as it is expected that the traffic projections will change between the submission of the State Significant Development Application and the construction of the final stage of the school. The traffic modelling outlined in Section 4 of this report demonstrates that the intersection will perform satisfactorily with the proposed layout.

## 6 SEARS

The Secretary's Environmental Assessment Requirements (SEARs) relevant to this traffic and parking impact assessment are reproduced in italics in the following sub-sections and responded to thereafter.

## 6. Transport and Accessibility (Construction and Operation)

Include a transport and accessibility impact assessment, which details, but not limited to the following:

### 6.1 Existing Vehicle Movements

accurate details of the current daily and peak hour vehicle, public transport, pedestrian and cycle movement and existing traffic and transport facilities provided on the road network located adjacent to the proposed development;

Please refer to Annexure B which provides an outline of the existing vehicle movements in the surrounds of the site. No existing public transport routes exist, there are no pedestrian paths along either Wallgrove Road or Kosovich Place and there are no notable cycling routes in the surrounds of the site.

### 6.2 Existing and Future Public Transport Networks

an assessment of the operation of existing and future transport networks including public transport networks, and their ability to accommodate the forecast number of trips to and from the development;

Transport for New South Wales (TFNSW) was consulted as part of this proposal and it was indicated that there are no current or future public transport routes within safe walking distance of the site. Transit Systems, the local bus operator, is in the process of consulting with TFNSW to provide school buses for the site.

### 6.3 Traffic Generation

details of estimated total daily and peak hour trips generated by the proposal, including vehicle, public transport, pedestrian and bicycle trips based on surveys of the existing and similar schools within the local area;

The traffic generation of the site has been estimated in Section 4.1 of this report. Considering the isolation of the school, the traffic generation has been based on a first principles assessment rather than surveys of other schools. The site is not expected to generate any pedestrian or cycling trips due to the lack of facilities for each of these travel modes and the young age of primary school children.

### 6.4 Adequacy of Existing Alternative Transport Facilities

the adequacy of public transport, pedestrian and bicycle networks and associated infrastructure to meet the likely future demand of the proposed development;

## See Sections 6.1, 6.2 \& 6.3.

### 6.5 Impact of Proposed Development

the impact of the proposed development on existing and future public transport infrastructure within the vicinity of the site in consultation with Council, Roads and Maritime Services and Transport for NSW and identify measures to integrate the development with the transport network;

The impacts of the site have been assessed using SIDRA Intersection, with the results provided in Section 4.3 of this report. Several infrastructure works are proposed as outlined in Section 5 of this report.

### 6.6 Infrastructure Works

the identification of infrastructure required to ameliorate any impacts on traffic efficiency and road safety impacts associated with the proposed development, including details on improvements required to affected intersections;

Several infrastructure works are proposed as outlined in Section 5 of this report.

### 6.7 Travel Demand Management

details of travel demand management measures to minimise the impact on general traffic and bus operations, including details of a location-specific sustainable travel plan and the provision of facilities to increase the non-car mode share for travel to and from the site;

The site is isolated from public transport, pedestrian and cycling networks. School buses are proposed for the site and are currently the subject of consultation between the local bus operator and TFNSW. To ameliorate impacts on the road network, it is proposed that school start and finish times be staggered to reduce the ultimate peak of kiss and drop traffic and parking demand. School management will propose and promote that parents arrange carshare pools in order to reduce the traffic and number of trips per week.

### 6.8 Traffic Impact Assessment

the impact of trips generated by the development on nearby intersections, (including but not limited to the intersection of Wallgrove Road with Kosovich Place), with consideration of the cumulative impacts from other approved developments in the vicinity;

The impacts of the site have been assessed using SIDRA Intersection, with the results provided in Section 4.3 of this report.

### 6.9 Funding of Road Improvements

details of any need/associated funding for, upgrades or road improvement works, if required;

Funding of the proposed improvement works is yet to be determined.

### 6.10 Traffic Modelling

Traffic modelling is to be undertaken using SIDRA network modelling for current and future years;

Traffic modelling has been undertaking using SIDRA for the existing and future cases, with 10-year future traffic growth provided by the RMS.

### 6.11 Walking, Cycling and Public Transport Access

the proposed walking and cycling access arrangements and connections to public transport services;

See Sections 6.1, 6.2 \& 6.3.

### 6.12 Proposed School Bus Routes

details of any proposed school bus routes along bus capable roads (i.e. travel lanes of 3.5 m minimum) and infrastructure (bus stops, bus layovers etc.);

School bus routes are currently in development by the local bus operator, Transit Systems.

### 6.13 Access Arrangements

the proposed access arrangements, including car and bus pick-up/drop-off facilities, and measures to mitigate any associated traffic impacts and impacts on public transport, pedestrian and bicycle networks, including pedestrian crossings and refuges and speed control devices and zones;

All kiss and drop operations will be provided for on-site, with internal traffic management and pedestrian crossing arrangements facilitating efficient and safe drop-off and pick-up of children. Buses will collect students from the site's frontage to Kosovich Place, where a footpath will be provided.

### 6.14 Kiss and Drop Operations

details of any traffic management measures to ensure the safe and efficient operation of student pick-up/drop-off;

Kiss and drop operations will occur on both sides of the proposed circulating roadway, with footpaths proposed on both sides. Two pedestrian crossings are proposed and will be controlled by school staff to facilitate the safe crossing of the internal road during kiss and drop hours.

### 6.15 CPTED

measures to maintain road and personal safety in line with CPTED principles;

All vehicular and pedestrian facilities associated with the site are designed both to meet the relevant Australian Standards and in response to the context and nature of the proposed school. In particular:

- Clear sight lines have been considered in the design of all driveways and pedestrian crossing locations, including the height of proposed landscaping;
- All vehicular and pedestrian facilities will be clearly signposted and linemarked;
- Pedestrian crossings and traffic control staff will be implemented to increase the safety of the proposed kiss and drop zone for pedestrians.


### 6.16 Parking and End of Trip Facilities

the proposed car and bicycle parking provision, including end of trip facilities, which must be taken into consideration of the availability of public transport and the requirements of Council's relevant parking codes and Australian Standards;

37 parking spaces are provided for staff, two spaces are provided for disabled staff and/or visitors and 30 spaces provided for parent drop-off and pick-up. No bicycle facilities are proposed as there are no safe cycling routes to and from the site. Refer to Section 3 of this report for analysis of the parking proposed.

### 6.17 Bicycle Parking and Facilities

proposed bicycle parking provision, including end of trip facilities, in secure, convenient, accessible areas close to main entries incorporating lighting and passive surveillance;

No bicycle facilities are proposed as there are no safe cycling routes to and from the site.

### 6.18 Proposed Car Parking

proposed number of on-site car parking spaces for teaching staff and visitors and corresponding compliance with existing parking codes and justification for the level of car parking provided on-site;

37 parking spaces are provided for staff, two spaces are provided for disabled staff and/or visitors and 30 spaces provided for parent drop-off and pick-up. The proposed provision of parking meets the requirements of the Council. No bicycle facilities are proposed as there are no safe cycling routes to and from the site. Refer to Section 3 of this report for analysis of the parking proposed.

### 6.19 On-Street Parking Impact

an assessment of the cumulative on-street parking impacts of cars and bus pick-up/drop-off, staff parking and any other parking demands associated with the existing and proposed development;

Sufficient car parking and queueing areas are proposed to accommodate all private vehicle operations on the site. A queueing assessment has been undertaken to confirm this, with the results provided in Section 3.2 of this report.

### 6.20 Emergency Vehicle Access

details of emergency vehicle access arrangements;
Emergency vehicles are able to access the site via the main driveway, with sufficient driveway width provided to meet the requirements of the Rural Fire Service, who operate the largest vehicles of any of the local emergency services. Access for emergency vehicles is also provided from the car park directly onto the hard-paved Civic Heart as well as down to the flood plain area.

### 6.21 Road and Pedestrian Safety Assessment

an assessment of road and pedestrian safety adjacent to the proposed development and the details of required road safety measures;

The proposed school is well self-contained and the design effectively separates the movements of vehicles and pedestrians along Kosovich Place. The design includes the following measures:

- An indented bus bay with sufficient length to contain up to four buses. Light vehicles are able to enter and depart the site without conflicting with queued or manoeuvring buses.
- A two-way driveway, with a median separating entering and exiting traffic;
- Pedestrian pathway connecting directly to the footpath adjacent to the indented bus bay area.

Considering the relative isolation of the site and the inclusion of sufficient parking on the site to contain all kiss and drop operations, any pedestrians exiting the site on foot are unlikely to walk along Kosovich Place or cross the path of any vehicles entering or leaving the site.

In view of the foregoing, the design passively ensures the safety of both drivers and pedestrians and no road safety measures are necessary. It is noted that a $40 \mathrm{~km} / \mathrm{h}$ school zone speed restriction will be implemented along Kosovich Place during peak school dropoff and pick-up times which will also act to improve vehicular and pedestrian safety.

### 6.22 Service Vehicle Operations

service vehicle access, delivery and loading arrangements and estimated service vehicle movements (including vehicle type and the likely arrival and departure times);

An assessment of service vehicle operations is provided in Section 3.5 of this report.

### 6.23 Construction Traffic Impacts and Management

in relation to construction traffic:

- assessment of cumulative impacts associated with other construction activities (if any);
- an assessment of road safety at key intersection and locations subject to heavy vehicle construction traffic movements and high pedestrian activity;
- details of construction program detailing the anticipated construction duration and highlighting significant and milestone stages and events during the construction process;
- details of anticipated peak hour and daily construction vehicle movements to and from the site;
- details of on-site car parking and access arrangements of construction vehicles, construction workers to and from the site, emergency vehicles and service vehicle;
- details of temporary cycling and pedestrian access during construction; and
- traffic and transport impacts during construction, including cumulative impacts associated with other construction activities, and how these impacts will be mitigated for any associated traffic, pedestrian, cyclists, parking and public transport, including the preparation of a draft Construction Traffic Management Plan in line with Council's Construction Management Plan Checklist to demonstrate the proposed management of the impact

A construction traffic management plan satisfying each of the above requirements has been completed and will be submitted separately with the SSDA submission.

## 7 CONCLUSION

The traffic and parking impacts of the proposed Saints Peter and Paul Primary School, which as shown in Annexure A, have been assessed. The proposed school will be completed in a number of stages which includes an initial student population of 210 students and a final population of 630 students.

The peak parent parking demand of the school has been estimated as some 65 vehicles, ascertained by the use of a microsimulation Aimsun model. Parent parking will be accommodated completely within the site, with no queueing of vehicles into Kosovich Place expected.

All 35 school staff will be provided with a dedicated parking space within the grounds of the school, satisfying the requirement of the Fairfield City Council Development Control Plan. A total of 39 angle parking spaces are provided within the site for staff and disabled visitors.

The traffic generation of the site, estimated at some 579 vehicles ( 272 IN / 307 OUT) in the PM peak period, has been assessed, with the following results:

- The intersection of Wallgrove Road and Kosovich Place is proposed to be upgraded to include an auxiliary right turn lane and a "No Right Turn" restriction from the Kosovich Place approach. These works will be completed prior to the opening of Stage 1 of the development.
- The intersection of Wallgrove Road / Elizabeth Drive is proposed to be upgraded with a left turn high angle slip lane. These works will be completed prior to the opening of the final stage of development, subject to modelling completed closer to the time which may demonstrate that the works are not needed.
- The intersection of Wallgrove Road/The Horseley Drive will not be noticeably impacted by the proposal either in its current or future layout (as shown on the most recently available RMS documentation).

In addition to upgrades of intersections, Kosovich Place will be upgraded to cater for bus traffic and a bus stop along the frontage of the site. The proposed infrastructure works are depicted in Annexure G for reference.

In view of the foregoing, the subject proposed development is fully supported in terms of its traffic and parking impacts.


ANNEXURE A: PROPOSED PLAN


CE B

 -as Masterplan


## ANNEXURE B: TURNING MOVEMENT COUNT RESULTS

 (6 SHEETS)TRANS TRAFFIC SURVEY = =an


| Period Starl | mereme | ${ }_{\text {North }}$ |  | con malaro | Tound |  | ${ }_{\text {a }}$ | Tin |  |  | Soult Aproae | Ner Wallar |  |  | ${ }_{\text {a }}$ |  |  |  | Peat |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7.00 | 7.15 | 0 | 6 | ${ }_{77}$ | 50 | 0 | 97 | ${ }^{24}$ | ${ }^{13}$ | 0 | $0{ }^{24}$ | 129 | ${ }_{7}$ | 0 |  | 41 | 10 | ${ }^{2051}$ |  |
| 7.15 | ${ }^{7} 38$ | 0 | 10 | 69 | ${ }_{5} 5$ | 0 | ${ }_{88}$ | ${ }^{24}$ | 6 |  | $0{ }^{25}$ | 165 | 3 | 0 | 4 | ${ }^{28}$ | 16 | 2157 |  |
| 7:30 | ${ }_{7} 7.45$ | 0 | 12 | 51 | ${ }^{61}$ | 0 | ${ }^{105}$ | ${ }^{32}$ | 5 |  | $0{ }^{33}$ | ${ }^{172}$ | 10 |  | 3 | ${ }^{36}$ | 12 | 2224 | Peak |
| ${ }^{7} 7.45$ | 800 | 0 | 8 | ${ }_{56}$ | 60 | 0 | ${ }_{88}$ | ${ }^{39}$ | 5 |  | $0 \quad 37$ | 169 | 7 | 0 | 3 | 52 | 14 | 2186 |  |
| 8.00 | $8: 15$ | $\bigcirc$ | ${ }^{13}$ | 62 | 52 | $\bigcirc$ | 114 | ${ }_{59}$ | 6 |  | $0{ }^{26}$ | ${ }^{156}$ | 13 | 0 | 10 | ${ }_{65}$ | ${ }^{14}$ | 2182 |  |
| 8.15 | 830 | 0 | 8 | ${ }_{56}$ | 69 | 0 | ${ }^{97}$ | 59 | 9 |  | $0 \quad 36$ | ${ }^{116}$ | ${ }^{20}$ | 0 |  | 79 | 9 | 2019 |  |
| 8.30 | 8.45 | 0 | 8 | 51 | 47 | 0 | ${ }_{9}$ | 54 | 8 |  | $0{ }^{18}$ | 120 | , | 0 | 8 | ${ }^{45}$ | ${ }^{20}$ | 1836 |  |
| 8.45 | 9.00 | 0 | 10 | 65 | ${ }_{58}$ | 0 | ${ }^{83}$ | 50 | 7 |  | $0{ }^{24}$ | ${ }^{122}$ | ${ }^{23}$ | 0 | ${ }^{21}$ | ${ }_{56}$ | ${ }_{15}$ |  |  |
| 9.00 | 9.15 | 0 | 18 | 45 | ${ }_{58}$ | 0 | ${ }^{73}$ | ${ }^{31}$ | 9 |  | $0 \quad 12$ | ${ }^{76}$ | ${ }^{18}$ | 0 | ${ }^{14}$ | 57 | ${ }^{16}$ |  |  |
| 9.15 | 930 | 0 | 10 | 42 | ${ }_{6}$ | 0 | ${ }^{62}$ | ${ }^{23}$ | 7 |  | $0{ }^{18}$ | ${ }^{75}$ | 9 | 0 | 8 | ${ }^{48}$ | ${ }^{13}$ |  |  |
| 14.00 | ${ }_{14,15}$ | 0 | 17 | 109 | 66 | 0 | ${ }^{67}$ | ${ }_{36}$ | 14 |  | $0 \quad 14$ | 57 | 4 | 0 | 6 | 22 | 7 | 1845 |  |
| 14.45 | 14.30 | 0 | ${ }^{18}$ | 122 | ${ }^{25}$ | 0 | ${ }^{67}$ | ${ }^{38}$ | ${ }^{13}$ |  | $0 \quad 20$ | ${ }_{52}$ |  | 0 | 10 | ${ }^{33}$ | 10 | 1910 |  |
| 14.30 | 14.45 | 0 | 15 | 110 | ${ }_{8} 8$ | - | 69 | 70 | 12 |  | $0{ }^{12}$ | ${ }^{47}$ | 8 | 0 | ${ }^{11}$ | ${ }^{38}$ | 9 | 2030 |  |
| 14.45 | 15.00 | - | 16 | ${ }^{113}$ | 60 | 0 | 59 | 70 | ${ }^{20}$ |  | $0{ }^{21}$ | ${ }^{46}$ | 14 |  |  | ${ }_{35}$ | 4 | 2081 |  |
| 15.00 | 15.15 | 0 | ${ }^{20}$ | ${ }^{113}$ | 48 | 0 | ${ }_{88}$ | 44 | ${ }^{21}$ |  | $0 \quad 16$ | ${ }^{63}$ | ${ }^{20}$ | 0 | 5 | ${ }^{41}$ | 5 | 2260 |  |
| 15.15 | 1530 | 0 | ${ }^{21}$ | 171 | 99 | 0 | 80 | ${ }^{37}$ | 32 |  | $0{ }^{17}$ | ${ }^{45}$ | 3 | 0 | ${ }^{23}$ | ${ }_{54}$ | 10 | ${ }^{2403}$ |  |
| 15.30 | 15.45 | 0 | 17 | 127 | 94 | 0 |  | 46 | 25 |  | $\bigcirc{ }^{\circ}$ | 71 | 9 | 0 | 10 | 4 | 11 | 2476 |  |
| 15.45 | 16:00 | 0 | 20 | 182 | 110 | 0 | ${ }_{5}$ | ${ }_{58}$ | ${ }_{35}$ |  | $0{ }^{16}$ | ${ }^{67}$ | 10 | 0 | 9 | ${ }_{32}$ | 10 |  |  |
| 16:00 | 16.15 | 0 | ${ }^{23}$ | 177 | ${ }^{128}$ | 0 | ${ }_{88}$ | ${ }_{45}$ | ${ }_{3} 9$ |  | $0{ }^{14}$ | ${ }^{57}$ | , | 0 | 10 | ${ }^{26}$ |  |  |  |
| 16:15 | 1830 | 0 | 16 | 180 | 123 | 0 | 100 | 66 | ${ }^{26}$ |  | $0 \quad 19$ | 62 | 2 | 0 | 16 | 47 | 8 |  |  |
|  |  | doorn | $\frac{\text { mapproace }}{\frac{11}{4}}$ |  | $$ | $\begin{array}{\|l\|l\|} \hline \text { Esast } A \\ \hline 0 \\ \hline \end{array}$ |  |  | Siey or | $\begin{aligned} & \text { soa } \\ & \frac{\text { so }}{0} \\ & 0 \\ & 0 \end{aligned}$ |  | $\frac{\text { acon Wallgoven }}{4}$ | $\begin{gathered} \text { ove end } \\ 50 \\ 50 \end{gathered}$ |  | $\frac{s_{\text {Slaproaen }}^{2}}{22}$ |  |  |  |  |



| Llat Vencicies |  |  |  |  |  |  |  |  |  | South Approash W Waltrove Rd |  |  |  | West Approash Tre Hestasey or |  |  |  |  |
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| 7.00 | 7.15 | 0 | 2 | ${ }_{69}$ | 35 | 0 | $0{ }^{86}$ | 15 | , | 0 | ${ }^{23}$ | ${ }^{120}$ | 6 | 0 | 6 | 34 | 10 |  |
| 7715 | ${ }^{7} 30$ | 0 | 7 | 60 | 40 | - | 06 | ${ }^{21}$ | 4 | - | ${ }^{23}$ | 147 | 3 | 0 | ${ }^{3}$ | ${ }^{22}$ | ${ }^{14}$ |  |
| 7.30 | ${ }^{7} 4.4$ | 0 | 12 | 41 | ${ }^{48}$ | - | $0{ }^{86}$ | 25 | 4 | 0 | ${ }^{33}$ | ${ }_{163}$ | 1 | 0 | 2 | ${ }^{32}$ | 7 |  |
| 7.45 | 8.00 | 0 | 7 | 55 | 40 | 0 | $0{ }^{12}$ | 36 | 3 | 0 | ${ }^{34}$ | ${ }_{1} 15$ | 7 | 0 | 3 | ${ }_{4}$ | 12 |  |
| 8.00 | 8.15 | 0 | 12 | 53 | 39 |  | $0 \quad 97$ | 52 | 3 | $\bigcirc$ | ${ }^{24}$ | ${ }^{141}$ | 13 | 0 | ${ }^{8}$ | ${ }_{60}$ | ${ }^{13}$ |  |
| 8:15 | ${ }^{8,30}$ | 0 | 7 | 50 | 45 | 0 | 080 | 55 | 6 | 0 | ${ }^{30}$ | 105 | 20 | 0 | 5 | ${ }^{75}$ | - |  |
| 8.30 | 8.45 | 0 | 5 | ${ }^{43}$ | ${ }^{36}$ | 0 | 07 | 52 | 6 | 0 | 17 | ${ }^{108}$ | 19 | 0 | ${ }^{8}$ | ${ }^{43}$ | 17 |  |
| 845 | 9.00 | 0 |  | 49 | 36 | 0 | $0{ }^{59}$ | 45 | 6 | 0 | 22 | 110 | 22 | 0 | 16 | 52 | ${ }^{15}$ |  |
| 9.00 | $9: 15$ | 0 | 16 | ${ }^{38}$ | ${ }^{38}$ | 0 | $0{ }^{51}$ | 29 | 7 | 0 | 7 | 70 | 17 | 0 | 12 | ${ }_{5} 5$ | 14 |  |
| 9:15 | 930 | 0 | 8 | ${ }_{36}$ | 44 | 0 | $0{ }^{47}$ | 22 | 4 | 0 | 15 | ${ }^{67}$ | 8 | 0 | 7 | 4 | 11 |  |
| 1400 | 14.15 | 0 | 14 | 96 | 51 | 0 | $0{ }^{57}$ | 32 | 12 | 0 | ${ }^{13}$ | ${ }^{48}$ | 4 | 0 | 6 | 20 | 5 |  |
| 14.15 | $14: 30$ | 0 | 16 | ${ }^{112}$ | 73 | 0 | 047 | 31 | 13 | 0 | 17 | ${ }^{39}$ | 4 | 0 | 7 | ${ }^{32}$ | 9 |  |
| 14.30 | 14.45 | 0 | 14 | 94 | 68 | 0 | $0{ }^{55}$ | 65 | 10 | - | 10 | ${ }^{38}$ | 7 | 0 |  | ${ }^{37}$ | 9 |  |
| 14.45 | 15.00 | 0 | 14 | 107 | 50 | 0 | $0{ }^{48}$ | ${ }^{66}$ | 18 | 0 | 19 | ${ }_{35}$ | 13 | 0 | 7 | ${ }^{30}$ | 3 |  |
| 15.00 | $15: 15$ | 0 | 17 | 99 | ${ }^{34}$ | 0 | 066 | 40 | 18 | 0 | 16 | 59 | ${ }^{20}$ | 0 | 5 | 33 | 5 |  |
| 15.15 | 15.30 | 0 | 18 | 159 | ${ }^{84}$ | 0 | $0 \quad 65$ | 31 | ${ }^{29}$ | 0 | ${ }^{14}$ | ${ }^{37}$ | 3 | 0 | ${ }^{22}$ | ${ }_{53}$ | ${ }^{10}$ |  |
| 15.30 | 1545 | 0 | 17 | 122 | 79 | 0 | $0{ }^{73}$ | 42 | 22 | 0 | 8 | ${ }^{68}$ | 7 | 0 |  | ${ }^{34}$ | 9 |  |
| 1545 | 16:00 | 0 | 19 | 167 | 94 | 0 | 080 | 50 | ${ }^{35}$ | 0 | ${ }^{15}$ | ${ }^{60}$ | 10 | 0 | - | ${ }^{30}$ | 7 |  |
| 16.00 | $16: 15$ | 0 | ${ }^{20}$ | 162 | ${ }^{116}$ | 0 | $0{ }^{18}$ | ${ }^{38}$ | ${ }^{34}$ | 0 | ${ }^{12}$ | 51 | 7 | 0 | 10 | ${ }^{23}$ | ${ }^{13}$ |  |
| $16: 15$ | $18: 30$ | 0 | 13 | 175 | 97 | 0 | $0{ }^{92}$ | 59 | 24 | 0 | 15 | 57 | 2 | 0 | 15 | 44 | 8 |  |
|  |  | $\begin{aligned} & \text { Nooth } h \\ & \hline 0 \end{aligned}$ |  |  |  | $\begin{aligned} & \text { East } \\ & \hline 0 \\ & \hline \end{aligned}$ |  |  | $\begin{gathered} \text { osey or } \\ \hline 16 \end{gathered}$ | $\frac{\text { sout }}{\text { Sou }}$ |  |  | $\begin{gathered} \text { overad } \\ \hline \end{gathered}$ | $\begin{gathered} \text { wost } \\ 0 \\ 0 \end{gathered}$ |  | $\begin{aligned} & \hline \text { h The Hors } \\ & \hline \begin{array}{\|c\|} \hline \text { EB } \\ \hline 211 \\ \hline \end{array} \end{aligned}$ | risievor or | Peak <br> toaral |






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| $6: 41: 29$$6: 42.35$ | Red | ${ }_{66}$ | Red | ${ }^{66}$ |
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| 6,3829 <br> 68835 | Yelow | ${ }_{6}^{6}$ | ${ }^{\text {Red }}$ | ${ }^{6}$ |
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TRANS TRAFFIC SURVEY = =an








| ${ }^{\text {coplolss }}$ Trime | ${ }^{\text {eriod End }}$ |  | ${ }_{\text {aproa }}$ | Walgro |  | ${ }_{\text {East }}$ | ${ }^{\text {a }}$ | TheTosse <br> We |  | Sout | At Appraat | $\xrightarrow{\text { WWalligive }}$ |  | ${ }^{\text {Wsist }}$ | ${ }_{\text {aproab }}$ | ${ }_{\text {ct }}$ |  |
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| 7.00 | 7.15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| r:15 | ${ }^{7} 30$ | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 7.30 | 7.45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\bigcirc$ | 0 | 0 |
| 7.45 | 8.00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| 8.00 | $8: 15$ | 0 | 0 | 0 | $\bigcirc$ | 0 | 0 | - | $\bigcirc$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| $8: 15$ | 8.30 | 0 | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 830 | 8.45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 8.45 | 9.00 | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9.00 | 9,15 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\bigcirc$ | 0 | 0 | 0 |
| $9: 15$ | 9,30 | 0 | 0 |  | 0 |  |  |  | 0 | 0 |  |  |  |  |  |  | 0 |
| 14.00 | 14.15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\bigcirc$ | 0 | $\bigcirc$ | 0 | 0 |
| 14.15 | 14330 | 0 |  | - | 0 | 0 | - | 0 | $\bigcirc$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
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| 15.00 | 15.15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 |  | 0 |  | 0 | - |
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| 6,15 | 16.30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |



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|  |  | 50.423 |  |  |  |  |  |  |  |  |  7:00 AM-9:30 <br> 2:00 PM-4:30  <br> 7:30 AM-8:30  <br> 3:30 PM-4:30  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| All Vehicles |  |  |  |  |  |  | Approac |  | nor | Sout | Anpmoae | mwallaro |  | West | sapproa | ach Elizabe |  | Houry | Toal |
| ${ }^{\text {a }}$ | ${ }_{7} 715$ | 0 | ${ }^{28}$ | ${ }^{0}$ | ${ }_{41}$ | 0 | 151 | ${ }^{129}$ | $\bigcirc$ | 0 | $\stackrel{2}{2}$ | ${ }^{10}$ | ${ }^{28}$ | 0 | 0 | 164 | ${ }_{103}$ | ${ }_{281}$ |  |
| 7:15 | ${ }^{7} 30$ | 0 | 20 | 0 | ${ }_{4}$ | 0 | ${ }^{133}$ | ${ }^{118}$ | 0 | 0 | 1 | ${ }^{23}$ | ${ }^{30}$ | 0 | 0 | 214 | 99 | 3041 |  |
| ${ }^{7} 30$ | ${ }_{7} 7.45$ | 0 | ${ }_{18}$ | 0 | ${ }_{56}$ | 0 | ${ }^{126}$ | 142 | 0 | 0 | 3 | 14 | ${ }^{27}$ | 0 | 0 | 213 | 105 | 3101 | ${ }_{\text {Peak }}$ |
| ${ }_{7} 7.45$ | 8.00 | $\bigcirc$ | ${ }^{20}$ | $\bigcirc$ | ${ }_{3}^{33}$ | $\bigcirc$ | ${ }_{182}$ | ${ }^{180}$ | $\bigcirc$ | 。 | 2 | 10 | ${ }^{28}$ | 0 | 0 | 256 | 120 | 3101 | ${ }_{\text {Pakk }}$ |
| 8.00 | ${ }_{8} 815$ | 0 | 20 | 0 | ${ }^{37}$ | 0 | ${ }^{191}$ | 155 | 0 | 0 | 4 | ${ }^{14}$ | ${ }^{32}$ | 0 | 0 | 259 | 114 | ${ }^{299}$ |  |
| $8: 15$ | 8.30 | 0 | ${ }^{23}$ | 0 | ${ }_{68}$ | 0 | ${ }^{99}$ | 152 | $\bigcirc$ | 0 | 7 | ${ }^{8}$ | ${ }^{23}$ | 0 | $\bigcirc$ | 246 | 114 | 2653 |  |
| ${ }_{8} 83$ | ${ }_{84}{ }^{4}$ | $\bigcirc$ | 17 | 0 | ${ }_{4}^{4}$ | 0 | ${ }^{105}$ | ${ }^{185}$ | 0 | 0 | 6 | 9 | ${ }^{21}$ | 0 | 0 | 208 | 109 | ${ }_{242}$ |  |
| 8.45 | 9.00 | 0 | 17 | 0 | ${ }^{34}$ | 0 | ${ }^{118}$ | ${ }^{134}$ | 0 | 0 | 5 | 4 | ${ }^{31}$ | 0 | 1 | ${ }^{175}$ | 110 |  |  |
| 9.00 | 9.15 | 0 | 13 | 0 | ${ }^{43}$ | 0 | 117 | 122 | 0 | 0 | 7 | ${ }^{12}$ | ${ }^{32}$ | 0 | 0 | 168 | ${ }_{6}^{6}$ |  |  |
| $9: 15$ | 930 | 0 | 16 | 0 | ${ }_{55}$ | 0 | 100 | ${ }^{92}$ | 0 | 0 | 8 | 7 | ${ }^{29}$ | - | 0 | 143 | ${ }_{57}$ |  |  |
| 14.00 | 14.45 | 0 | ${ }_{36}$ | 0 | 59 | 0 | 59 | 9 | 0 | 0 | 6 | 7 | ${ }^{33}$ | 0 | 0 | 145 | ${ }_{4}$ | 2364 |  |
| 14.15 | 14.30 | 0 | ${ }_{38}$ | 0 | ${ }^{97}$ | 0 | ${ }_{68}$ | 157 | 0 | 0 | 5 | 7 | ${ }_{58}$ | 0 | 0 | 179 | 53 | 2566 |  |
| 14.30 | 14.45 | 0 | 49 | 0 | ${ }^{78}$ | 0 | ${ }^{67}$ | 124 | 0 | 0 | ${ }^{11}$ | ${ }^{11}$ | ${ }^{41}$ | 0 | 0 | 152 | ${ }^{47}$ | ${ }^{2636}$ |  |
| 14.45 | 15.00 | 0 | ${ }_{3} 5$ | 0 | ${ }^{91}$ | 0 | ${ }_{93}$ | ${ }^{147}$ | 0 | 0 | 7 | 7 | ${ }^{37}$ | 0 | 0 | 174 | ${ }^{45}$ | 2813 |  |
| 15.00 | 15.15 | 0 | 45 | 0 | ${ }_{98}$ | 0 | ${ }_{69}$ | 170 | 0 | 0 | 9 | 5 | 51 | 0 | 0 | 179 | 52 | ${ }^{2938}$ |  |
| 15.15 | 15.50 | 0 | ¢ | 0 | ${ }^{126}$ | 0 | ${ }^{80}$ | 187 | 0 | 0 | 8 | 5 | ${ }_{5} 5$ | 0 | 0 | ${ }_{173}$ | ${ }^{38}$ | 3045 |  |
| 15.30 | 15.45 | 0 | 51 | 0 | 107 | 0 | ${ }_{68}$ | 176 | 0 | 0 | 11 | 7 | ${ }_{41}$ | 0 | 0 | 253 | ${ }^{43}$ | ${ }^{3174}$ | Peak |
| 15.45 | 16:00 | 0 | ${ }_{64}$ | 0 | ${ }^{11}$ | 0 | ${ }^{89}$ | 201 | 0 | 0 | ${ }^{13}$ | 3 | ${ }^{30}$ | 0 | 0 | ${ }^{245}$ | ${ }_{50}$ |  |  |
| 16:00 | 16:15 | 0 | ${ }^{69}$ | 0 | ${ }_{153}$ | 0 | ${ }^{73}$ | 168 | 0 | 0 | 1 | 6 | ${ }^{33}$ | 0 | 0 | ${ }^{201}$ | ${ }^{36}$ |  |  |
| 18.15 | $18: 30$ | 0 | 79 | $\bigcirc$ | ${ }^{128}$ | 0 | 94 | 194 | 0 | 0 | 9 | 7 | 57 | 0 | 0 | 257 | 46 |  |  |









| Pearios Starl | Peoriod End |  | Approad | ${ }_{\text {We }}$ |  | ${ }_{\square}^{\text {East }}$ | Approach |  |  | ${ }_{\text {South }}$ | It Approaen | nwalgrove |  |  | ${ }_{\text {Staparach }}^{\text {Sta }}$ | h Ilzaean |  |
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| 7.00 | ${ }^{7} 715$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| r:15 | ${ }^{7} 38$ | 0 | $\bigcirc$ | - | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7.30 | 7.45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\bigcirc$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7.45 | 8.00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 |  | 0 | 0 |
| 8.00 | 8.15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| $8: 15$ | 8.30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 830 | 8.45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8.45 | 9.00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9.00 | ${ }^{9.15}$ | - | 0 | - | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
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| 14.00 | 14.15 | 0 | - | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\bigcirc$ | 0 | $\bigcirc$ | 0 | 0 |
| 14.15 | ${ }^{1430}$ | 0 | - | - | 0 | 0 | - | 0 | $\bigcirc$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| 14.30 | ${ }^{14.45}$ | 0 | 0 | 0 | 0 | 0 | - |  | 0 | $\bigcirc$ | 0 | 0 |  | 0 | 0 | 0 | 0 |
| 14.45 | 15.00 | 0 | - | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\bigcirc$ | $\bigcirc$ | 0 | 0 | 0 |
| 15.00 | 15.15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 |  | - |  | 0 | - |
| 15.15 | 15.30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15.30 | ${ }_{1545}$ | - | 0 | - | - | 0 | 0 | 0 | - | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| 15.45 | $18: 00$ | 0 | 0 | 0 | - | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 |  | 0 |
| 18,00 | 16:15 | 0 | - | 0 | - | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - | $\bigcirc$ | 0 |
| 6,15 | 16.30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |





Intersection of Kosovich pl and Wallgrove Rd, Cecil Parl





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| Time  <br> Period Start Period End <br> $7: 00$  |  | $\stackrel{\text { aren }}{ }$ |  | Ster |  |  |  | \% | $\square_{\text {a }}$ |  |
|  |  | 121 | 0 |  |  |  |  |  |
| 7:15 | 7,30 |  |  | 0 | - | ${ }^{73}$ | 0 | 163 | 0 | 0 | 0 |  |
| 7.30 | ${ }_{7} 7.45$ | 0 | 0 | ${ }^{69}$ | 0 | 170 | 0 | 0 | 0 | 0 |
| 7.45 | $8: 00$ | $\bigcirc$ | - | ${ }^{76}$ | 0 | 220 | 0 | $\bigcirc$ | 0 |  |
| 8.00 | $8: 15$ | 0 | - | ${ }_{6} 6$ | 0 | 215 | 0 | 0 | 1 | 0 |
| $8: 15$ | ${ }_{8} 80$ | 0 | 0 | 101 | 0 | 181 | 0 | 0 | 0 | 0 |
| 830 | ${ }_{845}$ | $\bigcirc$ | $\bigcirc$ | ${ }^{64}$ | 0 | 169 | 0 | $\bigcirc$ | 0 |  |
| ${ }^{845}$ | 9.00 | $\bigcirc$ | 1 | ${ }^{57}$ | 0 | 163 | 0 | $\bigcirc$ | 2 | 0 |
| 9.00 | $9: 15$ | 0 | 0 | 55 | 0 | 116 | 1 | 0 |  | 0 |
| 9:15 | 930 | $\bigcirc$ | $\bigcirc$ | 63 | $\bigcirc$ | 103 | 0 | $\bigcirc$ | 0 | $\bigcirc$ |
| 14.00 | 14.15 | 0 | 1 | 94 | 0 | 52 | 0 | 0 | 0 | 0 |
| 14.15 | 14.30 | 0 | 1 | 162 | 0 | 71 | 1 | - | 0 | 1 |
| 14.30 | 14.45 | 0 | $\bigcirc$ | ${ }^{128}$ | 0 | 75 | 0 | $\bigcirc$ | 1 | 0 |
| ${ }_{1}^{14,45}$ | 15:00 | 0 | 0 | 139 | 0 | ${ }^{89}$ | 1 | 0 | 1 | 0 |
| 15.00 | 15.15 | 0 | 0 | 169 | 0 | 58 | 2 | 0 | 1 |  |
| 1515 | ${ }_{1} 1530$ | 0 | - | 24 | 0 | 69 | 0 | 0 | 0 | 2 |
| 1530 | ${ }_{1545}$ | 0 | 0 | 166 | 0 | 94 | 2 | 0 | 0 |  |
| ${ }_{1545}$ | 16:00 | 0 | - | 195 | 0 | ${ }^{80}$ | 0 | 0 | 0 | 0 |
| 16:00 | 16:15 | 0 | 0 | 237 | 0 | ${ }^{73}$ | 0 | 0 | 0 |  |
| $16: 15$ | 16.30 | 0 | 1 | 261 | 0 | 79 | 1 | $\bigcirc$ | 0 |  |







| Period start | meriod End | ${ }^{\text {map }}$ | A |  |  |  |  | U | R |  |
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|  | $7: 15$ | 0 | 0 | 0 | 0 | $\bigcirc$ | $\bigcirc$ | - | $\bigcirc$ | 0 |
| 7:15 | 7:30 | 0 | $\bigcirc$ | 0 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | 0 | $\bigcirc$ |  |
| ${ }^{7} 30$ | ${ }^{7} 4.45$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | 0 | 0 | 0 | 0 | 0 |
| 7.45 | 8.00 | 0 | $\bigcirc$ | $\bigcirc$ | 0 | $\bigcirc$ | 0 | 0 | 0 |  |
| 8.00 | $8: 15$ | 0 | $\bigcirc$ | 0 | $\bigcirc$ | 0 | 0 | 0 | 0 |  |
| ${ }_{8,15}$ | ${ }_{8} 83$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| 830 | ${ }_{8,45}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| ${ }^{8,45}$ | 9.00 | 0 | $\bigcirc$ | 0 | 0 | 0 | $\bigcirc$ | $\bigcirc$ | 0 |  |
| 9.00 | $9: 15$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| $9: 15$ | ${ }_{9} 93$ | 0 | 0 | 0 | 0 | $\bigcirc$ | $\bigcirc$ | 0 | 0 | 0 |
| 14.00 | 14.15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| ${ }_{14,15}$ | 1430 | 0 | $\bigcirc$ | 0 | 0 | $\bigcirc$ | $\bigcirc$ | 0 | 0 |  |
| ${ }^{1430}$ | 14.45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 14.45 | 15.00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| 15.00 | 15.15 | 0 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| 15.15 | 15.30 | 0 | $\bigcirc$ | 0 | 0 | 0 | 0 | 0 | 0 |  |
| 15.30 | 1545 | - | $\bigcirc$ | 0 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| 15.45 | 16.00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| 18.00 | 16.15 | $\bigcirc$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
|  |  |  |  |  |  |  |  |  |  |  |




ANNEXURE C: RMS GROWTH RATES (2 SHEETS)




ANNEXURE D: SIDRA MOVEMENT SUMMARIES (94 SHEETS)

## SITE LAYOUT

## Site: 101 [PM Existing +10yr Gr + S2 Elizabeth Dr/ Wallgrove Rd]

Elizabeth Dr/ Wallgrove Rd
Site Category: (None)
Signals - Fixed Time Coordinated


## SITE LAYOUT

Site: 101 [AM Existing +10yr Gr + S2 Elizabeth Dr/ Wallgrove Rd - LT Slip]
Elizabeth Dr/ Wallgrove Rd
Site Category: (None)
Signals - Fixed Time Coordinated


## SITE LAYOUT

## Site: 101 [AM Existing+ 10yr Gr Wallgrove Rd/ The Horsley Drive]

New Site
Site Category: (None)
Signals - Fixed Time Coordinated


## SITE LAYOUT

Site: 101 [AM Existing+ 10yr Gr Wallgrove Rd/ The Horsley Drive - Upgraded]
New Site
Site Category: (None)
Signals - Fixed Time Coordinated


## MOVEMENT SUMMARY

## Site: 101 [AM Existing Elizabeth Dr/ Wallgrove Rd]

Elizabeth Dr/ Wallgrove Rd
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time = 105 seconds (Site Optimum Cycle Time - Minimum Delay) Variable Sequence Analysis applied. The results are given for the selected output sequence.


Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Back Pedestrian ped | of Queue <br> Distance m | Prop. Queued | Effective Stop Rate |
| P1 | South Full Crossing | 1 | 46.7 | LOS E | 0.0 | 0.0 | 0.94 | 0.94 |
| P3 | North Full Crossing | 1 | 46.7 | LOS E | 0.0 | 0.0 | 0.94 | 0.94 |
| P4 | West Full Crossing | 1 | 46.7 | LOS E | 0.0 | 0.0 | 0.94 | 0.94 |
| All Pedestrians |  | 3 | 46.7 | LOS E |  |  | 0.94 | 0.94 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

[^0]
## PHASING SUMMARY

## Site: 101 [AM Existing Elizabeth Dr/ Wallgrove Rd]

Elizabeth Dr/ Wallgrove Rd
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time = 105 seconds (Site Optimum Cycle Time - Minimum Delay) Variable Sequence Analysis applied. The results are given for the selected output sequence.

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: TCS
Reference Phase: Phase A
Input Phase Sequence: A, B, C, D, E*
Output Phase Sequence: A, B, C, D
(* Variable Phase)

| Phase Timing Summary |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Phase | A | B | C | D |
| Phase Change Time (sec) | 0 | 41 | 76 | 89 |
| Green Time (sec) | 35 | 29 | 7 | 10 |
| Phase Time (sec) | 41 | 35 | 13 | 16 |
| Phase Split | 39\% | 33\% | 12\% | 15\% |

See the Phase Information section in the Detailed Output report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


Phase D
Wallgrove Road
(N)


REF: Reference Phase
VAR: Variable Phase
$\square$ Stopped Movement
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs

Other Movement Class (MC) Stopped $\quad$|  |
| :---: |
| $\square$ |

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## MOVEMENT SUMMARY

## Site: 101 [AM Existing +10yr Gr + S2 Elizabeth Dr/ Wallgrove Rd]

Elizabeth Dr/ Wallgrove Rd
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time $=140$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID |  | Deman Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: M7 Exit (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 107 | 42.0 | 0.956 | 103.6 | LOS F | 9.2 | 87.7 | 1.00 | 1.05 | 1.63 | 21.8 |
| 2 | T1 | 102 | 11.0 | 0.714 | 72.4 | LOS F | 7.3 | 55.6 | 1.00 | 0.84 | 1.12 | 27.5 |
| 3 | R2 | 24 | 9.0 | 0.177 | 72.7 | LOS F | 1.6 | 12.0 | 0.97 | 0.71 | 0.97 | 27.0 |
| Appr |  | 234 | 25.0 | 0.956 | 86.8 | LOS F | 9.2 | 87.7 | 1.00 | 0.93 | 1.34 | 24.5 |
| East: Elizabeth Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | T1 | 647 | 4.0 | 0.287 | 0.5 | LOS A | 0.7 | 5.3 | 0.03 | 0.02 | 0.03 | 59.5 |
| 6 | R2 | 863 | 12.0 | 0.901 | 26.8 | LOS B | 21.9 | 168.8 | 0.87 | 0.86 | 0.93 | 40.6 |
| Appro |  | 1511 | 8.6 | 0.901 | 15.5 | LOS B | 21.9 | 168.8 | 0.51 | 0.50 | 0.54 | 47.0 |
| North: Wallgrove Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 365 | 11.0 | 0.487 | 23.6 | LOS B | 12.7 | 97.0 | 0.76 | 0.80 | 0.76 | 42.1 |
| 9 | R2 | 98 | 22.0 | 0.949 | 100.1 | LOS F | 8.2 | 68.0 | 1.00 | 1.05 | 1.61 | 22.4 |
| Appr |  | 463 | 13.3 | 0.949 | 39.8 | LOS C | 12.7 | 97.0 | 0.81 | 0.85 | 0.94 | 35.5 |
| West: Elizabeth Drive (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 522 | 16.0 | 0.553 | 21.1 | LOS B | 20.0 | 159.2 | 0.66 | 0.77 | 0.66 | 43.8 |
| 11 | T1 | 1075 | 8.0 | 1.002 | 104.3 | LOS F | 56.8 | 425.2 | 1.00 | 1.28 | 1.50 | 22.1 |
| Approach |  | 1597 | 10.6 | 1.002 | 77.1 | LOS F | 56.8 | 425.2 | 0.89 | 1.12 | 1.22 | 26.4 |
| All Vehicles |  | 3804 | 11.0 | 1.002 | 48.7 | LOS D | 56.8 | 425.2 | 0.74 | 0.83 | 0.93 | 33.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements. SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Movement Performance - Pedestrians

| Mov ID | Description | Demand Flow ped/h | Average Delay sec | Level of Average Back of Queue Service <br> Pedestrian Distance |  |  | Prop. Queued | Effective Stop Rate |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P1 | South Full Crossing | 1 | 64.1 | LOS F | 0.0 | 0.0 | 0.96 | 0.96 |
| P3 | North Full Crossing | 1 | 64.1 | LOS F | 0.0 | 0.0 | 0.96 | 0.96 |
| P4 | West Full Crossing | 1 | 64.1 | LOS F | 0.0 | 0.0 | 0.96 | 0.96 |
| All Pe | estrians | 3 | 64.1 | LOS F |  |  | 0.96 | 0.96 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

## PHASING SUMMARY

## Site: 101 [AM Existing +10yr Gr + S2 Elizabeth Dr/ Wallgrove Rd]

Elizabeth Dr/ Wallgrove Rd
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time $=140$ seconds (Site Optimum Cycle Time - Minimum Delay)
Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Green Split Priority has been specified
Phase Sequence: TCS
Reference Phase: Phase A
Input Phase Sequence: A, B, C, D, E
Output Phase Sequence: A, B, C, D, E

## Phase Timing Summary

| Phase | A | B | C | D | E |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 0 | 50 | 83 | 98 | 115 |
| Green Time (sec) | 44 | 27 | 9 | 11 | 19 |
| Phase Time (sec) | 50 | 33 | 15 | 17 | 25 |
| Phase Split | $36 \%$ | $24 \%$ | $11 \%$ | $12 \%$ | $18 \%$ |

See the Phase Information section in the Detailed Output report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
$\longrightarrow$ Normal Movement $\quad \longrightarrow$ Slip/Bypass-Lane Movement $\quad \longrightarrow$ Opposed Slip/Bypass-Lane
$\square$ Stopped Movement
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs

Other Movement Class (MC) Stopped $\quad$|  |
| :---: |
| $\square$ |

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## MOVEMENT SUMMARY

## Site: 101 [PM Existing +10yr Gr + S2 Elizabeth Dr/ Wallgrove Rd]

Elizabeth Dr/ Wallgrove Rd
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time = 139 seconds (Site Optimum Cycle Time - Minimum Delay) Variable Sequence Analysis applied. The results are given for the selected output sequence.


Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Back Pedestrian ped | of Queue <br> Distance m | Prop. Queued | Effective Stop Rate |
| P1 | South Full Crossing | 1 | 63.6 | LOS F | 0.0 | 0.0 | 0.96 | 0.96 |
| P3 | North Full Crossing | 1 | 63.6 | LOS F | 0.0 | 0.0 | 0.96 | 0.96 |
| P4 | West Full Crossing | 1 | 63.6 | LOS F | 0.0 | 0.0 | 0.96 | 0.96 |
| All Pedestrians |  | 3 | 63.6 | LOS F |  |  | 0.96 | 0.96 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

## PHASING SUMMARY

## Site: 101 [PM Existing +10yr Gr + S2 Elizabeth Dr/ Wallgrove Rd]

Elizabeth Dr/ Wallgrove Rd
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time = 139 seconds (Site Optimum Cycle Time - Minimum Delay) Variable Sequence Analysis applied. The results are given for the selected output sequence.

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: TCS
Reference Phase: Phase A
Input Phase Sequence: A, B*, C, D, E*
Output Phase Sequence: A, C, D, E*
(* Variable Phase)

| Phase Timing Summary |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Phase | A | C | D | E |
| Phase Change Time (sec) | 0 | 47 | 75 | 92 |
| Green Time (sec) | 41 | 22 | 11 | 41 |
| Phase Time (sec) | 47 | 28 | 17 | 47 |
| Phase Split | 34\% | 20\% | 12\% | 34\% |

See the Phase Information section in the Detailed Output report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
$\square$ Stopped Movement
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs

Other Movement Class (MC) Stopped $\quad$|  |
| :---: |
| $\square$ |

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## MOVEMENT SUMMARY

## Site: 101 [PM Existing +10yr Gr Elizabeth Dr/ Wallgrove Rd]

Elizabeth Dr/ Wallgrove Rd
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time $=150$ seconds (Site Practical Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID |  | Deman <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: M7 Exit (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 128 | 36.0 | 1.003 | 128.1 | LOS F | 12.8 | 117.6 | 1.00 | 1.09 | 1.71 | 19.0 |
| 2 | T1 | 54 | 19.0 | 0.357 | 71.8 | LOS F | 3.8 | 31.2 | 0.98 | 0.74 | 0.98 | 27.6 |
| 3 | R2 | 32 | 8.0 | 0.207 | 76.1 | LOS F | 2.2 | 16.5 | 0.97 | 0.73 | 0.97 | 26.4 |
| Appr |  | 214 | 27.6 | 1.003 | 106.3 | LOS F | 12.8 | 117.6 | 0.99 | 0.95 | 1.42 | 21.6 |
| East: Elizabeth Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | T1 | 521 | 9.0 | 0.265 | 0.6 | LOS A | 0.6 | 4.6 | 0.03 | 0.02 | 0.03 | 59.4 |
| 6 | R2 | 424 | 5.0 | 0.595 | 28.1 | LOS B | 8.3 | 60.8 | 0.81 | 0.78 | 0.81 | 40.2 |
| Appro | ch | 945 | 7.2 | 0.595 | 13.0 | LOS A | 8.3 | 60.8 | 0.38 | 0.36 | 0.38 | 48.9 |
| North: Wallgrove Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 702 | 4.0 | 0.984 | 76.2 | LOS F | 54.2 | 392.2 | 1.00 | 1.04 | 1.35 | 26.3 |
| 9 | R2 | 215 | 12.0 | 0.897 | 88.7 | LOS F | 17.7 | 137.0 | 1.00 | 0.96 | 1.31 | 24.2 |
| Appro |  | 917 | 5.9 | 0.984 | 79.1 | LOS F | 54.2 | 392.2 | 1.00 | 1.02 | 1.34 | 25.8 |
| West: Elizabeth Drive (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 236 | 19.0 | 0.196 | 8.8 | LOS A | 3.5 | 28.7 | 0.27 | 0.63 | 0.27 | 51.3 |
| 11 | T1 | 1122 | 10.0 | 0.969 | 87.1 | LOS F | 55.2 | 419.7 | 1.00 | 1.17 | 1.34 | 24.7 |
| Approach |  | 1358 | 11.6 | 0.969 | 73.5 | LOS F | 55.2 | 419.7 | 0.87 | 1.07 | 1.16 | 27.2 |
| All Ve | icles | 3434 | 9.8 | 1.003 | 60.4 | LOS E | 55.2 | 419.7 | 0.78 | 0.86 | 1.01 | 29.9 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements. SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Movement Performance - Pedestrians

| Mov ID | Description | Demand Flow ped/h | Average Delay sec | Level of Average Back of Queue Service <br> Pedestrian Distance |  |  | Prop. Queued | Effective Stop Rate |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P1 | South Full Crossing | 1 | 69.1 | LOS F | 0.0 | 0.0 | 0.96 | 0.96 |
| P3 | North Full Crossing | 1 | 69.1 | LOS F | 0.0 | 0.0 | 0.96 | 0.96 |
| P4 | West Full Crossing | 1 | 69.1 | LOS F | 0.0 | 0.0 | 0.96 | 0.96 |
| All Pe | estrians | 3 | 69.1 | LOS F |  |  | 0.96 | 0.96 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

## PHASING SUMMARY

## Site: 101 [PM Existing +10yr Gr Elizabeth Dr/ Wallgrove Rd]

Elizabeth Dr/ Wallgrove Rd
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time $=150$ seconds (Site Practical Cycle Time)
Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: TCS
Reference Phase: Phase A
Input Phase Sequence: A, B, C, D, E
Output Phase Sequence: A, B, C, D, E

| Phase Timing Summary |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Phase | A | B | C | D | E |
| Phase Change Time (sec) | 0 | 57 | 76 | 103 | 122 |
| Green Time $(\mathbf{s e c})$ | 51 | 13 | 21 | 13 | 22 |
| Phase Time $(\mathbf{s e c})$ | 57 | 19 | 27 | 19 | 28 |
| Phase Split | $38 \%$ | $13 \%$ | $18 \%$ | $13 \%$ | $19 \%$ |

See the Phase Information section in the Detailed Output report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase

| $\longrightarrow$ Normal Movement | Permitted/Opposed |
| :---: | :---: |
| $\longrightarrow$ Slip/Bypass-Lane Movement | Opposed Slip/Bypass-Lane |
| d Stopped Movement | $\square$ Turn On Red |

$\square$ Other Movement Class (MC) Running
Mixed Running \& Stopped MCs

Other Movement Class (MC) Stopped $\quad$| $\longrightarrow$ |
| :--- |
| Undetected Movement |
| Continuous Movement |
| Phase Transition Applied |

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## MOVEMENT SUMMARY

## Site: 101 [AM Existing +10yr Gr Elizabeth Dr/ Wallgrove Rd]

Elizabeth Dr/ Wallgrove Rd
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time $=120$ seconds (Site Practical Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID |  | Deman Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: M7 Exit (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 107 | 42.0 | 0.901 | 80.8 | LOS F | 7.5 | 70.9 | 1.00 | 1.01 | 1.53 | 25.2 |
| 2 | T1 | 71 | 11.0 | 0.465 | 59.2 | LOS E | 4.1 | 31.6 | 0.99 | 0.76 | 0.99 | 30.5 |
| 3 | R2 | 24 | 9.0 | 0.166 | 62.9 | LOS E | 1.4 | 10.3 | 0.96 | 0.71 | 0.96 | 29.2 |
| Appr |  | 202 | 27.2 | 0.901 | 71.1 | LOS F | 7.5 | 70.9 | 0.99 | 0.89 | 1.27 | 27.3 |
| East: Elizabeth Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | T1 | 647 | 4.0 | 0.295 | 0.4 | LOS A | 0.6 | 4.6 | 0.03 | 0.03 | 0.03 | 59.6 |
| 6 | R2 | 702 | 12.0 | 0.850 | 24.7 | LOS B | 14.3 | 110.7 | 0.87 | 0.84 | 0.92 | 41.6 |
| Appro |  | 1349 | 8.2 | 0.850 | 13.0 | LOS A | 14.3 | 110.7 | 0.47 | 0.45 | 0.49 | 48.7 |
| North: Wallgrove Road ( N ) |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 207 | 11.0 | 0.307 | 21.6 | LOS B | 5.9 | 45.2 | 0.73 | 0.76 | 0.73 | 43.2 |
| 9 | R2 | 83 | 22.0 | 0.888 | 79.6 | LOS F | 5.7 | 47.1 | 1.00 | 0.98 | 1.53 | 25.6 |
| Appr |  | 291 | 14.1 | 0.888 | 38.2 | LOS C | 5.9 | 47.1 | 0.81 | 0.83 | 0.96 | 36.1 |
| West: Elizabeth Drive (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 491 | 16.0 | 0.473 | 14.3 | LOS A | 12.6 | 100.6 | 0.54 | 0.73 | 0.54 | 47.7 |
| 11 | T1 | 1075 | 8.0 | 0.912 | 57.8 | LOS E | 37.3 | 278.9 | 1.00 | 1.08 | 1.25 | 30.8 |
| Approach |  | 1565 | 10.5 | 0.912 | 44.2 | LOS D | 37.3 | 278.9 | 0.86 | 0.97 | 1.03 | 34.7 |
| All Vehicles |  | 3407 | 10.9 | 0.912 | 32.9 | LOS C | 37.3 | 278.9 | 0.71 | 0.75 | 0.82 | 38.6 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements. SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Movement Performance - Pedestrians

| Mov ID | Description | Demand Flow ped/h | Average Delay sec | Level of Average Back of Queue Service <br> Pedestrian Distance |  |  | Prop. Queued | Effective Stop Rate |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P1 | South Full Crossing | 1 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P3 | North Full Crossing | 1 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P4 | West Full Crossing | 1 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| All Pe | estrians | 3 | 54.2 | LOS E |  |  | 0.95 | 0.95 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

## PHASING SUMMARY

## Site: 101 [AM Existing +10yr Gr Elizabeth Dr/ Wallgrove Rd]

Elizabeth Dr/ Wallgrove Rd
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time $=120$ seconds (Site Practical Cycle Time)
Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Green Split Priority has been specified
Phase Sequence: TCS
Reference Phase: Phase A
Input Phase Sequence: A, B, C, D, E
Output Phase Sequence: A, B, C, D, E

## Phase Timing Summary

| Phase | A | B | C | D | E |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 0 | 45 | 71 | 84 | 100 |
| Green Time (sec) | 39 | 20 | 7 | 10 | 14 |
| Phase Time (sec) | 45 | 26 | 13 | 16 | 20 |
| Phase Split | $38 \%$ | $22 \%$ | $11 \%$ | $13 \%$ | $17 \%$ |

See the Phase Information section in the Detailed Output report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
$\longrightarrow$ Normal Movement $\quad \longrightarrow$ Slip/Bypass-Lane Movement $\quad$ Permitted/Opposed
$\square$ Stopped Movement
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs

Other Movement Class (MC) Stopped $\quad$|  |
| :---: |
| $\square$ |

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## MOVEMENT SUMMARY

## Site: 101 [PM Existing Elizabeth Dr/ Wallgrove Rd]

Elizabeth Dr/ Wallgrove Rd
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time $=130$ seconds (Site Practical Cycle Time)
Variable Sequence Analysis applied. The results are given for the selected output sequence.


Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Description | $\begin{gathered} \text { Demand } \\ \text { Flow } \\ \text { ped/h } \end{gathered}$ | Average Delay $\qquad$ sec | Level of Service | Average Back Pedestrian $\qquad$ | of Queue Distance $\qquad$ m | Prop. Queued | Effective Stop Rate |
| P1 | South Full Crossing | 1 | 59.1 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P3 | North Full Crossing | 1 | 59.1 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P4 | West Full Crossing | 1 | 59.1 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| All Pedestrians |  | 3 | 59.1 | LOS E |  |  | 0.95 | 0.95 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

## PHASING SUMMARY

## Site: 101 [PM Existing Elizabeth Dr/ Wallgrove Rd]

Elizabeth Dr/ Wallgrove Rd
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time $=130$ seconds (Site Practical Cycle Time)
Variable Sequence Analysis applied. The results are given for the selected output sequence.
Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: TCS
Reference Phase: Phase A
Input Phase Sequence: A, B*, C, D, E*
Output Phase Sequence: A, C, D, E*
(* Variable Phase)

| Phase Timing Summary |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Phase | A | C | D | E |
| Phase Change Time (sec) | 0 | 44 | 80 | 105 |
| Green Time $(\mathbf{s e c})$ | 38 | 30 | 19 | 19 |
| Phase Time $(\mathbf{s e c})$ | 44 | 36 | 25 | 25 |
| Phase Split | $34 \%$ | $28 \%$ | $19 \%$ | $19 \%$ |

See the Phase Information section in the Detailed Output report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Phase Actuation and Phase Frequency values (user-specified or implied) less than 100\%.


REF: Reference Phase
VAR: Variable Phase
$\square$ Stopped Movement
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs

Other Movement Class (MC) Stopped $\quad$|  |
| :---: |
| $\square$ |

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## MOVEMENT SUMMARY

## Site: 101 [AM Existing + S1 Elizabeth Dr/ Wallgrove Rd]

Elizabeth Dr/ Wallgrove Rd
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time = 130 seconds (Site User-Given Phase Times)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | Turn | Deman <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. <br> Satn <br> v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: M7 Exit (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 121 | 42.0 | 0.918 | 88.2 | LOS F | 9.2 | 87.6 | 1.00 | 1.01 | 1.52 | 24.0 |
| 2 | T1 | 85 | 11.0 | 0.508 | 62.9 | LOS E | 5.4 | 41.0 | 1.00 | 0.77 | 1.00 | 29.6 |
| 3 | R2 | 24 | 9.0 | 0.150 | 65.9 | LOS E | 1.5 | 11.0 | 0.95 | 0.71 | 0.95 | 28.5 |
| Appr |  | 231 | 27.1 | 0.918 | 76.5 | LOS F | 9.2 | 87.6 | 0.99 | 0.89 | 1.27 | 26.3 |
| East: Elizabeth Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | T1 | 727 | 4.0 | 0.325 | 6.6 | LOS A | 10.0 | 72.2 | 0.37 | 0.33 | 0.37 | 54.2 |
| 6 | R2 | 776 | 12.0 | 0.989 | 66.5 | LOS E | 31.0 | 239.2 | 0.98 | 1.03 | 1.42 | 28.2 |
| Appro | ach | 1503 | 8.1 | 0.989 | 37.5 | LOS C | 31.0 | 239.2 | 0.69 | 0.69 | 0.91 | 36.7 |
| North: Wallgrove Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 294 | 11.0 | 0.443 | 25.6 | LOS B | 10.4 | 79.3 | 0.79 | 0.79 | 0.79 | 41.2 |
| 9 | R2 | 101 | 22.0 | 0.909 | 86.7 | LOS F | 7.5 | 62.5 | 1.00 | 1.01 | 1.52 | 24.4 |
| Appro |  | 395 | 13.8 | 0.909 | 41.2 | LOS C | 10.4 | 79.3 | 0.84 | 0.85 | 0.98 | 35.0 |
| West: Elizabeth Drive (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 501 | 16.0 | 0.495 | 18.5 | LOS B | 16.1 | 128.3 | 0.61 | 0.75 | 0.61 | 45.2 |
| 11 | T1 | 1097 | 8.0 | 0.857 | 47.5 | LOS D | 36.7 | 274.6 | 0.98 | 0.96 | 1.08 | 33.7 |
| Approach |  | 1598 | 10.5 | 0.857 | 38.4 | LOS C | 36.7 | 274.6 | 0.86 | 0.89 | 0.93 | 36.7 |
| All Ve | icles | 3726 | 10.9 | 0.989 | 40.7 | LOS C | 36.7 | 274.6 | 0.80 | 0.81 | 0.95 | 35.6 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements. SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Movement Performance - Pedestrians

| Mov ID | Description | Demand Flow ped/h | Average Delay sec | Level of Average Back of Queue |  |  | Prop. Queued | Effective Stop Rate |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P1 | South Full Crossing | 1 | 59.1 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P3 | North Full Crossing | 1 | 59.1 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P4 | West Full Crossing | 1 | 59.1 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| All Pedestrians |  | 3 | 59.1 | LOS E |  |  | 0.95 | 0.95 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

## PHASING SUMMARY

Site: 101 [AM Existing + S1 Elizabeth Dr/ Wallgrove Rd]
Elizabeth Dr/ Wallgrove Rd
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time $=130$ seconds (Site User-Given Phase Times)
Timings based on settings in the Site Phasing \& Timing dialog
Phase Times specified by the user
Phase Sequence: TCS - Copy
Reference Phase: Phase A
Input Phase Sequence: A, B, C, D, E
Output Phase Sequence: A, B, C, D, E

| Phase Timing Summary |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Phase | A | B | C | D | E |
| Phase Change Time (sec) | 0 | 53 | 71 | 86 | 104 |
| Green Time $(\mathbf{s e c})$ | 47 | 12 | 9 | 12 | 23 |
| Phase Time $(\mathbf{s e c})$ | 53 | 18 | 15 | 15 | 29 |
| Phase Split | $41 \%$ | $14 \%$ | $12 \%$ | $12 \%$ | $22 \%$ |

See the Phase Information section in the Detailed Output report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase

| $\Rightarrow$ Normal Movement | Permitted/Opposed |
| :---: | :---: |
| $\geqslant$ Slip/Bypass-Lane Movement | Opposed Slip/Bypass-Lane |
| - Stopped Movement | $\square$ Turn On Red |

$\square$ Other Movement Class (MC) Running
Mixed Running \& Stopped MCs

Other Movement Class (MC) Stopped $\quad$| $\longrightarrow$ |
| :--- |
| Undetected Movement |
| Continuous Movement |
| Phase Transition Applied |

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## MOVEMENT SUMMARY

## Site: 101 [PM Existing + S1 Elizabeth Dr/ Wallgrove Rd]

Elizabeth Dr/ Wallgrove Rd
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time = 124 seconds (Site Optimum Cycle Time - Minimum Delay) Variable Sequence Analysis applied. The results are given for the selected output sequence.

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | Demand <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: M7 Exit (S) |  |  |  |  |  |  |  |  |  |  |  |
| L2 | 186 | 36.0 | 0.977 | 101.1 | LOS F | 15.3 | 140.2 | 1.00 | 1.10 | 1.67 | 22.1 |
| 2 T1 | 39 | 19.0 | 0.174 | 52.9 | LOS D | 2.1 | 17.4 | 0.93 | 0.69 | 0.93 | 32.2 |
| 3 R2 | 26 | 8.0 | 0.116 | 57.9 | LOS E | 1.4 | 10.7 | 0.92 | 0.72 | 0.92 | 30.4 |
| Approach | 252 | 30.4 | 0.977 | 89.1 | LOS F | 15.3 | 140.2 | 0.98 | 0.99 | 1.47 | 24.0 |
| East: Elizabeth Road (E) |  |  |  |  |  |  |  |  |  |  |  |
| $5 \quad \mathrm{~T} 1$ | 756 | 9.0 | 0.520 | 22.4 | LOS B | 19.1 | 144.0 | 0.71 | 0.62 | 0.71 | 43.9 |
| 6 R2 | 467 | 5.0 | 0.949 | 75.4 | LOS F | 20.9 | 152.5 | 1.00 | 0.95 | 1.29 | 26.4 |
| Approach | 1223 | 7.5 | 0.949 | 42.7 | LOS D | 20.9 | 152.5 | 0.82 | 0.75 | 0.93 | 35.0 |
| North: Wallgrove Road (N) |  |  |  |  |  |  |  |  |  |  |  |
| L2 | 692 | 4.0 | 0.950 | 53.7 | LOS D | 38.2 | 276.7 | 1.00 | 1.02 | 1.30 | 31.4 |
| 9 R2 | 326 | 12.0 | 0.788 | 57.0 | LOS E | 19.7 | 151.7 | 1.00 | 0.90 | 1.09 | 30.5 |
| Approach | 1018 | 6.6 | 0.950 | 54.8 | LOS D | 38.2 | 276.7 | 1.00 | 0.98 | 1.23 | 31.1 |
| West: Elizabeth Drive (W) |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 222 | 19.0 | 0.186 | 9.8 | LOS A | 3.5 | 28.4 | 0.33 | 0.64 | 0.33 | 50.6 |
| 11 T1 | 951 | 10.0 | 0.948 | 73.7 | LOS F | 36.4 | 276.9 | 1.00 | 1.17 | 1.37 | 27.2 |
| Approach | 1173 | 11.7 | 0.948 | 61.6 | LOS E | 36.4 | 276.9 | 0.87 | 1.07 | 1.17 | 29.8 |
| All Vehicles | 3665 | 10.2 | 0.977 | 55.3 | LOS D | 38.2 | 276.9 | 0.90 | 0.93 | 1.13 | 31.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Description | $\begin{gathered} \text { Demand } \\ \text { Flow } \\ \text { ped/h } \end{gathered}$ | Average Delay $\qquad$ sec | Level of Service | Average Back Pedestrian $\qquad$ | of Queue Distance $\qquad$ m | Prop. Queued | Effective Stop Rate |
| P1 | South Full Crossing | 1 | 56.1 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P3 | North Full Crossing | 1 | 56.1 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P4 | West Full Crossing | 1 | 56.1 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| All Pedestrians |  | 3 | 56.1 | LOS E |  |  | 0.95 | 0.95 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

## PHASING SUMMARY

## Site: 101 [PM Existing + S1 Elizabeth Dr/ Wallgrove Rd ]

Elizabeth Dr/ Wallgrove Rd
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time = 124 seconds (Site Optimum Cycle Time - Minimum Delay) Variable Sequence Analysis applied. The results are given for the selected output sequence.

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: TCS
Reference Phase: Phase A
Input Phase Sequence: A, B*, C, D, E*
Output Phase Sequence: A, C, D, E*
(* Variable Phase)

| Phase Timing Summary |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Phase | A | C | D | E |
| Phase Change Time (sec) | 0 | 40 | 76 | 98 |
| Green Time (sec) | 34 | 30 | 16 | 20 |
| Phase Time (sec) | 40 | 36 | 22 | 26 |
| Phase Split | 32\% | 29\% | 18\% | 21\% |

See the Phase Information section in the Detailed Output report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Phase Actuation and Phase Frequency values (user-specified or implied) less than 100\%.


REF: Reference Phase
VAR: Variable Phase
$\square$ Stopped Movement
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs

Other Movement Class (MC) Stopped $\quad$|  |
| :---: |
| $\square$ |

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## MOVEMENT SUMMARY

## Site: 101 [PM Existing +10yr Gr + S2 Elizabeth Dr/ Wallgrove Rd - LT Slip]

Elizabeth Dr/ Wallgrove Rd
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time = 110 seconds (Site Optimum Cycle Time - Minimum Delay)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID |  | Deman Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: M7 Exit (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 128 | 36.0 | 0.956 | 86.1 | LOS F | 9.0 | 82.2 | 1.00 | 1.09 | 1.72 | 24.3 |
| 2 | T1 | 43 | 19.0 | 0.274 | 52.5 | LOS D | 2.3 | 18.4 | 0.97 | 0.72 | 0.97 | 32.3 |
| 3 | R2 | 32 | 8.0 | 0.198 | 57.6 | LOS E | 1.6 | 12.2 | 0.96 | 0.72 | 0.96 | 30.5 |
| Appr |  | 203 | 28.0 | 0.956 | 74.5 | LOS F | 9.0 | 82.2 | 0.99 | 0.96 | 1.44 | 26.6 |
| East: Elizabeth Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | T1 | 521 | 9.0 | 0.293 | 0.6 | LOS A | 0.5 | 3.6 | 0.03 | 0.02 | 0.03 | 59.5 |
| 6 | R2 | 581 | 5.0 | 0.910 | 47.8 | LOS D | 19.8 | 144.4 | 0.95 | 0.88 | 1.07 | 33.0 |
| Appro |  | 1102 | 6.9 | 0.910 | 25.5 | LOS B | 19.8 | 144.4 | 0.52 | 0.48 | 0.58 | 41.8 |
| North: Wallgrove Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 896 | 4.0 | 0.939 | 47.5 | LOS D | 52.3 | 378.8 | 0.95 | 1.01 | 1.20 | 33.5 |
| 9 | R2 | 246 | 12.0 | 0.932 | 75.7 | LOS F | 16.4 | 126.8 | 1.00 | 1.05 | 1.49 | 26.4 |
| Appr |  | 1142 | 5.7 | 0.939 | 53.6 | LOS D | 52.3 | 378.8 | 0.96 | 1.02 | 1.26 | 31.7 |
| West: Elizabeth Drive (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 251 | 19.0 | 0.223 | 10.8 | LOS A | 4.2 | 34.5 | 0.39 | 0.66 | 0.39 | 49.9 |
| 11 | T1 | 1122 | 10.0 | 0.949 | 65.4 | LOSE | 39.7 | 301.9 | 1.00 | 1.19 | 1.39 | 28.9 |
| Approach |  | 1373 | 11.6 | 0.949 | 55.4 | LOS D | 39.7 | 301.9 | 0.89 | 1.10 | 1.20 | 31.4 |
| All Vehicles |  | 3820 | 9.4 | 0.956 | 47.3 | LOS D | 52.3 | 378.8 | 0.81 | 0.89 | 1.05 | 33.6 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements. SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Movement Performance - Pedestrians

| Mov ID | Description | Demand Flow ped/h | Average Delay sec | Level of Average Back of Queue |  |  | Prop. Queued | Effective Stop Rate |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P1 | South Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P3 | North Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P4 | West Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| All Pedestrians |  | 3 | 49.2 | LOS E |  |  | 0.95 | 0.95 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

## PHASING SUMMARY

Site: 101 [PM Existing +10yr Gr + S2 Elizabeth Dr/ Wallgrove Rd - LT Slip]
Elizabeth Dr/ Wallgrove Rd
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time $=110$ seconds (Site Optimum Cycle Time - Minimum Delay)
Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Green Split Priority has been specified
Phase Sequence: TCS Manual Phase Times
Reference Phase: Phase A
Input Phase Sequence: A, C, D, E
Output Phase Sequence: A, C, D, E

## Phase Timing Summary

| Phase | A | C | D | E |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 0 | 42 | 65 | 81 |
| Green Time (sec) | 36 | 17 | 10 | 23 |
| Phase Time (sec) | 42 | 23 | 16 | 29 |
| Phase Split | $38 \%$ | $21 \%$ | $15 \%$ | $26 \%$ |

See the Phase Information section in the Detailed Output report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
$\longrightarrow$ Normal Movement $\quad \longrightarrow$ Slip/Bypass-Lane Movement $\quad$ Permitted/Opposed
$\square$ Stopped Movement
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs

Other Movement Class (MC) Stopped $\quad$|  |
| :---: |
| $\square$ |

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## MOVEMENT SUMMARY

## Site: 101 [AM Existing +10yr Gr + S2 Elizabeth Dr/ Wallgrove Rd - LT Slip]

Elizabeth Dr/ Wallgrove Rd
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time $=120$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Deman <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: M7 Exit (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 107 | 42.0 | 1.002 | 110.9 | LOS F | 9.0 | 85.2 | 1.00 | 1.15 | 1.89 | 20.8 |
| 2 | T1 | 102 | 11.0 | 0.748 | 64.1 | LOS E | 6.4 | 48.8 | 1.00 | 0.87 | 1.19 | 29.4 |
| 3 | R2 | 24 | 9.0 | 0.185 | 64.2 | LOS E | 1.4 | 10.5 | 0.97 | 0.71 | 0.97 | 28.8 |
| Appr |  | 234 | 25.0 | 1.002 | 85.6 | LOS F | 9.0 | 85.2 | 1.00 | 0.98 | 1.49 | 24.7 |
| East: Elizabeth Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | T1 | 647 | 4.0 | 0.291 | 0.4 | LOS A | 0.6 | 4.6 | 0.03 | 0.02 | 0.03 | 59.6 |
| 6 | R2 | 863 | 12.0 | 0.901 | 33.1 | LOS C | 24.1 | 185.7 | 0.75 | 0.84 | 0.83 | 38.0 |
| Appr | ch | 1511 | 8.6 | 0.901 | 19.1 | LOS B | 24.1 | 185.7 | 0.44 | 0.49 | 0.49 | 45.0 |
| North: Wallgrove Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 365 | 11.0 | 0.359 | 16.3 | LOS B | 9.6 | 73.6 | 0.56 | 0.73 | 0.56 | 46.6 |
| 9 | R2 | 98 | 22.0 | 1.045 | 133.0 | LOS F | 9.1 | 75.5 | 1.00 | 1.21 | 2.08 | 18.4 |
| Appr |  | 463 | 13.3 | 1.045 | 41.0 | LOS C | 9.6 | 75.5 | 0.65 | 0.83 | 0.88 | 35.2 |
| West: Elizabeth Drive (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 522 | 16.0 | 0.559 | 19.1 | LOS B | 17.1 | 136.4 | 0.69 | 0.82 | 0.76 | 45.0 |
| 11 | T1 | 1075 | 8.0 | 0.976 | 81.3 | LOS F | 44.9 | 336.1 | 1.00 | 1.25 | 1.46 | 25.7 |
| Approach |  | 1597 | 10.6 | 0.976 | 61.0 | LOS E | 44.9 | 336.1 | 0.90 | 1.11 | 1.23 | 29.9 |
| All V | icles | 3804 | 11.0 | 1.045 | 43.4 | LOS D | 44.9 | 336.1 | 0.69 | 0.82 | 0.91 | 34.7 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements. SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Movement Performance - Pedestrians

| Mov ID | Description | Demand Flow ped/h | Average Delay sec | Level of Average Back of Queue Service <br> Pedestrian Distance |  |  | Prop. Queued | Effective Stop Rate |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P1 | South Full Crossing | 1 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P3 | North Full Crossing | 1 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P4 | West Full Crossing | 1 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| All Pe | estrians | 3 | 54.2 | LOS E |  |  | 0.95 | 0.95 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

[^1]
## PHASING SUMMARY

Site: 101 [AM Existing +10yr Gr + S2 Elizabeth Dr/ Wallgrove Rd - LT Slip]
Elizabeth Dr/ Wallgrove Rd
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time $=120$ seconds (Site Optimum Cycle Time - Minimum Delay)
Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Green Split Priority has been specified
Phase Sequence: TCS Manual Phase Times
Reference Phase: Phase A
Input Phase Sequence: A, C, D, E
Output Phase Sequence: A, C, D, E

## Phase Timing Summary

| Phase | A | C | D | E |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 0 | 43 | 56 | 71 |
| Green Time (sec) | 37 | 7 | 9 | 43 |
| Phase Time (sec) | 43 | 13 | 15 | 49 |
| Phase Split | $36 \%$ | $11 \%$ | $13 \%$ | $41 \%$ |

See the Phase Information section in the Detailed Output report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
$\longrightarrow$ Normal Movement $\quad \longrightarrow$ Slip/Bypass-Lane Movement $\quad$ Permitted/Opposed
$\square$ Stopped Movement
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs

Other Movement Class (MC) Stopped $\quad$|  |
| :---: |
| $\square$ |

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## MOVEMENT SUMMARY

## Site: 101 [AM Existing Wallgrove Rd/ The Horsley Drive]

Data from 25/7/18
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time = 110 seconds (Site Optimum Cycle Time - Minimum Delay) Variable Sequence Analysis applied. The results are given for the selected output sequence.

Movement Performance - Vehicles

| Mov ID | Turn | Demand Total veh/h | lows HV $\%$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles <br> veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| South: Wallgrove Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 50 | 0.0 | 0.067 | 19.6 | LOS B | 1.3 | 9.1 | 0.64 | 0.69 | 0.64 | 44.5 |
| 2 | T1 | 613 | 7.0 | 0.790 | 43.9 | LOS D | 18.7 | 139.0 | 0.98 | 0.87 | 1.03 | 34.9 |
| 3 | R2 | 132 | 8.0 | 0.326 | 34.7 | LOS C | 5.1 | 38.2 | 0.88 | 0.77 | 0.88 | 37.4 |
| Appr |  | 795 | 6.7 | 0.790 | 40.8 | LOS C | 18.7 | 139.0 | 0.94 | 0.84 | 0.98 | 35.8 |
| East: The Horsely Drive (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 25 | 36.0 | 0.609 | 49.5 | LOS D | 10.0 | 78.4 | 0.92 | 0.79 | 1.08 | 33.8 |
| 5 | T1 | 189 | 11.0 | 0.609 | 43.5 | LOS D | 10.0 | 78.4 | 0.92 | 0.79 | 1.08 | 34.9 |
| 6 | R2 | 404 | 17.0 | 0.656 | 29.0 | LOS C | 14.6 | 117.3 | 0.78 | 0.80 | 0.78 | 39.9 |
| Appr |  | 618 | 15.9 | 0.656 | 34.3 | LOS C | 14.6 | 117.3 | 0.83 | 0.80 | 0.89 | 38.0 |
| North: Wallgrove Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 242 | 29.0 | 0.346 | 26.7 | LOS B | 8.4 | 73.2 | 0.69 | 0.77 | 0.69 | 40.4 |
| 8 | T1 | 225 | 12.0 | 0.751 | 55.1 | LOS D | 7.7 | 59.4 | 1.00 | 0.84 | 1.10 | 31.5 |
| 9 | R2 | 41 | 7.0 | 0.217 | 37.0 | LOS C | 1.6 | 11.8 | 0.94 | 0.73 | 0.94 | 36.6 |
| Appr |  | 508 | 19.7 | 0.751 | 40.1 | LOS C | 8.4 | 73.2 | 0.85 | 0.80 | 0.89 | 35.6 |
| West: The Horsely Drive (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 49 | 16.0 | 0.798 | 55.8 | LOS D | 15.6 | 118.7 | 1.00 | 0.94 | 1.14 | 32.0 |
| 11 | T1 | 232 | 9.0 | 0.798 | 50.1 | LOS D | 15.6 | 118.7 | 1.00 | 0.94 | 1.14 | 32.8 |
| 12 | R2 | 22 | 18.0 | 0.064 | 24.6 | LOS B | 0.6 | 4.7 | 0.79 | 0.68 | 0.79 | 41.9 |
| Appr |  | 303 | 10.8 | 0.798 | 49.2 | LOS D | 15.6 | 118.7 | 0.98 | 0.92 | 1.12 | 33.2 |
| All V | icles | 2224 | 12.8 | 0.798 | 40.0 | LOS C | 18.7 | 139.0 | 0.89 | 0.83 | 0.95 | 35.9 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Back Pedestrian ped | of Queue Distance m | Prop. Queued | Effective Stop Rate |
| P1 | South Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P2 | East Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P3 | North Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P4 | West Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| All Pedestrians |  | 4 | 49.2 | LOS E |  |  | 0.95 | 0.95 |

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## PHASING SUMMARY

## Site: 101 [AM Existing Wallgrove Rd/ The Horsley Drive]

Data from 25/7/18
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time = 110 seconds (Site Optimum Cycle Time - Minimum Delay) Variable Sequence Analysis applied. The results are given for the selected output sequence.

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: TCS
Reference Phase: Phase A

Output Phase Sequence: A, D, D1*, E, F2*, G, G2*
(*Variable Phase)

| Phase Timing Summary |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Phase | A | D | D1 | E | F2 | G | G2 |
| Phase Change Time (sec) | 0 | 17 | 29 | 56 | 71 | 83 | 95 |
| Green Time $(\mathbf{s e c})$ | 11 | 6 | 21 | 9 | 6 | 6 | 9 |
| Phase Time $(\mathbf{s e c})$ | 17 | 12 | 27 | 15 | 12 | 12 | 15 |
| Phase Split | $15 \%$ | $11 \%$ | $25 \%$ | $14 \%$ | $11 \%$ | $11 \%$ | $14 \%$ |

See the Phase Information section in the Detailed Output report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.

| Output Phase Sequence |  |  |
| :---: | :---: | :---: |
| Phase A | Phase D |  |
| Phase E |  | Phase G |


| Phase G2 | VAR |
| :--- | :--- | :--- |
|  |  |
| Wallgrove Road |  |
| (N) |  |

REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement
Other Movement Class (MC) Running

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## MOVEMENT SUMMARY

## Site: 101 [AM Existing+10y Gr + S2 Wallgrove Rd/ The Horsley Drive]

New Site
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time = 110 seconds (Site Optimum Cycle Time - Minimum Delay) Variable Sequence Analysis applied. The results are given for the selected output sequence.

## Movement Performance - Vehicles

| Mov ID | Turn | Demand <br> Total veh/h | Hows | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| South: Wallgrove Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 64 | 0.0 | 0.102 | 32.3 | LOS C | 2.3 | 16.4 | 0.72 | 0.72 | 0.72 | 38.5 |
| 2 | T1 | 546 | 7.0 | 0.731 | 42.9 | LOS D | 16.0 | 118.8 | 0.96 | 0.83 | 0.99 | 35.2 |
| 3 | R2 | 227 | 8.0 | 0.583 | 37.5 | LOS C | 9.5 | 71.3 | 0.95 | 0.81 | 0.95 | 36.4 |
| Appr |  | 837 | 6.7 | 0.731 | 40.6 | LOS C | 16.0 | 118.8 | 0.94 | 0.82 | 0.96 | 35.8 |
| East: The Horsley Drive (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 87 | 36.0 | 0.649 | 45.3 | LOS D | 13.4 | 108.7 | 0.94 | 0.82 | 0.94 | 34.8 |
| 5 | T1 | 189 | 11.0 | 0.649 | 39.3 | LOS C | 13.4 | 108.7 | 0.94 | 0.82 | 0.94 | 36.0 |
| 6 | R2 | 360 | 17.0 | 0.611 | 24.3 | LOS B | 11.1 | 89.2 | 0.88 | 0.82 | 0.88 | 42.1 |
| Appr |  | 636 | 17.8 | 0.649 | 31.6 | LOS C | 13.4 | 108.7 | 0.91 | 0.82 | 0.91 | 39.0 |
| North: Wallgrove Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 242 | 29.0 | 0.346 | 26.7 | LOS B | 8.4 | 73.2 | 0.69 | 0.77 | 0.69 | 40.4 |
| 8 | T1 | 232 | 12.0 | 0.774 | 55.6 | LOS D | 8.0 | 61.8 | 1.00 | 0.85 | 1.12 | 31.4 |
| 9 | R2 | 41 | 7.0 | 0.205 | 37.0 | LOS C | 1.6 | 12.0 | 0.92 | 0.72 | 0.92 | 36.6 |
| Appr |  | 515 | 19.6 | 0.774 | 40.6 | LOS C | 8.4 | 73.2 | 0.85 | 0.80 | 0.90 | 35.5 |
| West: The Horsley Drive (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 44 | 16.0 | 0.749 | 52.6 | LOS D | 14.7 | 111.6 | 1.00 | 0.90 | 1.08 | 33.0 |
| 11 | T1 | 232 | 9.0 | 0.749 | 46.9 | LOS D | 14.7 | 111.6 | 1.00 | 0.90 | 1.08 | 33.8 |
| 12 | R2 | 53 | 18.0 | 0.141 | 24.6 | LOS B | 1.4 | 11.5 | 0.80 | 0.72 | 0.80 | 41.9 |
| Appr |  | 329 | 11.4 | 0.749 | 44.0 | LOS D | 14.7 | 111.6 | 0.96 | 0.87 | 1.03 | 34.7 |
| All V | icles | 2317 | 13.3 | 0.774 | 38.6 | LOS C | 16.0 | 118.8 | 0.91 | 0.82 | 0.94 | 36.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Back Pedestrian ped | f Queue Distance m | Prop. Queued | Effective Stop Rate |
| P1 | South Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P2 | East Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P3 | North Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P4 | West Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| All Pedestrians |  | 4 | 49.2 | LOS E |  |  | 0.95 | 0.95 |

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## PHASING SUMMARY

## Site: 101 [AM Existing+ 10y Gr + S2 Wallgrove Rd/ The Horsley Drive]

New Site
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time = 110 seconds (Site Optimum Cycle Time - Minimum Delay) Variable Sequence Analysis applied. The results are given for the selected output sequence.

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program

## Phase Sequence: TCS

Reference Phase: Phase A

Output Phase Sequence: A, D, D1*, E, G, G2*
(* Variable Phase)
Phase Timing Summary

| Phase | A | D | D1 | E | G | G2 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 0 | 17 | 29 | 56 | 84 | 96 |
| Green Time (sec) | 11 | 6 | 21 | 22 | 6 | 8 |
| Phase Time $(\mathbf{s e c})$ | 17 | 12 | 27 | 28 | 12 | 14 |
| Phase Split | $15 \%$ | $11 \%$ | $25 \%$ | $25 \%$ | $11 \%$ | $13 \%$ |

See the Phase Information section in the Detailed Output report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.

| Output Phase Sequence |  |  |
| :---: | :---: | :---: |
|  | Phase D |  |
| Phase E | Phase G |  |

REF: Reference Phase
VAR: Variable Phase
$\square$ Stopped Movement
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs

Other Movement Class (MC) Stopped $\quad$|  |
| :---: |
| $\square$ |

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## MOVEMENT SUMMARY

## Site: 101 [PM Existing+ 10y Gr + S2 Wallgrove Rd/ The Horsley Drive]

New Site
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time $=140$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman <br> Total <br> veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: Wallgrove Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 61 | 7.0 | 0.071 | 25.7 | LOS B | 2.2 | 16.1 | 0.56 | 0.69 | 0.56 | 41.2 |
| 2 | T1 | 298 | 8.0 | 0.426 | 50.8 | LOS D | 10.0 | 75.0 | 0.90 | 0.74 | 0.90 | 32.7 |
| 3 | R2 | 119 | 14.0 | 0.682 | 50.3 | LOS D | 6.3 | 49.6 | 1.00 | 0.81 | 1.07 | 32.2 |
| Appr |  | 478 | 9.4 | 0.682 | 47.5 | LOS D | 10.0 | 75.0 | 0.88 | 0.75 | 0.90 | 33.5 |
| East: The Horsley Drive (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 223 | 8.0 | 1.060 | 136.6 | LOS F | 67.2 | 513.1 | 1.00 | 1.33 | 1.65 | 18.4 |
| 5 | T1 | 389 | 12.0 | 1.060 | 131.0 | LOS F | 67.2 | 513.1 | 1.00 | 1.33 | 1.65 | 18.6 |
| 6 | R2 | 422 | 11.0 | 0.628 | 21.3 | LOS B | 13.2 | 101.0 | 0.65 | 0.76 | 0.65 | 43.7 |
| Appr |  | 1034 | 10.7 | 1.060 | 87.5 | LOS F | 67.2 | 513.1 | 0.86 | 1.10 | 1.24 | 24.3 |
| North: Wallgrove Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 455 | 15.0 | 0.558 | 32.7 | LOS C | 21.6 | 171.0 | 0.76 | 0.82 | 0.76 | 38.1 |
| 8 | T1 | 679 | 6.0 | 1.049 | 103.4 | LOS F | 43.6 | 320.6 | 0.99 | 1.17 | 1.43 | 22.0 |
| 9 | R2 | 138 | 9.0 | 0.487 | 46.1 | LOS D | 7.3 | 54.9 | 0.91 | 0.78 | 0.91 | 33.5 |
| Appr |  | 1272 | 9.5 | 1.049 | 71.9 | LOS F | 43.6 | 320.6 | 0.90 | 1.00 | 1.13 | 27.1 |
| West: The Horsley Drive (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 49 | 12.0 | 0.338 | 44.3 | LOS D | 10.0 | 76.4 | 0.81 | 0.71 | 0.81 | 35.5 |
| 11 | T1 | 145 | 10.0 | 0.338 | 38.6 | LOS C | 10.0 | 76.4 | 0.81 | 0.71 | 0.81 | 36.3 |
| 12 | R2 | 60 | 7.0 | 0.094 | 19.2 | LOS B | 1.8 | 13.0 | 0.50 | 0.67 | 0.50 | 44.9 |
| Approach |  | 254 | 9.7 | 0.338 | 35.1 | LOS C | 10.0 | 76.4 | 0.73 | 0.70 | 0.73 | 37.9 |
| All Vehicles |  | 3038 | 9.9 | 1.060 | 70.3 | LOS E | 67.2 | 513.1 | 0.87 | 0.97 | 1.10 | 27.5 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Description | Demand Flow ped/h | Average Delay sec | Level of Average Back of Queue Service Pedestrian Distance |  |  | Prop. Queued | Effective Stop Rate |
| P1 | South Full Crossing | 1 | 64.1 | LOS F | 0.0 | 0.0 | 0.96 | 0.96 |
| P2 | East Full Crossing | 1 | 64.1 | LOS F | 0.0 | 0.0 | 0.96 | 0.96 |
| P3 | North Full Crossing | 1 | 64.1 | LOS F | 0.0 | 0.0 | 0.96 | 0.96 |
| P4 | West Full Crossing | 1 | 64.1 | LOS F | 0.0 | 0.0 | 0.96 | 0.96 |
| All P | destrians | 4 | 64.1 | LOS F |  |  | 0.96 | 0.96 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## PHASING SUMMARY

## Site: 101 [PM Existing+10y Gr + S2 Wallgrove Rd/ The Horsley Drive]

New Site
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time $=140$ seconds (Site Optimum Cycle Time - Minimum Delay)
Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Green Split Priority has been specified
Phase Sequence: TCS - Tom Edit
Reference Phase: Phase A
Input Phase Sequence: A, D, E, G
Output Phase Sequence: A, D, E, G

## Phase Timing Summary

| Phase | A | D | E | G |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 0 | 36 | 74 | 124 |
| Green Time (sec) | 30 | 32 | 44 | 10 |
| Phase Time (sec) | 36 | 38 | 50 | 16 |
| Phase Split | $26 \%$ | $27 \%$ | $36 \%$ | $11 \%$ |

See the Phase Information section in the Detailed Output report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.

| Output Phase Sequence |  |  |
| :---: | :---: | :---: |
|  | Phase D | Phase E |
| Phase G |  |  |

REF: Reference Phase
VAR: Variable Phase

| $\longrightarrow$ Normal Movement | Slip/Bypass-Lane Movement |
| :--- | :--- |$\quad$| Permitted/Opposed |
| :--- |
| Opposed Slip/Bypass-Lane |

$\square$ Stopped Movement
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs

Other Movement Class (MC) Stopped $\quad$|  |
| :---: |
| $\square$ |

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## MOVEMENT SUMMARY

## Site: 101 [PM Existing + S1 Wallgrove Rd/ The Horsley Drive]

New Site
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time = 110 seconds (Site User-Given Cycle Time)
Variable Sequence Analysis applied. The results are given for the selected output sequence.

Movement Performance - Vehicles

| Mov ID | Turn | Deman Total veh/h | lows HV $\%$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles <br> veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| South: Wallgrove Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 43 | 0.0 | 0.028 | 7.1 | LOS A | 0.4 | 2.6 | 0.18 | 0.61 | 0.18 | 52.4 |
| 2 | T1 | 257 | 7.0 | 0.146 | 13.4 | LOS A | 3.9 | 28.7 | 0.53 | 0.43 | 0.53 | 49.2 |
| 3 | R2 | 89 | 8.0 | 0.534 | 38.8 | LOS C | 3.5 | 26.5 | 1.00 | 0.77 | 1.00 | 35.9 |
| Appr |  | 389 | 6.5 | 0.534 | 18.5 | LOS B | 3.9 | 28.7 | 0.60 | 0.53 | 0.60 | 45.6 |
| East: The Horsley Drive (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 174 | 36.0 | 0.903 | 60.8 | LOS E | 23.5 | 195.6 | 1.00 | 1.03 | 1.25 | 30.2 |
| 5 | T1 | 215 | 11.0 | 0.903 | 54.9 | LOS D | 23.5 | 195.6 | 1.00 | 1.03 | 1.25 | 31.1 |
| 6 | R2 | 364 | 17.0 | 0.612 | 22.2 | LOS B | 10.3 | 82.9 | 0.73 | 0.78 | 0.73 | 43.2 |
| Appr |  | 753 | 19.7 | 0.903 | 40.4 | LOS C | 23.5 | 195.6 | 0.87 | 0.91 | 1.00 | 35.7 |
| North: Wallgrove Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 455 | 29.0 | 0.551 | 23.8 | LOS B | 16.0 | 139.7 | 0.71 | 0.80 | 0.71 | 41.7 |
| 8 | T1 | 666 | 12.0 | 0.906 | 51.3 | LOS D | 25.4 | 196.0 | 0.98 | 0.97 | 1.16 | 32.6 |
| 9 | R2 | 76 | 7.0 | 0.221 | 34.2 | LOS C | 3.0 | 22.2 | 0.80 | 0.73 | 0.80 | 37.6 |
| Appr |  | 1197 | 18.1 | 0.906 | 39.8 | LOS C | 25.4 | 196.0 | 0.86 | 0.89 | 0.97 | 35.9 |
| West: The Horsley Drive (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 42 | 16.0 | 0.414 | 42.8 | LOS D | 8.4 | 64.4 | 0.88 | 0.75 | 0.88 | 36.0 |
| 11 | T1 | 145 | 9.0 | 0.414 | 37.1 | LOS C | 8.4 | 64.4 | 0.88 | 0.75 | 0.88 | 36.9 |
| 12 | R2 | 52 | 18.0 | 0.115 | 24.0 | LOS B | 1.3 | 10.9 | 0.79 | 0.71 | 0.79 | 42.2 |
| Appr |  | 239 | 12.2 | 0.414 | 35.3 | LOS C | 8.4 | 64.4 | 0.86 | 0.74 | 0.86 | 37.8 |
| All V | icles | 2578 | 16.3 | 0.906 | 36.3 | LOS C | 25.4 | 196.0 | 0.82 | 0.83 | 0.91 | 37.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Back Pedestrian ped | of Queue Distance m | Prop. Queued | Effective Stop Rate |
| P1 | South Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P2 | East Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P3 | North Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P4 | West Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| All Pedestrians |  | 4 | 49.2 | LOS E |  |  | 0.95 | 0.95 |

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## PHASING SUMMARY

## Site: 101 [PM Existing + S1 Wallgrove Rd/ The Horsley Drive]

New Site
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time = 110 seconds (Site User-Given Cycle Time)
Variable Sequence Analysis applied. The results are given for the selected output sequence.
Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: TCS
Reference Phase: Phase A
Input Phase Sequence: A, B*, C*, D, D1*, D2*, E, F1*, F2*, G, G1*, G2*
Output Phase Sequence: A, D, E, G
(*Variable Phase)

| Phase Timing Summary |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Phase | A | D | E | G |
| Phase Change Time (sec) | 0 | 33 | 65 | 98 |
| Green Time (sec) | 27 | 26 | 27 | 6 |
| Phase Time (sec) | 33 | 32 | 33 | 12 |
| Phase Split | $30 \%$ | $29 \%$ | $30 \%$ | $11 \%$ |

See the Phase Information section in the Detailed Output report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Phase Actuation and Phase Frequency values (user-specified or implied) less than 100\%.


Phase G


REF: Reference Phase
VAR: Variable Phase
$\square$ Stopped Movement
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs

Other Movement Class (MC) Stopped $\quad$|  |
| :---: |
| $\square$ |

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## MOVEMENT SUMMARY

## Site: 101 [AM Existing + S1 Wallgrove Rd/ The Horsley Drive]

New Site
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time = 110 seconds (Site Optimum Cycle Time - Minimum Delay) Variable Sequence Analysis applied. The results are given for the selected output sequence.

Movement Performance - Vehicles

| Mov ID | Turn | Deman <br> Total veh/h |  | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| South: Wallgrove Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 57 | 0.0 | 0.102 | 35.2 | LOS C | 2.2 | 15.4 | 0.76 | 0.72 | 0.76 | 37.4 |
| 2 | T1 | 613 | 7.0 | 1.140 | 133.9 | LOS F | 40.5 | 300.6 | 1.00 | 1.40 | 1.93 | 18.4 |
| 3 | R2 | 181 | 8.0 | 0.282 | 24.3 | LOS B | 5.7 | 42.3 | 0.74 | 0.76 | 0.74 | 41.9 |
| Appr |  | 851 | 6.7 | 1.140 | 104.0 | LOS F | 40.5 | 300.6 | 0.93 | 1.22 | 1.59 | 21.8 |
| East: The Horsley Drive (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 56 | 36.0 | 1.917 | 857.2 | LOS F | 57.4 | 459.2 | 1.00 | 2.11 | 5.05 | 3.8 |
| 5 | T1 | 189 | 11.0 | 1.917 | 851.2 | LOS F | 57.4 | 459.2 | 1.00 | 2.11 | 5.05 | 3.8 |
| 6 | R2 | 404 | 17.0 | 0.980 | 79.8 | LOS F | 23.9 | 191.7 | 1.00 | 1.24 | 1.84 | 25.7 |
| Appr |  | 649 | 16.9 | 1.917 | 371.6 | LOS F | 57.4 | 459.2 | 1.00 | 1.57 | 3.05 | 8.1 |
| North: Wallgrove Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 242 | 29.0 | 1.153 | 184.6 | LOS F | 26.3 | 229.8 | 1.00 | 1.41 | 2.54 | 12.9 |
| 8 | T1 | 225 | 12.0 | 1.377 | 263.6 | LOS F | 23.5 | 181.5 | 1.00 | 1.46 | 2.79 | 10.9 |
| 9 | R2 | 41 | 7.0 | 0.076 | 29.7 | LOS C | 1.4 | 10.5 | 0.75 | 0.71 | 0.75 | 39.4 |
| Appr |  | 508 | 19.7 | 1.377 | 207.1 | LOS F | 26.3 | 229.8 | 0.98 | 1.38 | 2.50 | 12.6 |
| West: The Horsley Drive (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 49 | 16.0 | 1.819 | 776.0 | LOS F | 64.5 | 491.2 | 1.00 | 2.25 | 4.87 | 4.2 |
| 11 | T1 | 232 | 9.0 | 1.819 | 770.3 | LOS F | 64.5 | 491.2 | 1.00 | 2.25 | 4.87 | 4.2 |
| 12 | R2 | 37 | 18.0 | 0.072 | 28.3 | LOS B | 1.3 | 10.2 | 0.69 | 0.68 | 0.69 | 40.2 |
| Appr |  | 318 | 11.1 | 1.819 | 684.8 | LOS F | 64.5 | 491.2 | 0.96 | 2.07 | 4.38 | 4.7 |
| All V | icles | 2326 | 13.0 | 1.917 | 280.6 | LOS F | 64.5 | 491.2 | 0.96 | 1.47 | 2.58 | 10.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Back Pedestrian ped | of Queue Distance m | Prop. Queued | Effective Stop Rate |
| P1 | South Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P2 | East Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P3 | North Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P4 | West Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| All Pedestrians |  | 4 | 49.2 | LOS E |  |  | 0.95 | 0.95 |

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## PHASING SUMMARY

## Site: 101 [AM Existing + S1 Wallgrove Rd/ The Horsley Drive]

New Site
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time = 110 seconds (Site Optimum Cycle Time - Minimum Delay) Variable Sequence Analysis applied. The results are given for the selected output sequence.

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: TCS - Copy
Reference Phase: Phase A
Input Phase Sequence: A, C*, D, E, G
Output Phase Sequence: A, C*, D, E, G
(* Variable Phase)

| Phase Timing Summary |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Phase | A | C | D | E | G |
| Phase Change Time (sec) | 0 | 12 | 24 | 39 | 75 |
| Green Time $(\mathbf{s e c})$ | 6 | 6 | 9 | 30 | 29 |
| Phase Time $(\mathbf{s e c})$ | 12 | 12 | 15 | 36 | 35 |
| Phase Split | $11 \%$ | $11 \%$ | $14 \%$ | $33 \%$ | $32 \%$ |

See the Phase Information section in the Detailed Output report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
$\square$ Stopped Movement
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs

Other Movement Class (MC) Stopped $\quad$|  |
| :---: |
| $\square$ |

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## MOVEMENT SUMMARY

## Site: 101 [PM Existing Wallgrove Rd/ The Horsley Drive]

Data from 26/7/18
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time = 110 seconds (Site User-Given Cycle Time)
Variable Sequence Analysis applied. The results are given for the selected output sequence.

Movement Performance - Vehicles

| Mov ID | Turn | Demand Total veh/h | Fows HV \% | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| South: Wallgrove Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 28 | 7.0 | 0.060 | 38.0 | LOS C | 1.1 | 8.3 | 0.78 | 0.70 | 0.78 | 36.2 |
| 2 | T1 | 257 | 8.0 | 0.509 | 46.7 | LOS D | 7.4 | 55.2 | 0.96 | 0.77 | 0.96 | 34.0 |
| 3 | R2 | 58 | 14.0 | 0.295 | 35.3 | LOS C | 2.1 | 16.8 | 0.94 | 0.74 | 0.94 | 37.1 |
| Appr |  | 343 | 8.9 | 0.509 | 44.1 | LOS D | 7.4 | 55.2 | 0.94 | 0.76 | 0.94 | 34.7 |
| East: The Horsley Drive (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 125 | 8.0 | 0.816 | 52.4 | LOS D | 18.1 | 138.2 | 0.98 | 0.92 | 1.09 | 32.7 |
| 5 | T1 | 215 | 12.0 | 0.816 | 46.7 | LOS D | 18.1 | 138.2 | 0.98 | 0.92 | 1.09 | 33.4 |
| 6 | R2 | 364 | 11.0 | 0.609 | 24.5 | LOS B | 11.0 | 84.5 | 0.78 | 0.79 | 0.78 | 42.1 |
| Appr | ach | 704 | 10.8 | 0.816 | 36.2 | LOS C | 18.1 | 138.2 | 0.88 | 0.85 | 0.93 | 37.2 |
| North: Wallgrove Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 455 | 15.0 | 0.466 | 19.8 | LOS B | 13.9 | 109.5 | 0.62 | 0.77 | 0.62 | 44.0 |
| 8 | T1 | 666 | 6.0 | 0.813 | 42.4 | LOS C | 21.9 | 160.9 | 0.96 | 0.88 | 1.03 | 35.4 |
| 9 | R2 | 76 | 9.0 | 0.179 | 30.7 | LOS C | 2.7 | 20.2 | 0.81 | 0.74 | 0.81 | 39.0 |
| Appr | ach | 1197 | 9.6 | 0.813 | 33.1 | LOS C | 21.9 | 160.9 | 0.82 | 0.83 | 0.86 | 38.5 |
| West: The Horsley Drive (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 42 | 12.0 | 0.529 | 48.9 | LOS D | 9.2 | 69.8 | 0.95 | 0.79 | 0.95 | 34.0 |
| 11 | T1 | 145 | 10.0 | 0.529 | 43.2 | LOS D | 9.2 | 69.8 | 0.95 | 0.79 | 0.95 | 34.8 |
| 12 | R2 | 45 | 7.0 | 0.117 | 25.8 | LOS B | 1.3 | 9.7 | 0.81 | 0.71 | 0.81 | 41.6 |
| Appr | ach | 232 | 9.8 | 0.529 | 40.8 | LOS C | 9.2 | 69.8 | 0.92 | 0.77 | 0.92 | 35.8 |
| All V | icles | 2476 | 9.9 | 0.816 | 36.2 | LOS C | 21.9 | 160.9 | 0.86 | 0.82 | 0.90 | 37.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Back Pedestrian ped | of Queue Distance m | Prop. Queued | Effective Stop Rate |
| P1 | South Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P2 | East Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P3 | North Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P4 | West Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| All Pedestrians |  | 4 | 49.2 | LOS E |  |  | 0.95 | 0.95 |

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## PHASING SUMMARY

## Site: 101 [PM Existing Wallgrove Rd/ The Horsley Drive]

Data from 26/7/18
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time = 110 seconds (Site User-Given Cycle Time)
Variable Sequence Analysis applied. The results are given for the selected output sequence.
Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program

## Phase Sequence: TCS

Reference Phase: Phase A

Output Phase Sequence: A, D, D1*, E, G, G1*
(*Variable Phase)

| Phase Timing Summary |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Phase | A | D | D1 | E | G | G1 |
| Phase Change Time (sec) | 0 | 23 | 35 | 58 | 85 | 98 |
| Green Time (sec) | 17 | 6 | 17 | 21 | 7 | 6 |
| Phase Time (sec) | 23 | 12 | 23 | 27 | 13 | 12 |
| Phase Split | $21 \%$ | $11 \%$ | $21 \%$ | $25 \%$ | $12 \%$ | $11 \%$ |

See the Phase Information section in the Detailed Output report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.

| Output Phase Sequence |  |  |
| :---: | :---: | :---: |
| Phase A | Phase D |  |
| Phase E | Phase G |  |

REF: Reference Phase
VAR: Variable Phase
$\square$ Stopped Movement
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs

Other Movement Class (MC) Stopped $\quad$|  |
| :---: |
| $\square$ |

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## MOVEMENT SUMMARY

## Site: 101 [PM Existing+10yr Gr Wallgrove Rd/ The Horsley Drive]

New Site
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time $=130$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman <br> Total <br> veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: Wallgrove Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 51 | 7.0 | 0.058 | 23.2 | LOS B | 1.6 | 12.1 | 0.54 | 0.69 | 0.54 | 42.5 |
| 2 | T1 | 298 | 8.0 | 0.424 | 47.2 | LOS D | 9.3 | 69.7 | 0.90 | 0.74 | 0.90 | 33.8 |
| 3 | R2 | 58 | 14.0 | 0.308 | 43.5 | LOS D | 2.7 | 20.8 | 0.97 | 0.74 | 0.97 | 34.2 |
| Appr |  | 407 | 8.7 | 0.424 | 43.6 | LOS D | 9.3 | 69.7 | 0.87 | 0.73 | 0.87 | 34.8 |
| East: The Horsley Drive (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 128 | 8.0 | 0.994 | 95.2 | LOS F | 44.8 | 343.4 | 1.00 | 1.19 | 1.44 | 23.8 |
| 5 | T1 | 389 | 12.0 | 0.994 | 89.5 | LOS F | 44.8 | 343.4 | 1.00 | 1.19 | 1.44 | 24.1 |
| 6 | R2 | 422 | 11.0 | 0.643 | 22.2 | LOS B | 13.2 | 100.9 | 0.70 | 0.78 | 0.70 | 43.3 |
| Appr |  | 939 | 11.0 | 0.994 | 60.0 | LOS E | 44.8 | 343.4 | 0.87 | 1.01 | 1.11 | 30.1 |
| North: Wallgrove Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 455 | 15.0 | 0.542 | 29.4 | LOS C | 19.6 | 154.6 | 0.74 | 0.81 | 0.74 | 39.4 |
| 8 | T1 | 679 | 6.0 | 1.029 | 91.8 | LOS F | 39.7 | 292.2 | 0.99 | 1.15 | 1.41 | 23.8 |
| 9 | R2 | 138 | 9.0 | 0.464 | 42.1 | LOS C | 6.7 | 50.3 | 0.90 | 0.78 | 0.90 | 34.8 |
| Appr |  | 1272 | 9.5 | 1.029 | 64.1 | LOS E | 39.7 | 292.2 | 0.89 | 0.99 | 1.11 | 28.9 |
| West: The Horsley Drive (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 49 | 12.0 | 0.372 | 44.9 | LOS D | 9.7 | 74.4 | 0.84 | 0.73 | 0.84 | 35.3 |
| 11 | T1 | 145 | 10.0 | 0.372 | 39.2 | LOS C | 9.7 | 74.4 | 0.84 | 0.73 | 0.84 | 36.1 |
| 12 | R2 | 46 | 7.0 | 0.096 | 26.3 | LOS B | 1.3 | 9.5 | 0.79 | 0.70 | 0.79 | 41.3 |
| Approach |  | 240 | 9.8 | 0.372 | 37.9 | LOS C | 9.7 | 74.4 | 0.83 | 0.72 | 0.83 | 36.8 |
| All Vehicles |  | 2858 | 9.9 | 1.029 | 57.7 | LOS E | 44.8 | 343.4 | 0.87 | 0.93 | 1.05 | 30.6 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Description | Demand Flow ped/h | Average Delay $\qquad$ sec | Level of Service | Average Back Pedestrian $\qquad$ | of Queue Distance $\qquad$ | Prop. Queued | Effective Stop Rate |
| P1 | South Full Crossing | 1 | 59.1 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P2 | East Full Crossing | 1 | 59.1 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P3 | North Full Crossing | 1 | 59.1 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P4 | West Full Crossing | 1 | 59.1 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| All Pedestrians |  | 4 | 59.1 | LOS E |  |  | 0.95 | 0.95 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## PHASING SUMMARY

## Site: 101 [PM Existing+ 10yr Gr Wallgrove Rd/ The Horsley Drive]

New Site
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time $=130$ seconds (Site Optimum Cycle Time - Minimum Delay)
Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Green Split Priority has been specified
Phase Sequence: TCS - Cut Down
Reference Phase: Phase A
Input Phase Sequence: A, D, E, G
Output Phase Sequence: A, D, E, G

## Phase Timing Summary

| Phase | A | D | E | G |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 0 | 34 | 71 | 114 |
| Green Time (sec) | 28 | 31 | 37 | 10 |
| Phase Time (sec) | 34 | 37 | 43 | 16 |
| Phase Split | $26 \%$ | $28 \%$ | $33 \%$ | $12 \%$ |

See the Phase Information section in the Detailed Output report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.

| Output Phase Sequence |  |  |
| :---: | :---: | :---: |
|  | Phase D | Phase E |
| Phase G |  |  |

REF: Reference Phase
VAR: Variable Phase

| $\longrightarrow$ Normal Movement | Slip/Bypass-Lane Movement |
| :--- | :--- |$\quad$| Permitted/Opposed |
| :--- |
| Opposed Slip/Bypass-Lane |

$\square$ Stopped Movement
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs

Other Movement Class (MC) Stopped $\quad$|  |
| :---: |
| $\square$ |

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## MOVEMENT SUMMARY

## Site: 101 [AM Existing+ 10yr Gr Wallgrove Rd/ The Horsley Drive]

New Site
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time = 110 seconds (Site Optimum Cycle Time - Minimum Delay) Variable Sequence Analysis applied. The results are given for the selected output sequence.

Movement Performance - Vehicles

| Mov ID | Turn | Demand <br> Total <br> veh/h | lows HV $\%$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| South: Wallgrove Road (S) 0 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 50 | 0.0 | 0.067 | 19.6 | LOS B | 1.3 | 9.1 | 0.64 | 0.69 | 0.64 | 44.5 |
| 2 | T1 | 613 | 7.0 | 0.790 | 43.9 | LOS D | 18.7 | 139.0 | 0.98 | 0.87 | 1.03 | 34.9 |
| 3 | R2 | 132 | 8.0 | 0.326 | 34.7 | LOS C | 5.1 | 38.2 | 0.88 | 0.77 | 0.88 | 37.4 |
| Appr |  | 795 | 6.7 | 0.790 | 40.8 | LOS C | 18.7 | 139.0 | 0.94 | 0.84 | 0.98 | 35.8 |
| East: The Horsley Drive (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 25 | 36.0 | 0.609 | 49.5 | LOS D | 10.0 | 78.4 | 0.92 | 0.79 | 1.08 | 33.8 |
| 5 | T1 | 189 | 11.0 | 0.609 | 43.5 | LOS D | 10.0 | 78.4 | 0.92 | 0.79 | 1.08 | 34.9 |
| 6 | R2 | 404 | 17.0 | 0.656 | 29.0 | LOS C | 14.6 | 117.3 | 0.78 | 0.80 | 0.78 | 39.9 |
| Appr |  | 618 | 15.9 | 0.656 | 34.3 | LOS C | 14.6 | 117.3 | 0.83 | 0.80 | 0.89 | 38.0 |
| North: Wallgrove Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 242 | 29.0 | 0.346 | 26.7 | LOS B | 8.4 | 73.2 | 0.69 | 0.77 | 0.69 | 40.4 |
| 8 | T1 | 225 | 12.0 | 0.751 | 55.1 | LOS D | 7.7 | 59.4 | 1.00 | 0.84 | 1.10 | 31.5 |
| 9 | R2 | 41 | 7.0 | 0.217 | 37.0 | LOS C | 1.6 | 11.8 | 0.94 | 0.73 | 0.94 | 36.6 |
| Appr |  | 508 | 19.7 | 0.751 | 40.1 | LOS C | 8.4 | 73.2 | 0.85 | 0.80 | 0.89 | 35.6 |
| West: The Horsley Drive (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 49 | 16.0 | 0.798 | 55.8 | LOS D | 15.6 | 118.7 | 1.00 | 0.94 | 1.14 | 32.0 |
| 11 | T1 | 232 | 9.0 | 0.798 | 50.1 | LOS D | 15.6 | 118.7 | 1.00 | 0.94 | 1.14 | 32.8 |
| 12 | R2 | 22 | 18.0 | 0.064 | 24.6 | LOS B | 0.6 | 4.7 | 0.79 | 0.68 | 0.79 | 41.9 |
| Appr |  | 303 | 10.8 | 0.798 | 49.2 | LOS D | 15.6 | 118.7 | 0.98 | 0.92 | 1.12 | 33.2 |
| All V | icles | 2224 | 12.8 | 0.798 | 40.0 | LOS C | 18.7 | 139.0 | 0.89 | 0.83 | 0.95 | 35.9 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Back Pedestrian ped | of Queue Distance m | Prop. Queued | Effective Stop Rate |
| P1 | South Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P2 | East Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P3 | North Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P4 | West Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| All Pedestrians |  | 4 | 49.2 | LOS E |  |  | 0.95 | 0.95 |

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## PHASING SUMMARY

## Site: 101 [AM Existing+ 10yr Gr Wallgrove Rd/ The Horsley Drive]

New Site
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time = 110 seconds (Site Optimum Cycle Time - Minimum Delay) Variable Sequence Analysis applied. The results are given for the selected output sequence.

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: TCS
Reference Phase: Phase A

Output Phase Sequence: A, D, D1*, E, F2*, G, G2*
(* Variable Phase)

| Phase Timing Summary |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Phase | A | D | D1 | E | F2 | G | G2 |
| Phase Change Time (sec) | 0 | 17 | 29 | 56 | 71 | 83 | 95 |
| Green Time (sec) | 11 | 6 | 21 | 9 | 6 | 6 | 9 |
| Phase Time (sec) | 17 | 12 | 27 | 15 | 12 | 12 | 15 |
| Phase Split | 15\% | 11\% | 25\% | 14\% | 11\% | 11\% | 14\% |

See the Phase Information section in the Detailed Output report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.

| O |  |  |
| :---: | :---: | :---: |
| Phase A <br> Wallgrove Road <br> (N) <br> (S) | Phase D |  |
| Phase E |  | Phase G |


| Phase G2 | VAR |
| :--- | :--- | :--- |
|  |  |
| Wallgrove Road |  |
| (N) |  |

REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement
Other Movement Class (MC) Running

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## MOVEMENT SUMMARY

## Site: 101 [AM Existing+ 10yr Gr Wallgrove Rd/ The Horsley Drive - Upgraded]

New Site
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time = 110 seconds (Site Optimum Cycle Time - Minimum Delay) Variable Sequence Analysis applied. The results are given for the selected output sequence.

Movement Performance - Vehicles

| Mov ID | Turn | Demand <br> Total veh/h | $\begin{array}{r} \text { lows } \\ \text { HV } \\ \hline \end{array}$ | Deg. Satn v/c | Average Delay | Level of Service | 95\% Back <br> Vehicles <br> veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| South: Wallgrove Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 50 | 0.0 | 0.064 | 18.3 | LOS B | 1.2 | 8.5 | 0.62 | 0.69 | 0.62 | 45.2 |
| 2 | T1 | 613 | 7.0 | 0.813 | 45.6 | LOS D | 19.1 | 141.4 | 0.98 | 0.89 | 1.06 | 34.4 |
| 3 | R2 | 132 | 8.0 | 0.391 | 36.2 | LOS C | 5.2 | 39.2 | 0.92 | 0.78 | 0.92 | 37.0 |
| Appr |  | 795 | 6.7 | 0.813 | 42.3 | LOS C | 19.1 | 141.4 | 0.95 | 0.86 | 1.01 | 35.3 |
| East: The Horsley Drive (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 25 | 36.0 | 0.085 | 32.5 | LOS C | 0.8 | 7.6 | 0.78 | 0.69 | 0.78 | 37.8 |
| 5 | T1 | 189 | 11.0 | 0.336 | 30.9 | LOS C | 6.9 | 53.1 | 0.72 | 0.60 | 0.72 | 39.9 |
| 6 | R2 | 404 | 17.0 | 0.667 | 31.0 | LOS C | 15.3 | 122.6 | 0.81 | 0.81 | 0.81 | 39.1 |
| Appr | ach | 618 | 15.9 | 0.667 | 31.0 | LOS C | 15.3 | 122.6 | 0.78 | 0.74 | 0.78 | 39.3 |
| North: Wallgrove Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 242 | 29.0 | 0.314 | 23.3 | LOS B | 7.7 | 66.9 | 0.63 | 0.75 | 0.63 | 41.9 |
| 8 | T1 | 225 | 12.0 | 0.545 | 48.7 | LOS D | 7.0 | 53.7 | 0.97 | 0.77 | 0.97 | 33.4 |
| 9 | R2 | 41 | 7.0 | 0.224 | 37.8 | LOS C | 1.6 | 12.0 | 0.95 | 0.73 | 0.95 | 36.3 |
| Appr |  | 508 | 19.7 | 0.545 | 35.7 | LOS C | 7.7 | 66.9 | 0.81 | 0.76 | 0.81 | 37.2 |
| West: The Horsley Drive (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 49 | 16.0 | 0.798 | 55.8 | LOS D | 15.6 | 118.7 | 1.00 | 0.94 | 1.14 | 32.0 |
| 11 | T1 | 232 | 9.0 | 0.798 | 50.1 | LOS D | 15.6 | 118.7 | 1.00 | 0.94 | 1.14 | 32.8 |
| 12 | R2 | 22 | 18.0 | 0.064 | 24.8 | LOS B | 0.6 | 4.6 | 0.80 | 0.68 | 0.80 | 41.8 |
| Appr |  | 303 | 10.8 | 0.798 | 49.2 | LOS D | 15.6 | 118.7 | 0.99 | 0.92 | 1.12 | 33.2 |
| All Ve | icles | 2224 | 12.8 | 0.813 | 38.6 | LOS C | 19.1 | 141.4 | 0.88 | 0.81 | 0.92 | 36.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Back Pedestrian ped | of Queue Distance m | Prop. Queued | Effective Stop Rate |
| P1 | South Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P2 | East Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P3 | North Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P4 | West Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| All Pedestrians |  | 4 | 49.2 | LOS E |  |  | 0.95 | 0.95 |

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## PHASING SUMMARY

## Site: 101 [AM Existing+ 10yr Gr Wallgrove Rd/ The Horsley Drive - Upgraded]

New Site
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time = 110 seconds (Site Optimum Cycle Time - Minimum Delay) Variable Sequence Analysis applied. The results are given for the selected output sequence.

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: TCS
Reference Phase: Phase A
Input Phase Sequence: A, B*, C ${ }^{*}$, D, D1 ${ }^{*}$, D2 ${ }^{*}$, E, F1*, F2 $^{*}$, G, G1*, G2*
Output Phase Sequence: A, D, D1*, E, F2*, G, G2*
(* Variable Phase)

| Phase Timing Summary |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Phase | A | D | D1 | E | F2 | G | G2 |
| Phase Change Time (sec) | 0 | 21 | 33 | 61 | 73 | 88 | 100 |
| Green Time $(\mathbf{s e c})$ | 15 | 6 | 22 | 6 | 9 | 6 | 4 |
| Phase Time $(\mathrm{sec})$ | 21 | 12 | 28 | 12 | 15 | 12 | 10 |
| Phase Split | $19 \%$ | $11 \%$ | $25 \%$ | $11 \%$ | $14 \%$ | $11 \%$ | $9 \%$ |

See the Phase Information section in the Detailed Output report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.

| O |  |  |
| :---: | :---: | :---: |
| Phase A <br> Wallgrove Road <br> (N) <br> (S) | Phase D |  |
| Phase E |  | Phase G |


| Phase G2 | VAR |
| :--- | :--- | :--- |
|  |  |
| Wallgrove Road |  |
| (N) |  |

REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement
Other Movement Class (MC) Running

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## MOVEMENT SUMMARY

## Site: 101 [PM Existing+ 10yr Gr Wallgrove Rd/ The Horsley Drive - Upgraded]

New Site
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time $=125$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman <br> Total <br> veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: Wallgrove Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 51 | 7.0 | 0.051 | 18.7 | LOS B | 1.4 | 10.2 | 0.48 | 0.67 | 0.48 | 44.8 |
| 2 | T1 | 298 | 8.0 | 0.377 | 42.4 | LOS C | 8.6 | 64.1 | 0.87 | 0.71 | 0.87 | 35.4 |
| 3 | R2 | 58 | 14.0 | 0.293 | 40.0 | LOS C | 2.4 | 19.1 | 0.96 | 0.74 | 0.96 | 35.6 |
| Appr |  | 407 | 8.7 | 0.377 | 39.1 | LOS C | 8.6 | 64.1 | 0.84 | 0.71 | 0.84 | 36.4 |
| East: The Horsley Drive (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 128 | 8.0 | 0.212 | 35.0 | LOS C | 4.6 | 34.7 | 0.63 | 0.73 | 0.63 | 37.3 |
| 5 | T1 | 389 | 12.0 | 0.996 | 92.5 | LOS F | 32.5 | 251.0 | 1.00 | 1.23 | 1.51 | 23.9 |
| 6 | R2 | 422 | 11.0 | 0.667 | 24.8 | LOS B | 14.1 | 108.2 | 0.77 | 0.80 | 0.77 | 42.0 |
| Appr |  | 939 | 11.0 | 0.996 | 54.2 | LOS D | 32.5 | 251.0 | 0.85 | 0.97 | 1.06 | 31.6 |
| North: Wallgrove Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 455 | 15.0 | 0.484 | 23.3 | LOS B | 16.5 | 130.5 | 0.65 | 0.78 | 0.65 | 42.2 |
| 8 | T1 | 679 | 6.0 | 0.903 | 56.6 | LOS E | 28.2 | 207.8 | 0.98 | 0.96 | 1.13 | 31.2 |
| 9 | R2 | 138 | 9.0 | 0.418 | 37.7 | LOS C | 6.1 | 46.2 | 0.86 | 0.77 | 0.86 | 36.3 |
| Appr |  | 1272 | 9.5 | 0.903 | 42.7 | LOS D | 28.2 | 207.8 | 0.85 | 0.87 | 0.93 | 35.0 |
| West: The Horsley Drive (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 49 | 12.0 | 0.487 | 51.6 | LOS D | 10.4 | 79.4 | 0.92 | 0.78 | 0.92 | 33.2 |
| 11 | T1 | 145 | 10.0 | 0.487 | 45.9 | LOS D | 10.4 | 79.4 | 0.92 | 0.78 | 0.92 | 33.9 |
| 12 | R2 | 46 | 7.0 | 0.085 | 24.8 | LOS B | 1.3 | 9.8 | 0.75 | 0.70 | 0.75 | 42.1 |
| Approach |  | 240 | 9.8 | 0.487 | 43.0 | LOS D | 10.4 | 79.4 | 0.89 | 0.76 | 0.89 | 35.0 |
| All Vehicles |  | 2858 | 9.9 | 0.996 | 46.0 | LOS D | 32.5 | 251.0 | 0.85 | 0.87 | 0.96 | 34.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Description | $\begin{aligned} & \text { Demand } \\ & \text { Flow } \\ & \text { ped/h } \end{aligned}$ | Average Delay sec $\qquad$ | Level of Service | Average Back Pedestrian $\qquad$ | of Queue Distance $\qquad$ | Prop. Queued | Effective Stop Rate |
| P1 | South Full Crossing | 1 | 56.6 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P2 | East Full Crossing | 1 | 56.6 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P3 | North Full Crossing | 1 | 56.6 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P4 | West Full Crossing | 1 | 56.6 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| All Pedestrians |  | 4 | 56.6 | LOS E |  |  | 0.95 | 0.95 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## PHASING SUMMARY

## Site: 101 [PM Existing+ 10yr Gr Wallgrove Rd/ The Horsley Drive - Upgraded]

New Site
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time $=125$ seconds (Site Optimum Cycle Time - Minimum Delay)
Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Green Split Priority has been specified
Phase Sequence: TCS - Cut Down
Reference Phase: Phase A
Input Phase Sequence: A, D, E, G
Output Phase Sequence: A, D, E, G

## Phase Timing Summary

| Phase | A | D | E | G |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 0 | 36 | 76 | 109 |
| Green Time (sec) | 30 | 34 | 27 | 10 |
| Phase Time (sec) | 36 | 40 | 33 | 16 |
| Phase Split | $29 \%$ | $32 \%$ | $26 \%$ | $13 \%$ |

See the Phase Information section in the Detailed Output report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.

| Output Phase Sequence |  |  |
| :---: | :---: | :---: |
|  | Phase D | Phase E |
| Phase G |  |  |

REF: Reference Phase
VAR: Variable Phase
$\longrightarrow$ Normal Movement $\quad \longrightarrow$ Slip/Bypass-Lane Movement $\quad$ Permitted/Opposed
$\square$ Stopped Movement
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs

Other Movement Class (MC) Stopped $\quad$|  |
| :---: |
| $\square$ |

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## MOVEMENT SUMMARY

## Site: 101 [AM Existing+ 10y Gr + S2 Wallgrove Rd/ The Horsley Drive - Upgraded]

New Site
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time $=110$ seconds (Site Optimum Cycle Time - Minimum Delay) Variable Sequence Analysis applied. The results are given for the selected output sequence.

Movement Performance - Vehicles


Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Back Pedestrian ped | f Queue Distance m | Prop. Queued | Effective Stop Rate |
| P1 | South Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P2 | East Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P3 | North Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P4 | West Full Crossing | 1 | 49.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| All Pedestrians |  | 4 | 49.2 | LOS E |  |  | 0.95 | 0.95 |

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## PHASING SUMMARY

## Site: 101 [AM Existing+ 10y Gr + S2 Wallgrove Rd/ The Horsley Drive - Upgraded]

New Site
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time = 110 seconds (Site Optimum Cycle Time - Minimum Delay) Variable Sequence Analysis applied. The results are given for the selected output sequence.

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: TCS
Reference Phase: Phase A

Output Phase Sequence: A, D, D1*, E, F2*, G, G2*
(* Variable Phase)

| Phase Timing Summary |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Phase | A | D | D1 | E | F2 | G | G2 |
| Phase Change Time (sec) | 0 | 17 | 32 | 55 | 72 | 84 | 96 |
| Green Time $(\mathbf{s e c})$ | 11 | 9 | 17 | 11 | 6 | 6 | 8 |
| Phase Time $(\mathbf{s e c})$ | 17 | 15 | 23 | 17 | 12 | 12 | 14 |
| Phase Split | $15 \%$ | $14 \%$ | $21 \%$ | $15 \%$ | $11 \%$ | $11 \%$ | $13 \%$ |

See the Phase Information section in the Detailed Output report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.

| O |  |  |
| :---: | :---: | :---: |
| Phase A <br> Wallgrove Road <br> (N) <br> (S) | Phase D |  |
| Phase E |  | Phase G |


| Phase G2 | VAR |
| :--- | :--- | :--- |
|  |  |
| Wallgrove Road |  |
| (N) |  |

REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement
Other Movement Class (MC) Running

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## MOVEMENT SUMMARY

## Site: 101 [PM Existing+ 10y Gr + S2 Wallgrove Rd/ The Horsley Drive - Upgraded]

New Site
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time $=125$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| South: Wallgrove Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 61 | 7.0 | 0.062 | 18.8 | LOS B | 1.7 | 12.3 | 0.48 | 0.68 | 0.48 | 44.7 |
| 2 | T1 | 298 | 8.0 | 0.377 | 42.4 | LOS C | 8.6 | 64.1 | 0.87 | 0.71 | 0.87 | 35.4 |
| 3 | R2 | 119 | 14.0 | 0.602 | 41.7 | LOS C | 5.2 | 41.1 | 1.00 | 0.79 | 1.01 | 35.0 |
| Appr |  | 478 | 9.4 | 0.602 | 39.2 | LOS C | 8.6 | 64.1 | 0.85 | 0.73 | 0.86 | 36.3 |
| East: The Horsley Drive (E) |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 223 | 8.0 | 0.369 | 37.0 | LOS C | 8.8 | 66.0 | 0.69 | 0.76 | 0.69 | 36.6 |
| 5 | T1 | 389 | 12.0 | 0.996 | 92.5 | LOS F | 32.5 | 251.0 | 1.00 | 1.23 | 1.51 | 23.9 |
| 6 | R2 | 422 | 11.0 | 0.667 | 24.8 | LOS B | 14.1 | 108.2 | 0.77 | 0.80 | 0.77 | 42.0 |
| Appr |  | 1034 | 10.7 | 0.996 | 52.9 | LOS D | 32.5 | 251.0 | 0.84 | 0.95 | 1.03 | 31.9 |
| North: Wallgrove Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 455 | 15.0 | 0.484 | 23.3 | LOS B | 16.5 | 130.5 | 0.65 | 0.78 | 0.65 | 42.2 |
| 8 | T1 | 679 | 6.0 | 0.903 | 56.6 | LOS E | 28.2 | 207.8 | 0.98 | 0.96 | 1.13 | 31.2 |
| 9 | R2 | 138 | 9.0 | 0.420 | 37.7 | LOS C | 6.1 | 46.2 | 0.86 | 0.77 | 0.86 | 36.3 |
| Appr |  | 1272 | 9.5 | 0.903 | 42.7 | LOS D | 28.2 | 207.8 | 0.85 | 0.87 | 0.93 | 35.0 |
| West: The Horsley Drive (W) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 49 | 12.0 | 0.487 | 51.6 | LOS D | 10.4 | 79.4 | 0.92 | 0.78 | 0.92 | 33.2 |
| 11 | T1 | 145 | 10.0 | 0.487 | 45.9 | LOS D | 10.4 | 79.4 | 0.92 | 0.78 | 0.92 | 33.9 |
| 12 | R2 | 60 | 7.0 | 0.110 | 24.9 | LOS B | 1.7 | 13.0 | 0.76 | 0.71 | 0.76 | 42.0 |
| Approach |  | 254 | 9.7 | 0.487 | 42.0 | LOS C | 10.4 | 79.4 | 0.88 | 0.76 | 0.88 | 35.3 |
| All V | icles | 3038 | 9.9 | 0.996 | 45.6 | LOS D | 32.5 | 251.0 | 0.85 | 0.87 | 0.95 | 34.1 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Description | $\begin{aligned} & \text { Demand } \\ & \text { Flow } \\ & \text { ped } / \mathrm{h} \end{aligned}$ | Average Delay $\qquad$ sec | Level of Service | Average Back Pedestrian $\qquad$ | of Queue Distance $\qquad$ | Prop. Queued | Effective Stop Rate |
| P1 | South Full Crossing | 1 | 56.6 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P2 | East Full Crossing | 1 | 56.6 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P3 | North Full Crossing | 1 | 56.6 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P4 | West Full Crossing | 1 | 56.6 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| All Pedestrians |  | 4 | 56.6 | LOS E |  |  | 0.95 | 0.95 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## PHASING SUMMARY

## Site: 101 [PM Existing+ 10y Gr + S2 Wallgrove Rd/ The Horsley Drive - Upgraded]

New Site
Site Category: (None)
Signals - Fixed Time Coordinated Cycle Time $=125$ seconds (Site Optimum Cycle Time - Minimum Delay)
Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Green Split Priority has been specified
Phase Sequence: TCS - Tom Edit
Reference Phase: Phase A
Input Phase Sequence: A, D, E, G
Output Phase Sequence: A, D, E, G

## Phase Timing Summary

| Phase | A | D | E | G |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 0 | 36 | 76 | 109 |
| Green Time (sec) | 30 | 34 | 27 | 10 |
| Phase Time (sec) | 36 | 40 | 33 | 16 |
| Phase Split | $29 \%$ | $32 \%$ | $26 \%$ | $13 \%$ |

See the Phase Information section in the Detailed Output report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.

| Output Phase Sequence |  |  |
| :---: | :---: | :---: |
|  | Phase D | Phase E |
| Phase G |  |  |

REF: Reference Phase
VAR: Variable Phase

| $\longrightarrow$ Normal Movement | Slip/Bypass-Lane Movement |
| :--- | :--- |$\quad$| Permitted/Opposed |
| :--- |
| Opposed Slip/Bypass-Lane |

$\square$ Stopped Movement
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs

Other Movement Class (MC) Stopped $\quad$|  |
| :---: |
| $\square$ |

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Site Category: (None)
Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | Demand <br> Total veh/h | $\begin{aligned} & \text { Flows } \\ & \text { HV } \\ & \% \end{aligned}$ | Arrive <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | Aver. B Que Vehicles veh | Back of ue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Averag Speed km/h |
| South: Wallgrove Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 1 | 0.0 | 1 | 0.0 | 0.488 | 5.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 58.2 |
| 2 T1 | 914 | 6.0 | 914 | 6.0 | 0.488 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 59.8 |
| Approach | 915 | 6.0 | 915 | 6.0 | 0.488 | 0.1 | NA | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 59.8 |
| North: Wallgrove Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 341 | 12.0 | 341 | 12.0 | 0.190 | 0.1 | LOS A | 0.0 | 0.1 | 0.01 | 0.00 | 0.01 | 59.8 |
| 9 R2 | 1 | 0.0 | 1 | 0.0 | 0.190 | 13.3 | LOSA | 0.0 | 0.1 | 0.01 | 0.00 | 0.01 | 56.2 |
| Approach | 342 | 12.0 | 342 | 12.0 | 0.190 | 0.1 | NA | 0.0 | 0.1 | 0.01 | 0.00 | 0.01 | 59.8 |
| West: Kosovich Place (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 1 | 0.0 | 1 | 0.0 | 0.006 | 10.2 | LOS A | 0.0 | 0.1 | 0.77 | 0.81 | 0.77 | 36.4 |
| 12 R2 | 1 | 0.0 | 1 | 0.0 | 0.006 | 17.3 | LOS B | 0.0 | 0.1 | 0.77 | 0.81 | 0.77 | 41.4 |
| Approach | 2 | 0.0 | 2 | 0.0 | 0.006 | 13.7 | LOS A | 0.0 | 0.1 | 0.77 | 0.81 | 0.77 | 39.6 |
| All Vehicles | 1259 | 7.6 | 1259 | 7.6 | 0.488 | 0.1 | NA | 0.0 | 0.1 | 0.00 | 0.00 | 0.00 | 59.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^10]
## New Site

Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | Demand <br> Total veh/h | Flows | Arrival Total veh/h | $\begin{array}{r} \text { =lows } \\ \text { HV } \\ \% \end{array}$ | Deg. Satn v/c | Average Delay sec | Level of Service | Aver. B <br> Vehicles veh | of <br> tance <br> m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Averag Speed km/h |
| South: Wallgrove Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $2 \quad \mathrm{~T} 1$ | 915 | 6.0 | 915 | 6.0 | 0.539 | 4.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.41 | 0.00 | 54.9 |
| 3 u U | 1 | 0.0 | 1 | 0.0 | 0.539 | 10.8 | LOSA | 0.0 | 0.0 | 0.00 | 0.41 | 0.00 | 39.7 |
| Approach | 916 | 6.0 | 916 | 6.0 | 0.539 | 4.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.41 | 0.00 | 54.9 |
| North: Wallgrove Road ( N ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 342 | 12.0 | 342 | 12.0 | 0.208 | 4.2 | LOSA | 0.4 | 3.4 | 0.02 | 0.40 | 0.02 | 53.0 |
| Approach | 342 | 12.0 | 342 | 12.0 | 0.208 | 4.2 | LOS A | 0.4 | 3.4 | 0.02 | 0.40 | 0.02 | 53.0 |
| All Vehicles | 1258 | 7.6 | 1258 | 7.6 | 0.539 | 4.1 | LOS A | 0.4 | 3.4 | 0.00 | 0.41 | 0.00 | 54.5 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Site Category: (None)
Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn | Demand Flows Arrival Flows |  |  |  | Deg. Satn v/c | Average Delay sec | Level of Service | Aver. Back of Queue Vehicles Distance veh |  | Prop. Queued | Effective Stop Rate | Aver. AveragNo. Cycles Speed |  |
|  | Total |  | Total | HV |  |  |  |  |  |  |  |  |  |
|  | veh/h |  | veh/h | \% |  |  |  |  |  |  |  | km/h |
| South: Wallgrove Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 2 | 0.0 | 2 | 0.0 | 0.200 | 5.6 | LOS A | 0.0 | 0.0 |  | 0.00 | 0.00 | 0.00 | 58.3 |
| 2 T 1 | 366 | 9.0 | 366 | 9.0 | 0.200 | 0.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 59.9 |
| Approach | 368 | 9.0 | 368 | 9.0 | 0.200 | 0.1 | NA | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 59.9 |
| North: Wallgrove Road ( N ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 946 | 7.0 | 946 | 7.0 | 0.509 | 0.0 | LOSA | 0.0 | 0.1 | 0.00 | 0.00 | 0.01 | 59.9 |
| 9 R2 | 2 | 0.0 | 2 | 0.0 | 0.509 | 8.3 | LOSA | 0.0 | 0.1 | 0.00 | 0.00 | 0.01 | 56.3 |
| Approach | 948 | 7.0 | 948 | 7.0 | 0.509 | 0.0 | NA | 0.0 | 0.1 | 0.00 | 0.00 | 0.01 | 59.9 |
| West: Kosovich Place (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 2 | 0.0 | 2 | 0.0 | 0.011 | 5.8 | LOS A | 0.0 | 0.1 | 0.63 | 0.70 | 0.63 | 37.3 |
| 12 R 2 | 2 | 0.0 | 2 | 0.0 | 0.011 | 19.4 | LOS B | 0.0 | 0.1 | 0.63 | 0.70 | 0.63 | 41.9 |
| Approach | 4 | 0.0 | 4 | 0.0 | 0.011 | 12.6 | LOSA | 0.0 | 0.1 | 0.63 | 0.70 | 0.63 | 40.3 |
| All Vehicles | 1320 | 7.5 | 1320 | 7.5 | 0.509 | 0.1 | NA | 0.0 | 0.1 | 0.00 | 0.00 | 0.01 | 59.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## SIDRA INTERSECTION 8.0 | Copyright © 2000-2018 Akcelik and Associates Pty Ltd | sidrasolutions.com

Organisation: MCLAREN TRAFFIC ENGINEERING | Processed: Wednesday, 29 August 2018 2:23:20 PM
Project: $\$ IImteserverlmte storage\Jobsl2018\18106IMTE SIDRAl18 0822 AM09.25 -IKosovich Wallgrove to Roundabout Network.sip8

## New Site

Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | Demand <br> Total veh/h |  | Arrival Total veh/h | ows <br> HV $\%$ | Deg. Satn v/c | Average Delay sec | Level of Service | Aver. B <br> Vehicles veh | ck of istance m | Prop. Queued | Effective Stop Rate | Aver. No Cycles | Averag Speed km/h |
| South: Wallgrove Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $2 \quad \mathrm{~T} 1$ | 368 | 9.0 | 368 | 9.0 | 0.220 | 4.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.41 | 0.00 | 54.8 |
| 3 u U | 1 | 0.0 | 1 | 0.0 | 0.220 | 10.8 | LOSA | 0.0 | 0.0 | 0.00 | 0.41 | 0.00 | 39.6 |
| Approach | 369 | 9.0 | 369 | 9.0 | 0.220 | 4.1 | LOSA | 0.0 | 0.0 | 0.00 | 0.41 | 0.00 | 54.8 |
| North: Wallgrove Road ( N ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 947 | 7.0 | 947 | 7.0 | 0.560 | 4.2 | LOSA | 2.0 | 14.5 | 0.03 | 0.40 | 0.03 | 53.0 |
| Approach | 947 | 7.0 | 947 | 7.0 | 0.560 | 4.2 | LOSA | 2.0 | 14.5 | 0.03 | 0.40 | 0.03 | 53.0 |
| All Vehicles | 1316 |  | 1316 | 7.6 | 0.560 | 4.2 | LOS A | 2.0 | 14.5 | 0.02 | 0.40 | 0.02 | 53.5 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

$\nabla$ site: 101 [NRT Existing AM+ S1 - Wallgrove/Kosovich]
Site Category: (None)
Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | Demand <br> Total veh/h | Flows HV \% | Arrival Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. <br> Satn v/c | Average Delay sec | Level of Service | $\begin{array}{r} 95 \% \mathrm{Ba} \\ \text { Que } \\ \text { Vehicles } \\ \text { veh } \end{array}$ | ack of ue Distance | Prop. Queued | Effective Stop Rate |  | Averag Speed $\mathrm{km} / \mathrm{h}$ |
| South: Wallgrove Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 107 | 0.0 | 107 | 0.0 | 0.545 | 5.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.06 | 0.00 | 57.6 |
| 2 T 1 | 914 | 6.0 | 914 | 6.0 | 0.545 | 0.1 | LOSA | 0.0 | 0.0 | 0.00 | 0.06 | 0.00 | 58.6 |
| Approach | 1021 | 5.4 | 1021 | 5.4 | 0.545 | 0.7 | NA | 0.0 | 0.0 | 0.00 | 0.06 | 0.00 | 58.4 |
| North: Wallgrove Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 426 | 12.0 | 426 | 12.0 | 0.237 | 0.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 59.9 |
| 9 R2 | 47 | 0.0 | 47 | 0.0 | 0.110 | 13.6 | LOSA | 0.4 | 2.7 | 0.78 | 0.91 | 0.78 | 41.8 |
| Approach | 473 | 10.8 | 473 | 10.8 | 0.237 | 1.4 | NA | 0.4 | 2.7 | 0.08 | 0.09 | 0.08 | 57.5 |
| West: Kosovich Place (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 142 | 0.0 | 142 | 0.0 | 0.282 | 11.9 | LOS A | 1.1 | 7.6 | 0.76 | 0.93 | 0.88 | 37.8 |
| Approach | 142 | 0.0 | 142 | 0.0 | 0.282 | 11.9 | LOS A | 1.1 | 7.6 | 0.76 | 0.93 | 0.88 | 37.8 |
| All Vehicles | 1636 | 6.5 | 1636 | 6.5 | 0.545 | 1.9 | NA | 1.1 | 7.6 | 0.09 | 0.15 | 0.10 | 55.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

Site: 101 [FU AM- Wallgrove/ Villiers + S1]

## New Site

Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | Demand Flows Arrival Flows |  |  |  | Deg. Satn v/c | Average Delay | Level of Service | 95\% Back of Queue Vehicles Distance veh |  | Prop. Queued | Effective Stop Rate | Aver. Averag No. e Cycles Speed km/h |  |
|  | Total veh/h |  | Total veh/h | $\begin{gathered} \mathrm{HV} \\ \% \end{gathered}$ |  |  |  |  |  |  |  |  |  |
| South: Wallgrove Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 971 | 6.0 | 971 | 6.0 | 0.620 | 4.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.44 | 0.00 | 54.2 |
| 3 u U | 85 | 0.0 | 85 | 0.0 | 0.620 | 10.8 | LOSA | 0.0 | 0.0 | 0.00 | 0.44 | 0.00 | 38.3 |
| Approach | 1056 | 5.5 | 1056 | 5.5 | 0.620 | 4.6 | LOSA | 0.0 | 0.0 | 0.00 | 0.44 | 0.00 | 53.8 |
| North: Wallgrove Road ( N ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 436 | 12.0 | 436 | 12.0 | 0.328 | 4.7 | LOS A | 2.0 | 15.4 | 0.27 | 0.43 | 0.27 | 50.9 |
| Approach | 436 | 12.0 | 436 | 12.0 | 0.328 | 4.7 | LOS A | 2.0 | 15.4 | 0.27 | 0.43 | 0.27 | 50.9 |
| All Vehicles | 1492 |  | 1492 | 7.4 | 0.620 | 4.7 | LOS A | 2.0 | 15.4 | 0.08 | 0.44 | 0.08 | 53.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^11]
## MOVEMENT SUMMARY

$\nabla$ Site: 101 [NRT Existing PM+ S1 + Wallgrove/Kosovich]
审审 Network: N101 [PM + S1]

Site Category: (None)
Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | Demand <br> Total veh/h | HV \% \% | Arrival Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% B Que <br> Vehicles veh | ack of ue Distance | Prop. Queued | Effective Stop Rate |  | Averag Speed $\mathrm{km} / \mathrm{h}$ |
| South: Wallgrove Road (S) sec |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 87 | 0.0 | 87 | 0.0 | 0.246 | 5.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.11 | 0.00 | 57.3 |
| 2 T 1 | 366 | 9.0 | 366 | 9.0 | 0.246 | 0.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.11 | 0.00 | 57.8 |
| Approach | 453 | 7.3 | 453 | 7.3 | 0.246 | 1.1 | NA | 0.0 | 0.0 | 0.00 | 0.11 | 0.00 | 57.6 |
| North: Wallgrove Road ( N ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 1053 | 7.0 | 1053 | 7.0 | 0.569 | 0.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 59.8 |
| 9 R2 | 57 | 0.0 | 57 | 0.0 | 0.051 | 7.2 | LOSA | 0.2 | 1.5 | 0.48 | 0.67 | 0.48 | 47.5 |
| Approach | 1110 | 6.6 | 1110 | 6.6 | 0.569 | 0.4 | NA | 0.2 | 1.5 | 0.02 | 0.03 | 0.02 | 59.0 |
| West: Kosovich Place (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 155 | 0.0 | 155 | 0.0 | 0.136 | 6.0 | LOSA | 0.5 | 3.8 | 0.43 | 0.63 | 0.43 | 42.7 |
| Approach | 155 | 0.0 | 155 | 0.0 | 0.136 | 6.0 | LOSA | 0.5 | 3.8 | 0.43 | 0.63 | 0.43 | 42.7 |
| All Vehicles | 1718 |  | 1718 | 6.2 | 0.569 | 1.1 | NA | 0.5 | 3.8 | 0.06 | 0.11 | 0.06 | 57.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

Site: 101 [FU PM- Wallgrove/ Villiers + S1]

## New Site

Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | HV |  | ows <br> HV \% | Deg. <br> Satn v/c | Average Delay sec | Level of Service | $\begin{array}{r} 95 \% \mathrm{Be} \\ \text { Que } \\ \text { Vehicles [ } \\ \text { veh } \end{array}$ | of <br> stance m | Prop. Queued | Effective Stop Rate |  |  |
| South: Wallgrove Road (S) mill |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $2 \quad \mathrm{~T} 1$ | 414 | 9.0 | . 414 | 9.0 | 0.308 | 4.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.50 | 0.00 | 53.0 |
| 3 u U | 107 | 0.0 | , 107 | 0.0 | 0.308 | 10.8 | LOSA | 0.0 | 0.0 | 0.00 | 0.50 | 0.00 | 36.3 |
| Approach | 521 | 7.2 | 221 | 7.2 | 0.308 | 5.5 | LOSA | 0.0 | 0.0 | 0.00 | 0.50 | 0.00 | 51.7 |
| North: Wallgrove Road ( N ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 1072 | 7.0 | 1072 | 7.0 | 0.774 | 5.6 | LOS A | 9.7 | 72.3 | 0.60 | 0.50 | 0.60 | 48.4 |
| Approach | 1072 | 7.0 | . 1072 | 7.0 | 0.774 | 5.6 | LOS A | 9.7 | 72.3 | 0.60 | 0.50 | 0.60 | 48.4 |
| All Vehicles | 1593 | 7.0 | 1593 | 7.0 | 0.774 | 5.5 | LOS A | 9.7 | 72.3 | 0.41 | 0.50 | 0.41 | 49.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^12]
## MOVEMENT SUMMARY

$\nabla$ Site: 101 [NRT Existing AM+ 10yr Gr+ S2 - Wallgrove/
䗆 Network: N101 [AM + Grwth Kosovich

```
+ S2]
```

Site Category: (None)
Giveway / Yield (Two-Way)


Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## New Site

Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | Demand <br> Total veh/h | Flows HV \% | Arrival Total veh/h | $\begin{gathered} =l o w s \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service |  | of <br> stance <br> m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Averag Speed km/h |
| South: Wallgrove Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $2 \quad \mathrm{~T} 1$ | 1015 | 6.0 | 1015 | 6.0 | 0.673 | 4.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.48 | 0.00 | 53.4 |
| 3 u U | 163 | 0.0 | 163 | 0.0 | 0.673 | 10.7 | LOSA | 0.0 | 0.0 | 0.00 | 0.48 | 0.00 | 37.0 |
| Approach | 1178 | 5.2 | 1178 | 5.2 | 0.673 | 5.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.48 | 0.00 | 52.7 |
| North: Wallgrove Road ( N ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 514 | 12.0 | 514 | 12.0 | 0.419 | 5.4 | LOS A | 2.8 | 21.3 | 0.42 | 0.50 | 0.42 | 49.7 |
| Approach | 514 | 12.0 | 514 | 12.0 | 0.419 | 5.4 | LOS A | 2.8 | 21.3 | 0.42 | 0.50 | 0.42 | 49.7 |
| All Vehicles | 1692 |  | 1692 | 7.2 | 0.673 | 5.1 | LOS A | 2.8 | 21.3 | 0.13 | 0.48 | 0.13 | 51.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

Vite: 101 [NRT Existing PM+ 10yr Gr+ S2- Wallgrove/ Kosovich]

审官 Network: N101 [PM + Grwth<br>+ S2]

Site Category: (None)
Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | Demano <br> Total veh/h | HVs | Arriva <br> Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% B <br> Vehicles <br> veh | ack of ue Distance | Prop. Queued | Effective Stop Rate |  | Averag Speed km/h |
| South: Wallgrove Road (S) sec min |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 165 | 0.0 | 165 | 0.0 | 0.296 | 5.6 | LOSA | 0.0 | 0.0 | 0.00 | 0.18 | 0.00 | 56.7 |
| 2 T 1 | 381 | 9.0 | 381 | 9.0 | 0.296 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.18 | 0.00 | 56.6 |
| Approach | 546 | 6.3 | 546 | 6.3 | 0.296 | 1.7 | NA | 0.0 | 0.0 | 0.00 | 0.18 | 0.00 | 56.7 |
| North: Wallgrove Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 1180 | 7.0 | 1180 | 7.0 | 0.638 | 0.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 59.7 |
| 9 R2 | 110 | 0.0 | 110 | 0.0 | 0.110 | 7.9 | LOSA | 0.5 | 3.2 | 0.55 | 0.74 | 0.55 | 46.9 |
| Approach | 1290 | 6.4 | 1290 | 6.4 | 0.638 | 0.7 | NA | 0.5 | 3.2 | 0.05 | 0.06 | 0.05 | 58.3 |
| West: Kosovich Place (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 309 | 0.0 | 309 | 0.0 | 0.275 | 6.3 | LOSA | 1.2 | 8.5 | 0.48 | 0.68 | 0.48 | 42.5 |
| Approach | 309 | 0.0 | 309 | 0.0 | 0.275 | 6.3 | LOS A | 1.2 | 8.5 | 0.48 | 0.68 | 0.48 | 42.5 |
| All Vehicles | 2145 |  | 2145 | 5.4 | 0.638 | 1.8 | NA | 1.2 | 8.5 | 0.10 | 0.18 | 0.10 | 55.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## New Site

Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | Demand Flows Arrival Flows |  |  |  | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back of Queue <br> Vehicles Distance veh |  | Prop. Queued | EffectiveStopRate | Aver. Averag No. Cycles Speed |  |
|  | Total |  | Total | HV |  |  |  |  |  |  |  |  |  |
|  | veh/h |  | \% veh/h | \% |  |  |  |  |  |  |  | km/h |
| South: Wallgrove Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 475 | 0.0 | . 475 | 0.0 | 0.385 | 4.1 | LOS A | 0.0 | 0.0 |  | 0.00 | 0.55 | 0.00 | 52.4 |
| 3 u U | 215 | 0.0 | . 215 | 0.0 | 0.385 | 10.7 | LOSA | 0.0 | 0.0 | 0.00 | 0.55 | 0.00 | 34.9 |
| Approach | 690 | 0.0 | . 690 | 0.0 | 0.385 | 6.2 | LOSA | 0.0 | 0.0 | 0.00 | 0.55 | 0.00 | 50.1 |
| North: Wallgrove Road ( N ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 1180 | 0.0 | . 1180 | 0.0 | 0.912 | 12.9 | LOSA | 22.9 | 160.3 | 1.00 | 0.88 | 1.30 | 42.7 |
| Approach | 1180 | 0.0 | . 1180 | 0.0 | 0.912 | 12.9 | LOSA | 22.9 | 160.3 | 1.00 | 0.88 | 1.30 | 42.7 |
| All Vehicles | 1870 | 0.0 | 1870 | 0.0 | 0.912 | 10.4 | LOS A | 22.9 | 160.3 | 0.63 | 0.76 | 0.82 | 45.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.


ANNEXURE E: SWEPT PATH TESTING




ANNEXURE F: CATCHMENT AREAS

## Cecil Park Catchment Area

The map below highlights the 43 individual Statistical Areas Level 2 (SA2s) which together form the Cecil Park Catchment Area. The Cecil Park Catchment Area includes all the SA2s which are located within a 12 kilometre radius of the Cecil Park development location at Kosovich Place, Cecil Park.

Combined, the Catchment Area covers nearly
471 square kilometres of Sydney's west.
Located in the outskirts of urban Sydney, the Cecil Park Catchment Area consists of a diverse array of areas including urban highdensity, residential suburban, industrial and rural agriculture.

## 43 SA2s which form the Cecil Park Catchment Area

The red dot in the centre of the map indicates the proposed development site at Kosovich Place, Cecil Park.


## Population

The residential population of the Cecil Park Catchment Area is 599,514 people. This represents one in eight people living in Greater Sydney (12\%), which had a population of 4,823,991 in 2016. The population of the Catchment Area has grown by nearly 50,000 people over the five-year period from 2011 to 2016, rising from 549,957 to 599,514.

| Census population count | $\mathbf{2 0 1 1}$ | $\mathbf{2 0 1 6}$ | Change (2011-2016) |
| :--- | :---: | :---: | :---: |
| Persons | 549,957 | 599,514 | 49,557 |

Growing at a steady pace of $9 \%$ over five years the Cecil Park Catchment Area is growing faster than New South Wales (8\%), however, marginally slower than the rest of Sydney which has grown by $10 \%$ over the same five-year period (2011-2016).


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ANNEXURE G: PROPOSED INFRASTRUCTURE UPGRADES






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[^2]:    Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

[^3]:    Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

[^4]:    Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

[^5]:    Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

[^6]:    Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

[^7]:    Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

[^8]:    Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

[^9]:    Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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[^12]:    SIDRA INTERSECTION 8.0 | Copyright © 2000-2018 Akcelik and Associates Pty Ltd | sidrasolutions.com
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