

APPENDIX E

SYDNEY HARBOUR DESIGN LEVELS AND SEA LEVEL RISE Sea Level Change Table

ARI Years	2008 ⁽¹⁾ Design Still Water Levels (m AHD)	Sea Level Rise ⁽³⁾ Scenerio	2050 ⁽¹⁾ (m AHD)	2100 ⁽¹⁾ (m AHD)
1		Low	1.275	1.395
1	1.235	Medium	1.445	1.765
		High	1.615	2.125
2		Low	1.315	1.435
2	1.275	Medium	1.485	1.805
_		High	1.655	2.165
-		Low	1.355	1.475
5	1.315	Medium	1.525	1.845
		High	1.695	2.205
		Low	1.385	1.505
10	1.345	Medium	1.555	1.875
		High	1.725	2.235
		Low	1.415	1.535
20	1.375	Medium	1.585	1.905
		High	1.755	2.265
		Low	1.455	1.575
50	1.415	Medium	1.625	1.945
		High	1.795	2.305
100100.000		Low	1.475	1.595
100	1.435	Medium	1.645	1.965
		High	1.815	2.325
(4)		Low	1.84	1.96
PMF ⁽⁴⁾	1.8	Medium	2.01	2.33
otes		High	2.18	2.53

Notes

1. Levels taken from Table 6.3 Fort Denison Sea Level Rise Vulnerablity Study (DECC, 2008)

2. Levels assume a linear increase rounded to the nearest 5mm

3. Low, Medium, High refer to climate change projections outlined in the table below

4. PMF calculated by taking the highest astronomical tide of 1.175m AHD

plus a surge component of 0.6m and then rounded to 1.8m

Table 6.2 Fort Denison Sea Level Rise Vulnerability Study (DECC, 2008)

Year 2050 (cm)	Year 2100 (cm)
4 (1)	16 ⁽³⁾
21	53
38 (2)	89 (4)
	4 ⁽¹⁾ 21

Notes

1. SLR estimate derived from Figure 11.12 (IPCC, 2001) corrected for application from 2008.

2. SLR estimates derived from Figure 11.12 (IPCC, 2001) corrected for application from 2008 (26cm) with the addition of 12 cm to account for the upper bound regional increase in SLR above the global average (CSIRO, 2007).

3. SLR estimate from Table SPM.3 (IPCC, 2007) using the 18cm advised, corrected for application from 2008 assuming average increase in MSL of 1.8mm/year from 1999.

4. SLR estimate from Table SPM.3 (IPCC, 2007) using the 59cm advised, corrected for application from 2008 assuming average increase in MSL of 1.8mm/year from 1999. An additional 20cm has been added to account for the possibility of ice sheet flow rates increasing linearly with increased temperature for upper bound projections as advised by IPCC (2007). A further 12cm has been added to account for the upper bound regional increase in SLR above the global average (CSIRO, 2007).

5. Medium position between "lower" and "upper" bound derived estimates rounded up to nearest cm.

APPENDIX F

RAINFALL, COCKLE BAY WATER LEVEL AND CATCHMENT RUNOFF COINCIDENCE

rom 1914-2012
t Rainfall Events
TO ANDISI

			Approximate	mate	ARIS from Bureau of N	ureau of Meteorology	Approximate Timing of Events	Dacand	A TANAL AND A T		
	Daily Rainfall (mm) 25min ARI	25min ARI		60min /		24hr ARI	Start of Series Tenis Review Bart Parts	ſ	Recorded Water Levels Fort Denison	Jenison	Calculated From Predicted Tide
36.6 27.8 178.5 lvr c1vr	178.5 1vr	178.5 1vr		ctur		Ene 10.0	Peak Kun	Peak Tide (m AHD) Tide ARI	Total Strength	Approx Tide at Peak Runoff Pea	Peak Anomaly (m) Anomaly Api
vr	101.0 2-5vr	101.0 2-5vr		Tur		JANT - JAC		1.01 <1 month	th	0 211	*00
	197 8 < 1ur	197 8 < 1ur		-11-1-	T	JAL 20	07:35 PM 07:57 PM	1.04 <1 month	4	0 801	JÁ T > TO:0
	174.7 2-5ur	174.7 2-5ur		10er 20er		TUYE - ZUYE	07:11 AM 07:33 AM	1.01 <1 month	4		0.40 20
				1607 - 1607		Jyr - Juyr	06:31 AM 06:53 AM	0.79 <1 month	5	0030	0.43 ZU Yr
142 11212	142 11212	142 11212		2 yl		zuyr-suyr	11:23 PM 11:45 PM	0.77 <1 month	-	67010	0.04 < 1 yr
	JÁTS C'C/T	JÁTS C'C/T		zyr - 5yr		5yr - 10yr	05:07 AM 05:29 AM	0 73 /1 month	4	9/0.0-	0.18 < 1 yr
5.62	192.5 <1yr	192.5 <1yr		<lyr< td=""><td></td><td>10yr</td><td>06:41 AM 07:03 AM</td><td>440000 17 VB U</td><td></td><td>0.251</td><td>-0.04 < 1 yr</td></lyr<>		10yr	06:41 AM 07:03 AM	440000 17 VB U		0.251	-0.04 < 1 yr
1.15	199.2 <1yr	199.2 <1yr		1yr		10yr - 20yr	04:05 PM 04:27 PM	110011 T> 100 1		0.776	0.25 < 1 yr
28.0	194.7 <1yr	194.7 <1yr		<1yr		10yr - 20yr		1101011 1 00 0		-0.052	0.37 5 yr
	132.9 10-20yr	132.9 10-20yr		20yr		2yr		UTINOTI I 2 00.0	5	0.161	0.20 < 1 yr
	174.2 2yr	174.2 2yr		10yr		5vr - 10vr		U./U <1 month	5	-0.02	0.04 < 1 yr
87.7 87.7 175.2 Syr 50yr - 100yr	175.2 5yr	175.2 5yr		50yr - 100yr		5vr - 10vr		0./8 <1 month	5	-0.125	0.14 < 1 vr
199.8 119.4 240.4 >100yr >100yr	240.4 >100yr	240.4 >100yr		>100yr	T	20vr-50vr		0.58 <1 month	£	0.157	0.03 < 1 vr
57.9 44.0 309.7 Ivr 2vr - 5vr	309.7 1yr	309.7 1yr		2vr - Svr		>100ur		0.69 <1 month	÷	0.169	0.09 < 1 vr
33.2 166.1 <1yr	166.1 <1yr	166.1 <1yr		lvr		Sur	Wd 17:70 Wd 66:10	1.01 <1 month	4	-0.293	0.34 3 vr
53.3 37.7 192.5 Ivr 1vr - 2vr	192.5 1yr	192.5 1yr		1vr - 2vr		10er		0.98 <1 month	£	0.465	0.04 < 1 vr
104.5 42.2 46.8 10-20vr 2vr	46.8 10-20vr	46.8 10-20vr		Dur		1		0.78 <1 month	4	-0.125	010 21.1
	169.7 Jur	169.7 Jur	.10-	Dur Luc	T	suyr	02:23 PM 02:45 PM	0.91 <1 month	4	035 U	1/ T > 07:0
	209 4 500	209 4 500				Syr	10:29 PM 10:51 PM	0.69 <1 month	-	200'0-	0.12 < 1 yr
125.8 /100	125.8 /100	125.8 /100		1041 - 2041		TUYE - 20yr	09:53 AM 10:15 AM	0.71 <1 month	-	NOE 0	-0.07 < 1 yr
	IATS OFFIT	IATS OFFIT		TYT	2	5yr - 10yr	07:35 PM 07:57 PM	1.23 1 vr		PUC-0	0.13 < 1 yr
								if a laws		1.2	0.34 3 vr

15 Worst Tide Events from 1914-2012 Event Recorded Water Levels Fort Davis

Calculated From Predicted Tide Reak Anomaly (m) Anomaly ARI 0.29 1 yr 0.20 1 yr 0.20 1 yr 0.20 1 yr 0.21 1 yr 0.23 1 yr 0.24 1 yr 0.25 1 yr 0.26 1 yr 0.23 1 yr 0.24 1 yr 0.25 1 0 yr 0.23 1 yr	Recorded Rainfall Observatory Hill	Daily Rainfall (mm) 1244 ADI	4	JAT> U.I	0.0 <1yr	0.8 <1yr	18.8 <1vr	0.0.71vr	AT OO	JÁT> 0:0	82.6 <1yr	2.8 <1yr	0.0 <1vr	0.0 .1	JÁTS N'N	0.0 <1yr	0.0 <1yr	0.0 <1vr	14-2 010	0.41.41.1
trice and an unit of the and		Anomaly ARI Daily		14 040	0.20 < 1 yr	0.26 < 1 yr	0.30 1 yr	0.29 1 yr	0.16 < 1 vr		1/ OUL > 20.0	0.32 1 yr	0.36 5 yr	0.37 5 vr	017 / 1	IAT STO	U.31 1 Vr	0.28 <1 yr		0.18 < 1 vr
	Ter	Tide ARI	1.31 2yr-5yr	1.29 2vr-5vr	1 30 Dur-Cur	1 40 20 10	1.40 ZUYE - SUYE	1.34 5yr - 10yr	1.28 2yr	1.48 >100vr	1 32 Sur		1.35 JUYF	1.43 50yr - 100yr	1.29 2yr - 5yr	1.34 10vr		1.26 IYr - 2yr	1 26 1vr - 2vr	

Notes

Rainfall data supplied by the Bureau of Meteorology Tidal recordings and predictions supplied by Sydney Ports Corportation Anomaly ARIs approximated using NSW Ocean Water Levels, MHL, 2011 Anomally refers to the water level recorded above the predicted.

Peak runoff times to Cockle Bay estimated based on catchment hydrology Tide ARIs approximated using the Fort Denison Sea Level Rise Vulnerability Study, DECC, 2008 Each event is monitored for 3 days with peaks refering to peaks which occur at anytime during this period Anomaliles are mainly caused by meteorlogical effects above the tidal recorder



Rainfall data recorded at Observatory Hill Sydt Anomallies are mainly caused by meteorlogics Runoff Peak refers to the estimated time at which maximum flow reached Cockle Bay

Tide data recorded at Fort Denison Tide data and predicted tide data supplied by the Sydney Ports Corporation



Fide data and predicted tide data supplied by the Sydney Ports Corporation





Tide data and predicted tide data supplied by the Sydney Ports Corporation





Runoff Peak refers to the estimated time at which maximum flow reached Cockle Bay Tide recordings from this time (1972-1976) were rounded to the nearest 100mm. Therefore anomalies of the order of +/- 100mm are likely due to rounding error.

> Fide data and predicted tide data supplied by the Sydney Ports Corporation Tide data recorded at Fort Denison





Tide data recorded at Fort Denison Tide data and predicted tide data supplied by the Sydney Ports Corporation Rainfall data recorded at Observatory Hill Sydney, Station number 66062

Notes



Fide data and predicted tide data supplied by the Sydney Ports Corporation





Tide data and predicted tide data supplied by the Sydney Ports Corporation





Tide data recorded at Fort Denison Tide data and predicted tide data supplied by the Sydney Ports Corporation



Tide ARI estimations made using Fort Denison Seal Level Rise Vulnerablility Study, DECC 2008

Tide data and predicted tide data supplied by the Sydney Ports Corporation Tide data recorded at Fort Denison



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> ride data recorded at Fort Denison Tide data and predicted tide data supplied by the Sydney Ports Corporation







Tide data and predicted tide data supplied by the Sydney Ports Corporation







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Rainfall data recorded at Observatory Hill Sydney, Station number 66062

Tide data and predicted tide data supplied by the Sydney Ports Corporation

Tide ARI estimations made using Fort Denison Seal Level Rise Vulnerablility Study, DECC 2008

APPENDIX G

EXISTING CONDITIONS FLOW REGIMES

EXISTING CONDITIONS FLOOD ASSESSMENT

Hyder Consulting has carried out this flood assessment of the SICEEP site for existing development conditions. The assessment is to enable the demonstration of potential flood impacts as a result of the SICEEP re-development, and that the development is in compliance with the Director General (DG) requirement that the proposed development will not adversely impact on flooding of neighbouring properties.

1.1 ASSESSMENT METHODOLOGY

1

The existing conditions DRAINS and TUFLOW model parameters and assumptions remained unchanged to those of the proposed modelling – the adjustments where simply limited to within the SICCEP site area where local sub-catchment areas, levels, flow paths and associated local inlets and stormwater conduits to represent existing conditions, replaced those of the design conditions. The existing conditions catchment sub-areas and local stormwater systems are shown in Appendix G2 along with the DRAINS model input information.

As per the proposed development modelling, the existing conditions DRAINS output hydrographs from each sub-catchment area (for the various storm events) have been put into the TUFLOW model to quantify existing conditions site flow regimes. Figure G1 and the associated photos (see Appendix G1) indicate various gates located along overland flow paths and a surface inlet pit under Pier Street have the potential to block. However, for the purpose of comparing potential flood impacts on upstream neighbouring property in Hay Street and Harbour Street, 0% blockage has been adopted in the TUFLOW modelling.

1.1.1 HISTORIC INFORMATION

To provide confidence in the model representation of existing condition flow regimes an investigation of historic information has been carried out involving the following.

City of Sydney Report (2012)

Flood hot spots have been identified in a report prepared for City of Sydney Council 'Decentralised Water Master Plan WSUD & Stormwater Infrastructure Report' by GHD (7 June 2012). Significantly, it indicates no major reported flooding at the Entertainment Centre or downstream within the Darling Harbour site.

Design Information (1980s)

While no stormwater design report has been found available for the Darling Harbour development carried out in the mid-1980s, the following design information has been.

- A record of major drainage amplification works carried out by Sydney Water in preparation for the mid-1980s Darling Harbour development. A summary figure of the Sydney Water drainage assets is included in Appendix D (of the main report) and identifies the major culvert amplifications.
- A design drawing of the Entertainment Centre Carpark Floodway Design dated June 1988 (see Appendix G3), which indicates an approximate 20 year flood flow depth of 0.3m through the ground floor driveway and discharging into the Sydney Water culvert amplification via a large (~70m²) grated stormwater pit located just to the north of the carpark under Pier Street (see Photos 7 and 8) within the SHFA works area.
- The existing Entertainment Centre ground floor level has been surveyed and found to be at RL3.36mAHD.

Recorded Rainfall and Flood Observations (November 1984)

Recorded rainfall data was obtained from Observatory Hill (Station 66062) during the course of this study. Intensities for the twenty most significant events between 1914 and 2012 have been summarised in Appendix F. Of those events, the most intense 25 minute and 60 minute rainfall on 8 November 1984 approximated as greater than 100 year design event, two other more recent events on 6 January 1989 and 10 April 1998 approximated 5 to 10 year design rainfalls.

Hyder interviewed John Dedousis, the Sydney Entertainment Centre Operations Supervisor, who had been working there since its opening in May 1983. Mr Dedousis recalled the largest flood event having occurred there during his time was on the night of 8 November 1984 at about 10pm. At the time he was at the 'local pub' just north-western of the Entertainment Centre building when he observed a massive storm. With respect to flooding, he recalled the water entering the north western loading dock bay (pavement level surveyed as RL2.68mAHD) and ponding up against the wall of the dock (dock height of 0.7m) to just below floor level. It is therefore estimated that the flood water level peaked at about 3.2 to 3.3mAHD.

Mr Dedousis also commented that the nearby stormwater pits had their lids 'pop' off from the water upwelling, and that the flood waters dissipated very quickly as the rain stopped. Furthermore he commented that even though he had experienced some other flood events during his time at the Entertainment Centre, there was nowhere near as much flooding.

The recorded rainfall for the 10 April 1998 event was modelled in DRAINS with the peak flow, in the Hay Street SWCP Main Channel, found to approximate that of a 5 ARI design event.

The event on 8 November 1984 was modelled in both DRAINS and TUFLOW. However:

- the Sydney Water WAE design drawings indicate that the box culvert amplifications were not operational in the 1984 event. As such a 'pre-culvert amplification' TUFLOW model was developed to represent the November 1984 event; and
- the surrounding landform and development at that time is uncertain, but probably less confining of overland flows to the south of Hay Street and the west of the Entertainment Centre (since the car park was not there).

Furthermore, the November 1984 event was also run in TUFLOW under existing conditions (i.e. with the culvert amplifications of the mid 1980s).

1.2 RESULTS AND COMMENT

DRAINS model output information is included in Appendix G2.

TUFLOW model flow regimes figures for existing conditions are included in Appendix C (of the main report) as are the potential flood impacts of the proposed SICEEP development, with discussion of potential flood impacts provided in Section 3 of the main report.

The TUFLOW figures indicate:

- for the November 1984 event;
 - under pre-culvert amplification conditions, the flood level at the south east corner of the building (near the Hay Street and Harbour Street intersection) is 4.0mAHD, and at western loading dock area 3.9mAHD. This is some 0.7m higher than observed, and would have flooded the Entertainment Centre above floor level. Since this was not observed, then the most likely explanation for the inconsistency is that the overland flow paths surrounding the Entertainment Centre in the 1984 event where more substantial than under existing conditions (which has been modelled). under post-culvert amplification conditions, the water levels adjacent to the south-
 - east corner Entertainment Centre are seen to be approximately 3.4mAHD (i.e.