

APPENDIX A – SURFACE WATER QUALITY MONITORING RESULTS

			-	-	Site D Mon	itoring Re	sults		-		-	
	рН	Dissolved	Electrical	Total Suspended Solids		Chloride	Sodium	Arsenic	Manganese	Dissolved Iron	Total Nitrogen	Total
	pr.	Oxygen	Conductivity	(TSS)	(TDS)							Phosphorus
Unit		mg/L	μS/cm k 25.00C	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L
Limit of Reporting	0.1		1	< 2	1	1	1	0.001	0.001	0.05	0.1	0.01
ANZECC Trigger Values for physical & chemical	6.5 - 8		30 - 350								0.25	0.02
stressors for south-east Australia for slightly	6.5 - 8		30 - 350								0.25	0.02
disturbed ecosystems (Upland River) ANZECC Trigger Values - Freshwater Ecosystems												
99% Level of Species Protection								< LOR	1.2			
95% Level of Species Protection								0.013	1.9			
90% Level of Species Protection								0.042	2.5			
80% Level of Species Protection								0.14	3.6			
Australian Drinking Water Guidelines												
Health								0.01	0.5			
Aesthetic	6.5 - 8.5	> 85%			600	250	180		0.1	0.3		
14/02/2007	6.4		69		111	4.8		< 0.001	0.111	1.54	4.2	3.15
27/02/2007	6.3		62		112	4.4			0.433	1.49		
22/03/2007	6.6		84		77	3.9	4		0.417	1.93	2.9	
26/04/2007	6.7		109		128	4.2			0.972	4.74		
28/05/2007	7		115		118	4.4			0.94	7.82		
18/06/2007	6.2		87		149				0.105	1.77	1.5	
16/07/2007	6.1		138		129	23.4			0.257 0.112	1.57	2.4	
13/02/2008	6.2 6.4		83 230		130 79	9 16.3	6		0.112	2.22	_	0.1 0.16
12/03/2008								< 0.001				
14/04/2008	6.9 6.5		98 103		107 86	17.2			0.143 0.125	1.69	3.4	0.07 0.18
14/05/2008 11/07/2008	7.1		103		99	6.1 16.6	7		0.125	1.83	2.8	0.18
11/07/2008	6.7		124		120	10.0		0.001	0.082	2.59	2.0	
14/10/2008	6.5		158		128	7	4		0.250	3.29	1.8	
6/03/2009	6.7	8.2	98		116.4	9.7			0.066			0.2
11/06/2009	6.3	10.4	66		117	12			0.058			
9/07/2009	6.1	8.8			110	12			0.031	0.76		
18/08/2009	6.8	10.7	87		120	13			0.097	0.79		
14/09/2009	7.1	10.2	96		130	14			0.21	1.1		
14/10/2009	8.3	10.8	110		130	15	7.9	0.001	0.47	2.1		
12/11/2009	7.5	6.4	130		120	18	8.7	0.001	0.12			
10/12/2009	8.3	10.8	200		160	23			0.061	0.26		
8/01/2010	5.9	5.8	110		220	12			0.56	2.1		
4/02/2010	6	8.9			450	6.6			0.12			
4/03/2010	6.9	7.9	52		80	7	3.6		0.11			
16/04/2010	10	9.1			58	7.7			0.009			
14/05/2010	6		50				4		0.033	0.27	1.9	0.14
16/06/2010	5.1	11.8	63		100	9			0.016	0.4		
20/07/2010	6.9	7.3	71 70		77	9.2	4.9	0.001	0.052	0.61		
13/08/2010 13/09/2010	6.7 7.2		70						1	1	1	
13/09/2010 8/10/2010	7.2		72 82						 	 	1	
8/10/2010 8/11/2010	6.6		82 51						 	 	1.6	0.14
15/12/2010	6.7		100	10					1	 	1.0	0.14
13/12/2010	7.1		110	16		 			 		1	
11/04/2011	6.7		110	19					1	<u> </u>	1.7	0.09
13/07/2011	7.3		110	6				0.001	0.011	0.43	1.6	
17/02/2012	6.2		100	36					1	0.43	2.5	
14/05/2012	7		160	13							2.6	
14/11/2012	6.8		190	5							2.1	
12/02/2013	7.1		280								4.1	0.18
16/05/2013	7.5		270	41							1.9	
16/08/2013	7.3		190	26							2.8	
14/11/2013	7.9		290	100							2.7	
14/02/2014	9.2		520	21							3	0.12
21/05/2014	7.4		340	20					1	ļ	2.3	
20/11/2014	8		600	4							4.1	
20/02/2015	8.2		1300	6			l				9.9	0.02

Gunlake Quarry Extension Project





	,		S	ite O Monitor	ing Results				•			
	рН	Dissolved Oxygen	Electrical Conductivity	Total Suspended Solids (TSS)	Total Dissolved Solids (TDS)	Chloride	Sodium	Arsenic	Manganese	Dissolved Iron	Total Nitrogen	Total Phosphorus
Unit		mg/L	μS/cm k 25.00C	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L
Limit of Reporting	0.1		1	< 2	1	1	1	0.001	0.001	0.05	0.1	0.01
ANZECC Trigger Values for physical & chemical stressors for south-east Australia for slightly disturbed ecosystems (Upland River)	6.5 - 8		30 - 350								0.25	0.02
ANZECC Trigger Values - Freshwater Ecosystems	s											
99% Level of Species Protection								< LOR	1.2			
95% Level of Species Protection								0.013	1.9 2.5			
90% Level of Species Protection 80% Level of Species Protection								0.042	3.6			
Australian Drinking Water Guidelines								0.14	3.0			
Health								0.01	0.5			
Aesthetic	6.5 - 8.5	> 85%			600	250	180		0.1	0.3		
14/02/2007	6.5		279		207	51.2	22	< 0.001	0.03	1.76	4.1	0.26
27/02/2007	7.7		253		190	34.1	14	0.002	0.044	0.91	2.5	0.1
22/03/2007	7.5		400		252	47.6	26	0.002	0.104	0.91	1.7	0.07
26/04/2007	8.1		542		364	82.1	42	< 0.001	0.08	0.44	1.7	0.05
28/05/2007	8		611		332	90.2	47	< 0.001	0.164	0.36	1.9	0.12
18/06/2007	7		240	-	193	42.5	20	< 0.001	0.025	1.43	3.6	0.22
16/07/2007	7.2		855		480	183	66	< 0.001	0.028	0.34	1.2	0.07
13/02/2008 12/03/2008	7.2		552 1372		446 894	91.2 401	43 118	< 0.001	0.094 0.103	1.17 0.32	1.6	0.01
14/04/2008	8.2		3960		2780	1220	357	< 0.001	0.103	1.02	0.8	0.03
14/05/2008	8.2		4260		2360	1180	430	0.001	0.071	0.05	0.8	0.01
11/07/2008	8.2		1329		808	373	112	< 0.001	0.013	0.19	0.9	0.37
11/09/2008	8.3		2280		1350	641		< 0.001	0.034	0.27	0.8	0.01
14/10/2008	7.6		686		468	144	61	< 0.001	0.062	2.08	0.7	0.08
6/03/2009	8.3	9.5	560		340	87	38	< 0.001	0.004	0.2		
11/06/2009	7.8	10.3	350		241	62	31	< 0.001	0.003	0.19		
9/07/2009	6.6	6.7	190		330	35	16	< 0.001	0.004	0.79		
18/08/2009	6.9	8.8	210		380	36	18	< 0.001	0.017	0.7		
14/09/2009	6.5	3	190		1100	28	16	< 0.001	0.011	0.62		
14/10/2009 12/11/2009	7.3 7.5	9.7 3.3	150		1400 920	19 23	30 24	0.001	0.007 0.086	1.5 0.85		-
10/12/2009	6	1.3	200 170		940	23	17	0.001	0.086	0.85		-
8/01/2010	6.9	7.2	380		260	55	25	0.001	0.19	0.39		
4/02/2010	6.3	1.4	370		370	56	26	0.001	0.53	0.33		
4/03/2010	8	8	470		320	73	39	0.001	0.003	0.13		
16/04/2010	8.5	9.3	540		340	87	46	0.001	0.003	0.06		
14/05/2010	8.5		550		350		49	0.001	0.004	0.03	1.3	0.05
16/06/2010	5.8	8.4	420		520	80	42	0.001	0.013	0.29		
20/07/2010	7.4	9.3	520		350	110	50	0.001	0.008	0.1		
13/08/2010	7.7		340	470						ļI		
13/09/2010	8.3		1200	22								
8/10/2010	8.5		1200	8							4.5	0.15
8/11/2010 15/12/2010	7.9 7.8		360 430	150 49						 	1.5	0.16
15/12/2010 13/01/2011	7.8 8.4		950	49		 				 		
11/04/2011	8		550	10							1.3	0.05
13/07/2011	8.3		1300	11				0.001	0.012	0.05	0.8	0.03
17/02/2012	6.6		240	23							2.2	0.10
14/05/2012	8.3		1500	4							0.8	0.01
14/11/2012	8.1		2900	8							0.7	0.02
12/02/2013	7.8		1100	19							1.5	0.08
16/05/2013	8.3		1200	7							0.8	0.02
16/08/2013	8.1		1700	3							0.8	0.01
14/11/2013	8.1		1200	13							0.6	0.02
14/02/2014	0.5		1000								10	0.05
21/05/2014	8.5		1200	7							1.8	0.06
20/11/2014 20/02/2015	8.2		930	14							0.94	0.02
20/02/2015 14/05/2015	8.2		2000	2		-					0.94	0.02
14/05/2015	6.5		2000				-	_	L		0.57	0.01

Gunlake Quarry Extension Project





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				Site Monitoring								
	рН	Dissolved Oxygen	Electrical Conductivity	Total Suspended Solids (TSS)	Total Dissolved Solids (TDS)	Chloride	Sodium	Arsenic	Manganese	Dissolved Iron	Total Nitrogen	Total Phosphorus
Unit		mg/L	μS/cm k 25.00C	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L
Limit of Reporting	0.1		1	< 2	1	1	1	0.001	0.001	0.05	0.1	0.01
ANZECC Trigger Values for physical & chemical												
stressors for south-east Australia for slightly	6.5 - 8		30 - 350								0.25	0.02
disturbed ecosystems (Upland River)												
ANZECC Trigger Values - Freshwater Ecosystems												
99% Level of Species Protection								< LOR	1.2			
95% Level of Species Protection								0.013	1.9			
90% Level of Species Protection								0.042	2.5			
80% Level of Species Protection								0.14	3.6			
Australian Drinking Water Guidelines												
Health								0.01	0.5			
Aesthetic	6.5 - 8.5	> 85%			600	250	180		0.1	0.3		
14/02/2007	6.8		111		110	17.5	11	< 0.001	0.189	8.8	4.7	5.55
27/02/2007	6.2		114		209	11.5	7	< 0.001	0.062	4.09	2.1	0.22
22/03/2007	6.6		142		213	7.3	8	0.003	0.832	5.57	2.5	0.12
26/04/2007	7		205		800	20.4	14	0.007	1.7	28.6	8.8	1.22
28/05/2007	6.5		61		91	6.2	9	< 0.001	0.023	2.52	1.6	0.04
18/06/2007	6.2 5.9		96 143		167	22.3 25.7	11	< 0.001	0.032 0.128	1.69	1.2	0.03 0.13
16/07/2007 13/02/2008	6.3		143 105		142 282	25.7 10.3	14 10	0.001	0.128	0.98 4.68	2	0.13
								0.001				
12/03/2008 14/04/2008	6.4 5.9		132 96		286 147	19.8 20.8	8	< 0.003	0.682	18.6 2.97	3.3 2.2	0.3 0.21
14/04/2008	8.2		3640		1950	846	376	< 0.001	0.025	0.08	1.8	0.91
11/07/2008	8.3		3230		2060	822	306	0.002	0.023	0.05	1.4	0.13
11/09/2008	5.7		149		398	27	300	< 0.002	0.312	6.21	0.9	0.13
14/10/2008	6.2		123		407	19	11	0.002	0.52	12.6	1.4	0.06
6/03/2009	0.2		123		407	15	11	0.002	0.32	12.0	1.4	0.00
11/06/2009												
9/07/2009												
18/08/2009												
14/09/2009												
14/10/2009												
12/11/2009												
10/12/2009												
8/01/2010												
4/02/2010												
4/03/2010												
16/04/2010												
14/05/2010												
16/06/2010												
20/07/2010												
13/08/2010	6.4		97	21								
13/09/2010												
8/10/2010	ļ										ļ	1
8/11/2010	!					ļ					-	-
15/12/2010	6.3		140	6		-					-	-
13/01/2011	 					_					-	-
11/04/2011	l										-	1
13/07/2011	 					 					.	1
17/02/2012	-					1					-	-
14/05/2012	-										 	-
14/11/2012	1										1	+
12/02/2013 16/05/2013	l										-	-
16/08/2013	8		1800	5		-					0.55	0.01
14/11/2013	·		1000	,		-					0.33	0.01
14/11/2015	 					-						
21/05/2014	l											1
20/11/2014	1											
20/02/2015	1					1					l	
14/05/2015	1					1					l	

Surface Water Assessment



APPENDIX B - WATER BALANCE SUMMARY SHEETS



Model Assumptions: Approved Operation (0.75 Mtpa)

Storage Assumptions

Storage Name	Surface Area	Average Depth	Volume	Contributing Catchments	Overflows	Function
	(m ²)	(m)	(ML)			
Process Water Dam	4500	2.2	10	DW -1 (19ha)	to Chapmans Creek	Captures runoff from DW-1 for process water use
Pit Sump	1500	3	5 plus flood storage	Pit (14ha)	no overflows	Captures runoff from the pit for process water use
Clean Water Dam 1	3500	2	7	CW -1 (70ha)	to Chapmans Creek	Captures runoff from CW-1 for process water use
Clean Water Dam 2	6000	2.5	15	CW -2 (62ha)	to Chapmans Creek	Captures runoff from CW-2 for process water use

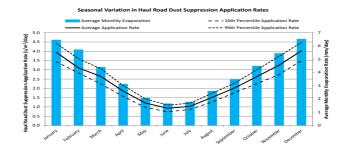
Note: Storage volumes have been estimated using available information and have not been confirmed by survey

Demand Assumptions

Haul Road Dust Suppression

Water use for haul road dust suppression is calculated as a function of the haul road area and prevailing climatic conditions using the following formulae

 $DSupp(t) = Max(0,((Evap(t) \times PanCoeff) - Rain(t)) \times HRArea \times 0.01)$ Where: $DSupp(t) = Daily \ water \ use \ for \ haul \ road \ dust \ suppression \ (ML/day)$ $Evap(t) = Daily \ pan \ evaporation \ (mm/day)$ $PanCoeff = Evaporation \ adjustment \ coefficient$ $Rain(t) = Daily \ rainfall \ (mm/day)$ $HRArea = Area \ of \ active \ haul \ road \ (ha)$



The following haul road area and Pan Coeff were adopted

Haul Road Area 5ha

Pan Coeff 0.72 (This equates to an average annual application rate of 3L/m² per day)

The calculated annual demand varies between 41 to 45 ML/year, depending on rainfall over the year.

The demand varies seasonally inline with evaporation rates as shown in the above chart.

Plant Water Use

Plant water use is calculated as a function of the plant throughput and a water use rate

Plant Throughput 0.75 Mtpa

Water use rate 18.2 L/t (Calculated from metered data provided by Gunlake)

Annual Water Use 13.7 ML/year

Process Water Use Order of Preference

The water balance model preferentially sources water to meet process water demands as follows:

1st preference: Water stored in the pit

2st preference: Water stored in the process water dam 3rd preference: Water stored in Clean water dams 4th preference: Water imported to site via tankers

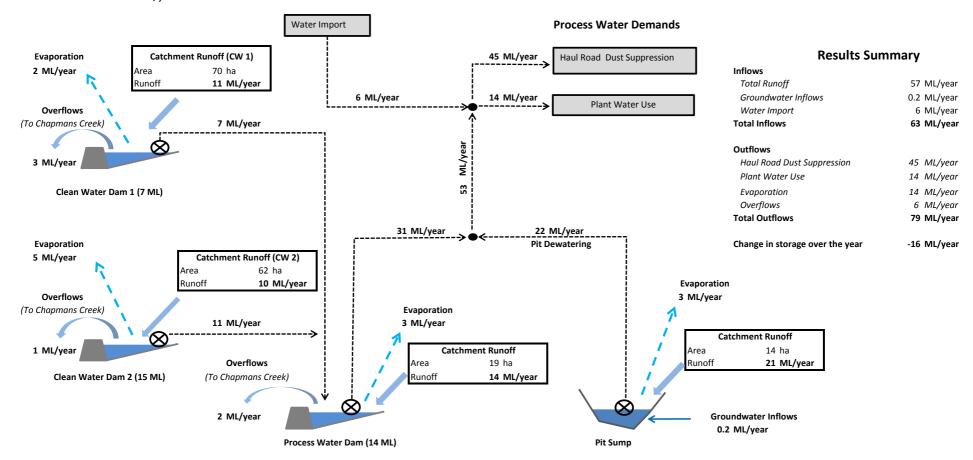




Gunlake Quarry: Site Water Balance: Approved Operation: Surface Water Management Plan

Typical Dry (10th Percentile) Rainfall Year

Annual Rainfall 451 mm/year

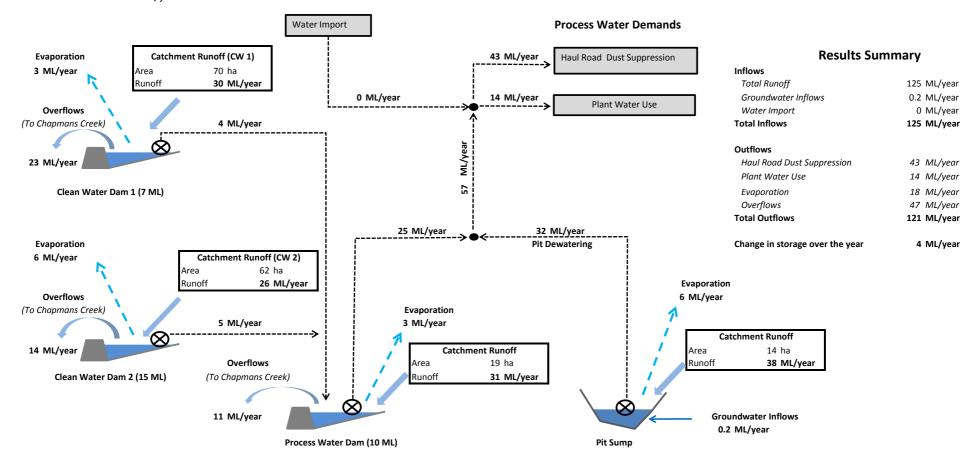




Gunlake Quarry: Site Water Balance: Approved Operation: Surface Water Management Plan

Typical Median (50th Percentile) Rainfall Year

Annual Rainfall 695 mm/year

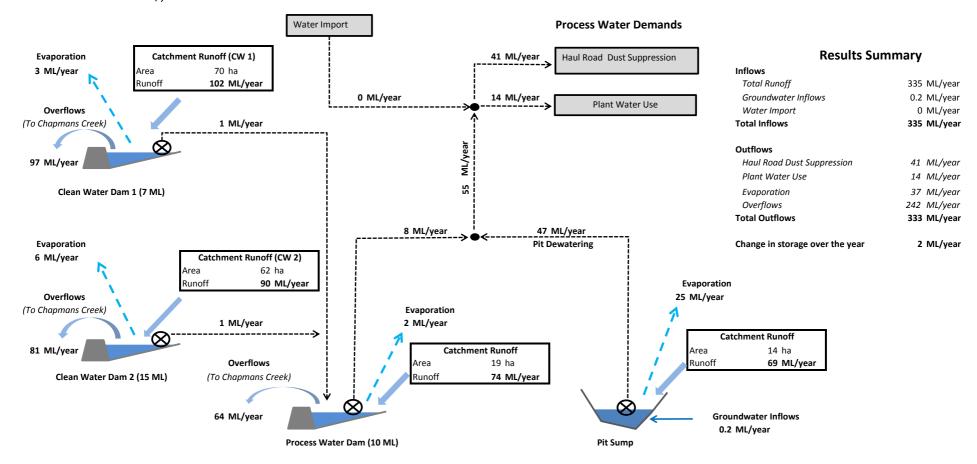




Gunlake Quarry: Site Water Balance: Approved Operation: Surface Water Management Plan

Typical Wet (90th Percentile) Rainfall Year

Annual Rainfall 982 mm/year





Gunlake Quarry: Site Water Balance

Model Assumptions: Quarry Year 1: Surface Water Management Plan

Storage Assumptions

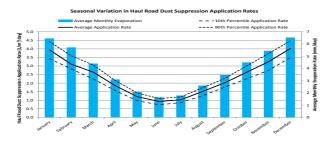
Storage Name	Surface Area	Average Depth	Volume	Contributing Catchments	Overflows	Function
	(m²)	(m)	(ML)			
Process Water Dam	7500	5	35	DW -4 (19ha)	to Chapmans Creek	Captures runoff from DW-4 for process water use
Pit Sump	+7000	+3	20 plus flood storage	Pit (29ha)	no overflows	Captures runoff from the pit
Clean Water Dam 2	6500	2.3	15	CW -2 (48ha) + DW-2 (5ha)	to Chapmans Creek	Sedimentation dam for emplacement area. Water stored for process water use
Pit Dewatering Dam	10000	3	30	DW 5 (16ha)	to Chapmans Creek	Treats water dewatered from the pit. Water stored for process water use

Demand Assumptions

Haul Road Dust Suppression

Water use for haul road dust suppression is calculated as a function of the haul road area and prevailing climatic conditions using the following formulae

 $DSupp(t) = Max(0, ((Evap(t) \times PanCoeff) - Rain(t)) \times HRArea \times 0.01)$ Where: $DSupp(t) = Daily \ water \ use \ for \ haul \ road \ dust \ suppression \ (ML/day)$ $Evap(t) = Daily \ pane \ vaporation \ (mm/day)$ $PanCoeff = Evaporation \ adjustment \ coefficient$ $Rain(t) = Daily \ rainfall \ (mm/day)$ $HRArea = Area \ of \ active \ haul \ road \ (ha)$



The following haul road area and Pan Coeff were adopted

Haul Road Area 8ha

Pan Coeff 0.72 (This equates to an average annual application rate of $2.3L/m^2$ per day)

The calculated annual demand varies between 66 to 74 ML/year, depending on rainfall over the year.

The demand varies seasonally inline with evaporation rates as shown in the above chart.

Plant Water Use

Plant water use is calculated as a function of the plant throughput and a water use rate

Plant Throughput 2.0 Mtpa

Water use rate 18.2 L/t (Calculated from metered data provided by Gunlake)

Annual Water Use 36.4 ML/year

Process Water Use Order of Preference

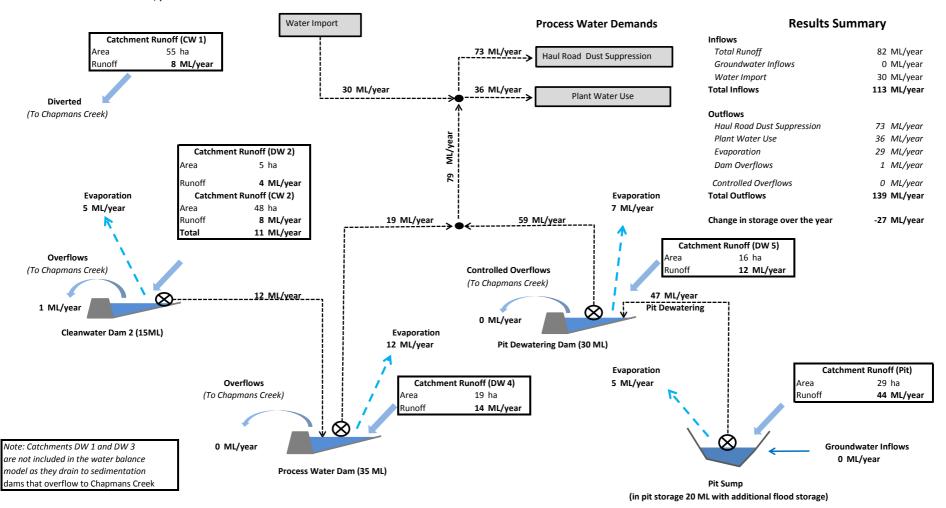
The water balance model preferentially sources water to meet process water demands as follows:

1st preference: Water stored in the process water dam
2st preference: Water stored in the Pit Dewatering Dam
3rd preference: Water stored in the Sed Dam 2
4th preference: Water imported to site via tankers



Gunlake Quarry: Site Water Balance: Quarry Year 1: Surface Water Management Plan Typical Dry (10th Percentile) Rainfall Year

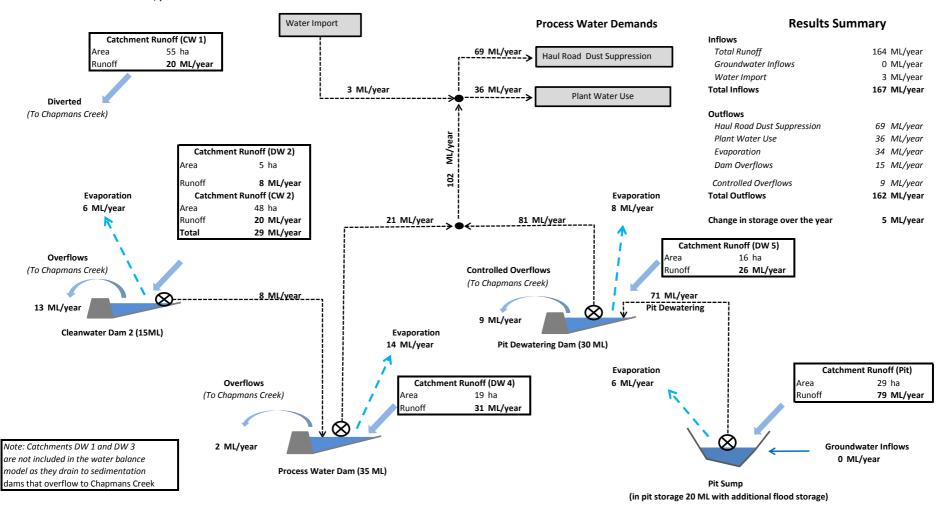
Annual Rainfall 451 mm/year





Gunlake Quarry: Site Water Balance: Quarry Year 1: Surface Water Management Plan Typical Median (50th Percentile) Rainfall Year

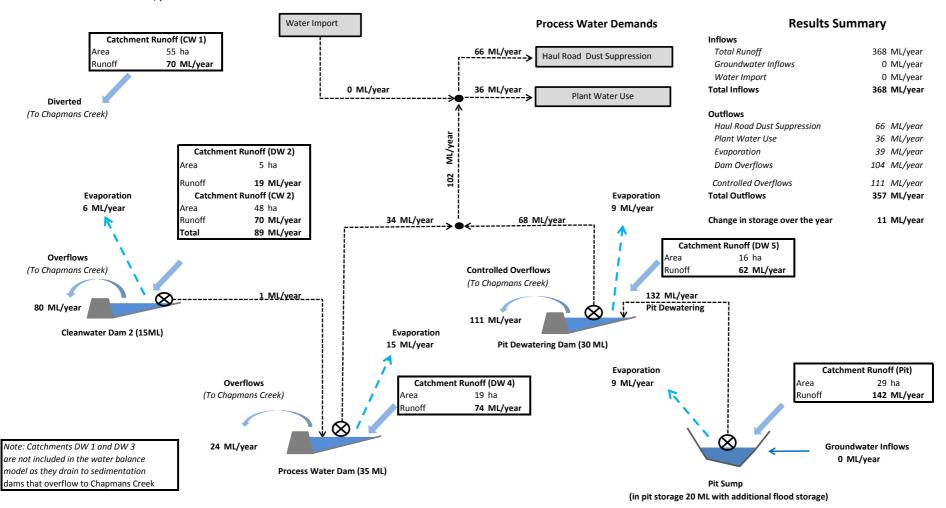
Annual Rainfall 695 mm/year





Gunlake Quarry: Site Water Balance: Quarry Year 1: Surface Water Management Plan Typical Wet (90th Percentile) Rainfall Year

Annual Rainfall 982 mm/year





Gunlake Quarry: Sedimentation Dam Calculations
Model Assumptions: Quarry Year 1: Surface Water Management Plan

Calculation Assumptions

Sedimentation dam volumes have been calculated in accordance with the methods provided in *Managing Urban Stormwater: Soils and Construction, Volume 2E – Mines and Quarries* (DECC, 2008). The following sizing methods have been adopted:

- The sedimentation dam sizing method for Type F and D soils has been adopted.
- Treatment volumes have been calculated based on the 90th Percentile 5 day rainfall event. This is in accordance with Table 6.1 *Managing Urban Stormwater: Soils and Construction, Volume 2E Mines and Quarries* (DECC, 2008) for a dam that operates form more than 3 years and overflows to a non-sensitive receiving water.
- A sediment storage volume equivalent to 50% of the treatment volume has been adopted.

Key assumptions are provided in the following table.

Assumption	Adopted Value	Source			
90th Percentile Rainfall Depth	28.6 mm	Table 6.3a Vol. 1 (Location Goulburn)			
Soil Hydrologic Group	D high runoff potential	Appendix F Vol. 1			

Calculated Dam Sizes

		Cardiated Paris 51265							
				Dam Name					
	Units	Process Water Dam	Sed Dam 1	Sed Dam 2	Sed Dam 3	Pit Dewatering Dam			
Catchment Area (ha)	(ha)	19	10	5	6	16			
5 day Rainfall Depth	(mm)	28.6	28.6	28.6	28.6	28.6			
Runoff Coefficient (Cv) ¹	-	0.56	0.56	0.56	0.56	0.56			
Sedimentation Dam Volume	(ML)	3.0	1.6	0.8	1.0	2.6			
Calculated Sediment Storage	(ML)	1.5	0.8	0.4	0.5	1.3			
Total Dam Volume	(ML)	4.6	2.4	1.2	1.4	3.8			
Proposed Dam Volume ²	(ML)	35.0	2.4	1.2	1.4	30			
Exceeds Minimum Requirements	-	Yes	Yes	Yes	Yes	Yes			

Note 1: From Table F2 Vol. 1

Note 2: Some dam volumes exceed minimum requirement as they are sized to store water for process water use



Gunlake Quarry: Site Water Balance

Model Assumptions: Quarry Year 5: Surface Water Management Plan

Storage Assumptions

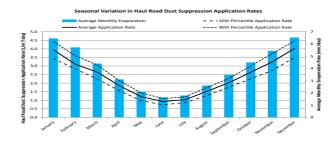
Storage Name	Surface Area	Average Depth	Volume	Contributing Catchments	Overflows	Function
	(m²)	(m)	(ML)			
Process Water Dam	7500	5	35	DW -4 (19ha)	to Chapmans Creek	Captures runoff from DW-4 for process water use
Pit Sump	+7000	+3	20 plus flood storage	Pit (29ha)	no overflows	Captures runoff from the pit
Clean Water Dam 2	6500	2.3	15	CW -2 (48ha) + DW-2 (5ha)	to Chapmans Creek	Sedimentation dam for emplacement area. Water stored for process water use
Pit Dewatering Dam	10000	3	30	DW 5 (6ha)	to Chapmans Creek	Treats water dewatered from the pit. Water stored for process water use

Demand Assumptions

Haul Road Dust Suppression

Water use for haul road dust suppression is calculated as a function of the haul road area and prevailing climatic conditions using the following formulae

 $DSupp(t) = Max(0, ((Evap(t) \times PanCoeff) - Rain(t)) \times HRArea \times 0.01)$ Where: $DSupp(t) = Daily \ water \ use \ for \ haul \ road \ dust \ suppression \ (ML/day)$ $Evap(t) = Daily \ pan \ evaporation \ (mm/day)$ $PanCoeff = Evaporation \ adjustment \ coefficient$ $Rain(t) = Daily \ rainfall \ (mm/day)$ $HRArea = Area \ of \ active \ haul \ road \ (ha)$



The following haul road area and Pan Coeff were adopted

Haul Road Area 8ha

Pan Coeff 0.72 (This equates to an average annual application rate of $2.3L/m^2$ per day)

The calculated annual demand varies between 66 to 74 ML/year, depending on rainfall over the year.

The demand varies seasonally inline with evaporation rates as shown in the above chart.

Plant Water Use

Plant water use is calculated as a function of the plant throughput and a water use rate

Plant Throughput 2.0 Mtpa

Water use rate 18.2 L/t (Calculated from metered data provided by Gunlake)

Annual Water Use 36.4 ML/year

Process Water Use Order of Preference

The water balance model preferentially sources water to meet process water demands as follows:

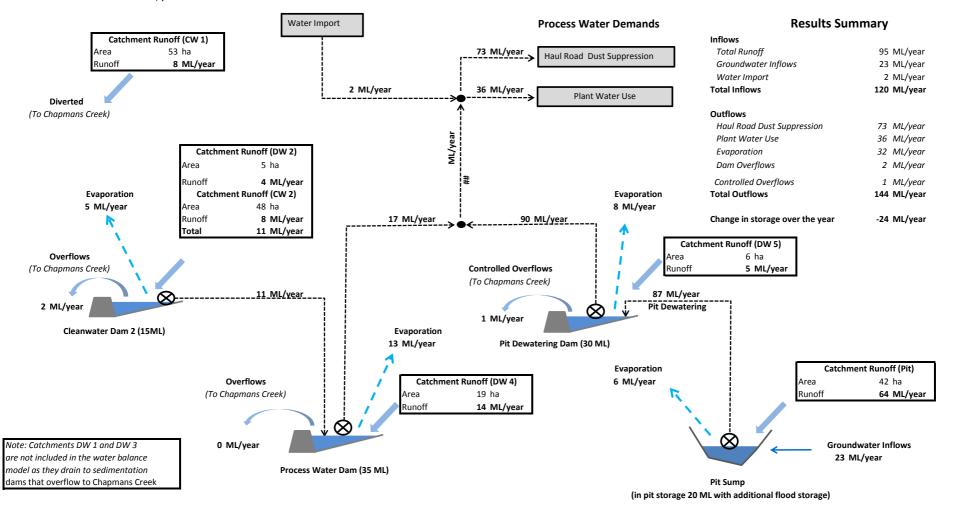
1st preference: Water stored in the process water dam
2st preference: Water stored in the Pit Dewatering Dam
3rd preference: Water stored in the Sed Dam 2
4th preference: Water imported to site via tankers



Gunlake Quarry: Site Water Balance: Quarry Year 5: Surface Water Management Plan

Typical Dry (10th Percentile) Rainfall Year

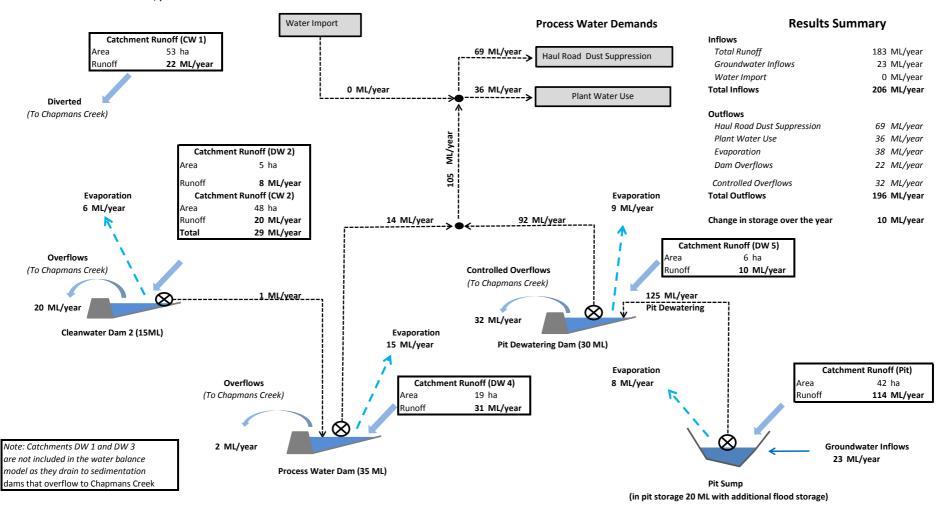
Annual Rainfall 451 mm/year





Gunlake Quarry: Site Water Balance: Quarry Year 5: Surface Water Management Plan Typical Median (50th Percentile) Rainfall Year

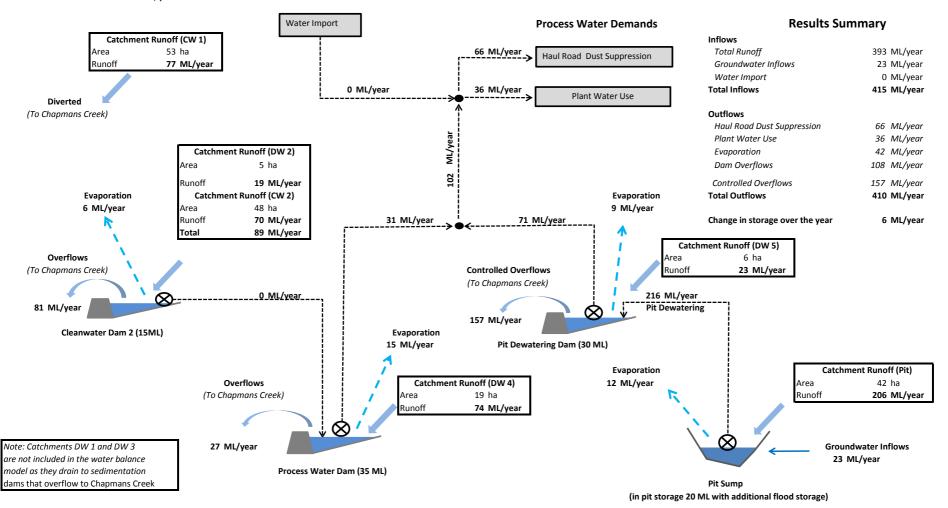
Annual Rainfall 695 mm/year





Gunlake Quarry: Site Water Balance: Quarry Year 5: Surface Water Management Plan Typical Wet (90th Percentile) Rainfall Year

Annual Rainfall 982 mm/year





Gunlake Quarry: Sedimentation Dam Calculations
Model Assumptions: Quarry Year 5: Surface Water Management Plan

Calculation Assumptions

Sedimentation dam volumes have been calculated in accordance with the methods provided in *Managing Urban Stormwater: Soils and Construction, Volume 2E – Mines and Quarries* (DECC, 2008). The following sizing methods have been adopted:

- The sedimentation dam sizing method for Type F and D soils has been adopted.
- Treatment volumes have been calculated based on the 90th Percentile 5 day rainfall event.
 This is in accordance with Table 6.1 Managing Urban Stormwater: Soils and Construction,
 Volume 2E Mines and Quarries (DECC, 2008) for a dam that operates form more than 3
 years and overflows to a non-sensitive receiving water.
- A sediment storage volume equivalent to 50% of the treatment volume has been adopted.

Key assumptions are provided in the following table.

Assumption	Adopted Value	Source			
90 th Percentile Rainfall Depth	28.6 mm	Table 6.3a Vol. 1 (Location Goulburn)			
Soil Hydrologic Group	D high runoff potential	Appendix F Vol. 1			

Calculated Dam Sizes

		Cardiated Paris 51265							
				Dam Name					
	Units	Process Water Dam	Sed Dam 1	Sed Dam 2	Sed Dam 3	Pit Dewatering Dam			
Catchment Area (ha)	(ha)	19	10	5	6	5			
5 day Rainfall Depth	(mm)	28.6	28.6	28.6	28.6	28.6			
Runoff Coefficient (Cv) ¹	-	0.56	0.56	0.56	0.56	0.56			
Sedimentation Dam Volume	(ML)	3.0	1.6	0.8	1.0	0.8			
Calculated Sediment Storage	(ML)	1.5	0.8	0.4	0.5	0.4			
Total Dam Volume	(ML)	4.6	2.4	1.2	1.4	1.2			
Proposed Dam Volume ²	(ML)	35.0	2.4	1.2	1.4	30			
Exceeds Minimum Requirements	-	Yes	Yes	Yes	Yes	Yes			

Note 1: From Table F2 Vol. 1

Note 2: Some dam volumes exceed minimum requirement as they are sized to store water for process water use



Gunlake Quarry: Site Water Balance

Model Assumptions: Quarry Years 10 to 30: Surface Water Management Plan

Storage Assumptions

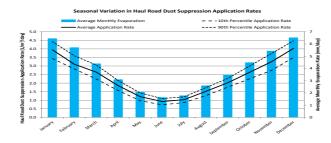
Storage Name	Surface Area	Average Depth	Volume	Contributing Catchments	Overflows	Function
	(m²)	(m)	(ML)			
Process Water Dam	7500	5	35	DW -4 (19ha)	to Chapmans Creek	Captures runoff from DW-4 for process water use
Pit Sump	+7000	+3	20 plus flood storage	Pit (53ha)	no overflows	Captures runoff from the pit
Clean Water Dam 2	6500	2.3	15	CW -2 (48ha) + DW-2 (5ha)	to Chapmans Creek	Sedimentation dam for emplacement area. Water stored for process water use
Pit Dewatering Dam	10000	3	30	DW - 5 (2ha)	to Chapmans Creek	Treats water dewatered from the pit. Water stored for process water use

Demand Assumptions

Haul Road Dust Suppression

Water use for haul road dust suppression is calculated as a function of the haul road area and prevailing climatic conditions using the following formulae

 $DSupp(t) = Max(0, ((Evap(t) \times PanCoeff) - Rain(t)) \times HRArea \times 0.01)$ Where: $DSupp(t) = Daily \ water \ use \ for \ haul \ road \ dust \ suppression \ (ML/day)$ $Evap(t) = Daily \ pan \ evaporation \ (mm/day)$ $PanCoeff = Evaporation \ adjustment \ coefficient$ $Rain(t) = Daily \ rainfall \ (mm/day)$ $HRArea = Area \ of \ active \ haul \ road \ (ha)$



The following haul road area and Pan Coeff were adopted

Haul Road Area 8ha

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The demand varies seasonally inline with evaporation rates as shown in the above chart.

Plant Water Use

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Plant Throughput 2.0 Mtpa

Water use rate 18.2 L/t (Calculated from metered data provided by Gunlake)

Annual Water Use 36.4 ML/year

Process Water Use Order of Preference

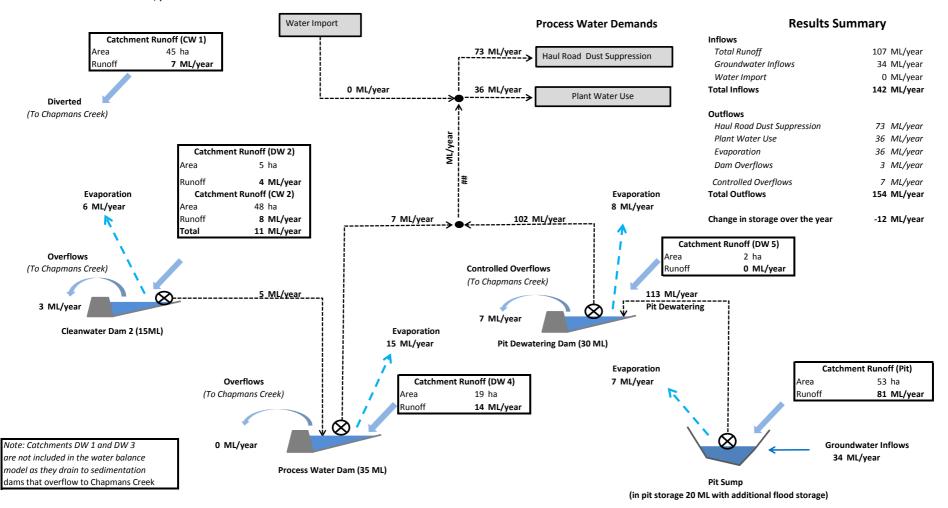
The water balance model preferentially sources water to meet process water demands as follows:

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4th preference: Water imported to site via tankers



Gunlake Quarry: Site Water Balance: Quarry Years 10 to 30: Surface Water Management Plan Typical Dry (10th Percentile) Rainfall Year

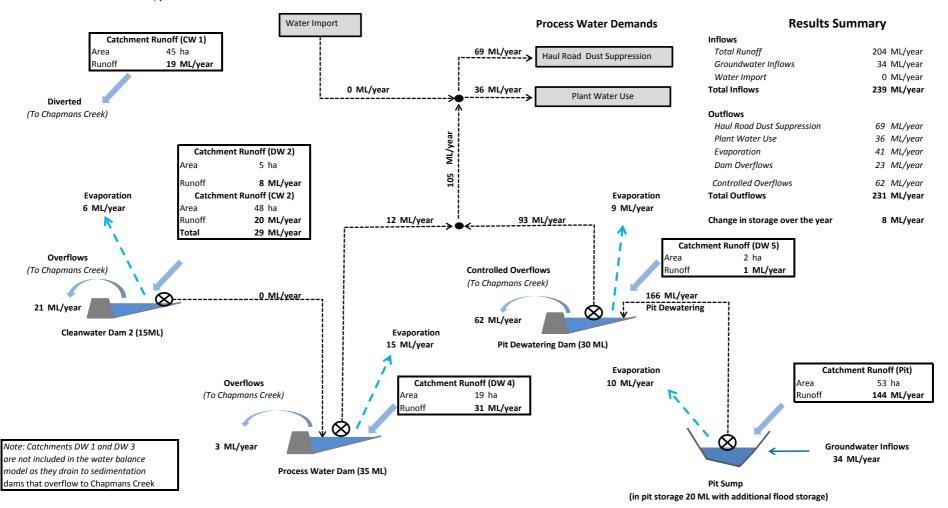
Annual Rainfall 451 mm/year





Gunlake Quarry: Site Water Balance: Quarry Years 10 to 30: Surface Water Management Plan Typical Median (50th Percentile) Rainfall Year

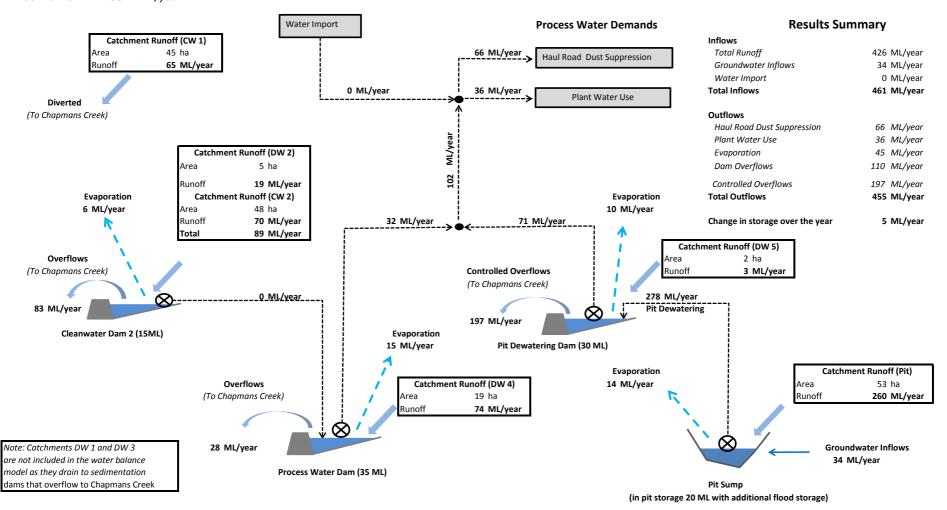
Annual Rainfall 695 mm/year





Gunlake Quarry: Site Water Balance: Quarry Years 10 to 30: Surface Water Management Plan Typical Wet (90th Percentile) Rainfall Year

Annual Rainfall 982 mm/year





Gunlake Quarry: Sedimentation Dam Calculations Model Assumptions: Quarry Years 10 to 30: Surface Water Management Plan

Calculation Assumptions

Sedimentation dam volumes have been calculated in accordance with the methods provided in *Managing Urban Stormwater: Soils and Construction, Volume 2E – Mines and Quarries* (DECC, 2008). The following sizing methods have been adopted:

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- Treatment volumes have been calculated based on the 90th Percentile 5 day rainfall event. This is
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 a non-sensitive receiving water.
- A sediment storage volume equivalent to 50% of the treatment volume has been adopted.

Key assumptions are provided in the following table.

Assumption	Adopted Value	Source		
90th Percentile Rainfall Depth	28.6 mm	Table 6.3a Vol. 1 (Location Goulburn)		
Soil Hydrologic Group	D – high runoff potential	Appendix F Vol. 1		

Calculated Dam Sizes

	Calcalated Ball Sizes						
		Dam Name					
	Units	Process Water Dam	Sed Dam 1	Sed Dam 2	Sed Dam 3	Pit Dewatering Dam	
Catchment Area (ha)	(ha)	19	10	5	6	2	
5 day Rainfall Depth	(mm)	28.6	28.6	28.6	28.6	28.6	
Runoff Coefficient (Cv) ¹	-	0.56	0.56	0.56	0.56	0.56	
Sedimentation Dam Volume	(ML)	3.0	1.6	0.8	1.0	0.3	
Calculated Sediment Storage	(ML)	1.5	0.8	0.4	0.5	0.2	
Total Dam Volume	(ML)	4.6	2.4	1.2	1.4	0.5	
Proposed Dam Volume ²	(ML)	35.0	2.4	1.2	1.4	30	
Exceeds Minimum Requirements	-	Yes	Yes	Yes	Yes	Yes	

Note 1: From Table F2 Vol. 1

Note 2: Some dam volumes exceed minimum requirement as they are sized to store water for process water use