APPENDIX 2

CIVIL ROAD DESIGN REPORT





Oakdale Central Development

Regional Link Roads



OWR Upgrade - Road Design Report

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Approver: Anthony McLandsborough

Report no: R002 Revision: 06 Date: August 2014

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Finalisation signatures

The design described in this report is considered to have been finalised.

Signature Peter Wark	P.a.	Date
Associate Director (Author)		07/08/14
Mark Marsic Lead Designer (Road)	Ato	07/08/14
Anthony McLandsborough Director	Sitt.	07/08/14
	MAN (

Notes: The finalisation signatures shown above do not provide evidence of approval to the design. Approval signatures are shown on the title sheet of the design plans.

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Authority Endorsement The concept design of the OWR Upgrade as described in this report has been reviewed and is endorsed as suitable for progressing to detailed design.

Department of Planning

Authorised Representative (Name)	Signature	Date
Fairfield City Council		
Authorised Representative (Name)	Signature	Date
Blacktown City Council		
Authorised Representative (Name)	Signature	Date
Road and Maritime Services		
Authorised Representative (Name)	Signature	Date

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1 Scope

1.1 Purpose of Design Report

The purpose of this Design Report is to:

- Describe the Project Scope and Background;
- Define the Project's objectives;
- Describe those documents which make up the Design and subsequent Application;
- Describe the Design Inputs;
- Describe the Design parameters and why they were selected;
- Describe the Road Scape Allocation and how guidelines are met;
- Describe the Road Typical Cross Sections and how standards are met;
- Describe Horizontal Curves and Alignments and how standards are met;
- Describe the Geometric Design and how constraints and standards are met; and
- Describe the Design Finalisation Process.

This Design Report describes *why things were done.* What was done is shown on the plans. The objectives of this Design Report are to provide the reasons for design decisions.

1.2 Context/Background

The existing section of Old Wallgrove Road (OWR) between the recently completed EPLR and the Oakdale Estate, is best categorised as a rural road, comprising a variable width pavement from 7 to 8m with flush shoulders and table drains. This section of road is approximately 1600m in length. The road is unlit and is in a poor condition with numerous pavement failures along the stretch of road.

Existing features of OWR (post temporary upgrade as described below) are:

- Total length of road 1600m.
- Single carriageway variable width, average of 7m, widening at access points to circa 12m.
- Unformed shoulders Stormwater freely drains to surrounding verge.
- Flexible pavement with flush seal.
- Significant pavement cracking and potholing.
- Sign posted speed limit 70km/h.



• Sight distance satisfactory apart from the area directly south of the SCA crossing.

As part of the Concept Approval for the Oakdale Estate, a section of OWR was to be temporarily upgraded to provide additional road width to cater for additional heavy traffic. These works were completed in 2011. Since the completion of these roadworks, the pavement has deteriorated and potholes have developed, calling for a need to rehabilitate OWR. The drawings associated with the completed upgrade works can be found in Appendix A – GHD OWR Upgrade Drawings (Works Completed).

In addition, Goodman proposes to develop the remainder of the Oakdale Estate, which necessitates consideration of the required road connection.

The Oakdale Estate is located within the Fairfield City Council Local Government area and is bounded by the future Chandos Parkway Road Corridor to the south, the SCA(SCA) pipeline to the north, OWR to the East, and Ropes Creek to the West. The Site forms part of the Oakdale Central Precinct Concept Plan Approval (08_0065) and is approximately 61.2ha in area.

The Concept Approval approved the developed of:

- Overall the subdivision, as modified, created:
 - 15 lot subdivision (total area ~ 45.8ha).
 - o 7 industrial buildings.
 - Recreation and biodiversity land (total area ~ 10.1ha)
 - o Road construction and upgrades
 - o Infrastructure
- Upgrade of a 1.6km section of OWR to provide a 7m wide road to provide B-Double access to the Estate, between the Estate Road entry location and a point on OWR located outside the Coles Myer Distribution Centre (Note: These works have been completed, refer above). Refer to Appendix A – GHD OWR Upgrade Drawings (Works Completed).
- Bulk earthworks

Much of the first half of the Estate is built, with the first leg of the Estate Road built, and the first three industrial buildings built and occupied. The remaining infrastructure is either under construction, or pending Development Approval from Fairfield City Council.

In addition, RMS have requested that the upgrade of OWR, south of the SCA pipeline, be developed and implemented to be compatible with the long term provision of a proposed north south link road. The objective of the future proposed north south link road will be to provide an connector route between the EPLR and the Chandos Parkway, and in addition, to support the development of lands along the corridor of the north south link road.

To support the ongoing development of the Oakdale Estate in the short term, the section of OWR north of the SCA pipeline through to the recently upgraded EPLR, is also required to be upgraded.



AT&L have been comissioned to develop and design the proposed permanent upgrade solution of OWR (including the section south of the SCA pipeline), which will ultimately support further development south of the pipeline.

The OWR road upgrade concept design resented in this report has been primarily developed through a series of design development negotiations with the Roads and Maritime Services in response to design options prepared by AT&L.

Transport for NSW and RMS indicated an objective to rationalise the project scope to provide an adequate level of capacity while providing a cost effective design in order to obtain a satisfactory return in the expenditure of funding generated by the State Infrastructure Levy.

This process and the background to the design development is documented in a letter prepared by AT&L and issued to the RMS on the 5 August 2104.

1.3 Project Objectives

1.3.1 Project Specific Objectives

The project specific objectives for the design are:

- Upgrade OWR to increase the traffic capacity, as outlined in the Traffic Impact Assessment prepared by Traffix and subsequent letter reports.
- Rehabilitate or replace existing pavement.
- Ensure the upgraded road can operate at the intended design speed of 80km/h and posted speed of 70km/h. NB: The section of Works south of the SCA Pipeline will as part of the OWR Upgrade, be designed to suit 60km/h due to the existing property constraints.
- Tie in with newly constructed/future regional link roads.
- Significantly improve the sight distance in the area directly south of the SCA crossing.
- Provide formal road shoulders implementation of kerb and gutter/stormwater system.
- Construct under live traffic conditions.
- Provide adequate Street lighting.
- Provide adequate road verges.

1.3.2 Common Objectives

The project will also meet the following objectives that are common to road design projects:

- Develop a cost-effective solution.
- Provide appropriate levels of safety for road users.



- Minimise land acquisition.
- Minimise disruption to adjacent property owners, being Transgrid, SCA and Austral Bricks.

1.4 Road Design Scope and Deliverables

1.4.1 Type and Stage of Design

The design stage is 'Concept'.

Note: Pending Approval of the 'Concept' design, detailed design drawings will be prepared suitable for Construction. The purpose of supplying the 'Concept' drawings is to obtain Approval from the relevant authorities.

1.4.2 Deliverables

The following documentation has been prepared to accompany the State Significant Development Application:

- Digital drawings including:
 - o Plan layouts.
 - Longitudinal sections.
 - Typical cross sections.
 - o Construction staging sketches
- Design report

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2 Design Input

2.1 Locality



Figure 1 - Locality Sketch

The Works are located along Old Wallgrove, located between the intersection with the EPLR at the north, and the intersection with the Oakdale Estate access road (Milner Avenue) to the South.

The works span two separate LGA's, Blacktown City Council and Fairfield City Council, where by the separation occurs roughly along the northern boundary of the SCA Pipeline.

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Photographs of the Site



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Photo of OWR showing pavement failure and potholing after widening works completed in 2011
Photo of OWR, located at approx. CH475 looking North

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Photo of OWR and existing access to SCA pipeline, located at approx. CH650 looking West
Photo of OWR and existing access to SCA pipeline, located at approx. CH700 looking South
Photo of OWR and existing access to SCA pipeline, located at approx. CH1000 facing Transgrid

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Photo of OWR, located at approx. CH1225 looking South.
Photo of OWR, located at approx. CH1225 lookng North.

2.2 Utility Information

The entire length of OWR has been surveyed to identify all boundary information, extent of existing pavement, drainage systems, fence lines and all service information. Potholing has been undertaken to understand and identify the exact location and size of buried services. Survey has also identified the overhead electrical services.

Services identified:

- Endeavour Energy overhead 132kV electrical.
- Transgrid Energy overhead 132kV Electrical.
- Endeavour Energy underground 11kV, overhead 11Kv and overhead LV.
- Telecommunications.

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- Sydney Water water supply.
- Jemena high pressure gas supply.

2.3

Community and Political Consultation

Community consultation of a localised nature will be carried out for those residences/business adjacent to OWR who may be affected by the construction or the adjusted geometric alignment. This will include:

- Pre-construction advice regarding construction work and staging.
- Monitoring of local residences/business during construction.

Other consultation specifically for the site:

- Liaison with Blacktown City Council and Fairfield City Council.
- Liaison with RMS.
- Route information signage (including VMS) usage covering all construction stages.
- Correspondence with identified transport organisations.
- SCA (SCA); SCA has provided 'In Principal' support of the proposed upgrade works to OWR. Evidence can be provided upon request.
- Transgrid: Transgrid has provided 'In Principal' support of the proposed upgrade works to OWR. Evidence can be provided upon request.
- Endeavour Energy; Endeavour Energy has provided 'In Principal' support of the proposed upgrade works to OWR. Evidence can be provided upon request.

Design Planning 3

3.1 **Design Parameters**

The design parameters used are listed below, in order of priority:

- 1. Austroads Guidelines.
- 2. Published RMS Supplements to Austroad Guidelines.
- 3. Australian Standards referenced in the Austroads Guidelines.
- 4. Published RMS Supplements to Australian Standards.

3.2 Variations from Original Design Constraints

Transgrid is a major property owner affected by the works. Lengthy negotiations have taken place over the last 12 months to understand what impact any widening of the existing 20.117m road reserve into their property would have.

Originally, the road reserve was proposed to be 25.7m which suggested a widening of some 5.5m into Transgrid lands (approximately CH750 to CH1600). Due to the proximity of the existing overhead structural electrical towers, the widening to this extent was not satisfactory to Transgrid. As such, the width of the overall reserve has been reduced to cater for this constraint. From these negotiations the resulting overall road reserve was 23.0m.

Through the design option review process undertaken with RMS, the road reserve width was further reduced to 21.45m. This has resulted in a reduced extent and width of the strip acquisition required along the project corridor from CH450 to Ch1600..

A localised section of 25.6m is proposed at the right hand turn into Transgrid.

Further minor encroachment into adjoining property may occur as a result of:

- cut and fill batters as a result of the final detailed vertical grading;
- requirements to accommodate drainage and/or water guality basins.

Road Function 3.3

OWR is currently the only means of road access to the Oakdale Development, Austral Brickworks and the CSR Site. A large percentage of vehicles that travel on this section of road are heavy vehicles, including B-Doubles and semi-trailers.

The section of OWR under consideration for upgrade, acts as a link between local Council Roads and other regional/state roads. By definition (as shown in section 3.4.1 below), OWR would be categorised as an interim regional road.

3.4 Road Hierarchy and Classification

3.4.1 Current Road Classification

The section of OWR proposed to be upgraded is currently not listed within the RMS 'Schedule of Classified Roads and Unclassified Regional Roads' (August 2013). It is stated that 'Local Roads are unclassified roads and therefore are not included in the Schedule'. Thus, it should be deemed that this section of OWR is currently classified as a local road, with different sections of the road under the control of both Blacktown City Council and Fairfield City Council.

3.4.2 Proposed Road Classification

The section of OWR subject to the road upgrade, from Milner Avenue to EPLR, is envisaged to be classified by TNSW as an Interim Regional Road remaining under the control of Fairfield City Council and Blacktown City Council respectively. It understood the Depart of Planning has been in consultation with Transport for New South Wales in respect of this matter.

3.4.3 Dedication of Roads

In locations where land acquisition is undertaken to widen OWR, it is proposed this land will be dedicated as public road reserve to FCC and BCC respectively.

3.5 Road Control

3.5.1 Current Control

At present, OWR is controlled by local Council. The road is controlled by:

- CH00-CH675, Fairfield Council.
- CH675-CH1650, Blacktown Council.

3.6 Design Speed

The existing posted speed limit along OWR is 70 km/h.

The design speed for the upgraded OWR section is 80 km/h. It should be noted that OWR will be signposted at 70km/h. NB: The section of Works south of the SCA Pipeline (CH350 – CH700) will be designed to a 60km/h design speed. This is a result of constraints in acquiring sufficient land to provide horizontal alignment to comply with a design speed greater than 60 km/h. In addition the section of OWR, from approximately CH350, to approximately CH700 will become redundant in the future upon delivery of the North South Link Road.

The final location of posted speed zones and advisory speed signage along the corridor will be subject to negotiation with FCC, BCC and RMS.



Traffic modelling will specifically look at each of the intersections and tie-ins that are affected by the proposed works.

3.7 Minimum Curve Radius

The minimum curve radius is governed by the proposed design speed. The minimum curve radius will be based on a design speed of 80km/h and will be designed to conform to the relevant design standards, where possible. As noted previously, the section of Works south of the SCA Pipeline may be designed to suit 60km/h due to the property constraints, and as such, minimum curve radii will differ through this section to suit the adjusted design speed.

If required, superelevation will be used if smaller curve radii are required.

Final minimum curve radii will be determined during the detailed design stage.

3.8 Design Vehicles

Design Parameter	Design Vehicle	Purpose
Design Heavy Vehicle	B-Double	Turning Path
Design Light Vehicle	Car	Stopping Site Distance

Table 1 - Design Vehicles

The choice of design heavy vehicle was influenced by the current high level of heavy vehicle usage of this section of OWR, connecting the various industrial developments with Sydney's nearby motorways.

There is potential for an increase in these heavy vehicle movements within this section of OWR due to the additional regional industrial developments, which would utilise OWR as an access road.

The section of road from CH00 to CH350 which will become part of the future North South Link Road route, will be designed to accommodate b-triples. It is noted this criteria will only apply to the through lanes between the nominated chainages and will not apply to the turning movements at the Milner Avenue and OWR intersection.

Traffic Signal Design

The OWR Upgrade will include the following traffic signal works:

- Installation of new signals at the OWR/ Milner Avenue (Oakdale Central Estate Road) Intersection CH190. The provision of new signals at this intersection is supported by advice provided by Traffix (letters dated 6 June 2014 and dated I August 2014 – attached in Appendix E).
- Minor adjustment of existing signals at the OWR/ EPLR Intersection.
- Installation of conduits to facilitate the potential for future signalisation of intersections of OWR and the access' to SCA and Transgrid respectively (no

3.9



design and./or approval of traffic signal design are proposed to be undertake for these locations).

The design of the new signals and adjustments to existing signals will be subject to RMS approval.

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4 Cross Section

4.1 Road Scape Allocation

Design Parameter	Minimum value adopted in the current design	Maximum value adopted in the current design	Within guideline limits*	Outside guideline limits	Reason for use of values that are outside guideline limits
Left carriageway (northbound)	6.8m	8.0m	Y	Ν	N/A
Right carriageway (southbound)	6.8m	11.5m	Y	Ν	N/A
Median	0.6m	5.0m	Y	N	N/A
Left Verge (western side)	3.75m	4.5m	Y	Ν	N/A
Right Verge (eastern side)	3.5m	4.5m	Y	Ν	N/A

Table 2 - Road Scape Allocation

*refer Ausroads Geometric Design Guidelines Section 3, Table 4.3



4.2 Typical Cross Sections

Please refer to AT&L's Civil Drawings, using the relevant chainages shown below, to locate where these typical sections apply.



Figure 2 - OWR - Typical SectionCH700-CH1600





4.2.1 Lane Widths

The existing single carriageway consists of 2×3.5 m-4.3m wide lanes. This will be upgraded to a dual carriageway, consisting of a 3.5m kerbside lane and a 3.3m median sidelane. In certain sections, lanes increase in width to a maximum of 4.5m to account for heavy vehicle turning requirements.

As part of the change to a dual carriageway, a central painted median will be included to separate the carriageways.

4.2.2 Median Type

The proposed median will vary in width, from a minimum of 0.6m to a maximum of 5.0m.

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At the intersection of Milner Avenue and OWR, and Erskine Park Link road and OWR the median will be of a raised concrete type. The remainder of the median will be a painted median.

4.2.3 Allocation of road space for utilities, pedestrians and bicycles

A sufficiently wide verge has been allowed. Typically, the verge is 3.75m along the western side, and 3.5m along the eastern side of the proposed road upgrade respectively. The verge widens to 4.5m along both sides of the proposed road upgrade through CH200 to CH350, where the OWR intersects with the Oakdale Estate Access Road. It is proposed to provide a 2.5m wide shared path along the western side of OWR for the length of the project.

The verge in all areas is wide enough to include the proposed pedestrian/cycle paths and for the inclusion of all proposed services.

As per the Austroads Design Guidelines, the verge width is referred as a 'Border'. The 'Border' is described in the figure below:



Source: VicRoads (2002b).

Figure 4 – Austroads Design Guidelines - Border Diagram

The wording below is taken from the RMS Supplement to the Austroads design guidelines. The wording describes the desirable verge, or border widths and the reason by which these widths have been selected. With reference to the proposed design, all verge or border widths are above the minimum width criteria.

Urban Border

Paragraph 1

Delete "The urban border usually comprises two parts, a path for pedestrians and the nature strip. The elements of the urban border are shown on Figure 4.37. The main functions of the border are:"

and replace with:

"The urban border usually comprises the area from the face of kerb to the road boundary. Desirably the footway should be at least 3.0m wide and desirably 3.5m wide in order to contain the footpath for pedestrians and space for public utilities. Any residual road reserve should be allocated to the footway to provide additional space for landscaping and driveways. The elements of the urban border are shown on Figure 4.37. If kerbed footways are not provided then sufficient verge width should be available to enable pedestrians to walk clear of the road carriageway, e.g. lanes and shoulders. The main functions of the urban border are:" at start of paragraph.

Figure 5 - RMS Supplement to Austroad Design Guidelines - Border or Verge Widths

4.2.4 Allocation of Road Space for Landscaping

Minimal landscaping works can occur within the verges where no pedestrian/cycle paths are constructed. No formal landscaping, other than the installation of turf, is proposed for the upgrade.

4.2.5 Cut and Fill Batter Slopes

The proposed upgrade of OWR has been designed to generally maintain the existing vertical grade of the road, thus minimal/no alteration to the existing batters is anticipated. Any changes to the final pavement levels which require a batter back to the surrounding existing surface levels, will batter back to the road surface at a nominal 2:1 (H:V) (or 3:1 where possible) slope.

The table below summarises the desirable and maximum batter slopes, as per the Austroad Design Guidelines.

	Cut		Fill	
	Desirable	Maximum	Desirable	Maximum
Earth batter	3:1	2:1	6:1	4:1 (2)
Rock batter	0.5:1	0.25:1 (1)	-	-
Median	10:1	6:1 (2)	10:1	6:1 (2)

Table 4.12: Typical design batter slopes

Figure 6 - Austroad Design Guidelines - Batter Slopes

The wording below is taken from the RMS Supplement to the Austroads design guidelines, and describes how the wording in the above table is modified to suit RMS guidelines. With reference to the proposed design, proposed batter slopes are within RMS guidelines.

Batters

Paragraph 4

Delete "desirable" after "Slopes flatter than the" and before "maximum (Table 4.12) should be used where possible"

Figure 7 - RMS Supplement to Austroads Guidelines - Batter Slopes

4.2.6 Crossfall/Adverse Crossfall

Nominal crossfall along the proposed upgrade of OWR will generally be at 3.0%.

Superelevation lengths with be at 7.0% maximum, which suit the proposed curve radii.

5 Geometric Design

5.1 Horizontal Curves and Alignment

5.1.1 Horizontal Sight Distance

The horizontal alignment will remain similar to existing, retaining the currently acceptable sight distance, with the addition of an extra width adjacent to the current roadway within the central median. Any proposal for planting of the median will need to be assessed for sight distance requirements, particularly on the inside of horizontal curves although the current project scope does not propose planting other than turf.

At present, horizontal sight distance on OWR is not optimal at the crossing of the SCA pipeline. As part of the proposed upgrade of OWR, horizontal sight distance at the SCA Crossing will be improved by the works. Horizontal sight distances will be checked to comply with the RMS Supplement to the Austroad Guidelines, with reference to Section 5.4.

5.1.2 Superelevation Transitions

The majority of the works in relatively straight with no horizontal curves apart from the SCA crossing where minimum radii are used and maximum superelevation is expect to be used.

5.1.3 Lane Widening

No lane widening is required on this section of the works, although this will be determined at the detailed design stage and in accordance with the design guides.

5.2 Vertical Alignment

5.2.1 Vertical Sight Distance/Stopping Distance

Vertical stopping sight distance along the works currently complies with design guidelines, due largely to the flat grades and long straights. Where the vertical alignment has been amended in the current concept design to enable reshaping of the superelevation transition areas, vertical stopping sight distance requirements have been achieved.

As per Austroads Design Guidelines, section 5.3, stopping sight distance is calculated based on the following equation:

 $SSD = \frac{R_T V}{3.6} + \frac{V^2}{254(d+0.01a)}$

- R_{T} = reaction time (sec)
- V = operating speed (km/h)
- d = coefficient of deceleration (longitudinal friction factor)
- a = longitudinal grade (%, + for upgrades and for downgrades).

Figure 8 - Stopping Sight Distance Calculation

It should be noted that the during the detailed design phase, stopping site distance will be checked for compliance with the above calculation to ensure that the minimum required stopping sight distance is achieved throughout the road length. The current design meets the required stopping site distance criteria.

5.3 Utilities

Utility locations were determined using Dial Before You Dig information, ground survey data and underground service potholing. The following is a summary of the existing utility assets and assumed impacts that will occur as a result of the OWR upgrade works.

5.3.1 Gas Mains

An existing Jemena high pressure 150mm diameter steel gas main is located on the eastern side verge of OWR from approximately CH100 – CH380. It is proposed to relocate this main further to the east within the proposed road reserve to accommodate the upgrade of the OWR/ Milner Avenue intersection.

5.3.2 Water Mains

There are two existing Sydney Water mains with the limit of works for the OWR Upgrade:

- 250mm diameter DICL pipe located on the western side verge of OWR between CH00–CH230. Based on the concept design, this main is not impacted by the upgrade works.
- 150mm diameter oPVC pipe located on the eastern side verge of OWR between approximately CH970-CH1600. Based on the concept design it is proposed to relocate this main between approximately CH900-CH1150 to accommodate the widened formation of the Trangsrid Access at CH1000.

5.3.3 Telecommunications

Telecommunications conduits and cables are located along the length of the OWR Upgrade.



The conduits are Telstra assets housing Telstra copper and optic fibre cables, sub-ducts for Optus, Uecomm and Pipe Networks.

Based on the concept design, it is expected that all of the existing conduits listed below will be required to be relocated along the length of the upgrade:

- CH00-CH430 2 x P100 conduits are located on the eastern side verge of OWR.
- CH430-CH600 2 x 1P100 conduits traverses between the eastern side to the western side of the road carriageway.
- CH600-CH1600 1 x P100 CH650-CH850, 2 x P100 CH850-CH1250, 3 x P100 CH1250-CH1450 conduits are located on the western side verge of OWR.

5.3.4 Electrical

Endeavour Energy existing assets are located as follows:

- Bank of eight underground conduits located longitudinally in western side verge CH100-CH1600.
- Bank of X conduits transverse underground road crossings at CH180, Ch200, CH1000, CH1200 and CH1300.
- Overhead electrical supply poles eastern side CH00-CH600, western side CH660-Ch1600.

Based on the concept design it is envisaged the longitudinal underground conduits and overhead poles will be impacted and will be required to be relocated along the length of the project as part of the upgrade works.

5.3.5 Street Lighting

The upgrade includes provision of street lighting from CH00-CH1600 with light standards to be provided on both sides of the road. In accordance with Council standard's the lighting will be designed in accordance with AS1158.1 to a category V3 standard.

It is envisaged that a non standard lighting design may be required adjacent to the existing overhead 132kV and11kV road crossings.

5.4 Relationship and Proximity to Electrical Infrastructure

Both Transgrid and Endeavour require the following clearances to exiting services where possible:

Item	Desirable Clearance	Minimum Clearance
Existing structural Stanchions (Horizontal Clearance)	30m	15m
Overhead 132kV (Vertical Clearance)		9m
Overhead 11kV (Vertical Clearance)		6m

Table 3 - Electrical Horizontal and Vertical Clearances

It should be noted that many of the existing Transgrid structure lattice towers are located with horizontal clearances less than 15m. The boundary within the section of the proposed upgrade to OWR adjacent to the Transgrid infrastructure is currently designed with no change, so that current clearances to the Transgrid infrastructure are maintained, despite the existing non-conformity. Refer to AT&L's for horizontal locality of Transgrid structures and proximity to the proposed road alignment.

With respect to vertical clearances, the vertical alignment of the proposed upgrade is generally the same as the existing OWR alignment. Thus, any existing vertical clearances to cables will be retained and shall stay within permissible heights. As noted in Table 3 above, the minimum vertical clearance to any 132kV electrical is 9m. The figure below, highlights a section of the proposed long section, showing the road surface level, the 9m vertical clearance to overhead electrical, and shows the vertical location of the overhead cables. It should be noted that all overhead electrical cables are above the 9m clearance line.

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Figure 9 - Proposed OWR Upgrade Longsection with 9m Electrical Clearance and Overhead Electrical Cables Shown



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5.5 Site Issues

5.5.1 Geotechnical

No geotechnical investigations have been undertaken at this stage. These works are to be undertaken at detailed design stage. It is expected boreholes and test-pits will be undertaken at regular intervals along the road. The investigation would identify the CBR of the existing subgrade, existing pavement depth and composition, ability to reuse the existing pavement, advice on a proposed pavement design etc.

5.5.2 Pavement Design

A final pavement design for both the semi-rigid and flexible pavement areas for the project is pending, subject to further analysis of the geotechnical data and a final decision on the preferred construction methodology and staging.

The section of Old Wallgrove from CH00 to approximately CH325 will be designed and constructed to the standard to adopted for the future North South Link Road. Accordingly it is envisaged this pavement may be semi-rigid pavement of similar composition to the approved pavement design for the EPLR and will be confirmed within the detailed design process.

The section of OWR from approximately CH325 to the tie in at the EPLR is proposed to be a flexible pavement which may comprise bound and unbound granular base layers. In accordance with Blacktown City Council's Engineering Guide for Development Road Design Parameters for Industrial Collector and heavy Duty roads, the adopted pavement design loading will be 1×10^7 ESA.

Our suggested pavement as below:

- Asphalt wearing course on,
- Granular or bound base on,
- Select Material Zone on,
- Subgrade improvements when required.

Final pavement designs will be prepared in accordance and in consultation with RMS, Council and RMS guidelines/specifications.



5.6 Property Acquisitions and Adjustments

The following property acquisitions have been identified (Refer to the Drawing C360):

Land Owner	Approximate Area of Land to Be Acquired (m2)
Transgrid	1284
SCA	814
Austral Brickworks	4,970

Table 4 - Property Acquisition Areas

Note: These areas are preliminary and are subject to confirmation during the detail design stage pending further development of the vertical grading, resulting cut and fill batter and location and dimensioning of basins. The final extent of acquisition will be subject to agreement with adjoining impacted land owners.

5.7 Tie In

5.7.1 Milner Ave (Oakdale Central Estate Road)

The existing intersection of OWR and Milner Avenue will be upgraded to accommodate the proposed upgrade cross section and proposed turn lanes. The upgrade will include the installation of new signals at the existing intersection. The provision of new signals at this intersection is supported by advice provided by Traffix (letter dated 6 June 2014).

5.7.2 Erskine Park Link Road (EPLR)

The recently completed EPLR made allowance for the future upgrade of OWR. Only minimal works are required to enable the tie-in to the intersection.

5.7.3 SCA Pipeline

It is proposed to provide adequate access to and from OWR at the SCA crossing by the inclusion of an uncontrolled protected dedicated right turn storage lane and raised median.. Through discussions with SCA, they identified their requirements and a provision has been made to satisfy SCA. Further consultation is required to ensure SCA are satisfied.

The design and construction of the intersection is such that, if required in the future, the intersection could be signalised. This would involve the installation of conduits to accommodate cabling for future signalisation.

The future design median width at this intersection proposed within the concept design is 0.6m which will require the installation of mast arms for any future traffic signals.

5.7.4 Transgrid Site Entry

Local widening has been provided at the Transgrid entrance at CH980m to enable provision of an uncontrolled protected dedicated right turn storage lane for traffic entering the site from the north. The design and construction of the intersection is such that, if required in the future, the intersection could be signalised. This would involve the installation of conduit to accommodate cabling for future signalisation.

The future design median width at this intersection proposed within the concept design is 0.6m which will require the installation of mast arms for any future traffic signals.

A second access to Transgrid on the western side of OWR at CH1540 is proposed to an uncontrolled left in/left out access only.

5.8 Stormwater Management

5.8.1 Design Information

The majority of the existing stormwater system will remain operational, with alterations to pit inlet levels and locations to accommodate the proposed finished surface levels or revised median width. New drainage lines will only be constructed where the carriageway pavement is to be shifted above an existing longitudinal drainage line.

Details of existing invert levels and pipe condition will be required prior to the detail design stage. As a means of obtaining this information, detailed survey has been undertaken; this has provided pit invert levels and pipe information.

There is an existing low point immediately to the south of the current limit of works a CH00. Works to upgrade the local drainage system at this location will be incorporated into the OWR Upgrade.

5.8.2 Hydrological Investigation

A hydrological investigation will be undertaken as part of the project, to determine the flooding effects from the works, primarily from upstream Creek catchments. A catchment plan has been prepared for the road upgrade which has been used to assess the existing cross drainage capacity.

5.8.3 Cross Drainage

The existing cross drainage is proposed to be upgraded to cater for the 100 year design storm. No additional stormwater from the upstream catchment east of the proposed OWR will be draining into the existing crossings. Confirmation has been received from Blacktown City Council that stormwater from the existing Coles Myer Distribution centre to the east of Old WallIgrove Road at approximately CH1000 does not drain through the cross drains but discharges to the east into an OSD basin within Roberts Road.

Longitudinal drainage will be directly connected to this cross drainage to minimise additional discharge points to the existing creek system.



Refer to Stormwater Catchment plan SKC04 in Appendix C for details of all catchment areas upstream of the cross drains and proposed pipe sizes of the crossings.

5.8.4 Longitudinal Drainage

Longitudinal (pavement) drainage will be directly connected to this cross drainage to minimise additional discharge points to the existing creek system. Council generally adopts the 1:20yr event criteria, while RMS generally adopts the 1:10yr event criteria.

Both scenarios will be assessed during detailed design and agreement sought with Council/RMS as to the event criteria to be adopted for the upgrade.

In addition, and as required, table drains and cut off drains will be incorporated to manage water flows at the toe of embankments and top of cut batters.

5.9 Water Sensitive Urban Design (WSUD)

5.9.1 Policy and Guidelines

The stormwater design considers the following guidelines:

- Australian Rainfall Quality (2006)
- Department of Environment and Climate Change NSW (DECC), Management Urban Stormwater: Urban Design (Consultation Draft, 2008)
- Blacktown City Council Stormwater Quality Control Policy (2001, reviewed 2009)
- Landcom Water Sensitive Urban Design Policy (2009)



5.9.2 Objectives

These stormwater management objectives were applied to treating stormwater runoff from the development to meet pollution reduction targets outlined in Table 5.

Pollutants	Retention Objectives
Total Suspended Solids (TSS)	85%
Total Phosphorus	65%
Total Nitrogen (TN)	45%
Gross Pollutants	90%
Total Hydrocarbons	90%

Table 5 Pollutant Retention

In order to achieve these reductions, a treatment train approach will be implemented into the development where the stormwater treatment flow path for runoff would generally be:

1. Runoff from the road reserve will be collected via pits and pipes and discharged into a bio-retention swale to be treated to the reduction targets as highlighted in Table 5.

5.9.3 MUSIC Analysis

The software package developed by the CRC for Catchment Hydrology termed "MUSIC" (Model for Urban Stormwater Improvement Conceptualisation) was used to assess the effectiveness of the proposed "treatment train" and therefore ensure compliance with the proposed objectives. Refer to Appendix B for MUSIC model data, results and catchment plan.

Based on the MUSIC analysis a total bio-retention area of 335m² will be required to treat all runoff within the Road Reserve from CH00 to CH1450.

It is proposed to locate the bio-retention swales on the western side of the carriageway to coincide with the existing low points along the corridor between approximately CH400-CH1600.

The road pavement drainage flows will be directed to the bio-swales which will then discharge into the downstream drainage system.

An indicative location for the bio-swales has been shown on the project land acquisition plan attached in Appendix F.


The location and footprint of individual basins will be developed as part of the detailed design.

5.10 Traffic Management, Staging

Generally, it is proposed to construct the works in two separate stages, maintaining the existing carriageway and constructing two of the new lanes and then switching the traffic and constructing the final two lanes. As described within drawings C370 to C376 refer Appendix D, the currently proposed construction staging and traffic management works are as follows:

Stage 1:

- Construct temporary pavement (width varies) adjacent to the existing north bound lane CH275 to CH525.
- Construct temporary pavement (width varies) adjacent to the existing south bound lane from approximately CH675 to CH1525.
- Install temporary concrete barriers from approximately CH40 to CH1550, leaving gaps to maintain access points.
 - Barriers approximately located along the existing edge of the southbound lane between CH40 and CH600.
 - Barriers approximately located along the edge of the northbound lane between CH575 and CH1550.
- Install temporary linemarking along the length of the project to provide two lane traffic (1 lane northbound, 1 lane southbound) plus turning lanes where required:
 - Temporary alignment located approximately along the existing northbound lane and new temporary pavement between CH40 and CH525.
 - Temporary alignment located approximately along the existing southbound lane and new temporary pavement between CH575 and CH550
- · Shift traffic from the existing alignment, to the temporary alignment
- Construct the new roadworks behind the concrete barriers

Stage 2:

- Shift the concrete barriers to their new position, leaving gaps to maintain access points
 - Barriers approximately located along the existing edge of the southbound lane between CH100 and CH200
 - Barriers approximately located along the edge of the existing southbound lane between CH255 and CH600



- Barriers approximately located along the edge of the existing northbound lane/centre of existing pavement between CH575 and CH1600
- Remove temporary linemarking from stage 1 and install new stage 2 temporary linemarking along the length of the project to provide two lane traffic (1 lane northbound, 1 lane southbound) plus turning lanes where required
 - Temporary alignment located approximately along the newly constructed final pavement for the full length of the project as well as along small sections of the existing pavement
- Shift traffic from the temporary stage 1 alignment to the temporary stage 2 alignment
- · Construct the remaining new roadworks behind the concrete barriers
- Remove concrete barriers, remove temporary linemarking and install final linemarking

Access to existing properties will be maintained during construction and any proposed temporary access arrangements will be agreed through consultation with the adjoining property owners.

Confirmation of this general traffic management and construction staging arrangement will be confirmed during the detailed design stage.

Prior to construction, a detailed Traffic Management Plan will be prepared in accordance with the relevant RMS Traffic Management Guidelines.

6 Finalisation

Once DA approval is granted, the following is required:

- Constructability Review.
- Road Safety Audit.
- Detailed Design including:
 - o Civil Design.
 - o Stormwater Design.
 - o Geotechnical Investigation.
 - o Pavement Design.
 - o Electrical Design.
 - o Water Relocation design.
- Detailed Cost Estimation.
- Design reviews.
- Submission to RMS and Council for approval.

7 Conclusion

The design to date has been prepared for inclusion in the development application giving due consideration to the existing stake holders, physical features on site, design constraints and relevant design guidelines.

It is concluded the design could be further advanced through to a Detailed Design/Construction documentation level, as further design will ensure with certainty that there will be no major unknown constraints.

Once complete, the road will operate at the intended design speed, safely and efficiently as a regional road.

The design is generally in accordance with the relevant RMS and Austroad Design Guidelines. Upon approval, detailed design shall be completed to comply with the relevant standards and to the satisfaction of RMS, as well as any conditions of the approval.

Currently, OWR acts as a link road between the local Council controlled roads and other regional/state roads controlled by RMS. Future developments within the area will further utilise OWR as a link road, providing access to additional local roads and other regional/state roads within the area. Thus, it is AT&L's considered opinion that the section of OWR described herein, should be classified as an Interim Regional Road, and therefore be controlled by Fairfield City Council and Blacktown City Council respectively.

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Appendices

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Appendix A – GHD OWR Upgrade Drawings (Works Completed)

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Appendix B – MUSIC Model and Results























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Goodman Property Services Pty Ltd Level 17 60 Castlereagh Street Sydney NSW 2000

Attention: Will Dwyer

Re: Oakdale Central SSD - Response to DoP

,IliW זאפר Dear

We refer to the subject development and note that the Department of Planning has queries the status of the form of control at the intersection of the Estate Road with Old Wallgrove Road. As you are aware, this was not addressed in the original traffic assessment report as it was acknowledged at that time that the area was subject to ongoing strategic review and assessment.

Nevertheless, it is noted that Buildings 1, 2 and 3 alone are predicted to generate some 430 veh/hr and this traffic will traverse this intersection. This volume is well above the RMS 'warrant' volume of 200 veh/hr for the provision of traffic signals. The future connection of a fourth approach to serve the Austral site is a further complication, which will introduce additional furn movements and conflicts.

Hence, we expect that traffic signal control will be a mandatory requirement at this intersection in the reasonably near future and certainly prior to the occupancy of all these three buildings. In this context, the signal design prepared by AT&L (which is based on a previous layout prepared by GHD) is considered acceptable in principle. Subject to detailed assessment, it will provide satisfactory operation in the short and medium terms.

We trust that this responds to the issue raised by the DoP and request that you contact the undersigned should you have any questions or would like to discuss this matter further.

Yours faithfully

Graham Pindar Director

traffic impact studies | expert witness | local govt. liaison | traffic calming | development advice | parking studies pedestrian studies | traffic control plans | traffic management studies | intersection design | transport studies

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traffic & transport planners

Reference: 13.282101v1

1 August 2014

AT&L Suite 702, 154 Pacific Highway St Leonards NSW 2065

Attention: Mr Anthony McLandsborough

Re: Oakdale Central, Old Wallgrove Road

Dear Anthony,

As requested, as part of the planning for the upgrade of Old Wallgrove Road in conjunction with the delivery of the Oakdale Central precinct, we have investigated the following issues:

- The need for a dedicated right turn pocket from Old Wallgrove Road into the existing Transgrid site;
- The need for a second right turn lane from Old Wallgrove Road into Erskine Park Link Road; and
- The need for the signalisation of the Old Wallgrove Road / Millner Avenue Intersection.

The results of these investigations are outlined following.

Sight Turn Pocket into Transgrid Site

It is understood that Old Wallgrove Road is to be upgraded in accordance with the "Rationalised Ultimate" configuration as part of the delivery of the Oakdale Central. This configuration will comprise a 4-lane cross-section with 3.3m – 3.5m through lanes and a 600mm wide painted central median.

We have investigated the need for the provision of a dedicated right turn pocket from Old Wallgrove Road into the Transgrid site, which is located approximately 500m to the north of the Oakdale Central precinct, and is currently accessed from Old Wallgrove Road via a driveway crossover.

Traffic surveys were undertaken at the access to the Transgrid site to record existing volumes entering and exiting the site, as well as through traffic on Old Wallgrove Road. The results of these surveys are included as **Attachment A**, and demonstrate reasonable volumes of traffic entering and exiting the site, as summarised following:

- AM Peak: 87 arrivals and 11 departures; and
- PM Peak: 11 arrivals and 102 departures.

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An assessment of the need for a right turn pocket into the Transgrid site has been undertaken, using the turn warrants outlined in Austroads Guide to Road Design Part 4A: Unsignalised and Signalised Intersections.

The results of this assessment are outlined in the table and graph below, and demonstrate that the current turning volumes into the Transgrid site combined with the through volumes on Old Wallgrove Road suggest that a short channelised right turn treatment (CHR(S)) into Transgrid is currently warranted.

Furthermore, the development of substantial land parcels to the south of the site (including the Austral Bricks site and the CSR Bricks site) will only serve to increase the through traffic volumes on Old Wallgrove Road.

In light of the above, it is recommended that a dedicated right turn pocket from Old Wallgrove Road into the Transgrid site be constructed as part of the upgrade of Old Wallgrove Road.

Table 1: Recorded Traffic Volumes for Turn Warrants Assessment, Transgrid Access

83	511/2* + 90 + 4 = 203	M Peak Hour
83	511/2* + 90 + 4 = 203	M Peak Hour

* assumes a 4-lane major road cross-section, i.e. based upon the "Rationalised Ultimate" configuration of Old Wallgrove Rd



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Second Right Turn Lane from Old Wallgrove Road into Erskine Park Link Road

The Erskine Park Link Road / Old Wallgrove Road intersection was constructed in mid-2013 as a signalised T-intersection, as part of the delivery of the Erskine Park Link Road.

Various intersection configurations were investigated by GHD as discussed in the report "Old Wallgrove Road Extension – Traffic and Transport Analysis, Summary of Modelling Findings, 18 July 2013." The results indicate that this intersection was expected to operate acceptably as a T-intersection with a single right turn from Old Wallgrove Road into Erskine Park Link Road at 2031, at a Level of Service C (although the modelled queue for this movement was about 230m).

It is understood however that this intersection is to be upgraded to a 4-way signalised intersection, with a fourth (northern leg) to be constructed to provide access to the Jacfin land parcel to the north.

Accordingly, this intersection has been analysed as a 4-way signalised intersection, with the modelled geometry and phasing arrangement as shown below.



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The modeled intersection volumes reflect those in the GHD report "Old Wallgrove Road Extension – Traffic and Transport Analysis, Summary of Modelling Findings, 18 July 2013" for the 2021 PM peak design horizon, with a nominal 50vph assumed for each movement into and out of the fourth (northern) intersection leg.

The results of these analyses indicate even with low volumes of traffic accessing the Jacfin land parcel to the north of the intersection, the intersection is expected to fail prior to 2021, with the fourth intersection leg. The table below provides the model results, which indicate a Level of Service F for the intersection, and queues on Old Wallgrove Road of approximately 500m.

Table 2: Modelled Intersection Performance, 2021 PM Peak Single Right Turn Lane from Old Wallgrove Road

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23.0	1.23	00.1	263.4	33.6	J SOJ	5.86	996.0	14.0	902	١٦	11
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Signals - Fixed Time Cycle Time = 150 seconds (Practical Cycle Time)

Given the results of the analyses above, the intersection was modelled with a second right turn lane from Old Wallgrove Road into Erskine Park Link Road. The results (shown in the table below) indicate substantially better performance, with a Level of Service C and 95th percentile queues on for critical movements in the order of 150m.



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Table 3: Modelled Intersection Performance, 2021 PM Peak Dual Right Turn from Old Wallgrove Road

Signals - Fixed Time Cycle Time = 100 seconds (Practical Cycle Time)

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7.15	26.0	66.0	152.5	191	a son	23.2	798.0	14.0	213	28	5
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6.13	9.05	65.0	6.65	1.2	A SOJ	٢.8	926.0	14.0	442		t
36.7	10.01	66'0	125.2	0.91	D SOT	4.14	292.0	14.0	653	11	9
38.2	67.0	49.0	1.21	7.1	D SOT	33.5	892.0	0.0	09	52	g
8.04	08.0	67.0	125.2	0.91	E SOL	2.82	292.0	13.4	1142		Appro
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2.95	88.0	98.0	125.5	19.4	D SOT	1.85	\$98.0	15.5	5813	picles	9V IIF

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Whilst a number of assumptions were made necessarily in these analyses (regarding broader road network modifications and the level of development in the area), and alternative signal phasing arrangements which may influence the performance of the intersection are feasible, it would appear that the introduction of a fourth (northern) intersection approach at the Old Wallgrove Road / Erskine Park Link Road intersection would be likely to trigger the need for a second right turn lane from Old Wallgrove Road in the short to medium term, even with relatively low traffic volumes from Old Wallgrove Road in the short to medium term, even with relatively low traffic volumes from Old Wallgrove Road in the short to medium term, even with relatively low traffic volumes from Old Wallgrove Road in the short to medium term, even with relatively low traffic volumes from Old Wallgrove Road in the short to medium term, even with relatively low traffic volumes from Old Wallgrove Road in the short to medium term, even with relatively low traffic volumes from Old Wallgrove Road in the short to medium term, even with relatively low traffic volumes from Old Wallgrove Road in the short to medium term, even with relatively low traffic volumes from Old Wallgrove Road in the short to medium term, even with relatively low traffic volumes from Old Wallgrove Road in the short to medium term, even with relatively low traffic volumes from Old Wallgrove Road in the short to medium term, even with relatively low traffic volumes from Old Wallgrove Road in the short to medium term, even with relatively low traffic volumes in the short to medium term, even with relatively low traffic volumes from Old Wallgrove Road in the short to medium term, even with relatively low traffic volumes in the short to the short to medium term, even with relatively low traffic volumes in the short to the short to medium term.

Need for the signalisation of the Old Wallgrove Road / Millner Avenue Intersection

The Old Wallgrove Road / Millner Avenue Intersection currently operates as a priority-controlled Tintersection, however as part of the upgrade of Old Wallgrove Road, a fourth (eastern) intersection approach is to be constructed, which will provide access to the Austral site. The two existing access driveways to the Austral site are to be closed, with all access to this site to be via the 4-way intersection.

Traffic surveys of the Old Wallgrove Road / Millner Avenue Intersection and the two access driveways to the Austral site have been undertaken, with the results provided in Attachment B.

Intersection analyses have been undertaken of the Old Wallgrove Road / Millner Avenue Intersection as a 4-way intersection (assumed geometry shown below), with all traffic which currently accesses the Austral site via the driveways, instead doing so via this intersection.





The results of these analyses indicate that during the critical PM peak period, the intersection is expected to operate acceptably with existing traffic volumes on Old Wallgrove Road and turning into and out of the Austral site, with the critical movement operating at Level of Service B.

However an increase in traffic volumes on Old Wallgrove Road and into and out of the Austral site would trigger the need for the signalisation of this intersection. Sensitivity analyses have been undertaken, with a summary of the results provided following:

Level of Service (Critical Movement)	- sesecsas - seeses Assumeta Traffic Assesses	Old Wallgrove Road – Assumed Traffic Volume Increase	วัตยาละเอ
Level of Service B	AN	AN	səmuloV gnitsix∃
Level of Service C	+100vph (entering from north) +100vph (exiting to north)	(punoqu]nos) \dv001+ (bnodd]non) \dv001+	Sensitivity Test 1
Level of Service D	+120vph (entering from north) +120vph (exiting to north)	(bnuodrinon) dqv021+ (bnuodrinos) fqv021+	S teaT vitivitieneS
Level of Service F	+150vph (entering from north) +150vph (exiting to north)	(bnuodniuos) dqv02f+ (bnuodninon) dqv02f+	Sensitivity Test 3

Table 4: Summary of Results of Sensitivity Analyses, Old Wallgrove Road / Millner Avenue Intersection

These results indicate that with just partial development of the approximately 75 ha land parcels to the south (the CSR site) and the east of the intersection (the Austral site), the intersection of Old Wallgrove Road / Millner Avenue will require signalisation.

Based upon the traffic generation rate of 10.5 trips per hectare assumed by GHD as part of previous studies, these traffic volumes equate to approximately the following level of development:

- trampione for a for the state of development •
- I20vph in and out: 23 ha of development
- 150vph in and out: 29 ha of development

In light of the results of the sensitivity analyses undertaken, it is recommended that the intersection of Old Wallgrove Road / Millner Avenue be signalised as part of the upgrade of Old Wallgrove Road.

Summary of Findings and Recommendations

In summary, based upon the results of our investigations and the assumptions outlined above, it is recommended that:

- a dedicated right turn pocket from Old Wallgrove Road;
 constructed as part of the upgrade of Old Wallgrove Road;
- a second right turn lane from Old Wallgrove Road to Erskine Park Link Road be provided when the fourth (northern) approach is constructed; and



 the intersection of Old Wallgrove Road / Millner Avenue be signalised as part of the upgrade of Old Wallgrove Road.

Please contact the undersigned should you have any queries or require any further information regarding the above.

Yours faithfully,

xiffsrf

Anne Coutts Senior Engineer



Reference: 13.282I01v2

traffic & transport planners

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1 August 2014

AT&L Suite 702, 154 Pacific Highway St Leonards NSW 2065

Attention: Mr Anthony McLandsborough

Re: Oakdale Central, Old Wallgrove Road

Dear Anthony,

As requested, as part of the planning for the upgrade of Old Wallgrove Road in conjunction with the delivery of the Oakdale Central precinct, we have investigated the following issues:

- 1. The need for a dedicated right turn pocket from Old Wallgrove Road into the existing Transgrid site;
- 2. The need for a second right turn lane from Old Wallgrove Road into Erskine Park Link Road; and
- 3. The need for the signalisation of the Old Wallgrove Road / Millner Avenue Intersection.

The results of these investigations are outlined following.

Right Turn Pocket into Transgrid Site

It is understood that Old Wallgrove Road is to be upgraded in accordance with the "Rationalised Ultimate" configuration as part of the delivery of the Oakdale Central. This configuration will comprise a 4-lane cross-section with 3.3m – 3.5m through lanes and a 600mm wide painted central median.

We have investigated the need for the provision of a dedicated right turn pocket from Old Wallgrove Road into the Transgrid site, which is located approximately 500m to the north of the Oakdale Central precinct, and is currently accessed from Old Wallgrove Road via a driveway crossover.

Traffic surveys were undertaken at the access to the Transgrid site to record existing volumes entering and exiting the site, as well as through traffic on Old Wallgrove Road. The results of these surveys are included as **Attachment A**, and demonstrate reasonable volumes of traffic entering and exiting the site, as summarised following:

- AM Peak: 87 arrivals and 11 departures; and
- PM Peak: 11 arrivals and 102 departures.

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An assessment of the need for a right turn pocket into the Transgrid site has been undertaken, using the turn warrants outlined in Austroads Guide to Road Design Part 4A: Unsignalised and Signalised Intersections.

The results of this assessment are outlined in the table and graph below, and demonstrate that the current turning volumes into the Transgrid site combined with the through volumes on Old Wallgrove Road suggest that a short channelised right turn treatment (CHR(S)) into Transgrid is currently warranted.

Furthermore, the development of substantial land parcels to the south of the site (including the Austral Bricks site and the CSR Bricks site) will only serve to increase the through traffic volumes on Old Wallgrove Road.

In light of the above, it is recommended that a dedicated right turn pocket from Old Wallgrove Road into the Transgrid site be constructed as part of the upgrade of Old Wallgrove Road.

	Major Road Traffic Volume (Q_M)	Turn Volume (Q _R)
AM Peak Hour	217/2* + 90 + 4 = 203	83
PM Peak Hour	83/2* + 184 + 0 = 226	11

Table 1: Recorded Traffic Volumes for Turn Warrants Assessment, Transgrid Access

* assumes a 4-lane major road cross-section, i.e. based upon the "Rationalised Ultimate" configuration of Old Wallgrove Rd



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Second Right Turn Lane from Old Wallgrove Road into Erskine Park Link Road

The Erskine Park Link Road / Old Wallgrove Road intersection was constructed in mid-2013 as a signalised T-intersection, as part of the delivery of the Erskine Park Link Road.

Various intersection configurations were investigated by GHD as discussed in the report "Old Wallgrove Road Extension – Traffic and Transport Analysis, Summary of Modelling Findings, 18 July 2013." The results indicate that this intersection was expected to operate acceptably as a T-intersection with a single right turn from Old Wallgrove Road into Erskine Park Link Road at 2031, at a Level of Service C (although the modelled queue for this movement was about 230m).

It is understood however that this intersection is to be upgraded to a 4-way signalised intersection, with a fourth (northern leg) to be constructed to provide access to the Jacfin land parcel to the north.

Accordingly, this intersection has been analysed as a 4-way signalised intersection, with the modelled geometry and phasing arrangement as shown below.



Figure 1: Erskine Park Link Road / Old Wallgrove Road Intersection (Modelled Geometry, 4-way intersection)



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The modeled intersection volumes reflect those in the GHD report "Old Wallgrove Road Extension – Traffic and Transport Analysis, Summary of Modelling Findings, 18 July 2013" for the 2021 PM peak design horizon, with a nominal 50vph assumed for each movement into and out of the fourth (northern) intersection leg.

The results of these analyses indicate even with low volumes of traffic accessing the Jacfin land parcel to the north of the intersection, the intersection is expected to fail prior to 2021, with the fourth intersection leg. The table below provides the model results, which indicate a Level of Service F for the intersection, and queues on Old Wallgrove Road of approximately 500m.

Single Right Turn Lane from Old Wallgrove Road

Mov ID	ODMo	Demand	Flows	Deg. Satn	Average	Level of	95% Back	of Queue	Prop.	Effective	Average
	V	Total	HV		Delay	Service	Vehicles	Distance	Queued	Stop Rate	Speed
		veh/h	%	v/c	sec		veh	m		per veh	km/h
South:	Old Wallgr	ove Road									
1	L2	50	14.0	0.092	17.5	LOS B	1.5	11.5	0.44	0.65	45.9
2	T1	50	0.0	0.966	86.8	LOS F	63.7	495.0	0.97	1.08	24.0
3	R2	612	14.0	0.966	92.6	LOS F	63.7	495.0	0.97	1.08	23.7
Approa	ich	712	13.0	0.966	86.9	LOS F	63.7	495.0	0.93	1.05	24.5
East: E	rskine Par	k Link Roa	d								
4	L2	442	14.0	0.358	7.7	LOS A	5.8	45.4	0.25	0.62	52.2
5	T1	653	14.0	0.903	78.5	LOS F	27.8	217.9	1.00	1.08	26.2
6	R2	50	0.0	0.393	55.6	LOS D	2.9	20.2	1.00	0.74	31.0
Approa	ch	1145	13.4	0.903	50.2	LOS D	27.8	217.9	0.71	0.89	32.8
North: /	Access to .	Jacfin Site									
7	L2	50	0.0	0.222	39.1	LOS C	2.5	17.8	0.72	0.72	36.3
8	T1	50	0.0	0.183	61.6	LOS E	3.2	22.7	0.92	0.70	29.9
9	R2	50	0.0	0.192	67.4	LOS E	3.3	22.8	0.92	0.74	28.3
Approa	ch	150	0.0	0.222	56.0	LOS D	3.3	22.8	0.85	0.72	31.2
West: E	Erskine Par	k Link Roa	d								
10	L2	50	0.0	0.048	13.1	LOS A	1.1	7.8	0.37	0.64	48.8
11	T1	706	14.0	0.956	98.2	LOS F	33.6	263.4	1.00	1.23	23.0
12	R2	50	14.0	0.414	56.0	LOS D	2.9	22.9	1.00	0.74	30.6
Approa	ch	806	13.1	0.956	90.3	LOS F	33.6	263.4	0.96	1.16	24.2
All Veh	icles	2813	12.5	0.966	71.3	LOS F	63.7	495.0	0.84	1.00	27.5

Signals - Fixed Time Cycle Time = 150 seconds (Practical Cycle Time)

Given the results of the analyses above, the intersection was modelled with a second right turn lane from Old Wallgrove Road into Erskine Park Link Road. The results (shown in the table below) indicate substantially better performance, with a Level of Service C and 95th percentile queues on for critical movements in the order of 150m.





Figure 2: Erskine Park Link Road / Old Wallgrove Road Intersection (Modelled Geometry, 4-way intersection - <u>Dual Right Turn from Old Wallgrove Road</u>)

Table 3: Modelled Intersection Performance, 2021 PM Peak Dual Right Turn from Old Wallgrove Road

Signals - Fixed Time Cycle Time = 100 seconds (Practical Cycle Time)

Mov ID	ODMo	Demand	Flows	Deg. Satn	Average	Level of	95% Back	of Queue	Prop.	Effective	Average
	V	Total	HV		Delay	Service	Vehicles	Distance	Queued	Stop Rate	Speed
		veh/h	%	v/c	sec		veh	m		per veh	km/h
South:	Old Wallgr	ove Road							C. AND SA		a transformer
1	L2	50	14.0	0.113	17.0	LOS B	1.2	9.1	0.54	0.67	46.1
2	T1	50	0.0	0.854	47.2	LOS D	15.8	121.6	0.97	0.98	32.5
3	R2	612	14.0	0.854	53.2	LOS D	19.4	152.5	0.99	0.97	31.7
Approa	ch	712	13.0	0.854	50.3	LOS D	19.4	152.5	0.95	0.95	32.5
East: E	rskine Par	k Link Road	d								
4	L2	442	14.0	0.376	8.1	LOS A	5.1	39.9	0.33	0.65	51.9
5	T1	653	14.0	0.767	41.4	LOS C	16.0	125.2	0.99	0.91	35.7
6	R2	50	0.0	0.268	33.5	LOS C	1.7	12.1	0.94	0.73	38.2
Approa	ch	1145	13.4	0.767	28.2	LOS B	16.0	125.2	0.73	0.80	40.8
North: A	Access to .	Jacfin Site									
7	L2	50	0.0	0.106	21.7	LOS B	1.4	9.9	0.62	0.68	43.8
8	T1	50	0.0	0.122	34.7	LOS C	2.0	13.9	0.85	0.64	38.3
9	R2	50	0.0	0.128	40.4	LOS C	2.0	14.0	0.85	0.73	35.7
Approa	ch	150	0.0	0.128	32.2	LOS C	2.0	14.0	0.77	0.68	39.0
West: E	rskine Par	rk Link Roa	id								
10	L2	50	0.0	0.058	16.1	LOS B	1.1	7.6	0.53	0.67	46.9
11	T1	706	14.0	0.823	44.9	LOS D	18.2	142.4	1.00	0.98	34.5
12	R2	50	14.0	0.275	33.6	LOS C	1.7	13.7	0.93	0.73	37.9
Approa	ch	806	13.1	0.823	42.4	LOS C	18.2	142.4	0.97	0.94	35.3
All Vehi	cles	2813	12.5	0.854	. 38.1	LOSC	19.4	152.5	0.86	0.88	36.7

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Whilst a number of assumptions were made necessarily in these analyses (regarding broader road network modifications and the level of development in the area), and alternative signal phasing arrangements which may influence the performance of the intersection are feasible, it would appear that the introduction of a fourth (northern) intersection approach at the Old Wallgrove Road / Erskine Park Link Road intersection would be likely to trigger the need for a second right turn lane from Old Wallgrove Road in the short to medium term, even with relatively low traffic volumes turning into and out of this northern leg.

Need for the signalisation of the Old Wallgrove Road / Millner Avenue Intersection

The Old Wallgrove Road / Millner Avenue Intersection currently operates as a priority-controlled Tintersection, however as part of the upgrade of Old Wallgrove Road, a fourth (eastern) intersection approach is to be constructed, which will provide access to the Austral site. The two existing access driveways to the Austral site are to be closed, with all access to this site to be via the 4-way intersection.

Traffic surveys of the Old Wallgrove Road / Millner Avenue Intersection and the two access driveways to the Austral site have been undertaken, with the results provided in **Attachment B**.

Intersection analyses have been undertaken of the Old Wallgrove Road / Millner Avenue Intersection as a 4-way intersection (assumed geometry shown below), with all traffic which currently accesses the Austral site via the driveways, instead doing so via this intersection.





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The results of these analyses indicate that during the critical PM peak period, the intersection is expected to operate acceptably with existing traffic volumes on Old Wallgrove Road and turning into and out of the Austral site, with the critical movement operating at Level of Service B.

However an increase in traffic volumes on Old Wallgrove Road and into and out of the Austral site would trigger the need for the signalisation of this intersection. Sensitivity analyses have been undertaken, with a summary of the results provided following:

Scenario	Old Wallgrove Road – Assumed Traffic Volume Increase	Austral Access - Assumed Traffic Volume Increase	Level of Service (Critical Movement)
Existing Volumes	NA	NA	Level of Service B
Sensitivity Test 1	+100vph (northbound) +100vph (southbound)	+100vph (entering from north) +100vph (exiting to north)	Level of Service C
Sensitivity Test 2	+120vph (northbound) +120vph (southbound)	+120vph (entering from north) +120vph (exiting to north)	Level of Service D
Sensitivity Test 3	+150vph (northbound) +150vph (southbound)	+150vph (entering from north) +150vph (exiting to north)	Level of Service F

Table 4: Summary of Results of Sensitivity Analyses, Old Wallgrove Road / Millner Avenue Intersection

These results indicate that with just partial development of the approximately 75 ha land parcels to the south (the CSR site) and the east of the intersection (the Austral site), and relatively modest resulting increases in traffic movement volumes on certain movements, the intersection of Old Wallgrove Road / Millner Avenue will require signalisation.

Based upon the peak hour traffic generation rate of 10.5 trips per hectare assumed by GHD as part of previous studies, these traffic volumes equate to approximately the following level of development:

- 100vph in and 100vph out: 19 ha of development
- 120vph in and 120vph out: 23 ha of development
- 150vph in and 150vph out: 29 ha of development

In light of the results of the sensitivity analyses undertaken, and to minimise redundant works and disruption to operations during future signalisation, it is recommended that the intersection of Old Wallgrove Road / Millner Avenue be signalised as part of the upgrade of Old Wallgrove Road.

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Summary of Findings and Recommendations

In summary, based upon the results of our investigations and the assumptions outlined above, it is recommended that:

- a dedicated right turn pocket from Old Wallgrove Road into the Transgrid site be constructed as part of the upgrade of Old Wallgrove Road;
- a second right turn lane from Old Wallgrove Road to Erskine Park Link Road be provided when the fourth (northern) approach is constructed; and
- the intersection of Old Wallgrove Road / Millner Avenue be signalised as part of the upgrade of Old Wallgrove Road.

Please contact the undersigned should you have any queries or require any further information regarding the above.

Yours faithfully,

traffix

Anne Coutts Senior Engineer

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Attachment A

traffic impact studies | expert witness | local govt. liaison | traffic calming | development advice | parking studies pedestrian studies | traffic control plans | traffic management studies | intersection design | transport studies

9





Attachment B

traffic impact studies | expert witness | local govt. liaison | traffic calming | development advice | parking studies pedestrian studies | traffic control plans | traffic management studies | intersection design | transport studies

10









Suite 702 154 Pacific Highway St Leonards NSW 2065 P 02 9439 1777 F 02 9460 8413 E info@atl.net.au ABN 96 130 882 405

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5th August 2014

Roads and Maritim	e Services	Your Ref:	
Level 9		Our Ref:	L001-RMS-05-08-14.docx
27-31 Argyle Street			
Parramatta NSW 215	0	Direct phone:	0433 973 423
Attention	Colin Langford		

VIA EMAIL: Colin.LANGFORD@rms.nsw.gov.au

Dear Colin

RE: PROPOSED UPGRADE OF OLD WALLGROVE ROAD, BETWEEN MILLNER AVENUE AND ERKSINE PARK LINK ROAD

In response to your request, we have provided the following summary of the design review process that has been undertaken with the RMS over the past 4 weeks to determine the most appropriate and cost effective cross sectional design for the upgrade of the above mentioned roadway.

The Project;

The proposed upgrade to Old Wallgrove Road (OWR) forms part of the State Significant Development Application (SSDA) that was lodged with the Department of Planning (DoP) in late 2013 by Goodman Property (Aust) Pty Ltd. The SSDA seeks approval for the construction of three large warehouse facilities along with the upgrade of OWR.

The existing OWR carriageway is in poor condition and requires a significant upgrade to cater for existing traffic and the future growth within the area. The proposed four (4) lane upgrade is from the recently constructed Erskine Park Link Road to the north stretching 1.65km south to Millner Avenue. In general terms the following works are proposed:

- Property acquisitions and adjustment;
- Utility services relocations;
- Demolition of existing pavements and structures;
- Stormwater infrastructure works cross drainage and pavement drainage;
- Pavements and kerb and gutter;
- Street lighting;
- Intersection works including new traffic signals; and
- Landscaping.

It is proposed for the upgrades works to be funded by State Infrastructure Contributions (SIC).

Purpose of Review;

The initial scope of works has received in principle approval from both Blacktown & Fairfield Council for the full 4 lane upgrade (**Original Green Ultimate**) as part of the SSDA consultation process and Goodman has been in negotiations with the Department of Planning to enter into a Voluntary Planning Agreement to deliver the proposed upgrade as 'Works in Kind' with the SIC contributions payable from the Oakdale Central and Oakdale South estates.

In June 2014, Transport NSW (TfNSW) provided in principle support for the application of SIC contributions to two lanes of the proposed upgrade (stage 1) with the remainder to be constructed at a later point in time following an agreed traffic 'trigger' event (stage 2). They also requested that the RMS conduct a design review of the proposed upgrade to determine the most cost effective design.

Civil Engineers & Project Managers



RMS Meetings and Outcomes;

On the 26 June 2014 a meeting was held with Roads and Maritime Services (RMS) and the Goodman Development team to discuss the proposed upgrade options. AT&L provided a briefing to the RMS on the proposed upgrade and the extent of works to be undertaken. At the meeting AT&L provided a set of drawings for RMS to review and a subsequent email containing all of the relevant drawings that had been prepared to date. **See attachment 1**

On the *11 July 2014* a subsequent meeting was held to discuss the review that RMS had undertaken of the above submission. The focus of the meeting was firstly for RMS to provide an update on the review with discussion centering on constructing the road in two stages, Stage 1 a single lane in each direction and Stage 2, widening to accommodate 2 lanes in each direction, this is known the **Interim Option**. A number of design constraints were discussed with the RMS Design section and with that, it was agreed to prepare a new concept design layout and cross section showing the upgrade being built in the two stages to a minimum stage 1 scope that was acceptable to the RMS. In addition to the two stages, we also agreed to look at a **Rationalised Ultimate** 4 lane option based on the RMS advised cross section. AT&L agreed to obtain a full strategic cost estimate be prepared for all options.

Following the meeting, AT&L issued an email on the *13 July 2014* summarising the outcome of the meeting and the proposed cross sectioned to be adopted for the purpose of providing a revised cost estimates. **See attachment 2**. Subsequent to that email, RMS made recommendations to optimise the scope of the project by reducing the carriageway cross section geometry for both the Interim and Rationalised Ultimate Options respectively.

On the 20th July 2014, AT&L issued via email (See attachment 3) to the RMS the revised concept design for both the Interim Option and the Rationalised Ultimate option along with cost estimates for those options. Included within the cost estimate was the estimate for the SSDA submission (Original Green Ultimate). The cost estimates were prepared by Raven North, a quantity surveying company pre-qualified on the RMS estimating panel who prepared cost estimates for the EPLR Upgrade project for RMS' consultant team.

In summary the estimates were as follows;

1.	Original Green Ultimate option Inc. Contingency	\$24,275,973
2.	Rationalized Ultimate option Inc. Contingency	\$23,417,733
3.	Interim Stage 1 Inc. Contingency	\$20,374,851
4.	Interim Stage 2 Inc. Contingency	<u>\$4,128,993</u>
	Total (3 + 4) combined Interim works	\$24,503,844 (extra over of \$1,086,111 to item 2 or
		extra over of \$227,871 to item 1)

As illustrated above, the expected cost premium for delivering the road in two stages is \$1,086,111 with 85% of the costs being incurred in the initial stage of works. This excludes any cost escalation associated with deferring the commencement of the stage 2 works. On the other hand, the rationalised ultimate option is expected to result in a reduction of the total cost of \$858,240 from that originally proposed.

On the 30th July 2014 a further meeting was held with RMS to discuss the Interim and Rationalised Ultimate options along with the findings of the respective cost estimates made in the 20th July submission. RMS provided a brief summary of their review and then indicated they would be supporting the construction of the Rationalised Ultimate option and as such, would be providing a recommendation to TfNSW on this basis.

Traffic Modelling;

As part of the ongoing discussion with the DoP, additional traffic modelling has been completed for OWR to assess the need for the following three items:

- Dedicated right turn lane at the Transgrid access;
- Potential duel right turn travelling northbound into the Erskine Park Link Road;
- Proposed traffic signals at the intersection of OWR and Millner Avenue.

The findings of the draft report have indicated that the above intersection treatments are warranted although the proposed duel right turn east into the EPLR requires further discussion with RMS, which is proposed to occur during the detailed design phase. The final report will be issued to the DoP as addendum to the SSDA submission. (See attachment 4)



Program;

A significant amount of work is required over the next 12 months to enable the road to be completed by 1st August 2015 including design, utility services Authority approvals, Section 138 Approvals from both Blacktown City Council and Fairfield City Council, RMS approval for the signal works (delivered via an RMS WAD) and physical construction works.

The project target dates for the upcoming 6 months are illustrated below along with a more detailed program in attachment 5.

Task Name	Finish
Prepare 50% detailed design	22/08/14
Prepare 100% detailed design	19/09/14
Obtain for Council Section 138 Approval	17/10/14
Prepare Utility Design	19/09/14
Utility Design Approval	31/10/14
Prepare Tender Documentation	19/09/14
Issue RFT & Tender Close	10/10/14
Commence Construction	01/11/14

Design Documentation and Approval;

We understand the approval process as follows;

- RMS
- RMS .
- Blacktown City Council
- Fairfield City Council .
 - Sydney Catchment Authority
- Section 138 Approval

WAD for Signal works

Section 138 Approval

80% design submission for review only

Transgrid

No approval required although information submission will be made No approval required although information submission will be made

We trust this has sufficiently outlined the process to date and also captures the process going forward. Should you have any questions, please don't hesitate to contact the undersigned.

Yours sincerely

Anthony McLandsborough Director

Attachments;

CC.

1	Email dated 27 June 2014
2	Email dated 13 July 2014
3	Email dated 20 July 2014
4	Traffix draft report
5	Draft program
6	Original SSDA drawings
DoP	Bruce Coleman
DoP	Pascal Van De Walle
DoP	Aaron Nangle
RMS	Matty Mathivanar
RMS	Ruhul Chowdhury
RMS	Pahee Rathan
RMS	Gordon Trotter
RMS	Ahmad Mangal
Goodman	Will Dwyer
Goodman	Richard Seddon
Goodman	Kym Dracopoulos

bruce.colman@planning.nsw.gov.au Pascal.VanDeWalle@planning.nsw.gov.au Aaron.Nangle@planning.nsw.gov.au Matty.MATHIVANAR@rms.nsw.gov.au Ruhul.CHOWDHURY@rms.nsw.gov.au Pahee.RATHAN@rms.nsw.gov.au Gordon.Trotter@rms.nsw.gov.au Ahmad.MANGAL@rms.nsw.gov.au Will.Dwyer@goodman.com Richard.Seddon@goodman.com Kym.Dracopoulos@goodman.com

Civil Engineers & Project Managers

at&l

Attachment 1 Email dated 27th June 2014

Civil Engineers & Project Managers

From:	Anthony McLandsborough
То:	"SAMY Shibree"
Cc:	LANGFORD Colin W (Colin.LANGFORD@rms.nsw.gov.au); "Bruce Colman"; "Richard Seddon"; Aaron Nangle
	(Aaron.Nangle@planning.nsw.gov.au); "Kym Dracopoulos"; "Suresh.Surendran@rms.nsw.gov.au"; Matty.MATHIVANAR@rms.nsw.gov.au; "Will Dwyer"
Subject:	OWR Upgrade Files
Date:	Friday, 27 June 2014 4:06:37 p.m.
Attachments:	image001.png
	13-143-R002-05-Old Wallgrove Road Road Design Statement low res.pdf
	SSDA OWR Upgrade.pdf

Shibree, attached is the current OWR upgrade drawings along with the design report for the proposed works. This all forms part of the SSDA which was submitted to the Department.

Below is a link to the presentation files which you saw yesterday. We look forward to your design sections, advice by this time next week.

Should you have any questions, please call.

https://atl.sharefile.com/d/sdfe687abdaf4636a

Regards

Anthony McLandsborough Director



Suite 702, 154 Pacific Highway St Leonards NSW 2065

P 02 9439 1777
 M 0433 973 423
 F 02 9460 8413
 anthony@atl.net.au
 www.atl.net.au



Attachment 2 Email dated 13th July 2014

Civil Engineers & Project Managers

From:	Anthony McLandsborough		
To:	Ahmad Mangal (Ahmad.MANGAL@rms.nsw.gov.au)		
Cc:	LANGFORD Colin W; CHOWDHURY Ruhul; RATHAN Pahee; MATHIVANAR Matty; ADAMS David C; ANTONY Saverimuthu L; "Aaron.Nangle@planning.nsw.gov.au"; "Will Dwyer"; "Richard Seddon"; "Kym Dracopoulos"; Peter Wark; Brendon Quinn (Brendon.Quinn@goodman.com); graham.pindar@traffix.com.au; Josh Barnett		
Subject:	OWR Upgrade - Meeting outcome		
Date:	Sunday, 13 July 2014 12:46:43 p.m.		
Attachments:	SKC110[P2].PDF image001.png		

Ahmad, further to our meeting on Friday, we have moved quickly to ratify the '**Interim**' Stage 1 Cross Section along with the '**Rationalised Ultimate**' Option.

In summary, the discussion on Friday;

- 1. RMS provided their initial proposed 'Interim' Stage 1 option. 2m hard shoulder, 3.3m lane, 0.6m painted, 3.3m lane, 1m verge (table drains either side)
- 2. The need for the Transgrid RTL was discussed. AM noted that we were undertaking traffic counts next week and will include the traffic in/out of Transgrid. Once known further discussion with regards to the ultimate option. RS did note that as part of the negotiations with Transgrid, a commitment had been made to the future RTL. The 'Interim' option should only allow for a BAR type intersection
- 3. Discussion regarding speed limit. The road is to be design to **80km/hr**, sign posted on the interim option at 60km/hr, 'Ultimate' Option to be sign posted 80km/hr (as 70km/hr is no longer used by RMS) Speed advisory signage to be installed at the bends
- 4. Proposed intersection works at the EPLR/OWR was discussed and the Jacfin proposal for the fourth leg. Due to the forth leg it will be difficult to allow for the duel RT from OWR to the EPLR without significant works to the EPLR. It was agreed to wait for the traffic numbers (due within 3 weeks) to understand the impact of a single RT vs a duel RT. David Adams made note that the design of the duel RT would need to accommodate duel B-doubles turning. (this is the case for the EPLR)
- 5. It was agreed we need to minimise the extent of works for both the interim and ultimate options
- 6. It was agreed the property acquisition should occur as part of the interim
- 7. It was agreed the services relocations should be relocated to suit the 'Ultimate' option.
- It was agreed street light is required. The extent of and category of the street lighting will be later determined by Council. (Note to date we have allow for V3. i.e. 9m poles at 40m staggered for the length of the road)
- 9. The Shared path was discussed. AM noted Council had previously requested this. It was generally agreed the shared path should be constructed in the 'Interim' option
- 10. Colin Langford noted irrespective of the 'Interim' option, the 'Ultimate' option needs to be rationalised. David Adams provided two options;
 - i. 21m road reserve <u>3.5 verge, K&G, 3.5 lane, 3.5 lane, BB Line,</u>
 - <u>3.5 lane, 3.5 lane, K&G, 3.5 verge</u>
 - ii. 21.2m road reserve <u>3.5 verge, K&G, 3.5 lane, 3.3 lane, 0.6 Painted</u> <u>median, 3.3 lane, 3.5 lane, K&G, 3.5 verge</u>
- 11. AM noted that with the narrower reserve, more consideration needs to be given to the construction methodology and the cost implications.
- 12. It was agreed the following would occur to move forward;

- AT&L to review all of the comments and discussion points of the meeting and provide a new 'Interim' and 'Ultimate' option cross section by Monday
- <u>Assuming</u> the sections are generally acceptable, AT&L to finalise concept plans and section for re-pricing by Mark Raven. Revised estimates to be issued by Friday 18th July. (Note we will show on the plans in colour the extent of the existing pavement)
- RMS to review revised plans and cost estimate and provide direction on how to proceed by Friday 25th July
- Once we have this direction, a meeting with the Councils to be arranged to inform them of the outcome.

Post Meeting

We have now taken on board all of the points above and the meeting as a whole and make the following comments;

- 13. Design Considerations 'Interim' Stage 1
 - We are of the opinion the Share path should be constructed as part of the 'Interim' stage
 - We agreed any services relocations need to be located in their ultimate level and alignment
 - Street lighting will be installed on one side of the road
 - If the above occurs, K&G is required along the western side
 - With a 2.5m shared path, we have allocated 3.75 as the verge width to accommodate the lighting and reasonable offset of 700mm from the face of kerb
 - We have allocated 2.5m shoulder for breakdown area, 3.3m travel lanes, 0.6 painted median and 2m shoulder with a table drain along the east side of the road
- 14. Design Considerations 'Rationalised Ultimate' option
 - Adopting the RMS option above and incorporating the 3.75m verge, we have proposed <u>3.75m verge</u>, K&G, 3.5 lane, 3.3m lane, 0.6 PM, 3.3 lane, 3.5 lane, K&G, 3.5 verge
- 15. We note that while the above options vary from the RMS proposed, the minor changes will have little impact on the estimate. Ultimately we're comparing one option vs the other to understand the percentage difference. The minor changes will have a very minor impact on this.
- 16. When we present our estimate on Friday, we will include 3 summarised options;
 - i. Original 23m Full option
 - ii. 'Interim' Stage 1 option
 - iii. 'Rationalised Ultimate' option

Should you have any comments, please don't hesitate to call to disucss.

Regards

Anthony McLandsborough

Director



Suite 702, 154 Pacific Highway St Leonards NSW 2065

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at&l

Attachment 3 Email dated 20th July 2014

Civil Engineers & Project Managers

From:	Anthony McLandsborough		
To:	Ahmad Mangal (Ahmad.MANGAL@rms.nsw.gov.au)		
Cc:	"LANGFORD Colin W"; "CHOWDHURY Ruhul"; "RATHAN Pahee"; "MATHIVANAR Matty"; "ADAMS David C"; "ANTONY Saverimuthu L"; "Aaron.Nangle@planning.nsw.gov.au"; "Will Dwyer"; "Richard Seddon"; "Kym Dracopoulos"; Peter Wark; Brendon Quinn (Brendon.Quinn@goodman.com); graham.pindar@traffix.com.au; Josh Barnett		
Subject:	RE: OWR Upgrade - Meeting outcome		
Date:	Sunday, 20 July 2014 2:38:41 p.m.		
Attachments:	image001.png Stage 2 Rationalised Ultimate Cost Estimate.pdf GoodmanATLUltimate Cost Estimate.pdf Rationalised Ulitmate Cost Estimate.pdf Rationalised Ulitmate DWGs.pdf Stage 1 and 2 DWGs.pdf Stage 1 Interim Cost Estimate.pdf		

Ahmad as committed to below, we have now finalized the preparation of the **Interim Stage 1 and 2** concept design along with the **Rationalized Ultimate** concept design. These have also been costed by Mark Raven as setout below;

1.	Origin	al Green Ultimate option inc. Contingency	\$24,275,973	
2.	Rationalized Ultimate option inc. Contingency		\$23,417,733	
3.	Interim Stage 1 inc. Contingency		\$20,374,851	
4.	Stage 2 inc. Contingency		<u>\$4,128,993</u>	
	a.	Total combined Interim works	\$24,503,844 (extra over of	
	\$1,086,111 to item 2 or extra over of \$227,871 to item 1)			

We would like to meet next Friday afternoon at 3pm. Could you confirm if this time is suitable.

Regards

Anthony McLandsborough

Director



M 0433 973 423 F 02 9460 8413 anthony@atl.net.au

www.atl.net.au

From: Anthony McLandsborough
Sent: Sunday, 13 July 2014 12:47 p.m.
To: Ahmad Mangal (Ahmad.MANGAL@rms.nsw.gov.au)
Cc: LANGFORD Colin W; CHOWDHURY Ruhul; RATHAN Pahee; MATHIVANAR Matty; ADAMS David C; ANTONY Saverimuthu L; 'Aaron.Nangle@planning.nsw.gov.au'; 'Will Dwyer'; 'Richard Seddon'; 'Kym Dracopoulos'; Peter Wark; Brendon Quinn (Brendon.Quinn@goodman.com);

Ahmad, further to our meeting on Friday, we have moved quickly to ratify the 'Interim' Stage 1 Cross Section along with the 'Rationalised Ultimate' Option.

In summary, the discussion on Friday;

- 1. RMS provided their initial proposed 'Interim' Stage 1 option. 2m hard shoulder, 3.3m lane, 0.6m painted, 3.3m lane, 1m verge (table drains either side)
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- 9. The Shared path was discussed. AM noted Council had previously requested this. It was generally agreed the shared path should be constructed in the 'Interim' option
- 10. Colin Langford noted irrespective of the 'Interim' option, the 'Ultimate' option needs to be rationalised. David Adams provided two options;

i.	21m road reserve –	<u>3.5 verge, K&G, 3.5</u>			
lane, 3.5 lane, BB Line, 3.5 lane, 3.5 lane, K&G, 3.5 verge					
ii.	21.2m road reserve –	<u>3.5 verge, K&G, 3.5</u>			
lane, 3.3 lane, 0.6 Painted median, 3.3 lane, 3.5 lane, K&G, 3.5 verge					
at with the narrower reserve, more consideration needs to be given to the					

- 11. AM noted that
- construction methodology and the cost implications. 12. It was agreed the following would occur to move forward;
 - AT&L to review all of the comments and discussion points of the meeting and
 - provide a new 'Interim' and 'Ultimate' option cross section by Monday
 - Assuming the sections are generally acceptable, AT&L to finalise concept plans and section for re-pricing by Mark Raven. Revised estimates to be issued by Friday 18th July. (Note we will show on the plans in colour the extent of the existing pavement)

- RMS to review revised plans and cost estimate and provide direction on how to proceed by Friday 25th July
- Once we have this direction, a meeting with the Councils to be arranged to inform them of the outcome.

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 - If the above occurs, K&G is required along the western side
 - With a 2.5m shared path, we have allocated 3.75 as the verge width to accommodate the lighting and reasonable offset of 700mm from the face of kerb
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 - Adopting the RMS option above and incorporating the 3.75m verge, we have proposed <u>3.75m verge</u>, K&G, 3.5 lane, 3.3m lane, 0.6 PM, 3.3 lane, 3.5 lane, K&G, 3.5 verge
- 15. We note that while the above options vary from the RMS proposed, the minor changes will have little impact on the estimate. Ultimately we're comparing one option vs the other to understand the percentage difference. The minor changes will have a very minor impact on this.
- 16. When we present our estimate on Friday, we will include 3 summarised options;
 - i. Original 23m Full option
 - ii. 'Interim' Stage 1 option
 - iii. 'Rationalised Ultimate' option

Should you have any comments, please don't hesitate to call to disucss.

Regards

Anthony McLandsborough Director

Suite 702, 154 Pacific Highway St Leonards NSW 2065

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 M 0433 973 423
 F 02 9460 8413
 anthony@atl.net.au
 www.atl.net.au

PROJECT: OLD WALLGROVE RD UPGRADE - OAKDALE CENTRAL

\$118 /m2

CLIENT: Goodman **OPTION: STAGE 1 - INTERIM**

Pavement-Main

Project Summary Rev A Project No: 14046 DATE: Estimate Stage: Concept Jul-14 Item Estimate Contingency Estimate % of Total Comments/Assumptions (excluding % Amount (including Estimate contingency) contingency) 1. Project Development (a) Survey/Potholing \$61,189 0% \$0 \$61,189 Actual cost incurred by GPS. 80% allocated 1 (b) Concept Road Design/ Project \$77,811 0% \$0 \$77.811 Actual cost incurred by GPS 80% allocated Management 1 (c) Environmental/Contamination \$23,600 0% \$0 \$23,600 Actual cost incurred by GPS. 80% allocated Assessment Sub total \$162,600 0% \$0 \$162,600 0.8% 2. Investigation and Design 2 (a) Investigation and Design \$990 935 20% \$198 187 \$1,189,122 AT&L Fee extra over for production of two sets 2 (b) Project Management Services \$0 0% \$0 \$0 incl. in 2 (a) Sub total \$990,935 20% \$198,187 \$1,189,122 5.8% 3. Property Acquisitions 3 (a) Acquire Property \$1,750,500 40% \$700,200 \$2,450,700 Based onGPC advice of \$250/m2 3 (b) Professional Services for Property \$122,535 40% \$49,014 \$171,549 3 (c) Project Management Services \$0 0% \$0 incl. in 2 (a) \$0 \$1,873,035 Sub total \$749.214 \$2,622 249 12.9% 4. Public Utility Adjustments 4 (a) Adjust Utilities \$0 35% \$0 \$0 Included in SOR 4 (b) Project Management Services 35% \$0 \$0 \$0 9% of Utilities cost 4 (c) Client Representation \$0 35% \$0 \$0 10% of Project Management Cost Sub total \$0 \$0 \$0 0.0% 5. Construction 5(a) Schedule of Rates \$1,020,211 - General 37% \$1 396 085 \$375 874 \$3,009,029 - Services \$4,166,441 38% \$1,157,412 \$1,185,043 - Traffic Control 35% \$414,765 \$1,599,808 \$912,540 - Drainage and Kerbing 37% \$334,807 \$1,247,347 - Earthworks \$1.523.868 35% \$538,778 \$2,062,646 - Pavements \$2,396,216 35% \$838,676 \$3,234,892 - Road furniture \$1,473,267 34% \$1,968,681 \$495,414 \$11,520,175 36% \$4,155,725 \$15,675,900 5 (b) Primary Testing Included in SOR 5 (c) Insurance \$63,361 36% \$22,856 \$86,217 0.55% of infrastructure costs 5 (d) Project Management Tender AT&L Fee. 80% Allocated (inc extra over for 2 \$280,000 35% \$98.000 \$378,000 Process/Construction/ Handover stages 5 (e) Independent Verification \$77.040 35% \$26,964 \$104,004 AT&L Fee. 80% Allocated Construction \$11,940,576 \$16,244,121 Sub total 36% \$4,303,545 79.7% 6. Handover 6 (a) Handover and Finalisation \$ % s Excluded \$ \$41,557 \$156,759 6 (b) Project data and conformance \$115,202 36% 1% of infrastructure costs 6 (c) Project Management Services 36% \$0 \$0 \$0 9% of Project data & Performance Review \$115,202 Sub total 36% \$41,557 \$158,759 0.8% TOTAL \$15,082,348 35% \$5,292,503 \$20,374,851 100% RMS require 25% to 40% Project Management \$357,811 \$98,000 \$455,811 2.2% Reality Checks Excluding Contingency Including Contingency Rate Qty Unit Rate Unit 1. Project Cost (Incl Contingency)/ km \$9,426,467 /cway-km \$12,734,282 /cway-km 16 2. Protect Cost / lane-km \$2,356,617 /lane-km 6.4 \$3.183.571 /lane-km Earthworks-Cut/Fill \$28 /m3 10,000 \$35 /m3 Farthworks-Imoort \$0 /m3 0

\$0 /m3 \$159 /m2

12,720

Prepared by: T.Yildirim
PROJECT: OLD WALLGROVE RD UPGRADE - OAKDALE CENTRAL

CLIENT: Goodman

OPTION: RATIONALISED ULTIMATE FULL CONSTRUCTION

Orolast No: 44046		DATE.	L.1.44		F . 41		
Project No: 14046		DATE:	Jul-14		Estimate Stage: Concept		
Item	Estimate	Continge	ncy	Estimate	% of Total	Comments/Assumptions	
	(excluding	%	Amount	(including	Estimate		
	contingency)			contingency)			
1. Project Development							
1 (a) Survey/Potholing	\$76,486	0%	\$0	\$76,486		Actual cost incurred by GPS	
1 (b) Concept Road Design/ Project							
Management	\$97,264	0%	\$0	\$97,264		Actual cost incurred by GPS	
1 (c) Environmental/Contamination	\$29,500	0%	\$0	\$29,500		Actual cost incurred by GPS	
Assessment							
Sub total	\$203,250	0%	\$0	\$203,250	0.9%		
2. Investigation and Design							
2 (a) Investigation and Design	\$870,935	20%	\$174,187	\$1,045,122		AT&L Fee	
2 (b) Project Management Services	\$0	0%	\$0	\$0		ind. in 2 (a)	
Sub total	\$870,935	20%	\$174,187	\$1,045,122	4.5%	-	
. Property Acquisitions							
3 (a) Acquire Property	\$1,750,500	40%	\$700,200	\$2,450,700	1	Based onGPC advice of \$250/m2	
3 (b) Professional Services for Property	\$122,535	40%	\$49,014	\$171,549			
3 (c) Project Management Services	\$0	0%	\$0	\$0		incl. in 2 (a)	
						4	
Sub total	\$1,873,035		\$749,214	\$2,622,249	11.2%		
I. Public Utility Adjustments							
4 (a) Adjust Utilities	\$0	35%	\$0	\$0		Included in SOR	
4 (b) Project Management Services	\$0	35%	\$0	\$O		9% of Utilities cost	
(c) Client Representation	\$0	35%	\$0	\$0	1	10% of Project Management Cost	
Sub total	\$0		\$0	60	0.0%		
5. Construction	30		30	\$0	0.0%		
5(a) Schedule of Rates							
- General	\$1,086,851	67%	\$730,602	\$1,817,454			
- Services	\$3,245,746	28%	\$920,694	\$4,166,441			
- Traffic Control	\$1,102,147	35%	\$385,752	\$1,487,899			
 Drainage and Kerbing Earthworks 	\$1,271,071	36%	\$463,552	\$1,734,623			
- Pavements	\$1,960,290 \$2,979,880	35% 35%	\$693,042 \$1,042,958	\$2,653,332 \$4,022,838			
- Road furniture	\$2,129,092	35%	\$1,042,958 \$736,828	\$4,022,838			
- Road full lide	\$13,775,077	36%	\$4,973,429	\$18,748,506	-		
5 (b) Primary Testing	410,110,011	30 /4	44,010,440	\$10,140,000	4	Included in SOR	
5 (c) Insurance	\$75,763	36%	\$27,354	\$103,117		0.55% of infrastructure costs	
6 (d) Project Management Tender							
Process/Construction/ Handover	\$280,000	35%	\$98,000	\$378,000		AT&L Fee	
5 (e) Independent Verification	\$96,300	35%	\$33,705	\$130,005		AT&L Fee	
Construction							
Sub total	\$14,227,139	36%	\$5,132,488	\$19,359,627	82.7%		
5. Handover							
6 (a) Handover and Finalisation	s	%	\$	s		Excluded	
3 (b) Project data and conformance	\$137,751	36%	\$49,734	\$187,485		1% of infrastructure costs	
6 (c) Project Management Services	\$0	36%	\$0	\$0	1	9% of Project data & Performance Review	
						<u>p</u>	
Cub total	\$437 784	9.61/	A40 704	\$487 485	-		
Sub total	\$137,751 \$17,312,110	36%	\$49,734	\$187,485	0.8%	DMC require 25% to 40%	
Project Management	\$17,312,110	35%	\$6,105,623 \$98,000	\$23,417,733 \$475,264	100% 4 2.0	RMS require 25% to 40%	
•						a na	
Reality Checks		iding Conting	20 CONSTR	100	Contingency		
	Rate	Unit	Qty	Rate	Unit		
. Project Cost (Incl Contingency)/ km	\$10,820,069	•	1.6	\$14,636,083	-		
2. Project Cost / Iane-km	\$2,705,017		6.4	\$3,659,02			
Earthworks-Cut/Fill		/m3	10,000		5 /m3		
entry order import	\$0	/m3	0	5	0 /m3		
Earthworks-Import Pavement-Main	\$118		16,960		9 /m2		

Prepared by: T.Yildirim

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PROJECT:OLD WALGROVE RD UPGRADE - OAKDALE CENTRAL

CLIENT: Goodman

Project Summary Rev C Project No: 14046 DATE: May-14 Estimate Stage: Concept Item Estimate Comments/Assumptions Contingency Estimate % of Total (excluding % Amount (including Estimate contingency) contingency) 1. Project Development 1 (a) Survey/Potholing \$76 486 0% \$0 \$76 486 Actual cost incurred by GPS 1 (b) Concept Road Design/ Project \$131,580 0% \$0 \$131,580 Actual cost incurred by GPS Management 1 (c) Environmental/Contamination \$29 500 0% \$0 \$29,500 Actual cost incurred by GPS Assessment Sub total \$237,566 0% \$0 \$237,566 1.0% 2. Investigation and Design 2 (a) Investigation and Design \$700,935 20% \$140,187 \$841,122 AT&L Fee 2 (b) Project Management Services \$150,000 20% \$30.000 \$180,000 AT&L Fee Sub total \$850.935 20% \$170.187 \$1.021.122 4.2% 3. Property Acquisitions 3 (a) Acquire Property \$2,077,750 40% \$831,100 \$2,908,850 Based on GPC advice of \$250/m2 3 (b) Professional Services for Property \$145,443 30% \$43,633 \$189,075 3 (c) Project Management Services 0% \$0 \$0 \$0 incl. in 2 (a) \$2,223,193 Sub total \$874,733 \$3,097,925 12.8% 4. Public Utility Adjustments 4 (a) Adjust Utilities 35% \$0 \$0 \$0 Included in SOR 4 (b) Project Management Services \$0 35% \$0 \$0 Included in 5d) Sub total \$0 \$0 \$0 0.0% 5. Construction 5(a) Schedule of Rates \$1 331 893 37% \$496,799 \$1 828 691 - General Refer to Scope Definition \$3,009,029 - Utility Relocations & Traffic Signals 38% \$1,157,412 \$4,166,441 For Breakdown \$1,051,789 - Traffic Control 35% \$368,126 \$1,419,915 of Coverage for these - Drainage and Kerbing \$1,293,561 \$1,739,547 34% Item headings \$445,987 - Earthworks \$2,105,226 35% \$744,317 \$2,849,543 - Pavements \$3,237,863 \$4,224,982 30% \$987.119 - Road furniture \$2,131,584 29% \$624,491 \$2,756,076 \$14,160,945 \$4,824,251 \$18,985,196 34% 5 (b) Primary Testing Included in SOR 5 (c) Insurance \$77.885 34% \$26,533 \$104,419 0.55% of infrastructure costs 5 (d) Project Management Tender \$305,000 35% \$106,750 \$411,750 AT&L Fee Process/Construction/ Handover 5 (e) Independent Verification Construction \$96,300 35% \$33,705 \$130,005 AT&L Fee Sub total \$14,640,130 \$4,991,239 \$19,631,369 80.9% 34% 6. Handover 6 (a) Handover and Finalisation s % S Evoluded S 6 (b) Project data and conformance \$141,609 34% \$48,243 \$189,852 1% of infrastructure costs 6 (c) Project Management Services \$73,201 34% \$24,937 \$98,138 0.5% of construction cost Sub total \$214,810 34% \$73,180 \$287,990 1.2% TOTAL \$24,275,973 \$18,166,634 34% \$6,109,339 100% RMS require 25% to 40% Project Management \$659.781 \$161,687 \$821,468 3.4% Excluding Contingency **Reality Checks** Including Contingency Rate Unit Qty Rate Unit 1. Project Cost (Incl Contingency)/ km \$15,172,483 /cway-km \$11,354,146 /cway-km 1.6 2. Project Cost / lane-km \$2,838,537 /lane-km 6.4 \$3,793,121 /lane-km Earthworks-Cut/Fill \$26 /m3 10,000 \$35 /m3 Earthworks-Import \$0 /m3 \$0 /m3 0 Pavement-Main \$118 /m2 18,430 \$157 /m2

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Prepared by: Mark Raven

PROJECT: OLD WALLGROVE RD UPGRADE - OAKDALE CENTRAL

Prepared by: T.Yildirim

CLIENT: Goodman

OPTION: STAGE 2 - RATIONALISED ULTIMATE

Project Summary						Rev A			
Project No: 14046		DATE:	Jui-14		Estimate Stage: Concept				
Item	Estimate	Continge	ncy	Estimate	% of Total	Comments/Assumptions			
	(excluding	%	Amount	(including	Estimate				
	contingency)			contingency}					
1. Project Development									
1 (a) Survey/Potholing	\$15,297	0%	\$0	\$15,297		Actual cost incurred by GPS. 20% Allocated			
1 (b) Concept Road Design/ Project	\$19,453	0%	\$0	\$19,453		Actual cost incurred by GPS			
Management 1 (c) Environmental/Contamination				,		,			
Assessment	\$5,900	0%	\$0	\$5,900		Actual cost incurred by GPS			
Sub total	\$40,650	0%	\$0	£ 40.010	4.00%	4			
2. Investigation and Design	940,000	U7a	\$0	\$40,650	1.0%				
2 (a) Investigation and Design	\$0	0%	\$0	\$0		completed in Stage 1 Interim Proposal			
2 (b) Project Management Services	\$75,000	0%	\$0	\$75,000		Additional contract docs			
Sub total	\$75,000	0%	\$0	\$75,000	1.8%	4			
3. Property Acquisitions									
3 (a) Acquire Property	\$0	40%	\$0	\$0		Based onGPC advice of \$250/m2			
3 (b) Professional Services for Property	\$0	40%	\$0	\$0					
3 (c) Project Management Services	\$0	0%	\$0	\$0		incl. in 2 (a)			
Sub total	\$0		\$0	\$0	0.0%	4			
4. Public Utility Adjustments									
4 (a) Adjust Utilities	\$0	35%	\$0	\$0		Included in SOR			
4 (b) Project Management Services	\$0	35%	\$0	\$0		9% of Utilities cost			
4 (c) Client Representation	\$0	35%	\$0	\$0		10% of Project Management Cost			
						4			
Sub total 5. Construction	\$0		\$0	\$0	0.0%				
5(a) Schedule of Rates									
- General - Services	\$440,787 \$0	38%	\$166,111	\$606,898 \$0					
- Traffic Control	\$310,411	35%	\$0 \$108,644	\$419,055					
- Drainage and Kerbing	\$305,838	42%	\$128,045	\$433,883					
- Earthworks	\$386,981	35%	\$136,960	\$523,941					
- Pavements	\$661,559	35%	\$231,546	\$893,105					
- Road furniture	\$704,955	36%	\$251,587	\$956,541					
5 (b) Primary Testing	\$2,810,531	36%	\$1,022,893	\$3,833,424					
5 (c) Insurance	\$15,458	36%	\$5,626	\$21,084		Included in SOR 0.55% of infrastructure costs			
5 (d) Project Management Tender	261 274					AT&L Fee. 20% Allocated, includes extra over for			
Process/Construction/ Handover	\$70,000	35%	\$24,500	\$94,500		2 stages			
5 (e) Independent Verification Construction	\$19,260	35%	\$6,741	\$26,001		AT&L Fee. 20% Allocated			
Sub total	£2.045.240	36%	£4 050 700	\$2 07F 000	00.08/	-			
6. Handover	\$2,915,249	30%	\$1,059,760	\$3,975,009	96.3%				
6 (a) Handover and Finalisation	\$	%	\$	\$		Excluded			
6 (b) Project data and conformance	\$28,105	36%	\$10,229	\$38,334		1% of infrastructure costs			
6 (c) Project Management Services	\$0	36%	\$0	\$0		9% of Project data & Performance Review			
						_			
Sub total	\$28,105	36%	\$10,229	\$38,334	0.9%				
TOTAL	\$3,059,004	36% 35%	\$1,069,989	\$4,128,993	100%	RMS require 25% to 40%			
TOTAL Project Management	\$3,059,004 \$164,453	35%	\$1,069,989 \$24,500	\$4,128,993 \$188,953	100% 4.6				
TOTAL	\$3,059,004 \$164,453 Exclu	35%	\$1,069,989 \$24,500 ency	\$4,128,993 \$188,953 Including (100% 4.6 Contingency				
TOTAL Project Management Reality Checks	\$3,059,004 \$164,453 Exclu <u>Rate</u>	35% Iding Conting <u>Unit</u>	\$1,069,989 \$24,500 ency <u>Qty</u>	\$4,128,993 \$188,953 Including (<u>Rate</u>	100% 4.6 Contingency <u>Unit</u>				
TOTAL Project Management Reality Checks 1. Project Cost (Inci Contingency)/ km	\$3,059,004 \$164,453 Exclu <u>Rate</u> \$1,911,878	35% Iding Conting <u>Unit</u> /cway-km	\$1,069,989 \$24,500 ency <u>Qtv</u> 1.6	\$4,128,993 \$188,953 Including (<u>Rate</u> \$2,580,621	100% 4.6 Contingency <u>Unit</u> /cway-km				
TOTAL Project Management Reality Checks	\$3,059,004 \$164,453 Exclu <u>Rate</u> \$1,911,878 \$477,969	35% Iding Conting <u>Unit</u> /cway-km	\$1,069,989 \$24,500 ency <u>Qty</u>	\$4,128,993 \$188,953 Including (<u>Rate</u> \$2,580,621 \$645,155	100% 4.6 Contingency <u>Unit</u> /cway-km /lane-km				
TOTAL Project Management Reality Checks 1. Project Cost (Inci Contingency)/ km 2. Project Cost / Iane-km	\$3,059,004 \$164,453 Exclu <u>Rate</u> \$1,911,878 \$477,969 \$0	35% Iding Conting <u>Unit</u> /cway-km /lane-km	\$1,069,989 \$24,500 ency <u>Qty</u> 1.6 6.4	\$4,128,993 \$188,953 Including (<u>Rate</u> \$2,580,621 \$645,155 \$0	100% 4.6 Contingency <u>Unit</u> /cway-km				























Attachment 4 Draft Traffic Report

Civil Engineers & Project Managers



suite 3.08

Reference: 13.282l01v1

traffic & transport planners

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1 August 2014

AT&L Suite 702, 154 Pacific Highway St Leonards NSW 2065

Attention: Mr Anthony McLandsborough

Re: Oakdale Central, Old Wallgrove Road

Dear Anthony,

As requested, as part of the planning for the upgrade of Old Wallgrove Road in conjunction with the delivery of the Oakdale Central precinct, we have investigated the following issues:

- 1. The need for a dedicated right turn pocket from Old Wallgrove Road into the existing Transgrid site;
- 2. The need for a second right turn lane from Old Wallgrove Road into Erskine Park Link Road; and
- 3. The need for the signalisation of the Old Wallgrove Road / Millner Avenue Intersection.

The results of these investigations are outlined following.

Right Turn Pocket into Transgrid Site

It is understood that Old Wallgrove Road is to be upgraded in accordance with the "Rationalised Ultimate" configuration as part of the delivery of the Oakdale Central. This configuration will comprise a 4-lane cross-section with 3.3m – 3.5m through lanes and a 600mm wide painted central median.

We have investigated the need for the provision of a dedicated right turn pocket from Old Wallgrove Road into the Transgrid site, which is located approximately 500m to the north of the Oakdale Central precinct, and is currently accessed from Old Wallgrove Road via a driveway crossover.

Traffic surveys were undertaken at the access to the Transgrid site to record existing volumes entering and exiting the site, as well as through traffic on Old Wallgrove Road. The results of these surveys are included as **Attachment A**, and demonstrate reasonable volumes of traffic entering and exiting the site, as summarised following:

- AM Peak: 87 arrivals and 11 departures; and
- PM Peak: 11 arrivals and 102 departures.

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An assessment of the need for a right turn pocket into the Transgrid site has been undertaken, using the turn warrants outlined in Austroads Guide to Road Design Part 4A: Unsignalised and Signalised Intersections.

The results of this assessment are outlined in the table and graph below, and demonstrate that the current turning volumes into the Transgrid site combined with the through volumes on Old Wallgrove Road suggest that a short channelised right turn treatment (CHR(S)) into Transgrid is currently warranted.

Furthermore, the development of substantial land parcels to the south of the site (including the Austral Bricks site and the CSR Bricks site) will only serve to increase the through traffic volumes on Old Wallgrove Road.

In light of the above, it is recommended that a dedicated right turn pocket from Old Wallgrove Road into the Transgrid site be constructed as part of the upgrade of Old Wallgrove Road.

Table 1: Recorded Traffic Volumes for Turn Warrants Assessment, Transgrid Access

	Major Road Traffic Volume (Q_M)	Turn Volume (Q _R)
AM Peak Hour	217/2* + 90 + 4 = 203	83
PM Peak Hour	83/2* + 184 + 0 = 226	11

* assumes a 4-lane major road cross-section, i.e. based upon the "Rationalised Ultimate" configuration of Old Wallgrove Rd



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Second Right Turn Lane from Old Wallgrove Road into Erskine Park Link Road

The Erskine Park Link Road / Old Wallgrove Road intersection was constructed in mid-2013 as a signalised T-intersection, as part of the delivery of the Erskine Park Link Road.

Various intersection configurations were investigated by GHD as discussed in the report "Old Wallgrove Road Extension – Traffic and Transport Analysis, Summary of Modelling Findings, 18 July 2013." The results indicate that this intersection was expected to operate acceptably as a T-intersection with a single right turn from Old Wallgrove Road into Erskine Park Link Road at 2031, at a Level of Service C (although the modelled queue for this movement was about 230m).

It is understood however that this intersection is to be upgraded to a 4-way signalised intersection, with a fourth (northern leg) to be constructed to provide access to the Jacfin land parcel to the north.

Accordingly, this intersection has been analysed as a 4-way signalised intersection, with the modelled geometry and phasing arrangement as shown below.



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The modeled intersection volumes reflect those in the GHD report "Old Wallgrove Road Extension – Traffic and Transport Analysis, Summary of Modelling Findings, 18 July 2013" for the 2021 PM peak design horizon, with a nominal 50vph assumed for each movement into and out of the fourth (northern) intersection leg.

The results of these analyses indicate even with low volumes of traffic accessing the Jacfin land parcel to the north of the intersection, the intersection is expected to fail prior to 2021, with the fourth intersection leg. The table below provides the model results, which indicate a Level of Service F for the intersection, and queues on Old Wallgrove Road of approximately 500m.

Single Right Turn Lane from Old Wallgrove Road

Mov ID	ODMo	Demand	- Veh	Deg. Satn	Average	Level of	95% Back	of Queue	Prop.	Effective	Average
	V	Total	HV		Delay	Service	Vehicles	Distance	Queued	Stop Rate	Speed
		veh/h	%	v/c	sec		veh	m		per veh	km/h
South:	Old Wallgr	ove Road									
1	L2	50	14.0	0.092	17.5	LOS B	1.5	11.5	0.44	0.65	45.9
2	T1	50	0.0	0.966	86.8	LOS F	63.7	495.0	0.97	1.08	24.0
3	R2	612	14.0	0.966	92.6	LOS F	63.7	495.0	0.97	1.08	23.7
Approa	ich	712	13.0	0.966	86.9	LOS F	63.7	495.0	0.93	1.05	24.5
East: E	rskine Par	k Link Road	d i								
4	L2	442	14.0	0.358	7.7	LOS A	5.8	45.4	0.25	0.62	52.2
5	T1	653	14.0	0.903	78.5	LOS F	27.8	217.9	1.00	1.08	26.2
6	R2	50	0.0	0.393	55.6	LOS D	2.9	20.2	1.00	0.74	31.0
Approa	ch	1145	13.4	0.903	50.2	LOS D	27.8	217.9	0.71	0.89	32.8
North:	Access to .	Jacfin Site									
7	L2	50	0.0	0.222	39.1	LOS C	2.5	17.8	0.72	0.72	36.3
8	T1	50	0.0	0.183	61.6	LOS E	3.2	22.7	0.92	0.70	29.9
9	R2	50	0.0	0.192	67.4	LOS E	3.3	22.8	0.92	0.74	28.3
Approa	ch	150	0.0	0.222	56.0	LOS D	3.3	22.8	0.85	0.72	31.2
West: E	Erskine Par	rk Link Roa	d								
10	L2	50	0.0	0.048	13.1	LOS A	1.1	7.8	0.37	0.64	48.8
11	T1	706	14.0	0.956	98.2	LOS F	33.6	263.4	1.00	1.23	23.0
12	R2	50	14.0	0.414	56.0	LOS D	2.9	22.9	1.00	0.74	30.6
Approa	ch	806	13.1	0.956	90.3	LOS F	33.6	263.4	0.96	1.16	24.2
All Veh	icles	2813	12.5	0.966	71.3	LOS F	63.7	495.0	0.84	1.00	27.5

Signals - Fixed Time Cycle Time = 150 seconds (Practical Cycle Time)

Given the results of the analyses above, the intersection was modelled with a second right turn lane from Old Wallgrove Road into Erskine Park Link Road. The results (shown in the table below) indicate substantially better performance, with a Level of Service C and 95th percentile queues on for critical movements in the order of 150m.



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Table 3: Modelled Intersection Performance, 2021 PM Peak Dual Right Turn from Old Wallgrove Road

Signals - Fixed Time	Cycle Time = 100 seconds (Practical Cycle Time)

			WARDON.	. 79407		N. Sarray					
Move	ement Per	formance	e - Vehi	cles							
Mov I	D ODMo	Demand	Flows I	Deg. Satn	Average	Level of	95% Back	of Queue	Prop.	Effective	Average
	v	Total	HV		Delay	Service	Vehicles	Distance	Queued	Stop Rate	Speed
		veh/h	%	v/c	Sec		veh	m		per veh	km/h
South	: Old Wallgr	ove Road									
1	L2	50	14.0	0.113	17.0	LOS B	1.2	9.1	0.54	0.67	46.1
2	T1	50	0.0	0.854	47.2	LOS D	15.8	121.6	0.97	0.98	32.5
3	R2	612	14.0	0.854	53.2	LOS D	19.4	152.5	0.99	0.97	31.7
Appro	ach	712	13.0	0.854	50.3	LOS D	19.4	152.5	0.95	0.95	32.5
East:	Erskine Par	k Link Roa	d								
4	L2	442	14.0	0.376	8.1	LOS A	5.1	39.9	0.33	0.65	51.9
5	T1	653	14.0	0.767	41.4	LOS C	16.0	125.2	0.99	0.91	35.7
6	R2	50	0.0	0.268	33.5	LOS C	1.7	12.1	0.94	0.73	38.2
Appro	ach	1145	13.4	0.767	28.2	LOS B	16.0	125.2	0.73	0.80	40.8
North	Access to	Jacfin Site									
7	L2	50	0.0	0.106	21.7	LOS B	1.4	9.9	0.62	0.68	43.8
8	T1	50	0.0	0.122	34.7	LOS C	2.0	13.9	0.85	0.64	38.3
9	R2	50	0.0	0.128	40.4	LOS C	2.0	14.0	0.85	0.73	35.7
Appro	ach	150	0.0	0.128	32.2	LOS C	2.0	14.0	0.77	0.68	39.0
West:	Erskine Par	rk Link Roa	ad								
10	L2	50	0.0	0.058	16.1	LOS B	1.1	7.6	0.53	0.67	46.9
11	T1	706	14.0	0.823	44.9	LOS D	18.2	142.4	1.00	0.98	34.5
12	R2	50	14.0	0.275	33.6	LOS C	1.7	13.7	0.93	0.73	37.9
Appro	ach	806	13.1	0.823	42.4	LOS C	18.2	142.4	0.97	0.94	35.3
All Ve	hicles	2813	12.5	0.854	38.1	LOS C	19.4	152.5	0.86	0.88	36.7

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Whilst a number of assumptions were made necessarily in these analyses (regarding broader road network modifications and the level of development in the area), and alternative signal phasing arrangements which may influence the performance of the intersection are feasible, it would appear that the introduction of a fourth (northern) intersection approach at the Old Wallgrove Road / Erskine Park Link Road intersection would be likely to trigger the need for a second right turn lane from Old Wallgrove Road in the short to medium term, even with relatively low traffic volumes turning into and out of this northern leg.

Need for the signalisation of the Old Wallgrove Road / Millner Avenue Intersection

The Old Wallgrove Road / Millner Avenue Intersection currently operates as a priority-controlled Tintersection, however as part of the upgrade of Old Wallgrove Road, a fourth (eastern) intersection approach is to be constructed, which will provide access to the Austral site. The two existing access driveways to the Austral site are to be closed, with all access to this site to be via the 4-way intersection.

Traffic surveys of the Old Wallgrove Road / Millner Avenue Intersection and the two access driveways to the Austral site have been undertaken, with the results provided in **Attachment B**.

Intersection analyses have been undertaken of the Old Wallgrove Road / Millner Avenue Intersection as a 4-way intersection (assumed geometry shown below), with all traffic which currently accesses the Austral site via the driveways, instead doing so via this intersection.



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The results of these analyses indicate that during the critical PM peak period, the intersection is expected to operate acceptably with existing traffic volumes on Old Wallgrove Road and turning into and out of the Austral site, with the critical movement operating at Level of Service B.

However an increase in traffic volumes on Old Wallgrove Road and into and out of the Austral site would trigger the need for the signalisation of this intersection. Sensitivity analyses have been undertaken, with a summary of the results provided following:

Scenario	Old Wallgrove Road – Assumed Traffic Volume Increase	Austral Access - Assumed Traffic Volume Increase	Level of Service (Critical Movement)	
Existing Volumes	NA	NA	Level of Service B	
Sensitivity Test 1	+100vph (northbound) +100vph (southbound)	+100vph (entering from north) +100vph (exiting to north)	Level of Service C	
Sensitivity Test 2	+120vph (northbound) +120vph (southbound)	+120vph (entering from north) +120vph (exiting to north)	Level of Service D	
Sensitivity Test 3	+150vph (northbound) +150vph (southbound)	+150vph (entering from north) +150vph (exiting to north)	Level of Service F	

Table 4: Summary of Results of Sensitivity Analyses, Old Wallgrove Road / Millner Avenue Intersection

These results indicate that with just partial development of the approximately 75 ha land parcels to the south (the CSR site) and the east of the intersection (the Austral site), the intersection of Old Wallgrove Road / Millner Avenue will require signalisation.

Based upon the traffic generation rate of 10.5 trips per hectare assumed by GHD as part of previous studies, these traffic volumes equate to approximately the following level of development:

- 100vph in and out: 19 ha of development
- 120vph in and out: 23 ha of development
- 150vph in and out: 29 ha of development

In light of the results of the sensitivity analyses undertaken, it is recommended that the intersection of Old Wallgrove Road / Millner Avenue be signalised as part of the upgrade of Old Wallgrove Road.

Summary of Findings and Recommendations

In summary, based upon the results of our investigations and the assumptions outlined above, it is recommended that:

- a dedicated right turn pocket from Old Wallgrove Road into the Transgrid site be constructed as part of the upgrade of Old Wallgrove Road;
- a second right turn lane from Old Wallgrove Road to Erskine Park Link Road be provided when the fourth (northern) approach is constructed; and

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 the intersection of Old Wallgrove Road / Millner Avenue be signalised as part of the upgrade of Old Wallgrove Road.

Please contact the undersigned should you have any queries or require any further information regarding the above.

Yours faithfully,

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Anne Coutts Senior Engineer

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Attachment 1



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Attachment 2





Attachment 5 Draft Program

Civil Engineers & Project Managers





Attachment 6 SSDA Drawings

Civil Engineers & Project Managers










































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