

9 July 2013

Lend Lease Developments 30 The Bond, 30 Hickson Road, Miller's Point, NSW 2000

Attention: James Hammill

Dear James.

RE: Supplementary Monitoring & Assessment Works - The Haymarket, Sydney

1. Introduction

Coffey Environments Australia Pty Ltd (Coffey) was commissioned by Lend Lease Development (LLD) to carry out additional groundwater and surface water monitoring in relation to the proposed redevelopment of the Haymarket, Sydney. Specifically, these monitoring works aim to gather data to assess whether groundwater encountered during the proposed redevelopment of the site could be discharged to local sewer connection or existing stormwater conduits that drain to Cockle Bay. Coffey was also appointed to carry out a preliminary dewatering appraisal to estimate the inflow of water anticipated during a possible localised construction excavation.

The scope of the monitoring and assessment works has been developed in response to comments made by the Environment Protection Authority (EPA) in their letter addressed to the Department of Planning and Infrastructure dated 10th May 2013 following a review of information submitted within LLD's Stage 1 Development Application (DA) for the redevelopment of the Haymarket Precinct.

Details of the planned assessment are provided in Coffey's proposal dated 27th May 2013 (ref: ENAURHOD04498AA-P07).

2. Proposed Development

LLD, on behalf of Darling Harbour Live, has applied for planning approval for development of the Haymarket Precinct for a mixture of residential and commercial uses with surrounding public realm having managed landscaped and paved areas. No basements are proposed as part of this development. As such, extensive construction dewatering is not anticipated during construction. However, localised elements of the development, such as service shafts and utilities, may require temporary dewatering during construction. Due to the design adopted, LLD do not anticipate any ongoing groundwater monitoring or management.

The proposed development will be constructed in a number of stages. As such, the anticipated peak volume of water abstracted from construction excavations at any one time would be less than if the development was constructed in a single stage.

At present, the following options are available to manage groundwater extracted from construction excavations:

Coffey Environments Australia Pty Ltd ABN 65 140 765 Level 19, Tower B, Citadel Tower 799 Pacific Highway Chatswood NSW 2067 Australia T +61 2 9406 1000 F +61 2 9406 1002 coffey.com

- temporary storage, transport and disposal offsite at a licensed liquid waste facility;
- on-site treatment and discharge to Cockle Bay via stormwater drains; or
- on site treatment and discharge to sewer connection.

As the site development is likely to occur in stages, one of the above options may be preferred for a particular stage of the project due to change in disposal quantity and access to means of disposal. For these reasons, LLD has not selected a preferred water management option, or specific discharge location. Selection of the most appropriate groundwater management treatment options will be determined and approved in accordance with the regulatory requirements as part of the detailed construction planning process.

3. Objectives

The objectives of additional groundwater and surface water monitoring were:

- a) Present an assessment of water quality conditions in Cockle Bay relative to the Guidelines for Fresh and Marine Water Quality and the Marine Water Quality Objectives for NSW Ocean Waters;
- b) Provide an assessment of the suitability of groundwater for discharge either to sewer under a trade waste agreement or to Cockle Bay via local stormwater drainage. This assessment would consider available groundwater data, and data collected during this assessment;
- c) Comment on whether treatment of groundwater would be required prior to discharge either to sewer or to stormwater drain;
- d) Outline recommendations for monitoring to periodically check that groundwater discharges meet quality limits relevant for discharges to Cockle Bay or local sewer connection; and
- e) Assess potential water inflows expected during possible localised construction excavation as part of the proposed redevelopment of the site.

4. Site Description

The site is located within the Haymarket district of Sydney's Central Business District and comprises the Sydney Entertainment Centre (SEC), associated car park and surrounding public realm. The location of the site is shown in Figure 1.

The site occupies an area of approximately 3.7ha and is generally bound by Pier Street and the off-ramp linking Pier Street and Darling Drive to the north. Hay Street forms the southern boundary to the site. The light rail corridor forms the west and Harbour Street to the east. The boundaries of the site are shown in Figure 2.

The site historically formed a part of Long Cove, a watercourse which extended generally north-south through the site. Much of the central parts of the site remained submerged until c.1860 where large scale land reclamation took place to establish railway and marine port infrastructure to the north of the site.

5. Review of Hydrogeological Conditions

Published geological records indicate the fill material overlies Quaternary-aged alluvium, which comprises gravel, sand, silt and clay deposits. Fill materials comprised heterogeneous mixtures of gravelly sand, sandy gravel, gravelly clay, clay and sandy clay/silt. The thickness of fill materials recorded within the site was variable ranging between 0.4m and 5.0m below ground surface (mbgs), with the thickness of fill materials increasing along the Long Cove paelochannel. The alluvial deposits are underlain by residual soil and rock of Triassic-aged Hawkesbury Sandstone Formation which comprises sandstone, quartz and shale. The sandstone bedrock beneath the SEC is intersected by the Great Sydney Dyke, which

comprises a dolerite intrusion through the sandstone. The dyke is orientated in a southeast-northwest direction through the southern part of the site (Coffey, August 2011a).

Recent ground investigations (Coffey, January 2013) recorded groundwater strikes at depths 2.4mbgs (BH120) to 3.0mbgs (BH118, BH127) which coincided predominantly with the upper alluvial deposits.

Coffey (August 2011a) reported that groundwater flows in a northerly direction towards Cockle Bay. Standing groundwater levels were recorded in MW120 using a data logger to assess the influence on tidal fluctuations (Coffey, January 2013). Groundwater levels measured over a 5 day period ranged between 0.751m and 0.788m Australian Height Datum (AHD), which suggests that tidal fluctuations have negligible influence on groundwater levels within the site.

No water bodies are located within the site. Cockle Bay is the nearest surface water feature and is located approximately 475m to the north. Coffey (June 2012b) notes that there are a number of artificial water features within land surrounding the site (e.g. Sydney Chinese Garden of Friendship site). It is understood these water bodies are tanked structures which are hydraulically separated from the underlying groundwater.

6. Review of Stormwater & Sewer Drainage Plans

The site is served by an established sewer and stormwater drainage network. Plans showing the location of this existing infrastructure are provided in Appendix A. These records indicate that stormwater from the site is channelled towards Cockle Bay via two separate conduits which pass through the site. The discharge locations shown in Hyder Consulting Drawing SKC013 (Rev. 02) (refer Appendix A) was used to determine the surface water sampling locations at the southern end of Cockle Bay.

7. Fieldwork & Laboratory Analysis

Investigation works for this assessment occurred on 20th and 21st June 2013 and included:

- Rising/falling head tests on two ground water monitoring wells (CBH9/MW9 and NBH/MW25) to estimate the hydraulic conductivity of the aguifer;
- Groundwater sampling from existing nine (9) groundwater wells installed within, or immediately
 adjacent to the Haymarket site. The groundwater wells sampled included BH1, CBH/MW6, CBH/MW9,
 BH12, BH13, NBH/MW25, NBH/MW30, BH120 and BH124. The location of these groundwater wells is
 shown in Figure 3; and
- Surface water sampling at three separate locations from Cockle Bay, including two locations at the
 southern end of Cockle Bay (SW1 and SW2) at existing stormwater discharge points, and one
 reference sampling point (SW3) located at the Pyrmont Bay Ferry Wharf. The surface water sampling
 locations are shown in Figure 4. Both a primary and field duplicate sample was collected from each
 sampling location to assess potential variability in chemical concentrations.

Groundwater and surface water sampling methodologies used in this assessment are presented in Appendix B.

- Groundwater and surface water samples were submitted for analysis at Eurofins MGT laboratory who
 hold NATA accreditation for the analyses scheduled. Groundwater samples were analysed for:
 - i) Total Petroleum Hydrocarbons (TPH)
 - ii) Benzene, Toluene, Ethylbenzene and Xylene (BTEX)
 - iii) Polycyclic Aromatic Hydrocarbons (PAH)
 - iv) Heavy metals including arsenic, cadmium, chromium (total), copper, iron, lead, manganese, mercury, nickel and zinc.

- v) Major anions (nitrate, chloride, and sulphate) and cations (sodium, calcium, magnesium and potassium), ammonia and alkalinity
- Surface water samples were analysed for the above parameters with the exception of major anions and cations, and alkalinity;
- Laboratory analytical results are summarised in tables presented in Appendix E. Laboratory analytical certificates are presented in Appendix F; and
- The following field Quality Control (QC) measures were employed during the sampling event:
 - i) Collection and analysis of one blind duplicate sample (DUP1). A primary and blind duplicate sample was collected from MW25.
 - ii) Collection and analysis of one equipment rinsate sample (WB). The equipment rinsate sample was collected by pouring deionised water over the IP meter following decontamination (refer Appendix B).
 - iii) Inclusion and analysis of one laboratory prepared trip blank (TB) and trip spike sample (TS).
 - iv) Samples were collected in laboratory provided containers and transported to the laboratory under Chain of Custody control.

Field QC data is presented in Tables 5 and 6 in Appendix E. An appraisal of the QC procedures adopted for this assessment is presented within Appendix G.

8. Discussion of Results

8.1 Water Quality Assessment Criteria

Discussion of selection of water quality assessment criteria is provided in Appendix D and values are included in data summary tables where appropriate.

8.2 Assessment of Surface Water Quality

With reference to the visual amenity objectives set out within Marine Water Quality Objectives for NSW Ocean Waters, the following was noted during the collection of the surface water samples:

- No visual or olfactory indications of chemical contamination were observed during the collection of surface water samples at any of the sampling locations;
- Floating debris occurred at the three sampling locations. Debris included general rubbish items (e.g. food wrappers, drink containers etc.) but were not present on a widespread basis; and
- Evidence of nuisance organisms (e.g. phytoplankton scums, filamentous algal mats, blue-green algae, and sewage fungus etc.) was not observed at any of the sampling locations.

Analytical results from the six surface water samples collected from Cockle Bay were compared against the trigger values for the protection of marine water species (refer Table 4, Appendix E). In summary, the following was noted:

- The water quality reported within samples collected at the southern end of Cockle Bay were generally comparable to the samples collected at the reference sampling point (SW3) located at the Pyrmont Bay Ferry Wharf;
- Concentrations of TPH, BTEX and PAH compounds were reported below the LOR in all samples collected:
- Concentrations of arsenic, cadmium, chromium, iron, lead, manganese and nickel were reported below the LOR in all samples collected;

- Concentrations of copper were reported above the assessment criterion in one sample (SW2B; 0.005mg/L) collected from the southern end of Cockle Bay. It is noted that both samples collected from the reference sampling location (SW3A and SW3B; both reported a concentration of 0.006mg/L) also reported concentrations of copper above the assessment criterion; and
- Concentrations of mercury were reported in one sample collected from the southern end of Cockle Bay (SW1A; 0.0002mg/L). All other samples reported concentrations below the laboratory limit of reporting (LOR).

In summary, the findings of the surface water quality assessment are considered to be indicative of a modified and highly trafficked marine environment. The analytical results of samples collected from Cockle Bay suggest that chemical quality of this water body generally meets the trigger levels for the protection of marine aquatic species as set out within ANZECC (2000). The presence of heavy metals such as copper and mercury may be attributable to antifouling measures applied to older ships and other marine structures, and/or derived from runoff from the urban environment which surrounds Cockle Bay, rather than a specific point source. With reference to the visual amenity criteria set out within the Marine Water Quality Objectives for NSW Ocean Waters, it is assessed that Cockle Bay generally meet these criteria although the presence of occasional floating debris was observed during sampling.

8.3 Assessment of Groundwater Quality – Discharge to Stormwater System

Analysis of groundwater samples collected from across the site indicates a pH neutral, brackish to saline environment which is consistent with historical reclamation of the land and with the proximity of the site to Cockle Bay.

A review of the proportion of major cations and anions within groundwater samples collected from the site indicates that the chemistry of groundwater within the central part of the site (i.e. those areas that were historically reclaimed) considerably different to that along the periphery of the site. The dominant ions present within samples collected from the central parts of the site are sodium and chloride, which is likely to be associated with the former Long Cove channel that historically dissected the site.

The ion balance is presented in Table 3 in Appendix E, and is illustrated graphically in Figure A

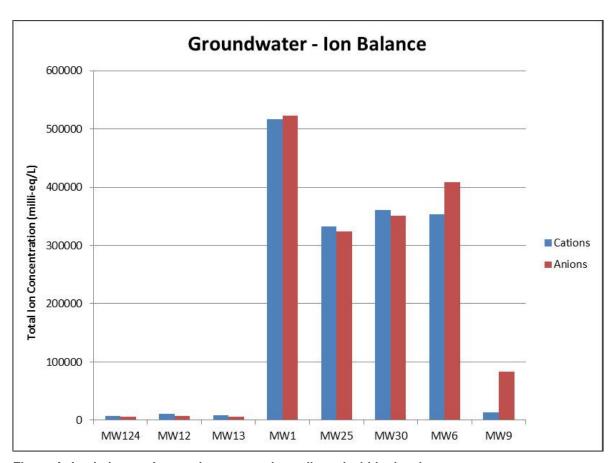


Figure A: Ion balance of groundwater samples collected within the site.

Groundwater samples have been collected from the site over five separate rounds although not all wells were sampled during each round. Groundwater analytical data collected from previous and the most recent sampling events are presented in Table 1 in Appendix E. This data has been compared to the trigger values for the protection of marine water species set within ANZECC (2000). In summary, the results indicated:

- No Phase Separated Hydrocarbon (PSH) was observed in any of the monitoring wells;
- Concentrations of PAH were reported below the LOR in all samples collected during the most recent
 event. Concentrations of PAH compounds were identified above the LOR in groundwater samples from
 MW9, MW25, MW30 during a previous sampling event. Analysis of filtered duplicate samples indicated
 that the reported PAH compounds were attributable to the inclusion of fine suspended sediment rather
 than dissolved within the groundwater itself (Coffey; Jan 2013);
- Compounds including BTEX, VOC and SVOC were reported below the LOR in all samples;
- TPH C₆-C₉ was identified in one groundwater sample from MW120 at 30μg/L which is slightly above the LOR (20μg/L). On review of the soil results, TPH C₆-C₉ and other indicator compounds such as Benzene, Toluene, Ethylbenzene, Xylene were not recorded above the LOR in any of the seven soil samples from this borehole (Coffey, Jan 2013). Furthermore, soil headspace measurements ranged from 0.9ppm to 10ppm suggesting a low likelihood that volatile hydrocarbons are present within the soil at this location. TPH C₆-C₉ was not reported above the LOR in groundwater samples collected during the June 2013 sampling event;

- TPH C₁₀-C₁₄ and C₁₅-C₂₈ were reported at concentrations less than the LOR with exception for the groundwater sample collected from MW124 during June 2013 sampling event. Concentrations of TPH C₁₀-C₁₄ and C₁₅-C₂₈ where reported at 80μg/L and 200μg/L respectively which is slightly above the LOR. During the previous sampling round, insufficient water was present to collect a representative sample from this well. Soil data (Coffey Jan 2013) from this position indicates that TPH C₁₀-C₁₄ and C₁₅-C₂₈ compounds were reported at depths between 2.9m and 4.8m below ground surface (mbgs), which may be the source of TPH impact to groundwater reported at this location;
- Arsenic, copper, chromium, lead, zinc were reported at concentrations above the assessment criteria in a number of samples. It is noted that arsenic, copper and zinc were reported at concentrations exceeding the assessment criteria in at least one sample from each of the previous groundwater monitoring events, where metals were scheduled for analysis;
- Concentrations of iron were reported above the aesthetic assessment criterion in one sample (MW124; 3.6mg/L) of the eight samples submitted for analysis. It is noted that pH of the groundwater sample recovered from MW124 was slightly acidic (6.31) which may promote the release of iron from the underlying sandstone;
- Manganese was reported at concentrations exceeding the assessment criterion in four samples (MW124, MW13, MW6, MW25) of the eight submitted for analysis; and
- Concentrations of ammonia were reported above the adopted assessment criteria in six of the eight samples submitted for analysis. Groundwater samples collected during previous events were not analysed for ammonia. The presence of ammonia in groundwater may derive from the degradation of organic materials within the naturally occurring alluvial sediment within an anaerobic environment, or leaking sewer pipes which is not uncommon with older infrastructure, particularly where land has been reclaimed.

In summary, it is assessed that the direct discharge to Cockle Bay of groundwater abstracted from excavations during construction would contribute to the existing contaminant load within Cockle Bay. In consideration of the magnitude of chemical concentrations detected in the majority of groundwater samples, and the dilution potential of receiving stormwater and that of Cockle Bay itself, it is assessed that any increases in chemical concentrations would generally be below the limits of detection. However, detailed assessment would be required where excavation dewatering is proposed in areas of the site where elevated concentrations of certain chemical stressors have been reported; namely MW124 (TPH, iron and ammonia), MW1 (copper and zinc) and MW9 (Ammonia). This assessment would form part of the detailed construction management planning process for each stage of the proposed development.

As well as possible chemical stressors, groundwater abstracted from excavations at the site is likely to include suspended solids. Direct discharge of sediment laden groundwater to stormwater drains that discharge to Cockle Bay would almost certainly generate visual sediment 'plumes' which would be aesthetically unacceptable. It is noted that a proportion of the chemical constituents reported within groundwater readily adsorb to sediment, which may lead to further concentration of certain chemical constituents in areas surrounding the existing stormwater outfalls.

8.4 Assessment of Groundwater Quality – Discharge to Sewer

Available groundwater analytical results were compared to the chemical acceptance standards set out within Sydney Water's *Acceptance Standards and Charging Rates for 2013–14 – Industrial Customers*. The output of this comparison is summarised in Table 2, Appendix E. In summary, the following is noted:

 All chemical constituents were reported below the chemical acceptance standards set by Sydney Water; and With reference to available laboratory data and electrical conductivity measurements during the
collection of groundwater samples, it is assessed that the concentrations of Total Dissolved Solids
(TDS) reported in samples collected from MW1, MW25, MW30, MW6 and MW9 exceed the allowable
level stipulated by Sydney Water. In consideration of the setting of the site, it assessed that the TDS
load is primarily due to the presence of marine salts. Samples collected from MW124, MW12 and
MW13 report a TDS less than the limit stipulated by Sydney Water.

8.5 Requirements for Treatment

On the basis of groundwater analytical data available for the site, it is assessed that groundwater abstracted from excavations within the site during construction would not be suitable for direct discharge to existing stormwater drainage or local sewer connection without some prior treatment which would depend on the location of dewatering.

Groundwater abstracted from excavations during construction is likely to have high levels of suspended solids and treatment would be required to reduce the sediment load prior to discharge from site. However, where discharge to sewer is proposed, the extent of treatment for suspended solids required would be less than that required for discharge to stormwater drainage system.

Treatment of suspended solids within groundwater would typically be achieved through primary sedimentation and filtration processes. However, further appraisal of the settleable characteristics of the sediment would be required to determine if flocculation is necessary, particularly where discharge to the stormwater system is proposed. This appraisal would form part of the detailed construction management planning process for each stage of the proposed development.

As noted in Section 2, several options to manage groundwater extracted from construction excavations are available. The selection of a specific management option and discharge location would depend on factors including the staging of site development, requirements for dewatering during that particular stage and the quality of water likely to be encountered as part of proposed works. A specific management option and discharge location, quantities and programme would be provided with any application for consent to discharge to the existing stormwater or sewer network.

8.6 Recommendations for Water Monitoring During the Construction Phase

Discharge of treated groundwater to either stormwater or sewer connections would require consent prior to discharge. Coffey understands that Sydney Water and the City of Sydney (in consultation with the NSW EPA) would be the consent authority for discharging groundwater to sewer and stormwater network respectively. The conditions of this consent would stipulate the minimum requirements for monitoring.

At this stage, based on the known site history, monitoring of treated groundwater is likely to include:

- pH;
- Suspended and Total Dissolved Solids;
- Heavy metals including arsenic, cadmium, chromium, copper, iron, lead, nickel, manganese, mercury and zinc;
- Inorganics including ammonia, nitrate, sulphide and sulphite; and
- Petroleum Hydrocarbons (TPH, BTEX and PAH)

In addition to the above, it is assessed that discharge rates would also need to be monitored and recorded.

8.7 Preliminary Dewatering Appraisal

8.7.1 Overview

Coffey understands that the proposed development does not include basements or other structures of substantial area below the groundwater level. Hence, extensive construction dewatering will not be required. However, elements of the development may require localised dewatering. These elements could include:

- Trenches for drainage and sewer works;
- Lift pits associated with new tower structures;
- Water retention structures as part of WSUD initiatives; and
- · Grease traps for trade waste generated from retail uses.

It is understood that these elements will be tanked and will not experience groundwater inflow/seepage during operation. However, these elements may require temporary localised dewatering during construction.

Coffey understands that design of the above listed elements is currently incomplete and details on the likely location and geometry of such structures are currently unavailable. Furthermore, construction programme information is not available. As such, it is not possible to reliably estimate the volume of water expected to be discharged, or the frequency of any discharges during construction at this stage. However, data from the rising/falling head tests carried out have been used to estimate groundwater inflow/seepage rates anticipated within typical excavations likely to be constructed on site during the proposed redevelopment. These inflow rates may be used to develop volume estimates associated with excavation dewatering.

8.7.2 Rising/Falling Head Test

To estimate the hydraulic conductivity of the aquifer, rising/falling head test has been carried out on groundwater monitoring wells CBH9/MW9 and NBH/MW25. Testing involved introduction of a plastic tube filled with sand into the borehole. This displaced water causing a temporary water level rise. The water level gradually recovered and the recovery was monitored using a pressure transducer and a data logger (a falling head test). Once the water level had recovered, the plastic tube was removed resulting in a temporary reduction in water level in the borehole. The water level gradually recovered and the gradual rise was monitored using a pressure transducer and data logger (a rising head test). A Solinst 'Levellogger' data logger (Serial No. 10175958) was used to measure changes in water levels during the rising and falling head tests.

The results of the rising and falling head tests were analysed using the methods developed Hvorslev (1951) were used to assess the hydraulic conductivity of materials adjacent to the borehole screen.

Analysis involves matching a straight-line solution to water-level displacement data collected during the test. The results of this assessment are presented in Figures 1 to 4 in Appendix H, and summarised in Table 8.1 below.

Table 8.1 – Hydraulic Conductivity Assessment from of Falling and Rising Head Tests

Borehole	Falling Head Test Result (m/d)	Rising Head Test Result (m/d)
CBH/MW9	0.06	0.07
NBH/MW25	0.18	0.11

Results for NBH/MW25 indicated higher permeability than that reported for CBH9/MW9. Falling and rising head test results reflect only a small volume of material surrounding a borehole as a result they may not be representative of the material properties over the site.

8.7.3 Assessment of Groundwater Inflow Rates during Construction

Elements of the development noted in Section 8.7.1 that may require dewatering during construction above fall within two broad categories:

- i) Narrow longitudinal excavations where one side of the excavation area is significantly longer than the other, such as trenches for drainage/sewer lines; and
- ii) Rectangular excavations, such as for lift pits and water retention (tank) structures.

Therefore, a preliminary assessment of the likely groundwater inflow during construction to two types of excavation has been presented in this section. A longitudinal excavation running north-south across the site (representative of trench excavation for drainage/sewer construction) and rectangular excavations (representative of excavation for lift pits, stair bases, grease traps, or other water retention structures).

The assessment was made using analytical methods assuming radial flow to rectangular excavations and parallel flow to linear excavations (trenches).

For the purpose of these assessments the following assumptions were made:

- Groundwater level is 2.4m below ground (based on site measurements);
- Hydraulic conductivity of fill is 0.2m/d (i.e. upper end of falling/rising head test results);
- Excavation of pits will be constructed no more than 2m below the groundwater level and excavation of trenches no more than 1m below groundwater level;
- Low permeability rock at a depth of 10m below ground level (typical value from earlier field studies);
 and
- No high permeability features such as gravel filled trenches intersect excavations below the water table.

Based on these assumptions it is assessed that inflow to individual open pits of up to 5m x 10m would be unlikely to exceed 0.2L/s and inflows to trenches would be unlikely to exceed 0.5L/s per 100m length of trench. Inflows would be greatest immediately following excavation and would reduce over time as the extent of influence gradually increases.

Should materials different from those anticipated for this assessment be encountered in subsequent investigations or during excavation it is recommended that further advice be obtained.

It is noted that this advice does not address stability of open excavations. Coffey recommends that specific geotechnical advice should be obtained in relation to shoring or battering of excavations deeper than 1.5m, or excavations below the groundwater table.

9. Limitations

Coffey notes that subsurface conditions are inherently variable both with location horizontally and vertically and over time. It is impractical to assess conditions at every location on a site and Coffey has used professional judgement of suitably qualified and experienced staff to provide an interpretation of conditions across the site.

The reader is directed to "Important Information About your Coffey Environmental Report", which is attached to this text.

10. Closure

We trust the assessment outlined herein meets your immediate requirements. If you do have any further queries, please do not hesitate to contact us.

The attached document entitled "Important Information about your Coffey Report" presents additional information about the uses and limitations of this report.

Yours sincerely,

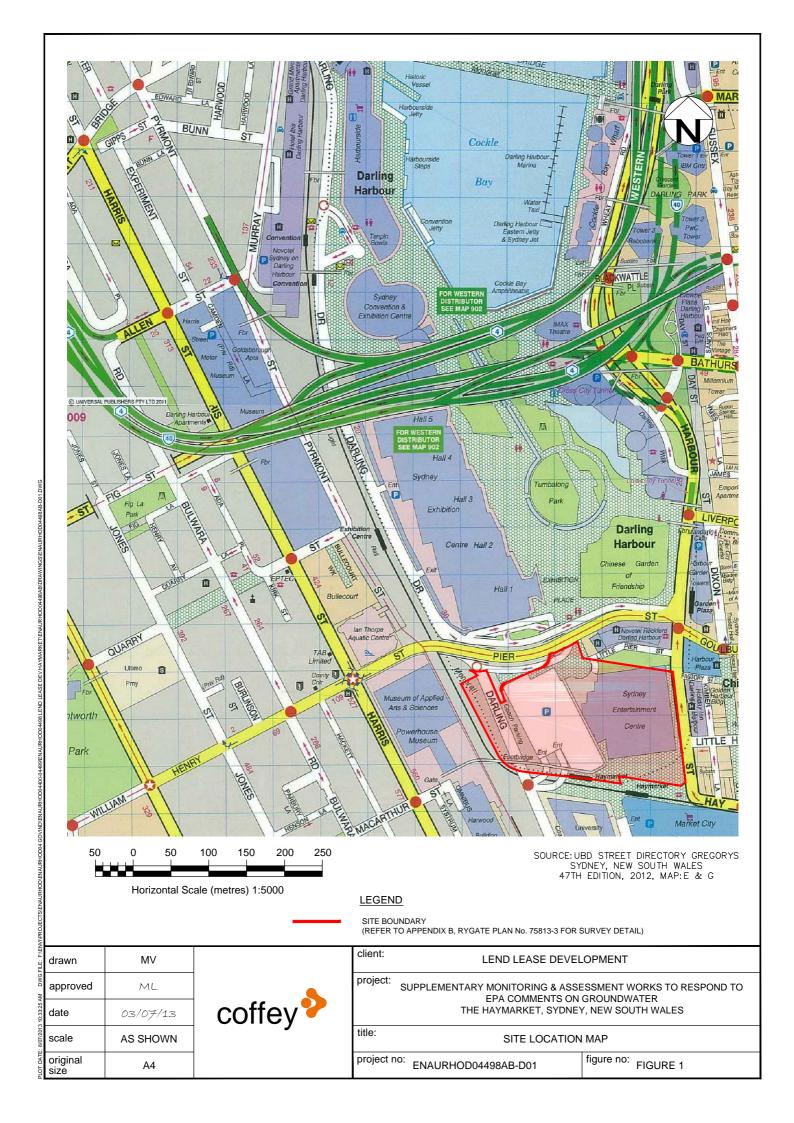
Matthew Locke Senior Associate Michael Dunbavan Senior Principal

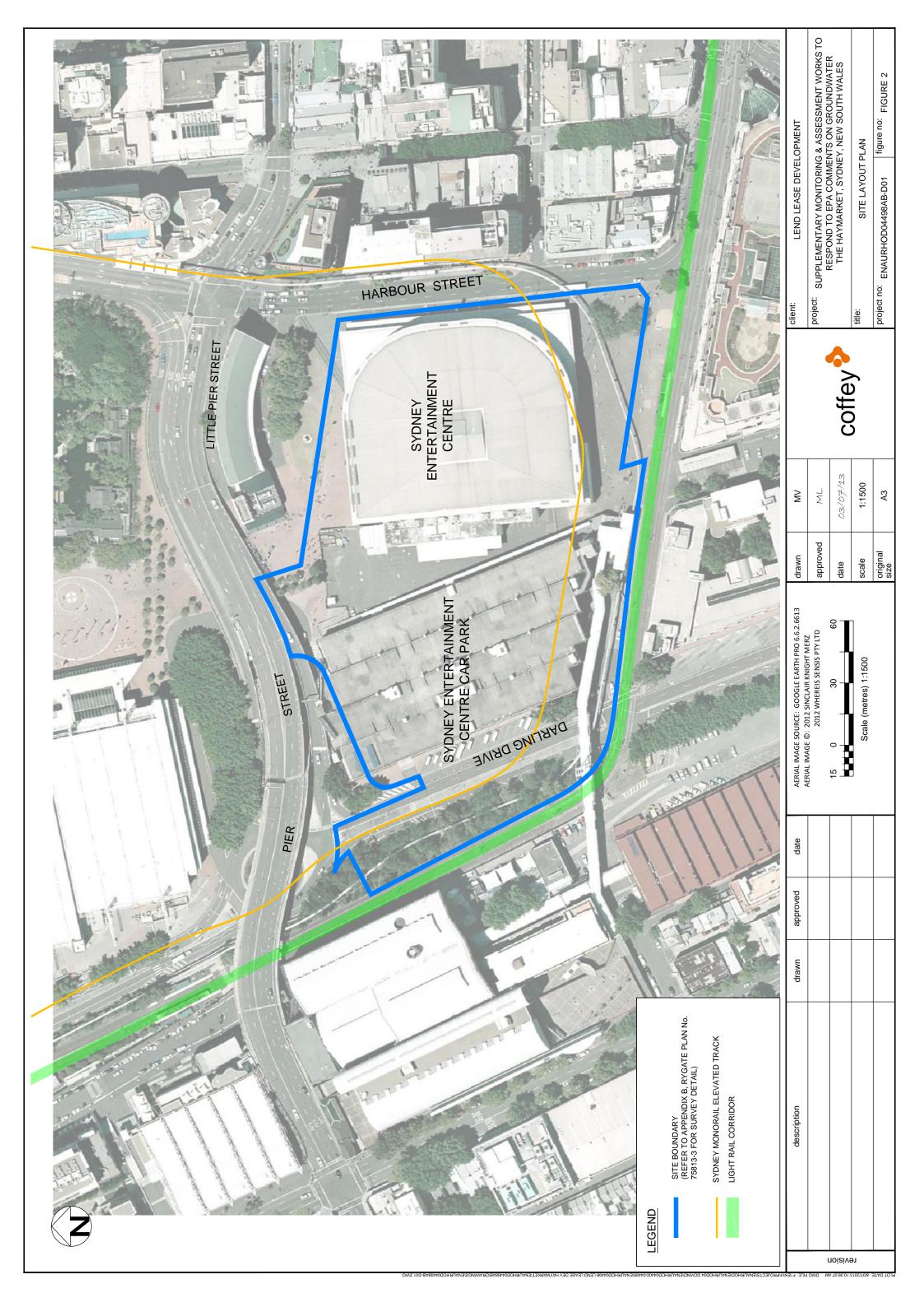
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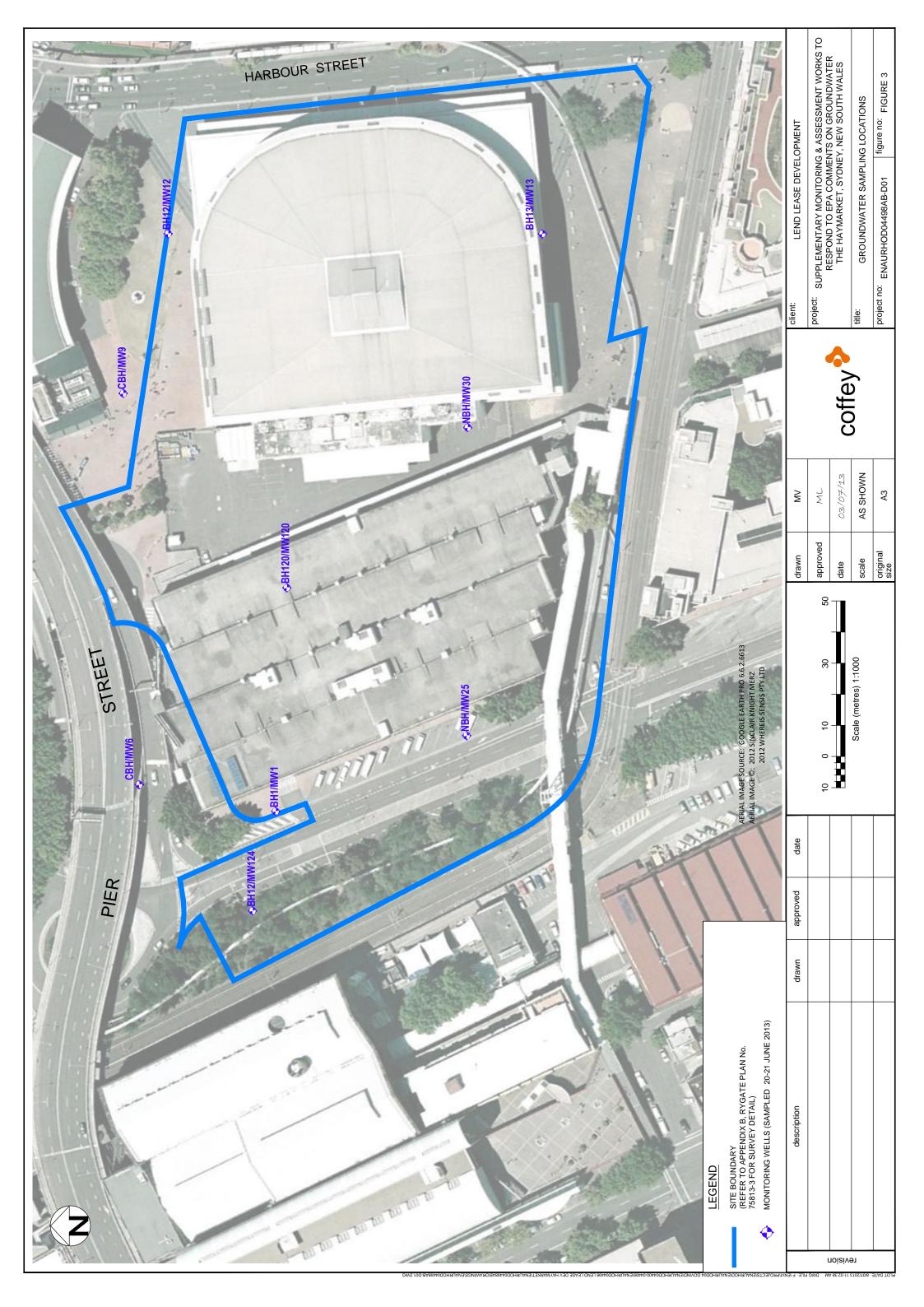
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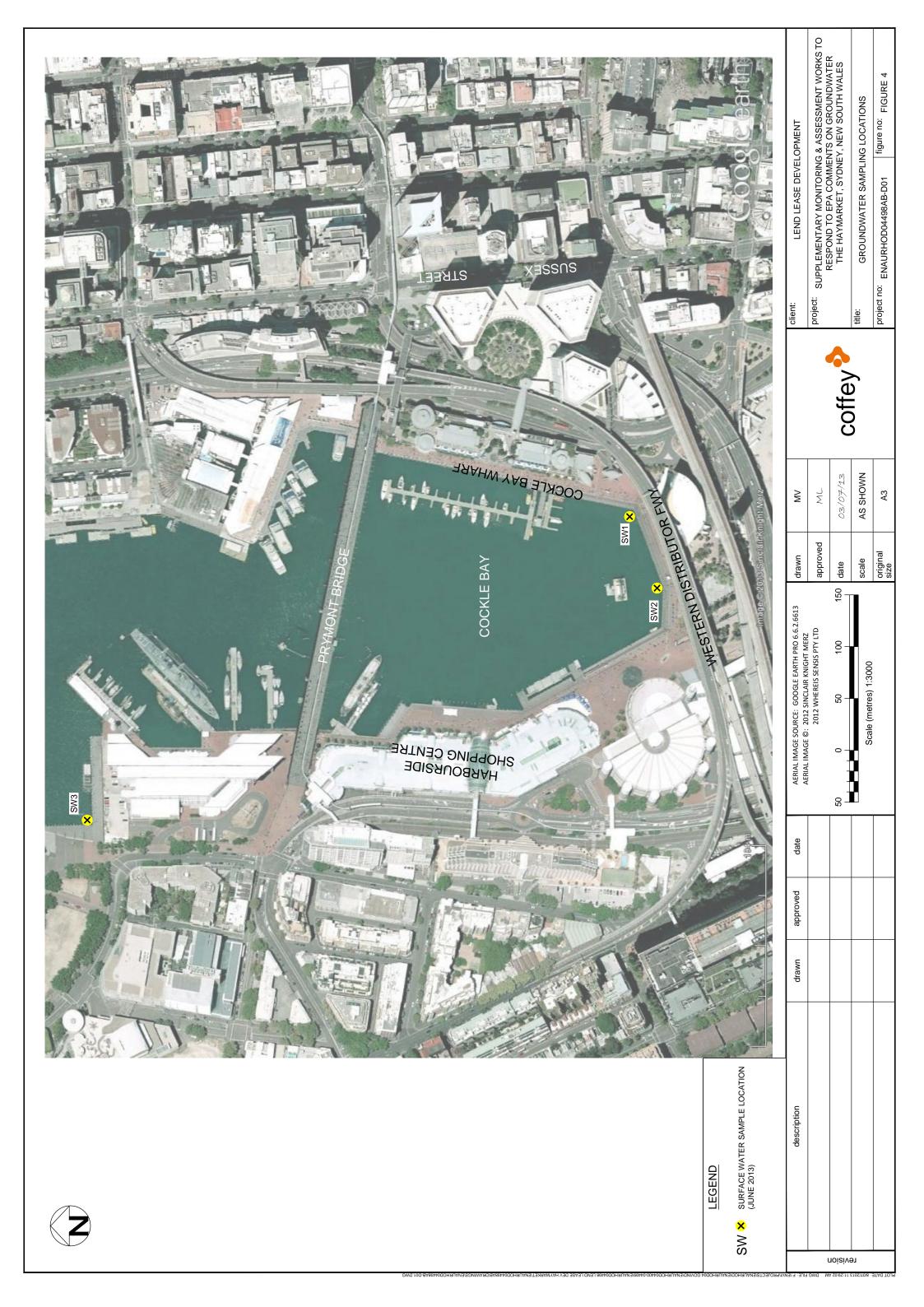
Important Information about your Coffey Report

FIGURES









REFERENCES

Information from the following reports was used to prepare this assessment:

- Coffey Geotechnics (July 2011); Environmental Desk Study: Proposed Sydney International Convention and Entertainment Centre, Darling Harbour prepared for SHFA.
- Coffey Geotechnics (August 2011a) *Geotechnical Investigation Report: Proposed Sydney International Convention and Entertainment Centre, Darling Harbour* prepared for SHFA.
- Coffey Geotechnics (August 2011b); Contamination Investigation, Sydney International Convention and Entertainment Centre prepared for SHFA.
- Coffey Geotechnics (May 2012); Geotechnical Investigation Report: Proposed Sydney International Convention Exhibition and Entertainment Precinct (SICEEP), Darling Harbour, Sydney prepared for INSW.
- Coffey Geotechnics (June 2012a); Stage 1 Preliminary Environmental Investigation, Sydney International Conference Exhibition and Entertainment Precinct (SICEEP), Darling Harbour, Sydney prepared for INSW.
- Coffey Geotechnics (June 2012b); Stage 2 Detailed Site Investigation: Sydney International Convention Exhibition and Entertainment Precinct (SICEEP), Darling Harbour, Sydney prepared for INSW.
- Coffey Geotechnics (August 2012); Supplementary Site Investigation: Sydney International Convention Exhibition and Entertainment Precinct (SICEEP), Darling Harbour, Sydney prepared for INSW.
- Coffey Geotechnics (January 2013); Supplementary Site Investigation: Factual Report, Sydney International Convention Exhibition and Entertainment Precinct (SICEEP), Darling Harbour prepared for INSW.
- Coffey Environments (February, 2013); Site Investigation Factual Report: Haymarket Precinct, Darling Harbour, Sydney, NSW prepared for INSW.
- Coffey Environments (March 2013); Overarching Remedial Action Plan: Haymarket Precinct, Darling Harbour, Sydney, NSW prepared for LLD.
- Coffey Environments (June 2013); Site Specific Remedial Action Plan for the Haymarket Planning Application, Haymarket, Sydney, NSW prepared for LLD.

APPENDIX A

PLANS SHOWING THE LOCATION OF EXISTING SEWER AND STORMWATER INFRASTRUCTURE



AFCINCT EXISTING STORMWATER



APPENDIX B

GROUNDWATER AND SURFACE WATER SAMPLING METHODOLOGY

B.1 GROUNDWATER SAMPLING METHODOLOGY

Groundwater monitoring wells were sampled by appropriately quality environmental scientists in general accordance with the methodology outlined in Table B.1.

Table B.1: Groundwater Sampling Methodology

Activity	Detail / Comments
Groundwater Level & LNAPL Measurements	Groundwater levels and the apparent thickness of any Light Non Aqueous Phase Liquids (LNAPL) were measured using an oil/water interface probe (IP).
Well Purging	Well purging was undertaken in accordance with Coffey Standard Operating Procedure (SOP) using a peristaltic (low-flow) pump with disposal tubing for each well. During purging, groundwater was monitored for pH, Temperature, Dissolved Oxygen, Electrical Conductivity and Redox Potential.
	In general each well was purged to remove a minimum of three equipment volumes (i.e. volume of sample tubing and flow-through cell) and/or stabilisation of the above water quality parameters (i.e +/- 10%). The following specific comments are noted with regard to well purging:
	 MW120 was purged dry after the removal of 0.4L. Insufficient water volume to measure post-purge water quality parameters.
	 MW124 was purged dry after the removal of 1L groundwater. Insufficient water volume to measure post-purge water quality parameters.
	Groundwater samples were collected from MW120 and MW124 approximately 24hours after well purging.
Sampling Method	In general, groundwater samples were collected following the stabilisation of groundwater quality parameters. Groundwater samples were recovered from each of the monitoring wells using low flow sampling with a peristaltic pump in accordance with Coffey SOP.
	Due to the poor recharge in MW120, it was not possible to collect sufficient groundwater volume for the full suite of chemical parameters. Samples collected from MW120 were analysed for metals and BTEX compounds.
	Groundwater sampling records are provided in Appendix C.
Sample Splitting	A blind duplicate sample (DUP1) was collected from MW25 by filling up two sample containers from the same low flow tubing.
Decontamination Procedure	The IP was decontaminated by scrubbing with Decon 90 solution and rinsed with deionised water between wells.
Sample Preservation	Samples were placed in laboratory supplied bottles containing appropriate preservatives and were filled to minimise headspace.
	Groundwater samples collected for metals were filtered using disposable 0.45µm filter packs. Sample containers were immediately capped and placed in an insulated container filled ice. The samples were dispatched to a NATA accredited laboratory under chain of custody control.

B.2 SURFACE WATER SAMPLING METHODOLOGY

Surface water samples were collected by appropriately quality environmental scientists in general accordance with the methodology outlined in Table B.2.

Table B.2: Surface Water Sampling Methodology

Activity **Detail / Comments** Surface water samples were collected from three sampling locations shown in Figure 4 Sampling Method using a dedicated long handled Swing Sampler. The pivoting head of the Swing Sampler was fixed so that the sampling bottle was in parallel with the sampler handle. The sample bottle was secured using elastic bands and masking tape. An indicator mark 1m above the top of sample container was made on the extendable handle of the Swing Sampler so that water samples were collected at practically the same depth. A small piece of plastic film was placed over the top of the open sample bottle and secured with an elastic band (refer Picture (a)). The elastic band was attached to a separate length of cord which was held by the environmental scientist carrying out the sampling. Once the plastic cover was in place, the sample bottle was lowered to a depth of approximately 1m below the surface of the water (refer Picture (b)). At the sampling depth, the cord was pulled, which dislodged the plastic film allowing water to enter the sampling bottle (refer Picture (c)). (a) (b) (c) easured from a sample of the water brought to surface. Surface water sampling records are provided in Appendix C. A primary and field duplicate sample was collected from each sampling location to assess chemical variability between samples. These samples are denoted with the suffix 'A' and 'B'. Each sample was collected using separate laboratory supplied bottles. No sample splitting was carried out. A new piece of plastic film was used when collecting

Activity	Detail / Comments
	each sample.
Sample Preservation & Decontamination	Samples were placed in 1L unpreserved laboratory supplied bottles and were filled to minimise headspace. A new sample container was used to collect each sample. As such, no decontamination of sampling equipment was considered necessary. Each sample bottle was capped and placed in an insulated container filled ice. The samples were dispatched to a NATA accredited laboratory under chain of custody control.

APPENDIX C

GROUNDWATER & SURFACE WATER SAMPLING RECORDS

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Well Gauging Form

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				,				
PROJECT NAME:	5	I	Haymarket		PROJECT	PROJECT NUMBER:	NAURHODOGH78AB	
FIELD PERSONNEL:	PD /ACM	ACM				DATE:	20/6/13	
PROJECT MANAGER:	35				I			
FIELD EQUIPMENT:					٠	REFER TO SO	PS WHEN GAUGING WELLS:	
Equipment Used: TP Meter	765		IP Serial Number:	Rewtall		SOP - Monitoring Well Gauging	Well Gauging and SOP – Decontamination of Sampling Equipment	
Time of Day Well ID	Well Diameter	Total Well Depth	Depth to PSH (NAPL)	Depth to Groundwater	PSH Thickness	Height of Well Stick-Up	COMMENTS (note 2)	
	•		E	[8]	[B-A]		ODOUR, COLOUR, SHEEN, NAPL (and its colour), REMEDIATION SYSTEM, etc	<i>シ</i> ラ
	mm	Э	MB I OC	mBTOC	mm	3	The state of the s	-
N M A	0.5	5.730	- The second sec	2.270		Augh	well in good consultion. No odour	0 -
+ CININ	= +	5,520	g:hondereq.	5.275	_{api} assip adé n	11	1/	0
MWSS	1	7.278		4.335	or, jegalagyman	11		Ο ()
EI WW 13	3 11	5.734		2.830	-	11	ii ii	0.0
* YW12	2 11	7.684	-	3.402	***************************************	11	Concrete Iruid & in well anthic, around well cap.	0,2
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HW30	0 11	4,346	31216	2.289	LAA	11	Perstante ordering matter (POM) - prayage is saite	o 0
MWG	0 11	5,436	140000000000000000000000000000000000000	2.382	Occumpage and a contract of the contract of th	//	Well in good condution. The order.	0.4
へいい	11	7.170	«суданняй»	4.105	i i vidolaga	1	No odour.	9.2
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S. O.								1/2
*								
Only on Hand Will	50	40.740	100EDicate	21.528	Ladermany	flush	No well cap. Top of casing appears slightly damaged.	300
Entertainment book/Operations augurk over	operations o	ambark ave	Ω.				Well asing slanted	- c
Notes: 1 Indicate in Comm	ents' column if	f méasured Total	Well Depth differs	from log. 2 Do not at	tempt to sniff the n		detect any odours, only note any <u>apparent</u> odour when the well cap is opened	

Gauging Form Well Issue Date: 05/02/2008 UNCONTROLLED WHEN PRINTED

750	1412104		PROJECT N	HNRER.	アスチンやエクプフト FOXAP	20P
IACM!				DATE:	6/13	
35						
•		7	SCREEN INTERVA			STICK-UP: flush mm
Depth to Water - Befo		0		5		PID READING
Ąf	- 1		Ō	**************************************	PPM:	0,2
DEPTH TO DISSOLVED WATER (m) OXYGEN note 2 (mg/l)	ELECTRICAL CONDUCTIVITY (mS or µS/cm)	pH (pH units)	REDOX POTENTIAL (mV)	TEMPERATURE (°C)	CLARITY – tick	id
READING CHANGE*	READING	READING	READING	READING	Cle Sligl Clou	TODOUR, COLLECTED, etc
3.45 ppm	40.8 MS	7.35		N 17.8 0C	7	No odour. Pale grey
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4.455 3.40	40.7	7.34	70	18.5	٢	11 11
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Groundwater Sampling Form (B) - Micro Purge

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			-		7			7 A 37					9 €	. E.	***	1 1 1	らう		
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Groundwater Sampling Form (B) - Micro Purge

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Groundwater Sampling Form (B) - Micro Purge

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JP: flush mm	m below TOC STICK-UP: + US	m be	 	AL:	SCREEN INTERVAL:		WELL DEPTH: 5.734 _m	LL DEPTH	mm WE		DIAMETER:	DIAN	13	MW13	WELL ID:
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Groundwater Sampling Form (B) - Micro Purge

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PROJECT NAME:	PROJECT NAME:	PD	Lease	Hay	Haymarket	ie+		-	PROJE	PROJECT NUMBER:	1	15/13	0044	20/5/12				
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*	~			- 1	2.080	3.070	3.040	2.995	2.896	2.734	2.647	2.380			DEPTH TO WATER (m) note 2			DI	R	r PD	E Land
Z	Z Z	I+ 3	2	g	ب ر	3.84	4.08	2.78	2.54	1, 39	1.93	1.28		READING		Depth to W	FIELD EQUIPMENT	DIAMETER:_		1 ACM	Lease
Unfiltered sa	DUPLICATE ID:	10%			ļ-	,					-acc	Bors		CHANGE	DISSOLVED OXYGEN (mg/l)	<u>Vater</u> - Befor Afte	DIPMENT	0.00		۷	+
Unfiltered samples must not be put into a preserved container (ie, 'metals' bottle)	TE 15:	+		(24.0	34.8	34.1	33.7	34,8	35.4	35.3	34.0		READING	CONDI	<u>Depth to Water</u> - Before Pump Installation: <u>△</u> After Pump Installation: <u></u> <u></u>		_mm v		-	Hay war ket
t be put into a		3%				3		7				SN		CHANGE	ELECTRICAL CONDUCTIVITY (mS or µS/cm)	allation:	٥	VELL DEP1			Ket
preserved cont		+			ا س	7.17	7.10	7.03	25.7	6.8	6.81	6.68		READING	ਓ		2	WELL DEPTH: 4.346			
ainer (ie. 'meta		± 0.1 unit			رر	7		00						3 CHANGE	pH (pH units)	m below TOC		<u>"</u> #			
ls' bottle)	TRIPLICATE	1				-2	8)	56	-0	120	120	128		E* READING	PC			SCREEN INTERVAL:			
	TRIPLICATE COLLECTED:	10mV				*	~	0	2			52		G CHANGE*	REDOX POTENTIAL (mV)	Pump In:		TERVAL:			PROJECT NUMBER:
	Ü	*		_	8.41	8-17	17.8	(8.0	0 t l	17		17.0		READING	TEMPE	Pump Intake Depth:_				DATE:	1
	۲ 	± 0.2°C			80	~	<u>∞</u>). 				000		CHANGE	TEMPERATURE (°C)	· · · · · · · · · · · · · · · · · · ·	2 .	р Б		21/6	ENAURITODO4498AR
	Z				7	7	7	7	5	6					intly CLA		'	m be		113	RHOD
	TRIPLICATE ID:					`		\						Clo	udy T	PID READING PPM: 0	WELL H	m below TOC			440
	, EB										4	1			ery udy rbid	ADING O O	EADSPA	STIC			98A
						11			5	80	No cabor	No a					WELL HEADSPACE PID READING	STICK-UP: Hush			P
							U	1/	odoc:	odenos.	abor.	OR ST		COLL	000		ADING	Hush			
					=	Monard 2/18	Pale Burnge	1)	Section 1995	Signey Constant	abount o	Oidings		COLLECTED, etc	COMMENTS) mm			
								,	ae Inae	e, Irases	POM	No solour. Oldrige logality matter.	,		NTS PSH						
					=	NO POM .	1/1		€ PON	POW]	Γ	Carotic Carotic	<u> </u>			<u> </u>		ŀ			
						andie.						5,									

Groundwater Sampling Form (B) - Micro Purge

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WERE METALS FIELD FILTERED?	DUPLICA	STABILISATION CRITERIA (3 readings within following ranges)							8:30a.M	0		TIME OF F	Meter ID:	Equipment ID:	WELL ID:	PRO.	Ŧ	
ALS FIELI	DUPLICATE COLLECTED:	TION CRIT							Te:	NA		CYCLE/ PUMP RATE (ml/min)	Renda	Reital	MW120	PROJECT MANAGER:	FIELD PERSONNEL:	PROJECT NAME:
FILTERE	ECTED:	ranges)							HOOM)			VOLUME (L) note 1	tal	Hal	20	NAGER:	SONNEL:	T NAME:
	~			Very	(ould	Colle			DRY			DEPTH TO WATER (m) note 2			DI.	ML		Land
Z	z (18 14		2007	5+	of ec		Well	5.67		READING			Depth to	DIAMETER:		PD/ACM) Lease
	7	:10%		7005	collest	MO#		-	7 000		3 CHANGE*	DISSOLVED OXYGEN (mg/l)		FIELD EQUIPMENT Depth to Water - Be	50		-	+_
Unfiltered samples must not be put into a preserved container (ie. 'metals' bottle)	DUPLICATE ID:				+ post	0	C	puwed	S			0	After Pump Installation:	PIELD EQUIPMENT Depth to Water - Before Pump Installation: 2.617	mm		-	Haymow ket
ust not be pu		± 3%		vechou	10	vidls		din	79 4		READING	ELECTRICAL CONDUCTIVITY (mS or µS/cm)	Installatio	o Installatio	WELL			wket
ıt into a presi				Jage J	Juge	+ 5		<u>a</u>	uSlcyn	10 m	CHANGE*	374	n: <u>4-620</u>	, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	. DEPTH:			
erved contain		± 0.7			Yar	etals		0,48	6.74		READING	d Hd)			WELL DEPTH: 2.771			
er (ie. 'metal	_	0.1 unit			Vec	SOMP			<u> </u>		CHANGE	pH (pH units)	m below TOC	m below TOC	3			
s' bottle)	TRIPLICATE COLLECTED:	diality			Willa	13/es			++		READING	70			SCREEN INTERVAL:			7
	E COLLEC	± 10mV			α <u>Ω</u>	Cod			7		NG CHANGE*	REDOX POTENTIAL (mV)		Pump	VTERVAL			ROJECT
	TED:					7057			∠∞			Ħ		Pump Intake Depth:	 		DATE:	PROJECT NUMBER:
	~	± 0.2°C			(Q			0		READING CH	TEMPERATURE (°C)		5	to L			1
						other			C		CHANGE			2.5 M			20/61	TURHO
	\					COMPS -			-		Slig Clo	— ₹	PPM:		.m below TOC		13	D04
	TRIPUCATE ID: _				_	moles			7		Clo Ve Clo	udy lick one udy	<u>₩</u> 0 · O	WELL HEADSPACE PID READING PID READING				ENAURHODO4498AB
		100				•			Z		Tur		0	PACE PID	TICK-UP:			B
) adour.		00	0		READING	STICK-UP: flush			***
:											LLECTED, e	COMMENTS			5 mm			
								. ,	Brown.		COLLECTED, etc	MENTS DOL	:					
					l										,			

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Groundwater Sampling Form (B) – Micro Purge

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WERE METALS FIELD FILTERED? Y N DUPLICATE ID: TRIPLIC Unfiltered samples must not be put into a preserved container (ie. 'metals' bottle)	(3 readings within following ranges) ± 10% ± 3% ± 0.1 unit	T-100/			Yem poor vechourge.	Post Purge: Not enough water for Wan Rea	800	Well burged dry at 12.	12:00pm. 1 5.269 1-19 ppm 891 uslam 6.31	0 NA	READING CHANGET READING CHANGET READING CHANGET	TIME OF PUMP (1) DEPTH TO DISSOLVED ELECTRICAL PH OXYGEN CONDUCTIVITY (pH units) DAY RATE (ml/min) note 1 note 2 (mg/l) (mS or µS/cm)	Meter ID: Rental After Pump Installation: m below TOC	Equipment ID: Revitor Depth to Water - Before Pump Installation: 5.270 m below TOC	FIELD EQUIPMENT FIELD EQUIPMENT	WELL ID: MVV124 DIAMETER: SO mm WELL DEPTH: 5.520 m	PROJECT MANAGER: ML	FIELD PERSONNEL:	-	TOUR LECTION	PROJECT NAME: LONG LEGISE, Hay warket
TRIPLICATE COLLECTED: Y N TRIPLICATE ID:	2:10mV 2:0.20C					ding · Symples calleded · .			-67 mV 21.0 °C . No adour. Colourless		Slig Clo	L	-	EADIN	WELL HEADSPACE PID READING	SCREEN INTERVAL:tom below TOC STICK-UP:tUS b		DATE: 20/6/13		- 1	PROJECT NUMBER: CZACRIO DOCTACRA

Surface Water.

Groundwater Sampling Form (A) - General

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coffey Fenvi	environments	0		Groun	Groundwater Sampling Form (A) - General	impling Fo	orm (A) -	General				PAGE OF	
PROJECT NAME:	Land	Lease, F	Haymarket	et l		 	PROJECT NUI	NUMBER:	NAURI	ENAURHODO4498AB	18AB	>	
FIELD PERSONNEL:	PD/	ACM	,					DATE:	21/6/13				
PROJECT MANAGER:	3								•				
WELL ID: SWIA &	の MET	METER ID:	Rental		101	TOTAL WELL DEPTH:	1	75	SCREE	SCREEN INTERVAL:	7 7	*	
			25	what water)	WELL DIAMETER:		ZA	WE	WELL STICK-UP:	ZA		
WELL GAUGING AND PURGE VOLUME CALCULATIONS	OLUME CALCUL	ATIONS	N V C	1000						WELL HEAD	WELL HEADSPACE PID READING	READING	
(TOTAL WELL DEPTH) - (DEPTH TO WATER) = (WATER COLUMN)) WATER) = (WATE	R COLUMN)	Use water column calculation together with the procedures in 'SOP- Groundwater Sampling - I to determine the cornect volume to be purged if	in calculation to OP- Groundwat correct volume	Use water column calculation together with the procedures in 'SOP- Groundwater Sampling - Bailers' to determine the correct volume to be purged from the	•	LITRES PER 1 WEL	—	ĮII.	PID READING	Z A		
			10 (Village of the Control of the Co		9:-7								
TIME OF PUMP VOLUME DAY	DEPTH TO WATER (m)	DISSOLVED (mg/l)	ELECTRICAL CONDUCTIVITY (mS or µS/cm)	an) VITY	pH (pH units)	PO F	REDOX POTENTIAL (mV)	TEMPERATURE (°C)		dy T	,	COMMENTS	
(IIIIIII)	733	READING CHANGE	READING	CHANGE* F	READING CHANGE	NGE" READING	G CHANGE	READING	CHANGE	Sligh Clou	Ver Clou Turb	ODOUR, COLLECTED, etc	
0 NA	Approx.												
SWIA		76 DOM	48.6	8 SW	-27	50	7	19.0	C C			No odour Glourless	V.
SINIS	(M)	.72 11	49.1	×3	.27	C7 &		17.5	7			ine water odour. (plouviess
STABILISATION CRITERIA (3 readings within following ranges)		± 10%	± 3%		± 0.1 unit	1+	10mV	± 0.2°C	C STATE				
DUPLICATE COLLECTED:	<u> </u>	N DUPLICATE ID:	CATE ID:		1	TRIPLICATE	TRIPLICATE COLLECTED:	 ~	z	TRIPUCATE ID:	Ë		
WERE METALS FIELD FILTERED?	~	N UNFILT	UNFILTERED SAMPLES MUST NOT BE PUT INTO A PRESERVED CONTAINER (IE. 'METALS' BOTTLE)	T NOT BE PUT	INTO A PRESERV	ED CONTAINER	(IE. 'METALS' B	OTTLE)					

Groundwater Sampling Form (A) - General

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Date:
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Groundwater 3
ir Sampling i
Form (A
) - General

WERE METALS FIELD FILTERED?	DUPLICATE COLLECTED:	STABILISATION CRITERIA (3 readings within following ranges)				The second secon	SW 2 B	SW2A	0 NA		TIME OF PUMP VOLUME DAY RATE (C)	Z D	(TOTAL WELL DEPTH) – (DEPTH TO WATER) = (WATER COLUMN)	EQUIPMENT OSED: BA		SIMPLET SW2A	PROJECT MANAGER:	FIELD PERSONNEL:	PROJECT NAME:	coffey P env	P
RED? Y							73	+ Im	Approx		DEPTH TO WATER (m)	II	FOWATER) = (V	BAILEX	; ;	Ω) - W	7. T	F PD	E Land	environments	
z		± 10%					7.62	7.82		READING	DISSOLVED OXYGEN (mg/l)	•	VATER COLUMN	WATERRA		METER ID:		1 PCT	y hearse	nts	
UNFILTERED	DUPLICATE ID:	3%						DDP FS		CHANGE*	n) NED VED	 ∃		CITEX					+		
UNFILTERED SAMPLES MUST NOT BE PUT INTO A PRESERVED CONTAINER (IE. 'METALS' BOTTLE)	<u>B</u>	± 3%					49.0	49.5		READING	ELECTRICAL CONDUCTIVITY (mS or µS/cm)	to determine the correct volume to be purged from the well (enter this value in the field to the right)	brocedures in 'SOP- Groundwater Sampling - Bailers'	1	Λ				Haymarket		6
JST NOT BE PI					·			マ い		CHANGE*	CAL TVITY S/cm)	e correct volume to the fier value in the fier v	mn calculation	Sampler	VILLAGE VI				-	Gro	Day Jack
UT INTO A PRE		± 0.4 t					36.8	8.26		READING	pH (pH units)	me to be purge ald to the right)	n together with water Sampling	[3	vatr vatr					Groundwater Sampling Form (A) - General	
SERVED CON	TRIP	unit								CHANGE	ts)	d from the	the 1 - Bailers'		Į.	TOTAL W				r Sampli	(
TAINER (IE. 'N	TRIPLICATE COL	± 10mV					75	70		READING	REDOX POTENTIAL (mV)		LITRES			TOTAL WELL DEPTH:			PROJECT	ng Form	
METALS' BOTT	COLLECTED:	X					and the same of	3/		CHANGE" F	AL.	NAL	U	1 .		H N/A		DATE:	CT NUMBER:	(A) - Ge	
<u> </u>	~	± 0.2°C					7.8	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \		READING CH	TEMPERATURE (°C)	г-	ER 1 WELL VOLUME					TE 21	1	neral	
	z						7	0		CHANGE C	ear				Ę	SCREE	-	6	ENAURHO DO44198AB		
	TRIPL										CLARITY – tick one	PPM:	PID READING	WELL BEAD	- STICK	SCREEN INTERVAL:		W	D04		
	TRIPLICATE ID:									Ve Clo		×1/A	ADING	8					+98AB	:	
								760			rbid	,			Z	NIA					
						•	()	No adour. (COLLE	MOD BILL	•	į							PAGE.	
	I							Colourles		COLLECTED, etc	COMMENTS									= OF	
							//	less		9	PSH								4	_	