

PREPARED FOR GAZCORP PTY LTD 16/04/2015 X122584-01C VERSION C WATER & ENVIRONMENT

Proposed Industrial Development 813-913 Wallgrove Rd, Horsely Park

Stormwater Concept Plan

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DOCUMENT CONTROL

X122584-01C

Issue	Date	Issue Details	Author	Checked	Approved
С	April 2015	Revised to reflect new road layour	PG/RB	PG	PG
В	August 2015	For DA	RB	PB	
Α	July 2013	Internal Review	RB	PB	

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1 INTRODUCTION

Brown Consulting has been engaged by Gazcorp Pty Ltd to develop a stormwater concept plan for a proposed industrial development at 813 – 913 Wallgrove Road, Horsely Park. This concept plan covers stormwater quality and quantity management issues to support the Development Application (DA) for the subdivision of 15 lots and proposed internal access road. The site is situated within the Local Government Area of Fairfield City Council. The locality sketch of the study area is shown in **Figure 1.1** below.

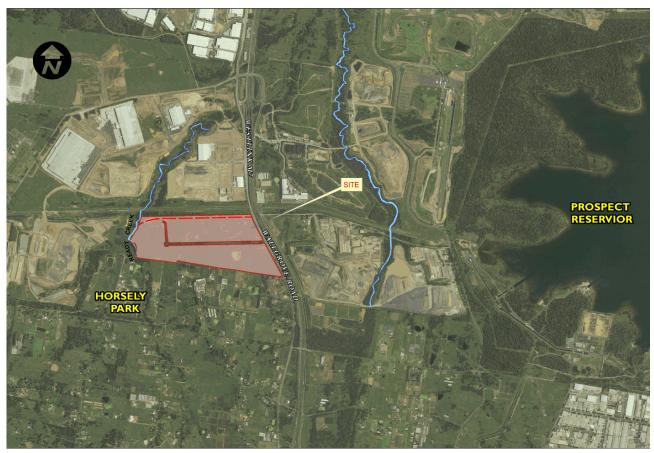


Figure 1.1: Locality Sketch

1.1 NOTE ABOUT THIS REVISION

Please note, this version of the Stormwater Concept Plan revises basin volumes to reflect revised internal road alignments and grading plans.

This version also realigns a proposed drainage swale that was noted to clash with electricity transmission towers.



1.2 DESCRIPTION OF THE STUDY AREA

The site is bordered by Wallgrove Road and Western Sydney Toll Road M7 at the east, Ready Creek at the west, and Sydney Catchment Authority pipeline at the northern boundary. Currently the site is used as grazing pasture land for cattle and horses.

The proposed development consists of 15 industrial lots with an internal access road to provide access to the proposed lots from Wallgrove Road. There is a future RMS Road reserve shared in part by the site, which will eventually run along the northern boundary of the site to be commissioned at a future stage. The general layout plan of the site is shown in **Figure 1.2** below.



Figure 1.2: The Proposed Layout Plan of the Site



1.3 OBJECTIVES

The proposed development will alter the natural catchment boundaries and increase the amount of stormwater runoff produced within the site.

A stormwater detention strategy is required to ensure that there is no net increase in stormwater discharge rates at each of the three principle outlets to neighbouring lands.

The objectives of the Stormwater Concept Plan for the subdivision prescribes detention basins that will meet the requirements of the Fairfield Development Concept Plan (November, 2010); Urban Area Onsite Detention Handbook (February, 1997) for water quantity and Sydney Metropolitan Catchment Management Authority, Interim Reference Guidelines for South East Queensland Concept Design Guidelines for WSUD for water quality management.

The objectives of this study is:

- To provide stormwater concept design of trunk drainage for the overall site
- To provide a concept sizing of detention storage requirement to match pre-development flows from the site.
- To demonstrate that the proposed stormwater treatment strategy meet the pollution reduction targets outlined in the Sydney Metropolitan Catchment Management Authority, Interim Reference Guidelines for South East Queensland Concept Design Guidelines for WSUD.
- To provide an interim stormwater concept design for the interim Stage 1 of works for the site.



2 HYDROLOGY

2.1 CATCHMENT AREAS

The total site area is 52.38 ha which currently drains to three principle outlets:

- Outlet 1 The South Eastern principle subcatchment is 14.12ha in size and drains to existing box culvert located under Wallgrove Road eventually drains to Eastern Creek.
- Outlet 2 The North Eastern subcatchment which is **13.0ha** in size, drains to north eastern corner of the site via an existing swale drain which then drains under the SCA pipeline.
- Outlet 3 The western subcatchments is the largest principle catchment area which is **26.0ha** in size and drains directly to Reedy Creek.

There are two external upstream catchment areas draining to the site:

- **External SE** The South Eastern external catchment is **74.71ha** in area, which drains through the south-eastern corner of the site which combines with the internal catchment areas of the site draining to Outlet 1.
- **External SW** The South Western external catchment is **5.6ha** in area, which drains through the site along to southern boundary and eventually discharges to Reedy Creek at the south-western corner of the site.

Stormwater runoff for the existing and proposed catchment conditions was modelled using the *XP-RAFTS* (version SP1, 2009) hydrological package. The Sub-catchments for the model were delineated using CatchmentSIM GIS based program based on a combination of 5m DEM of Smoothed ALS data supplied by the NSW Department of Lands and land survey of the site. The existing internal and external catchment areas shown in **Appendix A**.



2.2 MODEL PARAMETERS

Intensity Frequency Duration (IFD) data were obtained from Fairfield City Council, Stormwater Drainage Policy (Sept 2002). Hydrological modelling for the study area was undertaken for 5y and 100 year ARI events of storm durations from 10 minutes to 72 hours.

The Initial and Continuous Loss (IL/CL) model was adopted for modelling in *XP-RAFTS* and the parameters recommended in *Australian Rainfall and Runoff – Volume 2* (Institution of Engineers, Australia, 1987) we adopted for this study and are shown in **Table 2.1** below.

Table 2.1: Design Loss Rates

ltem	Pervious Area Loss	Impervious Area Loss	
Initial Loss (mm)	10	1	
Continuing Loss (mm/hr)	2.5	0	

A fraction impervious of 5% and 90% was adopted for undeveloped and developed (industrial) areas respectively. The model input and output data for XP-RAFTS is provided in **Appendix B**.

2.3 RESULTS OF MODELLING

2.3.1 EXISTING CONDITIONS

The peak flows for exiting catchment conditions were analysed using *XP-RAFTS* and the modelled peak flows and critical storm duration are shown in **Table 2.2** below for 5 year and 100 year ARI design storm events. Refer to Drawing 01 in **Appendix A** for sub-catchment references and outlet locations.

Table 2.2: Existing Peak Flows

Node	Peak Flow (m³/s)			
	5 Year	100 Year		
OUT 1	2.40 [2 hours]	4.60 [2 hours]		
OUT 2	2.30 2 hours]	4.00 [2 hours]		
OUT 3	3.40 [2 hours]	6.80 [2 hours]		

Note: [] denotes critical storm duration in hours.

The peak flow rates presented in Table 2.2 above at each discharge point of the site determine the Permissible Site Discharge (PSD) for the development. Refer to **Appendix B** for detailed results. The upstream catchments are not included in this study. Refer to Report and flood mapping BMT WBM.

2.3.2 DEVELOPED CONDITIONS – WITH NO DETENTION

The peak flows for developed catchment conditions without detention are shown in **Table 2.3** below for 5 year and 100 year ARI design storm events. Refer to Drawing 02 in **Appendix A** for sub-catchment references and outlet locations.



Table 2.3: Developed Peak Flows (No Detention)

Node	Peak Flo	ow (m³/s)
	5 Year	100 Year
OUT 1	5.51 [25min]	8.41 [15min]
OUT 2	3.84 [25min]	5.84 [15min]
OUT 3	9.64 [25min]	14.70 [15min]

The results in Table 2.3 above indicate that, without detention, the development increases the peak flows at the discharge points of the site above the PSD rates, due to the increase in the impervious area of the catchment. On-site Detention is required for the development.

2.4 ON-SITE DETENTION

2.4.1 PERFORMANCE TARGETS

Performance Targets as required for storm water quantity as outlined in *Fairfield City Council, Urban Area On Site Detention handbook (February, 1997)* are summarised below in **Table 2.4**.

Table 2.4: Performance Targets for storm water Quantity

	•
Reduction of peak flows to pre-development levels	5y and 100y ARI

2.4.2 DETENTION REQUIREMENTS

The overall stormwater quantity management strategy for the site is for each lot of the subdivision to provide an individual OSD system incorporated into their respective internal drainage systems. Each lot will have Site Storage Requirement (SSR) and Permissible Site Discharge (PSD) based on a lot area basis as summarised in **Table 2.5**.

Table 2.5: Summary of On-Site Detention Requirements

Attribute	5Y ARI	100Y ARI
PSD*, (m³/s/ha)	0.105 [0.10]	0.23 [0.20]
SSR*, (m³/ha)	220 [232]	315 [345]

Note:

- 1. PSD and SSR are to be provided at a rate of the total Lot Area
- 2. [] PSD and SSR to be provided only for proposed Catchment 3 which is sensitive to pre developed Catchment Flow at outlet

The PSD and SSR for each lot has been determined to compensate for internal road areas which will not have detention basins. The PSD and SSR for each lot will also accommodate catchments that bypass basins such as earthworks batters and landscaping areas which naturally bypasses detention. An allowance of up to 20% bypass has been factored into determining the PSD and SSR.



The actual arrangement of the detention tanks is subject to detailed design of each lot, however. For purposes of determining site SSR, a below ground detention tank with two stage outlet control structure was modelled for the OSD with no High Early Discharge (HED) included.

2.4.3 RESULTS OF MODELLING WITH DETENTION

The peak flows, critical storm durations and storage requirement for developed catchment conditions with on-site detention is summarised in **Table 2.6**. Refer to **Appendix B** for detailed model output.

Table 2.6: Summary of On-Site Detention Modelling Results

Outlet	Total Storage Required (m³)		Storage Requirement Rate, SSR (m³/ha)		Permissible site Discharge, PSD (m³/s/ha)		Peak Discharge At Outlet (m³/s)*	
	5Y	100Y	5Y	100Y	5Y	100Y	5Y	100Y
OUT 1	2,740	3,845	220	315	0.105	0.230	2.4	4.6
OUT 2 OUT 3	2,295 4,950	3,225 7300	220 235	315 345	0.105 0.100	0.230 0.200	1.8 3.4	3.5 6.8
TOTAL	9,255	12,990	220	315	0.105	0.230	-	-

Note:* Peak Discharge is total discharge at each outlet and includes 20% area bypass OSD.

2.4.4 COMPARISON WITH PRE AND POST DEVELOPMENT FLOWS

A comparison of pre and post developed with detention flows is presented in **Table 2.7** below. **OUT 1**, **OUT 2** and **OUT 3** represent the existing discharge points from the site.

Table 2.7: Comparison of Pre and Post Development Peak Flow Rates (with OSD)

ARI	OUT 1		OUT 2		OUT 3	
	Pre-dev (m³/s)	Post-dev (m³/s)	Pre-dev (m³/s)	Post-dev (m³/s)	Pre-dev (m³/s)	Post-dev (m³/s)
5	2.4 [2 hrs]	2.4 [1.5 hrs]	2.0 [2 hrs]	1.8 [1.5 hrs]	3.4 [2 hrs]	3.4 [1.5hrs]
100	4.6 [2 hrs]	4.6 [1.5hrs]	4.0 [2 hrs]	3.5 [1.5 hrs]	6.8 [2 hrs]	6.8 [1.5 hrs

Table 2.7 above shows that applying the proposed SSR and PSD rates to all lots attenuates the runoff from the post developed catchments to the existing flows at the discharge points from the site for 5 year and 100 year ARI. The OSD proposed for the lots provides adequate attenuation of flows to compensate for the roads and other bypass areas.



3 MANAGEMENT OF MAJOR AND MINOR FLOWS

Runoff from lots is generally directed to the internal access road drainage system. Inter-allotment drainage is to be provided for lots draining away from the road. Stormwater is to be generally conveyed through a below ground stormwater drainage network contained within the internal access road reserves. Peak discharges from the site is not to exceed the existing pre-development flow rate from the site. Detention requirements are described in more detail in **Section 2**.

3.1 MINOR FLOW MANAGEMENT

Stormwater runoff from Lots will be directed to a trunk drainage system for minor storm events in a conventional pit and pipe system. Each lot is required to have its own on site detention and water quality treatment to manage water quantity and quality at the outlet.

3.2 MAJOR FLOW MANAGEMENT UP TO 100 YEAR ARI

Flows in excess of the piped system capacity will be conveyed through the site to the nominated discharge pipes as overland flow along the internal access roads and temporary trunk drainage channels in place. The OSD system at each lot is designed in such a way to reduce post to pre developed peak flows for up to 100 year ARI and as such under normal operation of OSD systems, the major flows would be contained within the piped drainage system. Overland flow paths will be provided only as an emergency overflow provision for instances of blockage or OSD system failure.

The stormwater concept plan for the site is shown in **Appendix A**.



3.3 TEMPORARY CONVEYANCE STRUCTURES

During the development of the proposed site, the road drainage system under the future RMS road reserve located at the northern boundary of the site will not be planned as constructed until after the full development of the site. The proposed lots 1 to 2 and lots 11 to 15 will have their own individual OSD systems and be connected into the future road drainage system. As a temporary interim measure, two swales (Swale No 2 and Swale No 3) are proposed to convey 100 year ARI peak flows in place of the road drainage system. The swales will be contained within the area of the site reserved for the future road and will be decommissioned upon construction of the road drainage system. Refer to **Stormwater Concept Plan Drawing** provided in **Appendix A**. The proposed dimensions and hydraulic calculations of the temporary swales are summarised below in **Table 3.1**.

Table 3.1: Summary of Temporary Swales

Swale No	Depth (m)	Base Width (m)	Batter (1:X)	Slope (%)	Q (m3/s)	Flow Depth (m)	Freeboard (mm)	Top Width (m)
3	1.15	2.0	4.0	1.0	4.0	0.65	500	11
4	1.15	4.0	4.0	1.0	5.0	0.65	500	13

3.4 CONVEYANCE OF EXTERNAL CATCHMENTS

The two external catchment areas draining through the site are to be conveyed via vegetated swales and have been designed to for storms up to 100 year ARI based on flow information supplied by BMT WBM. The dimensions of the proposed vegetated swales located at South East (Swale No.1) and West (Swale No. 4) of site are summarised in **Table 3.2** below. Refer to **Stormwater Concept Plan Drawing** provided in **Appendix A** for locations of the respective swales.

Table 3.2: Dimensions of Swale for Upslope Diversion

Swale No.	Depth (m)	Base Width (m)	Batter (1:X)	Slope (%)	Top Width (m)
1	1.5	3.0	4	0.5	20
2	1.1	2.0	3	2.0	8.6

The hydraulic modelling of the proposed swales draining the external catchment areas has been undertaken by BMT WBM. Refer to report and flood maps by BMT WBM.



4 STORMWATER QUALITY TREATMENT

4.1 PERFORMANCE TARGETS

The proposed treatment strategy for the site is such that the development site is capable of reducing export loads to the requirements of the Sydney Metropolitan Catchment Management Authority, Interim Reference Guideline for the South East Queensland Concept Design Guidelines for WSUD. These target reduction rates are as referred to in the Director General's Environmental Assessment Requirements for the site and are provided in **Table 4.1** below.

Table 4.1: Reduction Rate Targets for Water Quality Treatment.

Parameter	Percentage Reduction (%)
Reduction in mean annual load of Total Gross Pollutant (GP)	90%
Reduction in mean annual load of Total Suspended Solids (TSS)	85%
Reduction in mean annual load of Total Phosphorous (TP)	65%
Reduction in mean annual load of Total Nitrogen (TN)	45%

4.2 STORMWATER TREATMENT STRATEGY

The stormwater treatment strategy for the overall site is to provide the majority of treatment as on-site treatment measures to within individual lots through adopting Waters Sensitive Urban Design (WSUD) principles. The access road is to provide primary treatment with Gross Pollutant Traps (GPTs). The removal rates to be employed by WSUD within the individual lots are to provide compensatory removal of pollutants for the access road such that the overall treatment of the site meets the removal rate targets presented in **Table 4.1**.

4.2.1 ONSITE TREATMENT FOR INDIVIDUAL LOTS

The stormwater treatment strategy for each individual lot is subject to the future development and building layout, however to compensate for the access road and bypass areas, the individual lots will need to achieve the following minimum reductions rate targets through WSUD:

Gross Pollutants 92%
Suspended Sediments 89%
Total Phosphorous 70%
Total Nitrogen 49%

4.2.2 GROSS POLLUTANT TRAPS (GPT'S)

The proposed gross pollutant traps for the access road area will be placed in line of the trunk drainage system prior to discharge into specific outlet to remove litter, debris and sediment. While the pollutant capture efficiency of various traps may vary, as a conservative measure for modelling purposes, it is assumed that the GPT will be capable of



removing of the following as per typical treatment performance provided in Sydney Catchment Authority, A guide to the Use of MUSIC in Sydney's Drinking Water Catchment ():

• Gross Pollutants 90%

Suspended Sediments 65%
Total Phosphorous 15%
Total Nitrogen 14%

The selection of the proprietary device is subject to detailed design, however the selection of the GPT will need to ensure the device is capable of removing the above reduction rate targets.

4.3 MUSIC MODELLING

1.1.1 Modelling Parameters

The performance of the proposed water quality treatment strategy has been modelled using the *MUSIC V5* water quality model. The parameters adopted for *MUSIC* modelling are provided in **Appendix C**.

4.3.1 MUSIC MODELLING NETWORK

A generic node was modelled to represent the WSUD removal rates to be applied to individual lots. Catchment areas were separated according to surface types with pollutant generation parameters assigned according to surface type. The music modelling adopted for this strategy lumped catchment areas representing total lot roof area, car park and loading area, taking into consideration bypassing catchment areas and road area such that the assessment of reduction rate covers the overall site. The music modelling network is shown in **Figure 4.1** below.



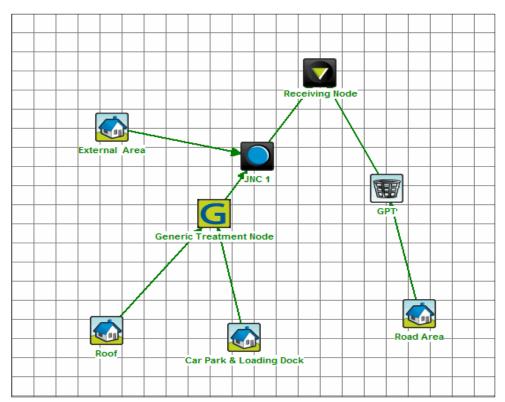


Figure 4.1: Music Model Network for Overall Site.



4.3.2 MUSIC MODELLING RESULTS

Table 4.2 shows the removal rates for the overall water quality treatment for the site. Refer to Appendix C for MUSIC model output.

Table 4.2: Results of MUSIC Modelling for Stormwater Treatment Strategy No 1 for Site

Parameter	Proposed Removal Targets for Road	Modelled Removal Rates for Lots	Modelled Removal Rates for Site	Required Removal rates*
TSS	65%	89%	86.4%	85%
TP	15%	70%	65.6%	65%
TN	14%	49%	46.0%	45%
Gross Pollutant	90%	92%	90.8%	90%

Note:

Table 4.2 shows the proposed removal rates for the future lots are capable of removing the pollutant loads below the required target removal rates for TSS, TP, TN and Gross Pollutants in Interim Reference Guideline for the South East Queensland Concept Design Guidelines for WSUD.

^{*} Performance targets as required in Interim Reference Guideline for the South East Queensland Concept Design Guidelines for WSUD



5 STAGE 1 INTERIM WORKS

5.1 ON-SITE DETENTION FOR STAGE 1

Stage 1 involves the construction of the central access road and the development of Lot 10 only. OSD is to be provided for Lot 10 under the SSR and PSD requirements to be applied to all lots

Temporary detention is to be provided for the access road until future lots are developed and OSD is incorporated on those lots.

Once the remaining lots have been developed, the temporary detention basins can be removed.

The Stormwater Concept Plan for Stage 1 is provided in Appendix A.

The interim detention strategy for Stage 1 was modelled using XP-RAFTS. A comparison of pre and post developed flows with detention is presented in **Table 5.1** below where, **OUT 1**, **OUT 2** and **OUT 3** represent the existing discharge points from the site.

It should be noted that, an addition outlet identified as **OUT 3a** will drain undeveloped catchments for the stage 1 interim strategy. There will be no increase in flows from this catchment. Under the ultimate strategy, this drainage line will only drain external catchments through the site (Swale number 2) and all internal catchments will drain to OUT 3. Refer to Drawing No. 05 in Appendix A for outlet locations.

Table 5.1: Comparison of Pre and Post Development Peak Flow Rates (with OSD)

ARI	OUT 1	OUT 1		OUT 2		OUT 3		OUT 3a	
	Pre-dev	Post-dev	Pre-dev	Post-dev	Pre-dev	Post-dev	Pre-dev	Post-dev	
	(m³/s)	(m³/s)	(m³/s)	(m³/s)	(m³/s)	(m³/s)	(m³/s)	(m³/s)	
5	2.4	2.35	2.0	2.0	3.4	3.40	0.8	0.7	
	[2 hrs]	[2 hrs]							
100	4.6	4.50	4.0	3.98	6.8	6.78	1.6	1.4	
	[2 hrs]	[2 hrs]							

Table 5.1 shows that the interim detention strategy for the site is capable of attenuating peak flows discharging from the site to existing peak flows for 5 years to 100 year ARI.



5.2 STORMWATER QUALITY TREATMENT

The drainage strategy for Stage 1 incorporates temporary catch drains to separate runoff from undeveloped catchments from the stage 1 development footprint. It is proposed to provide a temporary 600 mm diameter pipe culvert under the access road which will drain the undeveloped catchments under the access road and around stormwater treatment basins.

The treatment strategy for Stage 1 is to be with a combination of internal treatment devices for lot 10 and temporary bio retention basins for the access road. Once the future lots have been developed at a future stage, the on lot treatment system provided on all the lots will compensate for the access road catchment and the temporary basins can be decommissioned.

The target removal rate for Lot 10 proposed to be achieved through a combination of bioretention in car park areas, Enviropods located within gully pits for Hardstand areas and finally whole site routing through in line GPTs with Stormfilter treatment system fitted to the OSD tanks. Refer to the **Stormwater Concept Plan** for Stage 1 provided in **Appendix A**. The internal drainage of Lot 10 is subject to detailed design however the sizing of the treatment systems used for MUSIC modelling to achieve the target removal rates for Stage 1 is provided in **Appendix C**.

5.2.1 MUSIC MODELLING NETWORK

The music modelling adopted for the stage 1 interim strategy lumped catchment areas representing total lot roof area, car park and hardstand (loading) area, taking into consideration external catchment areas and road area such that the assessment of reduction rate covers Stage 1 site. The music modelling network for stage 1 is shown in **Figure 5.1** below.

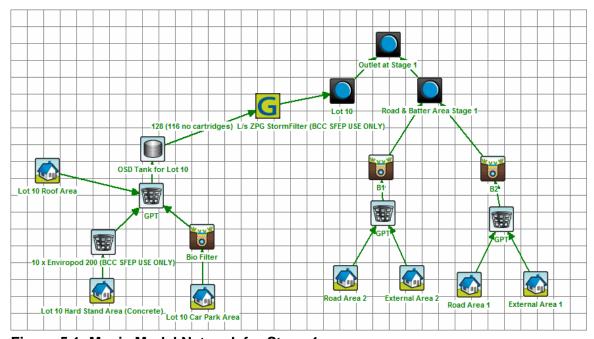


Figure 5.1: Music Model Network for Stage 1



MUSIC MODELLING RESULTS 5.2.2

Table 5.2 shows the removal rates for the overall water quality treatment for the site. Refer to Appendix C for MUSIC model output.

Table 5.2: Results of MUSIC Modelling for Stormwater Treatment Strategy for Stage 1

Parameter	Proposed Removal Targets for Lot 10	Modelled Removal Rate using Treatment Strategy for Lot 10	Modelled Overall Removal Rate for Road Area	Modelled Removal Rates for Site	Required Removal rates*
TSS	89%	93%	91.5%	92.6%	85%
TP	70%	69.2%	65.0%	68.0%	65%
TN	49%	51.9%	50.2%	51.5%	45%
Gross Pollutant	92%	100%	100%	100.0%	90%

Note:

Table 5.2 shows that, the stormwater treatment strategy for Stage 1 is capable of removing the pollutant loads below the required target removal rates for TSS, TP, TN and Gross Pollutants in Interim Reference Guideline for the South East Queensland Concept Design Guidelines for WSUD.

^{*} Performance targets as required in Interim Reference Guideline for the South East Queensland Concept Design Guidelines for WSUD



6 CONCLUSION

It is concluded that the proposed Stormwater Concept Plan for the site:

- Provides on-site detention (OSD) strategy capable of reducing developed peak flows to pre-developed flows from the site for 5 year to 100 year ARI design storm events for the ultimate developed site as well as the Interim Stage 1 to manage stormwater quantity discharging from the site.
- Provides stormwater treatment strategy which is capable of reducing pollutant loads of TSS, TP, TN and gross pollutants to the reduction targets outlined in the Sydney Metropolitan Catchment Management Authority, Interim Reference Guidelines for South East Queensland Concept Design Guidelines for WSUD.

7 REFERENCES

Fairfield City Council, Urban Area OnSite Detention handbook (February, 1997)

Fairfield Town Centre, Development Control Plan (November, 2010)

Fairfield City Council, Stormwater Drainage Policy (September, 2002)

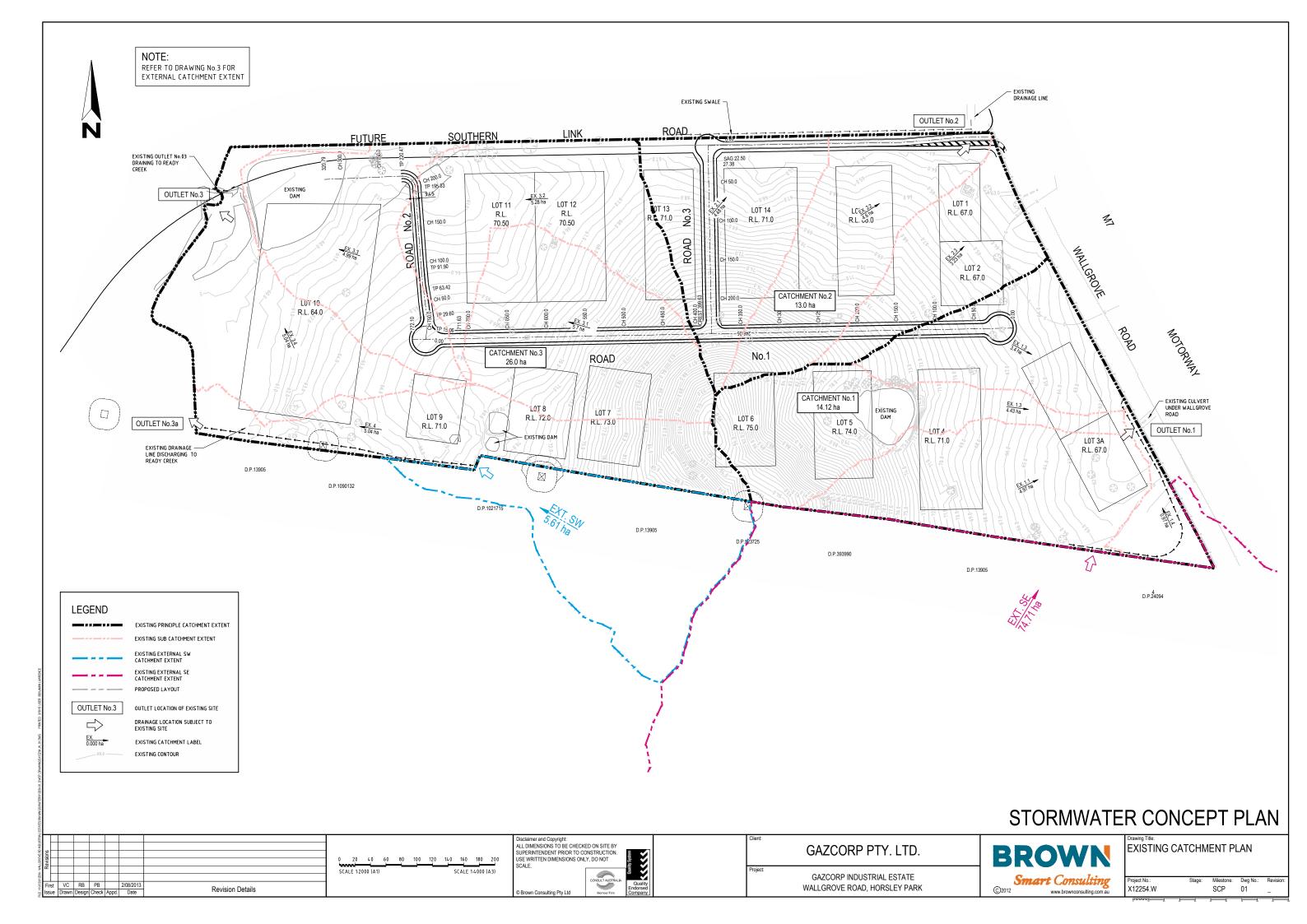
Sydney Metropolitan Catchment Management Authority, Interim Reference Guideline for the South East Queensland Concept Design Guidelines for WSUD.

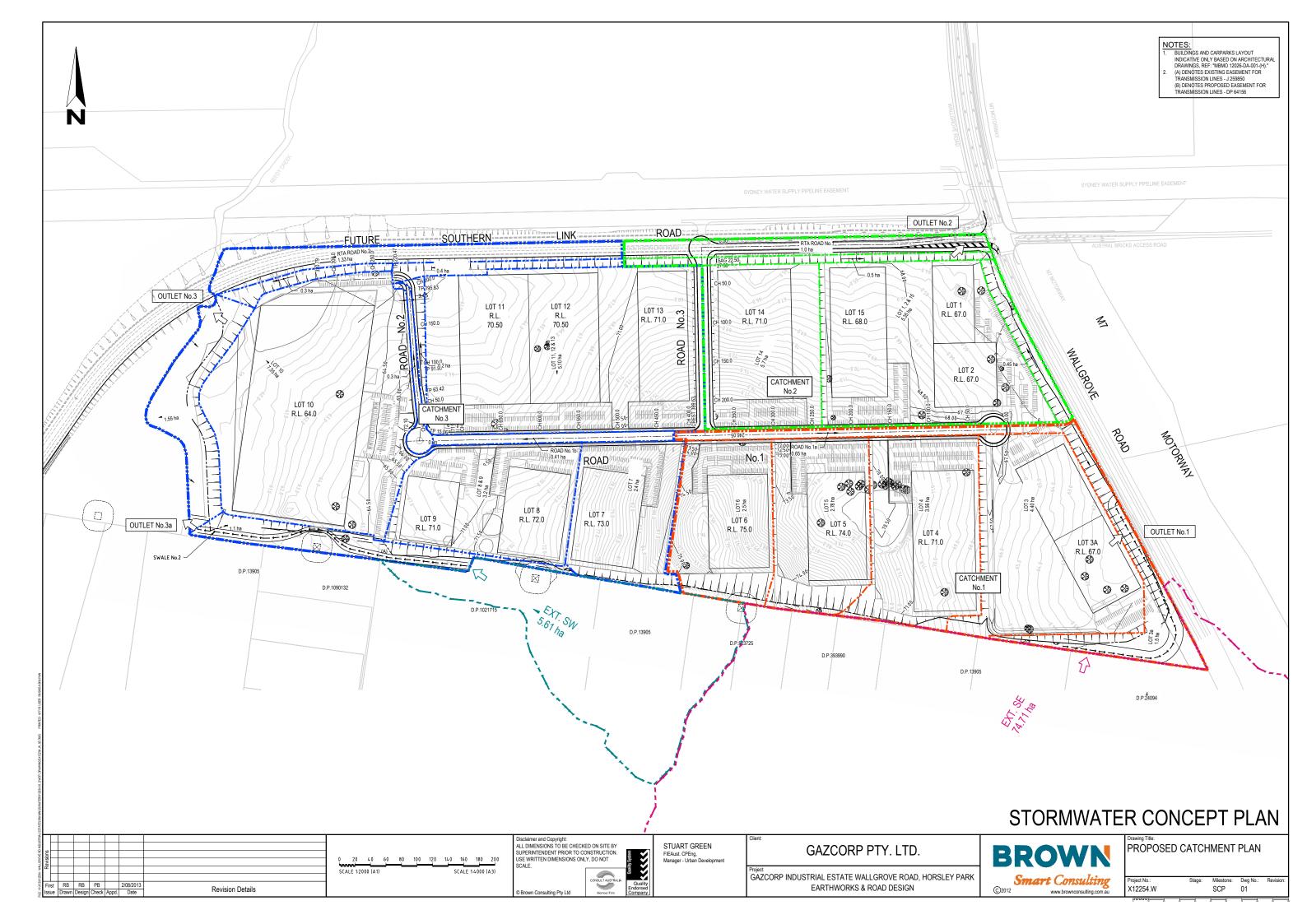
Sydney Metropolitan Catchment Management Authority, Draft NSW Music Modelling Guidelines (August 2010)

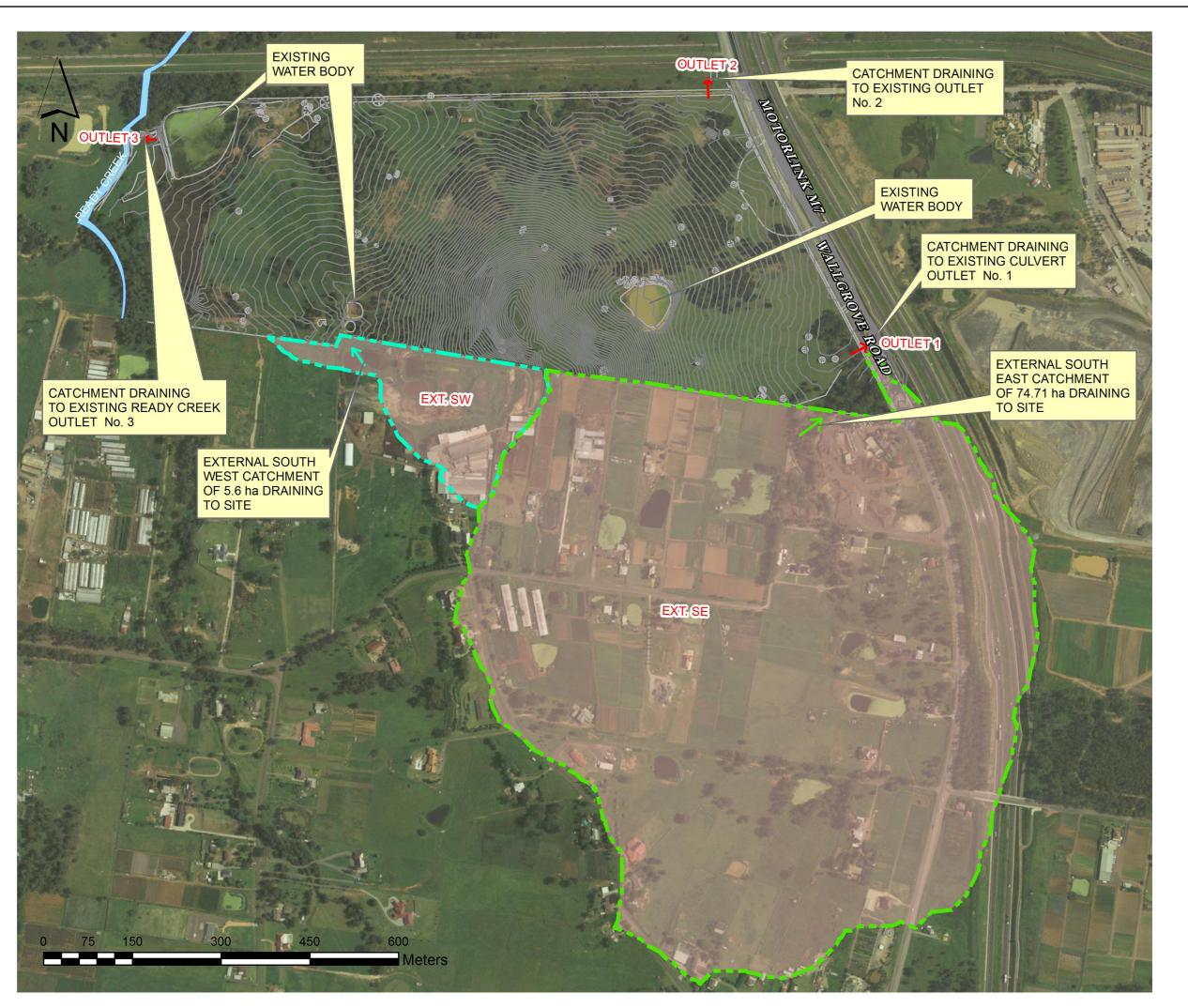
Sydney Catchment Authority, Draft a Guide to the Use of MUSIC in Sydney's Drinking Water Catchments



APPENDIX A DRAWINGS









Legend

EX. EXTERNAL SW CATCHMENT

EX. EXTERNAL SE CATCHMENT

READY CREEK

— EXISTING CONT. 1m INC.

Issue	Amendment	Date

Projec

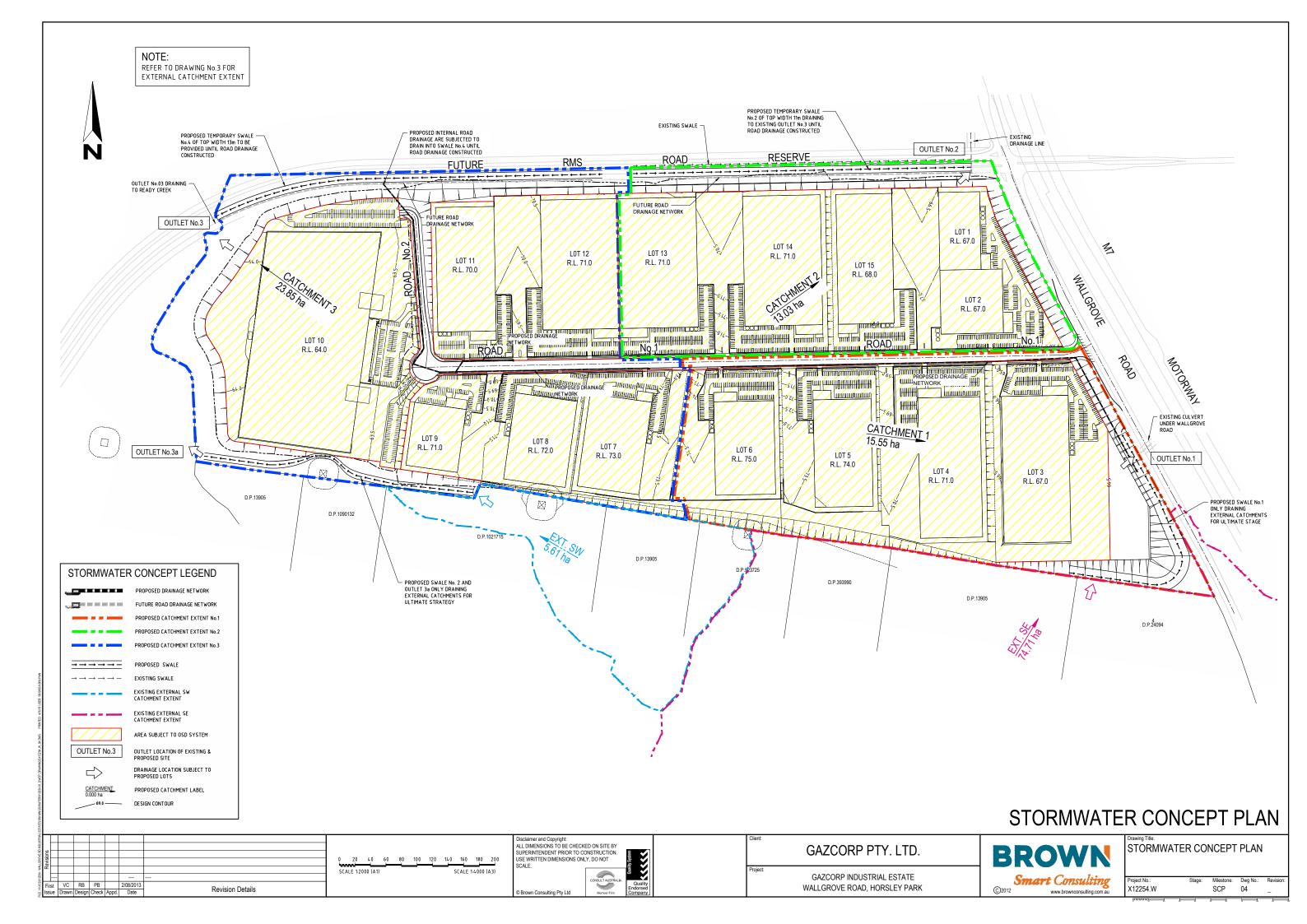
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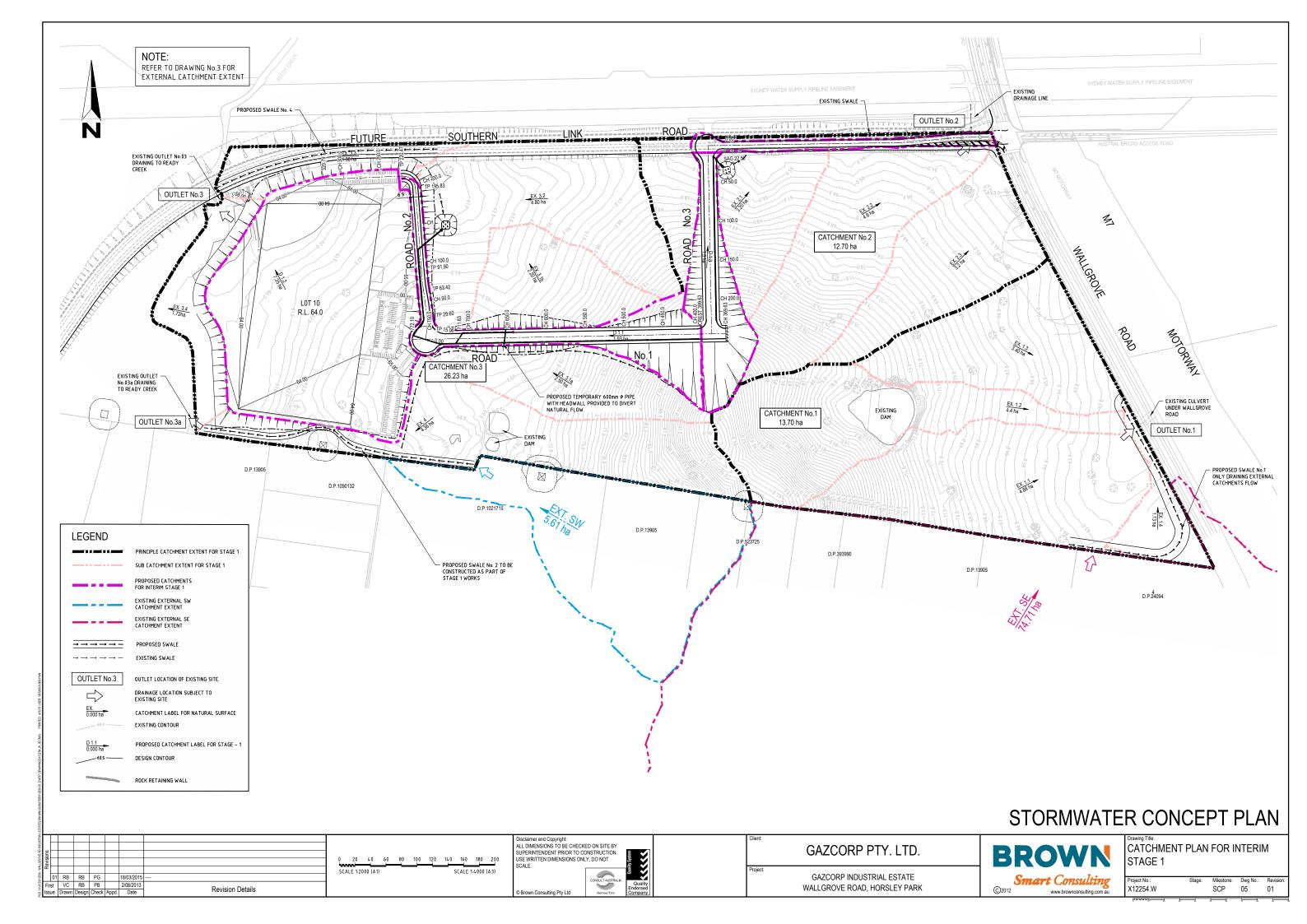
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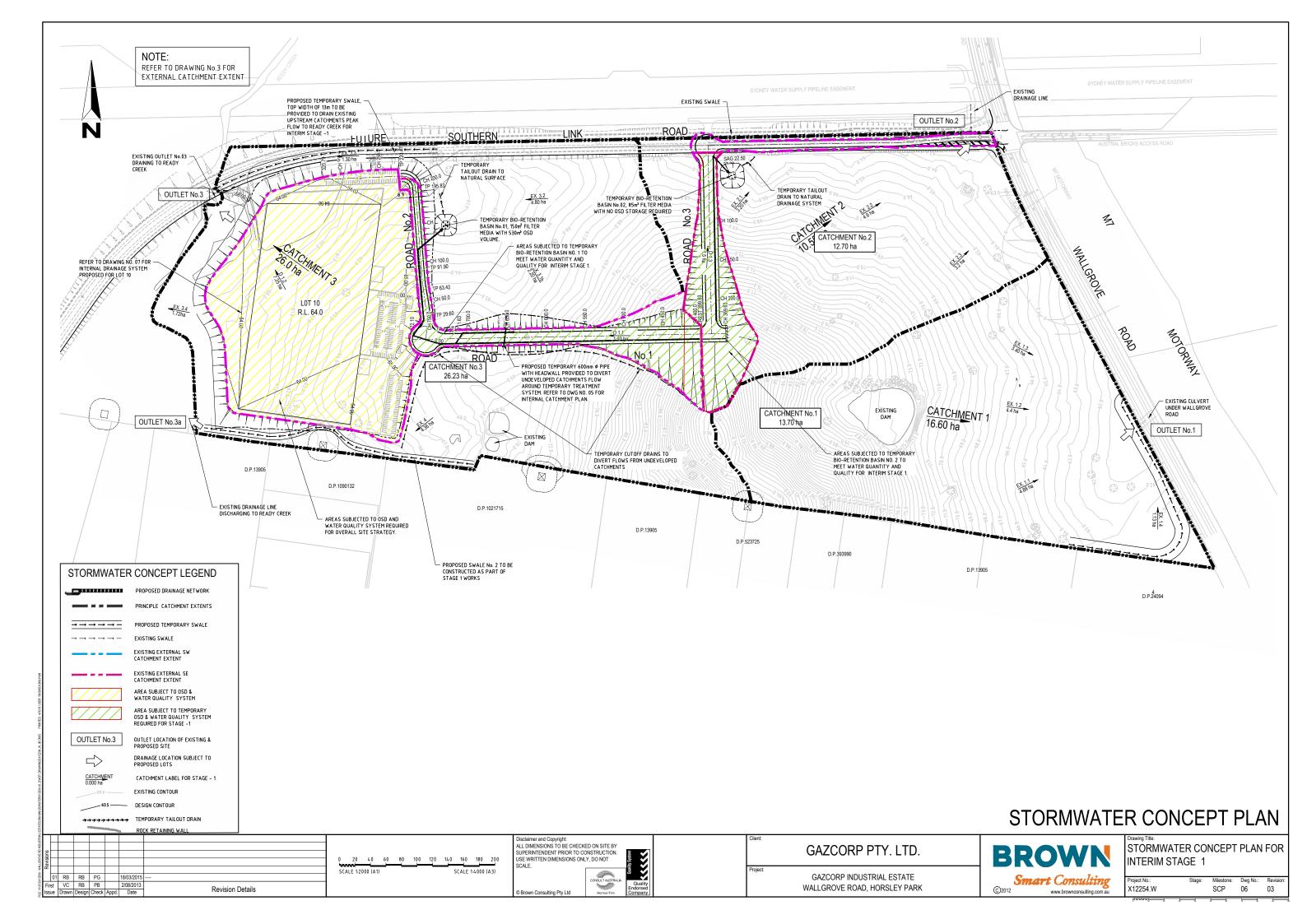
EXTERNAL CATCHMENT PLAN FOR EXISTING AND PROPOSED CONDITION

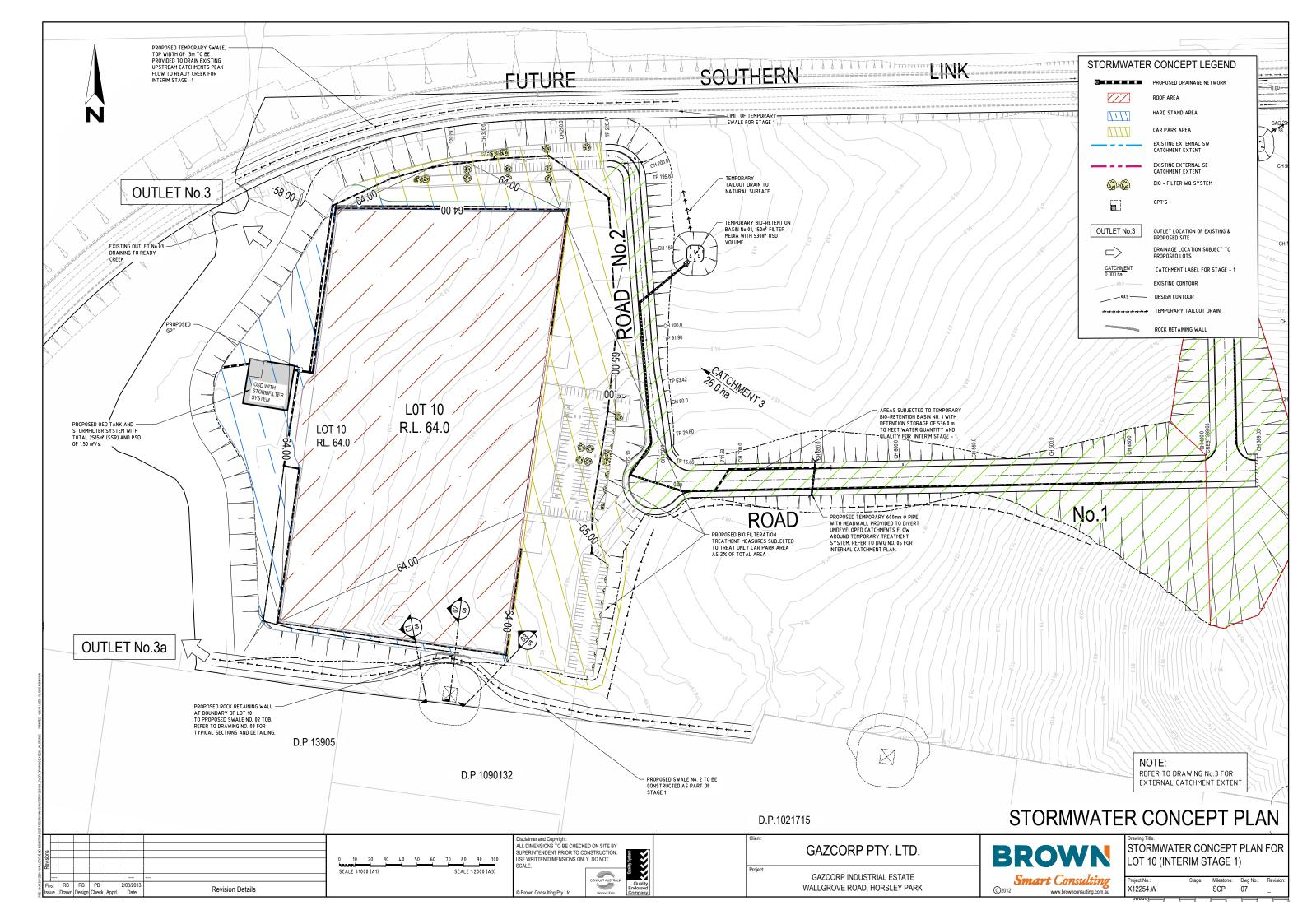
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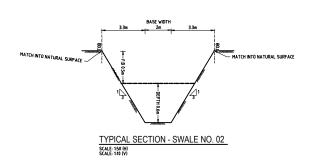
Issue

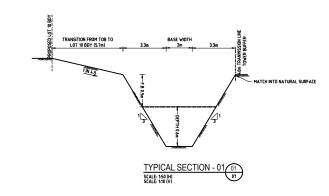


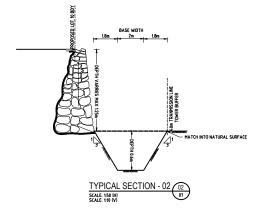


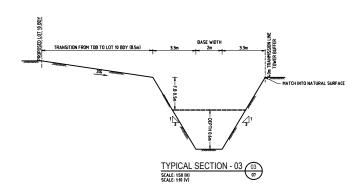












NOTES:

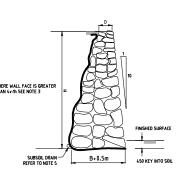
BACKFILL IS TO BE GRANULAR, FREE DRAINING AND COMPACTED.

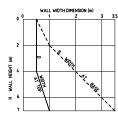
3. WHERE THE SURFACE SLOPE OF RETAINED MATERIAL IS BETWEEN 101 AND 4-1 THE WALL BASE DIMENSION IS TO BE INCREASED BY 0.5 METRES.

4. ROCK IS TO BE SOUND DURABLE SANDSTONE OR OTHER APPROVED HATERIAL AND AT LEAST 0.5 SQUARE HETRES PLAIN AREA.

6. ROCKS SHALL BE PLACED IN SUCH A MANNER THAT THEY ARE STABLE AND INTERLOCKING & BEDDED ON THEIR BROADEST BASE.

ROCK SPECIFICATION NOTES: BREADTH (B) - 0.4 TO 0.6m WIDTH (V) - 0.4 TO 0.6m LENGTH (L) - 2x(B OR W) -4-3 3x(B OR W) -2200 ±g/cum





ROCK RETAINING WALL DETAIL

Revision Details

Disclaimer and Copyright:
ALL DIMENSIONS TO BE CHECKED ON SITE BY
SUPERINTENDENT PRIOR TO CONSTRUCTION.
USE WRITTEN DIMENSIONS ONLY, DO NOT
SCALE.

GAZCORP PTY. LTD.

GAZCORP INDUSTRIAL ESTATE WALLGROVE ROAD, HORSLEY PARK



TYPICAL SECTIONS FOR SWALE NO. 02

Project No.: X12254.W Milestone: Dwg No



APPENDIX B - RAFTS RESULTS



```
Wallgrove Road
Results for period from 0: 0.0 1/1/2000
          to 3: 0.0 1/1/2000
ROUTING INCREMENT (MINS) =
                                              1.00
               STORM DURATION (MINS) =
                                             90.
               RETURN PERIOD (YRS)
                                           100.
                             = 1.0000
               TOTAL OF FIRST SUB-AREAS (ha) =
                                                 52.62
               TOTAL OF SECOND SUB-AREAS (ha) =
                                                    0.00
               TOTAL OF ALL SUB-AREAS (ha) =
                                                52.62
SUMMARY OF CATCHMENT AND RAINFALL DATA
Link
       Catch. Area
                   Slope
                         % Impervious
                                       Pern
                                               B
                                                   Link
Label
       #1
            #2
                         #1 #2 #1 #2 #1 #2
                #1
                    #2
                                                 No.
      (ha)
               (%)
                        (%)
Catch 1 12.440 0.000 2.000 0.000 90.00 0.000 .020 0.00 .0067 0.000 1.000
      .00001 0.000 .0010 0.000 0.000 0.000 .025 0.00 .0021 0.000 1.001
B1
       3.000 0.000 2.000 0.000 90.00 0.000 .020 0.00 .0032 0.000 2.000
B<sub>D</sub>1
      D1
Out 1
       .00001 0.000 .0010 0.000 0.000 0.000 .025 0.00 .0021 0.000 1.003
BP3
       5.000 0.000 2.000 0.000 90.00 0.000 .020 0.00 .0042 0.000 3.000
Catch 3 18.650 0.000 2.000 0.000 90.00 0.000 .020 0.00 .0083 0.000 4.000
      .00001 0.000 .0010 0.000 0.000 0.000 .025 0.00 .0021 0.000 4.001
B3
      .00001 0.000 .0010 0.000 0.000 0.000 .025 0.00 .0021 0.000 3.001
D3
      .00001 0.000 .1000 0.000 5.000 0.000 .025 0.00 .0002 0.000 3.002
Catch 2 10.400 0.000 2.500 0.000 90.00 0.000 .020 0.00 .0055 0.000 5.000
      .00001 0.000 .0010 0.000 0.000 0.000 .025 0.00 .0021 0.000 5.001
B2
       2.430 0.000 2.000 0.000 90.00 0.000 .020 0.00 .0029 0.000 6.000
Bp2
D2
      0.7000 0.000 2.000 0.000 0.000 0.000 .040 0.00 .0214 0.000 5.002
       .00001 0.000 .1000 0.000 5.000 0.000 .025 0.00 .0002 0.000 5.003
Out 2
outlet .00001 0.000 .0100 0.000 5.000 0.000 .025 0.00 .0005 0.000 1.004
Link Average Init. Loss Cont. Loss Excess Rain Peak Time Link
Label Intensity #1 #2 #1 #2
                              #1 #2 Inflow to
     (mm/h) ( mm )
                     (mm/h)
                              ( mm )
                                      (m<sup>3</sup>/s) Peak mins
Catch 1 53.019 1.000 0.000 0.000 0.000 78.528 0.000 6.498 29.00 0.000
B1
      53.019 1.000 0.000 0.000 0.000 78.528 0.000 6.498 29.00 0.000
Bp1
      53.019 1.000 0.000 0.000 0.000 78.528 0.000 1.581 28.00 0.000
D1
      53.019 1.000 0.000 0.000 0.000 78.528 0.000 4.325 30.00 0.000
      53.019 10.00 0.000 2.500 0.000 66.237 0.000 4.325 30.00 0.000
Out 1
BP3
       53.019 1.000 0.000 0.000 0.000 78.528 0.000 2.619 29.00 0.000
Catch 3 53.019 1.000 0.000 0.000 0.000 78.528 0.000 9.678 30.00 0.000
В3
      53.019 1.000 0.000 0.000 0.000 78.528 0.000 9.678 30.00 0.000
```

53.019 1.000 0.000 0.000 0.000 78.528 0.000 6.744 30.00 0.000 53.019 10.00 0.000 2.500 0.000 66.237 0.000 6.744 30.00 0.000

Catch 2 53.019 1.000 0.000 0.000 0.000 78.528 0.000 5.452 29.00 0.000 B2 53.019 1.000 0.000 0.000 0.000 78.528 0.000 5.452 29.00 0.000

D3

out 3



53.019 1.000 0.000 0.000 0.000 78.528 0.000 1.279 28.00 0.000 Bp2 D2 53.019 10.00 0.000 2.500 0.000 66.237 0.000 3.773 30.00 0.000 53.019 10.00 0.000 2.500 0.000 66.237 0.000 3.773 30.00 0.000 outlet 53.019 10.00 0.000 2.500 0.000 66.237 0.000 14.842 30.00 0.000

SUMMARY OF BASIN RESULTS

Link Time Peak Time Peak Total ----- Basin -----Label to Inflow to Outflow Inflow Vol. Vol. Stage Peak (m^3/s) Peak (m^3/s) (m^3) Used Avail Used B1 29.00 6.498 33.00 2.895 9762.8 0.0000 3963.7 1.5222 R3 30.00 9.678 33.00 4.345 14637.5 0.0000 5925.7 1.5091 29.00 5.451 32.00 2.432 8161.6 0.0000 3334.5 1.5268

SUMMARY OF BASIN OUTLET RESULTS

Link	No.	S/D	Dia	Widt	h Pip	рe	Pipe
Label	of	Factor			Length	SI	оре
	(m) (m	ı) (m	n) (r	(m) ((%)	
B1	1.0	1.000	0	.000	20.00	0 00	.2000
B3	1.0	1.000	0	.000	20.00	0 00	.2000
B2	1.0	1.000	0	.000	20.00	0 00	.2000

Results for Developed Catchment Condition with Detention for Interim stage 1

Wallgrove Road

Results for period from 0: 0.0 1/1/2000

to 4: 0.0 1/1/2000

Pern

В

Link

ROUTING INCREMENT (MINS) = 1.00 STORM DURATION (MINS) = 120. RETURN PERIOD (YRS) 5. ВХ = 1.0000 TOTAL OF FIRST SUB-AREAS (ha) =

48.39 TOTAL OF SECOND SUB-AREAS (ha) = 4.35 TOTAL OF ALL SUB-AREAS (ha) = 52.74

SUMMARY OF CATCHMENT AND RAINFALL DATA Slope

Catch. Area

Link

Label #1 #2 #1 #2 #1 #2 #1 #2 #1 #2 No. (ha) (%) (%)Ex 2.1 3.660 0.000 3.100 0.000 5.000 0.000 .035 0.00 .0296 0.000 1.000 .00001 0.000 .0010 0.000 5.000 0.000 .025 0.00 .0016 0.000 1.001 Ex 2.3 3.200 0.000 3.100 0.000 5.000 0.000 .035 0.00 .0276 0.000 2.000 .00001 0.000 .0100 0.000 5.000 0.000 .025 0.00 .0005 0.000 2.001 3.300 0.000 3.100 0.000 5.000 0.000 .035 0.00 .0280 0.000 3.000 .00001 0.000 .0010 0.000 5.000 0.000 .025 0.00 .0016 0.000 3.001 .00001 0.000 .1000 0.000 5.000 0.000 .025 0.00 .0002 0.000 1.002 Out 2 1.900 0.000 2.480 0.000 5.000 0.000 .035 0.00 .0235 0.000 4.000

% Impervious



```
4.400 0.000 4.470 0.000 5.000 0.000 .035 0.00 .0271 0.000 5.000
Ex 1.2
        4.880 0.000 3.940 0.000 5.000 0.000 .035 0.00 .0305 0.000 6.000
Fx 1 1
D 1.3
       0.6500 3.650 2.000 2.000 90.00 5.000 .020 .035 .0014 .0367 7.000
       .00001 0.000 .0010 0.000 0.000 0.000 .025 0.00 .0021 0.000 7.001
B2
D9
       .00001 0.000 .0010 0.000 0.000 0.000 .025 0.00 .0021 0.000 7.002
        1.130 0.000 1.690 0.000 5.000 0.000 .035 0.00 .0217 0.000 4.001
out1
Ex 3.1b 2.200 0.000 3.100 0.000 5.000 0.000 .035 0.00 .0227 0.000 8.000
Ex 3.1a 2.500 0.000 2.000 0.000 5.000 0.000 .035 0.00 .0302 0.000 9.000
       .00001 0.000 .0010 0.000 0.000 0.000 .025 0.00 .0021 0.000 8.001
D5
D 1.1
        1.000 0.7000 2.000 2.000 90.00 5.000 .020 .035 .0018 .0156 10.00
B1
       .00001 0.000 .0010 0.000 0.000 0.000 .025 0.00 .0021 0.000 10.00
        4.840 0.000 3.270 0.000 5.000 0.000 .035 0.00 .0333 0.000 8.002
Ex 3.2
        1.300 0.000 .5000 0.000 5.000 0.000 .035 0.00 .0429 0.000 11.00
Ex 3.3
D7
       .00001 0.000 .0010 0.000 5.000 0.000 .025 0.00 .0016 0.000 8.003
        7.350 0.000 2.000 0.000 90.00 0.000 .020 0.00 .0051 0.000 12.00
D1.2
B10
        .00001 0.000 .0010 0.000 0.000 0.000 .025 0.00 .0021 0.000 12.00
       .00001 0.000 .0010 0.000 0.000 0.000 .025 0.00 .0021 0.000 12.00
D6
EX 3.4
        1.720 0.000 1.000 0.000 5.000 0.000 .035 0.00 .0351 0.000 13.00
        4.360 0.000 2.930 0.000 5.000 0.000 .035 0.00 .0333 0.000 14.00
Ex 4.0
        .00001 0.000 .0010 0.000 0.000 0.000 .025 0.00 .0021 0.000 14.00
out 3a
       .00001 0.000 .1000 0.000 5.000 0.000 .025 0.00 .0002 0.000 8.004
Site Out .00001 0.000 .0100 0.000 5.000 0.000 .025 0.00 .0005 0.000 1.003
```

Link Average Init. Loss Cont. Loss Excess Rain Peak Time Link Label Intensity #1 #2 #1 #2 #1 #2 Inflow to Lag (mm/h) (mm) (mm/h) (mm) (m³/s) Peak mins Ex 2.1 26.932 10.00 0.000 2.500 0.000 39.738 0.000 0.6126 43.00 0.000 26.932 10.00 0.000 2.500 0.000 39.738 0.000 0.6126 43.00 1.330 Ex 2.3 26.932 10.00 0.000 2.500 0.000 39.738 0.000 0.5524 42.00 0.000 D₁ 26.932 10.00 0.000 2.500 0.000 39.738 0.000 0.5524 42.00 .5000 Ex 2.2 26.932 10.00 0.000 2.500 0.000 39.738 0.000 0.5668 42.00 0.000 D2 26.932 10.00 0.000 2.500 0.000 39.738 0.000 0.5668 42.00 .8000 26.932 10.00 0.000 2.500 0.000 39.738 0.000 1.730 43.00 0.000 Out 2 26.932 10.00 0.000 2.500 0.000 39.738 0.000 0.3157 43.00 0.000 Ex 1.2 26.932 10.00 0.000 2.500 0.000 39.738 0.000 0.8199 41.00 0.000 Ex 1.1 26.932 10.00 0.000 2.500 0.000 39.738 0.000 0.8430 42.00 0.000 26.932 1.000 10.00 0.000 2.500 52.863 39.738 0.5783 41.00 0.000 D 1.3 26.932 1.000 0.000 0.000 0.000 52.863 0.000 0.5783 41.00 0.000 B2 D9 26.932 1.000 0.000 0.000 0.000 52.863 0.000 0.3697 65.00 0.000 26.932 10.00 0.000 2.500 0.000 39.738 0.000 2.343 43.00 4.400 Ex 3.1b 26.932 10.00 0.000 2.500 0.000 39.738 0.000 0.4002 41.00 0.000 Ex 3.1a 26.932 10.00 0.000 2.500 0.000 39.738 0.000 0.3598 45.00 1.000 26.932 1.000 0.000 0.000 0.000 52.863 0.000 0.7323 44.00 1.000 D5 26.932 1.000 10.00 0.000 2.500 52.863 39.738 0.3947 35.00 0.000 D 1 1 B1 26.932 1.000 0.000 0.000 0.000 52.863 0.000 0.3947 35.00 0.000 Ex 3.2 26.932 10.00 0.000 2.500 0.000 39.738 0.000 1.647 45.00 1.500 Ex 3.3 26.932 10.00 0.000 2.500 0.000 39.738 0.000 0.1117 57.00 0.000 D7 26.932 10.00 0.000 2.500 0.000 39.738 0.000 1.754 47.00 1.000 26.932 1.000 0.000 0.000 0.000 52.863 0.000 2.398 34.00 0.000 D1.2 B10 26.932 1.000 0.000 0.000 0.000 52.863 0.000 2.398 34.00 0.000



26.932 10.00 0.000 2.500 0.000 39.738 0.000 0.7772 44.00 0.000 D6 EX 3.4 26.932 10.00 0.000 2.500 0.000 39.738 0.000 0.1935 50.00 0.000 Ex 4.0 26.932 10.00 0.000 2.500 0.000 39.738 0.000 0.6865 44.00 0.000 out 3a 26.932 1.000 0.000 0.000 0.000 52.863 0.000 0.6865 44.00 0.000 26.932 10.00 0.000 2.500 0.000 39.738 0.000 3.383 46.00 0.000 Site Out 26.932 10.00 0.000 2.500 0.000 39.738 0.000 7.395 46.00 0.000

SUMMARY OF BASIN RESULTS

Link Time Peak Time Peak Total ----- Basin -----Label to Inflow to Outflow Inflow Vol. Peak (m^3/s) Peak (m^3/s) (m^3) Used Avail Used B2 41.00 .5783 65.00 .3697 1792.3 0.0000 522.84 0.9593 B1 35.00 .3947 48.00 .1448 806.47 0.0000 306.97 0.8599 B10 34.00 2.397 44.00 .7772 3883.2 0.0000 1615.2 1.0461

SUMMARY OF BASIN OUTLET RESULTS

Link No. S/D Dia Width Pipe Pipe Label of Factor Length Slope (m) (m) (m) (m) (%) B2 20.000 0.2000 1.0 1.000 0.000 B1 1.0 1.000 0.000 20.000 0.2000 B10 1.0 1.000 0.000 20.000 0.2000

Wallgrove Road

Link

Results for period from 0: 0.0 1/1/2000

to 4: 0.0 1/1/2000

Pern

В

4.35

Link

ROUTING INCREMENT (MINS) = 1.00 STORM DURATION (MINS) = 120. RETURN PERIOD (YRS) 100. BX 1.0000 TOTAL OF FIRST SUB-AREAS (ha) = 48.39 TOTAL OF SECOND SUB-AREAS (ha) = TOTAL OF ALL SUB-AREAS (ha) = 52.74

SUMMARY OF CATCHMENT AND RAINFALL DATA

Catch. Area Slope % Impervious Label #2 #1 #2 #1 #2 #1 #2 #1 #2 No. (ha) (%) (%)Ex 2.1 3.660 0.000 3.100 0.000 5.000 0.000 .035 0.00 .0296 0.000 1.000 .00001 0.000 .0010 0.000 5.000 0.000 .025 0.00 .0016 0.000 1.001 Ex 2.3 3.200 0.000 3.100 0.000 5.000 0.000 .035 0.00 .0276 0.000 2.000 .00001 0.000 .0100 0.000 5.000 0.000 .025 0.00 .0005 0.000 2.001 3.300 0.000 3.100 0.000 5.000 0.000 .035 0.00 .0280 0.000 3.000 .00001 0.000 .0010 0.000 5.000 0.000 .025 0.00 .0016 0.000 3.001

.00001 0.000 .1000 0.000 5.000 0.000 .025 0.00 .0002 0.000 1.002 Out 2 1.900 0.000 2.480 0.000 5.000 0.000 .035 0.00 .0235 0.000 4.000



```
4.400 0.000 4.470 0.000 5.000 0.000 .035 0.00 .0271 0.000 5.000
Ex 1.2
        4.880 0.000 3.940 0.000 5.000 0.000 .035 0.00 .0305 0.000 6.000
Fx 1 1
D 1.3
       0.6500 3.650 2.000 2.000 90.00 5.000 .020 .035 .0014 .0367 7.000
       .00001 0.000 .0010 0.000 0.000 0.000 .025 0.00 .0021 0.000 7.001
B2
D9
       .00001 0.000 .0010 0.000 0.000 0.000 .025 0.00 .0021 0.000 7.002
        1.130 0.000 1.690 0.000 5.000 0.000 .035 0.00 .0217 0.000 4.001
out1
Ex 3.1b 2.200 0.000 3.100 0.000 5.000 0.000 .035 0.00 .0227 0.000 8.000
Ex 3.1a 2.500 0.000 2.000 0.000 5.000 0.000 .035 0.00 .0302 0.000 9.000
       .00001 0.000 .0010 0.000 0.000 0.000 .025 0.00 .0021 0.000 8.001
D5
D 1.1
        1.000 0.7000 2.000 2.000 90.00 5.000 .020 .035 .0018 .0156 10.00
B1
       .00001 0.000 .0010 0.000 0.000 0.000 .025 0.00 .0021 0.000 10.00
        4.840 0.000 3.270 0.000 5.000 0.000 .035 0.00 .0333 0.000 8.002
Ex 3.2
Ex 3.3
        1.300 0.000 .5000 0.000 5.000 0.000 .035 0.00 .0429 0.000 11.00
D7
       .00001 0.000 .0010 0.000 5.000 0.000 .025 0.00 .0016 0.000 8.003
        7.350 0.000 2.000 0.000 90.00 0.000 .020 0.00 .0051 0.000 12.00
D1.2
B10
        .00001 0.000 .0010 0.000 0.000 0.000 .025 0.00 .0021 0.000 12.00
       .00001 0.000 .0010 0.000 0.000 0.000 .025 0.00 .0021 0.000 12.00
D6
EX 3.4
        1.720 0.000 1.000 0.000 5.000 0.000 .035 0.00 .0351 0.000 13.00
        4.360 0.000 2.930 0.000 5.000 0.000 .035 0.00 .0333 0.000 14.00
Ex 4.0
        .00001 0.000 .0010 0.000 0.000 0.000 .025 0.00 .0021 0.000 14.00
out 3a
       .00001 0.000 .1000 0.000 5.000 0.000 .025 0.00 .0002 0.000 8.004
Site Out .00001 0.000 .0100 0.000 5.000 0.000 .025 0.00 .0005 0.000 1.003
```

Link Average Init. Loss Cont. Loss Excess Rain Peak Time Link Label Intensity #1 #2 #1 #2 #1 #2 Inflow to Lag (mm/h) (mm) (mm/h) (mm) (m³/s) Peak mins Ex 2.1 44.668 10.00 0.000 2.500 0.000 74.962 0.000 1.182 41.00 0.000 44.668 10.00 0.000 2.500 0.000 74.962 0.000 1.182 41.00 1.330 Ex 2.3 44.668 10.00 0.000 2.500 0.000 74.962 0.000 1.049 41.00 0.000 D₁ 44.668 10.00 0.000 2.500 0.000 74.962 0.000 1.049 41.00 .5000 Ex 2.2 44.668 10.00 0.000 2.500 0.000 74.962 0.000 1.079 41.00 0.000 D2 44.668 10.00 0.000 2.500 0.000 74.962 0.000 1.079 41.00 .8000 44.668 10.00 0.000 2.500 0.000 74.962 0.000 3.310 42.00 0.000 Out 2 44.668 10.00 0.000 2.500 0.000 74.962 0.000 0.6201 41.00 0.000 Ex 1.2 44.668 10.00 0.000 2.500 0.000 74.962 0.000 1.513 40.00 0.000 Ex 1.1 44.668 10.00 0.000 2.500 0.000 74.962 0.000 1.612 40.00 0.000 44.668 1.000 10.00 0.000 2.500 88.337 74.962 1.236 40.00 0.000 D 1.3 44.668 1.000 0.000 0.000 0.000 88.337 0.000 1.236 40.00 0.000 B2 D9 44.668 1.000 0.000 0.000 0.000 88.337 0.000 0.8542 51.00 0.000 44.668 10.00 0.000 2.500 0.000 74.962 0.000 4.640 41.00 4.400 Ex 3.1b 44.668 10.00 0.000 2.500 0.000 74.962 0.000 0.7451 40.00 0.000 Ex 3.1a 44.668 10.00 0.000 2.500 0.000 74.962 0.000 0.7403 41.00 1.000 44.668 1.000 0.000 0.000 0.000 88.337 0.000 1.469 41.00 1.000 D5 44.668 1.000 10.00 0.000 2.500 88.337 74.962 0.6878 35.00 0.000 D 1 1 B1 44.668 1.000 0.000 0.000 0.000 88.337 0.000 0.6878 35.00 0.000 44.668 10.00 0.000 2.500 0.000 74.962 0.000 3.208 42.00 1.500 Ex 3.2 Ex 3.3 44.668 10.00 0.000 2.500 0.000 74.962 0.000 0.2359 53.00 0.000 D7 44.668 10.00 0.000 2.500 0.000 74.962 0.000 3.426 44.00 1.000 44.668 1.000 0.000 0.000 0.000 88.337 0.000 3.707 34.00 0.000 D1.2 B10 44.668 1.000 0.000 0.000 0.000 88.337 0.000 3.707 34.00 0.000



SUMMARY OF BASIN RESULTS

Link Time Peak Time Peak Total -------- Basin -------Label to Inflow to Outflow Inflow Vol. Vol. Stage
Peak (m^3/s) Peak (m^3/s) (m^3) Avail Used Used
B2 40.00 1.235 51.00 .8542 3310.7 0.0000 809.18 1.4856
B1 35.00 .6878 48.00 .2577 1408.8 0.0000 531.82 1.4883
B10 34.00 3.706 42.00 1.730 6489.1 0.0000 2339.8 1.5154

SUMMARY OF BASIN OUTLET RESULTS

Link	No.	. S/D	Dia	Wid	th F	Pipe	Pipe
Label	of	Facto	r		Leng	th S	Slope
		(m) (ı	m) (r	n)	(m)	(%)	
B2	1.0	1.000	(0.000	20.	000	0.2000
B1	1.0	1.000	(0.000	20.	000	0.2000
B10	1.0	1.000)	0.000	20	.000	0.2000



APPENDIX C - - MUSIC MODELLING RESULTS



Table C.1: Adopted MUSIC modelling parameters for Rainfall Runoff Parameters

PARAMETER	INDUSTRIAL			
	Roof, Car Park and Road Areas	External Landscape Areas		
Friction Impervious (%)	90	5		
Impervious Area properties				
Rainfall Threshold (mm/day)	1.0	1.0		
Pervious Area Properties				
Soil Storage Capacity (mm)	120	120		
Soil Initial Storage (% of capacity)	25	25		
Field Capacity (mm)	80	80		
Infiltration Capacity Coefficient - a	200	200		
Infiltration Capacity Exponent - b	1	1		
Groundwater Properties				
Initial Depth (mm)	10	10		
Daily Recharge rate (%)	25	25		
Daily Baseflow rate (%)	5	5		
Daily Deep Seepage rate (%)	0.0	0.0		



Table C.2: Adopted MUSIC modelling parameters for Pollutant Load Generation

PARAMETER

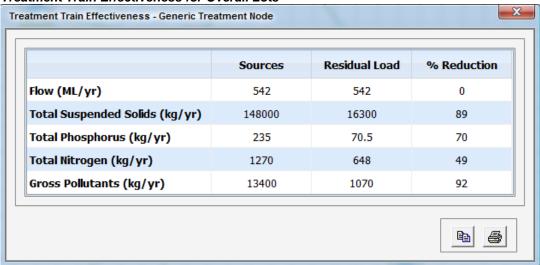
INDUSTRIAL AREA

_	Roof, and External Landscape Areas	Car Park and Road Areas
Baseflow TSS Mean (log mg/L)	1.20	1.20
Baseflow TSS Stand Dev (log mg/L)	0.17	0.17
Stormflow TSS Mean (log mg/L)	2.15	2.43
Stormflow TSS Stand Dev (log mg/L)	0.32	0.32
Baseflow TP Mean (log mg/L)	-0.85	-0.85
Baseflow TP Stand Dev (log mg/L)	0.19	0.19
Stormflow TP Mean (log mg/L)	-0.60	-0.30
Stormflow TP Stand Dev (log mg/L)	0.25	0.25
Baseflow TN Mean (log mg/L)	0.11	0.11
Baseflow TN Stand Dev (log mg/L)	0.12	0.12
Stormflow TN Mean (log mg/L)	0.30	0.34
Stormflow TN Stand Dev (log mg/L)	0.19	0.19

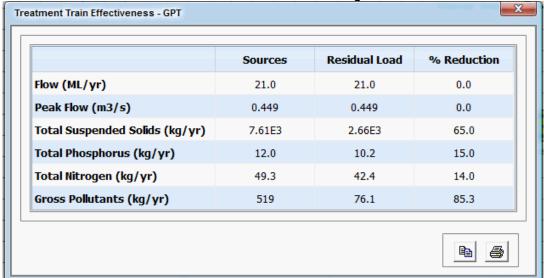


Results for Stormwater Treatment Strategy for Overall site

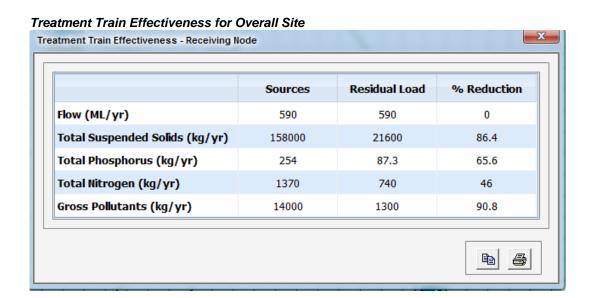
Treatment Train Effectiveness for Overall Lots



Treatment Train Effectiveness for Overall Road Areas using GPTs





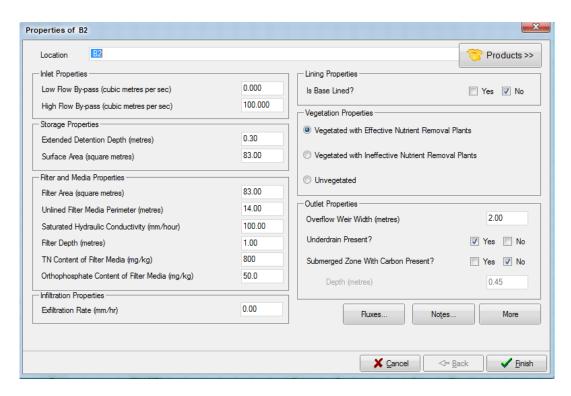


Music Modelling Parameters used for Treatment Strategy for Stage - 1

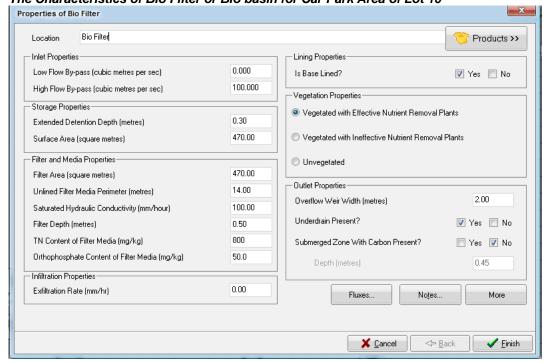
The Characteristics of Bio retention Basin 1 for Access Road Properties of B1 Location Products >> - Inlet Properties Lining Properties 0.000 Low Flow By-pass (cubic metres per sec) Is Base Lined? ▼ Yes
■ No 100.000 High Flow By-pass (cubic metres per sec) Vegetation Properties-Storage Properties Vegetated with Effective Nutrient Removal Plants Extended Detention Depth (metres) 0.30 150.00 Vegetated with Ineffective Nutrient Removal Plants Surface Area (square metres) Filter and Media Properties Unvegetated 150.00 Filter Area (square metres) Outlet Properties-14.00 Unlined Filter Media Perimeter (metres) 2.00 Overflow Weir Width (metres) 100.00 Saturated Hydraulic Conductivity (mm/hour) Underdrain Present? 🗸 Yes 🔳 No Filter Depth (metres) 1.00 TN Content of Filter Media (mg/kg) 800 Submerged Zone With Carbon Present? Pyes V No Orthophosphate Content of Filter Media (mg/kg) 50.0 Depth (metres) 0.45 Infiltration Properties Exfiltration Rate (mm/hr) 0.00Fluxes.. Notes.. More 💢 <u>C</u>ancel <⊳ Back ✓ <u>F</u>inish

The Characteristics of Bio retention Basin 2 for Access Road





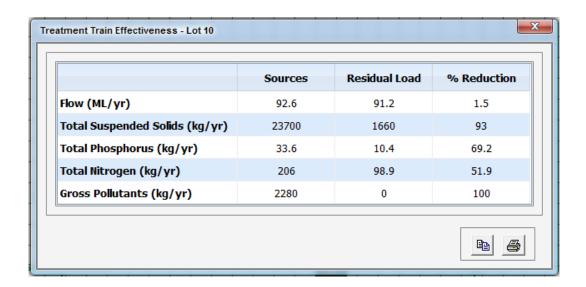
The Characteristics of Bio Filter or Bio basin for Car Park Area of Lot 10



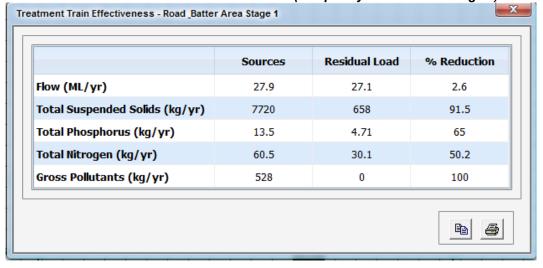
Results for Stormwater Treatment Strategy for Stage 1

Treatment Train Effectiveness for Lot 10





Treatment Train Effectiveness for Access Road (Temporary treatment for Stage 1)





Treatment Train Effectiveness at Site Outlet - Interim Stage 1

