# TRAFFIC AND PARKING IMPACT ASSESSMENT OF A PROPOSED EXPANSION OF A LIQUID WASTE PROCESSING BUSINESS 

14-16 Kiora Crescent in Yennora

## Traffic and Parking Impact Report

Prepared for: Enviro Waste Services Group

N1915887A (July 2020)

## 1. INTRODUCTION

ML Traffic Engineers was commissioned by Enviro Waste Services Group to undertake a traffic and parking impact assessment of a proposed expansion of a liquid waste processing business at 14-16 Kiora Crescent in Yennora.

The vehicle access and egress to the car park is via Kiora Crescent. Kiora Crescent ends in cul-de-sac.

This traffic report focuses on the proposed expansion of a liquid waste processing business and changes in car usage and car park utilisation and additional trips from the proposed expansion of a liquid waste processing business.

In the course of preparing this assessment, the subject site and its environs have been inspected, plans of the development examined, and all relevant traffic and parking data collected and analysed.

## 2. BACKGROUND AND EXISTING CONDITIONS OF THE PROPOSED LOCATION

### 2.1 Location and Land Use

The proposed expansion of a liquid waste processing business is located to the North-West of Yennora Train Station and Yennora Public School respectively. Yennora Distribution Centre is located north of the site. The liquid waste processing business lies in the area which is a primarily industrial. Residential buildings are primarily located north and west to the site.

Figure 1 shows the location of the liquid waste processing business from the aerial map perspective.

Figures 2 shows the location of the liquid waste processing business from the street map perspective and assessed intersections respectively.

Figures 3 shows the existing site.


Figure 1: Location of the Subject Site on Aerial


Figure 2a: Street Map of the Location of the Liquid waste processing business and Assessed Intersections


Figure 2b: surveyed signalised intersections in relation to development site


Figure 3: Liquid waste processing business (14 Kiora Crescent, Yennora)


Figure 4: Liquid waste processing business (16 Kiora Crescent, Yennora)

### 2.2 Road Network

This section describes the roads near the proposed expansion of a liquid waste processing business. The entrance to the liquid waste processing business is from Kiora Crescent.

Kiora Crescent is a local road with one lane each way. The default speed limit is $50 \mathrm{~km} / \mathrm{hr}$. Unlimited on-street parking is permitted on both sides of the road. Kiora Crescent ends in cul de sac. Figure 4 a shows the photograph of Kiora Crescent.

Norrie Street is a local road with one lane each way. The default speed limit is $50 \mathrm{~km} / \mathrm{hr}$. Unlimited on-street parking is permitted on both sides of the road. Figure 4 b shows the photograph of Norrie Street.

Loftus Road is a local road with one lane each way. The default speed limit is $50 \mathrm{~km} / \mathrm{hr}$. Unlimited on-street parking is permitted on both sides of the road. Figure 4 c shows the photograph of Loftus Road.

Dursley Road is a local road with one lane each way. The sign posted speed limit is $50 \mathrm{~km} / \mathrm{hr}$. Unlimited on-street parking is permitted on both sides of the road except near the intersection of Dursley Road with Fairfield Road. Figure 4d shows the photograph of Dursley Road.

Fairfield Road is a local collector road with one lane each way. The sign posted speed limit is $60 \mathrm{~km} / \mathrm{hr}$. On-street parking is not permitted on either side of the road. Figure 4 e shows the photograph of Fairfield Road.

Polding Street is a local collector road with one lane each way. The sign posted speed limit is $60 \mathrm{~km} / \mathrm{hr}$. On-street parking is not permitted on either side of the road. Figure 4 f shows the photograph of Polding Street.

The Horsley Drive is a sub arterial road with two lane each way. The sign posted speed limit is $60 \mathrm{~km} / \mathrm{hr}$. On-street parking is not permitted on either side of the road. School zone restrictions apply in the south east. Figure 4 g shows the photograph of Polding Street.


Figure 4a: Kiora Crescent Facing East from liquid waste processing business


Figure 4b: Norrie Street facing North from Kiora Crescent


Figure 4c: Loftus Road facing West

Proposed Expansion of a Liquid Processing Facility at 14-16 Kiora Crescent in


Figure 4d: Dursley Road facing East


Figure 4e: Fairfield Road facing North


Figure 4f: Polding Street facing North East


Figure 4g: The Horsley Drive facing North West

### 2.3 Public Parking Opportunities

The liquid waste processing business is located in an industrial zone. Unlimited onstreet parking is available on both sides of the Kiora Crescent and Norrie Street.

Site visits show that there are vacant car spaces on Kiora Crescent and Norrie Street.

### 2.4 Intersection Description

As part of this traffic impact assessment two intersections is assessed:

- Priority intersection of Norrie Street with Kiora Crescent
- Priority intersection of Loftus Road with Norrie Street
- Priority intersection of Loftus Road with Yennora Avenue
- Signalised intersection of Fairfield Road with Dursley Road
- Signalised intersection of The Horsley Drive with Polding Street

External traffic travelling to and from the site will most likely need to travel through the above intersection.

The priority intersection of Norrie Street with Kiora Crescent is a three-leg intersection with all turn movements permitted. Traffic on Kiora Crescent must give way to traffic on Norrie Street. Figure 5a shows a layout of the intersection using SIDRA (8) - an industry standard intersection assessment software.

The priority intersection of Loftus Road with Norrie Street is a three-leg intersection with all turn movements permitted. Traffic on Norrie Street must give way to traffic on Loftus Road. Figure 5 b shows a layout of the intersection using SIDRA.

The priority intersection of Loftus Road with Yennora Avenue is a three-leg intersection with all turn movements permitted. Traffic on Yennora Avenue must give way to traffic on Loftus Road. Figure 5c shows a layout of the intersection using SIDRA.

The signalised intersection of Fairfield Road with Dursley Road is a three-leg intersection. All turn movements are permitted. Pedestrian crossings are provided on all approaches. Figure 5d presents the layout of the intersection using SIDRA.

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The signalised intersection of The Horsley Drive with Polding Street is a four-leg intersection. All turn movements are permitted except right turn movement from north east approach of Polding Street into The Horsley Drive. Pedestrian crossings are provided on all approaches except south east approach. Figure 5e presents the layout of the intersection using SIDRA.


Figure 5a: Priority Intersection of Norrie Street with Kiora Crescent (SIDRA)

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Figure 5b: Priority Intersection of Loftus Road with Norrie Street (SIDRA)


Figure 5c: Priority Intersection of Loftus Road with Norrie Street (SIDRA)


Figure 5d: Signalised Intersection of Fairfield Road with Dursley Road (SIDRA)


Figure 5e: Signalised Intersection of The Horsley Drive with Polding Street (SIDRA)

### 2.5 Existing Traffic Volumes

As part of the traffic assessment, traffic counts have been undertaken at the intersection for the weekday AM and PM peak hour periods. The peak hours are 8:00am to 9:00am and $5: 00 \mathrm{pm}$ to $6: 00 \mathrm{pm}$ for the weekday AM and PM peak hours respectively.

Figures 6a and 6 b presents in vehicle numbers the existing weekday AM and PM peak hour traffic volumes respectively.


Figure 6a: Existing Weekday Traffic Volumes AM Peak Hour


Figure7: Existing Weekday Traffic Volumes PM Peak Hour

### 2.6 Intersection Assessment

An intersection assessment has been undertaken for:

- Priority Intersection of Norrie Street with Kiora Crescent
- Priority Intersection of Loftus Road with Norrie Street
- Priority intersection of Loftus Road with Yennora Avenue
- Signalised intersection of Fairfield Road with Dursley Road
- Signalised intersection of The Horsley Drive with Polding Street

The existing intersection operating performance was assessed using the SIDRA software package (version 9) to determine the Degree of Saturation (DS), Average Delay (AVD in seconds) and Level of Service (LoS) at each intersection. The SIDRA program provides Level of Service Criteria Tables for various intersection types. The key indicator of intersection performance is Level of Service, where results are placed on a continuum from ' $A$ ' to ' $F$ ', as shown in Table 1.

| LoS | Traffic Signal / <br> Roundabout | Give Way / Stop Sign / T-Junction <br> control |
| :--- | :--- | :--- |
| A | Good operation | Good operation |
| B | Good with acceptable <br> delays and spare capacity | Acceptable delays and spare capacity |
| C | Satisfactory | Satisfactory, but accident study required |
| D | Operating near capacity | Near capacity \& accident study required |
| E | At capacity, at signals <br> incidents will cause <br> excessive delays. | At capacity, requires other control mode |
| F | Unsatisfactory and <br> requires additional <br> capacity, Roundabouts <br> require other control <br> mode | At capacity, requires other control mode |

Table 1: Intersection Level of Service
The Average Vehicle Delay (AVD) provides a measure of the operational performance of an intersection as indicated below, which relates AVD to LOS. The AVD's should be taken as a guide only as longer delays could be tolerated in some locations (i.e. inner-city conditions) and on some roads (i.e. minor side street intersecting with a major arterial route). For traffic signals, the average delay over all movements should be taken. For roundabouts and priority control intersections
(sign control) the critical movement for level of service assessment should be that movement with the highest average delay.

| LoS | Average Delay per Vehicles (seconds/vehicle) |
| :--- | :--- |
| A | Less than 14 |
| B | 15 to 28 |
| C | 29 to 42 |
| D | 43 to 56 |
| E | 57 to 70 |
| F | $>70$ |

The degree of saturation (DS) is another measure of the operational performance of individual intersections. For intersections controlled by traffic signals both queue length and delay increase rapidly as DS approaches 1. It is usual to attempt to keep DS to less than 0.9 . Degrees of Saturation in the order of 0.7 generally represent satisfactory intersection operation. When DS exceed 0.9 queues can be anticipated.

The result of the intersection analysis is as follows:

## Priority Intersection of Norrie Street with Kiora Crescent

- The turn movements have a LoS A for the AM and PM peak hours
- There is a spare capacity at this intersection


## Priority Intersection of Loftus Road with Norrie Street

- The turn movements have a LoS A or B for the AM and PM peak hours
- There is spare capacity at this intersection.


## Priority Intersection of Loftus Road with Yennora Avenue

- The turn movements have a LoS A for the AM and PM peak hours
- There is spare capacity at this intersection.


## Signalised Intersection of Fairfield Road with Dursley Road

- Overall intersection has a LoS C and B for AM and PM peak hours respectively
- There is spare capacity at this intersection
- Overall intersection has a LoS D and C for the AM and PM peak hours respectively
- There is spare capacity at this intersection

The full Sidra results are presented in Appendix A.

### 2.7 Public Transport

The nearest bus stop to the liquid waste processing business is 550 metres away on Railway Street. This stop is serviced by Bus Route N60. This public transport service provides access to a range of suburbs including Fairfield, Merrylands, Parramatta, Lidcombe, Strathfield and City.

Yennora Train Station is within 500 metres from the liquid waste processing business. Yennora Train Station is frequently serviced by Sydney Trains T2 Inner West \& Leppington and T5 Cumberland line services during both AM and PM peak hours.

Figure 11 shows public transport network map.
Overall, the site has excellent access to public transport.


Figure 11: Public Transport Network Map

## 2.8 <br> Conclusions on the Existing Conditions

The proposed expansion of a liquid waste processing business is in an area where there are vacant car spaces on Kiora Crescent and Norrie Street.

The nearby intersection performs well to accommodate additional traffic of the liquid waste processing business.

The local area is serviced by both train and bus.

## 3. PROPOSED EXPANSION OF A LIQUID PROCESSING FACILITY

The details of the proposed expansion of a liquid processing facility are as follows:

## Infrastructure

A total of 3 car parking spaces are provided at the rear 16 Kiora Crescent. The remaining external hardstand area is proposed to be unoccupied to allow for greater vehicle manoeuvrability.

The parking is provided on the ground floor level.

The site has frontage to Kiora Crescent. The vehicle access and egress to the car park area is from Kiora Crescent.

Truck exit is via the existing driveway 16 Kiora Crescent and the exit is via the driveway on 14 Kiora Crescent.

A truck queuing area is provided on the south west area of 16 Kiora Crescent.

## Operational

Currently the liquid processing facility processes 900 tonnes of liquid waste per annum.
Enviro Waste proposes to increase the processing quantity to 110,000 tonnes per annum and increase the maximum quantity to be stored at any one time to 477 tonnes. Waste processing streams and proposed quantities per location are listed below:

14 Kiora Crescent (existing facility - industrial waste treatment/disposal, liquid waste material, sewage sludge, grease trap waste etc)

Processing capacity per annum: 100,000 tonnes.
Maximum storage at any one time: 377 tonnes.

## 16 Kiora Crescent (additional facility - out-of-date liquid product/food waste destruction)

Processing capacity per annum: 10,000 tonnes. Maximum storage at any one time: 100 tonnes

The liquid processing facility is proposed to operate 24 hours seven days a week.
Currently a truck arrives and departs per hour (typically). The number of staff will increase by three. The truck sizes are rigid trucks up to 10 metre.

Staff arrivals and departures are outside of the weekday peak hours.

A full scaled plan of the proposed expansion of a liquid processing facility is provided as part of the Development Application.

## 4. CAR AND TRUCK PARKING CONSIDERATIONS

## $4.1 \quad$ Holroyd Council Development Control Plan 2013

The car parking requirements for the proposed expansion of a liquid processing facility is presented in the Holroyd Council Development Control Plan August 2013 with the parking rates as follows as it applies to this development:

## Factory

- 1 car parking space per $300 \mathrm{~m}^{2}$ of GFA


## Office Units (ancillary)

- 1 car parking space per $40 \mathrm{~m}^{2}$ of GFA

Table 3 summarises the car parking requirements of the proposed development.

| Use | Number | GFAm ${ }^{2}$ | Parking Rate | Required Car Spaces | Provided Car Spaces |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Warehouse | 14 Kiora | 324 | 0.003 | 1 | 7 |
| Office |  | 106 | 0.025 | 3 |  |
| Warehouse | 16 Kiora | 318 | 0.003 | 1 |  |
| Office |  | 78 | 0.025 | 2 |  |
| Total |  |  |  | 7 | 7 |

Table 3: Summary of Car Parking Requirements
The proposed Liquid processing facility is provided 7 car spaces versus 7 car spacers required by Council's requirement. Therefore, it complies with car parking requirements by Council.

The liquid processing facility is an uncommon (or unique). The provision of seven on site will accommodate the expected car requirements for staff. Visitors arriving by car is a rare event. Business is generated by staff visiting the customers premises, discussions over the phone, and email etc.

The expected truck parking demand is four per hour. There is overall no peak hour for truck arrival and departures.

## 5. VEHICLE TRAFFIC IMPACT CONSIDERATIONS

### 5.1 Truck Traffic Generation

The NSW RTA Guide to Traffic Generating Development Documents does not publish truck trip generation rates for landscaping material supplies premises.

Traffic generation for the proposed development has been determined based on the annual tonnage of $110,000,000$ litres per year and operation of the site 7 days per week. Material would be transported in trucks ranging from 2000 to 22000 litres in size. The average truck capacity is 10000 L .

The following calculations are provided:

## 10000 litres trucks capacity

Average loads and truck movements using 22000L trucks for all loads.

| Incoming Materials: | $110,000,000 / 10000=$ | 11000 | Trucks p/a |
| ---: | :--- | :--- | :--- |
| Outgoing Materials: | $110,000,000 / 10000=$ | 11000 Trucks $p / a$ <br> Totals $\mathbf{2 2 0 0 0}$ Trucks p/a |  |

## Average annual truck trips

Using 10000 litres trucks 22000 trucks per year / 365 = 60 trucks per day
Based on the use of 10000 litres trucks, the number of truck movements expected would be between 60 truck trips per day, which will produce 30 movements in and 30 movements out per day over a 24 -hour period. which equates to 3 trucks per
hour. It is most likely to have 2 arrival and 1 departure truck for the AM peak hour and 1 arrival and 2 departure truck for PM peak hour.

### 5.2 Car Traffic Generation

The NSW RTA Guide to Traffic Generating Development 2002 publishes car trip generation rates for warehouse and office as follows

## warehouse

- 0.5 trips per $100 \mathrm{~m}^{2}$ gross floor area for AM peak hour
- It is assumed that generated trips for PM peak hour is as same as AM peak hour


## Office

- 2 trips per $100 \mathrm{~m}^{2}$ of Gross Floor Area in the PM peak hours
- It is assumed that generated trips for AM peak hour is as same as PM peak hour

Table 4 summarises the trip generations for the respective land uses during the peak hours.

| 14 Kiora |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Peak Hour | Use | GFA( $\mathrm{m}^{2}$ ) | Trip <br> Generation <br> Rate per <br> 100m2 | Trips Generated |
| AM | Warehouse Unit | 324 | 0.5 | 1.62 |
| PM |  |  | 0.5 | 1.62 |
| AM | Office Unit | 106 | 2 | 2.12 |
| PM |  |  | 2 | 2.12 |
|  |  |  |  |  |
| AM | Total trip Generation |  |  | 3.74 |
| PM |  |  |  | 3.74 |


| 16 Kiora |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Peak Hour | Use | GFA( $\mathrm{m}^{2}$ ) | Trip Generation Rate per 100m2 | Trips Generated |
| AM | Warehouse Unit | 318 | 0.5 | 1.59 |
| PM |  |  | 0.5 | 1.59 |
| AM | Office Unit | 78 | 2 | 1.56 |
| PM |  |  | 2 | 1.56 |
|  |  |  |  |  |
| AM | Total trip Generation |  |  | 3.15 |
| PM |  |  |  | 3.15 |

Table 4: Trip Generations in the Weekday Peak Hours
The total car trips can be obtained as the sum of the 14 and 16 Kiora Crescent. Table 5 presents the net trip generations and distributions. The generated trips in the peak hours are modest.

| Peak Hour | Origin | Destination | Total |
| :---: | :---: | :---: | :---: |
| AM | 0 | 7 | 6.9 |
| PM | 7 | 0 | 6.9 |

Table 5: Net Trip Generations and Distributions in the Weekday Peak Hours

## $5.3 \quad$ Traffic Volumes

The additional development trips are assigned onto the local traffic network. The following figures present the existing with the development trips (in red for origin and blue for destination trips) for the respective peak hours.

The additional development trips represent a low proportion of the existing traffic volumes.


Figure 12: Weekday AM Peak Hour Traffic Volumes with Proposed Expansion Traffic


Figure 13: Weekday PM Peak Hour Traffic Volumes with Proposed Expansion Traffic

### 5.4 Intersection Assessment

An intersection assessment has been undertaken for the surveyed intersection.
The results of the intersection analysis are as follows:

## Priority Intersection of Norrie Street with Kiora Crescent

- All turn movements have a LoS A for both the AM and PM peak hours
- The additional trips do not change the LoS for any turn movement or the overall intersection.


## Priority Intersection of Loftus Road with Norrie Street

- All turn movements have a LoS A for both AM and PM peak hours
- The additional trips do not change the LoS for any turn movement or the overall intersection.


## Priority Intersection of Loftus Road with Yennora Avenue

- All turn movements have a LoS A for AM and PM peak hours
- The additional trips do not change the LoS for any turn movement or the overall intersection.


## Signalised intersection of Fairfield Road with Dursley Road

- The overall intersection has a LoS C and B for the AM and PM peak hours respectively
- The additional trips do not change the LoS for any turn movement or the overall intersection.


## Signalised intersection of The Horsley Drive with Polding Street

- The overall intersection has a LoS D and C for the AM and PM peak hours respectively
- The additional trips do not change the LoS for any turn movement or the overall intersection.

The full SIDRA results with the development traffic are presented in Appendix B.

## 6. CONCLUSIONS

Based on the considerations presented in this report, it is considered that:

## Parking

- The proposed expansion of the liquid processing facility provides sufficient car spaces on site


## Traffic

- The proposed development is a low trip generator for the weekday AM and PM peak hours.
- The additional trips from the proposed development can be accommodated at the nearby intersection without significantly affecting intersection performance, delays or queues.
- There are no traffic engineering reasons why a development consent for the proposed expansion of a liquid processing facility at 14-16 Kiora Crescent Yennora should be refused.


## APPENDIX A

## SIDRA Intersection Results for Existing Traffic Conditions

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID Turn | INPUT VOLUMES [ Total HV ] veh/h veh/h |  | DEMA FLO [ Total veh/h | ND S HV ] \% | Deg. Aver. <br> Level Satn Delay Service v/c sec |  |  | 95\% BACK OF QUEUE <br> [ Veh. Dist ] veh |  | Prop. Que | Effective Stop Rate | Aver. Aver. Cycles Speed km/h |  |
| South: Norrie Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 1 | 0 | 1 | 0.0 | 0.012 | 4.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.03 | 0.00 | 49.3 |
| 2 T1 | 20 | 2 | 21 | 10.0 | 0.012 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.03 | 0.00 | 49.8 |
| Approach | 21 | 2 | 22 | 9.5 | 0.012 | 0.2 | NA | 0.0 | 0.0 | 0.00 | 0.03 | 0.00 | 49.8 |
| North: Norrie Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 42 | 0 | 44 | 0.0 | 0.030 | 0.0 | LOS A | 0.1 | 0.5 | 0.04 | 0.12 | 0.04 | 49.2 |
| 9 R2 | 12 | 0 | 13 | 0.0 | 0.030 | 4.6 | LOS A | 0.1 | 0.5 | 0.04 | 0.12 | 0.04 | 48.3 |
| Approach | 54 | 0 | 57 | 0.0 | 0.030 | 1.0 | NA | 0.1 | 0.5 | 0.04 | 0.12 | 0.04 | 49.0 |
| West: Kiora Crescent |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 16 | 3 | 17 | 18.8 | 0.012 | 4.8 | LOS A | 0.0 | 0.4 | 0.08 | 0.50 | 0.08 | 46.2 |
| 12 R2 | 1 | 0 | 1 | 0.0 | 0.012 | 4.8 | LOS A | 0.0 | 0.4 | 0.08 | 0.50 | 0.08 | 46.0 |
| Approach | 17 | 3 | 18 | 17.6 | 0.012 | 4.8 | LOS A | 0.0 | 0.4 | 0.08 | 0.50 | 0.08 | 46.2 |
| All <br> Vehicles | 92 | 5 | 97 | 5.4 | 0.030 | 1.5 | NA | 0.1 | 0.5 | 0.04 | 0.17 | 0.04 | 48.6 |

Table A1: Weekday Priority Intersection Performance of Norrie Street with Kiora Crescent AM Peak Hour

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID }^{2} \end{aligned}$ | $\begin{aligned} & \text { INP } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | TT MES HV] veh/h | DEMAND FLOWS | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \\ & \hline \end{aligned}$ | Deg. Aver. Satn Delay |  | $\begin{array}{r} \text { Level } \\ \text { of } \\ \text { Service } \end{array}$ | $95 \%$ Q <br> [ Veh. <br> veh | $\begin{gathered} \mathrm{K} \text { OF } \\ \text { E } \\ \text { Dist ] } \\ \mathrm{m} \end{gathered}$ | Prop. Que | Effective Stop Rate | $\begin{aligned} & \text { Aver. Aver. } \\ & \text { No. Speed } \\ & \text { Cycles } \end{aligned}$ |  |
| South: Norrie Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 41 | 5 | 43 | 12.2 | 0.043 | 5.5 | LOS A | 0.2 | 1.2 | 0.32 | 0.55 | 0.32 | 45.7 |
| 3 R2 | 6 | 0 | 6 | 0.0 | 0.043 | 6.7 | LOS A | 0.2 | 1.2 | 0.32 | 0.55 | 0.32 | 45.5 |
| Approach | 47 | 5 | 49 | 10.6 | 0.043 | 5.6 | LOS A | 0.2 | 1.2 | 0.32 | 0.55 | 0.32 | 45.7 |
| East: Loftus Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 18 | 0 | 19 | 0.0 | 0.131 | 4.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.04 | 0.00 | 49.2 |
| $5 \quad$ T1 | 216 | 11 | 227 | 5.1 | 0.131 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.04 | 0.00 | 49.7 |
| Approach | 234 | 11 | 246 | 4.7 | 0.131 | 0.4 | NA | 0.0 | 0.0 | 0.00 | 0.04 | 0.00 | 49.7 |
| West: Loftus Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 202 | 10 | 213 | 5.0 | 0.148 | 0.3 | LOS A | 0.4 | 2.7 | 0.16 | 0.11 | 0.16 | 49.0 |
| 12 R 2 | 47 | 0 | 49 | 0.0 | 0.148 | 5.5 | LOS A | 0.4 | 2.7 | 0.16 | 0.11 | 0.16 | 48.0 |
| Approach | 249 | 10 | 262 | 4.0 | 0.148 | 1.3 | NA | 0.4 | 2.7 | 0.16 | 0.11 | 0.16 | 48.8 |
| All <br> Vehicles | 530 | 26 | 558 | 4.9 | 0.148 | 1.3 | NA | 0.4 | 2.7 | 0.10 | 0.12 | 0.10 | 48.9 |

Table A2: Weekday Priority Intersection Performance of Loftus Street with Norrie Street AM Peak Hour

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{gathered} \text { INP } \\ \text { VOLL } \\ \text { [ Total } \\ \text { veh/h } \end{gathered}$ | JT <br> MES <br> HV] <br> veh/h | $\begin{gathered} \text { DEM/ } \\ \text { FLO } \\ \text { [ Total } \\ \text { veh/h } \end{gathered}$ | $\begin{gathered} \hline \text { ND } \\ \text { VS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. Aver. Satn Delay |  | Level <br> Service | 95\% BACK OF QUEUE | $\begin{aligned} & \hline \mathrm{K} \mathrm{OF} \\ & \mathrm{JE} \\ & \text { Dist ] } \\ & \mathrm{m} \\ & \hline \end{aligned}$ | Prop. Que | Effective Stop Rate |  |  |
| South: Yennora Avenue |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 27 | 0 | 28 | 0.0 | 0.040 | 5.3 | LOS A | 0.1 | 1.0 | 0.33 | 0.57 | 0.33 | 45.9 |
| 3 R2 | 15 | 0 | 16 | 0.0 | 0.040 | 6.5 | LOS A | 0.1 | 1.0 | 0.33 | 0.57 | 0.33 | 45.5 |
| Approach | 42 | 0 | 44 | 0.0 | 0.040 | 5.7 | LOS A | 0.1 | 1.0 | 0.33 | 0.57 | 0.33 | 45.7 |
| East: Loftus Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 6 | 0 | 6 | 0.0 | 0.122 | 4.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.02 | 0.00 | 49.4 |
| $5 \quad$ T1 | 212 | 11 | 223 | 5.2 | 0.122 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.02 | 0.00 | 49.9 |
| Approach | 218 | 11 | 229 | 5.0 | 0.122 | 0.2 | NA | 0.0 | 0.0 | 0.00 | 0.02 | 0.00 | 49.8 |
| West: Loftus Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 208 | 10 | 219 | 4.8 | 0.127 | 0.1 | LOS A | 0.1 | 0.9 | 0.06 | 0.04 | 0.06 | 49.6 |
| 12 R 2 | 15 | 0 | 16 | 0.0 | 0.127 | 5.4 | LOS A | 0.1 | 0.9 | 0.06 | 0.04 | 0.06 | 48.7 |
| Approach | 223 | 10 | 235 | 4.5 | 0.127 | 0.4 | NA | 0.1 | 0.9 | 0.06 | 0.04 | 0.06 | 49.6 |
| All Vehicles | 483 | 21 | 508 | 4.3 | 0.127 | 0.8 | NA | 0.1 | 1.0 | 0.05 | 0.07 | 0.05 | 49.3 |

Table A3: Weekday Priority Intersection Performance of Loftus Street with Yennora Avenue AM Peak Hour

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{gathered} \text { INPI } \\ \text { VOLUI } \\ \text { [ Total } \\ \text { veh/h } \\ \hline \end{gathered}$ | JT MES HV ] veh/h | DEM <br> [ Total veh/h | $\begin{gathered} \text { ND } \\ \text { VS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. Satn v/c | Aver. <br> Delay <br> sec | Level of Service | $\begin{gathered} 95 \% \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \\ \hline \end{gathered}$ | $\begin{gathered} \text { CK OF } \\ \text { JE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. <br> peed <br> km/h |
| South: Fairfield Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 891 | 39 | 938 | 4.4 | $\begin{array}{r} * \\ 0.938 \end{array}$ | 47.5 | LOS D | 61.1 | 443.9 | 1.00 | 1.11 | 1.23 | 33.7 |
| 12 R2 | 242 | 14 | 255 | 5.8 | 0.683 | 50.1 | LOS D | 13.0 | 95.4 | 0.98 | 0.84 | 1.00 | 32.3 |
| Approach | 1133 | 53 | 1193 | 4.7 | 0.938 | 48.1 | LOS D | 61.1 | 443.9 | 1.00 | 1.05 | 1.18 | 33.4 |
| East: Dursley Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 145 | 13 | 153 | 9.0 | 0.240 | 30.8 | LOS C | 5.7 | 42.9 | 0.74 | 0.75 | 0.74 | 34.9 |
| 3 R2 | 228 | 24 | 240 | 10.5 | 0.382 | 32.4 | LOS C | 9.5 | 72.6 | 0.79 | 0.78 | 0.79 | 34.5 |
| Approach | 373 | 37 | 393 | 9.9 | 0.382 | 31.8 | LOS C | 9.5 | 72.6 | 0.77 | 0.76 | 0.77 | 34.6 |
| North: Fairfield Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 513 | 32 | 540 | 6.2 | $\begin{array}{r} * \\ 0.682 \end{array}$ | 19.3 | LOS B | 13.7 | 101.0 | 0.85 | 0.83 | 0.85 | 44.5 |
| $5 \quad \mathrm{~T} 1$ | 671 | 35 | 706 | 5.2 | 0.710 | 40.3 | LOS C | 17.5 | 127.8 | 0.97 | 0.84 | 0.98 | 36.1 |
| Approach | 1184 | 67 | 1246 | 5.7 | 0.710 | 31.2 | LOS C | 17.5 | 127.8 | 0.92 | 0.84 | 0.92 | 39.3 |
| All <br> Vehicles | 2690 | 157 | 2832 | 5.8 | 0.938 | 38.4 | LOS C | 61.1 | 443.9 | 0.93 | 0.92 | 1.01 | 36.0 |

Table A4: Weekday Signalised Intersection Performance of Fairfield Road with Dursley Road AM Peak Hour

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | T <br> MES <br> HV ] <br> veh/h | $\begin{aligned} & \text { DEM/ } \\ & \text { FLOI } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% <br> [ Veh. <br> veh | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \mathrm{m} \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. <br> Speed <br> km/h |
| SouthEast: The Horsley Drive |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21a L1 | 495 | 15 | 521 | 3.0 | 0.393 | 8.9 | LOS A | 9.1 | 65.4 | 0.42 | 0.70 | 0.42 | 48.5 |
| 22 T1 | 1076 | 45 | 1133 | 4.2 | 0.759 | 29.8 | LOS C | 29.2 | 211.6 | 0.89 | 0.80 | 0.90 | 40.4 |
| 23 R2 | 378 | 18 | 398 | 4.8 | $\begin{array}{r} * \\ 0.963 \end{array}$ | 81.1 | LOS F | 28.4 | 206.7 | 1.00 | 1.08 | 1.51 | 25.1 |
| Approach | 1949 | 78 | 2052 | 4.0 | 0.963 | 34.4 | LOS C | 29.2 | 211.6 | 0.79 | 0.83 | 0.90 | 37.1 |
| NorthEast: Polding Street North |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 444 | 12 | 467 | 2.7 | 0.827 | 41.8 | LOS C | 20.5 | 146.6 | 0.97 | 1.02 | 1.09 | 35.0 |
| 26a R1 | 356 | 8 | 375 | 2.2 | 0.365 | 42.7 | LOS D | 8.5 | 60.6 | 0.89 | 0.78 | 0.89 | 31.2 |
| Approach | 800 | 20 | 842 | 2.5 | 0.827 | 42.2 | LOS C | 20.5 | 146.6 | 0.94 | 0.91 | 1.00 | 33.4 |
| NorthWest: The Horsley Drive |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 79 | 7 | 83 | 8.9 | 0.960 | 68.4 | LOS E | 56.1 | 408.1 | 1.00 | 1.17 | 1.34 | 28.5 |
| 28 T1 | 1313 | 52 | 1382 | 4.0 | $\begin{array}{r} * \\ 0.960 \end{array}$ | 62.8 | LOS E | 56.1 | 408.1 | 0.98 | 1.16 | 1.34 | 29.5 |
| 29b R3 | 173 | 5 | 182 | 2.9 | 0.496 | 48.4 | LOS D | 8.8 | 63.0 | 0.93 | 0.81 | 0.93 | 29.1 |
| Approach | 1565 | 64 | 1647 | 4.1 | 0.960 | 61.5 | LOS E | 56.1 | 408.1 | 0.97 | 1.12 | 1.30 | 29.5 |
| West: Polding Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10b L3 | 25 | 1 | 26 | 4.0 | 0.981 | 87.1 | LOS F | 36.2 | 266.0 | 1.00 | 1.15 | 1.53 | 21.4 |
| 10a L1 | 511 | 31 | 538 | 6.1 | 0.981 | 84.9 | LOS F | 36.9 | 266.9 | 1.00 | 1.15 | 1.53 | 20.9 |
| 12a R1 | 399 | 14 | 420 | 3.5 | $\begin{array}{r} * \\ 0.981 \end{array}$ | 84.7 | LOS F | 36.9 | 266.9 | 1.00 | 1.13 | 1.53 | 21.4 |
| Approach | 935 | 46 | 984 | 4.9 | 0.981 | 84.9 | LOS F | 36.9 | 266.9 | 1.00 | 1.14 | 1.53 | 21.1 |
| All <br> Vehicles | 5249 | 208 | 5525 | 4.0 | 0.981 | 52.7 | LOS D | 56.1 | 408.1 | 0.91 | 0.98 | 1.15 | 30.6 |

Table A5: Weekday Signalised Intersection Performance of the Horsley Drive with Polding Street AM Peak Hour

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{gathered} \text { INPL } \\ \text { VOLU } \\ \text { [ Total } \\ \text { veh/h } \\ \hline \end{gathered}$ | JT MES HV ] veh/h | $\begin{gathered} \text { DEMA } \\ \text { FLOI } \\ \text { [ Total } \\ \text { veh/h } \end{gathered}$ | $\begin{aligned} & \hline \text { ND } \\ & \text { IS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. <br> Delay <br> sec | Level of Service | $\begin{aligned} & \text { 95\% E } \\ & \text { Q } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | $\begin{aligned} & \mathrm{K} \text { OF } \\ & \mathrm{E} \\ & \text { Dist ] } \\ & \mathrm{m} \end{aligned}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. <br> Speed <br> km/h |
| South: Norrie Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 1 | 0 | 1 | 0.0 | 0.022 | 4.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.01 | 0.00 | 49.4 |
| $2 \quad \mathrm{~T} 1$ | 38 | 3 | 40 | 7.9 | 0.022 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.01 | 0.00 | 49.9 |
| Approach | 39 | 3 | 41 | 7.7 | 0.022 | 0.1 | NA | 0.0 | 0.0 | 0.00 | 0.01 | 0.00 | 49.9 |
| North: Norrie Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 23 | 2 | 24 | 8.7 | 0.017 | 0.0 | LOS A | 0.0 | 0.3 | 0.06 | 0.13 | 0.06 | 49.1 |
| 9 R2 | 7 | 0 | 7 | 0.0 | 0.017 | 4.7 | LOS A | 0.0 | 0.3 | 0.06 | 0.13 | 0.06 | 48.1 |
| Approach | 30 | 2 | 32 | 6.7 | 0.017 | 1.1 | NA | 0.0 | 0.3 | 0.06 | 0.13 | 0.06 | 48.8 |
| West: Kiora Crescent |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 16 | 1 | 17 | 6.3 | 0.012 | 4.7 | LOS A | 0.0 | 0.3 | 0.11 | 0.50 | 0.11 | 46.3 |
| 12 R2 | 1 | 0 | 1 | 0.0 | 0.012 | 4.8 | LOS A | 0.0 | 0.3 | 0.11 | 0.50 | 0.11 | 45.9 |
| Approach | 17 | 1 | 18 | 5.9 | 0.012 | 4.7 | LOS A | 0.0 | 0.3 | 0.11 | 0.50 | 0.11 | 46.3 |
| All Vehicles | 86 | 6 | 91 | 7.0 | 0.022 | 1.4 | NA | 0.0 | 0.3 | 0.04 | 0.15 | 0.04 | 48.8 |

Table A6: Weekday Priority Intersection Performance of Norrie Street with Kiora Crescent PM Peak Hour

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | INPUT VOLUMES | T <br> MES <br> HV] <br> veh/h | DEMAND FLOWS |  | Deg. Aver. <br> Satn Delay |  | Level of Service | 95\% Q [ Veh. veh | $\begin{aligned} & \mathrm{K} \text { OF } \\ & \mathrm{JE} \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. Que | Effective Stop Rate | $\begin{aligned} & \text { Aver. Aver. } \\ & \text { No. Speed } \\ & \text { Cycles } \end{aligned}$ |  |
| South: Norrie Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 39 | 4 | 41 | 10.3 | 0.038 | 5.3 | LOS A | 0.1 | 1.1 | 0.30 | 0.54 | 0.30 | 45.8 |
| 3 R2 | 5 | 0 | 5 | 0.0 | 0.038 | 6.6 | LOS A | 0.1 | 1.1 | 0.30 | 0.54 | 0.30 | 45.5 |
| Approach | 44 | 4 | 46 | 9.1 | 0.038 | 5.5 | LOS A | 0.1 | 1.1 | 0.30 | 0.54 | 0.30 | 45.8 |
| East: Loftus Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 15 | 1 | 16 | 6.7 | 0.113 | 4.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.04 | 0.00 | 49.1 |
| $5 \quad$ T1 | 189 | 5 | 199 | 2.6 | 0.113 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.04 | 0.00 | 49.7 |
| Approach | 204 | 6 | 215 | 2.9 | 0.113 | 0.4 | NA | 0.0 | 0.0 | 0.00 | 0.04 | 0.00 | 49.7 |
| West: Loftus Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 232 | 9 | 244 | 3.9 | 0.152 | 0.1 | LOS A | 0.3 | 1.9 | 0.10 | 0.07 | 0.10 | 49.4 |
| 12 R 2 | 30 | 2 | 32 | 6.7 | 0.152 | 5.5 | LOS A | 0.3 | 1.9 | 0.10 | 0.07 | 0.10 | 48.3 |
| Approach | 262 | 11 | 276 | 4.2 | 0.152 | 0.8 | NA | 0.3 | 1.9 | 0.10 | 0.07 | 0.10 | 49.3 |
| All <br> Vehicles | 510 | 21 | 537 | 4.1 | 0.152 | 1.0 | NA | 0.3 | 1.9 | 0.07 | 0.10 | 0.07 | 49.1 |

Table A7: Weekday Priority Intersection Performance of Loftus Street with Norrie Street PM Peak Hour

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | TT <br> MES <br> HV ] <br> veh/h |  | ND <br> S <br> HV ] <br> \% | Deg. Satn v/c | Aver. <br> Delay <br> sec | Level of Service | $\begin{gathered} 95 \% \text { E } \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | $\begin{gathered} \hline \text { K OF } \\ \text { E } \\ \text { Dist ] } \\ \mathrm{m} \\ \hline \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. <br> peed <br> km/h |
| South: Yennora Avenue |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 39 | 6 | 41 | 15.4 | 0.040 | 5.4 | LOS A | 0.2 | 1.2 | 0.30 | 0.54 | 0.30 | 45.7 |
| 3 R2 | 6 | 0 | 6 | 0.0 | 0.040 | 6.5 | LOS A | 0.2 | 1.2 | 0.30 | 0.54 | 0.30 | 45.5 |
| Approach | 45 | 6 | 47 | 13.3 | 0.040 | 5.6 | LOS A | 0.2 | 1.2 | 0.30 | 0.54 | 0.30 | 45.7 |
| East: Loftus Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 6 | 0 | 6 | 0.0 | 0.107 | 4.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.02 | 0.00 | 49.4 |
| $5 \quad$ T1 | 189 | 5 | 199 | 2.6 | 0.107 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.02 | 0.00 | 49.9 |
| Approach | 195 | 5 | 205 | 2.6 | 0.107 | 0.2 | NA | 0.0 | 0.0 | 0.00 | 0.02 | 0.00 | 49.8 |
| West: Loftus Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 232 | 9 | 244 | 3.9 | 0.139 | 0.1 | LOS A | 0.1 | 0.9 | 0.05 | 0.03 | 0.05 | 49.7 |
| 12 R 2 | 15 | 0 | 16 | 0.0 | 0.139 | 5.3 | LOS A | 0.1 | 0.9 | 0.05 | 0.03 | 0.05 | 48.7 |
| Approach | 247 | 9 | 260 | 3.6 | 0.139 | 0.4 | NA | 0.1 | 0.9 | 0.05 | 0.03 | 0.05 | 49.6 |
| All <br> Vehicles | 487 | 20 | 513 | 4.1 | 0.139 | 0.8 | NA | 0.2 | 1.2 | 0.05 | 0.07 | 0.05 | 49.3 |

Table A8: Weekday Priority Intersection Performance of Loftus Street with Yennora Avenue PM Peak Hour

| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | INPUT VOLUMES |  | DEMAND FLOWS |  | Deg. Satn v/c | Aver. <br> Delay sec | Level of Service | 95\% BACK OF QUEUE |  | Prop. Que | Effective Stop Rate | Aver. Aver. Speed km/h |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | [ Total veh/h | HV ] veh/h | [ Total veh/h | HV] |  |  |  | [ Veh veh | Dist $]$ <br> m |  |  |  |  |
| South: Fairfield Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 722 | 18 | 760 | 2.5 | $\begin{array}{r} * \\ 0.754 \end{array}$ | 16.4 | LOS B | 23.6 | 168.5 | 0.85 | 0.77 | 0.86 | 47.3 |
| 12 R 2 | 147 | 6 | 155 | 4.1 | 0.686 | 44.8 | LOS D | 6.3 | 45.4 | 1.00 | 0.85 | 1.12 | 34.0 |
| Approach | 869 | 24 | 915 | 2.8 | 0.754 | 21.2 | LOS B | 23.6 | 168.5 | 0.87 | 0.79 | 0.90 | 44.3 |
| East: Dursley Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 193 | 5 | 203 | 2.6 | 0.343 | 26.9 | LOS B | 6.1 | 43.6 | 0.80 | 0.77 | 0.80 | 36.3 |
| 3 R2 | 365 | 10 | 384 | 2.7 | 0.649 | 29.8 | LOS C | 13.0 | 93.5 | 0.91 | 0.83 | 0.91 | 35.4 |
| Approach | 558 | 15 | 587 | 2.7 | 0.649 | 28.8 | LOS C | 13.0 | 93.5 | 0.87 | 0.81 | 0.87 | 35.7 |
| North: Fairfield Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| L2 | 232 | 10 | 244 | 4.3 | $\begin{array}{r} * \\ 0.310 \end{array}$ | 13.8 | LOS A | 3.3 | 23.6 | 0.69 | 0.75 | 0.69 | 47.7 |
| $5 \quad$ T1 | 790 | 13 | 832 | 1.6 | 0.663 | 25.4 | LOS B | 14.2 | 100.6 | 0.92 | 0.79 | 0.92 | 42.4 |
| Approach | 1022 | 23 | 1076 | 2.3 | 0.663 | 22.7 | LOS B | 14.2 | 100.6 | 0.87 | 0.78 | 0.87 | 43.5 |
| All <br> Vehicles | 2449 | 62 | 2578 | 2.5 | 0.754 | 23.6 | LOS B | 23.6 | 168.5 | 0.87 | 0.79 | 0.88 | 41.7 |

# Table A9: Weekday Signalised Intersection Performance of Fairfield Road with Dursley Road PM 

 Peak Hour| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | INPUT VOLUMES [Total HV] veh/h veh/h |  | $\begin{aligned} & \text { DEMA } \\ & \text { FLOI } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | ND <br> VS <br> HV] <br> \% | Deg. Aver. Level Satn Delay Service v/c sec |  |  | 95\% BACK OF QUEUE |  | Prop. Que | Effective Stop Rate | $\begin{aligned} & \text { Aver. Aver. } \\ & \text { No. Speed } \\ & \text { Cycles } \end{aligned}$ |  |
| SouthEast: The Horsley Drive |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21a L1 | 348 | 7 | 366 | 2.0 | 0.284 | 7.5 | LOS A | 3.8 | 26.8 | 0.42 | 0.68 | 0.42 | 49.7 |
| 22 T1 | 1258 | 33 | 1324 | 2.6 | $\begin{array}{r} * \\ 0.879 \end{array}$ | 32.2 | LOS C | 26.0 | 186.4 | 1.00 | 1.07 | 1.26 | 39.3 |
| 23 R2 | 291 | 14 | 306 | 4.8 | $\begin{array}{r} * \\ 0.835 \end{array}$ | 41.7 | LOS C | 11.7 | 85.1 | 1.00 | 0.96 | 1.30 | 34.7 |
| Approach | 1897 | 54 | 1997 | 2.8 | 0.879 | 29.1 | LOS C | 26.0 | 186.4 | 0.89 | 0.98 | 1.11 | 39.7 |
| NorthEast: Polding Street North |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 241 | 8 | 254 | 3.3 | 0.356 | 12.6 | LOS A | 3.8 | 27.1 | 0.67 | 0.74 | 0.67 | 48.9 |
| 26a R1 | 517 | 13 | 544 | 2.5 | 0.603 | 32.4 | LOS C | 8.7 | 62.3 | 0.96 | 0.81 | 0.96 | 35.3 |
| Approach | 758 | 21 | 798 | 2.8 | 0.603 | 26.1 | LOS B | 8.7 | 62.3 | 0.87 | 0.79 | 0.87 | 39.4 |
| NorthWest: The Horsley Drive |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 75 | 2 | 79 | 2.7 | 0.785 | 30.1 | LOS C | 19.5 | 139.5 | 0.96 | 0.91 | 1.05 | 41.2 |
| 28 T1 | 1016 | 28 | 1069 | 2.8 | 0.785 | 24.4 | LOS B | 19.5 | 139.5 | 0.95 | 0.90 | 1.04 | 42.7 |
| 29b R3 | 76 | 2 | 80 | 2.6 | 0.245 | 33.5 | LOS C | 2.4 | 17.3 | 0.89 | 0.76 | 0.89 | 34.4 |
| Approach | 1167 | 32 | 1228 | 2.7 | 0.785 | 25.4 | LOS B | 19.5 | 139.5 | 0.94 | 0.89 | 1.03 | 42.1 |
| West: Polding Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10b L3 | 94 | 6 | 99 | 6.4 | 0.902 | 47.9 | LOS D | 16.1 | 116.5 | 1.00 | 1.07 | 1.45 | 30.1 |
| 10a L1 | 377 | 11 | 397 | 2.9 | 0.902 | 45.6 | LOS D | 16.7 | 121.2 | 1.00 | 1.07 | 1.45 | 29.8 |
| 12a R1 | 278 | 12 | 293 | 4.3 | $\begin{array}{r} * \\ 0.902 \end{array}$ | 45.5 | LOS D | 16.7 | 121.2 | 1.00 | 1.07 | 1.44 | 30.3 |
| Approach | 749 | 29 | 788 | 3.9 | 0.902 | 45.8 | LOS D | 16.7 | 121.2 | 1.00 | 1.07 | 1.45 | 30.0 |
| All <br> Vehicles | 4571 | 136 | 4812 | 3.0 | 0.902 | 30.4 | LOS C | 26.0 | 186.4 | 0.92 | 0.94 | 1.11 | 38.5 |

Table A10: Weekday Signalised Intersection Performance of the Horsley Drive with Polding Street PM Peak Hour

## APPENDIX B

## SIDRA Intersection Results for Existing Conditions with Expansion Traffic

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | INF <br> VOLU [ Total veh/h | UT MES HV ] veh/h | DEMA FLOW [ Total veh/h | ND V HV ] \% | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service | 95\% <br> Q <br> [Veh. <br> veh | $\begin{aligned} & \mathrm{K} \text { OF } \\ & \mathrm{E} \\ & \text { Dist ] } \\ & \mathrm{m} \end{aligned}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. <br> peed <br> km/h |
| South: Norrie Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 1 | 0 | 1 | 0.0 | 0.012 | 4.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.03 | 0.00 | 49.3 |
| 2 T1 | 20 | 2 | 21 | 10.0 | 0.012 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.03 | 0.00 | 49.8 |
| Approach | 21 | 2 | 22 | 9.5 | 0.012 | 0.2 | NA | 0.0 | 0.0 | 0.00 | 0.03 | 0.00 | 49.8 |
| North: Norrie Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 42 | 0 | 44 | 0.0 | 0.038 | 0.0 | LOS A | 0.1 | 0.9 | 0.06 | 0.19 | 0.06 | 48.8 |
| 9 R2 | 23 | 2 | 24 | 8.7 | 0.038 | 4.7 | LOS A | 0.1 | 0.9 | 0.06 | 0.19 | 0.06 | 47.7 |
| Approach | 65 | 2 | 68 | 3.1 | 0.038 | 1.7 | NA | 0.1 | 0.9 | 0.06 | 0.19 | 0.06 | 48.4 |
| West: Kiora Crescent |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 17 | 4 | 18 | 23.5 | 0.013 | 4.8 | LOS A | 0.1 | 0.4 | 0.08 | 0.50 | 0.08 | 46.1 |
| 12 R2 | 1 | 0 | 1 | 0.0 | 0.013 | 4.8 | LOS A | 0.1 | 0.4 | 0.08 | 0.50 | 0.08 | 46.0 |
| Approach | 18 | 4 | 19 | 22.2 | 0.013 | 4.8 | LOS A | 0.1 | 0.4 | 0.08 | 0.50 | 0.08 | 46.1 |
| All <br> Vehicles | 104 | 8 | 109 | 7.7 | 0.038 | 1.9 | NA | 0.1 | 0.9 | 0.05 | 0.21 | 0.05 | 48.3 |

Table B1: Weekday Priority Intersection Performance of Norrie Street with Kiora Crescent AM Peak Hour

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID }^{2} \end{aligned}$ | $\begin{aligned} & \text { INP } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | TT MES HV] veh/h | DEMAND FLOWS | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \\ & \hline \end{aligned}$ | Deg. Aver. Satn Delay |  | $\begin{array}{r} \text { Level } \\ \text { of } \\ \text { Service } \end{array}$ | $95 \%$ Q <br> [ Veh. <br> veh | $\begin{gathered} \mathrm{K} \text { OF } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | $\begin{aligned} & \text { Aver. Aver. } \\ & \text { No. Speed } \\ & \text { Cycles } \end{aligned}$ |  |
| South: Norrie Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 42 | 6 | 44 | 14.3 | 0.044 | 5.5 | LOS A | 0.2 | 1.3 | 0.33 | 0.55 | 0.33 | 45.7 |
| 3 R2 | 6 | 0 | 6 | 0.0 | 0.044 | 6.8 | LOS A | 0.2 | 1.3 | 0.33 | 0.55 | 0.33 | 45.4 |
| Approach | 48 | 6 | 51 | 12.5 | 0.044 | 5.7 | LOS A | 0.2 | 1.3 | 0.33 | 0.55 | 0.33 | 45.6 |
| East: Loftus Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 18 | 0 | 19 | 0.0 | 0.131 | 4.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.04 | 0.00 | 49.2 |
| $5 \quad$ T1 | 216 | 11 | 227 | 5.1 | 0.131 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.04 | 0.00 | 49.7 |
| Approach | 234 | 11 | 246 | 4.7 | 0.131 | 0.4 | NA | 0.0 | 0.0 | 0.00 | 0.04 | 0.00 | 49.7 |
| West: Loftus Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 202 | 10 | 213 | 5.0 | 0.159 | 0.4 | LOS A | 0.5 | 3.5 | 0.19 | 0.13 | 0.19 | 48.8 |
| 12 R 2 | 59 | 3 | 62 | 5.1 | 0.159 | 5.6 | LOS A | 0.5 | 3.5 | 0.19 | 0.13 | 0.19 | 47.8 |
| Approach | 261 | 13 | 275 | 5.0 | 0.159 | 1.5 | NA | 0.5 | 3.5 | 0.19 | 0.13 | 0.19 | 48.5 |
| All <br> Vehicles | 543 | 30 | 572 | 5.5 | 0.159 | 1.4 | NA | 0.5 | 3.5 | 0.12 | 0.13 | 0.12 | 48.7 |

Table B2: Weekday Priority Intersection Performance of Loftus Street with Norrie Street AM Peak Hour

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{gathered} \text { INP } \\ \text { VOLL } \\ \text { [ Total } \\ \text { veh/h } \end{gathered}$ | JT <br> MES <br> HV] <br> veh/h | $\begin{gathered} \text { DEM/ } \\ \text { FLO } \\ \text { [ Total } \\ \text { veh/h } \end{gathered}$ | $\begin{gathered} \hline \text { ND } \\ \text { VS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. Aver. Satn Delay |  | Level <br> Service | 95\% BACK OF QUEUE | $\begin{aligned} & \hline \mathrm{K} \mathrm{OF} \\ & \mathrm{JE} \\ & \text { Dist ] } \\ & \mathrm{m} \\ & \hline \end{aligned}$ | Prop. Que | Effective Stop Rate |  |  |
| South: Yennora Avenue |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 27 | 0 | 28 | 0.0 | 0.040 | 5.3 | LOS A | 0.1 | 1.0 | 0.33 | 0.57 | 0.33 | 45.9 |
| 3 R2 | 15 | 0 | 16 | 0.0 | 0.040 | 6.5 | LOS A | 0.1 | 1.0 | 0.33 | 0.57 | 0.33 | 45.5 |
| Approach | 42 | 0 | 44 | 0.0 | 0.040 | 5.7 | LOS A | 0.1 | 1.0 | 0.33 | 0.57 | 0.33 | 45.7 |
| East: Loftus Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 6 | 0 | 6 | 0.0 | 0.122 | 4.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.02 | 0.00 | 49.4 |
| $5 \quad$ T1 | 212 | 11 | 223 | 5.2 | 0.122 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.02 | 0.00 | 49.9 |
| Approach | 218 | 11 | 229 | 5.0 | 0.122 | 0.2 | NA | 0.0 | 0.0 | 0.00 | 0.02 | 0.00 | 49.8 |
| West: Loftus Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 208 | 10 | 219 | 4.8 | 0.127 | 0.1 | LOS A | 0.1 | 0.9 | 0.06 | 0.04 | 0.06 | 49.6 |
| 12 R 2 | 15 | 0 | 16 | 0.0 | 0.127 | 5.4 | LOS A | 0.1 | 0.9 | 0.06 | 0.04 | 0.06 | 48.7 |
| Approach | 223 | 10 | 235 | 4.5 | 0.127 | 0.4 | NA | 0.1 | 0.9 | 0.06 | 0.04 | 0.06 | 49.6 |
| All Vehicles | 483 | 21 | 508 | 4.3 | 0.127 | 0.8 | NA | 0.1 | 1.0 | 0.05 | 0.07 | 0.05 | 49.3 |

Table B3: Weekday Priority Intersection Performance of Loftus Street with Yennora Avenue AM Peak Hour

Proposed Expansion of a Liquid Processing Facility at 14-16 Kiora Crescent in

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & { }_{\text {ID }} \end{aligned}$ | $\begin{aligned} & \text { INPL } \\ & \text { VOLUN } \\ & \text { [ Total } \\ & \text { veh/h } \\ & \hline \end{aligned}$ | JT MES HV] veh/h | DEM <br> FLO [ Total veh/h | ND <br> WS <br> HV] <br> \% | Deg. Satn v/c | Aver. Delay sec | Level of Service | $\begin{gathered} \text { 95\% } \\ \text { Qu } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | OF JE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. <br> Speed <br> km/h |
| South: Fairfield Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 891 | 39 | 938 | 4.4 | $\begin{array}{r} * \\ 0.938 \end{array}$ | 47.5 | LOS D | 61.1 | 443.9 | 1.00 | 1.11 | 1.23 | 33.7 |
| 12 R2 | 253 | 16 | 266 | 6.3 | 0.717 | 51.2 | LOS D | 13.8 | 102.2 | 0.99 | 0.86 | 1.04 | 32.0 |
| Approach | 1144 | 55 | 1204 | 4.8 | 0.938 | 48.4 | LOS D | 61.1 | 443.9 | 1.00 | 1.05 | 1.19 | 33.3 |
| East: Dursley Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 146 | 14 | 154 | 9.6 | 0.243 | 30.8 | LOS C | 5.7 | 43.4 | 0.74 | 0.75 | 0.74 | 34.9 |
| $3 \quad \mathrm{R} 2$ | 228 | 24 | 240 | 10.5 | 0.382 | 32.4 | LOS C | 9.5 | 72.6 | 0.79 | 0.78 | 0.79 | 34.5 |
| Approach | 374 | 38 | 394 | 10.2 | 0.382 | 31.8 | LOS C | 9.5 | 72.6 | 0.77 | 0.76 | 0.77 | 34.6 |
| North: Fairfield Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 513 | 32 | 540 | 6.2 | $\begin{array}{r} * \\ 0.682 \end{array}$ | 19.3 | LOS B | 13.7 | 101.0 | 0.85 | 0.83 | 0.85 | 44.5 |
| $5 \quad$ T1 | 671 | 35 | 706 | 5.2 | 0.710 | 40.3 | LOS C | 17.5 | 127.8 | 0.97 | 0.84 | 0.98 | 36.1 |
| Approach | 1184 | 67 | 1246 | 5.7 | 0.710 | 31.2 | LOS C | 17.5 | 127.8 | 0.92 | 0.84 | 0.92 | 39.3 |
| All <br> Vehicles | 2702 | 160 | 2844 | 5.9 | 0.938 | 38.6 | LOS C | 61.1 | 443.9 | 0.93 | 0.92 | 1.02 | 35.9 |

Table B4: Weekday Signalised Intersection Performance of Fairfield Road with Dursley Road AM Peak Hour

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | JT <br> MES <br> HV ] <br> veh/h | DEM <br> FLO <br> [ Total veh/h | ND S HV ] \% | Deg. Satn <br> v/c | Aver. <br> Delay <br> sec | Level of Service | 95\% <br> Q <br> [ Veh. veh | CK OF <br> JE <br> Dist ] <br> m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. <br> Speed <br> km/h |
| SouthEast: The Horsley Drive |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21a L1 | 495 | 15 | 521 | 3.0 | 0.397 | 8.9 | LOS A | 8.6 | 61.8 | 0.44 | 0.70 | 0.44 | 48.5 |
| 22 T1 | 1076 | 45 | 1133 | 4.2 | 0.743 | 27.6 | LOS B | 23.3 | 168.7 | 0.90 | 0.80 | 0.90 | 41.4 |
| 23 R2 | 378 | 18 | 398 | 4.8 | $\begin{array}{r} * \\ 1.007 \end{array}$ | 97.1 | LOS F | 30.0 | 218.6 | 1.00 | 1.18 | 1.76 | 22.5 |
| Approach | 1949 | 78 | 2052 | 4.0 | 1.007 | 36.3 | LOS C | 30.0 | 218.6 | 0.80 | 0.85 | 0.95 | 36.3 |
| NorthEast: Polding Street North |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 444 | 12 | 467 | 2.7 | 0.817 | 37.7 | LOS C | 18.2 | 130.6 | 0.96 | 1.00 | 1.08 | 36.4 |
| 26a R1 | 357 | 9 | 376 | 2.5 | 0.362 | 39.1 | LOS C | 7.7 | 55.4 | 0.89 | 0.77 | 0.89 | 32.5 |
| Approach | 801 | 21 | 843 | 2.6 | 0.817 | 38.4 | LOS C | 18.2 | 130.6 | 0.93 | 0.90 | 1.00 | 34.8 |
| NorthWest: The Horsley Drive |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 86 | 9 | 91 | 10.5 | 0.984 | 77.2 | LOS F | 56.9 | 414.6 | 1.00 | 1.28 | 1.49 | 26.6 |
| 28 T1 | 1313 | 52 | 1382 | 4.0 | $\begin{array}{r} * \\ 0.984 \end{array}$ | 71.6 | LOS F | 56.9 | 414.6 | 0.99 | 1.29 | 1.50 | 27.6 |
| 29b R3 | 173 | 5 | 182 | 2.9 | 0.519 | 45.7 | LOS D | 8.1 | 58.3 | 0.94 | 0.81 | 0.94 | 30.0 |
| Approach | 1572 | 66 | 1655 | 4.2 | 0.984 | 69.1 | LOS E | 56.9 | 414.6 | 0.98 | 1.23 | 1.44 | 27.7 |
| West: Polding Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10b L3 | 25 | 1 | 26 | 4.0 | 0.973 | 79.1 | LOS F | 33.0 | 242.6 | 1.00 | 1.15 | 1.55 | 22.7 |
| 10a L1 | 515 | 31 | 542 | 6.0 | 0.973 | 76.9 | LOS F | 33.7 | 243.5 | 1.00 | 1.15 | 1.55 | 22.3 |
| 12a R1 | 399 | 14 | 420 | 3.5 | $\begin{array}{r} * \\ 0.973 \end{array}$ | 76.7 | LOS F | 33.7 | 243.5 | 1.00 | 1.14 | 1.54 | 22.8 |
| Approach | 939 | 46 | 988 | 4.9 | 0.973 | 76.8 | LOS F | 33.7 | 243.5 | 1.00 | 1.15 | 1.54 | 22.5 |
| All Vehicles | 5261 | 211 | 5538 | 4.0 | 1.007 | 53.6 | LOS D | 56.9 | 414.6 | 0.91 | 1.02 | 1.21 | 30.3 |

Table B5: Weekday Signalised Intersection Performance of the Horsley Drive with Polding Street AM Peak Hour

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { in } \end{aligned}$ | INPUT VOLUMES |  | DEMAND FLOWS |  | Deg. Aver. Satn Delay |  | Level of Service | $95 \%$ Qu <br> [ Veh. veh | $\begin{gathered} \mathrm{K} \text { OF } \\ \mathrm{JE} \\ \text { Dist ] } \\ \mathrm{m} \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. Aver Cycles No. Aveed |  |
| South: Norrie Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 1 | 0 | 1 | 0.0 | 0.022 | 4.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.01 | 0.00 | 49.4 |
| $2 \quad \mathrm{~T} 1$ | 38 | 3 | 40 | 7.9 | 0.022 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.01 | 0.00 | 49.9 |
| Approach | 39 | 3 | 41 | 7.7 | 0.022 | 0.1 | NA | 0.0 | 0.0 | 0.00 | 0.01 | 0.00 | 49.9 |
| North: Norrie Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 23 | 2 | 24 | 8.7 | 0.019 | 0.0 | LOS A | 0.0 | 0.4 | 0.07 | 0.14 | 0.07 | 49.0 |
| 9 R2 | 8 | 1 | 8 | 12.5 | 0.019 | 4.8 | LOS A | 0.0 | 0.4 | 0.07 | 0.14 | 0.07 | 47.9 |
| Approach | 31 | 3 | 33 | 9.7 | 0.019 | 1.3 | NA | 0.0 | 0.4 | 0.07 | 0.14 | 0.07 | 48.7 |
| West: Kiora Crescent |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 27 | 3 | 28 | 11.1 | 0.020 | 4.8 | LOS A | 0.1 | 0.6 | 0.11 | 0.50 | 0.11 | 46.2 |
| 12 R2 | 1 | 0 |  | 0.0 | 0.020 | 4.8 | LOS A | 0.1 | 0.6 | 0.11 | 0.50 | 0.11 | 45.9 |
| Approach | 28 | 3 | 29 | 10.7 | 0.020 | 4.8 | LOS A | 0.1 | 0.6 | 0.11 | 0.50 | 0.11 | 46.2 |
| All <br> Vehicles | 98 | 9 | 103 | 9.2 | 0.022 | 1.8 | NA | 0.1 | 0.6 | 0.05 | 0.19 | 0.05 | 48.4 |

Table B6: Weekday Priority Intersection Performance of Norrie Street with Kiora Crescent PM Peak Hour

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }_{\text {ID }}^{\text {Mov }} \text { Turn }$ | $\begin{aligned} & \text { INP } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | JT <br> MES <br> HV ] <br> veh/h | DEMAND FLOWS |  | Deg. Aver. Satn Delay |  | $\begin{gathered} \text { Level } \\ \text { of } \end{gathered}$ <br> Service | $\begin{array}{r} 95 \% \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \\ \hline \end{array}$ | $\begin{gathered} \mathrm{K} \text { OF } \\ \mathrm{EE} \\ \text { Dist ] } \\ \mathrm{m} \end{gathered}$ | Prop. Que | Effective Stop Rate | $\begin{aligned} & \text { Aver. Aver. } \\ & \text { No. Speed } \\ & \text { Cycles } \end{aligned}$ |  |
| South: Norrie Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| L2 | 49 | 6 | 52 | 12.2 | 0.048 | 5.4 | LOS A | 0.2 | 1.4 | 0.30 | 0.54 | 0.30 | 45.8 |
| 3 R2 | 6 | 0 | 6 | 0.0 | 0.048 | 6.7 | LOS A | 0.2 | 1.4 | 0.30 | 0.54 | 0.30 | 45.5 |
| Approach | 55 | 6 | 58 | 10.9 | 0.048 | 5.5 | LOS A | 0.2 | 1.4 | 0.30 | 0.54 | 0.30 | 45.7 |
| East: Loftus Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 15 | 1 | 16 | 6.7 | 0.113 | 4.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.04 | 0.00 | 49.1 |
| $5 \quad$ T1 | 189 | 5 | 199 | 2.6 | 0.113 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.04 | 0.00 | 49.7 |
| Approach | 204 | 6 | 215 | 2.9 | 0.113 | 0.4 | NA | 0.0 | 0.0 | 0.00 | 0.04 | 0.00 | 49.7 |
| West: Loftus Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 232 | 9 | 244 | 3.9 | 0.153 | 0.2 | LOS A | 0.3 | 2.0 | 0.10 | 0.07 | 0.10 | 49.4 |
| 12 R 2 | 31 | 3 | 33 | 9.7 | 0.153 | 5.5 | LOS A | 0.3 | 2.0 | 0.10 | 0.07 | 0.10 | 48.2 |
| Approach | 263 | 12 | 277 | 4.6 | 0.153 | 0.8 | NA | 0.3 | 2.0 | 0.10 | 0.07 | 0.10 | 49.2 |
| All <br> Vehicles | 522 | 24 | 549 | 4.6 | 0.153 | 1.1 | NA | 0.3 | 2.0 | 0.08 | 0.11 | 0.08 | 49.0 |

Table B7: Weekday Priority Intersection Performance of Loftus Street with Norrie Street PM Peak Hour

Proposed Expansion of a Liquid Processing Facility at 14-16 Kiora Crescent in

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { INP } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \\ & \hline \end{aligned}$ | TT MES HV] veh/h | $\begin{aligned} & \text { DEM } \\ & \text { FLO } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Aver. <br> Satn Delay |  | $\begin{aligned} & \text { Level } \\ & \text { of } \\ & \text { Service } \end{aligned}$ | 95\% <br> [ Veh. <br> veh | $\begin{gathered} \mathrm{K} \text { OF } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | $\begin{aligned} & \text { Aver. Aver. } \\ & \text { No. Speed } \\ & \text { Cycles } \end{aligned}$ |  |
| South: Yennora Avenue |  |  |  |  |  |  |  |  |  |  |  |  |  |
| L2 | 39 | 6 | 41 | 15.4 | 0.040 | 5.4 | LOS A | 0.2 | 1.2 | 0.30 | 0.54 | 0.30 | 45.7 |
| 3 R2 | 6 | 0 | 6 | 0.0 | 0.040 | 6.5 | LOS A | 0.2 | 1.2 | 0.30 | 0.54 | 0.30 | 45.5 |
| Approach | 45 | 6 | 47 | 13.3 | 0.040 | 5.6 | LOS A | 0.2 | 1.2 | 0.30 | 0.54 | 0.30 | 45.7 |
| East: Loftus Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 6 | 0 | 6 | 0.0 | 0.107 | 4.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.02 | 0.00 | 49.4 |
| $5 \quad$ T1 | 189 | 5 | 199 | 2.6 | 0.107 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.02 | 0.00 | 49.9 |
| Approach | 195 | 5 | 205 | 2.6 | 0.107 | 0.2 | NA | 0.0 | 0.0 | 0.00 | 0.02 | 0.00 | 49.8 |
| West: Loftus Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 233 | 9 | 245 | 3.9 | 0.140 | 0.1 | LOS A | 0.1 | 0.9 | 0.05 | 0.03 | 0.05 | 49.7 |
| 12 R 2 | 15 | 0 | 16 | 0.0 | 0.140 | 5.3 | LOS A | 0.1 | 0.9 | 0.05 | 0.03 | 0.05 | 48.7 |
| Approach | 248 | 9 | 261 | 3.6 | 0.140 | 0.4 | NA | 0.1 | 0.9 | 0.05 | 0.03 | 0.05 | 49.6 |
| All <br> Vehicles | 488 | 20 | 514 | 4.1 | 0.140 | 0.8 | NA | 0.2 | 1.2 | 0.05 | 0.07 | 0.05 | 49.3 |

Table B8: Weekday Priority Intersection Performance of Loftus Street with Yennora Avenue PM Peak Hour

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { INP } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | UT MES HV] veh/h | $\begin{gathered} \text { DEMA } \\ \text { FLOV } \\ \text { [ Total } \\ \text { veh/h } \\ \hline \end{gathered}$ | ND VS HV] \% | Deg. Satn v/c | Aver. <br> Delay <br> sec | Level of Service | $\begin{aligned} & \text { 95\% E } \\ & \text { Q } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | OF <br> JE <br> Dist ] <br> m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. <br> Speed <br> km/h |
| South: Fairfield Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 722 | 18 | 760 | 2.5 | $\begin{array}{r} * \\ 0.754 \end{array}$ | 16.4 | LOS B | 23.6 | 168.5 | 0.85 | 0.77 | 0.86 | 47.3 |
| 12 R2 | 148 | 7 | 156 | 4.7 | 0.694 | 45.0 | LOS D | 6.3 | 46.1 | 1.00 | 0.85 | 1.13 | 33.9 |
| Approach | 870 | 25 | 916 | 2.9 | 0.754 | 21.3 | LOS B | 23.6 | 168.5 | 0.87 | 0.79 | 0.90 | 44.3 |
| East: Dursley Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 200 | 7 | 211 | 3.5 | 0.358 | 27.1 | LOS B | 6.4 | 45.8 | 0.81 | 0.77 | 0.81 | 36.2 |
| 3 R2 | 368 | 10 | 387 | 2.7 | 0.654 | 29.9 | LOS C | 13.2 | 94.4 | 0.91 | 0.83 | 0.91 | 35.4 |
| Approach | 568 | 17 | 598 | 3.0 | 0.654 | 28.9 | LOS C | 13.2 | 94.4 | 0.88 | 0.81 | 0.88 | 35.7 |
| North: Fairfield Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 232 | 10 | 244 | 4.3 | $\begin{array}{r} * \\ 0.310 \end{array}$ | 13.8 | LOS A | 3.3 | 23.6 | 0.69 | 0.75 | 0.69 | 47.7 |
| $5 \quad$ T1 | 790 | 13 | 832 | 1.6 | 0.663 | 25.4 | LOS B | 14.2 | 100.6 | 0.92 | 0.79 | 0.92 | 42.4 |
| Approach | 1022 | 23 | 1076 | 2.3 | 0.663 | 22.7 | LOS B | 14.2 | 100.6 | 0.87 | 0.78 | 0.87 | 43.5 |
| All Vehicles | 2460 | 65 | 2589 | 2.6 | 0.754 | 23.6 | LOS B | 23.6 | 168.5 | 0.87 | 0.79 | 0.88 | 41.6 |

Table B9: Weekday Signalised Intersection Performance of Fairfield Road with Dursley Road PM Peak Hour

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { INPL } \\ & \text { VOLU } \end{aligned}$ <br> [ Total veh/h | UT MES HV ] veh/h | DEMAND FLOWS | $\begin{gathered} \text { ND } \\ \text { NS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. Satn v/c | Aver. Delay sec | Level of Service | $95 \%$ <br> [ Veh. veh | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ m \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. Aver. Cycles Speed |  |
| SouthEast: The Horsley Drive |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21a L1 | 348 | 7 | 366 | 2.0 | 0.284 | 7.6 | LOS A | 3.8 | 26.8 | 0.42 | 0.68 | 0.42 | 49.7 |
| 22 T1 | 1258 | 33 | 1324 | 2.6 | $\begin{array}{r} * \\ 0.879 \end{array}$ | 32.2 | LOS C | 26.0 | 186.4 | 1.00 | 1.07 | 1.26 | 39.3 |
| 23 R2 | 291 | 14 | 306 | 4.8 | $\begin{array}{r} * \\ 0.835 \end{array}$ | 41.7 | LOS C | 11.7 | 85.1 | 1.00 | 0.96 | 1.30 | 34.7 |
| Approach | 1897 | 54 | 1997 | 2.8 | 0.879 | 29.1 | LOS C | 26.0 | 186.4 | 0.89 | 0.98 | 1.11 | 39.7 |
| NorthEast: Polding Street North |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 241 | 8 | 254 | 3.3 | 0.356 | 12.6 | LOS A | 3.8 | 27.1 | 0.67 | 0.74 | 0.67 | 48.9 |
| 26a R1 | 524 | 15 | 552 | 2.9 | 0.613 | 32.4 | LOS C | 8.9 | 63.5 | 0.96 | 0.81 | 0.96 | 35.2 |
| Approach | 765 | 23 | 805 | 3.0 | 0.613 | 26.2 | LOS B | 8.9 | 63.5 | 0.87 | 0.79 | 0.87 | 39.3 |
| NorthWest: The Horsley Drive |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 75 | 2 | 79 | 2.7 | 0.785 | 30.1 | LOS C | 19.5 | 139.5 | 0.96 | 0.91 | 1.05 | 41.2 |
| 28 T1 | 1016 | 28 | 1069 | 2.8 | 0.785 | 24.4 | LOS B | 19.5 | 139.5 | 0.95 | 0.90 | 1.04 | 42.7 |
| 29b R3 | 76 | 2 | 80 | 2.6 | 0.245 | 33.5 | LOS C | 2.4 | 17.3 | 0.89 | 0.76 | 0.89 | 34.4 |
| Approach | 1167 | 32 | 1228 | 2.7 | 0.785 | 25.4 | LOS B | 19.5 | 139.5 | 0.94 | 0.89 | 1.03 | 42.1 |
| West: Polding Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10b L3 | 94 | 6 | 99 | 6.4 | 0.904 | 48.2 | LOS D | 16.2 | 117.3 | 1.00 | 1.08 | 1.46 | 30.0 |
| 10a L1 | 378 | 12 | 398 | 3.2 | 0.904 | 45.9 | LOS D | 16.8 | 121.9 | 1.00 | 1.08 | 1.46 | 29.7 |
| 12a R1 | 278 | 12 | 293 | 4.3 | $\begin{array}{r} * \\ 0.904 \end{array}$ | 45.7 | LOS D | 16.8 | 121.9 | 1.00 | 1.07 | 1.45 | 30.2 |
| Approach | 750 | 30 | 789 | 4.0 | 0.904 | 46.1 | LOS D | 16.8 | 121.9 | 1.00 | 1.08 | 1.45 | 29.9 |
| All Vehicles | 4579 | 139 | 4820 | 3.0 | 0.904 | 30.5 | LOS C | 26.0 | 186.4 | 0.92 | 0.94 | 1.11 | 38.5 |

Table B10: Weekday Signalised Intersection Performance of the Horsley Drive with Polding Street PM Peak Hour

