



# **SMEC Testing Services Pty Ltd**

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## **GEOTECHNICAL INVESTIGATION 157 REDFERN STREET, REDFERN**

**FOR**

**DEICORP PTY LIMITED**

**PROJECT NO. 17055/5911B  
REPORT NO. 09/0180**

**MARCH 2009**

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DRAWING NO. 09/0180 : BOREHOLE LOCATIONS

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## **1. INTRODUCTION**

This report presents the results of a geotechnical investigation for a proposed residential/commercial/retail development at 157 Redfern Street, Redfern. We understand the development is to consist of sixteen above ground storeys structure with basement car parking. The latter will involve excavating to a maximum depth of about 15 metres below the existing groundsurface.

The purpose of the investigation was to:

- determine the subsurface conditions at the site,
- provide comments on the foundation conditions,
- recommend foundation design parameters,
- comment on the temporary and permanent support of the proposed excavation,
- comment on the rock excavation, and
- comment on the affect of the proposed excavation on the proposed future rail line that will pass under the site.

The work was undertaken at the request of Mr. G. Colbran of DeiCorp Pty Limited.

Our scope of work did not include a contamination assessment.

## **2. SITE CONDITIONS**

The site is some 1500 m<sup>2</sup> in area and is located on the southeastern corner of the intersection of Gibbons and Redfern Streets. At the time of the fieldwork the site was occupied by the existing Redfern RSL Club. The surrounding buildings are commercial buildings.

There was no site vegetation, the non building areas were covered by pavement.

The existing ground surface falls towards the southwest, relief being about 2 metres.

### **3. GEOLOGY**

The Sydney geological series sheet, at a scale of 1:100,000 shows the site is underlain by Triassic Age Ashfield Shale of the Wianamatta Group near to the contact with Quaternary Age alluvial deposits. These are underlain by Triassic Age Hawkesbury Sandstone. Rocks within the Ashfield Shale formation typically comprise dark grey and black shale and laminite. The alluvial deposits comprise marine sands that were deposited as transgressive dunes. Hawkesbury Sandstone comprises medium to coarse grained quartz sandstone.

No rock outcrops were observed on the site.

### **4. FIELDWORK**

Three boreholes were drilled to depths of between 20.0 and 39.48 metres at the locations shown on Drawing No. 09/0180. The location of the boreholes was agreed with the client. The boreholes were advanced using either an Edson 3000 or Explorer 2000 drilling rig owned and operated by Terratest Pty Limited. The fieldwork was directed by one of our experienced geologists who chose the borehole locations and logged the subsurface conditions encountered. In order to determine soil strengths Standard Penetration Tests (SPTs) were periodically carried out in each of the boreholes. When the rock was of sufficient strength, it was cored with a diamond encrusted cutting shoe.

The subsurface conditions encountered are recorded on the borehole logs given in Appendix A. Photographs of the rock core retrieved are given in Appendix A together with a description of the terms used on the logs. Notes relating to geotechnical reports are also attached.



## 5. SUBSURFACE CONDITIONS

We have assumed the subsurface conditions encountered in the borehole are representative of the site.

In making an assessment of the subsurface conditions across a site from a limited number of boreholes there is the possibility that variations may occur between test locations. The data derived from the site investigation programme are extrapolated across the site to form a geological model and an engineering opinion is rendered about overall subsurface conditions and their likely behaviour with regard to the proposed development. No matter how comprehensive the investigation may be, it is not always possible to detect all subsurface anomalies and variations that may be present.

The subsurface conditions consist of pavement, minor filling and silty clays overlying weathered shale and sandstone. Details are given below:

**PAVEMENT AND FILL:** The pavement comprises both concrete and asphaltic concrete. Together with fill these are present to depths of 0.6 to 0.8 metres.

**SILTY CLAYS:** These are present to depths of 2.7 to 5.5 metres. The strength of these materials range between firm to stiff and very stiff.

**SHALE:** Weathered shale was observed in all boreholes. In BH2 and BH3, the shale was observed to the depth of drilling, 20.74 and 20.0 metres. In BH1, the shale was present to a depth of 28.8 metres. The shale is of extremely low strength when first encountered and becomes high strength with depth.

**SANDSTONE:** Weathered sandstone was encountered in BH1 below a depth of 28.8 metres to the depth of drilling, 39.48 metres. The rock is medium and high strength and generally massive.

When water is used in the drilling process it can mask the real water level present. The groundwater depths were measured on various occasions. The depths recorded are given below:

Date	Depth (m)		
	BH1	BH2	BH3
26/2/2009	5.0	4.5	-
10/3/2009	5.0	4.5	5.0
18/3/2009	5.0	4.2	5.0

## **6. EXCAVATION CONDITIONS AND SUPPORT**

The construction of the basement will involve excavating near to the property boundaries. It is of course important that the excavation is adequately supported at all times and that it does not endanger the adjacent properties.

Conventional earth moving equipment, such as excavators, should be capable of removing the soils and some of the jointed rock to a depth of 7 to 8 metres. Below these depths, rock excavation will more than likely require some form of assistance. Care should be taken when using this equipment not to damage adjacent buildings. Based on the subsurface conditions observed in the boreholes and general experience in this geological environment, it is expected that excavation on this site will encounter medium and high strength shales. It is important that the excavation contractor has equipment capable of removing this rock.

Excavators alone without assistance from a breaker will probably not be able to remove any significant amount of the rock below the jointed rock. Hydraulic breakers mounted on an excavator or jack hammers will be required to break up the majority of the rock before it can be removed using an excavator. Other forms of excavation that may be required include ripping, sawing and grinding.

Particular care will be required to ensure that buildings or other developments on adjacent properties are not damaged when excavating the rock. At their closest point some buildings will be adjacent to the excavation. The structures on the adjacent properties are likely founded directly on the shale. Buildings founded directly on rock can often be very susceptible to damage from vibrations transmitted directly through competent rock.

It is extremely difficult to definitively predict the affect of the above type of excavation on adjacent buildings. There are various relations available that have been used to carry out such predictions, but these do not easily take account of the natural variability of rock. There have been many cases in Sydney where predictions based on experience of the above relationships have been proved inaccurate and adjacent structures have been damaged. For these reasons the following comments should only be taken as a guide. Particular care must be exercised when removing the rock and onsite guidance by a vibration specialist will likely be necessary during the early part of the excavation.

When excavating rock adjacent to buildings in adjoining properties a specialist should be employed to monitor onsite vibrations and advise the permissible size of excavation equipment that can be used. If a specialist is not engaged, rock should not be excavated closer than 20 metres to adjoining buildings.

Saw cutting should be carried out before any rock breaking is commenced. It would be appropriate before commencing excavation to undertake a dilapidation survey of any adjacent structures that may potentially be damaged. This will provide a reasonable basis for assessing any future claims.

Because of the proximity of the excavation to some of the property boundaries, temporary support will be required for the soils and rock. Reinforced concrete piles with shotcrete infill are probably the most cost-effective option for providing this support. The piles may be drilled and fixed into the material below the base of the excavation. This will provide one fixing point. Where the pile toe is fixed in the rock a passive pressure of 600 kPa may be adopted for the design with a minimum embedment of 1 metre. Additional support may be provided using rows of anchors. These anchors may be installed into the jointed

shale and proportioned using an allowable bond of 500 kPa. All bond lengths should be located outside the active wedge and should not be less than 3 metres.

It is vital that an experienced engineering geologist or geotechnical engineer observes that excavation as it progresses. At that time he will be able to recommend any support that is required for either temporary or permanent conditions.

When considering the design of the supports, it will be necessary to allow for the ground surface slope, loading from adjacent structures and water pressure. Where the structures are within the zone of influence of the excavation, it will be necessary to adopt  $K_0$  conditions when designing the temporary support. Anchors or props can be used to provide the required support. If anchors extend into adjoining properties, it will be necessary to obtain the permission of the property owners. When props or anchors are used for support, a rectangular earth pressure distribution should be adopted on the active side of the support. The permanent basement support should be designed assuming  $K_0$  conditions.

The following parameters are suggested for the design of the temporary and permanent retaining wall system:

Soil & Weathered Shale (to a depth of 8 metres)

Active Earth Pressure Coefficient ( $K_a$ )	=	0.4
At Rest Pressure Coefficient ( $K_0$ )	=	0.5
Total (Bulk) Density	=	20 kN/m <sup>3</sup>

Shale (below a depth of 8 metres)

Earth Pressure Coefficient	=	0.1 or horizontal pressure of 10 kPa (whichever is smaller)
Total (Bulk) Density	=	23 kN/m <sup>3</sup>

## **7. FOUNDATIONS**

The allowable bearing pressures given below have been determined using the procedures given by Pells et al, in their paper titled “Design Loadings for Foundations on Shale and Sandstone in the Sydney Region,” published in the Australian Geomechanics Journal, 1998.

At the proposed depth of founding (15 metres) the medium to high strength rock is assessed to be at least Class III shale. An allowable bearing pressure of 3.5 MPa may be used to proportion the footings at this level.

In order to ensure the bearing values given can be achieved, care should be taken to ensure the base of the excavations are free of all loose material prior to concreting. It is recommended that all footing excavations be protected with a layer of blinding concrete as soon as possible, preferably immediately after excavating, cleaning, inspection and approval. The presence of groundwater needs to be considered when pouring concrete.

Some groundwater flow can be expected into the excavation. The amount of water is unknown, however, a sump with a pump should be adequate to remove most of the water.

## **8. PROPOSED RAILCORP TUNNEL**

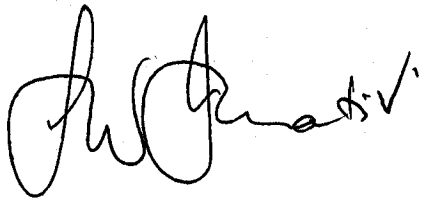
As noted above, we have been informed that RailCorp have plans for a tunnel below the site. We have been informed this tunnel is some 35 metres below the proposed base of the excavation and that provided there is at least 10 metres of sound sandstone above the tunnel, there will be no impact on the rail infrastructure.

Fresh generally high strength sandstone was encountered in BH1 below a depth of 28.8 metres. This means there is about 21 metres of sound sandstone over the proposed tunnel. Therefore, the minimum requirements of RailCorp have been more than satisfied and the proposed construction will not impact on the proposed tunnel.

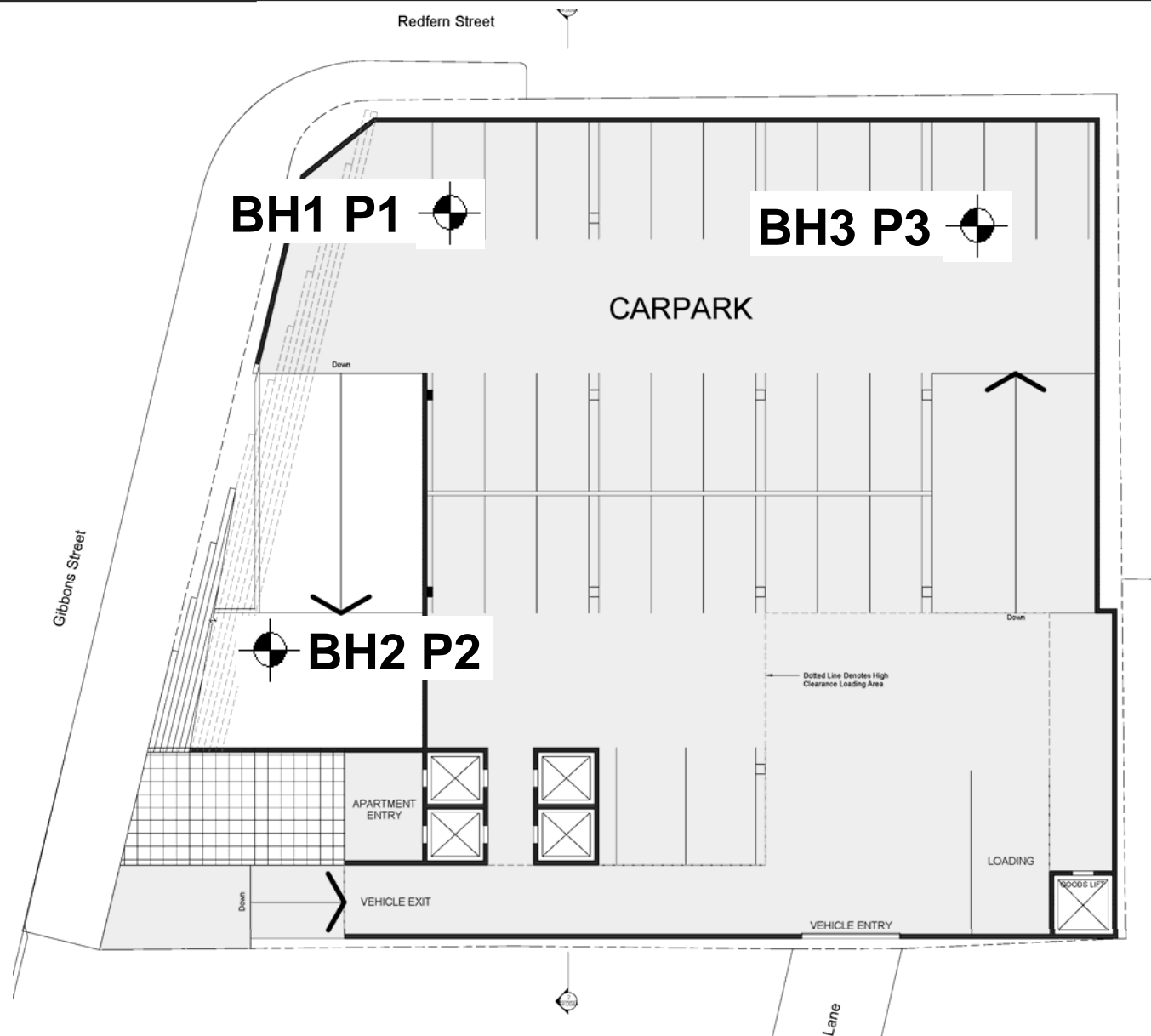
## 9. FINAL COMMENTS

During construction should the subsurface conditions vary from those inferred above we should be contacted to determine if any changes should be made to our recommendations.

The exposed bearing surfaces should be inspected by a geotechnical engineer to ensure the bearing value given have been achieved.

A handwritten signature in black ink, appearing to read 'L. Ihnativ'.

Laurie Ihnativ, BE, MEngSc, MBA  
Manager, SMEC Testing Services Pty Limited



**SMEC TESTING SERVICES Pty. Ltd.**

Scale: Unknown

Date: February 2009

**Client: DEICORP PTY LIMITED**

**GEOTECHNICAL INVESTIGATION  
157 REDFERN STREET, REDFERN  
BOREHOLE LOCATIONS**

Project No.  
17055/5911B

Drawing No: 09/0180

## NOTES RELATING TO GEOTECHNICAL REPORTS

### Introduction

These notes have been provided to outline the methodology and limitations inherent in geotechnical reporting. The issues discussed are not relevant to all reports and further advice should be sought if there are any queries regarding any advice or report.

When copies of reports are made, they should be reproduced in full.

### Geotechnical Reports

Geotechnical reports are prepared by qualified personnel on the information supplied or obtained and are based on current engineering standards of interpretation and analysis.

Information may be gained from limited subsurface testing, surface observations, previous work and is supplemented by knowledge of the local geology and experience of the range of properties that may be exhibited by the materials present. For this reason, geotechnical reports should be regarded as interpretative rather than factual documents, limited to some extent by the scope of information on which they rely.

Where the report has been prepared for a specific purpose (eg. design of a three-storey building), the information and interpretation may not be appropriate if the design is changed (eg. a twenty storey building). In such cases, the report and the sufficiency of the existing work should be reviewed by SMEC Testing Services Pty Limited in the light of the new proposal.

Every care is taken with the report content, however, it is not always possible to anticipate or assume responsibility for the following conditions:

- Unexpected variations in ground conditions. The potential for this depends on the amount of investigative work undertaken.
- Changes in policy or interpretation by statutory authorities.
- The actions of contractors responding to commercial pressures.

If these occur, SMEC Testing Services Pty Limited would be pleased to resolve the matter through further investigation, analysis or advice.

### Unforeseen Conditions

Should conditions encountered on site differ markedly from those anticipated from the information contained in the report, SMEC

Testing Services Pty Limited should be notified immediately. Early identification of site anomalies generally results in any problems being more readily resolved and allows re-interpretation and assessment of the implications for future work.

### Subsurface Information

Logs of a borehole, recovered core, test pit, excavated face or cone penetration test are an engineering and/or geological interpretation of the subsurface conditions. The reliability of the logged information depends on the drilling/testing method, sampling and/or observation spacings and the ground conditions. It is not always possible or economic to obtain continuous high quality data. It should also be recognised that the volume or material observed or tested is only a fraction of the total subsurface profile.

Interpretation of subsurface information and application to design and construction must take into consideration the spacing of the test locations, the frequency of observations and testing, and the possibility that geological boundaries may vary between observation points.

Groundwater observations and measurements outside of specially designed and constructed piezometers should be treated with care for the following reasons:

- In low permeability soils groundwater may not seep into an excavation or bore in the short time it is left open.
- A localised perched water table may not represent the true water table.
- Groundwater levels vary according to rainfall events or season.
- Some drilling and testing procedures mask or prevent groundwater inflow.

The installation of piezometers and long term monitoring of groundwater levels may be required to adequately identify groundwater conditions.

### Supply of Geotechnical Information or Tendering Purposes

It is recommended tenderers are provided with as much geological and geotechnical information that is available and that where there are uncertainties regarding the ground conditions, prospective tenders should be provided with comments discussing the range of likely conditions in addition to the investigation data.





## **APPENDIX A**

### **BOREHOLE LOGS & EXPLANATION SHEETS**

Client: DeiCorp Pty Limited		Project No.: 17055/5911B		<b>BOREHOLE NO.: BH 1</b>		
Project: 157 Redfern Street, Redfern		Date : February 18, 2009				
Location: Refer to Drawing No. 09/0180		Logged: JK		Sheet 1 of 8		
W A T E R L E V E	S A M P L E S	DEPTH (m)	DESCRIPTION OF DRILLED PRODUCT  (Soil type, colour, grain size, plasticity, minor components, observations)	S Y M B O L	CONSISTENCY (cohesive soils) or RELATIVE DENSITY (sands and gravels)	M O I S T U R E
SPT 1.5-1.95 m 3, 4, 6 N = 10		0.0	CONCRETE (200 mm thick)			
		0.5	CLAYEY GRAVELLY SAND: light grey/brown, fine to medium grained, gravel	SC	MEDIUM DENSE	M
		1.0	FILL			
		1.5	SILTY CLAY: orange brown with light grey, medium plasticity	CL	FIRM TO STIFF	M
		2.0	SILTY CLAY: light grey with red brown and orange brown, medium plasticity, trace of ironstone gravel	CL	STIFF	M
		2.5				
		3.0	SHALE: light grey/brown with orange brown, fine grained sand, clay seams		EXTREMELY LOW STRENGTH	D
		3.5				
		4.0	WASHBORE DRILLING DISCONTINUED AT 4.0 M			
		5.0	For core details, refer to core log sheets			
NOTES: D - disturbed sample      U - undisturbed tube sample      B - bulk sample WT - level of water table or free water      N - Standard Penetration Test (SPT)				Contractor: Terratest Equipment: Edson 3000		
See explanation sheets for meaning of all descriptive terms and symbols				Hole Diameter (mm): 100 Angle from Vertical (°) 0		

SMEC Testing Services Pty Ltd										GEOTECHNICAL LOG - CORED BOREHOLE												
Client: DeiCorp Pty Limited					Project / STS No.: 17055/5911B					BOREHOLE NO.: BH 1												
Project: 157 Redfern Street, Redfern					Date : February 18, 2009					Sheet 2 of 8												
Location: Refer to Drawing No. 09/0180					Logged: JK					Checked By: JH												
DRILLING			MATERIAL STRENGTH										DISCONTINUITIES									
Method	Water	Recovery	Depth (m)	Rock Type (Colour, Grain Size, Structure & Minor Components)	Weathering	Estimated Rock Strength						Joint Spacing (mm)					Visual	Additional Data (Joints, partings, seams, zones etc. Description, orientation, infilling, or coating, shape, roughness, thickness, other)				
						Extremely Low	Very Low	Low	Medium	High	Very High	Extremely High	20	40	100	300			1000			
			1.0 2.0 3.0 4.0																			
				For non core details, refer to non core log sheets																		
			4.0	START CORING AT 4.0 M																		
N Q  C O R I N G		11%	5.0	NO CORE 4.0 TO 5.78 M																		
			6.0	SHALE: orange brown with light grey and occasional cark grey, fine grained	MW/ HW												5.78-6.0 m, Jt, 0-15 deg. Ir, Ro Cy, fe					
Notes:																Contractor: Terratest Equipment: Edson 3000 Hole Diameter (mm): Angle from Vertical (°):						
See explanation sheets for meaning of all descriptive terms and symbols																						





SMEC Testing Services Pty Ltd										GEOTECHNICAL LOG - CORED BOREHOLE												
Client: DeiCorp Pty Limited					Project / STS No.: 17055/5911B					BOREHOLE NO.: BH 1												
Project: 157 Redfern Street, Redfern					Date : February 18, 2009					Sheet 5 of 8												
Location: Refer to Drawing No. 09/0180					Logged: JK					Checked By: JH												
DRILLING			MATERIAL STRENGTH										DISCONTINUITIES									
Method	Water	Recovery	Depth (m)	Rock Type (Colour, Grain Size, Structure & Minor Components)	Weathering	Estimated Rock Strength						Joint Spacing (mm)					Visual	Additional Data (Joints, partings, seams, zones etc. Description, orientation, infilling, or coating, shape, roughness, thickness, other)				
						Extremely Low	Very Low	Low	Medium	High	Very High	Extremely High	20	40	100	300			1000			
N	Q	100%		SHALE: dark grey with light grey, fine grained	Fr												18.56 m, Jt, 0 deg. Pl, Sm					
																	18.93 m, Pt, 0 deg. Pl, Sm 19.02-19.04 m, Jt, -45 deg. Ir, Ro 19.07-19.11 m, Jt, 45 deg. Pl, Sm 19.24-19.26 m, Jt, 20 deg. Pl, Sm					
C	O		19.0														19.68 m, Jt, 2 deg. Pl, Sm 19.8 m, Jt, 0 deg. PL, Ro					
																	20.08 m, Jt, 0 deg. PL, Sm 20.2 m, Jt, 0 deg. Pl, Sm 20.33 m, Jt, 0 deg. PL, Sm					
R	I		20.0														20.73 m, Jt, 0 deg. Pl, Sm 20.91 m, Pt, 0 deg. PL, Sm					
																	21.26 m, Jt, 0 deg. PL, Sm 21.5 m, Pt, 0 deg. Pl, Ro					
N	G		21.0														21.74 m, Jt, 0 deg. PL, Sm 21.88 m, Jt, 2 deg. Pl, Sm					
																	22.03 m, Pt, 0 deg. Pl, Sm 22.17 m, Jt, 0 deg. PL, Ro					
		100%	22.0														22.38 m, Pt, 0 deg. Pl, Sm 22.59 m, Pt, 0 deg. Pl, Sm					
																	23.17 m, Pl, 0 deg. Ro, cy veneer 23.2 m, Jt, 0 deg. PL, Sm					
			23.0														22.55 m, Pt, 0 deg. Pl, Ro 23.63-23.7 m, Jt, Und. Tight 23.73-23.76 m, Jt, 5-30 deg. Ir, Ro					
			24.0																			
Notes:																Contractor: Terratest Equipment: Edson 3000 Hole Diameter (mm): Angle from Vertical (°):						
See explanation sheets for meaning of all descriptive terms and symbols																						

Revision:5







Project: 157 Redfern St., Redfern  
Project No: 17055/5911B  
Client: DelCorp Pty Limited  
Date Cored: 18/02/09  
Borehole No: 1  
Depth (m): Start 4.00 - 9.00  
Box 1 of 8



4	START	NO CORE	
5		NO CORE	
6		NO CORE	6.75
7			
8		NO CORE	8.50

Project: 157 Redfern St., Redfern  
Project No: 17055/5911B  
Client: DeiCorp Pty Limited  
Date Cored: 18/02/09  
Borehole No: 1  
Depth (m): 9.00 - 14.00  
Box 2 of 8

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9 NO CORE

10 NO CORE

11

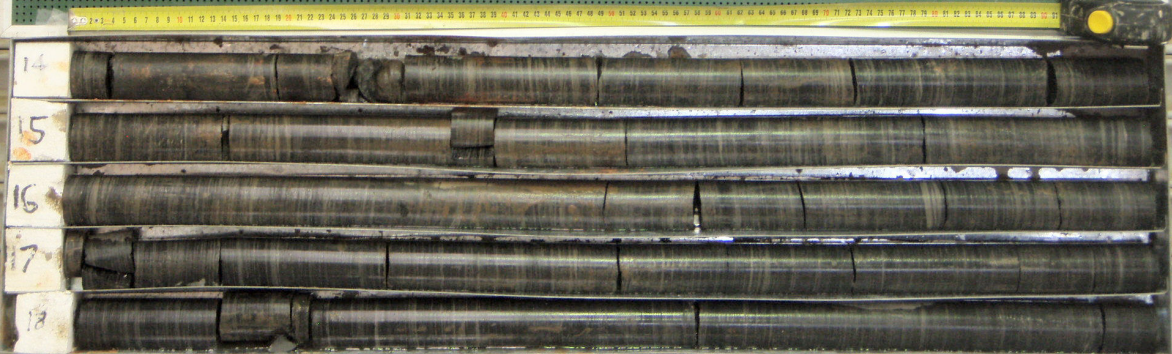
12

13



Project: 157 Redfern St., Redfern  
Project No: 17055/5911B  
Client: DeiCorp Pty Limited  
Date Cored: 18/02/09  
Borehole No: 1  
Depth (m): 14.00 - 19.00  
Box 3 of 8

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Project: 157 Redfern St., Redfern  
Project No: 17055/5911B  
Client: DelCorp Pty Limited  
Date Cored: 18/02/09  
Borehole No: 1  
Depth (m): 19.00 - 24.00  
Box 4 of 8

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19

20

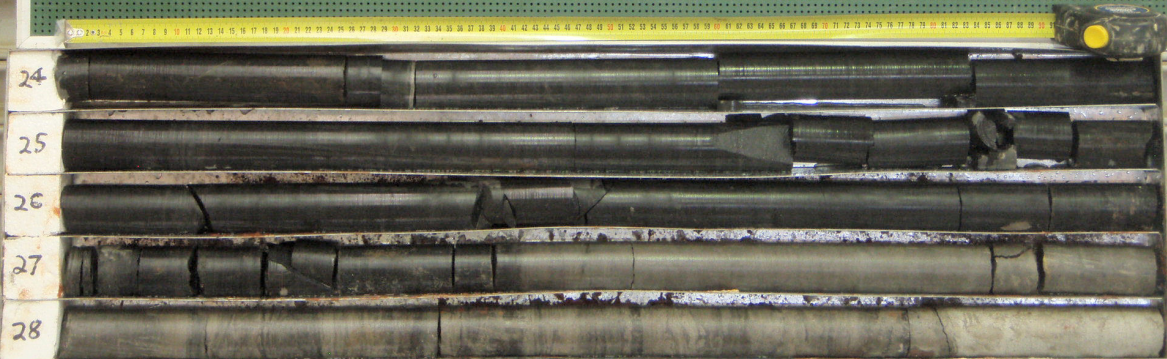
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23



Project: 157 Redfern St., Redfern  
Project No: 17055/5911B  
Client: DeiCorp Pty Limited  
Date Cored: 18/02/09  
Borehole No: 1  
Depth (m): 24.00 - 29.00  
Box 5 of 8



Project: 157 Redfern St., Redfern  
Project No: 17055/5911B  
Client: DelCorp Pty Limited  
Date Cored: 18/02/09  
Borehole No: 1  
Depth (m): 29.00 - 34.00  
Box 6 of 8

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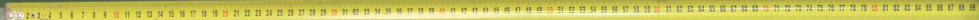
32

33



Project: 157 Redfern St., Redfern  
Project No: 17055/5911B  
Client: DelCorp Pty Limited  
Date Cored: 18/02/09  
Borehole No: 1  
Depth (m): 34.00 - 39.00  
Box 7 of 8

**SMEC**  
**Testing**  
**Services**



34

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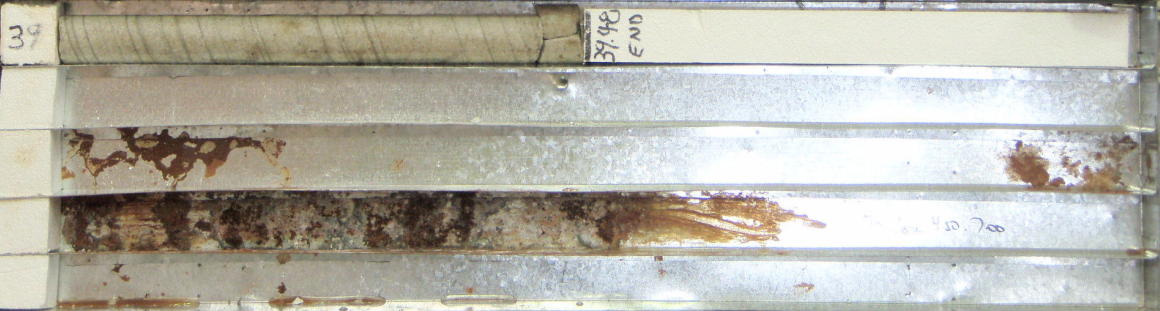
37

38



Project: 157 Redfern St., Redfern  
Project No: 17055/5911B  
Client: DelCorp Pty Limited  
Date Cored: 16/02/09  
Borehole No: 1  
Depth (m): 39.00 - 39.48 End  
Box 8 of 8

**SMEC**  
**Testing**  
**Services**



Revision 4

Client: DeiCorp Pty Limited		Project No.: 17055/5911B		BOREHOLE NO.: BH 2		
Project: 157 Redfern Street, Redfern		Date : February 19, 2009				
Location: Refer to Drawing No. 09/0180		Logged: JK		Sheet 2 of 5		
W A T E R L E	S A M P L E S	DEPTH (m)	DESCRIPTION OF DRILLED PRODUCT  (Soil type, colour, grain size, plasticity, minor components, observations)	S Y M B O L	CONSISTENCY (cohesive soils) or RELATIVE DENSITY (sands and gravels)	M O I S T U R E
			SHALE: dark brown/grey with occasional orange brown, fine grained WASHBORE DRILLING DISCONTINUED AT 6.1 M		EXTREMELY LOW STRENGTH	D
			For core details, refer to core log sheets			
		7.0				
		8.0				
		9.0				
		10.0				
		11.0				
NOTES: D - disturbed sample                      U - undisturbed tube sample                      B - bulk sample WT - level of water table or free water                      N - Standard Penetration Test (SPT)				Contractor: Terratest Equipment: Explorer 2000		
See explanation sheets for meaning of all descriptive terms and symbols				Hole Diameter (mm): 100 Angle from Vertical (°) 0		







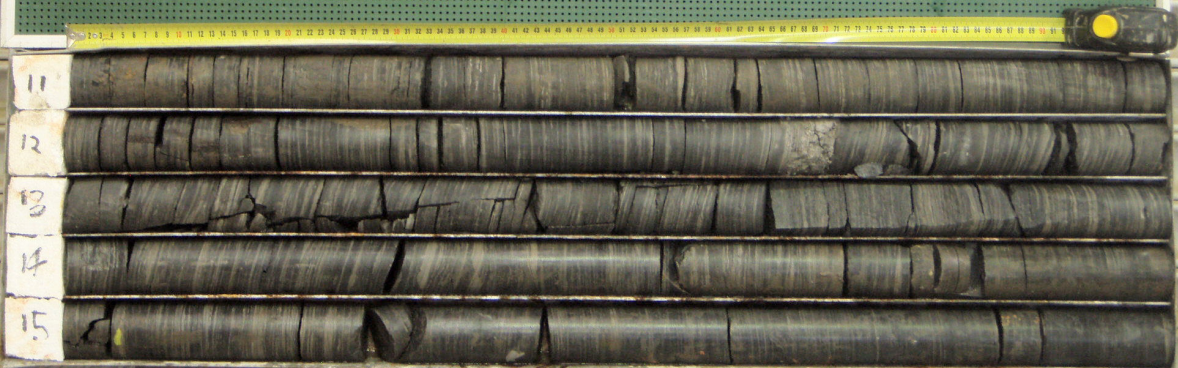


Project: 157 Redfern St., Redfern  
Project No: 17055/5911B  
Client: DeiCorp Pty Limited  
Date Cored: 18/02/09  
Borehole No: 2  
Depth (m): Start 6.10 - 11.00  
Box 1 of 3



Project: 157 Redfern St., Redfern  
Project No: 17055/5911B  
Client: DeiCorp Pty Limited  
Date Cored: 18/02/09  
Borehole No: 2  
Depth (m): 11.00 - 16.00  
Box 2 of 3

**SMEC**  
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Project: 157 Redfern St., Redfern  
Project No: 17055/5911B  
Client: DeiCorp Pty Limited  
Date Cored: 18/02/09  
Borehole No: 2  
Depth (m): 16.00 - 20.74 End  
Box 3 of 3

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19

20

20.74 End

Client: DeiCorp Pty Limited		Project No.: 17055/5911B		<b>BOREHOLE NO.: BH 3</b>		
Project: 157 Redfern Street, Redfern		Date : February 20, 2009		Sheet 1 of 5		
Location: Refer to Drawing No. 09/0180		Logged: JK				
W A T E R L E V E	S A M P L E S	DEPTH (m)	DESCRIPTION OF DRILLED PRODUCT  (Soil type, colour, grain size, plasticity, minor components, observations)	S Y M B O L	CONSISTENCY (cohesive soils) or RELATIVE DENSITY (sands and gravels)	M O I S T U R E
			ASPHALT/SANDY GRAVEL: dark grey, fine to medium grained	GW	DENSE	D
			CLAYEY SAND: dark brown with orange brown, fine to medium grained, trace of gravel	SC	STIFF	M
			FILL			
		1.0	SILTY CLAY: orange brown with red brown and light grey, medium plasticity. occasional ironstone gravel	CL	STIFF	M
	SPT 1.5-1.95 m 4, 4, 7 N = 11	2.0	SILTY CLAY: light grey with red brown, medium plasticity, trace of ironstone gravel occasional bands of shale and ironstone	CL	STIFF WITH BANDS OF VERY STIFF	M
	SPT 2.5-2.95 m 7, 12, 14 N = 26	3.0				
	SPT 4.0-4.45 m 12, 16, 19 N = 35	4.0				
		5.0	SHALE: orange brown with red brown and dark grey, fine grained, clay seams		EXTREMELY LOW STRENGTH	D
NOTES: D - disturbed sample      U - undisturbed tube sample      B - bulk sample WT - level of water table or free water      N - Standard Penetration Test (SPT)				Contractor: Terratest Equipment: Edson 3000		
See explanation sheets for meaning of all descriptive terms and symbols				Hole Diameter (mm): 100 Angle from Vertical (°): 0		

Client: DeiCorp Pty Limited		Project No.: 17055/5911B		BOREHOLE NO.: BH 3		
Project: 157 Redfern Street, Redfern		Date : February 20, 2009				
Location: Refer to Drawing No. 09/0180		Logged: JK		Sheet 2 of 5		
W A T E R L E	S A M P L E S	DEPTH (m)	DESCRIPTION OF DRILLED PRODUCT  (Soil type, colour, grain size, plasticity, minor components, observations)	S Y M B O L	CONSISTENCY (cohesive soils) or RELATIVE DENSITY (sands and gravels)	M O I S T U R E
		7.0	SHALE: orange brown with red brown and dark grey, fine grained, clay seams		EXTREMELY LOW STRENGTH	D
		8.0				
			WASHBORE DRILLING DISCONTINUED AT 8.5 M			
		9.0	For core details, refer to core log sheets			
		10.0				
		11.0				
NOTES: D - disturbed sample                      U - undisturbed tube sample                      B - bulk sample WT - level of water table or free water                      N - Standard Penetration Test (SPT)				Contractor: Terratest Equipment: Edson 3000		
See explanation sheets for meaning of all descriptive terms and symbols				Hole Diameter (mm): 100 Angle from Vertical (°) 0		





SMEC Testing Services Pty Ltd										GEOTECHNICAL LOG - CORED BOREHOLE												
Client: DeiCorp Pty Limited					Project / STS No.: 17055/5911B					BOREHOLE NO.: BH 3												
Project: 157 Redfern Street, Redfern					Date : February 20, 2009					Sheet 5 of 5												
Location: Refer to Drawing No. 09/0180					Logged: JK					Checked By: JH												
DRILLING			MATERIAL STRENGTH										DISCONTINUITIES									
Method	Water	Recovery	Depth (m)	Rock Type (Colour, Grain Size, Structure & Minor Components)	Weathering	Estimated Rock Strength						Joint Spacing (mm)					Visual	Additional Data (Joints, partings, seams, zones etc. Description, orientation, infilling, or coating, shape, roughness, thickness, other)				
						Extremely Low	Very Low	Low	Medium	High	Very High	Extremely High	20	40	100	300			1000			
N M L C  C O R I N G		100%	18.43	SHALE: dark grey with light grey bands, fine grained	Fr												18.43-19.08 m, Jt, 90 deg. Ir, Ro, fractured					
			18.95																			
			19.00																			
			19.24																19.24 m, Jt, 0 deg. Pl, Sm			
			19.40																19.4 m, Jt, 0 deg. Pl, Sm			
			19.66																19.66 m, Jt, 0 deg. PL, Ro			
			19.95																19.95 m, Pt, 0 deg. Pl, Sm			
			20.00																			
			20.00																			
			20.00																			
			21.00	BOREHOLE DISCONTINUED AT 20.0 M																		
			21.50																			
			22.00																			
			22.50																			
			23.00																			
			23.50																			
			24.00																			
			24.50																			
			25.00																			
			25.50																			
Notes:															Contractor: Terratest Equipment: Edson 3000 Hole Diameter (mm): Angle from Vertical (°):							
See explanation sheets for meaning of all descriptive terms and symbols																						



Project: 157 Redfern St., Redfern  
Project No: 17055/5911B  
Client: DelCorp Pty Limited  
Date Cored: 18/02/09  
Borehole No: 3  
Depth (m): Start 8.50 - 13.00  
Box 1 of 3



BH: 17055

Start

End No  
Core

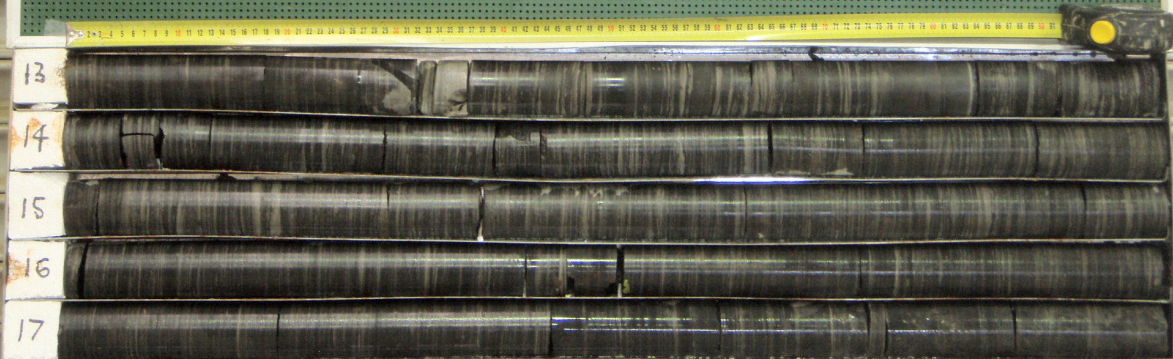
9

10

11

12

Project: 157 Redfern St., Redfern  
Project No: 17055/5911B  
Client: DelCorp Pty Limited  
Date Cored: 18/02/09  
Borehole No: 3  
Depth (m): 13.00 - 18.00  
Box 2 of 3





Project: 157 Redfern St., Redfern  
Project No: 17055/5911B  
Client: DelCorp Pty Limited  
Date Cored: 18/02/09  
Borehole No: 3  
Depth (m): 18.00 - 20.00 End  
Box 3 of 3

**SMEC**  
**Testing**  
**Services**



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## E1. CLASSIFICATION OF SOILS

### E1.1 Soil Classification and the Unified System

An assessment of the site conditions usually includes an appraisal of the data available by combining values of engineering properties obtained by the site investigation with descriptions, from visual observation of the materials present on site.

The system used by SMEC in the identification of soil is the Unified Soil Classification system (USC) which was developed by the US Army Corps of Engineers during World War II and has since gained international acceptance and has been adopted in its metricated form by the Standards Association of Australia.

The Australian Site Investigation Code (AS1726-1981, Appendix D) recommends that the description of a soil includes the USC group symbols which are an integral component of the system.

The soil description should contain the following information in order:

#### Soil composition

- SOIL NAME and USC classification symbol (IN BLOCK LETTERS)
- plasticity or particle characteristics
- colour
- secondary and minor constituents (name estimated proportion, plasticity or particle characteristics, colour)

#### Soil condition

- moisture condition
- consistency or density index

#### Soil structure

- structure (zoning, defects, cementing)

#### Soil origin

interpretation based on observation eg FILL, TOPSOIL, RESIDUAL, ALLUVIUM.

### E1.2 Soil Composition

- (a) Soil Name and Classification Symbol

The USC system is summarized in Figure E1.2.1. The primary division separates soil types on the basis of particle size into:

- Coarse grained soils - more than 50% of the material less than 60 mm is larger than 0.06 mm (60  $\mu$ m).
- Fine grained soils - more than 50% of the material less than 60 mm is smaller than 0.06 mm (60  $\mu$ m).

Initial classification is by particle size as shown in Table E1.2.1. Further classification of fine grained soils is based on plasticity.

TABLE E1.2.1 - CLASSIFICATION BY PARTICLE SIZE

NAME	SUB-DIVISION	SIZE
Clay (1)		< 2 $\mu$ m
Silt (2)		2 $\mu$ m to 60 $\mu$ m
Sand	Fine Medium Coarse	60 $\mu$ m to 200 $\mu$ m 200 $\mu$ m to 600 $\mu$ m 600 $\mu$ m to 2 mm
Gravel (3)	Fine Medium Coarse	2 mm to 6 mm 6 mm to 20 mm 20 mm to 60 mm
Cobbles (3)		60 mm to 200 mm
Boulders (3)		> 200 mm

Where a soil contains an appropriate amount of secondary material, the name includes each of the secondary components (greater than 12%) in increasing order of significance, eg sandy silty clay.

Minor components of a soil are included in the description by means of the terms "some" and "trace" as defined in Table E1.2.2.

TABLE E1.2.2 - MINOR SOIL COMPONENTS

TERM	DESCRIPTION	APPROXIMATE PROPORTION (%)
Trace	presence just detectable, little or no influence on soil properties	0-5
Some	presence easily detectable, little influence on soil properties	5-12

The USC group symbols should be included with each soil description as shown in Table E1.2.3

TABLE E1.2.3 - SOIL GROUP SYMBOLS

SOIL TYPE	PREFIX
Gravel	G
Sand	S
Silt	M
Clay	C
Organic	O
Peat	Pt

The group symbols are combined with qualifiers which indicate grading, plasticity or secondary components as shown on Table E1.2.4

TABLE E1.2.4 - SOIL GROUP QUALIFIERS

SUBGROUP	SUFFIX
Well graded	W
Poorly Graded	P
Silty	M
Clayey	C
Liquid Limit <50% - low to medium plasticity	L
Liquid Limit >50% - low to medium plasticity	H

## (b) Grading

“Well graded”	Good representation of all particle sizes from the largest to the smallest.
“Poorly graded”	One or more intermediate sizes poorly represented
“Gap graded”	One or more intermediate sizes absent
“Uniformly graded”	Essentially single size material.

## (c) Particle shape and texture

The shape and surface texture of the coarse grained particles should be described.

**Angularity** may be expressed as “rounded”, “sub-rounded”, “sub-angular” or “angular”.

Particle **form** can be “equidimensional”, “flat” or “elongate”.

**Surface texture** can be “glassy”, “smooth”, “rough”, “pitted” or “striated”.

## (d) Colour

The colour of the soil should be described in the moist condition using simple terms such as:

Black	White	Grey	Red
Brown	Orange	Yellow	Green
Blue			

These may be modified as necessary by “light” or “dark”. Borderline colours may be described as a combination of two colours, eg. red-brown.

For soils that contain more than one colour terms such as:

- Speckled Very small (<10 mm dia) patches
- Mottled Irregular
- Blotched Large irregular (>75 mm dia)
- Streaked Randomly oriented streaks

## (e) Minor Components

Secondary and minor components should be individually described in a similar manner to the dominant component.

## E1.3 Soil Condition

## (a) Moisture

Soil moisture condition is described as “dry”, “moist” or “wet”.

The moisture categories are defined as:

Dry (D) - Little or no moisture evident. Soils are running.  
Moist (M) - Darkened in colour with cool feel. Granular soil particles tend to adhere. No free water evident upon remoulding of cohesive soils.

In addition the moisture content of cohesive soils can be estimated in relation to their liquid or plastic limit.

## (b) Consistency

Estimates of the consistency of a clay or silt soil may be made from manual examination, hand penetrometer test, SPT results or from laboratory tests to determine undrained shear or unconfined compressive strengths. The classification of consistency is defined in Table E1.3.1.

TABLE E1.3.1 - CONSISTENCY OF FINE-GRAINED SOILS

TERM	UNCONFINED STRENGTH (kPa)	FIELD IDENTIFICATION
Very Soft	<25	Easily penetrated by fist. Sample exudes between fingers when squeezed in the fist.
Soft	25 – 50	Easily moulded in fingers. Easily penetrated 50 mm by thumb.
Firm	50 – 100	Can be moulded by strong pressure in the fingers. Penetrated only with great effort.
Stiff	100 – 200	Cannot be moulded in fingers. Indented by thumb but penetrated only with great effort.
Very Stiff	200 – 400	Very tough. Difficult to cut with knife. Readily indented with thumb nail.
Hard	>400	Brittle, can just be scratched with thumb nail. Tends to break into fragments.

Unconfined compressive strength as derived by a hand penetrometer can be taken as approximately double the undrained shear strength ( $q_u = 2 c_u$ ).

## (c) Density Index

The insitu density index of granular soils can be assessed from the results of SPT or cone penetrometer tests. Density index should not be estimated visually.

TABLE E1.3.2 - DENSITY OF GRANULAR SOILS

TERM	SPT N VALUE	STATIC CONE VALUE q <sub>c</sub> (MPa)	DENSITY INDEX (%)
Very Loose	0 – 3	0 - 2	0 - 15
Loose	3 – 8	2 - 5	15 - 35
Medium Dense	8 – 25	5 - 15	35 - 65
Dense	25 – 42	15 - 20	65 - 85
Very Dense	>42	>20	>85

#### E1.4 Soil Structure

##### (a) Zoning

A sample may consist of several zones differing in colour, grain size or other properties. Terms to classify these zones are:

Layer - continuous across exposure or sample

Lens - discontinuous with lenticular shape

Pocket - irregular inclusion

Each zone should be described, their distinguishing features, and the nature of the interzone boundaries.

##### (b) Defects

Defects which are present in the sample can include:

- fissures
- roots (containing organic matter)
- tubes (hollow)
- casts (infilled)

Defects should be described giving details of dimensions and frequency. Fissure orientation, planarity, surface condition and infilling should be noted. If there is a tendency to break into blocks, block dimensions should be recorded

#### E1.5 Soil Origin

Information which may be interpretative but which may contribute to the usefulness of the material description should be included. The most common interpreted feature is the origin of the soil. The assessment of the probable origin is based on the soil material description, soil structure and its relationship to other soil and rock materials.

Common terms used are:

“Residual Soil” - Material which appears to have been derived by weathering from the underlying rock. There is no evidence of transport.

“Colluvium” - Material which appears to have been transported from its original location. The method of movement is usually the combination of gravity and erosion.

“Landslide Debris” - An extreme form of colluvium where the soil has been transported by mass movement. The material is obviously distributed and contains distinct defects related to the slope failure.

“Alluvium” - Material which has been transported essentially by water. Usually associated with former stream activity.

“Fill” - Material which has been transported and placed by man. This can range from natural soils which have been placed in a controlled manner in engineering construction to dumped waste material. A description of the constituents should include an assessment of the method of placement.

#### E1.6 Fine Grained Soils

The physical properties of fine grained soils are dominated by silts and clays.

The definition of clay and silt soils is governed by their Atterberg Limits. Clay soils are characterised by the properties of cohesion and plasticity with cohesion defines as the ability to deform without rupture. Silts exhibit cohesion but have low plasticity or are non-plastic.

The field characteristics of clay soils include:

- dry lumps have appreciable dry strength and cannot be powdered
- volume changes occur with moisture content variation
- feels smooth when moist with a greasy appearance when cut.

The field characteristics of silt soils include:

- dry lumps have negligible dry strength and can be powdered easily
- dilatancy - an increase in volume due to shearing - is indicated by the presence of a shiny film of water after a hand sample is shaken. The water disappears upon remoulding. Very fine grained sands may also exhibit dilatancy.
- low plasticity index
- feels gritty to the teeth

#### E1.7 Organic Soils

Organic soils are distinguished from other soils by their appreciable content of vegetable matter, usually derived from plant remains.

The soil usually has a distinctive smell and low bulk density.

The USC system uses the symbol Pt for partly decomposed organic material. The O symbol is combined with suffixes “O” or “H” depending on plasticity.

Where roots or root fibres are present their frequency and the depth to which they are encountered should be recorded. The presence of roots or root fibres does not necessarily mean the material is an “organic material” by classification.

Coal and lignite should be described as such and not simply as organic matter.

## E2 CLASSIFICATION OF ROCKS

### E2.1 Uniform Rock Description

The aim of a rock description for engineering purposes is to give an indication of the expected engineering properties of the material.

In a similar manner to soil materials, the assessment of site conditions where rock is encountered has to be based on the use of a descriptive method which is uniform and repeatable. Description has to:

- provide a clear identification of the rock substance and its engineering properties, and
- include details of the features which affect the engineering properties of the rock mass.

There is no internationally accepted system for rock description but SMEC Testing Services Pty Ltd has adopted a method which incorporates terminology defined by common usage in the engineering geological profession. Most feature definitions are as recommended by the International Society of Rock Mechanics and by the Standards Association of Australia.

For uniform presentation the different features are described in order:

#### Rock Substance

- NAME (in block letters)
- Mineralogy
- Grain Size
- Colour
- Fabric
- Strength
- Weathering/Alteration

#### Rock Mass

- Defect type
- Defect orientation
- Defect features
- Defect spacing

### E2.2 Rock Substance

#### (a) Rock name

Each rock type has a specific name which is based on:

- mineralogy
- grain size
- fabric
- origin

The only method of determining the precise rock name is by thin section petrography.

Field identification of rocks for engineering purposes should be based on the use of common, easily understood, simple, geological names. In many cases knowledge of the precise name is of little consequence in the assessment of site conditions. If required the "field name" can be qualified by reference to a petrographic report. Reference to local geological reports often provides information on the rock types which may be expected.

#### (b) Mineralogy

The rock description should include the identification of the prominent minerals. This identification is usually restricted to the more common minerals in medium and coarse grained rocks.

#### (c) Grain Size

Rock material descriptions should include general grouping of the size of the predominant mineral grains as defined in Table E2.2.1. The maximum size, or size range, of the larger mineral grains or rock fragments should be recorded.

TABLE E2.2.1. - GRAIN SIZE GROUPS

TERM	GRAIN SIZE (mm)
Very Coarse	>60
Coarse	2 - 60
Medium	0.06 - 2
Fine	0.002 - 0.06
Very Fine	<0.002
Glassy	

#### (d) Colour

The colour of the rock should be described in the moist condition using simple terms such as:

Black	White	Grey	Red
Brown	Orange	Yellow	Green
Blue			

These may be modified as necessary by "light" or "dark". Borderline colours may be described by a combination of two colours, eg: grey-blue.

#### (e) Fabric

The fabric of a rock includes all the features of texture and structure, though the term refers specifically to the arrangement of the constituent grains or crystals in a rock. The fabric can provide an indication of the mode of formation of the rock:

- in sedimentary rocks bedding indicates depositional conditions,
- in igneous rocks the texture indicates the rate of cooling, and
- in metamorphic rocks the foliation indicates the stress conditions

Descriptions of fabric should include structure orientation, either with reference to North and horizontal, or to a plane normal to the core axis.

Tables E2.2.2, E2.2.3 and E2.2.4 list common textural features of sedimentary, igneous and metamorphic rocks with the subdivision of stratification spacing in Table E2.2.5.

TABLE E2.2.2 - COMMON STRUCTURES IN IGNEOUS ROCKS

STRATIFICATION (Planar)	STRATIFICATION (Irregular)
Bedding	Washout
Cross Bedding	Slump Structure
Graded Bedding	Shale Breccia
Lamination	
Cross Lamination	

TABLE E2.2.3 - COMMON STRUCTURES IN IGNEOUS ROCKS

Uniform Grain Size	FINE GRAINED ROCKS	COARSE GRAINED ROCKS
	Massive	Massive
	Flow Banded	Granitic
	Vesicular	Pegmatitic
Different Grain Size	Porphyritic	Porphyritic

TABLE E.2.2.4 - COMMON STRUCTURES IN METAMORPHIC ROCKS

FINE GRAINED ROCKS	COARSE GRAINED ROCKS
Slatey Cleavage	Granoblastic
Spotted	Porphyroblastic
Hornfelsic	Lincated
Foliated	Gneissic
Mylonitic	Mylonitic

TABLE E2.2.5 - STRATIFICATION SPACING

TERM	SEPARATION (mm)
Very Thickly Bedded	>2000
Thickly Bedded	600 - 2000
Medium Bedded	200 - 600
Thinly Bedded	60 - 200
Very Thinly Bedded	20 - 60
Laminated	6 - 20
Thinly Laminated	<6

(f) Strength

Substance strength is one of the most important engineering features of a rock and every description should include at least an estimate of the rock strength class of the material. This estimate can be calibrated by test results, either by Point Loan Strength Index or by Unconfined Compressive Strength.

The rock strength class in As 1726-1981 is defined by Point Loan Strength Index  $I_s(50)$ . The relationship between Point Loan and Unconfined Strength is commonly assumed to be about 20, but can range from 4 (in some carbonate rocks) to 40 (in some igneous rocks). It is necessary to confirm the relationship for each rock type and project. classification should be based on material at field moisture content, as some rocks give a significantly higher strength when tested dry.

Table E2.2.6 defines the rock strength classes, with indicative field tests listed in Table E2.2.7 which assist in classification when testing equipment is not available.

TABLE E2.2.6 - CLASSIFICATION OF ROCK STRENGTH

SYMBOL	TERM	POINT LOAD STRENGTH (MPa)	APPROX Qu (MPa)
EL	extremely low	<0.03	<1
VL	very low	0.03 - 0.1	1 - 3
L	low	0.1 - 0.3	3 - 10
M	medium	0.3 - 1	10 - 30
H	high	1 - 3	30 - 70
VH	very high	3 - 10	70 - 200
EH	extremely high	>10	>200

TABLE E2.2.7 - FIELD TESTS FOR ROCK STRENGTH CLASSIFICATION

STRENGTH CLASS	FIELD TEST
Extremely Low	Indented by thumb nail with difficulty
Very Low	Scratched by thumb nail
Low	Easily broken by hand or pared with a knife
Medium	Broken by hand or scraped with a knife
High	Broken in hand by firm hammer blows
Very High	Broken against solid object with several hammer blow
Extremely High	Difficult to break against solid object with several hammer blows

(g) Weathering/Alteration

In addition to the description of rock substance as examined, an assessment is required of the extent to which the original rock material has been affected by subsequent events. The usual processes are:

- Weathering - Decomposition due to the effect of surface or near surface activities
- Alteration - Chemical modification by the action of materials originating from within the mantle below.

The classification of weathering/alteration presented in Table E2.2.8 is based on the extent/degree to which the original rock substance has been affected. This classification has little engineering significance, as the properties of the rock as examined may bear no relationship to the properties of the fresh rock.

TABLE E2.2.8 - CLASSIFICATION OR ROCK WEATHERING/ALTERATION

TERMS	DEFINITION
Fresh (Fr)	Rock substance unaffected.
Fresh Stained (FR St)	Rock substance unaffected. Staining of defect surfaces.
Slightly (SW)	Partial staining or discolouration of rock substance.
Moderately (MW)	Staining or discolouration extends throughout the whole rock substance.
Highly (HW)	Rock substance partly decomposed.
Completely (CW)	Rock substance entirely decomposed.

## E2.3 Rock Mass

The engineering properties of rock mass reflect the effect which the presence of defects has on the properties of the rock substance. Description of the rock mass properties consists of supplementing the description covered by Section E2.2 with data on the defects which are present.

### (a) Defect type

The different defect types are described in Table E2.3.1.

### (b) Defect orientation

Descriptions of defects should include orientation, either of individual fractures or of groups of fractures. Orientation should be with reference to North and horizontal, or to a plane normal to the core axis.

TABLE E2.3.1 - ROCK DEFECT TYPES

TYPE	SYMBOL	DESCRIPTION
Parting	Pt	A defect parallel or subparallel to a layered arrangement of mineral grains or micro-fractures which has caused planar anisotropy in the rock substance.
Joint	Jt	A defect across which the rock substance has little tensile strength and is not related to textural or structural features with the rock substance.
Sheared Zone	SZ	A zone with roughly parallel planar boundaries or rock substance containing closely spaced, often slickensided, joints.
Crushed Zone	CZ	A zone with roughly parallel planar boundaries of rock substance composed of disoriented, usually angular, fragments of rock.
Seam	Sm	A zone with roughly parallel boundaries infilled by soil or decomposed rock.

### (c) Defect features

The character of a defect is described by its continuity, planarity, surface roughness, width, and infilling.

**Continuity** In outcrop the extent of a joint, bedding plane or similar defect both along and across the strike can be measured. In core, continuity measurement is restricted to defects nearly parallel to the core axis.

**Planarity** Described as “Planar”, “Irregular”, “Curved” or “Undulose”.

**Roughness** Described as “Rough”, “Smooth”, “Polished” or “Slickensided”.

**Width** Measured in millimetres normal to the plane of the defect

**Infilling** Described as “Clean”, “Stained”, “Veneer” (<1 mm) or “Infill” (>1 mm). The coating or infilling material should be identified.

### (d) Defect spacing

The spacing of defects, particularly where they occur in parallel groups or sets, provides an indication of the rock block sizes which:

- have to be supported in the face or roof of an excavation
- will be produced by the excavation operation.

It is preferable to provide measured data but discontinuity spacing is grouped as shown in Table E2.3.2.

TABLE E2.3.2 - DISCONTINUITY SPACING

DESCRIPTION	SPACING (mm)
Extremely Widely Spaced	>6000
Very Widely Spaced	2000 - 6000
Widely Spaced	600 - 2000
Medium Spaced	200 - 600
Closely Spaced	60 - 200
Very Closely Spaced	20 - 60
Extremely Closely Spaced	<20



**APPENDIX B**

**POINT LOAD TEST RESULTS**



**SMEC Testing Services Pty Ltd**

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**Point Load Strength Index Report**

Project: 157 Redfern Street, Redfern

**Client: DiCorp Pty Limited**

Address: 5/140 - 152 New Canterbury Rd, Petersham

Test Method: AS 4133.4.1

Project No.: 17055 / 5911B

Report No.: 09/0174

Report Date: 24/02/2009

Page: 1 of 2

Samples Supplied By: Terratest

Date Samples Drilled / Taken: 18/2/09

Borehole No. BH1

Samples Supplied By: Terratest

Date Samples Drilled / Taken: 18/2/09

Borehole No. BH1

Depth	Test Type	Is(50) (Mpa)	Rock Type	Rock Structure	Moisture	Depth	Test Type	Is(50) (Mpa)	Rock Type	Rock Structure	Moisture
9.68	D	0.22	SH	LA	M/D	25.88	D	0.46	SH	LA	M/D
9.68	A	0.03	SH	LA	M/D	25.88	A	0.43	SH	LA	M/D
12.78	D	0.14	SH	LA	M/D	27.93	D	0.94	SH	LA	M/D
12.78	A	0.36	SH	LA	M/D	27.93	A	1.72	SH	LA	M/D
13.96	D	1.08	SH	LA	M/D	29.96	D	1.39	SS	MA	M/D
13.96	A	1.15	SH	LA	M/D	29.96	A	1.22	SS	MA	M/D
15.40	D	1.33	SH	LA	M/D	32.94	D	1.19	SS	MA	M/D
15.40	A	2.70	SH	LA	M/D	32.94	A	1.24	SS	MA	M/D
17.07	D	1.21	SH	LA	M/D	34.04	D	1.89	SS	MA	M/D
17.07	A	1.68	SH	LA	M/D	34.04	A	1.44	SS	MA	M/D
20.24	D	0.03	SH	LA	M/D	36.36	D	1.67	SS	MA	M/D
20.24	A	1.48	SH	LA	M/D	36.36	A	1.38	SS	MA	M/D
22.08	D	0.30	SH	LA	M/D	39.43	D	1.80	SS	MA	M/D
22.08	A	0.45	SH	LA	M/D	39.43	A	1.34	SS	MA	M/D

**STRUCTURE**

MA= MASSIVE

BE= BEDDED

LA= LAMINATED

CR= CRYSTALLINE

**TEST TYPE**

A= AXIAL

D= DIMETRAL

I= IRREGULAR

C= CUBE

**MOISTURE CONDITION**

W= WET

M= MOIST

D= DRY

**ROCK TYPE**

SS= SANDSTONE

ST= SILTSTONE

SH= SHALE

YS= CLAYSTONE

IG= IGNEOUS

Remarks:

Approved Signatory.....

James Hughes - QA Manager

Technician: JK

**SMEC Testing Services Pty Ltd**

14/1 Cowpasture Place, Wetherill Park NSW 2164

Phone: (02)9756 2166 Fax: (02)9756 1137 Email: smectesting@pacific.net.au



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**Point Load Strength Index Report**

Project: 157 Redfern Street, Redfern

**Client: DiCorp Pty Limited**

Address: 5/140 - 152 New Canterbury Rd, Petersham

Test Method: AS 4133.4.1

Project No.: 17055 / 5911B

Report No.: 09/0174

Report Date: 24/02/2009

Page: 2 of 2

Samples Supplied By: Terratest

Date Samples Drilled / Taken: 18/2/09

Borehole No. BH2

Samples Supplied By: Terratest

Date Samples Drilled / Taken: 18/2/09

Borehole No. BH3

Depth	Test Type	Is(50) (Mpa)	Rock Type	Rock Structure	Moisture	Depth	Test Type	Is(50) (Mpa)	Rock Type	Rock Structure	Moisture
8.28	D	0.40	SH	LA	M/D	10.42	D	0.14	SH	LA	M/D
8.28	A	0.57	SH	LA	M/D	10.42	A	0.70	SH	LA	M/D
10.41	D	0.40	SH	LA	M/D	12.6	D	0.34	SH	LA	M/D
10.41	A	0.43	SH	LA	M/D	12.6	A	3.51	SH	LA	M/D
12.10	D	0.76	SH	LA	M/D	14.09	D	0.20	SH	LA	M/D
12.10	A	2.51	SH	LA	M/D	14.09	A	4.95	SH	LA	M/D
15.04	D	2.46	SH	LA	M/D	16.5	D	1.43	SH	LA	M/D
15.04	A	6.04	SH	LA	M/D	16.5	A	3.03	SH	LA	M/D
17.21	D	1.98	SH	LA	M/D	18.06	D	1.44	SH	LA	M/D
17.21	A	2.41	SH	LA	M/D	18.06	A	3.47	SH	LA	M/D
20.04	D	0.70	SH	LA	M/D	20.6	D	2.36	SH	LA	M/D
20.04	A	6.13	SH	LA	M/D	20.6	A	2.77	SH	LA	M/D

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Remarks:

Approved Signatory.....

James Hughes - QA Manager

Technician: JK