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Huntingwood West - Bungaribee Estate Huntingwood Report on Geotechnical Assessment

October 2009

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30 October 2009

Goodman International Ltd Level 10, 60 Castlereagh Street Sydney NSW 2000

Our ref: 21/17871/00/AZ035 Rev1.doc

Attn: Brendon Quinn

Dear Brendon,

Huntingwood West - Bungaribee Estate Huntingwood Report on Geotechnical Assessment

This report presents the results of a geotechnical investigation undertaken by GHD Geotechnics at the above site. We understand that the site is to be developed for light industrial / commercial use.

The report contains the factual results of the field investigations and laboratory testing, together with comments and recommendations on earthworks, batter stability, foundation conditions, pavement subgrade and construction considerations.

The concurrent Contamination and Salinity Assessments are issued under separate cover.

The findings of the geotechnical assessment indicate that there do not appear to be any major underlying geotechnical issues that would prevent development of the site.

We trust this report is satisfactory for your current needs. Please contact either of the undersigned should you have any questions in regard to this report or require further assistance with this project.

Yours faithfully GHD Geotechnics

Roberta Lamont Principal Geotechnical Engineer

A ldenbrande

Tony Colenbrander Group Manager, Geotechnics and Dams

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1. Introduction

1.1 General

This report presents the results of a geotechnical investigation undertaken by GHD Geotechnics (GHD) for the proposed Bungaribee Estate development.

The proposed development site is located in Huntingwood West, bounded to the north by the Great Western Highway, to the east by Brabham Drive, to the south by the M4 Motorway and to the west by Eastern Creek.

The investigation was undertaken in accordance with our proposal submitted to Goodman on 4 August 2008 (reference AY783).

We understand that the project will involve

- Earthworks on the Stage 1 (Southern) Site, expected to comprise up to 9 m in cut and 8 m in fill;
- Earthworks on the Stage 2 (Northern) Site, expected to comprise 3 m in cut and 3 m in fill;
- Formation of cut and embankment slopes;
- Construction platforms for future industrial development (ie footings, etc);
- An internal road network; and
- New intersections at the Great Western Highway and Brabham Road.

1.2 Scope of Work

The objectives of the geotechnical investigation were to:

- Assess subsurface conditions, including an assessment of moisture, groundwater and soil aggressivity;
- Discuss excavatability of subsurface materials;
- Assess the foundation conditions for the proposed pads and warehouse structures;
- Discuss footing options;
- Assess subgrade strength of subsurface materials;
- Provide general comments relating to stability of cut and embankment slopes; and
- Consider possible construction constraints.

1.3 Limitations

This report has been prepared for the use of Goodman International Ltd in relation to the proposed development of Bungaribee Estate – Huntingwood West, and takes account of information provided to us. Changes to project scope may require review and revision of the recommendations provided herein.

This report should be read in conjunction with the attached General Notes.



2. Site Setting

2.1 Description

The site is located on the southern side of the Great Western Highway, Huntingwood, and comprises 56 ha of land known as Huntingwood West – Bungaribee Industrial Estate (refer to Figure 1). The site can be sub-divided into two areas: Stage 1 (Southern Site and Estate Rd) and Stage 2 (Northern Site).

Topographically, the site comprises a gently undulating 'upland' region for the most part, with a narrow region along the western boundary, which is relatively flat where it joins the 'floodplain' of Eastern Creek.



Plate 1 - View from upland section of site to the flatter section in the west



Plate 2 - View of flatter, 'floodplain' area in western part of site

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The site generally slopes and drains toward the west. Drainage lines were observed in the areas of the 'gullies' indicated by topographic information. The northeastern part of the site contains a drainage channel, which begins as a stormwater culvert from Brabham Drive and drains to the west. We understand that this drainage line then turns toward the north, which is supported by topographical survey information.



Plate 3 – View of reed-filled drainage channel on eastern boundary

The northeastern part of the site was observed to be marshy and contains standing water in places. Vehicular access to these areas, even with a backhoe, was not possible.



Plate 4 – View of marshy area in north east of site



Some paddocks showed minor excavations (furrow and/or drainage lines) and there were several small dams, used for livestock watering, located towards the centre of the site.



Plate 5 – View of farm dam in centre of site

Remnants of a former racing/training track are bisected by the western site boundary.

Fill and dumped material were found to exist in several localised areas throughout the site. Some of these materials were visually observed to comprise clay, gravels, and demolition rubble. There were also some tyres present. It should be noted that, during the period of the fieldworks, illegal dumping was observed being undertaken.



Plate 6 – Example of fill material

Vegetation generally comprises grass cover, with some sections containing medium-sized trees. There is a greater concentration of trees in the eastern portion of the site.

2.2 Regional Geology

Reference to the 1:100,000 scale Geological Series Sheet for Penrith (sheet 9030) indicates that most of the site is underlain by Bringelly Shale of the Wianamatta Group, which comprises



shale, carbonaceous claystone, claystone, laminate, fine to medium grained lithic sandstone, rare coal and tuff. The western boundary of the site is underlain by quaternary alluvium comprising fine-grained sands, silts and clays (refer to Figure 2).

2.3 Soil Landscape

Reference to the 1:100,000 scale Soil Landscape Series Sheet for Penrith (sheet 9030) indicates that the site lies within the residual soil landscape of the Blacktown Formation (refer to Figure 3).

Landscapes comprise gently undulating rises on Wianamatta Group shales, with local relief to 30 m. Slopes are usually of <5% grade. The landscape comprises broad rounded crests and ridges with gently inclined slopes. Vegetation comprises cleared eucalypt woodland and tall open forest (dry sclerophyll forest).

Soils comprise shallow to moderately deep (<1m) hard-setting mottled texture contrast soils, red and brown podsolic soils on crests grading to yellow podsolic soils on lower slopes and in drainage lines.

Clay soils were observed to be exposed in a small cutting on the site and showed evidence of shrinkage cracking (refer to Plate 7).



Plate 7 – Cutting exposure of clay soils indicating shrinkage cracking



3. Site Investigation

3.1 Desktop Study

A desktop study was conducted, including the collation of relevant geotechnical and engineering geological information for the site obtained from published sources and previous investigations.

Information from published sources included aerial photographs and regional geology and soil landscape maps. This information has been detailed in Section 2 'Site Setting' and was used to plan the fieldwork.

The previous investigation reports that were provided to us are listed below:

- "Report on Phase 1 Environmental Site Assessment, Parcel 4 West Huntingwood, Western Sydney Parklands", prepared for Landcom, Douglas Partners, January 2006 (Ref 40465-2).
- "Report on Phase 2 Environmental Site Assessment, Land Capability Study West Huntingwood", prepared for Landcom and Department of Planning, Douglas Partners, September 2006 (Ref 40465A), contained within the supporting documents to the Concept Plan.
- Working Paper Huntingwood West Geotechnical, SKM, 13 April 2007.
- Environmental Assessment Volume 2, Employment Lands (Huntingwood West) for Landcom, The Planning Group (NSW) Pty Ltd, 18 September 2006.

The previous reports by others were prepared for the purposes of due diligence and contamination assessment, so were of limited use for the current geotechnical investigation. They were, however, reviewed as part of the GHD Contamination Assessment (reported under separate cover).

The "Report on Phase 2 Environmental Site Assessment, Land Capability Study - West Huntingwood", prepared for Landcom and Department of Planning, Douglas Partners, September 2006 (Ref 40465A) provided a general indication of the subsurface profile as being stiff to very stiff residual clay, overlying, at an average depth of 2 m, low grading to medium strength shale. No free groundwater was observed in the test pits.

The test pit logs described the material type and colour encountered but did not contain any strength, plasticity or secondary constituent information. This supported the information on regional geology and soil landscapes reviewed as part of the desktop study.

3.2 Safety

In accordance with standard GHD procedure, a Job Safety and Environment Analysis (JSEA) was prepared for site work. A project safety briefing of all site personnel was completed prior to the commencement of the field investigations.

3.3 Site Walkover

A Principal Geotechnical Engineer of this firm conducted a walkover and mapping visit of the site, observing features such as watercourses, erosion, vegetation (possibly indicating changes



in nature of subsurface material), boggy ground, etc. The existing fill mounds were visually observed to determine if the material is uncontrolled (i.e. presence of waste products, large boulders, etc.).

The findings of the site walkover are included in Section 2 'Site Setting' and Section 4 'Results of Site Investigation'.

3.4 Services

Prior to the investigation, a Dial-Before-You-Dig services search was conducted, and underground service plans were obtained and reviewed. The test locations were set out using hand-held GPS, with reference to these plans, in areas well away from underground services. Each test location was then scanned by a services locator subcontractor to clear the area for underground services prior to the commencement of drilling or excavation.

3.5 Subsurface Investigation

The purpose of the subsurface investigation was to provide a broad coverage of geotechnical information. The specific locations of test sites were determined with this aim in mind and with consideration of accessible areas, following the site walkover.

3.5.1 Borehole Investigation

A total of 9 boreholes were drilled, as follows:

- Stage 1 (Southern):
 - 2 boreholes to 6 m depth (BH01, BH04);
 - 4 boreholes to 10 m depth (BH02, BH03, BH05, BH06) in areas of proposed deeper cut;
 - Standpipe piezometers were installed in three of the boreholes (BH01, BH04, BH06).
- Stage 2 (Northern):
 - 3 boreholes to 6 m depth (BH07, BH08, BH09);
 - Standpipe piezometers were installed in two of the boreholes (BH07, BH09).

Drilling was conducted using a truck-mounted Scout drilling rig. Boreholes were advanced using solid flight augers fitted with a V-bit to auger refusal, followed by continuous core sampling of bedrock to target depths in all boreholes.

Standard penetration tests (SPT's) were conducted at regular (typically 1.5 m) intervals during drilling in addition to the collection of disturbed auger samples for visual / tactile assessment.

Point-load testing of core samples was conducted at regular (typically 1m) intervals.

An experienced Geotechnical Engineer from GHD supervised the borehole drilling, logged the encountered profile, boxed and photographed recovered core, obtained representative samples and directed piezometer installation.



The borehole logs are included in Appendix A. These should be read in conjunction with the attached Standard Sheets that explain the terms, abbreviations and symbols used, together with the interpretation and limitations of the logging procedures.

3.5.2 Test Pit Investigation

A total of 13 test pits in Stage 1 and 14 test pits in Stage 2 were excavated. Two of the test pits proposed for the northeastern area of Stage 2 had to be abandoned due to the inability to access the area with a backhoe due to boggy conditions.

The test pits will be advanced using a rubber-tyred CAT 428C backhoe, fitted with a 600 mm wide toothed bucket, to depths of 1.8-2.6 m (where bucket refusal was obtained) or to maximum depths of 3.2 m. Following completion, the test pits were backfilled with excavated spoil and nominally compacted by traversing the backfilled test pit with the backhoe's pneumatic tyres and tamping with the backhoe bucket during backfilling.

Insitu Dynamic Cone Penetrometer (DCP) tests were also undertaken at some of the test pit locations to provide additional information of the strength/consistency of the subsurface materials.

All test pit excavations were supervised full-time by an experienced Geotechnical Engineer, who conducted representative sampling, logged the excavated test pit profiles and obtained representative disturbed and bulk samples.

The test pit logs are included in Appendix B. These should be read in conjunction with the attached Standard Sheets that explain the terms, abbreviations and symbols used, together with the interpretation and limitations of the logging procedures. The DCP test results are included in Appendix C.

3.6 Laboratory Testing

Samples of soil and rock collected in the field were submitted to our NATA-accredited laboratory for geotechnical classification, compaction and strength testing. Limited testing was also conducted on samples collected from the fill bund. The testing undertaken comprised:

- Field Moisture Content (FMC) to assess in-situ moisture content (40 tests);
- Atterberg Limit and Linear Shrinkage tests to assess soil plasticity and confirm the soil descriptions obtained in the field (20 tests);
- Particle Size Distribution (8 tests);
- Emerson Class Number tests to assess potential dispersive soil characteristics (20 tests);
- Compaction (8 tests) and California Bearing Ratio (CBR) for subgrade assessment (5 tests);
- Point load testing of rock core samples (21 tests).

The laboratory test reports are included in Appendix D and should be read in conjunction with the standard sheets, which explain the limitations of the testing undertaken.



4. Results of Investigation

As described in Section 2, the site can be topographically divided into an 'upland' region, for the most part, and a 'floodplain' region along the western boundary of the site. The results of the investigation are described separately herein for these two areas of the site. Discussion of groundwater encountered is also provided.

4.1 'Upland' Region Subsurface Conditions

This section refers to the subsurface conditions of the majority 'upland' region, represented by test locations (BH01-06 and BH08-09 and TP11-12, TP14-16, TP18-19, TP21-31 and TP33-38).

The following sections provide a summary description of the subsurface units encountered. Reference should be made to the individual borehole and test pit logs in conjunction with the standard sheets for detailed subsurface description. Refer to Figure 1 – Test Location Plan.

Groundwater conditions for the site (both 'upland' and 'floodplain' regions) are reported in Section 4.3 'Groundwater'.

4.1.1 Topsoil

Topsoil was present at the majority of test locations, generally extending to depths of 0.1-0.50 m. The topsoil comprised brown and dark brown, low plasticity, clayey sand, sandy clay, clay, silty sand and sandy silt with a trace of gravel and sand. The topsoil ranged from slightly moist to very moist.

4.1.2 Fill

Fill was encountered at TP19, TP22, TP27, TP36, BH01, BH05 and BH08 to depths of 0.1-0.45 m. The fill was often located immediately below, or mixed with, topsoils and comprised brown, silty sand with gravel, sandy gravel, sandy clay or sand. Some fragments of tiles, ash, brick and concrete were noted. The fill was generally moist.

It is inferred that these relatively thin layers of fill occur in the vicinity of former development and in lower-lying areas of the upland region and are likely to be the results of localised levelling works to support the former development.

Some localised stockpiles of fill were also encountered in this region, as described in Section 2 'Site Setting'.

4.1.3 Alluvium/Colluvium

The alluvium/colluvium was quite widespread in this region and extended generally to depths of 0.35-1.0 m. However, colluvial materials were encountered to 1.4 m depth in TP22.

These materials generally comprised red brown, orange brown, light grey and brown, medium to high plasticity clay and sandy clay with a trace of sand and gravel. Some very high plasticity colluvial clays were identified from the laboratory testing. The laboratory testing for linear



shrinkage also indicated that the materials subjected to moisture content changes will be prone to shrink/swell movements.

Laboratory testing indicated that the alluvium/colluvium is moderately dispersive.

The materials ranged from soft to very stiff in consistency and were moist (generally 4% wet of optimum moisture content and plastic limit). This reflects prevailing wet conditions prior to, and during, the investigation.

Alluvial/colluvial materials were encountered in the majority of test locations and consist of materials similar to the residual soils and bedrock at the site, indicating short travel distance for these deposits. It is inferred that they have resulted from localised weathering and transport of residual soils and rock from other parts of the 'upland' region into drainage lines, or as slopewash, over time. The deeper profile of colluvial materials in TP22 is consistent with a deeper slopewash deposit at this junction between the 'upland' region and the 'floodplain'.

4.1.4 Residual

Residual soils were encountered at all test locations, extending to depths of auger refusal at 0.9-4.89 m. The residual soils typically comprise orange brown, red brown, light grey, light brown, medium to high plasticity clay and sandy clay with a trace of sand and gravel. There were some occurrences of clayey sands in a minority of test locations. Some very high plasticity residual clays were identified from the laboratory testing. The laboratory testing for linear shrinkage also indicated that the materials subjected to moisture content changes will be prone to shrink/swell movements.

Laboratory testing indicates that these materials vary in terms of dispersive potential, from moderately dispersive to non-dispersive due to the presence of gypsum and carbonate.

Soft residual soils were encountered in a limited number of test locations to depths of 0.2-1.0 m. The majority of residual soils were firm to depths of 0.6-3.0 m and stiff to very stiff thereafter.

The residual soils above the water table were generally moist and were approximately 3% wet of optimum moisture content and the plastic limit of the materials.

The soils contain ironstone gravel. A gradational transition into extremely to highly weathered bedrock was observed at some test locations.

4.1.5 Bedrock

The bedrock generally comprised shale and siltstone, although fine to medium grained sandstone was encountered at a number of locations, which is consistent with Bringelly Shale deposits.

The boreholes encountered grey, extremely to highly weathered, extremely low strength shale and siltstone/shale to 3.6-5.0 m depth. The test pits encountered the same type materials, however, backhoe refusal was encountered as shallow as at 2.0-3.1 m.

Underlying the extremely low strength rocks are grey and light brown, highly weathered, very low strength shale, shale/siltstone and siltstone/sandstone to depths of 4.6-9.3 m, overlying dark grey and grey, moderately to highly weathered, low strength shale and siltstone to depths of borehole termination at 6.0 m and 10.0-10.1 m, respectively.



Sandstone was encountered at the following locations:

- TP24 light grey, extremely to highly weathered, extremely to very low strength sandstone at 1.3 m depth to test pit completion at 2.2 m.
- ▶ BH01 light brown, extremely weathered, extremely low strength, fine to medium grained sandstone from 4.9-5.0 m depth, over light brown, highly weathered, very low to low strength sandstone to borehole termination at 6.0 m depth.
- ▶ BH06 a 900 mm thick band of brown and grey fine grained, highly to moderately weathered, low to medium strength sandstone was encountered at 6.2 m depth.

4.1.6 Laboratory Testing

Results of the geotechnical laboratory testing for materials within the 'upland' region of the site are summarised in Table 1.

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Table 1 Summary of geotechnical laboratory testing for "upland" region.

Test Location	Uepth (m)	Sample Type	FMC (%)	PL (%)	LL (%)	٦	LS (%)	PSD	ECN	OMC (%)	OMC (%) MDD (t/m ³) CBR (%)	CBR (%)
Fill materials							Y					
TP22	0.25-0.4	D	9.3					30/22/48				
TP27	0.2-0.4	D	8.6						2			8
Alluvial/Colluvial soils	soils					2					0	
TP11	0.4-0.6	D	26	22	67	45	16.5		2(m)			
TP14	0.5-0.7	D	25.2	23	68	45	17.0		2(m)			
TP15	0.3-0.5	D	20.8					78/17/5				
TP15	0.6-0.8	D	22.6	20	58	38	16.0					
TP21	0.3-0.5	D	25.1	20	64	44	16.5		2(m)			
TP22	0.9-1.1	D	30.9	23	91	68	22.0		2(m)			
TP23	0.3.0.5	В	21.3									
TP24	0.6-0.7	В	24.8	19	75	56	17.5					
TP27	0.6-0.8	D	27.5									
TP33	0.2-0.4	D	20.3									
TP33	0.5-0.6	D	13.7					46/3/51				
TP34	0.3-0.5	D	25.3	18	61	43	16.5		2(m)			
TP35	0.3-0.45	D	19.1				ł					

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Test Location	Depth (m)	Sample Type	FMC (%)	PL (%)	rr (%)	٦	(%) ST	PSD	ECN	OMC (%)	MDD (t/m ³) CBR (%)	CBR (%)
TP35	0.5-0.7	D	22.5									
TP37	0.5-0.7	В	25.1						ę	20.5	1.68	
TP38	0.5-08	В	26.9							24.3	1.57	2.0
Residual soils												
BH01	0.5	SPT							2(s)			
BH06	0.5								4			
BH09	1.5	SPT							2(s)			
TP11	1.1-1.3	В	19.7									
TP12	0.8-0.9	В	18.9							16.6	1.85	4.5
TP12	1.9-2.0	В	22.7	16	53	37	16.0		2(m)			
TP15	1.4-1.6	Ш	23.1		21					18.8	1.70	
TP16	0.8-1.0	В	21.4	19	53	34	16.0					
TP18	0.6-0.7	Θ	21.2	16	50	34	16.5		3(m)	16.8	1.73	
TP23	2.4-2.6	В	15.1	24	58	34	13.5					
TP24	1.0-1.2	D	16.2	16	50	34	15.5		3(m)			
TP25	2.0-2.2	Ш	18.8					65/25/10	_			
TP26	0.5-0.6	Ξ	24.5							20.2	1.71	2.0
TP26	1.0-1.2	D	25.5	21	75	54	17.5		2(s)			
TP28	0.5-0.7	Ω	25.7	18	59	41	18		3(m)			-
											17	

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Test Location		Depth (m)	Sample Type	FMC (%)	PL (%)	PL (%) LL (%)	Ы	LS (%)	PSD	ECN	OMC (%)	OMC (%) MDD (t/m ³)	CBR (%)
TP29	.0	0.4-0.6	D	18.6	23	66	43	16.0		3(s)			
TP29	0.	0.7-0.9	D	19.7	20	58	38	15.0		2(m)			
TP34	0.	0.6-0.7	D	25.6	19	70	51	15.0		2(m)			
TP36	0.	0.5-0.6	D	17.5									
TP37	1.1	1.0-1.2	D	19.0	14	42	28	14.5					
TP38	1.	1.4-1.5	В	15.6	12	44	32	11.5		2(m)			
Bedrock													
TP19	1.5	1.8-1.9	В	8.1							12.8	1.92	8.0
TP36	1.1	1.5-1.6	D	11.4									
Legend:	FMC – Fiel	FMC – Field Moisture Content	intent			- OSA	- Particle	e Size Distri	PSD – Particle Size Distribution (% clay & silt / % sand / % gravel)	silt / % sa	nd / % gravel)		
	PL – Plastic Limit	c Limit				ECN -	- Emers	ECN – Emerson Class Number	umber				
	LL – Liquid Limit	l Limit				OMC	– Optim	OMC – Optimum Moisture Content	e Content				
	PI – Plastic Index	c Index				MDD	– Maxin	MDD – Maximum Dry Density	nsity				
	LS – Linea	LS – Linear Shrinkage				CBR -	- Califor	CBR – California Bearing Ratio	Ratio				

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4.2 'Floodplain' Region Subsurface Conditions

This section refers to the subsurface conditions of the 'floodplain' region, represented by test locations (BH07 and TP10, TP17, TP20, TP32).

The following provides a summary description of the subsurface units encountered. Reference should be made to the individual borehole and test pit logs in conjunction with the standard sheets for detailed subsurface description. Refer to Figure 1 – Test Location Plan.

Groundwater conditions for the site (both 'upland' and 'floodplain' regions) are reported in Section 4.3 'Groundwater'.

4.2.1 Topsoil

Topsoil was present at all test locations, generally extending to depths of 0.15-0.4 m. The topsoil comprised dark brown, generally silty sand but included sandy silt, sandy clay and clayey sand. The topsoil was generally moist.

4.2.2 Alluvium

The alluvial materials were quite variable and comprised light brown, grey mottled and light brown, low to high plasticity clay and medium dense clayey sand, with a trace of sand and gravel. The materials extended to depths of 0.8-2.6 m and generally overlie residual soils. The firm alluvial clays were encountered to depths of 0.8-1.5 m, with stiff to very stiff clays thereafter.

The materials above the water table were generally moist. The alluvial materials have been found to be moderately to completely dispersive.

It is inferred that these materials occur within the western, flatter, Eastern Creek 'floodplain' region of the site.

4.2.3 Residual

Residual soils were encountered at most test locations, extending to depths of 1.7-4.17 m. The residual soils typically comprise brown, red brown, light brown, grey mottled, stiff to hard, low to high plasticity, sandy clay or clay and medium dense to dense clayey sand. The residual soils above the water table were generally moist.

The soils contain ironstone bands and gravel. A gradational transition into extremely weathered bedrock was observed at some test locations.

4.2.4 Bedrock

The bedrock comprised grey and brown, extremely to highly weathered, very low strength sandstone. The sandstone was encountered to depths of test pit termination at depths of 1.8-2.2 m and to BH07 termination at 6.0 m.

4.2.5 Laboratory Testing

Results of the geotechnical laboratory testing for materials within the 'floodplain' region of the site are summarised in Table 2.

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Table 2	Summar	y of geote	Summary of geotechnical laboratory testing for "floodplain" region.	ory testing f	or 'flood	olain" reg	ion.						
Test Location		Depth (m)	Sample Type	FMC (%) PL (%) LL (%)	PL (%)	(%) TT	PI Li	(%) ST	PSD	ECN	OMC (%)	OMC (%) MDD (t/m ³)	CBR (%)
Alluvial soils	soils												
BH07	0.5	10	SPT							~			
TP13	0.4	0.4-0.5	D	22.5									
TP17	0.5	0.5-0.7	D	17.7					97/3/0				
TP20	0.4	0.4-0.5	В	21.2									
TP20	0.6	0.6-0.8	D	23.4	18	60	42	19		2(m)			
TP32	0.5	0.5-0.7	В	9.6							17.4	1.73	1.5
Residual soils	ıl soils												
TP13	1.5	1.5-1.7	D	13.4									
TP32	1.5	1.5-1.7	в	17.6	2				77/23/0				
Legend:	FMC – Field	FMC – Field Moisture Content	ontent		2	PSD -	- Particle S	size Distrik	PSD – Particle Size Distribution (% clay & silt / % sand / % gravel)	silt / % sar	nd / % gravel)		
	PL – Plastic Limit	s Limit				ECN -	ECN – Emerson Class Number	Class Nu	mber				
	LL – Liquid Limit	Limit				OMC -	OMC – Optimum Moisture Content	n Moisture	Content				
	PI – Plastic Index	Index				- DDM	MDD – Maximum Dry Density	n Dry Den	sity				
	LS – Linear Shrinkage	· Shrinkage				CBR -	CBR – California Bearing Ratio	a Bearing I	Ratio				

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4.3 Groundwater

No groundwater seepage was observed during auger drilling or excavation of test pits in the 'upland' region. In addition, the standpipe piezometers installed at BH04, BH06 and BH09 were observed to be dry when measured for groundwater depth during the drilling investigation period.

The piezometer at BH06 was sampled as part of the Salinity Assessment. The water level measurement, taken in November 2008, was 3.2 m depth.

Groundwater seepage was observed in TP17 at 1.8 m depth and TP32 at 2.0 m depth.

The piezometers installed at BH01 and BH07 were measured for groundwater depth during the drilling investigation period. Groundwater was encountered at depths of 4.0 m and 4.3 m, respectively.



5. Engineering Discussion

5.1 General

The proposed development requires cut to fill earthworks for the development of foundation pads. We understand at this stage, that there may be 9 m of cut and 8 m of fill for Stage 1 (Southern). There may be 3 m of cut and 3 m of fill for Stage 2 (Northern). We note that the proposed earthworks levels are preliminary.

There will also be a new internal road network (refer Figure 1 – Test Location Plan) and new intersections at the Great Western Highway and Brabham Road.

5.2 Earthworks

5.2.1 Site Preparation

The topsoil materials present on site are organic and were moist at the time of the investigation. They are unsuitable as foundation materials and should be removed from fill areas. Topsoil is also unsuitable for reuse as general fill. The topsoil should be separately stockpiled for later use for landscaping purposes, subject to remediation (if required) and landscaping assessment.

The northeastern part of the site, in the vicinity of proposed test pits TP30 and TP31, was unable to be accessed due to boggy ground conditions at the time of investigation. There are also a number of farm dams/channels in the centre of the site that contain water, vegetation and (potentially) saturated soft soils. Organic and soft soils are unsuitable as foundation materials and should be removed from fill areas. Organic materials are also unsuitable for reuse as general fill. Saturated, soft soils may be suitable for reuse as fill, subject to being allowed to dry out.

The uncontrolled fill materials and uncontrolled fill stockpiles present on site generally comprise clay, gravels, sands, demolition rubble and foreign objects (ie. tyres). Fill materials are unsuitable as foundation materials and should be removed from fill areas. The uncontrolled fill materials may be suitable for reuse as fill, subject to separate stockpiling, removal of foreign objects, remediation (if required) and assessment for suitability.

Given the high plasticity of the in-situ materials, site accessibility for earthmoving plant and other vehicles may be limited following rainfall periods. Adequate earthworks protection, including temporary drainage measures, should be provided during construction.

5.2.2 Excavatability of Cut Materials

Cut materials will be sourced form the 'upland' regions of Stage 1 and Stage 2.

In the 'upland' region of Stage 1, cut excavations are likely to encounter limited alluvium/colluvium, residual soils and extremely weathered (Class V) rock to an average depth of around 3 m. Underlying these materials is generally very low strength (Class IV) shale and siltstone, overlying low strength (Class III) shale and siltstone. The Class III shale and siltstone were encountered at an average depth of about 6.5 m.



In the 'upland' region of Stage 2, cut excavations are likely to encounter limited alluvium/colluvium, residual soils and extremely weathered (Class V) rock to an average depth of around 3 m, which is the proposed cut depth.

It is considered that the excavation of colluvial, residual and alluvial soils and extremely weathered rock can be accomplished using conventional earthmoving equipment without difficulty. Highly to moderately weathered rock materials are considered rippable using conventional earthmoving equipment fitted with ripping types to the currently proposed excavation levels. Deeper excavation of the moderately weathered Class III rock material (ie, below an average 6.5 m depth) may require the use of rock breakers (hydraulic hammers), though the laminated nature of these materials is often suitable for ripping.

5.2.3 Fill Material Suitability

It is envisaged that fill materials will include soils of colluvial, residual and shale/siltstone bedrock origin. The shale/siltstone bedrock will likely vary in terms of strength and weathering, according to the depth of cut from which it is obtained.

General requirements of suitable materials for use during construction are that they are free from unsuitable or organic materials and the anticipated cut materials meet these requirements.

Laboratory test results indicate that the soils within the site possess CBR strengths of 2.0% to 4.5%, with samples sourced from the weathered bedrock having a CBR strength of 8%. However, shale breaks down over time so this high CBR value should not be adopted for pavement design purposes. The soils are highly reactive, as demonstrated by the swelling behaviour during soaking in preparation of CBR testing and the results of Atterberg limits testing. Thus, the fill material for the site will be moisture sensitive. That is, it will be prone to swelling on wetting up and shrinkage on drying. From the limited compaction testing undertaken, the naturally occurring materials were approximately 3% wet of optimum moisture content.

Given the reactive / dispersive nature and low CBR strength of the fill materials proposed, lime modification of the upper zone of formation is recommended in addition to applying moisture controls of between -3% to +1% of OMC and compaction controls of 98% to 102% of standard compaction. Lime stabilisation will reduce dispersive erosion, increase soil strength and reduce its moisture sensitivity. Whilst no trials of lime modification have been undertaken, a dosage rate of 2% lime by dry mass for the upper 300 mm of formation is considered appropriate, based on experience.

In particular, we understand that future minor cut to fill earthworks may occur across the site to achieve building levels. Any future excavation through the lime-modified zone should be followed by reapplication of lime in areas where the modified thickness has been significantly reduced.

As an alternative to lime modification, the high plasticity cohesive soils could be placed in embankment 'zones' where they are protected from changes in moisture content by covering with lower plasticity materials (ie. high plasticity soils at the base and shales at the top). Such zoning should consider requirements for self-filtering of the materials to control migration of fines.



5.2.4 Materials Management

Whilst the developer will likely prefer to excavate from cut directly to fill placement, there may be requirements to separately stockpile materials in order to construct 'zoned' fill embankments using high plasticity materials and low plasticity (ie. shale) materials.

Prior to stockpiling, excavated materials should be re-worked, sorted and/or mixed into a uniform material. Stockpiles should be managed so that the material they contain is uniform throughout. Temporary drainage, erosion control and stormwater protection should be applied to stockpile sites in order to maintain the uniformity of stockpiled materials.

Our observations in October 2008 of the uncontrolled fill material stockpiles suggest that the materials vary locally; hence, further inspection (preferably observation during excavation works) is warranted to assess the nature and condition of these materials.

We are aware that ongoing dumping of uncontrolled fill stockpiles continued after the site investigations. These stockpiles have not been investigated. These materials are not considered suitable for reuse in the works, subject to further inspections / testing, if required.

5.2.5 Dispersivity and Erosion

Laboratory testing indicates that soils at this site are moderately to highly dispersive with Emerson Class Numbers generally of 2. Dispersive soils are particularly susceptible to sheet and gully erosion when there is limited vegetation cover.

Adequate protection of cut batters should be provided by methods such as hydromulching, grassing, or revegetating as soon as possible following excavation to reduce erosion. Where a flatter cut batter of 3H:1V can be accommodated for cut slopes, this would improve revegetation.

All cut batters should be provided with cut-off or dish drains located behind the crest to minimise run off of water over the face of the batter.

Drainage lines and channels should also incorporate appropriate erosion protection measures, including lime stabilisation to reduce the potential for dispersion erosion. This stabilisation rate should be 2% lime by dry mass as per that specified for fill modification.

5.2.6 Groundwater

In the 'floodplain' region, groundwater was measured in piezometers at depths of 4.0 m and 4.3 m. A perched groundwater table may be inferred from the groundwater seepage observed in TP17 at 1.8 m depth and TP32 at 2.0 m depth. It should be noted that there had been rainfall during the investigation and that conditions may be drier during construction.

In the 'upland' region, piezometers installed to depths of 10 m recorded no groundwater.

It is, therefore, anticipated that excavations will be able to be undertaken in dry conditions, with any runoff able to be controlled by pumping from sumps. It should be noted, however, that groundwater levels are subject to weather and rainfall conditions, and may fluctuate over time.



5.2.7 Settlement

Firm alluvial clays were encountered to depths of 0.8-1.5 m in the 'floodplain' region of the site. This region is likely to accept the greatest amount of engineered fill and it is anticipated that there will be some settlement due to consolidation of the firm clays under the fill loads.

Whilst the amount of settlement is likely to only be of the order of tens of millimetres and much of this settlement may take place during construction of the engineered fill, some settlement will take place over a number of years. Detailed design should consider the characteristics of the firm alluvial clays, the amount of potential settlement from fill loads and the ability of proposed development to withstand any remnant (post completion of fill placement) differential settlements.

5.3 Cut and Embankment Slopes

5.3.1 Soils

Cut and fill batter slopes in soil materials would be expected to satisfy slope stability criteria at gradients no steeper than 2.5H:1V. However, due to the highly reactive and dispersive nature of the soils on site, batter slopes of 3H:1V or flatter are recommended. Where flatter batter slopes are possible this will improve the ability of the batter to resist surface erosion and shrink / swell effects and allow vegetation growth to protect the earthworks. Where soils are lime modified, steeper batter slopes could be considered.

5.3.2 Rock

Whilst cut batters located in bedrock material will satisfy stability requirements at slopes of 1H:1V with localised shotcreting or bolting within fractured or jointed areas, cut batter slopes in rock steeper than 2H:1V should be subject to geotechnical inspection to confirm stabilisation requirements. Where rock slopes cannot be flattened, ongoing slope maintenance may be required.

All batter slopes should include appropriate crest drainage to minimise surface water erosion and instability on the batter face. It is also critical that vegetation is established on all batter slopes to reduce the effect of surface water flow and protect the batter from moisture variation effects.

5.4 Footings

As discussed earlier, there may be 9 m of cut grading to 8 m of fill for Stage 1 (Southern) and 3 m of cut grading to 3 m of fill for Stage 2 (Northern). Therefore, the formation level will vary from cut at the eastern side to fill at the western side of the site.

For footings located on stiff to very stiff residual soil, an allowable bearing capacity of 150 kPa can be assumed. For footings on Class IV or better shale/siltstone or sandstone, an allowable bearing capacity of 1000 kPa can be assumed. Higher bearing capacities may be determined during detailed design by consideration of the relative level of higher strength rock present at some locations.



Much of the final developed site will be located on engineered fill. Provided the fill is suitable general fill and is placed in accordance with a suitable specification, allowable bearing capacities of 25 kPa for floor loadings and 100 kPa for pad footings should be achieved.

Given the variation between the conditions in cut areas and those for engineered fill, allowable bearing pressures and likely settlement will vary across the site. These should be assessed on a case by case basis.

5.5 Pavement Subgrade

Results from compaction and CBR testing (Appendix D) indicate that site soils in areas of likely pavement subgrade will achieve a CBR value between 2.0% and 4.5%. It is therefore recommended that a CBR of 2% be used for pavement design purposes. However, the recommended lime modification of the upper zone of formation will improve the pavement subgrade CBR. A design subgrade of 3% may be assumed for pavements constructed on at least 150 mm of lime-stabilised soil as recommended herein.



References

- 1. Soil Conservation Service of NSW, Soil Landscape Series Sheet 9030, Penrith.
- 2. Geological Survey of NSW, Department of Minerals and Energy, *Geological Series Sheet* 9030, *Penrith*, Edition 1, 1991.
- 3. P.J.N. Pells, G. Mostyn and B.F. Walker, *Foundations on Sandstone and Shale in the Sydney Region*, Australian Geomechanics, December 1998, pp 17-29.



Standard Sheets

General Notes Glossary of Symbols Soil Description Rock Description Core Log Sheet Notes DCP Testing Laboratory Testing Reactive Soils

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GENERAL NOTES



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The report contains the results of a geotechnical investigation conducted for a specific purpose and client. The results should not be used by other parties, or for other purposes, as they may contain neither adequate nor appropriate information. In particular, the investigation does not cover contamination issues unless specifically required to do so by the client.

TEST HOLE LOGGING

The information on the test hole logs (boreholes, test pits, exposures etc.) is based on a visual and tactile assessment, except at the discrete locations where test information is available (field and/or laboratory results). The test hole logs include both factual data and inferred information. Moreover, the location of test holes should be considered approximate, unless noted otherwise (refer report). Reference should also be made to the relevant standard sheets for the explanation of logging procedures (Soil and Rock Descriptions, Core Log Sheet Notes etc.).

GROUNDWATER

Unless otherwise indicated, the water levels presented on the test hole logs are the levels of free water or seepage in the test hole recorded at the given time of measuring. The actual groundwater level may differ from this recorded level depending on material permeabilities (i.e. depending on response time of the measuring instrument). Further, variations of this level could occur with time due to such effects as seasonal, environmental and tidal fluctuations or construction activities. Confirmation of groundwater levels, phreatic surfaces or piezometric pressures can only be made by appropriate instrumentation techniques and monitoring programmes.

INTERPRETATION OF RESULTS

The discussion or recommendations contained within this report normally are based on a site evaluation from discrete test hole data, often with only approximate locations (e.g. GPS). Generalised, idealised or inferred subsurface conditions (including any geotechnical cross-sections) have been assumed or prepared by interpolation and/or extrapolation of these data. As such these conditions are an interpretation and must be considered as a guide only.

CHANGE IN CONDITIONS

Local variations or anomalies in the generalised ground conditions do occur in the natural environment, particularly between discrete test hole locations. Additionally, certain design or construction procedures may have been assumed in assessing the soil-structure interaction behaviour of the site. Furthermore, conditions may change at the site from those encountered at the time of the geotechnical investigation through construction activities and constantly changing natural forces.

Any change in design, in construction methods, or in ground conditions as noted during construction, from those assumed or reported should be referred to this firm for appropriate assessment and comment.

GEOTECHNICAL VERIFICATION

Verification of the geotechnical assumptions and/or model is an integral part of the design process - investigation, construction verification, and performance monitoring. Variability is a feature of the natural environment and, in many instances, verification of soil or rock quality, or foundation levels, is required. There may be a requirement to extend foundation depths, to modify a foundation system and/or to conduct monitoring as a result of this natural variability. Allowance for verification by appropriate geotechnical personnel must be recognised and programmed for construction.

FOUNDATIONS

Where referred to in the report, the soil or rock quality, or the recommended depth of any foundation (piles, caissons, footings etc.) is an engineering estimate. The estimate is influenced, and perhaps limited, by the fieldwork method and testing carried out in connection with the site investigation, and other pertinent information as has been made available. The material quality and/or foundation depth remains, however, an <u>estimate</u> and therefore liable to variation. Foundation drawings, designs and specifications should provide for variations in the final depth, depending upon the ground conditions at each point of support, and allow for geotechnical verification.

CLIMATE CHANGE

GHD Geotechnics acknowledges the occurrence of ongoing climate change. Cognisance is given to climate change issues as may be applicable to specific geotechnical investigations and assessments.

REPRODUCTION OF REPORTS

Where it is desired to reproduce the information contained in our geotechnical report, or other technical information, for the inclusion in contract documents or engineering specification of the subject development, such reproductions must include at least all of the relevant test hole and test data, together with the appropriate Standard Description sheets and remarks made in the written report of a factual or descriptive nature.

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GLOSSARY OF SYMBOLS

Ref: DS6.5.1 Issue 1.6 Date: 20/11/2008

KT

CA

FE

MI

Mn

Py QZ

VE

Chlorite

Iron Oxide

Micaceous

Manganese Pyrite

Calcite

Quartz

Veneer

ST

IR

Stepped

Irregular



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This standard sheet should be read in conjunction with all test hole log sheets and any idealised geological sections prepared for the investigation report.

GENERAL	i the investigation i	epon.					
Symbol	Descr	iption		Symbol	D	escriptio	n
D U	Disturbed Sample Undisturbed Sam tube diameter in	e Ipled (suffixed		PZ eor R	Piezometer Insta Rising Head Per	allation meability	/ Test
С	Core Sample (su			F PBT	Falling Head Pe Plate Bearing T		y lest
SV SPT	Shear Vane Test	(suffixed by va	alue in kPa)		Water Inflow (ma	ake)	
N	Standard Penetra SPT Value		1 blows per U. I	5m) —◀ ▽	Water Outflow (I Temporary Wate		
HB PM	SPT hammer bou Pressuremeter Te			T	Final Water Leve Point Load Test		
PP	Pocket Penetrom		by value in kPa	a) o	Point Load Test	(diametri	ic)
PK	Packer Test			IMP	Impression Devi	ce Test	
SOIL SYMB							
	Main Com	ponents					
	SAND			CLAY			SILT
5 2 2	GRAVEL			FILL			TOPSOIL
_	Minor Con	nponents					
	sandy			clayey			silty
p	gravelly		* * * * * * * *	vegetation, r	roots	177777	
		latural soils ar	e generally a c	combination o	f constituents, e.g		sandy CLAY
ROCK SYM	BOLS Sedimenta					6.7.8.9	
F	Sedimenta	ii y	E				Igneous
	SANDSTO	NE		SHALE		+ + + + + + + + + + + + + + + + + + + +	GRANITIC ROCK
	CLAYSTON	NE		CONGLOME	ERATE		IGNEOUS DYKE
	SILTSTON			COAL		公	BASALTIC ROCK
Note: A	dditional rock sym	bols may be a	llocated for a p	articular proje	ect.		
NATURAL F	RACTURES (Codi	ing)					
Fracture Typ JT Joint	be	Orientation		"D: "			
BP Beddir	ng Plane	For inclined	non-oriented of	core "Angle	" measured relativ	e to core	lative to horizontal axis.
Cb Cross SS Sheare	Bed ed Surface	For inclined	oriented core	"Dip" angle a	nd "Dip Direction" a	angle (eg.	45°/225° mag.)
SM Seam		VT	Vertical				
	ed Seam ented Zone	HZ or 0° d	Horizontal degrees				
SZ Shear		-	augrooo				
VN Vein	opting	Chana		Dente	ų		
Infilling or C CN Clean	oating	Shape PLN Plana	ar	Roughne POL Po		Othe DIS	Discontinuous
	naceous	CU Curve	ed	SLK Sli	ckensided	OP	Open
CLAY Clay KT Chlorite	<u>م</u>	UN Undu ST Stepr			nooth	CI	Closed

Smooth Rough

Very Rough

RF

VR

CI Closed Tight TI

SOIL DESCRIPTION



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This procedure involves the description of a soil in terms of its visual and tactile properties, and relates to both laboratory samples and field exposures as applicable. A detailed soil profile description, in association with local geology and experience, will facilitate the initial (and often complete) site assessment for engineering purposes.

The method involves an evaluation of each of the items listed below and is in general agreement with both Australian Standard AS 1726 (the Site Investigation Code) and ASTM D2487 and D2488.

The moisture condition of the soil is most applicable for cohesive soils as a precursor to the assessment of consistency and workability. The moisture condition is described as:

Slightly Moist Moist (damp, no visible water) Very Moist or Wet (visible free water, saturated condition) Dry (dusty, dry to the touch)

In addition, the presence of any seepage or free water is noted on the testhole logs.

COLOUR

Colour is important for correlation of data between testholes and during subsequent excavation operations. The prominent colour is noted, followed by (spotted, mottled, streaked etc.) then secondary colours as applicable. Colour is usually described at as-received moisture condition, though both wet and dry colours may also be appropriate.

CONSISTENCY / DENSITY INDEX

This assessment is based on the effort required to penetrate and/or mould the soil, and is an indicator of shear strength.

Granular soils are generally described in terms of density index as listed in AS 1726. These soils are inherently difficult to assess and normally a penetration test procedure (SPT, DCP or CPT) is used in conjunction with published correlations. Alternatively, in-situ density tests can be conducted in association with minimum and maximum densities performed in the laboratory.

Term	Symbol	Density Index (%)
Very Loose	VL	< 15
Loose	L	15 - 35
Medium Dense	MD	35 - 65
Dense	D	65 - 85
Very Dense	VD	>85

Cohesive soils can be assessed by direct measurement (shear vane, CPT etc), or estimated approximately by tactile means and/or the aid of a geological pick as given on the following table. It is emphasised that a "design shear strength" must take cognisance of the mode of testing and the in-situ moisture content with the possible variations of moisture with time.

Term	Symbol	Tactile Properties	Undrained Strength S _u (kPa)
Very Soft	VS	Extrudes between fingers when squeezed in hand	<12
Soft	S	Easily penetrated by thumb about 30-40 mm. Pick head can be pushed in up to shaft.	12-25
Firm	F	Penetrated by thumb 20-30mm with moderate effort. Sharp end of pick pushed in 30-40mm.	25-50
Stiff	St	Indented by thumb about 5mm with moderate effort. Pick pushed in up to 10mm.	50-100
Very Stiff	VSt	Readily indented by thumb nail. Slight indentation produced by pushing pick into soil.	100-200
Hard	н	Difficult to indent with thumb nail. Requires power tools for excavation.	>200

STRUCTURE/OTHER FEATURES

The soil structure is generally applicable to cohesive soils and mainly refers to the presence or absence of joints and layering. Typical terms use are intact (no joints), fissured (closed joints), shattered (open joints), slickensided (polished joints indicative of movement), and stratified/laminated. In addition, the presence of other features (ferricrete nodules, timber inclusions) should also be noted as applicable.

For granular soils, an assessment of grading (well, uniform or poor), particle size (fine, medium etc.) and angularity and shape may also be given.

The soil is described in terms of its estimated grain size composition and the tactile behaviour (plasticity of any fines (less than *0.06 mm)). This system does not differentiate on grading below 0.06 mm, in accordance with the Unified Soil Classification (USC) procedure.

However, in some situations a soil can exhibit different characteristics between the undisturbed and disturbed/remolded condition (eq. 'sand' sized particles which break down a clay). The Soil Type generally relates to the latter state but the former condition should be noted where applicable. Furthermore, as most natural soils frequently are combinations of various constituents, the primary soil is described and modified by minor components. In brief, the system is as follows:-

	Coarse Grained Soils	Fine Grained Soils		
% Fines	Modifier	% Coarse	Modifier	
<5	omit, or use "trace"	<15	omit, or use "trace"	
5-12	describe as "with clay/silt" as applicable	15-30	described as "with sand/gravel" as applicable	
>12	prefix soil as "silty/clayey" as applicable	>30	prefix soil as "sandy/gravelly" as applicable	

(*The 200# sieve (0.075 mm) is commonly used in practice to differentiate between fine and coarse grained soils). Note: For soils containing both sand and gravel the minor coarse fraction is omitted if less than 15%, or described as "with sand/gravel" as applicable when greater than 15%

The appropriate USC symbol may also be given after the soil type description in accordance with ASTM D2487 and D2488.

ORIGIN

An attempt is made, where possible, to assess origin (transported, residual, pedogenic, or fill etc.) since this assists in the judgement of probable engineering behaviour. This assessment is generally restricted to field logging activities. An interpretation of landform is a useful guide to the origin of transported soils (e.g. colluvium, talus, slide debris, slope wash, alluvium, lacustrine, estuarine, aeolian and littoral deposits) while local geology and remnant fabric will assist identification of residual soils.

ROCK DESCRIPTION



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This method is based on Australian Standard AS 1726 and is orientated to the field logging of diamond drill core, but may be used for the profiling of natural exposures and cuttings, as applicable. The procedure involves a visual and tactile assessment of the rock mass and the nature of defects within it in order to facilitate a prediction of engineering behaviour.

DESCRIPTION:

W: Rock Type is described on the basis of origin (sedimentary, metamorphic and igneous) with the common types listed below:-

Sedimentary				Metamorphic	No. Anna Cara		Igneous		
Clastic	Non clastic (chemical)	Non clastic (organic)	Pyroclastic			Acid	Intern	nediate	Basic
Conglomerate Sandstone Siltstone Shale Claystone	Limestone Chert Gypsum Salt	Coal Some Limestone	Tuff Agglomerate Volcanic Breccia	Slate Phyllite Schist Quartzite Gneiss	Extrusive Intrusive (medium grained) (coarse grained)	Rhyolite Quartz Porphyry Granite	Trachyte Porphyry Syenite	Andesite Porphyrite Diorite	Basalt Dolerite Gabbro

<u>Colour</u> is given to assist in rock identification and the interpolation of field data. Colour is usually described at as-received moisture condition, though both wet and dry colours may also be appropriate.

<u>Texture</u> refers to the degree of crystallinity and granularity (grain size) and the fabric relationship between the constituents of a rock. Often only grain size is given for simplified descriptions of certain sedimentary rocks.

<u>Structure</u> and texture are commonly used synonymously in describing rocks since there is no clear delineation between terms. In general, structure refers to large-scale features recognisable in the field (banding, lineation, massive, porphyritic, schistose etc.). For sedimentary rocks in particular, the thickness of sedimentary layering (bedding) is described as:-

Thinly laminated	<6mm	very thinly bedded	20-60mm	medium bedded	0.2-0.6m	very thickly bedded	>2m
Laminated	6-20mm	thinly bedded	60-200mm	thickly bedded	0.6-2m		

In addition, mineral composition, hardness, alteration, cementation is given as applicable.

WEATHERING: The assignment of weathering is somewhat subjective. Weathering assists identification and does <u>not</u> imply engineering behaviour. No distinction is drawn between chemical weathering and alteration for most engineering purposes. These procedures are collectively described as "weathering" using the following terms which do not describe the related strength change. This system is general, and in this format may not apply to all rock types. Carbonate rocks generally do not conform to this classification.

Term	Symbol	Definition
Completely Weathered	CW	Residual soil with rock fabric not visible.
Extremely Weathered	EW	The rock exhibits soil-like properties though the texture of the original rock is still evident.
Highly Weathered	HW	Limonite staining or colour change affects the whole of the rock mass and other signs of chemical or physical decomposition are evident.
Moderately Weathered	MW	Staining extends throughout the whole of the rock mass and the original colour is no longer recognisable.
Slightly Weathered	SW	Partial staining or discolouration of the rock mass, usually by limonite, has taken place.
Fresh	Fr	Rock mass unaffected by weathering.

ESTIMATED STRENGTH: This refers to the strength of the <u>rock substance</u> and not that of the rock mass. The strength of the rock substance is estimated by the Point Load Strength Index $I_{S}(50)$ and refers to the strength measured in the direction normal to the bedding for sedimentary rocks. A field guide is given below:-

Term	Symbol	Is(50)	Field Guide
		MPa	(The core refers to a 150mm long x 50mm dia. sample)
Extremely Low	EL	< 0.03	Remoulded by hand to a material with soil properties.
Very Low	VL	0.03-0.1	May be crumbled in the hand. Sandstone is "sugary" and friable.
Low	L	0.1-0.3	The core may be broken by hand and easily scored with a knife. Sharp edges of core may be friable and break during handling.
Medium	M	0.3-1.0	The core may be broken by hand with considerable difficulty. Readily scored with knife.
High	н	1-3	The core cannot be broken by unaided hands, can be slightly scratched or scored with knife.
Very High	VH	3-10	The core may be broken readily with hand held hammer. Cannot be scratched with knife.
Extremely High	EH	>10	The core is difficult to break with hand held hammer. Rings when struck with a hammer.

DEFECTS: This important feature can control the overall engineering behaviour of a rock mass. All types of <u>natural</u> fractures across which the core is discontinuous are noted. These fractures include bedding plane partings, joints and other defects but exclude artificial fractures such as drilling breaks. The nature of the defects (joints, bedding partings, seams, zones and veins) is also noted with description, orientation, infilling or coating, shape, roughness, thickness, etc. given generally in accordance with AS 1726. The spacing of natural fractures <u>excludes</u> bedding partings unless there is evidence that they were separated prior to drilling. This notwithstanding, bedding partings maybe considered as planes of weakness in an engineering assessment.

CORE LOG SHEET NOTES



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The intention of Core log Sheets is to present factual information measured from the core or as recorded in the field. Some interpretative information is inevitable in the location of core loss, description of weathering and identification of drilling induced fractures. This should be noted in the use of Core Log Sheets and remembered in their utilisation.

DRILLING AND CASING

The types of drilling used to advance the drill hole are recorded for relevant intervals. The types of drilling may include: NMLC coring, NQTT (NQ triple tube wire line), HW, HX, NW and NX casing, wash boring (tri-cone roller bit, TC drag bit, TC blade bit), or auger drilling (V-bit, TC drag bit).

The relevant progress is shown by abbreviated dates in the column.

WATER

Water lost or water made during drilling is recorded and subsequent readings of water levels in the borehole or piezometers are recorded here with dates of observation.

DRILL DEPTH AND CORE LOSS

Drilling intervals are shown by depth increments and horizontal marker lines. Core loss is measured as a percentage of the drill run. If the location of the core loss is known or strongly suspected, it is shown in a region of the column bounded by dashed horizontal lines. If unknown, core loss is assigned to the bottom of a coring run.

SAMPLES AND FIELD TESTS

The location of samples taken for testing or the location of field tests are indicated by the appropriate symbol from the GLOSSARY OF SYMBOLS Standard Sheet (or as applicable for the project) and are shown at the relevant location or over the relevant depth interval.

DEPTH (RL)

Changes in rock types or the locations of piezometer tips, samples, test intervals or other depths are shown as appropriate in terms of depth from the hole collar or in terms of RL.

For inclined holes the depths shown on the log refer to the drilled length along the borehole. The RL, where used, is the only transformed reference to true vertical depth.

STRATA

Rock types are presented graphically using the symbols shown on the GLOSSARY OF SYMBOLS Standard Sheet or as assigned for the project.

DESCRIPTION

The rock type is described in accordance with the ROCK DESCRIPTION Standard Sheet.

WEATHERING

Weathering is described, by code letters, in accordance with the ROCK DESCRIPTION Standard Sheet. A weathering term or range of terms is usually assigned to various strata.

It is noted, however, that the assignment of a term of weathering is subjective and is normally used for identification and does <u>not</u> imply engineering behaviour (such behaviour being controlled principally by rock substances strength and defect frequency - collectively, rock mass strength). Consequently, boundaries are often not shown and weathering may even not be reported where potentially misleading.

ESTIMATED STRENGTH

The strength of the rock substance is estimated by a combination of Point Load testing and tactile appraisal in accordance with the ROCK DESCRIPTION Standard Sheet. The estimated strength is presented in a histogram form. Both axial and diametric point load test results can be presented using the symbols on the GLOSSARY OF SYMBOLS Standard Sheet and the variation between axial and diametric values is indicative of anisotropy or fissility of the rock unit.

NATURAL FRACTURES

The identification of <u>natural</u> fractures requires an endeavour to exclude drilling induced breaks in the core and, as such, can be somewhat subjective. Natural fractures exist prior to coring the rock, whereas artificial fractures occur either during coring, during placing core in the core boxes, or during examination or transportation, or core after being boxed.

The log of Natural Fractures is presented as a combination of Fracture Spacing, Visual and Description columns. Coding is presented on the GLOSSARY OF SYMBOLS Standard Sheet.

ROCK QUALITY DESIGNATION (RQD) INDEX OPTION

The Core Log Sheet has an optional field column to record the RQD index. For certain projects, such as tunnelling or underground mining investigations, rock mass ratings or classifications can be required as part of the design process. The Rock Quality Designation (RQD) Index forms a component of these rock mass ratings and provides a quantitative estimate of rock mass quality from rock core logs. The core must be a minimum of 54.7mm diameter (although NMLC-sized core is probably OK) for derivation of an RQD index.

The RQD index is expressed as a <u>percentage of intact rock core</u> (excludes extremely weathered rock/residual soil) <u>greater than 100 mm</u> in length over the total selected core length. The total selected core length should be based on identifiable engineering geological domain characteristics. Should this not be practicable, RQD can be measured on a per run basis.

DYNAMIC CONE PENETROMETER (DCP) TESTING



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SCOPE

The Dynamic Cone Penetrometer (DCP) test comprises the measurement of the soil resistance to a steel rod driven into the ground by a dropped weight.

The DCP test is a simple manual test used in both sandy and clayey soils. The test is a measure of the shear strength of the soil at relatively shallow depth.

EQUIPMENT AND METHOD

A general description of the dynamic penetrometer apparatus used by our firm is presented in Australian Standard AS 1289.6.3.2. The equipment utilises a 9kg sliding weight with a drop height of 510mm. It is fitted with a conical tip. The equipment can be adjusted for a fall of 600mm and use of a blunt tip in accordance with AS 1289.6.3.3.

The test data are generally recorded as the number of blows (n) per 50mm of penetration. The test data are processed by our in-house computer software. For specific applications (such as pavement investigations), the data may be collected in the reverse form, i.e. as mm per blow. The results are presented either in tabular or graphic form for reporting purposes.

INTERPRETATION

The interpretation of the DCP results is generally based on the assumption that the measured resistance is a function of soil strength. A profile of soil strength (cohesive soils) or density index (cohesionless soils) can thus be established. The test often can be used to qualitatively indicate the presence of soft or loose zones within a soil profile.

The energy of the system per unit area is similar to that of an SPT approach. Thus, the common relationships of SPT and other parameters (say Dutch cone) can be utilised as a means of estimating soil properties, after appropriate site specific correlation. The interpretations from the test are approximate only, and this is particularly pertinent to sand profiles where the magnitude of confinement stress is important in the assessment of the results.

Interpretation of the DCP penetration rate at depth (up to 5m) must be conducted with due regard to side friction effects. In particular, care must be exercised with soft clay profiles where shaft resistance may have a significant unconservative impact upon the results.

In-situ California Bearing Ratio (CBR) values of clay soil subgrades are sometimes interpreted directly from DCP test results for use in road pavement design. In this case, the correlation between DCP and CBR based on that published in AUSTROADS Pavement Design Manual (1992) may be applied. This correlation should be verified by site specific laboratory testing, where appropriate. In addition, the effects of moisture content variations (in-situ verses design conditions) must be considered, as clearly the DCP test only reflects the shear strength of the soil at the time of testing.

LABORATORY TESTING



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GENERAL

Samples extracted during the fieldwork stage of a site investigation may be "disturbed" or "undisturbed" (as generally indicated on the trial hole logs) depending upon the nature and purpose of the sample as well as the method of extraction, transportation, extrusion and testing. This aspect should be taken into account when assessing test results, which must of necessity reflect the effects of such disturbance.

All soil properties (as measured by laboratory testing) exhibit inherent variability and thus a certain statistical number of tests is required in order to predict an average property with any degree of confidence. The site variability of soil strata, future changes in moisture and other conditions and the discrete sampling positions must also be considered when assessing the representative nature of the laboratory programme.

Certain laboratory test results provide interpreted soil properties as derived by conventional mathematical procedures. The applicability of such properties to engineering design must be assessed with due regard to the site, sample condition, procedure and project in hand.

TESTING

Laboratory testing is normally carried out in accordance with Australian Standard AS 1289 as amended, or RTA Standards when specified. The routine Australian Standard tests are as follows:-

Moisture Content	AS1289 2.1.1
Liquid Limit	AS1289 3.1.1)
Plastic Limit	AS1289 3.2.1) collectively known as Atterberg Limits
Plasticity Index	AS1289 3.3.1)
Linear Shrinkage	AS1289 3.4.1
Particle Density	AS1289 3.5.1
Particle Size Distribution	AS1289 3.6.1, 3.6.2 and 3.6.3
Emerson Class Number	AS1289 3.8.1)
Percent Dispersion	AS1289 3.8.2) collectively, Dispersive Classification
Pinhole Dispersion Classification	AS1289 3.8.3)
Hole Erosion (HE)	GHD Method
No Erosion Filter (NEF)	GHD Method
Organic Matter	AS1289 4.1.1
Sulphate Content	AS1289 4.2.1
pH Value	AS1289 4.3.1
Resistivity	AS1289 4.4.1
Standard Compaction	AS1289 5.1.1
Modified Compaction	AS1289 5.2.1
Dry Density Ratio	AS1289 5.4.1
Minimum Density	AS1289 5.5.1
Density Index	AS1289 5.6.1
California Bearing Ratio	AS1289 6.1.1 and 6.1.2
Shear Box	AS1289 6.2.2
Undrained Triaxial Shear	AS1289 6.4.1 and 6.4.2
One Dimensional Consolidation	AS1289 6.6.1
Permeability Testing	AS1289 6.7.1, 6.7.2 and 6.7.3

Where tests are used which are not covered by appropriate standard procedures, details are given in the report.

LABORATORY

Our laboratory is NATA accredited to AS ISO / IEC17025 for the listed tests.

The oedometer, triaxial and shear box equipment are fully automated for continuous operation using computer controlled data acquisition, processing and plotting systems.
REACTIVE SOILS

SITE MANAGEMENT PRECAUTIONS



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These precautions are considered supplementary to any structural and/or foundation design measures for the subject building, and are intended for distribution to the prospective building owner / occupier.

Reactive clays are prone to heave/shrink movements with changes in soil moisture content due to natural or artificial means. The basic design philosophy employed for the building is to provide a foundation/superstructure adequate to accommodate ground movements due to extreme seasonal moisture changes only. The possibility of other abnormal and/or localised moisture changes (the cause of most building distress) has been assumed to be controlled by the following site management procedures.

In particular, leaking plumbing or blocked drains should be repaired promptly and site grading maintained to prevent ponding near foundations. Garden watering, particularly by fixed systems, should be controlled carefully to avoid gross over-watering. On the other hand, proper garden maintenance should produce year round uniform moisture conditions.

Trees and shrubs can cause a substantial drying of the clay soil profile and associated shrinking of reactive clays. This effect is most likely to result in damage when added to the drying from a drought or a long dry spell. The problem can be avoided by planting trees at substantial distances from the building. The distance depends upon the species, soil conditions, and site classification.

Problems during droughts can be minimised by extensive pruning (thus reducing water demand) and/or providing trees with adequate water. This watering can be achieved by boreholes or trenches dug well into the clay between the tree and the footing. To avoid settlement problems, the holes or trenches should not be too close to the footing and should be filled with compacted screenings. The installation of root barriers is another option. Frequent moderate watering during dry periods also should assist in minimising the extraction of excessive moisture from beneath the foundation of the building by trees and other vegetation as well as the environmental effects.

This action should also be immediately undertaken by the owner / occupier if brickwork cracking due to tree drying is noticed. Most reactive clay failures can be avoided or the effects minimised by controlling the combined drying effects of trees and drought.

The owner / occupier should also appreciate that on reactive clays it is virtually impossible to design an economic foundation system which will totally prevent movement. Some minor aesthetic cracking, while undesirable, will occur in a significant proportion of houses. In addition, some minor problems should be expected with jamming of windows and doors, especially during the settling-in period or following a major drought, and such repairs should be regarded as part of normal building maintenance. Even significant masonry cracking with widths over 5mm usually has little influence on the function of the wall and presents an aesthetic problem. Just as it is difficult to design an immovable footing system, it is almost impossible to provide remedial measures that will prevent further movements if distress does occur. Consequently, extreme remedial measures should not be undertaken for minor problems.

Advice on these matters is addressed in Australian Standard AS2870 "Residential slabs and footings – Construction". In particular the designer, owner and occupier are referred to Appendix B "Performance Criteria and Foundation Maintenance" in AS2870.



Figures

Figure 1 – Test Location Plan Figure 2 – Geology Plan Figure 3 – Soils Plan

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Huntingwood West - Bungaribee Estate Huntingwood Report on Geotechnical Assessment







PROPOSED FIXED ROAD NETWORK 0 50 100 150m SCALE 1:5000 AT ORIGINAL SIZE

NOTE: CONTOUR INTERVAL 0.25m

REFERENCE: BASE SURVEY PROVIDED BY GOODMAN PROPERTY SERVICE PTY LTD



Plot Date: 11 December, 2008 - 11:56 AM Cad File No: 21-17871-FIG-001.dwg

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57-63 Herbert Street Artarmon NSW 2064 T 61 2 9462 4700 F 61 2 9462 4710 E artmail@ghd.com.au W www.ghd.com.au © 2008. While GHD has taken care to ensure the accuracy of this product, GHD and DATA SUPPLIER(S) make no representations or warranties about its accuracy, completeness or suitability for any particular purpose. GHD and DATA SUPPLIER(S) cannot accept liability of any kind (whether in contract, tort or otherwise) for any expenses, losses, damages and/or costs (including indirect or consequential damage) which are or may be incurred as a result of the product being inaccurate, incomplete or unsuitable in any way and for any reason. Data Sources: NSW Department of Primary Industries 100K Geology 2005 NSW Department of Lands DCDB 2008 Created by: rojohnson, hwarr



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Appendix A

Borehole Logs and Core Photographs

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Huntingwood West - Bungaribee Estate Huntingwood Report on Geotechnical Assessment



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		8	3.43				圉					8	8.41-8	
	-			:					-			Ž	8.48, E	9, 10°, CLAY, PLN, SO 91, FZ (EW zone)
-9				(9)	r							L	9.20, E	3P/JT, HZ/VT, CN, ST, SC
-													9.41, E	8P, HZ, CN, PLN, SO 8P/JT, VT/HZ, CN, ST, SC 8P, HZ, CN, PLN, SO
•				-		9.86		CORE LOSS 140mm thick (left down hole).						
-10		10	.00			10.00	М	End of borehole at 10.0 metres.						
						or 📕		GHD GEOTECHNICS					Job N	



	oject catio	n :	Н	UNT	ING	woo	D	and a second		<u></u>				SHEET	2 OF 2
-	sitior							5.0 N MGA94 / 56 Surface RL:	• • • • • • • • • • • • • • • • • • • •		Angle from I			· · · · · ·	Processed : RY
	д Тур				P So			ing: Truck Contractor :			Driller : T Hi				Checked : RML
	-	Dia. :						·	nond (stepfaced)		Bit Condition				Date: 5/12/08
Da		irted :		5/10/	08	D	ate C	ompleted : 16/10/08 Logged b			Date Logged				
D		RILLI						MATERIA Description	· · · · · · · · · · · · · · · · · · ·	1	Estimated		ITA		ACTURES
SCALE (m)	Drilling & Casing	Water / /		(Core Loss / Run %)	SAMPLES & TESTS	Depth / (RL) metres	Graphic Log	ROCK TYPE, colour, grain size (texture, mineral composition, alteration, cementation, etc. as and SOIL TYPE, moisture, co consistency, structure, minor comp Start of coring at 5 metres. For Non Cored interval, see Borehn	hardness, applicable) blour, ponents (origin)		Strength Is ₍₅₀₎ MPa	Spacing (mm) 000 000 000 000 000 000 000 000 000	Visual	(joints, p Fracture	artings, seams, zones ar veins) type, orientation, infilling shape, roughness, other
	· ·	5.9		0)		5.00		SHALE, dark grey/black, indist some bands of silty material.						5.16, BP/ 5.17, BP, 5.47-5.58 5.60, JT, 5.62, BP, 5.76, BP, SO 5.80, BP, 5.80, BP, 5.80, BP, 5.80, BP,	
	coring + HQ casing to 4.86m 06'9		0)						c				DIS heale	, JT, 85°, PLN/CU, FE, ed/intact	
-7	+ HQ casing to 4			0)					MW					7.07, JT, 7.08, BP, TI 7.37, JT,	70°, CN, PLN, RF, OP sub HZ, CN, PLN, SO, 80°, CN, ST/IR, RF, OP sub HZ, PLN, SO, TI
-8	Z	8.4	3_			•									20°, CLAY, PLN, SO HZ, CN, UN/PLN, RF
- - - -9								8.50-8.65, siltstone lamination	5. HW EW					8.95-8.98	5°, CN, UN, RF, OP , SM, CLAY SM, CLAY
				0)					HW MW				-	9.94&9.9	7.
ار ا	ļ	10.0	0			10.00		End of borehole at 10.0 metres	3.				=	BP's,HZ, zone)	5°,CLAY,UN/IR,SO,(EW
·10		10.0	0			10.00	<u></u>		.				<u> </u>	^{zone)} Job No	



Lo	oject : cation : sition :	: +	HUNTIN	ARIBEE INI NGWOOD)			56 Surface RL: 45.1m approx AHD Angle from Horiz.: 90°			ET 1 OF 3 Processed	
	g Type :			Scout Mo				Contractor : Terratest Driller : T Higgs			Checked :	
	ite Start							npleted : 15/10/08 Logged by : CS				5/12/0
		DRILL	ING					MATERIAL				<u></u>
		ر ا	[·	s.				T_	П		
SCALE (m)	Drilling Method	Hole Support \ Casing	Water	Samples & Tests	Depth / (RL) metres	Graphic Log	USC Symbol	Description SOIL TYPE, colour, structure, minor components (origin), and ROCK TYPE, colour, grain size, structure, weathering, strength	Moisture Condition	Consistency / Density Index	Comm Observ	
	 				0.10		!	CLAY, dark brown, low plasticity, with fine grained sand (topsoil).	м			
	, * , -*						CI- CH	CLAY, red brown, medium to high plasticity, with fine to medium ironstone gravel (alluvium).	M	F-St		
	•				0.50		-CL-	Sandy CLAY, light brown, low plasticity, fine grained sand, some black laminations and red brown ironstone	M	F-St		
				SPT 3/3/4 N=7			. 	(residual).				
-1				N=7			; {	At 1.0m, becoming grey and light brown mottled with				
				··			· 	depth.	,			
$\left \right $				 			۱ ۱					
	-		· ·				CI- CH	From 1.5m, some bands with remnant rock structure. No sand - clay, medium to high plasticity.		St		
				SPT 3/4/5 N=9			 					
-2	er						 		-			
	V-bit auge			r []		$\langle \rangle$. vi	
	3											
$\left \frac{1}{2} \right $. . 									
-3			(× -	, LI	3.00		 					
				SPT				SHALE, grey with black carbonaceous bands laminated, extremely weathered, extremely low strength (very stiff to hard clay).				
	, j			4/9/11 N=20			 					
-	1			· []			· . 					
	· ·			- -			. 					
-4			.				 	At 4.0m, sandstone and carbonaceous laminations, becoming highly weathered, very low to low strength.				
	14			SPT 7/15/21			 	Decoming inging weathered, very low to low suchgar.		1 1 1		
┣ ┣		$\left - \right $	<u>,</u>	N=36	4.50		 	Start of coring at 4.5 metres.	-			
			• •	· · · []			1.1 	For Cored interval, see Core Log Sheet.				
-5											۰	
Se	e stand tails of	dard s	sheets			GHI	D GE	OTECHNICS Street, Artarmon NSW 2064 Australia	J	Job N	10.	

	HEET				
Client :			TY SERVICES PTY LTD	HOLE No. B	H04
Project : .ocation :	HUNTING		TRIAL ESTATE		HEET 2 OF 3
Position :			0 N MGA94 / 56 Surface RL: 45.1m approx AHD	Angle from Horiz. : 90°	Processed : RY
Rig Type :		cout Mounting		Driller : T Higgs	Checked : frue
asing Dia. :	HQ		m): NMLC 3.5m Bit : Diamond (stepfaced)	Bit Condition : Good	Date : 5/12/08
ate Started :	15/10/08	Date Con	mpleted: 15/10/08 Logged by: CS	Date Logged : 15/10/08	
DRILLI	NG		MATERIAL	NATUR	AL FRACTURES
rogress	STS	es	Description	Estimated Spacing	Additional Data
Drilling & Casing Water Drill Depth (m)	Core Loss / Run %) SAMPLES & TESTS	Depth / (RL) metres Graphic Log	ROCK TYPE, colour, grain size, structure (texture, mineral composition, hardness, alteration, cementation, etc. as applicable) and SOIL TYPE, moisture, colour, consistency, structure, minor components (origin)	IS ₍₅₀₎ MPa Fr	ioints, partings, seams, zones ar veins) racture type, orientation, infilling coating, shape, roughness, other
		- F	Start of coring at 4.5 metres. For Non Cored interval, see Borehole Log Sheet.		
<10% loss			SHELE, grey, indistinctly bedded, highly friable rock, occasional brown iron staining.	4	.71, BP, 20°, CLAY+X, PLN, S

Progress (%) SI Description Estimated Spacing Additional Volume (%) <th>'</th> <th>catio</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>MGA</th> <th>01/54</th> <th>C</th> <th></th> <th>. AE</th> <th>1m c-</th> <th></th> <th></th> <th>۸-</th> <th></th> <th>from</th> <th>Hor</th> <th> (</th> <th>200</th> <th></th> <th>SHE</th> <th></th> <th>OF 3</th> <th></th>	'	catio								MGA	01/54	C		. AE	1m c-			۸-		from	Hor	(200		SHE		OF 3	
Case in plat. HQ Barrel (m): NMLC 3.5m Bit: Diamond (tespface) Bit Condition : Good Date : Date Started : 15/1008 Date Completed : 15/1008 Logged by : CS Date Logged : 15/1008 Date Logged : 15/1008 Date Completed : 15/1008 MATURAL FRACTUR Pogress (a) (b) (b) MATURAL FRACTUR Solid TPE: Joing and the appletable in puts and the appletable in puts and the appletable in puts and the appletable is appletable in puts and the appletable in puts and the appletable in puts and the appletable is appletable in puts and the appletable is appletable in puts and the appletable in puts and the appletable in puts and the appletable in puts appletable in puts and the appletable in puts appletable in puts	Ri																ULP		_			<u> </u>	50					
DRILLING MATERIAL NATURAL FRACTUR Progress S G <td< th=""><th>Ca</th><th>sing</th><th>Dia</th><th>ı.: I</th><th>HQ</th><th></th><th>E</th><th>Barrel</th><th>(m) :</th><th>NML</th><th>C 3.5m</th><th>ן E</th><th>Bit : Dia</th><th>amono</th><th>l (step</th><th></th><th></th><th>Bi</th><th>t Co</th><th>nditio</th><th>n: (</th><th></th><th></th><th></th><th></th><th></th><th></th><th>5ļ</th></td<>	Ca	sing	Dia	ı.: I	HQ		E	Barrel	(m) :	NML	C 3.5m	ן E	Bit : Dia	amono	l (step			Bi	t Co	nditio	n: (5ļ
Progress B Spacing B Spacing B Addition (units, structure (units, intruit components (origin)) B B B C B B B B C B B B B C B B B B C B B B B C B B B B C B B B B C B B B B C B B B B C B B B B C B B B B C B B B C B B B B C B B B B C B B B B C B B B C B B B B C B B B B C B B B B C B B B B C B B B B C C B B					-)/08	. C	Date C	omp	eted :	15/10				CS			Da	te L	ogge	d: 1	5/10			1175 4 1			
Bit Strength (mm) Strength (mm) (mm) <th< td=""><td></td><td></td><td></td><td>LLIN</td><td>1</td><td>S</td><td></td><td>1</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>F</td><td>stim</td><td>ated</td><td>S</td><td>oaci</td><td>-</td><td></td><td>JKAL</td><td></td><td></td><td>_</td></th<>				LLIN	1	S		1										F	stim	ated	S	oaci	-		JKAL			_
Image: State of the state	SCALE (m)	& Casing		Drill Depth (m)	(Core Loss / Run %	SAMPLES & TEST	Depth / (RL) metres	Graphic Log		(te alte	xture, m ration, c SOIL	E, colou ineral co ementati a TYPE, n	r, grain s impositic ion, etc. and noisture,	iize, stru n, hardr as appli colour,	ness, cable)	n)	Weathering	S Is 00.00	tren (50) I	gth /IPa		(mm)	Visual	Fractu	s, partin ire type	gs, sear veins) , orienta	ns, : tion
End of borehole at 6.0 metres.	- - - - -	NMLC coring + HQ casing		6.00	-		6.00		SH	ALE, a	is prev	rious.		• • • • • • • • • • • • • • • • • • •		· · · · · · · · · · · · · · · · · · ·	-			-								
	- - - - - - - - - - - -	· · ·																										
	•			•	-								•															
	-8 - - -								· · ·																			
	- - -9 -				-		· · ·				•																	
	-			- •										· · · ·														-

GOODMAN PROPERTY SERVICES CLIENT PROJECT BUNGARIAGE INDUSTRIAL ESTATE LOCATION HUNTINGNOOD GHD GEOTECHNICS BOREHOLE BH 04 4.57 m TO 60 m 21/1787100 JOB No DATE 15/10/08 21/17871/00 - BOREHOLE BH4 START ODRE AT 257m 15/10/08 5 BOREHOLE TERMINATE AT 6.0m 15/10/00

	ent : oject :			MAN PRO ARIBEE IN				HOLE No), I	BH)5
Lo	cation			NGWOOD						SHEE	T 1 OF 4
	sition :		1					Surface RL: 53.7m approx AHD Angle from Horiz.: 90°			Processed : RY
	y Type te Starf			Scout Mo	unting:			Contractor : Terratest Driller : T Higgs pleted : 13/10/08 Logged by : CS		· ·	Date: 5/12/09
		DRILL				Du	ie eeni	MATERIAL			54101 371401
SUALE (M)	Drilling Method	Hole Support \ Casing		Samples & Tests	Depth / (RL) metres	Graphic Log	USC Symbol	Description SOIL TYPE, colour, structure, minor components (origin), and ROCK TYPE, colour, grain size, structure, weathering, strength	Moisture Condition	Consistency / Density Index	Comments/ Observations
					0.10	\bigotimes		SAND, dark grey, fine to medium grained, fragments of \tiles, ash, concrete (fill).			
-				SPT 2/3/7			CH	CLAY, red brown, high plasticity (residual).	Μ	F-St	
	V-bit + Solid Flight Auger	Nil		N=10 SPT	0.90			SILTSTONE/SHALE, brown, horizontally bedded, iron oxide and manganese oxide stained joints, highly weathered, very low strength.			
				22/15/21 N=36	2.60			Start of coring at 2.6 motion			
								Start of coring at 2.6 metres. For Cored interval, see Core Log Sheet.			
			-			· · ·					
ե. 		I		······································					·		
	e stan tails of				HD	57 He	erbert S	DTECHNICS treet, Artarmon NSW 2064 Australia	J		
		of des				1:61	1 2 9462	2 4700 F: 61 2 9462 4710 E: atnmail@ghd.com.au	1	- 71	-17871-00

Lo	catio	n <u>;</u>			GWOC					EET 2 OF 4
Po	sitior	i t	302	550.0)E 62	58199	.0 N MGA94 / 56 Surface RL: 53.7m approx AHD	Angle from I	loriz. : 90°	Processed : R
	д Тур			roP S				Driller : T Hig		Checked : RA
	sing							Bit Condition		Date : ろ/い
Da	te Sta			0/08	1	Date C		Date Logged		
_		RILLI	NG		ļ		MATERIAL			L FRACTURES
Pro	ogres	5	(%)	STS	Les		• • • • • • • • • • • • • • • • • • • •	Estimated Strength	Spacing	Additional Data
SCALE (m)	Drilling & Casing	Water Drill Denth (m)	(Core Loss / Run %)	SAMPLES & TESTS	Depth / (RL) metres	Graphic Log	ROCK TYPE, colour, gran size, structure (texture, mineral composition, hardness, alteration, cementation, etc. as applicable) and D SOIL TYPE, moisture, colour, consistency, structure, minor components (origin) D C	ls ₍₅₀₎ МРа	Frac	tts, partings, seams, zon veins) ture type, orientation, inf tting, shape, roughness,
•1										
2										
			-		2.60		Start of coring at 2.6 metres. For Non Cored interval, see Borehole Log Sheet. SHALE, dark grey, thinly to moderately			
•3			(24)	3.28		bedded, generally horizontal.		3.14	, BP, 20°, FE, CU, SO, 1
	Ð	3.5	0		3.50		CORE LOSS 220mm thick. SHALE, as above.		3.54	, JT, 60°, CN, PLN, SO,
•4	NMLC coring				-				TI	, BP, sub HZ, CN, PLN, , BP, HZ, CN, PLN, SO,
			(3)				HW		TI 4.26 4.29 TI 4.45	, BP, 10°, FE, PLN, ST, , BP, 15°, CN, PLN, SO, , BP, sub HZ, CN, PLN, , BP, 10°, FE, UN/IR, SC , BP, 5°, CN, PLN, VR, 1
.				1		+===			79 لا 🏳 🛛 🔜 🗌 🗌 🗌 🗌	, BP, 50°, FE, IR, SO, T

Big Type: HydroP Scout Mounting: Truck Contractor: Terratest Driller: Higgs D Casing Dia:: HQ Barrel (m): NMLC 3.5m Bit: Diamond (terpfaced) Bit Condition: Good D Date Startid:: S10/08 Dete Completed: 131/008 Dete Completed: Startig MATERIAL NATURAL FRA Progress Startig Startig Startig Startig Startig Startig Material Sparsing AnturAL FRA Progress Startig Startig Startig Progress Startig Sparsing AnturAL FRA Progress Startig Startig Startig Progress Startig Sparsing AnturAL FRA Progress Startig Startig Startig Progress Startig Sparsing AnturAL FRA Progress Startig Startig Progress Sparsing Startig Sparsing Startig Startig Startig Sparsing Sparsing Sparsing <td< th=""><th>ET 3 OF 4 Processed</th><th>SHEE</th><th></th><th></th><th>from</th><th>Aniele</th><th></th><th>OON MCADA / 56 Surface DL - 50 7</th><th></th><th>WOC</th><th></th><th></th><th></th><th></th><th>catio</th><th></th></td<>	ET 3 OF 4 Processed	SHEE			from	Aniele		OON MCADA / 56 Surface DL - 50 7		WOC					catio	
Case DBa: HO Barra (m): MMLC 3.5m Bit: Damond (stepface) Bit: Condition :: Good Description Total Started: 13/10/06 Logged by: CS Date Logged 1: 13/10/07 VALUEA: FALL	Checked :															
DRILLING MATURAL MATURAL FRA Progress (E) (E) (E) (E) (E) (E) (E) (E) (E) (E)	Date : S											-				_
Progress Spacing Spacing Add 0				: 13/10/08	ogged	Date L		Completed: 13/10/08 Logged by: CS	Date C	0	/08	3/10	e d : 1	arte	te St	Da
Strength (build and measure (build and measure			ΙΑΤΙ	N				MATERIAL				3	LINC			
66 6.60 5.76, BP, HZ 7 (0) 5.80 5.76, BP, HZ 8 6.60 5.76, BP, HZ 5.83, BP, HZ 9 8.60 90, BP, 57 6.84, BP, 57	Additional D s, partings, seams, veins) rre type, orientation ng, shape, roughn	(joints, Fractur	Visual	(mm)	igth APa	Stren Is ₍₅₀₎ I	Weathering	ROCK TYPE, colour, grain size, structure (texture, mineral composition, hardness, alteration, cementation, etc. as applicable) and SOIL TYPE, moisture, colour,	Graphic Log	Depth / (RL) metres	SAMPLES & TESTS	(Core Loss / Run %)	Drill Depth (m)) & Casing	
SILTSTONE, dark grey and grey laminations, within bedden to laminated, some sandy bands and shaley bands.								SHALE, as above.								۲ ۲
0 008, BP, 5* 0 0	8P, HZ, CN, PLN, S 8P, sub HZ, FE, PL1 8P, HZ, CLAY, UN,	5.47, BF				•		very thinly bedded to laminated, some sandy		5.40			5.60			
-7 (0) (0) -8 -8 -8 -8 -9 -9 -9 -0 -7 -7 -0 -0 -0 -0 -0 -0 -0 -0 -0 -0	99, 5°-10°, CLAY, IF 19, 5-10°, CLAY, IR 19, 5°, CN, PLN, SC	6.08, BF									-					6
-8 8.60 -9 WW	SP, 10 CLAY, PLN, T's, Cb, VT, PLN, C M, CLAY, 35mm	6.91, BF 6.93, JT 6.96, SN	I			•	мw					(0)	-			7
8.60 8.48-8.51, E															NMLC coring	
-9 8.60	3.21, EW zone	8.14,-8.2	Ħ								-					8
мw-	.51, EW zone	8.48-8.5	H (3)									, , ,	8.60			
	3P, 5°, CN, PLN, S(9.08, BF					MW HW				•	(0)				9
		-					-									

Po	ocatio ositio	n :		3025	50.0		58199	.0 N MGA94 / 56 Surface RL: 53.7m approx Al	HD		Horiz. : 90°	HEET 4 OF 4 Processed : RY
_	g Typ				oP S			ng: Truck Contractor : Terratest		Driller : T Hi		Checked : RML
	ising ite St			HQ	1/08			(m): NMLC 3.5m Bit : Diamond (stepfaced) ompleted : 13/10/08 Logged by : CS		Bit Conditio		Date : 5/12/0
			LIN				ale C	MATERIAL		Date Logget	1	AL FRACTURES
Pro	ogres			—	S			Description		Estimated	Spacing	Additional Data
Pro SCALE (m)	g & Casing	Water	Drill Depth (m)	(Core Loss / Run %)	SAMPLES & TESTS	Depth / (RL) metres	Graphic Log	ROCK TYPE, colour, grain size, structure (texture, mineral composition, hardness,	Weathering	Strength Is ₍₅₀₎ MPa	(mm) (ji	oints, partings, seams, zones veins) racture type, orientation, infillir coating, shape, roughness, oth
┠──┤			0.06			_10.06	· ·	_SILTSTONE, as previous.	_	┉╱┈╱╌╱╙	04+0+ >	
t I								End of borehole at 10.06 metres.				
11												
- - 12 - - - - -									and the second			
- 13 - - -	ан Х С				ч Т. 							
- - - -14						-						
						•						

GOODMAN PROPERTY CLIENT PROJECT BUNGARIBEE ESTATE LOCATION HUNTINGWOOD GHD GEOTECHNIC BOREHOLE BH05 , 2.58 m TO 7.0 m 21/17871/00 DATE 13/10/08 JOB No GOODMAN-BUNGARIBEE ESTATE - BHOS- START COPE AT 2.58m cone Loss - 226m 3 4 CORE 5 6 GOODMAN PROPERTY CLIENT PROJECT BUNGARIBEE ESTATE LOCATION HUNITINGWOOD GHD GEOTECHNICS BOREHOLE BHØ5 ,7.0 m TO10.06m 21/17871/00 DATE 13/10/08 JOB No 8.02 9 BOREHOLE BH5 TERMINATED AT 10.06 m - 13/10/08 10 1.8



	catio sitior					W00		3.3 N MGA94 / 56 Surface RL: 56.8m approx Al		Angle from I	Hori- 1009		SHEE	T 2 OF 2 Processed :
	g Typ							ing: Truck Contractor : Terratest	עה	Driller : T Hi				Checked :
	singl			IQ ·				(m): NMLC 3.5m Bit : Diamond (stepfaced)		Bit Condition				Date : 5
Dat	te Sta	rted	: 1	6/10	/08			ompleted: 16/10/08 Logged by: CS		Date Logged	1: 13/10/08	3		
	D	RILL	ING	;				MATERIAL			· · · · ·	NATI	JRAL	FRACTURES
Pro	gres	3		(%	TS	se		Description		Estimated	Spacing	Ι		Additional D
SCALE (m)	Drilling & Casing	Water	unii uepm (m)	(Core Loss / Run %)	SAMPLES & TESTS	Depth / (RL) metres	Graphic Log	ROCK TYPE, colour, grain size, structure (texture, mineral composition, hardness, alteration, cementation, etc. as applicable) and SOIL TYPE, moisture, colour, consistency, structure, minor components (origin)	Weathering	Strength Is ₍₅₀₎ MPa 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	(mm)	Visual	Fractu	, partings, seams, veins) re type, orientatior ıg, shape, roughne
		6.	09_	(0)		5.00		SHALE, grey and light brown bands, horizontal to 10°, bedding with bands up to 150mm of siltstone, thinly bedded.	HW- EW				5.55, B	P, HZ, CLAY, UN, P, 20°, CLAY, PLN P, 10°, CLAY, PLN
•			-			6.20		SANDSTONE, brown and grey brown, fine grained, thinly to very thinly bedded, with siltstone laminations up to 2mm thick at variable spacing. From 6.6m, becoming grey.	нw	B			6.20, B 6.38, B 6.46-6. 6.56, B healed	P, 10°, CLAY, PLN P, 5°, FE, CU, SO P, 5°, FE, PLN, RF 49, FZ P, 15°, CLAY, PLN P, sub HZ, FE, PLN
-7						7.10		N SILTSTONE/SHALE, dark grey/grey, indistinctly bedded, highly friable rock.	ww				6.82, B 6.91, B	P, sub HZ, FE, PL1 P, sub HZ, FE, PL1
	NMLC coring			(0)					нw				7.55, J	P/ST, 45°, FZ (drill T, 75°, CLAY, PLN,
-8	-													T, 60°, CLAY, PLN, 00, FZ (drill induce T, 70°, CLAY, ST/P
		8.	46					From approx 8.50m, evident laminated structure, alternating SILTSTONE/SHALE laminates.					8.73-8.	75, BP, HZ, CN, Pl
-9				12)					ΜW					
						9.81			w					
-10		10.	<u></u>		l	10.00			I				Job N	



Cate Started: 16/10/06 Date Completed: 16/10/06 Logged by: CS Date: DRULING MATERIAL Description 50 Difference Difference 50 Difference 50 Difference Difference	Po Rig	cation sition : J Type	3 : ⊦	02248 lydroP	Scout Mc	8633.0 I	Truc	k .	6 Surface RL: 41.3m approx AHD Angle from Horiz.: 90° Contractor: Terratest Driller: T Higgs upleted: 16/10/08 Logged by: CS		SHEE	T 1 OF 3 Processe Checked	: pri
1 1 <th>Da</th> <th></th> <th></th> <th></th> <th>0</th> <th></th> <th>Da</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>5/0/</th>	Da				0		Da						5/0/
CL grained, low plasticity (topsol). CL grained, low plasticity, trace fine grained M F CL CL CLAY, brown, low to medium plasticity, trace fine grained M F SPT 2335 N=5 At 1.5m, becoming brown and gray motified, with red-brown ironstone gravel. SPT 5/10/10 N=20 At 3.0m, increasing ironstone gravel to bands approx 15 0mm thick. SPT 5/10/10 N=20 At 3.0m, increasing ironstone gravel to bands approx 15 0mm thick.	SCALE (m)	Drilling Method	Hole Support \Casing	Water	Samples & Tests	Depth / (RL) metres	Graphic Log	USC Symbol	SOIL TYPE, colour, structure, minor components (origin), and ROCK TYPE, colour, grain size, structure,	Moisture Condition	Consistency / Density Index	Observ	
-1 -1 SPT 2/35 N=8 C.I. Sand/slit. C.I. Sand/slit. C.I. Sand/slit. M F -1 -1 SPT 2/35 N=8 At 1.5m, becoming brown and grey mottled, with red-brown ironstone gravel. M F -2 -2 -3 SPT 3/5/8 N=11 At 1.5m, becoming brown and grey mottled, with red-brown ironstone gravel. St -3 -3 -4 -4 -4 -4 -4 -4 -4 -4 -4								SC/ CL		M			
At 1.5m, becoming brown and grey motified, with St SPT SPT SPT SPT SPT SPT SPT SPT						0.30			CLAY, brown, low to medium plasticity, trace fine grained sand/silt.	м	F		
-2 B SPT 35% N=11 SPT 35% N=11 red-brown ironstone gravel. -3 SPT 5/10/10 N=20 At 3.0m, increasing ironstone gravel to bands approx VSt -4 SPT 18 4.17 Start of coring at 4.17 metres. VSt					2/3/5						ж. 		
-2 Borner 13/3/5/6 N=11 SPT 3/5/6 N=11 red-brown ironstone gravel. -3 SPT 5/10/10 N=20 At 3.0m, increasing ironstone gravel to bands approx 150mm thick. VSt	-1	• •			2								
-2 -3 -3 -3 -3 -3 -4 <			-						At 1.5m, becoming brown and grey mottled, with red-brown ironstone gravel.		St	• •	
At 3.0m, increasing ironstone gravel to bands approx SPT 5/10/10 N=20 4.17 Start of coring at 4.17 metres.	-2	rger			3/5/6								
At 3.0m, increasing ironstone gravel to bands approx SPT 5/10/10 N=20 VSt 150mm thick. VSt VSt VSt VSt VSt VSt VSt 150mm thick.	•	V-bit au			- - -								
At 3.0m, increasing ironstone gravel to bands approx 150mm thick. SPT 5/10/10 N=20 4 SPT 5/10/10 N=20 SPT 5/10/10 N=20 Start of coring at 4.17 metres.	-			-									
-4 ¥ -4 ¥ -4 SPT -4 HB 4 4.17	- -3			•					At 3.0m, increasing ironstone gravel to bands approx		VSt	-	
SPT 18 4.17 HB Start of coring at 4.17 metres.	•			-	5/10/10				150mm thick.				
SPT 18 4.17 HB Start of coring at 4.17 metres.		·			•								
HB Start of coring at 4.17 metres.	-4			Ţ		4.17							
	-	-			HB				Start of coring at 4.17 metres. For Cored interval, see Core Log Sheet.				
	-												

<u> </u>	catio					SWOO		·	_			HEET 2 OF 3
≤—	sition g Typ							3.0 N MGA94 / 56 Surface RL: 41.3m approx AH ing: Truck Contractor : Terratest	D	Angle from I Driller : T Hi		Processed : RY Checked : P.U.
101 —	g iyp Ising				or 3			(m): NMLC 3.5m Bit : Diamond (stepfaced)	<u></u>	Bit Conditio		Date : 5/12/08
<u> </u>	ite Sta	_	_)/08			completed : 16/10/08 Logged by : CS		Date Logged		Date: STIENO
H								MATERIAL				AL FRACTURES
-	ogres	s		(%	<u></u> δ	ي ي		Description		Estimated	Spacing	Additional Data
SCALE (m)	Drilling & Casing	Water	Drill Depth (m)	(Core Loss / Run %)	SAMPLES & TESTS	Depth / (RL) metres	Graphic Log	ROCK TYPE, colour, grain size, structure (texture, mineral composition, hardness, alteration, cementation, etc. as applicable) and SOIL TYPE, moisture, colour, consistency, structure, minor components (origin)	Weathering	Strength Is ₍₅₀₎ MPa		oints, partings, seams, zones a veins) racture type, orientation, infillin coating, shape, roughness, oth
GEO 			· · · ·									
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• • •												
- - - -3												
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-4	bu					4.17			IW,			
- - - - - -5	NMLC coring + HQ casing		5.00	(14)		4.90	\setminus	to thickly bedded, with carbonaceous laminations <1mm thick at variable spacing.			4. 4. R	22, BP, sub HZ, FE, PLN, RF 24, JT, VT, CN, PLN, RF, OP 27, BP, 5°, FE, CU/UN, RF/VF 43, BP 10°, FE+CLAY, PLN/C F, OP 74, BP, sub HZ, X, PLN, RF, T

Project: BUNGARIBEE INDUSTRIAL ESTATE HOLE No. BH07 coation: HUNTINGWOOD SHEET 3 OF 3 selicition: 302240.5E 6258633.01 M MGA94 / 56 Surface RL: 41.3m approx AHD Angle from Horz. ::0'' hype: HydroP Scout Mounting: Truck Contractor: asting Dia: HO Barrel (m): MNLC 3.3m Bit ::Diamond (step/aced) Bit Condition: Good Date: Visita Startd: 10/1008 Date Completed: 10/108 Logged: 10/1008 Date Completed: DRILLING MATERIAL NATURAL FRACTURES NATURAL FRACTURES NATURAL FRACTURES Ording altapa, rough stat, miner compania, structure, and attract, miner compania, structure, and attract in a septexted; structure, and attract, and attr	CI	ient :	:	(GOO	DM/	N PR	OPEF	RTY SERVICES PTY LTD	
Castina: 302248.0 E E 26833.0 N MC640/168 Surface RL 413m approx AHD Angle from Hotz:: 00* Processed: RY Ngh Tyn: Hydro? Scout Mounting: Truck Contractor: Transies Dellar: THiggs Checkled: DAX Big Tyn: Hydro? Scout Mounting: Truck Contractor: Transies Dellar: THiggs Checkled: DAX Big Tyn: Bit Completed: 1101005 Date Complete: Transies Output: Contractor: Transies Date Complete: Contractor: Transies Date Complete: Contractor: Transies Date Complete: Contractor: Transies Date Complete: Contractor: Contractor: Transies Date Complete: Contractor: Transies Date Complete: Contractor: Transies Date Complete: Contractor: Contractor: Transies Date Complete: Contractor: Contractor: Contractor: Transies Date Complete: Contractor: Contracto									HOLE No	BH07
Big Type: Hydro P Scont Mounting: Truck Contractor : Territent Differ: T Higgs Checkel: 2, p.1. Bare (Br): MOL 0.56 Bit : Diamod (steppicet) Bit : Diamod (steppicet) Bit : Diamod (steppicet) Bit : Diamod (steppicet) Diate : Diaged : 16/10/08 Diate :		_								
Barray Din: HO Barray (m): NMLC 25:m Bit: Diamond (stepficeer) Bit Condition: Codd Date: STATU: DRLLMO Date Completed: 16/1008 Date Cognet: Codd Date: STATU: Codd: Marking Bit: Discurption: Date: Status: Date: Codd Date: Status: Date:										
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DetLinio MATERIAL NATURAL FRACTURES regress (a) (b) (b) (b) (b) (b) (b) (b) (b) (b) (b	_)/08				Build Shich
Strength (m) (m) (m) <th(m)< th=""> <th(m)< th=""> <th< th=""><th></th><th>[</th><th>DRI</th><th>LLING</th><th>3</th><th></th><th></th><th></th><th></th><th>ATURAL FRACTURES</th></th<></th(m)<></th(m)<>		[DRI	LLING	3					ATURAL FRACTURES
9 6 9	Pro	ogres	ss		(%	TS	s			Additional Data
B 002 SANDSTONE, as previous. 000 00	SCALE (m)	Drilling & Casing	Water	Drill Depth (m)	(Core Loss / Run		Depth / (RL) metre	Graphic Log	ACUCK TYPE, colour, gran size, structure (texture, mineral composition, hardness, alteration, cementation, etc. as applicable) and SOIL TYPE, moisture, colour,	Fracture type, orientation, infilling coating, shape, roughness, other
ee standard sheets for SHEEL ATARMON NSW 2004 Australia	6	NMLC coring + HQ casing		6.00	(0)				From 5.73m, becoming grey with bands of MW-	PLN, VR, OP 5.22-5.24, SM, CLAY 5.29, JT, 80°, CN, ST/PLN, VR, OP
ee standard sheets for ST Herbert Street, Artamon NSW 2064 Australia				2.00			0.00		End of borehole at 6.0 metres.	
57 Herbert Street, Artarmon NSW 2064 Australia										
57 Herbert Street, Artarmon NSW 2064 Australia		ι.		-						
57 Herbert Street, Artarmon NSW 2064 Australia	יע 	o 04-	304	امروا	shee	te f		······		
								GHI	57 Herbert Street, Artarmon NSW 2064 Australia	

PROJECT BUNCANDER INDUSTRIAL CSIME	OTECHNICS
21/17871/00 - GOODMAN PROPERTY SERVICES - BINGARIBEE INDUSTRIL ESTA	re - BHØ7- 16/10/08
START CORE ON 417m	3759 <u>9</u> 2
BOREHOLE (BHØ7) TERMINATED AT 60m. 16/10/08	
	A CHARGE AND A

	ient : oject :			MAN PRO ARIBEE IN					HOLE N	o.	BH	08
	cation			NGWOOD			017112				SHEE	T 1 OF 3
	sition	: 3	302547	7.5 E 6258	817.6	N MG	A94 / 5	6 Surface RL: 50.8m approx AHD	Angle from Horiz. : 90°			Processed : RY
Ri	д Туре	: +	HydroF	Scout Mo	unting			Contractor : Terratest	Driller : T Higgs			Checked : FM
Da	ite Star	ted : 1	15/10/0	8		Da	te Com	pleted : 15/10/08	Logged by : CS			Date : 5/12/0
		DRILL	ING					MATERIAL				,
SCALE (m)	Drilling Method	Hole Support \ Casing		Samples & Tests	Depth / (RL) metres	Graphic Log	USC Symbol	Descriptio SOIL TYPE, colour, minor components and ROCK TYPE, colour, grai	, structure, s (origin),	Moisture Condition	Consistency / Density Index	Comments/ Observations
SCAI	Drillir	Hole \Cas	Water	Sam	Dept	Grap	nsc	weathering, str		Moist	Cons Dens	
					0.30		SC/ CL	Sandy CLAY/Clayey SAND, dark b low plasticity (topsoil/fill).	prown, fine grained sand,	M		
-					0.00		CI- CH	CLAY, red brown, brown and grey plasticity, trace fine grained sand a	mottled, medium to high and rootlets (residual).	M	F	
- - -			k i	SPT 2/4/4 N=8					• • • •		: :	
- -1 -				N-0			ан са Стала Стала са	From 0.9m, no red brown mottling.				Increased drilling resistance from
⊾ -` -	er											1.0m
	V-bit + Solid Flight Auger	Nil		SPT				1.5m, becoming grey with orange bands, some remnant rock structu	/ red brown ironstone re.	M	St	
-2	it + Solid I			6/4/5 N=9								
	q-7											
	- -											
				<i>9</i> .	2.80			SHALE, dark grey, with black lamin bedded, highly weathered to extre low to extremely low strength.	nations, horizontally mely weathered, very			2.8m, Increased drilling resistance
-3 -		asing		SPT 21/				iow to extremely low strength.				
		HQ Casing		20 for 120mm HB N=ref	3.60							
								Start of coring at 3.6 metres. For Cored interval, see Core Log S	Sheet.			
-4 -					;							
						-						
		5.							an an Arta An Arta Arta an Arta			
-5	*• 											
l Se	e stan	dard s	sheets		HD	GHI	DGE	OTECHNICS Street, Artarmon NSW 2064 Austral	· .	J	ob N	10.

<u>ب</u>	ocati ositi					E 62		N MGA94 / 56 Surface RL: 50.8m approx AHD Angle from Horiz. : 90°	HEET 2 OF 3 Processed : 1
	lig Ty			Hydr	oP S	cout N	lount	g: Truck Contractor : Terratest Driller : T Higgs	Checked : ƙ
- C	asing			HQ				n): NMLC 3.5m Bit : Diamond (stepfaced) Bit Condition : Good	Date : 5/
				15/1	0/08		Date C	npleted : 15/10/08 Logged by : CS Date Logged : 15/10/08	
			ILLIN	1	T		1		AL FRACTURES
	Drilling & Casing		Drill Depth (m)	(Core Loss / Run %)	SAMPLES & TESTS	Depth / (RL) metres	Graphic Log	(texture, mineral composition, hardness, alteration, cementation, etc. as applicable)	Additional Dat bints, partings, seams, zo veins) acture type, orientation, i coating, shape, roughnes
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ŀ								Start of coring at 3.6 metres.	
ŀ						3.60	.	For Non Cored interval, see Borehole Log	
Į	· · ·	-				0.00	E	SHALE, grey brown, with brown iron stained	69, FZ, FE
╞							臣	nedium bedded, highly friable rock.	80-3.82, FZ/BP's, 5-10°,
Ę,	casing						鬪		E+CLAY, UN, SO 94, BP/SM, HZ, CLAY, I
ŀ	2 cat				, ,		圜	HW	D, OP
ŀ	¥	Loss					臣		18, SM, 5mm CLAY
t	ring	<10% Loss		(0)					25, BP, ~HZ, CLAY, FR. F, OP 31, BP, HZ, CN, PLN, S
ŀ	00	Ý					圉		, -, , , , , , , , , , , , , , , , ,
ŀ	NMLC coring + HQ						圜		. •
Į	²						Ē	4.70-4.80m, siltstone/silty sandstone band from 4.80, with siltstone and fine sandstone	69, BP, 20°, CN, PLN, S
ŀ			4.99				Ē	aminations.	
-5	I		-1.32	<u></u>	<u>.</u>		Ļ- <u>-</u>		

Rig	sition g Type sing I	e :	ł	lydr		cout N	lount	7.6 N MGA94 / 56 Surface RL: 50.8m approx AHD Angle from Horiz.: ing: Truck Contractor: Terratest Driller: T Higgs (m): NMLC 3.5m Bit : Diamond (stepfaced) Bit Condition: Good	-	SHE	Processed : RY Checked : $RALL$ Date : $5/(2/0)$
Dat	te Sta	arte	d: 1	5/10)/08			ompleted : 15/10/08 Logged by : CS Date Logged : 15/10	0/08		
			LINC	•				MATERIAL		TURAL	FRACTURES
SCALE (m) of	Drilling & Casing		Drill Depth (m)	(Core Loss / Run %)	SAMPLES & TESTS	Depth / (RL) metres	Graphic Log	Description ROCK TYPE, colour, grain size, structure (texture, mineral composition, hardness, alteration, cementation, etc. as applicable) and SOIL TYPE, moisture, colour, consistency, structure, minor components (origin)) 	Fractu	Additional Data , partings, seams, zones a veins) re type, orientation, infilling ng, shape, roughness, othe
SCALE	NMLC coring + HQ casing	<10% Loss	3 00	(0)				As previous. From 5.33m, Shale, dark grey, indistinct bedding. Occasional siltstone/sandstone laminations. MW			3P, HZ, FE, PLN, RF 3P, HZ, CN, PLN/UN, RF
-6 -		+	<u>3.00</u>			6.00		End of borehole at 6.0 metres.			
-8			•		-						
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Clien	t :	(MAN PRO		•				BH	ng
Proje ocat	ct: tion:			ARIBEE IN NGWOOD		RIALE	STATE				ET 1 OF 3
ositi						N MG	A94 / 5	6 Surface RL: 50.3m approx AHD Angle from Horiz. : 90°			Processed : RY
tig T	ype :			Scout Mo				Contractor : Terratest Driller : T Higgs			Checked : RML
)ate \$	Start	ed: 1	7/10/0	8		Dat	te Com	pleted: 17/10/08 Logged by: CS			Date: ちんとの
	I	DRILL	ING					MATERIAL			
	Drilling Method	Hole Support \ Casing	Water	Samples & Tests	Depth / (RL) metres	Graphic Log	USC Symbol	Description SOIL TYPE, colour, structure, minor components (origin), and ROCK TYPE, colour, grain size, structure, weathering, strength	Moisture Condition	Consistency / Density Index	Comments/ Observations
								Clayey SAND/Sandy CLAY, fine grained low plasticity (topsoil).	м		
				SPT 2/2/3 N=5	0.20		CI- CH	CLAY, orange brown, medium to high plasticity, with fine grained grained sand, trace coarse grained sand and fine sub-rounded to sub-angular gravel (colluvium/alluvium).		S-F	
					1.00		-CL	CLAY/Sandy CLAY, brown and grey mottled, fine grained sand, low to medium plasticity (residual).	M	St	
	Flight Auger			SPT 3/6/6 N=12							
	V-bit + Solid Flig										
		-			-		-				
				SPT 6/6/11 N=17				From 3.0m - with ironstone bands, and manganese oxide stained defects, grading to extremely weathered rock.			
-	-			SPT 9/17/ 23 for	4.00			SHALE, grey with brown bands, highly weathered low to very low strength.			
		-		110mm HB N=ref	4.43		•	Start of coring at 4.43 metres. For Cored interval, see Core Log Sheet.			
tail	s of	abbro	heets eviatio	ons C	HD	57 He T: 61	erbert S 2 946	OTECHNICS Street, Artarmon NSW 2064 Australia 2 4700 F: 61 2 9462 4710 E: atnmail@ghd.com.au NG GEÒTECHNICAL ENGINEERS AND GEOLOGISTS	J	lob N 2'	io. 1-17871-00

Loca Posi Rig 1 Casi Date Prog	ition Type	ı :				SWOC	DD				54	EET 2 OF 3
Rig Casi Date	Тур			302							011	
Casi Date		<u>ه</u> .						0.0 N MGA94 / 56 Surface RL: 50.3m approx A	HD	Angle from		Processed : RY
Date	ing I				oP S			ing: Truck Contractor : Terratest		Driller : T H		Checked : ent
·				HQ				(m): NMLC 3.5m Bit : Diamond (stepfaced)		Bit Conditio		Date : 5/12/08
Prog					0/08	1	Date C	completed : 17/10/08 Logged by : CS		Date Logge		
Prog			LIN	G				MATERIAL				L FRACTURES
SCALE (m)	g & Casing		Drill Depth (m)	(Core Loss / Run %)	SAMPLES & TESTS	Depth / (RL) metres	Graphic Log	Description ROCK TYPE, colour, grain size, structure (texture, mineral composition, hardness, alteration, cementation, etc. as applicable) and SOIL TYPE, moisture, colour, consistency, structure, minor components (origin)	Weathering	Estimated Strength Is ₍₅₀₎ MPa	Fra	Additional Data nts, partings, seams, zones an veins) cture type, orientation, infilling of ating, shape, roughness, other
1												
3												
5				(0)		4.43		Start of coring at 4.43 metres. For Non Cored interval, see Borehole Log Sheet. SHALE, grey with bands of brown and dark-grey/black, bedded from 5°-30°, indistinct bedding structure, highly friable.	H W H W H W H W H W H W H W H W H W H W		4.7	5-4.65, FZ/SM, 20°, CLAY+FE vel 1-4.73, SM, 15°, CLAY 3-4.79, FZ, FE 3, SM 10mm, 20° 5, SM, 5mm, 5°

Po Ri	ocation osition g Type): 9:		3027 Hydro	33.0	cout N	58469 Iount	i ng: Truck	Contractor			Angle from Driller : T H	iggs	51	HEET 3 OF 3 Processed : RY Checked : P.UL
	asing I ate Sta)/08			(m): NMLC 3	/10/08 Logged	amond (stepfaced)		Bit Conditio		3	Date : 5/12/0
			LIN			_			MATER				1		AL FRACTURES
SCALE (m)	Drilling & Casing		Drill Depth (m)	(Core Loss / Run %)	SAMPLES & TESTS	Depth / (RL) metres	Graphic Log	(textur alteratio S	Description TYPE, colour, grain s e, mineral compositio n, cementation, etc. a and OIL TYPE, moisture, y, structure, minor cor	ize, structure n, hardness, as applicable) colour,	Weathering	Estimated Strength Is ₍₅₀₎ MPa	Spacing (mm)	(jo Fra co	Additional Data oints, partings, seams, zones a veins) acture type, orientation, infilling oating, shape, roughness, othe
	NMLC coring + HQ casing		5.45	(13)		5.93 6.00		As previous.	3 70mm thick.		нw			5.0 5.0 CU 5.4 5.4 5.4	13, JT, 45°, CLAY, PLN/UN, RI 14-5.17, JT, 80°, CLAY, PLN, I, RF 11, BP, 25°, CLAY, PLN, SO 16, JT/BP, 70°, CLAY, ST, SO 10, BP, sub HZ, FE+CLAY, N/IR, SO
-6		+	0.00			0.00			ole at 6.0 metre	s.					
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GOODITIAN PHOPOHY SERVICES CLIENT PROJECT BUNGARIBEE INDUSTRIAL ESTATE LOCATION HUNTINGWOOD GHD GEOTECHNICS BOREHOLE BH 09 4:43 m TO 6.0 m 21/17871/00 DATE 17/10/08 JOB No 21/17871/00 - GOODMAN PROPERTY SERVICES - BUNGARIBEE INDUSTRIAL ESTATE 17/10/08 START CORING AT 4-43m -5 BOREHOLE (BH9) TERMINATED 6.0m AT



Appendix B

Test Pit Logs

GHD GEOTECHNICS 21/17871/00/AZ035 Rev1.doc 30 October 2009 /

Huntingwood West - Bungaribee Estate Huntingwood Report on Geotechnical Assessment

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		ation:						SHE		1 OF 1
		tion:			258493.01	-		AHL)	Processed: R
					Backh	oe CAT4		-		Checked: RL
Da	ate	:	02/10/0	8	· .		Logged by: CS	1	1 1	Date: 5/12/0
Scale (m)	Water		Samples & Tests	Depth / (RL) metres	Graphic Log	USC Symbol	Material Description SOIL TYPE, colour, structure, minor components (origin), and ROCK TYPE, colour, grain size, structure, weathering, strength	Moisture Condition	Consistency / Density Index	Comments Observations
						SM/ ML	Sandy SILT/Silty SAND, dark brown, fine grained, low plasticity, grass roots throughout (topsoil)	SM	VSt	50-100mm of fill at
-			D	0.20		CI- CL	CLAY, light brown with grey brown mottles, low to medium plasticity, with fine to medium grained sand/sandy, trace coarse grained sand/fine sub-rounded lithic gravel, remnant roots (alluvium).		VSt	surface in areas of te pit
				0.90		- <u>SC</u> / CL	Clayey SAND/Sandy CLAY, brown and red brown mottles, low plasticity, fine grained, lightly cemented,	M	VSt- H	
							remnant rootlets (residual).	•		
				1.90		,	From 1.5 - 1.8m, band of ironstone gravel.			
				2.20			horizontal to sub-horizontal bedding, highly to extremely weathered, very low strength, traces of iron and manganese oxide staining at base of test pit.	-		
							End of test pit at 2.2 metres. Terminated on backhoe refusal. No free groundwater encountered.			· · · ·
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ie	e si	tanda	rd sheet	s for		GHD	GEOTECHNICS	-	Job	No.
			obreviati		GHD	57 Hert	pert Street, Artarmon NSW 2064 Australia 9462 4700 F: 61 2 9462 4710 E: atnmail@ghd.com.au			21-17871-00



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							AHL	, 	Processed: R
		od of Explor		Backh	oe CAT4				Checked: RM
∪a T	te:	01/10/08	0			Logged by: CS	1		Date: 5/12/c
ocale (III)	Water	Samples & Tests	Depth / (RL) metres	Graphic Log	USC Symbol	Material Description SOIL TYPE, colour, structure, minor components (origin), and ROCK TYPE, colour, grain size, structure, weathering, strength	Moisture Condition	Consistency / Density Index	Comments Observations
		D	0.35		SC CI- CH	Clayey SAND, dark brown, fine to medium grained, trace coarse sand and fine sub-rounded gravel (topsoil). CLAY, brown and orange brown mottled, medium to high plasticity, trace medium to coarse grained sand and fine gravel (alluvium/colluvium).	M	F	Only on western side pit approx. 200mm of residual soil. Fill possibly colluvium.
			0.70		СН	CLAY, red brown and grey mottled, high plasticity, trace fine grained sand (residual).	м	St	
		В				From 1.3m, with ironstone bands/lenses.			
-			-			From 1.7m, grades to extremely weathered shale.			
			2.20						
		В	2.30			SILTSTONE/SHALE, grey and grey brown, laminated to very thinly bedded, horizontal bedding, highly weathered with extremely weathered clay bands, very low strength, manganese and iron oxide staining. End of test pit at 2.3 metres. Terminated on backhoe near refusal, slow excavation. No free groundwater encountered.			

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	-		INGWOO	INDUSTR			SHE	ЕТ	1 OF 1
				58433.0 N	N MGA	.94 / 56 Surface RL: 51.8m approx			Processed: R)
M	eth	od of Explor	ation:	Backho	be CAT4				Checked: RM
Da	ate:	07/10/0	8			Logged by: CS			Date: 5/12/0
ocare (III)	Water	Samples & Tests	Depth / (RL) metres	Graphic Log	USC Symbol	Material Description SOIL TYPE, colour, structure, minor components (origin), and ROCK TYPE, colour, grain size, structure, weathering, strength	Moisture Condition	Consistency / Density Index	Comments Observations
		· · · · · ·			SC	Clayey SAND, dark brown, fine grained, grass rootlets (topsoil).	VM		· · · · ·
			0.20		CL	Sandy CLAY, light brown, low plasticity, fine to medium grained sand, trace coarse sand/fine gravel (alluvium).	M	F	
			0.40		CL	Sandy CLAY, grey and brown mottled with bands/lenses of red brown ironstone gravel, low plasticity, fine grained sand, medium to coarse ironstone gravel lenses, roots (residual) (completely to extremely weathered sandstone).	M	VSt	
		В							
						From 1.4m, reducing sand content with depth to trace/ with fine grained sand (extremely weathered shale).			
		В							
-			2.50			End of test pit at 2.5 metres.			
						No free groundwater encountered.			
								ψ ¹	
L		· · · · · · · · · · · · · · · · · · ·							
ė	e st	andard sheets	sfor		GHD	GEOTECHNICS Dert Street, Artarmon NSW 2064 Australia		Job	No.

CUEET



_	ien		SHEET			SERVIC	ES PTY LTD			
		ect:		ARIBEE				HC	DLE	No. TP13
		tion:						SHE	FT	1 OF 1
		tion:		0.0 E 62			94 / 56 Surface RL: 43.3m approx			Processed: RY
		od of l				oe CAT4			<u> </u>	Checked: RML
	ate:		02/10/0		Backin		Logged by: CS			
	110.	•	02/10/0				Logged by. 03			Date: 5/12/08
Scale (m)	Water	Samples	& Tests	Depth / (RL) metres	Graphic Log	USC Symbol	Material Description SOIL TYPE, colour, structure, minor components (origin), and ROCK TYPE, colour, grain size, structure, weathering, strength	Moisture	Consistency / Density Index	Comments Observations
				<i>,</i>		SM	Silty SAND, brown, fine to medium grained (topsoil).	M		
			D	0.20		CL- CI	CLAY, light brown, low to medium plasticity, with fine to medium grained sand, trace coarse grained sand and fine sub-rounded gravel, remnant roots/rootlets (alluvium).	M	F-St	
·1							From 0.7m, reducing sand content, with red brown mottling.	-		
			-	1.10 1.30		CI- CH SC	CLAY, grey and red brown mottled, with fine grained sand, remnant rootlets (residual).	M	St	
			D			30	Clayey SAND, grey and light brown mottling, fine to medium grained cementation increasing with depth (residual).	M	VSt/E	
2	-			1.70			SANDSTONE, grey and brown, fine to medium grained, horizontal to sub-horizontal bedding, highly weathered to extremely weathered, very low strength, manganese oxide staining at base of test pit. End of test pit at 1.8 metres. Terminated on backhoe refusal. No free groundwater encountered.			
3										
	·							-		
det	tails	tandard s of abt is of de	oreviatio	ons 🕻	GHD	57 Hert T: 61 2	GEOTECHNICS pert Street, Artarmon NSW 2064 Australia 2 9462 4700 F: 61 2 9462 4710 E: atnmail@ghd.com.au JLTING GEOTECHNICAL ENGINEERS AND GEOLOGISTS			No. 21-17871-00



	:31	PIT LOG SHEET	Γ						
C	lien	t: GOOD	MAN PR	OPERTY	SERVIC	ES PTY LTD	ЦО		No. TP14
P	roje	ect: BUNG	ARIBEE	INDUSTR	RIAL EST	ATE	по		NO. 1714
L	oca	tion: HUNTI	INGWOO	D			SHEE	ET 🥤	1 OF 1
P	osit	ion: 30237	9.0 E 62	58367.0	N MGA	94 / 56 Surface RL: 47.8m appro	x AHC)	Processed: RY
М	eth	od of Explor	ation:	Backh	oe CAT4	4.28C Hole Size: 1.3m x 4.0m			Checked: R.M.
D	ate:	03/10/0	8			Logged by: CS			Date: 5/12/08
Scale (m)	Water	Samples & Tests	Depth / (RL) metres	Graphic Log	USC Symbol	Material Description SOIL TYPE, colour, structure, minor components (origin), and ROCK TYPE, colour, grain size, structure, weathering, strength	Moisture Condition	Consistency / Density Index	Comments Observations
-			0.20		ML	Sandy SILT, brown, low plasticity, fine grained sand, trace fine gravel (topsoil).	SM		-
-		D	0.20		CI- CH	CLAY, brown, medium to high plasticity, trace coarse lithic sand/fine sub-rounded lithic gravel, remnant roots (colluvium/alluvium). From 0.3m, with red-brown mottling.	M	F	-
-			0.95		СН	CLAY, grey with orange brown and red brown ironstone	M	F-St	-
-		D	1.50			mottles, high plasticity (residual).			
2	· ·					SHALE, grey, orange brown and dark brown bands, very thinly bedded at approx 20°, extremely weathered bands with highly weathered bands increasing in thickness with depth, extremely low strength to low strength, evident manganese and iron oxide staining.			
			0.00						•
-			2.20			End of test pit at 2.2 metres. Terminated on backhoe refusal, slow excavation. No free groundwater encountered.			
- - -3									-
-									
			g 1		СПр	GEOTECHNICS		Job	No
de	tails	andard sheets s of abbreviati is of description	ons 🛛	GHD	57 Herl T: 61 2	GEOTECHNICS bert Street, Artarmon NSW 2064 Australia 2 9462 4700 F: 61 2 9462 4710 E: atnmail@ghd.com.au JLTING GEOTECHNICAL ENGINEERS AND GEOLOGISTS			^{NO.} 1-17871-00

GEO TEST PIT 211787100.GPJ GHD GEO TEMPLATE.GDT 1/12/08



Pos		30251	Depth / (RL) 8 metres	58294.0 N	N MGA De CATA DS CATA SC		Moisture Condition)	1 OF 1 Processed: R Checked: R Date: 5/\2/9 Comments Observations
Met Date	hod of e:	02/10/0	Depth / (RL) 8 metres	Backho	NSC Symbol	Hole Size: 1.5m x 4.5m Logged by: CS Material Description SOIL TYPE, colour, structure, minor components (origin), and ROCK TYPE, colour, grain size, structure,		;	Checked: RM Date: 5/12/1 Comments
Date	e:	02/10/0	Depth / (RL) metres		USC Symbol	Logged by: CS Material Description SOIL TYPE, colour, structure, minor components (origin), and ROCK TYPE, colour, grain size, structure,	oisture ondition	sistency / sity Index	Date: 5/\2/0 Comments
(E)		& Tests	Depth / (RL) metres	Second Se		Material Description SOIL TYPE, colour, structure, minor components (origin), and ROCK TYPE, colour, grain size, structure,	oisture ondition	sistency / sity Index	Comments
Scale (m) Water	water Samulas	· · · · · · · · · · · · · · · · · · ·		••••••••••••••••••••••••••••••••••••••		SOIL TYPE, colour, structure, minor components (origin), and ROCK TYPE, colour, grain size, structure,	oisture ondition	sistency / sity Index	
			0.25		SC		20	Deŭ Deŭ	
					-	Clayey SAND, dark brown, fine to medium grained, trace coarse grained sand / fine gravel (topsoil).	M	-	
					CL	CLAY, light brown, low plasticity, with coarse grained sand and fine sub-rounded gravel (alluvium).	м	St/MD	
		D	0.55		CI- CH	CLAY, light grey and orange brown mottled, medium to high plasticity, with medium to coarse lithic sand and fine sub-rounded to sub-angular lithic gravel (colluvium). From 0.7-0.8m, with medium to coarse sub-angular	м	St	
1			0.00		СН	gravel clasts. CLAY, light grey and red-brown mottled, high plasticity, trace/with fine sand/silt, fragments/clasts of ironstone amongst ironstone bands, remnant rock structure. Ironstone band cementation increasing with depth	M	VSt	
			-			(residual)			
		В							
-									
2									
			2.20			SILTSTONE/SHALE, brown and grey bands, very thinly bedded to thin horizontal bedding, highly weathered with extremely to completely weathered clay bands, very low to extremely low strength, iron and manganese oxide stained bedding partings and joints.			
			2.60			End of test pit at 2.6 metres. No free groundwater encountered.	-		
3		н н			1. J.				
			-		· · ·				
	standard					GEOTECHNICS		Job	



CI D							CES PTY LTD	HC)LE	No. TP16
	-			IGWOC		IAL EST		SHE	ET	1 OF 1
					58211.0 N	J MGA	N94 / 56 Surface RL: 57.1m approx			Processed: R
		od of Ex								Checked: RAJ
	ate:		/10/08		Buokin		Logged by: CS		•	Date: 5/12/0
			, 10,00						·	Date: 3(40
Scale (m)	Water	Samples & Tests		Depth / (RL) metres	Graphic Log	USC Symbol	Material Description SOIL TYPE, colour, structure, minor components (origin), and ROCK TYPE, colour, grain size, structure, weathering, strength	Moisture Condition	Consistency / Density Index	Comments Observations
						SM	Sandy SILT, dark brown, low plasticity, fine to medium grained sand (topsoil).	м		
				0.00						-
			1 a.	0.30		СН	CLAY, brown and orange brown mottled, high plasticity, trace fine to medium grained lithic sand, remnant roots (colluvium/residual).	М	F-St	
			в							
1			,	1.00		CL	CLAY, grey and brown mottled, low plasticity, with fine grained sand/silt, sandy patches/lenses (residual)	М	VSt	
							From 1.4m, with ironstone lenses/bands, becoming lightly to moderately cemented (extremely weathered sandstone).		н	
						-				
2										
				- 		СН	From 2.1m, no fine grained sand, no remnant rock structure, stiff to very stiff, high plasticity clay.		St- VSt	•
						-	From 2.5m, some remnant rock structure.			
			в							
3				3.00				- -		
				<u>3.20</u>			End of test pit at 3.2 metres. No free groundwater encountered.			·
						······································				
		andard s s of abbre			GHD	GHD	GEOTECHNICS bert Street, Artarmon NSW 2064 Australia		Job	No.







HOLE No. TP1 Project: BUNGARIBEE INDUSTRIAL ESTATE Location: HUNTINGWOOD SHEET 1 OF 1 Position: 302441.0 E 6258242.0 N MGA94 / 56 Surface RL: 49.7m approx AHD Processed Method of Exploration: Backhoe CAT428C Hole Size: 1.2m x 3.5m Checked: Date: 03/10/08 Logged by: CS Date: 5/12	Client				SERVIC				· · · · · · · · · · · · · · · · · · ·
Location: HUNTINGWOOD SHET 1 OF 1 Position: 302441.01 625242.01 MGA94/65 Surface RL: 49.7m approx AHD Processee Method of Exploration: Backhoe CAT428C Hole Size: 12m x3.6m Checked: Date: 09/10/08 Image: Size in 2m x3.6m Checked: Date:: Size in 2m x3.6m (i) graph graph graph graph graph Graph Date:: Size in 2m x3.6m (ii) graph graph graph graph graph Graph Date:: Size in 2m x3.6m (ii) graph graph graph graph graph Graph Date:: Size in 2m x3.6m (ii) graph graph graph graph graph Graph Date:: Size in 2m x3.6m (ii) graph graph graph graph graph Graph Comment (ii) graph graph graph graph Graph Graph Comment (iii) graph graph graph Graph Graph Graph Graph (iii) graph graph Graph Graph Graph Graph Fraph (iii) graph graph Graph </th <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>НС</th> <th>DLE</th> <th>No. TP18</th>							НС	DLE	No. TP18
Position: 302441.0 E 6238242.0 M MGA94 / 50 Surface RL: 49.7m approx AHD Processed Method of Exploration: Backhoe CAT428C Hole Size: 1.2m x 3.5m Checked: Date: 091008 Logged by: CS Date:: 5.0m (i) ging ging ging ging ging ging ging gi	-						SHF	ET	1 OF 1
Method of Exploration: Backhoe CAT428C Hole Size: 1.2m x3.5m Checked: Date: 03/10/08 Logged by: CS Date:: 5/12 Image: 03/10/08 Image: Image					N MGA	94 / 56 Surface RI : 49 7m appro			-
Date: 03/10/08 Logged by: CS Date: St (a) (a) (b) (c)							~ ~ ~ ~		
Image: State in the second st				Buon			· · · ·		
Image: State of the second state of									Date. SILO
a medium grained sand, with fine to medium sub-rounded gravel (topsoil). CI CLAY, red-brown with brown mottling, medium to high plasticity, with fine grained sand, trace fine to coarse sub-rounded to angular gravel, few coarse gravel, rootels and remnant rootlets (colluvium/residual) B 0.70 CL Sandy CLAY, brown and light brown mottled, low plasticity, fine to medium grained sand, numerous premnant roots (residual). SANDSTORE, Forown with red-brown bands, thinly bedded at approx 30°, highly fractured, highly weathered, low strength. 1 SHALE, grey with red brown bands, thinly bedded at approx 30°, highly meathered with extremely to completely weathered clay bands, very low to extremely low strength. 2 210	Scale (m) Water	Samples & Tests	Depth / (RL) metres	Graphic Log	USC Symbol	SOIL TYPE, colour, structure, minor components (origin), and ROCK TYPE, colour, grain size, structure,	Moisture Condition	Consistency / Density Index	Comments Observations
2 Ch CLAY, red-brown with brown mottling, medium to high plasticity, with fine grained sand, race fine to coarse sub-rounded to angular gravel, few coarse gravel, rootlets and remnant rootlets (colluvium/residual) M F-St 0.70 CL Sandy CLAY, brown and light brown mottled, low plasticity, fine to medium grained sand, numerous remnant roots (residual). M St 1 CL Sandy CLAY, brown and light brown mottled, low plasticity, fine to medium grained sand, numerous remnant roots (residual). M St 2 ShADSTONE, brown with red-brown bands, thinly bedded at approx 30°, highly fractured, highly weathered, low strength. SHALE, grey with red brown bands, thinly bedded at 30°, highly weathered with extremely to completely weathered clay bands, very low to extremely low strength. 2 2.10 End of test pit at 2.1 metres. No free groundwater encountered. N		• • ·	0.20		CL	medium grained sand, with fine to medium sub-rounded	м	F	
1 CL Sandy CLAY, brown and light brown mottled, low plasticity, fine to medium grained sand, numerous remnant roots (residual). M St 1 SANDSTONE, brown with red-brown bands, thinly bedded at approx 30°, highly fractured, highly weathered, low strength. M St 1.40 SHALE, grey with red brown bands, thinly bedded at 30°, highly weathered with extremely to completely weathered tay bands, very low to extremely low strength. Image: strength in the image: str			0.20		CI- CH	plasticity, with fine grained sand, trace fine to coarse sub-rounded to angular gravel, few coarse gravel,	M	F-St	
1 Important roots (residual). SANDSTONE, brown with red-brown bands, thinly bedded at approx 30°, highly fractured, highly weathered, low strength. 1.40 SHALE, grey with red brown bands, thinly bedded at 30°, highly weathered with extremely to completely weathered day bands, very low to extremely low strength. 2 2 2		В]	7777	CL	Sandy CLAY, brown and light brown mottled, low	M	St	
1 SANDSTONE, brown with red-brown bands, thinly bedded at approx 30°, highly fractured, highly weathered, low strength. 1.40 SHALE, grey with red brown bands, thinly bedded at 30°, highly weathered with extremely to completely weathered clay bands, very low to extremely low strength. 2 2.10 End of test pit at 2.1 metres. No free groundwater encountered.			0.80	<u> </u>		, plasticity, fine to medium grained sand, numerous	/—		
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1					SANDSTONE, brown with red-brown bands, thinly bedded at approx 30°, highly fractured, highly			
SHALE, grey with red brown bands, thinly bedded at 30°, highly weathered with extremely to completely weathered clay bands, very low to extremely low strength. 2.10 End of test pit at 2.1 metres. No free groundwater encountered.									
2.10 End of test pit at 2.1 metres. No free groundwater encountered.			1.40			30°, highly weathered with extremely to completely weathered clay bands, very low to extremely low		•	
No free groundwater encountered.	2		2.10						
						End of test pit at 2.1 metres.			
					· .				
					. *				
					на. 1 1				
		а 1					-	-	
See standard sheets for GHD GEOTECHNICS Job No.	ion of	andard shact	e for		GHD	GEOTECHNICS		Joh	No.
57 Herbert Street, Artarmon NSW 2064 Australia			ions	GHD	57 Her	bert Street, Artarmon NSW 2064 Australia			21-17871-00



	lier	PIT LOG SHEET nt: GOOD		OPERTY	SERVIC	ES PTY LTD			
P	roje	ect: BUNG	ARIBEE	INDUSTR	RIAL EST	TATE	HC)LE	No. TP19
Lo	oca	tion: HUNT	INGWOO	, do			SHE	ET	1 OF 1
Pe	osi	tion: 30263	4.0 E 62	58127.0	N MGA	.94 / 56 Surface RL: 55.0m approx		2	Processed: RY
		od of Explor		Backh	oe CAT4				Checked: RML
Da	ate	: 03/10/0	8	1		Logged by: CS			Date: 5/\2/03
Scale (m)	Water	Samples & Tests	Depth / (RL) metres	Graphic Log	USC Symbol	Material Description SOIL TYPE, colour, structure, minor components (origin), and ROCK TYPE, colour, grain size, structure, weathering, strength	Moisture Condition	Consistency / Density Index	Comments Observations
•			0.15		SM	Silty SAND, brown, fine to coarse grained, with fine to coarse round to angular gravel (topsoil/fill).	м		
	-		0.40		CH	CLAY, red brown, high plasticity, trace/with coarse sand and fine sub-rounded to angular gravel (colluvium).	М	St	
					CI- CH	CLAY, grey with red brown and brown mottling, medium to high plasticity, trace/with fine grained sand/silt, trace ironstone gravel (residual).	M	VSt	
						From 0.7m, ironstone lenses/bands, moderately cemented, grading to extremely weathered shale.			
1	;								
			1.40					, , ,	
						SILTSTONE/SHALE, grey, brown and red-brown bands, very thinly bedded to laminated at 0-10°, alternating highly weathered and extremely to completely weathered bands, extremely low to very low strength.		~	
		В	2.00						
2						End of test pit at 2.0 metres. Terminated on backhoe refusal. No free groundwater encountered.			
					· .				
3									
				· ·					
de	tails	tandard sheets s of abbreviati is of description	ions 🕻	GHD	57 Herl T: 61 2	GEOTECHNICS bert Street, Artarmon NSW 2064 Australia 2 9462 4700 F: 61 2 9462 4710 E: atnmail@ghd.com.au ULTING GEOTECHNICAL ENGINEERS AND GEOLOGISTS	-		No. 21-17871-00



	ien	,				XES PTY LTD	НС	LE	No. TP20
	•				RIAL EST	AIE	SHE		
		<u></u>		58034.0 I		.94 / 56 Surface RL: 43.6m approx	-		
		od of Explor							Processed: R
	ate:			Dackii	UE CATA	Logged by: CS			Date: 5/12/0
	ile.	02/10/0				Logged by. 03			Date. 5/12/0
scale (m)	Water	Samples & Tests	Depth / (RL) metres	Graphic Log	USC Symbol	Material Description SOIL TYPE, colour, structure, minor components (origin), and ROCK TYPE, colour, grain size, structure, weathering, strength	Moisture Condition	Consistency / Density Index	Comments Observations
			0.15		SM	Silty SAND, dark brown, fine to medium grained (topsoil).	м		
			0.15		CI- CH	CLAY, light brown, medium to high plasticity, with fine grained sand (alluvium).	М	F	
		в							
			· · · .			From 0.5m, trace to no sand, with grey mottles.			
		D	0.80		- .	CLAY, light brown with grey mottles, high plasticity	M	St-	
						(residual).		VSt	
					.	From 1.2-1.3m, ironstone gravel band.			
			1.50		SC	From 1.4-1.5m, ironstone gravel band. Clayey SAND, grey and light brown mottled, fine to	M		· .
	-	D	÷ .			medium grained sand, lightly cemented, trace ironstone gravel (residual).			
		- 	2.10			End of test pit at 2.1 metres.	-		
						No free groundwater encountered.			
		*							
			-						
		andard chact	e for		GHD	GEOTECHNICS		Job	No
		andard sheet of abbreviati		GHD	57 Her	bert Street, Artarmon NSW 2064 Australia 2 9462 4700 F: 61 2 9462 4710 E: atnmail@ghd.com.au			NO. 21-17871-00

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	ier					CES PTY LTD	HO	LFI	No. TP22	
	Project: BUNGARIBEE INDUSTRIAL ESTATE									
			TINGWO				SHEE	T 1		
			246.0 E 62	· · ·					Processed: R	
		od of Explo		Backh	be CAT4				Checked: RM	
Da	ate	: 02/10	/08		r	Logged by: CS		1.	Date: S/\2/	
ocare (III)	Water	Samples & Tests	Depth / (RL) metres	Graphic Log	USC Symbol	Material Description SOIL TYPE, colour, structure, minor components (origin), and ROCK TYPE, colour, grain size, structure, weathering, strength	Moisture Condition	Density Index	Comments Observations	
_			0.2		SM	Silty SAND, brown, fine to medium grained, with fine to medium gravel (topsoil).	M			
		. D	0.40		GC	Sandy Gravel, light brown, fine to coarse grained sand, fine to medium, rounded to sub-rounded gravel	M			
					CI- CH	 (alluvium/fill). CLAY, red-brown and brown mottled, medium to high plasticity, with/trace coarse grained sand and fine to coarse sub-rounded to sub-angular lithic gravel (colluvium) 	MF	-St		
		D			СН	From 0.9m, reducing sand and gravel content with depth. Trace coarse grained sand / fine gravel.				
2			1.40		- <u>CH</u> -	CLAY, light grey with orange brown and red brown mottles, high plasticity, with bands/lenses of gravel		St- VSt		
	-	D				(fragmented iron rich rock) (residual). From 1.7m, grading to extremely weathered shale/siltstone with iron cemented lenses.				
			2.00		i.		*		• •	
	-		2.00			End of test pit at 2.0 metres. No free groundwater encountered.				
									· · · · · · · · · · · · · · · · · · ·	
et	tails	tandard shee s of abbrevia is of descrip	tions	GHD	57 Herl T: 61 2	GEOTECHNICS bert Street, Artarmon NSW 2064 Australia 2 9462 4700 F: 61 2 9462 4710 E: atnmail@ghd.com.au ULTING GEOTECHNICAL ENGINEERS AND GEOLOGISTS		Job N 2	₁o. 1-17871-00	



	lient roje		MAN PF	HOLE No. TP23					
	-		NGWOO				SHE	ET	1 OF 1
			2.0 E 62	58542.0	N MGA	N94 / 56 Surface RL: 47.1m approx	< AHI		Processed: R
M	etho	od of Explor	ation:	Backh	be CAT4		~		Checked: PM
	ate:	01/10/0				Logged by: CS			Date: 5/12/
Scale (m)	Water	Samples & Tests	Depth / (RL) metres	Graphic Log	USC Symbol	Material Description SOIL TYPE, colour, structure, minor components (origin), and ROCK TYPE, colour, grain size, structure, weathering, strength	Moisture Condition	Consistency / Density Index	Comments Observations
•		·			SC	Clayey SAND, dark brown, fine to coarse grained, trace fine round to sub-rounded gravel. Fragments of building rubble at surface (topsoil).	м		
			0.20		СН	CLAY, orange brown, high plasticity, trace coarse grained sand and fine sub-rounded to sub-angular gravel (colluvium).	M	VSt	
		В	0.50						
	-		5.00		СН	CLAY, light grey with orange brown/red brown mottles reducing with depth, high plasticity, trace fine to medium grained sand and fine to medium sub-angular ironstone gravel (residual).	. M	St	
1									
								∨St	
2					·	From 2.0m, with ironstone lenses, extremely to completely weathered rock.		н	
		В	0.00						
			2.60			SHALE, dark grey brown, horizontally bedded, highly weathered, low to very low strength, some manganese oxide staining.			
3			3.00			End of test pit at 3.0 metres.			
			-			Terminated on backhoe near refusal, slow excavation. No free groundwater encountered.			
- 									
Se	e sta	andard sheet	sfor		GHD	GEOTECHNICS		Joh	No.
		of abbreviati		GHD	57 Her	bert Street, Artammon NSW 2064 Australia 2 9462 4700 F: 61 2 9462 4710 E: atnmail@ghd.com.au			21-17871-00



CI	ien	t:	GOOD	MAN PF	ROPERTY	SERVIC	ES PTY LTD	нс		No. TP24
Pr	oje	ct:	BUNG	ARIBEE	INDUST	RIAL EST	ATE	ITC.		NU. 1724
Lc	ocat	tion:	HUNT	INGWOO	DD			SHE	ET	1 OF 1
Pc	osit	ion:	30260	6.0 E 62	258493.0	N MGA	94 / 56 Surface RL: 52.2m appro>	à he)	Processed: R
Me	etho	od of E	Explor	ration:	Backh	oe CAT4	Hole Size: 1.2m x 4.2m			Checked: RM
Da	ate:		03/10/0	8			Logged by: CS			Date: 5/12/
Scale (m)	Water	Samples	& Tests	Depth / (RL) metres	Graphic Log	USC Symbol	Material Description SOIL TYPE, colour, structure, minor components (origin), and ROCK TYPE, colour, grain size, structure, weathering, strength	Moisture Condition	Consistency / Density Index	Comments Observations
			<u></u>	0.20		SM	Silty SAND, dark brown, fine to medium grained, with fine sub-rounded gravel, numerous grass rootlets (topsoil). CLAY, brown, high plasticity, with fine to medium	M	F-St	
							sub-rounded lithic gravel/gravelly (alluvium/colluvium). From 0.5m, red brown and grey mottled, trace gravel.			
			В	0.80		СН	CLAY, light grey with red brown and orange brown mottles, high plasticity, with medium to coarse angular	M	VSt	
			D				ironstone gravel (residual).			
				1.30	× / / / / /		SANDSTONE, light grey with red brown bands and lenses, fine grained, horizontal bedding, highly weathered with extremely to completely weathered bands, very low to extremely low strength.			
		ta a						· ·		
		· ·		2.20			End of test pit at 2.2 metres.			
						- -	No free groundwater encountered.			
				· ·						
				· · · · ·				-		
							GEOTECHNICS	Job No.		
et	57 Herbert S						pert Street, Artarmon NSW 2064 Australia 2 9462 4700 F: 61 2 9462 4710 E: atnmail@ghd.com.au			1-17871-00






	lien					CES PTY LTD	HC)LE	No. TP26
	•	- 1					SHE	ЕТ	1 OF 1
			· · ·	58482.0	N MGA	.94 / 56 Surface RL: 54.3m approx			Processed: R
		od of Explor	ation:	Backh	oe CAT4				Checked: pr
	ate					Logged by: CS			Date: 5/12/0
				÷					· · · · · · · · · · · · · · · · · · ·
ocare (III)	Water	Samples & Tests	Depth / (RL) metres	Graphic Log	USC Symbol	Material Description SOIL TYPE, colour, structure, minor components (origin), and ROCK TYPE, colour, grain size, structure, weathering, strength	Moisture Condition	Consistency / Density Index	Comments Observations
			0.15		CL	Sandy CLAY, dark brown, low plasticity, fine grained sand, grass roots (topsoil).	м	S-F	
		x	0.10		CL	CLAY, brown, low plasticity, trace fine grained sand and fine to medium sub-rounded gravel (alluvium).	м	F	
		-	0.35		СН	CLAY, red brown and grey mottled, high plasticity,	M	St	
		В				gravelly ironstone bands, up to 30mm sub-rounded gravel fragments (residual).			
						From 0.9m, arey with rod brown mettles		Ve	
		D				From 0.9m, grey with red brown mottles.		VSt	
	-								
	-								
			· ·		•				
		В							
		D			-	From 2.6m, some remnant rock structure, ie; extremely weathered shale, some highly weathered lenses/bands.			· · · · ·
ļ			3.20						
						End of test pit at 3.2 metres. No free groundwater encountered.			
	0.04	andard sheet	e for	· · · · ·	GHD	GEOTECHNICS	. 	Joh	No.
		andard sneet s of abbreviati		GHD	57 Her	bert Street, Artarmon NSW 2064 Australia 2 9462 4700 F: 61 2 9462 4710 E: atnmail@ghd.com.au			21-17871-00



	oie	· · · · · · · · · · · · · · · · · · ·		INDUSTR	SERVIC		HO	LE	No. TP27
	- T.		NGWOO				SHEE	ET	1 OF 1
Po	osit	tion: 302328	3.0 E 62	58629.0 1	MGA	94 / 56 Surface RL: 42.7m approx)	Processed: R
M	eth	od of Explor	ation:	Backh	be CAT4				Checked:RAU
Da	ate:	02/10/0	8			Logged by: CS	e.		Date: 5/12/06
	Water	Samples & Tests	Depth / (RL) metres	Graphic Log	USC Symbol	Material Description SOIL TYPE, colour, structure, minor components (origin), and ROCK TYPE, colour, grain size, structure, weathering, strength	Moisture Condition	Consistency / Density Index	Comments Observations
					ML	Sandy SILT, brown, low plasticity, fine to medium grained sand, numerous grass rootlets (topsoil).	M		
		D	0.20		GP	Sandy GRAVEL, brown, fine to medium, sub-rounded to rounded gravel, fine to coarse grained sand, trace/with silt (alluvium/fill).	М		Variable depth of Sandy Gravel across test pit
		D	0.45		CI- CH	CLAY, red brown and brown mottled, medium to high plasticity, trace fine to coarse, sub-angular to sub-rounded gravel, few coarse gravel, remnant roots/rootlets (colluvium).	М	St	
			0.90		СН	CLAY, grey with brown mottling, bands of red brown	м	St	
						ironstone, high plasticity, brown sandy bands (residual).			
		D	-						
			1.80			Interbedded SILTSTONE/SANDSTONE, grey with brown lenses, fine grained, laminated to very thinly bedded, extremely weathered, very low strength to extremely low strength.			
			2.25	· · · ·		End of test pit at 2.25 metres.			
					ч	No free groundwater encountered.			· · ·
									• • •
	e ef	andard sheets	for		GHD	GEOTECHNICS		Joh) No.
		s of abbreviation		GHD	57 Hert	pert Street, Artarmon NSW 2064 Australia 9462 4700 F: 61 2 9462 4710 E: atnmail@ghd.com.au			



	lient roje			INDUSTR		EES PTY LTD TATE	HC	C	No. TP28	
La	ocat	ion: HUNTI	NGWOO	DD			SHE	ET	1 OF 1	
Po	ositi	on: 30240	1.0 E 62	58629.0 1	N MGA	.94 / 56 Surface RL: 44.2m approx		C	Processed: R	
M	ethc	od of Explor	ation:	Backh	oe CAT4	Hole Size: 1.4m x 4.0m			Checked: RA	
Da	ate:	30/09/0	8			Logged by: CS			Date: 5/12/0	
ocale (m)	Water	Samples & Tests	Depth / (RL) metres	Graphic Log	USC Symbol	Material Description SOIL TYPE, colour, structure, minor components (origin), and ROCK TYPE, colour, grain size, structure, weathering, strength	Moisture Condition	Consistency / Density Index	Comments Observations	
			0.40		SC/ CL	Sandy CLAY/Clayey SAND, dark brown, low plasticity, fine to coarse grained (topsoil).	M			
		D/B			CH	Sandy CLAY, brown, low plasticity, fine to medium grained sand, trace fine sub-rounded gravel, remnant roots and fine rootlets (alluvium/residual). From 0.8m, brown with grey mottles, completely weathered shale with ironstone bands/lenses.	M	St		
		D				From 1.1-1.3m, band of ironstone gravel. From 1.5-1.8m, band/lense of ironstone.	VM-			
		D	2.10				W	· .		
						End of test pit at 2.1 metres. No free groundwater encountered.		۰. د		
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e	tails	andard sheets of abbreviations of descriptions	ons 🕻	GHD	57 Herl T: 61 2	GEOTECHNICS bert Street, Artarmon NSW 2064 Australia 2 9462 4700 F: 61 2 9462 4710 E: atnmail@ghd.com.au JLTING GEOTECHNICAL ENGINEERS AND GEOLOGISTS	-		o No. 21-17871-00	

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	lier						ES PTY LTD	НС	DLE	No. TI	>29	
	-	ect:			INDUSTF	RIAL EST	ATE					
		ation: tion:			58636.0 I		.94 / 56 Surface RL: 49.3m approx			1 OF Proces	sod: P	
			Explor						, 	Checke		
	ate		07/10/08		Dackii		Logged by: CS					
Da	ale	-	0//10/0	,			Logged by. CS	1		Date:	6/12/C	
Scale (m)	Water	Samoles	& Tests	Depth / (RL) metres	Graphic Log	USC Symbol	Material Description SOIL TYPE, colour, structure, minor components (origin), and ROCK TYPE, colour, grain size, structure, weathering, strength	Moisture Condition	Consistency / Density Index	Comr Observ		
						CL	CLAY, brown, low plasticity, with fine to medium, sub-rounded to sub-angular gravel (topsoil).	м		-		
			D	0.25		CI- CH	CLAY, light grey brown with lenses of dark brown 'topsoil' material and roots, medium to high plasticity, roots up to 20mm (residual/alluvium).	M	F-St	<i></i>		
		-		0.60		СН	CLAY, grey with red brown and orange-brown mottles, high plasticity (residual).	м	St	,		
			D	0.95		<u></u>	SILTSTONE/SANDSTONE, brown and red-brown, fine				•	
		-					grained, thinly bedded, ironstone bands, highly weathered, very low strength.					
			D	1.40			SHALE, light grey with red brown mottles/lenses, generally horizontally bedded, extremely weathered with highly weathered siltstone bands, extremely low strength.					
				2.00								
				<i>2.2</i> 3			End of test pit at 2.25 metres. Terminated on backhoe refusal on siltstone. No free groundwater encountered.				<u></u> .	
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			-									
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ie	e si	tandarc	l sheets			GHD	GEOTECHNICS		Job	No.		
e	tails	s of abl	oreviatio	ons 🛛	GHD	57 Herl	oert Street, Artarmon NSW 2064 Australia 2 9462 4700 F: 61 2 9462 4710 E: atnmail@ghd.com.au	21-17871-00				



	lien oje			INDUST		ES PTY LTD	HO)LE	No. TP32		
	-						SHEE	ΞT	1 OF 1		
				58743.0	N MGA	94 / 56 Surface RL: 40.8m appro.			Processed: RY		
_		od of Explor	ation:	Backh	oe CAT4	· · · · · · · · · · · · · · · · · · ·		•	Checked: PM		
	ate:					Logged by: CS			Date: 5/12/0		
			Ĺ)	бo		Material Description		cy / dex	Comments		
Scale (m)	Water	Samples & Tests	Depth / (RL) metres	Graphic Log	USC Symbol	SOIL TYPE, colour, structure, minor components (origin), and ROCK TYPE, colour, grain size, structure, weathering, strength	Moisture Condition	Consistene Density Inc	Observations		
		ť			CL	Sandy CLAY, dark brown, low plasticity, fine grained sand, grass rootlets (topsoil).	M	F			
			0.20		CI- CH	CLAY, brown with grey mottling, medium to high plasticity, with fine to medium grained sand, some lithic, remnant roots, lithic sand reducing with depth (alluvium).	М	F			
		В									
1			0.95		CI- CH	CLAY, brown and grey mottled, medium to high plasticity, with fine grained sand, fine rootlets. Some sandy bands/lenses, lightly cemented in regions, sand	М	St			
			1.40			generally increasing with depth (residual).					
		D			- <u>S</u> C/ CL	Sandy CLAY/Clayey SAND, brown and grey mottled, fine grained sand, low plasticity (residual).	М	St/MD			
					· · ·				· ·		
2	•		2.10			End of test pit at 2.1 metres.			Seepage at back of p		
3			-								
			, ,		-						
		andard sheet s of abbreviati	s for	GHD	57 Her	GEOTECHNICS bert Street, Artarmon NSW 2064 Australia 2 9462 4700 F: 61 2 9462 4710 E: atnmail@ghd.com.au			No. 21-17871-00		



	-				RIAL EST	ATE	•			No. TP33
			INGWOO					SHEE	T 1	
				58735.0				AHD		Processed: R
-		od of Explor		Backh	oe CAT4		.2m x 4.3m			Checked: RA
Da	ate:	30/09/0	8			Logged by: C	S	, <u>,</u>		Date: 5/12/0
ocale (III)	Water	Samples & Tests	Depth / (RL) metres	Graphic Log	USC Symbol	Material Description SOIL TYPE, colour, structure, minor component and ROCK TYPE, colour, grain size, structure weathering, strength	s (origin), e,	Moisture Condition	Consistency / Density Index	Comments Observations
			0.45		SC	Clayey SAND, brown, fine to medium grained, sub-rounded gravel, grass rootlets (topsoil).	, trace fine	м		······································
		D	0.15		CL- CI	CLAY, red brown and orange brown/brown, lo medium plasticity, trace fine to medium graine and fine sub-rounded to sub-angular gravel (c possible alluvium). At 0.5m, 100mm band of clayey GRAVEL, fine coarse rock fragments (siltstone), angular to sub-angular.	d sand olluvium	м	St	
			0.60		SC	Clayey SAND, grey and light brown bands, low plasticity, fine to medium grained (extremely w sandstone) (residual).		м	/St/D	
						From 0.8m, with red brown ironstone bands.				
-			1.00		CI- CH	CLAY, light grey with orange-brown and red bi mottles, medium to high plasticity, occasional roots, trace fine rootlets (residual).		м	VSt	
		D								
			-			From 1.6m, becoming grey, with ironstone bands/lenses, grading to extremely weathered	l shale		н 	
					н н н	extremely low strength.	i onaio,			
			2.10							
						End of test pit at 2.1 metres. No free groundwater encountered.				•
			· · · · · · · · · · · · · · · · · · ·							
	-				- 					
			с. Ст. 4							
							· · · · · · · · · · · · · · · · · · ·			· · · · · · · · · · · · · · · · · · ·
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	lien					ES PTY LTD	НС	DLE	No. TP35
	· -		ARIBEE NGWOO		RIALES	AIE	SHE	FT	1 OF 1
				258867.0 1	N MGA	94 / 56 Surface RL: 44.6m appro			Processed: H
		od of Explor			oe CAT4		~ /		Checked: PA
	ate					Logged by: CS			Date: 5/2/0
									Duto: 3/12/6
oraic (III)	Water	Samples & Tests	Depth / (RL) metres	Graphic Log	USC Symbol	Material Description SOIL TYPE, colour, structure, minor components (origin), and ROCK TYPE, colour, grain size, structure, weathering, strength	Moisture Condition	Consistency / Density Index	Comments Observations
			0.30		SC	Clayey SAND, fine to medium grained, abundant grass roots (topsoil).	M		
		D	0.45		CL/ SC	Sandy CLAY/Clayey SAND, brown and light brown mottled, fine grained sand, low plasticity, trace/with fine to medium sub-rounded to rounded gravel, numerous	M	VSt	
		D/B			CL- CI	\rootlets (alluvium). CLAY, red brown and brown mottled, low to medium	м	VSt	
						plasticity, with fine to medium grained sand, trace fine to coarse sub-rounded to sub-angular gravel, remnant root/rootlets, numerous fine rootlets (alluvium/colluvium).			
	•		0.90		СН	CLAY, grey with orange brown mottled, high plasticity, numerous fine rootlets (residual possible alluvium).	M	St	
						From 1.4m, lightly cemented ironstone bands/lenses, becoming extremely weathered rock.			
			1.80			SILTSTONE/SHALE, grey with red brown and brown			
			2.00			bands, horizontally bedded, extremely weathered with highly weathered, very low strength, iron and manganese oxide stained joints/bedding partings.			
						End of test pit at 2.0 metres. Terminated on backhoe near refusal, slow excavation. No free groundwater encountered.			
				-					
				;					
e	e st	tandard sheet		GHD	GHD	GEOTECHNICS Dert Street, Artarmon NSW 2064 Australia		Job	No.









Lc	ocatio	on: HUNT	INGWOO	DD					SHE	ЕТ	1 OF	1
Po	ositio	n: 30275	2.0 E 62	57981.0	N MGA	94 / 56	Surface RL:	57.8m approx)	Proces	ssed: HV
M	ethoo	of Explor	ation:	Backh	oe CAT4	28C	Hole Size:	2.0m x 4.3m			Check	ed: RU
Da	ate:	03/10/0	8			· · · · · · · · · · · · · · · · · · ·	Logged by:	CS			Date:	5/12/0
Scale (m)	Water	Samples & Tests	Depth / (RL) metres	Graphic Log	USC Symbol	SOIL TYPE, colour, structu ROCK TYPE, colou	and		Moisture Condition	Consistency / Density Index		ments vations
		· · · · · · · · · · · · · · · · · · ·	0.40		СН	Sandy SILT, dark brown, lo grained sand, with fine sub CLAY, red brown, high plas sand and fine sub-rounded	-rounded gravel	(topsoil).	M	S-F	. [.]	
1		В				From 0.7m, with grey mottl particles, remnant roots.				F		
	-	В	1.30		- <u>-</u> ci -	Sandy CLAY, brown and g plasticity, fine to medium g ironstone bands / lenses in cemented (residual).	rained sand, gra	velly	M	VSt		
2												-
3						From 2.5m, numerous clos ironstone gravel bands 20- spacing.	ely spaced irons 50mm thick at 2	stone bands / 0-50mm				
· ·			3.10			End of test pit at 3.1 metre Terminated on backhoe ne No free groundwater encou	ar refusal, slow	excavation.				······
Ĺ		ndard sheet	L	<u> </u>		GEOTECHNICS				Job	NI	





Appendix C

DCP Test Results

GHD GEOTECHNICS 21/17871/00/AZ035 Rev1.doc 30 October 2009 /

Huntingwood West - Bungaribee Estate Huntingwood Report on Geotechnical Assessment



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File:G:\Geo_Lab\DCP Results\2117871\DCP32.xls



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File:G:\Geo_Lab\DCP Results\2117871\DCP36.xls
Appendix D

Laboratory Test Certificates

GHD GEOTECHNICS 21/17871/00/AZ035 Rev1.doc 30 October 2009 /

Huntingwood West - Bungaribee Estate Huntingwood Report on Geotechnical Assessment

	NTS PEOPI			CE	email: artarmon(ory 2064 7 St Leonards 1590 @ghd.com.au com.au/ghdgeotechnics 860	
Material Test	Report						o: SYD081553 Issue No:
Client: Goodman F	Property Services				NATA Accredited Laboratory Number 679	Date of Issue: 19/11/2008	ordance with NATA's credited for compliance 79 poke (Sydney
Meterial Details					THIS DOCUMENT	SHALL NOT BE REPRODUCEI	D EXCEPT IN FULL.
Material DetailsSource:N/ADescription:N/ASpecification:N/A			Locatio	d From: n: Method:	N/A N/A		
Sample Details							Limits
Sample ID: Field Sample ID: Date Sampled: Progressive Quantity (t):		SYD08-2923 BH01, 0.5m 15/10/2008	SYD08-2924 BH06, 0.5m 15/10/2008	SYD08-2925 BH07, 0.5m 15/10/2008	SYD08-2926 BH09, 1.5m 15/10/2008		
Particle Size Distrib	ution						
Method:	Sieve Size			% P	assing		Limits
Description: Drying by: N/A Washed: Sample Washed							
Other Test Results							
Description Emerson Class Number Soil Description Type of Water Temperature of Water (°C)	Method AS 1289.3.8.1	2(s) clay distilled 21	4 clay distilled 21	Res 1 clay distilled 21	distilled		Limits
Comments							

GHI		nts peopl D GEOT			CE	GHD GEOTEC Sydney Labora 57 Herbert St Artarmon NSW Locked Bag 27 email: artarmo web: www.ghd Tel: (02) 9462 Fax:(02) 9462	atory / 2064 /27 St Leonar n@ghd.com.a .com.au/ghdg 4860	au	
Materia	I Test I	Report						Report No:	SYD081539 Issue No:
								places all previous is nt is issued in accord	
Client:		roperty Services idustrial Estate d NSW				NATA	accreditation with ISO IEC Laboratory Ac	requirements. Accrea	dited for compliance
Project:	2117871/00					NATA Accredite Laboratory Numb 679	er:	lanager)	s (Syuney
								2: 18/11/2008 E REPRODUCED E	XCEPT IN FULL.
Material De	etails								
Source:	N/A			Sample	d From:	N/A			
Description:	N/A			Locatio	on:	N/A			
Specification:	N/A			Sample	Method:				
Sample De	atails								Limits
Sample ID: Field Sample I Date Sampled Progressive Q	:		SYD08-2753 TP11, 0.4-0.6m 13/10/2008	SYD08-2754 TP11, 1.1-1.3m 13/10/2008	SYD08-2755 TP12, 0.8-0.9m 13/10/2008	SYD08-2756 TP12, 1.9-2.0m 13/10/2008	SYD08-2757 TP13, 0.4-0.5m 13/10/2008	SYD08-2758 TP13, 1.5-1.7m 13/10/2008	
Particle Siz	ze Distribu	ution							
Method:		Sieve Size			% P	assing			Limits
Description:									
Drying by: N/A Washed: Sample Washed									
N/A Washed: Sample Washed Other Test									
N/A Washed: Sample Washed Other Test Description Sample History Preparation Linear Shrinkage Mould Lengt Crumbling Curling Liquid Limit (%) Method Plastic Limit (%)	e (%) th (mm)	Method AS 1289.3.1.1, AS 1289.3.2.1 AS 1289.3	Dry Sieved 16.5 125 No Yes 67 Four Point 22		Res	Air-dried Dry Sieved 16.0 125 No Yes 53 Four Point 16			Limits
N/A Washed: Sample Washed Other Test Description Sample History Preparation Linear Shrinkage Mould Lengt Crumbling Curling Liquid Limit (%) Method	Results e (%) th (mm)	AS 1289.3.1.1, AS	^{3.3 1} Dry Sieved 16.5 125 No Yes 67 Four Point		. Res	Air-dried Dry Sieved 16.0 125 No Yes 53 Four Point 16 37	22.5	13.4	Limits



N/A

GHD	CLIENTS PEC				GHD GEOTE Sydney Labor 57 Herbert St Artarmon NSV Locked Bag 2 email: artarmo web: www.gho Tel: (02) 9462 Fax:(02) 9462	ratory N 2064 727 St Leonal on@ghd.com.a d.com.au/ghdg 2 4860	au	
Material T	est Repor	t				This issue re	Report No:	SYD081540 Issue No
Bun	dman Property Servi garibe Industrial Esta tingwood NSW	ces ite			NATA Accredite	This docume accreditation with ISO IEC Laboratory A Approved Si Laboratory A	nt is issued in accord requirements. Accre 17025 ccreditation No. 679 gnatory: D.P Brook	dance with NATA's dited for complianc
Project: 2117	871/00				Laboratory Numl 679 THIS DOCUME	Date of Issue	e: 18/11/2008 SE REPRODUCED E	XCEPT IN FULL.
Material Detail	S							
Source:	N/A		Sample	d From:	N/A			
Description:	N/A		Locatio	on:	N/A			
Specification:	N/A		Sample	Method:				
Sample Details	5							Limits
Sample ID: Field Sample ID: Date Sampled: Progressive Quanti	ty (t):	SYD08-2759 TP14, 0.5-0.7m 13/10/2008	SYD08-2760 TP15, 0.3-0.5m 13/10/2008	SYD08-2761 TP15, 0.6-0.8m 13/10/2008	SYD08-2762 TP15, 1.4-1.6m 13/10/2008	SYD08-2763 TP16, 0.8-1.0m 13/10/2008	SYD08-2764 TP17, 0.5-0.7m 13/10/2008	
Particle Size D	istribution							
Method:	Sieve Siz	e		% Pa	assing			Limits
Description:	53.0mm 37.5mm 26.5mm 19.0mm 13.2mm 9.5mm							
Drying by:	6.7mm 4.75mm		100 99					
N/A	2.36mm		99 95	*			100	
Washed: Sample Not Washed	1.18mm 600µm 425µm 300µm 150µm 75µm		87 84 83 82 78	l- 			100 99 99 99 99 99 99	
Other Test Res	ults							
Description	Method			Resi	ults			Limits
Sample History Preparation Linear Shrinkage (%)	AS 1289.3.1.1, 1289.3.2.1 AS	AS Air-dried ^{1289 3 3 1} Dry Sieved 17.0	ł.	Air-dried Dry Sieved 16.0		Air-dried Dry Sieved 16.0		Linita
Mould Length (mm Crumbling Curling)	125 No Yes		125 No Yes		125 No Yes		
iquid Limit (%)		68		58		53		
Method Plastic Limit (%)		Four Point 23	t	Four Point		Four Point		
Plasticity Index (%)		23 45		20 38		19 34		
Moisture Content (%) Emerson Class Numbe	AS 1289.2.1.1 AS 1289.3.8.1	25.2	20.8	22.6	23.1	21.4	17.7	
	AS 1289.3.8.1	2 (m)				3 (s)		
Comments								







Natural Moisture Content = 8.1%

(c) QESTLab by SpectraQEST.com











Form No: 18909.V1.00



Natural moisture content (%) = 24.5

(c) QESTLab by SpectraQEST.com













N/A



CLIENTS PEOPLE PERFORMANCE GHD GEOTECHNICS	GHD GEOTECHNICS Sydney Laboratory 57 Herbert St Artarmon NSW 2064 Locked Bag 2727 St Leonards 1590 email: artarmon@ghd.com.au web: www.ghd.com.au/ghdgeotechnics Tel: (02) 9462 4860 Fax:(02) 9462 4710
Material Test Report	Report No: SYD081558 Issue No: This issue replaces all previous issues of Report No:
Client: Goodman Property Services Bungaribe Industrial Estate Huntingwood NSW Project: 2117871/00	NATA Accredited Laboratory Number: 679 THIS DOCUMENT SHALL NOT BE REPRODUCED EXCEPT IN FULL.
Sample Details	Particle Size Distribution
Sample ID: SYD08-2792 Field Sample: TP36, 0.5-0.6m Date Sampled: 13/10/2008 Source: N/A Material: N/A	Method: Drying by: Date Tested:
Specification: N/A Sampling Method: N/A Location: N/A Time Sampled: N/A Sampled By: GHD Geotechnics	Sieve Size % Passing Limits
Other Test ResultsDescriptionMethodResultLimitsMoisture Content (%)AS 1289.2.1.117.5N/A	
	Chart
Comments N/A	











Natural moisture content (%) = 26.9

Client Projec Locat		ngaribe	Property e Indust ood			•			Sa	Number.: mple No.: ehole No.:	21/17871/0 08-2875 BH01	00
TEST	METH	OD: A	S4133.4	.1				$\supset \subset$	Client S	ample ID:		
Depth	Test		Dimens	ions			Results			Sample I	Description	~
(m)	Type (D,A,I)	D (mm)	L (mm)	W (mm)	De (mm)	Load P (kN)	Failure Mode (1,2,3)	Is (MPa)	Is ₍₅₀₎ (MPa)	Rock Type	Structure	Moisture
5.18 5.21	D A	51.2 32.8	32.8	51.2	51.2 46.2	0.14 0.01	2 3	0.05 0.00	0.05 0.00	SH SH	BE/LA BE/LA	M M
	•											
-				-								
	- -				· · · · ·							
Comme			ROCK T	YPE.		TRUCTURE		FAILURE MO				
(M) N (D) I (AD) A (AR) A	Wet Moist Dry As Drilled As Receive TYPES	(((d	(SS) Sa (ST) Sil (SH) Sh (CL) Cl	andstone ltstone aale aystone anitic	() () () () ()	AA) Massiv BE) Beddee B) Interbe A) Lamina CR) Crysta	e d dded ted lline	 1 = Fracture the 2 = Fracture and 3 = Fracture the 4 = Fracture in (J) Joint play 5 = Partial fraction 	rough fabric o ong bedding rough rock ma fluenced by pr ane, (M) Micro ture or chip (It	uss e-existing: ofracture, (F) i nvalid result)	Foliation, (V) V	/ein
D = Diar A = Axia	netral (<u>) (</u>]⊤⊳]Þ		L > 0.5 D 0.3W < D			V X WR	me Since Drill RE BOX APPED WRAPPED aratus: LM05		Days UNDER COVI OPEN AIR UNKNOWN	ER
I = Irregu	ılar Lump			<u></u>	0.3W < D	< W De =	$2 \times \sqrt{\frac{\text{Area}}{\text{pi}}}$	in F	$S = \frac{P \times 1000}{(De)^2}$) Ic	$\int = \text{Is x} \left[\frac{\text{De}}{50} \right]$	0.45
Ľ	e Sample Date Test Tested I Checked I	ed: 20 3y: C	/10/08 /10/08 S			GHD	57 Herbert S Tel: (02) 94	EOTECHNI Street, Artarmon, 162 4700 Fax: (1 CHNICAL TE	N.S.W. 2064)2) 9462 4710	/ICES		
	Authoris Signator Da	sed f	J.	oke 28			requireme	ament is issued ents. Accredited y Accreditation	l for complian	ce with ISO/I	s accreditation EC 17025 .	

Client Projec Locat	00	ngaribe	e Indust	v Service rial Esta					Sa	Number.: Imple No.: rehole No.:	21/17871/ 08-2875 BH02	00
	метн			.1						sample ID:		
Depth	Test	r	Dimens	ions			Results			Sample I	Description	
(m)	Type (D,A,I)	D (mm)	L (mm)	W (mm)	De (mm)	Load P	Failure Mode	Is (MPa)	Is ₍₅₀₎ (MPa)	Rock Type	Structure	Moisture
7.92	D	50.9	30.3		50.9	(kN) 0.25	(1,2,3)	0.10	0.10	CII	BE/LA	M
7.92	A	30.3	30.3	50.9	44.3	0.25	23	0.10 0.13	0.10 0.12	SH SH	BE/LA BE/LA	M M
9.32	A	35.1		50.9	47.6	0.25	3	0.15	0.12	SH	BE/LA	M
4.02	A	33.2		50.8	46.3	0.25	3	0.12	0.11	SH	BE/LA	M
4.04	D	50.8	33.2		50.8	0.22	2	0.09	0.09	SH	BE/LA	M
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												1.
		•										
									•			
		ĺ										
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	× (
,												
Comme	ents:			-							-	
MOIST			ROCK T			RUCTURE	-	FAILURE MC				
	Wet Moist			indstone tstone	(M (B	IA) Massiv E) Bedde		= Fracture thr = Fracture alc		blique to bedd	ling	
· ·	Dry			ale	(II			= Fracture thr		ass		
` '	As Drilled			aystone	(L	•	ated 4	= Fracture inf	luenced by p	re-existing:		
(AR) A	As Receive		(G) GI Vther	anitic		R) Crysta her		(J) Joint pla = Partial fract		ofracture, (F) I	Foliation, (V)	/ein
TEST	TYPES		L		.,				ne Since Dril		Days	
D = Diar		$\overline{0}$			L > 0.5 D	De=	= D		E BOX		UNDER COV	ER
	w	<u>v </u>					DxW		APPED	=	OPEN AIR	
A = Axia					0.3W < D	< W De =	$= 2 \text{ x} \sqrt{\frac{\text{pi}}{\text{pi}}}$		VRAPPED		UNKNOWN	
		≥⊥″ ──					Area min		aratus: LM05 ORMULAE			0.45
I = Irreg	ular Lump	۲		_ <u>}[</u> D	0.3W < D	< W De=	$= 2 \text{ x} \sqrt{\frac{\text{pi}}{\text{pi}}}$	-	$s = \frac{P \times 100}{(De)^2}$	0 10	$I = Is x \left[\frac{De}{50} \right]$	
Dat	e Sampl	ed: 14	/10/08				GHD-GE	OTECHNIC	CS			
Ľ	Date Test		/10/08			GH	57 Herbert S	treet, Artarmon,	N.S.W. 2064			
	Tested I		S				161. (02) 94	62 4700 Fax: (0 HNICAL TES		VICES		
	Checked	\sim	0				GEUIEU		ALLIG SEK			
	Authoris Signator	< <	×	1 lo			requireme	ment is issued nts. Accredited	for compliant	nce with ISO/II		
		-	OBre	\boldsymbol{p}_{\perp}				Accreditation				
_	Da	e:	אור	108		,	ory certificate may	-	-	unless permissio	n for the publicat	ion of an

Projec Locat	et: Bu ion: Hu	-	e Indust ood	rial Esta	te					mple No.: ehole No.:	08-2875 BH03	
TEST	METH	OD: AS	<u>54133.4</u>	.1					Client S	ample ID:		
Depth	Test		Dimens	ions			Results			Sample	Description	
(m)	Type (D,A,I)	D (mm)	L (mm)	W (mm)	De (mm)	Load ~ P	Failure Mode	Is (MPa)	Is ₍₅₀₎ (MPa)	Rock Type	Structure	Moisture
6.66 6.67 7.22 7.24 8.56	D A D A D	49.9 23.4 51.6 45.7 50.6	23.4 45.7 34.8	49.9 51.6	49.9 38.6 51.6 54.8 50.6	(kN) 0.06 0.11 0.47 0.64 0.12	(1,2,3) 3 3 3 3 3 3 3	0.02 0.07 0.18 0.21 0.05	0.02 0.07 0.18 0.22 0.05	SH SH SH SH ST/SS	BE/LA BE/LA BE/LA BE/LA LA	M M M M M
8.54	A	34.8		50.6	47.3	0.64	3	0.29	0.28	ST/SS	LA	М
					~							-
(M) N (D) I (AD) A (AR) A	URE Wet Moist Dry As Drilled As Receive	(((d	(ST) Sil (SH) Sh (CL) Cl	YPE indstone tstone iale aystone anitic	() (E (1 (1 (0	TRUCTURE (AA) Massiv (BE) Bedded (B) Interbe (A) Lamina (CR) Crysta (ther:	e d dded ted lline	5 = Partial frac	rough fabric o ong bedding rough rock ma fluenced by pr ane, (M) Micr ture or chip (I	ass re-existing: ofracture, (F) nvalid result)	ding Foliation, (V) V	Jein
D = Diar A = Axia	w			<u> </u>	L > 0.5 D 0.3W < D 0.3W < D	<w de="</td"><td>$2 x \sqrt{\frac{D x}{pi}}$</td><td></td><td>me Since Dril RE BOX APPED WRAPPED baratus: LM05 FORMULAE: $S = \frac{P \times 1000}{(De)^2}$</td><td>56</td><td>Days UNDER COV OPEN AIR UNKNOWN $_{0} = \text{Is x} \left[\frac{\text{De}}{50} \right]$</td><td>ER 0.45</td></w>	$2 x \sqrt{\frac{D x}{pi}}$		me Since Dril RE BOX APPED WRAPPED baratus: LM05 FORMULAE: $S = \frac{P \times 1000}{(De)^2}$	56	Days UNDER COV OPEN AIR UNKNOWN $_{0} = \text{Is x} \left[\frac{\text{De}}{50} \right]$	ER 0.45
Ľ	e Sample Date Test Tested I Checked	ed: 20 By: C	/10/08 /10/08 S	·		GHD	57 Herbert Tel: (02) 9	EOTECHNI Street, Artarmon, 462 4700 Fax: (CHNICAL TE	CS N.S.W. 2064 02) 9462 4710			
	Authoris Signator	sed	R R	role			requirem	ument is issued ents. Accredited ty Accreditation	d for compliar	ice with ISO/I	's accreditation EC 17025 .	······································

Report No.: SYD081499.4

Client Projec Locat		ngaribe	Property e Indust ood						Sa	o Number.: ample No.: rehole No.:	21/17871/0 08-2875 BH04	00
TEST	METH	OD: A	S4133.4	.1				$\supset \sqsubset$	Client S	Sample ID:	······	
Depth	Test		Dimens	ions			Results	······································		Sample I	Description	
(m)	Type (D,A,I)	D (mm)	L (mm)	W (mm)	De (mm)	Load P (kN)	Failure Mode (1,2,3)	Is (MPa)	Is ₍₅₀₎ (MPa)	Rock Type	Structure	Moisture
5.01 5.03	A D	27.0 51.1	27.0	51.1	41.9 51.1	0.00 0.09	3 2	0.00 0.03	0.00 0.03	SH SH	BE/LA BE/LA	M M
							-					
							×	•				
				-								
-	-			-								
(M) N (D) I (AD) A (AR) A	URE Wet Moist Dry As Drilled As Receive TYPES netral		(ST) Sil (SH) Sh (CL) Cl	andstone itstone aale aystone anitic	() () () () ()		$\frac{1}{2} \frac{1}{2} \frac{1}$	$\begin{array}{c} P = Fracture aloge \\ P = Fracture the end of the$	rough fabric o ong bedding rough rock m fluenced by p ane, (M) Micr	re-existing: rofracture, (F) H Invalid result) Iling = 5		
Dat	ular Lump e Sample Date Test		/10/08 /10/08		0.3W < D	O <w de="</td"><td>GHD-GE 57 Herbert S</td><td>COTECHNIC treet, Artarmon,</td><td>N.S.W. 2064</td><td>: 0 Ia</td><td>$= \text{Is x} \left[\frac{\text{De}}{50} \right]$</td><td>0.45</td></w>	GHD-GE 57 Herbert S	COTECHNIC treet, Artarmon,	N.S.W. 2064	: 0 Ia	$= \text{Is x} \left[\frac{\text{De}}{50} \right]$	0.45
	Tested I <u>Checked</u> Authoris Signator Da	By: A sed y:	Bru 7/11	de 108		This laborator	GEOTEC This docu requireme	nts. Accredited Accreditation not be reproduce	in accordance for compliant Number : 6' d except in full	ce with NATA's nce with ISO/II 79	EC 17025 .	ion of an

Report No.: SYD081499.5

Client				v Service rial Esta					\bigcap		Number.: mple No.:	21/17871/ 08-2875	00
Locat	ion: Hu									Bor	ehole No.:	BH05	
TEST	Г МЕТН	(OD: A	\$4133.4	.1]	\vdash		ample ID:		
	Test	1					D14-						
Depth	Test	D	Dimens L	W	De	Load	Results Failure	I		Is(50)	Rock	Description Structure	Moisture
(m)	(D,A,I)	(mm)	(mm)	(mm)	(mm)	P	Mode	(MI		(MPa)	Туре	Siruciure	withsture
(ш)		(mm)	()	(mm)	(initi)	(kN)	(1,2,3)	(m)	aj	(1911 a)	Type		
3.78	D	50.8	36.9		50.8	0.28	2	0.1	1	0.11	SH	BE/LA	М
3.80	A	36.9		50.8	48.9	0.51	3	0.2		0.21	SH	BE/LA	M
5.64	D	50.8	28.2		50.8	0.76	2	0.2	29	0.30	SH	BE/LA	М
5.62	A	28.2		50.8	42.7	0.70	3	0.3	88	0.36	SH	BE/LA	М
6.64	D	51.4	28.8		51.4	0.90	2	0.3	34	0.34	SH	BE/LA	М
6.62	Α	28.8		51.4	43.4	0.75	2	0.4		0.37	SH	BE/LA	М
8.92	D	51.1	24.2		51.1	0.31	2	0.1		0.12	SH	BE/LA	М
8.90	A	24.2		51.1	39.7	0.30	3	0.1		0.17	SH	BE/LA	М
10.07	D	50.8	26.5		50.8	0.39	2	0.1		0.15	SH	BE/LA	Μ
10.05	A	26.5		50.8	41.4	0.36	3	0.2	21	0.19	SH	BE/LA	M
													. ×
					4	· .							
												-	
							-						
7											1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -		
Comme	ents:	•									,		
MOIST	URE	J	ROCK T	YPE	S	TRUCTURE		FAILUI	RE MO	DDE			
	Wet		. ,	indstone		MA) Massiv					blique to bedo	ling	
	Moist Dry			tstone ale	•	BE) BeddeaB) Interbe				ong bedding rough rock m	966		
. ,	As Drilled			aystone		.A) Lamina				fluenced by p			
(AR)	As Receive	•		anitic		CR) Crysta		~ /				Foliation, (V) V	/ein
			Athor:		0	ther [.]		<u>5 = Parti</u>	al frac	ture or chip ()	Invalid result)		
TEST D = Diai	TYPES metral	0 0			L > 0.5 D	De =	D		COF	me Since Dri RE BOX APPED		Days UNDER COV OPEN AIR	ER
A = Axia		J.			0.3W < D	< W De =	2 x √ pi		UNV UNV	WRAPPED aratus: LM05	556	UNKNOWN	
I = Irreg	ular Lump			Ĵ₽	0.3W < D	< W De =	$2 \text{ x} \sqrt{\frac{\text{Area}_{\text{m}}}{\text{pi}}}$	<u>in</u>		$s = \frac{P \times 100}{(De)}$	0Ts	$I_0 = I_S x \left[\frac{De}{50} \right]$	0.45
	te Sampl Date Test	ed: 20	/10/08 /10/08	-		GHD		Street, Art	armon,	N.S.W. 2064			
Ċ	Tested I Checked	·					161. (02) 9)2) 9462 4710 STING SER	VICES		
	Authoris		À.					ument is	issued	in accordance	e with NATA'	s accreditation	
	Signator	<i>e</i> .	Br	uply			-			l for complian Number : 6	nce with ISO/I 79	EC 17025 .	
	Da	ite:	2	11/08		,	y certificate may act has been obta	-		-	unless permissio	n for the publicat	ion of an

Clie			.	<u> </u>			·····	$\overline{}$				
Proj			Property e Indust							Number.: mple No.:	21/17871/ 08-2875	00
	ation: Hu	÷		nai esta	lle					ehole No.:		
	т метн			1				— <u> </u> —		ample ID:	Dillo	
									Chent			
Deptl	n Test Type	D	Dimens L	ions W	De	Load	Results Failure	Is	Is(50)	Sample I Rock	Description Structure	Moisture
(m)	(D,A,I)	(mm)	(mm)	(mm)	(mm)	Р	Mode	(MPa)	(MPa)	Туре	Structure	Moisture
6.41	D	51.0	33.1		51.0	(kN) 0.57	(1,2,3) 2	0.22	0.22	SS	BE	M
6.39		33.1		51.0	46.4	0.75	3	0.35	0.34	SS	BE	М
8.52	D	51.5	30.0		51.5	0.76	2	0.29	0.29	ST/SH	BE	М
8.54	Α	30.0		51.5	44.4	0.50	3	0.25	0.24	ST/SH	BE	М
9.72	D	50.9	35.4		50.9	0.85	2	0.33	0.33	ST/SH	BE	М
9.70		35.4		50.9	47.9	0.51	2	0.22	0.22	ST/SH	BE	М
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										. '		
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Comn	nents:				[]				:		<u> </u>	·. ·
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MOIS	FURE		ROCK T	YPE	S	TRUCTURE		FAILURE M	ODE			
(W)	Wet		· · ·	indstone		MA) Massiv				blique to bedd	ing	
(M) (D)	Moist Dry		· · ·	tstone ale	•	BE) BeddeB) Interb	-	2 = Fracture al 3 = Fracture th		955		
(AD)	As Drilled		• •	aystone	-	LA) Lamin		4 = Fracture in	•			
(AR)	As Receive		(G) Gr	anitic		CR) Crysta				ofracture, (F) I	Foliation, (V) V	/ein
TES	T TYPES		L			ther	:	5 = Partial fracElement T			Dert	
	ametral	ᡣ᠊ᡮ			L>0.5 E	De=	= D	-	ime Since Dril RE BOX		Days UNDER COV	ER
	W		<u>_</u>						RAPPED		OPEN AIR	
A = Ax	ial 🥅	TD			0.3W < D	< W De =	$= 2 \text{ x} \sqrt{\frac{1}{\text{pi}}}$	- UN	WRAPPED		UNKNOWN	
		⊐ [⊥] لا					Area m		oaratus: LM05 ORMULAE			0.45
I = Irre	gular Lump	٢		<u>]</u> D	0.3W < D	< W De	$= 2 \text{ x} \int \frac{11 \text{ cu}_{\text{m}}}{\text{pi}}$	_	P x 100	0 10	$=$ Is x $\left[\frac{\text{De}}{50}\right]$	0.45
			·w-				V P7		$ls = (De)^{2}$	<u>,</u> 1350	<u> </u>	
D	ate Sampl	ed: 13	/10/08				GHD-GI	EOTECHNI	CS			
	Date Test		/10/08			GH	57 Herbert S	Street, Artarmon	N.S.W. 2064			
	Tested I	•	S				Tel: (02) 92	462 4700 Fax: (CHNICAL TE	•	VICES		
	Checked	By: A	F				GEUIEC	MUNCAL IE	STING SEK	ALLS		
	Authori	L	R-		(•			e with NATA's		
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Client Projec Locat		ngaribe	e Indust	/ Service rial Esta					Sa	Number.: mple No.: ehole No.:	21/17871/0 08-2875 BH07	00
	METH			.1						ample ID:		
Depth	Test		Dimens	ions			Results			Sample	Description	
(m)	Туре (D,A,I)	D (mm)	L (mm)	W (mm)	De (mm)	Load P	Failure Mode	Is (MPa)	Is ₍₅₀₎ (MPa)	Rock Type	Structure	Moisture
4.39	D	51.3	37.8	51.0	51.3	(kN) 0.28	(1,2,3) 2	0.11	0.11	SS	BE	M
4.41 5.94 5.95	A D A	37.8 51.5 42.1	42.1	51.3 51.5	49.7 51.5 52.5	0.37 1.69 1.83	3 2 5	0.15 0.64 0.66	0.15 0.65 0.68	SS SS SS	BE BE BE	M M M
0.50				51.5	52.0	1.05		0.00				
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				×.		<i>,</i>						
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Comme	nts:										· · ·	J,
(M) N (D) I (AD) A (AR) A	URE Wet Moist Dry As Drilled As Receive TYPES	(((d	(ST) Sil (SH) Sh (CL) Cl	YPE andstone tstone aale aystone anitic	() () () () ()	TRUCTURE MA) Massiv BE) Bedded (B) Interbe LA) Lamina CR) Crysta Wher Interbe	e d dded ted lline	5 = Partial frac	rough fabric o ong bedding rough rock m fluenced by p ane, (M) Micr	ass re-existing: ofracture, (F) invalid result)	ding Foliation, (V) V Days	Vein
D = Diar A = Axia	metral (<u>) (</u>]⊤⊳	ŪIÞ		L > 0.5 E 0.3W < D		$\int D x V$	V X WR	RE BOX APPED WRAPPED		UNDER COV OPEN AIR UNKNOWN	ER
I = Irrega	ılar Lump			<u>_</u>	0.3W < D	< W De =	$2 \text{ x} \sqrt{\frac{\text{Area}}{\text{pi}}}$	in F	$\frac{\text{paratus: LM05}}{\text{ORMULAE}}$ $s = \frac{P \times 100}{(De)}$: 0 ₁₋	$_0 = \text{Is x} \left[\frac{\text{De}}{50} \right]$	0.45
E	e Sample Date Test Tested I Checked	ed: 20 By: Ci	/10/08 //10/08 S			GHD	57 Herbert S Tel: (02) 94	EOTECHNIC Street, Artarmon, 162 4700 Fax: (1 CHNICAL TE	N.S.W. 2064)2) 9462 4710	VICES	-	
	Authoris Signator	sed T	g kruo	 ke		NATA	requireme	ument is issued ints. Accredited y Accreditation	l for complia	nce with ISO/I	's accreditation EC 17025 .	
	Da	te: ך	111/08				y certificate may	-	d except in full		on for the publicat	ion of an

Client Projec Locat		ngaribe	Property e Indust ood						Sa	Number.: mple No.: ehole No.:		00
TEST	METH	OD: A	<u> 84133.4</u>	.1					Client S	ample ID:		
Depth	Test		Dimens	ions			Results			Sample	Description	
(m)	Type (D,A,I)	D (mm)	L (mm)	W (mm)	De (mm)	Load P (kN)	Failure Mode (1,2,3)	Is (MPa)	Is ₍₅₀₎ (MPa)	Rock Type	Structure	Moisture
4.93 4.95 5.74 5.73	D A D A	51.5 36.0 51.3 20.1	36.0 20.1	51.5 51.3	51.5 48.6 51.3 36.2	1.10 1.94 0.33 0.42	2 3 2 3	0.41 0.82 0.13 0.32	0.42 0.81 0.13 0.28	SS/ST SS/ST SH SH	BE BE BE/LA BE/LA	M M M M
									• .			
				•	-							
(M) N (D) I (AD) A (AR) A	URE Wet Moist Dry As Drilled As Receive	(((d ((ST) Sil (SH) Sh (CL) Cl	YPE ndstone tstone ale aystone anitic	(M (B (II (L (C	,	ve ed edded ated alline	5 = Partial frac	rough fabric o ong bedding rough rock m fluenced by p ane, (M) Micr ture or chip ()	ass re-existing: rofracture, (F) Invalid result)	ding Foliation, (V) V	Vein
TEST D = Diar A = Axia	- w][¤		L > 0.5 D 0.3W < D	De = < W De =	$= D$ $= 2 x \sqrt{\frac{D x V}{pi}}$		me Since Dril RE BOX RAPPED WRAPPED paratus: LM05		Days UNDER COV OPEN AIR UNKNOWN	ER
I = Irreg	ular Lump	5			0.3W < D	< W De =	$= 2 \text{ x} \sqrt{\frac{\text{Area}_{\text{m}}}{\text{pi}}}$		formulation Form	0Ie	$_0 = \text{Is x} \left[\frac{\text{De}}{50} \right]$	0.45
D	te Sample Date Test Tested I Checked	ed: 20 3y: C				GHI	57 Herbert Tel: (02) 9	EOTECHNI Street, Artarmon, 462 4700 Fax: (I CHNICAL TE	N.S.W. 2064 02) 9462 4710	VICES		
	Authoris Signator	sed y: €	¥ PBru	ste			requireme Laborator	ents. Accrediter y Accreditation	d for complian n Number : 67	nce with ISO/I 79		
	Da	ie:	אןר	108		1	ry certificate may ract has been obta		-	unless permissio	on for the publicat	ion of an

Report No.: SYD081499.9

Clien Proje	ct: Bu	ngaribe	Property e Indust				· ·		Sa	o Number.: ample No.:	21/17871/ 08-2875	00	
	tion: Hu							·		ehole No.:	BH09		
		UD: A	AS4133.4.1						Client Sample ID:				
Depth	Test	D	Dimensions			Results			T	Sample Description			
(m)	Type (D,A,I)	D (mm)	L (mm)	W (mm)	De (mm)	Load P (kN)	Failure Mode (1,2,3)	Is (MPa)	Is ₍₅₀₎ (MPa)	Rock Type	Structure	Moisture	
4.48	D	49.7	41.4	10.7	49.7	0.12	2	0.05	0.05	SH	BE/LA	M	
4.46	A	41.4		49.7	51.2	0.09	3	0.03	0.03	SH	BE/LA	М	
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(M) 1 (D) (AD)		(((d ((ST) Sil (SH) Sh (CL) Cl	YPE indstone tstone ale aystone anitic	(M (E (I) (L (C	TRUCTURE IA) Massiv BE) Bedde B) Interbe A) Lamina CR) Crysta	ve d edded ated illine	2 = Fracture 3 = Fracture 4 = Fracture (J) Joint p	MODE through fabric of along bedding through rock m influenced by p plane, (M) Mici acture or chip (ass re-existing: rofracture, (F) l		Vein	
TEST TYPES L D = Diametral $()$ $()$ $()$							Elapsed Time Since Drilling = 0 Days X CORE BOX X UNDER COVER						
$A = Axia1 \qquad 0.3W < D < W \qquad De = 2x \sqrt{pi} \qquad \Box UNWRAPPED \qquad \Box UNKNOWN \\ Test Apparatus: LM0556 \qquad \Box UNKNOWN$													
I = Irreg	ular Lump			Ĵ₽	0.3W < D	< W De =	$= 2 \text{ x} \sqrt{\frac{\text{Area}_{\text{m}}}{\text{pi}}}$	<u>in</u>	$FORMULAE$ $Is = \frac{P \times 100}{(De)}$	0 10	$D = \text{Is x} \left[\frac{\text{De}}{50} \right]$	0.45	
Ι	te Sampl Date Test Tested I Checked	ed: 17 By: C	/10/08 /10/08 S			GHI	57 Herbert Tel: (02) 94	62 4700 Fax	NICS on, N.S.W. 2064 : (02) 9462 4710 ESTING SER	VICES			
	Authoris Signator	sed f	Ba	rde			requireme	nts. Accredi	ed in accordance ted for complia- ion Number : 6'	nce with ISO/I		-	
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Document Status

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0	Roberta Lamont	Tony Colenbrander		Tony Colenbrander		11/12/08		
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