DRAINAGE REPORT



Allen Price & Scarratts Pty Ltd Land & Development Consultants 75 Plunkett Street NOWRA NSW 2541

Client: Shoalhaven Starches

Project: Proposed Development Stormwater Concept

Project No: N26856 SCC Ref: N/A

Date: 20 October 2016

PROPOSED DEVELOPMENT DRAINAGE DESIGN REPORT at

160 BOLONG ROAD, BOMADERRY

This report has been prepared to support a development application in accordance with Shoalhaven City Council's DCP2014 and Subdivision Engineering Specification D5 for events from the 10% AEP to 1% AEP.

Calculations have been prepared by a qualified practicing engineer using Colebrook-White Method, Bernoulli's Principle and Rational Methods.

The proposed development includes an industrial building 'Flour Mill B' and a related Mill Silo. The existing condition of the areas to be developed is a mixture of concrete and asphalt surfaces, as such the existing area is considered to be 100% impervious.

As there is no change in impervious area for the development, the total discharge pre and post development is determined to be equal and as such no additional detention is required. It is also noted that as the water will be captured from the roof of Flour Mill B it will be significantly cleaner than existing ground surface run-off.

Existing building Flour Mill A currently discharges its roof stormwater via a 150mm diameter PVC pipe the runs down the northern side of the building. Once underground the existing pipe turns south and extends under the Flour Mill A building before entering a Gross Pollutant Trap (AGLASS PTY LTD GPT-10-150). The GPT then discharges to the salt water cooling return pit which discharges into the Shoalhaven River.

It is concluded that as the runoff from the new Flour Mill roof will be cleaner than the current ground level runoff, and will also pass through the GPT prior to discharge, this runoff will be cleaner than the current arrangement and will therefore improve as a result.

Flows from the existing building under a 10% AEP event are calculated to be approximately 16L/s, while the manufacturer reports the GPT to have a maximum design flow of 150L/s.

The pipe as it runs under Flour Mill A is charged and hence has a higher than normal outlet capacity due to the available head (approximately 30m). To determine the suitability of the existing stormwater line some key factors needed to be determined:

- a) Total discharge of proposed and roof drainage system
- b) Head required to discharge this flow assuming orifice conditions
- c) Head required to overcome friction in the line from the base of the down pipe to the outlet
- d) Head required to overcome height rise in the pipe as well as the GPT

In compliance with Shoalhaven City Council's DCP2014 and Subdivision Engineering Specification D5 the Major and Minor drainage systems have been designed and summarised as follows:

Minor Drainage (10% AEP):

- Piped flows from the existing Flour Mill A and future Flour Mill B are to discharge to the Shoalhaven River via the existing GPT.
- Based upon the site being 100% paved, the permissible discharge of the site is 0.036m³/s for 10% AEP (See Appendix A).
- Post development the total discharge from the proposed allotment is 0.036m³/s for 10% AEP (See Appendix A).
- The post-development peak flow rates from the site do not exceed the predevelopment peak flow rates.

- Total discharge from the site is 36.1L/s which is still far below the existing GPT capcity (as reported by manufacturers).
- Appendix E indicates the location for possible pipe work and survey requirements.

Major Drainage (1% AEP):

- All major drainage flows are to discharge from the site overland as sheet flows. No stormwater is proposed to discharge into adjoining private properties in a concentrated manner.
- Based upon the site being 100% paved, the permissible discharge of the site is 0.053m³/s for 1% AEP.
- Post development the total discharge from the proposed allotment is 0.053m³/s for 1% AEP.
- The post-development peak flow rate from the site does not exceed the predevelopment peak flow rate.

Using the 1:10 ARI storm the head pressures requried for successful outlet of stormwater are calculated in Appendix C and D. It is determined that the existing system is capable of discharging the 36.1L/s generated in the 10yr storm event and hence downpipes are able to be slung from the walls of proposed Flour Mill B as long as the connection point to the main stormwater line is greater than 4.21m above ground level. It is recommended that the connection point be no lower than 6m above ground level to ensure adequate discharge.

As part of the design, it is noted that the proposed Flour Mill B building must incorporate the existing 150mm down pipe into its structure to maintain the existing flow from Flour Mill A.

As the Mill Silo has no nearby drainage connections available and is so small in catchment area it is proposed to diffuse the roof water via a modified tee junction as shown in Appendix E. This will maintain the existing flow path, volume and quality of the surface run-off.

It is also noted that the location of existing drainage structures must be confirmed by survey at detail design stage to divert any active stormwater from under the proposed building footprint.

Appendix A to E show the calculations verifying that the discharge from the site for design events up to and including the 100 year average recurrence interval does not exceed the predeveloped conditions.

APPENDIX A - Flour Mill B Flow Generation Calculation Sheet

FLOW GENERATION CALCULATIONS



Allen Price & Scarratts Pty Ltd 75 Plunkett Street NOWRA NSW 2541

Client: Shoalhaven Starches

Project: Concept Stormwater - Proposed Flour Mill B
Project No: N26856

Project No: N26856 Council's Ref: N/A Date: 14-Oct-16

FLOUR MILL A

FLOUR MILL B

Q=Cy*I*A*2.78 (in L/s)

ROOF AREA

ROOF AREA

Time of Concentration (mins) = 5
Rainfall Intensity 1:10 ARI (mm/hr) for Nowra I = 194
Rainfall Intensity 1:100 ARI (mm/hr) for Nowra I = 282

Co-efficient of Runoff Cy= 0.9 (assume 100% impervious)

Total Site Area (ha) = 0.0744

Total Site Discharge (L/s) = 36.1 1:10 ARI Total Site Discharge (L/s) = 52.5 1:100 ARI

Catchment Area Discharge Min Size Min Cumulative Cumulative **Catchment Description** Catchment Type Discharge (L/s) Discharge (m3/s) (m2) Q (L/s) (mm) Grade **EXISTING CONDITIONS** FLOUR MILL A **ROOF AREA** 334 16.2 16.2 0.016 150 0.5% **EXISTING** CONCRETE/BITUMEN HARDSTAND AREA OVERLAND FLOW 36.1 0.036 410 19.9 N/A N/A Total Pre-development discharge to Shoalhaven River 36.1 0.036 ASSUMING FLOUR MILL COMBINED DRAINAGE **ROOF AREA** FLOUR MILL A 334 16.2 16.2 0.016 150 0.5% FLOUR MILL B **ROOF AREA** 410 19.9 36.1 0.036 150 2.0% OR 225 0.5% Total Post-developmentdischarge to Shoalhaven River 0.036 36.1 ASSUMING FLOUR MILL PARALLEL PIPE DRAINAGE

410

Total Post-developmentdischarge to Shoalhaven River

16.2

19.9

19.9

36.1

0.016

0.020

0.036

150

150

0.5%

1.0%

APPENDIX B - Mill Silo Flow Generation Calculation Sheet

FLOW GENERATION CALCULATIONS



Allen Price & Scarratts Pty Itd 75 Plunkett Street NOWRA NSW 2541

Client: Shoalhaven Starches
Project: Concept Stormwater - Mill Silo
Project No: N26856

Project No: N26856
Council's Ref: N/A
Date: 14-Oct-16

Q=Cy*I*A*2.78 (in L/s)

Time of Concentration (mins) = 5
Rainfall Intensity 1:10 ARI (mm/hr) for Nowra I = 194
Rainfall Intensity 1:100 ARI (mm/hr) for Nowra I = 282

Co-efficient of Runoff Cy= 0.9 (assume 100% impervious)

Total Site Area (ha) = 0.0011

Total Site Discharge (L/s) = 0.5 1:10 ARI Total Site Discharge (L/s) = 0.7 1:100 ARI

Total Post-developmentdischarge to Shoalhaven River

Catchment Area Discharge Cumulative Cumulative Min Size Min **Catchment Description** Catchment Type Q (L/s) Discharge (L/s) Discharge (m3/s) (m2) (mm) Grade **EXISTING CONDITIONS** ASPHALT HARD EXISTING GROUND SURFACE STAND AREA 11 0.5 0.5 0.001 N/A N/A Total Pre-development discharge to Shoalhaven River 0.5 0.001 ASSUMING FLOUR MILL COMBINED DRAINAGE MILL SILO ROOF AREA 11 0.5 0.001 100 0.5%

0.5

0.001

APPENDIX C - Flour Mill B Friction Loss through a uPVC pipe

Charged Stormwater System - Friction Loss through a PVC-U Stormwater Pipe



Allen Price & Scarratts Pty Ltd Land & Development Consultants

75 Plunkett Street NOWRA NSW 2541

Client: Shoalhaven Starches

Project: Flour Mill B Concept Stormwater Drainage

Project No: N26856 SCC Ref: N/A Date: 20-Oct-16

Note: Bold cells only are inputs

Discharge

Development Size = **744** m2

ARI = **10** years
tc = **5** mins

C = **0.9** (100% impervious roof area)

I = 194 mm/hr

Area = 744 m2 (100% of roof area)

Q = 36.1 L/s

L = **40** m for length of pipe from bottom of downpipe to GPT (x2 for safety)

D = **0.15** m for diameter of pipe

k = 0.03 mm for upVC with chemically cemented joints

v = 1.14E-06 Water at 15 degrees C

V = 2.04 m/s $N_R = 2.69E+05$ f = 0.01651

Sf = 0.02339 m/m

 $\label{eq:harmonic} \begin{array}{ll} \text{Hf =} & 0.936 \text{ m} \\ \text{Therefore Hf \approx} & 1 \text{ m} \end{array}$

<u>APPENDIX D</u> – Flour Mill B Charged Stormwater System Summary and calculation sheets

Charged Stormwater System - Summary Sheet



Allen Price & Scarratts Pty Ltd Land & Development Consultants 75 Plunkett Street NOWRA NSW 2541

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Project: Flour Mill B Concept Stormwater Drainage

Project No: N26856 SCC Ref: N/A Date: 20-Oct-16

Note: Bold cells only are inputs

Discharge

Required Flow = **36.1** L/s (calculated as per Flow Generation Sheet)

Orifice Diameter (base of downpipe) = 150 mm

Pressure Head required at orifice (h1) = **0.21** m (See calculation Sheet)

Friction Head Loss (hf)= 1 m (calculated as 0.936m)

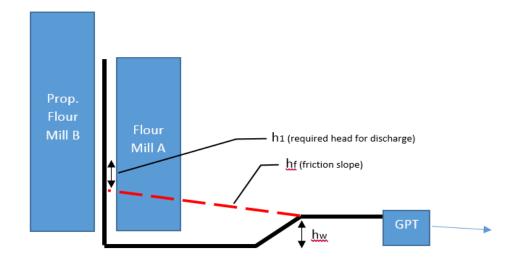
Head Loss through system layout (hw)= 3 m (See head loss for rise over wall)

Total Head Required at downpipe = 4.21 m (recommended 6m minimum for safety)

Available Head at downpipe = **30.0** m

Maximum Head For Discharge = 26.0 m

Maximum Theoretical Line Capacity = **243.5** L/s (assuming Cd = 0.61)



Charged Stormwater System - Calculation Sheet



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Project: Flour Mill B Concept Stormwater Drainage

Project No: N26856 SCC Ref: N/A Date: 20-Oct-16

Note: Bold cells only are inputs

Bernoulli Equation:

$$g \cdot h_1 + \frac{p_1}{\rho} + \frac{V_1^2}{2} = g \cdot h_2 + \frac{p_2}{\rho} + \frac{V_2^2}{2}$$

Assumptions:

 $V_1 = 0$ (negligible as compared to V_2)

 $p_1 = p_2$ (Pressure differential negligible under gravity)

h₂ = 0 (Near 0 as per Manildra Elevations)

Simplified Equation

$$g \cdot h_1 = \frac{V_2^2}{2}$$

Assuming Full flow through charged pipe:

$$V = \frac{Q}{A}$$

$$\therefore g \cdot h_1 = \frac{\left(\frac{Q_2}{A_2}\right)^2}{2} \qquad \rightarrow h_1 = \frac{\left(\frac{Q_2}{A_2}\right)^2}{2g}$$

 $g = 9.81 \text{ ms}^{-2}$

 $Q_2 =$ **36.1** L/s (Value from Flow Generation Calcs)

Diameter of Pipe = 150 mm $A_2 = 0.0177 \text{ m}^2$

 $h_1 = 0.21 \text{ m}$

Friction Loss in pipe = 1 m (see attached spreadsheet)

Assumed conservative head loss through

system for rise over wall GPT = 3 m

Total Head required for adequate

discharge = 4.21 m (recommended 6m minimum for safety)

Available head from building elevation = 30 m

Therefore adequate capacity achieved with existing pipe outlet

<u>APPENDIX E: ENGINEERING DRAWINGS</u> <u>N26856-401 & 402</u> – Stormwater Concept Drawings

