Appendix A

Assumptions and Exclusions

Appendix A Assumptions and Exclusions

Assumptions

The following assumptions have been used in the preparation of this inventory:

- Fuel used for all construction vehicles and by all vehicles to transport materials is diesel oil
- The energy content factor for diesel oil is 38.6 GJ/kL (DCC, NGA Factors, June 2009. Table 4)
- The Scope 1 emission factors for the combustion of diesel oil are:
 - EFCO2: 69.2 kg CO2-e/GJ
 - EFCH4: 0.2 kg CO2-e/GJ
 - EFN2O: 0.5 kg CO2-e/GJ (DCC, NGA Factors, June 2009. Table 4)
- The Scope 3 emission factor for diesel oil is 5.3 kg CO2-e/GJ (DCC, NGA Factors, June 2009. Table 38)
- Transport of materials to/from site is by road only
- Fuel used for transport of materials to/from site is diesel (general transport), with a fuel consumption rate of 0.542L/km
- Fuel used for transport of staff is gasoline, with a fuel consumption rate of 0.107L/km
- The Scope 2 emission factor for consumption of purchased electricity from the grid in NSW is 0.89 kg CO2e/kWh (DCC, NGA Factors, June 2009. Table 5)
- The Scope 3 emission factor for consumption of purchased electricity from the grid in NSW is 0.18 kg CO2-e/kWh (DCC, NGA Factors, June 2009. Table 39)
- All construction materials will be delivered by the supplier, therefore the Scope 1 and Scope 3 emissions
 associated with the transport of construction materials will be categorised as a scope 3 emissions for the
 project.
- Fuel used during transportation of materials is calculated based on round trips
- 15,000 tonnes of waste per annum will be landfilled
- The existing waste transfer station is proposed to be used during the operation of the Armidale Regional Landfill.
- The landfill management will be responsible for the transport of waste and cover material to the landfill site.
- The landfill will operate for 6 days a week, 52 weeks a year.
- Vegetation *temporarily* cleared will be revegetated as part of the construction works. Whilst removal of vegetation within the development footprint would be *permanent*, clearing for access and compound areas would be temporary as these areas would be rehabilitated post-construction.
- 12.7 ha of vegetation will be permanently cleared.

Materials

Bulk Densities

- Clay Density 2.82 t/m3
- Fill/Cover Material Density 2.0 t/m3
- HDPE Density 0.97 t/m3
- Gravel Density 1.522 t/m3
- Soil Density 1.800 t/m3

Waste

It was assumed that the waste landfilled will be transported from the existing waste transfer facility on Long Swamp Road to the proposed landfill site. Three trucks per day will deliver the waste to the landfill.

The landfill will be classed as a General Solid Waste (putrescibles) landfill. It is Council's longer term objective, however, to begin operating the landfill, as soon as possible in the future (and then until final closure) only as a General Solid Waste (non-putrescible) facility, when appropriate additional off-site sorting and/or treatment technologies are able to be procured and successfully employed.

Exclusions

This assessment excludes GHG emissions associated with:

- The end of life (demolition, decommissioning, etc) of the project's infrastructure (site sheds, road, etc)
- The use of materials and construction equipment for maintenance purposes
- The mixed waste generated by construction and operational staff
- The removal of any existing infrastructure
- The operation, maintenance and sorting of waste at the waste transfer station
- Fugitive emissions of refrigerants from refrigeration and air conditioning systems
- Support services for the facility

Appendix B

Input Data and Resource Consumption Calculations

Appendix B Input Data and Resource Consumption Calculations

Typical Excavation Dimensions	Per Cell
Width (m)	80
Length (m)	275
Depth (m)	14
Area (m2)	22,000
Volume (m3)	308,000

Material requirements for landfill and pond lining	Quantity
Landfill cell area (m2)	22,000
Number of Cells	5
Total landfill area (m2)	110,000
Leachate pond base area (m2)	4,900
Total area of landfill and leachate pond which will be	444.000
lined (m2)	114,900
Thickness of clay lining (m)	0.3
Clay required (for landfill and leachate pond lining) (m3)	34,470
HDPE thickness for lining (m)	0.0015
HDPE required (for landfill and leachate pond lining) (m3)	172.35
Thickness of gravel for leachate drainage layer (m)	0.3
Gravel required for leachate drainage layer (m3)	33,000

Material requirements for landfill cap	Quantity
Surface area of landfill cap (m2)	171,366
Thickness of revegetation layer (Soil) (m)	1
Volume of soil required (m3)	171,366
Thickness of gravel drainage layer (m)	0.3
Volume of gravel required (m3)	51,410
Thickness of clay capping (m)	0.5
Volume of clay required (m3)	85,683
Volume of Waste and Cover (m3)	211,000
Percentage of cover	20%
Cover material required (m3)	42,200

Note: The above estimate of the construction materials which will be used in the project's construction is based on the preliminary concept design.

Emedon Source Guantity (#)	Gusntey (md Density (**)	Density (*)	Suzmith	Scope 2 Emis Source	Source:	Ca Total Scop (I)	ratage cancift	Movement	Distance	Fotal Km Francised	Efficiency (L/kon)	Efficiency Fuel Using (L/lon) (Act)					
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Cover Material	42280		75.950		C.COTS Econwert Database		DJ.		20	ш	0.233	ш					
OTAL						2,347				fot	Fotal brei use	1,995,531					
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				Puel Used	Chergy Cortent	Stope 1 Embasion factor (EP)		71	Fotal Foops 1 GHG Emission	Scape 3 Freisslan Fector	Straye 3 GHG	Treat GHG					
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Proc'toxis	340	9	4872	37.44	1573	39.6	65.3	60	1 0.5	101	8.3	80	1183	5,051	383	5.4%	
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Stratigies	20	74	624	12.48		38.6	88.2	0.5	0.5	34	ari ari	25				l.	
-OTAL	A 100	0.00000	Section 2		14,050				-cate/	640		49	600	34 503	2,427	34,415	
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Appendix C

Landfill Greenhouse Gas Emissions Calculation Results

Appendix C Landfill Greenhouse Gas Emissions Calculation Results

waste mix type	DOC	K
Food	0.15	0.185
Paper & paper	0.4	0.06
Garden & green	0.2	0.1
Wood	0.42	0.03
Textiles	0.24	0.06
Sludge	0.05	0.185
Nappies	0.24	0.06
Rubber & Leather	0.39	0.06
metal, plastics & glass	.0	0

	Ρ	ar	a	m	e	te	rs
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DOO	
DOC,	0.5
M	13 M=7 means no delay; M=13 means 6 months delay; normally 0-6
F	0.5
MCF	1.0
7	0.01425
OF	0.1

NSW waste streams	%
Municipal (M)	31%
Commercial &	2.20
Industrial (C&D)	42%
Construction &	
Demolition (C&I)	27%
total	100%

waste mix type	M (%)	C&I (%)	C&D (%)
Food	26%	6%	0%
Paper & paper board	26%	55%	3%
Garden & Park	10%	3%	2%
Wood & wood waste	2%	14%	6%
Textiles	4%	2%	0%
Sludge	0%	3%	0%
Nappies	5%	0%	0%
Rubber & Leather Concrete, metal, plastic	0%	1%	0%
and glass	26%	16%	89%
total	100%	100%	100%

waste composition	M (%)	C&I (%)	C&D (%)	total (%)
Food	8%	3%	0%	11%
Paper & paper board	8%	23%	1%	32%
Garden & Park	3%	1%	1%	5%
Wood & wood waste	1%	6%	2%	8%
Textiles	1%	1%	0%	2%
Sludge	0%	1%	0%	1%
Nappies	2%	0%	0%	2%
Rubber & Leather Concrete, metal, plastic	0%	0%	0%	0%
and glass	8%	7%	24%	39%
total	31%	42%	27%	100%

Scenario 1

				Food			
Year	waste (t)	DDOC _{midap}	DDOC _m	DDOC _{mi remain}	DDOC _{m accum}	DDOC _{m discom}	CH _{4 generated} (t
1	1,587	119.0	0.0	119.0	119.0	0.0	0.
2	1,587	119.0	0.0	119.0	217.9	20.1	13.
3	1,587	119.0	0.0	119.0	300.2	36.8	24.
4	1,587	119.0	0.0	119.0	368.5	50.7	33.
5	1,587	119.0	0.0	119.0	425.3	62.2	41.
6	1,587	119.0	0.0	119.0	472.5	71.8	47.
5 6 7	1,587	119.0	0.0			79.8	53.
8	1,587	119.0	0.0		544.3	86.4	57.
8 9	1,587	119.0	0.0		571.4	91.9	61.
10	1,587	119.0	0.0		593.9	96.5	64.
11	1,587	119.0	0.0		612.6	100.3	66.
12	1,587	119.0	0.0	119.0	628.2	103.5	69.
13	1,587	119.0	0.0		641.1	106.1	70.
14	1,587	119.0	0.0	119.0	651.9	108.3	72.
15	1,587	119.0	0.0		660.8	110.1	73.
16	1,587	119.0	0.0		668.2	111.6	74.
17	1,587	119.0	0.0		674.4	112.9	75.
18	1,587	119.0	0.0	119.0	679.5	113.9	75.
19	1,587	119.0	0.0	119.0	683.8	114.8	76.
20	1,587	119.0	0.0	119.0	687.3	115.5	77.
21	1,587	119.0	0.0	119.0	690.2	116.1	77.
22	1,587	119.0	0.0	119.0	692.7	116.6	77.
23	1,587	119.0	0.0		694.7	117.0	78.
24	1,587	119.0	0.0	119,0	696.4	117.3	78.
25	1,587	119.0	0.0	119.0	697.8	117.6	78.
26	1,587	119.0	0.0		699.0	117.9	78.
27	1,587	119.0	0.0		700.0	118.1	78.
28	1,587	119.0	0.0		700.8	118.2	78.
29	1,587	119.0	0.0	119.0	701.4	118.4	
30	1,587	119.0	0.0	119.0	702.0	118.5	79.
31	1,587	119.0	0.0	119.0	702.4	118.6	79.
32	1,587	119.0	0.0	119.0	702.8	118.6	79.
33	1,587	119.0	0.0	119.0	703.2	118.7	79.
34	1,587	119.0	0.0		703.4	118.8	79.
35	1,587	119.0	0.0	119.0	703.6	118.8	79.
36	1,587	119.0	0.0	119.0	703.8	118.8	79.
37	1,587		0.0	119.0	704.0	118.9	79.
38	1,587		0.0	119.0	704.1	118.9	79.
39	1,587		0.0		704.2	118.9	79.
40	1,587		0.0		704.3	118.9	79.
41	1,587		0.0		704.4	119.0	79.
42	1,587		0.0		704.4	119.0	79.
43	1,587		0.0		704.5		79.
44	1,587		0.0		704.5	119.0	79.
45	1,587		0.0		704.6	119.0	79.
46	1,587		0.0		704.6	119.0	79.
47	1,587				704.6	119.0	79.
48	1,587		0.0		704.6	119.0	79.
49	1,587		0.0		4.20.10	119.0	79.
50	1,587		0.0	119.0	704.7	119.0	79.
51			0.0			119.0	79.

Scenario 1

The Marie	ushaca ass	DDOC _{m desum}	DDOG	DDOC _{m account}	DDOC _{m decom} *	and the
vaste (t)	DDOC _{m dep} (t)	(f)	(t)	(t)	(t)	CH _{4 generated} (
4,796	959.1	0.0	959.1	959.1	0.0	0.
4,796	959.1	0.0	959.1	1,862.3	55.9	37.
4,796	959.1	0.0	959.1	2,713.0	108.5	72
4,796	959.1	0.0	959.1	3,514.1	158.0	105
4,796	959.1	0.0	959.1	4,268.6	204.6	136
4,796	959.1	0.0	959.1	4,979.1		165
4,796	959.1	0.0	959.1	5,648.2	290.0	193
4,796	959 1	0.0	959.1	6,278.4	328.9	219
4,796	959.1	0.0	959.1			243
4,796	959.1	0.0			400.2	266
4,796	959.1	0.0			432.7	288
4,796	959.1	0.0	959.1		463.4	308
4,796	959.1	0.0	959.1	8,919.7	492.3	328
4,796	959.1	0.0	959.1	9,359.4		
4,796	959.1	0.0	959.1	9,773.4	545.0	363
4,796	959.1	0.0	959.1	10,163.4	569.2	379
4,796	959.1	0.0	959,1	10,530.6	591.9	394
4,796	959.1	0.0	959.1	10,876.4	613.3	408
4,796	959.1	0.0	959.1	Margar Mary Mary	633.4	422
4,796	959.1	0.0	959.1	11,508.9	652.4	434
4,796	959.1	0.0	959,1		670.2	446
4,796	959.1	0.0	959.1		687.0	458
4,796	959.1					468
- NO - 1000		0,0	959.1		702.9	
4,796 4,796	959.1 959.1	0.0	959.1		717.8	478 487
			959.1	12,794.5	731.9	
4,796	959.1	0.0	959.1		745.1	496
4,796	959.1	0.0	959.1	13,210.1	757.6	505
4,796	959.1	0.0	959.1	13,399.9	769.3	512
4,796	959.1	0.0	959.1	13,578,6	780.3	
4,796	959.1	0.0	959.1	13,747.0	790.8	527
4,796	959.1	0.0	959.1	13,905.5	800.6	533
4.796	959.1	0.0	959,1	14,054.8	809.8	539
4,796	959.1	0.0	959.1	14,195.4	818.5	545
4,796	959.1	0.0	959.1	14,327.9	826.7	551
4,796	959.1	0.0	959.1	14,452.6	834.4	556
4,796	959.1	0,0	959,1	14,570.0	841.7	561
4,796	959.1	0,0	959.1			565
4,796	959.1	0.0	959.1	14,784.8	854.9	570
4,796	959.1	0.0	959.1	14,882.9	861.0	574
4,796	959.1	0.0	959.1	14,975.3	866.7	577
4,796	959.1	0.0	959.1	15,062.3	872.1	581
4,796	959.1	0.0	959.1	15,144.2	877.2	584
4,796	959.1	0.0	959.1	15,221.4	881.9	588
4,796	959.1	0.0	959.1	15,294.1	886.4	
4,796	959.1	0.0	959.1	15,362.5	890.7	593
4,796	959.1	0.0	959,1	15,427.0	894.6	596
4.796	959.1	0.0	959.1	15,487.7		598
4,796	959.1	0.0	959.1	15,544.8	901.9	
4,796	959.1	0.0		15,598.7	905.3	
4,796	959.1	0.0	959.1	15,649.4	908.4	605
4,796	959.1	0.0		15,697.1	911.3	607

Scenario 1

735 736 736 737 737 738 738 738 738 738 738 738 738	73.5 73.5 73.5 73.5 73.5 73.5 73.5 73.5	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	73.5 73.5 73.5 73.5 73.5 73.5	73.5 140.0 200.2 254.6 303.9 348.5 388.8 425.3	0.0 7.0 13.3 19.0 24.2 28.9 33.2	0. 4. 8. 12. 16.
735 735 735 735 735 735 735 735 735 735	73.5 73.5 73.5 73.5 73.5 73.5 73.5 73.5	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	73.5 73.5 73.5 73.5 73.5 73.5 73.5 73.5	140.0 200.2 254.6 303.9 348.5 388.8 425.3	7.0 13.3 19.0 24.2 28.9	4, 8. 12. 16.
735 736 736 737 737 738 738 738 738 738 738 738 738	73.5 73.5 73.5 73.5 73.5 73.5 73.5 73.5	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	73.5 73.5 73.5 73.5 73.5 73.5 73.5 73.5	200.2 254.6 303.9 348.5 388.8 425.3	13.3 19.0 24.2 28.9	8. 12. 16.
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735 735 735 735 735 735 735 735 735 735	73.5 73.5 73.5 73.5 73.5 73.5 73.5 73.5	0.0 0.0 0.0 0.0 0.0 0.0	73.5 73.5 73.5 73.5 73.5	348.5 388.8 425,3	28.9	
735 735 735 735 735 735 735 735 735 735	73.5 73.5 73.5 73.5 73.5 73.5 73.5 73.5	0.0 0.0 0.0 0.0 0.0 0.0	73.5 73.5 73.5 73.5	388.8 425,3		19.
735 735 735 735 735 735 735 735 735 735	73,5 73.5 73.5 73.5 73.5 73.5 73.5 73.5 73.	0.0 0.0 0.0 0.0 0.0	73.5 73.5 73.5	425,3	33.2	
735 735 735 735 735 735 735 735 735 735	73.5 73.5 73.5 73.5 73.5 73.5 73.5 73.5	0.0 0.0 0.0	73.5 73.5			22
735 735 735 735 735 735 735 735 735 735	73.5 73.5 73.5 73.5 73.5 73.5 73.5	0.0 0.0 0.0	73.5		37.0	24
735 735 735 735 735 735 735 735 735 735	73.5 73.5 73.5 73.5 73.5 73.5	0.0		458.3	40.5	27
735 735 735 735 735 735 735 735 735 735	73.5 73.5 73.5 73.5 73.5	0.0	(Alana com	488.2		29
735 735 735 735 735 735 735 735 735 735	73.5 73.5 73.5 73.5		73.5	515.3	46.5	31
735 735 735 735 735 735 735 735	73.5 73.5 73.5		73.5	539.7	49.0	32
735 735 735 735 735 735 735 735	73.5 73.5	0.0	73.5	561.9	51.4	34
735 735 735 735 735 735 735 735	73.5 73.5	0.0	73.5	581.9	53,5	35
735 735 735 735 735 735 735 735 735 735		0.0	73.5	600.0	55.4	36
735 735 735 735 735 735 735 735 735 735		0.0	73.5	616.4	57.1	38
735 735 735 735 735 735 735 735		0.0	73.5	631.3	58.7	39
735 735 735 735 735 735 735 735 735 735	73.5	0.0	73.5	644.7	60.1	40
735 735 735 735 735 735 735 735	73.5	0.0	73.5	656.8	61,4	40
735 735 735 735 735 735 735 735 735 735	73.5	0.0	73.5	667.8	62.5	41
735 735 735 735 735 735 735 735	73.5	0.0	73.5	677.8	63.6	42
735 735 735 735 735 735 735 735	73.5	0.0	73.5	686.8	64.5	43
735 735 735 735 735 735 735 735 735 735	73.5	0.0	73.5	694.9	and the second s	43
735 735 735 735 735 735 735 735	73.5	0.0	73.5	702.3	66.1	44
735 735 736 735 735 735 735 735 735 735 735 735 735	73.5	0.0	73.5	709.0	66.8	44
735 736 735 735 735 735 735 735 735 735 735 735	73.5	0.0	73.5	715.0	67.5	45
735 735 735 735 735 735 735 735 735 735	73.5	0.0	73.5	720.5	68.0	45
735 735 735 735 735 735 735 735 735 735	73.5	0.0	73.5	725.4		45
735 735 735 735 735 735 735 735 735 735	73.5	0.0	73.5	729.9	69.0	46
735 735 735 735 735 735 735 735 735 735	73.5	0.0	73.5	733.9	69.5	46
735 735 735 735 735 735 735 735 735 735	73.5	0.0	73.5	737.6		46
735 735 735 735 735 735 735 735 735	73.5	0.0		740.9		46
735 735 735 735 735 735 735 735	73.5	0.0	73.5	743.9	70.5	47
735 735 735 735 735 735 735	73.5	0.0	73.5	746.6	70.8	47
735 735 735 735 735 735	73.5	0.0	73.5	749.0	71.0	47
735 735 735 735 735					71.3	
735 735 735 735	73.5	0.0	73.5	751.3		47 47
735 735 735	73.5	0.0	73.5 73.5	753.3 755.1	71.5	47
735 735	73.5		73.5		71.7 71.9	47
735	73.5	0.0	73.5	756.7 758.2	72.0	48
/33	73.5	0.0	73.5	759.6		48
	73.5		73,5	760.8		48
735	73.5	0.0	73,5	761.9		48
735	73.5	0.0	73.5	762.9	72.5	48
735	73.5	0.0	73.5	763,8	72.6	48
735	73,5		73.5	764.6		48
735	73.5		73.5	765.3	72.8	48
735		0.0			72.8	48
	73.5	0.0	73.5		72.9	
735 735		0.0	73.5 73.5	767.2 767.7	73.0 73.0	-48 -48

Scenario 1

1,218 1,218 1,218 1,218 1,218 1,218 1,218 1,218 1,218 1,218 1,218 1,218 1,218	255.8 255.8 255.8 255.8 255.8 255.8	(t) 0.0 0.0 0.0	DDOC _{m memalin} (t) 255.8 255.8	DDOC _{macoum T} (t) 255.8	DDOC _{m dessor T}	CH ₄ generated (t
1,218 1,218 1,218 1,218 1,218 1,218 1,218 1,218 1,218 1,218 1,218 1,218 1,218	255.8 255.8 255.8 255.8 255.8	0.0 0.0 0.0	255.8			- Strietmen it
1,218 1,218 1,218 1,218 1,218 1,218 1,218 1,218 1,218 1,218	255.8 255.8 255.8 255.8	0.0		255.8		
1,218 1,218 1,218 1,218 1,218 1,218 1,218 1,218 1,218 1,218	255.8 255.8 255.8	0.0	255.0		0,0	0.
1,218 1,218 1,218 1,218 1,218 1,218 1,218 1,218 1,218	255.8 255.8			504.0	7.6	5.
1,218 1,218 1,218 1,218 1,218 1,218 1,218 1,218	255.8	100	255.8	744.9	14.9	9.
1,218 1,218 1,218 1,218 1,218 1,218 1,218		0.0	255.8	978.7	22.0	14.
1,218 1,218 1,218 1,218 1,218 1,218		0.0	255.8	1,205.5	28.9	19.
1,218 1,218 1,218 1,218 1,218	255.8	0.0	255.8	1,425.7	35.6	23.
1,218 1,218 1,218 1,218	255.8	0.0	255.8	1,639.3	42.1	28.
1,218 1,218 1,218	255.8	0.0	255.8	1,846.6	48.4	32.
1,218 1,218	255.8	0.0	255,8	2,047.8	54,6	36
1,218	255.8	0.0	255.8	2,243.1	60.5	40.
1,218	255.8	0.0	255.8	2,432.6	66.3	44
	255.8	0.0	255.8	2,616.5	71.9	47
1,218	255.8	0.0	255.8	2,794.9	77,3	51
1,218	255.8	0.0	255.8	2,968.1	82.6	55.
1,218	255.8	0.0	255.8	3,136.2	87.7	- 58
1,218	255.8	0.0	255.8	3,299.3	92.7	61
1,218	255.8	0.0	255.8	3,457.5	97.5	
1,218	255.8	0.0	255.8	3,611.1	102.2	68
1,218	255.8	0.0	255.8	3,760,2	106.7	71.
1,218	255.8	0.0	255.8	3,904.8	111.1	74
1,218	255.8	0.0	255.8	4,045.2	115.4	76
1,218	255.8	0.0	255.8	4,181.4	119.6	79
1,218	255.8	0.0	255.8	4,313.6	123.6	82
	255.8	0.0	255.8	4,441.9	127.5	85
1,218 1,218	255.8	0.0	255.8	4,566.4	131.3	87.
1,218	255.8	0.0	255.8	4,687.2	135.0	90
1,218	255.8	0.0	255.8	4.804.5	138.5	92
1,218	255.8	0.0	255.8	4,918.3	142.0	94
1,218	255.8	0.0	255.8	5,028.7	145.4	
1,218	255.8	0.0	255.8	5,135.9	148.6	99
1,218	255.8	0.0	255.8	5,239.9	151.8	101
1,218	255.8	0.0	255,8	5,340.8	154.9	103
1,218	255.8	0.0	255.8	5,438.7	157.8	
1,218	255.8	0.0	255.8	5,533.7	160.7	107
1,218	255.8	0.0	255.8	5,626.0	163.5	109
1,218	255.8	0.0	255.8	5,715.5	166.3	110
1,218	255.8	0.0	255.8	5,802.4	168.9	112
1,218	255.8	0.0	255.8	5,886.6	171.5	114
1,218	255.8	0.0	255.8	5,968.4	174.0	116
1,218	255.8	0.0	255.8	6,047.8	176.4	117
1,218	255.8	0.0	255.8	6,124.9	178.7	119
1,218	255.8	0.0	255.8	6,199.6		120
1,218	255.8	0.0	255.8	6,272.2	183.2	122
1,218	255.8	0.0	255.8	6,342.6		123
1,218	255.8	0.0	255.8	6,410.9	187.5	125
1,218	255.8	0,0	255.8	6,477.2		126
1,218	255.8	0.0	255.8	6,541.6	191.4	127
1,218	255.8	0.0	255.8	6,604.0	193.3	
1,218	255.8		255.8	6,664.6	195.2	
1,218	255.8	0.0	255.8	6,723.4	197.0	131
1,218	255.8			6,780.5		

Scenario 1

			Textiles			
CH ₄ generated	DDOC _{rty accom; ₹} (t)	DDOG _{m account}	DDOC _{m-remain}	DDOC _{m dettern} (t)	DDOC _{mdeo} (t)	waste (t)
	0.0	37.4	37.4	0.0	37.4	312
	2.2	72.7	37.4	0,0	37.4	312
2	4.2	105.9	37.4	0,0	37.4	312
. 4	6.2	137.2	37.4	0.0	37.4	312
5	8.0	166.6	37.4	0.0	37.4	312
6	9.7	194.4	37.4	0.0	37.4	312
7	11.3	220.5	37.4	0.0	37.4	312
8	12.8	245.1	37.4	0.0	37.4	312
9	14.3	268.3	37.4	0.0	37.4	312
10	15.6	290.1	37.4	0.0	37.4	312
11	16.9	310.6	37.4	0.0	37.4	312
12	18.1	330.0	37.4	0.0	37.4	312
12	19.2	348.2	37.4	0.0	37.4	312
13	20.3	365.4	37.4	0.0	37.4	312
14	21.3	381.5	37.4	0.0	37.4	312
14	22.2	396.7	37.4	0.0	37.4	312
15	23.1	411.1	37.4	0.0	37.4	312
16	23.9	424.6	37.4	0.0	37.4	312
16	24.7	437.3	37.4	0.0	37.4	312
17	25.5	449.3	37.4	0.0	37.4	312
17	26.2	460.5	37.4	0.0	37.4	312
17	26.8	471.2	37.4	0.0	37.4	312
18	27.4	481.2	37.4	0.0	37.4	312
18	28.0	490.6	37.4	0.0	37.4	312
19	28.6	499.5	37.4	0.0	37.4	312
19	29.1	507.8	37.4	0.0	37.4	312
19	29.6	515.7	37.4	0.0	37.4	312
20	30.0	523.1	37.4	0.0	37.4	312
20	30.5	530.1	37.4	0.0	37.4	312
20	30.9	536.6	37.4	0.0	37.4	312
20	31.3	542.8	37,4	0.0	37.4	312
21	31.6	548.7	37.4	0.0	37.4	312
21	32.0	554.1	37.4	0.0	37.4	312
21	32.3	559.3	37.4	0.0	37.4	312
21	32.6	564.2	37.4	0.0	37.4	312
21	32.9 33.1	568.8	37.4 37.4	0.0	37.4 37.4	312 312
	33.4	573.1 577.1	37.4			312
22	33.6	581.0	37.4	0.0	37.4	312
	33.8	584.6	37.4	0.0		312
22						312
22	34.0 34.2	588.0 591.2	37.4 37.4	0.0	37.4	312
					37.4	312
	(In all 1) and (In all 1)	594.2	37.4	0.0	37.4	
23	34.6	597.0	37.4	0.0	37.4	312
23	34.8	599.7	37.4	0.0	37.4	312
23	34.9	602,2	37,4	0.0	37.4	312
23	35.1	604.6	37.4	0.0	37.4	312
23	35.2	606.8	37.4	0.0	37.4	312
	35.3	608.9	37.4	0.0		312
23	35.5	610.9	37.4	0.0	37.4	312
23	35.6	612.8	37.4	0.0	37.4	312

Scenario 1

			Sludges			
vaste (t)	DDOC _{in dep} (t)	DDOC _{m decom}	DDOC _{int repression}	DDOC _{m ecoum 1} (t)	DDOC _{m decarroT}	CH _{4 generales} (t
189	4.7	0.0	4.7	4.7	0.0	0.0
189	4.7	0.0	4.7	8.7	0.8	0.5
189	4.7	0.0	4.7	11.9	1.5	1.
189	4.7	0.0	4.7	14.6	2.0	1.3
189	4.7	0.0	4.7	16.9	2.5	1.0
189	4.7	0.0	4.7	18.8	2.9	1
189	4.7	0.0	4.7	20.3	3.2	2.
189	4.7	0.0	4.7	21.6	3.4	2.
189	4.7	0.0	4.7	22.7	3.6	2.
189	4.7	0.0	4.7	23.6	3.8	2.
189	4.7	0.0	4.7	24.3	4.0	2,
189	4.7	0.0	4.7	24.9	4.1	2.
189	4.7	0.0	4.7	25.5	4.2	2.
189	4.7	0.0	4.7	25.9	4.3	2.
189	4.7	0.0	4.7	26.2	4.4	2.
189	4.7	0.0	4.7	26.5	4.4	3.0
189	4.7	0.0	4.7	26.8	4.5	3.
189	4.7	0.0	4.7	27.0	4.5	3.
189	4.7	0.0	4.7	27.1	4.6	3,
189	4.7	0.0	4.7	27.3	4.6	3.
189	4.7	0.0	4.7	27.4	4.6	3.
189	4.7	0.0	4.7	27.5	4.6	3.
189	4.7	0.0	4.7	27.6	4.6	3,
189	4.7		4.7	27.6	4.7	-3,
189	4.7	0.0	4.7	27.7	4.7	3.
189	4.7	0.0	4.7	27.7	4.7	3.
189	4.7	0.0	4.7	27.8	4.7	3.
189	4.7	0.0	4.7	27.8	4.7	3.
189	4.7	0.0	4.7	27.8	4.7	3.
189	4.7	0.0	4.7	27.9	4.7	3
189	4.7	0.0	4.7	27.9	4.7	3.
189	4.7	0.0	4.7	27.9	4.7	3.
189	4.7	0.0	4.7	27.9	4.7	3.
189	4.7	0.0	4.7	27.9	4.7	3.
189	4.7	0.0	4.7	27.9	4.7	3.
189	4.7	0.0	4.7	27.9	4.7	3.
189	4.7	0.0	4.7	27.9	4.7	3.
189	4.7	0.0	4.7	28.0	4.7	3,
189	4.7	0.0	4.7	28.0	4.7	3.
189	4.7	0.0	4.7	28.0	4.7	3.
189	4.7	0.0	4.7	28.0	4.7	3.
189	4.7	0.0	4.7	28.0	4.7	3.
189	4.7	0.0	4.7	28.0	4.7	
189	4.7	0.0	4.7	28.0	4.7	3.
189	4.7	0.0	4.7	28.0	4.7	3.
189	4.7	0.0	4.7	28.0	4.7	3.
189	4.7			28.0	4.7	3.
189	4.7	0.0		28.0	4.7	
189	4.7	0.0	4.7	28.0	4.7	
189	4.7	0.0	4.7	28.0	4.7	
189		0.0		28.0	4.7	

Scenario 1

			Nappies	2.2		
CH _{4 generated}	DDOC _{midenorr} T (t)	DDOC _{m annum T}	DDOC _{m remain} (t)	DDOC _{m secon}	$DDOC_{mideo}(t)$	waste (t)
	0.0	33.5	33.5	0.0	33.5	279
	1.9	65.0	33.5	0.0	33.5	279
	3.8	94.7	33.5	0.0	33.5	279
3	5.5	122.7	33.5	0.0	33.5	279
4	7.1	149.0	33.5	0.0	33,5	279
	8.7	173.8	33.5	0.0	33.5	279
	10.1	197.2	33.5	0.0	33.5	279
	11.5	219.2	33.5	0.0	33.5	279
	12.8	239.9	33.5	0.0	33.5	279
	14.0	259.4	33.5	0.0	33.5	279
	15.1	277.8	33.5	0.0	33.5	279
	16.2	295.1	33.5	0.0	33,5	279
	17.2	311.4	33.5	0.0	33.5	279
	18.1	326.7	33.5	0.0	33.5	279
	19.0	341.2	33.5	0.0	33.5	279
	19.9		33.5	0.0	33.5	279
		354.8				
	20.7	367.6	33.5	0.0	33.5	279
	21.4	379.7	33.5	0.0	33.5	279
	22.1	391.0	33.5	0.0	33.5	279
	22.8	401.7	33.5	0.0	33,5	279
	23.4	411.8	33.5	0.0	33.5	279
	24.0	421.3	33.5	0.0	33.5	279
	24.5	430.3	33.5	0.0	33.5	279
	25.1	438.7	33.5	0.0	33.5	279
	25.5	446.6	33.5	0.0	33,5	279
17	26.0	454.1	33.5	0.0	33.5	279
17	26.4	461.1	33.5	0.0	33,5	279
17	26.9	467.8	33.5	0.0	33.5	279
	27.2	474.0	33.5	0.0	33.5	279
	27.6	479.9	33.5	0.0	33.5	279
	27.9	485.4	33.5	0.0	33.5	279
	28.3	490.6	33.5	0.0	33.5	279
	28.6	495.5	33.5	0.0	33.5	279
	28.9	500.2	33.5	0.0	33,5	279
	29.1	504.5	33.5	0.0	33.5	279
	29.4	508.6	33.5	0.0	33.5	279
	29.6	512.5	33.5	0.0	33.5	279
	29.8	516.1	33.5	0.0	33.5	279
	30.1	519.5	33.5	0.0	33.5	279
	30.3	522.8	33.5		33.5	279
				0.0		
	30.4	525.8	33.5	0.0	33,5	279
	30.6	528.7	33.5	0.0	33,5	279
	30.8	531.3	33.5	0.0	33,5	279
	30.9	533.9	33.5	0.0	33.5	279
	31.1	536.3	33.5	0.0	33.5	279
	31.2	538.5	33.5	0.0	33.5	279
	31.4	540.6	33.5	0.0	33.5	279
	31.5	542.6	33.5	0.0	33.5	279
	31.6	544.5	33.5	0.0	33.5	279
	31.7	546,3	33.5	0.0	33.5	279
	31.8	548.0	33.5	0.0	33.5	279

Scenario 1

			Rubber			
CH4 generaled	DDOC _{m classor} r (t)	DDOC _{maccum} T	DDOC _{m remain}	DDOC _{m delaore}	DDOC _{mdeo} (t)	waste (kt)
0	0.0	12.3	12.3	0.0	12.3	63
0	0.7	23.9	12.3	0.0	12.3	63
0	1.4	34.8	12.3	0.0	12.3	63
1	2.0	45.0	12.3	0.0	12.3	63
1	2.6	54.7	12.3		12.3	63
2	3.2	63.8	12,3	0.0	12.3	63
2	3.7	72.3	12.3	0.0	12.3	63
2	4.2	80.4	12.3	0.0	12.3	63
3	4.7	88.0	12.3	0.0	12.3	63
3	5.1	95.2	12.3	0.0	12.3	63
3	5.5	101.9	12.3	0.0	12.3	63
4	5.9	108.3	12.3	0.0	12.3	63
4	6.3	114.3	12.3	0.0	12.3	63
4	6.7	119.9	12.3	0.0	12.3	63
4	7.0	125.2	12.3	0.0	12.3	63
4	7.3	130.2	12.3	0.0	12.3	63
5	7.6	134.9	12.3	0.0	12.3	63
5	7.9	139.3	12.3	0.0	12.3	63
	8.1	143.5	12.3	0.0	12.3	63
5						
. 5	8.4	147.4	12.3	0.0	12.3	63
5	8.6	151.1	12.3	0.0	12.3	63
5	8.8	154.6	12.3		12.3	63
6	9.0	157.9	12,3	0.0	12.3	63
6	9.2	161.0	12,3	0.0	12.3	63
- 6	9.4	163.9	12.3	0.0	12.3	63
6	9,5	166.6	12,3	0.0	12,3	63
6	9.7	169.2	12.3	0.0	12.3	63
6	9.9	171.6	12.3	0.0	12.3	63
6	10.0	173.9	12.3	0.0	12,3	63
6	10.1	176.1	12.3	0.0	12.3	63
6	10.3	178.1	12.3	0.0	12.3	63
6	10.4	180.0	12.3	0.0	12.3	63
7	10.5	181.8	12.3	0.0	12.3	63
7	10.6	183.5	12.3	0.0	12.3	63
7	10.7	185.1	12.3	0.0	12.3	63
7	10.8	186.6	12.3			63
7	10.9	188.0	12.3		12.3	63
7	11.0	189.4	12.3		12.3	63
7	11.0	190.6	12.3		12.3	63
7	11.1	191.8	12.3	0.0	12.3	63
7	11.2	192.9	12.3	0.0	12.3	63
7	11.2	194.0	12.3	0.0	12.3	63
7	11.3	195.0	12.3	0.0	12.3	63
7	11.4	195.9	12.3		12.3	63
7	11.4	196.8	12.3	0.0	12.3	63
7	11.5	197.6	12.3	0.0	12.3	63
7	11.5	198.4	12.3	0.0	12.3	63
7	11.6	199.1	12.3		12.3	63
7	11.6	199.8	12.3	0.0	12.3	63
7.	11.6	200.5	12.3	0.0	12.3	63
7	11.7	201.1	12,3	0.0	12.3	63

Scenario 1

Total CH4	Me	than recovere	d	Carrier No.	1.5	A. 57.
Generated (f)	Q _{cap} (m ³)	Q _{flared} (m ³)	$\Omega_{tr}(m^3)$	CH ₄ * (t)	E	Ej (t CO ₂ -e)
0.0	0	0	-0	0.0	0.0	0.0
64.1	0	0	0	64.1	57.7	1211.
122.9	0	0	0	122.9	110.6	2322.
177.0	0	0	0	177.0	159.3	3344.
226.8	0	0	0	226.8	204.2	4287.
272.9	0	0	0	272.9	245.6	5158.
315.6	0	0	0	315.6	284.0	5964.
355.2	0	0	0	355.2	319.7	6712.
392.0	0	0	0	392.0	352,8	7408.
426.3	0	0	0	426.3	383.6	8056.
458.2	0	0	0	458.2	412.4	8660.
488.1	0	0	0	488.1	439,3	9224.
516.0	0	0	0	516.0	464.4	9751.
542.1	0	0	0	542,1	487.9	10245.
566.6	0	0	Ö	566,6	509.9	10708.
589.6	0	0	0	589.6	530.6	11142.
611.1	0	0	0	611.1	550.0	11550.
631.4	0	0	0	631.4	568.3	11933.
650.5	0	0	0	650.5	585.4	12294.
668.4	. 0	0	0	668.4	601.6	12633.
685.3	0	0	0	685.3	616.8	12953.
701.3	0.	0	0	701.3	631.1	13254.
716.3	0.	0	0	716.3	644.7	13538.
730.5	0	0	0	730.5	657.4	13805.
743.8	0	0	0	743.8	669.5	14058.
756.5	0	0	0	756,5	680.8	14297
768.4	0	0	0	768.4	691.6	14522.
779.7	0	0	0	779.7	701.7	14735.
790.3	0	0	0	790.3	711.3	14937.
800.4	0	0	0	800.4	720.4	15127.
809.9	0	0	0	809,9	728.9	15307.
819.0	0	0	0	819.0	737.1	15478.
827.5	0	0	0	827.5	744.8	15639.
835.6	0	0	0	835.6	752.0	15792.
843.3			0	843.3	758.9	
850.5	0	0	.0	850.5	765.5	
857.4	0	0	0	857.4	771.7	16204.
863.9	0	0	.0	863.9 870.1	777.5	
870.1 876.0	0	0	0	876.0	783.1 788.4	16445. 16556.
	0	0	0	881.5	793.4	16661.
881.5						
886.8 891.8	0	0	0	886.8 891.8	798,1	16761. 16855.
896.6	0	0	0	896.6	802,7 806.9	
901.1	0	0	0	901.1	811.0	
901.1	0	0	0	905.4	814.9	And the second second second
909.5	0	0	0	909.5	818.6	17112.
913.4	0	0	0	913.4	822.0	17169.
917.1	0	0	0	917.1	825.4	17332
920.6	0	Õ	0	920.6	828.5	
923.9		0	0	923.9	831.5	
525.9	· ·	, o	Ų.	320.5	951.5	641,62

41,622 Total

irst 10 Years of simula	tion	Notes on Calculations	Remaining 40 years of simulation	
NSW waste streams	×	Purple cells	NSW waste streams	%
funishal (M)	319	31% Assume 85% of waste is diverted be new value is 15% of original	Municipal (M)	31%
ommercial &. idustrial (C&D)	429	Green cells	Commercial & Industrial (C&D)	42%
onstruction & emolition (C&I)	279	Adjusted % for each waste type, calculated as per formula on	Construction & Demoirron (C&I)	27%
ital	1009	6 0.252 of 2009 technical guidelines	total	10086

waste mix type	(%) W	C&I (%)	C&D (%)
Food	5.3%	3.2%	0.0%
Paper & paper board	2.0%	2.3%	0.536
Garden & Park	Z 5%	89'0	0.3%
Wood & wood waste	0.2%	1.9%	张670
Textiles	佐丁サ	7.6%	800
Sludge	9500	3,0%	0.01%
Nappees	0.6%	0.0%	0.0%
Rubber & Leather	7.6%	6.9%	0.038
Concrete, metal, plastic and glass	82.2%	78.2%	38.8%
total	36001	100%	9600I

Waste composition	M (%)	C&I (%)	C&D (%)	total (%)
Food	3%	136	0.0%	388
Paper & paper board	1%	13%	0%0	758
Garden & Park	1%	960	0%0	138
Wood & wood waste	900	128	05%	188
Hiller	1%	386	OW6	285
den	86	*F	0%	18
opies	8	%6	008	8
Rubber & Leather	13%	3%	260	88
orrete, metal, plastic and glass	25%	31%	27%	83%
In the second	31%	42%	27%	100%

vaste composition	(%) W	C&I (%)	C8D (%)	(%) letot
por	9611	966	960	30%
per & paper board	4%	1986	138	138
Inden & Park	36	238	1%	8K.
and & wood waste.	360	265	2%	22
xtiles	※0	2%	860	298
udbo	960	28	Ko.	198
apples	17%	80	860	158
ubber & Leather process, metal,	6	138	Dy	2%
astic and glass	366	16%	24%	48%
121	31%	42%	27%	100%

waste mix type	DOC	K
Food	0.15	0.185
Paper & paper	0.4	0.06
Garden & green	0.2	0.1
Wood	0.42	0.03
Textiles	0.24	0.06
Sludge	0.05	0,185
Nappies	0.24	0.06
Rubber & Leather	0.39	0.06
Concrete, metal, plastics & glass	0	0

Parameters 4 8 1

DOC	0.5
M	13 M=7 means no delay; M=13 means 6 months delay; normally 0-6
F	0.5
MCF	1.0
Y	0.0142464
OF	0.1

Scenario 2

				Food			
Year	waste (I)	DDOC _{miclep} (t)	DDOC _{m decom}	DDOC _{m remein}	DDOC _{m accom T}	DDOC _{m decom 7}	CH _{4 generated} (
1	2,982	223.7	0.0	223.7	223.7		
2	2,982	223.7	0.0	223.7		37.8	25.
3	2,982	223.7	0.0	223.7	564.0	69.2	46.
4	2,982	223.7	0,0	223.7	692.4	95,3	63.
5	2,982	223.7	0,0	223.7	799.1	116.9	78.
6	2,982	223.7	0.0	223.7			
7	2,982	223.7	0.0	223.7	961.5		
8			0.0	223.7			
9	2,982	223.7	0.0	223.7		172.7	
10		223.7		223.7			
11		33.5	0.0	33.5			
12		33.5	0.0	33.5			
13		33.5	0.0	33.5			
14		33.5	0.0	33.5			
15		33.5	0.0	33.5			
16		33.5	0.0	33.5			
17		33.5	0.0				
18		33.5	0.0	33.5			
19		33.5	0.0	33.5			
20							
		33.5	0.0	33.5			
21	447	33.5	0.0	33.5			
22	447	33.5	0,0	33.5			
23	447	33.5	0,0	33.5			
24		33.5	0.0	33.5			
25		33.5	0,0	33.5			
26		33.5	0.0	33.5			
27		33.5	0.0	33.5			
28	447	33.5	0.0				
29		33.5	0.0	33.5			
30		33.5	0.0	33.5	221.3	38.2	25
- 31		33.5	0.0	33.5	217.5	37.4	24
32	447	33.5	0.0	33.5	214.3	36.7	24
33		33.5	0.0	33.5	211.6	36,2	24
34	447	33.5	0.0	33.5	209.4	35.7	23
35	447	33.5	0.0	33.5	207.6		
36		33.5	0.0	33.5		35.1	
37		33,5	0.0	33.5			
38		33.5	0.0	33.5			
39			0.0	33.5			
40			0.0	33.5			
41				33.5			
42							
43	447						
44			0.0				
45							
46							
47		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.0				
48			0.0				
49				33.5			
50			0.0	33.5			
51	447	33.5	0,0	33.5	199.1	33.6	22

Scenario 2

		Pap	er & Paper B	V		
waste (t)	DDOC _{m/dep} (t)	DDOC _{m denom}	DDOC _{myemein}	DDOC _{maccount} T	DDOC _{m decom T} (t)	CH _{4 generated} (
1,703	340.5	0.0	340.5	340.5	0.0	0.
1,703	340.5	0.0	340.5	661.2	19.8	13.
1,703	340.5	0.0	340.5		38.5	
1,703		0.0	340.5		56.1	37.
1,703						
1,703		0.0	340.5		88.3	
1,703			340.5		102.9	
1,703			340.5	2000	116.8	
1,703		0.0	340.5		129.8	
1,703		0.0	340.5		142.1	94.
255		0.0	51.1	L. O. Sec. 120	153.6	
255		0.0	51.1		147.7	
255		0.0	51.1		142.0	
255		0.0	51.1		136.7	
255		0.0	51.1		131.7	
255		0.0	51.1		127.0	84.
255		0.0	51.1		122.6	
255		0.0	51.1	to the second se	118.5	
255		0.0	51.1		114.5	76.
255		0.0	51,1	1,843.5	110.8	
255		0.0	51.1	1,787.2	107.4	71.
255		0.0	51.1	1,734.2	107.4	69.
255						67.
255	6.1.175	0.0	51.1 51.1		101.0	65.
255		0.0			98.1	
		0.0	51.1		95.3	
255		0.0	51.1		92,8	
255	1 march 1 marc	0.0	51,1		90.3	
255		0.0	51.1		88.1	58.
255		0.0	51.1			
255		0.0			83.9	
255	7-5, 5.71	0.0	51.1		82.0	
255	7 -40,70 1,70	0.0	51.1	The state of the s	80.2	
255		0.0	51.1		78.5	52.
255	and the second s	0.0		and the second second	76.9	
255		0.0	51,1	1,270.0	75.4	50,
255		0.0	51.1			49.
255		0.0	51.1		72.6	
255		0.0			71.4	
255		0.0			70.2	
255		0.0	51.1		69.1	46.
255			51.1			
255			51.1			
255			51.1		66.1	44.
255			51.1		65.2	
255		0.0	51.1		64.4	42.
255		0.0	51.1		63.6	
255		0.0	51.1			
255		0.0	51.1			41.
255		0.0	51.1	1,046.7		
255		0.0			61.0	
255	51.1	0.0	51.1	1,027.5	60.4	40.

Scenario 2

		G	arden & Gree	mremein DDOC _{m sooum T} DDOC _{m decom T} CH. (b)				
waste (t)	DDOC _{m dep} (t)	DDOC _{m decem}	DDOC _{m remain}	DDOC _{m scoum T} (t)	DDOC _{m decom T} (t)	CH _{4 generated} (
1,100	110.0	0.0	110.0	110.0	0.0	0.		
1,100	110.0	0.0	110.0	209.6	10.5	7.		
1,100	110.0	0.0	110.0	299.7	19.9	13:		
1,100	110.0	0.0	110.0	381.2	28.5	19.		
1,100	110.0	0.0	110.0	454.9	36.3	24.		
1,100	110.0	0.0	110.0	521.7	43.3	28.		
1,100	110.0	0.0	110.0	582.0	49.6	33.		
1,100	110.0	0.0	110.0	636.7	55.4	36.		
1,100	110.0	0.0	110.0	686,1	60.6	40.		
1,100	110,0	0.0	110.0	730.8	65,3	43.		
165	16,5	0.0	16.5	677.8	69,5	46		
165	16,5	0.0	16.5	629.8	64.5	43		
165	16.5	0.0	16.5	586.4	59.9	40		
165	16.5	0.0	16.5	547.1	55.8	37		
165	16.5	0.0	16.5	511.5	52.1	34		
165	16.5	0.0	16.5	479.3	48.7	32		
165	16.5	0.0	16.5	450.2	45.6	30		
165	16.5	0.0	16.5	423.9	42.8	28		
165	16.5	0.0	16.5	400.1	40.3	26		
165	16,5	0.0	16,5	378.5	38.1	25		
165	16.5	0.0	16.5	359.0	36.0	24		
165	16.5	0.0	16.5		34.2	22		
165	16.5	0.0	16.5		32.5	21		
165	16.5	0.0	16.5		31.0	20		
165	16.5	0.0	16.5	297.8	29.6			
165	16,5	0.0	16.5		28.3	18		
165	16.5	0.0	16.5		27.2	18		
165	16.5	0.0	16,5		26.2	17		
165	16.5	0.0	16.5		25.3	16		
165	16.5	0.0	16.5		24.4	16		
165	16.5	0.0	16.5		23.7	15		
165	16.5	0.0	16.5		23.0	15		
165	16.5	0.0	16.5		22.4	14		
165	16.5	0.0	16.5		21.8	14		
165	16.5	0.0	16.5		21.3	14		
165	16.5	0.0	16.5		20.9			
165	16.5	0.0	16.5		20.4	13		
165	16.5	0.0	16.5		20.1	13		
165	16.5	0.0	16.5		19.7	13		
165	16.5	0.0			19.4	12		
165	16.5	0.0	16.5	8.01.444	19.1	12		
165	16.5		16.5		18.9	12		
165	16.5	0.0	16.5		18.7			
165	16.5	0.0	16.5		18.5			
165	16.5	0.0			18.3	12		
165								
165	16.5	0.0	16.5		18.1	12		
165	16.5	0.0	16.5		18.0	12		
165	16.5	70.7.2	16.5		17.8			
165	16,5 16,5	0.0	16.5		17.7			
100	16.5	0.0	16.5	183.6	17.6	11		

Scenario 2

			Wood			
waste (t)	DDOC _{mides} (t)	DDOC _{m decom}	DDOC _{m remain}	DDOC _{m accum T}	DDOC _{m:decom T}	CH _{d generated} (
1,077	226.2	0.0	226.2	226.2	0.0	0.
1,077	226.2	0.0	226.2	445.7	6.7	4.
1,077	226.2	0.0	226.2		13.2	8.
1,077	226.2	0.0	226.2		19.5	
1,077	226.2	0.0	226.2		25.6	17.
1.077	226.2	0.0	226.2		31.5	21.
1,077	226.2	0.0	226.2		37.3	
1,077	226.2	0.0	226.2	1,632.9	42.8	
1,077	226.2	0.0	226.2		48.3	32.
1,077	226.2	0.0	226.2		53.5	35.
162		0,0	33.9	20.00	58.6	
162		0.0	33.9		57.9	
162		0.0			57.2	
162		0.0	33.9		56.5	
162		0.0			55.8	37
162		0.0	33.9		55.2	36
162	33.9	0.0	33.9		54.6	
162	10° A.1.1.1.	0.0	33.9		53.9	36
162		0.0	33.9		53.4	35
162		0.0	33,9		52.8	
162		0.0	33.9		52.2	34
162		0.0	33.9	1.00	51.7	
162		0.0	33.9		51.2	34
162		0.0	33.9		50.6	33
162			33.9		50.2	33
162		0.0	33,9	the second secon	49.7	33
162		0.0	33.9		49.2	32
162		0.0			48.8	32
162		0.0	33.9			32
162		0.0	33.9		47.9	31
162		0.0	33.9		47.5	31
162		0.0	33.9		47.1	31
162		0.0	33.9		46.7	31
162		0.0			46.3	30
162		0.0			45.9	
162		0.0	33.9		45.6	
162		0.0	33,9		45.2	
162		0.0	33,9		44.9	29
162		0.0	33.9		44.6	
162		0.0	33.9		44.3	
162	1 CA 1 1 CA	0.0				29
162		0.0			43.7	
162		0.0				
162		0.0			43.1	28
162		0.0				
						28
162		0.0	33.9			
162		0.0	33.9		42.3	28
162			33.9		42.1	28
162					41.8	
162						
162	33.9	0.0	33,9	1,392.1	41.4	27

Scenario 2

			Textiles			
waste (t)	DDOC _{midep} (t)	DDOC _{m decom}	DDOC _{m remain}	DDOC _{m secoum T} (t)	DDOC _{in decoin T}	CH _{4 generated} (
322	38.6	0.0	38.6	38,6	0.0	0.
322	38.6	0.0	38.6	75.0	2.2	1.
322	38.6	0.0	38.6	109.2	4.4	2.
322	38.6	0.0	38.6		6.4	4.
322	38.6	0.0	38.6		8.2	
322	38.6	0.0	38.6		10.0	
322	38.6	0.0	38.6		11.7	7.
322	38.6	0.0	38.6		13.2	8
322	38.6				14.7	
322	38.6	0.0	38.6		16.1	10
703	84.4	0.0	84.4		17.4	11.
703	84.4	0.0	84.4		21.3	14
703	84.4	0.0	84.4		25.0	16.
703	84.4	0.0	84.4	1 1 6 1011	28,5	19
703	84.4	0.0	84.4		31.7	21
703	84.4	0.0	84.4		34.8	23.
703	84.4	0.0	84.4		37.7	25
703	84.4	0.0	84.4		40.4	26
703	84.4		84.4			
	84.4	0.0	84.4		43.0	
703		0.0			45.4	30
703	84.4	0.0			47.6	
703	84.4	0.0			49.8	
703	84.4	0.0	84.4		51.8	34
703	84.4	0.0	84.4		53.7	35
703	84.4	0.0	84.4		55.5	
703	84.4	0.0	84.4	W 4.7 12 10 10 1	57.2	38
703	84.4	0.0	84.4	W - W - W - W - W - W - W - W - W - W -	58.8	
703	84.4	0.0	84.4	WW. 11 7 7 8 10 10	60.2	40
703	84.4	0.0	84.4	1,081,4	61.7	41
703	84.4	0.0	84.4	1,102.8	63.0	
703	84.4	0.0	84.4	1,123.0	64.2	42
703	84.4	0.0	84.4	1,142.0	65.4	43
703	84.4	0.0	84.4	1,159.9	66.5	44
703	84.4	0.0	84.4	1,176.7	67.5	45
703	84.4	0.0	84.4	1,192.6	68.5	45
703	84.4	0.0	84.4	1,207.5	69.5	46
703	84.4	0.0	84.4		70.3	46
703	84.4	0.0	84.4		71.1	47
703	84.4	0.0	84.4		71.9	
703	84.4	0.0			72.6	48
703	84.4	0.0	84.4		73.3	
703	84.4	0.0	84.4		74.0	
703	84.4	0.0	84.4	1.70-5-7 8 9 - 1		49
703	84.4	0.0	84.4	AMERICAN T	75.1	50
703	84.4	0.0	84.4		75.7	50
703	84.4	0.0	84.4		76.2	50
703	84.4	0.0	84.4			51
	84.4		84.4		76.7	51
703		0.0			77.1	
703	84.4	0.0	84.4		77.5	
703	84.4	0.0	84.4		77.9	
703	84.4	0.0	84.4	1,350.9	78.3	52

Scenario 2

		DDOC _{m-decom} DDOC _{m-remein} DDOC _{m-acculin T} DDOC _{m-acculin T} DDOC _{m-acculin T} CH _{d-peneralise} (t)					
waste (t)	DDOC _{m dep} (t)	DDOC _{m decom}	DDOC _{n remain}	DDOC _{macculm T}	DDOC _{m decom 1}	CH _d penerated (
95	2.4	0.0	2.4		0.0	0.	
95		0.0	2.4		0.4		
95	2.4		2.4		0.7	0.	
95	2.4	0.0	2.4		1.0		
95	2.4	0.0	2.4	8.4	1.2		
95	2.4	0.0	2.4	9.4	1.4		
95	2.4	0.0	2.4		1.6		
95	2.4	0.0	2.4	10.8	1.7		
95	2.4	0.0	2.4	11.3	1.8		
95	2.4	0.0	2,4		1.9		
187	4.7	0.0	4.7		2.0		
187	4.7	0.0	4.7		2.4		
187	4.7	0.0	4.7		2.8		
187	4.7	0.0	4.7	20.1	3.1		
187	4.7	0.0	4.7	21.4	3.4	2,	
187	4.7	0.0	4.7	22.4	3.6		
187	4.7	0.0	4.7	23.3	3.8		
187	4.7	0.0	4.7	24.1	3.9		
187	4.7	0.0	4.7	24.7	4.1	2.	
187	4.7	0.0	4.7	25.2	4.2		
187	4.7	0.0	4.7	25.6	4.3		
187	4.7	0.0	4.7	25.9	4.3		
187	4.7	0,0	4.7	26.2	4.4		
187	4.7	0.0	4.7	26.5	4.4		
187	4.7	0.0	4.7	26.7	4.5		
187	4.7	0.0	4.7		4.5		
187	4.7	0.0	4.7		4.5		
187	4.7	0.0		27.1	4.6		
187	4.7	0.0	4.7	27.2	4.6		
187	4.7	0.0	4.7	27.3	4.6		
187	4.7	0.0	4.7	27.3			
187	4.7	0.0	4.7	27.4	4.6		
187	4.7	0.0	4.7	27.4	4.6		
187	4.7	0.0			4.6		
187	4.7	0.0	4.7		4.6		
187	4.7	0.0	4.7				
187	4.7	0,0	4.7				
187	4.7	0,0	4.7				
187	4.7	0.0	4.7				
187	4.7	0.0	4.7				
187	4.7	0.0	4.7	27.6			
187	4.7	0.0			4.7	3.	
187	4.7		4.7	27.6	4.7		
187	4.7		4.7	27.6			
187	4.7	0.0	4.7				
187	4.7	0.0	4.7				
187	4.7	0.0	4.7	27.7	4.7		
187	4.7	0.0	4.7		4.7		
187	4.7	0.0	4.7		4.7		
187		0.0	4.7		4.7		
187	4.7	0.0	4.7		4.7		

Scenario 2

			Nappies	DDOC _{m account} DDOC _{m decom} CH _{4 generated} (I				
waste (t)	DDOC _{m dep} (t)	DDOC _{m decom}	DDOC _{m remain}	DDOC _{m accum T}	DDOC _{m decom T}	CH.		
Mapre (r)	DDCCm dep (t)	(t)	(1)	(t)	(t)	C/14 generated \		
186	22.3	0.0	22:3	22.3	0.0	0.		
186		0.0	22.3	43.3	1.3	0.		
186	22.3	0.0	22.3	63.1	2.5	1.		
186	22,3	0.0	22.3	81,8	3.7	2		
186		0.0	22.3	99.3	4.8	3		
186	22.3	0.0	22.3	115.9	5.8	3		
186	22.3	0.0	22.3	131.4	6.7	4		
186		0.0	22.3	146.1	7.7	5		
186		0.0	22.3	159.9	8.5	5		
186		0.0	22.3		9.3	6		
28	3.3	0.0	3.3	166.2	10.1	6		
28	3,3	0.0	3.3	159.9	9.7	6		
28		0.0	3.3		9.3	6		
28	3.3	0.0	3.3	148.3	9.0	6		
28	3.3	0.0	3.3	143.0	8.6	- 5		
28	3,3	0.0	3.3	138.0	8.3	5		
28		0.0	3.3	133.3	8.0	5		
28	3.3	0.0	3.3		7.8	5		
28	3.3	0.0	3.3	124.8	7.5	5		
28	3,3	0.0	3.3	120.8	7.3	4		
28		0.0	3.3		7.0	4		
28		0.0	3.3		6.8			
28		0.0	3.3		6.6			
28	3.3	0.0	3.3		6.4			
28	3.3	0.0	3.3		6.3			
28		0.0	3.3		6.1	4		
28		0.0	3.3		5.9	3		
28		0.0	3.3		5.8			
28		0.0	3.3		5.6			
28		0.0	3.3		5.5			
28		0.0	3.3		5.4	3		
28		0.0	3.3		5.3			
28		0.0	3.3		5.1	3		
28		0.0	3.3		5.0	3		
28	3,3	0.0	3.3	83.2	4.9	3		
28		0.0	3.3		4.8			
28		0.0	3.3		4.8	3		
28		0.0	3.3		4.7	3		
28		0.0	3.3		4.6			
28		0.0	3.3		4.5			
28		0.0	3.3		4.5			
28		0.0	3.3		4.4	2		
28	3.3	0.0	3.3		4.3	2		
28		0.0	3.3		4.3	2		
28		0.0	3.3	71.6	4.3			
28		0.0	3.3		4.2	2		
28			3.3		4.1	2		
28			3.3		4.1	2		
28		0.0	3.3		4.0			
28		0.0	3.3		4.0			
28	3.3	0,0	3.3	67,4	4.0	2		

Scenario 2

			Rubber			
waste (kt)	DDOC _{modest} (t)	DDOC _{m decom}	DDOC _{m remain}	DDOC _{macoum T}	DDOC _{m decom T}	CH _{4 generated} (
267	52.1	0.0	52.1	10	0.0	0.
267	52.1	0.0	52.1			2.
267	52.1	0.0	52.1			3.
267	52.1	0.0	52.1			5.
267	52.1	0.0	52.1		11.1	
267	52.1	0.0	52.1			9.
267	52.1	0.0	52.1			10.
267	52.1	0.0	52.1		17.9	
267	52.1	0.0	52.1			13
267	52.1	0.0	52.1		21.7	
573		0.0	111.7			
573	111.7	0.0	111.7			19.
573	111.7	0.0	111.7		33.5	
573	111.7	0.0	111.7			25
573	111.7	0.0	111.7	795.9	42.3	
573	111.7	0.0	111.7		46.3	30
573	111.7	0.0	111.7		50.2	33
573	the state of the s	0.0	111.7		53.7	35
573		0.0	111.7	1,035.2	57.1	38.
573		0.0	111.7	1,086.6	60.3	40.
573		0.0	111.7	1,135.0	63.3	42
573		0.0	111.7		66.1	44
573		0.0	111.7			
573		0.0	111.7			47.
573		0.0	111.7		73.6	49.
573		0.0	111.7			50.
573		0.0	111.7			51.
573		0.0	111.7		79.9	53.
573		0.0	111.7		81.7	
573		0.0	111.7		83.5	
573		0.0	111.7		85.1	56
573		0.0	111.7		86.7	57
573		0.0	111.7		88.1	58.
573		0.0	111.7			59
573			111.7			
573		0.0	111.7			
573			111.7			
573		0.0	111.7			
573		0.0	111.7			
573			111.7		96.2	
573			111.7			64
573			111.7		97.9	65.
573		0.0	111.7			
573			111.7			
573		0.0	111.7			66.
573			111.7			
573			111.7			
573			111.7			68.
573		0.0	111.7			
573			111.7			68
573			111.7		103.2	69.

Scenario 2

Total CH ₄	Me	than recovere	d	Jezon I		Ej (t CO ₂ -e)
Generated (t)	Q _{cap} (m ³)	Q _{flared} (m ³)	$Q_{tr}\left(m^3\right)$	CH ₄ * (t)	E	
0.0	0	0	0	0.0	0.0	0:0
54.5	0	0	0	54.5	49.0	1029.9
102.9	0	0	0	102.9	92.6	1944.1
146.0	0	0	0	146.0	131.4	2758.8
184.5	0	0	0	184.5	166.1	3487.6
219.1	0		0	219.1	197.2	4141.9
250.4	0		0	250.4	225.3	4731.7
278.6	0	0	0	278.6	250.7	5265.
304.2	0	0	0	304.2	273.8	5749.2
327.5	0	0	0	327.5	294.8	6190.2
348.8	0	0	0	348.8	314.0	6593.0
329.6	0	0	0	329.6	296.7	6229.9
313.5	0	0	0	313.5	282.2	5925.8
300.1	O	0	0	300.1	270.1	5671.1
288.8	0	0	0	288.8	259.9	5457.7
279.3	D	0	0	279.3	251.4	5278.8
271.4	D		0	271.4	244.2	5128.8
264.7	0	0	0	264.7	238.2	5002.9
259.1	0	0	0	259.1	233.2	4897.3
254.4	0	0	0	254.4	229.0	4808.5
250.5	0	0	0	250.5	225.4	4734.0
247.2	o o	0	0	247.2	222.4	4671.3
244.4	0	0	0	244.4	219.9	4618.6
242.0	0	ū	o o	242.0	217.8	4574.2
240.0	0	0	0	240.0	216.0	4536.8
238.4	. 0	0	0	238.4	214.5	4505.3
237.0	0	0	0	237.0	213.3	4478.7
235.8	0	o o	o	235.8	212.2	4456.3
234.8	0	0	o	234.8	211.3	4437.4
233.9	o o		o	233.9	210.5	4421.3
233.2	0	0	0	233.2	209.9	4407.7
232.6	0	0	0	232.6	209.3	4396.2
232.1	0	0	0	232.1	208.9	4386,4
231,6	0	Ö	o	231.6	208.5	4378.
231.3	0	0	o	231.3	208.1	4371.0
230.9	0	0	0	230.9	207.9	4364.9
230.7	0	o	o	230.5	207.6	4359.6
230.4	0	o o	o	230.4	207.4	4355.1
230.2	0	ū	0	230.2	207.2	4351.2
230.0	0	0	o o	230.0	207.0	4347.9
229.9	0	0	o	229.9	206.9	4344.9
229.8	0	0	0	229.8	206.8	4342.3
229.6	0	0			206.7	4340.0
229.5	0	0	0	229.6 229.5	206.7	4340.0
229.5	0	0	0	229.5	206.5	4336.
		0				
229.3	D		0	229.3	206.4	4334.5
229.3	0	0	0	229.3	206.3	4332.9
229.2	D	0	0	229.2	206.3	4331.5
229.1	0	0	0	229.1	206.2	4330,3
229,1	0	0	0	229.1	206.1	4329,0
229.0	0	0	0	229.0	206.1	4327.9 227,132

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