## asongroup

## Traffic Impact Assessment

Light Horse Interchange Business Hub, Eastern Creek State Significant Development Application (SSD 9667) Response to Submissions

## Document Control

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## 1 Introduction

### 1.1 Background \& Overview

Ason Group has previously prepared a Traffic Impact Assessment (TIA) for this State Significant Development Application (SSDA) — refer 0541r03v2 traffic report dated 24/05/2019. The SSDA was then proceeded to public exhibition with the Department of Planning, Industry \& Environment (DPIE), Roads and Maritime Services (RMS), Transport for NSW (TfNSW) and Council providing a number of comments. Accordingly, we have been re-engaged by Western Sydney Parklands Trust (WSPT) to prepare a revised Traffic Impact Assessment (TIA) regarding this SSDA which is related to development of the Light Horse Interchange Business Hub (LIBH), Eastern Creek (the Site). This SSDA also considers the comments provided at Project Team's meeting with RMS dated 12 December 2019.

The SSDA generally provides for the following:

- A Masterplan for the staged development of the LIBH, including: -
- Development of a regional warehousing and distribution hub with 24 hours/day, 7 days/week operation, with a total yield of $165,500 \mathrm{~m}^{2}$ of gross floor area (GFA) that includes $157,600 \mathrm{~m}^{2}$ of warehouse space and $7,900 \mathrm{~m}^{2}$ of ancillary office space;
- Indicative site/lot layout, site access, internal road network, site levels, drainage, building envelopes, parking and landscaping;
- Development controls; and
- Biodiversity offsets.
- In the context of this TIA, the SSDA also provides for: -
- Site access connection to Ferrers Road, and in turn access north to the Great Western Highway (GWH) and south to The Horsley Drive. The existing access to Wallgrove Road will be retained (and improved) for use by emergency vehicles only;
- In conjunction with broader upgrades to the local road network, localised upgrades along the key access routes to / from the Site;
- Site road and access intersection design profiles which provide for the largest heavy vehicles accessing the Site; and
- A sustainable level of on-site parking provision.

Full details of the Masterplan are provided in the Environmental Impact Statement (EIS) to which this TIA accompanies. DPIE issued Secretary's Environmental Assessment Requirements (SEARs) regarding the LIBH proposal on $7^{\text {th }}$ November 2018; a copy of which are included in Appendix A. The SEARs include a number of "Traffic and Transport" requirements as outlined in Table 1 of Section 1.3,
including a summary response to each SEAR and reference to the section of this TIA that provides more detailed steps / explanation / analysis of each SEAR.

### 1.2 Site \& Location

The Site has a total area of approximately 29.5 hectares (ha) development and is legally known as Part of Lot 10 in DP 1061237 and Part of Lot 5 in DP 804051, with a formal address of 165 Wallgrove Road and 475 Ferrers Road, Eastern Creek. The Site is bordered by the M4 Western Motorway to the north; a SUEZ recycling centre to the south; Eastern Creek Raceway to the east; and the M7 Westlink Motorway to the west. The Site is shown in its local context in Figure 1.

The Site is located within the Blacktown City Council (Council) Local Government Area (LGA) and is zoned as WSP (Western Sydney Parklands) by the Council's Local Environmental Plan (BCC LEP). It is subject to State Environmental Planning Policy - Western Sydney Parklands - 2009 (SEPP-WSP) and Western Sydney Parklands - Plan of Management - 2030 (POM).


Figure 1: Site Location - Light Horse Interchange Business Hub

### 1.3 Secretary's Environmental Assessment Requirements

Secretary's Environmental Assessment Requirements (SEARs) were issued by the Department of Planning \& Environment (DPE) on $7^{\text {th }}$ November 2018 in regard to the LIBH proposal. The SEARs outline the key areas for consideration in any subsequent development application (i.e. in the SSDA) with specific requirements relating to the assessment of potential traffic and transport impacts.

The SEARs specifically relating to the traffic and transport characteristics of the Masterplan are outlined in Table 1 below, noting that Table 1 also provides a summary response to each SEAR, and reference to the section of this TIA providing a more detailed analysis of each SEAR.

Table 1: Secretary's Environmental Assessment Requirements - General

| Source | SEARs | Summary Response | TIA Section |
| :---: | :---: | :---: | :---: |
| DPIEDPIE <br> Traffic <br> and <br> Transport | A quantitative Traffic Impact Assessment prepared in accordance with relevant Blacktown City Council, Austroads and Roads and Maritime Services guidelines | Austroads, Councils DCP and RMS Guide were reviewed to identify appropriate traffic generation as well as parking provisions. Quantitative analysis was carried out to predict traffic distribution as well as the potential impact of development traffic. | $\begin{gathered} 3.4 \\ 4.1 \text { to } 4.3 \\ 5.1 \text { to } 5.7 \end{gathered}$ |
| DPIE: <br> Traffic and Transport | Details of all daily and peak traffic and transport movements likely to be generated by the development including the impact on the nearby intersections and the need/associated funding for the upgrading or road improvements works (if required) | Trip generation rates were based on RMS and Ason Group surveys of like developments, while trip distribution references available Journey to Work data. SIDRA modelling was then undertaken to identify the impact of development traffic. This modelling determined that in addition to currently committed RMS upgrades and the planned upgrades within the local road network, no additional upgrade is required and the local intersections can to appropriately accommodate Base 2036 traffic flows as well as Base 2036 + Development traffic flows. | 5.1 to 5.7 |
| DPIE: <br> Traffic and Transport | Impacts on the safety and capacity of the surrounding road network and access points, using SIDRA or similar modelling, to assess impacts from current traffic counts and cumulative traffic from existing and proposed development | As stated, SIDRA modelling was undertaken to identify the impact of development traffic. This modelling determined that in addition to currently committed RMS upgrades within the local road network, no additional upgrade is required and the local intersections can appropriately accommodate Base 2036 traffic flows as well as Base 2036 + Development traffic flows. | $\begin{gathered} 3.4 \\ 4.1 \text { to } 4.3 \\ 5.1 \text { to } 5.7 \end{gathered}$ |
| DPIE: <br> Traffic and Transport | Demonstrate that sufficient pedestrian and cyclist facilities have been provided for the development | The Site enjoys excellent access to the Western Sydney Parklands existing and proposed bicycle network. Accordingly, pedestrian / cyclists shared paths have been proposed to connect to Wallgrove Road ( 3.5 metres wide concrete footpath) and Ferrers Road ( 2.5 metres wide concrete footpath), along with an internal pedestrian path along eastern side of the access road ( 1.2 metres wide concrete footpath). | 2.5 |
| DPIE: <br> Traffic and Transport | Details and a justification of access to, from and within the site (vehicular and pedestrian) | Primary vehicle access to the Site will be provided to Ferrers Road, while emergency vehicle access will be provided from Wallgrove Road. <br> Access for pedestrians (and cyclists) will be provided from Wallgrove Road and Ferrers Road. | $\begin{aligned} & 2.2 \\ & 2.3 \\ & 2.5 \end{aligned}$ |
| DPIE: <br> Traffic and Transport | Details of road upgrades, new roads or access points required for the development, if necessary | To facilitate access, a new roundabout is proposed linking the Site to Ferrers Road. | $\begin{aligned} & 2.2 \\ & 5.6 \end{aligned}$ |
| Council: <br> Traffic matters | Parking rates for the development should be provided in accordance with Blacktown Council's Development Control Plan for the area | Council's DCP parking rates have been referenced in the assessment; however, it has been determined that an appropriate and sustainable level of parking provision is provided with reference to RMS Guide parking rates, which also reflect numerous Ason Group surveys of similar industrial sites. | 6.1 |


| Source | SEARs | Summary Response | TIA Section |
| :---: | :---: | :---: | :---: |
| RMS | Daily and peak traffic movements likely to be generated by the development including the impact on the nearby intersections and the need/associated funding for the upgrading or road improvements works (if required). The key intersections to be examined / modelled include: <br> - Wallgrove Road / Site Access; <br> - The Horsley Drive / Ferrers Road; <br> - Great Western Highway / Brabham Drive | As stated, trip generation rates were based on RMS and Ason Group surveys of like developments, while trip distribution references available Journey to Work data. SIDRA modelling was then undertaken to identify the impact of development traffic. This modelling determined that the RMS planned upgrades at The Horsley Drive / Ferrers Road intersection would perform at a satisfactory level with 2036 Base + Development traffic. <br> Furthermore, additional upgrades recently delivered at Great Western Highway / Brabham Drive / Doonside Road intersection can appropriately accommodate 2036 Background traffic flows (as well as 2036 Base + Development traffic). <br> The Wallgrove Road access is an existing access intended for use by emergency vehicles only and therefore not materially impacted by the development. As such, the proposal does not trigger a need for changes to the intersection. | 5.1 to 5.7 |
| RMS | Details of the proposed accesses and the parking provisions associated with the proposed development including compliance with the requirements of the relevant Australian Standards (i.e.: turn paths, sight distance requirements, aisle widths, etc) and relevant parking codes. Swept path plans need to be provided. | Swept path analysis of all critical movements at proposed Ferrers Road roundabout as well as internal access roads have been undertaken to confirm compliance with relevant standards. Relevant swept path diagrams are provided in civil engineering report, provided separately to this report. <br> It is expected that a Condition of Consent would be imposed requiring compliance with AS 2890.1 and AS 2890.2 prior to the issue of a Construction Certificate. In this regard, swept path analysis for individual building hardstands (paved area for heavy vehicle parking) will be undertaken during future stages to accompany the design development of built forms on each lot. | 2.2 to 2.4 |
| RMS | Details of service vehicle movements (including vehicle type and likely arrival and departure times) | The details of service vehicle movements to and from the Site is unknown at this stage; however, the assessment provides for some 28\% of traffic movements to be heavy vehicle movements, which is in line with the heavy vehicle percentages determined by the RMS at similar industrial sites. | 5.1.3 |
| RMS | Assess the implications of the proposed development for non-car travel modes (including public transport use, walking and cycling); the potential for implementing a location-specific sustainable travel plan, and the provision of facilities to increase the non-car mode share for travel to and from the site. This will entail an assessment of the accessibility of the development site by public transport | The JTW data suggests that no employees currently travel to work in the local area by either public or active transport, with the predominant mode of choice being private vehicle, which is consistent with on-site observations. Notwithstanding, there is excellent potential for future public transport routes to service the Site, as well as future pedestrian and cycle connections to Ferrers Road and M7 Cycleway. | $\begin{aligned} & 2.5 \\ & 3.2 \end{aligned}$ |
| Transport for NSW | Details of all daily and peak traffic and transport movements likely to be generated (light and heavy vehicle, public transport, pedestrian and cycle trips) during construction and operation of the development | As stated, trip generation rates were based on RMS and Ason Group surveys of like developments, while trip distribution references available Journey to Work data. <br> An assessment of construction traffic impacts has not been undertaken at this time as the details of the construction task are not currently available. <br> However, a 'high-level' Construction Traffic Management Plan (CTMP) has been provided in Section 7 to include preliminary CTMP principles. <br> It is expected that a detailed Construction Traffic Management Plan would be provided in future | $\begin{gathered} 5.1 \\ 5.2 \\ 7 \end{gathered}$ |


| Source | SEARs | Summary Response | TIA Section |
| :---: | :---: | :---: | :---: |
|  |  | development applications, or prior to issue of a Construction Certificate |  |
| Transport for NSW | Details of the current daily and peak hour vehicle, public transport, pedestrian and bicycle movements and existing traffic and transport facilities provided on the road network located adjacent to the proposed development | This assessment provides analysis of existing and future road network operations; and existing and future public and active transport services/infrastructure. | $\begin{aligned} & 3.1 \\ & 3.2 \\ & 3.3 \end{aligned}$ |
| Transport for NSW | An assessment of the operation of existing and future transport networks including public transport, pedestrian and bicycle provisions and their ability to accommodate the forecast number of trips to and from the development | As stated, this assessment provides analysis and existing and future public and active transport services/infrastructure. | $\begin{gathered} 3.4 \\ 4.3 \\ 5.5 \text { to } 5.7 \end{gathered}$ |
| Transport for NSW | Details the type of heavy vehicles likely to be used (e.g. B-doubles) during the operation of the development and the impacts of heavy vehicles on nearby intersections | The percentage of heavy vehicles in the future traffic generation of the Site has been specifically identified with reference to RMS surveys and included in the SIDRA modelling of key intersections. From a design perspective, it is expected that the maximum vehicle accessing the Site would be B-Doubles and, as such, the future design of all access roads would appropriately consider such vehicles. | $\begin{gathered} 2.3 \\ 5.1 .3 \\ 5.5 \text { to } 5.7 \end{gathered}$ |
| Transport for NSW | Details of access to, from and within the site to/from the local road and strategic (motorway) network including intersection location, design and sight distance (i.e. turning lanes, swept paths, sight distance requirements) | As stated, to facilitate access, a new roundabout is proposed linking the Site to Ferrers Road. <br> Both access points comply with the sight distance requirements recommended in Austroads Guide to Road Design. | $\begin{aligned} & 2.2 \\ & 2.3 \end{aligned}$ |
| Transport for NSW | Impact of the proposed development on existing and future public transport and walking and cycling infrastructure within and surrounding the site | The Site enjoys excellent access to the Western Sydney Parklands existing and proposed bicycle network. Accordingly, Pedestrian / cyclists shared paths have been proposed to connect to Wallgrove Road ( 3.5 metres wide concrete footpath) and Ferrers Road ( 2.5 metres wide concrete footpath), along with an internal pedestrian path along eastern side of Access road ( 1.2 metres wide concrete footpath). | $\begin{aligned} & 2.5 \\ & 3.2 \end{aligned}$ |
| Transport for NSW | An assessment of the existing and future performance of key intersections providing access to the site (Site access with Wallgrove Road, Ferrers Road with Brabham Drive - subject to likely access routes to/from the motorway network), and any upgrades (road/intersections) required as a result of the development | As stated, SIDRA modelling was undertaken to identify the impact of development traffic. This modelling determined that in addition to currently committed RMS upgrades within the local road network, no additional upgrade is required and the local intersections can to appropriately accommodate Base 2036 traffic flows as well as Base 2036 + Development traffic flows. | $\begin{gathered} 3.4 \\ 4.3 \\ 5.5 \text { to } 5.7 \end{gathered}$ |
| Transport for NSW | An assessment of predicted impacts on road safety and the capacity of the road network to accommodate the development | Both access points comply with the sight distance requirements recommended in Austroads Guide to Road Design. <br> As stated, SIDRA modelling was undertaken to identify the impact of development traffic and the capacity of the road network to accommodate the traffic. | $\begin{gathered} 3.4 \\ 4.3 \\ 5.5 \text { to } 5.7 \end{gathered}$ |
| Transport for NSW | Demonstrate the measures to be implemented to encourage employees of the development to make sustainable travel choices, including walking, cycling, public transport and car sharing | The Site enjoys excellent access to the Western Sydney Parklands existing and proposed bicycle network. It is anticipated that potential future development along Ferrers Road will increase the potential for new public transport (bus) routes | $\begin{aligned} & 2.5 \\ & 3.2 \end{aligned}$ |


\left.| Source | SEARs | Summary Response |
| :--- | :--- | :--- | :--- |$\right\left.] \begin{array}{c}\text { Section }\end{array}\right]$


| Source | SEARs | Summary Response | TIA Section |
| :---: | :---: | :---: | :---: |
|  | these impacts will be mitigated for any associated traffic, pedestrians, cyclists and public transport operations |  |  |
| Transport for NSW | The EIS should detail how the proposed development will be consistent and align with the objectives, goals and directions of the following: <br> - Greater Sydney Region Plan; <br> - Western Sydney District Plan; <br> - Future Transport Strategy 2056; <br> - Future Transport- Greater Sydney Services and Infrastructure Plan <br> - NSW Freight \& Ports Plan 2018-2023 | This is a matter for the EIS (generally) and not specific to this TIA. <br> It is expected that these documents are suitably reflected in the RMS strategic model of 2036, which formed the basis for predicting future background traffic for this TIA. | $\begin{aligned} & 4.1 \\ & 4.2 \end{aligned}$ |

### 1.4 Consultation Process

The following Table 2 presents the authority comments in relation to the original SSD submission, respective commentary and sections within this TIA where those comments are addressed.

Table 2: Authority Comments and Ason Group Response

| No. | Authority Comments | Ason Group Response | TIA |
| :--- | :--- | :--- | :--- |
| Section |  |  |  |
| Blacktown City Council - Planning Comments |  |  |  |
| 3 | The Urban Design guidelines adopts the <br> RMS traffic rates where the parking rates <br> should be the same as that applied in <br> Eastern creek Precinct Stage 3 (across <br> Wallgrove Road) which is 1 space per 100 <br> sqm of GFA up to 7,500 sqm and for greater <br> than 7,500 sqm it is 1 space per 200 sqm for <br> that part of floor space that is over 7,500 <br> sqm. | It is further noted that other developments in the <br> locality (such as Ropes Crossing) have also been <br> approved with rates less than stipulated by Council. <br> surveyed sites to justify the use of the standard RMS <br> there is not a clear basis. | Section 6. |
| 4 | Consequently, we are unable to support a <br> masterplan for buildings that nominate floor <br> spaces for building footprints that have not <br> been the subject of detailed assessment, <br> specially as the building footprints are based <br> on the parking rates in the EIS.... | Thates for which |  |
| 5 | There is insufficient detail about the building <br> footprints, including how access to docks by <br> B-Double trucks will be provided. The <br> indicative footprints represent an <br> overdevelopment of each site. We are only <br> prepared to support a subdivision <br> masterplan provided the driveways and car <br> parking are consistent with the reciprocal <br> right of ways. | This is a detailed matter that can be resolved at DA <br> stage. <br> Nevertheless, reference should be made to the swept <br> path drawings prepared by the civil engineer <br> demonstrating manoeuvrability. | NA |


| No. | Authority Comments | TIA |  |
| :--- | :--- | :--- | :--- |
| 6 | The building concept plan is not clear about <br> what appear to be ramps. More information <br> is required on the ramps proposed in front of <br> each warehouse as indicated on the <br> Concept Masterplan. | This comment is assumed to relate to the recessed <br> docks; typical of many warehouse type developments. | NA |
| Blacktore |  |  |  |


| No. | Authority Comments | Ason Group Response | TIA Section |
| :---: | :---: | :---: | :---: |
| 8 | Shared pedestrian and cyclist access from Wallgrove Road and Ferrers Road should be provided, including the new access road for this development. Shared paths should comply with the latest State Government guideline(s). | Refer to updated civil and architectural design packages, provided separately. | NA |
| RMS |  |  |  |
| 1 | Further information is required in relation to the impacts of the emergency access point and shared path. | Emergency vehicles are expected to access the Site infrequently and therefore are anticipated to have negligible traffic impact on the surrounding road network. | NA |
| 2 | Detailed plans are to be submitted detailing the treatment of the M7 boundary fence on Wallgrove Road. Drawing 18652_SSDA_EX01 states that the existing fences and gate will remain. Clarification is required in relation to the existing locked gate across the M7 access road. | Refer to updated civil and architectural design packages, provided separately. | NA |
| 3 | There is reference to a rock rubble drainage on Roads and Maritime / M7 land. WSPT is to clarify the extent of this work and who is to manage and maintain this asset and any resulting access issues. | Refer to consolidated response in EIS. | NA |
| 4 | Further information is required in relation to the overall management of the access gates in relation to the Emergency Access Point. | The proposed gate will generally be secured; opened as necessary for emergency vehicles. |  |
| 5 | Further information is required in relation as to how WSPT propose to manage, maintain and operate the share path asset on Roads and Maritime / M7 land. | Refer to WSPT response in EIS. | NA. |
| 6 | An additional left turn lane is proposed at the intersection of Great Western Highway / Doonside Road / Brabham Drive. <br> The applicant is to provide concept civil design plans, TCS plans and swept path plans for the proposed signal work for further assessment. | This TIA has undertaken revised modelling following additional detailed traffic and pedestrian surveys (in response to TfNSW comments) at the intersection of Doonside Drive / Great Western Highway. This revised analysis has determined that the previously identified upgrade is NOT required to support this development. <br> With no requirements to upgrade that intersection, the need for a concept design becomes redundant. | NA. |
| TfNSW |  |  |  |
| 7 | Based on comparison of historical aerial imagery (via Nearmap), it is noted that intersection upgrades at the Great Western Highway with Brabham Drive/Doonside Road were completed and operational in Sep/Oct 2018. Furthermore, the assessment had undertaken the intersection analysis based on survey data obtained from November 2017, which establishes the base case scenario. <br> Having regard for the above, the existing traffic conditions may have changed, such | As recommended by TfNSW, this TIA has undertaken revised intersection counts at this signalised intersection and re-run the following scenarios: <br> - Existing base (October 2019), <br> - Future Base (2036 EMME projections), and <br> - Project Case (2036 Base + Development). <br> Results of the updated modelling for the Future Project Case suggests that this intersection does not require any additional upgrades. <br> Regarding the additional traffic from Eastern Creek Quarter and Sydney Zoo, it is noteworthy that the future base model (RMS EMME projections) are | Section 5.5. |


| No. | Authority Comments | Ason Group Response | TIA |
| :--- | :--- | :--- | :--- |
|  | Section <br> that new intersection analysis would be <br> warranted, in response to: <br> Potential changes in signal operations and <br> green time allocation having regard for new <br> dual right-turns on the Great Western <br> Highway and new pedestrian crossing legs. <br> Potential changes in traffic volumes due to <br> land use changes and growth (between <br> surveyed period and current) surrounding the <br> Huntingwood/Bungarribee area and Greater <br> Penrith and Blacktown area. <br> In addition to the above, it is unclear whether <br> traffic associated with the under-construction <br> developments at the Eastern Creek Quarter <br> (shopping centre) and the Sydney Zoo have <br> been accounted for within the traffic <br> assessment. <br> assumed to have incorporated a reasonable <br> contingency for future traffic associated with these <br> components. | DPIE |  |

### 1.5 Study Objectives \& Methodology

The key objectives of this TIA are to:

- Provide an appropriate response to the SEARs;
- Establish that the development of the Site in accordance with the Masterplan is compliant and consistent with the relevant Council planning guidelines;
- Establish that the trip generation of the Site can be appropriately accommodated by the local and sub-regional network, with due consideration of committed (by others) upgrades to several key intersections providing access for the Site;
- Demonstrate that proposed Site access driveways, car parks and service facilities can be designed to provide full compliance with the relevant Australian Standards; and
- Demonstrate that there is an appropriate and sustainable allocation of car parking across the Site.

To achieve these objectives, this TIA provides an assessment of the existing and future operation of the road network servicing the LIBH, as well as other traffic and transport related issues including car parking requirements, vehicle access, and public and active transport accessibility.

The following key tasks have been undertaken in the preparation of this TIA:

- A review of the existing and proposed future road network providing access to the regional road network.
- The quantification of existing and future traffic flows in key roads and at key intersections providing access for the LIBH, including the commission and review of peak period traffic surveys.
- An assessment of the traffic generation and distribution characteristics of the proposed LIBH, and the potential impact of those additional traffic flows on nearby key roads and intersections.
- An assessment of internal access, parking and servicing provisions with reference to the appropriate Australian Standards.


### 1.6 Reference Documents

This TIA specifically references the most recent assessments of key infrastructure projects within the sub-regional network providing for the Site, such as

- Aecom, Eastern Creek Resource Energy and Business Precinct - Flood, Traffic and Access Study, November 2013 (TAS 2013)

This TIA also references general access, traffic, and parking guidelines, including:

- RMS Guide to Traffic Generating Developments (RMS Guide)
- RMS Guide to Traffic Generating Development Updated Traffic Surveys (RMS Guide Update)
- Austroads Guide to Road Design Part 3: Road Geometry (Austroads GRD3)
- Austroads Guide to Road Design Part: 4A Unsignalised and Signalised Intersections (Austroads GRD4A)
- Austroads Guide to Traffic Management Part 3: Traffic Studies and Analysis (Austroads GTM3)
- Australian Standard 2890.1: Parking Facilities - Off Street Car Parking (AS 2890.1)
- Australian Standard 2890.2: Parking Facilities - Off Street Commercial Vehicle Facilities (AS 2890.2)
- Australian Standard 2890.6: Parking Facilities - Off Street Parking for People with Disabilities (AS 2890.6)


## 2 The Light Horse Business Hub Masterplan

### 2.1 Overview

As stated, a detailed description of the Masterplan is provided in the EIS which this TIA accompanies. In summary, the broader SSDA provides for the following:

- Approximately $157,600 \mathrm{~m}^{2}$ GFA of warehouse space and $7,900 \mathrm{~m}^{2}$ GFA of ancillary office space;
- Site access connections to Ferrers Road (primary access) and Wallgrove Road (emergency);
- In conjunction with broader upgrades to the local road network, localised upgrades along the key access routes to/from the Site;
- Design profiles of Site road and access intersections which provide for the largest heavy vehicles accessing the Site; and
- A sustainable level of on-site parking provision.


Figure 2: Light Horse Interchange Business Hub Masterplan

### 2.2 Site Access

### 2.2.1 Access Options Considered

As part of initial concept design development for this project, the following 3 access options were investigated with relevant commentary provided below.

Table 3: Access Options Considered

| Ref | Description | Comments |
| :---: | :---: | :---: |
| 1 | Access from the south, via SUEZ | This option was deemed unsuitable having regard for: <br> - High traffic volumes in Wallgrove Road and close-proximity to signals preventing suitable (signalised) access opportunities <br> - Insufficient headroom under the M7 overpass bridge <br> - Impacts on bus services - increased use of the Wallgrove Rd slip lane would likely require relocation of the existing bus stop provided therein. <br> - Difficulties in providing required upgrades to the Wallgrove Road / SUEZ access required to support the increased cumulative traffic using that access point. |
| 2 | Wallgrove Road access | This option was deemed unsuitable having regard for: <br> - Fundamentally, this option relies upon private land to the south which is therefore subject to timing, liability and other issues. <br> - Difficulties in providing required upgrades to the Wallgrove Road / SUEZ access required to support the development |
| 3 | Ferrers Road connection | This option was found to be supportable and, as such, has formed the basis for further assessment. |

### 2.2.2 Proposed Vehicular Access

Access to the LIBH will be provided through 2 connection points:

- Primary Access: via Ferrers Road, providing a new roundabout intersection to approximately 200 metres west of the existing (roundabout) intersection of Ferrers Road / Brabham Drive / Peter Brock Drive. This new roundabout would provide primary access for all vehicles. This access road has been termed "LIBH Access" for ease of reference.
- Emergency Access: via Wallgrove Road for emergency vehicles only. In this regard, the existing private road that runs eastbound from Wallgrove Road through M7 underpass is proposed to be extended to connect with LIBH Access.

The design of Ferrers Road roundabout will necessarily consider meeting the requirements of:

- Lane capacity, as determined by SIDRA modelling; and
- Turning path requirements of the largest heavy vehicles permitted to access the Site, expected to be B-Doubles.

It is noted that Ferrers Road north of the intersection with LIBH Access is already approved for heavy vehicles up to and including 26m B-Doubles, while south of the Austral Bricks site, Ferrers Road is approved for 25 m B-Doubles travelling southbound only.

The Emergency Access road shall be constructed to achieve a minimum carriageway width of 6 metres to comply with NSW Fire \& Rescue Guidelines for Emergency Vehicle Access (Policy No. 4) and other relevant emergency service access requirements.

### 2.3 Internal Access \& Circulation for Motor Vehicles

From its intersection with Ferrers Road, the LIBH Access will run west and then south through the centre of the LIBH.

LIBH Access will be constructed in accordance with the road profiles of Blacktown City Council's Development Control Plan (BCC DCP), comprising of a 15.5 metre wide carriageway for its full length to enable two-way traffic and on-street parking (though on-street parking demand is expected to be minimal). Swept path analysis of all critical movements at proposed Ferrers Road roundabout as well as internal access roads have been undertaken to confirm compliance with relevant standards, noting that it is expected that a Condition of Consent would be imposed requiring compliance with AS 2890.1 and AS 2890.2 prior to the issue of a Construction Certificate. All swept path diagrams are provided in the Civil Engineering Report, submitted separately.

Proposed vehicular access and circulation within the Site are shown in Figure 3.


Figure 3: Vehicle Access and Circulation

### 2.4 Built Form

All car park and loading area access will be provided from LIBH Access via industrial driveways that will be constructed to provide full compliance with the appropriate Australian Standards; specifically AS 2890.1 and AS 2890.2. Swept path analysis for individual hardstand (paved area for heavy vehicle parking) will be undertaken during future stages to accompany the design development of that future built form on each lot, at that time.

### 2.5 Pedestrian and Cyclist Access

The Westlink M7 Shared Path runs parallel to the Westlink M7 directly west of the Site. While there is currently no immediate access to the Shared Path in this location, the opportunity exists to provide a shared path connection via the (currently closed) access road under the Westlink M7.

From Ferrers Road, cycle access is also available to the extensive off-road cycle network to the east of the Site (the Prospect Loop) linking to key sub-regional centres as well as public transport interchanges. Paired with the provision of appropriate on-site cycle facilities, such as bicycle storage, lockers and shower facilities, the Site is well located to generate cycle trips.

Accordingly, the following onsite Pedestrian and Cyclists facilities have been provided with this SSDA:

- Pedestrian / Cyclists shared path from Wallgrove Road (3.5 metres wide concrete footpath);
- Pedestrian / Cyclists shared path from Ferrers Road ( 2.5 metres wide concrete footpath); and
- Internal Pedestrian path along eastern side of LIBH Access (1.2 metres wide concrete footpath).

The proposed Pedestrian / cyclists facilities are summarised in Figure 4.


Figure 4: Proposed Pedestrian and Cyclist Facilities

## 3 Existing Conditions

### 3.1 Existing Road Network

The existing road network in the vicinity of the LIBH is shown in Figure 5, and key roads and intersections are further detailed below.


Figure 5: Existing Road Network

### 3.1.1 M4 Motorway

The M4 Motorway is a high capacity road link of national significance and the primary east-west connection to Western Sydney. The M4 Motorway provides a key western link between the inner west of Sydney to the M7 Motorway and the Blue Mountains. Near the Site, the M4 Motorway carries six traffic lanes within a divided carriageway and provides a major interchange with the M7 Motorway. The speed limit on the M4 Motorway is $110 \mathrm{~km} / \mathrm{h}$, and it carries approximately 100,000 vehicles per day (vpd).

### 3.1.2 M7 Western Motorway

The M7 Motorway is a high capacity road link of national significance and was built to accommodate future traffic growth in Western Sydney. The M7 Motorway provides a key western link between the M2 Motorway (to the north) and the M5 Motorway (to the south). Near the Site, the M7 Motorway has four traffic lanes within a divided carriageway and has a major interchange with the Great Western Highway (and as described with the M4 Motorway). Additional connections to the M7 are provided from Wallgrove Road at its intersections with Old Wallgrove Road and Mini Link Road. The speed limit on the M7 Motorway is $100 \mathrm{~km} / \mathrm{h}$, and it carries approximately $70,000 \mathrm{vpd}$.

### 3.1.3 Great Western Highway

The Great Western Highway (GWH) is a high capacity road link that runs parallel to the M4 Western Motorway and provides a key link between Penrith and Parramatta. In the vicinity of the Site, the GWH has four traffic lanes within a divided carriageway and on/off ramps to the M7 Westlink Motorway to the west of the Site. The speed limit on the GWH is $80 \mathrm{~km} / \mathrm{h}$, and it carries approximately $40,000 \mathrm{vpd}$.

### 3.1.4 Doonside Road

Doonside Road is an arterial road to the north of the Site that runs generally north-south from its intersection with Great Western Highway in the south to Bungarribee Road in the north. Near the Site, Doonside Road provides four traffic lanes within a divided carriageway. The speed limit on Doonside Road is $70 \mathrm{~km} / \mathrm{h}$, and it carries approximately $25,000 \mathrm{vpd}$.

### 3.1.5 Wallgrove Road

Wallgrove Road is an arterial road that runs parallel to the M7 motorway, connecting Great Western Highway at its northern end and Elizabeth Drive at its southern end. Near the site, Wallgrove Road has four traffic lanes and on/off ramps to the M4 motorway. Wallgrove Road also provides connectivity with eastern suburbs via The Horsley Drive and western areas via Old Wallgrove Road. The posted speed is $70 \mathrm{~km} / \mathrm{h}$.

### 3.1.6 Ferrers Road

Ferrers Road is a regional road that runs in a north-south direction between Brabham Drive to the north of the Site to The Horsley Drive to the south of the Site. Ferrers Road provides a single traffic lane in each direction, and has a posted speed limit of $60 \mathrm{~km} / \mathrm{h}$.

### 3.1.7 Huntingwood Drive

Huntingwood Drive is a local (industrial) road that generally runs east-west between Brabham Drive and the Great Western Highway. Huntingwood Drive provides a single traffic lane in each direction and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$.

### 3.1.8 Brabham Drive

Brabham Drive is a local (industrial) road that runs north-south between Ferrers Road in the south and the GWH in the north (where is provides the southern approach to the intersection of GWH \& Doonside Road). Brabham Drive provides a single wide traffic lane in each direction, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$.

### 3.1.9 The Horsley Drive

The Horsley Drive is an arterial road that runs east-west near the intersection with Ferrers Road and provides two lanes in each direction. It provides key link between Eastern Creek and Hume Highway near Fairfield. The posted speed is $60 \mathrm{~km} / \mathrm{h}$ and it carries approximately $40,000 \mathrm{vpd}$.

### 3.2 Public Transport

### 3.2.1 Mode Share - Journey to Work Data

The online open data hub of Transport for New South Wales (TfNSW) provides Journey to Work (JTW) data, which is derived from the 5 -yearly Census of Population and Housing conducted by the Australian Bureau of Statistics (ABS). It includes data on trips related to employment as well as mode of travel to work. JTW data for the travel zone containing the Site is presented in Figure 6, noting that in summary the following mode share is reported:

- Vehicle (Driver and Passenger): 94\%;
- Public and Active Transport: 0\%; and
- Mode not stated: 6\%.

The high dependence on private vehicle trips is consistent with our observations and can be largely attributed to the relatively isolated location of the area, as well as a lack of public and active transport infrastructure in the area.


Figure 6: Journey to Work Data for the Subject Site

### 3.2.2 Bus Services

Busways bus services operate along Wallgrove Road to the west of the Site, and include the following routes:

- Route 738 Mount Druitt to Eastern Creek via Rooty Hill
- Route 723 Blacktown to Mount Druitt via Eastern Creek Business Park

Busways also operates services through the local industrial precinct to the north of the Site, including the following routes:

- Route 723 Blacktown to Mount Druitt via Huntingwood Drive and Brabham Drive
- Route 724 Blacktown loop service via Peter Brock Drive

These bus services operate approximately once every 30 minutes through the broader AM and PM peak periods.

It must be acknowledged that the walk distance between the Site and bus stops along these routes is outside of the 800 m walk distance, which is generally considered an acceptable walk distance as part of a trip to work. While the bus stops in Wallgrove Road are nearer the Site, there is no pedestrian infrastructure on the eastern side of Wallgrove Road, nor any potential to provide an appropriate pedestrian crossing in this vicinity by which to reach the northbound bus stop on the western side of Wallgrove Road.

In addition, if the general trip profile of industrial workers is considered - including work shifts often outside of public transport peak periods and the daily use of private vehicles (for work) - there is little potential for public transport to attract any significant work trips in the short term.

Conversely, in the medium to long term there are good opportunities to provide additional bus services linking to the LIBH. The most obvious route would be along Ferrers Road itself, potentially extending north to Mount Druitt or Blacktown, and south to Fairfield or Liverpool. The viability of such a future route would specifically depend upon further development along the Ferrers Road corridor (particularly to the south near Horsley Drive), noting that the available north-south routes to the east (Cumberland Highway) and west (Wallgrove Road) provide the more efficient sub-regional routes at this time.

### 3.3 Existing Traffic Flows

### 3.3.1 Traffic Survey Locations

Traffic surveys were undertaken in November 2017 (the 2017 surveys) at the key intersections north and south of the Site, including:

- Great Western Highway / Huntingwood Road;
- Great Western Highway / Brabham Drive / Doonside Road;
- Brabham Drive / Huntingwood Drive;
- Brabham Drive / Ferrers Road / Peter Brock Drive; and
- Ferrers Road / The Horsley Drive.

Furthermore, as part of this revised TIA, a revised traffic survey has been undertaken in October 2019 at the signalised intersection of Great Western Highway / Doonside Road / Brabham Drive (the 2019 survey) in response to TfNSW comments in consideration of the recent changes to that intersection. Accordingly, the base scenario SIDRA results undertaken as part of this TIA refers to the updated 2019 surveys at this intersection. Furthermore, it is also noted that the 2019 surveys included pedestrian counts at this intersection which have now been included in the modelled intersection.

The traffic survey data is provided in Appendix B.

### 3.4 Intersection Performance - Existing Conditions

Performance of the key intersections were assessed using SIDRA Intersection modelling.

It is noted that during Site visits undertaken by Ason Group through AM and PM peak periods, it was observed that queues at the key intersections detailed above did not "spill back" to any upstream intersections. As such, SIDRA modelling was carried out on isolated intersections.

SIDRA assessment of "Existing Conditions" refers to analysis of the surveyed peak hour traffic at each intersection under existing road geometries.

SIDRA Modelling outputs provide various performance parameters. The key parameters are:

- Average Vehicle Delay (AVD) - The AVD (or average delay per vehicle in seconds) for intersections provides a measure of the operational performance of an intersection and is used to determine an intersection's Level of Service. For signalised intersections, the AVD reported relates to the average of all vehicle movements through the intersection. For priority (Give Way, Stop \&

Roundabout controlled) intersections, the AVD reported is that for the movement with the highest AVD.

- Level of Service (LoS) - This is a comparative measure that provides an indication of the operating performance, based on AVD.

Table 4 provides a baseline for LoS assessment as recommended by the RMS Guide to Traffic Generating Developments.

Table 4: RMS Level of Service Summary

| Level of Service | Average Delay per Vehicle (secs/veh) | Traffic Signals, Roundabout | Give Way and Stop Signs |
| :---: | :---: | :---: | :---: |
| A | less than 14 | Good operation | Good operation |
| B | 15 to 28 | Good with acceptable delays \& spare capacity | Acceptable delays \& spare capacity |
| C | 29 to 42 | Satisfactory | Satisfactory, but accident study required |
| D | 43 to 56 | Operating near capacity | Near capacity \& accident study required |
| E | 57 to 70 | At capacity; at signals, incidents will cause excessive delays. Roundabouts require other control mode | At capacity, requires other control mode |
| F | More than 70 | Unsatisfactory and requires additional capacity. | Unsatisfactory and requires other control mode or major treatment. |

SIDRA layouts for these intersections are presented in the figures below.


Figure 7: GWH / Brabham Drive / Doonside Road - Existing Layout

It is noteworthy that this intersection has recently been upgraded as part of the RMS identified upgrade works which is discussed in the next section of this TIA.


Figure 8: GWH / Huntingwood Drive - Existing Layout


Figure 9: Brabham Drive / Huntingwood Drive - Existing Layout


Figure 10: Brabham Drive / Ferrers Road / Peter Brock Drive - Existing Layout


Figure 11: The Horsley Drive / Ferrers Road - Existing Layout

A summary of the SIDRA analysis of Existing Conditions is provided in Table 5; detailed SIDRA outputs are provided in Appendix C.

Table 5: Intersection Performance - Existing Conditions

| Intersection | Control Type | Period | Intersection Delay | Level of Service |
| :---: | :---: | :---: | :---: | :---: |
| Great Western Highway / <br> Doonside Road / <br> Brabham Drive | Signals | AM | 44 | D |
| Great Western Highway / <br> Huntingwood Drive | Signal | AM | PM | D |
| Brabham Drive / <br> Huntingwood Drive | Roundabout ${ }^{1}$ | PM | PM | A |
| Ferrers Road / <br> Brabham Drive / <br> Peter Brock Drive | Roundabout ${ }^{1}$ | PM | 14 | B |
| The Horsley Drive / <br> Ferrers Road | Signals | PM | 11 | A |

Note 1: Intersection delay / LoS for roundabouts, as well as other types of priority-controlled intersections, relates to Worst Movement result. For signalized intersections, reported delay relates to overall average intersection delay, weighted by turn volumes.

With reference to Table 5, the SIDRA analysis indicates that the key intersections currently operate satisfactorily under the existing baseline scenario.

## 4 Future Base Case

### 4.1 Background Traffic

### 4.1.1 Future Base Year

Further to the determination of an estimated construction completion date of 2026 for the LIBH, a forecast year of 2036 has been selected for the assessment of future conditions. Base 2036 traffic volumes (i.e. without the LIBH) were determined with reference to annual growth forecasts in the local road network, as described below.

### 4.1.2 Growth Rate for Background Traffic

In order to determine background traffic volumes for the Base 2036 forecast year, Ason Group has collated RMS traffic growth rates from the 2036 Sydney Traffic Forecasting Model (2036 STFM). It may be noted that "Link" growth rates reported in the 2036 STFM were the primary reference in determining turn volumes at respective approaches, while intersection growth rates (also reported in the 2036 STFM) were adopted where 'Link' rates were not available.

These growth rates were then applied to the traffic survey data to obtain 2036 traffic volume (Base 2036), again noting that these volumes do not include the potential traffic generation of the LIBH.

### 4.2 Recent and Planned Road Network Upgrades

RMS has identified a number of upgrade requirements within the local road network to appropriately accommodate forecast traffic flow increases within the broader sub-region. Recently installed and planned upgrades of specific relevance to the assessment of the LIBH are detailed in sections below.

### 4.2.1 Great Western Highway / Doonside Road / Brabham Drive

Recent upgrades at the Great Western Highway / Doonside Road / Brabham Drive includes:

- Widening of the Great Western Highway (from the central median) to provide additional right turn lanes for the movements from Great Western Highway to both Doonside Road and to Brabham Drive;
- Widening of the existing eastbound and westbound left turn slip lanes from Great Western Highway to both Doonside Road and to Brabham Drive and
- The introduction of signalised pedestrian crossings on both the Doonside Road and Brabham Drive approaches to Great Western Highway.

These upgrades are shown in Figure 12 and the modified intersection configuration is provided in Figure 13.


Figure 12: Recent Upgrades at Great Western Highway / Brabham Drive / Doonside Road


Figure 13: GWH / Brabham Drive / Doonside Road - Existing intersection

### 4.2.2 The Horsley Drive

Proposed upgrades along the Horsley Drive include:

- Widening of the existing road to a 4-lane divided carriageway road between the M7 Motorway and Cowpasture Road, to include a wide central median allowing for further widening to a 6-lane divided carriageway in the future;
- The provision of an additional eastbound lane from west of Ferrers Road to Cowpasture Road; and
- The construction of a pedestrian and cyclist shared path along the length of The Horsley Drive, connecting to the existing Western Sydney Parklands cycleway.


### 4.2.3 The Horsley Drive / Ferrers Road intersection

Potential proposed upgrades at the Horsley Drive / Ferrers Road intersection include:

- The provision of a left turn slip-lane from The Horsley Drive to Ferrers Road;
- The duplication of the right turn bays from The Horsley Drive to Ferrers Road; and
- The Duplication of the left-turn slip lane from Ferrers Road to The Horsley Drive.

These upgrades are presented in the Figure 14 while the modified SIDRA layout for testing the upgrade is provided in Figure 15.


Figure 14: Planned Upgrades to The Horsley Drive


Figure 15: The Horsley Drive / Ferrers Road - Existing and Future Layouts

It should be noted that during a recent meeting with RMS on 12 December 2019, RMS indicated that the planned upgrade of this intersection has not yet been funded and there is no committed timing for this upgrade. As a result, the Horsley Drive / Ferrers Road Intersection has additionally been modelled for the 2036 Base Case without upgrades.

### 4.3 Intersection Performance - 2036 Base Case

The key intersections were assessed in SIDRA for 2036 Base Case, which includes:

- background traffic volumes,
- as mentioned above, two options for the intersection of The Horsley Drive / Ferrers Road as follows:
- considering existing geometry,
- with planned upgrades and
- existing road geometry at the remaining intersections.

SIDRA results are summarised in the following tables, while detailed outputs are provided in Appendix C.

Table 6: Intersection Performance - 2036 Base

| Intersection | Control Type | Period | Intersection Delay | Level of Service |
| :---: | :---: | :---: | :---: | :---: |
| Great Western Highway / Doonside Road / Brabham Drive | Signals | AM | 50 | D |
|  |  | PM | 47 | D |
| Great Western Highway / Huntingwood Drive | Signals | AM | 11 | A |
|  |  | PM | 26 | B |
| Brabham Drive / Huntingwood Drive | Roundabout | AM | 15 | B |
|  |  | PM | 17 | B |
| Ferrers Road / Brabham Drive / Peter Brock Drive | Roundabout | AM | 13 | A |
|  |  | PM | 21 | B |
| The Horsley Drive / Ferrers Road (Existing Geometry) | Signals | AM | 177 | F |
|  |  | PM | 245 | F |
| The Horsley Drive / Ferrers Road (Planned Upgrades) | Signals | AM | 19 | B |
|  |  | PM | 21 | B |

With reference to Table 6, the SIDRA analysis indicates that the key intersections would operate satisfactorily under the 2036 Base scenario when the intersection of The Horsley Drive / Ferrers Road is upgraded as discussed previously. However, without the intersection upgrades, the Horsley Drive / Ferrers Road intersection performs at LoS F, exceeding capacity as a result of forecast background growth. With the exception of this intersection, the average delay and LoS does not significantly change when compared to the existing SIDRA results.

## 5 Project Case

### 5.1 Traffic Generation

### 5.1.1 Daily Vehicle Trips

The RMS Guide recommends daily vehicle trip rates of 4 per $100 \mathrm{~m}^{2}$ GFA for warehouse floorspace, and 10 trips per $100 \mathrm{~m}^{2}$ GFA for office floorspace.

Application of these trip rates to the Masterplan results in a daily trip generation of 7,078 vehicle trips per day.

### 5.1.2 Peak Hour Trips - Standard Use Assessment

The peak hour trip generation of the LIBH has been estimated with reference to the RMS Guide Update, which reports surveys of a number of large industrial developments; specifically, Ason Group has referenced the trip rates surveyed by the RMS at the following sites, which provide similarly land use profiles to the LIBH:

- Site 1: Erskine Park Industrial Estate, Erskine Park;
- $\quad$ Site 3: Wonderland Business Park, Eastern Creek; and
- $\quad$ Site 4: Riverwood Business Park, Riverwood.

With reference to the RMS Guide Update, the average AM and PM peak hour trip rates for these three sites are as follows:

- AM Rate 0.247 trip per $100 \mathrm{~m}^{2}$ of GFA.
- PM Rate 0.182 trip per $100 \mathrm{~m}^{2}$ of GFA.

With reference to the RMS Guide Update trip rates, and to provide a robust assessment, this assessment adopts trip rates that are conservatively higher than the average of the three sites mentioned above, as shown below, being:

- AM Rate: $\quad 0.25$ trip per $100 m^{2}$ of GFA
- PM Rate: $\quad 0.20$ trip per $100 \mathrm{~m}^{2}$ of GFA

Accordingly, the estimated maximum generation of the LIBH is summarised in Table 7.

Table 7: Summary of LIBH Traffic Generation
$\left.\begin{array}{ccccc}\hline \text { Land-use } & \text { GFA }\left(\mathrm{m}^{2}\right) & \begin{array}{c}\text { AM Trip Rate } \\ \left(\text { per } 100 \mathrm{~m}^{2} \text { of GFA) }\right.\end{array} & \begin{array}{c}\text { PM Trip Rate } \\ \left(\text { per } 100 \mathrm{~m}^{2} \text { of GFA) }\right.\end{array} & \begin{array}{c}\text { AM Trips } \\ (\mathrm{veh} / \mathrm{hr})\end{array}\end{array} \begin{array}{c}\text { PM Trips } \\ (\mathrm{veh} / \mathrm{hr})\end{array}\right]$

* Rounded up

With reference to Table 7, the LIBH is therefore estimated to generate up to 420 vehicle trips and 340 vehicle trips in the AM and PM peak hours respectively., noting that these totals represent two-way traffic flows.

### 5.1.3 Percentage of Heavy Vehicles

Further reference to the RMS Guide Update indicates that heavy vehicles constitute a significant percentage of the total trip generation of similar industrial sites; referring again to the surveys of the Eastern Creek and Erskine Park industrial sites provided in the RMS Guide Update, heavy vehicles (for example: B-Triples) made up $28 \%$ and $26 \%$ of the total peak hour vehicle flows respectively.

A heavy vehicle percentage of $28 \%$ has been adopted for the assessment.

### 5.2 Trip Distribution

### 5.2.1 Arrival and Departure Distribution

The arrival and departure distribution profile adopted for the assessment is based on past surveys and assessments of industrial sites across Western Sydney, being: -

- AM Peak Hour - 80\% arrival and 20\% departure
- PM Peak Hour - 20\% arrival and 80\% departure

Accordingly, the total number of inbound and outbound trips are as follows:

- AM Peak Hour - 336 in and 84 out
- PM Peak Hour - 68 in and 272 out


### 5.2.2 Directional Distribution - Journey to Work Data

The assignment of trips to the road network referenced the JTW data, and indicates the following direction distribution of trips:

- $54 \%$ of trips to/from the north-west (e.g. Mount Druitt, St Marys, Penrith);
- $20 \%$ of trips to/from the north (e.g. Blacktown);
- $20 \%$ of trips to/from the south (e.g. Campbelltown, Fairfield); and
- $6 \%$ of trips to/from east (e.g. Parramatta).


### 5.2.3 Route Choice Assumptions

A review of the most efficient travel routes between the LIBH and key metropolitan and regional centres was carried out to determine the assignment of trips to the available routes. In this regard, a total of eight (8) travel zones were identified (to which trips are generated to / from), as shown in Figure 16.


Figure 16: Travel Zones adopted for Trip Distribution

With reference to Figure 16, the following trip assignment assumptions were adopted based on JTW data (section 5.2.2) and Google travelling routes:

- All vehicles travelling to / from the north-west (54\%) were assigned to the western side of GWH (Zone 1 in Figure 16).
- For all vehicle trips travelling to / from the north (20\%), a $50-50$ split has been estimated between Doonside Road (Zone 2) and eastern side of GWH (Zone 3).
- Vehicles travelling to / from the south were further divided into two groups such as south-east (e.g. Fairfield) and south-west (e.g. Campbelltown) and assigned to different sides of The Horsley Drive. All vehicles to / from south-east (13\%) were assigned to zone 8, whereas those travelling to / from south-west (7\%) were assigned to zone 7.
- All vehicles traveling to and from the east (6\%) have been assigned on Ferrers Road via Peter Brock Drive (Zone 5).


### 5.3 Project Case Traffic Volumes

The LIBH traffic flows were added to the 2036 background traffic to form the "Project Case" traffic volumes, as presented in Appendix B.

### 5.4 SIDRA Layout of LIBH Access

The proposed roundabout at Ferrers Road and LIBH Access has been modelled as a single lane roundabout with two lanes (1 per direction) on each approach. It was estimated that the proposed roundabout will be located approximately 250 metres west of the Brabham Drive / Ferrers Road / Peter Brock Drive roundabout. The SIDRA layout of the proposed Ferrers Road / LIBH Access roundabout is shown in Figure 17.


Figure 17: LIBH Access at Ferrers Road - SIDRA Layout

### 5.5 Intersection Performance - 2036 Project Case

The operation of all key intersections has been assessed for "Project Case", which includes:

- project Case traffic volumes (2036 Background plus LIBH traffic, section 5.3);
- two options for the intersection of The Horsley Drive / Ferrers Road which includes with and without proposed upgrades (refer section 4.2);
- proposed layout for LIBH Access (section 5.4); and
- existing road geometry at the remaining intersections.

Table 8: SIDRA Results - Project Case

| Intersection | Control Type | Period | Intersection Delay | Level of Service |
| :---: | :---: | :---: | :---: | :---: |
| Great Western Highway / Doonside Road / Brabham Drive (Existing layout) | Signals | AM <br> PM | 56 <br> 53 | D <br> D |
| Great Western Highway / Huntingwood Drive | Signals | $\begin{aligned} & \text { AM } \\ & \text { PM } \end{aligned}$ | 12 27 | A B |
| Brabham Drive / Huntingwood Drive | Roundabout | AM <br> PM | 18 <br> 19 | B <br> B |
| Ferrers Road / Brabham Drive / Peter Brock Drive | Roundabout | AM <br> PM | 19 <br> 28 | B <br> B |
| The Horsley Drive / Ferrers Road (Existing Geometry) | Signals | AM <br> PM | $\begin{aligned} & 202 \\ & 246 \end{aligned}$ | F F |
| The Horsley Drive / Ferrers Rd (Planned Upgrades) | Signals | $\begin{aligned} & \text { AM } \\ & \text { PM } \end{aligned}$ | 20 <br> 26 | B B |
| Ferrers Road / LIBH Access | Roundabout | AM PM | 51 30 | D C |

As demonstrated, generally the results indicate similar performance to the 2036 Baseline Results in Table 6, with generally minor increases to intersection delay throughout. This is attributed to the relatively minor impact of development traffic volumes distributed to the network. Similarly, The Horsley

Drive / Ferrers Road intersection with existing geometry continues to perform at LoS F, prior to planned upgrades at that location; a result of forecast background traffic growth.

Table 9 below compares the total modelled demand flows of the 2036 Base and Project scenarios for the intersection.

Table 9: The Horsley Park / Ferrers Road Future Traffic Volumes

| Peak | 2036 Base | 2036 Project Case | \% Difference |
| :---: | :---: | :---: | :---: |
| AM | 4,361 |  |  |
|  | $(4,591)$ | 4,443 |  |
| $(4,677)$ | $+1.9 \%$ |  |  |
| PM | 5,006 | 5,070 | $+1.3 \%$ |

Note: Numbers above are modelling input volumes. Numbers in brackets denote modelled demand total flows as veh/hr.

The above table demonstrates that increased traffic volumes of the 2036 Project Case resultant from the development traffic are relatively insignificant, denoting an increase of only $1.9 \%$ and $1.3 \%$ in the respective AM and PM Peaks. This confirms that the future intersection performance remains largely attributed to background growth.

### 5.6 Interim Network Performance

With the exception of The Horsley Drive / Ferrers Road intersection, all intersections are deemed to operate satisfactorily under future 2036 conditions and do not rely upon upgrades. As such, assessment of 'interim' conditions is not considered necessary.

The Horsley Drive / Ferrers Road will also operate satisfactorily following completion of earmarked upgrades. However, with no funding or timing commitment to those upgrades, further consideration has been given to the interim performance of that intersection.

Sensitivity modelling has been undertaken to explore the impact of the addition of development traffic to the existing (surveyed) base volumes. A summary of these results is provided below.

Table 10: The Horsley Drive / Ferrers Road Results

|  |  | 2019 Existing Base | 2019 Project Case |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection | Period | Intersection Delay | Level of Service | Intersection Delay | Level of Service |
| The Horsley Drive <br> / Ferrers Road <br> (Existing <br> Geometry) | AM | 38 | C | 53 | D |

It is evident that the intersection will still operate satisfactorily, with LoS D during the AM Peak and the retention of the LoS B during the PM Peak.

Regardless, the proposed upgrades to The Horsley Drive / Ferrers Road intersection would readily accommodate both the future base and project case traffic volumes, as indicated in the SIDRA results above.

## 6 Parking Requirements

### 6.1 Proposed Car Parking Rates

SEPP (Western Sydney Parklands) 2009 states the following:

Clause 6A - Development control plans - A development control plan does not apply to the Western Sydney Parklands unless it is made by the Director-General.

As such, the provisions of the Blacktown City Council DCP do not strictly apply to the proposed development.

Notwithstanding, the SEPP does not provide alternative parking requirements and, as such, reference is made to Council's controls and the widely accepted RMS Guide to Traffic Generating Developments, the latter being adopted as relevant parking rates for numerous State Significant Development (SSD) concept plan approvals in the locality (Oakdale for example).

### 6.1.1 Council DCP Parking Requirement

Part A6 of the BCC DCP requires that car parking for general industries, warehouses and distribution centres across the LGA be provided at the rate of 1 space per $75 \mathrm{~m}^{2}$ GFA plus 1 space per $40 \mathrm{~m}^{2}$ for the office component of such development.

The application of these rates to the proposed development result in a significant theoretical car parking requirement of 2,292 spaces. In the opinion of Ason Group, this is a level of parking that is significantly in excess of the parking actually required for the LIBH, as detailed in sections below.

Furthermore, it is emphasised that the BCC DCP does not strictly apply and these figures are provided for information only.

### 6.1.2 RMS Guide Parking Requirement

Section 5.11 .2 of the RMS Guide requires parking for warehouse developments be provided at the rate of 1 space per $300 \mathrm{~m}^{2}$ of GFA.

The car parking rate of 1 space per $300 \mathrm{~m}^{2}$ adopted in the RMS Guide was established through surveys of 10 facilities. The surveys undertaken by the RMS demonstrated car parking requirements that ranged between one space per $80 \mathrm{~m}^{2}$ and one space per $960 \mathrm{~m}^{2}$ with a mean and standard deviation of one space per $338 \mathrm{~m}^{2}$ and one space per $280 \mathrm{~m}^{2}$ respectively. The adopted rate of 1 space per $300 \mathrm{~m}^{2}$ therefore reflected a "middle range" parking rate. Furthermore, the adopted parking rate was also based
on employee densities of approximately 45 employees per hectare - almost double the densities established by the DPIE for the WSEA.

### 6.1.3 Standard Use Demands Derived from Other Similar Developments

For the purpose of this assessment, Ason Group has undertaken surveys of eight comparable industrial developments to establish the effective parking rate of operational developments within the WSEA, surveys which have adopted the same methodology as that used in establishing the RMS Guide rates. The surveys included industrial developments (generally warehouse) in numerous locations including:

- Erskine Park,
- Oakdale Central; and
- M7 Business Hub.

The results of these surveys are summarised in Table 11.
Table 11: Effective Parking Rates for Surveyed Developments

| Site Address | Car Parking <br> Provided | Total GFA <br> $\left(\mathbf{m}^{2}\right)$ | Maximum <br> Parking <br> Demand | Effective <br> Parking Rate <br> $(1$ space per Xm$)$ |
| :--- | :---: | :---: | :---: | :---: |
| Bunning's - 8 Interchange Dr | 140 | 55,550 | 68 | 817 |
| Toll - Lot 11 Wonderland Dr | 137 | 27,440 | 47 | 584 |
| Ingram Micro - 23 Wonderland Dr | 300 | 36,610 | 183 | 200 |
| DHL - Milner Avenue | 115 | 20,170 | 109 | 185 |
| Kimberly Clarke - 35 Sarah Andrews | 100 | 45,210 | 78 | 580 |
| Cl | 217 | 51,200 | 116 | 441 |
| Linfox - 25 Sarah Andrews CI | 150 | 10,865 | 71 | 153 |
| Ubeeco - 28 Sarah Andrews CI | 280 | 52,705 | 197 | 268 |
| Woolworths - 29 Sarah Andrews CI |  |  |  | 403 |
| Total Average Rate |  |  |  |  |

The surveys demonstrated a range of between 1 space per $153 m^{2}$ and 1 space per $817 m^{2}$ with a mean and standard deviation of 1 space per $403 \mathrm{~m}^{2}$ and 1 space per $241 \mathrm{~m}^{2}$ respectively. Accordingly, based on the methodology adopted in the RMS Guide, the "middle range" car parking rate based on the surveys would be in the order of 1 space per $350 \mathrm{~m}^{2}$.

These rates are consistent with those established by the RMS Guide and indeed suggest that a reduction in overall car parking is justified in comparison to the parking rates provided in the BCC DCP. Furthermore, as mentioned above, these rates are consistent with other approved developments within the broader area. For example, the industrial precincts of Oakdale South and Oakdale West to the west of the Site which provide similar development to this SSDA.

### 6.2 Proposed Parking Provision

Having regard for the above, it is recommended that the car parking rates as approved in the Oakdale South be adopted as minimum requirement. The proposed car parking rates are outlined Table 12.

Table 12: Proposed Warehouse Car Parking Rates

| Land Use | Minimum Car Parking Rate |
| :---: | :---: |
| Warehouse / Distribution | 1 space per $300 \mathrm{~m}^{2}$ |
| Office | 1 space per $40 \mathrm{~m}^{2}$ |

The adoption of a minimum rate of 1 space per $300 \mathrm{~m}^{2}$ GFA for warehouse floorspace and 1 space per $40 \mathrm{~m}^{2}$ for office floorspace is considered appropriate and sustainable and is consistent with both the RMS Guidelines and State planning policies. The proposed minimum rates will also enable the required flexibility in the design of future developments whilst still ensuring that parking is provided to accommodate both the current and future parking requirements of tenants. For all other non-warehouse uses, it is proposed that parking be provided in accordance with the BCC DCP.

The specific car parking requirements for each lot/building within the Site would be considered in more detail at the relevant DA stages. However, based on the current master plan, these rates can be readily satisfied.

It is noted that the Disability (Access to Premises - Buildings) Standards 2010 require accessible car parking spaces be provided at the following rate for Class $5,7,8$ and 9 c buildings:

- 1 accessible space for every 100 car parking spaces, or part thereof

It is assumed that any subsequent applications will demonstrate a satisfactory provision of accessible car parking is provided.

Finally, it is expected that a Condition of Consent in regard to future applications would require that all car parking and service vehicle areas be designed in accordance with the relevant Australian Standards including, AS2890.1 AS 2890.2 and AS2890.6.

## 7 Preliminary Construction Traffic Management Plan

A detailed Construction Traffic Management Plan (CTMP) will be provided as part of detailed construction phase planning, once a builder is appointed. For the purposes of this TIA, the following general principles for managing construction traffic have been assumed and provide an understanding of the likely traffic impacts during the construction period. It should be noted that the construction programme for the development has not yet been finalised.

### 7.1 Haulage Routes

The primary potential haulage route to and from the Site would be via Wallgrove Road, with trucks accessing the Site from the M7 Motorway from the north and via Great Western Highway or Western Motorway. M7 is also anticipated to be the primary arterial route to provide access for construction vehicles via Horsley Drive interchange to/from the south of the Site. Given that these routes currently carry high volumes of heavy vehicles, construction of the development would not have a significant impact on the performance of these roads. The movement of materials shall be managed through the scheduling of deliveries and would aim to minimise, as far as practicable, the number of heavy vehicles accessing the Site during peak network periods and weekends. Furthermore, it is important to note that the Wallgrove Road currently provides a left turn deceleration lane into the existing access point connecting the M7 underpass running towards the Site which provides further safety for the construction vehicle accessibility. In this regard reference should be made to Figure 18.


Figure 18: Wallgrove Road Deceleration Lane - Looking South
Once the Ferrers Road access road is complete, it is expected that construction traffic will then also benefit from that access point.

Construction periods generating more than 20 heavy vehicle movements per day shall include:

- Vehicle Movement Plan (VMP) showing access routes
- Suitable Traffic Control Plan (TCPs), prepared by a person with Traffic Control at Worksites to safely manage access to the site.


### 7.2 Proposed Working Hours

Construction works will vary depending on the phase of construction and associated activities and includes both construction and design personnel. The size of the on-site workforce has not been finalised and as a result, the peak working population on-site at any given time during the construction period may vary. Construction works would be undertaken during standard construction-working hours, which are likely to be as follows:

- Monday to Friday:
- Saturday:
- Sunday and Public holidays: No planned work.

It may (on occasions) be necessary to undertake night works to minimise disruption to traffic.

### 7.3 Construction Traffic Generation

Light vehicle traffic generation would be generally associated with staff movements to and from the Site. Staff would be comprised of project managers, various trades and general construction staff. Over the full construction period, the peak workforce represents the worst-case scenario for vehicle movements during the morning or evening road network peak hour. The workforce arrival and departure periods (6.30-7.00AM and $5.00-5.30 \mathrm{PM}$ ) represent the peak construction traffic generation periods.

Light vehicle construction trips are expected to arrive in the morning and depart in the evening and the number of trips would be based on the workforce numbers. Parking for all construction related-vehicles shall be provided wholly on-site.

Heavy vehicle traffic would mainly be generated by activities associated with the delivery of construction equipment and delivery of material for construction works. As the construction programme has yet to be finalised, a worst-case scenario for heavy vehicle movements per day required for the delivery of construction materials to the Site cannot be accurately determined. However, these deliveries are likely to occur outside of the peak network traffic periods and would have limited (if any) impact to traffic on the surrounding major road network.

Importantly, the construction traffic volumes are expected to be lower than the volumes anticipated for the Proposal once it becomes operational. Therefore, recognising that the key intersections are anticipated to perform satisfactorily once the Proposal is completed, it can be assumed that the intersection would satisfactorily accommodate the lower volumes of construction traffic.

Furthermore, it is expected that suitable TCPs shall be prepared to safely manage site access for any periods generating more than 20 heavy vehicle movements per day, in accordance with the Traffic Control at Worksites Manual.

### 7.4 Construction Mitigation Measures

While the traffic impacts of construction of the development are likely to be negligible, the following measures shall be undertaken to minimise the impacts of the construction activities of the development:

- Traffic control would be required at the site access (including the existing Wallgrove Road access point and the M7 underpass) to manage and regulate traffic movements into and out of the site during construction.
- Disruption to road users would be kept to a minimum by scheduling intensive delivery activities outside of peak network hours.
- Construction and delivery vehicles shall be restricted from using residential roads in the locality. Given the nature of the locality, this is not expected to cause undue impact on construction vehicle access.


### 7.5 Relevant Documents

As discussed before, a construction management plan has been prepared by Western Sydney Parkland Trust in March 2019 which provides preliminary information regarding the infrastructure and earthworks of the Proposal. Reference can also be made to this document as necessary.

## 8 Conclusions

- Western Sydney Parklands Trust has engaged Ason Group to prepare a Traffic Impact Assessment (TIA) to examine the access, traffic and parking characteristics of a SSDA providing for the development of the Light Horse Interchange Business Hub (LIBH) at 165 Wallgrove Road and 475 Ferrers Road, Eastern Creek.
- This revised report (RtS TIA) has been updated in response to the matters raised as part of the initial submission of the SSDA. Of note, this revised TIA includes:
- updated assessment of the Great Western Highway / Doonside Road / Brabham Drive having regard for more recent traffic surveys in 2019.
- further detail in relation to construction impacts and traffic management measures.
- updated assessment of The Horsley Drive / Ferrers Road intersection having regard for recent advice provided by RMS in December 2019.
- The SSDA provides for -
- A Masterplan development providing a regional warehousing and distribution hub with 24 hours/day, 7 days/week operation.
- A total yield of $165,500 \mathrm{~m}^{2}$ GFA, including $157,600 \mathrm{~m}^{2}$ of warehouse floorspace and $7,900 \mathrm{~m}^{2}$ of ancillary office floorspace;
- Site access connections to Ferrers Road (LIBH Access) forming a single-lane roundabout. The existing Wallgrove Road access is to be maintained for emergency vehicle access only;
- In conjunction with broader upgrades to the local road network, localised upgrades along the key access routes to/from the Site;
- A sustainable level of on-site parking provision; and
- Shared pedestrian and cyclist access from Wallgrove Road and Ferrers Road (3.5m and 2.5m wide concrete footpath, respectively), as well as internal pedestrian path along eastern side of LIBH access road ( 1.2 m wide concrete footpath).
- Traffic surveys were undertaken at the key intersections providing access between the Site and the sub-regional road network, including:
- Great Western Highway / Huntingwood Road (November 2017 and October 2019);
- Great Western Highway / Brabham Drive / Doonside Road (November 2017);
- Brabham Drive / Huntingwood Drive (November 2017);
- Brabham Drive / Ferrers Road / Peter Brock Drive (November 2017); and
- Ferrers Road / The Horsley Drive (November 2017).
- Background traffic growth at the key intersection through to a future forecast year of 2036 was determined with reference to the RMS 2036 STFM outputs.
- The traffic generation of the LIBH was determined with reference to the RMS Guide and RMS Guide Update, as well as relevant survey data of other similar developments. Trip distribution was determined with reference to Journey-to-Work data.
- SIDRA intersection analysis was undertaken to measure the performance of the key intersections during the AM and PM peak hours for the following scenarios:
- Existing Conditions,
- 2036 Base Case (background traffic with and without planned upgrades at the intersection of The Horsley Drive / Ferrers Road), and
- Project Case (2036 background plus development traffic, with planned upgrades).
- The SIDRA modelling outcomes can be summarised as:
- LIBH Access: The proposed one-lane roundabout at Ferrers Road is expected to operate at acceptable Level of Service (or LoS) during both peak periods.
- All key local intersections will operate at a LoS D or better during both peak hours through 2036 even with the introduction of the LIBH traffic flows and considering planned upgrades at the intersection of The Horsley Drive / Ferrers Road.
- As such, no additional modification of these intersections beyond the anticipated upgrades are required.
- Planned upgrades to The Horsley Drive / Ferrers Road are required as a result of forecast background traffic growth and not directly as a result of this development. In the short-term, prior to realisation of that forecast background growth, there is sufficient spare capacity to accommodate development traffic without upgrades; Existing Project Case (2019 surveys + development) modelling resulting in a LoS $D$ and $B$ during $A M$ and $P M$ peak periods, respectively.
- It is proposed that minimum car parking rates - based on the RMS Guide and detailed parking surveys undertaken by Ason Group - be adopted for the LIBH. The application of these rates being 1 space per $300 \mathrm{~m}^{2}$ GFA for warehouse floorspace and 1 space per $40 \mathrm{~m}^{2}$ GFA for office floorspace.
- It is expected that any future development applications will demonstrate a satisfactory provision of car parking (including accessible car parking) and that Conditions of Consent relating to future development applications shall require that all car parking and service vehicle areas be designed in accordance with the relevant Australian Standards.
- Construction traffic volumes will be less than the future operational traffic and, therefore, will not have an unacceptable impact on the surrounding road network. A detailed and comprehensive Construction Traffic Management Plan (CTMP) is expected to be prepared prior to construction that identifies further pedestrian and traffic management measures, as necessary, in response to the further development of the construction methodology.

It is therefore concluded that the Light Horse Interchange Business Hub is supportable on traffic planning grounds.

## Appendix A

Secretary's Environmental Assessment Requirements

## Planning Secretary's Environmental Assessment Requirements

## Section 4.12(8) of the Environmental Planning and Assessment Act 1979 Schedule 2 of the Environmental Planning and Assessment Regulation 2000

| Application Number | SSD 9667 |
| :---: | :---: |
| Project Name | Light Horse Interchange Business Hub, Eastern Creek |
| Development | - concept proposal for the staged redevelopment of the site as an industrial business hub with approximately 157,000 sqm of industrial and light industrial floorspace and 8,000 sqm ancillary office floorspace <br> - detailed proposal for the first stage of development which will include demolition works, bulk earthworks, installation of infrastructure and subdivision of the site |
| Location | Lot 10 in DP 1061237 and Lot 5 in DP 804051, Eastern Creek within Blacktown Local Government Area |
| Applicant | Western Sydney Parklands Trust |
| Date of Issue | 7 November 2018 |
| General Requirements | The environmental impact statement (EIS) must be prepared in accordance with, and meet the minimum requirements of, clauses 6 and 7 of Schedule 2 of the Environmental Planning and Assessment Regulation 2000 (the Regulation). In addition, the EIS must include: <br> - a detailed description of the development, including: <br> - the need for the proposed development <br> - justification for the proposed development <br> - likely staging of the development <br> - likely interactions between the development and existing, approved and proposed operations in the vicinity of the site <br> - plans of any proposed building works <br> - consideration of all relevant environmental planning instruments, including identification and justification of any inconsistencies with these instruments <br> - a risk assessment of the potential environmental impacts of the development, identifying the key issues for further assessment <br> - a detailed assessment of the key issues specified below, and any other significant issues identified in this risk assessment, which includes: <br> - a description of the existing environment, using sufficient baseline data <br> - an assessment of the potential impacts of all stages of the development, including any cumulative impacts, taking into consideration relevant guidelines, policies, plans and statutes <br> - a description of the measures that would be implemented to avoid, minimise, mitigate and if necessary, offset the potential impacts of the development, including proposals for adaptive management and/ or contingency plans to manage significant risks to the environment <br> - a consolidated summary of all the proposed environmental management and monitoring measures, highlighting commitments included in the EIS. <br> The EIS must also be accompanied by a report from a qualified quantity surveyor providing: |


| - a detailed calculation of the capital investment value (CIV) (as defined |
| :--- | :--- |
| in clause 3 of the Regulation) of the proposal, including details of all |
| assumptions and components from which the CIV calculation is |
| derived. The report shall be prepared on company letterhead and |
| indicate applicable GST component of the CIV |
| an estimate of jobs that will be created during the proposed |
| and |
| development |
| certification that the information provided is accurate at the date of |
| preparation. |$|$

- demonstrate that sufficient pedestrian and cyclist facilities have been provided for the development
- details and a justification of access to, from and within the site (vehicular and pedestrian)
- details of road upgrades, new roads or access points required for the development, if necessary.
- Contamination - including:
- a detailed assessment of the extent and nature of any contamination of the soil, groundwater and soil vapour
- an assessment of potential risks to human health and the environmental receptors in the vicinity of the site
- a description and appraisal of any mitigation and monitoring measures
- consideration of whether the site is suitable for the proposed development.
- Flooding - a detailed hydrological and hydraulic assessment which includes the following:
- a comprehensive assessment of the impact of flooding on the development for the full range of flood events up to the probable maximum flood. This assessment should address any relevant provisions of the NSW Floodplain Development Manual (2005) including the potential effects of climate change, sea level rise and an increase in rainfall intensity
- consideration of current flooding behaviour and impacts, including on flood detention areas, how flood behaviour and impacts will change due to the proposal and how these changes will be mitigated
- assessment of the impact of the development on flood behaviour (i.e., levels, velocities and duration of flooding) and on adjacent, downstream and upstream areas
- detail an emergency response plan for the site, which includes consideration of a flood-free access to or from the development site in extreme flood events.
- Hazards and Risk - including:
- a preliminary risk screening completed in accordance with State Environmental Planning Policy No. 33 - Hazardous and Offensive Development and Applying SEPP 33 (DoP, 2011), with a clear indication of class, quantity and location of all dangerous goods and hazardous materials associated with the development. Should the preliminary risk screening indicate that the development is "potentially hazardous", a Preliminary Hazard Analysis (PHA) must be prepared in accordance with Hazardous Industry Planning Advisory Paper No. 6 - Guidelines for Hazard Analysis (DoP, 2011) and Multi-Level Risk Assessment (DoP, 2011)
- ongoing consultation with Jemena on the high-pressure gas pipeline adjacent to the development area with regards to requirements of Australian Standard AS 2885 Pipelines - Gas and liquid petroleum
- a hazard analysis undertaken in accordance with the Department of Planning's Hazardous Industry Planning Advisory Paper No. 6, 'Hazard Analysis' and Multi-Level Risk Assessment (DoP, 2011). It must include, and not be limited to, an assessment on risk exposures to potential populations within the development from the high-pressure gas pipeline located within or near the development area. The risks established in the hazard analysis must be compared against the relevant qualitative and quantitative risk criteria detailed in the Department of Planning's Hazardous Industry Planning Advisory Paper No. 10, 'Land Use Safety Planning'. If a Safety Management Study (SMS) required under AS

|  | 2885 Pipelines - Gas and liquid petroleum is available, the SMS must be included in the hazard analysis. <br> Soils and Water - including: <br> - a description of the water demands and a breakdown of water supplies, including a detailed site water balance <br> - identification of any water licensing requirements under the Water Act 1912 or Water Management Act 2000 <br> - details of proposed erosion and sediment controls during construction <br> - an assessment of potential impacts on surface and groundwater resources, drainage patterns, soil (stability, salinity and acid sulfate soils), related infrastructure, watercourses and riparian land and proposed mitigation, management and monitoring measures. <br> - Biodiversity - including an assessment of the proposal's biodiversity impacts in accordance with the Biodiversity Conservation Act 2016, including the preparation of a Biodiversity Development Assessment Report (BDAR) where required under the Act, except where a waiver for preparation of a BDAR has been granted. <br> - Infrastructure Requirements - including: <br> - a detailed written and/or geographical description of infrastructure required on the site <br> - identification of any infrastructure upgrades required off-site to facilitate the development, and describe any arrangements to ensure that the upgrades will be implemented in a timely manner and maintained <br> - an infrastructure delivery and staging plan, including a description of how infrastructure on and off-site will be co-ordinated and funded to ensure it is in place prior to the commencement of construction <br> - an assessment of the impacts of the development on existing infrastructure surrounding the site. <br> Urban Design and Visual - including: <br> - consideration of the layout and design of the development having regard to the surrounding vehicular, pedestrian and cycling networks <br> - detailed plans showing suitable landscaping which incorporates endemic species. <br> - Heritage - including an Aboriginal Cultural Heritage Assessment Report prepared in consultation with Aboriginal people and in accordance with Office of Environment and Heritage guidelines. <br> - Noise and Vibration- including: <br> - a quantitative noise and vibration impact assessment undertaken by a suitably qualified person in accordance with the relevant Environment Protection Authority guidelines and including an assessment of nearby sensitive receivers <br> - cumulative impacts of other developments <br> - details of proposed mitigation, management and monitoring measures. <br> - Bushfire - including an assessment against the requirements of Planning for Bushfire Protection 2006, particularly access and provision of water supply for firefighting purposes. <br> - Waste - including: <br> - details of the quantities and classification of all waste streams to be generated on site during the development <br> - details of waste storage, handling and disposal during the development and <br> - details of the measures that would be implemented to ensure that the development is consistent with the aims, objectives and |
| :---: | :---: |


|  | guidance in the NSW Waste Avoidance and Resource Recovery Strategy 2014-2021. <br> - Air Quality - including: <br> - an assessment of the air quality impacts (including dust) during the development, in accordance with the relevant Environment Protection Authority guidelines <br> - details of proposed mitigation, management and monitoring measures. |
| :---: | :---: |
| Plans and Documents | The EIS must include all relevant plans, architectural drawings, diagrams and relevant documentation required under Schedule 1 of the Regulation. You should provide these as part of the EIS rather than as separate documents. |
| Consultation | During the preparation of the EIS, you must consult with the relevant local, State or Commonwealth Government authorities, service providers, community groups and affected landowners. <br> In particular you must consult with: <br> - Blacktown City Council <br> - Jemena Gas Networks <br> - Roads and Maritime Services <br> - Transport for NSW <br> - Department of Industry - Crown Lands and Water <br> - Office of Environment and Heritage <br> - Environment Protection Authority <br> - Fire and Rescue NSW <br> - Rural Fire Service <br> - Sydney Water <br> - WaterNSW <br> - surrounding local residents and stakeholders <br> - any other public transport, utilities or community service providers. <br> The EIS must describe the consultation process and the issues raised and identify where the design of the development has been amended in response to these issues. Where amendments have not been made to address an issue, a short explanation should be provided. |
| Further consultation after 2 years | If you do not lodge a Development Application and EIS for the development within 2 years of the issue date of these SEARs, you must consult further with the Secretary in relation to the preparation of the EIS. |
| References | The assessment of the key issues listed above must take into account relevant guidelines, policies, and plans as identified. While not exhaustive, the following attachment contains a list of some of the guidelines, policies, and plans that may be relevant to the environmental assessment of this proposal. |

## Appendix B

Traffic Diagrams

B1:
Existing Traffic (Surveyed)



B2:
2036 Background Traffic



B3:
Development Trafific



## B4:

2036 Background plus Development Traffic



Appendix C
SIDRA Results

C1:
Existing Conditions

## USER REPORT FOR SITE

## Project: [0541] GWH_Doonside Road_Brabham Drive

## 目 Site: 1 [[2019 Existing_AM] Doonside x GWH x Brabham]

Doonside Road x Great Western Highway x Brabham Drive Intersection, Eastern Creek
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time)
Variable Sequence Analysis applied. The results are given for the selected output sequence.
Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Green Split Priority has been specified
Phase Sequence: Standard Diamond (VV1120)
Reference Phase: Phase A
Input Phase Sequence: G, G1*, G2*, A, B*, C*, D, D1*, D2*, E, F1*, F2*
Output Phase Sequence: G, G2*, A, D, E
(* Variable Phase)

Site Layout


Input Volumes

Volume Display Method: Total and Veh

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | $\begin{aligned} & \text { Lane } \\ & \text { Util. } \\ & \% \end{aligned}$ | Average Delay sec | Level of Service | 95\% Back Veh | Queue Dist m | Lane Config | Lane Length m | Cap. <br> Adj. <br> \% | Prob. Block. \% |
| South: Brabham Drive (380m) min |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 245 | 18.9 | 645 | 0.380 | 100 | 30.2 | LOS C | 10.2 | 83.1 | Full | 380 | 0.0 | 0.0 |
| Lane 2 | 260 | 8.9 | 684 | 0.380 | 100 | 29.2 | LOS C | 11.0 | 83.1 | Full | 380 | 0.0 | 0.0 |
| Lane 3 | 153 | 12.4 | 196 | 0.779 | 100 | 66.9 | LOS E | 9.4 | 73.2 | Short | 50 | 0.0 | NA |
| Approach | 658 | 13.4 |  | 0.779 |  | 38.3 | LOS C | 11.0 | 83.1 |  |  |  |  |
| East: Great Western Highway (1600m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 129 | 12.2 | 862 | 0.150 | 100 | 19.2 | LOS B | 3.4 | 26.0 | Short | 215 | 0.0 | NA |
| Lane 2 | 145 | 10.3 | 196 | 0.742 | 100 | 60.2 | LOS E | 8.8 | 67.3 | Short | 135 | 0.0 | NA |
| Lane 3 | 147 | 10.3 | 198 | 0.742 | 100 | 60.2 | LOS E | 8.9 | 68.0 | Full | 1600 | 0.0 | 0.0 |
| Lane 4 | 147 | 10.3 | 198 | 0.742 | 100 | 60.2 | LOS E | 8.9 | 68.0 | Full | 1600 | 0.0 | 0.0 |
| Lane 5 | 95 | 7.2 | 133 | 0.711 | 100 | 70.8 | LOS F | 5.9 | 43.5 | Short | 125 | 0.0 | NA |
| Lane 6 | 95 | 7.2 | 133 | 0.711 | 100 | 70.8 | LOS F | 5.9 | 43.5 | Short | 120 | 0.0 | NA |
| Approach | 758 | 9.9 |  | 0.742 |  | 55.8 | LOS D | 8.9 | 68.0 |  |  |  |  |
| North: Doonside Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 583 | 9.7 | 737 | 0.790 | 100 | 39.2 | LOS C | 30.4 | 230.8 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 479 | 5.8 | $607^{1}$ | 0.790 | 100 | 37.6 | LOS C | 24.6 | 180.9 | Full | 500 | 0.0 | 0.0 |
| Lane 3 | 132 | 9.6 | 204 | 0.646 | 100 | 63.9 | LOS E | 7.7 | 58.5 | Short | 70 | 0.0 | NA |
| Lane 4 | 130 | 9.6 | 202 | 0.646 | 100 | 64.0 | LOS E | 7.6 | 58.0 | Short | 60 | 0.0 | NA |
| Approach | 1324 | 8.3 |  | 0.790 |  | 43.6 | LOS D | 30.4 | 230.8 |  |  |  |  |
| West: Great Western Highway (390m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 521 | 9.1 | 1242 | 0.420 | 100 | 11.6 | LOS A | 9.3 | 70.3 | Short | 150 | 0.0 | NA |
| Lane 2 | 294 | 8.5 | 436 | 0.675 | $85^{6}$ | 45.5 | LOS D | 15.8 | 118.9 | Full | 390 | 0.0 | 0.0 |
| Lane 3 | 345 | 8.5 | 436 | 0.791 | 100 | 50.3 | LOS D | 20.1 | 151.1 | Full | 390 | 0.0 | 0.0 |
| Lane 4 | 341 | 8.5 | 431 | 0.791 | 100 | 50.3 | LOS D | 19.9 | 149.7 | Full | 390 | 0.0 | 0.0 |
| Lane 5 | 262 | 7.6 | 354 | 0.740 | 100 | 58.4 | LOS E | 15.1 | 112.4 | Short | 145 | 0.0 | NA |
| Lane 6 | 262 | 7.6 | 354 | 0.740 | 100 | 58.4 | LOS E | 15.1 | 112.4 | Short | 140 | 0.0 | NA |
| Approach | 2025 | 8.4 |  | 0.791 |  | 41.8 | LOS C | 20.1 | 151.1 |  |  |  |  |
| Intersection | 4765 | 9.3 |  | 0.791 |  | 44.0 | LOS D | 30.4 | 230.8 |  |  |  |  |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Lane LOS values are based on average delay per lane.
Intersection and Approach LOS values are based on average delay for all lanes.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
1 Reduced capacity due to a short lane effect. Short lane queues may extend into the full-length lanes. Some upstream delays at entry to short lanes are not included.
6 Lane under-utilisation due to downstream effects

## 目Site: 1 [[2019 Existing_PM] Doonside x GWH x Brabham]

Doonside Road x Great Western Highway x Brabham Drive Intersection, Eastern Creek
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time)
Variable Sequence Analysis applied. The results are given for the selected output sequence.
Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Green Split Priority has been specified
Phase Sequence: Standard Diamond (VV1120)
Reference Phase: Phase A
Input Phase Sequence: G, G1*, G2*, A, B*, C*, D, D1*, D2*, E, F1*, F2*
Output Phase Sequence: G, G1*, A, D, D2*, E
(*Variable Phase)

## Site Layout



| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. $\%$ | Average Delay sec | Level of Service | 95\% Bac <br> Veh | Queue Dist $m$ | Lane Config | Lane Length m | Cap. Adj. \% | Prob. Block. \% |
| South: Brabham Drive (380m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 517 | 4.6 | 666 | 0.776 | 100 | 40.1 | LOS C | 27.4 | 199.2 | Full | 380 | 0.0 | 0.0 |
| Lane 2 | 438 | 2.5 | $565{ }^{1}$ | 0.776 | 100 | 37.5 | LOS C | 22.5 | 160.9 | Full | 380 | 0.0 | 0.0 |
| Lane 3 | 115 | 4.6 | 221 | 0.519 | 100 | 60.3 | LOS E | 6.5 | 47.2 | Short | 50 | 0.0 | NA |
| Approach | 1071 | 3.7 |  | 0.776 |  | 41.2 | LOS C | 27.4 | 199.2 |  |  |  |  |
| East: Great Western Highway (1600m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 122 | 7.8 | 1186 | 0.103 | 100 | 11.7 | LOS A | 1.9 | 14.0 | Short | 215 | 0.0 | NA |
| Lane 2 | 347 | 6.1 | 448 | 0.773 | 100 | 48.5 | LOS D | 19.8 | 146.2 | Short | 135 | 0.0 | NA |
| Lane 3 | 350 | 6.1 | 453 | 0.773 | 100 | 48.4 | LOS D | 20.0 | 147.6 | Full | 1600 | 0.0 | 0.0 |
| Lane 4 | 350 | 6.1 | 453 | 0.773 | 100 | 48.4 | LOS D | 20.0 | 147.6 | Full | 1600 | 0.0 | 0.0 |
| Lane 5 | 182 | 3.2 | 304 | 0.597 | 100 | 58.3 | LOS E | 10.1 | 72.3 | Short | 125 | 0.0 | NA |
| Lane 6 | 182 | 3.2 | 304 | 0.597 | 100 | 58.3 | LOS E | 10.1 | 72.3 | Short | 120 | 0.0 | NA |
| Approach | 1533 | 5.6 |  | 0.773 |  | 47.8 | LOS D | 20.0 | 147.6 |  |  |  |  |
| North: Doonside Road ( 500 m ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 379 | 6.7 | 736 | 0.515 | 100 | 33.6 | LOS C | 16.7 | 123.4 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 354 | 5.3 | 688 | 0.515 | 100 | 33.0 | LOS C | 16.1 | 118.0 | Full | 500 | 0.0 | 0.0 |
| Lane 3 | 193 | 10.4 | 246 | 0.782 | 100 | 65.4 | LOS E | 11.8 | 89.7 | Short | 70 | 0.0 | NA |
| Lane 4 | 191 | 10.4 | 244 | 0.782 | 100 | 65.5 | LOS E | 11.6 | 88.8 | Short | 60 | 0.0 | NA |
| Approach | 1117 | 7.5 |  | 0.782 |  | 44.3 | LOS D | 16.7 | 123.4 |  |  |  |  |
| West: Great Western Highway ( 390 m ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 314 | 13.1 | 985 | 0.318 | 100 | 17.0 | LOS B | 7.9 | 61.6 | Short | 150 | 0.0 | NA |
| Lane 2 | 143 | 4.2 | 272 | 0.525 | $85^{6}$ | 52.6 | LOS D | 7.9 | 57.5 | Full | 390 | 0.0 | 0.0 |
| Lane 3 | 167 | 4.2 | 272 | 0.615 | 100 | 53.5 | LOS D | 9.4 | 68.4 | Full | 390 | 0.0 | 0.0 |
| Lane 4 | 165 | 4.2 | 269 | 0.615 | 100 | 53.5 | LOS D | 9.3 | 67.7 | Full | 390 | 0.0 | 0.0 |
| Lane 5 | 83 | 15.8 | 112 | 0.744 | 100 | 72.9 | LOS F | 5.2 | 41.7 | Short | 145 | 0.0 | NA |
| Lane 6 | 83 | 15.8 | 112 | 0.744 | 100 | 72.9 | LOS F | 5.2 | 41.7 | Short | 140 | 0.0 | NA |
| Approach | 955 | 9.2 |  | 0.744 |  | 44.8 | LOS D | 9.4 | 68.4 |  |  |  |  |
| Intersection | 4675 | 6.3 |  | 0.782 |  | 44.9 | LOS D | 27.4 | 199.2 |  |  |  |  |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Lane LOS values are based on average delay per lane.
Intersection and Approach LOS values are based on average delay for all lanes.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
1 Reduced capacity due to a short lane effect. Short lane queues may extend into the full-length lanes. Some upstream delays at entry to short lanes are not included.
6 Lane under-utilisation due to downstream effects

## MOVEMENT SUMMARY

## Site: 2 [Huntingwood x GWH_Existing_AM]

Huntingwood Drive x Great Western Highway T-Intersection, Huntingwood
Road Conditions: 2018 Existing
Traffic: 2018 AM Base
Signals - Fixed Time Isolated Cycle Time $=66$ seconds (Optimum Cycle Time - Minimum Delay) Variable Sequence Analysis applied. The results are given for the selected output sequence.

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Huntingwood Drive (1800m) |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 19 | 50.0 | 0.706 | 37.2 | LOS C | 3.4 | 29.8 | 1.00 | 0.88 | 54.3 |
| 3 | R2 | 192 | 22.5 | 0.706 | 39.5 | LOS C | 3.6 | 30.4 | 1.00 | 0.87 | 49.4 |
| Appr |  | 211 | 25.0 | 0.706 | 39.3 | LOS C | 3.6 | 30.4 | 1.00 | 0.88 | 49.9 |
| East: Great Western Highway ( 780 m ) |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 482 | 10.0 | 0.278 | 7.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.60 | 73.2 |
| 5 | T1 | 715 | 8.8 | 0.355 | 9.1 | LOS A | 6.5 | 49.0 | 0.60 | 0.52 | 73.8 |
| Appr |  | 1197 | 9.3 | 0.355 | 8.6 | LOS A | 6.5 | 49.0 | 0.36 | 0.55 | 73.5 |
| West: Great Western Highway ( 1600 m ) |  |  |  |  |  |  |  |  |  |  |  |
| 11 | T1 | 1973 | 7.0 | 0.727 | 5.6 | LOS A | 18.4 | 136.4 | 0.63 | 0.58 | 76.0 |
| 12 | R2 | 45 | 18.6 | 0.304 | 40.1 | LOS C | 1.5 | 12.0 | 0.97 | 0.74 | 55.1 |
| Approach |  | 2018 | 7.3 | 0.727 | 6.4 | LOS A | 18.4 | 136.4 | 0.64 | 0.58 | 75.1 |
| All Vehicles |  | 3425 | 9.1 | 0.727 | 9.2 | LOS A | 18.4 | 136.4 | 0.56 | 0.59 | 72.1 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^0]
## MOVEMENT SUMMARY

## Site: 2 [Huntingwood x GWH_Existing_PM]

Huntingwood Drive x Great Western Highway T-Intersection, Huntingwood
Road Conditions: 2018 Existing
Traffic: 2018 PM Base
Signals - Fixed Time Isolated Cycle Time = 107 seconds (Optimum Cycle Time - Minimum Delay)
Variable Sequence Analysis applied. The results are given for the selected output sequence.

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|l} \hline \text { Mov } \\ \text { ID } \end{array}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Deman Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Huntingwood Drive (1800m) |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 54 | 23.5 | 0.799 | 59.8 | LOS E | 16.3 | 121.3 | 1.00 | 0.96 | 50.0 |
| 3 | R2 | 564 | 4.3 | 0.799 | 56.1 | LOS D | 16.6 | 120.7 | 1.00 | 0.93 | 45.9 |
| Appr |  | 618 | 6.0 | 0.799 | 56.4 | LOS D | 16.6 | 121.3 | 1.00 | 0.93 | 46.3 |
| East: Great Western Highway ( 780 m ) |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 178 | 19.5 | 0.109 | 7.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.59 | 72.6 |
| 5 | T1 | 1687 | 4.4 | 0.797 | 19.8 | LOS B | 34.8 | 252.6 | 0.86 | 0.79 | 67.6 |
| Appr |  | 1865 | 5.8 | 0.797 | 18.7 | LOS B | 34.8 | 252.6 | 0.78 | 0.77 | 68.1 |
| West: Great Western Highway ( 1600 m ) |  |  |  |  |  |  |  |  |  |  |  |
| 11 | T1 | 931 | 3.7 | 0.363 | 8.0 | LOS A | 10.3 | 74.5 | 0.47 | 0.41 | 74.5 |
| 12 | R2 | 7 | 28.6 | 0.085 | 62.4 | LOS E | 0.4 | 3.4 | 0.97 | 0.66 | 50.0 |
| Approach |  | 938 | 3.9 | 0.363 | 8.4 | LOS A | 10.3 | 74.5 | 0.47 | 0.42 | 74.1 |
| All Vehicles |  | 3421 | 5.3 | 0.799 | 22.7 | LOS B | 34.8 | 252.6 | 0.73 | 0.70 | 63.6 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^1]
## MOVEMENT SUMMARY

$\square$ Site: 3 [Huntingwood x Brabham_Existing_AM]
Huntingwood Drive x Brabham Drive Intersection, Eastern Creek
Road Conditions: 2018 Existing
Traffic: 2018 AM Base
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Deman Total veh/h | lows HV $\%$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | f Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Brabham Drive (640m) |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 129 | 18.7 | 0.370 | 4.7 | LOS A | 2.9 | 21.9 | 0.45 | 0.45 | 53.8 |
| 2 | T1 | 582 | 8.7 | 0.370 | 4.4 | LOSA | 2.9 | 21.9 | 0.46 | 0.49 | 55.3 |
| 3 | R2 | 268 | 9.0 | 0.370 | 10.4 | LOSA | 2.8 | 20.9 | 0.48 | 0.58 | 57.2 |
| Appr |  | 980 | 10.1 | 0.370 | 6.1 | LOS A | 2.9 | 21.9 | 0.46 | 0.51 | 56.0 |
| East: Huntingwood Drive (1800m) |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 95 | 18.9 | 0.292 | 6.0 | LOS A | 1.2 | 10.6 | 0.60 | 0.73 | 56.7 |
| 5 | T1 | 52 | 34.7 | 0.292 | 6.2 | LOSA | 1.2 | 10.6 | 0.60 | 0.73 | 57.0 |
| 6 | R2 | 65 | 40.3 | 0.292 | 12.2 | LOSA | 1.2 | 10.6 | 0.60 | 0.73 | 56.8 |
| Appr |  | 212 | 29.4 | 0.292 | 7.9 | LOS A | 1.2 | 10.6 | 0.60 | 0.73 | 56.8 |
| North: Brabham Drive (380m) |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 403 | 10.4 | 0.519 | 6.7 | LOS A | 4.3 | 32.6 | 0.75 | 0.70 | 56.5 |
| 8 | T1 | 683 | 5.1 | 0.519 | 7.3 | LOSA | 4.3 | 32.6 | 0.76 | 0.75 | 54.4 |
| 9 | R2 | 25 | 16.7 | 0.519 | 13.9 | LOSA | 4.3 | 31.7 | 0.77 | 0.77 | 52.0 |
| Appr |  | 1112 | 7.3 | 0.519 | 7.3 | LOS A | 4.3 | 32.6 | 0.76 | 0.73 | 55.5 |
| West: Huntingwood Drive (360m) |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 38 | 52.8 | 0.285 | 7.1 | LOS A | 1.1 | 9.1 | 0.58 | 0.72 | 49.1 |
| 11 | T1 | 98 | 19.4 | 0.285 | 6.0 | LOSA | 1.1 | 9.1 | 0.58 | 0.72 | 56.9 |
| 12 | R2 | 68 | 24.6 | 0.285 | 12.0 | LOSA | 1.1 | 9.1 | 0.58 | 0.72 | 53.7 |
| Approach |  | 204 | 27.3 | 0.285 | 8.2 | LOS A | 1.1 | 9.1 | 0.58 | 0.72 | 55.3 |
| All Vehicles |  | 2507 | 11.9 | 0.519 | 6.9 | LOS A | 4.3 | 32.6 | 0.61 | 0.64 | 55.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^2]
## MOVEMENT SUMMARY

$\square$ Site: 3 [Huntingwood x Brabham_Existing_PM]
Huntingwood Drive x Brabham Drive Intersection, Eastern Creek
Road Conditions: 2018 Existing
Traffic: 2018 PM Base
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Deman Total veh/h | $\begin{gathered} =\text { lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Brabham Drive (640m) |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 119 | 21.2 | 0.468 | 6.5 | LOS A | 4.0 | 29.6 | 0.76 | 0.62 | 52.3 |
| 2 | T1 | 718 | 4.4 | 0.468 | 6.2 | LOS A | 4.0 | 29.6 | 0.77 | 0.66 | 54.1 |
| 3 | R2 | 121 | 12.2 | 0.468 | 12.6 | LOS A | 3.7 | 27.2 | 0.78 | 0.71 | 57.0 |
| Appr |  | 958 | 7.5 | 0.468 | 7.1 | LOS A | 4.0 | 29.6 | 0.77 | 0.66 | 54.6 |
| East: Huntingwood Drive (1800m) |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 269 | 4.7 | 0.747 | 8.3 | LOS A | 5.5 | 40.5 | 0.76 | 0.97 | 56.1 |
| 5 | T1 | 168 | 6.3 | 0.747 | 8.2 | LOS A | 5.5 | 40.5 | 0.76 | 0.97 | 56.4 |
| 6 | R2 | 231 | 9.1 | 0.747 | 14.0 | LOS A | 5.5 | 40.5 | 0.76 | 0.97 | 56.5 |
| Appr |  | 668 | 6.6 | 0.747 | 10.3 | LOS A | 5.5 | 40.5 | 0.76 | 0.97 | 56.3 |
| North: Brabham Drive (380m) |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 85 | 28.4 | 0.318 | 5.3 | LOS A | 2.2 | 17.1 | 0.51 | 0.49 | 56.6 |
| 8 | T1 | 683 | 6.0 | 0.318 | 5.0 | LOS A | 2.2 | 17.1 | 0.53 | 0.51 | 55.5 |
| 9 | R2 | 17 | 25.0 | 0.318 | 11.4 | LOS A | 2.2 | 16.0 | 0.54 | 0.52 | 53.2 |
| Appr |  | 785 | 8.8 | 0.318 | 5.2 | LOS A | 2.2 | 17.1 | 0.52 | 0.50 | 55.7 |
| West: Huntingwood Drive (360m) |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 45 | 23.3 | 0.261 | 6.8 | LOS A | 1.1 | 8.7 | 0.66 | 0.80 | 49.2 |
| 11 | T1 | 46 | 11.4 | 0.261 | 6.3 | LOS A | 1.1 | 8.7 | 0.66 | 0.80 | 56.6 |
| 12 | R2 | 81 | 11.7 | 0.261 | 12.1 | LOS A | 1.1 | 8.7 | 0.66 | 0.80 | 53.4 |
| Approach |  | 173 | 14.6 | 0.261 | 9.2 | LOS A | 1.1 | 8.7 | 0.66 | 0.80 | 54.1 |
| All Vehicles |  | 2584 | 8.1 | 0.747 | 7.4 | LOS A | 5.5 | 40.5 | 0.68 | 0.71 | 55.5 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^3]
## MOVEMENT SUMMARY

Vite: 4 [Ferrers x Brabham x Peter Brock_Existing_AM]
Ferrers Road x Brabham Drive x Peter Brock Drive, Eastern Creek
Road Conditions: 2018 Existing
Traffic: 2018 AM Base
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Deman Total veh/h | $\begin{gathered} =\text { lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | f Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| East: Peter Brock Drive (500m) per men min |  |  |  |  |  |  |  |  |  |  |  |
| 5 | T1 | 33 | 19.4 | 0.120 | 5.8 | LOS A | 0.5 | 4.5 | 0.61 | 0.73 | 51.2 |
| 6 | R2 | 52 | 22.4 | 0.120 | 11.4 | LOS A | 0.5 | 4.5 | 0.61 | 0.73 | 50.0 |
| Appr |  | 84 | 21.3 | 0.120 | 9.2 | LOS A | 0.5 | 4.5 | 0.61 | 0.73 | 50.5 |
| North: Brabham Drive (640m) |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 123 | 23.9 | 0.120 | 4.3 | LOS A | 0.7 | 5.7 | 0.25 | 0.44 | 52.1 |
| 9 | R2 | 778 | 7.7 | 0.471 | 9.6 | LOS A | 4.1 | 30.3 | 0.30 | 0.58 | 54.8 |
| Appr |  | 901 | 9.9 | 0.471 | 8.9 | LOS A | 4.1 | 30.3 | 0.29 | 0.56 | 54.5 |
| West: Ferrers Road (820m) |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 894 | 8.0 | 0.336 | 3.9 | LOS A | 2.3 | 17.1 | 0.24 | 0.42 | 56.7 |
| 11 | T1 | 63 | 8.3 | 0.336 | 3.8 | LOS A | 2.2 | 16.8 | 0.24 | 0.42 | 54.7 |
| Approach |  | 957 | 8.0 | 0.336 | 3.9 | LOS A | 2.3 | 17.1 | 0.24 | 0.42 | 56.6 |
| All Vehicles |  | 1942 | 9.5 | 0.471 | 6.5 | LOS A | 4.1 | 30.3 | 0.28 | 0.50 | 55.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

## © Site: 4 [Ferrers x Brabham x Peter Brock_Existing_PM]

Ferrers Road x Brabham Drive x Peter Brock Drive, Eastern Creek
Road Conditions: 2018 Existing
Traffic: 2018 PM Base
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Deman Total veh/h | $\begin{gathered} \text { =lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | f Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| East: Peter Brock Drive (500m) |  |  |  |  |  |  |  |  |  |  |  |
| 5 | T1 | 78 | 6.8 | 0.346 | 9.4 | LOS A | 2.0 | 15.5 | 0.79 | 0.90 | 49.5 |
| 6 | R2 | 128 | 15.6 | 0.346 | 15.2 | LOS B | 2.0 | 15.5 | 0.79 | 0.90 | 48.1 |
| Appr |  | 206 | 12.2 | 0.346 | 13.0 | LOS A | 2.0 | 15.5 | 0.79 | 0.90 | 48.7 |
| North: Brabham Drive (640m) |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 40 | 7.9 | 0.035 | 3.8 | LOS A | 0.2 | 1.4 | 0.13 | 0.42 | 52.6 |
| 9 | R2 | 1015 | 6.0 | 0.574 | 9.4 | LOSA | 6.3 | 46.4 | 0.20 | 0.57 | 55.1 |
| Appr |  | 1055 | 6.1 | 0.574 | 9.2 | LOS A | 6.3 | 46.4 | 0.20 | 0.57 | 55.1 |
| West: Ferrers Road (820m) |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 880 | 6.0 | 0.349 | 4.3 | LOS A | 2.4 | 18.0 | 0.39 | 0.48 | 56.3 |
| 11 | T1 | 22 | 14.3 | 0.349 | 4.3 | LOS A | 2.4 | 17.6 | 0.40 | 0.49 | 54.2 |
| Approach |  | 902 | 6.2 | 0.349 | 4.3 | LOS A | 2.4 | 18.0 | 0.40 | 0.48 | 56.3 |
| All Vehicles |  | 2163 | 6.7 | 0.574 | 7.5 | LOS A | 6.3 | 46.4 | 0.34 | 0.57 | 55.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

## Site: 5 [Horsley x Ferrers_ Existing_AM]

The Horsley Drive x Ferrers Road T-Intersection, Horsley Park
Road Conditions: 2018 Existing
Traffic: 2018 AM Base
Signals - Fixed Time Isolated Cycle Time $=78$ seconds (Optimum Cycle Time - Minimum Delay)


Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Movement Performance - Pedestrians

| Mov ID | Description | Demand Flow ped/h | Average Delay sec | Level of Average Back of Queue |  |  | Prop. Queued | Effective Stop Rate per ped |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Service | Pedestrian | Distance |  |  |
|  |  |  |  |  | ped | m |  |  |
| P2 | East Full Crossing | 21 | 33.3 | LOS D | 0.0 | 0.0 | 0.92 | 0.92 |
| P3 | North Full Crossing | 21 | 16.0 | LOS B | 0.0 | 0.0 | 0.64 | 0.64 |
| All P | estrians | 42 | 24.6 | LOS C |  |  | 0.78 | 0.78 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

## MOVEMENT SUMMARY

## Site: 5 [Horsley x Ferrers_ Existing_PM]

The Horsley Drive x Ferrers Road T-Intersection, Horsley Park
Road Conditions: 2018 Existing
Traffic: 2018 PM Base
Signals - Fixed Time Isolated Cycle Time $=65$ seconds (Optimum Cycle Time - Minimum Delay)


Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Movement Performance - Pedestrians

| Mov ID | Description | Demand Flow ped/h | Average Delay sec | Level of Average Back of Queue Service Pedestrian Distance |  |  | Prop. Queued | Effective Stop Rate per ped |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P2 | East Full Crossing | 21 | 26.8 | LOS C | 0.0 | 0.0 | 0.91 | 0.91 |
| P3 | North Full Crossing | 21 | 20.0 | LOS C | 0.0 | 0.0 | 0.79 | 0.79 |
| All P | estrians | 42 | 23.4 | LOS C |  |  | 0.85 | 0.85 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

C2:

## 2036 Base Case

## USER REPORT FOR SITE

Project: [0541] GWH_Doonside Road_Brabham Drive

## 目 Site: 1 [[2036 Future_AM] Doonside x GWH x Brabham]

Doonside Road x Great Western Highway x Brabham Drive Intersection, Eastern Creek
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time $=120$ seconds (Site User-Given Cycle Time)
Variable Sequence Analysis applied. The results are given for the selected output sequence.
Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Green Split Priority has been specified
Phase Sequence: Standard Diamond (VV1120)
Reference Phase: Phase A
Input Phase Sequence: G, G1*, G2*, A, B*, C*, D, D1* ${ }^{*}$ D2*, E, F1*, F2*
Output Phase Sequence: G, G2*, A, D, D1*, E, F2*
(* Variable Phase)

## Site Layout



| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | Lane \% | Average Delay sec | Level of Service | $\begin{gathered} \text { 95\% Bac } \\ \text { Veh } \end{gathered}$ | Queue Dist m | Lane Config | Lane Length m | Cap. Adj. \% | Prob. Block. \% |
| South: Brabham Drive (380m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 318 | 17.8 | 507 | 0.628 | 100 | 39.2 | LOS C | 15.3 | 123.1 | Full | 380 | 0.0 | 0.0 |
| Lane 2 | 273 | 8.9 | $435{ }^{1}$ | 0.628 | 100 | 38.2 | LOS C | 13.4 | 100.6 | Full | 380 | 0.0 | 0.0 |
| Lane 3 | 179 | 12.4 | 196 | 0.913 | 100 | 78.8 | LOS F | 12.4 | 96.2 | Short | 50 | 0.0 | NA |
| Approach | 771 | 13.4 |  | 0.913 |  | 48.1 | LOS D | 15.3 | 123.1 |  |  |  |  |
| East: Great Western Highway (1600m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 145 | 12.3 | 793 | 0.183 | 100 | 23.0 | LOS B | 4.4 | 34.0 | Short | 215 | 0.0 | NA |
| Lane 2 | 163 | 10.3 | 196 | 0.830 | 100 | 64.1 | LOS E | 10.4 | 78.8 | Short | 135 | 0.0 | NA |
| Lane 3 | 164 | 10.3 | 198 | 0.830 | 100 | 64.0 | LOS E | 10.5 | 79.6 | Full | 1600 | 0.0 | 0.0 |
| Lane 4 | 164 | 10.3 | 198 | 0.830 | 100 | 64.0 | LOS E | 10.5 | 79.6 | Full | 1600 | 0.0 | 0.0 |
| Lane 5 | 106 | 7.5 | 118 | 0.895 | 100 | 80.5 | LOS F | 7.2 | 53.3 | Short | 125 | 0.0 | NA |
| Lane 6 | 106 | 7.5 | 118 | 0.895 | 100 | 80.5 | LOS F | 7.2 | 53.3 | Short | 120 | 0.0 | NA |
| Approach | 848 | 9.9 |  | 0.895 |  | 61.1 | LOS E | 10.5 | 79.6 |  |  |  |  |
| North: Doonside Road ( 500 m ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 721 | 6.3 | 799 | 0.902 | 100 | 51.5 | LOS D | 46.3 | 341.9 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 576 | 5.5 | $639{ }^{1}$ | 0.902 | 100 | 50.4 | LOS D | 35.8 | 262.5 | Full | 500 | 0.0 | 0.0 |
| Lane 3 | 161 | 16.8 | 292 | 0.551 | 100 | 32.8 | LOS C | 4.8 | 38.8 | Short | 70 | 0.0 | NA |
| Lane 4 | 159 | 16.8 | 289 | 0.551 | 100 | 32.8 | LOS C | 4.8 | 38.4 | Short | 60 | 0.0 | NA |
| Approach | 1617 | 8.1 |  | 0.902 |  | 47.4 | LOS D | 46.3 | 341.9 |  |  |  |  |
| West: Great Western Highway (390m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 539 | 9.2 | 1256 | 0.429 | 100 | 12.2 | LOS A | 10.1 | 76.2 | Short | 150 | 0.0 | NA |
| Lane 2 | 304 | 8.5 | 405 | 0.753 | $85^{6}$ | 49.8 | LOS D | 17.4 | 130.6 | Full | 390 | 0.0 | 0.0 |
| Lane 3 | 356 | 8.5 | 405 | 0.881 | 100 | 60.2 | LOS E | 23.3 | 174.6 | Full | 390 | 0.0 | 0.0 |
| Lane 4 | 353 | 8.5 | 400 | 0.881 | 100 | 60.3 | LOS E | 23.0 | 173.0 | Full | 390 | 0.0 | 0.0 |
| Lane 5 | 271 | 7.6 | 310 | 0.874 | 100 | 70.3 | LOS E | 17.7 | 132.2 | Short | 145 | 0.0 | NA |
| Lane 6 | 271 | 7.6 | 310 | 0.874 | 100 | 70.3 | LOS E | 17.7 | 132.2 | Short | 140 | 0.0 | NA |
| Approach | 2095 | 8.4 |  | 0.881 |  | 49.0 | LOS D | 23.3 | 174.6 |  |  |  |  |
| Intersection | 5331 | 9.3 |  | 0.913 |  | 50.3 | LOS D | 46.3 | 341.9 |  |  |  |  |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Lane LOS values are based on average delay per lane.
Intersection and Approach LOS values are based on average delay for all lanes.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
1 Reduced capacity due to a short lane effect. Short lane queues may extend into the full-length lanes. Some upstream delays at entry to short lanes are not included.
6 Lane under-utilisation due to downstream effects

## USER REPORT FOR SITE

Project: [0541] GWH_Doonside Road_Brabham Drive

## 目 Site: 1 [[2036 Future_PM] Doonside x GWH x Brabham]

Doonside Road x Great Western Highway x Brabham Drive Intersection, Eastern Creek
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time $=120$ seconds (Site User-Given Cycle Time)
Variable Sequence Analysis applied. The results are given for the selected output sequence.
Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Green Split Priority has been specified
Phase Sequence: Standard Diamond (VV1120)
Reference Phase: Phase A
Input Phase Sequence: G, G1*, G2*, A, B*, C*, D, D1*, D2*, E, F1*, F2*
Output Phase Sequence: G, G1 ${ }^{*}$, A, D, D2*, E
(* Variable Phase)
Site Layout


Input Volumes

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | $\begin{aligned} & \text { Lane } \\ & \text { Util. } \\ & \% \end{aligned}$ | Average Delay sec | Level of Service | 95\% Bac <br> Veh | Queue Dist m | Lane Config | Lane Length m | Cap. <br> Adj. <br> \% | Prob. Block. \% |
| South: Brabham Drive (380m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 552 | 4.5 | 667 | 0.829 | 100 | 44.3 | LOS D | 31.5 | 229.2 | Full | 380 | 0.0 | 0.0 |
| Lane 2 | 469 | 2.5 | $565{ }^{1}$ | 0.829 | 100 | 41.8 | LOS C | 25.8 | 184.7 | Full | 380 | 0.0 | 0.0 |
| Lane 3 | 122 | 4.3 | 222 | 0.551 | 100 | 60.5 | LOS E | 6.9 | 50.4 | Short | 50 | 0.0 | NA |
| Approach | 1143 | 3.7 |  | 0.829 |  | 45.0 | LOS D | 31.5 | 229.2 |  |  |  |  |
| East: Great Western Highway (1600m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 120 | 7.9 | 1149 | 0.104 | 100 | 12.6 | LOS A | 2.0 | 15.2 | Short | 215 | 0.0 | NA |
| Lane 2 | 341 | 6.1 | 418 | 0.816 | 100 | 52.7 | LOS D | 20.5 | 150.8 | Short | 135 | 0.0 | NA |
| Lane 3 | 344 | 6.1 | 422 | 0.816 | 100 | 52.7 | LOS D | 20.7 | 152.2 | Full | 1600 | 0.0 | 0.0 |
| Lane 4 | 344 | 6.1 | 422 | 0.816 | 100 | 52.7 | LOS D | 20.7 | 152.2 | Full | 1600 | 0.0 | 0.0 |
| Lane 5 | 178 | 3.2 | 258 | 0.690 | 100 | 62.6 | LOS E | 10.4 | 74.7 | Short | 125 | 0.0 | NA |
| Lane 6 | 178 | 3.2 | 258 | 0.690 | 100 | 62.6 | LOS E | 10.4 | 74.7 | Short | 120 | 0.0 | NA |
| Approach | 1506 | 5.6 |  | 0.816 |  | 51.8 | LOS D | 20.7 | 152.2 |  |  |  |  |
| North: Doonside Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 419 | 6.6 | 750 | 0.559 | 100 | 33.5 | LOS C | 18.7 | 138.0 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 377 | 5.3 | $675{ }^{1}$ | 0.559 | 100 | 32.6 | LOS C | 17.2 | 125.7 | Full | 500 | 0.0 | 0.0 |
| Lane 3 | 209 | 10.4 | 261 | 0.802 | 100 | 65.7 | LOS E | 12.9 | 98.1 | Short | 70 | 0.0 | NA |
| Lane 4 | 207 | 10.4 | 258 | 0.802 | 100 | 65.7 | LOS E | 12.7 | 97.2 | Short | 60 | 0.0 | NA |
| Approach | 1212 | 7.5 |  | 0.802 |  | 44.3 | LOS D | 18.7 | 138.0 |  |  |  |  |
| West: Great Western Highway (390m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 399 | 13.2 | 976 | 0.409 | 100 | 18.8 | LOS B | 11.4 | 88.9 | Short | 150 | 0.0 | NA |
| Lane 2 | 181 | 4.2 | 304 | 0.597 | $85^{6}$ | 51.6 | LOS D | 10.1 | 73.1 | Full | 390 | 0.0 | 0.0 |
| Lane 3 | 212 | 4.2 | 304 | 0.700 | 100 | 53.5 | LOS D | 12.2 | 88.6 | Full | 390 | 0.0 | 0.0 |
| Lane 4 | 210 | 4.2 | 301 | 0.700 | 100 | 53.5 | LOS D | 12.1 | 87.7 | Full | 390 | 0.0 | 0.0 |
| Lane 5 | 106 | 15.9 | 126 | 0.841 | 100 | 75.8 | LOS F | 6.9 | 54.9 | Short | 145 | 0.0 | NA |
| Lane 6 | 106 | 15.9 | 126 | 0.841 | 100 | 75.8 | LOS F | 6.9 | 54.9 | Short | 140 | 0.0 | NA |
| Approach | 1215 | 9.2 |  | 0.841 |  | 45.7 | LOS D | 12.2 | 88.9 |  |  |  |  |
| Intersection | 5076 | 6.5 |  | 0.841 |  | 47.0 | LOS D | 31.5 | 229.2 |  |  |  |  |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Lane LOS values are based on average delay per lane.
Intersection and Approach LOS values are based on average delay for all lanes.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
1 Reduced capacity due to a short lane effect. Short lane queues may extend into the full-length lanes. Some upstream delays at entry to short lanes are not included.
6 Lane under-utilisation due to downstream effects

## MOVEMENT SUMMARY

Site: 2 [Huntingwood $x$ GWH $\qquad$ Future
AM ]
Huntingwood Drive x Great Western Highway T-Intersection, Huntingwood
Road Conditions: 2018 Existing
Traffic: 2036 AM Background
Signals - Fixed Time Isolated Cycle Time $=110$ seconds (User-Given Cycle Time)
Variable Sequence Analysis applied. The results are given for the selected output sequence.

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | f Queue <br> Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Huntingwood Drive (1800m) min |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 22 | 47.6 | 0.686 | 56.3 | LOS D | 6.3 | 54.7 | 1.00 | 0.86 | 50.1 |
| 3 | R2 | 219 | 22.6 | 0.686 | 58.4 | LOS E | 6.6 | 55.4 | 1.00 | 0.85 | 44.9 |
| Appr |  | 241 | 24.9 | 0.686 | 58.2 | LOS E | 6.6 | 55.4 | 1.00 | 0.85 | 45.4 |
| East: Great Western Highway (780m) |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 560 | 10.0 | 0.323 | 7.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.60 | 73.2 |
| 5 | T1 | 831 | 8.9 | 0.349 | 9.4 | LOS A | 10.0 | 75.5 | 0.49 | 0.43 | 73.6 |
| Appr |  | 1391 | 9.3 | 0.349 | 8.8 | LOS A | 10.0 | 75.5 | 0.29 | 0.50 | 73.4 |
| West: Great Western Highway ( 1600 m ) |  |  |  |  |  |  |  |  |  |  |  |
| 11 | T1 | 2043 | 7.1 | 0.701 | 6.1 | LOS A | 26.0 | 192.8 | 0.53 | 0.49 | 75.7 |
| 12 | R2 | 47 | 17.8 | 0.351 | 61.6 | LOS E | 2.5 | 20.5 | 0.98 | 0.75 | 50.3 |
| Approach |  | 2091 | 7.3 | 0.701 | 7.4 | LOS A | 26.0 | 192.8 | 0.54 | 0.50 | 74.5 |
| All Ve | cles | 3722 | 9.2 | 0.701 | 11.2 | LOS A | 26.0 | 192.8 | 0.48 | 0.52 | 70.9 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

Site: 2 [Huntingwood $x$ GWH $\qquad$ Future
_PM ]
Huntingwood Drive x Great Western Highway T-Intersection, Huntingwood
Road Conditions: 2018 Existing
Traffic: 2036 PM Background
Signals - Fixed Time Isolated Cycle Time $=140$ seconds (User-Given Cycle Time)
Variable Sequence Analysis applied. The results are given for the selected output sequence.

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov OD  <br> ID Mov | Dema Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \\ \hline \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | f Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Huntingwood Drive (1800m) |  |  |  |  |  |  |  |  |  |  |
| L2 | 58 | 23.6 | 0.740 | 65.9 | LOS E | 20.7 | 154.7 | 0.98 | 0.91 | 48.8 |
| 3 R 2 | 605 | 4.3 | 0.740 | 61.8 | LOS E | 21.3 | 154.7 | 0.98 | 0.88 | 44.6 |
| Approach | 663 | 6.0 | 0.740 | 62.2 | LOS E | 21.3 | 154.7 | 0.98 | 0.89 | 45.1 |
| East: Great Western Highway (780m) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 172 | 19.6 | 0.105 | 7.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.59 | 72.6 |
| $5 \quad$ T1 | 1626 | 4.3 | 0.760 | 23.0 | LOS B | 42.0 | 305.0 | 0.80 | 0.74 | 65.9 |
| Approach | 1798 | 5.8 | 0.760 | 21.6 | LOS B | 42.0 | 305.0 | 0.73 | 0.73 | 66.6 |
| West: Great Western Highway ( 1600 m ) |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 1098 | 3.7 | 0.434 | 11.6 | LOS A | 17.3 | 124.7 | 0.51 | 0.46 | 72.2 |
| 12 R 2 | 8 | 25.0 | 0.125 | 81.3 | LOS F | 0.6 | 5.0 | 0.99 | 0.67 | 46.5 |
| Approach | 1106 | 3.9 | 0.434 | 12.2 | LOS A | 17.3 | 124.7 | 0.51 | 0.46 | 71.8 |
| All Vehicles | 3567 | 5.3 | 0.760 | 26.2 | LOS B | 42.0 | 305.0 | 0.71 | 0.67 | 62.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

## Gite: 3 [Huntingwood x Brabham_ Future_AM]

Huntingwood Drive x Brabham Drive Intersection, Eastern Creek
Road Conditions: 2018 Existing
Traffic: 2036 AM Background
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Deman Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Brabham Drive (640m) min |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 137 | 18.5 | 0.396 | 4.8 | LOS A | 3.1 | 24.1 | 0.48 | 0.46 | 53.6 |
| 2 | T1 | 614 | 8.7 | 0.396 | 4.5 | LOS A | 3.1 | 24.1 | 0.49 | 0.50 | 55.1 |
| 3 | R2 | 283 | 8.9 | 0.396 | 10.5 | LOS A | 3.0 | 22.9 | 0.51 | 0.59 | 57.2 |
| Appro |  | 1034 | 10.1 | 0.396 | 6.2 | LOS A | 3.1 | 24.1 | 0.49 | 0.52 | 55.9 |
| East: Huntingwood Drive (1800m) |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 103 | 19.4 | 0.333 | 6.3 | LOS A | 1.5 | 12.7 | 0.63 | 0.77 | 56.6 |
| 5 | T1 | 56 | 35.8 | 0.333 | 6.5 | LOS A | 1.5 | 12.7 | 0.63 | 0.77 | 56.9 |
| 6 | R2 | 72 | 39.7 | 0.333 | 12.5 | LOS A | 1.5 | 12.7 | 0.63 | 0.77 | 56.7 |
| Appro |  | 231 | 29.7 | 0.333 | 8.2 | LOS A | 1.5 | 12.7 | 0.63 | 0.77 | 56.7 |
| North: Brabham Drive (380m) |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 425 | 10.4 | 0.562 | 7.6 | LOS A | 5.3 | 39.9 | 0.79 | 0.77 | 56.3 |
| 8 | T1 | 720 | 5.1 | 0.562 | 8.3 | LOS A | 5.3 | 39.9 | 0.81 | 0.82 | 54.1 |
| 9 | R2 | 26 | 16.0 | 0.562 | 14.9 | LOS B | 5.2 | 38.0 | 0.81 | 0.84 | 51.7 |
| Appro |  | 1172 | 7.3 | 0.562 | 8.2 | LOS A | 5.3 | 39.9 | 0.80 | 0.80 | 55.3 |
| West: Huntingwood Drive (360m) |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 41 | 53.8 | 0.322 | 7.5 | LOS A | 1.3 | 10.9 | 0.61 | 0.75 | 48.8 |
| 11 | T1 | 106 | 19.8 | 0.322 | 6.4 | LOS A | 1.3 | 10.9 | 0.61 | 0.75 | 56.8 |
| 12 | R2 | 75 | 23.9 | 0.322 | 12.3 | LOS A | 1.3 | 10.9 | 0.61 | 0.75 | 53.4 |
| Appro |  | 222 | 27.5 | 0.322 | 8.6 | LOS A | 1.3 | 10.9 | 0.61 | 0.75 | 55.1 |
| All Ve | cles | 2658 | 12.0 | 0.562 | 7.5 | LOS A | 5.3 | 39.9 | 0.65 | 0.69 | 55.7 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

SIDRA INTERSECTION 7.0 | Copyright © 2000-2017 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: ASON GROUP PTY LTD | Processed: Thursday, 8 November 2018 9:28:41 AM
Project: C:IUsers\Sharif Hasan\Desktopl0541 Lighthorselsidra\AG0541m2v2 Lighthorse_ Future Base.sip7

## MOVEMENT SUMMARY

## (7) Site: 3 [Huntingwood x Brabham_ Future_PM]

Huntingwood Drive x Brabham Drive Intersection, Eastern Creek
Road Conditions: 2018 Existing
Traffic: 2036 PM Background
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|l\|l} \text { Mov } \\ \hline \end{array}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Deman Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Brabham Drive (640m) |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 129 | 21.1 | 0.540 | 7.4 | LOS A | 5.2 | 38.7 | 0.84 | 0.72 | 51.9 |
| 2 | T1 | 782 | 4.4 | 0.540 | 7.3 | LOS A | 5.2 | 38.7 | 0.85 | 0.78 | 53.6 |
| 3 | R2 | 132 | 12.0 | 0.540 | 14.1 | LOS A | 5.0 | 36.8 | 0.85 | 0.85 | 56.7 |
| Appro |  | 1043 | 7.5 | 0.540 | 8.2 | LOS A | 5.2 | 38.7 | 0.85 | 0.78 | 54.2 |
| East: Huntingwood Drive (1800m) |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 299 | 4.6 | 0.854 | 10.9 | LOS A | 8.2 | 60.9 | 0.86 | 1.12 | 55.2 |
| 5 | T1 | 186 | 6.2 | 0.854 | 10.8 | LOS A | 8.2 | 60.9 | 0.86 | 1.12 | 55.4 |
| 6 | R2 | 256 | 9.1 | 0.854 | 16.6 | LOS B | 8.2 | 60.9 | 0.86 | 1.12 | 55.5 |
| Appro |  | 741 | 6.5 | 0.854 | 12.8 | LOS A | 8.2 | 60.9 | 0.86 | 1.12 | 55.3 |
| North: Brabham Drive (380m) |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 89 | 28.2 | 0.343 | 5.5 | LOS A | 2.5 | 18.9 | 0.55 | 0.51 | 56.5 |
| 8 | T1 | 720 | 6.0 | 0.343 | 5.2 | LOS A | 2.5 | 18.9 | 0.56 | 0.53 | 55.3 |
| 9 | R2 | 18 | 23.5 | 0.343 | 11.6 | LOS A | 2.4 | 17.6 | 0.57 | 0.54 | 53.0 |
| Appro |  | 827 | 8.8 | 0.343 | 5.4 | LOS A | 2.5 | 18.9 | 0.56 | 0.52 | 55.5 |
| West: Huntingwood Drive (360m) |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 51 | 22.9 | 0.318 | 7.3 | LOS A | 1.4 | 11.4 | 0.71 | 0.84 | 48.8 |
| 11 | T1 | 52 | 12.2 | 0.318 | 6.9 | LOS A | 1.4 | 11.4 | 0.71 | 0.84 | 56.4 |
| 12 | R2 | 89 | 11.8 | 0.318 | 12.7 | LOS A | 1.4 | 11.4 | 0.71 | 0.84 | 53.1 |
| Appro |  | 192 | 14.8 | 0.318 | 9.7 | LOS A | 1.4 | 11.4 | 0.71 | 0.84 | 53.8 |
| All Ve | cles | 2803 | 8.1 | 0.854 | 8.7 | LOS A | 8.2 | 60.9 | 0.76 | 0.80 | 54.9 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

Site: 4 [Ferrers x Brabham x Peter Brock_ Future_AM]

Ferrers Road x Brabham Drive x Peter Brock Drive, Eastern Creek
Road Conditions: 2018 Existing
Traffic: 2036 AM Background
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov OD  <br> ID Mov | Deman Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | f Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| East: Peter Brock Drive (500m) mid |  |  |  |  |  |  |  |  |  |  |
| 5 T1 | 36 | 20.6 | 0.147 | 6.9 | LOS A | 0.7 | 6.1 | 0.68 | 0.79 | 50.6 |
| 6 R2 | 56 | 22.6 | 0.147 | 12.5 | LOS A | 0.7 | 6.1 | 0.68 | 0.79 | 49.4 |
| Approach | 92 | 21.8 | 0.147 | 10.3 | LOS A | 0.7 | 6.1 | 0.68 | 0.79 | 49.9 |
| North: Brabham Drive (640m) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 139 | 24.2 | 0.136 | 4.4 | LOS A | 0.8 | 6.6 | 0.27 | 0.44 | 52.1 |
| 9 R2 | 876 | 7.7 | 0.532 | 9.7 | LOS A | 5.0 | 37.4 | 0.33 | 0.57 | 54.7 |
| Approach | 1015 | 10.0 | 0.532 | 9.0 | LOS A | 5.0 | 37.4 | 0.32 | 0.56 | 54.5 |
| West: Ferrers Road (820m) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 942 | 8.0 | 0.356 | 4.0 | LOS A | 2.5 | 19.0 | 0.26 | 0.43 | 56.7 |
| 11 T1 | 66 | 7.9 | 0.356 | 3.8 | LOS A | 2.5 | 18.6 | 0.26 | 0.42 | 54.6 |
| Approach | 1008 | 8.0 | 0.356 | 3.9 | LOS A | 2.5 | 19.0 | 0.26 | 0.43 | 56.5 |
| All Vehicles | 2115 | 9.6 | 0.532 | 6.6 | LOS A | 5.0 | 37.4 | 0.31 | 0.50 | 55.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

Site: 4 [Ferrers x Brabham x Peter Brock_ Future_PM]

Ferrers Road x Brabham Drive x Peter Brock Drive, Eastern Creek
Road Conditions: 2018 Existing
Traffic: 2036 PM Background
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov OD  <br> ID Mov | Dema Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | queue <br> Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| East: Peter Brock Drive (500m) mer |  |  |  |  |  |  |  |  |  |  |
| 5 T1 | 86 | 7.3 | 0.460 | 15.3 | LOS B | 3.4 | 26.0 | 0.90 | 1.05 | 46.7 |
| 6 R2 | 139 | 15.9 | 0.460 | 21.2 | LOS B | 3.4 | 26.0 | 0.90 | 1.05 | 45.2 |
| Approach | 225 | 12.6 | 0.460 | 18.9 | LOS B | 3.4 | 26.0 | 0.90 | 1.05 | 45.8 |
| North: Brabham Drive (640m) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 45 | 7.0 | 0.039 | 3.8 | LOS A | 0.2 | 1.6 | 0.14 | 0.42 | 52.6 |
| 9 R2 | 1142 | 6.0 | 0.647 | 9.4 | LOS A | 8.3 | 61.0 | 0.24 | 0.56 | 55.0 |
| Approach | 1187 | 6.0 | 0.647 | 9.2 | LOS A | 8.3 | 61.0 | 0.24 | 0.56 | 54.9 |
| West: Ferrers Road (820m) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 959 | 6.0 | 0.387 | 4.4 | LOS A | 2.9 | 21.1 | 0.44 | 0.50 | 56.2 |
| 11 T1 | 24 | 13.0 | 0.387 | 4.4 | LOS A | 2.8 | 20.6 | 0.44 | 0.50 | 54.1 |
| Approach | 983 | 6.2 | 0.387 | 4.4 | LOS A | 2.9 | 21.1 | 0.44 | 0.50 | 56.1 |
| All Vehicles | 2396 | 6.7 | 0.647 | 8.2 | LOS A | 8.3 | 61.0 | 0.38 | 0.58 | 54.5 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## 目 Site: 5 [[s02] Horsley x Ferrers_Future_AM]

The Horsley Drive x Ferrers Road T-Intersection, Horsley Park
Road Conditions: 2018 Existing
Traffic: 2036 AM Future Baseline
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time $=78$ seconds (Site User-Given Phase Times)
Timings based on settings in the Site Phasing \& Timing dialog
Phase Times specified by the user
Phase Sequence: Three Phase
Reference Phase: Phase B
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

## Input Volumes

Volume Display Method: Total and Veh

\[

\]



|  | All MCs | Light Vehicles (LV) | Heavy Vehicles (HV) |
| :--- | :---: | :---: | :---: |
| E: The Horsley Drive (160m) | 2145 | 1705 | 440 |
| N: Ferrers Road (5000m) | 531 | 470 | 61 |
| W: The Horsley Drive (1500m) | 1685 | 1386 | 299 |
| Total | 4361 | 3561 | 800 |


| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | $\begin{aligned} & \text { Lane } \\ & \text { Util. } \\ & \% \end{aligned}$ | Average Delay sec | Level of Service | 95\% Back <br> Veh | f Queue Dist m | Lane Config | Lane Length | Cap. Adj. \% | Prob. Block. \% |
| East: The Horsley Drive (160m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 769 | 25.6 | 1279 | 0.601 | 100 | 4.1 | LOS A | 12.5 | 106.6 | Full | 160 | 0.0 | 0.0 |
| Lane 2 | 769 | 25.6 | 1279 | 0.601 | 100 | 4.1 | LOS A | 12.5 | 106.6 | Full | 160 | 0.0 | $100.0^{8}$ |
| Lane 3 | 720 | 9.6 | $461{ }^{1}$ | 1.562 | 100 | 548.3 | LOS F | 138.7 | 1051.5 | Short | 75 | 0.0 | NA |
| Approach | 2258 | 20.5 |  | 1.562 |  | 177.7 | LOS F | 138.7 | 1051.5 |  |  |  |  |
| North: Ferrers Road ( 5000 m ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 521 | 8.9 | 989 | 0.527 | 100 | 18.9 | LOS B | 10.3 | 77.9 | Short | 55 | 0.0 | NA |
| Lane 2 | 38 | 47.2 | 160 | 0.236 | 100 | 42.1 | LOS C | 1.4 | 13.8 | Full | 5000 | 0.0 | 0.0 |
| Approach | 559 | 11.5 |  | 0.527 |  | 20.5 | LOS B | 10.3 | 77.9 |  |  |  |  |
| West: The Horsley Drive (1500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 886 | 17.8 | 738 | 1.200 | 100 | 226.5 | LOS F | 106.3 | 858.1 | Full | 1500 | 0.0 | 0.0 |
| Lane 2 | 888 | 17.7 | 740 | 1.200 | 100 | 225.5 | LOS F | 106.3 | 856.4 | Full | 1500 | 0.0 | 0.0 |
| Approach | 1774 | 17.7 |  | 1.200 |  | 226.0 | LOS F | 106.3 | 858.1 |  |  |  |  |
| Intersection | 4591 | 18.3 |  | 1.562 |  | 177.2 | LOS F | 138.7 | 1051.5 |  |  |  |  |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Lane LOS values are based on average delay per lane.
Intersection and Approach LOS values are based on average delay for all lanes.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
1 Reduced capacity due to a short lane effect. Short lane queues may extend into the full-length lanes. Some upstream delays at entry to short lanes are not included.
8 Probability of Blockage has been set on the basis of a queue that overflows from a short lane.

## 目 Site: 5 [[s02] Horsley x Ferrers_Future_PM ]

The Horsley Drive x Ferrers Road T-Intersection, Horsley Park
Road Conditions: 2018 Existing
Traffic: 2036 PM Future Baseline
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time $=65$ seconds (Site User-Given Phase Times)
Timings based on settings in the Site Phasing \& Timing dialog
Phase Times specified by the user
Phase Sequence: Three Phase
Reference Phase: Phase B
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

## Input Volumes

Volume Display Method: Total and Veh

|  | R2 | L2 |
| :--- | ---: | ---: |
| Tot | 213 | 716 |
| LV | 202 | 678 |
| HV | 11 | 38 |


| HV | LV | Tot |  |
| :--- | :--- | :--- | :--- |
| 44 | 36 | 80 | L2 |
| 325 | 1203 | 1528 | T1 |



|  | Tot | LV | HV |
| :--- | :--- | :--- | :--- |
| R2 | 540 | 503 | 37 |
| T1 | 1929 | 1737 | 192 |


|  | All MCs | Light Vehicles (LV) | Heavy Vehicles (HV) |
| :--- | :---: | :---: | :---: |
| E: The Horsley Drive (160m) | 2469 | 2240 | 229 |
| N: Ferrers Road (5000m) | 929 | 880 | 49 |
| W: The Horsley Drive (1500m) | 1608 | 1239 | 369 |
| Total | 5006 | 4359 | 647 |


| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{array}{r} \text { Flows } \\ \text { HV } \\ \% \\ \hline \end{array}$ | Cap. veh/h | Deg. Satn v/c | Lane \% | Average Delay sec | Level of Service | 95\% Back <br> Veh | Queue m | Lane Config | Lane Length m | $\begin{aligned} & \text { Cap. } \\ & \text { Adj. } \\ & \% \end{aligned}$ | Prob. Block. \% |
| East: The Horsley Drive (160m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 1142 | 10.0 | 1233 | 0.926 | 100 | 29.4 | LOS C | 47.3 | 359.1 | Full | 160 | 0.0 | 80.5 |
| Lane 2 | 889 | 10.0 | $960{ }^{1}$ | 0.926 | 100 | 30.9 | LOS C | 32.2 | 244.8 | Full | 160 | 0.0 | $79.5{ }^{8}$ |
| Lane 3 | 568 | 6.9 | 515 | 1.104 | 100 | 146.7 | LOS F | 47.9 | 355.3 | Short | 75 | 0.0 | NA |
| Approach | 2599 | 9.3 |  | 1.104 |  | 55.6 | LOS D | 47.9 | 359.1 |  |  |  |  |
| North: Ferrers Road (5000m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 754 | 5.3 | 1244 | 0.606 | 100 | 12.6 | LOS A | 9.8 | 71.9 | Short | 55 | 0.0 | NA |
| Lane 2 | 224 | 5.2 | 331 | 0.678 | 100 | 34.5 | LOS C | 7.2 | 52.3 | Full | 5000 | 0.0 | 0.0 |
| Approach | 978 | 5.3 |  | 0.678 |  | 17.6 | LOS B | 9.8 | 71.9 |  |  |  |  |
| West: The Horsley Drive (1500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 839 | 24.7 | 492 | 1.705 | 100 | 667.6 | LOS F | 174.2 | 1476.9 | Full | 1500 | 0.0 | 3.6 |
| Lane 2 | 854 | 21.3 | 501 | 1.705 | 100 | 666.4 | LOS F | 177.0 | 1465.3 | Full | 1500 | 0.0 | 2.9 |
| Approach | 1693 | 22.9 |  | 1.705 |  | 667.0 | LOS F | 177.0 | 1476.9 |  |  |  |  |
| Intersection | 5269 | 12.9 |  | 1.705 |  | 244.9 | LOS F | 177.0 | 1476.9 |  |  |  |  |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Lane LOS values are based on average delay per lane.
Intersection and Approach LOS values are based on average delay for all lanes.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
1 Reduced capacity due to a short lane effect. Short lane queues may extend into the full-length lanes. Some upstream delays at entry to short lanes are not included.
8 Probability of Blockage has been set on the basis of a queue that overflows from a short lane.

## MOVEMENT SUMMARY

## Site: 5 [Horsley x Ferrers_ Future (with RMS Upgrade)_AM]

The Horsley Drive x Ferrers Road
Road Conditions: The Horsley Drive Upgrades (RMS)
Traffic: 2036 AM Background
Signals - Fixed Time Isolated Cycle Time $=80$ seconds (Optimum Cycle Time - Minimum Delay)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov OD  <br> ID Mov | Deman Total veh/h | $\begin{gathered} \text { =lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue <br> Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| East: The Horsley Drive (750m) |  |  |  |  |  |  |  |  |  |  |
| 5 T1 | 1538 | 25.6 | 0.593 | 4.0 | LOS A | 12.4 | 106.0 | 0.45 | 0.41 | 64.6 |
| 6 R2 | 720 | 9.6 | 0.753 | 37.3 | LOS C | 13.9 | 105.3 | 0.97 | 0.90 | 54.0 |
| Approach | 2258 | 20.5 | 0.753 | 14.6 | LOS B | 13.9 | 106.0 | 0.62 | 0.57 | 58.4 |
| North: Ferrers Road (5000m) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 521 | 8.9 | 0.322 | 22.2 | LOS B | 6.8 | 51.1 | 0.71 | 0.76 | 56.2 |
| 9 R2 | 38 | 47.2 | 0.364 | 47.7 | LOS D | 1.5 | 15.2 | 0.99 | 0.73 | 54.3 |
| Approach | 559 | 11.5 | 0.364 | 23.9 | LOS B | 6.8 | 51.1 | 0.73 | 0.76 | 56.1 |
| West: The Horsley Drive (1500m) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 117 | 18.9 | 0.115 | 10.4 | LOS A | 1.4 | 11.1 | 0.39 | 0.67 | 60.1 |
| 11 T1 | 1657 | 17.7 | 0.745 | 23.4 | LOS B | 19.0 | 153.0 | 0.90 | 0.84 | 55.8 |
| Approach | 1774 | 17.7 | 0.745 | 22.5 | LOS B | 19.0 | 153.0 | 0.87 | 0.83 | 56.5 |
| All Vehicles | 4591 | 18.3 | 0.753 | 18.8 | LOS B | 19.0 | 153.0 | 0.73 | 0.69 | 57.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Description | Demand Flow ped/h | Average Delay $\qquad$ sec | Level of Service | Average Back Pedestrian $\qquad$ ped | of Queue Distance $\qquad$ | Prop. Queued | Effective Stop Rate per ped |
| P21 | East Stage 1 | 21 | 34.3 | LOS D | 0.0 | 0.0 | 0.93 | 0.93 |
| P22 | East Stage 2 | 21 | 34.3 | LOS D | 0.0 | 0.0 | 0.93 | 0.93 |
| P3 | North Full Crossing | 21 | 19.6 | LOS B | 0.0 | 0.0 | 0.70 | 0.70 |
| P3S | North Slip/Bypass Lane Crossing | 21 | 17.6 | LOS B | 0.0 | 0.0 | 0.66 | 0.66 |
| P41 | West Stage 1 | 21 | 17.6 | LOS B | 0.0 | 0.0 | 0.66 | 0.66 |
| P42 | West Stage 2 | 21 | 34.3 | LOS D | 0.0 | 0.0 | 0.93 | 0.93 |
| All Pe | estrians | 126 | 26.3 | LOS C |  |  | 0.80 | 0.80 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

## MOVEMENT SUMMARY

## Site: 5 [Horsley x Ferrers_ Future (with RMS Upgrade)_PM]

The Horsley Drive x Ferrers Road
Road Conditions: The Horsley Drive Upgrades (RMS)
Traffic: 2036 PM Background
Signals - Fixed Time Isolated Cycle Time $=80$ seconds (Optimum Cycle Time - Minimum Delay)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue <br> Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed $\mathrm{km} / \mathrm{h}$ |
| East: The Horsley Drive (750m) |  |  |  |  |  |  |  |  |  |  |  |
| 5 | T1 | 2031 | 10.0 | 0.792 | 9.2 | LOS A | 27.0 | 205.4 | 0.73 | 0.69 | 62.1 |
| 6 | R2 | 568 | 6.9 | 0.755 | 41.0 | LOS C | 11.3 | 84.1 | 0.99 | 0.90 | 53.5 |
| Appro |  | 2599 | 9.3 | 0.792 | 16.1 | LOS B | 27.0 | 205.4 | 0.79 | 0.73 | 58.2 |
| North: Ferrers Road ( 5000 m ) |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 754 | 5.3 | 0.442 | 22.6 | LOS B | 10.3 | 75.2 | 0.74 | 0.78 | 56.2 |
| 9 | R2 | 224 | 5.2 | 0.834 | 48.5 | LOS D | 9.8 | 71.6 | 1.00 | 0.97 | 54.7 |
| Appro |  | 978 | 5.3 | 0.834 | 28.5 | LOS C | 10.3 | 75.2 | 0.80 | 0.83 | 55.8 |
| West: The Horsley Drive (1500m) |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 84 | 55.0 | 0.093 | 10.0 | LOS A | 0.8 | 8.4 | 0.34 | 0.65 | 60.0 |
| 11 | T1 | 1608 | 21.3 | 0.761 | 25.0 | LOS B | 19.1 | 158.4 | 0.92 | 0.87 | 55.2 |
| Approach |  | 1693 | 22.9 | 0.761 | 24.3 | LOS B | 19.1 | 158.4 | 0.89 | 0.86 | 55.8 |
| All Vehicles |  | 5269 | 12.9 | 0.834 | 21.1 | LOS B | 27.0 | 205.4 | 0.82 | 0.79 | 56.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Description | Demand Flow ped/h | Average Delay sec $\qquad$ | Level of Service | Average Back Pedestrian $\qquad$ | of Queue Distance $\qquad$ m | Prop. Queued | Effective Stop Rate per ped |
| P21 | East Stage 1 | 21 | 34.3 | LOS D | 0.0 | 0.0 | 0.93 | 0.93 |
| P22 | East Stage 2 | 21 | 34.3 | LOS D | 0.0 | 0.0 | 0.93 | 0.93 |
| P3 | North Full Crossing | 21 | 20.3 | LOS C | 0.0 | 0.0 | 0.71 | 0.71 |
| P3S | North Slip/Bypass Lane Crossing | 21 | 18.2 | LOS B | 0.0 | 0.0 | 0.68 | 0.68 |
| P41 | West Stage 1 | 21 | 16.9 | LOS B | 0.0 | 0.0 | 0.65 | 0.65 |
| P42 | West Stage 2 | 21 | 32.4 | LOS D | 0.0 | 0.0 | 0.90 | 0.90 |
| All Pe | estrians | 126 | 26.1 | LOS C |  |  | 0.80 | 0.80 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

C3:
Project Case

## USER REPORT FOR SITE

Project: [0541] GWH_Doonside Road_Brabham Drive

目 Site: 1 [[2036 Future+Dev_AM] Doonside x GWH x Brabham]
Doonside Road x Great Western Highway x Brabham Drive Intersection, Eastern Creek
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time $=120$ seconds (Site User-Given Phase Times)
Timings based on settings in the Site Phasing \& Timing dialog
Phase Times specified by the user
Phase Sequence: Standard Diamond (VV1120) - Copy
Reference Phase: Phase A
Input Phase Sequence: G, G2, A, D, E, F2
Output Phase Sequence: G, G2, A, D, E, F2

## Site Layout



| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | Lane \% | Average Delay sec | Level of Service | 95\% Bac <br> Veh | Queue Dist m | Lane Config | Lane Length m | $\begin{aligned} & \text { Cap. } \\ & \text { Adj. } \\ & \% \end{aligned}$ | Prob. Block. \% |
| South: Brabham Drive (380m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 358 | 19.6 | 507 | 0.705 | 100 | 38.4 | LOS C | 17.3 | 141.7 | Full | 380 | 0.0 | 0.0 |
| Lane 2 | 290 | 9.2 | $411{ }^{1}$ | 0.705 | 100 | 39.4 | LOS C | 14.5 | 109.7 | Full | 380 | 0.0 | 0.0 |
| Lane 3 | 179 | 12.4 | 182 | 0.983 | 100 | 99.8 | LOS F | 14.2 | 110.2 | Short | 50 | 0.0 | NA |
| Approach | 826 | 14.4 |  | 0.983 |  | 52.1 | LOS D | 17.3 | 141.7 |  |  |  |  |
| East: Great Western Highway ( 1600 m ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 145 | 12.3 | 686 | 0.212 | 100 | 29.1 | LOS C | 5.2 | 40.3 | Short | 215 | 0.0 | NA |
| Lane 2 | 163 | 10.3 | 181 | 0.900 | 100 | 71.2 | LOS F | 11.0 | 83.9 | Short | 135 | 0.0 | NA |
| Lane 3 | 164 | 10.3 | 183 | 0.900 | 100 | 71.1 | LOS F | 11.1 | 84.7 | Full | 1600 | 0.0 | 0.0 |
| Lane 4 | 164 | 10.3 | 183 | 0.900 | 100 | 71.1 | LOS F | 11.1 | 84.7 | Full | 1600 | 0.0 | 0.0 |
| Lane 5 | 106 | 7.5 | 162 | 0.651 | 100 | 67.6 | LOS E | 6.3 | 47.2 | Short | 125 | 0.0 | NA |
| Lane 6 | 106 | 7.5 | 162 | 0.651 | 100 | 67.6 | LOS E | 6.3 | 47.2 | Short | 120 | 0.0 | NA |
| Approach | 848 | 9.9 |  | 0.900 |  | 63.1 | LOS E | 11.1 | 84.7 |  |  |  |  |
| North: Doonside Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 740 | 6.7 | 780 | 0.948 | 100 | 66.3 | LOS E | 54.5 | 403.0 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 593 | 6.4 | $626{ }^{1}$ | 0.948 | 100 | 65.1 | LOS E | 42.2 | 311.7 | Full | 500 | 0.0 | 0.0 |
| Lane 3 | 161 | 16.8 | 264 | 0.609 | 100 | 34.2 | LOS C | 4.9 | 39.4 | Short | 70 | 0.0 | NA |
| Lane 4 | 159 | 16.8 | 261 | 0.609 | 100 | 34.2 | LOS C | 4.9 | 39.0 | Short | 60 | 0.0 | NA |
| Approach | 1653 | 8.5 |  | 0.948 |  | 59.6 | LOS E | 54.5 | 403.0 |  |  |  |  |
| West: Great Western Highway ( 390 m ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 539 | 9.2 | 1243 | 0.434 | 100 | 12.5 | LOS A | 10.7 | 80.6 | Short | 150 | 0.0 | NA |
| Lane 2 | 304 | 8.5 | 436 | 0.699 | $85^{6}$ | 46.1 | LOS D | 16.6 | 124.5 | Full | 390 | 0.0 | 0.0 |
| Lane 3 | 356 | 8.5 | 436 | 0.818 | 100 | 52.1 | LOS D | 21.4 | 160.5 | Full | 390 | 0.0 | 0.0 |
| Lane 4 | 353 | 8.5 | 431 | 0.818 | 100 | 52.2 | LOS D | 21.2 | 159.0 | Full | 390 | 0.0 | 0.0 |
| Lane 5 | 367 | 12.9 | 385 | 0.954 | 100 | 85.6 | LOS F | 27.9 | 217.1 | Short | 145 | 0.0 | NA |
| Lane 6 | 367 | 12.9 | 385 | 0.954 | 100 | 85.6 | LOS F | 27.9 | 217.1 | Short | 140 | 0.0 | NA |
| Approach | 2286 | 10.1 |  | 0.954 |  | 52.7 | LOS D | 27.9 | 217.1 |  |  |  |  |
| Intersection | 5614 | 10.2 |  | 0.983 |  | 56.2 | LOS D | 54.5 | 403.0 |  |  |  |  |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Lane LOS values are based on average delay per lane.
Intersection and Approach LOS values are based on average delay for all lanes.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
1 Reduced capacity due to a short lane effect. Short lane queues may extend into the full-length lanes. Some upstream delays at entry to short lanes are not included.
6 Lane under-utilisation due to downstream effects

## USER REPORT FOR SITE

Project: [0541] GWH_Doonside Road_Brabham Drive

## 目 Site: 1 [[2036 Future+Dev_PM] Doonside x GWH x Brabham]

Doonside Road x Great Western Highway x Brabham Drive Intersection, Eastern Creek
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time $=120$ seconds (Site User-Given Cycle Time)
Variable Sequence Analysis applied. The results are given for the selected output sequence.
Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Green Split Priority has been specified
Phase Sequence: Standard Diamond (VV1120)
Reference Phase: Phase A
Input Phase Sequence: G, G1*, G2*, A, B*, C*, D, D1*, D2*, E, F1*, F2*
Output Phase Sequence: G, G1 ${ }^{*}$, A, D, D2*, E
(* Variable Phase)
Site Layout


Input Volumes

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | $\begin{aligned} & \text { Lane } \\ & \text { Util. } \\ & \% \end{aligned}$ | Average Delay sec | Level of Service | $\begin{gathered} \text { 95\% Bac } \\ \text { Veh } \end{gathered}$ | Queue Dist m | Lane Config | Lane Length m | Cap. Adj. \% | Prob. Block. \% |
| South: Brabham Drive (380m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 644 | 10.7 | 719 | 0.896 | 100 | 51.9 | LOS D | 41.5 | 317.3 | Full | 380 | 0.0 | 0.0 |
| Lane 2 | 561 | 3.5 | $626{ }^{1}$ | 0.896 | 100 | 49.0 | LOS D | 34.7 | 250.3 | Full | 380 | 0.0 | 0.0 |
| Lane 3 | 122 | 4.3 | 222 | 0.551 | 100 | 60.5 | LOS E | 6.9 | 50.4 | Short | 50 | 0.0 | NA |
| Approach | 1327 | 7.1 |  | 0.896 |  | 51.5 | LOS D | 41.5 | 317.3 |  |  |  |  |
| East: Great Western Highway (1600m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 120 | 7.9 | 1125 | 0.107 | 100 | 12.9 | LOS A | 2.1 | 15.7 | Short | 215 | 0.0 | NA |
| Lane 2 | 341 | 6.1 | 371 | 0.918 | 100 | 68.1 | LOS E | 23.7 | 174.7 | Short | 135 | 0.0 | NA |
| Lane 3 | 344 | 6.1 | 375 | 0.918 | 100 | 68.0 | LOS E | 23.9 | 176.3 | Full | 1600 | 0.0 | 0.0 |
| Lane 4 | 344 | 6.1 | 375 | 0.918 | 100 | 68.0 | LOS E | 23.9 | 176.3 | Full | 1600 | 0.0 | 0.0 |
| Lane 5 | 178 | 3.2 | 243 | 0.733 | 100 | 64.7 | LOS E | 10.6 | 76.5 | Short | 125 | 0.0 | NA |
| Lane 6 | 178 | 3.2 | 243 | 0.733 | 100 | 64.7 | LOS E | 10.6 | 76.5 | Short | 120 | 0.0 | NA |
| Approach | 1506 | 5.6 |  | 0.918 |  | 62.8 | LOS E | 23.9 | 176.3 |  |  |  |  |
| North: Doonside Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 424 | 6.7 | 780 | 0.544 | 100 | 32.8 | LOS C | 18.7 | 138.5 | Full | 500 | 0.0 | 0.0 |
| Lane 2 | 379 | 5.6 | $696{ }^{1}$ | 0.544 | 100 | 31.0 | LOS C | 16.8 | 123.2 | Full | 500 | 0.0 | 0.0 |
| Lane 3 | 209 | 10.4 | 232 | 0.902 | 100 | 76.6 | LOS F | 14.2 | 108.6 | Short | 70 | 0.0 | NA |
| Lane 4 | 207 | 10.4 | 229 | 0.902 | 100 | 76.8 | LOS F | 14.1 | 107.6 | Short | 60 | 0.0 | NA |
| Approach | 1219 | 7.6 |  | 0.902 |  | 47.2 | LOS D | 18.7 | 138.5 |  |  |  |  |
| West: Great Western Highway (390m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 399 | 13.2 | 898 | 0.445 | 100 | 22.2 | LOS B | 13.1 | 101.9 | Short | 150 | 0.0 | NA |
| Lane 2 | 181 | 4.2 | 288 | 0.631 | $85^{6}$ | 52.8 | LOS D | 10.2 | 74.1 | Full | 390 | 0.0 | 0.0 |
| Lane 3 | 212 | 4.2 | 288 | 0.738 | 100 | 55.5 | LOS D | 12.5 | 90.7 | Full | 390 | 0.0 | 0.0 |
| Lane 4 | 210 | 4.2 | 285 | 0.738 | 100 | 55.6 | LOS D | 12.4 | 89.8 | Full | 390 | 0.0 | 0.0 |
| Lane 5 | 125 | 17.6 | 138 | 0.906 | 100 | 81.5 | LOS F | 8.6 | 69.5 | Short | 145 | 0.0 | NA |
| Lane 6 | 125 | 17.6 | 138 | 0.906 | 100 | 81.5 | LOS F | 8.6 | 69.5 | Short | 140 | 0.0 | NA |
| Approach | 1254 | 9.7 |  | 0.906 |  | 49.7 | LOS D | 13.1 | 101.9 |  |  |  |  |
| Intersection | 5306 | 7.4 |  | 0.918 |  | 53.3 | LOS D | 41.5 | 317.3 |  |  |  |  |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Lane LOS values are based on average delay per lane.
Intersection and Approach LOS values are based on average delay for all lanes.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
1 Reduced capacity due to a short lane effect. Short lane queues may extend into the full-length lanes. Some upstream delays at entry to short lanes are not included.
6 Lane under-utilisation due to downstream effects

## MOVEMENT SUMMARY

## Site: 2 [Huntingwood x GWH <br> Future + Dev_AM ]

Huntingwood Drive x Great Western Highway T-Intersection, Huntingwood
Road Conditions: 2018 Existing (Site access to/from Ferrers Road only)
Traffic: 2036 AM Background with Development
Signals - Fixed Time Isolated Cycle Time = 110 seconds (User-Given Cycle Time)
Variable Sequence Analysis applied. The results are given for the selected output sequence.

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov OD  <br> ID Mov | Dema Total veh/h | $\begin{array}{r} \text { Flows } \\ \text { HV } \\ \% \end{array}$ | $\begin{aligned} & \text { Deg. } \\ & \text { Satn } \\ & \text { v/c } \end{aligned}$ | Average Delay sec | Level of Service | 95\% Back Vehicles veh | f Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Huntingwood Drive (1800m) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 22 | 47.6 | 0.659 | 55.2 | LOS D | 6.5 | 55.9 | 1.00 | 0.85 | 50.4 |
| 3 R2 | 228 | 22.6 | 0.659 | 57.2 | LOS E | 6.8 | 56.8 | 1.00 | 0.84 | 45.2 |
| Approach | 251 | 24.8 | 0.659 | 57.0 | LOS E | 6.8 | 56.8 | 1.00 | 0.84 | 45.7 |
| East: Great Western Highway ( 780 m ) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 596 | 11.1 | 0.346 | 7.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.60 | 73.1 |
| $5 \quad$ T1 | 831 | 8.9 | 0.349 | 9.4 | LOS A | 10.0 | 75.5 | 0.49 | 0.43 | 73.6 |
| Approach | 1426 | 9.8 | 0.349 | 8.8 | LOS A | 10.0 | 75.5 | 0.29 | 0.50 | 73.3 |
| West: Great Western Highway ( 1600 m ) |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 2043 | 7.1 | 0.709 | 6.6 | LOS A | 27.1 | 200.9 | 0.55 | 0.51 | 75.4 |
| 12 R2 | 47 | 17.8 | 0.395 | 63.1 | LOS E | 2.6 | 20.9 | 0.99 | 0.75 | 50.0 |
| Approach | 2091 | 7.3 | 0.709 | 7.9 | LOS A | 27.1 | 200.9 | 0.56 | 0.52 | 74.2 |
| All Vehicles | 3767 | 9.4 | 0.709 | 11.5 | LOS A | 27.1 | 200.9 | 0.48 | 0.53 | 70.7 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^4]
## MOVEMENT SUMMARY

Site: 2 [Huntingwood x GWH_Future + Dev_PM ]
Huntingwood Drive x Great Western Highway T-Intersection, Huntingwood
Road Conditions: 2018 Existing (Site access to/from Ferrers Road only)
Traffic: 2036 PM Background with Development
Signals - Fixed Time Isolated Cycle Time = 140 seconds (User-Given Cycle Time)
Variable Sequence Analysis applied. The results are given for the selected output sequence.

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov OD ID Mov | Dema Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue <br> Distance | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Huntingwood Drive (1800m) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 58 | 23.6 | 0.755 | 66.7 | LOS E | 21.8 | 163.8 | 0.98 | 0.92 | 48.6 |
| 3 R2 | 634 | 5.3 | 0.755 | 62.2 | LOS E | 22.4 | 163.7 | 0.98 | 0.89 | 44.5 |
| Approach | 692 | 6.8 | 0.755 | 62.6 | LOS E | 22.4 | 163.8 | 0.98 | 0.89 | 44.9 |
| East: Great Western Highway (780m) |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 179 | 20.0 | 0.110 | 7.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.59 | 72.6 |
| $5 \quad$ T1 | 1626 | 4.3 | 0.772 | 23.8 | LOS B | 43.0 | 312.1 | 0.82 | 0.75 | 65.5 |
| Approach | 1805 | 5.9 | 0.772 | 22.2 | LOS B | 43.0 | 312.1 | 0.73 | 0.74 | 66.2 |
| West: Great Western Highway ( 1600 m ) |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 1098 | 3.7 | 0.439 | 12.1 | LOS A | 17.6 | 127.4 | 0.52 | 0.47 | 71.9 |
| 12 R2 | 8 | 25.0 | 0.125 | 81.3 | LOS F | 0.6 | 5.0 | 0.99 | 0.67 | 46.5 |
| Approach | 1106 | 3.9 | 0.439 | 12.7 | LOS A | 17.6 | 127.4 | 0.52 | 0.47 | 71.5 |
| All Vehicles | 3603 | 5.5 | 0.772 | 27.0 | LOS B | 43.0 | 312.1 | 0.72 | 0.69 | 61.5 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^5]
## MOVEMENT SUMMARY

## © Site: 3 [Huntingwood x Brabham_ Future + Dev_AM]

Huntingwood Drive x Brabham Drive Intersection, Eastern Creek
Road Conditions: 2018 Existing (Site access to/from Ferrers Road only)
Traffic: 2036 AM Background with Development
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h |  | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | f Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Brabham Drive (640m) |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 137 | 18.5 | 0.426 | 4.8 | LOS A | 3.6 | 27.6 | 0.51 | 0.47 | 53.5 |
| 2 | T1 | 671 | 10.4 | 0.426 | 4.6 | LOS A | 3.6 | 27.6 | 0.52 | 0.51 | 55.0 |
| 3 | R2 | 292 | 9.7 | 0.426 | 10.6 | LOS A | 3.4 | 26.2 | 0.54 | 0.59 | 57.1 |
| Appr |  | 1099 | 11.2 | 0.426 | 6.2 | LOS A | 3.6 | 27.6 | 0.52 | 0.52 | 55.8 |
| East: Huntingwood Drive (1800m) |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 139 | 21.2 | 0.473 | 8.1 | LOS A | 2.5 | 21.8 | 0.77 | 0.91 | 56.1 |
| 5 | T1 | 56 | 35.8 | 0.473 | 8.4 | LOS A | 2.5 | 21.8 | 0.77 | 0.91 | 56.4 |
| 6 | R2 | 72 | 39.7 | 0.473 | 14.4 | LOS A | 2.5 | 21.8 | 0.77 | 0.91 | 56.2 |
| Appr | ch | 266 | 29.2 | 0.473 | 9.9 | LOS A | 2.5 | 21.8 | 0.77 | 0.91 | 56.2 |
| North: Brabham Drive (380m) |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 425 | 10.4 | 0.694 | 10.0 | LOS A | 8.9 | 68.2 | 0.89 | 0.92 | 55.6 |
| 8 | T1 | 947 | 10.6 | 0.694 | 11.2 | LOS A | 8.9 | 68.2 | 0.90 | 0.97 | 52.1 |
| 9 | R2 | 26 | 16.0 | 0.694 | 18.0 | LOS B | 8.5 | 64.7 | 0.91 | 1.00 | 48.9 |
| Appr |  | 1399 | 10.6 | 0.694 | 11.0 | LOS A | 8.9 | 68.2 | 0.90 | 0.95 | 53.7 |
| West: Huntingwood Drive (360m) |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 41 | 53.8 | 0.338 | 7.9 | LOS A | 1.4 | 11.9 | 0.64 | 0.78 | 48.6 |
| 11 | T1 | 106 | 19.8 | 0.338 | 6.7 | LOS A | 1.4 | 11.9 | 0.64 | 0.78 | 56.7 |
| 12 | R2 | 75 | 23.9 | 0.338 | 12.6 | LOS A | 1.4 | 11.9 | 0.64 | 0.78 | 53.3 |
| Appr |  | 222 | 27.5 | 0.338 | 8.9 | LOS A | 1.4 | 11.9 | 0.64 | 0.78 | 55.0 |
| All V | cles | 2986 | 13.7 | 0.694 | 9.0 | LOS A | 8.9 | 68.2 | 0.73 | 0.78 | 54.9 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Organisation: ASON GROUP PTY LTD | Processed: Tuesday, 5 February 2019 10:26:45 AM
Project: C:IUsers\Sharif Hasan\Desktopl0541 Lighthorselsidralmodels\AG0541m3v3 (No Wallgrove access)_Lighthorse_Future Base + Development.sip7

## MOVEMENT SUMMARY

## © Site: 3 [Huntingwood x Brabham_ Future + Dev_PM]

Huntingwood Drive x Brabham Drive Intersection, Eastern Creek
Road Conditions: 2018 Existing (Site access to/from Ferrers Road only)
Traffic: 2036 PM Background with Development
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \mathrm{Mov} \\ & \mathrm{ID} \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Deman Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Brabham Drive (640m) min |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 129 | 21.1 | 0.670 | 9.5 | LOS A | 8.4 | 64.2 | 0.93 | 0.90 | 51.3 |
| 2 | T1 | 966 | 8.9 | 0.670 | 9.6 | LOS A | 8.4 | 64.2 | 0.94 | 0.93 | 52.6 |
| 3 | R2 | 161 | 15.0 | 0.670 | 16.7 | LOS B | 7.9 | 60.2 | 0.94 | 0.98 | 56.0 |
| Appro |  | 1257 | 11.0 | 0.670 | 10.5 | LOS A | 8.4 | 64.2 | 0.94 | 0.93 | 53.3 |
| East: Huntingwood Drive (1800m) |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 306 | 5.2 | 0.898 | 13.3 | LOS A | 10.1 | 75.1 | 0.90 | 1.23 | 54.4 |
| 5 | T1 | 186 | 6.2 | 0.898 | 13.2 | LOS A | 10.1 | 75.1 | 0.90 | 1.23 | 54.5 |
| 6 | R2 | 256 | 9.1 | 0.898 | 19.0 | LOS B | 10.1 | 75.1 | 0.90 | 1.23 | 54.6 |
| Appro |  | 748 | 6.8 | 0.898 | 15.2 | LOS B | 10.1 | 75.1 | 0.90 | 1.23 | 54.5 |
| North: Brabham Drive (380m) |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 89 | 28.2 | 0.378 | 5.8 | LOS A | 2.9 | 22.0 | 0.61 | 0.53 | 56.4 |
| 8 | T1 | 766 | 7.3 | 0.378 | 5.5 | LOS A | 2.9 | 22.0 | 0.62 | 0.55 | 55.0 |
| 9 | R2 | 18 | 23.5 | 0.378 | 11.9 | LOS A | 2.7 | 20.4 | 0.63 | 0.57 | 52.6 |
| Appro |  | 874 | 9.8 | 0.378 | 5.6 | LOS A | 2.9 | 22.0 | 0.62 | 0.55 | 55.2 |
| West: Huntingwood Drive (360m) |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 51 | 22.9 | 0.390 | 8.8 | LOS A | 2.0 | 15.4 | 0.79 | 0.92 | 47.8 |
| 11 | T1 | 52 | 12.2 | 0.390 | 8.3 | LOS A | 2.0 | 15.4 | 0.79 | 0.92 | 55.9 |
| 12 | R2 | 89 | 11.8 | 0.390 | 14.1 | LOS A | 2.0 | 15.4 | 0.79 | 0.92 | 52.2 |
| Appro |  | 192 | 14.8 | 0.390 | 11.1 | LOS A | 2.0 | 15.4 | 0.79 | 0.92 | 53.1 |
| All Ve |  | 3071 | 9.8 | 0.898 | 10.3 | LOS A | 10.1 | 75.1 | 0.83 | 0.90 | 54.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

© Site: 4 [Ferrers x Brabham x Peter Brock_ Future + Dev_AM]

Ferrers Road x Brabham Drive x Peter Brock Drive, Eastern Creek
Road Conditions: 2018 Existing (Site access to/from Ferrers Road only)
Traffic: 2036 AM Background with Development
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov OD  <br> ID Mov | Deman Total veh/h |  | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | f Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| East: Peter Brock Drive (500m) mid |  |  |  |  |  |  |  |  |  |  |
| 5 T1 | 58 | 21.8 | 0.294 | 13.1 | LOS A | 1.8 | 15.0 | 0.89 | 0.94 | 40.6 |
| 6 R2 | 56 | 22.6 | 0.294 | 18.6 | LOS B | 1.8 | 15.0 | 0.89 | 0.94 | 46.5 |
| Approach | 114 | 22.2 | 0.294 | 15.8 | LOS B | 1.8 | 15.0 | 0.89 | 0.94 | 43.9 |
| North: Brabham Drive (640m) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 139 | 24.2 | 0.138 | 4.4 | LOS A | 0.8 | 6.7 | 0.28 | 0.45 | 52.1 |
| 9 R2 | 1140 | 12.4 | 0.710 | 10.1 | LOS A | 9.3 | 71.8 | 0.47 | 0.56 | 50.4 |
| Approach | 1279 | 13.7 | 0.710 | 9.4 | LOS A | 9.3 | 71.8 | 0.45 | 0.54 | 50.6 |
| West: Ferrers Road (250m) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 1007 | 9.3 | 0.384 | 4.0 | LOS A | 3.0 | 22.8 | 0.28 | 0.43 | 54.6 |
| 11 T1 | 72 | 10.3 | 0.384 | 3.9 | LOS A | 2.9 | 22.2 | 0.29 | 0.42 | 51.1 |
| Approach | 1079 | 9.4 | 0.384 | 4.0 | LOS A | 3.0 | 22.8 | 0.28 | 0.43 | 54.4 |
| All Vehicles | 2472 | 12.2 | 0.710 | 7.4 | LOS A | 9.3 | 71.8 | 0.40 | 0.51 | 51.7 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Development.sip7

## MOVEMENT SUMMARY

© Site: 4 [Ferrers x Brabham x Peter Brock_ Future + Dev_PM]

Ferrers Road x Brabham Drive x Peter Brock Drive, Eastern Creek
Road Conditions: 2018 Existing (Site access to/from Ferrers Road only)
Traffic: 2036 PM Background with Development
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov OD  <br> ID Mov | Deman Total veh/h |  | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | f Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| East: Peter Brock Drive (500m) per veh |  |  |  |  |  |  |  |  |  |  |
| 5 T1 | 91 | 8.1 | 0.563 | 21.7 | LOS B | 4.8 | 37.3 | 0.97 | 1.17 | 36.7 |
| 6 R2 | 142 | 15.6 | 0.563 | 27.6 | LOS B | 4.8 | 37.3 | 0.97 | 1.17 | 42.3 |
| Approach | 233 | 12.7 | 0.563 | 25.3 | LOS B | 4.8 | 37.3 | 0.97 | 1.17 | 40.5 |
| North: Brabham Drive (640m) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 45 | 7.0 | 0.041 | 3.9 | LOS A | 0.2 | 1.7 | 0.20 | 0.42 | 52.4 |
| 9 R2 | 1196 | 7.0 | 0.702 | 9.7 | LOS A | 10.2 | 75.6 | 0.38 | 0.54 | 51.3 |
| Approach | 1241 | 7.0 | 0.702 | 9.5 | LOS A | 10.2 | 75.6 | 0.38 | 0.54 | 51.4 |
| West: Ferrers Road (250m) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 1173 | 10.0 | 0.488 | 4.6 | LOS A | 4.1 | 31.3 | 0.50 | 0.52 | 53.7 |
| 11 T1 | 42 | 20.0 | 0.488 | 4.7 | LOS A | 4.0 | 30.5 | 0.51 | 0.52 | 50.0 |
| Approach | 1215 | 10.3 | 0.488 | 4.6 | LOS A | 4.1 | 31.3 | 0.50 | 0.52 | 53.5 |
| All Vehicles | 2688 | 9.0 | 0.702 | 8.6 | LOS A | 10.2 | 75.6 | 0.48 | 0.58 | 50.9 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Development.sip7

## 目 Site: 5 [[s03] Horsley x Ferrers_Future + Dev_AM]

The Horsley Drive x Ferrers Road T-Intersection, Horsley Park
Road Conditions: 2018 Existing
Traffic: 2036 AM Future Baseline with Development
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time $=78$ seconds (Site User-Given Phase Times)
Timings based on settings in the Site Phasing \& Timing dialog
Phase Times specified by the user
Phase Sequence: Three Phase
Reference Phase: Phase B
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

## Input Volumes

Volume Display Method: Total and Veh


| HV | LV | Tot |  |
| :--- | :--- | :--- | :--- |
| 27 | 106 | 133 | L2 |
| 278 | 1296 | 1574 | T1 |



|  | Tot | LV | HV |
| :--- | :--- | :--- | :--- |
| R2 | 727 | 649 | 78 |
| T1 | 1461 | 1087 | 374 |


|  | All MCs | Light Vehicles (LV) | Heavy Vehicles (HV) |
| :--- | :---: | :---: | :---: |
| E: The Horsley Drive (160m) | 2188 | 1736 | 452 |
| N: Ferrers Road (5000m) | 548 | 482 | 66 |
| W: The Horsley Drive (1500m) | 1707 | 1402 | 305 |
| Total | 4443 | 3620 | 823 |


| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{array}{r} \text { Flows } \\ \text { HV } \\ \% \\ \hline \end{array}$ | Cap. veh/h | Deg. Satn v/c | Lane \% | Average Delay sec | Level of Service | 95\% Back <br> Veh | Queue m | Lane Config | Lane Length m | $\begin{aligned} & \text { Cap. } \\ & \text { Adj. } \\ & \% \end{aligned}$ | Prob. Block. \% |
| East: The Horsley Drive (160m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 769 | 25.6 | 1279 | 0.601 | 100 | 4.1 | LOS A | 12.5 | 106.6 | Full | 160 | 0.0 | 0.0 |
| Lane 2 | 769 | 25.6 | 1279 | 0.601 | 100 | 4.1 | LOS A | 12.5 | 106.6 | Full | 160 | 0.0 | $100.0^{8}$ |
| Lane 3 | 765 | 10.7 | $457{ }^{1}$ | 1.673 | 100 | 646.8 | LOS F | 160.4 | 1226.2 | Short | 75 | 0.0 | NA |
| Approach | 2303 | 20.7 |  | 1.673 |  | 217.7 | LOS F | 160.4 | 1226.2 |  |  |  |  |
| North: Ferrers Road (5000m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 527 | 9.4 | 986 | 0.535 | 100 | 19.0 | LOS B | 10.5 | 79.2 | Short | 55 | 0.0 | NA |
| Lane 2 | 49 | 40.4 | 166 | 0.297 | 100 | 42.3 | LOS C | 1.8 | 17.4 | Full | 5000 | 0.0 | 0.0 |
| Approach | 577 | 12.0 |  | 0.535 |  | 21.0 | LOS B | 10.5 | 79.2 |  |  |  |  |
| West: The Horsley Drive (1500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 897 | 18.1 | 737 | 1.216 | 100 | 240.7 | LOS F | 111.4 | 900.8 | Full | 1500 | 0.0 | 0.0 |
| Lane 2 | 900 | 17.7 | 740 | 1.216 | 100 | 239.6 | LOS F | 111.5 | 898.8 | Full | 1500 | 0.0 | 0.0 |
| Approach | 1797 | 17.9 |  | 1.216 |  | 240.2 | LOS F | 111.5 | 900.8 |  |  |  |  |
| Intersection | 4677 | 18.5 |  | 1.673 |  | 202.1 | LOS F | 160.4 | 1226.2 |  |  |  |  |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Lane LOS values are based on average delay per lane.
Intersection and Approach LOS values are based on average delay for all lanes.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
1 Reduced capacity due to a short lane effect. Short lane queues may extend into the full-length lanes. Some upstream delays at entry to short lanes are not included.
8 Probability of Blockage has been set on the basis of a queue that overflows from a short lane.

## 目 Site: 5 [[s03] Horsley x Ferrers_Future + Dev_PM]

The Horsley Drive x Ferrers Road T-Intersection, Horsley Park
Road Conditions: 2018 Existing
Traffic: 2036 PM Future Baseline with Development
Site Category: (None)
Signals - Fixed Time Isolated Cycle Time $=65$ seconds (Site User-Given Phase Times)
Timings based on settings in the Site Phasing \& Timing dialog
Phase Times specified by the user
Phase Sequence: Three Phase
Reference Phase: Phase B
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

## Input Volumes

Volume Display Method: Total and Veh


| HV | LV | Tot |  |
| :--- | :--- | :--- | :--- |
| 45 | 40 | 85 | L2 |
| 325 | 1203 | 1528 | T1 |



|  | Tot | LV | HV |
| :--- | :--- | :--- | :--- |
| R2 | 548 | 509 | 39 |
| T1 | 1929 | 1737 | 192 |


|  | All MCs | Light Vehicles (LV) | Heavy Vehicles (HV) |
| :--- | :---: | :---: | :---: |
| E: The Horsley Drive (160m) | 2477 | 2246 | 231 |
| N: Ferrers Road (5000m) | 980 | 916 | 64 |
| W: The Horsley Drive (1500m) | 1613 | 1243 | 370 |
| Total | 5070 | 4405 | 665 |


| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | Lane \% | Average Delay sec | Level of Service | 95\% Bac <br> Veh | Queue Dist m | Lane Config | Lane Length m | $\begin{aligned} & \text { Cap. } \\ & \text { Adj. } \\ & \% \end{aligned}$ | Prob. Block. \% |
| East: The Horsley Drive (160m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 1140 | 10.0 | 1233 | 0.925 | 100 | 29.1 | LOS C | 47.0 | 356.8 | Full | 160 | 0.0 | 79.9 |
| Lane 2 | 890 | 10.0 | $963{ }^{1}$ | 0.925 | 100 | 30.6 | LOS C | 32.1 | 244.0 | Full | 160 | 0.0 | $87.0{ }^{8}$ |
| Lane 3 | 577 | 7.1 | 514 | 1.122 | 100 | 161.3 | LOS F | 51.6 | 383.4 | Short | 75 | 0.0 | NA |
| Approach | 2607 | 9.3 |  | 1.122 |  | 58.8 | LOS E | 51.6 | 383.4 |  |  |  |  |
| North: Ferrers Road (5000m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 772 | 6.5 | 1234 | 0.625 | 100 | 12.8 | LOS A | 10.5 | 77.4 | Short | 55 | 0.0 | NA |
| Lane 2 | 260 | 6.5 | 328 | 0.793 | 100 | 37.9 | LOS C | 9.0 | 66.5 | Full | 5000 | 0.0 | 0.0 |
| Approach | 1032 | 6.5 |  | 0.793 |  | 19.1 | LOS B | 10.5 | 77.4 |  |  |  |  |
| West: The Horsley Drive (1500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 841 | 24.6 | 492 | 1.710 | 100 | 672.1 | LOS F | 175.3 | 1486.5 | Full | 1500 | 0.0 | 4.2 |
| Lane 2 | 856 | 21.3 | 501 | 1.710 | 100 | 670.8 | LOS F | 178.2 | 1474.4 | Full | 1500 | 0.0 | 3.5 |
| Approach | 1698 | 22.9 |  | 1.710 |  | 671.5 | LOS F | 178.2 | 1486.5 |  |  |  |  |
| Intersection | 5337 | 13.1 |  | 1.710 |  | 246.1 | LOS F | 178.2 | 1486.5 |  |  |  |  |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Lane LOS values are based on average delay per lane.
Intersection and Approach LOS values are based on average delay for all lanes.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
1 Reduced capacity due to a short lane effect. Short lane queues may extend into the full-length lanes. Some upstream delays at entry to short lanes are not included.
8 Probability of Blockage has been set on the basis of a queue that overflows from a short lane.

## MOVEMENT SUMMARY

## Site: 5 [Horsley x Ferrers_ Future + Dev (RMS Upgrade)_AM]

The Horsley Drive x Ferrers Road
Road Conditions: The Horsley Drive Upgrades (RMS)
Traffic: 2036 AM Background with Development (Site access to/from Ferrers Road only)
Signals - Fixed Time Isolated Cycle Time $=80$ seconds (Optimum Cycle Time - Minimum Delay)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov OD  <br> ID Mov | Deman Total veh/h | $\begin{gathered} \text { =lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles <br> veh | f Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| East: The Horsley Drive (750m) |  |  |  |  |  |  |  |  |  |  |
| 5 T1 | 1538 | 25.6 | 0.593 | 4.0 | LOS A | 12.4 | 106.0 | 0.45 | 0.41 | 64.6 |
| 6 R2 | 765 | 10.7 | 0.771 | 37.4 | LOS C | 14.9 | 114.3 | 0.98 | 0.91 | 54.0 |
| Approach | 2303 | 20.7 | 0.771 | 15.1 | LOS B | 14.9 | 114.3 | 0.63 | 0.58 | 58.2 |
| North: Ferrers Road (5000m) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 527 | 9.4 | 0.318 | 21.5 | LOS B | 6.7 | 50.9 | 0.69 | 0.76 | 56.3 |
| 9 R2 | 49 | 40.4 | 0.458 | 48.0 | LOS D | 2.0 | 19.2 | 1.00 | 0.75 | 54.3 |
| Approach | 577 | 12.0 | 0.458 | 23.8 | LOS B | 6.7 | 50.9 | 0.72 | 0.75 | 56.1 |
| West: The Horsley Drive (1500m) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 140 | 20.3 | 0.142 | 10.9 | LOS A | 1.7 | 14.4 | 0.41 | 0.68 | 60.1 |
| 11 T1 | 1657 | 17.7 | 0.769 | 25.3 | LOS B | 19.9 | 160.5 | 0.92 | 0.88 | 55.1 |
| Approach | 1797 | 17.9 | 0.769 | 24.2 | LOS B | 19.9 | 160.5 | 0.88 | 0.86 | 56.0 |
| All Vehicles | 4677 | 18.5 | 0.771 | 19.7 | LOS B | 19.9 | 160.5 | 0.74 | 0.71 | 57.1 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Description | Demand Flow ped/h | Average Delay $\qquad$ sec | Level of Service | Average Back Pedestrian $\qquad$ ped | of Queue Distance $\qquad$ | Prop. Queued | Effective Stop Rate per ped |
| P21 | East Stage 1 | 21 | 34.3 | LOS D | 0.0 | 0.0 | 0.93 | 0.93 |
| P22 | East Stage 2 | 21 | 34.3 | LOS D | 0.0 | 0.0 | 0.93 | 0.93 |
| P3 | North Full Crossing | 21 | 20.3 | LOS C | 0.0 | 0.0 | 0.71 | 0.71 |
| P3S | North Slip/Bypass Lane Crossing | 21 | 18.2 | LOS B | 0.0 | 0.0 | 0.68 | 0.68 |
| P41 | West Stage 1 | 21 | 16.9 | LOS B | 0.0 | 0.0 | 0.65 | 0.65 |
| P42 | West Stage 2 | 21 | 34.3 | LOS D | 0.0 | 0.0 | 0.93 | 0.93 |
| All Pe | estrians | 126 | 26.4 | LOS C |  |  | 0.80 | 0.80 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

## MOVEMENT SUMMARY

## Site: 5 [Horsley x Ferrers_ Future + Dev (RMS Upgrade)_PM]

The Horsley Drive x Ferrers Road
Road Conditions: The Horsley Drive Upgrades (RMS)
Traffic: 2036 PM Background with Development (Site access to/from Ferrers Road only)
Signals - Fixed Time Isolated Cycle Time = 110 seconds (Optimum Cycle Time - Minimum Delay)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov OD  <br> ID Mov | Deman Total veh/h | Fows HV $\%$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | f Queue <br> Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| East: The Horsley Drive (750m) |  |  |  |  |  |  |  |  |  |  |
| 5 T1 | 2031 | 10.0 | 0.841 | 12.2 | LOS A | 41.9 | 318.7 | 0.71 | 0.67 | 60.7 |
| 6 R2 | 577 | 7.1 | 0.718 | 49.7 | LOS D | 14.8 | 110.1 | 0.98 | 0.86 | 52.3 |
| Approach | 2607 | 9.3 | 0.841 | 20.5 | LOS B | 41.9 | 318.7 | 0.77 | 0.71 | 56.9 |
| North: Ferrers Road (5000m) |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 772 | 6.5 | 0.439 | 27.5 | LOS B | 14.0 | 103.3 | 0.73 | 0.78 | 55.4 |
| 9 R2 | 261 | 6.5 | 0.851 | 61.9 | LOS E | 15.4 | 113.6 | 1.00 | 0.95 | 53.0 |
| Approach | 1033 | 6.5 | 0.851 | 36.2 | LOS C | 15.4 | 113.6 | 0.80 | 0.83 | 54.7 |
| West: The Horsley Drive (1500m) |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 89 | 52.9 | 0.095 | 10.1 | LOS A | 1.1 | 10.8 | 0.29 | 0.64 | 60.0 |
| 11 T1 | 1608 | 21.3 | 0.730 | 28.5 | LOS C | 24.2 | 200.3 | 0.88 | 0.81 | 53.9 |
| Approach | 1698 | 22.9 | 0.730 | 27.6 | LOS B | 24.2 | 200.3 | 0.85 | 0.80 | 54.7 |
| All Vehicles | 5338 | 13.1 | 0.851 | 25.8 | LOS B | 41.9 | 318.7 | 0.80 | 0.76 | 55.6 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Description | Demand Flow ped/h | Average Delay sec $\qquad$ | Level of Service | Average Back Pedestrian $\qquad$ | of Queue Distance $\qquad$ m | Prop. Queued | Effective Stop Rate per ped |
| P21 | East Stage 1 | 21 | 45.5 | LOS E | 0.1 | 0.1 | 0.91 | 0.91 |
| P22 | East Stage 2 | 21 | 43.7 | LOS E | 0.1 | 0.1 | 0.89 | 0.89 |
| P3 | North Full Crossing | 21 | 23.6 | LOS C | 0.0 | 0.0 | 0.66 | 0.66 |
| P3S | North Slip/Bypass Lane Crossing | 21 | 21.7 | LOS C | 0.0 | 0.0 | 0.63 | 0.63 |
| P41 | West Stage 1 | 21 | 20.4 | LOS C | 0.0 | 0.0 | 0.61 | 0.61 |
| P42 | West Stage 2 | 21 | 41.1 | LOS E | 0.1 | 0.1 | 0.86 | 0.86 |
| All Pe | estrians | 126 | 32.7 | LOS D |  |  | 0.76 | 0.76 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

## MOVEMENT SUMMARY

© Site: 6 [Site x Ferrers_ Future + Dev_AM]

Site Access x Ferrers Road Intersection, Eastern Creek
Road Conditions: Existing 2018 (plus Proposed Site access to/from Ferrers Road only)
Traffic: 2036 AM Background with Development
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov OD  <br> ID Mov | Dema Total veh/h | $\begin{gathered} \text { Fows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue <br> Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| East: Ferrers Road (250m) sec |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 913 | 8.2 | 0.768 | 4.1 | LOS A | 15.5 | 120.1 | 0.34 | 0.40 | 55.2 |
| 9 R2 | 285 | 28.0 | 0.768 | 9.0 | LOS A | 15.5 | 120.1 | 0.34 | 0.40 | 51.3 |
| Approach | 1198 | 12.9 | 0.768 | 5.3 | LOS A | 15.5 | 120.1 | 0.34 | 0.40 | 54.5 |
| North: Site Access |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 72 | 27.9 | 0.283 | 13.8 | LOS A | 2.0 | 17.4 | 0.98 | 0.99 | 38.7 |
| 12 R2 | 17 | 31.3 | 0.283 | 18.5 | LOS B | 2.0 | 17.4 | 0.98 | 0.99 | 48.5 |
| Approach | 88 | 28.6 | 0.283 | 14.7 | LOS B | 2.0 | 17.4 | 0.98 | 0.99 | 41.3 |
| West: Ferrers Road (1000m) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 68 | 27.7 | 1.017 | 50.7 | LOS D | 53.2 | 402.1 | 1.00 | 1.96 | 38.2 |
| 2 T1 | 1008 | 8.0 | 1.017 | 49.7 | LOS D | 53.2 | 402.1 | 1.00 | 1.96 | 36.1 |
| Approach | 1077 | 9.3 | 1.017 | 49.8 | LOS D | 53.2 | 402.1 | 1.00 | 1.96 | 36.3 |
| All Vehicles | 2363 | 11.8 | 1.017 | 25.9 | LOS B | 53.2 | 402.1 | 0.67 | 1.13 | 43.5 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Development.sip7

## MOVEMENT SUMMARY

Gite: 6 [Site x Ferrers_ Future + Dev_PM]

Site Access x Ferrers Road Intersection, Eastern Creek
Road Condition: Existing 2018 (plus Proposed Site access to/from Ferrers Road only)
Traffic: 2036 PM Background with Development
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov OD  <br> ID Mov | Deman Total veh/h | $\begin{gathered} =\text { lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | f Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| East: Ferrers Road (820m) mer min |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 1231 | 6.1 | 0.884 | 5.4 | LOS A | 23.9 | 177.4 | 0.88 | 0.45 | 53.9 |
| 9 R2 | 58 | 27.3 | 0.884 | 10.6 | LOS A | 23.9 | 177.4 | 0.88 | 0.45 | 46.4 |
| Approach | 1288 | 7.0 | 0.884 | 5.7 | LOS A | 23.9 | 177.4 | 0.88 | 0.45 | 53.6 |
| North: Site Access |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 232 | 27.7 | 0.674 | 25.6 | LOS B | 7.0 | 60.5 | 1.00 | 1.27 | 33.2 |
| 12 R 2 | 56 | 28.3 | 0.674 | 30.1 | LOS C | 7.0 | 60.5 | 1.00 | 1.27 | 44.0 |
| Approach | 287 | 27.8 | 0.674 | 26.5 | LOS B | 7.0 | 60.5 | 1.00 | 1.27 | 36.1 |
| West: Ferrers Road (1000m) |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 14 | 30.8 | 0.692 | 5.0 | LOS A | 9.5 | 70.3 | 0.50 | 0.43 | 52.3 |
| 2 T1 | 983 | 6.2 | 0.692 | 4.8 | LOS A | 9.5 | 70.3 | 0.50 | 0.43 | 54.9 |
| Approach | 997 | 6.5 | 0.692 | 4.8 | LOS A | 9.5 | 70.3 | 0.50 | 0.43 | 54.9 |
| All Vehicles | 2573 | 9.2 | 0.884 | 7.7 | LOS A | 23.9 | 177.4 | 0.74 | 0.54 | 52.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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