

Report on Detailed Geotechnical Investigation

Proposed New Hospital Metford Road, Metford

Prepared for Multiplex Constructions Pty Ltd

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Integrated Practical Solutions



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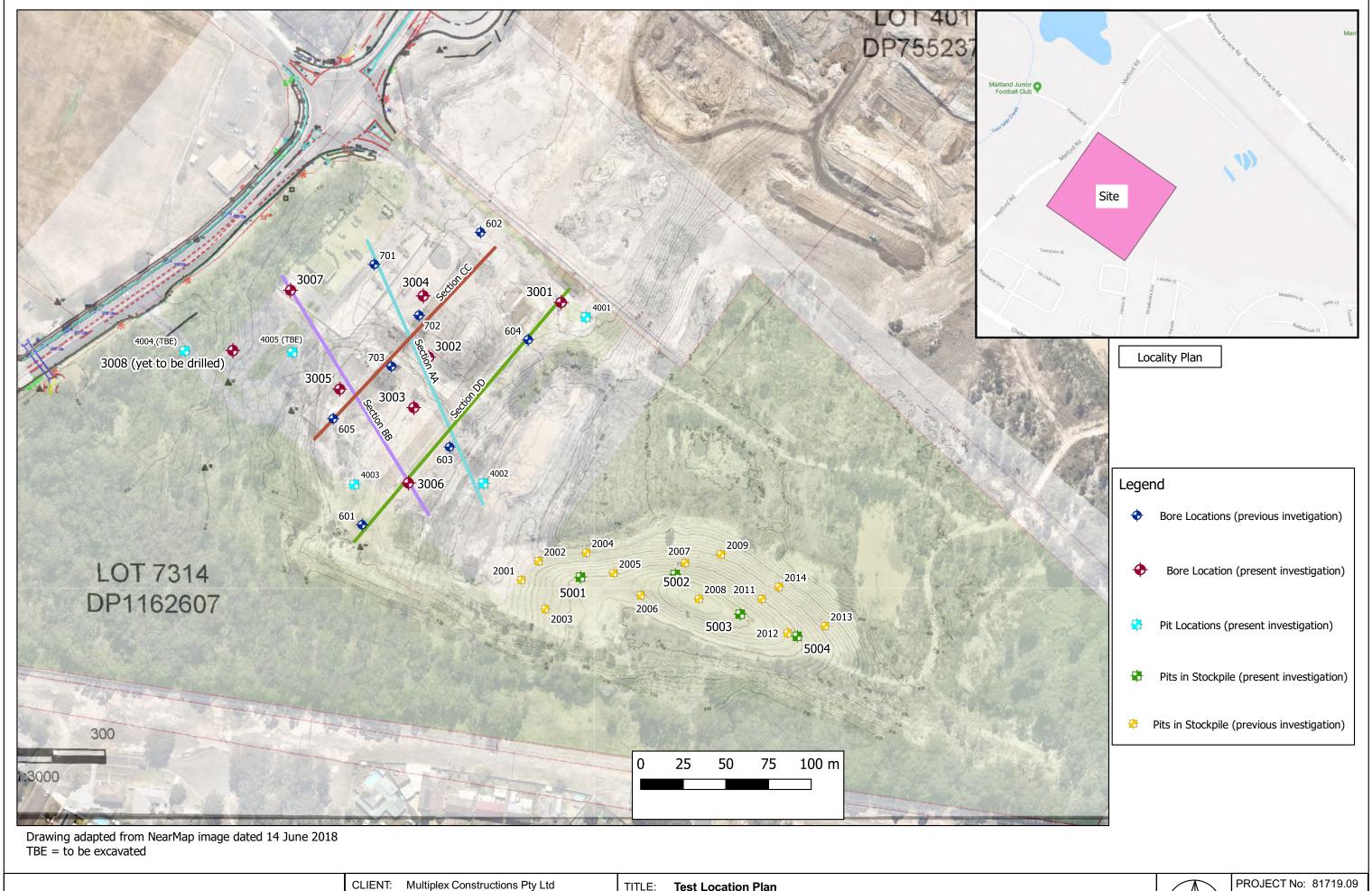
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The undersigned, on behalf of Douglas Partners Pty Ltd, confirm that this document and all attached drawings, logs and test results have been checked and reviewed for errors, omissions and inaccuracies.

Signature		Date
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# Report on Detailed Geotechnical Investigation Proposed New Hospital Metford Road, Metford

#### 1. Introduction

This report presents the results of a detailed geotechnical investigation undertaken for a proposed new hospital at Metford Road, Metford. The investigation was undertaken with reference to Douglas Partners' proposal NCL180660 dated 13 November 2018. The work was commissioned by Multiplex Australasia in a consultancy agreement between Multiplex Constructions Pty Ltd and Douglas Partners Pty Ltd (DP).

The key features of the development include the following:

- A building envelope within the north-western part of Lot 7314 mostly on previously disturbed areas:
- Building mass of up to seven storeys (including lower ground but excluding plant level);
- Approximate gross floor area of 48,000 m<sup>2</sup>;
- Primary access from Metford Road at a new roundabout junction opposite Fieldsend Street;
- Secondary access for ambulances from Metford Road, south of the Primary access. This allows for accessing the hospital from both points;
- An on-grade helipad located to the northeast of the hospital;
- Two car parking facilities;
- Stormwater drainage to the east of the hospital, to manage stormwater flows through the site from
  offsite lands as well as from the hospital precinct; and
- Partial retention of vegetation at the southern, western and eastern end of the site, with some clearing and understorey removal to meet bushfire mitigation requirements (APZ).

The aim of the investigation was to provide supplementary information on subsurface conditions as well as the following geotechnical items:

- Excavation conditions;
- Identification of areas of filling;
- Estimates of settlements in areas of deep filling subject to proposed building loads;
- Geotechnical parameters for high level and piled footings;
- Subgrade conditions for proposed pavement areas;
- Indicative pavement thickness designs;
- Risk of instability in the existing quarry excavation faces;
- Appropriate stabilisation/mitigation measures against quarry face instability;



- Construction methodology for filling of existing pond, if required;
- Material quality and compaction requirements for engineered filling; and
- Subgrade preparation measures.

This investigation comprised the drilling of seven bores, excavation of seven test pits, laboratory testing of selected samples, engineering analysis and reporting to supplement geotechnical investigations already undertaken.

## 2. Background Data

Douglas Partners Pty Ltd (DP) has undertaken a number of previous investigations at the site. The most relevant to the present investigation is the "Report on Geotechnical Assessment, New Maitland Hospital, Metford", Report 81719.00.R.001.Rev2, dated 9 May 2018 (Ref 16).

The previous geotechnical assessment carried out in July 2015 by DP (Ref 14) provided information on geotechnical conditions based on previous investigations within and near the site together with preliminary design parameters (end bearing, shaft adhesion parameters) for various foundation types as well as comments on a range of other geotechnical items. The 2018 report (Ref 16) included supplementary investigation comprising boreholes drilled during July 2017.

This present report should be read in conjunction with the previous report (Ref 16).

## 3. Site Description

The site is located within the former PGH Bricks site at Metford and is identified as Lot 7314 DP 1162607. The site is irregular in shape with an approximate area of 16.4ha. Figure 1 shows the PGH Bricks site (outlined black) and the site subject of this investigation extent (red).



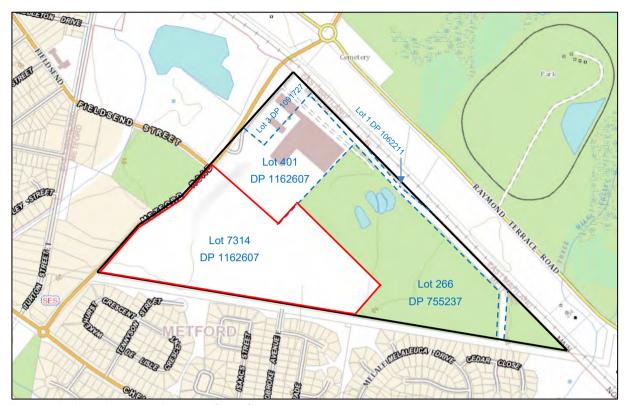


Figure 1: Location and Extent of the Site

The hospital is to be situated within the western half of Lot 7314, which is located within the south-western area of the former PGH Bricks site. The proposed hospital layout is shown on the attached test location plan in Appendix D. The site is bounded to the north and east by the former PGH Bricks site and the Northern Railway beyond. The site is bounded to the south by existing residential developments and Metford Road to the west.

The site ranges in surface level from 8 m AHD to 26 m AHD, generally comprised areas of fill above ground level (stockpiles), rock outcrops, water bodies, unsealed access roads, areas of dense vegetation (south-western area) as well as stripped / bare areas.

A full description of the site is provided in Ref 16 and is not repeated herein. Since the preparation of the previous report some civil works have been undertaken on the site and include the following:

- Bulk earthworks in the proposed hospital footprint and beyond, which has re-graded areas of the site;
- The prominent change in grade is still present between the higher western area and the lower area dominated by the existing pond (refer Figure 2);
- A construction compound which includes several temporary buildings has been created along the western boundary of the site; and
- The carbonaceous material stockpile located to the east-south-east of the proposed hospital footprint has been covered with a capping layer.





Figure 2: View of the site taken in September 2018 (sourced from Nearmap images)

Since the preparation of the report the site has been further altered. It should be noted however, that the geotechnical comments contained herein relate to the site condition at the time of investigation September to December 2018 – i.e. Figure 2).

General site features which are pertinent to the present investigation are discussed below.

- Based on survey information provided by the client, the surface levels within the proposed building footprint and immediate surrounds range from about RL 28 m AHD (within some stockpiles) but is generally around RL 20 m AHD in the higher western area, to about RL 8 AHD near the existing pond;
- The footprint of the hospital has been cleared of existing vegetation with the exception of the southern extent of the development (proposed car park and access pavement) where dense vegetation remains. DP was not able to complete the test locations in this area prior to preparation of this report. Further testing to be undertaken if requested by the structural or civil engineer.
- The majority of the proposed building footprint has been highly disturbed as is characterised by bare soil and rock surfaces with numerous stockpiles (Refer Figure 3 and 4);



- The stockpiles are typically about 5 m to 10 m in height above the surrounding ground level. The stockpiled material is variable but predominantly comprised either cohesive soils and ripped bedrock (clay, sandy clay, silty clay and weathered rock); or gravel, chitter (coarse coal reject) and coal:
- The lower area of the site, which includes the existing pond and surrounding area is characterised by weak sandy sediments and surface water, with carbonaceous material, including coal exposed in the area to the east (refer Figure 5);
- The depth of the water and weak sediments within the existing pond is not known but based on probing around the edges it was anticipated to be greater than 1 m to 2 m;
- The remainder of this lower area (beyond the pond) is covered by accumulated sediments and low vegetation; and
- A large capped stockpile of carbonaceous material is present to the east and south-east of the hospital footprint. A proposed car parking area is to be constructed over the existing pond and may encroach on the north-western edge of the stockpile (refer Drawing 1 and Figure 6).



Figure 3: Looking south from near Bore 3004 towards large stockpile in the central area of the site.



Figure 4: Looking north east from near pit 4003 towards construction compound (distant left and large stockpile in the central area of the site (distant right)





Figure 5: View of the site near Pit 4002, looking east.



Figure 6: Looking south-east towards low lying area from large stockpile in central area of the site.

Sandstone bedrock was observed outcropping in the northern area of the site near Pit 4001 and Bore 3001 as well as the rock cutting at in southern area of the site (refer Figure 7). The sandstone was generally very low strength or stronger.





Figure 7: Looking south-east towards sandstone cutting in southern area of the site

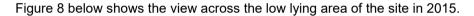




Figure 8: Looking south from top of a stockpile, carbonaceous stockpiles (left), water body (left), existing quarry cutting (back), stockpile (right) (2015)

Coal was observed to be outcropping in excavations around the existing stockpile.





Figure 9: In-situ coal exposed beneath edge of carbonaceous material stockpile in eastern area of the site (2015)

Surface water was present in various water bodies / ponds across this area of the site and was most likely perched. There may be some connection between the ponds and groundwater however the rock permeability would be relatively low and flow rates would also be low. Preferential flow potentially occurs along strata interfaces within the rock, particularly coal and shale layers which tend to have higher permeability than neighbouring sandstone, siltstone and claystone layers.

## 4. Regional Geology

The Newcastle Coalfields 1:100,000 Geology map indicates that the site is underlain by the Tomago Coal Measures of Permian age (geology code Pt). This formation is described as comprising laminated sandstone, claystone, siltstone, coal and tuff. Figure 10 below shows the site overlain with the geological map and site topography (contours at 2 m intervals). Based on information provided by the project surveyor, these 2 m contours are not considered accurate for this site and should be treated as indicative only.





Figure 10: Geological Setting of the Site

The site topography also indicates where the natural drainage path exits the site along the western boundary, along Metford Road.

The Newcastle 1:100,000 Soil Landscapes Sheet indicated that the site includes two soil landscape types, as shown blow in Figure 11.



Figure 11: Soil Landscape Setting of the Site

The features of these soil landscapes are summarised in Table 1.



**Table 1: Soil Landscape Features** 

Feature		Description	
Colour (in Figure 11)	Dark green	Light green	Grey
Soil Landscape Code	Ве	СС	xx
Soil Process Group	RESIDUAL	ALLUVIAL	DISTURBED TERRAIN
Soil Landscape Name	Beresfield	Cockle Creek	Disturbed Terrain
Landscape Description	Undulating low hills and rises on Permian sediments in the East Maitland Hills region. Slope gradients 3-15%, local relief to 50m, elevation is 20-50m. Partially cleared tall open-forest.	Narrow floodplains, alluvial fan deposits and broad delta deposits. Slope gradients are 0-2%, elevation is <1-50m, local relief is <1m; Cleared open forest.	Level plain to hummocky terrain, extensively disturbed by human activity, including complete disturbance, removal or burial of soil. Local relief variable. Land fill includes soil, rock, building and waste materials. Original vegetation completely cleared.
Soils Description (summary only)	Crests: moderately deep (<120cm), Yellow Podzolic Soils, Brown Podzolic Soils and brown Soloths.  Upper Slopes: moderately deep (<120cm) Red Podzolic Soils and red Soloths.  Sideslopes: brown Soloths and yellow Soloths.  Lower Slopes: deep (>200cm), imperfectly to poorly drained Yellow Podzolic Soils, yellow Soloths and Gleyed Podzolic Soils.	Floodplains: deep (>200cm), imperfectly to poorly drained yellow Soloths (Dy3.41) and Yellow Podzolic soils.  Delta / Fan Deposits: deep (>200cm), moderately well to poorly drained Yellow Earths and Grey Earths; with deep (>200cm) imperfectly drained, to well-drained Yellow Podzolic Soils.	Highly variable.
Limitations	High foundation hazard, water erosion hazard, seasonal waterlogging and high run-on localised lower slopes, highly acid soils of low fertility.	Flood hazard, water erosion hazard, permanently high watertables (localised), periodic to permanent waterlogging (localised), high run-on, acid, and infertile sodic / dispersible soils of low wet strength.	Dependent on nature of site.  Limitations may include mass movement hazard, steep slopes, foundation hazard, unconsolidated low wet bearing strength materials, potential acid sulfate soils, impermeable soils, poor drainage or erosion hazard.

The NSW Acid Sulfate Soils Risk map indicates no risk of actual or potential acid sulfate soils.



#### 5. Field Work Methods

## 5.1 Investigation Episodes

The initial field work was carried out in the period of 12 October 2015 to 5 November 2015. A supplementary investigation was then carried out from 11 August 2017 to 12 August 2017.

The present investigation was undertaken over the period extending from 29 November 2018 to 13 December 2018.

The initial investigation comprised the following:

- Drilling of six boreholes (Boreholes 601 to 606) to depths of between 8.0 m and 21.9 m;
- Excavation of 20 test pits (Pits 301 to 318 and 320 to 321) to depths of between 0.6 m and 2.8 m;
- Drilling of one borehole (Borehole 319) to 0.65 m using hand tools;
- Installation of groundwater wells in Bores 605 and 606; and
- Walk-over inspection by a Principal Geotechnical engineer to assess site conditions and possible instability in the existing quarry cutting.

A supplementary investigation comprised the following:

- Drilling of three boreholes (Boreholes 701 to 703) to depths of ranging from 8.55 m to 12.0 m;
- Installation of a groundwater well in Bore 703.

The present investigation comprised the following:

- Drilling of seven boreholes (Boreholes 3001 to 3007) to depths of between 18.65 m and 23.3 m;
- Excavation of three test pits (Pits 4001 to 4003) to depths of between 1.6 m to 2.0 m. These pits were excavated at client nominated locations and were generally within proposed pavement areas (Pits 4001 and 4003), and on the edge of the existing pond (Pit 4002); and
- Excavation of four additional pits (Pits 5001 to 5004) in the carbonaceous stockpile to depths of between 1.6 m to 2.0 m. The purpose of the pits was to collect samples of the carbonaceous material for laboratory testing purposes.

It is noted that for the initial investigation, limited access was available to the majority of the site owing to the presence of trees, overly wet ground and stockpiled materials, subsurface investigation was limited to accessible locations.

The supplementary investigation (August 2017) and present investigation (Nov-Dec 2018) bores were drilled at client nominated locations.

A summary of the field investigation is presented in Table 2 below.



Table 2: Summary of Field Investigations - Bores

Bore	Surface Level (m AHD) <sup>(1)</sup>	Approximate Finished Floor Level of Development (m AHD)	Drilled Depth of Bore (m)	Elevation of Bore Termination (m AHD)				
		Present Investigation (Nov	/ - Dec 2018)					
3001	21.4	15.3 (lower ground floor)	18.65	2.75				
3002	18.6	15.3 (lower ground floor)	19.80	-1.2				
3003	16.8	15.3 (lower ground floor)	20.15	-3.35				
3004	21.5	20.3 (ground floor) 15.3 (lower ground floor)	23.30	-1.8				
3005	16.8	20.3 (ground floor) 15.3 (lower ground floor)	20.21	-3.41				
3006	16.1	15.3 (lower ground floor)	20.18	-4.08				
3007	19.2	15.3 (lower ground floor)	20.35	-1.15				
		2015 Investigati	on					
601	17.0	15.3 (lower ground floor)	8.17	8.83				
602	21 <sup>(2)</sup>	20.3 (ground floor) 15.3 (lower ground floor)	21.85	-0.85				
603	18.4	15.3 (lower ground floor)	8.2	10.2				
604	19.3	15.3 (lower ground floor)	8.6	10.7				
605	24.3		7.98	16.32				
	2017 Investigation							
701	20.5 <sup>(3)</sup>	20.3 (ground floor)	8.55	11.95 <sup>(3)</sup>				
702	21 <sup>(3)</sup>	20.3 (ground floor)	11.55	9.44 <sup>(3)</sup>				
703	17 <sup>(3)</sup>	20.3 (ground floor)	12.00	5 <sup>(3)</sup>				

Notes to Table 2:

Point load index testing was undertaken on the recovered core samples prior to it being photographed by the geotechnical engineer. Photos of the recovered core are provided in the photo plates in Appendix B.

## 5.2 Investigation Methods

The test pits were excavated with a either a 4.5 tonne or 6.5 tonne excavator fitted with a 450 mm or 600 mm wide bucket with teeth.

The bores (except Bores 604 and 606) were drilled with a using a truck-mounted rotary drilling rig equipped with solid flight augers and wash boring equipment for drilling in soil and weathered rock, as well as NMLC diamond coring equipment for coring bedrock (refer Figure 12). Standard penetration tests (SPTs) were performed at selected bore locations and depths. A bobcat-mounted drilling rig was used for Boreholes 604 to 606.

<sup>(1)</sup> See Section 5.3 for comment in relation to surface levels

<sup>(2)</sup> Surface level interpolated from survey plan provided by client and should be considered approximately only

<sup>&</sup>lt;sup>(3)</sup> Surface level inferred from approximate coal level and should be considered very approximate only NA = Not applicable





Figure 12: Drilling Rig set up at Borehole 601 (looking west)

Groundwater monitoring wells constructed of 50 mm PVC casing and machine slotted 50 mm PVC screen were installed in Boreholes 605, 606 and 703 to depths of 8 m to 12.0 m. The wells were completed with a gravel pack extending several metres above the well screen and a bentonite plug of at least 0.5 m thickness in each well. Details of the monitoring well construction are provided on the detailed borehole logs in Appendix B.

The test locations were set out by a geotechnical engineer from DP. The engineer also logged the subsurface conditions encountered at each test location and collected samples for subsequent laboratory testing and identification purposes. The engineer boxed and photographed the rock core and carried out point load strength index tests on the core. Pocket penetrometer tests and dynamic penetrometer tests were performed at selected depths and locations.

## 5.3 Borehole Survey

The surface levels of the bores have been estimated and determined as follows:

## Bores 601 to 606 – 2015 Investigation

The surface level of the bores was provided by the project surveyor. The surface level for Bores 602 and 606 were not provided and were interpolated from survey drawings and should therefore be considered as approximate.

#### Bores 701 to 703 - 2017 Investigation

Determination of the surface level of the bores was not possible at the time of the investigation. Reduction of surface levels from the 2 m digital contour mapping was not possible as the limited survey provided by the project surveyor reveals that the 2 m digital mapping is not accurate for this site. The MGA coordinates at each pit location were recorded using a hand held GPS unit which is normally accurate to within about ±5 to 10 m depending on satellite coverage.



DP has estimated a surface level for these bores based on interpolation of the level of the coal seam within all of the bores. The estimated surface level should be taken as indicative only and care should be undertaken attributing levels to the subsurface conditions encountered in these bores.

#### Bores 3001 to 3007 - Present Investigation

The surface level of the present investigation bores was recorded using a differential GPS unit, which is typically accurate to about 0.1 m in elevation. It should be noted, however, that DP is not a registered surveyor and hence it is recommended that all test locations are accurately surveyed prior to further design.

The approximate locations of the boreholes and test pits are indicated on the Test Location Plan, Drawing 1, in Appendix D.

#### 6. Field Work Results

The previous geotechnical assessment (Ref 14) indicated the principal geotechnical conditions at the site would comprise sequences of four main elements: fill above general ground level (stockpiles), filled depressions / voids, residual clays and bedrock.

The subsurface conditions encountered in the bores and test pits undertaken for the present investigation are presented in detail in the borehole logs and test pit logs in Appendix B. These should be read in conjunction with the accompanying general notes in Appendix A which explain the descriptive terms and classification methods used in the logs. The results of the dynamic penetrometer tests are also included in Appendix B. The subsurface conditions encountered in the bores and pits are summarised in Tables 2 to 4 below. For the descriptions of the bedrock, the following general classifications were utilised:

- Class V Extremely low strength sandstone or siltstone and coal;
- Class IV Very low to low strength sandstone or siltstone; and
- Class III Medium strength or stronger sandstone or siltstone.

A summary of the field investigations, along with the approximate finished floor level of the development in the area of the bores is shown in Table 3.



Table 3: Summary of Subsurface Conditions – Depth Range of Each Unit

Bore		I	Depth range of Strat	tum (m)	
Unit	Filling	Residual Clay	Bedrock Class V	Bedrock Class IV	Bedrock Class III
3001	NE	NE	0.0 – 1.15 8.21 – 13.77	1.15 – 8.21 13.77–18.65	NE
3002	0.0 – 2.0	NE	2.0 – 2.5 11.8 – 16.78	2.5 – 11.8 16.78 – 19.8	NE
3003	0.0 - 0.3	0.3 – 1.1	1.1 – 2.61 9.0 – 20.15	2.61 – 9.0	NE
3004	0.0 – 4.2	4.2 – 4.65	4.65 – 8.6 17.18 – 23.3	8.6 – 17.18	NE
3005	0.0 – 0.3	0.3 – 0.9	14.42 – 19.05	0.9 – 14.401 9.05 – 20.21	NE
3006	0.0 - 0.5	0.5 – 1.2	7.98 – 20.18	1.2 – 7.98	NE
3007	0.0 – 2.1	NE	2.1 – 2.5 5.57 – 8.83	2.5 – 5.57 8.83 – 10.81 12.46 – 20.35	10.81 – 12.46
601	0.0 – 0.1	0.1 – 1.1	5.05 – 6.0	1.1 – 5.05 6.0 – 8.17	NE
602	0.0 – 0.8	NE	0.8 – 7.64 15.54 – 20.28	7.64 –15.54 20.28 – 21.85	NE
603	0.0 – 2.2	NE	NE	2.2 – 3.8 8.07 – 8.2	3.8 – 8.07
604	0.0 - 0.2	NE	0.2 – 2.08	2.08 – 8.6	NE
605	0.0 - 0.4	NE	0.4 – 4.47	4.47 – 7.98	NE
606	0.0 - 2.2	NE	NE	2.2 – 8.2	NE
701	0.0 - 0.15	0.15 – 0.6	0.6 – 4.1	4.1 – 8.55	NE
702	0.0 – 3.8	NE	3.8 – 4.4 6.75 – 7.08	4.4 - 6.75 7.08 - 8.68 10.73 - 11.55	8.68 – 10.73
703	0.0 – 0.3	0.3 – 0.7	0.7 – 1.35 11.71 – 12.00	2.0 – 5.08 10.78 – 11.71	1.35 – 2.0 5.08 – 10.78



No free groundwater was observed in the bores during auger drilling, however the introduction of drilling fluids during core drilling precluded further groundwater observations. Groundwater standpipes were installed in Boreholes 605, 606 and 703. Monitoring of standpipes 605 and 606 was undertaken on 5 November 2015, at which time Bore 606 was dry and Bore 605 had a groundwater at a depth of 7.2 m (RL 17.1 m AHD). Based on information received from GHD, groundwater was recorded in the installed wells at levels ranging from about 6.5 m AHD to 8 m AHD (wells located within the northwestern and eastern areas of the site) and RL 16 to 17 m AHD in a well installed in the western corner of the site. No information on Well 703 groundwater level has been provided.

It should be noted that groundwater levels are affected by factors such as climatic conditions and soil permeability and will therefore vary with time.

Mapping of the rock batter located to the south-east of the proposed hospital footprint was undertaken by a Principal Geotechnical Engineer on 5 November 2015 as part of the previous investigation. The inspection revealed the following:

- The batter was generally formed at a slope ranging from about 20° to 25°;
- Interbedded siltstone and sandstone was exposed within the batter;
- Within the upper portion of the batter, bedding was observed with a dip of 5° to 15° and a dip direction of about 310° to 340° M;
- The dominant jointing in this lower portion of the batter was sub-vertical to 80° with a dip direction of 080° to 090° M and a spacing ranging from about 0.05 m to 0.2 m;
- Within the lower half of the batter, bedding was observed with a dip of 0 to 5° and a dip direction ranging from about 000° to 050° M;
- The dominant joints were dipping at about 65° with a dip direction of around 060° M and a spacing ranging from 200 mm to 1000 mm; and
- Coal was exposed within the lower approximately 1 m towards the eastern visible extent of the batter (refer Figure 13 and Figure 14).





Figure 13: Coal exposed in lower area of batter



Figure 14: Coal in exposed batter



# 7. Laboratory Testing

Laboratory testing was undertaken on samples of soil and rock retrieved during the investigation, and included the following:

- Unconfined compressive strength (UCS) testing on samples of the recovered core; and
- Standard compaction testing on samples of the carbonaceous material blended with excess materials from the test pits (4000 series).

California Bearing Ratio (CBR) laboratory testing on three samples was in the process of being undertaken at the time of this draft report and the results were not available.

Detailed results are provided in Appendix C and are summarised in **Table 4** and Table 5.

Table 4: Results of CBR and Standard Compaction Testing

Pit	Depth (m)	Description	FMC (%)	SOMC (%)	SMDD (t/m3)	CBR (%)	Swell During Soaking Phase (%)
4001	0.6 – 0.8	Extremely weathered SANDSTONE	8.3	14.0	1.79	25	0
4002	0.3 – 0.45	Clayey SAND	27.8	16.0	1.75	16	0
4003	0.4 – 0.6	Extremely weathered SILTSTONE	12.3	16.5	1.73	4.5	7.5
	SPM / 1 (0.6 – 0.8)	40% carbonaceous material and 60% Non- Carbonaceous Sandstone	-	14.5	1.63	ı	-
SPM / Pit 4003 (0.4 – 0.6)		40% carbonaceous material and 60% Non- Carbonaceous Siltstone	-	18.0	1.58	-	-
SPM / Pit 4001 (0.6 – 0.8)		50% carbonaceous material and 50% Non- Carbonaceous Sandstone	-	16.0	1.56	-	-
SPM / Pit 4003 (0.4 – 0.6)		50% carbonaceous material and 50% Non- Carbonaceous Siltstone	-	19.0	1.53	-	-
	SPM / 1 (0.6 – 0.8)	60% carbonaceous material and 40% Non- Carbonaceous Sandstone	-	16.5	1.55	-	-

Notes to Table 4:

FMC – Field Moisture content

SOMC - Optimum Moisture Content (Standard)

SPM - Stockpile Material

SMDD – Maximum Dry Density (Standard)

CBR - Californian Bearing Ratio



**Table 5: Results of Unconfined Compressive Testing** 

Bore	Depth (m)	Description	UCS (Mpa)
3001	7.69 – 8.0	Sandstone	7.7
3001	14.79 – 15.0	Sandstone / Siltstone	5.5
3002	4.72 – 5.0	Sandstone	3.8
3003	2.0 – 2.25	Laminite	0.8
3004	7.53 – 7.8	Sandstone	1.6
3005	5.72 – 6.0	Laminite	1.1
3006	2.1 – 2.4	Sandstone	7.3
3007	11.45 – 11.71	Sandstone	75.5

## 8. Proposed Development

Health Infrastructure has committed to undertaking a Stage Infrastructure Application in accordance with Section 115ZD (1) of the Environmental Planning and Assessment Act 1979 (EP&A Act) for the following works:

- Stage 1: Site clearance and preparatory works (approved under SSI9022); and
- Stage 2: Design and construction of the hospital main works (this application SSI9775).

Stage 2 works include the design and construction work generally comprising:

- A new seven storey Acute Services Building, including:
  - o Emergency services;
  - o Medical, surgical, paediatric and maternity services;
  - Critical care services for adults and babies, including a special care nursery;
  - o Operating theatres, delivery suites and assessment rooms;
  - o Palliative care and rehabilitation services;
  - o Mental health services;
  - Satellite renal dialysis;
  - o New chemotherapy services;
  - o Oral health service;
  - o A range of ambulatory care and outpatient clinics;
  - o Internal road network and car parking for staff, patients and visitors;
  - o Signage;
  - o Site landscaping and open space improvements;
  - o Tree removal;
  - o Utility and services connection and amplifications works.



• The development is within the north-western part of Lot 7314 mostly on previously disturbed areas (refer Figure 15);

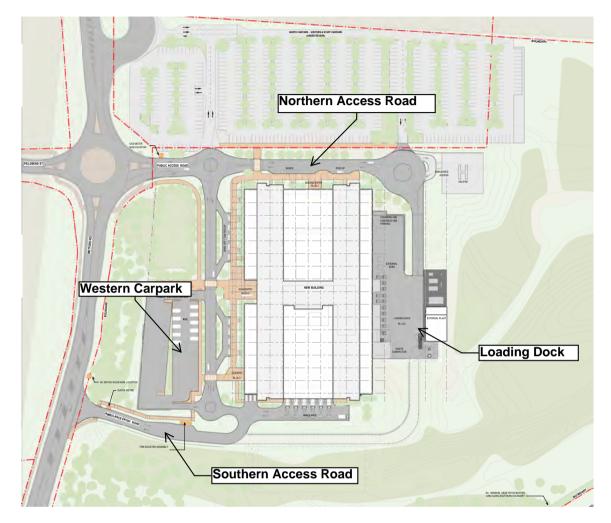


Figure 15: Extract from Master Plan showing layout of proposed hospital development



Based on the plans provided by the client, the bulk earthworks level for the development will be as follows:

- Raising of the site in the western area of the hospital building to raise site levels to about RL 20 m AHD. This will require placement of up to about 2 m to 3 m in some areas of the car parks and roadways, and also under the western tower of the proposed structure;
- Excavation to accommodate a finished floor level of 14.8 m AHD within the lower ground floor, which covers the area under approximately half of the western tower and the remaining building footprint to the east. This will require excavation ranging from less than 1 m to greater than 8 m;
- Filling of the existing pond to the east of the proposed building to create a new loading dock. The
  ground surface will be raised to approximately RL 14.8 m AHD, which will require up to 3 m of
  filling; and
- Figure 16, below, shows a typical elevation of the proposed hospital building.



Figure 16: Elevation of the proposed development

Limited information in relation to the proposed foundation loads and proposed foundation system have been provided to DP for preparation of this report, as follows:

- Working loads are anticipated to be in the order of 4000 kN;
- The western, higher section of the building will be supported on piled footings, drilled through the existing filling to derive support from within the underlying bedrock;
- Bored piles are proposed at this stage, and are anticipated to be approximately 1.2 m in diameter;
   and
- The lower, eastern section of the building is to be supported on pad footings.



#### 9. Comments

## 9.1 Conceptual Geotechnical Model

Based on the conditions encountered in the bores, the conceptual geotechnical model for the site has been developed and is described in Section 6, Table 3.

A review of the bores drilled during the present investigation using the three key classification parameters (UCS, defect spacing and allowable seams) is provided below in Table 6 for the proposed elevation range of the proposed pad footings.

**Table 6: Interpreted Rock Classifications at Foundation Level** 

Bore	Approximate Foundation Level	UCS (Mpa) (based on multiplier of 17)	Defect Spacing(mm)	Seam(%)	Assessed Class of Rock
	20 (ground floor)	0.6 to 1	50 to 500	0	Class IV
3001	13.5 (lower ground floor)	2 to 10	500 to 1000	0	Class V (owing to presence of coal at RL 12.8)
3002	13.5 (lower ground floor)	0.8 to 6	500 to 1000	0	Class IV
3003	13.5 (lower ground floor)	3 to 6	30 to 1000	0	Class IV
3004	13.5 (lower ground floor)	1.2 to 3.5	500 to >1000	0	Class V/IV
3005	13.5 (lower ground floor)	3 to 6	100 to >1000	0	Class IV
3006	13.5 (lower ground floor)	2.2 to 3.4	100 to >1000	0	Class IV
3007	20 (ground floor)	Filling			
601	13.5 (lower ground floor)	7 to 12	500 to >1000	0	Class IV
602	13.5 (lower ground floor)	0.6 to 1.5	200 to 1000	0	Class IV
603	13.5 (lower ground floor)	4 to 6	300 to 500	0	Class III
604	13.5 (lower ground floor)	3 to 7	200 to 500	0	Class IV
605	20 (ground floor)	2 to 5	700 to >1000	0	Class V/IV
701 <sup>(1)</sup>	20 (ground floor)		Filling		
702 <sup>(1)</sup>	13.5 (lower ground floor)	3 to 7	600 to >1000	0	Class IV
703 <sup>(1)</sup>	13.5 (lower ground floor)	2 to 5	>1000	0	Class IV

Notes to Table 6:

Table 7 below shows the anticipated conditions at proposed bulk excavation level based on the conditions encountered in the bores.

<sup>1.</sup> The surface level of these bores is very approximate only and hence the conditions at anticipated foundation level are also approximate

<sup>2.</sup> Piles founded within the coal or within 2 m above the coal should be designed for Class V parameters for the affected section of pile, as discussed below.



Table 7: Summary of Conditions Anticipated at Bulk Excavation Level

Bore	Approximate Surface Level (m AHD) <sup>(2)</sup>	Approximate Bulk Excavation Level (m AHD) <sup>(1)</sup>	Anticipated Conditions at Bulk Excavation Level				
3001	21.4	14.8 (lower ground floor)	Low strength SANDSTONE				
3002	18.6	14.8 (lower ground floor)	Very low strength LAMINITE				
3003	16.8	14.8 (lower ground floor)	Low strength LAMINITE				
3004	21.53	20 (ground floor)	Existing sandy clay FILLING				
3004	21.53	14.8 (lower ground floor)	Very low to low strength SANDSTONE				
3005	16.8	20 (ground floor)	Filling (above existing surface level)				
3005	16.8	14.8 (lower ground floor) Low strength SANDSTON					
3006	16.1	14.8 (lower ground floor)	Very low strength SILTSTONE				
3007	19.2	20 (ground floor) Filling (above existing surface lev					
3008	Yet to be drilled						
		2015 Investigation					
601	17	17 14.8 (lower ground floor)(outside of footprint) Low to medium strength SANDSTONE					
602	21	14.8 (lower ground floor)(outside of footprint)	Low strength SILTSTONE				
603	18.4	14.8 (lower ground floor) Low strength SANDSTONE					
604	19.3	14.8 (lower ground floor) Low to medium strength SANDSTO					
605	24.3	14.8 (lower ground floor)	Below drilled depth				
	2017 Investigation						
701	20.5	20 (ground floor)	Very stiff SANDY CLAY				
702	21	14.8 (lower ground floor)	FILLING				
703	17	14.8 (lower ground floor)	Low strength SANDSTONE				

Notes to Table 7:

<sup>(1)</sup> Bulk excavation level has been based on finished floor level minus about 0.3 m and 0.5 m for the ground floor and lower ground floor levels respectively.

<sup>(2)</sup> See section 5.3 for comments in relation to surface levels of bores.



A graphical representation of the inferred UCS based on a correlation of 17 times the  $I_{50}$  point load index values for the sandstone and siltstone units of the test bedrock is presented in Figure 17 and Figure 18. The UCS ranges for the various classifications of the bedrock are based on the strength parameter alone and assessment of other factors such as discussed in Table 6 above should be considered in designation of rock classification.

For the model above and the graphical representation below, it can be seen that the assessed rock ranges from Class V to lower end Class II. Reference to the Pells et all paper indicates that appropriate ultimate end bearing pressures for these rock classes are as follows:

		Sandstone	Siltstone
•	Class V	3 MPa	3 MPa
•	Class IV	4 to 15 MPa	3 MPa
•	Class III	20 to 40 MPa	6 to 30 MPa

As can be seen in Figure 17 and Figure 18, at the anticipated lower ground floor foundation level (about RL 13.5 m AHD) the anticipated bedrock is either predominantly Class IV sandstone or Class IV/III siltstone. Some areas of the site, however, are likely to expose weaker (Class V) bedrock.

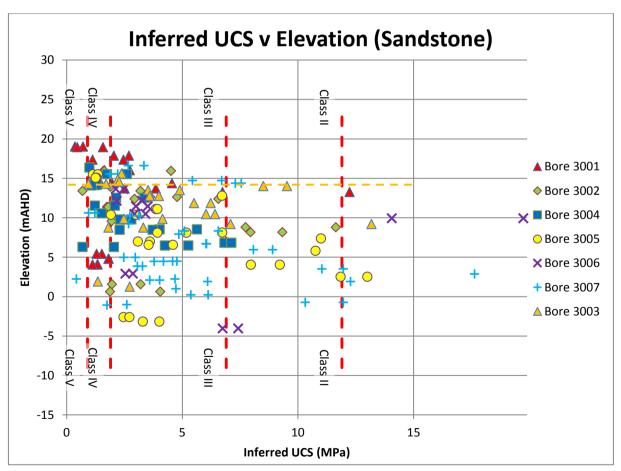


Figure 17: Inferred UCS against elevation for sandstone units



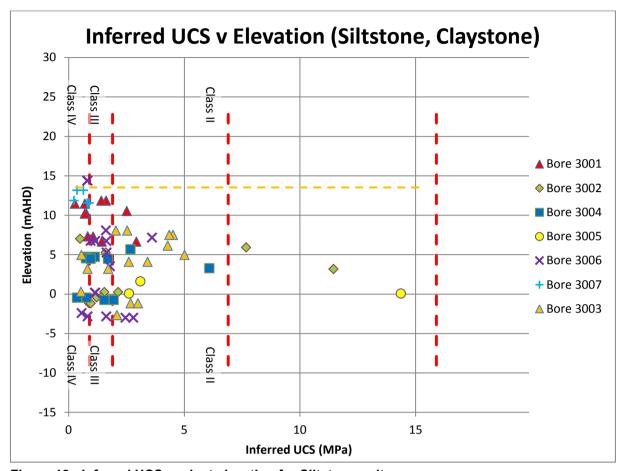


Figure 18: Inferred UCS against elevation for Siltstone units

## 9.2 Earthworks and Site Preparation (Stage 1 Works)

The earthworks associated with development of the site are expected to include bulk excavation of up to about 8 m depth and placement of filling to up to about 3 m.

The building will have several floor levels, as follows:

• Lower ground floor and loading dock RL 15.3 m AHD; and

• Ground floor RL 20.3 m AHD.

Based on a review of the drawings provided by the client along with the conditions encountered in the bores, the anticipated conditions at bulk excavation level (taken to be finished floor level minus about 0.3 m to 0.5 m) is shown in Table 7 in Section 9.1.

The earthworks associated with development of the site are expected to include excavation and recompaction of existing fill materials, where present, and the placement and compaction of relocated or imported fill materials.



Based on conditions encountered within the bores, the strength of the bedrock within the upper 6 m to 8 m is generally very low to low strength and would be commensurate to Class V and Class IV sandstone, as defined in Ref 12. Some layers of medium strength rock were however encountered in the bores in the upper metres of rock.

Depending on the final layout of the development, placement of up to approximately 3 m of filling may be required within the former quarry floor.

Excavation through fill materials, in-situ clays and the zones of weaker rock (extremely low to low strength) is expected to be relatively straightforward using conventional excavation equipment such as excavators fitted with rock teeth, possibly a pneumatic or hydraulic hammer for harder zones and detailed excavation. It is noted the rock strength encountered in the boreholes ranged from very low to medium strength, generally the sandstone layers exhibit higher strength than siltstone and claystone which tend to weather more rapidly.

The production rate is expected to decrease as rock strength increases and fracture spacing is wider, such as the medium strength sandstone observed at the site. The excavation of Class III sandstone or Class II siltstone is likely to require a rock hammer or medium to heavy ripping by D9 dozer (or larger).

The following procedure is generally suggested for placement and compaction of engineered filling over existing natural soils / rock:

- Remove vegetation, topsoil, uncontrolled filling and deleterious materials;
- Test roll the surface in order to determine any soft zones and assess moisture condition.
   Moisture contents should be in the range OMC -2% (dry) to OMC+2% where OMC is the optimum content at standard compaction;
- Compact the tyned natural surface (where rock is not exposed) to a dry density ratio of at least 100% Standard. The re-compacted clay should be left exposed for a minimum of time prior to placement of additional fill layers, to minimise the occurrence of desiccation cracking or softening;
- Suitable filling should be placed in horizontal layers not exceeding 300 mm loose thickness and compacted to a dry density ratio of at least 95% to 100% Standard up to within 0.5 m of design bulk earthworks level and to at least 100% Standard in the upper 0.5 m. Moisture content should be in the range as stated above;
- Particle size should generally by less than 150 mm, however, an occasional absolute maximum particle size of up to 200 mm could be used;
- Unsuitable material at cut / fill transitions should be over excavated and replaced with select fill;
- Where carbonaceous materials are to be used as controlled fill, the filling should be blended with non-carbonaceous materials and placed in horizontal layers not exceeding 300 mm loose thickness and compacted to a dry density ratio of at least 100% Standard, as determined by test methods AS1289.5.1.1 (Ref 3) and AS1289.5.4.1 (Ref 10). Moisture content determinations are to be in accordance with AS1289.2.1.1 (Ref 11) with the exception that a 50°C oven is to be used (Ref 3).

In the lower, eastern area of the site, where the existing pond is located, additional site preparation will be required, as follows:

Removal of all weak sediments and moisture affected soils;



- The depth of the sediments or the volume of water contained within the pond is not known at this stage and hence extensive dewatering should be anticipated at this stage, unless further investigation is undertaken to further quantify these volumes;
- Site drainage measures will be required to allow placement of engineered filling over the prepared surface once all the weak sediments have been removed;
- The use of a rock drainage blanket may be required to allow placement and compaction of the lower levels of the filling;
- Furthermore, it is anticipated that coal seams are likely to be exposed in this lower area during site stripping. Future groundwater flows through such seams should be anticipated and hence drainage should be designed to allow such groundwater flows to efficiently drain from the seam and from beneath the future pavement areas;
- The limited investigation carried out to date in this area (Pit 4002 and probing during previous investigations) has not established the depth of the weak sediments. Hence is it recommended that additional investigation is undertaken in this area once the surface water has been removed to further quantify the volume of weak sediments and provide further comments on likely site preparation measures required to allow placement of filling.

It is noted that the existing clay and silty clay soils are of medium to high plasticity and likely be difficult to work, particularly when wet. Site trafficability will be reduced when these soils become wet. If the soils become wet, they should be tyned and allowed to dry. Careful control of moisture will be required during compaction of these soils.

In the event that unfavourable weather conditions occur prior to and during construction, trafficability for non-tracked plant is expected to be very poor in the lower parts of the site and therefore the use of a layer of granular crushed rock, crushed recycled concrete, or similar may be required over the natural clays to provide a working platform for temporary access roads.

Alternatively, structures could be supported on piles installed through the fill to rock, as discussed in Section 9.8.

## 9.3 Retaining Structures

The design parameters for retaining structures for both short-term and long-term situations are shown in Table 8 for each of the principal geological units. These would apply to the design of cantilevered walls or shoring, contiguous pile walls and soldier pile walls. Any walls that will form part of a permanent structure should be based on long-term parameters.

The design values given are based on level ground behind the wall and do not include any surcharge loads that may be imposed near the top of the wall.

Passive pressures are given as either an earth pressure coefficient (Kp) for granular soils and / or ultimate passive pressures for residual clays and rock. The values given below are unfactored and because passive pressures are used as a resisting force, an appropriate factor of safety should be applied to determine working values and to limit deflections.

Table 8 provides suggested design parameters.



**Table 8: Design Parameters for Retaining Structures** 

	Design Parameters (unfactored)								
Description	γь	Short Term			Long Term				
	kN/m³	Ka	K <sub>0</sub>	K <sub>p</sub>	P <sub>p</sub> kPa	Ka	K <sub>0</sub>	K <sub>p</sub>	P <sub>p</sub> kPa
Filling –cohesive	18	0.25	0.40	3.5	-	0.30	0.60	3.5	-
Filling – granular	20	0.30	0.50	3.3	-	0.30	0.50	3.3	-
Clay – stiff to very stiff	19	0.25	0.40	-	200	0.30	0.60	2.5	-
Clay – hard / extremely weathered rock	20	0.25	0.40	-	200	0.35	0.55	3.0	-
Class V (extremely low to very low strength sandstone or siltstone or coal)	22	0.15	0.30	-	400	0.20	0.35	-	400
Class IV (very low to low strength sandstone or siltstone)	22	0.00	0.10	-	2000	0.10	0.25	-	2000
Class III (medium strength sandstone or siltstone)	22	0.00	0.10	-	3000	0.10	0.25	-	3000

Notes to Table 8:

The use of active pressure coefficients ( $K_a$ ) requires that there will be sufficient deflection of the retaining system during construction to reach active conditions. If lateral deflections are prevented or restricted, at-rest coefficients ( $K_0$ ) should be used.

Any surcharge loads such as pavements, construction equipment or sloping backfill should be added to the design pressures determined for the soil / rock profile alone. Below the water table the additional load due to hydrostatic pressure should be added.

The parameters provided above are based on the provision of full drainage behind the retaining walls.

## 9.4 Batter Slope Stability

During site works temporary batters may be needed to facilitate construction, such as building retaining walls or filling in quarry voids with controlled fill that will cover the slope.

Permanent batter slopes may be required where they form part of the completed development. Preliminary assessment may be based on the slopes provided in Table 9.

K<sub>a</sub> – Active earth pressure coefficient

 $K_0$  – 'At-rest' earth pressure coefficient

K<sub>D</sub> – Passive earth pressure coefficient

P<sub>D</sub> - Passive earth pressure



**Table 9: Temporary and Permanent Batter Slopes** 

Stratum	Short Term (Temporary) <sup>(1)</sup>	Long Term (Permanent) <sup>(1)</sup>
Fill - Compacted	2H:1V	2.5H:1V
Residual Clays	1.5H:1V	2H:1V
Class V (extremely low to very low strength sandstone or siltstone or coal) <sup>2</sup>	1H:1V	1.5H:1V
Class IV (very low to low strength sandstone or siltstone) <sup>2</sup>	0.5H:1V	1H:1V
Class III (medium strength sandstone or siltstone) <sup>2</sup>	Vertical	0.25H:1V to Vertical <sup>(3)</sup>

#### Notes to Table 9:

- Above values are for a maximum vertical height of 3 m. Greater depths to be specifically assessed, and may require measures for stability and drainage.
- 2. Batters in rock are dependent on jointing and will require confirmation at time of excavation.
- 3. Vertical cuts may be feasible subject to geological mapping and rock bolting or similar, if needed.

All batter slopes will require appropriate erosion protection measures, depending on the location, depth, drainage conditions and longevity of the slope in question.

In this regard, the former quarry excavation face has been formed at around 22°, which is about 2.5H:1V. No signs of gross instability were observed within this batter, although it is noted that some erosion has taken place. It is noted that some soils on the site returned high pH values. Careful selection of vegetation which is tolerant of these pH levels will be required on these slopes.

#### 9.5 Existing Filling

Based on the conditions encountered in the pits and bores, filling to depths (below surrounding ground surface levels) of greater than about 1 m is generally restricted to the north-western area and south-western area. Stockpiles of filling, which are about 5 m to 10 m in height are also present.



Table 10: Summary of Depth of Filling

Bore	Depth of Filling (m)
3001	Nil
3002	2.0
3003	0.3
3004	4.2
3005	0.3
3006	0.5
3007	2.1
601	0.1 <sup>(1)</sup>
602	0.8 <sup>(1)</sup>
603	2.2 <sup>(1)</sup>
604	0.2 <sup>(1)</sup>
605	0.4 <sup>(1)</sup>
606	2.2 <sup>(1)</sup>
701	0.15 <sup>(1)</sup>
702	3.8 <sup>(1)</sup>
703	0.3 <sup>(1)</sup>

Notes to Table 10

The majority of the deeper filling (greater than about 1 m) is located within the central and north-western area of the proposed building footprint.

#### 9.6 Suitability of Site Materials for Reuse as Filling

## 9.6.1 Soils and Extremely Weathered Rock

The results of the present investigation suggest that the majority of the former upper clayey profile has been removed, although some residual clay remains (Bore 3003 to 1.1 m depth and Bore 3006 to 1.2 m depth). Existing sandy clay filling is present in some locations (notably Bore 3002 to 2 m depth, Bore 3004 to 4.2 m depth and Bore 3007 to 2.1 m depth). The natural clay material was typically described as having very stiff or stronger consistency whereas the clay filling appeared to be in a variable compacted condition.

Figure 19 and Figure 20, below, present a graphical summary of soil plasticity and shrink-swell data obtained for soils in the vicinity of the site during the previous investigation by DP (Ref 14).

<sup>1.</sup> It should be noted that extensive site regrading has occurred since drilling of these bores and hence the depth of fill is likely to vary from that shown in this table.



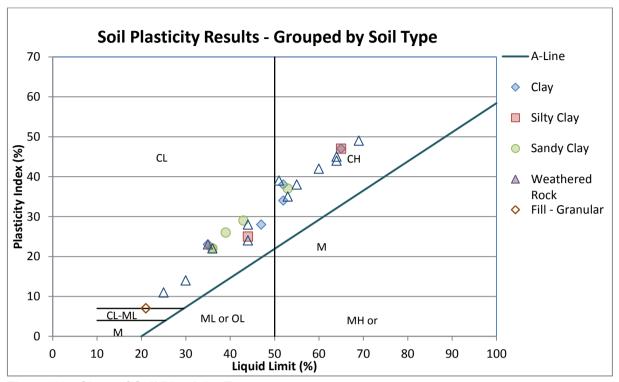


Figure 19: Chart of Soil Plasticity Tests

Available data on clay reactivity in terms of the shrink-swell index is shown plotted in Figure 20.



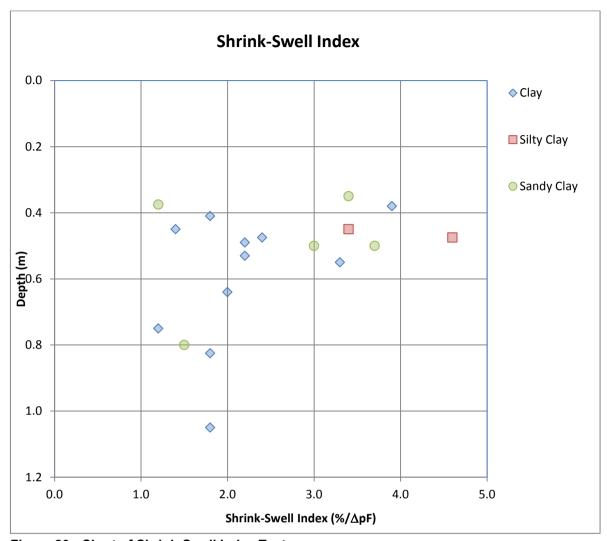


Figure 20: Chart of Shrink-Swell Index Tests

The testing indicates that the clay has a moderate propensity to change in volume with changes with moisture content. The results also indicate that the underlying clays have a moderate potential to soften on exposure to moisture, as indicated by the low soaked CBR values (as low as 5%).

The potential large characteristic surface movements associated with the use of the high plasticity clays needs to be considered if the clay is to be used beneath building areas. The use of at least 1.0 m of low-reactivity filling over the high plasticity clay will reduce the characteristic surface movement of the final profile.

The soils present within the eastern, low lying, area of the site are anticipated to have elevated moisture content and are not likely to be suitable for re-use without significant moisture reconditioning. Pit 4002, which was excavated within the edge of the existing pond (refer Drawing 1), encountered loose/soft clayey sand to 1.4 m depth overlying soft sandy clay sediments to 1.6 m depth where collapse of the pit precluded further investigation (refer Figure 21). These water-charged sediments are anticipated to be difficult to work with and would require removal to expose the underlying stiff or stronger natural soils prior to placement of filling.





Figure 21: Conditions encountered in Pit 4002

# 9.6.2 Weathered Rock

The ability to re-use weathered rock material won from bulk earthworks will be a function of the particle size achieved during excavation. In general, particle size should not exceed 150 mm for re-use as engineered filling. The purpose of this is to reduce the likelihood of difficulties if excavations are required at a later date, for example, to install footings and to reduce void spaces which could lead to piping / erosion as well as to assist with compaction. The material should be well-graded to control the compacted density and void ratio. All material to be re-used as engineered filling should be free of organics and other deleterious materials and debris.

It is anticipated that very low to medium strength weathered siltstone and sandstone encountered in Pits 301 to 305, and Bores 601 to 606, could be readily excavated / ripped to a particle size of less than about 0.3 m but more likely less than 0.15 m. It is suggested that cross-ripping methods and heavy pad foot rollers could be used to further break down excavated bedrock to material with a maximum particle size of less than 150 mm. Pits 4001 and 4003 were excavated in the areas of proposed pavements. These pits do, however, provide an indication of the excavatability of the weathered siltstone and sandstone. The weathered bedrock was relatively readily excavated using a 6.5 tonne excavator into particles in the order of 50 mm to 300 mm in Pit 4001 (refer Figure 22), and hence with additional preparation (breaking down of particles) this material would be suitable for reuse as engineered filling.





Figure 22: Weathered rock conditions in Pit 4001

It may be possible to use the coal within the bulk filling provided it is blended with other non-combustible material (refer Section 9.6.4).

# 9.6.3 Stockpiled Material

It is considered that the existing stockpiled material (predominantly ripped sandstone and siltstone with some clay) would be suitable for reuse as engineered fill in embankments or in building pads, provided that the material is moisture conditioned to achieve a moisture content at the time of placement as recommended in Section 9.2. Coarse material within the stockpile would need to be broken down such that the maximum particle size is no greater than 150 mm.

# 9.6.4 Carbonaceous Stockpiled Material

An assessment of the combustibility of the stockpiled carbonaceous material was undertaken during the previous investigation (Ref 17) and concluded the following:

- A capping Layer ranging in thickness from 0.3 m to 1.5 m is present; overlying;
- Carbonaceous siltstone and coal.

The carbonaceous material is likely to be high in combustible material. In this regard, previous assessment of samples from the site (Ref 16) indicated that combustible percentages of up to 90% were recorded in the samples of coal testing. The pits undertaken within the stockpile (Pits 5001 to 5004) encountered a blend of coal and carbonaceous material (refer Figure 23).





Figure 23: Photo of Pit 5002, showing existing capping and underlying carbonaceous material

It is understood that consideration is being given to the re-use of this carbonaceous material. This material may be suitable for re-use provided it is blended with non-carbonaceous material (ripped sandstone or siltstone, residual clay or clayey filling). In order to reduce the combustible material to an acceptable level (maximum combustibles of 40% - Ref 17) an initial blending ratio of 50:50 between the carbonaceous material and the non-carbonaceous material is recommended. If an alternative blend is proposed, additional assessment, including laboratory testing to characterise the combustibility of the blended mix should be undertaken.

Compaction testing was undertaken on a blended mix of material from the carbonaceous stockpile and completely weathered bedrock retrieved from Pits 4001 and 4003. Various blends were tested as follows:

- 40% carbonaceous material and 60% non-carbonaceous material;
- 50% carbonaceous material and 50% non-carbonaceous material; and
- 60% carbonaceous material and 40% non-carbonaceous material.

The results indicate that the material is likely to be moderately difficult to work with some sensitivity to changes in moisture. Careful control of moisture content will be required to achieve adequate compaction of this material.

Furthermore, a re-use management plan should be developed if this material is to be considered further for re-use as engineered filling, which outlines measures to ensure adequate blending to avoid pockets of high combustibility material, control of moisture content and compaction achieved.



DP has not considered chemical concentrations of the carbonaceous materials in this assessment. Recommendations from GHD in relation to contamination issues at the site may render the material unsuitable for re-use. However, provided that the material is deemed suitable for re-use from a contamination viewpoint, it may be suitable as bulk filling provided the recommendations outlined below are followed.

Development of detailed procedures and specifications for remediation will be required prior to remediation works. A combustion risk mitigation program, including a Remediation Action Plan will be required which will outline the procedures, specifications and responsibilities for remediation works at the site.

It is also recommended that a management plan is prepared for future management of combustion risk at the sites.

# 9.7 High Level Footings (Stage 1 Works)

It is preferable that all footings found on material of similar stiffness, (i.e. all footings to bear on the bedrock). Careful consideration of detailing and articulation of the structures would be needed during the design to allow the structures to tolerate the differential movements which could result from founding on materials of differing stiffness, such as bedrock and clay or filling.

Spread footings founded within the relevant strata should be designed for the following ultimate limit state bearing pressures:

Class V (Extremely low to very low strength siltstone or sandstone, or coal)
 3000 kPa;

Class IV (Very Low strength or stronger siltstone or sandstone)
 5000 kPa;

Class III (Typically Medium strength or stronger sandstone)
 10000 kPa.

A factor of safety of 3 should be applied to these values to derive an allowable bearing pressure but serviceability (settlement) analysis needs to be undertaken during detailed design.

As outlined in Table 6, the anticipated conditions at foundation level for the lower ground floor level generally includes very low strength through to medium strength sandstone or laminate bedrock (i.e. Class IV rock but may include some areas of Class V bedrock).

It is suggested that the design of pad footings could be design on Class IV parameters, however, it should be noted that some localised widening or deepening of footings may be required in some areas of the site. Careful geotechnical inspection of all pad footing excavations must be undertaken during construction to determine where such alterations to the footing design is required.

Reference to the geological sections provided in Appendix D show that coal or carbonaceous material is not generally anticipated at foundation level, with the coal seam generally several metres below the anticipated foundation level. In some bores, however, such as Bore 701 and Bore 3001, coal was encountered within 1 m to 2 m of the proposed foundation level. The shear strength of the coal and associated carbonaceous material is highly sensitive to changes in moisture, and they will soften appreciably if subjected to increased moisture.



Therefore, if carbonaceous rock or coal is encountered at foundation level, the design and construction of the footings must account for the moisture-sensitive ground conditions and lower bearing pressures, commensurate with Class V rock conditions should be adopted. Further advice should be sought from the geotechnical engineer during construction in relation to these areas of the site.

# 9.8 Deep Footings / Piles (Stage 1 Works)

# 9.8.1 Geotechnical Strength Reduction Factor

In the current Piling Code (Ref 1), the design geotechnical strength of a pile ( $R_{d,g}$ ) is the ultimate geotechnical strength ( $R_{d,ug}$ ) multiplied by the geotechnical strength reduction factor ( $\varphi_0$ ), such that:

•  $R_{d,g} = \phi_{g} R_{d,ug}$ 

The calculated value  $R_{d,g}$  must equal or exceed the structural design action effect  $E_d$ .

Selection of the geotechnical strength reduction factor  $(\phi_g)$  is based on a series of individual risk ratings (IRR) which are weighted and lead to an average risk rating (ARR). The individual risk ratings and final value of  $\phi_q$  depend on the following factors:

- Site: the type, quantity and quality of testing;
- · Design: design methods and parameter selection;
- Installation: construction control and monitoring;
- Pile testing regime; testing benefit factor based on percentage of piles tested and the type of testing; and
- Redundancy: whether other piles can take up load if a given pile settles or fails.

Using the methodology outlined in the piling code and the supplementary site data retrieved during the present investigation, average risk ratings have been assessed for future foundations.

The recommended geotechnical strength reduction factors  $(\phi_g)$  for piles founded in bedrock is as follows in Table 11.

**Table 11: Recommended Geotechnical Strength Reduction Factor** 

	Geotechnical Strength Reduction Factor $(\phi_g)$		
Foundation Strata	Low Redundancy in design of piles	High Redundancy in design of piles	
Piles founded in underlying bedrock	0.55	0.60	



These strength reduction factors are based on inspections to be completed by a qualified geotechnical engineer during piling operations, and on dynamic or static load testing in accordance with the requirements of AS2159 (Ref 1) during piling operations. It is however pointed out that the final strength reduction factor will depend on the piling contractor chosen and experience of the pile designer. The strength reduction factors should be checked when this information is available. Piles should be installed by experienced operators, using suitably sized piling rigs, monitoring equipment and supervision.

## 9.8.2 Pile Parameters

Deep foundation systems would be appropriate for the support of major loads and where the presence of uncontrolled fill precludes the use of shallow footings. Bored piles would be suitable founded within the very low to low strength sandstone bedrock. Given the presence of shallow bedrock driven piles are not considered suitable for this site.

The recommended preliminary design parameters for piles are shown in Table 12.

**Table 12: Design Parameters for Piles** 

	Ultim	nate <sup>(7)</sup>	Serviceability (Working Loads)
Stratum	End Bearing (kPa)	Shaft Adhesion (kPa)	End Bearing (kPa)
Clay – hard / extremely weathered rock	1800	80	600
Class V (extremely low to very low strength sandstone or siltstone or coal) <sup>2</sup>	4000	200	1200
Class IV (very low to low strength sandstone or siltstone) <sup>2</sup>	10000	500	2500
Class III (medium strength sandstone or siltstone) <sup>2</sup>	20000	1100	4000

Notes to Table 12:

- 1. The design bearing pressures should be adjusted to account for weaker layers below the bearing layer if present.
- 2. Piles founded on coal or claystone should be avoided due to potential for softening and excessive settlement.
- 3. Ultimate Values occur at large settlements (> 5% of minimum pile diameter / width)
- 4. Design geotechnical strength ( $R_{d,g}$ ) should initially be based on a strength reduction factor of  $\phi_g = 0.55$
- 5. Serviceability / Max Allowable end bearing to cause settlement of < 1% of minimum pile diameter / width
- 6. AS 2159 2009 requires that the contribution of the shaft from ground surface to 1.5 times pile diameter or 1 m (whichever is greater) shall be ignored
- 7. Piles founded within the coal or within 2 m above the coal should be designed for Class V parameters for the affected section of pile, as discussed below.

For piles in tension, the shaft adhesion parameters should be reduced to 75% of the values in Table 12.

For vertical loading, it is suggested that piles should be spaced at 2.5 pile diameters or greater such that the overall capacity of the pile group can be equivalent to the sum of the individual piles (i.e. group efficiency factor of unity).

It should be noted that the parameters given in Table 12 are for clean rock sockets (with an R2 roughness rating) and bases. Specific cleaning buckets and grooving tools should be used in pile construction, together with suitable inspection or verification methods.



For calculation of serviceability geotechnical strength, the capacity can be calculated using the serviceability end bearing values and ultimate shaft adhesion values within the rock units. In the serviceability case, these values do not need to be factored. It is recommended that deflection under load is checked and compared to serviceability deflection limits.

It is noted that higher strength seams are present within the sandstone and conglomerate and hence careful selection of piling equipment should be made by the piling contractor, which is able to penetrate through these higher strength seams.

Pile installation could be affected by the possible presence of obstructions within existing fill such as concrete, steel and other coarse inclusions. The available information suggests that this will not be a widespread problem however the possibility cannot be precluded. Piles founded within the coal or within 2 m above the coal should be designed for Class V parameters.

Given the presence of coal seams within the subsurface profile, it is considered of reasonable likelihood that pile excavations which intersect coal seams may encounter groundwater as coal seams often act as permeable conduits within the rock mass. Allowances should be made to either remove groundwater from the base of the pile excavations prior to the placement of concrete and steel (if feasible) or the placement of concrete via tremie methods to the base of the pile excavation. A contingency of providing temporary casing may also be required if collapsing conditions occur within the coal seam.

# 9.8.3 Pile Testing and Geotechnical Inspections

Section 8 of AS2159 – 2009 (Ref 1) outlines the pile load testing requirements. Clause 8.2.4 of AS2159 states that where the basic geotechnical strength reduction factor is greater than 0.4, testing shall be performed to verify the integrity of pile shafts. Assessment of pile shaft integrity may be by high-strain dynamic pile testing or other methods of integrity testing. Seismic integrity testing may be suitable in this instance. It is recommended that a percentage of piles are tested as outlined in AS2159 (Ref 1).

It is also recommended that comprehensive inspections and monitoring be undertaken during the installation of piles, including but not necessarily limited to geotechnical inspection during installation to record the depth of pile, the conditions encountered at the toe of the pile and review of any pile installation data acquired during drilling.

During construction the design bearing pressures should be confirmed by geotechnical inspection and / or quality assurance testing relevant to the type of pile and method of installation.

# 9.9 Seismic Design

The earthquake code (AS1170.4-2007, Ref 13) provides design factors based on location (earthquake risk) geotechnical conditions.

The Hazard Factor (Z) for Maitland is 0.10 as given in Table 3.2 of AS1170.4. This is the bedrock acceleration coefficient with an annual probability of exceedance of 1 in 500.



The site sub-soil class is assessed to be Class  $C_e$  – "shallow soil site", with reference to Table 4.1 of AS1170.4 due to the presence of soil beneath some areas of the proposed building footprint, with the remained of the building foot print to comprise bedrock at bulk excavation level.

However, a site subsoil class of  $B_e$  – "Rock Site" could be considered if the proposed building can be designed such that the areas of the site can be designed to be founded on bedrock and with a UCS rock strength > 1 Mpa and the building is appropriately designed to be isolated from the shallow soils.

The building maybe isolated from the shallow soils by constructing a suspended slab supported on sleaved piles. All foundations should a permanent steel casing sleave through the soil with the outer permanent casing creating an annulus (gap) between the outer casing and the pile.

An alternative option could include removal of all soil from the building footprint to expose bedrock with a UCS of greater than 1 MPa and replacing the soil with a stabilised soil material such that the stabilised soil which has an average compacted UCS of at least 1.5 MPa and not less 1 MPa. If this option is to be further considered, further geotechnical advice should be sought together with additional laboratory testing which will be required to confirm the appropriate cementitious material and percentage to be incorporated into the soil to achieve the design UCS strength.

# 9.10 Pavements

# 9.10.1 Subgrade Conditions and Design CBR

Pavements are proposed to be constructed to allow access from Metford Road, with an entrance on both the northern and southern side of the building. A main, terraced car parking area is shown in the eastern part of the site on the revised master plan for the site. A secondary car park, located to the west of the proposed hospital is also shown on the plans. Limited investigation has been undertaken within these areas of the site to date (particularly within the eastern, low lying areas). Once further access is available, it is recommended that additional investigation is undertaken to characterise the subsurface conditions in these areas of the site and to allow further comment on subgrade preparation measures. Preliminary comments are provided below to allow preliminary design of pavements.

Based on the results of the pits and bores, conditions anticipated to be exposed at subgrade levels are discussed for each development area in Table 13 below.



**Table 13: Anticipated Subgrade Conditions** 

Pavement Area	Relevant Bores/Pits	Anticipated Subgrade Level (m AHD)	Anticipated Subgrade Conditions
Northern Access Road	602, 3001, 4001	19 to 21	Clayey filling, residual clay soils or weak bedrock
Western Carpark and Access Road	3007, 3008 and 4004	19.3 to 21	Existing sandy clay filling (Bore 3007). Remainder of bores/pits not excavated at date of reporting, waiting for site clearance
New West Hospital Road	701 and 4005	19.3	Residual clay soils or weak bedrock. (Pit 4005 not excavated at date of reporting, waiting on site clearance)
Car Park, Loading Dock and New East Hospital Road	3006, 603, 604, 4002	13.8 (loading dock) to 19.3 (car park)	Very low strength or stronger sandstone (part of loading dock) and weak sediments in existing pond (to be removed and replaced with engineered filling)

As discussed in Section 9.2, groundwater and surface water inflow into the lower, eastern area of the site should be anticipated, and hence extensive drainage measures will be required to allow placement and compaction of engineered filling. The provision of a rock drainage blanket may also be required.

The further comments provided below are based on the assumption that further assessment is undertaken and site preparation measures are enacted to remove all weak sediments and unsuitable material followed by placement and adequate compaction of engineered filling under all pavement areas.

It should be noted that variable depth of filling is present throughout the site and hence subgrade conditions are likely to vary considerably throughout pavement alignments. Additional investigation is strongly recommended once the site has been cleared of existing stockpiles and trees (where remaining) to allow further assessment of subgrade conditions.

The existing filling is deemed as "uncontrolled". It is likely to exhibit variation in compaction levels and materials present, as noted in the test bores and pits. The filling appears to have been progressively placed over the last 20 to 30 years. Ongoing settlement of the filling is likely to have occurred over this time, although it is not currently possible to determine the magnitude of any future settlements of the filling. The results of the in-situ testing within the filling indicate that it is generally moderately compacted.

In order to provide uniform support for the proposed road pavements and to reduce the risk of future differential settlements, it is recommended that rigorous subgrade improvements are undertaken within the area of the existing fill. These measures are discussed in Section 9.10.2.2.

Provided that residual soils, where encountered at subgrade level, are of at least stiff consistency, it is suggested that the standard subgrade preparation measures outlined in Section 9.10.2.1 would be appropriate. Similar subgrade preparation measures would be suitable for areas where bedrock is exposed.



The results of the laboratory testing indicated a soaked CBR of 16% and 25% for clayey sand and sandstone and a soaked CBR of only 4.5% for extremely weathered siltstone (clay-like properties). Based on previous experience in the Metford area, the natural clays have a soaked CBR of about 3% Based on the results of the testing a design CBR value of 3% has been adopted for areas comprising residual clay and fill subgrade. It is noted that the design CBR value of the fill subgrade will be dependent on the quality of the filling used during in bulk earthworks and the subgrade preparation measures enacted as discussed in Section 9.10.2.2 below.

A preliminary design subgrade CBR of 8% is recommended for areas where weathered sandstone rock is exposed at subgrade level.

# 9.10.2 Subgrade Preparation

# 9.10.2.1 Standard Subgrade

Pavement subgrade preparation should be carried out in general accordance with the following methodology:

- Strip all vegetation and organic topsoils from the pavement alignment;
- Excavate to design subgrade level;
- Undertake geotechnical inspection of the exposed surface to assess the suitability of any existing
  filling to remain in place. This may require proof rolling of the exposed surface together with
  additional dynamic penetrometer testing at close spacing (say every 20 m);
- Where rock is encountered at formation level it should be ripped to a depth of 300 mm below the subgrade level and re-compacted;
- In areas of natural ground at nominal subgrade level, roll the exposed subgrade surface with at least six passes of a minimum 12 tonne deadweight vibrating roller, with a final proof rolling pass undertaken at slow speed with careful visual inspection by a geotechnical engineer to allow the detection of any soft or compressible zones;
- In the event that sections of the exposed subgrade are deemed unsuitable to remain in place, additional excavation and replacement with approved filling will be required;
- Any subgrade replacement filling should be placed in horizontal layers of less than 250 mm loose thickness with each layer compacted to at least 100% Standard dry density ratio with moisture contents maintained within the range of -4% to -1% of optimum moisture content for Standard compaction in accordance with AS3798-2007 (Ref 9);
- Adjust the moisture content of the exposed subgrade to the moisture range as presented above;
- Compact the subgrade to a density ratio of at least 100% relative to Standard compaction with moisture contents as presented above;
- Protect the area after subgrade preparation to maintain moisture contents as far as practicable.
  Previous experience suggests that shrinkage of clay soils may result if they are allowed to dry
  and then subsequently swell as they return to their equilibrium moisture content following
  completion of pavement construction. Therefore excessive surface drying should be avoided in
  pavement subgrade areas.



# 9.10.2.2 In Deep Fill Areas

A more rigorous subgrade preparation will be required in areas of the site which have deep existing filling (such as anticipated within the western car park where filling was encountered to 2.1 m in Bore 3007).

Where the filling is likely to not be affected by groundwater and is anticipated to be in a moderately compacted conditions (i.e. western car park), re-compaction of at least the upper 1 m of the existing filling below nominal subgrade level, where suitable for re-use in terms of particle size, moisture condition and material types, is considered to be the minimum required to provide a relatively uniform support for the future pavement.

It should be recognised that construction of the pavement over the existing filling will result in an increased, yet unquantifiable, risk of premature failure of the pavement owing to ongoing settlement of the filling. Such failures may lead to increased maintenance costs and the need to re-sheet the pavement at shorter intervals, possibly every three to five years. Whilst the more rigorous subgrade preparation outlined below is aimed at reducing this risk, it cannot economically be completely eliminated and therefore the client must accept this increased risk.

The rigorous pavement subgrade preparation should include:

- Excavate to 1 m below the nominal subgrade level within the existing filling or to the natural soils
  in areas of proposed pavement and stockpile for assessment by a geotechnical engineer for its
  suitability for re-use;
- Remove any additional topsoil, overly wet or deleterious filling or other material;
- Where rock is encountered at formation level it should be ripped to a depth of 300 mm below the subgrade level and re-compacted;
- Undertake a series of dynamic cone penetrometer tests (DCP) on a grid pattern (say 5 10 m centres) across the site to assess the condition of the underlying material and its suitability to act as a subgrade;
- Roll the exposed subgrade surface with at least six passes of a minimum 12 tonne deadweight
  vibrating roller, with a final proof rolling pass undertaken at slow speed with careful visual
  inspection by a geotechnical engineer to allow the detection of any soft or compressible zones;
- In the event that sections of the exposed subgrade are deemed unsuitable to remain in place as a
  result of either the DPT or the proof rolling, additional excavation and replacement with approved
  filling will be required or alternative measures such as the provision of a geogrid and geotextile
  layer will be required;
- A provisional rate for over excavation of additional unsuitable material and importation of suitable replacement filling should be included in the cost schedule for this site;
- Compact the exposed natural soils or existing filling deemed suitable to act as subgrade to a minimum dry density ratio of 100% Standard in accordance with AS3798-2007 (Ref 9); and
- Any subgrade replacement filling should be placed in horizontal layers of less than 250 mm loose thickness with each layer compacted to at least 100% Standard dry density ratio with moisture contents maintained within the range of -4% to -1% of optimum moisture content for Standard compaction.



Based on tactile assessment of the upper filling material encountered in the bores and the results of the CBR testing, the majority of the material is anticipated to be suitable for re-use within the improved subgrade provided that all deleterious, oversized and organic material is removed.

Compaction testing of all engineered filling and prepared subgrade surfaces should be carried out with sufficient density testing to justify that it is well compacted. AS 3798: *Guidelines on Earthworks for Commercial and Residential Developments* (Ref 9) provides information regarding the placement of filling. A Level 1 inspection and testing regime as defined in AS3798 is suggested for the rigorous subgrade preparation measures.

# 9.10.2.3 Loading Dock

Limited investigation has been undertaken within the area of the loading dock and eastern car park owing to the presence of the existing pond and weak surface soils. It is strongly recommended that additional investigation is undertaken within these areas once site access is available to further characterise the subsurface conditions and allow further comment on pavement preparation measures. Preliminary comments on site preparation in these areas are presented in Section 9.2.

# 9.10.3 Pavement Drainage

The pavement should be designed to incorporate the provision of adequate surface and subsoil drainage so as to maintain the subgrade as close to the optimum moisture content as possible and to ensure that the pavement layers do not become saturated.

Normally, subsoil drainage should be installed at least 0.5 m below subgrade level adjacent to pavements. Preparation of subgrade surfaces should be such that adequate crossfalls for surface drainage are achieved across the final pavement.

Given the presence of deep, uncontrolled filling in some areas of proposed pavement, it is suggested that subsurface drainage is installed with a slightly steeper grade than is normally required to reduce the risk of reversal of drainage paths in the event that ongoing settlement occurs within the filling.

# 9.10.4 Pavement Thickness Design

The design traffic loading for the proposed link road has not been provided to DP.

Two pavement thickness designs are presented based on the following design traffic loadings:

- 4 x 10<sup>4</sup> ESA, which is based on the roads being consistent with "local access with no buses" as defined in Austroads; and
- 3 x 10<sup>5</sup> ESA, which is based on the roads being consistent with "local access in industrial area" as defined in Austroads.

If the traffic loading is to be significantly different from this value, the pavement thickness designs presented in the following sections should be reviewed.



# 9.10.5 Flexible Pavement Thickness Design

It is understood that the pavements will be privately owned and therefore not a Council asset. The pavement thickness design presented below has been based on procedures outlined in Austroads – Guide to Pavement Technology (Ref 6).

The proposed pavement thickness design is outlined in Table 14 below.



Table 14: Pavement Thickness Design - Sealed Flexible Pavement

Layer	Layer Thickness (mm)			
Traffic Loading (ESA)	4 x 10 <sup>4</sup> ESA		3 x 10 <sup>5</sup> ESA	
Design Subgrade CBR	3% 8% (new filling or clay soil) (weathered sandstone rock)		3% (new filling or clay soil)	8% (weathered sandstone rock)
Wearing Course	40 mm AC10*	40 mm AC10*	40 mm AC10*	40 mm AC10*
Basecourse	120	100	120	120
Subbase	200	150	280	150
Select Subgrade	200 <sup>(1)</sup>	-	200 <sup>(1)</sup>	-
Total	360 (excluding select)	290	440 (excluding select)	310

Notes to Table 14:

A 7 mm or 10 mm prime seal should be placed over the basecourse

<sup>(1)</sup> Additional select may be required dependent on conditions exposed at the time of excavation



The recommended material quality and compaction requirements for sealed flexible pavement are presented in Table 15, below.

Table 15: Material Quality and Compaction Requirements - Sealed Flexible Pavement

Pavement Layer	Material Quality	Compaction Requirements
Basecourse	CBR ≥ 80%, PI ≤ 6%, Grading in accordance with Table 242.3 of Ref 17	Compact to at least 98% dry density ratio Modified (AS 1289.5.2.1, Ref 8)
Subbase	CBR ≥ 30%, PI ≤ 12%. Grading in accordance with Table 242.4 (Ref 17)	Compact to at least 95% dry density ratio Modified (AS 1289.5.2.1, Ref 8)
Select Subgrade (if required)	Soaked CBR ≥ 15%	Compact to 100% dry density ratio Standard (AS 1289.5.1.1, Ref 3)
Subgrade	Refer to Section 9.10.1 and Section 9.10.2	Compact to at least 100% dry density ratio Standard (AS 1289.5.1.1, Ref 3)

Notes to Table 15

CBR - California bearing ratio (4 day soaked)

PI - Plasticity Index

The select subgrade should be a well-graded material which is suitable for placement over the clay, filling and weathered bedrock subgrade, and which requires minimal working / rolling to achieve compaction. Thus coarse material is not expected to be suitable. The maximum particle size of the select should be no greater than one-half the layer thickness.

# 10. References

- 1. Australian Standard 2159-2009, "Piling Design and Installation", Standards Australia.
- 2. Wollongong City Council, "Wollongong Development Control Plan 2009, Part E: General Controls Environmental Controls, Chapter E19: Earthworks (Land Reshaping Works)".
- Australian Standard AS 1289.5.1.1-2003, "Methods of testing soils for engineering purposes", Standards Australia.
- 4. Australian Standard AS2870-2011, 'Residential Slabs and Footings', April 2011, Standards Australia.
- Cement Concrete Aggregates Australia, Technical Note 61 "Articulated Walling".
- 6. Austroads, "Guide to Pavement Technology, Part 2: Pavement Structural Design", 2017.
- 7. Australian Road Research Board, Special Report No.41, "Into a New Age of Pavement Design, A Structural Design Guide for Flexible Residential Street Pavements", dated 1989.
- 8. Australian Standard AS 1289.5.2.1-2003, "Methods of testing soils for engineering purposes", Standards Australia.
- 9. Australian Standard AS 3798-2007 "Guidelines on Earthworks for Commercial and Residential Developments", Standards Association of Australia.



- Australian Standard AS 1289.5.4.1-2007, "Methods of testing soils for engineering purposes", Standards Australia.
- 11. Australian Standard AS 1289.2.11-2005, "Methods of testing soils for engineering purposes", Standards Australia.
- 12. P.J.N.Pells, G. Mostyn and B.F.Walker, "Foundations on Sandstone and Shale in the Sydney Region", Australian Geomechanics December 1998.
- 13. Australian Standard 1170.4-2007, "Structural design actions, Part 4: Earthquake actions in Australia", Standards Australia.
- 14. Douglas Partners Pty Ltd, "Report on Geotechnical Assessment, New Maitland Hospital, Metford", Report 81719.00.R.001.Rev1, dated 15 July 2015.
- 15. Douglas Partners Pty Ltd, "Report on Geotechnical Investigation, Proposed New Maitland Hospital, Metford Road, Metford", Report 81719.01.R.001.Rev0, dated 14 December 2015.
- 16. Douglas Partners Pty Ltd, "Report on Geotechnical Investigation, Proposed New Maitland Hospital, Metford Road, Metford", Report 81719.01.R.001.Rev2, dated 9 May 2018.
- 17. Douglas Partners Pty Ltd, "Assessment of Existing Capping over Carbonaceous Material Stockpile, Proposed New Maitland Hospital (Chitter Pile), Metford Road, Metford", Report 81719.07.R.001.Rev1, dated 12 July 2018.
- 18. Maitland City Council, "Manual of Engineering Standards".

# 11. Limitations

Douglas Partners Pty Ltd (DP) has prepared this report for this project at Metford Road, Metford with reference to DP's proposal NCL180660 dated 13 November 2018 and acceptance received from Multiplex Constructions Pty Ltd dated 22 November 2018. The work was carried out under a consultancy agreement between DP and Multiplex Constructions Pty Ltd. This report is provided for the exclusive use of Multiplex Constructions Pty Ltd for this project only and for the purposes as described in the report. It should not be used by or relied upon for other projects or purposes on the same or other site or by a third party. Any party so relying upon this report beyond its exclusive use and purpose as stated above, and without the express written consent of DP, does so entirely at its own risk and without recourse to DP for any loss or damage. In preparing this report DP has necessarily relied upon information provided by the client and/or their agents.

The results provided in the report are indicative of the sub-surface conditions on the site only at the specific sampling and/or testing locations, and then only to the depths investigated and at the time the work was carried out. Sub-surface conditions can change abruptly due to variable geological processes and also as a result of human influences. Such changes may occur after DP's field testing has been completed.



DP's advice is based upon the conditions encountered during this investigation. The accuracy of the advice provided by DP in this report may be affected by undetected variations in ground conditions across the site between and beyond the sampling and/or testing locations. The advice may also be limited by budget constraints imposed by others or by site accessibility.

This report must be read in conjunction with all of the attached and should be kept in its entirety without separation of individual pages or sections. DP cannot be held responsible for interpretations or conclusions made by others unless they are supported by an expressed statement, interpretation, outcome or conclusion stated in this report.

This report, or sections from this report, should not be used as part of a specification for a project, without review and agreement by DP. This is because this report has been written as advice and opinion rather than instructions for construction.

The scope for work for this investigation/report did not include the assessment of surface or subsurface materials or groundwater for contaminants, within or adjacent to the site. Should evidence of filling of unknown origin be noted in the report, and in particular the presence of building demolition materials, it should be recognised that there may be some risk that such filling may contain contaminants and hazardous building materials.

The contents of this report do not constitute formal design components such as are required, by the Health and Safety Legislation and Regulations, to be included in a Safety Report specifying the hazards likely to be encountered during construction and the controls required to mitigate risk. This design process requires risk assessment to be undertaken, with such assessment being dependent upon factors relating to likelihood of occurrence and consequences of damage to property and to life. This, in turn, requires project data and analysis presently beyond the knowledge and project role respectively of DP. DP may be able, however, to assist the client in carrying out a risk assessment of potential hazards contained in the Comments section of this report, as an extension to the current scope of works, if so requested, and provided that suitable additional information is made available to DP. Any such risk assessment would, however, be necessarily restricted to the geotechnical components set out in this report and to their application by the project designers to project design, construction, maintenance and demolition.

# **Douglas Partners Pty Ltd**

# Appendix A

About This Report Sampling Methods Soil Descriptions Symbols and Abbreviations Rock Descriptions

# About this Report

### Introduction

These notes have been provided to amplify DP's report in regard to classification methods, field procedures and the comments section. Not all are necessarily relevant to all reports.

DP's reports are based on information gained from limited subsurface excavations and sampling, supplemented by knowledge of local geology and experience. For this reason, they must be regarded as interpretive rather than factual documents, limited to some extent by the scope of information on which they rely.

# Copyright

This report is the property of Douglas Partners Pty Ltd. The report may only be used for the purpose for which it was commissioned and in accordance with the Conditions of Engagement for the commission supplied at the time of proposal. Unauthorised use of this report in any form whatsoever is prohibited.

# **Borehole and Test Pit Logs**

The borehole and test pit logs presented in this report are an engineering and/or geological interpretation of the subsurface conditions, and their reliability will depend to some extent on frequency of sampling and the method of drilling or excavation. Ideally, continuous undisturbed sampling or core drilling will provide the most reliable assessment, but this is not always practicable or possible to justify on economic grounds. In any case the boreholes and test pits represent only a very small sample of the total subsurface profile.

Interpretation of the information and its application to design and construction should therefore take into account the spacing of boreholes or pits, the frequency of sampling, and the possibility of other than 'straight line' variations between the test locations.

### Groundwater

Where groundwater levels are measured in boreholes there are several potential problems, namely:

 In low permeability soils groundwater may enter the hole very slowly or perhaps not at all during the time the hole is left open;

- A localised, perched water table may lead to an erroneous indication of the true water table;
- Water table levels will vary from time to time with seasons or recent weather changes. They may not be the same at the time of construction as are indicated in the report;
- The use of water or mud as a drilling fluid will mask any groundwater inflow. Water has to be blown out of the hole and drilling mud must first be washed out of the hole if water measurements are to be made.

More reliable measurements can be made by installing standpipes which are read at intervals over several days, or perhaps weeks for low permeability soils. Piezometers, sealed in a particular stratum, may be advisable in low permeability soils or where there may be interference from a perched water table.

## Reports

The report has been prepared by qualified personnel, is based on the information obtained from field and laboratory testing, and has been undertaken to current engineering standards of interpretation and analysis. Where the report has been prepared for a specific design proposal, the information and interpretation may not be relevant if the design proposal is changed. If this happens, DP will be pleased to review the report and the sufficiency of the investigation work.

Every care is taken with the report as it relates to interpretation of subsurface conditions, discussion of geotechnical and environmental aspects, and recommendations or suggestions for design and construction. However, DP cannot always anticipate or assume responsibility for:

- Unexpected variations in ground conditions.
   The potential for this will depend partly on borehole or pit spacing and sampling frequency:
- Changes in policy or interpretations of policy by statutory authorities; or
- The actions of contractors responding to commercial pressures.

If these occur, DP will be pleased to assist with investigations or advice to resolve the matter.

# About this Report

### **Site Anomalies**

In the event that conditions encountered on site during construction appear to vary from those which were expected from the information contained in the report, DP requests that it be immediately notified. Most problems are much more readily resolved when conditions are exposed rather than at some later stage, well after the event.

# **Information for Contractual Purposes**

Where information obtained from this report is provided for tendering purposes, it is recommended that all information, including the written report and discussion, be made available. In circumstances where the discussion or comments section is not relevant to the contractual situation, it may be appropriate to prepare a specially edited document. DP would be pleased to assist in this regard and/or to make additional report copies available for contract purposes at a nominal charge.

# **Site Inspection**

The company will always be pleased to provide engineering inspection services for geotechnical and environmental aspects of work to which this report is related. This could range from a site visit to confirm that conditions exposed are as expected, to full time engineering presence on site.

# Sampling Methods Douglas Partners

# Sampling

Sampling is carried out during drilling or test pitting to allow engineering examination (and laboratory testing where required) of the soil or rock.

Disturbed samples taken during drilling provide information on colour, type, inclusions and, depending upon the degree of disturbance, some information on strength and structure.

Undisturbed samples are taken by pushing a thinwalled sample tube into the soil and withdrawing it to obtain a sample of the soil in a relatively undisturbed state. Such samples yield information on structure and strength, and are necessary for laboratory determination of shear strength and compressibility. Undisturbed sampling is generally effective only in cohesive soils.

### **Test Pits**

Test pits are usually excavated with a backhoe or an excavator, allowing close examination of the insitu soil if it is safe to enter into the pit. The depth of excavation is limited to about 3 m for a backhoe and up to 6 m for a large excavator. A potential disadvantage of this investigation method is the larger area of disturbance to the site.

### **Large Diameter Augers**

Boreholes can be drilled using a rotating plate or short spiral auger, generally 300 mm or larger in diameter commonly mounted on a standard piling rig. The cuttings are returned to the surface at intervals (generally not more than 0.5 m) and are disturbed but usually unchanged in moisture content. Identification of soil strata is generally much more reliable than with continuous spiral flight augers, and is usually supplemented by occasional undisturbed tube samples.

# **Continuous Spiral Flight Augers**

The borehole is advanced using 90-115 mm diameter continuous spiral flight augers which are withdrawn at intervals to allow sampling or in-situ testing. This is a relatively economical means of drilling in clays and sands above the water table. Samples are returned to the surface, or may be collected after withdrawal of the auger flights, but they are disturbed and may be mixed with soils from the sides of the hole. Information from the drilling (as distinct from specific sampling by SPTs or undisturbed samples) is of relatively low

reliability, due to the remoulding, possible mixing or softening of samples by groundwater.

# **Non-core Rotary Drilling**

The borehole is advanced using a rotary bit, with water or drilling mud being pumped down the drill rods and returned up the annulus, carrying the drill cuttings. Only major changes in stratification can be determined from the cuttings, together with some information from the rate of penetration. Where drilling mud is used this can mask the cuttings and reliable identification is only possible from separate sampling such as SPTs.

# **Continuous Core Drilling**

A continuous core sample can be obtained using a diamond tipped core barrel, usually with a 50 mm internal diameter. Provided full core recovery is achieved (which is not always possible in weak rocks and granular soils), this technique provides a very reliable method of investigation.

# **Standard Penetration Tests**

Standard penetration tests (SPT) are used as a means of estimating the density or strength of soils and also of obtaining a relatively undisturbed sample. The test procedure is described in Australian Standard 1289, Methods of Testing Soils for Engineering Purposes - Test 6.3.1.

The test is carried out in a borehole by driving a 50 mm diameter split sample tube under the impact of a 63 kg hammer with a free fall of 760 mm. It is normal for the tube to be driven in three successive 150 mm increments and the 'N' value is taken as the number of blows for the last 300 mm. In dense sands, very hard clays or weak rock, the full 450 mm penetration may not be practicable and the test is discontinued.

The test results are reported in the following form.

 In the case where full penetration is obtained with successive blow counts for each 150 mm of, say, 4, 6 and 7 as:

> 4,6,7 N=13

 In the case where the test is discontinued before the full penetration depth, say after 15 blows for the first 150 mm and 30 blows for the next 40 mm as:

15, 30/40 mm

# Sampling Methods

The results of the SPT tests can be related empirically to the engineering properties of the soils.

# Dynamic Cone Penetrometer Tests / Perth Sand Penetrometer Tests

Dynamic penetrometer tests (DCP or PSP) are carried out by driving a steel rod into the ground using a standard weight of hammer falling a specified distance. As the rod penetrates the soil the number of blows required to penetrate each successive 150 mm depth are recorded. Normally there is a depth limitation of 1.2 m, but this may be extended in certain conditions by the use of extension rods. Two types of penetrometer are commonly used.

- Perth sand penetrometer a 16 mm diameter flat ended rod is driven using a 9 kg hammer dropping 600 mm (AS 1289, Test 6.3.3). This test was developed for testing the density of sands and is mainly used in granular soils and filling.
- Cone penetrometer a 16 mm diameter rod with a 20 mm diameter cone end is driven using a 9 kg hammer dropping 510 mm (AS 1289, Test 6.3.2). This test was developed initially for pavement subgrade investigations, and correlations of the test results with California Bearing Ratio have been published by various road authorities.

# Soil Descriptions

# **Description and Classification Methods**

The methods of description and classification of soils and rocks used in this report are based on Australian Standard AS 1726-1993, Geotechnical Site Investigations Code. In general, the descriptions include strength or density, colour, structure, soil or rock type and inclusions.

# Soil Types

Soil types are described according to the predominant particle size, qualified by the grading of other particles present:

Туре	Particle size (mm)
Boulder	>200
Cobble	63 - 200
Gravel	2.36 - 63
Sand	0.075 - 2.36
Silt	0.002 - 0.075
Clay	<0.002

The sand and gravel sizes can be further subdivided as follows:

Туре	Particle size (mm)
Coarse gravel	20 - 63
Medium gravel	6 - 20
Fine gravel	2.36 - 6
Coarse sand	0.6 - 2.36
Medium sand	0.2 - 0.6
Fine sand	0.075 - 0.2

The proportions of secondary constituents of soils are described as:

Term	Proportion	Example
And	Specify	Clay (60%) and
		Sand (40%)
Adjective	20 - 35%	Sandy Clay
Slightly	12 - 20%	Slightly Sandy Clay
With some	5 - 12%	Clay with some sand
With a trace of	0 - 5%	Clay with a trace of sand

Definitions of grading terms used are:

- Well graded a good representation of all particle sizes
- Poorly graded an excess or deficiency of particular sizes within the specified range
- Uniformly graded an excess of a particular particle size
- Gap graded a deficiency of a particular particle size with the range

# **Cohesive Soils**

Cohesive soils, such as clays, are classified on the basis of undrained shear strength. The strength may be measured by laboratory testing, or estimated by field tests or engineering examination. The strength terms are defined as follows:

Description	Abbreviation	Undrained shear strength (kPa)
Very soft	VS	<12
Soft	S	12 - 25
Firm	f	25 - 50
Stiff	st	50 - 100
Very stiff	vst	100 - 200
Hard	h	>200

# **Cohesionless Soils**

Cohesionless soils, such as clean sands, are classified on the basis of relative density, generally from the results of standard penetration tests (SPT), cone penetration tests (CPT) or dynamic penetrometers (PSP). The relative density terms are given below:

Relative Density	Abbreviation	SPT N value	CPT qc value (MPa)
Very loose	vl	<4	<2
Loose	1	4 - 10	2 -5
Medium dense	md	10 - 30	5 - 15
Dense	d	30 - 50	15 - 25
Very dense	vd	>50	>25

# Soil Descriptions

# Soil Origin

It is often difficult to accurately determine the origin of a soil. Soils can generally be classified as:

- Residual soil derived from in-situ weathering of the underlying rock;
- Transported soils formed somewhere else and transported by nature to the site; or
- Filling moved by man.

Transported soils may be further subdivided into:

- Alluvium river deposits
- Lacustrine lake deposits
- Aeolian wind deposits
- Littoral beach deposits
- Estuarine tidal river deposits
- Talus scree or coarse colluvium
- Slopewash or Colluvium transported downslope by gravity assisted by water.
   Often includes angular rock fragments and boulders.

# Symbols & Abbreviations

# Introduction

These notes summarise abbreviations commonly used on borehole logs and test pit reports.

# **Drilling or Excavation Methods**

Diamond core - 81 mm dia

С	Core drilling
R	Rotary drilling
SFA	Spiral flight augers
NMLC	Diamond core - 52 mm dia
NQ	Diamond core - 47 mm dia
HQ	Diamond core - 63 mm dia

# Water

PQ

$\triangleright$	Water seep
$\nabla$	Water level

# **Sampling and Testing**

Α	Auger sample
В	Bulk sample
D	Disturbed sample
E	Environmental sample
$U_{50}$	Undisturbed tube sample (50mm)
W	Water sample

pp Pocket penetrometer (kPa)
PID Photo ionisation detector
PL Point load strength Is(50) MPa
S Standard Penetration Test

V Shear vane (kPa)

# **Description of Defects in Rock**

The abbreviated descriptions of the defects should be in the following order: Depth, Type, Orientation, Coating, Shape, Roughness and Other. Drilling and handling breaks are not usually included on the logs.

## **Defect Type**

_0.000	. <b>,</b> , , , ,
В	Bedding plane
Cs	Clay seam
Cv	Cleavage
Cz	Crushed zone
Ds	Decomposed seam

F Fault
J Joint
Lam Lamination
Pt Parting
Sz Sheared Zone

V Vein

### Orientation

The inclination of defects is always measured from the perpendicular to the core axis.

h	horizontal
V	vertical
sh	sub-horizontal
sv	sub-vertical

# **Coating or Infilling Term**

cln	clean
СО	coating
he	healed
inf	infilled
stn	stained
ti	tight
vn	veneer

# **Coating Descriptor**

ca	calcite
cbs	carbonaceous
cly	clay
fe	iron oxide
mn	manganese
slt	siltv

## **Shape**

cu	curved
ir	irregular
pl	planar
st	stepped
un	undulating

# Roughness

ро	polished
ro	rough
sl	slickensided
sm	smooth
vr	verv rough

## Other

fg	fragmented
bnd	band
qtz	quartz

# Symbols & Abbreviations

Talus

Graphic Symbols for Soil and Rock				
General Sedimentary Rocks				
	Asphalt		Boulder conglomerate	
	Road base		Conglomerate	
A. A. A. A.	Concrete		Conglomeratic sandstone	
	Filling		Sandstone	
Soils			Siltstone	
	Topsoil		Laminite	
* * * * :	Peat		Mudstone, claystone, shale	
	Clay		Coal	
	Silty clay		Limestone	
	Sandy clay	Metamorphic	Rocks	
	Gravelly clay	~~~~	Slate, phyllite, schist	
-/-/-/-/- -/-/-/-/-	Shaly clay	- + + + + +	Gneiss	
	Silt		Quartzite	
	Clayey silt	Igneous Roc	ks	
	Sandy silt	+++++++++++++++++++++++++++++++++++++++	Granite	
	Sand	<	Dolerite, basalt, andesite	
	Clayey sand	× × × ; × × × ;	Dacite, epidote	
	Silty sand		Tuff, breccia	
	Gravel		Porphyry	
$\begin{array}{c} \begin{array}{c} \begin{array}{c} \\ \\ \\ \end{array} \\ \begin{array}{c} \\ \\ \\ \end{array} \\ \begin{array}{c} \\ \\ \end{array} \\ \begin{array}{c} \\ \\ \\ \\ \\ \\ \end{array} \\ \begin{array}{c} \\ \\ \\ \\ \\ \\ \end{array} \\ \begin{array}{c} \\ \\ \\ \\ \\ \end{array} \\ \begin{array}{c} \\ \\ \\ \\ \\ \\ \end{array} \\ \begin{array}{c} \\ \\ \\ \\ \\ \end{array} \\ \begin{array}{c} \\ \\ \\ \\ \\ \\ \end{array} \\ \begin{array}{c} \\ \\ \\ \\ \\ \\ \end{array} \\ \begin{array}{c} \\ \\ \\ \\ \\ \\ \end{array} \\ \begin{array}{c} \\ \\ \\ \\ \\ \\ \end{array} \\ \begin{array}{c} \\ \\ \\ \\ \\ \\ \end{array} \\ \begin{array}{c} \\ \\ \\ \\ \\ \\ \end{array} \\ \begin{array}{c} \\ \\ \\ \\ \\ \\ \\ \end{array} \\ \begin{array}{c} \\ \\ \\ \\ \\ \\ \\ \end{array} \\ \begin{array}{c} \\ \\ \\ \\ \\ \\ \\ \end{array} \\ \begin{array}{c} \\ \\ \\ \\ \\ \\ \\ \end{array} \\ \begin{array}{c} \\ \\ \\ \\ \\ \\ \\ \end{array} \\ \begin{array}{c} \\ \\ \\ \\ \\ \\ \\ \end{array} \\ \begin{array}{c} \\ \\ \\ \\ \\ \\ \\ \end{array} \\ \begin{array}{c} \\ \\ \\ \\ \\ \\ \\ \\ \end{array} \\ \begin{array}{c} \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \end{array} \\ \begin{array}{c} \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \end{array} \\ \begin{array}{c} \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\$	Sandy gravel			
	Cobbles, boulders			

# **Rock Strength**

Rock strength is defined by the Point Load Strength Index  $(Is_{(50)})$  and refers to the strength of the rock substance and not the strength of the overall rock mass, which may be considerably weaker due to defects. The test procedure is described by Australian Standard 4133.4.1 - 1993. The terms used to describe rock strength are as follows:

Term	Abbreviation	Point Load Index Is <sub>(50)</sub> MPa	Approx Unconfined Compressive Strength MPa*
Extremely low	EL	<0.03	<0.6
Very low	VL	0.03 - 0.1	0.6 - 2
Low	L	0.1 - 0.3	2 - 6
Medium	M	0.3 - 1.0	6 - 20
High	Н	1 - 3	20 - 60
Very high	VH	3 - 10	60 - 200
Extremely high	EH	>10	>200

<sup>\*</sup> Assumes a ratio of 20:1 for UCS to Is(50)

# **Degree of Weathering**

The degree of weathering of rock is classified as follows:

Term	Abbreviation	Description
Extremely weathered	EW	Rock substance has soil properties, i.e. it can be remoulded and classified as a soil but the texture of the original rock is still evident.
Highly weathered	HW	Limonite staining or bleaching affects whole of rock substance and other signs of decomposition are evident. Porosity and strength may be altered as a result of iron leaching or deposition. Colour and strength of original fresh rock is not recognisable
Moderately weathered	MW	Staining and discolouration of rock substance has taken place
Slightly weathered	SW	Rock substance is slightly discoloured but shows little or no change of strength from fresh rock
Fresh stained	Fs	Rock substance unaffected by weathering but staining visible along defects
Fresh	Fr	No signs of decomposition or staining

# **Degree of Fracturing**

The following classification applies to the spacing of natural fractures in diamond drill cores. It includes bedding plane partings, joints and other defects, but excludes drilling breaks.

Term	Description
Fragmented	Fragments of <20 mm
Highly Fractured	Core lengths of 20-40 mm with some fragments
Fractured	Core lengths of 40-200 mm with some shorter and longer sections
Slightly Fractured	Core lengths of 200-1000 mm with some shorter and loner sections
Unbroken	Core lengths mostly > 1000 mm

# Rock Descriptions

# **Rock Quality Designation**

The quality of the cored rock can be measured using the Rock Quality Designation (RQD) index, defined as:

RQD % = <u>cumulative length of 'sound' core sections ≥ 100 mm long</u> total drilled length of section being assessed

where 'sound' rock is assessed to be rock of low strength or better. The RQD applies only to natural fractures. If the core is broken by drilling or handling (i.e. drilling breaks) then the broken pieces are fitted back together and are not included in the calculation of RQD.

# **Stratification Spacing**

For sedimentary rocks the following terms may be used to describe the spacing of bedding partings:

Term	Separation of Stratification Planes
Thinly laminated	< 6 mm
Laminated	6 mm to 20 mm
Very thinly bedded	20 mm to 60 mm
Thinly bedded	60 mm to 0.2 m
Medium bedded	0.2 m to 0.6 m
Thickly bedded	0.6 m to 2 m
Very thickly bedded	> 2 m

# **Appendix B**

Borehole Logs (3001 to 3007) current investigation Borehole Logs (601 to 606 and 701 to 703) previous investigation Core Photoplates Test Pit Logs (4001 to 4003 and 5001 to 5004) current investigation Test Pit Logs (2001 to 2014) previous investigation

**CLIENT:** Multiplex Constructions Pty Ltd **PROJECT:** Proposed New Maitland Hospital

**LOCATION:** Metford Road, Metford

**SURFACE LEVEL:** 21.4 AHD **EASTING:** 369387

NORTHING: 6374546 DIP/AZIMUTH: 90°/-- **BORE No:** 3001 **PROJECT No:** 81719.09 **DATE:** 13/12/2018

**SHEET** 1 OF 4

	Dareth	Description	Degree of Weathering	.je	Rock Strength	Fracture Spacing	Discontinuities	Sa	mplir	ng &	In Situ Testing
R	Depth (m)	of Strata	Weathering  A A A A S & & & & & & & & & & & & & & &	Graph Log	Strength Nedium   Ex Low   Nedium   High   Ex High   Ex High   Water   Water	(m) (m)	B - Bedding J - Joint S - Shear F - Fault	Туре	Core Rec. %	RQD %	Test Results & Comments
21		SANDSTONE - Extremely low strength, extremely weathered, fine to coarse grained sandstone						D D			Comments
	- - -1	From 0.75m, becomes very low to low strength (auger screech)									
20	1.15	SILTSTONE - Very low strength, highly weathered, grey to pale grey siltstone					1.29m: P, sh, pl, ro 1.32m: J, 80°,un, ro 1.35m: P, sh, un, ro, inf, fe				
	1.78 - 1.83 1.83 -2 2.0 -	SANDSTONE - Medium strength, moderately weathered, fine to medium grained sandstone  SILTSTONE - Very low strength, highly weathered, pale grey siltstone with significant ironstaining	-				1.83m: P, 10°, pl, ro 2m: P, sh, pl, ro, inf, fe	С	100	86	DI (A) = 0.07
10	- - - 2.86- -3	SANDSTONE - Low to medium strength, moderately weathered, fine to medium grained sandstone  LAMINITE - Very low strength, moderately weathered, grey to pale grey fine to medium grained sandstone (70%) and siltstone \(30%) laminite  SANDSTONE - Very low strength, highly weathered, grey fine to medium grained sandstone with significant ironstaining					2.98m: J, 10°, pl, or, inf, fe				PL(A) = 0.07 PL(D) = 0.04 PL(A) = 0.14 PL(D) = 0.05
-118	3.42	SANDSTONE - Low strength, slightly weathered, grey fine to medium grained sandstone with some ironstaining From 3.7m to 4.22m, very low strength						С	100	100	PL(A) = 0.18 PL(D) = 0.23
	-4 -4 -										PL(A) = 0.1 PL(D) = 0.21
	- - -						4.47m: J, 50°, pl, ro 4.84m: J, 45°, pl, ro				

RIG: Explora 140 DRILLER: Groundtest LOGGED: Ma CASING: HW to 1.15m

**TYPE OF BORING:** Solid flight auger drilling with V-bit to 1.15m, then NMLC coring to 18.65m

WATER OBSERVATIONS: No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring

**REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m. Noticeable water loss experienced at 5.7m and again at

	12.911				
	SAMI	PLING	& IN SITU TESTING	LEGI	END
Α	Auger sample	G	Gas sample	PID	Photo ionisation detector (ppm)
В	Bulk sample	Р	Piston sample	PL(A	) Point load axial test Is(50) (MPa)
BLK	Block sample	U,	Tube sample (x mm dia.)	PL(D	) Point load diametral test (\$(50) (MPa)
С	Core drilling	WÎ	Water sample	pp ·	Pocket penetrometer (kPa)
D	Disturbed sample	⊳	Water seep	s	Standard penetration test
E	Environmental sample	Ŧ	Water level	V	Shear vane (kPa)







Proposed New Ma	Douglas Partners Geotechnics   Environment   Groundwater
Metford Street, Me	Geotechnics   Environment   Groundwater
Multipley C	

Core P	hotoplates	PROJECT:	81719.09
Propos	ed New Maitland Hospital	PLATE No:	1
Metford	d Street, Metford	REV:	0
CLIENT:	Multiplex Constructions Pty Ltd	DATE:	Dec 2018

**CLIENT:** Multiplex Constructions Pty Ltd **PROJECT:** Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

**SURFACE LEVEL:** 21.4 AHD **EASTING:** 369387

NORTHING: 6374546 DIP/AZIMUTH: 90°/-- BORE No: 3001 PROJECT No: 81719.09 DATE: 13/12/2018 SHEET 2 OF 4

	<b>.</b>	Description	Degree of Weathering	.je	Rock Strength	Fracture Spacing	Discontinuities				n Situ Testing
묎	Depth (m)	of	Weathering	srapt Loo	Strength Low Nedium High Very High Ex High Water	(m)	B - Bedding J - Joint	Туре	ore c.%	RQD %	Test Results &
		Strata	E E SW E E		Low High Very Very	0.05	S - Shear F - Fault	Ę.	ဝန္	α -	Comments
	-	SANDSTONE - Low strength, slightly weathered, grey fine to medium grained sandstone with some ironstaining <i>(continued)</i>					5.16m: J, 70°, un, ro	С	100	100	PL(A) = 0.15
	- - - -	From 6.0m to 6.6m, with					5.64m: J, 75°, pl, in, fe				PL(D) = 0.24
- 12	- - -	carbonaceous lenses up to 2 mm thick					6.15m: P, 10°, pl, ro				
-	- - -						6.6m: P, sh, pl, ro				PL(A) = 0.12
- 4	- 7 - 7 						7.11m: J, 30°, pl, ro	С	100	97	PL(A) = 0.17 PL(D) = 0.39
	-	From 7.7m, medium to high strength						U			PL(A) = 0.33 UCS = 7.7 MPa
	- 8 - - 8.21 -	SILTSTONE - Very low strength, highly weathered, grey to brown				<b>   </b>	8.08m: J, 20°, pl, ro	С			PL(A) = 1.03 PL(D) = 0.57
-2	-	siltstone				┖╬╎╎╎	From 8.33 to 8.35m, fractured				
-	8.52 8.58 8.58 8.82 8.89	COAL - Very low strength, moderately weathered, black coal CORE LOSS - Probable coal  COAL - Low strength, slightly weathered, black coal  CARBONACEOUS SILTSTONE -					8.47m: P, sh, pl, ro, inf, fe 8.54m: P, sh, pl, ro 8.58m: CORE LOSS: 240mm From 8.82m to 8.89m, fractured 8.91m: J, sv, un, ro				
12	9.25 9.3	Low strength, slightly weathered, black to dark brown carbonaceous slitstone From 9.2m, black coal CLAYSTONE - Low strength,					9.03m: P, sh, pl, ro 9.09m: J, 70°, pl, ro 9.17m: J, 85°, healed (iron and coal infill) 9.27m: J, 80°, un, tight From 9.29m to 9.42m, fractured	С	91	65	
-	-	moderately weathered, brown claystone  COAL - Low strength, slightly weathered, black coal					nactureu				PL(A) = 0.13 PL(D) = 0.14
.	9.91	SILTSTONE - Low strength, moderately weathered, grey to dark grey siltstone	-     <b>         </b>	17							PL(A) = 0.07

RIG: Explora 140 DRILLER: Groundtest LOGGED: Ma CASING: HW to 1.15m

**TYPE OF BORING:** Solid flight auger drilling with V-bit to 1.15m, then NMLC coring to 18.65m

**WATER OBSERVATIONS:** No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring

**REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m. Noticeable water loss experienced at 5.7m and again at 12.9m

SAMPLING & IN SITU TESTING LEGEND

A Auger sample G Gas sample Plid Photo ionisation detector (ppm)
B Bulk sample P Piston sample PL(A) Point load axial test is(50) (MPa)
BLK Block sample U, Tube sample (xmm dia.)
C Core drilling W Water sample PL(D) Point load diametral test is(50) (MPa)
D Disturbed sample P Water seep S S Standard penetration test
E Environmental sample Water level V Shear vane (kPa)



**CLIENT:** Multiplex Constructions Pty Ltd **PROJECT:** Proposed New Maitland Hospital

**LOCATION:** Metford Road, Metford

**SURFACE LEVEL:** 21.4 AHD **EASTING:** 369387

NORTHING: 6374546 DIP/AZIMUTH: 90°/-- BORE No: 3001 PROJECT No: 81719.09 DATE: 13/12/2018 SHEET 3 OF 4

	5 "	Description	Degree of Weathering	Rock 의 Strength	Fracture Spacing	Discontinuities				n Situ Testing
R	Depth (m)	of	Weathering	Graphic Log Ex Low Very Low High Ex Hi	(m)	B - Bedding J - Joint	Type	ore c. %	RQD %	Test Results &
		Strata  CARBONACEOUS SILTSTONE -	W H W W E H	Med High	0.00	S - Shear F - Fault	É.	ပည္	ď	Comments PL(D) = 0.03
11	- - 10.3 - - 10.4 -	Low strength, slightly weathered, brown to black carbonaceous siltstone (continued)  SILTSTONE - Low to medium strength, moderately weathered, grey siltstone  COAL - Low strength, slightly				From 10.42m to 10.51m, fractured	С	91	65	1 2(3) = 0.00
	10.65	Weathered, black coal TUFFACEOUS SILTSTONE - Extremely low to very low strength,			            					PL(A) = 0.22
	10.93 - 11	highly weathered, grey tuffaceous siltstone								1 L(11) - 0.22
-	- 11.1 - - - 11.36 -	COAL - Low strength, slightly weathered, black coal  TUFFACEOUS SILTSTONE - Very low strength, highy weathered,			<b>  </b>   	11.1m: P, sh, pl, ro	С	100	66	PL(A) = 0.07
-10	11.44	tuffaceous siltstone  CARBONACEOUS SILTSTONE -		<u></u>		From 11.44m to 11.51m,				
	- 11.59 - - -	very low strength, slightly weathered, black carbonaceous siltstone From 11.22m to 11.26m, very low strength, highly weathered,				11.55m: J, sv, un, ro 11.59m: CORE LOSS: 1300mm				
	- - 12 -	CLAYSTONE - Low strength, moderately weathered, brown claystone								
- 6	-	COAL - Low strength, slightly weathered, black coal CORE LOSS - Probable coal					С	42	16	
	- 12.89 - - 13 -	COAL / CARBONACEOUS SILTSTONE - Low strength, slightly weathered, black coal / carbonaceous siltstone				From 12.89m to 13.23m, fractured				
- 80	-					From 13.61m to 13.62m, fractured				
-	_ 13.77 - - - 14	SILTSTONE - Very low to low strength, highly weathered, grey siltstone From 14m, slightly weathered								DI (D) = 0.00
	-						С	100	95	PL(D) = 0.08 PL(A) = 0.1 PL(D) = 0.1
-	- - - 15.0	From 14.65m to 14.91m, low strength, slightly weathered, fine to medium grained sandstone					U			PL(A) = 0.25 PL(D) = 0.13 UCS = 5.5 MPa

RIG: Explora 140 DRILLER: Groundtest LOGGED: Ma CASING: HW to 1.15m

**TYPE OF BORING:** Solid flight auger drilling with V-bit to 1.15m, then NMLC coring to 18.65m

**WATER OBSERVATIONS:** No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring

**REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m. Noticeable water loss experienced at 5.7m and again at 12.9m

A Auger sample G G Sas sample Piston sample Piston sample Piston sample PL(A) Point load daxial test Is(50) (MPa) PL(C) Core drilling W Water sample Piston sample Puckation test Sample Puckation tes







	Core Ph	notoplates	PROJECT:	81719.09
Douglas Partners	Propos	ed New Maitland Hospital	PLATE No:	2
Geotechnics   Environment   Groundwater	Metford	Street, Metford	REV:	0
	CLIENT:	Multiplex Constructions Pty Ltd	DATE:	Dec 2018

**CLIENT:** Multiplex Constructions Pty Ltd **PROJECT:** Proposed New Maitland Hospital

**LOCATION:** Metford Road, Metford

**SURFACE LEVEL:** 21.4 AHD **EASTING:** 369387

NORTHING: 6374546 DIP/AZIMUTH: 90°/-- BORE No: 3001 PROJECT No: 81719.09 DATE: 13/12/2018 SHEET 4 OF 4

	D-: "	Description	Degree of Weathering	ا اناد .	Rock Strength	Fracture Spacing	Discontinuities				n Situ Testing
씸	Depth (m)	of		raph	Ex Low Very Low Very Low Medium High Very High Ex High Ex High Water	(m)	B - Bedding J - Joint	Туре	ore S.	RQD %	Test Results &
			W M M M M M M M M M M M M M M M M M M M	<u> </u>	Kery Very Very Very Very Very Very Very V	0.05 0.50 1.00	S - Shear F - Fault	F	S &	8	Comments
9	- - -	SANDSTONE - Low strength, slightly weathered, grey siltstone  From 15.41m to 15.58m, carbonaceous / coal					ղ 15.44m: P, sh, un, ro,	С	100	95	
	- 15.6 - - -	SANDSTONE - Low strength, slightly weathered, grey, fine grained sandstone with bands of siltstone up to 30%					15.47m: P, sh, un, ro, cbs lam				PL(A) = 0.12
- 10	- 16 - - - -										PL(D) = 0.14 PL(A) = 0.16 PL(D) = 0.16
	- - - 17 -	From 16.78m, less than 10% siltstone content						C C	, 100	84	PL(D) = 0.12
- 4	- 17.54 - -	SILTSTONE - Low strength, slightly weathered, grey siltstone									PL(A) = 0.1 PL(D) = 0.12
	- 18 -	From 17.97m to 18.22m, high strength		1   1   1			From 17.98m to 18.2m, fractured 18.08m: J, sv, un, ro				PL(A) = 3.98
-6	- 18.44 - - 18.49	From 18.22m to 18.44m, very low strength, highly weathered  COAL - Low strength, slightly weathered, black coal		- · -			18.36m: P, sh, pl, ro 18.44m: P, sh, pl, ro, inf, coal				
	- 18.65 - - - - 19	SILTSTONE - Very low strength, highly weathered, grey siltstone  Bore discontinued at 18.65m, limit of investigation					18.55m: P, sh, pl, ro, cbs lam				
- 2	-										

RIG: Explora 140 DRILLER: Groundtest LOGGED: Ma CASING: HW to 1.15m

**TYPE OF BORING:** Solid flight auger drilling with V-bit to 1.15m, then NMLC coring to 18.65m

WATER OBSERVATIONS: No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring

**REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m. Noticeable water loss experienced at 5.7m and again at 12.9m

	SAN	IPLING	& IN SITU TESTING		
Α	Auger sample	G	Gas sample	PID	Photo ionisation detector (ppm)
	Bulk sample	Р	Piston sample	PL(A)	Point load axial test Is(50) (MPa)
BLK	Block sample	U,	Tube sample (x mm dia.)	PL(D	Point load diametral test Is(50) (MPa
С	Core drilling	WÎ	Water sample	pp	Pocket penetrometer (kPa)
	Disturbed sample	⊳	Water seep	S	Standard penetration test
E	Environmental sample	Ī	Water level	V	Shear vane (kPa)



**CLIENT:** Multiplex Constructions Pty Ltd PROJECT: Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

**SURFACE LEVEL:** 18.6 AHD **EASTING**: 369307

**NORTHING**: 6374510 **DIP/AZIMUTH:** 90°/--

**BORE No:** 3002 **PROJECT No:** 81719.09 **DATE:** 14/12/2018 SHEET 1 OF 4

П		Description	Degree of Weathering	Rock	Fracture	Discontinuities	Sa	mplir	ng &	In Situ Testing
뮙	Depth (m)	of	Meaniening id	Strength   Fe Low   Cow   Cow	Spacing (m)	B - Bedding J - Joint	e e	% g	۵ .	Test Results
	(111)	Strata	EW HW SW FS FS	LOC Ex Low Low Medium Medium High Very High Ex High	0.05	S - Shear F - Fault	Type	S S	RQD %	& Comments
18	_	FILLING - Generally comprising gravelly fine to coarse grained sand filling with subangular to subrounded gravel up to 50mm, moist From 0.3m, becoming fine to coarse grained sandy clay filling					D			Comment
	- 1						_D			4,9,9
							S			N = 18
11	-2 2.0-	SANDSTONE - Extremely low strength, extremely weathered, yellow fine to coarse grained sadnstone (starts screeching)		X			D			
-1-	2.5 -	SANDSTONE - Low strength, moderately weathered, grey to yellow fine to coarse grained sandstone with ironstaining								PL(D) = 0.1 PL(A) = 0.1 PL(D) = 0.27
15	-3	From 3.22m to 3.75m, very low strength From 3.35m to 3.75m, highly weathered				3.29m: P, sh, pl, ro, inf, fe 3.33m: P, sh, pl, ro, inf, fe	С	100	98	
	3.78 - - -4	From 3.75m to 3.78m, extremely low strength, extremely weathered LAMINITE - Extremely low strength, highly weathered, grey to dark grey, fine to coarse grained condetes (70%), and dilltone.				3.83m: J, sv, un, ro 4.12m: P, sh, pl, ro, inf				
4-	4.74 <b>-</b> 5.0	sandstone (70%) and siltstone (30%) laminite with some ironstaining From 3.89m, very low strength From 4.12m, low strength, slightly weathered From 4.21m, no ironstaining SANDSTONE - Low to medium strength, slightly weathered, grey, fine to coarse grained sandstone				, 5., 5, 10, 111	С	100	98	PL(A) = 0.12 UCS = 3.8 MPa

RIG: Explora 140 **DRILLER:** Groundtest LOGGED: Ma CASING: HW to 2.5m

TYPE OF BORING: Solid flight auger drilling with V-bit 2.5m, then NMLC coring to 19.8m

WATER OBSERVATIONS: No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring REMARKS: Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

**SAMPLING & IN SITU TESTING LEGEND** 

A Auger sample
B Bulk sample
BLK Block sample
C Core drilling
D Disturbed sample
E Environmental sample Gas sample
Piston sample
Tube sample (x mm dia.)
Water sample
Water seep
Water level







N Douglas Partners	Proposed New Maitland H
Douglas Partners  Geotechnics   Environment   Groundwater	Metford Street, Metford
	CLIENT: Multiplex Construction

Core Pl	notoplates	PROJECT:	81719.09
Propos	ed New Maitland Hospital	PLATE No:	3
Metford	Street, Metford	REV:	0
CLIENT:	Multipley Constructions Pty		Dec 2018

**CLIENT:** Multiplex Constructions Pty Ltd **PROJECT:** Proposed New Maitland Hospital

**LOCATION:** Metford Road, Metford

**SURFACE LEVEL:** 18.6 AHD **EASTING:** 369307

NORTHING: 6374510 DIP/AZIMUTH: 90°/-- **BORE No:** 3002 **PROJECT No:** 81719.09

**DATE**: 14/12/2018 **SHEET** 2 OF 4

П		Description	Degree of Weathering	.ie	Rock Strength ់ភូ	Fracture	Discontinuities				n Situ Testing
씸	Depth (m)	of	, vocationing	raph	Strength Medium Medium Medium Fx High Ex High	Spacing (m)	B - Bedding J - Joint	Type	% ie	RQD %	Test Results &
	, ,		EW HW EW SW FR FS	g	Ex Lo Low High Very Very Very Very Very Very Very Very	0.05	S - Shear F - Fault	Ţ	2 8	R <sub>o</sub>	Comments
13	-	SANDSTONE - Low to medium strength, slightly weathered, grey, fine to coarse grained sandstone					5.51m: P, sh, pl, ro 5.59m: P, sh, pl, ro				PL(A) = 0.19
-	- -6										PL(A) = 0.22 PL(D) = 0.29
	-	From 6.25m, ironstaining									PL(A) = 0.18 PL(D) = 0.39
12	- - - - -7							С	100	98	
11	-										PL(A) = 0.11 PL(D) = 0.11
	- - -8 -	From 7.89m to 8.64m, very low strength, moderately weathered					8.09m: J, sv, pl, ro (joint				
	-	From 8.2m to 8.64m, highly weathered					is 0.22m long)				
10	-										
	-9 - -	From 9.22m to 10.87m, medium strength, slightly weathered					9.05m: P, sh, pl, ro, inf, coal 9.31m: J, 70°, pl, ro	С	100	100	PL(A) = 0.12
-6	-						9.5m: J, 70°, pl, ro, healed, (joint is 0.5 m long)				PL(A) = 0.46
-	10.0										PL(D) = 0.69

RIG: Explora 140 DRILLER: Groundtest LOGGED: Ma CASING: HW to 2.5m

TYPE OF BORING: Solid flight auger drilling with V-bit 2.5m, then NMLC coring to 19.8m

**WATER OBSERVATIONS:** No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring **REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

SAMPLING & IN SITU TESTING LEGEND

A Auger sample G Gas sample PID
B Bulk sample P Piston sample PID
BLK Block sample U, Tube sample (x mm dia.) PLC
C Core drilling W Water sample pp
D Disturbed sample D Water seep S
E Environmental sample W Water level V



**CLIENT:** Multiplex Constructions Pty Ltd **PROJECT:** Proposed New Maitland Hospital

**LOCATION:** Metford Road, Metford

**SURFACE LEVEL:** 18.6 AHD **EASTING:** 369307

NORTHING: 6374510 DIP/AZIMUTH: 90°/-- **BORE No:** 3002 **PROJECT No:** 81719.09

**DATE**: 14/12/2018 **SHEET** 3 OF 4

		Description	Degree of Weathering ⊖	Rock Strength	Fracture	Discontinuities				In Situ Testing
귐	Depth (m)	of	Weathering of the control of the con	Ex Low Very Low Nerd High High Ex High String Strin	Spacing (m)	B - Bedding J - Joint	Туре	; %	RQD %	Test Results &
	,	Strata	EW HW SW WH EW	Ex Low Very I Medic Very I Ver	0.05	S - Shear F - Fault	\	ပြည်	R <sub>%</sub>	Comments
	-11	SANDSTONE - Medium strength, slightly weathered, grey, fine to coarse grained sandstone				10.95m: J, 70°, pl	С	100	100	PL(A) = 0.47 PL(D) = 0.55
	11.1	LAMINITE - Very low strength, slightly weathered, grey fine grained sandstone (20%) and siltstone (80%) From 11.3m, moderately weathered				11.32m: P, sh, pl, ro 11.39m: P, sh, pl, ro 11.43m: P, sh, pl, ro 11.46m: J, 20°, un, ro 11.56m: P, sh, pl, ro				PL(D) = 0.03
	11.8 - 12 12.0 - 12.12	COAL - Low strength, fresh, black coal  CORE LOSS - Probable coal  COAL - Low strength, black coal 12.19m to 12.25m, tuffaceous siltstone, extremely low strength,				From 11.8m to 11.87m, fractured  12m: CORE LOSS: 120mm From 12.12m to 12.32m, fractured	С	92	32	
9	12.67	CARBONACEOUS SANDSTONE - Low to medium strength, slightly weathered, dark brown to black				From 12.46m to 12.52m, fractured From 12.57m to 12.67m, fractured 12.78m: J, p, sv, pl, ro				PL(A) = 0.46
	- 13 . 13.15	\text{carbonaceous sandstone} / COAL - Low strength, fresh, black coal}  CORE LOSS - Probable coal				12.9m: P, sh, pl, ro 12.95m: P, sh, pl, ro 13.04m: P, sh, pl, ro 13.09m: J, sv, un, ro 13.15m: CORE LOSS:	С	82	0	
	13.3 13.5 13.63	COAL - Low strength, fresh, black coal  TUFFACEOUS SAND / CLAYSTONE - Low strength, highly weathered, pale to grey tuffaceous sand / claystone  COAL - Low strength, fresh, black coal				150mm  13.35m: P, sh, pl, ro From 13.42m to 13.5m, fractured  13.76m: J, 80°, pl, ro, (joint runs for 0.12m)	С	98	60	PL(A) = 0.1
- 4 -	14.29 14.37 14.38	CLAYSTONE - Very low strength, highly weathered, brown claystone COAL - Low strength, fresh, black coal CORE LOSS - Probable coal				From 14.2m to 14.29m, fractured From 14.37m to 14.38m, fractured 14.38m: CORE LOSS: 520mm From 14.9m to 15.1m,	С	50	0	

RIG: Explora 140 DRILLER: Groundtest LOGGED: Ma CASING: HW to 2.5m

TYPE OF BORING: Solid flight auger drilling with V-bit 2.5m, then NMLC coring to 19.8m

**WATER OBSERVATIONS:** No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring **REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

	SAME	PLING	& IN SITU TESTING	LEGI	END
Α	Auger sample	G	Gas sample		Photo ionisation detector (ppm)
B	Bulk sample	Р.	Piston sample		) Point load axial test Is(50) (MPa)
	Block sample	U <sub>x</sub>	Tube sample (x mm dia.)		) Point load diametral test Is(50) (MPa)
ΙÇ	Core drilling	W	Water sample	pp	Pocket penetrometer (kPa)
ΙĐ	Disturbed sample	⊵	Water seep	S	Standard penetration test
E	Environmental sample	Ŧ	Water level	V	Shear vane (kPa)









Core Pr	notoplates	PROJECT:	81719.09
Propos	ed New Maitland Hospital	PLATE No:	4
Metford	Street, Metford	REV:	0
CLIENT:	Multiplex Constructions Pty Ltd	DATE:	Dec 2018

**CLIENT:** Multiplex Constructions Pty Ltd PROJECT: Proposed New Maitland Hospital

LOCATION: Metford Road, Metford **SURFACE LEVEL: 18.6 AHD EASTING**: 369307

**NORTHING:** 6374510 **DIP/AZIMUTH:** 90°/-- **BORE No: 3002 PROJECT No: 81719.09 DATE:** 14/12/2018 SHEET 4 OF 4

		Description	Degree of Weathering :≧	Rock Strength	Fracture	Discontinuities			<del>.                                      </del>	In Situ Testing
킴	Depth (m)	of	Weathering Did Constitution of the Constitutio	Ex Low Very Low Medium High Very High Ex High Ex High Ex High	Spacing (m)	B - Bedding J - Joint	Туре	; e	RQD %	Test Results &
	,	Strata	MW HW SW SW FR	Ex Lo Medit Medit Medit Medit	0.050	S - Shear F - Fault	\ \frac{1}{2}	2 %	R .	Comments
-	15.2 - 15.3 -	COAL - Low strength, fresh, black coal (continued)  TUFFACEOUS SILTSTONE - Very low to low strength, moderately weathered, grey to pale tuffaceous siltstone				fractured 15.15m: J, sv, un, ro From 15.2m to 15.45m, fractured	С	50	0	PL(A) = 0.68
7	16.2- 16.2- 16.28- 16.64- 16.78-	COAL - Low to medium strength, fresh black coal  From 15.92m to 15.94m, low strength  CORE LOSS - Probable coal  COAL - Low strength, fresh, black coal with trace pyrite  SILTSTONE - Very low strength, highly weathered, dark brown siltstone with interbedded lenses of coal  COAL - Low to medium strength, fresh, black coal  From 16.68m to 16.71m, carbonaceous siltstone, slightly				15.58m: P, sh, pl, ro 15.64m: J, sv, un, ro 15.83m: J, 80°, un, ro From 15.94m to 16.0m, fractured 16m: CORE LOSS: 200mm	С	92	40	PL(A) = 0.12
	17.78 - .18 18.25 - .19 19.0 -	Weathered   SILTSTONE - Low strength, highly   weathered, grey siltstone   SANDSTONE - Low strength, moderately weathered, grey, fine to medium grained sandstone   From 17.5 m, very low strength, highly weathered silt/sandstone   LAMINITE - Low to medium strength, slightly weathered, grey to dark grey, fine to coarse grained sandstone (80%) and siltstone (20%) laminite   SILTSTONE - Very low to low strength, moderately weathered, grey siltstone   CARBONACEOUS SILTSTONE - Very low strength, highly weathered, dark brown   carbonaceous siltstone   CARBONACEOUS SILTSTONE - Very low strength, highly weathered, dark brown   carbonaceous siltstone   CARBONACEOUS SILTSTONE - Very low strength, siltstone   CARBONACEOUS SILTSTONE - Very low strength   CARBONACEOUS SILTSTONE - Very low st				18.69m: J, 40°, un, ro 18.9m: J, sv, un, ro (joints run for 0.18m)	С	100	94	PL(A) = 0.19 PL(D) = 0.19 PL(A) = 0.11 PL(D) = 0.24 UCS = 3.7 Mi PL(A) = 0.11 PL(D) = 0.11
	19.8 -	Venses up to 2mm thick  SILTSTONE - Very low strength, moderately weathered, grey siltstone  Bore discontinued at 19.8m, limit of investigation								PL(A) = 0.0 PL(D) = 0.0

RIG: Explora 140 **DRILLER:** Groundtest LOGGED: Ma CASING: HW to 2.5m

TYPE OF BORING: Solid flight auger drilling with V-bit 2.5m, then NMLC coring to 19.8m

WATER OBSERVATIONS: No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring **REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

**SAMPLING & IN SITU TESTING LEGEND** 

A Auger sample
B Bulk sample
BLK Block sample
C Core drilling
D Disturbed sample
E Environmental sample Gas sample
Piston sample
Tube sample (x mm dia.)
Water sample
Water seep
Water level



**CLIENT:** Multiplex Constructions Pty Ltd PROJECT: Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

**SURFACE LEVEL:** 16.8 AHD **EASTING**: 369299

**NORTHING**: 6374480 **DIP/AZIMUTH:** 90°/--

**BORE No: 3003 PROJECT No: 81719.09** 

**DATE:** 6/12/2018 SHEET 1 OF 5

	Dooth	Description	Degree of Weathering	از _	Rock Strength	Fracture Spacing	Discontinuities				n Situ Testing
R	Depth (m)	of Strata	Degree of Weathering  A A A A S S S E E	Graph Log		0.00 0.10 0.50 0.50 0.50	B - Bedding J - Joint S - Shear F - Fault	Туре	Core Rec. %	RQD %	Test Results & Comments
16 ' ' ' ' 1	- - -	FILLING - Generally comprising brown silty fine to medium grained sand filling with some subangular to subrounded gravel up to 10mm in size, trace clay  CLAY - Stiff to very stiff brown clay with some fine to medium grained sand, trace subangular to subrounded gravel up to 10mm in size, M <wp< td=""><td>                                     </td><td></td><td></td><td></td><td></td><td>D</td><td></td><td></td><td>Comments</td></wp<>						D			Comments
	-1	From 1m, hard, no sand						D S			25/70,-,- refusal
	- 1.11 1.74 	SANDSTONE - Low strength, moderately weathered, grey, fine grained sandstone with 10% interbedded siltstone bands up to 5mm thick  LAMINITE - Low strength, moderately weathered, grey, fine grained sandstone (30%) and siltstone (70%) laminite					1.45m: P, sh, pl, ro, fe	С	100	100	pp >500 PL(A) = 0.15 PL(D) = 0.15 PL(D) = 0.14 UCS = 0.8 MPa
	-			  							PL(A) = 0.14
-14	- - - - - -3	From 2.54m, very low strength SANDSTONE - Medium strength, slightly weathered, grey, fine to coarse grained sandstone					2.4m: P, sh, pl, ro, fe 2.54m: P, sh, pl, ro, fe 2.61m: J, 15°, pl, ro, fe				PL(A) = 0.11 PL(D) = 0.06 PL(A) = 0.51 PL(D) = 0.57
13	-	From 3.3m to 4.38m, low strength						С	100	97	PL(A) = 0.29 PL(D) = 0.21
	- 4   	From 4.38m to 4.47m, carbonaceous, very low strength					3.81m: J, 55°, pl, ro				PL(A) = 0.24 PL(D) = 0.22
12	- - - 5.0										PL(A) = 0.33

RIG: Explora 140 **DRILLER:** Groundtest LOGGED: Ma CASING: HW to 1.05m

TYPE OF BORING: Solid flight auger drilling with V-bit to 1.1m, then NMLC coring to 20.15m

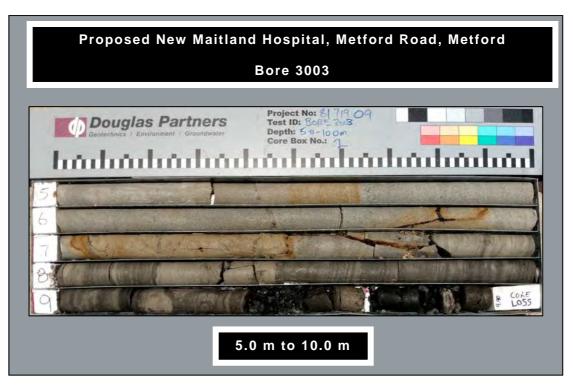
WATER OBSERVATIONS: No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring **REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

**SAMPLING & IN SITU TESTING LEGEND** 

A Auger sample
B Bulk sample
BLK Block sample
C Core drilling
D Disturbed sample
E Environmental sample Gas sample
Piston sample
Tube sample (x mm dia.)
Water sample
Water seep
Water level







	Core Ph	notoplates	PROJECT:	81719.09
<b>Douglas Partners</b>	Propos	ed New Maitland Hospital	PLATE No:	5
Geotechnics   Environment   Groundwater	Metford	Street, Metford	REV:	0
	CLIENT:	Multiplex Constructions Pty Ltd	DATE:	Dec 2018

Multiplex Constructions Pty Ltd **CLIENT:** PROJECT: Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

**SURFACE LEVEL:** 16.8 AHD

**EASTING**: 369299 **NORTHING**: 6374480 **DIP/AZIMUTH:** 90°/-- **PROJECT No:** 81719.09 **DATE:** 6/12/2018

SHEET 2 OF 5

**BORE No:** 3003

	<b>5</b>	Description	Degree of Weathering	Si	Rock Strength	Fracture	Discontinuities	Sa	mplii	ng & l	n Situ Testing
집	Depth (m)	of Strata	Weathering  A A A S S S E	Graph Log	Strength Kery High Kery Hi	Spacing (m) 930 1	B - Bedding J - Joint S - Shear F - Fault	Туре	Core Rec. %	RQD %	Test Results & Comments
		SANDSTONE - Medium strength, fresh, grey, fine to coarse grained sandstone						С	100		PL(D) = 0.37
101	7.5	From 6.7m, low strength  SANDSTONE - Extremely low strength, extremely weathered, grey, fine to coarse grained sandstone (friable, soil like properties)  SANDSTONE - Medium strength, slightly weathered, grey, fine to coarse grained sandstone  From 7.78m low strength, fine to					6.8m: J, 80°, un, ro, tight, fe  7.07m: J, 40°, pl, ro 7.2m: J, 50°, pl, ro, tight 7.26m: J, 50°, pl, ro, tight 7.42m: J, 40°, un, ro 7.48m: P, sh, pl, ro, fe 7.55m: P, sh, pl, ro, fe 7.68m: J, 70°, pl, ro, fe	С	100	77	PL(A) = 0.38 PL(D) = 0.36 PL(A) = 0.25 PL(D) = 0.15 pp = 400 PL(A) = 0.78 PL(D) = 0.42
	-8	From 7.78m, low strength, fine to medium grained  From 8m to 8.22m, fine grained sandstone (50%) and siltstone (50%) laminite					7.8m: J, 70°, pl, ro, fe				PL(A) = 0.2 PL(D) = 0.11
	8.46 ·	SILTSTONE - Low strength, fresh, grey siltstone					8.35m: P, 5°, un, ro 8.4m: J, 80°, un, ro 8.42m: P, 10°, un, ro	С	100	89	PL(A) = 0.13 PL(D) = 0.16
   	9.0	CARBONACEOUS SILTSTONE - Low strength, fresh, dark grey carbonaceous siltstone with 30% interbedded fine grained sandstone  COAL - Low strength, fresh, black coal From 9.52m, tuffaceous siltstone to					From 9.4m to 9.52m, fg 9.56m: P, 5°, un, ro				PL(A) = 0.26 PL(D) = 0.27
	. 9.9-	9.64m From 9.84m to 9.9m, \carbonaceous claystone					From 9.64m to 9.84m, fractured  9.9m: CORE LOSS:	С	50	0	pp = 500

**DRILLER:** Groundtest LOGGED: Ma CASING: HW to 1.05m RIG: Explora 140

TYPE OF BORING: Solid flight auger drilling with V-bit to 1.1m, then NMLC coring to 20.15m

WATER OBSERVATIONS: No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring REMARKS: Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

	SAMI	PLING	& IN SITU TESTING		
Α	Auger sample	G	Gas sample	PID	Photo ionisation detector (ppm)
В	Bulk sample	Р	Piston sample	PL(A	Point load axial test ls(50) (MPa)
BLK	Block sample	U,	Tube sample (x mm dia.)	PL(C	) Point load diametral test (s(50) (MPa)
С	Core drilling	WÎ	Water sample	pp ·	Pocket penetrometer (kPa)
D	Disturbed sample	⊳	Water seep	S	Standard penetration test
E	Environmental sample	Ŧ	Water level	V	Shear vane (kPa)



**CLIENT:** Multiplex Constructions Pty Ltd PROJECT: Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

**SURFACE LEVEL:** 16.8 AHD **EASTING**: 369299

**NORTHING**: 6374480 **DIP/AZIMUTH:** 90°/--

**PROJECT No: 81719.09 DATE:** 6/12/2018 SHEET 3 OF 5

**BORE No: 3003** 

	Donth	Description	Degree of Weathering	Rock Strength	Fracture Spacing	Discontinuities			<del>-</del>	n Situ Testing
귛	Depth (m)	of	Weathering	Graphic Log	(m)	B - Bedding J - Joint S - Shear F - Fault	Туре	c.%	RQD %	Test Results &
		Strata	MW HW EW	Med Very	0.05		-	0 %	α_	Comments
-		CORE LOSS - 250mm (continued)				250mm	С	50	0	
	10.15 · - - - -	COAL - Low strength, fresh, black coal with interbedded carbonaceous mudstone bands up to 100mm thick				From 10.15m to 10.26m, fractured  10.35m: P, sh, pl, ro From 10.35m to 10.63m, fractured	С	100	0	PL(A) = 0.26
	- - - 11	From 10.82m to 10.94m, tuffaceous siltstone				10.68m: P, sh, pl, ro From 10.72m to 10.82m, fractured 10.93m: J, 45°, pl, ro 10.94m: P, sh, pl, ro 10.97m: P, sh, pl, ro 11.05m: J, sv, pl, ro				
2	- - - - - - - - 12	From 11.32m to 11.58m, extremely low strength, extremely weathered, tuffaceous siltstone with carbonaceous bands up to 50mm in thickness From 11.58m to 11.65m, very low strength, interbedded carbonaceous siltstone and tuffaceous siltstone From 11.65m to 11.93m, very low to low strength interbedded carbonaceous siltstone				From 11.15m to 11.22m, fractured 11.25m; J, 75°, pl, ro 11.3m; P, sh, pl, ro 11.8m; P, sh, pl, ro From 11.93m to 12.11m, fragmented	С	100	40	PL(A) = 0.3 PL(D) = 0.04
*	- - - - -13 - -	From 12.75m to 12.82m, very low strength, highly weathered, carbonaceous siltstone From 12.82m to 13.0m, carbonaceous siltstone From 13m to 13.47m, medium strength				12.46m: P, 5°, pl, ro  From 12.75m to 12.86m, fractured 12.9m: J, 45°, pl, ro 12.96m: P, sh, pl, ro From 13m to 13.08m, fractured 13.2m: J, sv, un, ro 13.3m: J, sv, un, ro				PL(A) = 0.2' PL(D) = 0.16
°	- - - - - 14 14.0 - -	From 13.47m to 13.52m, very low strength From 13.52m to 13.91m, low strength, carbonaceous siltstone  From 13.91m to 14m, medium strength  CORE LOSS - 0.2m				From 13.81m to 13.83m, fractured From 13.9m to 14.0m, fractured 14m: CORE LOSS: 200mm	С	83	27	PL(A) = 0.11 PL(D) = 0.05
7	17.2	SANDSTONE - Low strength, slightly weathered, grey, fine grained sandstone with 30% interbedded siltstone					С	100	88	PL(A) = 0.08

RIG: Explora 140 **DRILLER:** Groundtest LOGGED: Ma CASING: HW to 1.05m

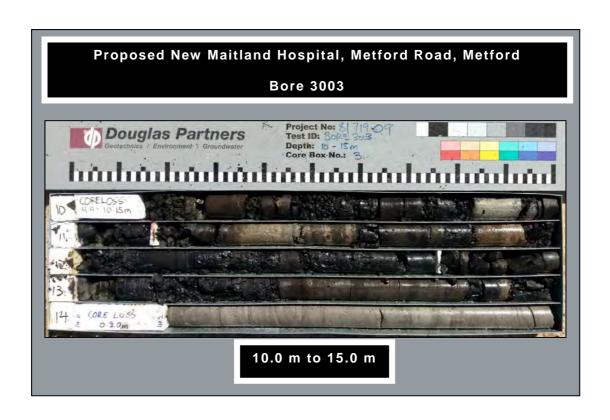
**TYPE OF BORING:** Solid flight auger drilling with V-bit to 1.1m, then NMLC coring to 20.15m

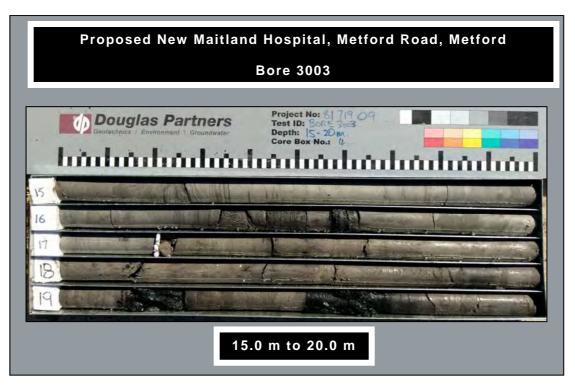
WATER OBSERVATIONS: No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring REMARKS: Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

	SAMPLING	& IN SITU	TESTING	LEGE	END
Auger sample	G	Gas sample		PID	Phot

A Auger sample
B Bulk sample
BLK Block sample
C Core drilling
D Disturbed sample
E Environmental sample Gas sample
Piston sample
Tube sample (x mm dia.)
Water sample
Water seep
Water level P U W







do	Douglas Partners Geotechnics   Environment   Groundwater
	Geotechnics   Environment   Groundwater

Core Pr	otoplates	PROJECT:	81719.09
Propos	ed New Maitland Hospital	PLATE No:	6
Metford	Street, Metford	REV:	0
CLIENT:	Multiplex Constructions Pty Ltd	DATE:	Dec 2018

**CLIENT:** Multiplex Constructions Pty Ltd **PROJECT:** Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

**SURFACE LEVEL:** 16.8 AHD **EASTING:** 369299

NORTHING: 6374480 DIP/AZIMUTH: 90°/-- **PROJECT No:** 81719.09 **DATE:** 6/12/2018 **SHEET** 4 OF 5

**BORE No: 3003** 

		Description	Degree of Weathering	Rock Strength 등	Fracture	Discontinuities				n Situ Testing
R	Depth (m)	of	3	Graphic Graphi	Spacing (m)	B - Bedding J - Joint S - Shear F - Fault	Type	ore sc. %	RQD %	Test Results &
		Strata	W H M S S E E	Media (Service)	0.00	3 - Siledi F - Fault	_	0 %	œ	Comments
-	15.25	SANDSTONE - Low strength, fresh, grey, fine to medium grained sandstone  SILTSTONE - Very low strength,								PL(A) = 0.17
-	- 16 - 16 	moderately weathered, grey siltstone with 10% fine to medium grained sandstone  From 16.84m to 17.2m, low				16.3m: J, 35°, un, ro 16.39m: J, 45°, un, ro 16.43m: P, sh, pl, ro 16.51m: P, sh, pl, ro From 16.56m to 16.63m, fractured	С	100	88	PL(A) = 0.04
	- 17 	From 17.78m to 18m, low strength								PL(A) = 0.16
	- 10	From 18m, highly weathered				18.13m: J, 45°, un, ro 18.55m: P, sh, pl, ro	С	100	68	
-2-	- - - - - - 19.26	From 19.15m to 19.26m, medium strength, fresh, black coal From 19.26m to 19.51m, low strength				From 19.15m to 19.26m, fractured				PL(A) = 0.13 PL(D) = 0.18
- 57	19.51 - 19.65 -	From 19.51m to 19.65m, medium strength, fresh, black coal				\ 19.5m: P, sh, pl, ro From 19.51m to 19.65m, fractured				PL(U) = 0.18

RIG: Explora 140 DRILLER: Groundtest LOGGED: Ma CASING: HW to 1.05m

**TYPE OF BORING:** Solid flight auger drilling with V-bit to 1.1m, then NMLC coring to 20.15m

**WATER OBSERVATIONS:** No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring **REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

_						
Γ		SAMP	LING	& IN SITU TESTING	LEGI	END
		Auger sample	G	Gas sample	PID	Photo ionisation detector (ppm)
		Bulk sample	Р	Piston sample		) Point load axial test Is(50) (MPa)
	BLK	Block sample	U,	Tube sample (x mm dia.)	PL(D	) Point load diametral test Is(50) (MP
Т	С	Core drilling	WÎ	Water sample	pp ·	Pocket penetrometer (kPa)
		Disturbed sample	$\triangleright$	Water seep	S	Standard penetration test
	E	Environmental sample	Ī	Water level	V	Shear vane (kPa)



**CLIENT:** Multiplex Constructions Pty Ltd **PROJECT:** Proposed New Maitland Hospital

**LOCATION:** Metford Road, Metford

SURFACE LEVEL: 16.8 AHD

**EASTING**: 369299 **NORTHING**: 6374480 **DIP/AZIMUTH**: 90°/--

**PROJECT No:** 81719.09 **DATE:** 6/12/2018 **SHEET** 5 OF 5

**BORE No: 3003** 

		Description	De	egre	e of	Graphic		S	Ro	ock ng	th.	_		Frac	ture	е	Discor	ntinuities	Sa	mpli	ng &	In Situ Testing
R	Depth (m)	of		Juli	011119	raph	) ×	آج ادا	1	 	틸	Water		Spad m	1)		B - Bedding	J - Joint	Туре	Core Rec. %	g,	Test Results &
	, ,	Strata	M M	≥ €	§ 82 E	٥	EX Lo	\seconder	٤١٥	E je			0.01	0.05	0.50	1.00	S - Shear	F - Fault	Ę	ပည္တ	χ.	Comments
-	-										 								С	100	68	
-	20.15	Bore discontinued at 20.15m, limit	T.		11					T			Ţ		T	П						
+	-	of investigation	ļ	ij	ij			ij	i	İ			ļ	ij	į	i						
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RIG: Explora 140 DRILLER: Groundtest LOGGED: Ma CASING: HW to 1.05m

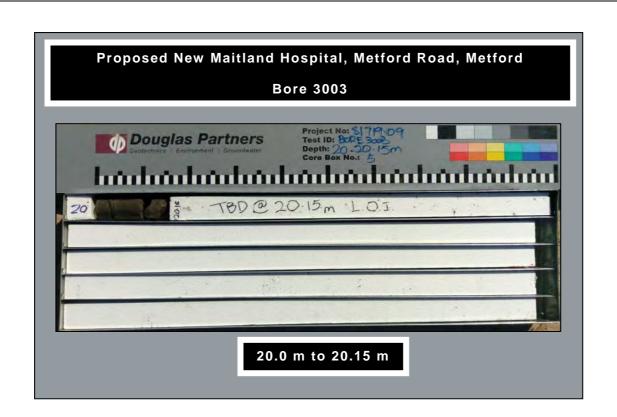
**TYPE OF BORING:** Solid flight auger drilling with V-bit to 1.1m, then NMLC coring to 20.15m

**WATER OBSERVATIONS:** No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring **REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

### SAMPLING & IN SITU TESTING LEGEND

A Auger sample
B Bulk sample
B Bulk Sample
B Bulk Slock sample
C Core drilling
C Core drilling
D Disturbed sample
E Environmental sample
W Water sample
W Water seep
Water level







Core Ph	otoplates	PROJECT:	81719.09
Propose	ed New Maitland Hospital	PLATE No:	7
Metford	Street, Metford	REV:	0
CLIENT:	Multiplex Constructions Pty Ltd	DATE:	Dec 2018

**CLIENT:** Multiplex Constructions Pty Ltd PROJECT: Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

**SURFACE LEVEL: 21.5 AHD EASTING**: 369305

**NORTHING**: 6374546 **DIP/AZIMUTH:** 90°/-- **BORE No: 3004 PROJECT No:** 81719.09 **DATE:** 12/12/2018 SHEET 1 OF 5

		Description	Degree of Weathering	၌	Rock Strength	Fracture	Discontinuities				n Situ Testing
RL	Depth (m)	of	Degree of Weathering	3raph Log	Strength   Strength   Mater	Spacing (m)	B - Bedding J - Joint S - Shear F - Fault	Type	ore c. %	RQD %	Test Results &
		Strata FILLING - Generally comprising	₩ ¥ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩	XX	E KING MEN	0.05	5 - Sriear F - Fauit	<u>⊢</u>	0 %	œ	Comments
21	0.2	gravelly fine to coarse grained sand filling with some clay with subangular to subrounded gravel up to 30mm in size  FILLING - Generally comprising fine to coarse grained sandy clay filling with some subangular to subrounded gravel upto 10mm in size  From 0.6m, trace gravel						D			
-	-1							D			
20	-							S			4,3,4 N = 7
19	- - -2 -										
	- 3 3	From 2.5m, becoming clay filling with some subangular to subrounded gravel and trace fine to coarse grained sand						S			7,5,6 N = 11
18	- - - - - -4							_D_			
17	- 4.2 - - - - - 4.65 -	CLAY - Hard, brown mottled yellow clay, M <wp< td=""><td></td><td></td><td></td><td></td><td></td><td>S</td><td>-</td><td></td><td>pp &gt;400 12,12,15 N = 27</td></wp<>						S	-		pp >400 12,12,15 N = 27
-	- 4.65 - - - 5.0	SANDSTONE - Very low strength, moderately weathered, light grey fine to coarse grained sandstone, some ironstaining, carbonaceous lenses up to 2mm thick						С	100	100	

RIG: Explora 140 **DRILLER:** Groundtest LOGGED: Ma CASING: HW to 4.65m

TYPE OF BORING: Solid flight auger drilling with V-bit to 4.65m, then NMLC coring to 23.3m

WATER OBSERVATIONS: No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring **REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

**SAMPLING & IN SITU TESTING LEGEND** 

A Auger sample
B Bulk sample
BLK Block sample
C Core drilling
D Disturbed sample
E Environmental sample Gas sample
Piston sample
Tube sample (x mm dia.)
Water sample
Water seep
Water level









Core Ph	otoplates	PROJECT:	81719.09
Propose	ed New Maitland Hospital	PLATE No:	8
Metford	Street, Metford	REV:	0
CLIENT:	Multiplex Constructions Pty Ltd	DATE:	Dec 2018

Multiplex Constructions Pty Ltd **CLIENT:** PROJECT: Proposed New Maitland Hospital

LOCATION: Metford Road, Metford **SURFACE LEVEL: 21.5 AHD EASTING**: 369305

**NORTHING:** 6374546 **DIP/AZIMUTH:** 90°/-- **BORE No: 3004 PROJECT No:** 81719.09 **DATE:** 12/12/2018 SHEET 2 OF 5

_		Description	Degree of Weathering	ji _	Rock Strength	Fracture Spacing	Discontinuities				n Situ Testing
	epth m)	of	Weathering	irap! Log	Strength Nedium Nedium Nedium Ex High Ex High Strength St	(m)	B - Bedding J - Joint	Туре	ore 2.%	RQD %	Test Results &
		Strata	EW HW EW FR	g	FIGURE LOW	0.05	S - Shear F - Fault	🖹	S §	, R	Comments
-		SANDSTONE - Very low strength, fresh, light grey fine to coarse grained sandstone with some ironstaining and carbonaceous lenses up to 2mm thick					5.08m: P, sh, pl, ro				PL(A) = 0.06
-		From 5.46m, moderately weathered				┆ <b>╷╷┎┚</b> ┆┆	5.46m: P, sh, pl, ro				
-	5.64 5.66 5.69	From 4.89m to 5.63m, becoming slightly weathered dark grey fine grained sandstone		<b>&gt;</b> <			5.65m: P, sh, pl, ro 5.66m: CORE LOSS: 30mm				
-6		COAL - Low strength, slightly weathered black coal CORE LOSS - Probable coal					O O Free Death and are list	С	100	100	PL(A) = 0.16 PL(D) = 0.11
-		SANDSTONE - Low strength, slightly weathered, grey, fine to coarse grained sandstone with some carbonaceous and coal lenses up to 2mm thick From 6.02m to 6.05m, coal From 6.47m to 6.9m, ironstaining					6.05m: P, sh, pl, ro, inf, coal 6.2m: J, 40°, un, ro				
-7	6.9	SANDSTONE - Very low strength, slightly weathered, grey, fine to									PL(A) = 0.08
_		medium grained sandstone									PL(A) = 0.08 PL(D) = 0.08 PL(D) = 0.07
-8	7.89	From 7.79m to 7.89m, moderately weathered  SANDSTONE - Very low strength, highly weathered, yellow sandstone with lamination of siltstone (30%)					8.06m: J, 80°, pl, ro	U			UCS = 1.6 MP
-								С	100	100	
-9	8.6 -	From 8.56m, low strength, moderately weathered  LAMINITE - Low strength, moderately weathered, grey, fine to coarse grained sandstone (60%) and siltstone (40%)  From 8.69m, slightly weathered					8.5m: P, sh, un, ro				PL(A) = 0.2 PL(D) = 0.13
ŀ								С	100	99	PL(A) = 0.13

RIG: Explora 140 **DRILLER:** Groundtest LOGGED: Ma CASING: HW to 4.65m

TYPE OF BORING: Solid flight auger drilling with V-bit to 4.65m, then NMLC coring to 23.3m

WATER OBSERVATIONS: No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring **REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

	SAMPLING	& IN SITU	<b>TESTING</b>	LEGE	END
Auger sample	G	Gas sample		PID	Phot

A Auger sample
B Bulk sample
BLK Block sample
C Core drilling
D Disturbed sample
E Environmental sample Gas sample
Piston sample
Tube sample (x mm dia.)
Water sample
Water seep
Water level



**CLIENT:** Multiplex Constructions Pty Ltd PROJECT: Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

**SURFACE LEVEL: 21.5 AHD EASTING**: 369305

**NORTHING**: 6374546 **DIP/AZIMUTH:** 90°/-- **BORE No: 3004 PROJECT No:** 81719.09 **DATE:** 12/12/2018 SHEET 3 OF 5

	<b>5</b> "	Description	Degree of Weathering	Si	Rock Strength Spacing	Discontinuities				n Situ Testing
R	Depth (m)	of		Srapt Log	Strength Medium	B - Bedding J - Joint	Type	ore c. %	RQD %	Test Results &
		Strata	WH WE WE AT		Ex LC Very Very Very Very Very Very Very Very	S - Shear F - Fault	<u> </u>	O &	α	Comments
11	- 10.19 <sup>-</sup> - -	At 10.16m, coal band, 1mm thick SANDSTONE - Low strength, slightly weathered, grey fine to coarse grained sandstone				10.37m: J, 45°, un, ro				
	- - - 11 -	From 10.86m to 11.03m, very low strength siltstone laminations								PL(A) = 0.09 PL(D) = 0.08
10	-						С	100	99	PL(A) = 0.14 PL(D) = 0.17
-	- -12 -					12m: J, 80°, pl, ro				
- 6	- - -	From 12.4m, low to medium strength				12.31m: J, sv, un, ro				
-	- - -13 -					13.06m: J, 40°, pl, ro				PL(A) = 0.24 PL(D) = 0.34 PL(A) = 0.22 PL(D) = 0.14
- 8	-					13.5m: J, sv, pl, ro				
	- 14 						С	100	100	
2	- - - - 15.0									PL(A) = 0.42 PL(D) = 0.41

RIG: Explora 140 **DRILLER:** Groundtest LOGGED: Ma CASING: HW to 4.65m

TYPE OF BORING: Solid flight auger drilling with V-bit to 4.65m, then NMLC coring to 23.3m

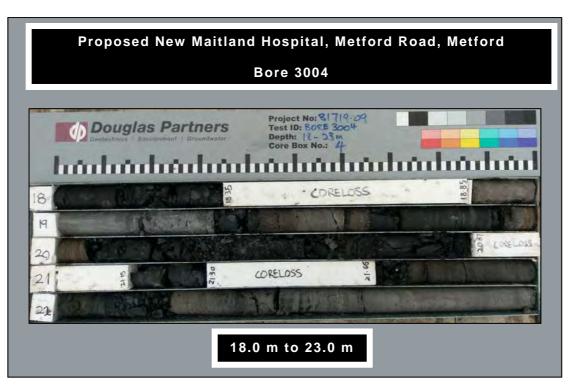
WATER OBSERVATIONS: No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring **REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

**SAMPLING & IN SITU TESTING LEGEND** 

A Auger sample
B Bulk sample
BLK Block sample
C Core drilling
D Disturbed sample
E Environmental sample Gas sample
Piston sample
Tube sample (x mm dia.)
Water sample
Water seep
Water level







	Core Ph	notoplates	PROJECT:	81719.09
Douglas Partners	Propos	ed New Maitland Hospital	PLATE No:	9
Geotechnics   Environment   Groundwater	Metford	Street, Metford	REV:	0
	CLIENT:	Multiplex Constructions Pty Ltd	DATE:	Dec 2018

**CLIENT:** Multiplex Constructions Pty Ltd PROJECT: Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

**SURFACE LEVEL: 21.5 AHD EASTING**: 369305

**NORTHING**: 6374546 **DIP/AZIMUTH:** 90°/-- **BORE No: 3004 PROJECT No:** 81719.09 **DATE:** 12/12/2018

SHEET 4 OF 5

D	Description	Degree of Weathering 은	Rock Strength	Fracture Spacing	Discontinuities			<u> </u>	n Situ Testing
전 (n		Degree of Weathering Section 19 19 19 19 19 19 19 19 19 19 19 19 19	시》이라 나타를 나타를 어느니다.	(m)	B - Bedding J - Joint S - Shear F - Fault	Туре	Core tec. %	RQD %	Test Results &
	SANDSTONE - Low to medium strength, slightly weathered, grey fine to coarse grained sandstone From 15.17m to 15.28m, interbedded bands of carbonaceous sandstone	EW HWW NWW SW SW SW SW SW SW SW SW SW SW SW SW S			15.23m: P, sh, pl, ro	С	100		Comments PL(A) = 0.32 PL(D) = 0.26 PL(A) = 0.13
-16	5.74 SILTSTONE - Low strength, moderately weathered, grey siltstone with 10°-20° bands of fine grained sandstone From 15.9m, with 10% interbedded sandstone laminates		.		15.74m: P, sh, pl, ro				PL(A) = 0.16
1 	SANDSTONE - Low to medium strength, slightly weathered, grey fine to medium grained sandstone				16.36m: J, 70°, pl, ro 16.4m: P, sh, pl, ro 16.5m: P, sh, pl, ro				
1 1	6.73  LAMINITE - Very low strength, slightly weathered, grey fine to medium grained sandstone (50%) and siltstone (50%) laminite								PL(A) = 0.07 PL(D) = 0.05 PL(A) = 0.05 PL(A) = 0.11 PL(D) = 0.06
1	7.18 COAL / CARBONACEOUS SILTSTONE - Low strength, slightly weathered, black coal / carbonaceous siltstone  7.51 SANDSTONE - Low to medium strength, moderately weathered, fine to medium grained sandstone COAL - Low to medium strength, fresh, black coal From 17.7m to 17.91m, carbonaceous siltstone				From 17.22m to 17.35m, fractured  17.47m: P, sh, pl, ro 17.51m: P, sh, pl, ro 17.63m: J, sv, un, ro	С	83	66	
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	From 18m, medium strength  CORE LOSS - Probable coal				18.35m: CORE LOSS: 500mm				PL(A) = 0.36
1 - 19	TUFFACEOUS SILTSTONE - Very low strength, highly weathered, tuffaceous siltstone		-		19.18m: P, sh, pl, ro				
- 27 -	COAL - Low to medium strength, fresh, black coal  CLAYSTONE - Very low strength, highly weathered, brown claystone  From 19.47m, grey siltstone  COAL - Low strength, fresh, black				19.33m: P, sh, pl, ro 19.36m: J, sv, pl, ro	С	87	67	
1	coal 9.94				19.85m: P, sh, pl, ro 19.91m: P, sh, pl, ro				

RIG: Explora 140 **DRILLER:** Groundtest LOGGED: Ma CASING: HW to 4.65m

TYPE OF BORING: Solid flight auger drilling with V-bit to 4.65m, then NMLC coring to 23.3m

WATER OBSERVATIONS: No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring **REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

**SAMPLING & IN SITU TESTING LEGEND** 

A Auger sample
B Bulk sample
BLK Block sample
C Core drilling
D Disturbed sample
E Environmental sample Gas sample
Piston sample
Tube sample (x mm dia.)
Water sample
Water seep
Water level



**CLIENT:** Multiplex Constructions Pty Ltd **PROJECT:** Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

**SURFACE LEVEL:** 21.5 AHD **EASTING:** 369305

NORTHING: 6374546 DIP/AZIMUTH: 90°/-- BORE No: 3004 PROJECT No: 81719.09 DATE: 12/12/2018 SHEET 5 OF 5

	Description	Degree of Weathering	Rock	Fracture	Discontinuities	Sa	ımpliı	ng & I	In Situ Testing
	epth of	Weathering	Graphic Log Log Low Very Low Very Low Very High Very High Ex High Water	Spacing					
L  (n	m) Strata	< > > < % < % < % < % < % < % < % < % <	Gra CLow Service Gelium Gelium CHigh	0.05 0.10 1.00 ( <b>m</b> )	B - Bedding J - Joint S - Shear F - Fault	Туре	Core	RQD %	& Commonto
H-	CLAYSTONE Very low street			0 00 07	<sup>L</sup> 19.93m: P, sh, pl, ro		<u> </u>		Comments
	20.07   moderately weathered, brown claystone (continued)  COAL - Low to medium stren fresh, black coal				From 20.2m to 20.36m, fractured				
					From 20.52m to 20.67m, fractured	С	87	67	
-21	CORE LOSS - Probable coal				From 20.79m to 20.87m, fractured 20.87m: CORE LOSS: 280mm				
-0-	21.3 CORE LOSS - Probable coal	gth,			21.24m: J, sv, pl, ro 21.29m: P, sh, un, ro 21.3m: CORE LOSS: 360mm				
22	COAL - Low strength, fresh, local From 21.73m to 22.1m, very strength, highly weathered, carbonaceous siltstone	1 1 1 1 1			21.72m: P, sh, pl, ro 21.77m: P, 10°, pl, ro 21.85m: P, 10°, pl, ro				PL(A) = 0.05 PL(D) = 0.03
F F	22.25 SANDSTONE - Low strength moderately weathered, grey- fine grained sandstone SILTSTONE - Very low stren moderately weathered, grey siltstone	prown			22.36m: J, 75°, pl, ro 22.48m: J, 70°, pl, ro	С	83	60	PL(A) = 0.12 PL(D) = 0.1
	Bore discontinued at 23.3m,	mit of							
-9-	investigation								

RIG: Explora 140 DRILLER: Groundtest LOGGED: Ma CASING: HW to 4.65m

**TYPE OF BORING:** Solid flight auger drilling with V-bit to 4.65m, then NMLC coring to 23.3m

**WATER OBSERVATIONS:** No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring **REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

	SAME	PLING	& IN SITU TESTING	LEGI	END
Α	Auger sample	G	Gas sample		Photo ionisation detector (ppm)
B	Bulk sample	Р.	Piston sample		) Point load axial test Is(50) (MPa)
	Block sample	U <sub>x</sub>	Tube sample (x mm dia.)		) Point load diametral test Is(50) (MPa)
ΙÇ	Core drilling	W	Water sample	pp	Pocket penetrometer (kPa)
ΙĐ	Disturbed sample	⊵	Water seep	S	Standard penetration test
E	Environmental sample	Ŧ	Water level	V	Shear vane (kPa)







Core Pr	notoplates	PROJECT:	81719.09
Propos	ed New Maitland Hospital	PLATE No:	10
Metford	Street, Metford	REV:	0
CLIENT:	Multiplex Constructions Pty Ltd	DATE:	Dec 2018

**CLIENT:** Multiplex Constructions Pty Ltd PROJECT: Proposed New Maitland Hospital

LOCATION: Metford Road, Metford **SURFACE LEVEL: 16.8 AHD EASTING**: 369256

**NORTHING:** 6374493 **DIP/AZIMUTH:** 90°/-- **BORE No: 3005 PROJECT No:** 81719.09 **DATE:** 10/12/2018 SHEET 1 OF 5

		Description	Degree of Weathering	Rock Strength 등	Fracture	Discontinuities				n Situ Testing
씸	Depth (m)	of		Graphic Log Log Log Log Log Log Log Log Log Log	Spacing (m)	B - Bedding J - Joint	Туре	ore 5. %	RQD %	Test Results &
	` ,	Strata	EW HW SW FS FS	Medii Wedii Very	0.05 0.10 1.00	S - Shear F - Fault	Ту	Cc Red	, B	Comments
	-	FILLING - Generally comprising brown to pale clay with some rootlets					О			
	- 0.3 · - -	SANDY CLAY - Very stiff, brown mottled orange clay with fine to coarse grained sand, M <wp< td=""><td></td><td></td><td></td><td></td><td>D</td><td></td><td></td><td></td></wp<>					D			
-9-	-	From 0.7m, becoming hard (auger screaches)								
	- 0.9 -1 1.0	SANDSTONE - Extremely low			<u> </u>					
	-	strength, extremely weathered, pale grey to yellow fine to coarse grained sandstone								
	-	SANDSTONE - Very low strength, slightly weathered, fine to medium grained sandstone				1.28m: P, sh, pl, ro				PL(A) = 0.07 PL(D) = 0.06
	-	From 1.52m to 2.5m, fresh					0	400	400	
-	-	From 1.63m to 1.7m, low strength					С	100	100	PL(A) = 0.07
15		From 1.78m, becoming low strength		:::::    <b>4</b>		1.77m: P, sh, pl, ro				PL(D) = 0.07
13	3.9 - 4	From 3.0m to 3.78m, moderately weathered  SANDSTONE - Medium strength, fresh, grey, fine to medium grained sandstone with 10% interbedded bands of siltstone				3.6m: P, sh, pl, ro 3.7m: J, 80°, un, ro 3.78m: P, sh, pl, ro	C	100	98	PL(A) = 0.34
	- - - - - - 5,0									

RIG: Explora 140 **DRILLER:** Groundtest LOGGED: Ma CASING: HW to 1.0m

TYPE OF BORING: Solid flight auger drilling with V-bit to 1.0m, then NMLC coring to 20.21m

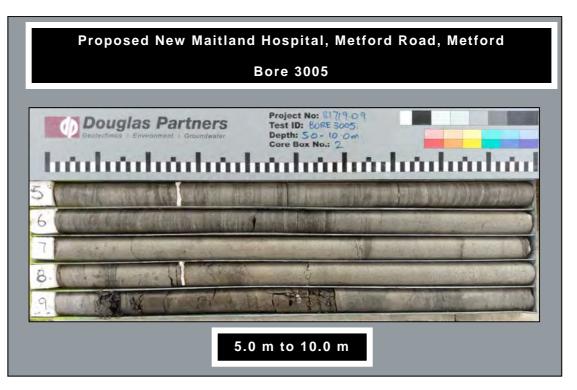
WATER OBSERVATIONS: No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring **REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

**SAMPLING & IN SITU TESTING LEGEND** 

A Auger sample
B Bulk sample
BLK Block sample
C Core drilling
D Disturbed sample
E Environmental sample Gas sample
Piston sample
Tube sample (x mm dia.)
Water sample
Water seep
Water level







do	Douglas Partners Geotechnics   Environment   Groundwater
	Geotechnics   Environment   Groundwater

Core Ph	otoplates	PROJECT:	81719.09
Propose	ed New Maitland Hospital	PLATE No:	11
Metford	Street, Metford	REV:	0
CLIENT:	Multiplex Constructions Pty Ltd	DATE:	Dec 2018

**CLIENT:** Multiplex Constructions Pty Ltd **PROJECT:** Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

SURFACE LEVEL: 16.8 AHD

**EASTING:** 369256 **NORTHING:** 6374493 **DIP/AZIMUTH:** 90°/--

BORE No: 3005 PROJECT No: 81719.09 DATE: 10/12/2018 SHEET 2 OF 5

		Description	Degree of Weathering	. <u>e</u>	Rock Strength	Fracture	Discontinuities	Sa	mplir	ng &	In Situ Testing
뮙	Depth (m)	of	Wedthering	raph	Ex Low Very Low Medium High Very High Kx High Kx High Water	Spacing (m)	B - Bedding J - Joint	Туре	ore S.%	RQD %	Test Results &
Ш			E S S E E		K Kely High Cov		S - Shear F - Fault	<u></u>	ပည် မြောင်	8.	Comments
		LAMINITE - Low strength, fresh, grey, 50% fine grained sandstone, 50% siltstone laminite						С	100	98	
	- 6 							U			PL(A) = 0.2 PL(D) = 0.2 UCS = 1.1 MPa
-	. 6.58						>>				PL(A) = 0.16 PL(D) = 0.1
10		SANDSTONE - Low to medium strength, fresh, grey fine to medium grained sandstone						С	100	100	
	-7										
-6-	- 8 										
- 8	- - - - - - 9								463	00	PL(D) = 0.34 PL(A) = 0.2 PL(D) = 0.26
	- - -	From 9.2m to 9.5m, medium strength, slightly weathered, sandstone with calcite laminations up to 100mm thick					9.18m: P, sh, un, ro, infil From 9.2m to 9.5m, vein, calcite 9.45m: J, 25°, un, ro 9.52m: J, sv, un, ro	С	100	98	PL(D) = 0.55
		From 9.6m to 10.45m, 50% low strength interbedded bands of sandstone up to 50mm thick									PL(A) = 0.19 PL(D) = 0.16

RIG: Explora 140 DRILLER: Groundtest LOGGED: Ma CASING: HW to 1.0m

TYPE OF BORING: Solid flight auger drilling with V-bit to 1.0m, then NMLC coring to 20.21m

**WATER OBSERVATIONS:** No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring **REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

SAMPLING & IN SITU TESTING LEGEND

SAMPLING & IN SITU TESTING LEGEND

A Auger sample Gas sample PID Photo ion
BLK Block sample U<sub>x</sub> Tube sample (x mm dia.)
C C core drilling W Water sample pP PC(D) Point load
D Disturbed sample PW Water seep S Standard
E Environmental sample Water level V Shear var



**CLIENT:** Multiplex Constructions Pty Ltd PROJECT: Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

**SURFACE LEVEL:** 16.8 AHD

**EASTING**: 369256 **NORTHING**: 6374493 **DIP/AZIMUTH:** 90°/-- **BORE No: 3005 PROJECT No: 81719.09 DATE:** 10/12/2018

SHEET 3 OF 5

		Description	Degree of Weathering	U	Rock Strength	Fracture	Discontinuities	Sa	ımpliı	ng &	In Situ Testing
묍	Depth (m)	of	vveaulering	aphi og	Ex Low Very Low Medium High Str High Ex High Ex High Ex High Ex High Water	Spacing (m)	B - Bedding J - Joint	ĕ	% يو	RQD %	Test Results
	(111)	Strata	EW HW SW SH	ق ا	Ex Low Very Livery High High Ex High Ex High O:01	' '	S - Shear F - Fault	Туре	Re o	RO %	& Comments
Н		SANDSTONE - Low to medium		:::::		00 04					Commission
	-	strength, fresh, grey fine to medium grained sandstone <i>(continued)</i>									PL(A) = 0.23 PL(D) = 0.18
											1 L(B) = 0.10
	-				i i <b>l</b> i i i i    i   i i		40 04 1	С	100	98	
+	_						10.64m: J, sv, pl, ro				
- 9	-										
H	- 11					- i i ii l					PL(D) = 0.54
	-										
H	-										
$\mid \cdot \mid$	-										
	-										
-2	-			:::::							
H	-					<u> </u>					
	- 12 -										
H	-										
H	-					ii ii	12.25m: P, sh to 5°, un, ro				
Ħ	-										
H	-					ii ii					PL(A) = 0.47
-4	-						12.76m: P, sh to 5°, un, ro	C	100	100	PL(D) = 0.4
	- 13										
	-					<u> </u>					
$ \cdot $	-										
H	-						13.27m: J, 80°, pl, ro				
}	-										
}	-										
-6											
	- 14										
$ \cdot $	-										
+									<u></u>		PL(A) = 0.66
				:::::							PL(Ď) = 0.6
	14.42	COAL - Medium strength, fresh			▎ ▎┆┆┆		3 14 5m; P sh nl ro				
$ \cdot $	-	SILTSTONE - Low strength,		-			14.5m: P, sh, pl, ro	С	79	49	
	14.72	moderately weathered, grey siltstone with iron bands up to					14.56m: P, sh, pl, ro				
2		20mm thick					14.76m: J, 75°, un, ro				
Ш			Liiii				14.93m: J, 75°, un, ro				

RIG: Explora 140 **DRILLER:** Groundtest LOGGED: Ma CASING: HW to 1.0m

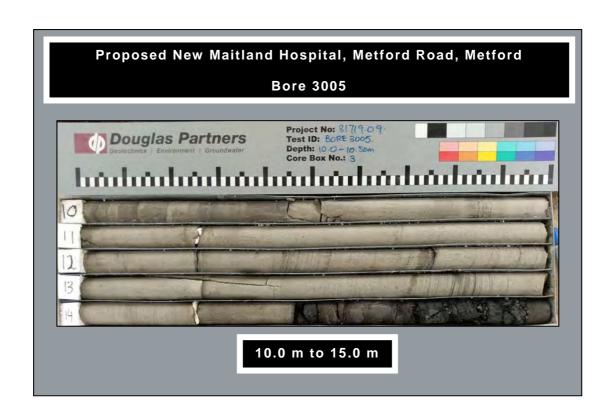
TYPE OF BORING: Solid flight auger drilling with V-bit to 1.0m, then NMLC coring to 20.21m

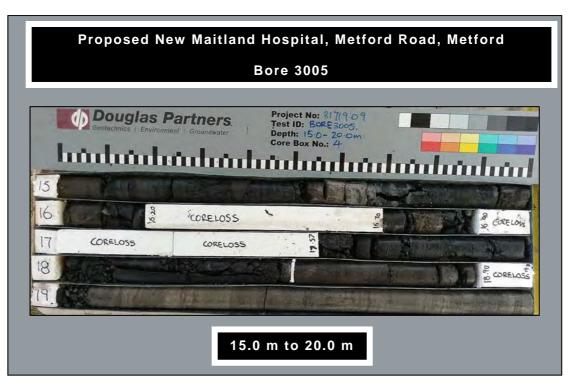
WATER OBSERVATIONS: No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring **REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

**SAMPLING & IN SITU TESTING LEGEND** 

A Auger sample
B Bulk sample
BLK Block sample
C Core drilling
D Disturbed sample
E Environmental sample Gas sample
Piston sample
Tube sample (x mm dia.)
Water sample
Water seep
Water level









Core Ph	notoplates	PROJECT:	81719.09
Propos	ed New Maitland Hospital	PLATE No:	12
Metford	Street, Metford	REV:	0
CLIENT:	Multiplex Constructions Pty Ltd	DATE:	Dec 2018

**CLIENT:** Multiplex Constructions Pty Ltd **PROJECT:** Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

SURFACE LEVEL: 16.8 AHD

**EASTING:** 369256 **NORTHING:** 6374493 **DIP/AZIMUTH:** 90°/--

**BORE No:** 3005 **PROJECT No:** 81719.09

**DATE**: 10/12/2018 **SHEET** 4 OF 5

		Description	Degree of Weathering	Rock Strength 5	Fracture	Discontinuities	Sa	mplii	ng &	n Situ Testing
묍	Depth (m)	of		Graphic Log Ex Low Very High High Water War High Water Make Key High Water War High Water	Spacing (m)	B - Bedding J - Joint	Туре	e	RQD %	Test Results &
	()	Strata	EW HW SW FS	EX Low Low High Light EX Loy Low Low Low Low Low Low Low Low Low Low	` '	S - Shear F - Fault	Ţ	ပြည်	RG %	Comments
		COAL - Low strength, fresh, black coal (continued) From 14.88m to 15.1m, carbonaceous siltstone				15.1m: P, sh, pl, ro 15.37m: J, 40°, un, ro 15.43m: J, 40°, un, ro				PL(A) = 0.16
	15.55 15.69	TUFFACEOUS SILTSTONE - Very low strength, highly weathered, grey tuffaceous siltstone / COAL - Low strength, fresh, black coal / From 15.93m to 16.1m, moderately weathered carbonaceous siltstone				15.95m: P, sh, pl, ro	С	79	49	
	16.2	CORE LOSS - Probable coal				16.15m: J, 80°, un, ro 16.2m: CORE LOSS: 500mm				
-0-	16.7	COAL - Medium strength, fresh, black coal				16.74m: P, sh, pl, ro 16.81m: P, sh, pl, ro				PL(A) = 0.72 PL(D) = 0.14
	16.9	CORE LOSS - Probable coal				From 16.81m to 16.9m, fractured 16.9m: CORE LOSS: 670mm				
	17.57 ·	COAL - Medium strength, fresh, black coal				17.6m: J, 70°, pl, ro 17.68m: P, sh, pl, ro	С	61	28	
						From 18m to 18.1m, fractured				
						18.3m: J, sv, un, ro				
-2		CARBONACEOUS SILTSTONE - Low strength, slightly weathered carbonaceous siltstone				40.00 % 5				
-	18.9 - 19 19.0	CORE LOSS - Probable coal				18.86m: P, sh, un, ro 18.9m: CORE LOSS: 100mm				
	19.05	black coal  SANDSTONE - Low strength, fresh, grey, fine to medium grained sandstone, interbedded siltstone bands up to 30mm thick				From 19.0m to 19.05m, fractured	С	94	79	PL(A) = 0.14 PL(D) = 0.13
ey-										PL(A) = 0.17

RIG: Explora 140 DRILLER: Groundtest LOGGED: Ma CASING: HW to 1.0m

TYPE OF BORING: Solid flight auger drilling with V-bit to 1.0m, then NMLC coring to 20.21m

**WATER OBSERVATIONS:** No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring **REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

	SAME	LINC	& IN SITU TESTING	LEGI	END
A B BL C	Auger sample Bulk sample K Block sample Core drilling	G P U, W	Gas sample Piston sample Tube sample (x mm dia.) Water sample	PID PL(A	Photo ionisation detector (ppm)  ) Point load axial test Is(50) (MPa)  ) Point load diametral test Is(50) (MPa)  Pocket penetrometer (kPa)
D E	Disturbed sample Environmental sample	₽	Water seep Water level	Š	Standard penetration test Shear vane (kPa)



**CLIENT:** Multiplex Constructions Pty Ltd **PROJECT:** Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

SURFACE LEVEL: 16.8 AHD

**EASTING:** 369256 **NORTHING:** 6374493 **DIP/AZIMUTH:** 90°/--

BORE No: 3005 PROJECT No: 81719.09 DATE: 10/12/2018 SHEET 5 OF 5

	<b>.</b>	Description	De We	gree	e of	Graphic		Str Neuv Low	Roc	k gth		<u></u>	Fract	ure	Discor	ntinuities	Sa	mpli	ng &	In Situ Testing
귐	Depth (m)	of			J	raph	8	NO	151	Je Je	ie :	Wate	Spac (m	)	B - Bedding	J - Joint	Туре	ore c. %	RQD %	Test Results &
		Strata	¥ ĕ	₩ %	ω E		M	[6]	Je	A Figh	ĮÄ.			1.00	S - Shear	F - Fault	Ę.	0 %	α -	Comments PL(D) = 0.21
-	-				ij			ij	ij	į	i I						С	94	79	1 L(D) = 0.21
ŀ	20.21	Bore discontinued at 20.21m, limit			<u>     </u>	1::::	:			+	1	-	<u>                                     </u>	11						
[		of investigation		 	 								 							
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RIG: Explora 140 DRILLER: Groundtest LOGGED: Ma CASING: HW to 1.0m

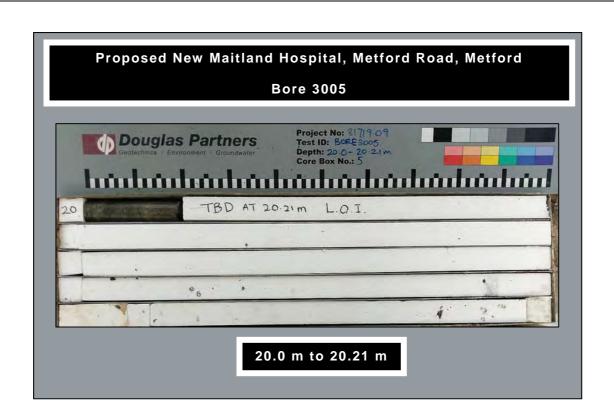
**TYPE OF BORING:** Solid flight auger drilling with V-bit to 1.0m, then NMLC coring to 20.21m

**WATER OBSERVATIONS:** No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring **REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

### **SAMPLING & IN SITU TESTING LEGEND**

A Auger sample
B Bulk sample
B Bulk Sample
B Bulk Slock sample
C Core drilling
C Core drilling
D Disturbed sample
E Environmental sample
W Water sample
W Water seep
Water level







Core Ph	otoplates	PROJECT:	81719.09
Propose	ed New Maitland Hospital	PLATE No:	13
Metford	Street, Metford	REV:	0
CLIENT:	Multiplex Constructions Pty Ltd	DATE:	Dec 2018

**CLIENT:** Multiplex Constructions Pty Ltd PROJECT: Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

**SURFACE LEVEL:** 16.1 AHD **EASTING**: 369295

**NORTHING**: 6374436 **DIP/AZIMUTH:** 90°/-- **BORE No: 3006 PROJECT No: 81719.09 DATE:** 7/12/2018

SHEET 1 OF 5

	D4b	Description	Degree of Weathering		Rock Strength	Fracture Spacing	Discontinuities				n Situ Testing
R	Depth (m)	of Strata	Degree of Weathering	Grapl	Strow Very Low Nedium Medium High Very High Ex High X High Noter High Notes H	(m)	B - Bedding J - Joint S - Shear F - Fault	Туре	Core Rec. %	RQD %	Test Results & Comments
	. 0.5 -	FILLING - Generally comprising brown gravelly silty fine to coarse grained sand with subangular to subrounded gravel up to 20mm in size, moist  CLAYEY SAND - Brown clayey fine to coarse grained clayey sand,						D D			Commente
	- - - -1	\( \text{moist} \) CLAY - Very stiff, brown clay, M <wp 1.0m,="" from="" hard<="" td=""><td></td><td></td><td></td><td></td><td></td><td>D</td><td></td><td></td><td>25/70,-,- refusal</td></wp>						D			25/70,-,- refusal
-12	1.2	SILTSTONE Vary law strangth	11111	/_							Terusar
		SILTSTONE - Very low strength, moderately weathered, grey siltstone with 30% interbedded fine grained sandstone bands up to 30mm thick					1.41m: P, sh, pl, ro, inf, clay  1.7m: P, 5°, pl, ro, fe				PL(A) = 0.05
- 4-	1.82 - - - 2 -	From 1.79m to 1.82m, ironstaining SANDSTONE - Low strength, moderately weathered, grey, fine to coarse grained sandstone From 2m to 6.61m, slightly					1.8m: P, 5°, pl, ro, fe 1.82m: P, 5°, pl, ro, fe	С	100	98	PL(D) = 0.05
	-	weathered						U			UCS = 7.3 MPa
13	3						2.65m: J, 50°, un, ro, inf, carbonaceous 2.75m: J, 50°, un, ro, inf, carbonaceous				PL(A) = 0.13 PL(D) = 0.15
12-	- 4  							С	100	100	PL(A) = 0.13 PL(D) = 0.2
							>>				PL(A) = 0.21 PL(D) = 0.18

RIG: Explora 140 **DRILLER:** Groundtest LOGGED: Ma CASING: HW to 1.2m

TYPE OF BORING: Solid flight auger drilling with V-bit to 1.2m, then NMLC coring to 20.18m

WATER OBSERVATIONS: No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring **REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

**SAMPLING & IN SITU TESTING LEGEND** 

A Auger sample
B Bulk sample
BLK Block sample
C Core drilling
D Disturbed sample
E Environmental sample Gas sample
Piston sample
Tube sample (x mm dia.)
Water sample
Water seep
Water level







	Core Pr	iotoplates	PROJECT:	81719.09
<b>Douglas Partners</b>	Propose	ed New Maitland Hospital	PLATE No:	14
Geotechnics   Environment   Groundwater	Metford	Street, Metford	REV:	0
	CLIENT:	Multiplex Constructions Pty	DATE:	Dec 2018

**CLIENT:** Multiplex Constructions Pty Ltd **PROJECT:** Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

**SURFACE LEVEL:** 16.1 AHD **EASTING:** 369295

**NORTHING:** 6374436 **DIP/AZIMUTH:** 90°/--

**BORE No:** 3006 **PROJECT No:** 81719.09

**DATE:** 7/12/2018 **SHEET** 2 OF 5

		Description	Degree of Weathering	2	Rock Strength	Fracture	Discontinuities				n Situ Testing
R	Depth (m)	of	Degree of Weathering :	Log	Wate	Spacing (m)	B - Bedding J - Joint S - Shear F - Fault	Туре	ore c. %	RQD %	Test Results &
		SANDSTONE - Low strength,	WH W SER	::::		0.00	3 - Shear 1 - Fault	_	28	ır.	Comments
- 11	-	moderately weathered, grey, fine to coarse grained sandstone (continued)				                          		С	100	100	
101	- - - - - - -										PL(A) = 0.21 PL(D) = 0.18 PL(A) = 0.83
-	-	From 6.2m to 6.61m, medium strength					6.14m: J, 85°, pl, ro	С	100	100	PL(D) = 1.17
	- - - -7	From 6.61m, high strength, fresh					6.61m: J, 55°, pl, ro				
-6	- - 7.26	LAMINITE - Low strength,									PL(A) = 1.71 PL(D) = 1.4
	-	moderately weathered, grey, 70% fine grained sandstone and 30% siltstone laminite					7.33m: P, sh, pl, ro 7.4m: P, sh, pl, ro 7.58m: P, sh, un, ro 7.67m: J, 20°, un, ro	С	100	50	
-8	-8 7.98 - - -	COAL - Low strength, fresh, black coal  From 8.27m to 8.44m, becoming					7.98m: P, sh, un, ro 8.06m: P, sh, pl, ro From 8.06m to 8.27m, fractured				PL(A) = 0.1
-	-	carbonaceous siltstone  From 8.58m to 8.83m, low strength, moderately weathered, carbonaceous claystone					\ 8.4m: J, 60°, un, ro 8.42m to 8.57m, fractured				
7	- -9 -	From 9.06m to 9.2m,					8.84m: P, sh, pl, ro 8.92m: P, sh, pl, ro 9.06m: P, sh, pl, ro				PL(A) = 0.22
	9.27	carbonaceous siltstone  TUFFACEOUS SANDSTONE -		::::		i ii <b>d</b> iii	9.27m: P, sh, pl, ro	С	82	39	
	9.42	Very low strength, moderately weathered, fine to coarse grained tuffaceous sandstone with 20% interbedded siltstone bands up to 5mm thick					9.42m: P, sh, pl, ro 9.55m: J, sv, un, ro				PL(D) = 0.06 PL(A) = 0.1 PL(D) = 0.07
-	9.07	COAL - Low strength, fresh, black coal		$\sqrt{}$			9.67m: CORE LOSS: 280mm				
-	9.95	CORE LOSS - 0.28m		_\			_				

RIG: Explora 140 DRILLER: Groundtest LOGGED: Ma CASING: HW to 1.2m

**TYPE OF BORING:** Solid flight auger drilling with V-bit to 1.2m, then NMLC coring to 20.18m

**WATER OBSERVATIONS:** No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring **REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

SAMPLING & IN SITU TESTING LEGEND

A Auger sample G G Gas sample Pl(A) Point load axial test Is(50) (MPa)
BLK Block sample U, Tube sample (x mm dia.)
C Core drilling W Water sample Pl(B) Pl(B) Ploint load diametral test Is(50) (MPa)
D Disturbed sample D Water seep S S Standard penetration test Environmental sample Water level V Shear vane (kPa)



**CLIENT:** Multiplex Constructions Pty Ltd **PROJECT:** Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

**SURFACE LEVEL:** 16.1 AHD **EASTING:** 369295

NORTHING: 6374436 DIP/AZIMUTH: 90°/-- BORE No: 3006 PROJECT No: 81719.09

**DATE**: 7/12/2018 **SHEET** 3 OF 5

	Б "	Description	Degree of Weathering	Rock Strength 5	Fracture Spacing	Discontinuities				In Situ Testing
R	Depth (m)	of Strata	Meathering S	Graphic Craphic Log Ex Low Medium Medium Very High Kx High Kx High Xer High	(m) (m)	B - Bedding J - Joint S - Shear F - Fault	Type	Core Rec. %	RQD %	Test Results & Comments
- 9 -	10.25	TUFFACEOUS SILTSTONE - Low strength, highly weathered grey tuffaceous siltstone (continued)  COAL - Low strength, fresh, black coal  From 10.43m to 10.49m, very low strength, highly weathered tuffaceous claystone  CORE LOSS - 0.29m  CARBONACEOUS SILTSTONE -				9.98m: P, sh, pl, ro 10.2m: P, sh, pl, ro 10.22m: P, sh, pl, ro 10.27m: J, sv, un, ro 10.36m: J, 80°, un, healed 10.41m: P, sh,un, ro From 10.48m to 10.54m, fractured 10.54m: CORE LOSS: 290mm	С	72	30	PL(A) = 0.1
	- -11 11.0- - - - - 11.44-	Low strength, fresh, dark grey to black carbonaceous siltstone  CORE LOSS - 0.44m  COAL - Medium strength, fresh, black coal				10.88m: P, sh, un, ro 11m: CORE LOSS: 440mm  From 11.44m to 11.74m, fractured				
- 4 -	- - - - - - - - - - - - - - - - - - -	From 12.26m to 12.62m, low strength, moderately weathered carbonaceous siltstone  SILTSTONE - Low strength, highly				11.79m: P, sh, ro, un 11.81m: P, sh, ro, un 11.83m: J, sv, ro, un 11.89m: J, 40°, un, ro 12m: J, 80°, pl, ro 12.2m: P, sh, pl, ro 12.4m: P, sh, pl, ro 12.55m: J, 10°-30°, pl, ro 12.63m: P, 5°, pl, ro 12.67m: P, 5°, pl, ro	С	76	25	PL(A) = 0.11
2	12.92 - 13 - 13 - 13 - 13 - 13 - 13 - 13 - 1	weathered siltstone with 20% fine grained sandstone  LAMINITE - Low strength, slightly weathered, grey, fine grained sandstone (70%) and siltstone (30%)				12.83m: P, sh, pl, ro 12.91m: P, sh, pl, ro	С	100	61	PL(A) = 0.16 PL(D) = 0.17
	-					14.67m: P, sh, pl, ro	С	100	93	

RIG: Explora 140 DRILLER: Groundtest LOGGED: Ma CASING: HW to 1.2m

**TYPE OF BORING:** Solid flight auger drilling with V-bit to 1.2m, then NMLC coring to 20.18m

**WATER OBSERVATIONS:** No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring **REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

		SAMPLING	& IN SITU TE	STING LEGE	ND
Α	Auger sample	G	Gas sample	PID	Photo ior

A Auger sample
B Bulk sample
C Core drilling
D Disturbed sample
E Environmental sample

G Gas sample
U₁ Tube sample (x mm
W Water sample
V Water seep
Water level

Gas sample
Piston sample
Puston sample
Puston sample
Puston sample
Tube sample (x mm dia.)
Water sample
Water seep
Water level
Pipton Photo ionisation detector (ppm)
PL(A) Point load axial test Is(50) (MPa)
PL(D) Point load diametral test Is(50) (MPa)
PL(D) Point load diametral test Is(50) (MPa)
PD
Pocket penetrometer (kPa)
Standard penetration test
V Shear vane (kPa)









Core Ph	otoplates	PROJECT:	81719.09
Propose	ed New Maitland Hospital	PLATE No:	15
Metford	Street, Metford	REV:	0
CLIENT:	Multiplex Constructions Pty Ltd	DATE:	Dec 2018

**CLIENT:** Multiplex Constructions Pty Ltd **PROJECT:** Proposed New Maitland Hospital

**LOCATION:** Metford Road, Metford

**SURFACE LEVEL:** 16.1 AHD **EASTING:** 369295

NORTHING: 6374436 DIP/AZIMUTH: 90°/-- **PROJECT No:** 81719.09 **DATE:** 7/12/2018 **SHEET** 4 OF 5

**BORE No: 3006** 

		Description	Degree of Weathering	<u>.0</u>	Rock Strength	Fracture	Discontinuities	Sa	mplir	ng & I	n Situ Testing
귐	Depth (m)	of		raph	Strength Nedlum   Ned	Spacing (m)	B - Bedding J - Joint	Type	Sre	RQD %	Test Results &
		Strata	EW HW SW RE	Ō	Ex Lo Low Medic High Very Ex High	0.05	S - Shear F - Fault	Ţ	လို့ လို့	RO %	Comments
	15.31 - - 16	LAMINITE - Low strength, slightly weathered, grey, fine grained sandstone (70%) and siltstone (30%) (continued) From 15.12m, low strength, moderately weathered, 50% sandstone and 50% siltstone From 15.15m to 15.18m, coal SILTSTONE - Very low to low strength, slightly weathered, grey siltstone with 10% interbedded fine grained sandstone bands					15.93m: P, sh, un, ro	С	100		PL(A) = 0.07 PL(D) = 0.07
} }		From 17.19m, very low strength					17.19m: J, 20°, pl, ro				
	17.29 17.3	SILTSTONE - Medium to high strength, slightly weathered, grey siltstone (possibly sideritic) CORE LOSS - 0.38m					17.3m: CORE LOSS: 380mm				
	17.68 - 17.81 -	SILTSTONE - Medium to high strength, slightly weathered, grey siltstone (possibly sideritic)  SILTSTONE - Very low strength,					17.83m: J, 30°, un, healed				
-7-	- 18	moderately weathered, grey siltstone		· _ ·				С	78	36	
	18.33	COAL - Low strength, fresh, black coal From 18.41m, becomes very low					∖ 18.41m: J, 30°, un, ro √18.44m: J, 30°, un, ro				PL(A) = 0.04
	18.64	strength, moderately weathered carbonaceous SILTSTONE - Very low to low		— ·			18.53m: J, 5°, un, ro				-(-), 0.01
	-19	strength grey siltstone					18.91m: J, 45°, un, ro				PL(A) = 0.1 PL(D) = 0.05
<u>-</u> ကု-							19.13m: P, sh, un, ro				PL(A) = 0.15 PL(D) = 0.17
	19.38 -	From 19.3m, low strength, fresh, \coal \( \) SANDSTONE - Low strength, fresh, fine to coarse grained grey sandstone	-     <del>                                 </del>					С	100	81	
		From 19.72m, medium strength					19.73m: J, 30°, pl, ro				

RIG: Explora 140 DRILLER: Groundtest LOGGED: Ma CASING: HW to 1.2m

**TYPE OF BORING:** Solid flight auger drilling with V-bit to 1.2m, then NMLC coring to 20.18m

**WATER OBSERVATIONS:** No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring **REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

SAMPLING & IN SITU TESTING LEGEND

A Auger sample G G as sample P Piston sample PL(A) Point load axial test Is(50) (MPa)
BLK Block sample U, Tube sample (x mm dia.)
C Core drilling W Water sample
D Disturbed sample D Water seep S Standard penetration test Is(50) (MPa)
E Environmental sample \$ Water level V Shear vane (kPa)



**CLIENT:** Multiplex Constructions Pty Ltd **PROJECT:** Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

**SURFACE LEVEL:** 16.1 AHD **EASTING:** 369295

NORTHING: 6374436 DIP/AZIMUTH: 90°/-- **BORE No:** 3006 **PROJECT No:** 81719.09

DATE: 7/12/2018 SHEET 5 OF 5

П		Description	D	egr	ee (	of na	Graphic		S	Ro	ck ngt	th.		ı	racti	ure	Discon				In Situ Testing	
씸	Depth (m)	of	'	out		9	raph	2 3	ادًا	1		틸	Water	,	Spaci (m)	)	B - Bedding	J - Joint	Туре	e	RQD %	Test Results &
	. ,	Strata	M S	≧ ≧	S S	E E	G	EX	el	٩١٤	High		<u> </u>	0.01	0.05	0.50	S - Shear	F - Fault	Ļ	2 %	R,	Comments
-4	-																		С	100	81	PL(A) = 0.4 PL(D) = 0.44
+ +	. 20.18	Bore discontinued at 20.18m, limit	$\Box$	+	<del>   </del> 	<del>  </del> 			$\frac{\square}{\square}$	7	<del> </del>	<del>   </del> 		-	<del>-  - -</del>	++-						PL(D) = 0.44
	-	of investigation												1								
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RIG: Explora 140 DRILLER: Groundtest LOGGED: Ma CASING: HW to 1.2m

**TYPE OF BORING:** Solid flight auger drilling with V-bit to 1.2m, then NMLC coring to 20.18m

**WATER OBSERVATIONS:** No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring **REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

SAMPLING & IN SITU TESTING LEGEND

A Auger sample
B Bulk sample
B Bulk Sample
B Bulk Slock sample
C Core drilling
C Core drilling
D Disturbed sample
E Environmental sample
W Water sample
W Water seep
Water level







Core Ph	otoplates	PROJECT:	81719.09
Propose	ed New Maitland Hospital	PLATE No:	16
Metford	Street, Metford	REV:	0
CLIENT:	Multiplex Constructions Pty Ltd	DATE:	Dec 2018

**CLIENT:** Multiplex Constructions Pty Ltd PROJECT: Proposed New Maitland Hospital

LOCATION: Metford Road, Metford **SURFACE LEVEL: 19.2 AHD** 

**EASTING**: 369226 **NORTHING**: 6374549 **DIP/AZIMUTH:** 90°/-- **BORE No: 3007 PROJECT No:** 81719.09 **DATE:** 12/12/2018 SHEET 1 OF 5

		Description	Degree of Weathering	Rock Strength 등	Fracture	Discontinuities	Sampling & In Situ Testing		-	
RL	Depth (m)	of		Graphic Log Ex Low Very Low Medium High Ex Hig	Spacing (m)	B - Bedding J - Joint	Туре	Core Rec. %	۵ %	Test Results &
			M M M M M M M M M M M M M M M M M M M	Kery High	0.00	S - Shear F - Fault		2 g	α .	Comments
19 1	0.2	FILLING - Generally comprising gravelly sand filling with subangular to subrounded gravel up to 20mm in size  FILLING - Generally comprising fine to coarse grained sandy clay filling with trace subangular to subrounded gravel up to 5mm in size					D			
	-1						D			
18	-						S			12,10,14 N = 24
17	- - - - 2.1	SANDSTONE - Extremely low strength, extremely weathered, fine to coarse grained sandstone					D			
	- 2.5 · - -	SANDSTONE - Low strength, moderately weathered, fine to coarse grained grey with ironstaining sandstone				2.59m: J, 30°, un, ro				PL(A) = 0.2 PL(D) = 0.16
-	- -3	From 2.9m to 2.98m, very low strength				2.85m: J, 40°, un, ro 2.88m: J, 20°, pl, ro				
16	-	From 3.14m to 3.39m, very low strength, grey			<del>                                  </del>	3.14m: J, 30°, un, ro				
	-	From 3.49m to 5.06m with some subangular to subrounded gravel up to 5mm in size					С	100	90	PL(A) = 0.12 PL(D) = 0.14
15 , 15	-4	From 4.35m to 5.06m, medium strength				4.53m: J, 30°, pl, ro				PL(A) = 0.4 PL(D) = 0.33
-	- - - 5.0									PL(A) = 0.43 PL(D) = 0.45

RIG: Explora 140 **DRILLER:** Groundtest LOGGED: Ma CASING: HW to 2.5m

TYPE OF BORING: Solid flight auger drilling with V-bit to 2.2m, then NMLC coring to 20.35m

WATER OBSERVATIONS: No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring REMARKS: Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

**SAMPLING & IN SITU TESTING LEGEND** 

A Auger sample
B Bulk sample
BLK Block sample
C Core drilling
D Disturbed sample
E Environmental sample Gas sample
Piston sample
Tube sample (x mm dia.)
Water sample
Water seep
Water level



**CLIENT:** Multiplex Constructions Pty Ltd **PROJECT:** Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

**SURFACE LEVEL**: 19.2 AHD **EASTING**: 369226

NORTHING: 369226 NORTHING: 6374549 DIP/AZIMUTH: 90°/-- BORE No: 3007 PROJECT No: 81719.09 DATE: 12/12/2018 SHEET 2 OF 5

		Description	Degree of Weathering	Rock 은 Strength	Fracture	Discontinuities	Sampling & In Situ To Rest Results of Sampling & Communication of Sampling &			
씸	Depth (m)	of	Weathering	Graphic Log Ex Low Very Low High Water High Ex High Water 10.01	Spacing (m)	B - Bedding J - Joint	Туре		۵ %	Test Results &
	, ,	Strata	EW HW SW SW FR	Ex Low Low High High Ex High Ex Low Low Low Low Low Low Low Low Low Low	0.05 0.10 1.00	S - Shear F - Fault	Ļ	ပြည်	X	Comments
- 4-	-	SANDSTONE - Medium strength, moderately weathered, fine to coarse grained grey with ironstaining sandstone From 5.14m, very low strength From 5.14m to 5.21m, highly weathered				5.07m: P, 5°-10°, pl, ro 5.16m: P, sh, pl, ro 5.26m: P, 10°, pl, ro 5.3m: J, 25°, pl, ro	С	100		
13		COAL - Very low strength, moderately weathered, black coal / Carbonaceous siltstone / CARBONACEOUS CLAYSTONE - Very low strength, highly weathered, brown carbonaceous claystone / SILTSTONE - Very low strength, highly weathered, grey siltstone /				5.87m: J, 10°, un, ro				PL(A) = 0.04 PL(D) = 0.03
12 - 1	7 7.8 - 7.96	moderately weathered, fine to medium grained grey sandstone				7.24m: J, 70°, un, ro 7.4m: J, 30°, un, ro	С	100	90	PL(A) = 0.02 PL(A) = 0.05 PL(D) = 0.06
- - - -	-	with siltstone laminations up to 50%  SILTSTONE - Very low strength, highly weathered, grey siltstone with some ironstaining				8.35m: J, 40°, pl, ro 8.5m: J, 30°, pl, ro 8.65m: P, sh, un, ro				PL(A) = 0.08 PL(D) = 0.06
- 10	-9 -	COAL - Very low strength, highly weathered black coal CORE LOSS - Probable coal SANDSTONE - Low strength, slightly weathered, fine to medium grained sandstone				8.74m: J, 20°, un, ro 8.78m: CORE LOSS: 50mm	С	98	97	PL(A) = 0.19 PL(D) = 0.17

RIG: Explora 140 DRILLER: Groundtest LOGGED: Ma CASING: HW to 2.5m

**TYPE OF BORING:** Solid flight auger drilling with V-bit to 2.2m, then NMLC coring to 20.35m

**WATER OBSERVATIONS:** No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring **REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

SAMPLING & IN SITU TESTING LEGEND

A Auger sample G Gas sample PID Photo ionisation detector (pp
B Bulk sample P Piston sample PL(A) Point load axial test Is(50) (M
B B B lock sample U U Tube sample (x mm dia ) Pl (D) Point load diamel test Is(5)

A Auger sample
B Bulk sample
B Bulk Sample
B Bulk Slock sample
C Core drilling
C Core drilling
D Disturbed sample
E Environmental sample
W Water sample
W Water seep
Water level









Core Pr	notoplates	PROJECT:	81719.09
Propos	ed New Maitland Hospital	PLATE No:	17
Metford	Street, Metford	REV:	0
CLIENT:	Multiplex Constructions Pty Ltd	DATE:	Dec 2018

**CLIENT:** Multiplex Constructions Pty Ltd **PROJECT:** Proposed New Maitland Hospital

**LOCATION:** Metford Road, Metford

**SURFACE LEVEL:** 19.2 AHD **EASTING:** 369226

NORTHING: 6374549 DIP/AZIMUTH: 90°/-- BORE No: 3007 PROJECT No: 81719.09 DATE: 12/12/2018 SHEET 3 OF 5

П		Description	Degree of Weathering	္ဍ	Rock Strength	Fracture	Discontinuities				n Situ Testing
R	Depth (m)	of		3rapt Log	Strength Nedium High Kery	Spacing (m)	B - Bedding J - Joint S - Shear F - Fault	Type	ore c. %	RQD %	Test Results &
		Strata	WH WE WE WE		Kary High Kery Kery Kery Kery Kery Kery Kery Kery	0.00	S - Shear F - Fault	-	O &	ď	Comments
- 6	10.22	LAMINITE - Low strength, slightly weathered, fine grained sandstone (50%) and siltstone (50%) laminite  SANDSTONE - Medium strength, slightly weathered, fine to medium grained sandstone					>>	С	98	97	PL(A) = 0.31 PL(D) = 0.39
- 8	- 11 - - - - -	From 11.47m, high to very strength									PL(A) = 0.29
7	- - - 12 -										PL(D) = 4.3 PL(D) = 4.52
	- 12.46 · -	LAMINITE - Medium strength, slightly weathered, grey laminite, fine grained sandstone (70%) and siltstone (30%)	-				12.28m: J, 50°, pl, ro	С	100	100	PL(A) = 0.36 PL(D) = 0.36
-9	- 13 - 13 	From 13.3m, low strength									PL(A) = 0.53 PL(D) = 0.48
- 2	-						14.3m: P, sh, un, ro				PL(A) = 0.18 PL(D) = 0.15
	- - 15.0						14.7m: P, sh, po, ro	С	100	100	PL(A) = 0.29 PL(D) = 0.28 PL(A) = 0.25 PL(D) = 0.23

RIG: Explora 140 DRILLER: Groundtest LOGGED: Ma CASING: HW to 2.5m

**TYPE OF BORING:** Solid flight auger drilling with V-bit to 2.2m, then NMLC coring to 20.35m

**WATER OBSERVATIONS:** No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring **REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

SAMPLING & IN SITU TESTING LEGEND

A Auger sample
B Bulk sample
B Bulk Sample
B Bulk Slock sample
C Core drilling
C Core drilling
D Disturbed sample
E Environmental sample
W Water sample
W Water seep
Water level



**CLIENT:** Multiplex Constructions Pty Ltd PROJECT: Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

**SURFACE LEVEL:** 19.2 AHD **EASTING**: 369226

**NORTHING**: 6374549 **DIP/AZIMUTH:** 90°/-- **BORE No: 3007 PROJECT No:** 81719.09 **DATE:** 12/12/2018 SHEET 4 OF 5

		Description	Degree of Weathering	Rock	Fracture	Discontinuities	Sa	mplir	ng & I	n Situ Testing
귐	Depth (m)	of	vveauleiling :	Extrow Strength Medium High Ex	Spacing (m)	B - Bedding J - Joint	ě	e %	۾ ا	Test Results
	(111)	Strata	HW HW SW SW FS edian LCOW LCOW LCOW LCOW LCOW LCOW LCOW LCOW		S - Shear F - Fault	Туре	S S	RQD %	& Comments	
-4-		LAMINITE - Low strength, slightly weathered, grey laminite, fine grained sandstone (70%) and siltstone (30%)								PL(A) = 0.2 PL(D) = 0.19
- · · ·	15.66 -	SANDSTONE - Low to medium strength, fine to medium grained sandstone with some interbedded siltstone layers up to 3mm thick				16.4m: P, sh, po, ro	С	100	100	PL(A) = 0.66 PL(D) = 0.71 PL(A) = 0.28 PL(D) = 0.03
-0-1	17	From 16.59m to 16.94m, medium to high strength								PL(A) = 0.24 PL(D) = 0.22 PL(A) = 0.73 PL(D) = 0.36
	- 18 - 18 -					18.05m: J, sv, un, ro (runs for 0.15m) 18.4m: P, 30°, pl, ro				PL(A) = 0.28
						18.6m: J, 75°, pl, ro				PL(A) = 0.37
-0-	-19 - - - - -	From 19.11m to 19.40m, carbonaceous sandstone / coal laminates up to 2mm thick				19.32m: P, sh, un, ro 19.36m: J, 80°, pl, ro				PL(D) = 0.32
		From 19.8m to 20.17m, carbonaceous sandstone / coal								PL(A) = 0.71 PL(D) = 0.61

RIG: Explora 140 **DRILLER:** Groundtest LOGGED: Ma CASING: HW to 2.5m

TYPE OF BORING: Solid flight auger drilling with V-bit to 2.2m, then NMLC coring to 20.35m

WATER OBSERVATIONS: No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring REMARKS: Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

**SAMPLING & IN SITU TESTING LEGEND** 

A Auger sample
B Bulk sample
BLK Block sample
C Core drilling
D Disturbed sample
E Environmental sample Gas sample
Piston sample
Tube sample (x mm dia.)
Water sample
Water seep
Water level









Core Ph	notoplates	PROJECT:	81719.09
Propos	ed New Maitland Hospital	PLATE No:	18
Metford	Street, Metford	REV:	0
CLIENT:	Multiplex Constructions Pty	DATE:	Dec 2018

**CLIENT:** Multiplex Constructions Pty Ltd **PROJECT:** Proposed New Maitland Hospital

**LOCATION:** Metford Road, Metford

SURFACE LEVEL: 19.2 AHD

**EASTING:** 369226 **NORTHING:** 6374549 **DIP/AZIMUTH:** 90°/--

BORE No: 3007 PROJECT No: 81719.09 DATE: 12/12/2018 SHEET 5 OF 5

		Description	Degree of Weatherin	of na .≌		R	ock engtl	n	_	Fracture	Discon	tinuities				n Situ Testing
씸	Depth (m)	of		sraph	Fog §	Stro Neuv Low Low Neuv Low	<u> </u>     <u> </u>	High	Wate	Spacing (m)	B - Bedding	J - Joint	Type	ore c. %	RQD %	Test Results &
			S M H W	£ 0	Ă L				- 5	0.05	S - Shear	F - Fault	-	0 %	ď	Comments
-7	20.35	laminations up to 2mm thick SANDSTONE - Low to medium strength, fine to medium grained sandstone with some interbedded siltstone layers up to 3mm thick (continued)														PL(A) = 0.16 PL(D) = 0.11
-	- - - - -21	From 20.17m to 20.35m, carbonaceous sandstone / coal laminations up to 2mm thick Bore discontinued at 20.35m, limit of investigation														
	-															
- - - -	- 22 															
- 4-	- 23 - 23 															
	- 24 - 24 															

RIG: Explora 140 DRILLER: Groundtest LOGGED: Ma CASING: HW to 2.5m

**TYPE OF BORING:** Solid flight auger drilling with V-bit to 2.2m, then NMLC coring to 20.35m

**WATER OBSERVATIONS:** No free groundwater observed whilst augering, then groundwater obscured by drilling fluid during coring **REMARKS:** Co-ordinates obtained from using differential GPS, typical accuracy +0.1m

SAMPLING & IN SITU TESTING LEGEND

A Auger sample
B Bulk sample
BLK Block sample
C Core drilling
D Disturbed sample
E Environmental sample
W Water sample
W Water sample
W Water level



**CLIENT:** Health Infrastructure PROJECT: **Proposed Maitland Hospital** LOCATION: Metford Road, Metford

**SURFACE LEVEL:** 17.0 AHD\* **EASTING**: 369268 **NORTHING**: 6374412 **DIP/AZIMUTH:** 90°/--

**BORE No:** 601 **PROJECT No:** 81719.01 **DATE:** 16/10/2015 SHEET 1 OF 1

П		Description	Degree of Weathering Strength			Fracture	Discontinuities	Sampling & In Situ Testing				
귐	Depth (m)	of	vvcatricing	raph	Strength   Strength	Spacing (m)	B - Bedding J - Joint	) e	e %.	Ω,	Test Results	
	(111)	Strata	EW HW SW FR FS u>ა</u> _	Ex Low Very Low Low Medium High Very High Ex High	. ,	S - Shear F - Fault	Туре	လိမ္တ	RQD %	& Comments		
16		FILLING - Generally comprising brown, fine to medium grained gravelly sand filling, sandstone gravel, trace coal on surface SANDSTONE - (Extremely low to very low strength) grey, stained orange, fine to medium grained									PL(A) = 1.6	
	1.1 1.2						1.36m: P, sh, pl, stn, fe	С	100	66	PL(D) = 1.1 PL(A) = 0.05	
15		slightly fractured, orange-brown, fine to medium grained sandstone  SANDSTONE - Very low strength,					1.82m: P, sh, pl, stn, fe		100	00	PL(A) = 0.32	
14	-3 3.22	moderately weathered, orange-brown, slightly fractured, fine to medium grained sandstone  SANDSTONE - Low to medium strength, fresh stained, slightly fractured, grey, fine grained sandstone, some silt					2.59m: J, 10°, pl, un, clay 2.62m: J, 10°, pl, cbs				PL(A) = 0.23 PL(D) = 0.26	
13	-4	From 2.62m to 2.67m, very low strength  SANDSTONE - Medium strength, fresh stained, slightly fractured to unbroken, pale grey, medium grained sandstone, carbonaceous bands in parts					3.85m: P, sh, pl, cbs	С	100	93	PL(A) = 0.75 PL(D) = 0.42	
12	<sup>-5</sup> 5.05	From 4.05m to 4.20m, 1mm carbonaceous layers horizontally bedded From 4.12m to 4.15m, low strength From 5.00m to 5.01m, carbonaceous coal band									PL(A) = 0.72 PL(D) = 0.65	
	-6 6.0	SANDSTONE - Extremely low strength, highly weathered, friable, orange-brown, medium grained sandstone  SANDSTONE - Medium strength, slightly weathered, slightly fractured to unbroken, pale grey, stained orange in parts, medium grained sandstone					6.08m: J, 20°, pl, ro, stn, fe	С	100	73	PL(A) = 0.38 PL(D) = 0.26	
9	-7								100	70	PL(A) = 0.6 PL(D) = 0.3	
- 0	8.17	Bore discontinued at 8.17m, limit of investigation										

DRILLER: Ground Test (Simon) LOGGED: Parkinson RIG: Explorer CASING: HQ to 1.1m

TYPE OF BORING: Solid flight auger TC bit to 1.1m, NMLC core to 8.17m WATER OBSERVATIONS: Observations obscured by drilling fluids below 1.1m

**REMARKS:** \*Surface level provided by project surveyor

	SAMPLING	3 & IN SITU	TESTING	LEGE	:ND
,	G	Gas sample		PID	Phot

A Auger sample
B Bulk sample
BLK Block sample
C Core drilling
D Disturbed sample
E Environmental sample

Gas sample
Piston sample
Piston sample
Piston sample
PL(A)
Point load axial test Is(50) (MPa)
PL(B)
Point load diametral test Is(50) (MPa)
PL(D)
Point load diametral test Is(50) (MPa)
PL(D)
Point load diametral test Is(50) (MPa)
PL(D)
Point load diametral test Is(50) (MPa)
PL(D)
Point load diametral test Is(50) (MPa)
Poket penetrometer (kPa)
Standard penetration test
V Shear vane (kPa)







	Core Photoplates	PROJECT:	81719.01
Douglas Partners  Geotechnics   Environment   Groundwater	New Maitland Hospital, Metford	PLATE No:	1
Geolechnics i Environment i Groundwater		REV:	0
	CLIENT: Health Infrastructure	DATE:	25-Nov-15

CLIENT: Health Infrastructure
PROJECT: Proposed Maitland Hospital
LOCATION: Metford Road, Metford

SURFACE LEVEL: 21 AHD\* EASTING: 369340 NORTHING: 6374598 DIP/AZIMUTH: 90°/-- BORE No: 602 PROJECT No: 81719.01 DATE: 15/10/2015 SHEET 1 OF 3

21 RL	Depth (m)	of	1	_	_  Suengui   <u></u>	Spacing	-			<u> </u>	n Situ Testing
7			Weathering	raph	Strength Medium Medium Medium Medium Medium Medium Medium Medium Medium Mater Month Medium Mater Month Medium Mater Month Medium Mater Month Medium Mater Month Medium Mater Month Medium Mater Month Medium Mater Month Medium Mater Month Medium Mater Month Medium Mater Month Medium Mater Month Medium Mater Month Medium Mater Month Medium	(m)	B - Bedding J - Joint	Type	ore c. %	RQD %	Test Results &
7		Strata	EW SW M H W FR SW W H	O .	Ex Low Medi High Very Very Ex H	0.05 0.50 1.00	S - Shear F - Fault	F	Q §	ĕ̈́	Comments
20		FILLING - Brown-grey sandy clay filling, comprising fine to medium grained sand with some fine to medium sized gravel (coal, siltstone, sandstone and brick fragments)  SILTSTONE - Extremely low to very low strength, highly weathered brown siltstone						A A S			17,25/100 refusal
19	· 2 2.1	From 1.75m to 1.85m, extremely weathered coal/carbonaceous siltstone  SANDSTONE - Low strength,			-		√ 2.3m: P, 3°, pl, sm				PL(A) = 0.3 PL(D) = 0.28
	-3	moderately weathered, slightly fractured, light brown fine to medium grained sandstone					2.4m: P, 5°, pl, sl				, ,
-	3.1 <sup>-</sup>	SILTSTONE - Low to very low strength, highly weathered, slightly fractured, pale grey and brown	┤╎┎┼┛┆┆┆ ┆╏┆┆┆┆				3.36m: P, 3°, pl, sm, Cn				PL(A) = 0.27 PL(D) = 0.09
17	3.59	siltstone with carbonaceous lenses  SANDSTONE - Very low strength, highly weathered, unbroken brown,		· · · · · · · · · · · · · · · · · · ·	- - - - - - - - - - - - - - - - - - -			С	100	56	PL(A) = 0.06 PL(D) = 0.07
		fine to medium grained sandstone with trace carbonaceous lenses up to 2mm thick From 4.26m to 4.65m, extremely					455 0 00				PL(A) = 0.04 PL(D) = 0.04
19	· 5	low strength  At 4.93m, low strength					4.57m: P, 2°, pl, sm				PL(A) = 0.08 PL(D) = 0.1 PL(A) = 0.28
		From 5.15m, fine grained					5.13m: P, 3°, pl, sm, Fe				PL(D) = 0.25 PL(A) = 0.39 PL(D) = 0.25
15	· 6 6.0	SANDY SILTSTONE - Low					5.59m: P, 3°, pl, sm				PL(A) = 0.43 PL(D) = 0.27
		strength, fresh stained, slightly fractured, fine grained sandy siltstone					6.56m: BP, 2°, pl, sm	С	100	90	PL(A) = 0.21 PL(D) = 0.2
4	-7				.		6.74m: BP, 2°, pl, sm		100	90	DL(A)
	7.64	SANDSTONE - Low strength,			.		7.39m: BP, 2°, pl, sl				PL(A) = 0.3 PL(D) = 0.13 PL(A) = 0.24
	-8	slightly weathered, slightly fractured, fine to medium grained sandstone with trace carbonaceous lenses up to 2mm thick					8.12m: P, 3°, un, sm				PL(D) = 0.23 PL(A) = 0.28
											PL(D) = 0.3
12	- 9	From 9.09m, medium strength, some low strength, moderately weathered bands					9.59m: P, sh, pl, sm, fe	С	100	96	PL(A) = 0.41 PL(D) = 0.33

RIG: Explorer DRILLER: Ground Test (Simon) LOGGED: Fulham CASING: HQ to 1.1m

**TYPE OF BORING:** Solid flight auger to 1.25m, rock roller to 2.15m, NMLC to 21.85m **WATER OBSERVATIONS:** Free groundwater obscured due to drilling methods

**REMARKS:** \*Surface level interpolated from historic survey plan

SAMPLING & IN SITU TESTING LEGEND

A Auger sample
B Bulk sample
B Bulk Slock sample
C Core drilling
C Core drilling
D Disturbed sample
E Environmental sample

SAMPLING & IN SITU IESTINU
G as sample
P Piston sample (x mm dia.)
W Water sample (x mm dia.)
W Water sample
W Water level

Gas sample
Piston sample PL(A) Point load axial test Is(50) (MPa)
Puston sample PL(A) Point load axial test Is(50) (MPa)
Puston sample PL(B) Point load diametral test Is(50) (MPa)
Puston sample PL(D) Point load diametral test Is(50) (MPa)
Puston sample Puston Is Pocket penetrometer (kPa)
Standard penetration test
Water level V Shear vane (kPa)







	Core Pl	notoplates	PROJECT:	81719.01
Douglas Partners  Geotechnics   Environment   Groundwater	New Ma	aitland Hospital, Metford	PLATE No:	2
Geolecinics   Environment   Groundwater			REV:	0
	CLIENT:	Health Infrastructure	DATE:	25-Nov-15

**CLIENT:** Health Infrastructure PROJECT: **Proposed Maitland Hospital** LOCATION: Metford Road, Metford

**SURFACE LEVEL:** 21 AHD\* **EASTING**: 369340 **NORTHING**: 6374598 **DIP/AZIMUTH:** 90°/--

**BORE No:** 602 **PROJECT No: 81719.01 DATE:** 15/10/2015 SHEET 2 OF 3

		Description	Degree of Weathering :≌	Rock Strength	Fracture	Discontinuities				In Situ Testing
귛	Depth (m)	of	Weathering Single Oil	Vate	Spacing (m)	B - Bedding J - Joint	Type	% <u>ه</u>	RQD %	Test Results &
_	(***)	Strata	EW HW SW SW FS FS FS FS	Ex Low Very Low Very Low Nedium High Very High Ex High Ex High	0.05 0.10 0.50 1.00	S - Shear F - Fault	Ty	Seg	RG %	Comments
_	-	SANDSTONE - Low strength, slightly weathered, slightly fractured, fine to medium grained sandstone with trace carbonaceous lenses up to 2mm thick				10.12m: J, 75°, pl, ti, fe	С	100	96	PL(A) = 0.3 PL(D) = 0.34 PL(A) = 0.3
10	- 11 11	(continued)								PL(D) = 0.26 PL(I) = 0.13
0	-12	From 11.77m to 12.0m, some medium sized subrounded gravel					С	100	100	PL(A) = 0.35 PL(D) = 0.38 PL(A) = 0.25
8	- 13 - 13 					12.82m: BP, 2°, pl, sm, coal  13.36m: J, 40°, pl, sm, fe				PL(D) = 0.24 PL(A) = 0.51 PL(D) = 0.38
_	- - 14 - -	From 13.75m, fine grained with some carbonaceous lenses								PL(A) = 0.2 PL(D) = 0.1 PL(A) = 0.31 PL(D) = 0.21
9	- - - - <sup>15</sup> 15.04 -	SILTSTONE - Low strength, fresh, grey siltstone				14.49m: P, 2°, pl, sm, coal	С	82	62	PL(A) = 0.56 PL(D) = 0.31 PL(A) = 0.15
5	15.54 - - - 16 16.0	COAL/CARBONACEOUS SILTSTONE - Low strength, fresh, black coal with bands of carbonaceous siltstone up to 40mm thick				15.54m to 16.0m, fractured 16m: CORE LOSS: 400mm		02	02	PL(D) = 0.07 PL(A) = 0.23 PL(A) = 0.48
	- 16.4 - 16.8 - 17.17.0	From 15.83m to 15.9m, medium strength  CORE LOSS - 0.4m in probable coal				16.8m: CORE LOSS: 200mm	С	66	17	PL(A) = 0.06
	- 17.0	COAL/CARBONACEOUS SILTSTONE - Very low strength, fresh, black coal with some bands of high strength carbonaceous siltstone				17.13m to 18.0m, P, 3°, pl, sm at 140mm spacings				PL(A) = 0.11 PL(D) = 0.03 PL(A) = 0.52 PL(D) = 0.24
?	- - 18 - -	CORE LOSS - 0.20m, in probable coal COAL/CARBONACEOUS SILTSTONE - Very low strength, fresh black coal with interbedded carbonaceous siltstone bands				18.1m: 3 x J, sv, pl, sm 18.32m: P, sh, pl, sl	С	85	25	PL(A) = 0.57 PL(D) = 0.17 PL(I) = 1.42
ļ	18.62	CORE LOSS - 0.28m				18.62m: CORE LOSS: 280mm				,, ,
7	- 18.9 - 19 19.0	COAL - Low to medium strength,				18.90m to 19.0m,	С	100	0	
	- - - -	\fresh, fragmented, black coal / CORE LOSS - 0.79m, in probable coal				fragmented 19m: CORE LOSS: 790mm	С	6	0	
ł	19.79					19.79m to 20m,	С	100	60	

DRILLER: Ground Test (Simon) LOGGED: Fulham RIG: Explorer CASING: HQ to 1.1m

TYPE OF BORING: Solid flight auger to 1.25m, rock roller to 2.15m, NMLC to 21.85m WATER OBSERVATIONS: Free groundwater obscured due to drilling methods

**REMARKS:** \*Surface level interpolated from historic survey plan

**SAMPLING & IN SITU TESTING LEGEND** 

A Auger sample
B Bulk sample
BLK Block sample
C Core drilling
D Disturbed sample
E Environmental sample

Gas sample
Piston sample
Piston sample
Piston sample
PL(A)
Point load axial test Is(50) (MPa)
PL(B)
Point load diametral test Is(50) (MPa)
PL(D)
Point load diametral test Is(50) (MPa)
PL(D)
Point load diametral test Is(50) (MPa)
PL(D)
Point load diametral test Is(50) (MPa)
PL(D)
Point load diametral test Is(50) (MPa)
Poket penetrometer (kPa)
Standard penetration test
V Shear vane (kPa)







	Core Photoplates	PROJECT:	81719.01
Douglas Partners  Geotechnics   Environment   Groundwater	New Maitland Hospital, Metford	PLATE No:	3
Geolechnics i Environment i Groundwater		REV:	0
	CLIENT: Health Infrastructure	DATE:	25-Nov-15

**SURFACE LEVEL**: 21 AHD\*

CLIENT: Health Infrastructure
PROJECT: Proposed Maitland Hospital
LOCATION: Metford Road, Metford

ord Road, Metford

EASTING: 369340

NORTHING: 6374598

DIP/AZIMUTH: 90°/--

BORE No: 602 PROJECT No: 81719.01 DATE: 15/10/2015 SHEET 3 OF 3

		Description	Degree of Weathering	<u>.</u>	Rock Strength		Fracture	Discontinuities				In Situ Testing
씸	Depth (m)	of Charles	Degree of Weathering	Graph Log	Strength Nedium Nedium Nedium Nedium Nedium Nedium Nedium Nedium Nety High Nety High Nety High Nety High Nety High Nety High Nety High Nety Nety Nety Nety Nety Nety Nety Nety	אם אם ב	Spacing (m)	B - Bedding J - Joint S - Shear F - Fault	Туре	Core Rec. %	ROD %	Test Results &
		Strata  CARBONACEOUS SILTSTONE -	W H W W E E		E Ve Hale Cole	5	0.050	fragmented	_	Re	ъ.	Comments PL(A) = 0.13
	20.28	Very low strength, fresh, black to dark brown carbonaceous siltstone (continued)		// 				20.19m to 20.28m, fragmented				PL(D) = 0.07 PL(A) = 0.11
	20.65	SILTSTONE - Fresh, slightly fractured, grey siltstone	·		<del> </del>	j			С	100	60	PL(D) = 0.11
-0	-21 : :	SANDSTONE - Low strength, fresh, unbroken grey fine grained sandstone with laminations of siltstone							C	100	60	PL(A) = 0.24 PL(D) = 0.14
	21.85 - 22	Bore discontinued at 21.85m				ļ						PL(A) = 0.22 PL(D) = 0.23
[ ]	- 22											
						j						
-7	-23											
	:											
- 6	-24											
-4	- 25											
						i						
	•											
9	-26					i						
-	-27					j						
F												
						ĺ						
	-28											
	·											
						- li						
_φ -	- 29											
						j						

RIG: Explorer DRILLER: Ground Test (Simon) LOGGED: Fulham CASING: HQ to 1.1m

**TYPE OF BORING:** Solid flight auger to 1.25m, rock roller to 2.15m, NMLC to 21.85m **WATER OBSERVATIONS:** Free groundwater obscured due to drilling methods

**REMARKS:** \*Surface level interpolated from historic survey plan

#### **SAMPLING & IN SITU TESTING LEGEND**

A Auger sample
B Bulk sample
B Bulk Slock sample
C Core drilling
C Core drilling
D Disturbed sample
E Environmental sample

SAMPLING & IN SITU IESTINU
G as sample
P Piston sample (x mm dia.)
W Water sample (x mm dia.)
W Water sample
W Water level

Gas sample
Piston sample
Piston sample
Piston sample (x mm dia.)
Tube sample (x mm dia.)
Water sample
Water seep
Water level
PID
Photo ionisation detector (ppm)
PL(A) Point load axial test Is(50) (MPa)
PL(D) Point load diametral test Is(50) (MPa)
pp
Pocket penetrometer (kPa)
Standard penetration test
V Shear vane (kPa)



CLIENT: Health Infrastructure
PROJECT: Proposed Maitland Hospital
LOCATION: Metford Road, Metford

SURFACE LEVEL: 18.4 AHD\* EASTING: 369326 NORTHING: 6374480 DIP/AZIMUTH: 90°/-- BORE No: 603 PROJECT No: 81719.01 DATE: 16/10/2015 SHEET 1 OF 1

	Description	Degree of Weathering	⊇ _	Rock Strength	Fracture	Discontinuities	Sa	mpli	ng &	In Situ Testing
Depth (m)	of	Weathering	Log E	Strength Medium High Ex High Ex High Ex High Ex High Out	Spacing (m)	B - Bedding J - Joint	Туре	ore %	RQD %	Test Results &
	Strata	WH W W R R	ן פ	K Kery Very Very Low Low Low Low Low Low Low Low Low Low	0.05 0.50 1.00	S - Shear F - Fault	🕝	S &	80	Comments
-1 -1 -2 -2	FILLING - Generally comprising grey-brown, fine to medium grained, gravelly sand filling, sandstone gravel, possible sandstone cobbles, trace clay						s			10,19,18 N = 37
2.47	SANDSTONE - (Low strength) grey, fine grained sandstone, some silt SANDSTONE - Low strength,					2.02m; I 40° nl am	С	100	100	PL(A) = 0.2 PL(D) = 0.3
-3	slightly weathered, slightly fractured, grey, fine grained					2.82m: J, 10°, pl, sm, stn, fe				PL(A) = 0.23
-  -  -  -	sandstone, some silt, some carbonaceous bands up to 1mm thick, horizontally bedded					3.28m: J, 10°, ir, ro, stn, fe				PL(D) = 0.13
3.8	SANDSTONE - Medium strength, slightly weathered, slightly					3.71m: J, 10°, pl, ro, cbs				
	fractured, pale grey, medium grained sandstone, some					4.17m: P, sh, pl, ro, cbs	С	100	100	PL(A) = 0.29 PL(D) = 0.20 PL(A) = 0.30
-	carbonaceous bands, horizontally bedded At 4.30m, 30mm carbonaceous					4.51m: J, 20°, ir, ro, cbs				PL(D) = 0.34
- -5 -	\band At 4.73m, 10mm carbonaceous band					5.07m: J, 80°, ir, ro, stn,				
	24.14				i	fe 5.54m: Cs, sh, pl, 5mm				
-6						clay				PL(A) = 0.5
										PL(D) = 0.5
							С	100	98	
7										
						7.16m to 7.22m, Cs, sh, pl, 5mm clay spaced generally 20mm				PL(A) = 0.3
-						7.78m: P, sh, pl, ro, stn,				PL(D) = 0.3
8.07	_ SILTSTONE - Low strength, slightly ,		<u>::::</u>			fe 8m: J, 10°, pl, ro, stn, fe				PL(A) = 0.1
8.2	\text{weathered, grey siltstone, some fine grained sand} \text{Bore discontinued at 8.2m, limit of}									<u>PL(D) = 0.1</u>
-9	investigation									
,										
ī										

RIG: Ground Test DRILLER: Ground Test (Simon) LOGGED: Parkinson CASING: HQ to 2.47m

**TYPE OF BORING:** Solid flight auger TC bit to 2.47m, NMLC core to 8.20m **WATER OBSERVATIONS:** Observations obscured by drilling fluids below 2.47m

**REMARKS:** \*Surface level provided by project surveyor

SAMPLIN	G & IN	SITU	TESTING	LEGEND

A Auger sample
B Bulk sample
B Bulk Slock sample
C Core drilling
D Disturbed sample
E Environmental sample
W Water sample
W Water sample
W Water seep
W Water level

Gas sample
Piston sample
Piston sample
Piston sample (x mm dia.)
Tube sample (x mm dia.)
Water sample
Water seep
Water level
PID
Photo ionisation detector (ppm)
PL(A) Point load axial test Is(50) (MPa)
PL(D) Point load diametral test Is(50) (MPa)
pp
Pocket penetrometer (kPa)
Standard penetration test
V Shear vane (kPa)







	Core Photoplates	PROJECT:	81719.01
Douglas Partners  Geotechnics   Environment   Groundwater	New Maitland Hospital, Metford	PLATE No:	4
Geotechnics   Environment   Groundwater		REV:	0
	CLIENT: Health Infrastructure	DATE:	25-Nov-15

CLIENT: Health Infrastructure
PROJECT: Proposed Maitland Hospital
LOCATION: Metford Road, Metford

SURFACE LEVEL: 19.3 AHD\* EASTING: 369372 NORTHING: 6374543 DIP/AZIMUTH: 90°/-- **BORE No:** 604 **PROJECT No:** 81719.01 **DATE:** 21 - 22/10/2015

SHEET 1 OF 1

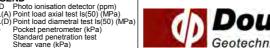
D- "	Description	Degree of Weathering :≘	Rock Strength	Fracture	Discontinuities			<del>.                                      </del>	In Situ Testin
Depth (m)	of	Weathering Since Of S	Nate Nate	Spacing (m)	B - Bedding J - Joint	Туре	ore 2.%	RQD %	Test Resul &
	Strata	SW MW	Kery Kery Kery Kery Kery Kery Kery Kery	0.00	S - Shear F - Fault	F	ŭğ	<u>፠</u> ຶ	Comment
-	FILLING - Generally comprising brown, sandy gravel filling (ripped sandstone and siltstone)  SANDSTONE - Extremely low to very low strength, highly weathered, brown fine to medium		Strength Str						
- -1	grained sandstone								
1.2 1.3	SILTSTONE - Extremely low to very low strength, highly weathered, grey siltstone				1.2m: CORE LOSS: 100mm				PL(A) = 0.0
- - -2	CORE LOSS - 0.1m, (1.2 - 1.3m) in probable siltstone SILTSTONE - Extremely low to	<b>   </b>	<b></b>		1.68m: P, sh. pl, sm, fe	С	93	36	PL(A) = 0.0 PL(A) = 0.0 PL(A) = 0.0
2.08	very low strength, extremely to highly weathered, slightly fractured, dark grey siltstone From 1.84m, light brown								PL(D) = 0.0 PL(A) = 0.0 PL(D) = 0.0 PL(A) = 0.0 PL(D) = 0.0
-3	SANDSTONE - Low strength, slightly weathered, unbroken, grey, fine to medium grained sandstone with some lenses of dark grey siltstone				3.08m: P, sh, pl, sm, fe 3.13m to 3.58m, 45° to 90°, un, sm, fe				PL(A) = 0. PL(A) = 0. PL(D) = 0.
	From 3.89m, extremely low	│ │ │┗┱ │ │┎┷┷┛┆ ┆ ┆┆							PL(A) = 0. PL(D) = 0.
4.06 4.19	strength highly weathered friable /				4.06m: CORE LOSS: 130mm	С	96	73	PL(A) = 0 $PL(A) = 0$
4.56			######################################		5.06m: B, sh, pl, sm				PL(A) = 0.
	SANDSTONE - Low to medium strength, moderatley weathered to fresh stained, slightly fractured,				5.26m: J, 70°, pl, sm				PL(A) = 0.:
- 6	brown and grey, fine to medium grained sandstone			i ii <b>L</b> ii	5.67m: P, sh, pl, sm				
-0	granica sanasione				5.97m: J, 45°, pl, sm, fe				PL(A) = 0.
					6.43m: J, 20°, pl, sm,				, ,
			:::	<b> </b>     	coal				PL(A) = 0.4 PL(D) = 0.5
·7						С	100	93	PL(A) = 0. PL(D) = 0
					7.53m: J, 20°, pl, sm, fe				PL(A) = 0. PL(D) = 0.
-8 . 8.3	SIL ISTOINE - Low strength, slightly				8.08m: B, sh, pl, sm				PL(A) = 0.4 PL(D) = 0.4 PL(A) = 0.4
8.6	weathered slightly fractured dark		<u>-                                      </u>		8.52m: P, 3°, pl, sm				PL(D) = 0
-9	investigation			               					
• • •				 					

RIG: DT25 DRILLER: Ground Test (Kerny-Enrlis)GGED: Fulham CASING: HQ to 1.2m

**TYPE OF BORING:** Solid flight auger to 1.2m, NMLC core to 8.6m **WATER OBSERVATIONS:** Free groundwater obscured by drilling methods

**REMARKS:** 10% water loss from 3.89m. \*Surface level provided by project surveyor

	SAMPLING	3 & IN SITU TESTING	LEGE	END
A Auger sample	G	Gas sample	PID	Photo ionisation detecto
B Bulk sample	P	Piston sample		) Point load axial test ls(5
BLK Block sample	U,	Tube sample (x mm dia.)	PL(D	) Point load diametral test
0 0	147	Marianananala		Deal of a set of a sector of the









	Core Photoplates	PROJECT:	81719.01
Douglas Partners  Geotechnics   Environment   Groundwater	New Maitland Hospital, Metford	PLATE No:	5
Geotechnics i Environment i Groundwater		REV:	0
	CLIENT: Health Infrastructure	DATE:	25-Nov-15

**CLIENT:** Health Infrastructure PROJECT: **Proposed Maitland Hospital** LOCATION: Metford Road, Metford

SURFACE LEVEL: 24.3 AHD\* **EASTING**: 369257 **NORTHING**: 6374488 **DIP/AZIMUTH:** 90°/--

**BORE No**: 605 **PROJECT No:** 81719.01 **DATE:** 22/10/2015 SHEET 1 OF 1

D- "	Description	Degree of Weathering	اج ۔	Rock Strength	Fracture	Discontinuities			<u> </u>	In Situ Testin
Depth (m)	of	Weathering	rapt	Ex Low Very Low Medium High Ex High Ex High Ex High Out	Spacing (m)	B - Bedding J - Joint	Туре	).ee	RQD %	Test Resul
( )	Strata	EW HW EW SW	Ex Lov Low Medit High Ex High	0.05 0.10 1.00	S - Shear F - Fault	\ \cdot \cdo	2 %	R,	Comment	
0.05	FILLING - Generally comprising light grey silt filling, humid FILLING - Brown gravelly sand filling, comprising fine to medium grained sand and fine to medium sized gravel (ripped sandstone, siltstone and coal)									
1.2	SILTSTONE - Very low strength, highly weathered, brown and grey siltstone  SANDSTONE - Extremely low strength, slightly weathered, slightly fractured, pale grey, fine to medium grained sandstone		· —			1.26m: P, 2°, un, sm, coal	С	100	88	PL(A) = 0.1
	From 2.31m to 2.87m, very low strength					2.11m: P, sh, pl, ro, fe 2.2m: B, 3°, un, sm, coal 2.25m: P, 2°, pl, sm, fe				PL(A) = 0.4 PL(D) = 0.2
	suengui				<u>                                      </u>	2.5m: P, 2°, pl, sm 2.71m: P, 5°, pl, sm				PL(A) = 0.0 PL(D) = 0.0
-3 - - - - - - - - - - - - - - - - - -						3.11m to 3.32m, J, 70°, pl, ro	С	92	42	PL(A) = 0. PL(D) = 0. PL(A) = 0. PL(D) = 0.
3.87 -4 -4 -4 -4.47	CORE LOSS - 0.2m (3.67m to 3.87m) in probable extremely weathered sandstone  SANDSTONE - Extremely low strength, extremely weathered, friable, brown, fine to medium grained sandstone (with soil like properties)  SANDSTONE - Low strength,					3.6m: J, 60°, pl, sm 3.67m: CORE LOSS: 200mm 4.61m: J, 50°, pl, sm				PL(D) = 0.0 PL(A) = 0.0
-6	SANDSTONE - Low strength, slightly weathered, slightly fractured, grey, fine to medium grained sandstone with wisps of dark grey siltstone From 4.72m, fresh									PL(A) = 0 PL(D) = 0
6.2	LAMINATE - Low strength, fresh, slightly fractured, grey, interbedded siltstone and fine grained sandstone	_				6.35m: J, 45°, pl, sm	С	100	100	PL(A) = 0.2 PL(D) = 0.2
-7 - 7.1 	SANDSTONE - Medium strength, fresh, unbroken, grey, medium grained sandstone					7.1m: P, 2°, pl, sm, cn				PL(A) = 0.4 PL(D) = 0.4
- 8 7.98 	Bore discontinued at 7.98m, limit of investigation									

DRILLER: Ground Test (Kerny-Enrlis)GGED: Fulham CASING: HQ to 1.2m RIG: DT25

TYPE OF BORING: Solid flight auger to 1.2m, NMLC core to 7.98m WATER OBSERVATIONS: Free groundwater obscured by drilling methods

**REMARKS:** \*Surface level provided by project surveyor

		SAMPLING	& IN SITU TESTING	G LEGE	ND
	Auger sample	G	Gas sample		Photo ionisation detector (p)
В	Bulk sample	Р	Piston sample	PL(A)	Point load axial test Is(50) (I
BLK	Block sample	U,	Tube sample (x mm dia.	) PL(D)	Point load diametral test Is(
С	Core drilling	WÎ	Water sample	pp	Pocket penetrometer (kPa)
	Disturbed sample		Water seep	S	Standard penetration test
E	Environmental sa	mple 📱	Water level	V	Shear vane (kPa)

ppm) (MPa) (50) (MPa) Standard penetration test Shear vane (kPa)







	Core Photoplates	PROJECT:	81719.01
Douglas Partners  Geotechnics   Environment   Groundwater	New Maitland Hospital, Metford	PLATE No:	6
Geolecinics   Environment   Gloundwater		REV:	0
	CLIENT: Health Infrastructure	DATE:	25-Nov-15

**CLIENT:** Health Infrastructure PROJECT: **Proposed Maitland Hospital** LOCATION: Metford Road, Metford

SURFACE LEVEL: --**EASTING**: 369285 **NORTHING**: 6374363 **DIP/AZIMUTH:** 90°/--

**BORE No:** 606 **PROJECT No:** 81719.01 **DATE:** 22/10/2015 SHEET 1 OF 1

Donth	Description	Degree of Weathering	Rock Strength ເຄ	Fracture Spacing	Discontinuities				n Situ Testin
Depth (m)	of		Caraphic Car	(m)	B - Bedding J - Joint	Type	ore	RQD %	Test Resul &
	Strata	EW HW SW RE	Medi Medi G	0.05 0.10 1.00	S - Shear F - Fault	Ţ	ς ğ	8	Comment
-1	FILLING - Brown, gravelly sand filling comprising fine to medium grained sand and fine to medium sized gravel (ripped sandstone and siltstone, trace coal) trace cobbles and tree roots					A A			
2.2	SANDSTONE - Very low strength,								PL(D) = 0.0
2.7	0				2.58m: P, 5°, un, sm, fe				PL(A) = 0.1
-3	SANDSTONE - Low strength, highly weathered, unbroken, brown, fine to medium grained sandstone with bands of extremely low strength, moderately weathered pale grey sandstone				3.71m: P, 2°, Pl, sm, cn	С	100	44	PL(A) = 0.0
·4					3.91m: P, 10°, PI, ro, fe				PL(A) = 0.7 PL(A) = 0.7 PL(D) = 0.7
- 5									PL(A) = 0. PL(D) = 0. PL(A) = 0
5.18 5.24 <sup>/</sup> 5.45	CORE LOSS - 0.06m (5.18m to 5.24m)				5.18m: CORE LOSS:				PL(A) = 0.0
-6	LAMINATE - Very low strength, extremely weathered, friable, orange-brown and pale grey interbeddd fine to medium			<b>-</b>	5.3m: P, 2°, un, sm, fe 5.74m: B, 2°, cu, sm, fe 5.88m: B, 2°, cu, sm, fe				PL(A) = 0
	sandstone and siltstone  LAMINATE - Low to medium strength, moderately weathered,		···	<b>5</b>       	6.12m: P, 2°, PL, sm, fe				PL(A) = 0.
7	slightly fractured, grey and brown fine grained sandstone interbedded with siltstone		· · · · · · · · · · · · · · · · · · ·		6.59m: P, 2°, PI, sm, cn 6.78m: P, 2°, PI, sm, cn	С	98	72	PL(A) = 0.
7.42	CARBONACEOUS SILTSTONE - Low strength, highly weathered, dark brown siltstone From 7.2m, very low strength,				7.29m: P, 3°, PI, sm, coal				PL(A) = 0. PL(D) = 0. PL(A) = 0. PL(D) = 0.
-8	extremely weathered  SANDSTONE - Medium strength, slightly weathered, slightly	<b>     </b>			7.65m: P, 5°, PI, sm, fe 7.84m: P, 2°, pI, sm, fe 7.9m: P, 2°, PI, sm				PL(A) = 0 PL(D) = 0
	fractured brown and grey, fine to medium grained sandstone Bore discontinued at 8.2m, limit of investigation				\*8.08m: J, 65°, PI, sm 8.13m: P, 2°, PI, sm, carbonaceous				
-9									

RIG: DT25 DRILLER: Ground Test (Kerny-Ennlist)GGED: Fulham CASING: HW to 1.2m, HQ to 2.2m

TYPE OF BORING: Solid flight auger to 2.2m, NMLC core to 8.2m WATER OBSERVATIONS: No free groundwter observed whilst augering

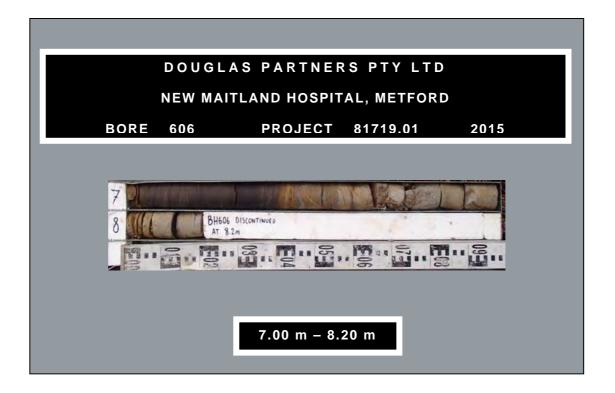
**REMARKS:** Surface level not recorded

SAMPLING	& IN SITU	TESTING	LEGE	END
G	Gas sample		PID	Phot

A Auger sample
B Bulk sample
BLK Block sample
C Core drilling
D Disturbed sample
E Environmental sample Gas sample
Piston sample
Tube sample (x mm dia.)
Water sample
Water seep
Water level







	Core Photoplates	PROJECT:	81719.01
Douglas Partners  Geotechnics   Environment   Groundwater	New Maitland Hospital, Metford	PLATE No:	7
Geolecimics   Environment   Groundwater		REV:	0
	CLIENT: Health Infrastructure	DATE:	25-Nov-15

CLIENT: Health Infrastructure
PROJECT: Proposed Maitland Hospital
LOCATION: Metford Road, Metford

SURFACE LEVEL: 20.5 AHD EASTING: 369283 NORTHING: 6374585 DIP/AZIMUTH: 90°/--

BORE No: 701 PROJECT No: 81719.01 DATE: 11/7/2017 SHEET 1 OF 2

	Б ::	Description	Degree of Weathering	.je	Rock Strength	Fracture Spacing	Discontinuities				n Situ Testing
R	Depth (m)	of Strata	Weathering	Graph Log	Strength   Strength	(m)	B - Bedding J - Joint S - Shear F - Fault	Туре	Core Rec. %	RQD %	Test Results &
20	0.15	FILLING - Generally comprising grey brown, fine to medium grained sandy clay filling, some medium sized subangular gravel, M <wp -="" brown,="" clay="" clay,="" fine="" grained="" grey="" m<wp<="" medium="" sandy="" stiff,="" td="" to="" very=""><td>EW HWW HWW HWW HWW HWW HWW HWW HWW HWW H</td><td></td><td>  Ex Low   Company   Compa</td><td>0.000</td><td></td><td>D</td><td>LE.</td><td></td><td>Comments</td></wp>	EW HWW HWW HWW HWW HWW HWW HWW HWW HWW H		Ex Low   Company   Compa	0.000		D	LE.		Comments
	- 0.6 - -	SANDSTONE - Extremely low strength, extremely weathered, grey stained orange, medium grained sandstone		/ /							
	-1 - -							S	-		25/80 refusal
- 19	- 1.5 - -	Start coring at 1.50m  CORE LOSS - 0.46m, probable sandstone					1.5m: CORE LOSS: 460mm				
-	- 1.96	SANDSTONE - Extremely low		/ \ 				С	54	0	
	- 2.1 - -	strength, extremely weathered, orange grey, medium grained sandstone (soil properties)  CLAYSTONE - Extremely low strength, extremely weathered, grey claystone, some fine to	-								pp = 450
- 18	-	medium grained sand (soil like properties)		X			2.5m: CORE LOSS: 190mm				
	- - -3 3.0	claystone   SANDSTONE - Extremely low   strength, extremely weathered, grey stained orange, medium   grained sandstone   From 2.9m to 3.0m, clay seam					2.90-3.0m, Cs, sh, pl	С	81	0	pp = 350 pp = 400
	- - - 3.4	(very stiff)  COAL - Extremely low strength, highly weathered, black coal	_				3.27m: Cz, 20°, ir, ro				
- 1	-	CARBONACEOUS SILTSTONE - Extremely low to very low strength, slightly weathered, dark brown carbonaceous siltstone					3.68m: P, 30°, ir, he				PL(A) = 0.06
	-4	From 3.84m to 3.91m, coal seam From 3.91m to 4.10m, clay seam		· — ·	<b>,</b>		3.9m: P, sh, pl	С	100	40	
	- 4.1 - -	SANDSTONE - Low strength, slightly weathered, grey, fine grained sandstone, stained orange in parts, slightly fractured, some horizontal carbonaceous bands 1-5mm thick									PL(A) = 0.11 PL(D) = 0.1
-	- - -	. Offin thou					4.72-4.79m, P, sh, pl, ro, he, stn fe, spaced 20mm 4.88m: J, 10°, pl, ro, stn,	С	100	91	PL(A) = 0.11

RIG: Isuzu Mounted TD101 DRILLER: Total Drilling LOGGED: Parkinson CASING: HWt to 1.5m

**TYPE OF BORING:** Solid flight auger v-bit to 1.5m (refusal), NMLC from 1.5m to 8.55m **WATER OBSERVATIONS:** Observations obscured below 1.5m due to drilling fluids

**REMARKS:** 30% water loss from 1.5m, backfilled at completion

SAMPL	.ING &	IN	SITU	<b>TESTING</b>	LEGEND

A Auger sample
B Bulk sample
B Bulk Sample
B Bulk Slock sample
C Core drilling
C Core drilling
D Disturbed sample
E Environmental sample
W Water sample
W Water seep
Water level



CLIENT: Health Infrastructure
PROJECT: Proposed Maitland Hospital
LOCATION: Metford Road, Metford

SURFACE LEVEL: 20.5 AHD EASTING: 369283 NORTHING: 6374585 DIP/AZIMUTH: 90°/--

BORE No: 701 PROJECT No: 81719.01 DATE: 11/7/2017 SHEET 2 OF 2

	Б ;;	Description	Degree of Weathering	.je	Rock Strength	Fracture Spacing	Discontinuities	Sa	mplir	ng & I	n Situ Testing
R	Depth (m)	of Strata	Degree of Weathering	Graph Log	Strength  Nedium Nedium Nedium Nery High Nery High Nery High Nater	(m)	B - Bedding J - Joint S - Shear F - Fault	Туре	Core ec. %	RQD %	Test Results &
15	-	SANDSTONE - Low strength, slightly weathered, grey, fine grained sandstone, stained orange in parts, slightly fractured, some horizontal carbonaceous bands 1-5mm thick (continued)	EW HWW WWW SWW SWW SWW SWW SWW SWW SWW SW		EX L. LOW Weiny High High EX H. LOW Weiny High High EX H. LOW Weiny High High High EX H. LOW Weiny High High High High High High High High	0005	fe 5.06m: J, 10°, pl, ro, stn fe 5.09m: Cz, 10°, pl, ro, stn fe	С	100		PL(A) = 0.16 PL(D) = 0.16
-	- 5.6 - - -	SILTSTONE - Low strength, slightly weathered, grey siltstone, slightly fractured									PL(A) = 0.19 PL(D) = 0.19
	- 6 - - - - 6.42 -						6.21m: P, sh, pl, sm				PL(A) = 0.09
-14		COAL - Low strength, slightly weathered, black coal, fragmented SANDSTONE - Low strength, slightly weathered, grey, fine to medium grained sandstone, slightly fractured					6.42-6.54m, fg 6.75m: J, 10°, pl, sm	С	100	83	PL(A) = 0.12 PL(D) = 0.07
13	- - -						7.1m: P, sh, pl, cbs	0	100	00	PL(A) = 0.32
	- - - -8						7.9m: P, sh, pl, ro 7.95m: P, sh, pl, ro				PL(D) = 0.27
12	-						8.23m: P, sh, pl, ro				PL(A) = 0.06 PL(A) = 0.3 PL(D) = 0.27
	8.55 - - - - - - 9	Bore discontinued at 8.55m, limit of investigation									
-11-	- - -										
	-										

RIG: Isuzu Mounted TD101 DRILLER: Total Drilling LOGGED: Parkinson CASING: HWt to 1.5m

**TYPE OF BORING:** Solid flight auger v-bit to 1.5m (refusal), NMLC from 1.5m to 8.55m **WATER OBSERVATIONS:** Observations obscured below 1.5m due to drilling fluids

**REMARKS:** 30% water loss from 1.5m, backfilled at completion

#### SAMPLING & IN SITU TESTING LEGEND

A Auger sample
B Bulk sample
B Bulk Sample
C Core drilling
D Disturbed sample
E Environmental sample

SAMPLING & IN STILL IES IIK
G Sas sample
P Fiston sample (x mm dia
W Water sample (x mm dia
W Water sample
E Environmental sample
W Water level

LING & IN SITU TESTING LEGENU

G Gas sample
Piston sample
VI Tube sample (x mm dia)
W Water sample
W Water sample
V Water seep
Water level
V Shear vane (kPa)



CLIENT: Health Infrastructure
PROJECT: Proposed Maitland Hospital
LOCATION: Metford Road, Metford

SURFACE LEVEL: 18 AHD EASTING: 369315 NORTHING: 6374543 DIP/AZIMUTH: 90°/--

BORE No: 702 PROJECT No: 81719.01 DATE: 11 - 12/7/2017 SHEET 1 OF 3

		Description	Degree of Weathering	ဋ	Rock Strength ់ច	Fracture	Discontinuities				n Situ Testing
RL	Depth (m)	of	Degree of Weathering	Graph Log	Strength Str	Spacing (m)	B - Bedding J - Joint S - Shear F - Fault	Type	ore c. %	RQD %	Test Results &
8		Strata FILLING - Generally comprising	W W W W W W W W W W W W W W W W W W W		KING KEN	0.05	5 - Sriear F - Fauit	_	0 %	œ	Comments
	- - - - -	grey brown gravelly sandy clay filling, fine to medium grained sand, gravel ripped sandstone medium to boulder sized, abundant silt, trace coal, humid									
	-							S			pp = 200 4,2,6 N = 8
- 1	-2	From 2.0m, brown, moist									000
15	- - - -3							S			pp = 200 2,4,5 N = 9
	- - - - - 3.8	CARBONACEOUS SANDSTONE - Extremely low strength, extremely									
-1	-4	weathered, grey black, fine to medium grained carbonaceous sandstone						S			pp = 450 9,16,25/100 refusal
	4.4	Start coring at 4.4m SANDSTONE - Low strength,									
-	- - -	moderately weathered, grey stained orange, medium grained sandstone, slightly fractured to unbroken						С	100	100	PL(A) = 0.11 PL(D) = 0.12
	-										

RIG: Isuzu Mounted TD101 DRILLER: Total Drilling LOGGED: Parkinson CASING: HWt to 4.4m

**TYPE OF BORING:** Solid flight auger v-bit to 4.4m, NMLC from 4.4m to 11.55m **WATER OBSERVATIONS:** Observations obscured below 4.4m due to drilling fluids

**REMARKS:** Backfilled at completion

#### **SAMPLING & IN SITU TESTING LEGEND**

A Auger sample
B Bulk sample
B Bulk Sample
C C Core drilling
D Disturbed sample
E Environmental sample

SAMPLING & IN SITU IESTIN
G Gas sample
P Fiston sample (x mm dia
W Water sample (x mm dia
W Water sample
E Environmental sample
W Water level

LING & IN SITU TESTING LEGENU

G Gas sample
Piston sample
VI Tube sample (x mm dia)
W Water sample
W Water sample
V Water seep
Water level
V Shear vane (kPa)



CLIENT: Health Infrastructure
PROJECT: Proposed Maitland Hospital
LOCATION: Metford Road, Metford

SURFACE LEVEL: 18 AHD EASTING: 369315 NORTHING: 6374543 DIP/AZIMUTH: 90°/--

BORE No: 702 PROJECT No: 81719.01 DATE: 11 - 12/7/2017 SHEET 2 OF 3

			Description	Degree of Weathering	ည်	Rock Strength	Fracture	Discontinuities				n Situ Testing
R		epth (m)	of		Fraph Log	Strength Strength Water Water	Spacing (m)	B - Bedding J - Joint S - Shear F - Fault	Туре	ore c. %	RQD %	Test Results &
13			SANDSTONE - Low strength,	W M M W M M M M M M M M M M M M M M M M		Kery Kery Kery Kery Kery Kery Kery Kery	0.05	S - Shear F - Fault	É.	ပည္	ď	Comments
	-		SANDS I ONE - Low strength, moderately weathered, grey stained orange, medium grained sandstone, slightly fractured to unbroken (continued)						С	100	100	
12	- - -6							5.66m: J, 10°, pl, ro, stn fe 5.81m: P, sh, pl, ro, stn fe				PL(A) = 0.17
	-		From 6.25-6.4m, extremely low strength, extremely weathered From 6.4-6.75m, medium strength					6.3m: Cz, sh, pl, ro				PL(A) = 0.56 PL(D) = 0.46
-	-							6.57m: J, 10°, pl, ro, stn				
	-		From 6.75-7.08m, extremely low strength, extremely weathered					6.67m: P, sh, pl, ro				
-=	-7		From 7.09m your low strength					7.09m; D. ah. al	С	100	78	
-	-	7.25	From 7.08m, very low strength, slightly weathered	<b>   </b>				7.08m: P, sh, pl, ro, stn fe				PL(A) = 0.05
	-	7.20	SANDSTONE - Low to medium strength, slightly weathered, grey, fine grained sandstone, some horizontal carbonaceous bands 1-2mm thick, slightly fractured									PL(A) = 0.34
10	- - -8							7.92m: P, sh, pl, cbs				
-	ļ											PL(A) = 0.27
	_	8.68 -	From 8.55m to 8.68m, extremely low to very low strength									
- 6	-9	0.00	SANDSTONE - Medium strength, slightly weathered, grey stained orange in parts, medium to coarse grained sandstone, slightly fractured					8.7m: P, sh, pl, ro, stn fe				PL(A) = 0.45 PL(D) = 0.4
									С	100	89	
								9.4m: P, sh, pl, he				
								9.55m: P, sh, pl, ro, stn fe				
	-											PL(A) = 0.42 PL(D) = 0.42

RIG: Isuzu Mounted TD101 DRILLER: Total Drilling LOGGED: Parkinson CASING: HWt to 4.4m

**TYPE OF BORING:** Solid flight auger v-bit to 4.4m, NMLC from 4.4m to 11.55m **WATER OBSERVATIONS:** Observations obscured below 4.4m due to drilling fluids

**REMARKS:** Backfilled at completion

#### **SAMPLING & IN SITU TESTING LEGEND**

A Auger sample
B Bulk sample
B Bulk Slock sample
C Core drilling
D Disturbed sample
E Environmental sample
W Water sample
W Water sample
W Water seep
W Water level

LING & IN SITU TESTING LEGENU

G Gas sample
Piston sample
VI Tube sample (x mm dia)
W Water sample
W Water sample
V Water seep
Water level
V Shear vane (kPa)



CLIENT: Health Infrastructure
PROJECT: Proposed Maitland Hospital
LOCATION: Metford Road, Metford

SURFACE LEVEL: 18 AHD EASTING: 369315 NORTHING: 6374543 DIP/AZIMUTH: 90°/-- BORE No: 702 PROJECT No: 81719.01 DATE: 11 - 12/7/2017 SHEET 3 OF 3

		Description	Degree of Weathering	<u>.</u> 2	S	Ro	ck ngth	٠	Fracture Discontinuities		Sampling & In Situ Testing			
R	Depth (m)	of		3raph Log	N-ow / Low	   <u>  [</u>	High Very High Ex High	Water	Spacing (m)	B - Bedding J - Joint S - Shear F - Fault	Type	Core Rec. %	%D %D	Test Results &
	-	Strata  SANDSTONE - Medium strength, slightly weathered, grey stained orange in parts, medium to coarse grained sandstone, slightly fractured (continued)	EW EW EW EW EW EW EW EW EW EW EW EW EW E							10.16m: J, 10°, pl, ro, cbs	F	0 %	ш.	Comments
	10.73 · - - - 11	SANDSTONE - Low strength, slightly weathered, grey, fine to medium grained sandstone, some horizontal carbonaceous bands 1-2mm thick, slightly fractured									С	100	89	PL(A) = 0.12
	-	From 11.35-11.55m, very low strength								11.21m: P, sh, ir, cbs 11.4m: J, 20°, pl, ro				PL(A) = 0.03
	11.55 · - - -	Bore discontinued at 11.55m, limit of investigation			         	<del>   </del>             	+ + + + + + + + + + + + + + + + + + +							. 26.9 - 0.00
9	-12 - - - -													
	- 13 - 13 													
4	- -14 - - - - -													

RIG: Isuzu Mounted TD101 DRILLER: Total Drilling LOGGED: Parkinson CASING: HWt to 4.4m

**TYPE OF BORING:** Solid flight auger v-bit to 4.4m, NMLC from 4.4m to 11.55m **WATER OBSERVATIONS:** Observations obscured below 4.4m due to drilling fluids

**REMARKS:** Backfilled at completion

#### **SAMPLING & IN SITU TESTING LEGEND**

A Auger sample
B Bulk sample
B Bulk Sample
B Bulk Slock sample
C Core drilling
C Core drilling
D Disturbed sample
E Environmental sample
W Water sample
W Water seep
Water level



CLIENT: Health Infrastructure
PROJECT: Proposed Maitland Hospital
LOCATION: Metford Road, Metford

SURFACE LEVEL: 17 AHD EASTING: 369291 NORTHING: 6374511 DIP/AZIMUTH: 90°/-- BORE No: 703 PROJECT No: 81719.01 DATE: 12/7/2017 SHEET 1 OF 3

		Description	Degree of	o	Rock Strength	Fracture	Discontinuities	Sa	mpli	ng &	In Situ Testing
R	Depth (m)	of	Weathering	aphi -og	Strew Very Low Medium High Ex High Ex High Ex High O.01	Spacing (m)	B - Bedding J - Joint	g.	% و	RQD %	Test Results
	(111)	Strata	HW HW EW	Ex Low Very Low Mediur High Very H Ex Higl	0.05	S - Shear F - Fault	Туре	Pec.	RQ %	& Comments	
-	0.3	FILLING - Generally comprising brown, fine grained silty sand filling, trace coal fines and rootlets, moist (slope wash)  CARBONACEOUS CLAY - Hard, black carbonaceous clay with some fine to medium grained sand, M <wp -<="" carbonaceous="" siltstone="" td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>Commente</td></wp>									Commente
16	- - 1 -	Extremely low strength, extremely weathered, black carbonaceous siltstone, some coal bands (soil like properties)						s	-		pp = 400 8,25/50
+	-	Start coring at 1.3m			<b>!</b>				1		refusal
15	- 1.3 - 1.35	CARBONACEOUS SILTSTONE - Extremely low strength, extremely weathered, black carbonaceous siltstone, some coal bands (soil like properties)  SANDSTONE - Medium strength, moderately weathered, grey stained orange, fine to medium grained sandstone, slightly fractured  From 2.0m, low strength		<i>##</i>			1.56-1.58m, Cz, sh, pl, ro, stn fe	С	100	94	PL(A) = 0.49 PL(D) = 0.47 PL(A) = 0.11 PL(D) = 0.08
- 4-	-3	From 2.58m to 3.25m, very low strength, highly weathered					2.58m: P, sh, pl, ro, stn fe 2.77m: P, sh, pl, he, stn fe 3.04m: P, sh, pl, ro, stn fe 3.07m: P, sh, pl, ro, stn fe				PL(A) = 0.08
	3.35	SANDSTONE - Low strength, slightly weathered, grey, fine grained sandstone, some horizontal carbonaceous bands 1-3mm thick, unbroken					3.25m: Cz, sh, pl, ro, stn fe  4.17m: Handling break	С	100	74	PL(A) = 0.15 PL(D) = 0.12 PL(A) = 0.29 PL(D) = 0.16

RIG: Isuzu Mounted TD101 DRILLER: Total Drilling LOGGED: Parkinson CASING: HWt to 1.3m

**TYPE OF BORING:** Solid flight auger v-bit to 1.3m, NMLC from 1.3m to 12.0m **WATER OBSERVATIONS:** Observations obscured below 1.3m due to drilling fluids

**REMARKS:** Well installed at completion

#### SAMPLING & IN SITU TESTING LEGEND

A Auger sample
B Bulk sample
B Bulk Sample
B Bulk Slock sample
C Core drilling
C Core drilling
D Disturbed sample
E Environmental sample
W Water sample
W Water seep
Water level



CLIENT: Health Infrastructure
PROJECT: Proposed Maitland Hospital
LOCATION: Metford Road, Metford

SURFACE LEVEL: 17 AHD EASTING: 369291 NORTHING: 6374511 DIP/AZIMUTH: 90°/-- BORE No: 703 PROJECT No: 81719.01 DATE: 12/7/2017 SHEET 2 OF 3

		Description	Degree of Weathering	.ie	Rock Strength ់ច	Fracture Spacing	Discontinuities	Sa	mplir	ng & I	n Situ Testing
R	Depth (m)	of Strata	Degree of Weathering	Grapt Log	Strength Nedium Nedium Nedium Nedium Nedium Nedium Nedium Nedium Nedium Netra	(m) (2000) (m) (2000)	B - Bedding J - Joint S - Shear F - Fault	Type	Core Rec. %	RQD %	Test Results & Comments
-	5.08	SANDSTONE - Medium strength, slightly weathered, grey, medium to coarse grained sandstone, unbroken						С	100		PL(A) = 0.32 PL(D) = 0.29
	- - - -6										PL(D) = 0.29
-	- 6.5	SANDSTONE - Low strength, slightly weathered, grey, medium to coarse grained sandstone, unbroken					>>				PL(A) = 0.22
- 1	- 7 - 7 							С	100	100	PL(A) = 0.11
- 6	- - - - -8						7.65m: Handling break				
	-										PL(A) = 0.2 PL(D) = 0.16
	- - - 9 -										PL(A) = 0.36 PL(D) = 0.22
-	-						9.4m: Pt, sh, pl, ro 9.67m: J, 40°, ir, inf cbs	С	98	98	. L(D) = 0.22
_	-					<b>     </b>	9.9m: J, 10°, pl, ro, inf				PL(D) = 0.13

RIG: Isuzu Mounted TD101 DRILLER: Total Drilling LOGGED: Parkinson CASING: HWt to 1.3m

**TYPE OF BORING:** Solid flight auger v-bit to 1.3m, NMLC from 1.3m to 12.0m **WATER OBSERVATIONS:** Observations obscured below 1.3m due to drilling fluids

**REMARKS:** Well installed at completion

#### **SAMPLING & IN SITU TESTING LEGEND**

A Auger sample
B Bulk sample
B Bulk Sample
B Bulk Slock sample
C Core drilling
C Core drilling
D Disturbed sample
E Environmental sample
W Water sample
W Water seep
Water level



CLIENT: Health Infrastructure
PROJECT: Proposed Maitland Hospital
LOCATION: Metford Road, Metford

SURFACE LEVEL: 17 AHD EASTING: 369291 NORTHING: 6374511 DIP/AZIMUTH: 90°/-- BORE No: 703 PROJECT No: 81719.01 DATE: 12/7/2017 SHEET 3 OF 3

	Description	Degree of Weathering		Rock Strength	Fracture Spacing	Discontinuities	Sa	mplir	ng & I	In Situ Testing
교 Depth (m)	of Strata	Degree of Weathering	Grapt	Strength Nater Water	(m)	B - Bedding J - Joint S - Shear F - Fault	Туре	Core Rec. %	RQD %	Test Results &
10.23		H H H H H H H H H H H H H H H H H H H				cbs		LE.		Comments
- 10.28	SANDSTONE - Low strength, slightly weathered, grey, medium to coarse grained sandstone, some siltstone inclusions					10.28-10.4m, fg, possibly drill induced 10.57m: J, 30°, ir, ro, cbs	С	98	98	PL(A) = 0.11
						11.24m: J, 70°, pl, sm				PL(A) = 0.1
11.71	CORE LOSS - 0.19m, probable coal					11.71m: CORE LOSS: 190mm	С	62	42	PL(D) = 0.16
	COAL - Medium strength, slightly					11.9-12.0m, Pt, sh, pl, sm, spaced 20mm				PL(A) = 0.33

RIG: Isuzu Mounted TD101 DRILLER: Total Drilling LOGGED: Parkinson CASING: HWt to 1.3m

**TYPE OF BORING:** Solid flight auger v-bit to 1.3m, NMLC from 1.3m to 12.0m **WATER OBSERVATIONS:** Observations obscured below 1.3m due to drilling fluids

**REMARKS:** Well installed at completion

#### SAMPLING & IN SITU TESTING LEGEND

A Auger sample
B Bulk sample
B Bulk Sample
B Bulk Slock sample
C Core drilling
C Core drilling
D Disturbed sample
E Environmental sample
W Water sample
W Water seep
Water level



**CLIENT:** Multiplex Constructions Pty Ltd **PROJECT:** Proposed New Maitland Hospital

**LOCATION:** Metford Road, Metford

SURFACE LEVEL: --EASTING: 369398 NORTHING: 6374534 PIT No: 4001

**PROJECT No:** 81719.09 **DATE:** 29/11/2018 **SHEET** 1 OF 1

		Description of			San	npling &					
R	Depth (m)			)e	e to e Results &			Vater	Dynamic Penetrometer Test (blows per 150mm)		
	(111)	Strata		1	Dep	Sam	Comments	>		10 15	20
	Depth (m)	of	うつう Craphic Log	А	Sam the part of th	and and and and and and and and and and	Results & Comments	Water			

RIG: Hitachi 6.5t Excavator Zaxis LOGGED: Millard SURVEY DATUM: MGA94

WATER OBSERVATIONS: No free groundwater observed, whilst pit remained open

**REMARKS:** Hand held GPS ±10m

SAMPLING & IN SITU TESTING LEGEND

A Auger sample
B Bulk sample
B Bulk Slock sample
C Core drilling
D Disturbed sample
E Environmental sample

SAMPLING & IN SITU TESTING
G Sas sample
P Piston sample (x mm dia.)
W Water sample (x mm dia.)
W Water sample
W Water level

LING & IN STU TESTING LEGEND

G Gas sample PID Photo ionisation detector (ppm)
P Piston sample PID Photo ionisation detector (ppm)
PL(A) Point load axial test Is(50) (MPa)
PL(D) Point load diametral test Is(50) (MPa)
PD Water sample Pocket penetrometer (kPa)
Water seep S Standard penetration test
Water level V Shear vane (kPa)



□ Sand Penetrometer AS1289.6.3.3⊠ Cone Penetrometer AS1289.6.3.2

**CLIENT:** Multiplex Constructions Pty Ltd **PROJECT:** Proposed New Maitland Hospital

**LOCATION:** Metford Road, Metford

SURFACE LEVEL: --EASTING: 369338 NORTHING: 6374434 **PIT No:** 4002 **PROJECT No:** 81719.09

DATE: 29/11/2018 SHEET 1 OF 1

		Description			Sam	Sampling & In Situ Testing			Dimamia Danatromator Toot		
R	Depth (m)	of Strata	Graphic Log	Туре	Depth	Sample	Results & Comments	Water	Dynamic Penetrometer Test (blows per 150mm)		
	-	FILLING - Firm to soft, clayey fine to medium grained sand filling, moist to wet			0.3	3)		-			
	0.45			В	0.45						
	-1	FILLING - Fine to medium grained sand filling, saturated  Cobbles (sandstone) subangular to subrounded to 350mm in size						-	.1		
	- - 1.4	FILLING - Soft, grey sandy clay filling, wet			1.4		pp = 30	-			
	-2 -	Pit discontinued at 1.6m, due to pit walls collapsing	· · ·					-	.2		

RIG: Hitachi 6.5t Excavator Zaxis LOGGED: Millard SURVEY DATUM: MGA94

WATER OBSERVATIONS: Free groundwater observed at 0.45m

**REMARKS:** Pit collapse due to water ingress. Hand held GPS  $\pm 10$ m

**SAMPLING & IN SITU TESTING LEGEND** 

A Auger sample
B Bulk sample
B Bulk Slock sample
C Core drilling
D Disturbed sample
E Environmental sample

SAMPLING & IN SITU TESTING
G Sas sample
P Piston sample (x mm dia.)
W Water sample (x mm dia.)
W Water sample
W Water level

LING & IN STI O TESTING LEGEND

G Gas sample PID Photo ionisation detector (ppm)
P Piston sample PID Photo ionisation detector (ppm)
PL(A) Point load axial test Is(50) (MPa)
PL(D) Point load diametral test Is(50) (MPa)
PD Water sample Pocket penetrometer (kPa)
Water seep S Standard penetration test
Water level V Shear vane (kPa)



□ Sand Penetrometer AS1289.6.3.3⊠ Cone Penetrometer AS1289.6.3.2

Multiplex Constructions Pty Ltd **CLIENT:** PROJECT: Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

SURFACE LEVEL: --**EASTING**: 369260 **NORTHING**: 6374434 **PIT No: 4003** 

**PROJECT No:** 81719.09 **DATE:** 29/11/2018 SHEET 1 OF 1

			Description	Graphic Log		San		& In Situ Testing					
귐	Dep (m	oth ı)	of		Туре	Depth	Sample	Results & Comments	Water	Dynamic Penetrometer Test (blows per 150mm)			
		+	Strata  CLAYEY SAND - Yellow brown very dense, moist, fine to medium grained sand, trace medium to coarse grained subrounded sandstone gravel		F	Ğ	Sar	Comments		5	10	15 2 : :	20
	-	0.1		. —						. :			
	_		SILTSTONE - Extremely low strength, highly weathered, grey siltstone, thinly laminated										
	-			· — · ·						. :			
	_					0.4				-			
					В					- :	:	:	•
	-					0.6				-			
		0.75								. :	:	:	•
	_		COAL - Black, with carbonaceous siltstone										•
	_									-			:
	-1	1.0	SILTSTONE - Extremely low strength grey siltstone,							-1			•
	_		carbonaceous lenses, thinly laminated							-	:	:	•
	_	1.2	CLAYEY SAND - (Completely weathered sandstone),	////						-			•
	-		CLAYEY SAND - (Completely weathered sandstone), extremely low strength, pale brown, moist, fine to medium grained sand, carbonaceous clay lenses (1mm thickness)							-			•
	_		unomessy							_			
	-									-	:	:	•
	-												
	_									-	:	:	•
	-												•
	-			(7./7. (7/7.)						- :	:	:	:
	-2	2.0	Pit discontinued at 2.0m, limit of investigation	///						2	:	:	:
	-									- -	:	:	•
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RIG: Hitachi 6.5t Excavator Zaxis LOGGED: Millard **SURVEY DATUM: MGA94** 

WATER OBSERVATIONS: No free groundwater observed, whilst pit remained open

**REMARKS:** Hand held GPS ±10m

**SAMPLING & IN SITU TESTING LEGEND** 

A Auger sample
B Bulk sample
BLK Block sample
C Core drilling
D Disturbed sample
E Environmental sample

LING & IN STU TESTING LEGEND

G Gas sample PID Photo ionisation detector (ppm)
P Piston sample PID Photo ionisation detector (ppm)
PL(A) Point load axial test Is(50) (MPa)
PL(D) Point load diametral test Is(50) (MPa)
PD Water sample Pocket penetrometer (kPa)
Water seep S Standard penetration test
Water level V Shear vane (kPa)



☐ Sand Penetrometer AS1289.6.3.3 ☑ Cone Penetrometer AS1289.6.3.2

Multiplex Constructions Pty Ltd **CLIENT:** PROJECT: Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

SURFACE LEVEL: --**EASTING**: 369396 **NORTHING**: 6374381 **PIT No:** 5001 **PROJECT No:** 81719.09 **DATE:** 29/11/2018

SHEET 1 OF 1

		Description	je.		Sam		& In Situ Testing	_	Durania Barata mata Tart
RL	Depth (m)	th	Graphic Log	Туре	Depth	Sample	Results & Comments	Water	Dynamic Penetrometer Test (blows per mm)
	-	FILLING (Capping) - Medium to coarse grained sandy gravel filling, trace clay, cobbles to 200m in size		L		S.			5 10 15 20
	- 0.6- - -1 -	FILLING - Intermixed carbonaceous siltstone and coal filling (rejects), dark grey with coal fines and coal / carbonaceous siltstone fragments up to 150mm in size, moist		В	0.8				-1
	-2 2.0 ·	Pit discontinued at 2.0m, limit of investigation			-2.0-				-

RIG: Hitachi 6.5t Excavator Zaxis LOGGED: Millard **SURVEY DATUM: MGA94** 

WATER OBSERVATIONS: No free groundwater observed, whilst pit remained open

**REMARKS:** Hand held GPS ±10m

**SAMPLING & IN SITU TESTING LEGEND** 

A Auger sample
B Bulk sample
BLK Block sample
C Core drilling
D Disturbed sample
E Environmental sample

LING & IN STU TESTING LEGEND

G Gas sample PID Photo ionisation detector (ppm)
P Piston sample PID Photo ionisation detector (ppm)
PL(A) Point load axial test Is(50) (MPa)
PL(D) Point load diametral test Is(50) (MPa)
PD Water sample Pocket penetrometer (kPa)
Water seep S Standard penetration test
Water level V Shear vane (kPa)



☐ Sand Penetrometer AS1289.6.3.3 ☐ Cone Penetrometer AS1289.6.3.2

Multiplex Constructions Pty Ltd **CLIENT:** PROJECT: Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

SURFACE LEVEL: --**EASTING**: 369450 **NORTHING**: 6374382 **PIT No:** 5002 **PROJECT No:** 81719.09

**DATE:** 29/11/2018 SHEET 1 OF 1

	<b>.</b>	Description	:E _		Sam		& In Situ Testing		Dimomio Do	notromotor	Toot
집	Depth (m)	of Strata	Graphic Log	Туре	Depth	Sample	Results & Comments	Water	Dynamic Pe (blows		
		FILLING (Capping) - Medium to coarse grained sandy gravel filling, trace clay, cobbles to 250m in size				Š			5 10	15	20
	- 0.d	FILLING - Intermixed carbonaceous siltstone and coal filling (rejects), dark grey with coal fines and coal / carbonaceous siltstone fragments up to 150mm in size, moist		В	1.0				-1		
	- 1.	Pit discontinued at 1.6m, limit of investigation			-1.6-				-2		

RIG: Hitachi 6.5t Excavator Zaxis LOGGED: Millard **SURVEY DATUM: MGA94** 

WATER OBSERVATIONS: No free groundwater observed, whilst pit remained open

REMARKS: Hand held GPS ±10m

**SAMPLING & IN SITU TESTING LEGEND** 

A Auger sample
B Bulk sample
BLK Block sample
C Core drilling
D Disturbed sample
E Environmental sample G Gas sample
P Piston sample (x mm dia.)
Tube sample (x mm dia.)
W Water sample
Water seep
Water level

PID Photo ionisation detector (ppm)
PL(A) Point load axial test Is(50) (MPa)
PL(D) Point load diametral test Is(50) (MPa)
PL(D) Point load diametral test Is(50) (MPa)
pp Pocket penetrometer (kPa)
S Standard penetration test
V Shear vane (kPa)



☐ Sand Penetrometer AS1289.6.3.3 ☐ Cone Penetrometer AS1289.6.3.2

**CLIENT:** Multiplex Constructions Pty Ltd **PROJECT:** Proposed New Maitland Hospital

**LOCATION:** Metford Road, Metford

SURFACE LEVEL: --EASTING: 369489 NORTHING: 6374359 **PIT No:** 5003

**PROJECT No:** 81719.09 **DATE:** 29/11/2018 **SHEET** 1 OF 1

		Description	i		San		& In Situ Testing	<u>_</u>				. <b>.</b> .
씸	Depth (m)	of	Graphic Log	Туре	Depth	Sample	Results & Comments	Water	Dynan	nic Pene (blows p	etromete per mm)	er i est
		Strata	O	Ļ	De	San	Comments		5	10	15	20
-		FILLING (Capping) - Medium to coarse grained sandy gravel filling, trace clay, cobbles to 150m in size										
	•									:		
╽┟	-1 1.0	FILLING - Intermixed carbonaceous siltstone and coal			1.0				-1			
-		filling (rejects), dark grey with coal fines and coal / carbonaceous siltstone fragments up to 150mm in size, moist		В				-				
	1.8	Pit discontinued at 1.8m, limit of investigation			-1.8-			+	:	:		- :
-		Pit discontinued at 1.011, limit of frivesugation							-2			

RIG: Hitachi 6.5t Excavator Zaxis LOGGED: Millard SURVEY DATUM: MGA94

WATER OBSERVATIONS: No free groundwater observed, whilst pit remained open

**REMARKS:** Hand held GPS ±10m

**SAMPLING & IN SITU TESTING LEGEND** 

A Auger sample
B Bulk sample
B Bulk Slock sample
C Core drilling
C Core drilling
D Disturbed sample
E Environmental sample

SAMPLING & IN SITU IESTINU
G as sample
P Piston sample (x mm dia.)
W Water sample (x mm dia.)
W Water sample
W Water level

LING & IN STU TESTING LEGEND

G Gas sample PID Photo ionisation detector (ppm)
P Piston sample PID Photo ionisation detector (ppm)
PL(A) Point load axial test Is(50) (MPa)
PL(D) Point load diametral test Is(50) (MPa)
PD Water sample Pocket penetrometer (kPa)
Water seep S Standard penetration test
Water level V Shear vane (kPa)



☐ Sand Penetrometer AS1289.6.3.3 ☐ Cone Penetrometer AS1289.6.3.2

Multiplex Constructions Pty Ltd **CLIENT:** PROJECT: Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

SURFACE LEVEL: --**EASTING**: 369522 **NORTHING**: 6374347 **PIT No: 5004** 

**PROJECT No:** 81719.09 **DATE:** 29/11/2018 SHEET 1 OF 1

		Description	Ö		Sam		& In Situ Testing				
R	Depth (m)	of Strata	Graphic Log	Туре	Depth	Sample	Results & Comments	Water	Dynamic (b	Penetrometer lows per mm)	r Test
	- 0.8	FILLING (Capping) - Medium to coarse grained sandy gravel filling, trace clay, cobbles to 200m in size									
	- 1	FILLING - Intermixed carbonaceous siltstone and coal filling (rejects), dark grey with coal fines and coal / carbonaceous siltstone fragments up to 150mm in size, moist			1.0				-1		
				В	1.0				-		
	- 1.8 -	Pit discontinued at 1.8m, limit of investigation	XXX		—1.8—				-		
	-2								-2		

RIG: Hitachi 6.5t Excavator Zaxis LOGGED: Millard **SURVEY DATUM: MGA94** 

WATER OBSERVATIONS: No free groundwater observed, whilst pit remained open

**REMARKS:** Hand held GPS ±10m

**SAMPLING & IN SITU TESTING LEGEND** 

A Auger sample
B Bulk sample
BLK Block sample
C Core drilling
D Disturbed sample
E Environmental sample

LING & IN STU TESTING LEGEND

G Gas sample
P Piston sample (PID) Photo ionisation detector (ppm)
PL(A) Point load axial test Is(50) (MPa)
W Water sample (x mm dia).
W Water sample (y mm dia).
P Water seep
Water seep
Water level
V Shear vane (kPa)



☐ Sand Penetrometer AS1289.6.3.3 ☐ Cone Penetrometer AS1289.6.3.2

**CLIENT:** Health Infrastructure

**PROJECT:** Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

SURFACE LEVEL: PIT No: 2001 EASTING: 369362 PROJECT NO: 81719.07

**NORTHING**: 6374380 **DATE**: 29/6/2018 **DIP/AZIMUTH**: 90°/-- **SHEET**: 1 of 1

									DIP/AZIMUTH: 90°/			SHEET: 1 of	<u>'</u>
				DRI	LLING				MATERIAL				
PROG	RESS	TER	s	AM	PLING	ĵ.	C	ر	DECODISTION	Щ.	Z U		TEOT DE0: :: TE
9 g	~	ID WA			IDs	RL YTH (r	H	[ 8	DESCRIPTION OF STRATA	STUR	STEI ATIV	DCP	TEST RESULTS & COMMENTS
DRILLING & CASING	WATER	GROUND WATER LEVELS	GEO	ENV	and REMARKS	RL DEPTH (m)	GRA	LOG	STRATA	MOIS	CONSISTENCY RELATIVE DENSITY	blows/150mm (tip: cone)	COMMENTS
A 8	Š		Ö	Ξ	KLINAKKS	0.0	Ŧ,	$\overline{}$		+	ŏ	5 10 15 20 25	
		No free groundwater observed					K	$\boxtimes$	FILL/SANDY GRAVEL: medium to coarse; brown; trace clay; cobbles to 300mm			i i   i	
		erob					$\triangleright$	$\bowtie$	,				
		ıdwat					₹	$\boxtimes$				:	-
		grour	В				K	X				i i Li	
		free					$\triangleright$	$\langle \! \! \! \! \! \! \! \! \! \! \! \! \! \! \! \! \! \! \!$					
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							K	$\bowtie$					
							-	$\bowtie$				. i i i i	-
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							K	X					
							≯	$\bowtie$					1
							K	$\bowtie$					
							$\mathbb{K}$	$\bowtie$					
							$\triangleright$	$\boxtimes$					
							K	$\times$					
							∱	$\bowtie$					-
1.03.04							K	$\bowtie$				i i i i i	
p6pdp						1.0-	$\mathbb{X}$	$\bowtie$					
Toal - DGD   Lib: apdgd 1.04.02 Prj: apdgd 1.03.04						1.0	$\triangleright$	$\boxtimes$					
1.04 1.04							K	$\times$					
pdp :qi							∱	$\bowtie$				: i i i i	-
11 G9C							K	$\times$					
							$\mathbb{X}$	$\langle \! \rangle$				[ i i i i	
lln Situ							$\langle \rangle$	$\boxtimes$	1.25m				1
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FIG: Excavator DRILLER: LOGGED: Millard CHECKED: West

REMARKS: Hand Held GPS ± 10 m GRID DATUM: MGA94 Zone 56

### SAMPLING & IN SITU TESTING LEGEND

A Auger sample P Piston sample Bulk sample U<sub>x</sub> Tube sample (x mm dia.)
Core drilling Water seep
Disturbed sample Water level
Envirnmental Sample PID Photo ionisation detector (ppm)



**CLIENT:** Health Infrastructure

PROJECT: Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

**SURFACE LEVEL: PIT No:** 2002 **EASTING:** 369372 **PROJECT NO:** 81719.07

**NORTHING**: 6374391 **DATE**: 29/6/2018 **DIP/AZIMUTH**: 90°/-- **SHEET**: 1 of 1

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		L C	_					WATERIAL			
DRILLING & CASING	WATER	GROUND WATER LEVELS			PLING  IDs and REMARKS	RL DEPTH (m)	GRAPHIC LOG	DESCRIPTION OF STRATA	MOISTURE CONDITION CONSISTENCY RELATIVE DENSITY	DCP blows/150mm	TEST RESULTS & COMMENTS
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						0.5 -		FILL/CARBONACEOUS SILTSTONE & COAL FILLING  0.55m (REJECTS), DARK GREY WITH COAL FINES AND COAL / CARBONACEOUS SILTSONE FRAGMENTS Pit discontinued at 0.55m depth Limit of investigation			-
719 16:04 8.30.004 Dagge Lab and in Silu Tod - DGD   Lib: qbggd 1.04.02 Pj; dpggr 1.03.04						1.0-					-
002_SOIL_WGATE_B1719.07.L.001.REV0.GPJ < <cdrawingfile>&gt; 11/01/20</cdrawingfile>						1.5 -	REFI	ER TO EXPLANATORY NOTES FOR DESCRIPTION OF SYMBOLS AND ABBREV	IATIONS  ATTIONS		

RIG: Excavator DRILLER: LOGGED: Millard CHECKED: West

REMARKS: Hand Held GPS ± 10 m GRID DATUM: MGA94 Zone 56

### SAMPLING & IN SITU TESTING LEGEND

Auger sample P Piston sample Ut Tube sample (X mm dia.)
Core drilling
Disturbed sample
Envirmental Sample
PiD Photo ionisation detector (ppm)



**CLIENT:** Health Infrastructure

PROJECT: Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

SURFACE LEVEL: PIT No: 2003 EASTING: 369376 PROJECT NO: 81719.07

NORTHING: 6374363 DATE: 29/6/2018 DIP/AZIMUTH: 90°/-- SHEET: 1 of 1

							_	DIP/AZIMUTH: 90 /			SHEET: 101	
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	RESS	GROUND WATER LEVELS	S	AM	PLING	Ê	⊋	DESCRIPTION	₩ 8	√E VE		TEST RESULTS
DRILLING & CASING	<u>بر</u>	IND W EVELS	_		IDs	RL DEPTH (m)	GRAPHIC LOG	OF STRATA	DTSI	CONSISTENCY RELATIVE DENSITY	DCP blows/150mm	TEST RESULTS & COMMENTS
RILL	WATER	3ROU LE	GEO	EN	IDs and REMARKS	DEF	la L	STRATA	18 8	SON BENEFICIAL STATES	(tip: cone)	COMMENTS
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		No free groundwater observed					$\bowtie$	FILL/SANDY GRAVEL: medium to coarse; grey brown; trace silt; cobbles to 200mm				
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RIG: Excavator DRILLER: LOGGED: Millard CHECKED: West

REMARKS: Hand Held GPS ± 10 m GRID DATUM: MGA94 Zone 56

### SAMPLING & IN SITU TESTING LEGEND

A Auger sample P Piston sample
B Bulk sample U, Tube sample (x mm dia.)
C Core drilling P Water seep
D Disturbed sample F Water level
Envirnmental Sample PID Photo ionisation detector (ppm)



**CLIENT:** Health Infrastructure

**PROJECT:** Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

SURFACE LEVEL: PIT No: 2004 EASTING: 369400 PROJECT NO: 81719.07

**NORTHING**: 6374396 **DATE**: 29/6/2018 **DIP/AZIMUTH**: 90°/-- **SHEET**: 1 of 1

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PROGRE	ESS	er.			PLING	_			1	≿		
I		GROUND WATER LEVELS				н (m.)	GRAPHIC LOG	DESCRIPTION	TURE	CONSISTENCY RELATIVE DENSITY	DCP	TEST RESULTS
DRILLING & CASING	WATER	OUND	GEO	EN	and I	RL EPTH	GRAF	OF STRATA	MOIS	NSIS RELA DENS	blows/150mm (tip: cone)	TEST RESULTS & COMMENTS
S O S	Ϋ́		ß	面	REMARKS	0.0			20	8-	5 10 15 20 25	
10 8	\$	No free groundwater observed				- <del>0.0 -</del>		FILL/SANDY GRAVEL: medium to coarse; grey brown; trace medium plasticity clay; cobbles to 200mm  FILL/CARBONACEOUS SILTSTONE & COAL FILLING (REJECTS), DARK GREY WITH COAL FINES AND COAL / CARBONACEOUS SILTSONE FRAGMENTS	mois		10 15 20 25	
RIG: E						1.5-	REFI	Pit discontinued at 1.00m depth Limit of investigation  ER TO EXPLANATORY NOTES FOR DESCRIPTION OF SYMBOLS AND ABBREV			D: West	

RIG: Excavator DRILLER: LOGGED: Millard CHECKED: West

REMARKS: Hand Held GPS ± 10 m GRID DATUM: MGA94 Zone 56

### SAMPLING & IN SITU TESTING LEGEND

Auger sample P Piston sample
Bulk sample U<sub>x</sub> Tube sample (x mm dia.)
Core drilling P Water seep
Disturbed sample
Envirnmental Sample
PID Photo ionisation detector (ppm)



**CLIENT:** Health Infrastructure

**PROJECT:** Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

SURFACE LEVEL: PIT No: 2005 EASTING: 369416 PROJECT NO: 81719.07

NORTHING: 6374384 DATE: 29/6/2018 DIP/AZIMUTH: 90°/-- SHEET: 1 of 1

									DIP/AZIMUTH: 90°/			SHEET: 1 of	<u> </u>
				DRI	LLING				MATERIAL				
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PR S C	× ×		GE	Ы	KEMARKS			_			, 12_	(tip: cone) 5 10 15 20 25	
108 - 1050   LEC 40097 105 27 Pr) 00699 1 LEC 40097 105 14   DEPLICATION		No free groundwater observed GROLIND WATER	_	AM	PLING	(ii) ALD 0.0			DESCRIPTION OF STRATA  FILL/SANDY GRAVEL: medium to coarse; silt; cobbles to 200mm  FILL/CARBONACEOUS SILTSTONE & COAL FILLING (REJECTS), DARK GREY WITH COAL FINES AND (COAL / CARBONACEOUS SILTSONE FRAGMENTS) Pit discontinued at 0.95m depth Limit of investigation	MOISTURE		DCP blows/150mm (tip: cone) 5 10 15 20 25 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	TEST RESULTS & COMMENTS
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<u>[</u>							L,	DE	D TO EVOLANATORY NOTEO FOR RECORDINION OF CAMPALA AND ASSESSMENT	ATIO:			
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REMARKS: Hand Held GPS ± 10 m GRID DATUM: MGA94 Zone 56

### SAMPLING & IN SITU TESTING LEGEND

Auger sample P Piston sample PL(A) Poi
Bulk sample U, Tube sample (x mm dia.) PL(D) Poi
Core drilling 
Disturbed sample
Envirnmental Sample
PID Photo ionisation detector (ppm) V Shi



**CLIENT:** Health Infrastructure

**PROJECT:** Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

SURFACE LEVEL: PIT No: 2006 EASTING: 369432 PROJECT NO: 81719.07

**DATE**: 29/6/2018 **SHEET**: 1 of 1

NORTHING: 63743 DIP/AZIMUTH: 90°/--

DRILLING MATERIAL MOISTURE CONDITION CONSISTENCY RELATIVE DENSITY PROGRESS **SAMPLING** DEPTH (m) GRAPHIC LOG DESCRIPTION TEST RESULTS DCP DRILLING & CASING OF STRATA GROUND V R & COMMENTS IDs blows/150mm and REMARKS GEO EN (tip: cone) groundwater observed FILL/SANDY GRAVEL: medium to coarse; grey brown; with medium plasticity clay; cobbles to 20mm No free moist FILL/CARBONACEOUS SILTSTONE & COAL FILLING
(REJECTS), DARK GREY WITH COAL FINES AND
COAL / CARBONACEOUS SILTSONE FRAGMENTS dry Pit discontinued at 1.00m depth Limit of investigation 1.5 REFER TO EXPLANATORY NOTES FOR DESCRIPTION OF SYMBOLS AND ABBREVIATIONS

Fig. Excavator DRILLER: LOGGED: Millard CHECKED: West

**REMARKS**: Hand Held GPS ± 10 m GRID DATUM: MGA94 Zone 56

### SAMPLING & IN SITU TESTING LEGEND

Auger sample P Piston sample U<sub>x</sub> Tube sample (xmm dia.)
Core drilling be Water seep
Disturbed sample Water level
Envirmmental Sample
PID Photo ionisation detector (ppm)



**CLIENT:** Health Infrastructure

**PROJECT:** Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

SURFACE LEVEL: PIT No: 2007

**EASTING:** 369458 **PROJECT NO:** 81719.07

**NORTHING**: 6374390 **DATE**: 29/6/2018 **DIP/AZIMUTH**: 90°/-- **SHEET**: 1 of 1

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DRILLING & CASING	WATER	SROU	GEO	ENV	and REMARKS	DEF	R <sub>2</sub>	STRATA	8 8	CONSISTENCY RELATIVE DENSITY	(tip: cone)	COMMENTS
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FIG: Excavator DRILLER: LOGGED: Millard CHECKED: West

REMARKS: Hand Held GPS ± 10 m GRID DATUM: MGA94 Zone 56

### SAMPLING & IN SITU TESTING LEGEND





**CLIENT:** Health Infrastructure

PROJECT: Proposed New Maitland Hospital

**LOCATION:** Metford Road, Metford

SURFACE LEVEL: PIT No: 2008
EASTING: 369466 PROJECT NO: 81719.07

NORTHING: 6374369 DATE: 29/6/2018

DIP/AZIMUTH: 90°/-- SHEET: 1 of 1

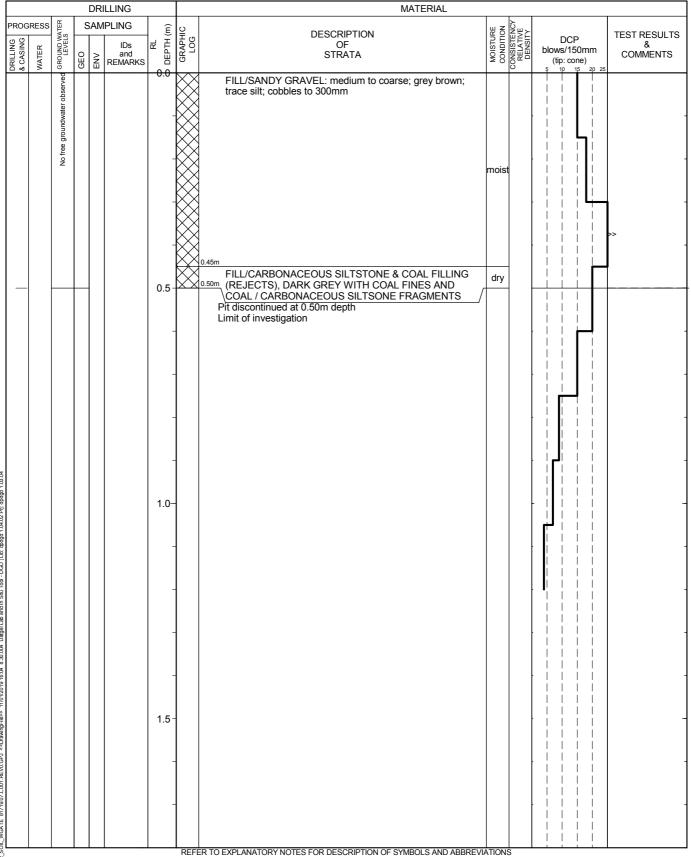


Fig. Excavator DRILLER: LOGGED: Millard CHECKED: West

REMARKS: Hand Held GPS ± 10 m GRID DATUM: MGA94 Zone 56

### SAMPLING & IN SITU TESTING LEGEND

Auger sample P Piston sample U, Tube sample (x mm dia.)

Bulk sample U, Tube sample (x mm dia.)

Water seep

Disturbed sample

Envirmmental Sample

PID Photo ionisation detector (ppm)



**CLIENT:** Health Infrastructure

PROJECT: Proposed New Maitland Hospital

**LOCATION:** Metford Road, Metford

**SURFACE LEVEL: PIT No:** 2009 **EASTING:** 369479 **PROJECT NO:** 81719.07

NORTHING: 6374395 DATE: 29/6/2018 DIP/AZIMUTH: 90°/-- SHEET: 1 of 1

DRILLING MATERIAL MOISTURE CONDITION CONSISTENCY RELATIVE DENSITY PROGRESS **SAMPLING** DEPTH (m) GRAPHIC LOG DESCRIPTION TEST RESULTS DCP DRILLING & CASING OF STRATA GROUND V & COMMENTS IDs 씸 blows/150mm and REMARKS GEO EN (tip: cone) groundwater observed FILL/SANDY GRAVEL: medium to coarse; grey brown; trace silt; cobbles to 100mm No free В moist 1.5 FILL/CARBONACEOUS SILTSTONE & COAL FILLING (REJECTS), DARK GREY WITH COAL FINES AND dry COAL / CARBONACEOUS SILTSONE FRAGMENTS Pit discontinued at 1.55m depth Limit of investigation REFER TO EXPLANATORY NOTES FOR DESCRIPTION OF SYMBOLS AND ABBREVIATIONS

Fig. Excavator DRILLER: LOGGED: Millard CHECKED: West

**REMARKS**: Hand Held GPS ± 10 m GRID DATUM: MGA94 Zone 56

### SAMPLING & IN SITU TESTING LEGEND

A Auger sample P Piston sample
B B Lik sample U, Tube sample (x mm dia.)
- Water seep
D E Envirmental Sample
E Envirmental Sample



**CLIENT:** Health Infrastructure

**PROJECT:** Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

SURFACE LEVEL: PIT No: 2010 EASTING: 369481 PROJECT NO: 81719.07

**NORTHING:** 6374351 **DATE:** 29/6/2018 **DIP/AZIMUTH:** 90°/-- **SHEET:** 1 of 1

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FIG: Excavator DRILLER: LOGGED: Millard CHECKED: West

REMARKS: Hand Held GPS ± 10 m GRID DATUM: MGA94 Zone 56

### SAMPLING & IN SITU TESTING LEGEND

Auger sample P Piston sample
Bulk sample U, Tube sample (x mm dia.)
Core drilliangle
Disturbed sample
Envirmmental Sample
P Water level
PID Photo ionisation detector (ppm)



**CLIENT:** Health Infrastructure

PROJECT: Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

SURFACE LEVEL: PIT No: 2011 EASTING: 369503 PROJECT NO: 81719.07

**NORTHING**: 6374369 **DATE**: 29/6/2018 **DIP/AZIMUTH**: 90°/-- **SHEET**: 1 of 1

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RIG: Excavator DRILLER: LOGGED: Millard CHECKED: West

REMARKS: Hand Held GPS ± 10 m GRID DATUM: MGA94 Zone 56

### SAMPLING & IN SITU TESTING LEGEND

A Auger sample P Piston sample
B Bulk sample U, Tube sample (x mm dia.)
Core drilling Water seep
D Disturbed sample
E Envirnmental Sample
PID Photo ionisation detector (ppm)



**CLIENT:** Health Infrastructure

**PROJECT:** Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

 SURFACE LEVEL:
 PIT No: 2012

 EASTING: 369518
 PROJECT NO: 81719.07

**NORTHING**: 6374349 **DATE**: 29/6/2018 **DIP/AZIMUTH**: 90°/-- **SHEET**: 1 of 1

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	& CASING	WATER	RO UE	GEO	ENV	and REMARKS	)EP	GR/	OF STRATA	MON	NS E	blows/150mm (tip: cone)	COMMENTS
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								$\langle \times \rangle$	0.90m	1		<b>  </b>	4
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10d 1.0								Γ	COAL / CARBONACEOUS SILTSONE FRAGMENTS		]		
Prj: dpc							1.0-	1	Pit discontinued at 0.95m depth Limit of investigation			-	-
04.02								1	Limit of investigation			▎▕▟▏▏▕▕▋	
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FIG: Excavator DRILLER: LOGGED: Millard CHECKED: West

REMARKS: Hand Held GPS ± 10 m GRID DATUM: MGA94 Zone 56

### SAMPLING & IN SITU TESTING LEGEND





**CLIENT:** Health Infrastructure

PROJECT: Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

SURFACE LEVEL: PIT No: 2013

**EASTING:** 369540 **PROJECT NO:** 81719.07

**NORTHING:** 6374353 **DATE:** 29/6/2018 **DIP/AZIMUTH:** 90°/-- **SHEET:** 1 of 1

								DIPIAZIWOTA: 90 /			SHEET: 101	•
				DRI	LLING			MATERIAL		1		
PROG		GROUND WATER LEVELS	S	AM	PLING	RL DEPTH (m)	⊋	DESCRIPTION	H S	VE VE		TEST RESULTS
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		No free groundwater observed					$\bowtie$	FILL/SANDY GRAVEL: medium to coarse; grey brown; trace silt; cobbles to 200mm				
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Soli_MGATE BITTBUT.LUOTAEVUGFJ < <ur><urboration< td="">*SOLOW DaggetLab and missing</urboration<></ur>							$\boxtimes$	1.35m (REJECTS), DARK GREY WITH COAL FINES AND	dry			
5.								COAL / CARBONACEOUS SILTSONE FRAGMENTS Pit discontinued at 1.35m depth	/			
91.61						-	1	Limit of investigation				1
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RIG: Excavator DRILLER: LOGGED: Millard CHECKED: West

REMARKS: Hand Held GPS ± 10 m GRID DATUM: MGA94 Zone 56

### SAMPLING & IN SITU TESTING LEGEND

Auger sample
Bulk sample
Cred drilling
Disturbed sample
Envirnmental Sample

P
Piston sample (x mm dia.)
Water seep
Water ievel
PID
Photo ionisation detector (ppm)



**CLIENT:** Health Infrastructure

PROJECT: Proposed New Maitland Hospital

LOCATION: Metford Road, Metford

SURFACE LEVEL: PIT No: 2014
EASTING: 369513 PROJECT NO: 81719.07

**NORTHING**: 6374376 **DATE**: 29/6/2018 **DIP/AZIMUTH**: 90°/-- **SHEET**: 1 of 1

DDII/ WG	DIPIAZINIO I R. 90 /	SHEET. 1011
DRILLING	MATERIAL	
PROGRESS   SAMPLING (E)	DESCRIPTION	TEST RESULTS
SING SING SING SING SING SING SING SING	OF STDATA	E COMMENTS    SO S S S S S S S S S S S S S S S S S S
WAT A SAWAWAT ENV.	O SIRAIA	US 0 0 (tip: cone) COMMENTS
0.5	DESCRIPTION OF STRATA  FILL/SANDY GRAVEL: medium to coarse; grey brown; trace silt; cobbles to 250mm  SILTY CLAY: dark grey; medium plasticity, abundant organics; alluvial  Pit discontinued at 1.00m depth Limit of investigation	moist    DCP   blows/150mm (tp: cone)   TEST RESULTS & COMMENTS
1.5		

REMARKS: Hand Held GPS ± 10 m

### SAMPLING & IN SITU TESTING LEGEND

DRILLER:

A Auger sample P
B Bulk sample U<sub>x</sub>
C Core drilling 
D Disturbed sample
E Envirnmental Sample PID

g RIG: Excavator

P Piston sample
U<sub>x</sub> Tube sample (x mm dia.)
Water seep
Water level
PID Photo ionisation detector (ppm)

PL(A) Point load axial test Is(50) (MPa)
PL(D) Point load diametral test Is(50) (MPa)
pp Pocket penetrometer (kPa)
SPT Standard penetration test
V Shear vane (kPa)

LOGGED: Millard



**CHECKED:** West

GRID DATUM: MGA94 Zone 56

# Appendix C

Laboratory Test Results

**Report Number:** 81719.09-2

Issue Number:

Date Issued: 11/01/2019

Client: Multiplex Constructions Pty Ltd

GPO Box 172, Sydney NSW 2000

**Project Number:** 81719.09

**Project Name:** Proposed New Maitland Hospital

**Project Location:** Metford Road, Metford

Work Request: 2910 Sample Number: 19-2910D **Date Sampled:** 29/11/2018

Sampling Method: Sampled by Engineering Department Sample Location: Stockpile Material / Pit 4001 (0.6-0.8)

Material: 40% Carbonaceous Material / 60% non-Carbonaceous

Sandstone

Dry Density - Moisture Relationship (AS 12	289 5.1.1 & 2.1.1)
Mould Type	2.4 LITRE MOULD B
Compaction	Standard
No. Layers	3
No. Blows / Layer	60
Maximum Dry Density (t/m <sup>3</sup> )	1.63
Optimum Moisture Content (%)	14.5
Oversize Sieve (mm)	37.5
Oversize Material (%)	0.6
Method used to Determine Plasticity	Visual Assessment
Curing Hours	2



Newcastle Laboratory

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Email: Peter.Gorseski@douglaspartners.com.au

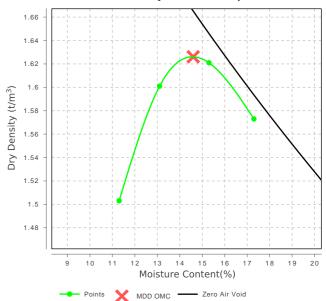


Approved Signatory: Peter Gorseski

Laboratory Manager

NATA Accredited Laboratory Number: 828

### **Moisture Density Relationship**



Report Number: 81719.09-2 Page 1 of 5

**Report Number:** 81719.09-2

Issue Number:

Date Issued: 11/01/2019

Client: Multiplex Constructions Pty Ltd

GPO Box 172, Sydney NSW 2000

**Project Number:** 81719.09

**Project Name:** Proposed New Maitland Hospital

**Project Location:** Metford Road, Metford

Work Request: 2910 Sample Number: 19-2910E **Date Sampled:** 29/11/2018

Sampling Method: Sampled by Engineering Department Sample Location: Stockpile Material / Pit 4003 (0.4-0.6)

40% Carbonaceous Material / 60% non-Carbonaceous Siltstone Material:

Dry Density - Moisture Relationship (AS 12	289 5.1.1 & 2.1.1)
Mould Type	2.4 LITRE MOULD B
Compaction	Standard
No. Layers	3
No. Blows / Layer	60
Maximum Dry Density (t/m <sup>3</sup> )	1.58
Optimum Moisture Content (%)	18.0
Oversize Sieve (mm)	37.5
Oversize Material (%)	1.9
Method used to Determine Plasticity	Visual Assessment
Curing Hours	2



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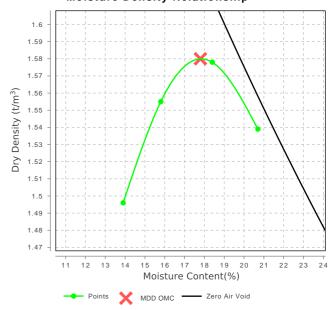


Peter Gorseski

Laboratory Manager

NATA Accredited Laboratory Number: 828

### **Moisture Density Relationship**



Report Number: 81719.09-2 Page 2 of 5

**Report Number:** 81719.09-2

Issue Number:

Date Issued: 11/01/2019

Client: Multiplex Constructions Pty Ltd

GPO Box 172, Sydney NSW 2000

81719.09 **Project Number:** 

**Project Name:** Proposed New Maitland Hospital

**Project Location:** Metford Road, Metford

Work Request: 2910 Sample Number: 19-2910F **Date Sampled:** 29/11/2018

Sampling Method: Sampled by Engineering Department Sample Location: Stockpile Material / Pit 4001 (0.6-0.8)

50% Carbonaceous Material / 50% non Carbonaceous Sandstone Material:

Dry Density - Moisture Relationship (AS 12	289 5.1.1 & 2.1.1)
Mould Type	2.4 LITRE MOULD B
Compaction	Standard
No. Layers	3
No. Blows / Layer	60
Maximum Dry Density (t/m <sup>3</sup> )	1.56
Optimum Moisture Content (%)	16.0
Oversize Sieve (mm)	37.5
Oversize Material (%)	5.7
Method used to Determine Plasticity	Visual Assessment
Curing Hours	2.3



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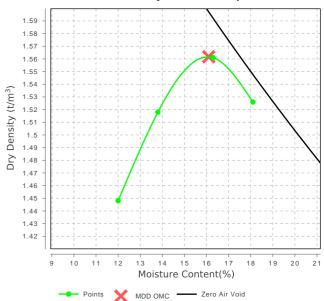


Peter Gorseski

Laboratory Manager

NATA Accredited Laboratory Number: 828

### **Moisture Density Relationship**



Report Number: 81719.09-2 Page 3 of 5

**Report Number:** 81719.09-2

Issue Number:

Date Issued: 11/01/2019

Client: Multiplex Constructions Pty Ltd

GPO Box 172, Sydney NSW 2000

**Project Number:** 81719.09

**Project Name:** Proposed New Maitland Hospital

**Project Location:** Metford Road, Metford

Work Request: 2910 Sample Number: 19-2910G **Date Sampled:** 29/11/2018

Sampling Method: Sampled by Engineering Department Sample Location: Stockpile Material / Pit 4003 (0.4-0.6)

50% Carbonaceous Material / 50% non Carbonaceous Siltstone Material:

Dry Density - Moisture Relationship (AS 12	289 5.1.1 & 2.1.1)
Mould Type	2.4 LITRE MOULD B
Compaction	Standard
No. Layers	3
No. Blows / Layer	60
Maximum Dry Density (t/m <sup>3</sup> )	1.53
Optimum Moisture Content (%)	19.0
Oversize Sieve (mm)	37.5
Oversize Material (%)	1
Method used to Determine Plasticity	Visual Assessment
Curing Hours	2.3



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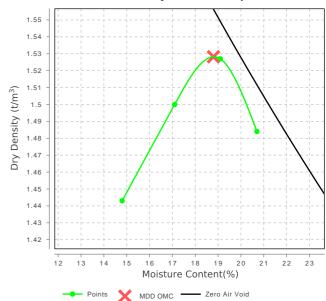


Peter Gorseski

Laboratory Manager

NATA Accredited Laboratory Number: 828

### Moisture Density Relationship



Report Number: 81719.09-2 Page 4 of 5

**Report Number:** 81719.09-2

Issue Number:

Date Issued: 11/01/2019

Client: Multiplex Constructions Pty Ltd

GPO Box 172, Sydney NSW 2000

**Project Number:** 81719.09

**Project Name:** Proposed New Maitland Hospital

**Project Location:** Metford Road, Metford

Work Request: 2910 Sample Number: 19-2910H **Date Sampled:** 29/11/2018

Sampling Method: Sampled by Engineering Department Stockpile Material / Pit 4001 (0.6-0.8) Sample Location:

Material: 60% Carbonaceous Material / 40% non-Carbonaceous

Sandstone

Dry Density - Moisture Relationship (AS 12	289 5.1.1 & 2.1.1)
Mould Type	1 LITRE MOULD A
Compaction	Standard
No. Layers	3
No. Blows / Layer	60
Maximum Dry Density (t/m <sup>3</sup> )	1.55
Optimum Moisture Content (%)	16.5
Oversize Sieve (mm)	37.5
Oversize Material (%)	4.1
Method used to Determine Plasticity	Visual Assessment
Curing Hours	3



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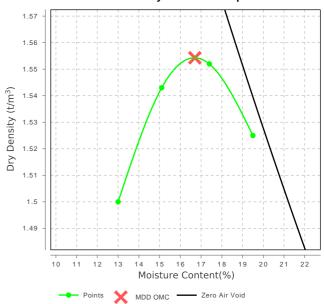


Peter Gorseski

Laboratory Manager

NATA Accredited Laboratory Number: 828

### **Moisture Density Relationship**



Report Number: 81719.09-2 Page 5 of 5

Report Number: 81719.09\_1

Issue Number:

Date Issued: 10.01.2018

Client: Multiplex Constructions Pty Ltd

Project Number: 81719.09

Project Name: Proposed New Maitland Hospital

Project Location: Metford Road, Metford

Work Request: 2909
Date Sampled: 13.12.2018

Sampling Method: Sampled by DP Engineering



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Accredited for Compliance with ISOIEC 17025 - Testing

Approved Signatory: Peter Gorseski NATA Accredited Laboratory Number: 828

Sample Number	3001	
Sample Location	-	
Depth (m)	7.69 - 8.0	
Rock Description		
	Sandstone	
Storage History and Environment	Tested as Received	Alt Control
Orientation to Bedding	-	
Compression Machine	Autocon Model CL10320	- 0
Date of Testing	07.01.2018	
Duration of Test (seconds)	210	
Average Diameter (mm)	51.8	
Average Height (mm)	138	
Height to Diameter Ratio	2.7 : 1	
Moisture Content (%)	7.6	
Wet Mass / Unit Volume (t/m³)	2.27	
Dry Mass / Unit Volume (t/m³)	2.11	
Uniaxial Compressive Strength (MPa)	7.7	The same of the sa
Comments		A STATE OF THE STA
		Control of the Contro

Report Number: 81719.09\_1

Issue Number:

Date Issued: 10.01.2018

Client: Multiplex Constructions Pty Ltd

Project Number: 81719.09

Project Name: Proposed New Maitland Hospital

Project Location: Metford Road, Metford

Work Request: 2909
Date Sampled: 13.12.2018

Sampling Method: Sampled by DP Engineering



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Accredited for Compliance with ISOIEC 17025 - Testing

1

Approved Signatory: Peter Gorseski

NATA Accredited Laboratory Number: 828

	ck Core AS 4133.4.2, AS 4133.1.	
Sample Number	3001	A STATE OF THE PARTY OF THE PAR
Sample Location	-	A STATE OF THE STA
Depth (m)	14.79 - 15.0	
Rock Description	Sandstone / Siltstone	
Storage History and Environment	Tested as Received	48 23
Orientation to Bedding	-	191
Compression Machine	Autocon Model CL10320	
Date of Testing	07.01.2018	
Duration of Test (seconds)	185	
Average Diameter (mm)	51.6	
Average Height (mm)	131	
Height to Diameter Ratio	2.5 : 1	
Moisture Content (%)	8.8	
Wet Mass / Unit Volume (t/m3)	2.29	
Dry Mass / Unit Volume (t/m³)	2.11	
Uniaxial Compressive Strength (MPa)	5.5	
Comments		

Report Number: 81719.09\_1

Issue Number:

Date Issued: 10.01.2018

Client: Multiplex Constructions Pty Ltd

Project Number: 81719.09

Project Name: Proposed New Maitland Hospital

Project Location: Metford Road, Metford

Work Request: 2909
Date Sampled: 14.12.2018

Sampling Method: Sampled by DP Engineering



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Approved Signatory: Peter Gorseski

NATA Accredited Laboratory Number: 828

Uniaxial Compressive Strength of Ro	ock Core AS 4133 4.2 AS 4
Sample Number	3002
Sample Location	-
Depth (m)	4.72 - 5.0
Rock Description	
	Sandstone
Storage History and Environment	Tested as Received
Orientation to Bedding	-
Compression Machine	Autocon Model CL10320
Date of Testing	07.01.2018
Duration of Test (seconds)	205
Average Diameter (mm)	51.3
Average Height (mm)	125
Height to Diameter Ratio	2.5 : 1
Moisture Content (%)	9.1
Wet Mass / Unit Volume (t/m³)	2.28
Dry Mass / Unit Volume (t/m³)	2.09
Uniaxial Compressive Strength (MPa)	3.8
Comments	

Report Number: 81719.09\_1

Issue Number:

Date Issued: 10.01.2018

Client: Multiplex Constructions Pty Ltd

Project Number: 81719.09

Project Name: Proposed New Maitland Hospital

Project Location: Metford Road, Metford

Work Request: 2909
Date Sampled: 14.12.2018

Sampling Method: Sampled by DP Engineering



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Approved Signatory: Peter Gorseski

Approved Signatory: Peter Gorseski NATA Accredited Laboratory Number: 828

Sample Location Depth (m) Rock Description  Storage History and Environment  Compression Machine Date of Testing Duration of Test (seconds) Average Diameter (mm) Average Height (mm) Height to Diameter Ratio Moisture Content (%) Wet Mass / Unit Volume (t/m³) Dunaxial Compressive Strength (MPa)  Comments  Laminite  Tested as Received  Autocon Model CL10320  07.01.2018  200  51.6  Autocon Model CL10320  07.01.2018  200  311  422  423  424  425  426  427  428  428  428  428  437  437  437  437  437  437  437  43	Sample Number	3002	4133.1.1.1	· 等位的图形 (5)的
Rock Description  Laminite  Storage History and Environment  Tested as Received  Orientation to Bedding  Compression Machine Date of Testing Duration of Test (seconds) Average Diameter (mm) Average Height (mm) Height to Diameter Ratio Moisture Content (%) Wet Mass / Unit Volume (t/m³) Dry Mass / Unit Volume (t/m³) Uniaxial Compressive Strength (MPa)  Tested as Received  Autocon Model CL10320 07.01.2018 0	Sample Location	-	Car I	
Storage History and Environment  Tested as Received  Orientation to Bedding  Compression Machine Date of Testing Duration of Test (seconds) Average Diameter (mm) Average Height (mm) Height to Diameter Ratio Moisture Content (%) Wet Mass / Unit Volume (t/m³) Uniaxial Compressive Strength (MPa)  Tested as Received  Autocon Model CL10320 07.01.2018  200  Autocon Model CL10320 07.01.2018  200  311  401  402  403  404  405  406  407  407  408  408  408  408  408  408	Depth (m)	18.0 - 18.25		
Storage History and Environment  Tested as Received  Orientation to Bedding  Compression Machine Date of Testing Duration of Test (seconds) Average Diameter (mm) Average Height (mm) Height to Diameter Ratio Moisture Content (%) Wet Mass / Unit Volume (t/m³) Uniaxial Compressive Strength (MPa)  Tested as Received  Autocon Model CL10320 07.01.2018  200  Autocon Model CL10320 07.01.2018  200  311  401  402  403  404  405  406  407  407  407  408  407  407  407  407	Rock Description			
Orientation to Bedding  Compression Machine Date of Testing Duration of Test (seconds) Average Diameter (mm) Average Height (mm) Height to Diameter Ratio Moisture Content (%) Wet Mass / Unit Volume (t/m³) Duriaxial Compressive Strength (MPa)  Autocon Model CL10320 07.01.2018  200  Autocon Model CL10320 07.01.2018  200  401 200 200 200 211 200 200 200 200 200 2		Laminite	1	
Orientation to Bedding  Compression Machine Date of Testing Duration of Test (seconds) Average Diameter (mm) Average Height (mm) Height to Diameter Ratio Moisture Content (%) Wet Mass / Unit Volume (t/m³) Duriaxial Compressive Strength (MPa)  Autocon Model CL10320 07.01.2018  200  Autocon Model CL10320 07.01.2018  200  401 200 200 200 211 200 200 200 200 200 2				
Compression Machine Date of Testing Duration of Test (seconds) Average Diameter (mm) Average Height (mm) Height to Diameter Ratio Moisture Content (%) Wet Mass / Unit Volume (t/m³) Duration of Test (seconds)  Autocon Model CL10320  07.01.2018  200  131  131  1431  151  161  1731  174  175  175  175  175  175  175  17	Storage History and Environment	Tested as Received		
Date of Testing         07.01.2018           Duration of Test (seconds)         200           Average Diameter (mm)         51.6           Average Height (mm)         131           Height to Diameter Ratio         2.5:1           Moisture Content (%)         9.8           Wet Mass / Unit Volume (t/m³)         2.28           Dry Mass / Unit Volume (t/m³)         2.08           Uniaxial Compressive Strength (MPa)         3.7	Orientation to Bedding	-	1,000	1
Duration of Test (seconds)  Average Diameter (mm)  Average Height (mm)  Height to Diameter Ratio  Moisture Content (%)  Wet Mass / Unit Volume (t/m³)  Dry Mass / Unit Volume (t/m³)  Uniaxial Compressive Strength (MPa)  200  210  211  211  212  213  214  215  216  217  218  218  218  218  218  218  218	Compression Machine	Autocon Model CL10320		
Average Diameter (mm)  Average Height (mm)  Height to Diameter Ratio  Moisture Content (%)  Wet Mass / Unit Volume (t/m³)  Dry Mass / Unit Volume (t/m³)  Uniaxial Compressive Strength (MPa)  51.6  2.5 : 1  9.8  9.8  9.8  9.8  9.8  9.8  9.8  9.	Date of Testing	07.01.2018	(THE PASSE)	
Average Height (mm)  Height to Diameter Ratio  2.5:1  Moisture Content (%)  Wet Mass / Unit Volume (t/m³)  Dry Mass / Unit Volume (t/m³)  Uniaxial Compressive Strength (MPa)  3.7	Ouration of Test (seconds)	200		
Height to Diameter Ratio  Moisture Content (%)  Wet Mass / Unit Volume (t/m³)  Dry Mass / Unit Volume (t/m³)  Uniaxial Compressive Strength (MPa)  2.5 : 1  9.8  2.28  2.08  3.7	Average Diameter (mm)	51.6		
Moisture Content (%)         9.8           Wet Mass / Unit Volume (t/m³)         2.28           Dry Mass / Unit Volume (t/m³)         2.08           Uniaxial Compressive Strength (MPa)         3.7	Average Height (mm)	131		
Wet Mass / Unit Volume (t/m³)  Dry Mass / Unit Volume (t/m³)  2.28  Uniaxial Compressive Strength (MPa)  3.7	Height to Diameter Ratio	2.5 : 1	8 2 2 1 5	
Dry Mass / Unit Volume (t/m³)  Uniaxial Compressive Strength (MPa)  3.7	Noisture Content (%)	9.8		
Uniaxial Compressive Strength (MPa) 3.7	Wet Mass / Unit Volume (t/m³)	2.28		
5.1	Ory Mass / Unit Volume (t/m³)	2.08		
Comments	Jniaxial Compressive Strength (MPa)	3.7		
	Comments			

Report Number: 81719.09\_1

Issue Number:

Date Issued: 10.01.2018

Client: Multiplex Constructions Pty Ltd

Project Number: 81719.09

Project Name: Proposed New Maitland Hospital

Project Location: Metford Road, Metford

Work Request: 2909
Date Sampled: 06.12.2018

Sampling Method: Sampled by DP Engineering



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Approved Signatory: Peter Gorseski

NATA Accredited Laboratory Number: 828

3003	
-	
2.0 - 2.25	
	and the same of th
Laminite	
Tested as Received	The American
-	
Autocon Model CL10320	(A) (基本) (基本)
07.01.2018	
180	
52.7	
132	
2.5 : 1	
11.8	-1- Cream (\$6,070) (A. 17)
2.21	
1.97	
0.8	No market of
	- 2.0 - 2.25  Laminite  Tested as Received  - Autocon Model CL10320 07.01.2018 180 52.7 132 2.5 : 1 11.8 2.21 1.97

Report Number: 81719.09\_1

Issue Number:

Date Issued: 10.01.2018

Client: Multiplex Constructions Pty Ltd

Project Number: 81719.09

Project Name: Proposed New Maitland Hospital

Project Location: Metford Road, Metford

Work Request: 2909
Date Sampled: 12.12.2018

Sampling Method: Sampled by DP Engineering



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Approved Signatory: Peter Gorseski NATA Accredited Laboratory Number: 828

Uniaxial Compressive Strength of Ro	ck Core AS 4133.4.2, AS 4133.	1.1.1
Sample Number	3004	
Sample Location	-	
Depth (m)	7.53 - 7.8	
Rock Description		
	Sandstone	
Storage History and Environment	Tested as Received	
Orientation to Bedding	-	
Compression Machine	Autocon Model CL10320	
Date of Testing	07.01.2018	
Duration of Test (seconds)	177	
Average Diameter (mm)	51.7	
Average Height (mm)	141	A STATE OF THE STA
Height to Diameter Ratio	2.7 : 1	
Moisture Content (%)	11.2	
Wet Mass / Unit Volume (t/m³)	2.29	
Ory Mass / Unit Volume (t/m³)	2.06	
Uniaxial Compressive Strength (MPa)	1.6	The state of the s
Comments		

Report Number: 81719.09\_1

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Date Issued: 10.01.2018

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Project Number: 81719.09

Project Name: Proposed New Maitland Hospital

Project Location: Metford Road, Metford

Work Request: 2909
Date Sampled: 10.12.2018

Sampling Method: Sampled by DP Engineering



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Approved Signatory: Peter Gorseski NATA Accredited Laboratory Number: 828

Sample Number	ck Core AS 4133.4.2, AS 4
Sample Normber Sample Location	-
Depth (m)	5.72 - 6.0
Rock Description	5.72 - 6.0
Rock Description	Laminite
Storage History and Environment	Tested as Received
Orientation to Bedding	-
Compression Machine	Autocon Model CL10320
Date of Testing	07.01.2018
Duration of Test (seconds)	181
Average Diameter (mm)	51.6
Average Height (mm)	133
Height to Diameter Ratio	2.6 : 1
Moisture Content (%)	9.8
Wet Mass / Unit Volume (t/m3)	2.25
Dry Mass / Unit Volume (t/m³)	2.05
Uniaxial Compressive Strength (MPa)	1.1
Comments	

Report Number: 81719.09\_1

Issue Number:

Date Issued: 10.01.2018

Client: Multiplex Constructions Pty Ltd

Project Number: 81719.09

Project Name: Proposed New Maitland Hospital

Project Location: Metford Road, Metford

Work Request: 2909
Date Sampled: 07.12.2018

Sampling Method: Sampled by DP Engineering



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Approved Signatory: Peter Gorseski

NATA Accredited Laboratory Number: 828

Sample Location         -           Depth (m)         2.1 - 2.4           Rock Description         Sandstone           Storage History and Environment         Tested as Received           Orientation to Bedding         -           Compression Machine         Autocon Model CL10320           Date of Testing         07.01.2018           Duration of Test (seconds)         222           Average Diameter (mm)         51.7           Average Height (mm)         130           Height to Diameter Ratio         2.5 : 1           Moisture Content (%)         7.9           Wet Mass / Unit Volume (t/m³)         2.23           Dry Mass / Unit Volume (t/m³)         2.07	No. of the same of
Rock Description  Sandstone  Tested as Received  Orientation to Bedding  Compression Machine Date of Testing Duration of Test (seconds) Average Diameter (mm) Average Height (mm) Height to Diameter Ratio Moisture Content (%) Wet Mass / Unit Volume (t/m³)  Tested as Received  Autocon Model CL10320  O7.01.2018  222  51.7  Autocon Model CL10320  07.01.2018  222  223  44.7  Autocon Model CL10320  07.01.2018  07.01.2018  222  45.7  46.7  47.9  47.9  47.9  47.9	11
Storage History and Environment  Tested as Received  Orientation to Bedding  Compression Machine Date of Testing Duration of Test (seconds) Average Diameter (mm) Average Height (mm) Height to Diameter Ratio  Wet Mass / Unit Volume (t/m³)  Tested as Received  Autocon Model CL10320  07.01.2018  222  51.7  Autocon Model CL10320  07.01.2018  222  225  307  408  Autocon Model CL10320  71.7  409  225  409  409  409  409  409  409  409  40	
Storage History and Environment  Tested as Received  Orientation to Bedding  Compression Machine Date of Testing Duration of Test (seconds) Average Diameter (mm) Average Height (mm) Height to Diameter Ratio  Wet Mass / Unit Volume (t/m³)  Tested as Received  Autocon Model CL10320  07.01.2018  222  51.7  Autocon Model CL10320  07.01.2018  225  107.01.2018  226  227  228  Average Height (mm)  130  2.5 : 1  7.9  Wet Mass / Unit Volume (t/m³)	N STORY OF THE PARTY OF THE PAR
Orientation to Bedding  Compression Machine Date of Testing Duration of Test (seconds)  Average Diameter (mm)  Average Height (mm)  Height to Diameter Ratio  Moisture Content (%)  Wet Mass / Unit Volume (t/m³)  Autocon Model CL10320  07.01.2018  222  51.7  130  2.5 : 1  7.9  2.23	
Orientation to Bedding  Compression Machine Date of Testing Duration of Test (seconds)  Average Diameter (mm)  Average Height (mm)  Height to Diameter Ratio  Moisture Content (%)  Wet Mass / Unit Volume (t/m³)  Autocon Model CL10320  07.01.2018  222  51.7  130  2.5 : 1  7.9  2.23	
Compression Machine         Autocon Model CL10320           Date of Testing         07.01.2018           Duration of Test (seconds)         222           Average Diameter (mm)         51.7           Average Height (mm)         130           Height to Diameter Ratio         2.5 : 1           Moisture Content (%)         7.9           Wet Mass / Unit Volume (t/m³)         2.23	A Land
Date of Testing         07.01.2018           Duration of Test (seconds)         222           Average Diameter (mm)         51.7           Average Height (mm)         130           Height to Diameter Ratio         2.5 : 1           Moisture Content (%)         7.9           Wet Mass / Unit Volume (t/m³)         2.23	W Ato
Duration of Test (seconds)         222           Average Diameter (mm)         51.7           Average Height (mm)         130           Height to Diameter Ratio         2.5 : 1           Moisture Content (%)         7.9           Wet Mass / Unit Volume (t/m³)         2.23	
Average Diameter (mm)  Average Height (mm)  Height to Diameter Ratio  Moisture Content (%)  Wet Mass / Unit Volume (t/m³)  51.7  130  2.5 : 1  7.9  2.23	
Average Height (mm)  Height to Diameter Ratio  Moisture Content (%)  Wet Mass / Unit Volume (t/m³)  130  2.5 : 1  7.9  2.23	
Height to Diameter Ratio         2.5 : 1           Moisture Content (%)         7.9           Wet Mass / Unit Volume (t/m³)         2.23	
Moisture Content (%)  Wet Mass / Unit Volume (t/m³)  2.23	
Wet Mass / Unit Volume (t/m³)	
Dry Mass / Unit Volume (t/m³)	No. of the last of
2.07	ELECTRICAL PROPERTY.
Jniaxial Compressive Strength (MPa) 7.3	
Comments	

Report Number: 81719.09\_1

Issue Number:

Date Issued: 10.01.2018

Client: Multiplex Constructions Pty Ltd

Project Number: 81719.09

Project Name: Proposed New Maitland Hospital

Project Location: Metford Road, Metford

Work Request: 2909
Date Sampled: 12.12.2018

Sampling Method: Sampled by DP Engineering



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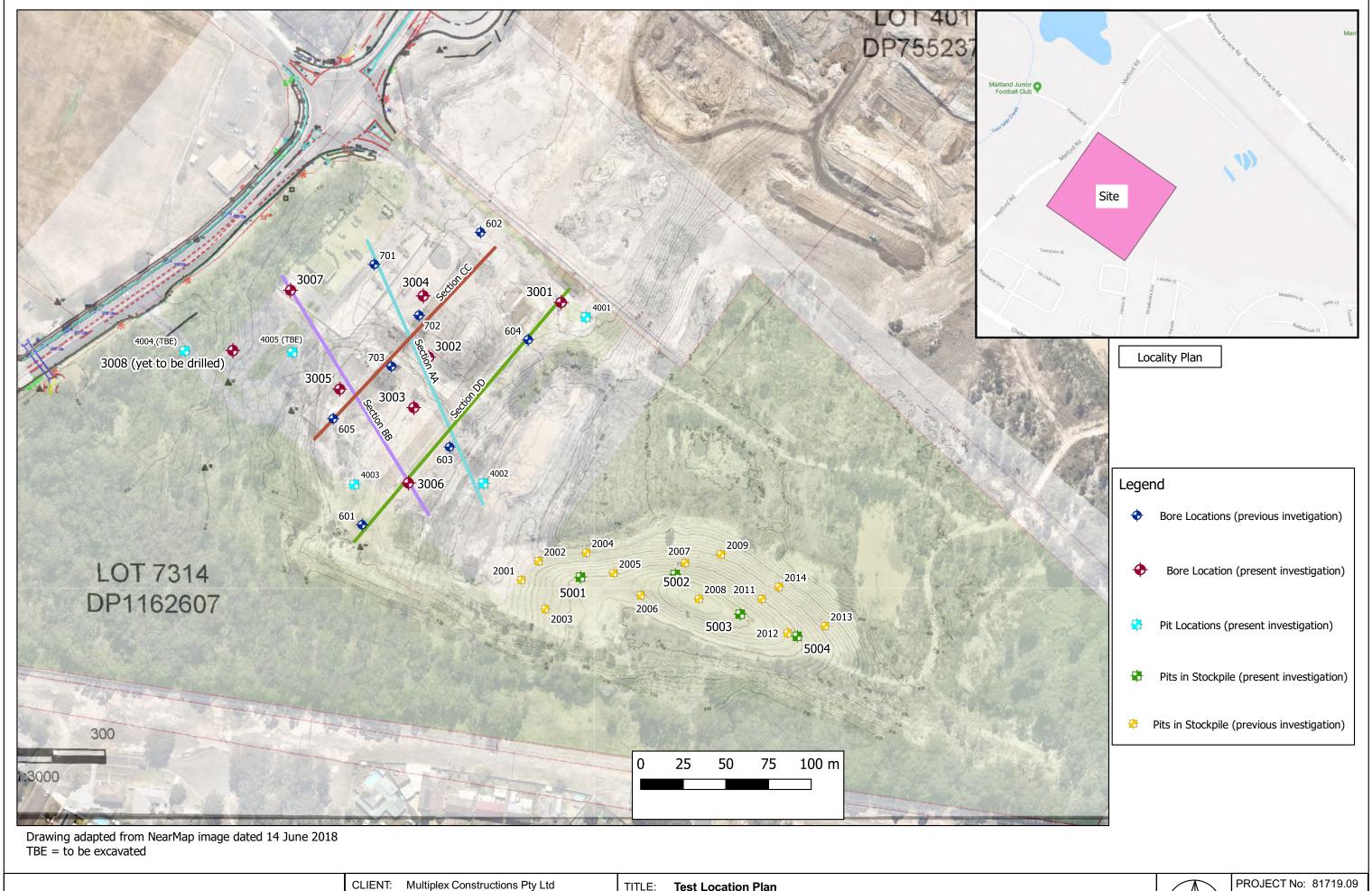
Approved Signatory: Peter Gorseski

NATA Accredited Laboratory Number: 828

Uniaxial Compressive Strength of Ro	ck Core AS 4133.4.2. AS 4
Sample Number	3007
Sample Location	-
Depth (m)	11.45 - 11.71
Rock Description	Sandstone
Storage History and Environment	Tested as Received
Orientation to Bedding	-
Compression Machine	Autocon Model CL10320
Date of Testing	07.01.2018
Duration of Test (seconds)	310
Average Diameter (mm)	51.8
Average Height (mm)	131
Height to Diameter Ratio	2.5 : 1
Moisture Content (%)	2.5
Wet Mass / Unit Volume (t/m³)	2.55
Dry Mass / Unit Volume (t/m³)	2.49
Uniaxial Compressive Strength (MPa)	75.5
Comments	

# Appendix D

Drawing 1 – Test Location Plan Drawings 2 to 6 – Cross-sections A'-A to E'-E



Douglas Partners

Geotechnics | Environment | Groundwater

OFFICE: Newcastle DRAWN BY: MPG

SCALE: 1:2000 @ A3 DATE: 24.12.2018

TITLE: Test Location Plan
Proposed Maitland Hospital
Metford Road, Metford



PROJECT No: 81719.09
DRAWING No: 1
REVISION: 0

