## TECHNICAL PAPER <br> 

## Transport and traffic

ARTC INLAND RAIL

## ALBURY TO ILLABO (A2I) PROJECT

TECHNICAL PAPER 1 TRANSPORT AND TRAFFIC

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## GLOSSARY

| AADT | Average Annual Daily Traffic |
| :---: | :---: |
| AUL | Auxiliary Left-turn treatment |
| AUR | Auxiliary Right-turn treatment |
| BAL | Basic Left-turn treatment |
| BAR | Basic Right- turn treatment |
| CEMP | Construction Environment Management Plan |
| CHL | Channelised Left-turn treatment |
| CHR | Channelised Right-turn treatment |
| CSSI | Critical State Significant Infrastructure |
| CTTAMP | Construction Traffic, Transport and Access Management Plan |
| DDA | Disability Discrimination Act |
| DOS | Degree of Saturation |
| EIS | Environmental Impact Statement |
| EP\&A Act | NSW Environmental Planning and Assessment Act 1979 |
| EPBC Act | Commonwealth Environment Protection and Biodiversity Conservation Act 1999 |
| EPL | Environment protection licence |
| HV | Heavy Vehicle |
| km/h | Kilometres-per-hour |
| LOS | Level of Service |
| PC | Passenger Car |
| PCU | Passenger Car Unit |
| RMAR | Rail Maintenance Access Road |
| RMS | NSW Roads and Maritime Service (now part of TfNSW) |
| RTA | Roads and Traffic Authority (Now TfNSW) |
| SEAR | Secretary's Environmental Assessment Requirements |
| SFAIRP | So Far As Is Reasonably Possible |
| SSI | State Significant Infrastructure |
| TfNSW | Transport for New South Wales |
| TMP | Traffic Management Plan |
| TTIA | Transport and Traffic Impact Assessment |

## DEFINITIONS

| Active level crossing | At grade road crossing of the rail corridor which uses flashing lights and boom barriers for motorists, and automated gates for pedestrians. These devices are activated prior to and during the passage of a train through a level crossing. |
| :---: | :---: |
| Construction environmental management plan | A site-specific plan developed for the construction phase of a project, to ensure that all contractors and sub-contractors comply with the environmental conditions of approval for the project and manage environmental risks properly. |
| Construction compound | An area used as the base for construction activities, usually for the storage of plant, equipment and materials and/or construction site offices and worker facilities. |
| Culvert | A structure that allows water to flow under a road, railway, track, or similar obstruction. |
| Cumulative impacts | Impacts that, when considered together, have different and/or more substantial impacts |
| Down line | Track within a dual-track section of corridor on which trains travel away from Sydney Central station |
| Enhancement site | Discrete sites within the proposal site that are proposed for infrastructure enhancement. |
| Gantry | An overhead metal structure with a frame supporting equipment such as a signals, lighting or cameras. |
| Inland Rail program | The Inland Rail program comprises the design and construction of a new Inland Rail connection between Melbourne and Brisbane, via Wagga, Parkes, Moree, and Toowoomba. The route for Inland Rail is about $1,700 \mathrm{~km}$ in length. Inland Rail will involve a combination of upgrades of existing rail track and the provision of new track. |
| Loop line | Track which briefly leaves the main line and re-join to allow for train passing or access to minor locations. |
| Main line | Primary track on which trains travel within a single-track section of corridor |
| Main South Line | A major rail line between Sydney and Albury, passing through the Southern Highlands, Southern Tablelands, South West Slopes and Riverina regions of NSW. |
| Passive level crossing | At grade road crossing of the rail corridor which uses stop or give way signs for motorists, and 'look for trains' signs for pedestrians. |
| Pedestrian bridge | A bridge designed solely for pedestrians to cross a watercourse, rail corridor or road. |
| Precinct | Groupings of enhancement sites in line with the LGAs including Albury, Greater Hume - Lockhart, Wagga Wagga and Junee. |
| The proposal | Proposed enhancement works to structures and sections of track along 185 kilometres of the existing operational standard gauge railway between Albury and Illabo for the purpose of meeting Inland Rail specifications. |
| The proposal site | The areas that enhancement works are required to operate the Albury to Illabo section of Inland Rail. It includes the location of construction worksites, operational rail infrastructure, new bridge structures, level crossings and other ancillary infrastructure. |

Overbridge

Rail corridor
Study area

Track

A bridge over a railway or road. For the proposal, overbridges refer to those structures which allow a road to pass over the railway.

The corridor within which the rail tracks and associated infrastructure are located The wider area, including and surrounding the proposal site, with the potential to be directly or indirectly affected by the proposal. The extent of the study area varies according to the requirements of each assessment and the potential for impacts.

The structure consisting of the rails, fasteners, sleepers and ballast, which conveys trains.

## EXECUTIVE SUMMARY

## THE PROPOSAL

The Australian Government has committed to delivering a significant piece of national transport infrastructure by constructing a high performance and direct interstate freight rail corridor between Melbourne and Brisbane, via centralwest New South Wales (NSW) and Toowoomba in Queensland. Inland Rail is a major national project that would enhance Australia's existing national rail network and serve the interstate freight market. Inland Rail has been divided into 13 projects, seven of which are located in NSW. Each of these projects can be delivered and operated independently with tie-in points on the existing railway. Australian Rail Track Corporation Ltd (ARTC) ('the proponent') is seeking approval to construct and operate the Albury to Illabo section of Inland Rail ('the proposal').

The proposal involves enhancement works to structures and sections of track along 185 kilometres of the existing operational standard gauge railway to provide the increased vertical and horizontal clearances required for doublestacked freight trains. The proposal is generally within the existing active rail corridor between the towns of Albury and Illabo. Works are proposed at 24 locations along the Main South Line corridor, described as "enhancement sites", within four precincts aligned with the local government areas of Albury, Greater Hume and Lockhart, Wagga Wagga and Junee.

The proposal is State significant infrastructure and is subject to approval by the NSW Minister for Planning under the NSW Environmental Planning and Assessment Act 1979 (EP\&A Act). On 29 June 2020, the Australian Government Department of Agriculture, Water and Environment (DAWE) notified that the proposal is a not controlled action, and hence approval under the EPBC Act is not required.

## THIS REPORT

This report has been prepared by WSP Australia on behalf of ARTC as part of the Environmental Impact Statement (EIS) for the proposal to address the transport and traffic related Secretary's Environmental Assessment Requirements (SEARs) issued by the Secretary of the then NSW Department of Planning Industry and Environment (now the Department of Planning and Environment) for the proposal on 14 October 2020.

This report provides a description of the existing conditions on the transport network and details the expected construction activities and timeframes of the proposal. It provides an impact assessment of peak construction traffic and proposed road closures on the surrounding transport networks, including implications for access, cyclists, pedestrians, and public transport. The report also provides a review of operational impacts, including impacts at level crossings and the number of peak hour vehicles expected to be impacted by a level crossing closure.

Recommended mitigation and management measures are identified in response to the impact assessment findings and are detailed by planning stages of the proposal.

## EXISTING ENVIRONMENT

The proposal site is an approximately 185 km section of existing rail corridor that runs generally north - south between Albury and Illabo, crossing five Local Government Areas (LGAs) Albury City Council, Greater Hume Shire Council, Lockhart Regional Council, Wagga Wagga City Council and Junee Shire Council). The land use throughout the LGAs is predominantly rural land used for agriculture and grazing, with Albury and Wagga Wagga featuring higher density urban environments.

The road network expected to support the proposal is typically local rural roads, State highways (the Hume Highway and the Olympic Highway), and local urban roads within the cities of Albury and Wagga Wagga and the town of Junee. Other key transport facilities within the proposal study area are:

- public transport
- public and school bus services including limited regional services linking rural towns and urban routes within the cities of Albury and Wagga Wagga
- passenger rail services along The Main South Line
- heavy vehicle and Traveling Stock Routes
- provision for active transport in the vicinity of most enhancement sites is minimal, however pedestrian and cyclist networks exist within the urban areas.


## CONSTRUCTION IMPACTS

Construction of the proposal includes 24 individual enhancement sites across four precincts (Albury, Greater Hume and Lockhart, Wagga Wagga and Junee). Typical construction activities at enhancement sites would include:

- site establishment and enabling works
- main construction works as relevant to the enhancement site and
- finishing works with associated activities.

Construction of the proposal would result in a temporary increase in light and heavy vehicle movements on the road network. Light vehicles trips are associated with construction workers moving to and from the enhancement sites. Heavy vehicles would generally be associated with trucks delivering plant or materials to and from the enhancement sites.

Although unlikely to occur, a conservative approach was taken in the assessment of construction vehicle impact on the road network by assuming that peak hour construction vehicle trips would occur during the existing network peak hour. As peak hour construction vehicle trips are low, this showed negligible impact to the performance of surrounding links and intersections, all of which continued to operate with stable flow conditions and an acceptable Level of Service, respectively, and typically with no change to the existing Level of Service.

The road closures and associated diversions required to facilitate construction in Henty, Wagga Wagga, and Junee result in temporary impacts to localised intersection performance, travel times, and public and active transport, particularly in the denser urban area of Wagga Wagga. The Edmondson Street bridge closure in Wagga Wagga, would impact public and school bus routes, stops, and would require bus service rerouting, amended stopping patterns and alternative stop locations. Pedestrian and cycling connectivity would also be affected by the bridge closure.

The low traffic volumes generated from construction activities are not expected to impact the operation of Heavy Vehicle and Travelling stock routes although there may be minor delays from traffic control. Rail freight and passenger services would not be impacted as rail possessions would occur during regularly scheduled maintenance periods. Active transport facilities for pedestrians and cyclists are not expected to be impacted by construction vehicle movements, however the closure of active transport facilities to allow for pedestrian and road bridge replacements within Wagga Wagga and Junee would result in temporary loss of connectivity and travel time impacts.

## OPERATIONAL IMPACTS

The proposal would allow for increases in rail services, with an increase between 2025 and 2040 of up to two daily services.

As the proposal solely provides enhancements to the existing rail line, operational impacts would be associated with:

- increased daily train services resulting in an increased frequency of closures per day at level crossings
- increased delay where level crossings have been upgraded from passive to active.

The proposal would not generate additional traffic during operation; as such, no impacts to the road network performance during operation of the proposal from vehicle movements would occur.

An increase in the number of daily train numbers and therefore the number of times level crossings on public roads are activated is expected during the operation of the proposal. It is anticipated that the maximum closure time encountered at a level crossing (with or without the proposal) would be 121 seconds. An assessment of active level crossing LOS was undertaken and found that all level crossings on public roads will operate at a delay-based LOS of A.

Amendments to the road network as part of the permanent works will not remove any existing turn movements and are not expected to impact on the current capacity, level of service or safety of any intersections. Short stacking deficiencies at the existing level crossings were assessed and some potential storage deficiencies identified.

It is noted that all operation impacts would be expected to occur with and without the proposal, however the potential occurrence of these impacts is expected to increase due to the increase in average rail services per day.

## RECOMMENDED MITIGATIONS

During the design, construction and operational phases of the proposal, mitigation measures have been identified to reduce the impact on the local transport network. During construction of the proposal a Traffic Management Plan (TMP) sub-plan will be prepared as part of the Construction Environmental Management Plan (CEMP) detailing construction sites activities, impacted transport facilities and specifying the mitigation measure. Key mitigation measures that will be undertaken, as far as practicable, include:

- road safety audits where changes to the road network are required or increased traffic movements during the construction phase may present an increased crash risk
- consultation with relevant stakeholders (state, local government, emergency services, transport service providers and impacted property owners)
- heavy vehicle diversionary signage would be implemented to divert Heavy vehicle traffic outside of Junee on the existing heavy vehicle routes via Goldfields Way and Old Junee Road
- community notification of any proposed road or pedestrian network closures and diversions and provision of appropriate wayfinding signage for road and pedestrian diversions, clearly articulating alternative routes
- rectification of pavement where necessary to support diversion of vehicles from the Olympic Highway to local roads in Junee
- restricted access to level crossings for oversize vehicles that may present a short-stacking risk.

With these mitigation measures in place the proposal construction activities are expected to have minimal impact on the transport network. Residual traffic impacts are likely to be experienced during construction of the proposal, particularly associated with road closures and diversions in Wagga Wagga and Junee. The post-construction operation of the proposal has been shown to have no significant impact to the transport network in this assessment.

## 1 INTRODUCTION

### 1.1 OVERVIEW

The Australian Government has committed to delivering a significant piece of national transport infrastructure by constructing a high performance and direct interstate freight rail corridor between Melbourne and Brisbane, via centralwest New South Wales (NSW) and Toowoomba in Queensland. Inland Rail is a major national program that would enhance Australia's existing national rail network and serve the interstate freight market.

The Inland Rail route, which is about 1,700 kilometres long, would involve:

- using the existing interstate rail line through Victoria and southern NSW
- upgrading about 400 kilometres of existing track, mainly in western NSW
- providing about 600 kilometres of new track in northern NSW and south-east Queensland.

Inland Rail has been divided into 13 projects, seven of which are located in NSW. Each of these projects can be delivered and operated independently with tie-in points on the existing railway.

Australian Rail Track Corporation Ltd (ARTC) ('the proponent') is seeking approval to construct and operate the Albury to Illabo section of Inland Rail ('the proposal').

The proposal is Critical State Significant Infrastructure (CSSI) and is subject to approval by the NSW Minister for Planning under Division 5.2, Part 5 of the Environmental Planning and Assessment Act 1979 (EP\&A Act). This report has been prepared as part of the Environmental Impact Statement (EIS) for the proposal. The EIS has been prepared to support the application for approval of the proposal, and address the environmental assessment requirements of the Secretary of the then NSW Department of Planning, Industry and Environment (the SEARs), dated 14 October 2020.

### 1.2 THE PROPOSAL

The proposal involves enhancement works to structures and sections of track along 185 kilometres of the existing operational standard gauge railway between Albury and Illabo. Enhancement works are required to provide the increased vertical and horizontal clearances required for double-stacked freight trains.

### 1.2.1 LOCATION

The proposal is generally within the existing active rail corridor between the town of Albury on the Victorian-NSW border and around three kilometres to the north-east of Illabo. The alignment passes through two major regional towns, Albury and Wagga Wagga, NSW, and several smaller regional towns. Works are proposed at 24 locations along the 'Main South Line' corridor, described as 'enhancement sites'.

The enhancement sites have been broken down into four precincts which align with the local government areas (LGA) of Albury, Greater Hume - Lockhart, Wagga Wagga and Junee, as identified in Table 1.1 and shown in Figure 1.1.

Table 1.1
Enhancement sites

| PRECINCT | ENHANCEMENT SITES |
| :---: | :---: |
| Albury | Murray River bridge |
|  | Albury Station pedestrian bridge |
|  | Albury Yard clearances |
|  | Riverina Highway bridge |
|  | Billy Hughes bridge |
|  | Table Top Yard clearances |
| Greater Hume - Lockhart | Culcairn pedestrian bridge |
|  | Culcairn Yard clearances |
|  | Henty Yard clearances |
|  | Yerong Creek Yard clearances |
|  | The Rock Yard clearances |
| Wagga Wagga | Uranquinty Yard clearances |
|  | Pearson Street bridge |
|  | Cassidy Parade pedestrian bridge |
|  | Edmondson Street bridge |
|  | Wagga Wagga Station pedestrian bridge |
|  | Wagga Wagga Yard clearances |
|  | Bomen Yard clearances |
| Junee | Harefield Yard clearances |
|  | Kemp Street bridge |
|  | Junee Station pedestrian bridge |
|  | Junee Yard clearances |
|  | Olympic Highway underbridge |
|  | Junee to Illabo clearances |

### 1.2.2 KEY FEATURES

The key features of the proposal include:

- adjustments to approximately 44 kilometres of track across 14 enhancement sites to accommodate the vertical and horizontal clearances according to Inland Rail clearance specifications, comprising:
- realignment of track within the rail corridor
- lowering of track up to 1.6 metres at three enhancement sites
- changes to bridges and culverts at enhancement sites to accommodate vertical clearances and track realignment as follows:
- replacement of two road bridges and adjustments to adjoining intersections
- replacement of three pedestrian bridges
- removal of two redundant pedestrian bridges
- modifications to four rail bridges
- ancillary works, including adjustments to nine level crossings, modifications to drainage and road infrastructure, signalling infrastructure, fencing, signage, and services and utilities.

No additional works would be required outside the enhancement sites identified in Figure 1.1 as they meet the clearance requirement for the Inland Rail program.


### 1.2.3 TIMING

Subject to approval, further design and procurement, construction of the proposal is planned to start in early 2024 and is expected to take about 16 months. The proposal would be fully operational in 2025 with enhancement sites progressively commissioned on completion of construction. Inland Rail as a whole would be operational once all 13 sections are complete, which is estimated to be in 2027.

### 1.2.4 CONSTRUCTION

An indicative construction methodology has been developed based on the current design to be used as a basis for the environmental assessment process. Overall, the construction strategy is based on an approach of dividing the proposal into four construction packages which align with the precincts: Albury, Greater Hume - Lockhart, Wagga Wagga and Junee.

Construction of the proposal would require:

- construction compounds, laydown areas and other areas needed to facilitate construction works
- temporary changes to the road network, including road closures to undertake works on road bridges and level crossings
- other ancillary works.

Construction within each precinct would generally involve the site establishment and enabling works, main construction works as relevant to the enhancement site and finishing works as outlined in Table 1.2.

Further information on the construction of the proposal is provided in Chapter 8: Construction of the proposal of the EIS.
Table 1.2 Indicative construction activities

| CONSTRUCTION STAGES | INDICATIVE ACTIVITIES |
| :--- | :--- |
| Site establishment and enabling works | $-\quad$ Establishment of key construction infrastructure, work areas, access |
|  | points and other construction facilities |
|  | - Installation of environmental controls, fencing and site services |
|  | - Preliminary activities including clearing/trimming of vegetation |

### 1.2.5 OPERATION

The proposal would form part of the rail network managed and maintained by ARTC. Train services would be provided by a variety of operators.

The proposal would enable the use of double stacked trains along its entire length. Inland Rail would operate 24 hours per day and would initially accommodate double-stacked freight trains up to 6.5 metres high and up to 1,800 metres in length. The possible future use of the railway between Albury and Illabo by freight trains up to 3,600 metres long would be subject to separate assessment. Freight train speeds would range from 60 to 115 kilometres per hour, which is consistent with current train speeds.

The average number of freight trains movements between Albury and Illabo would increase from a current average of up to 12 per day in 2021 to 18 per day in 2025, further increasing to about 20 per day in 2040.

ARTC would continue to maintain the Main South Line. This would typically involve minor maintenance works, such as bridge and culvert inspections, rail grinding and track tamping, through to major maintenance, such as reconditioning of track and topping up of ballast as required. Maintenance works and schedule are not proposed to change as a result of the proposal and would continue in accordance with the existing Environmental Protection Licence which applies to the rail corridor (EPL 3142).

Further information on the operation of the proposal is in Chapter 7: Proposal features and operation of the EIS.

### 1.3 PURPOSE AND SCOPE OF THIS REPORT

This report has been prepared by WSP Australia as part of the Environmental Impact Statement (EIS) for the proposal to assess Transport and Traffic impacts related to the construction and operation of the Inland Rail corridor between Albury and Illabo.

This traffic and transport assessment addresses the relevant Secretary's Environmental Assessment Requirements (SEARs) issued by the Secretary of the then NSW Department of Planning Industry and Environment (now the Department of Planning and Environment)for the proposal on 14 October 2020. The SEARs relevant to the assessment of Transport and Traffic are presented in Table 1.3.

## Table 1.3 Secretary's Environmental Assessment Requirements - Transport and traffic

## KEY ISSUE ASSESSMENT REQUIREMENT $\quad$ REPORT REFERENCE

1. Transport and Traffic
1) The Proponent must assess construction transport and traffic
(vehicle, pedestrian and cyclists, bus services, and train
operations) impacts, including, but not necessarily limited
to:
a) the likely construction access routes (including haul routes) and scheduling of construction vehicle movements
b) the indicative number, frequency and size of construction related vehicles (passenger, commercial and heavy vehicles, including spoil management movements and track machines)
c) construction worker parking

Access routes are discussed in sections 5.1.1, 5.2.1, 5.3.1, and 5.4.1

Construction vehicle traffic generation is discussed in sections 5.1.1.3, 5.2.1.3, 5.3.1.3 and 5.4.1.3

Construction worker parking is discussed in section 5.1.1, 5.2.2, 5.3.2, and 5.4.2

| KEY ISSUE | ASSESSMENT REQUIREMENT | REPORT REFERENCE |
| :---: | :---: | :---: |
|  | d) the nature of existing traffic (types and number of movements) on construction access routes (including consideration of peak traffic times, movement of livestock, agricultural machinery, farm vehicles and other farm infrastructure, construction deliveries and parking arrangements and sensitive road users) and assessment of traffic impacts on these routes including identifying traffic management measures to mitigate any impacts | Existing transport environment discussed in Chapter 4 |
|  | e) provisions proposed to ensure safe access and egress to/from the classified road network | Enhancement site access assessments are discussed in sections 5.1.3, 5.2.3, 5.3.3, 5.4.3 |
|  | f) the nature of any train paths (types and number of movements) and potential impact to these train paths due to additional track possession requirements | Rail construction impacts are discussed in sections 5.1.10, 5.2.10, 5.3.10, and 5.4.10 |
|  | g) the need to close, divert or otherwise reconfigure elements of the road and cycle network associated with construction of the project and the duration of these changes; and | Closures, diversions, and associated impacts are discussed in sections 5.1.1, 5.2.1, 5.3.1, and 5.4.1 and mitigations are discussed in section 8.2 |
|  | h) impacts to on-street parking, including to residents and businesses. | Construction impacts to parking are discussed in Chapter 5 |
|  | 2) Operational transport impacts of the project (vehicle, pedestrian and cyclists, bus services, and train operations), including: | Operational impacts are discussed in Chapter 6 |
|  | a) forecast travel demand and traffic volumes for the project (road and rail) | Forecast traffic volumes relevant to the operation of the proposal are discussed in section 6.2. |
|  | b) travel time analysis | Travel time impacts relevant to the operation of the proposal are discussed in section 6.3.1. |
|  | c) the performance of key intersections and level crossings by undertaking a level of service analysis at key locations along the project alignment | Performance of key intersections and level crossings relevant to the operation of the proposal are discussed in section 6.3.8.3. |
|  | d) wider transport interactions (local and regional roads, cycling, public and freight transport and the broader NSW rail network) | Impacts to active, public, and freight transport relevant to the operation of the proposal are discussed in Chapter 6 |
|  | e) consideration of how increased train movements would impact level crossings and emergency access across the rail line | Consideration of train movements relevant to the operation of the proposal are discussed in section 6.3 |


| KEY ISSUE | ASSESSMENT REQUIREMENT | REPORT REFERENCE |
| :---: | :---: | :---: |
|  | f) identification of traffic and transport measures to mitigate any impacts. | Mitigation measures are discussed in section 8.2 |
|  | The assessment must include modelling of the operational impact of the project. | Modelling of operational impacts are included throughout Chapter 6 |
|  | 3) Assess the feasibility of level and grade-separated crossings along the project alignment (existing and proposed) and justify the safety and operational impacts and/or benefits of the proposed crossing type, taking into account the NSW Government's Construction of New Level Crossings Policy. | The assessment of level crossings feasibility has been undertaken separately to this transport impact assessment; it is discussed in section 6.3 and the process undertaken by ARTC is provided in section 3.3 and Appendix A. <br> Operational impacts of level crossings are assessed in section 6.3.8 |
|  | 4) In the assessment of level crossings, the EIS must: |  |
|  | a) provide a safety assessment for each level crossing. The safety assessment is to be consistent with ALCAM and any Interface Agreements and Safety Management Plans | The assessment of safety of level crossings has been undertaken separately to this transport impact assessment; it is discussed in section 6.3 and the process undertaken by ARTC is provided in Appendix A. |
|  | b) demonstrate how the risks would be reduced So Far As Is Reasonably Practical (SFAIRP) in consultation with the relevant road authority | The assessment of safety of level crossings has been undertaken separately to this transport impact assessment; it is discussed in section 6.3 and the process undertaken by ARTC is provided in Appendix A. |
|  | c) assess potential short-stacking impacts | Short-stacking assessment relevant to operation of the proposal is performed in section 6.3.5. |
|  | d) confirm road approaches to level crossings are fit for purpose, safe and designed and constructed in accordance with Austroads Guide to Road Design | Design elements are discussed and detailed within the relevant design reports. |
|  | e) account any rationalisation of private and public level crossings in line with the NSW Government's Level Crossing Closure Policy. | N/A - No rationalisation of private and public level crossings is included in the proposal. |

### 1.4 STRUCTURE OF THIS REPORT

The structure of the report is as follows:

- Chapter 1 - Introduction - provides an introduction to the report.
- Chapter 2 - Legislation and policy context - describes the legislative and policy context for the assessment and relevant guidelines.
- Chapter 3 - Methodology - describes the methods and assessment criteria adopted in this report to characterise and assess potential impacts on the transport network.
- Chapter 4 - Existing environment - describes the existing transport network environment including road, rail and public transport services.
- Chapter 5 - Construction impact assessment - identifies and assesses potential transport network impacts from construction of the proposal.
- Chapter 6 - Operational impact assessment - identifies and assesses potential transport network impacts from operation of the proposal.
- Chapter 7 - Cumulative impacts - details cumulative impact on adjacent Inland Rail projects/other proposed major developments during Construction and Operation.
- Chapter 8 - Mitigation and management measures - details recommended mitigation and management measures to reduce transport network impacts.
- Chapter 9 - Conclusion - overview of the key findings of the report.


## 2 LEGISLATION AND POLICY CONTEXT

### 2.1 COMMONWEALTH LEGISLATION

### 2.1.1 ENVIRONMENT PROTECTION AND BIODIVERSITY CONSERVATION ACT 1999

Under the EPBC Act, proposed 'actions' that have the potential to significantly impact on matters of national environmental significance, the environment of Commonwealth land, or that are being carried out by an Australian Government agency, must be referred to the Australian Minister for the Environment for assessment.

Preliminary environmental investigations identified threatened species under the EPBC Act which have the potential to be impacted by the proposal. As a result of the potential for impacts on protected matters, the proposal was referred to the (then) Australian Minister for the Environment on 2 June 2020 (EPBC Referral No 2020/8670). On 29 June 2020, the Australian Government Department of Agriculture, Water and the Environment (DAWE) notified that the proposal is a not controlled action, and hence approval under the EPBC Act is not required.

### 2.2 NSW STATE LEGISLATION

### 2.2.1 ENVIRONMENTAL PLANNING AND ASSESSMENT ACT 1979

The EP\&A Act and Environmental Planning and Assessment Regulation 2021 (EP\&A Regulation) establish a framework for the assessment and approval of developments in NSW.

The proposal has been declared as Critical State Significant Infrastructure (CSSI) and is subject to approval by the Minister for Planning under Division 5.2, Part 5 of the EP\&A Act. An EIS has been prepared for the proposal to assess the impacts of the proposal in accordance with the SEARs. This technical paper supports the EIS.

### 2.2.2 ROADS ACT 1993

The Roads Act 1993 (Roads Act) aims to establish the rights of members of the public to pass along public roads, rights of persons who own land adjoining a public road to have access to the public road, and to establish the procedures for the opening and closing of a public road. The Roads Act also aims to provide a structure for the classification of roads, empower the public agencies such as Transport for NSW as the road authorities and regulate the carrying out of various activities on public roads, including the transportation of construction materials with heavy vehicles.

This proposal is consistent with this legislation by ensuring that the appropriate processes and measures are in place to manage the impacts to users of the public roads, property owners and the opening/closing of public roads.

Consent from the appropriate road authority is required under section 138 of the Roads Act for certain activities, such as disturbing the surface of a public road, or carrying out work in, on or above a public road. Section 138 of the Roads Act, does not apply for works that relate to the exercise of a public authority's functions in, on or over an unclassified road (other than a Crown road) (Schedule 2 of the Roads Act). However, ARTC is not a public authority for the Roads Act. Section 5.24 of the EP\&A Act provides that a section 138 Roads Act consent cannot be refused for a State significant infrastructure project for which planning approval has been given, and any section 138 consent must not be inconsistent with the terms of that planning approval.

### 2.3 POLICIES, GUIDELINES AND STANDARDS

### 2.3.1 STRATEGIC POLICIES

### 2.3.1.1 FUTURE TRANSPORT STRATEGY 2056

Future Transport Strategy 2056 (TfNSW 2018a) provides a 40-year strategy outlining a vision and strategic directions for the transport system in NSW. In particular, Inland Rail is discussed as a major focus of Australian governments, providing an enhanced link between Melbourne and Brisbane and supporting intermodal hubs in regional NSW.

### 2.3.1.2 NSW FREIGHT AND PORTS PLAN 2018-2023

Key objectives of the NSW Freight and Ports Plan 2018-2023 (TfNSW 2018b) are to increase economic growth, increase efficiency, connectivity and access, greater freight capacity, improved safety and enhanced sustainability. The accompanying Implementation Plan includes supporting the delivery of Inland Rail. The NSW Freight and Ports Plan 2018-2023 recognises investment the east-west rail freight network to NSW ports is critical to optimising the benefits of the Inland Rail project for NSW and the Plan details several measures recommended to maximise the benefits of Inland Rail.

### 2.3.1.3 REROC REGIONAL FREIGHT TRANSPORT PLAN

The REROC Regional Freight Transport Plan (Riverina Joint Organisation (RivJO) 2019) and the Riverina Eastern Regional Organisation of Councils (REROC) to provide guidance on transport and freight management planning for the eastern Riverina region of NSW. The Plan covers the following Local Government Areas: Bland, Coolamon, Cootamundra-Gundagai, Greater Hume, Junee, Lockhart, Temora and Wagga Wagga.

### 2.3.2 GUIDELINES

### 2.3.2.1 GUIDE TO TRAFFIC GENERATING DEVELOPMENT, VERSION 2.2

The Guide to Traffic Generating Development, Version 2.2 (RTA 2002) outlines the appropriate methodology for conducting traffic impact studies and compiling traffic impact statements. It also includes a checklist style table of information required to conduct such studies (Table 2.1 in the guide) which this TTIA has adhered to, where relevant to the project. The guide has been adopted as the overarching methodology in producing the TTIA and method for calculation of link LOS.

### 2.3.2.2 GUIDE TO TRAFFIC MANAGEMENT, PARTS 1-13

The Austroads Guide to Traffic Management - Parts 1-13 (Austroads 2020) provide comprehensive traffic management guidance for practitioners involved in traffic engineering, road design and road safety. Guidance adopted in this TTIA to address the SEARs requirements includes methodologies for Integrated Transport Assessments for Developments, methods and criteria for calculation of LOS, link capacity and performance and determining the need for auxiliary lanes at intersections based on through and turning vehicle volumes.

### 2.3.2.3 CYCLING ASPECTS OF AUSTROADS GUIDES

Cycling Aspects of Austroads Guides (Austroads 2017) provides information that relates to the planning, design and traffic management of cycling facilities sourced from Austroads Guides, primarily the Guide to Road Design, the Guide to Traffic Management and the Guide to Road Safety. Its use is intended as a guide for planning, design, construction and management of cycling facilities. As this Transport Impact Assessment is not an input into the design of the proposal this guide has not been used in the assessment.

### 2.3.2.4 NSW BICYCLE GUIDELINES V 1.2

The NSW Bicycle Guidelines V 1.2 (RTA 2005) is provided as a guide to practitioners on how bicycle network facilities should be developed as part of the wider NSW transportation network. It lists the government's four strategies as:

- improving the bike network by making provisions for cyclists on new major road infrastructure projects
- making it safer to cycle
- improving personal and environmental health by promoting benefits of cycling; and
- raising the community awareness of the importance of cycling and raising community involvement.

As this Transport Impact Assessment is not an input into the design of the proposal this guide has not been used in the assessment.

### 2.3.2.5 NSW SUSTAINABLE DESIGN GUIDELINES VERSION 4.0

The NSW Sustainable Design Guidelines (TfNSW 2017) seek to incorporate sustainable development practices into the design and construction of transport infrastructure projects. Key aims of the guidelines are to:

- minimise impacts of transport on the environment, through transport operations, infrastructure delivery and maintenance
- ensure development, expansion and management of the transport network is sustainable and resilient to climate change; and
- procure, deliver and promote sustainable transport options that achieve value for money and reduced life cycle costs.

The aims of this guideline have been considered within the other elements of assessment undertaken as part of the EIS which included climate change and sustainability assessment.

### 2.3.2.6 PLANNING GUIDELINES FOR WALKING AND CYCLING

The Planning Guidelines For Walking And Cycling (DIPNR 2004) aims to improve consideration of walking and cycling in the planning of new infrastructure. The guideline has been designed to provide a walking and cycling focus to the NSW Government's Integrating Land Use and Transport Planning Policy Package. It is primarily targeted at land-use planners and development on private land. As this Transport Impact Assessment is not an input into the design of the proposal this guide has not been used in the assessment.

### 2.3.2.7 AUSTRALIAN LEVEL CROSSING ASSESSMENT MODEL: LEVEL CROSSING ASSESSMENT HANDBOOK

The Australian Level Crossing Assessment Model (ALCAM) (National ALCAM Committee 2017) is a tool used to identify potential key risks at level crossings and assess the overall effects of proposed treatments. It does not specify what treatment is warranted at level rail-road crossing sites nor attempt to define a 'safe' or acceptable level of risk. It is a risk model used to support a decision-making process, with the decision to be made for each jurisdiction based on the standard of existing crossings, upgrade budgets and the level of risk prepared to be tolerated. ALCAM assessments have been undertaken for all public road level crossings proposed as part of the proposal as part of the design process.

### 2.3.2.8 CONSTRUCTION OF NEW LEVEL CROSSING POLICY

The purpose of Construction of New Level Crossing Policy (TFNSW 2014) is to provide guidance and direction to transport planners and infrastructure managers in the ongoing development and management of the NSW rail network. The approach taken by TfNSW and rail and road agencies is to avoid building new level crossings wherever possible given the inherent risk attached to any level crossing, even those with modern active controls. Although upgrades of passive to active level crossings are included, no new level crossings are proposed as part of the scope of works.

### 2.3.2.9 RAILWAY CROSSING SAFETY SERIES 2011, PLAN: ESTABLISHING A RAILWAY CROSSING SAFETY MANAGEMENT PLAN

The Railway Crossing Safety Series 2011, Plan: Establishing A Railway Crossing Safety Management Plan (RTA 2011) outlines the process, procedures and tools required to meet the legislative, occupational health and safety and project management requirements for safety at railway crossings. The planning and management of safety risks, safety management measures and railway crossing safety management plans requires a systematic planning approach, involving collaboration with both internal and external stakeholders. This plan has been considered throughout the proposal to maximise safety outcomes at railway crossings.

## 3 METHODOLOGY

### 3.1 ASSESSMENT PROCESS

To assess the impact of the construction and operation of the proposal on the existing transport network (road, rail, public and active transport) the following methodology, based on the Guide to Traffic Management Part 12: Integrated Transport Assessments for Developments (RTA 2002), is adopted. This process consists of:

- identification of study area
- documentation of the existing transport environment
- documentation of expected construction movements
- estimation of future (construction and operational horizons) baseline traffic volumes
- assessment of construction impacts to existing transport environment
- assessment of operational impacts to existing transport environment
- assessment of cumulative impacts to existing transport environment
- development of mitigation measures.


### 3.1.1 STUDY AREA

The study area for this Transport and Traffic Impact Assessment has been identified as the transport networks that may be impacted by construction movements to the enhancement sites, required diversions or by the operation of the proposal (staff and maintenance movements and level crossing closures). As construction workforce and material origins are expected to be widely distributed across the broader region, the study area is identified as those roads and associated transport facilities (e.g. parking, active transport, heavy vehicle, public transport networks) which provide access to the enhancement sites, back to the nearest highway. Beyond this point, the construction traffic is expected to diminish as it is distributed across the broader network to multiple origins and represents no measurable impact.

### 3.1.2 EXISTING TRAFFIC AND TRANSPORT ENVIRONMENT

The existing traffic and transport environment has been documented for each enhancement site within the identified study area, including:

- link characteristics including controlling agency, geometric configurations, and key connections
- key intersections
- crash history near the proposal or on roads expected to support construction or operational activities using online TfNSW data
- on-street and parking facilities expected to support construction or operational activities based on aerial imagery and Google Street View
- the rail network and services based on TfNSW online information
- daily flow profiles for rural areas
- seasonal variation in traffic demands
- observed or estimated traffic volumes sourced from:
- TfNSW online traffic volumes viewer (adopted traffic volumes range from 2006 to 2018)
- Annual Average Daily Traffic (AADT) volumes provided by local councils (provided traffic volumes range from 2010 to 2020)
- 24-hour (to identify daily flow profiles and peak period volumes) and 10-hour peak period (to provide peak period traffic flows) traffic surveys were undertaken from the $22^{\text {nd }}$ to the $24^{\text {th }}$ of June 2021). Surveys were not taken in the Greater Hume-Lockhart precinct as existing data (listed above) was sufficient to complete traffic analysis. Surveys were undertaken at the following locations:
- Albury precinct
- East Street and Atkins Street (10 hour)
- Young Street and Smollet Street (10 hour)
- Guinea Street and Hume Highway NB on off ramps (10 hour)
- Wagga Wagga precinct
- Sturt Highway and Olympic Highway and Pearson Street (10 hour)
- Glenfield Road and Fernleigh Road (10 hour)
- Edward Street and Docker Street (10 hour)
- Docker Street and Bourke Street and Coleman Street (10 hour)
- Edward Street and Best Street (10 hour)
- Coleman Street and Edmondson Street and Mitchelmore Street (24-hour)
- Urana Street and Bourke Street (10 hour)
- Junee precinct
- Olympic Highway and Seignior Street and Kemp Street (24-hour)
- Olympic Highway and Seignior Street and Broadway Street (10 hour).

Where traffic volume data was not available, traffic volumes used for the assessment have been estimated based on recorded traffic volumes on adjacent road segments, roads within the study area that have a similar configuration and serve a similar function, or as proportions of higher order roads in proximity (considering road type, connectivity and surrounding land uses).

It is noted that traffic volumes have been affected in many areas by changes in travel behaviour due to COVID-19. These changes are considered unlikely to affect the traffic surveys procured for this project as no travel restrictions were in place during the survey periods.

At a precinct level, the following transport facilities have been detailed:

- Travelling Stock Reserves near the proposal or on roads expected to support construction or operational activities using NSW Local Land Services, Travelling Stock Reserves (TSR) online mapping software
- heavy vehicle routes near the proposal or on roads expected to support construction or operational activities using NSW (RMS) online heavy vehicle restricted access vehicles map
- public transport infrastructure and services near the proposal or on roads expected to support construction or operational activities (rail and bus)
- active transport infrastructure near the proposal or on roads expected to support construction or operational activities
- existing rail freight and passenger rail service movements.


### 3.1.3 IDENTIFICATION OF EXPECTED CONSTRUCTION VEHICLE MOVEMENTS

Construction activity and associated generated traffic movements has been identified:

- review of forecast workforce and construction vehicle types, quantities and staging:
- locations for construction sites and lay down areas
- construction staging and the peak period of construction
- construction worker parking locations
- construction worker accommodation is expected to be dispersed in the local community
- identification of peak construction workforce light vehicle (assuming an average vehicle occupancy of 1.5) and heavy vehicle volumes - typically during a track possession.


### 3.1.4 ESTIMATION OF FUTURE BASELINE TRAFFIC VOLUMES

Estimation of future baseline traffic has been undertaken through application of a compounding annual growth rate to observed and estimated existing traffic volumes for:

- 2024 - peak year of construction
- 2025 and 2040 - year of opening and 15 year operational horizons.

The growth rates applied have been developed through analysis of historic growth rates and consultation with state and local government representatives. Further detail of growth rates and application to observed volumes is provided in section 4.2.3.

### 3.1.5 ASSESSMENT OF CONSTRUCTION IMPACTS

Construction activities would generate vehicle movements, including light and heavy vehicles. Light vehicles trips would be generated by construction workers moving to and from the enhancement sites. Heavy vehicle movements would generally be associated with trucks delivering plant or materials to the enhancement sites. Impacts expected to occur as a result of the construction of the proposal have been assessed as follows:

- Link (mid-block) LOS assessment of construction routes with and without the proposal, during the peak period of construction for each enhancement site, using the method outlined in the Guide to Traffic Generating Developments Version 2.2 (RTA 2002) where:
- the total volumes of the highest hour of construction generated traffic are assessed against the background traffic peak hour for each part of the proposed access route
- total peak hour construction traffic flows have been assumed as the highest flows expected during the construction duration, typically during rail possession periods
- light vehicles would have an average occupancy of 1.5 worker per vehicle and would all arrive or depart within the background peak hour. This adoption of the background peak hour for assessment of the arrival/departure of the workforce is assumed to be a worst-case scenario for workforce arrivals as expected construction start and finish times end outside of typical peak periods
- to maintain the worst-case scenario assessment each potential access route has been assessed with the total expected light and heavy vehicles expected to arrive/depart within this peak hour with no proportioning of expected traffic volumes across multiple access routes
- where available, the highest peak hour period background traffic volumes from 2021 counts have been utilised, where this information is not available, a $10 \%$ proportion of AADT flows (two way, $5 \%$ one way) has been adopted. This is considered a conservative approach as assessed (see section 4.2.1) network peak hour flows are less than this proportion.
- Access intersections turn warrant assessments adopting peak construction demands as per the link assessment for each enhancement site using the method outlined in the Guide to Traffic Management - Part 6 Intersection, Interchanges and Crossings (Austroads 2020) to provide guidance on the appropriate access intersection form as:
- Basic Left-turn treatment (BAL)
- Basic Right- turn treatment (BAR)
- Auxiliary Left-turn treatment (AUL)
- Auxiliary Right-turn treatment (AUR)
- Channelised Left-turn treatment (CHL)
- Channelised Right-turn treatment (CHR).
- Intersections along the construction route, during the peak period of construction (typically the possession period), using SIDRA modelling software. Only the heaviest trafficked intersections (on a per lane basis) or those deemed most likely to be affected by construction traffic were assessed in each precinct to reduce needless assessment. The process for selecting the intersections for each enhancement site is described in the relevant sections in Chapter 5. The intersection assessment has assessed peak hour construction traffic in conjunction with peak hour background traffic as per the link assessment to create a worst-case scenario, as expected construction start and finish times are outside of typical peak periods.
- Construction related temporary diversions in relation to:
- peak hour road performance
- peak hour intersection performance using SIDRA modelling software
- travel time impacts.
- Qualitative assessment of the impacts to road safety.
- Qualitative assessment of the impacts to parking facilities.
- Qualitative assessment of impacts to other transport facilities:
- rail movements
- heavy vehicle routes
- Travelling Stock Reserves
- public transport networks, including impacted bus stops, school bus stops and drop off areas
- active transport networks.

Details of performance criteria and standards adopted for the construction impact assessment are outlined in section 3.2.

### 3.1.6 ASSESSMENT OF OPERATIONAL IMPACTS

Assessment of construction and operation impacts to transport networks expected to occur as a result of the operation of the proposal have been undertaken for:

- Road link and intersection operations - qualitative assessment of expected impacts from additional daily rail services and the associated maintenance and operational staff movements resulting from the proposal.
- Level crossings in the vicinity of enhancement sites:
- feasibility of level crossings (existing and proposed)
- calculation of expected closure time and number of peak period impacted vehicles at each public road level crossing for the operational horizon years of 2025 and 2040
- SIDRA analysis of level crossings assessing LOS and average delay and queue lengths
- safety assessment for each level crossing in accordance with ALCAM and any Interface Agreements and Safety Management Plans
- sight lines at all modified level crossings checked in accordance with the methodology documented in Appendix D of Australian Standard AS1742.7 - Manual of uniform traffic control devices Railway crossings
- demonstrate how the risks would be reduced So Far As Is Reasonably Practical (SFAIRP) in consultation with the relevant road authority plans
- potential for short stacking deficiencies.
- Other transport facilities - qualitative assessment of expected impacts from additional daily rail services and the associated maintenance and operational staff movements resulting from the proposal.


### 3.1.7 ASSESSMENT OF CUMULATIVE IMPACTS

In addition to assessment of the proposal impacts in isolation, the cumulative impacts of the proposal in conjunction with other projects within proximity to the proposal site has been undertaken. This qualitative cumulative impact assessment includes:

- review of the relevant traffic and transport aspects of concurrent projects in the region
- qualitative assessment of the cumulative impacts from the construction/operation of the proposal and these projects.


### 3.1.8 DEVELOPMENT OF MITIGATION MEASURES

Proposal specific mitigations have been developed to reduce the likelihood or severity of impacts to the surrounding transport networks and their users during the construction and operation of the proposal. The developed mitigations have been designed to be implemented at various stages of the proposal from pre-construction to operation.

### 3.2 IMPACT ASSESSMENT CRITERIA AND PERFORMANCE STANDARDS

It is understood that the proposed redevelopment is not a typical traffic generating development, however, the overarching methodology and performance standards from the Guide to Traffic Generating Developments (RMS 2002) and the Austroads Guide to Traffic Management (Austroads 2020) are used to inform the assessment of the transport networks. Key analysis methods and metrics are described in the following sections.

### 3.2.1 LINK ASSESSMENTS

The assessment of the road (mid-block) network performance has been performed in relation to Level of Service (LOS) for the road links and intersections with and with the project traffic generated during the construction and operational period. LOS metrics are detailed in Table 3.1.

Table 3.1 Level of Service description (Guide to Traffic Generating Developments (RMS 2002))

| LEVEL OF <br> SERVICE | DESCRIPTION |
| :---: | :--- |
| A | Free flow in which individual drivers are virtually unaffected by the presence of others in the traffic <br> stream. Freedom to select desired speeds and to manoeuve within the traffic stream is extremely high, <br> and the general level of comfort and convenience provided is excellent. |
| B | Stable flow and drivers still have reasonable freedom to select their desired speed and to manoeuvre <br> within the traffic stream, although the general level of comfort and convenience is little less than that of <br> the level of Service A. |
| C | Stable flow, but most drivers are restricted to some extent in their freedom to select their desired speed <br> and to manoeuvre within the traffic stream. The general level of comfort and convenience declines <br> noticeably at this level. |
| D | Close to the limit of stable flow but is approaching unstable flow. All drivers are severely restricted in <br> their freedom to select their desired speed and to manoeuvre within the traffic stream. The general level of <br> comfort and convenience is poor, and small increases in traffic flow will generally cause operational <br> problems. |
| E | Traffic volumes are at or close to capacity and there is virtually no freedom to select desired speeds or to <br> manoeuve within the traffic stream. Flow is unstable and minor disturbances within the traffic stream <br> will cause a traffic-jam. |
| F | This service level is in the zone of forced flow. With it, the amount of traffic approaching the point under <br> consideration exceeds that which can pass it. Flow break-down occurs, and queuing and delays result. |

The Guide to Traffic Generating Developments (RTA 2002) notes that during peak periods on weekdays on major and minor rural roads LOS C is the performance standard. LOS D is noted as the performance standard on weekends.

Local urban road link LOS will be assessed using Table 4.4 from the Guide to Traffic Generating Developments (RTA 2002) (shown in Table 3.2) to calculate a peak hour.

Table 3.2 Link LOS adapted from The Guide to Traffic Generating Developments (2002) Table 4.4

| LOS | ONE LANE PER DIRECTION <br> (VEH/HR) | TWO LANE PER DIRECTION <br> (VEH/HR) |
| :---: | :---: | :---: |
| A | 200 | 900 |
| B | 380 | 1,400 |
| C | 600 | 1,800 |
| D | 900 | 2,200 |
| E | $>900$ | 2,800 |

Local rural road link LOS will be assessed using Table 4.5 from the Guide to Traffic Generating Developments (RTA 2002) (shown in Table 3.3) to calculate a peak hour, peak direction LOS peak direction LOS assuming 10 per cent Heavy Vehicle proportions and level terrain.

Table 3.3 Link LOS adapted from The Guide to Traffic Generating Developments (2002) Table 4.5

| LOS | ONE LANE (VEH/HR) |
| :---: | :---: |
| B | 590 |
| C | 920 |
| D | 1,480 |
| E | $>1,480$ |

Highway road link LOS has been calculated based on Table 5.5 of the Guide to Traffic Management Part 3, (Austroads 2020) as shown in Table 3.4 for an road of 80 kilometres-per-hour ( $\mathrm{km} / \mathrm{h}$ ). It is noted that the criteria for Highways is based on Passenger Car Units (PCU), which has been accounted for by factoring expected background and proposal vehicle demands to PCUs based on heavy vehicles percentages and a PCU factor of 2.

Table 3.4 Highway Capacity Manual Highway peak hour flows per lane direction LOS criteria

| LEVEL OF SERVICE | MAXIMUM SERVICE FLOW (PCU/LN/HR) |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | A | B | C | D | E |
| $80 \mathrm{~km} / \mathrm{h}$ | 550 | 900 | 1,300 | 1,710 | 2,000 |

### 3.2.2 INTERSECTION ASSESSMENTS

Intersection LOS assessment for the heaviest trafficked intersection within each work precinct has been undertaken using SIDRA intersection software based on Delay based LOS, with reporting on the average delay, Degree of Saturation (DOS) and LOS by approach, as output by the SIDRA analysis for each intersection under assessment for base and during project construction scenarios.

LOS is defined in SIDRA as:
An index of the operational performance of traffic on a given roadway, traffic lane, approach, intersection, route or network, based on measures such as delay and degree of saturation etc. during a given flow period. This provides a quantitative stratification of a performance measure or measures that represent quality of service, measured on an A to F scale, with LOS A representing the best operation conditions from the traveller's perspective and LOS F the worst.

Delay is defined in SIDRA as:
The additional (excess) travel time experienced by a vehicle or pedestrian relative to a base travel time, e.g. the free-flow travel time. Average delay considering all vehicles or pedestrians that are queued and not queued is a common performance measure used for intersection and network analysis.

Degree of Saturation (DOS) is defined in SIDRA as:
The ratio of arrival (demand) flow rate to capacity during a given flow period. Also, known as the volume to capacity ratio ( $\mathrm{v} / \mathrm{c}$ ration), utilisation ratio, utilisation factor and traffic intensity.
$95^{\text {th }}$ Percentile Queue Length is defined in SIDRA as:
The $95^{\text {th }}$ percentile queue length is the value below which 95 percent of all observed cycle queue lengths fall, or 5 per cent of all queue lengths exceed.

Table 4.2 of the Guide to Traffic Generating Developments (RTA 2002), shown as Table 3.5 below, sets out average delays for different levels of service.

Table $3.5 \quad$ Level of service criteria for intersections (Table 4.2 of RTA 2002)

| LEVEL OF <br> SERVICE | AVERAGE DELAY PER <br> VEHICLE (SECS/VEH) | TRAFFIC SIGNALS, <br> ROUNDABOUT | GIVE WAY \& STOP SIGNS |
| :---: | :---: | :--- | :--- |
| A | $<14$ | Good Operation | Good Operation |
| B | 15 to 28 | Good with acceptable delays \& spare <br> capacity | Acceptable delays \& spare <br> capacity |
| C | 29 to 42 | Satisfactory | Satisfactory, but accident study <br> required |
| D | 43 to 56 | Operating near capacity | Near capacity \& accident study <br> required |
| E | 57 to 70 | At capacity; at signals, incidents will <br> cause excessive delays <br> Roundabouts require other control <br> mode | At capacity, requires other <br> control mode |

RTA 2002 notes 'any particular assessment should take into account site-specific factors including maximum queue lengths (and their effect on lane blocking), the influence of nearby intersections and the sensitivity of the location to delays'.

All intersections which operate between LOS A and LOS C (to cover the range between LOS A: good operation, LOS B: acceptable and LOS C: satisfactory) or where no change has been noted as a result of the proposal are referred to as operating with an 'acceptable' Level of Service in this assessment.

### 3.2.3 SITE ACCESS ASSESSMENTS

The appropriateness of the proposed work site accesses has been undertaken based on The Guide to Traffic Management - Part 6 Intersection, Interchanges and Crossings (Austroads 2020) which provides guidance for determining the need for auxiliary lanes at intersections based on through and turning vehicle volumes. The 'major road traffic volume' (QM) is required to determine the need for auxiliary lanes at intersections. Figure 2.27 in this guide (shown in Figure 3.1) provides the calculation for QM on two-lane, two-way roads. This turn warrant assessments have been undertaken at the access intersection with the highest combined construction and background peak hour volumes within each work precinct. The AM peak period has been adopted for the assessment, and construction vehicles turning into the enhancement sites would impact traffic on the adjacent road network, while the impact of exiting construction vehicles in the PM peak would be confined to queuing within the enhancement site.

Figure 2.27: Calculation of the major road traffic volume $Q_{M}$


Figure 3.1 Calculation of the major road traffic volume QM

### 3.2.4 ROAD SAFETY ASSESSMENT

This study has primarily considered the operation and capacity of the road network rather than the appropriateness of use of certain roads by construction vehicles. A separate risk assessment and Road Safety Audit (RSA) will be required to be undertaken by the contractor for each enhancement site prior to commencement of construction activities on site to ensure the safety of all road users is considered. A review of historical crash data for a five-year period (2015-2019) has been taken from Transport for New South Wales (TfNSW) crash and causality statistics site for the roads in the vicinity of the enhancement sites. The data was used to identify locations on the road network expected to be used to support the construction or operational activities related to the proposal that may require addressing, in relation to road safety, during construction activities.

### 3.2.5 OTHER TRANSPORT FACILITIES

Set assessment or performance criteria were not adopted for impacts to other transport facilities in the vicinity of the proposal. However potential impacts to these facilities have been qualitatively assessed and detailed for construction and operation periods and considered:

- parking facilities
- heavy vehicle routes
- Travelling Stock Reserves
- public transport routes (Rail and bus)
- active transport routes and infrastructure
- property access.


### 3.2.6 LEVEL CROSSINGS

Impacts resulting from level crossings on public roads have been assessed for a 2025 and 2040 operational horizon based on expected maximum closure time during a train passing and the expected number of vehicles that would be stopped at the level crossing while a train is passing. Assessment elements adopted for determining impacts from level crossings on public roads were:

- maximum expected closure time based on level crossing activation times
- average numbers of vehicles impacted during a peak hour level crossing closure
- SIDRA assessment of LOS, average delay and average queue length
- potential short stacking.


### 3.3 LEVEL CROSSING ASSESSMENT

### 3.3.1 ASSESSMENT OF LEVEL CROSSINGS

Public road rail interfaces are points where the rail alignment crosses a public road. The proposal would require the crossing of state-controlled roads, local government roads as well as road controlled by Crown Lands and the Forestry Corporation of NSW.

The Construction of New Level Crossings Policy (TfNSW 2014) notes that building new level crossings is to be avoided wherever possible, and all other options, including grade separation and use of existing level crossings, should be explored before a new crossing is proposed.

Therefore, a methodical process of review was undertaken by ARTC to determine the appropriate treatment at public road-rail interfaces in the vicinity of enhancement sites within the study area, in consultation with potentially impacted landowners.

Considerations in the review process included:

- determining the interface location and type: i.e. public roads, private access roads, farm tracks, pedestrian interfaces and travelling stock routes
- assessing the need for the interface: Legal and physical access to both properties and severed properties is retained, potential traffic levels, land use, nearby interfaces, adjoined properties, vertical geometry of the rail alignment (in the context of the property and access for other local connectivity)
- determining feasible options for public road interfaces.

The process for identifying and assessing feasible options for public road interfaces broadly involved the following main steps:

- identifying opportunities for grade separation
- determining locations where provision of a level crossing would not be practicable and where road closures or realignments are likely to be required
- determining the preferred type of level crossings treatments (i.e. active or passive).

Further information on these steps is provided below.

### 3.3.2 OPPORTUNITIES FOR GRADE SEPARATIONS

ARTC's policy is that rail-road interfaces would be automatically grade separated in the following three instances:

- rail-road crossings with four rail tracks
- rail-road crossings of freeways and highways of four or more lanes (current and committed future plans)
- where grade separation is the logical option for topographical or engineering reasons.

Provision of grade separations were considered where the height between the existing road and the proposed rail line was sufficient to provide for the required legal clearance for road traffic.

### 3.3.3 LOCATIONS WHERE PROVISION OF A LEVEL CROSSING WOULD NOT BE REASONABLY PRACTICABLE

This step involved identifying where:

- provision of a new level crossing was not possible due to height differences between the road and rail
- provision of a new level crossing was not possible due to the location of crossing loops
- road crossings were closely spaced along the rail line and could be consolidated into a single crossing.

Generally, public roads would be retained wherever possible. However, where public roads cross the proposal rail corridor, the road would need to be closed in the following instances:

- the road exists only as a road reserve and is not being used as a road (i.e. no formed road exists) or required for legal access
- grade separation and raising/lowering the road is not reasonably practicable
- providing a level crossing on the existing road alignment would not be possible
- there is a nearby grade separation or level crossing enabling diversion of the road.

Formed public roads would only be proposed for closure where the impact of diversions or consolidations is considered acceptable, or the existing location is not considered safe and cannot be reasonably made safe.

### 3.3.4 DETERMINING THE PREFERRED LEVEL CROSSING TREATMENTS

Where it has been determined that a level crossing is the preferred solution, a consistent methodology which aligns with the Office of the National Rail Safety Regulator guidelines (2016) has been used to develop proposed level crossing treatments.

This approach involves applying the Australian Level Crossing Assessment Model (ALCAM) to determine the 'risk score' for each level crossing, and then undertaking cost-benefit analysis to assess whether higher levels of protection are justified (e.g. upgrade passive protection to active, active to grade separation).

ALCAM is the nationally accepted risk tool for level crossings which looks at a range of factors including road and rail volumes and speeds, heavy vehicle use, sighting distances and road/rail geometry. The road inputs are validated by the relevant road manager through the stakeholder consultation process.

The ALCAM assessment has been carried out separate to this TTIA. The requirement to minimise safety risks is an ongoing process that must be adhered to in future design changes.

Level crossings would be provided with warning signage, line marking, and other relevant controls; in accordance with the relevant ARTC and Australian standards. Through the application of this process, the safety risks would be eliminated or minimised SFAIRP.

In accordance with Rail Safety National Law (NSW) No 82a requirements, public road crossings would be subject to an Interface Agreement with the relevant road manager in order to ensure that safety risks are also identified and minimised so far as is reasonably practicable during the operations phase.

The interface agreements would be prepared to cover each public road crossing location to ensure a formal written agreement between the responsible road and/or rail managers is in place consistent with the requirements of section 105 of the Rail Safety National Law (NSW) No 82a, including responsibilities of parties for implementing safety measures and a process for monitoring these.

Further information regarding the methodology undertaken to determine the preferred level crossing treatments is provided in Appendix A.

## 4 EXISTING ENVIRONMENT

### 4.1 REGIONAL CONTEXT

The proposal site includes discreet enhancement sites located on the existing The Main South Line. These sites are located over a total distance of about 185 km , between the towns of Albury and Illabo. The proposal site is located within five Local Government Areas (LGAs):

- Albury City Council
- Greater Hume Shire Council
- Lockhart Regional Council
- Wagga Wagga City Council
- Junee Shire Council.

Albury is located at the southern extent of the proposal in the Albury City Council LGA, north of the Murray River on the border of NSW and Victoria, both of which separate the city from the neighbouring Victorian city of Wodonga. Illabo is a small town located at the northern end of the proposal, located within Junee Shire council. The proposal also includes the major town of Wagga Wagga and smaller towns of Culcairn, Henty, Yerong Creek, The Rock, Uranquinty, Bomen, Harefield and Junee. The land use throughout the LGAs is predominantly rural land used for agriculture and grazing, with Albury and Wagga Wagga featuring higher density urban environments. An overview of the regional road and rail network is presented in Figure 4.1 and shows the north south connectivity between the urban areas along the proposal is provided by:

- Hume Highway - connecting to Melbourne and Sydney and running through Albury, connecting to the Olympic Highway 18 km north of Albury. The Hume Highway is generally four lanes and in 2018 carried approximately 11,400 vehicles per day on average in the Albury precinct
- Olympic Highway, which runs generally north south from the Hume Highway connecting to Culcairn, Henty, Yerong Creek, The Rock, Uranquinty, Bomen, Wagga Wagga, Harefield and Junee. The Olympic Highway is generally two lanes and in 2011 carried approximately 2,800 vehicles per day on average in the Greater Hume Lockhart precinct.
- The Main South Line runs from Albury to Sydney, passing through each of the work precincts. Operational stations within the study area are located at Albury, Culcairn, Henty, The Rock, Wagga Wagga, and Junee.

The east-west connections are provided by a network of roads including the Sturt Highway and Riverina Highway, as well as regional arterial roads. Movements within urban areas are facilitated by a supporting network of local roads.


### 4.2 TRAFFIC CHARACTERISTICS

Regional historic traffic data was analysed to establish an understanding of the directionality and proportion of AADT flows that is experienced in the peak period in the region. This analysis informed estimates of peak hour traffic volumes along key roads around the enhancement sites where traffic surveys have not been undertaken, as described in section 3.1.2. Availability of recent and complete historical data for regional and rural daily and seasonal traffic analysis is limited in the area of the proposal, with the most recent and complete data available identified at the Hume Highway (Site ID: ALBSTC) count site, sourced from the TfNSW traffic volume viewer. This count site is taken as representative of the background regional traffic environment and the existing traffic characteristics.

### 4.2.1 DAILY TRAFFIC VOLUME FLOW PROFILE

A daily traffic volume flow profile has been developed using the most recent, complete data recorded (January to September, 2018) using data from the Hume Highway (Site ID: ALBSTC) as shown in Figure 4.2. This daily flow profile shows that northbound and southbound traffic follows broadly similar profiles, with no significant peaks in traffic activity, although volumes are generally highest in the mid-afternoon. The highest proportion for two-ways flows is under 8 per cent of the AADT and the highest directional flow is 4 per cent of AADT. Based on this, a 5 per cent proportion of AADT has been adopted to calculate a one-way peak hour flow for highways and rural roads. It is noted that this data was not available for other roads near the proposal, however, this site is expected to provide a reasonable representation of traffic flows across a day on highways and in rural areas.


Figure 4.2 Percentage of AADT by hour - Hume Highway at Table Top (2018 - excluding October - December)
It is noted this count site represents a daily flow profile outside of urban areas. Additional data has been collected from traffic survey within the Albury, Wagga Wagga and Junee which has been used to determine peak hour flows within these urban areas.

### 4.2.2 SEASONAL TRAFFIC

Seasonal variations to daily traffic flows are expected to occur associated with such factors as agricultural production, freight movement and tourism. Limited information is available to understand seasonal variations in traffic flows within the study area, however the most recent complete calendar year (2017) of traffic volumes from the Hume Highway at Table Top (Site ALBSTC) are presented in Figure 4.3 showing average daily traffic flow per month. The analysis of monthly variation in traffic flows shows that although variation is evident, there is relatively low change in total or heavy vehicle monthly flows across the year and it is not expected that seasonal variations shown would have a significant effect on the impact assessment undertaken.

Similar representative data was not available for other roads in or near the study area, however, the Hume Highway in this location provides a good indication of activity along the north south corridor and it is expected that the wider highway and regional road network supporting the region would have similar seasonal variations to that shown for Hume Highway. It is noted that the performance of rural roads within the study area is less likely to be affected by seasonality, mostly due to the lower baseline traffic volumes expected on these roads.

As discussed in Chapter 12: Land use and property of the EIS, land use surrounding the proposal includes a high proportion of agriculture, including grazing, and cropping land. Traffic generated by these land uses can be highly seasonal and timed around harvesting periods or transportation of livestock to market. Traffic generated during these periods can include heavy vehicles associated with transportation of agricultural product, machinery, farm vehicles, and other farm infrastructure as well as increased light vehicle movements from the seasonal workforce. Review of seasonal change in vehicle movements for the Hume Highway did not identify a significant seasonal trend, however this may be more pronounced in discreet local areas. Transportation of agricultural product also occurs within some enhancement sites, where vehicles transport grain and other produce to the rail line for transportation by train. Further discussion of agricultural infrastructure, grain silos or agricultural produce storage and transportation facilities relevant to each precinct is provided in Chapter 5.

Temporary events may result in periodical influxes of vehicles to an area. Technical paper 4: Social identified a number of events scheduled to occur which may result in vehicles travelling roads relevant to the proposal. Predominantly, these events occur in the urban areas of Albury, Wagga and Junee.


Figure 4.3

### 4.2.3 TRAFFIC GROWTH RATES

Historic growth rates within the study area have been collected from several sources including:

- Advice from TfNSW
- Advice from Junee Shire and Albury City Council
- TfNSW Traffic viewer counts.

The advice received during discussions with TfNSW representatives suggested that a 2 per cent per annum compounding growth rate would be acceptable on State controlled roads in some areas, however a 3 per cent per annum compounding growth rate would be more appropriate in Wagga Wagga and Albury.

Junee Shire Council provided advice in relation to expected growth rates with the local area ranging from 1 per cent to 2 per cent per annum compounding. Advice from Albury City Council suggested a 1.7 per cent growth rate on Local roads in the area surrounding Table Top.

In addition to the advice from transport agencies detailed above, historic data from the most recent and complete count site for the region for the Hume Highway at Table Top (Site ID: ALBSTC) from 2010 to 2018 was assessed to determine historic annual compounding growth rates as shown in Table 4.1. This site is considered to provide a good representation of growth along the north south corridor and it is expected that the wider road network supporting the study area would have similar growth characteristics.

Table 4.1 Hume Highway at Table Top (Site ID: ALBSTC) average historic growth rates to 2018

| PERIOD | AVERAGE GROWTH RATE (\%) |
| :---: | :---: |
| 1-year | 1.2 |
| 2-year | 2.2 |
| 3-year | 3.0 |
| 8-year | 3.0 |

Based on the provided advice and analysis of historic growth rates, the growth rates shown in Table 4.2 have been adopted for extrapolation of observed traffic volumes to the construction and operational horizon years for roads within the study area each work precinct.

Table 4.2 Adopted growth rates

| WORK PRECINCT | ADOPTED GROWTH RATES | DISCUSSION |
| :--- | :--- | :--- |
| Albury | $3 \%$ - Highways <br> $2 \%-$ Other roads | As per TfNSW advice and highest observed <br> Hume Highway historical growth rate for state- <br> controlled roads. <br> As per Albury City advice for local roads. |
| Greater Hume - Lockhart | $3 \%$ - Highways <br> $3 \%-$ Other roads | As per TfNSW advice and highest observed <br> Hume Highway historical growth rate. |
| Wagga Wagga | $3 \%$ - Highways <br> $3 \%-$ Other roads | As per TfNSW advice and highest observed <br> Hume Highway historical growth rate. |
| Junee | $1.5 \%$ - Highways <br> $2 \%-$ Byrnes Road <br> $1 \%-$ Other roads | As per Junee Shire Council advice. |

### 4.3 ALBURY PRECINCT

Albury precinct includes the following enhancement sites:

- Murray River bridge
- Albury Station pedestrian bridge
- Albury Yard clearances
- Riverina Highway bridge
- Billy Hughes bridge
- Table Top Yard clearances.

Due to their proximity, Albury Station pedestrian bridge, Albury Yard clearances, and Riverina Highway bridge were considered collectively (referred to as Albury Station and surrounds).

The existing traffic and transport network relevant to Albury precinct is discussed in the following sections.

### 4.3.1 ROAD NETWORK

Enhancement sites within Albury precinct are connected by the Hume Highway. The enhancement sites and key road links are shown below in Figure 4.4.


### 4.3.1.1 MURRAY RIVER BRIDGE ENHANCEMENT SITE

The key road links and intersections expected to support the construction or operational movements related to the proposal for the Murray River bridge enhancement site are depicted below in Figure 4.5. Key road characteristics are described in Table 4.3 and key intersection configurations are shown in Appendix C.

Table 4.3 Key road links - Murray River bridge enhancement site
$\begin{array}{|l|l|}\hline \text { ROAD } \\ \text { NAME }\end{array} \quad$ ROAD DESCRIPTION $\left.\quad \begin{array}{l}\text { Atkins } \\ \text { Street }\end{array} \begin{array}{l}\text { Two-way, two lane urban locally controlled street with sections running both north-south and east-west. } \\ \text { The north-south section runs from Hume Street, crosses East Street and connects to the east-west section } \\ \text { that runs through south Albury to Townsend Street, crossing Kiewa, Olive, and Macauley Streets, and } \\ \text { providing access to industrial areas in South Albury. } \\ \text { In the vicinity of the enhancement site the north-south section of the road generally features 3.6m wide } \\ \text { lanes, sealed shoulders, and has a posted speed limit of 60km/h. The east-west section generally features a } \\ \text { l2m sealed width, sealed shoulders with parking, and has a posted speed limit of 50km/h. }\end{array}\right\}$

| ROAD |
| :--- | :--- |
| NAME |$\quad$ ROAD DESCRIPTION



## TRAFFIC VOLUMES

Observed traffic volumes for the roads expected to support the construction or operational movements related to the Murray River bridge enhancement site are shown below in Table 4.4.

Table 4.4 Murray River bridge enhancement site observed traffic volumes

| ROAD NAME | COUNT YEAR | DAILY (TWO-WAY) <br> VOLUME | HV PROPORTION |
| :--- | :---: | :---: | :---: |
| East Street $^{1}$ | 2021 | 10,991 | $5 \%$ |
| Atkins Street $^{1}$ | 2021 | 3,297 | $14 \%$ |
| Hume Highway $^{2}$ | 2007 | 21,501 | Not available |
| Macauley Street $^{3}$ | 2021 | 330 | $14 \%$ |
| Panmure Street $^{3}$ | 2021 | 330 | $14 \%$ |
| Abercorn Street $^{3}$ | 2021 | 330 | $14 \%$ |
| Kiewa Street $^{4}$ | 2021 | 989 | $14 \%$ |
| Townsend Street $^{3}$ | 2021 | 330 | $14 \%$ |
| Olive Street $^{4}$ | 2021 | 989 | $14 \%$ |

(1) 10 -hour ( 5 am to 10 am and 2 pm to 7 pm ) traffic survey volumes
(2) Hume Highway - 120m East of Olive Street, South Albury 2640. This is the most recent data publicly available for an urban location on the Hume Highway in Albury
(3) No data available, volumes estimated as $10 \%$ of Atkins Street 10 -hour with equivalent HV proportion
(4) No data available, volumes estimated as $30 \%$ of Atkins Street 10-hour with equivalent HV proportion.

## ROAD SAFETY

Figure 4.6 shows the crashes that occurred in the data collection period in the vicinity of the Murray River bridge enhancement site, with the following observations

- Hume Highway around the East Street interchange (key road link and intersection) - 13 crashes
- Kiewa Street (key road link) - four crashes
- Kiewa Street (key road link) - one fatal crash occurring in 2018.

It is noted that the Hume Highway also carries a high volume of vehicles (relative to the rest of the network), increasing the overall likelihood of crash occurrence.


Source: https://roadsafety.transport.nsw.gov.au/statistics/interactivecrashstats
Figure 4.6 Crash data (2015-2019) Murray River bridge enhancement site

## PARKING

On-street kerbside parking is generally allowed on the local road network in the vicinity of the Murray River bridge enhancement site and demand for this parking would be low due to provision of off-street parking within commercial, industrial, retail, and residential uses in the surrounding area. There is no designated parking within the enhancement site.

### 4.3.1.2 ALBURY STATION AND SURROUNDS

The key road links and intersections expected to support the construction or operational movements related to the proposal for the Albury Station and surrounds are depicted below in Figure 4.7. Key road characteristics are described in Table 4.5 and key intersection configurations are shown in Appendix C.

Table 4.5 Key road links - Albury Station and surrounds

| ROAD NAME | ROAD DESCRIPTION |
| :--- | :--- |
| Young Street | Two-way, four lane state-controlled street that forms part of the Riverina Highway and runs <br> north-south between North Street and Atkins Street, crossing Dean Street, Wilson Street and <br> Borella Road and provides access to commercial areas and Albury Railway Station. <br> In the vicinity of the enhancement site the road generally features 3.4m wide lanes, sealed <br> shoulders with parking, and has a posted speed limit of 60km/h. |
| Borella Road (Riverina <br> Highway) | Two-way, four lane state-controlled road that forms part of the Riverina Highway and that runs <br> east-west from Young Street, crossing the rail line and Hume Highway via a road overpass and <br> provides access to Albury Airport, residential and commercial areas in East Albury. <br> In the vicinity of the enhancement site the road generally features 3.2m wide lanes, sealed <br> shoulders with parking, and has a posted speed limit of 60km/h between Young Street and <br> Drome Street, and 80km/h west of Drome Street. |
| Hume Highway | Two-way, four lane state-controlled urban highway that runs from Melbourne in the southwest <br> and Sydney in the northeast. In Albury the Hume Highway includes interchanges at East Street, <br> Riverina Highway, Racecourse Road, and Thurgoona Road. <br> In the vicinity of the enhancement site the single lane northbound off ramp to Borella Road <br> generally features a 3.6m wide lane, sealed shoulders, and has a posted speed limit of 110km/h. |
| Smollet Street | Two-way, two lane urban locally controlled street that runs east-west from Young Street and <br> provides access to the Albury Railway Station. <br> In the vicinity of the enhancement site the road generally features 3.5m wide lanes, sealed <br> shoulders with parking, and a posted speed limit of 50km/h. |
| Railway Place) | Two-way, two lane urban locally controlled street running north-south between Borella Road <br> and East Street and provides access to residential areas in Albury east of the rail line and Hume <br> Highway. <br> In the vicinity of the enhancement site the road generally features a 11.8m sealed width, limited <br> line marking, sealed shoulders with parking, and has a posted speed limit of 50km/h. |
| Schubach Street | Two-way, two lane urban locally controlled street that runs east-west, from Schubach Street <br> and provides and eastern access to the Albury Station pedestrian bridge. <br> In the vicinity of the enhancement site the road generally features a 11.8m sealed width, limited <br> line marking, sealed shoulders with parking, and has a posted speed limit of 50km/h. |



## TRAFFIC VOLUMES

Observed traffic volumes for the roads expected support the construction or operational movements related to the proposal for the Albury Station and surrounds are shown below in Table 4.6.

Table 4.6 Albury Station and surrounds observed traffic volumes

| ROAD NAME | COUNT YEAR | DAILY (TWO-WAY) <br> VOLUME | HV <br> PROPORTION |
| :--- | :---: | :---: | :---: |
| Young Street $^{1}$ | 2021 | 7,496 | $3 \%$ |
| Smollet Street (Railway Place) $^{1}$ | 2021 | 472 | $3 \%$ |
| Borella Road $^{1}$ | 2021 | 13,894 | $3 \%$ |
| Hume Highway Northbound Off Ramps $^{1}$ | 2021 | 3,668 | $5 \%$ |
| Schubach Street $^{2}$ | 2021 | 3,297 | $14 \%$ |
| Kenilworth Street $^{3}$ | N/A | 50 | Not available |

(1) 10-hour ( 5 am to 10 am and 2 pm to 7 pm ) traffic survey volumes
(2) No data available, volumes estimated as Atkins Street 10-hour with equivalent HV proportion
(3) Estimated traffic volume based on road type and surrounding land uses

## ROAD SAFETY

Figure 4.8 shows the crashes that occurred in the data collection period in the vicinity of the Albury Station and surrounds, with the following observations:

- Hume Highway around the Borella Road (Riverina Highway) interchange (key road links and intersection) 15 crashes around the interchange
- Young Street/Borella Road intersection (key road links and intersection) - seven crashes around the interchange
- no fatal crashes are noted in the vicinity of this enhancement site.

It is noted that the areas with a greater occurrence of crashes are also roads carrying a high volume of vehicles (relative to the rest of the network), increasing the overall crash exposure risk.


Source: https://roadsafety.transport.nsw.gov.au/statistics/interactivecrashstats
Figure $4.8 \quad$ Crash data (2015-2019) Albury Station and surrounds

## PARKING

On-street kerbside parking is generally allowed on the road network in the Albury Station and surrounds unless signed otherwise and there may be some competition for this parking in higher demand areas such as near the railway station, although off street parking is present within commercial, industrial and retail uses within the surrounding area. Further detail of parking on key roads expected to support construction or operational activities related to the proposal is provided in Table 4.7.

Table 4.7 Parking provision - Albury Station and surrounds

| LOCATION | PARKING | RESTRICTIONS |
| :---: | :---: | :---: |
| Young Street | Kerbside parking | 2P ${ }^{1}$ 8:30am - 6 pm Monday - Friday; 8:30am - 12:30pm Saturday |
| Borella Road | Kerbside parking east of East Street | No Restrictions |
| Hume Highway and ramps | No parking | N/A |
| Albury Station parking on Railway Place and Smollett Street | Informal station parking to the north of the Albury Station pedestrian bridge: approximately 13 spaces <br> Short-term kerbside station parking: 21 spaces <br> Short-term parking in front of station: 24 spaces (including two disabled spaces) <br> Taxi parking in front of station: three spaces <br> Albury Station Visitor Centre parking: 28 spaces (including one disabled space) <br> Designated parking to south of station building: 61 spaces (including two disabled spaces) <br> Caravan parking: approximately two spaces <br> Long-distance coach parking: four bays <br> Recreational vehicle servicing: five bays | Informal: Unsigned <br> Short-term kerbside parking: 2P <br> 8:30am - 6pm Monday - Friday; <br> 8:30am - 12:30pm Saturday <br> Short-term parking in front of station: 16 quarter-hour parking, others unknown <br> Albury Station Visitor Centre parking: Unsigned <br> Designated parking to south of station building: Unsigned <br> Caravan parking: Unsigned <br> Long-distance coach parking: Unsigned <br> Recreational vehicle servicing: Unsigned |
| Schubach Street | Kerbside Parking | No Restrictions |
| Kenilworth Street | Kerbside Parking | No Restrictions |

(1) Two-hour parking

### 4.3.1.3 BILLY HUGHES BRIDGE ENHANCEMENT SITE

The key road links and intersections expected to support the construction or operational movements related to the proposal for the Billy Hughes bridge enhancement site are depicted below in Figure 4.9. Key road characteristics are described in Table 4.8 and key intersection configurations are shown in Appendix C.

Table 4.8 Key road links - Billy Hughes bridge enhancement site

| ROAD NAME | ROAD DESCRIPTION |
| :---: | :---: |
| Wagga <br> Road | Two-way, two lane road state-controlled rural road generally running north-south between Mate Street in Lamington and the Hume Highway northbound on ramps at Ettamogah and crossing the Hume. <br> In the vicinity of the Billy Hughes bridge enhancement site the road generally features 3.9 m wide lanes, sealed shoulders, and has a posted speed limit of $100 \mathrm{~km} / \mathrm{h}$. |
| Hume <br> Highway | Two-way, four lane state-controlled highway with existing north-facing ramps at Wagga Road and southfacing ramps currently under construction and due to be completed in late 2021. <br> In the vicinity of the Billy Hughes bridge enhancement site the single lane northbound on ramp from Wagga Road generally features a 3.5 m wide lane, sealed shoulders, and has a posted speed limit of $100 \mathrm{~km} / \mathrm{h}$, increasing to $110 \mathrm{~km} / \mathrm{h}$ near the Hume Highway main alignment. |
| R W Henry Drive | Two-way, two lane road council controlled rural road generally running north-south adjacent Wagga Road to the south and Hume Highway to the north. <br> In the vicinity of the Billy Hughes bridge enhancement site the road generally features 3.9 m wide lanes, sealed shoulders, and has posted advisory warning speed limit of $65 \mathrm{~km} / \mathrm{h}$ for a $100 \mathrm{~km} / \mathrm{h}$ speed limit rural road. |

## TRAFFIC VOLUMES

Observed traffic volumes for the roads expected support the construction or operational movements related to the proposal for the Billy Hughes bridge enhancement site are shown below in Table 4.9. Where published AADT data was not available or considered inappropriate, estimations based on comparable locations, as detailed in section 3.1.4, are presented.

Table $4.9 \quad$ Billy Hughes bridge enhancement site observed traffic volumes

| ROAD NAME | COUNT YEAR | DAILY (TWO -WAY) | HV PROPORTION |
| :--- | :---: | :---: | :---: |
| Wagga Road $^{1}$ | 2006 | 5,392 | Not Available |
| Hume Highway $^{2}$ | 2018 | 11,529 | $32 \%$ |
| R W Henry Drive |  |  |  |

(1) No data available, volumes estimated as Wagga Road - 110m South of Waldner Court, Lavington
(2) No data available, volumes estimated as Hume Highway - 200m North of Ford Lane, Table Top
(3) No data available, volumes estimated as $10 \%$ of Wagga Road - 110m South of Waldner Court, Lavington


| $50 \quad 100$ |  |
| :---: | :---: |
| Coordinate System: GDA 1994 MGA Zone 55 |  |
|  |  |
|  |  |
|  |  |
|  |  |
|  |  |
| Date: 3/11/2021 | Paper: A3 |
| Author. WSP | Scale: 1:5,00 |
| Data Sources: AR |  |

Proposal site
Existing railway
Main road
Local road
Key intersection
Key road links

## INLAND RAIL

The Austraian Govermment is delivering inland Rail through the Australian Rail Track Corporation (ARTC) in parnership with the private sector.

## ROAD SAFETY

Figure 4.10 shows the crashes that occurred in the data collection period in the vicinity of the Billy Hughes bridge enhancement site. It is noted that an insufficient number of crashes were recorded to identify any significant observations in the in the vicinity of this enhancement site.


Source: https://roadsafety.transport.nsw.gov.au/statistics/interactivecrashstats
Figure 4.10 Crash data (2015-2019) Billy Hughes bridge enhancement site

## PARKING

Within the rural areas in the vicinity of the Billy Hughes bridge enhancement site there is limited provision of on street parking and demand for this parking would be low due to provision of off-street parking within commercial and industrial areas. There is no designated parking within the enhancement site. Further detail around parking on key links is provided below in Table 4.10.

Table 4.10 Parking provision - Billy Hughes bridge enhancement site

| LOCATION | PARKING | TIME OF DAY RESTRICTIONS |
| :--- | :--- | :--- |
| Wagga Road | No formal provision however no limitation <br> on verge parking where space allows | No Restrictions |
| Hume Highway and ramps | Emergency stopping only | N/A |
| R W Henry Drive | No formal provision however no limitation <br> on verge parking where space allows | No Restrictions |

### 4.3.1.4 TABLE TOP YARD CLEARANCES ENHANCEMENT SITE

The key road links and intersections expected to support the construction or operational movements related to the proposal for the Table Top Yard clearances enhancement site are depicted below in Figure 4.11. Key road characteristics are described in Table 4.11 and key intersection configurations are shown in Appendix C.

Table 4.11 Key road links - Table Top Yard clearances enhancement site

| ROAD NAME | ROAD DESCRIPTION |
| :--- | :--- |
| Perryman Lane | Two-way, two lane locally controlled rural road that runs generally north south from Tynan Road and <br> provides access to rural properties in Table Top. <br> In the vicinity of Table Top Yard clearances enhancement site the road generally features 3.3 m wide <br> lanes, sealed shoulders, and has a posted speed limit of $100 \mathrm{~km} / \mathrm{h}$. |
| Tynan Road | Two-way, two lane locally controlled rural road that runs generally east west between Gregory Road <br> and the Hume Highway and provides access to rural properties and cross connectivity within Table <br> Top via a rail level crossing west of the Hume Highway. <br> In the vicinity of Table Top Yard clearances enhancement site the road generally features a 6.4 m <br> sealed width, unsealed shoulders, and has a posted speed limit of $80 \mathrm{~km} / \mathrm{h}$. |
| Hume Highway <br> and ramps | Two-way, four lane state-controlled highway that connects to Tynan Road via an at-grade intersection. <br> In the vicinity of Table Top Yard clearances enhancement site the Highway and features 3.7 m wide <br> lanes, sealed shoulders, and has a posted speed limit of $110 \mathrm{~km} / \mathrm{h}$. |



## TRAFFIC VOLUMES

Observed traffic volumes for the roads expected support the construction or operational movements related to the proposal for the Table Top Yard clearances enhancement site are shown below in Table 4.12.

Table 4.12 Table Top Yard clearances enhancement site observed traffic volumes

| ROAD NAME | COUNT YEAR | DAILY (TWO-WAY) <br> VOLUME | HV <br> PROPORTION |
| :--- | :---: | :---: | :---: |
| Perryman Lane $^{1}$ | 2018 | 576 | $32 \%$ |
| Tynan Road $^{2}$ | 2013 | 655 | Not available |
| Hume Highway $^{3}$ | 2018 | 11,529 | $32 \%$ |

(1) No data available, volumes estimated as 5\% of Hume Highway with equivalent HV proportion
(2) Tynan Road - between Gerogery Road and Perryman Lane, Table Top
(3) Hume Highway - 200 m North of Ford Lane, Table Top

## ROAD SAFETY

Figure 4.12 shows the crashes that occurred in the data collection period in the vicinity of the Table Top Yard clearances enhancement site, with the following observations noted:

- Tynan Road/Hume Highway intersection (key road links and intersection) - two non casualty crashes
- no fatal crashes are noted in in the vicinity of this enhancement site


Source: https://roadsafety.transport.nsw.gov.au/statistics/interactivecrashstats
Figure 4.12 Crash data (2015-2019) Table Top Yard clearances enhancement site

## PARKING

Within the rural areas in the vicinity of the Table Top Yard clearances enhancement site there is limited provision of formal on-street parking. Parking is allowed on road verges however considering the road environment and the provision of off-street parking within commercial, industrial, and residential uses in the surrounding area it is expected demand for this road side parking would be low. There is no designated public parking within the enhancement site.

### 4.3.2 RAIL NETWORK

The Main South Line intersects all enhancement sites within the Albury precinct. Existing road rail interfaces include eight rail crossings (four grade separated road crossings, three grade separated pedestrian crossings, and one level crossing) in the vicinity of the enhancement sites.

The heritage-listed Albury Railway Station located on Railway Place is the only operating railway station in the Albury precinct and is located adjacent to the Albury Station and surrounds. The station features commuter parking, passenger drop-off, public bus stops, regional coach parking, and taxi staging areas. Pedestrian access to the station is provided via footpaths on Railway Place and also connect to pedestrian overpasses spanning the rail line and the Hume Highway to connect to Kenilworth Street to the east.

The Main South Line that runs through the Albury precinct carries the passenger rail services connecting Melbourne, Sydney, Canberra, and Griffith. Melbourne services terminate at Albury station. Additionally, the rail line is an important freight corridor. Table 4.13 shows the average daily passenger and freight rail services that currently operate through the area.

Table 4.13 Existing passenger and rail freight services - Albury Railway Station

| SERVICE | PASSENGER | FREIGHT | TOTAL |
| :--- | :---: | :---: | :---: |
| Average daily two-way services | 10 | 12 | 16 |

Source: $\quad$ https://transportnsw.info/trip\#/departures? depart $=26501$ \& type $=$ platform\&accessible=false
The rail line, station, and road/rail interfaces are illustrated in Figure 4.13 below.
The existing road/rail interfaces in the Albury work precinct including a rail level crossing, road bridges and underpasses, and pedestrian bridges are described below in Table 4.14.

Table 4.14 Existing rail crossings - Albury work precinct

| WORK SITE | ROAD NAME | ROAD TYPE | CROSSING TYPE |
| :--- | :--- | :--- | :--- |
| Albury South | Kiewa Street | One lane - two way | Grade-separated - rail over road |
|  | East Street | Two-way, four lanes | Grade-separated - rail over road |
|  | Pedestrian Bridge | Pedestrian bridge | Grade-separated pedestrian bridge |
|  | Pedestrian Bridge | Pedestrian bridge | Grade-separated pedestrian bridge |
|  | Harold Mair Bridge | Pedestrian bridge | Grade-separated pedestrian bridge |
|  | Borella Road (Riverina Highway) | Two-way, five lanes | Grade-separated - road over rail |
| Ettamogah | Wagga Road | Two-way, four lanes | Grade-separated - road over rail |
| Table Top | Tynan Road | Two lane - two way | Level Crossing - active |



### 4.3.3 HEAVY VEHICLES ROUTES

Figure 4.14 shows the designated heavy vehicle routes that exist within the Albury work precinct. Heavy vehicle routes are located along the enhancement site access routes within the Albury precinct on the following roads:

- Hume Highway
- Borella Road
- Atkins Street
- MacLeay Street
- Panmure Street
- East Street.
- Young Street
- Wilson Street
- Railway Place
- Wagga Road.

In addition to these routes the Regional Freight Transport Plan 2019 (RFTP) by Riverina Eastern Regional Organisation of Councils (REROC) identifies Hume Highway (from Albury to Olympic Highway interchange) as a REROC Strategic Highway.



### 4.3.4 TRAVELLING STOCK RESERVES

Travelling Stock Reserves (TSR) are reserves of connected crown land which are designated for the movement of stock between watering and grazing land, but are also used for emergency stock refuge and transport of stock to market, providing biodiversity corridors, providing access and connection to country for Aboriginal peoples maintaining heritage. Often the TSR will be along roads and consequently interface with road vehicles. A TSR, when on public roads, is referred to as a livestock highway.

Figure 4.15 shows that there are no Livestock Highways or stock routes in the vicinity of enhancement sites within the Albury precinct. Moving stock on public roads outside of Travelling Stock Reserves is possible with the necessary permits and so stock may at times require limited use of rail crossings within the proposal.


### 4.3.5 PUBLIC TRANSPORT NETWORKS

### 4.3.5.1 PUBLIC BUSES

Figure 4.16 shows the public bus routes that operate within the Albury precinct in the vicinity of the Murray River, and Albury Station and surrounds. No public bus routes were identified relevant to the Billy Hughes bridge or Table Top Yard clearances enhancement sites.

Table 4.15 details the Albury precinct bus services for the routes shown in Figure 4.16.
Table $4.15 \quad$ Existing public bus services - Albury

| SERVICE | DESTINATION | SERVICES PER DAY MON-FRI | SERVICES PER DAY SATURDAY | SERVICES PER DAY <br> SUNDAY AND PUBLIC HOLIDAYS |
| :---: | :---: | :---: | :---: | :---: |
| 901 | West Albury | 10 | 8 | - |
| 902 | East Albury | 11 | 7 | - |
| 903 | South Albury | 9 | 6 | - |
| 904 | Wodonga | 24 | - | - |
| 906 | Lavington | 20 | 9 | - |
| 907 | Glenroy and Quicks Hill | 13 | 9 | - |
| 908 | Thurgoona | 12 | 9 | - |
| 915 | Corowa | 3 | - | - |
| 150 | Wodonga | - | 8 | - |
| 160 | Wodonga | - | 7 | - |
| 741 (TrainLink) | Echuca (Tuesdays, Thursdays, and Saturdays only) | 1 | 1 | - |



The public buses services operating on key road links within the Albury precinct are detailed in Table 4.16.
Table $4.16 \quad$ Existing public bus routes on key road links - Albury
\(\left.$$
\begin{array}{|l|l|l|l|}\hline \text { SERVICE } & \begin{array}{l}\text { ENHANCEMENT } \\
\text { SITES }\end{array} & \text { KEY ROAD LINKS } & \text { KEY BUS STOP NAME / NUMBER } \\
\hline \begin{array}{l}902-\text { Albury to } \\
\text { East Albury }\end{array} & \text { Murray River bridge } & \begin{array}{l}\text { Uses East Street and } \\
\text { Borella Road }\end{array} & - \text { No stops on key links } \\
\hline \begin{array}{l}903-\text { Albury to } \\
\text { South Albury }\end{array} & \text { Murray River bridge } & \begin{array}{l}\text { Uses and stops on Atkins } \\
\text { Street, Abercorn Street, } \\
\text { Kiewa Street, and Olive } \\
\text { Street }\end{array} & \begin{array}{l}\text { Atkins Street after Macauley Street / } \\
264077 \\
\text { Olive Street/Atkins Street / 264078 }\end{array}
$$ <br>

\hline Olive Street before Abercorn Street /\end{array}\right]\)| 264079 |
| :--- |

### 4.3.5.2 SCHOOL BUSES

The school bus routes in the Albury precinct are detailed in Table 4.17.
Table 4.17 Existing school bus services on key road links - Albury

| SERVICE | SERVICE RUNNING AREA |
| :--- | :--- |
| School Service 1 | Uses and stops on Young Street |
| Lara Lakes | Uses and stops on Tynan Road and Perryman Lane |

Source: https://martinsalbury.com.au/direct-school-services/albury-high-school/

### 4.3.6 ACTIVE TRANSPORT NETWORKS

### 4.3.6.1 CYCLING NETWORK

Figure 4.17 shows the designated cycle infrastructure that TfNSW has classified within the Albury precinct. No dedicated cycle infrastructure is provided in the vicinity of the Billy Hughes bridge or Table Top Yard clearances enhancement sites. In all areas the existing road lanes or shoulders may be used informally by cyclists.

### 4.3.6.2 PEDESTRIAN NETWORK

Footpaths are present on most roads within the urban area of the Albury precinct and pedestrian crossings are provided at most signalised intersections, and many unsignalised intersections. Typically, there is not provision of connected pedestrian infrastructure in the vicinity of enhancement sites in rural areas. There are also several opportunities to cross the rail line at grade-separated road bridges and three pedestrian overpasses as described in Table 4.18.

Table $4.18 \quad$ Pedestrian rail crossing opportunities - Albury precinct

| WORK SITE | LOCATION | CROSSING TYPE |
| :--- | :--- | :--- |
| Murray River bridge | East Street | Grade-separated - rail over road |
| Albury Station and surrounds | Harold Mair Bridge | Pedestrian overpass |
|  | Amatex Street pedestrian bridge | Pedestrian overpass |
|  | Albury Station pedestrian bridge | Pedestrian overpass |
|  |  | Bridge does not feature ramps |

Figure 4.18 shows existing opportunities to cross the rail line in the Albury precinct.



### 4.3.7 WATER BASED TRANSPORT

In the vicinity of the study area the Murray River is used primarily for tourism, recreational activities, and events including but not limited to:

- water ski school and users
- annual sporting events such as:
- Murray River kayak race
- Murray River long distance river swim
- Frank Harrison Interstate Marathon Cup
- commercial canoe kayak hire operators
- commercial river cruises
- private watercraft.

Any water-based emergency services would also access the waterway beneath the Murray River bridge.
At the time of preparation of this report, river tour operators were closed due to COVID-19 restrictions and could not be contacted for comment on duration or location of activities on the Murray River.

The river features several public and private jetties that allow users to access the river, including at the new Albury Riverside precinct that is due to be completed in December 2022 and Oddies Creek Park, both to the north of the Murray River bridge enhancement site. The river does not support public transport, trade, or shipping freight routes. In the vicinity of the study area the river is crossed by the Murray River rail bridge and the Hume Highway.

### 4.4 GREATER HUME - LOCKHART

Greater Hume - Lockhart precinct includes the following enhancement sites:

- Culcairn Yard clearances
- Culcairn pedestrian bridge
- Henty Yard clearances
- Yerong Creek clearances
- The Rock Yard clearances.

Due to their proximity, Culcairn Yard clearances and Culcairn pedestrian bridge were considered collectively (referred to as Culcairn enhancement sites).

The existing traffic and transport network relevant to Greater Hume - Lockhart precinct is discussed in the following sections.

### 4.4.1 ROAD NETWORK

The sites within the precinct are connected by the Olympic Highway. The enhancement sites and main road links within the precinct are shown below in Figure 4.19.


### 4.4.1.1 CULCAIRN ENHANCEMENT SITES

The enhancement sites in Culcairn share the same road network and have been considered collectively.
The key road links and intersections expected to support the construction or operational movements related to the proposal for Culcairn are depicted below in Figure 4.20. Key road characteristics are described in Table 4.19 and key intersection configurations are shown in Appendix C.

Table 4.19 Key road links - Culcairn enhancement sites

| ROAD NAME | ROAD DESCRIPTION |
| :--- | :--- |
| Olympic <br> Highway/ <br> Melville Street | Two-way, two lane state-controlled highway that runs from the Hume Highway 18 km north of <br> Albury (23km north of the Murray River) to the Mid-Western Highway at Cowra. <br> In the vicinity of the enhancement site the highway is generally rural and features 3.6m wide lanes, <br> sealed shoulders with parking, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |
| Railway Parade | Two-way, two lane locally controlled urban road that generally runs north-south from Balfour Street <br> and provides access to rural properties and commercial areas in central Culcairn on the western side <br> of the rail line. <br> In the vicinity of the enhancement site the road generally features 3.5 m wide lanes, areas of sealed <br> and unsealed shoulders with parking, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |
| Balfour Street | Two-way, two lane state-controlled road, that is classified as a regional road and forms part of the <br> state-controlled Olympic Highway between Railway Street and Melville Street. The road runs east- <br> west and provides cross connectivity within Culcairn via a rail level crossing. <br> In the vicinity of the enhancement site the road generally features 3.7 m wide lanes, sealed shoulders, <br> and has a posted speed limit of 50km $/ \mathrm{h}$. |

## TRAFFIC VOLUMES

Observed traffic volumes for the roads expected support the construction or operational movements related to the proposal for the Albury Station and surrounds are shown in Table 4.20. Where published AADT data was not available or considered inappropriate, estimations based on comparable locations, as detailed in the methodology, are presented.

Table $4.20 \quad$ Culcairn enhancement sites observed traffic volumes

| ROAD NAME | COUNT YEAR | DAILY (TWO-WAY) <br> VOLUME | HV <br> PROPORTION |
| :--- | :---: | :---: | :---: |
| Olympic Highway/Melville Street $^{1}$ | 2011 | 2,454 | $28 \%$ |
| Balfour Street | 2010 | 5,527 | Not available |
| Railway Parade South |  |  |  |
| Railway Parade North $^{3}$ | 2006 | 3,625 | Not available |

(1) No data available, volumes estimated as Olympic Highway - 290m North of Calool Lane, Culcairn
(2) No data available, volumes estimated as Railway Parade - 80m South of Balfour Street, Culcairn 2660
(3) No data available, volumes estimated as $25 \%$ of Railway Parade - 80 m South of Balfour Street, Culcairn 2660


Figure 4.20 Key road links and intersections - Culcairn Yard clearances

| $\square$ Proposal site |
| :--- |
| Existing railway |
| Main road |
| Local road |
| Key intersection |
| Key road links |

INLAND RAIL-

ART̄C

## ROAD SAFETY

Figure 4.21 shows the crashes that occurred in the data collection period in the vicinity of the Culcairn enhancement sites, with the following observations:

- Railway Parade/Balfour Street (key road links and intersection) - four crashes
- Balfour Steer/Melville Street (key road links and intersection) - one crash
- No fatal crashes are noted in the vicinity of this enhancement site.

It is noted that the areas with a greater occurrence of crashes are also roads carrying a high volume of vehicles (relative to the rest of the network), increasing the overall crash exposure risk.


Source: https://roadsafety.transport.nsw.gov.au/statistics/interactivecrashstats
Figure 4.21 Crash data (2015-2019) Culcairn enhancement sites

## PARKING

Within the urban and rural areas in the vicinity of the Culcairn enhancement sites, on-street kerbside parking is generally allowed unless signed otherwise and demand for this parking would be low due to provision of off-street parking within commercial, industrial, retail, and residential uses in the surrounding area, and the Culcairn Railway Station. There is no designated parking within the enhancement site. Further detail around parking on key links is provided below in Table 4.21 .

Table 4.21 Parking provision - Culcairn

| LOCATION | PARKING | TIME OF DAY RESTRICTIONS |
| :--- | :--- | :--- |
| Olympic Highway / Melville Street | Kerbside parking | No Restrictions |
| Railway Parade | Kerbside parking | Heavy vehicle parking restriction 9pm - 7am |
| Balfour Street | Kerbside and angle parking | No Restrictions |

### 4.4.1.2 HENTY YARD CLEARANCES ENHANCEMENT SITE

The key road links and intersections expected to support the construction or operational movements related to the proposal for the Henty Yard clearances enhancement site are depicted below in Figure 4.22. Key road characteristics are described in Table 4.22 and key intersection configurations are shown in Appendix C.

Table 4.22 Key road links - Henty Yard clearances enhancement site
$\left.\begin{array}{|l|l|}\hline \text { ROAD NAME } & \text { ROAD DESCRIPTION } \\ \hline \begin{array}{l}\text { Olympic } \\ \text { Highway/ } \\ \text { Railway Parade }\end{array} & \begin{array}{l}\text { Two-way, two lane state-controlled highway that runs from the Hume Highway l8km north of Albury } \\ \text { (23km north of the Murray River) to the Mid-Western Highway at Cowra. The highway runs through } \\ \text { Henty is also known as Railway Parade, running east of the rail line and providing access to central } \\ \text { Henty and the Henty Railway station, Henty highway rest area and Bi-Centennial Park. } \\ \text { In the vicinity of the Henty Yard clearances enhancement site the highway is generally rural and } \\ \text { features 3.5m wide lanes, sealed shoulders with parking, and has a posted speed limit of 50km/h. }\end{array} \\ \hline \text { Sladen Street } & \begin{array}{l}\text { Two-way, two lane locally controlled urban road that generally runs east-west through Henty and } \\ \text { provides cross connectivity across the Olympic Highway and rail line via a level crossing. The road } \\ \text { provides access to Henty Public School, St Paul's Lutheran Primary School, and residential areas in } \\ \text { Henty. } \\ \text { In the vicinity of the Henty Yard clearances enhancement site the road features a } 6.8 \mathrm{~m} \text { wide eastbound } \\ \text { lane and 3.8m westbound lane (approx.) through the level crossing, unsealed shoulders, and has a } \\ \text { posted speed limit of 50km/h. }\end{array} \\ \hline \begin{array}{l}\text { Rosler Parade/ } \\ \text { Yankee } \\ \text { Crossing Road }\end{array} & \begin{array}{l}\text { Two-way, two lane locally controlled urban road that generally runs east-west through Henty and } \\ \text { provides cross connectivity across the Olympic Highway and rail line via a level crossing. The road } \\ \text { provides access to residential areas inside and outside of Henty. } \\ \text { In the vicinity of the enhancement site the road features a 6.8m wide eastbound lane and 3.8m } \\ \text { westbound lane (approx.) through the level crossing, unsealed shoulders, and has a posted speed limit } \\ \text { of 50km/h. }\end{array} \\ \hline \text { Ivor Street } & \begin{array}{l}\text { Two-way, two lane locally controlled urban road that generally runs north-south through Henty and } \\ \text { provides access to Henty Memorial Park, and residential areas inside and outside of Henty. } \\ \text { In the vicinity of the Henty Yard clearances enhancement site the road features a } 6.8 \mathrm{~m} \text { wide sealed } \\ \text { width, unsealed shoulders, and has a posted speed limit of 50km/h. }\end{array} \\ \hline \begin{array}{l}\text { Two-way, two lane locally controlled urban road that generally runs north-south between Sladen Street } \\ \text { and Rosler Parade, and residential areas inside and outside of Henty. } \\ \text { In the vicinity of the Henty Yard clearances enhancement site the road features a } 6.8 \mathrm{~m} \text { wide sealed } \\ \text { width, unsealed shoulders, and has a posted speed limit of 50km/h. }\end{array} \\ \hline \text { Stree }\end{array}\right\}$


## TRAFFIC VOLUMES

Observed traffic volumes for the roads expected support the construction or operational movements related to the proposal for the Henty Yard clearances enhancement site are shown below in Table 4.23. Where published AADT data was not available or considered inappropriate, estimations based on comparable locations, as detailed in the methodology, are presented.

Table 4.23 Henty Yard clearances enhancement site observed traffic volumes

| ROAD NAME | COUNT YEAR | AADT (TWO -WAY) | HV PROPORTION |
| :--- | :---: | :---: | :---: |
| Railway Parade (Olympic Highway) ${ }^{1}$ | 2011 | 2,454 | $28 \%$ |
| Sladen Street | 2014 | 764 | $12 \%$ |
| Rosler Parade/Yankee Crossing Road $^{2}$ | 2014 | 153 | $12 \%$ |
| Allan Street $^{3}$ | 2011 | 491 | $28 \%$ |
| Ivor Street $^{3}$ | 2011 | 491 | $28 \%$ |

(1) No data available, volumes estimated as Olympic Highway - 290m North of Calool Lane, Culcairn
(2) No data available, volumes estimated as $50 \%$ of Sladen Street with equivalent HV proportion
(3) No data available, volumes estimated as $20 \%$ of Railway Parade with equivalent HV proportion

## ROAD SAFETY

Figure 4.23 shows the crashes that occurred in the data collection period in the vicinity of the Henty Yard clearances enhancement site, with the following observations noted:

- Olympic Highway (key road link) - six crashes, five of which occurred in dark lighting conditions
- no fatal crashes are noted in in the vicinity of this enhancement site

It is noted that the areas with a greater occurrence of crashes are also roads carrying a high volume of vehicles (relative to the rest of the network), increasing the overall crash exposure risk.


Source: https://roadsafety.transport.nsw.gov.au/statistics/interactivecrashstats
Figure $4.23 \quad$ Crash data (2015-2019) Henty Yard clearances enhancement site

## PARKING

Within the urban areas of Henty, on-street kerbside parking is generally allowed unless signed otherwise and demand for this parking would be low due to provision of off-street parking within commercial, industrial, retail, and residential uses in the surrounding area, and the Henty Railway Station. There is no designated parking within the enhancement site.

### 4.4.1.3 YERONG CREEK YARD CLEARANCE ENHANCEMENT SITE

The key road links and intersections expected to support the construction or operational movements related to the proposal for the Yerong Creek Yard clearances enhancement site are depicted below in Figure 4.24. Key road characteristics are described in Table 4.24 and key intersection configurations are shown in Appendix C.

Table 4.24 Key road links - Yerong Creek Yard clearances enhancement site

| ROAD NAME | ROAD DESCRIPTION |
| :--- | :--- |
| Olympic <br> Highway/ <br> Cox Street | Two-way, two lane state-controlled highway that runs from the Hume Highway 18 km north of Albury <br> (23km north of the Murray River) to the Mid-Western Highway at Cowra. The highway through <br> Yerong Creek is also known as Cox Street, running east of the rail line and providing access to central <br> Yerong Creek and residential areas. <br> In the vicinity of the Yerong Creek Yard clearances enhancement site the highway is generally rural <br> and features 3.6m wide lanes, unsealed shoulders with parking, and has a posted speed limit of 50km/h. |
| Plunkett Street | Two-way, two lane locally controlled urban street that generally runs east-west from the Olympic <br> Highway and provides cross connectivity within Yerong Creek via a rail level crossing west of <br> Olympic Highway. <br> In the vicinity of the Yerong Creek Yard clearances enhancement site the road generally features 4.6m <br> wide lanes, areas of sealed and unsealed shoulders with parking, and has a posted speed limit of <br> $50 \mathrm{~km} / \mathrm{h}$. |
| Finlayson | Two-way, two lane locally controlled urban street that generally runs north-south to the west of the <br> Street |
| Olympic Highway, crossing Plunkett Street and provides access to residential properties and the <br> Yerong Creek Rural Fire Brigade within Yerong Creek. <br> In the vicinity of the Yerong Creek Yard clearances enhancement site the road generally features a 5m <br> sealed width, no shoulders, and has a posted speed limit of 50km/h. |  |



## TRAFFIC VOLUMES

Observed traffic volumes for the roads expected support the construction or operational movements related to the proposal for the Yerong Creek Yard clearances enhancement site are shown below in Table 4.25. Where published AADT data was not available or considered inappropriate, estimations based on comparable locations, as detailed in the methodology, are presented.

Table 4.25
Yerong Creek Yard clearances enhancement site observed traffic volumes

| ROAD | OBSERVED VOLUMES |  |  |  |
| :--- | :--- | :---: | :---: | :---: |
| Road name | Road type | Count year | AADT (two-way) | HV Proportion |
| Olympic Highway / Cox Street $^{1}$ | Highway | 2010 | 3,077 | $18 \%$ |
| Plunkett Street $^{2}$ | Urban | 2014 | 764 | $12 \%$ |
| ${\text { Finlayson } \text { Lane }^{3}}$ | Urban | 2014 | 191 | $12 \%$ |

(1) No data available, volumes estimated as Olympic Highway - 50 m East of Mangoplah Road, The Rock 2655 with equivalent HV proportion
(2) No data available, volumes estimated as Sladen Street, Henty (East-West road through town) with equivalent HV proportion
(3) No data available, volumes estimated as $25 \%$ of Plunkett St with equivalent HV proportion

ROAD SAFETY
Figure 4.25 shows that no crashes were recorded in the vicinity of the Yerong Creek Yard clearances enhancement site during the data collection period.


Source: https://roadsafety.transport.nsw.gov.au/statistics/interactivecrashstats
Figure 4.25 Crash data (2015-2019) Yerong Creek Yard clearances enhancement site

## PARKING

On-street kerbside parking is generally allowed on the urban road network in the vicinity of the Yerong Creek Yard clearances enhancement site unless signed otherwise and demand for this parking would be low due to provision of offstreet parking within retail, and residential uses in the surrounding area. There is no designated parking within the enhancement site.

### 4.4.1.4 THE ROCK YARD CLEARANCES ENHANCEMENT SITE

The key road links and intersections expected to support the construction or operational movements related to the proposal for The Rock Yard clearances enhancement site are depicted below in Figure 4.26. Key road characteristics are described in Table 4.26 and key intersection configurations are presented in Appendix C.

Table 4.26 Key road links - The Rock Yard clearances enhancement site

| ROAD NAME | ROAD DESCRIPTION |
| :--- | :--- |
| Olympic <br> Highway/ <br> Railway Street | Two-way, two lane state-controlled highway that runs from the Hume Highway 18km north of Albury <br> (23km north of the Murray River) to the Mid-Western Highway at Cowra. Through The Rock the <br> highway generally runs east-west and provides access to residential areas in south The Rock and The <br> Rock Railway Station. <br> Within the vicinity of The Rock Yard clearances enhancement site the highway is generally rural and <br> features 3.6m wide lanes, sealed shoulders with parking, and has a posted speed limit of 50km $/ \mathrm{h}$. |
| Urana Street | Two-way, two lane two lane urban locally controlled street generally runs north-south and provides <br> cross connectivity within The Rock via a rail level crossing north of Olympic Highway. The road <br> provides access central urban areas of The Rock and residential properties. <br> Within the vicinity of The Rock Yard clearances enhancement site the road generally features 3.6 m <br> wide lanes, unshoulders, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |




## TRAFFIC VOLUMES

Observed traffic volumes for the roads expected support the construction or operational movements related to the proposal for The Rock Yard clearances enhancement site are shown below in Table 4.27. Where published AADT data was not available or considered inappropriate, estimations based on comparable locations, as detailed in the methodology, are presented.

Table 4.27
The Rock Yard clearances enhancement site observed traffic volumes

| ROAD NAME | COUNT YEAR | AADT (TWO -WAY) | HV PROPORTION |
| :--- | :---: | :---: | :---: |
| Olympic Highway/Melville Street $^{1}$ | 2010 | 3,077 | $18 \%$ |
| Urana Street $^{2}$ | 2014 | 764 | $12 \%$ |

(1) No data available, volumes estimated as Olympic Highway - 50m East of Mangoplah Road, The Rock 2655
(2) No data available, volumes estimated as Sladen Street, Henty with equivalent HV proportion.

## ROAD SAFETY

Figure 4.27 shows the crashes that occurred in the data collection period in the vicinity of The Rock Yard clearances enhancement site. It is noted that an insufficient number of crashes were recorded for any significant observations in the vicinity of this enhancement site.


Source: https://roadsafety.transport.nsw.gov.au/statistics/interactivecrashstats
Figure 4.27 Crash data (2015-2019) The Rock Yard clearances enhancement site

## PARKING

Within the urban areas of The Rock, on-street kerbside parking is generally allowed unless signed otherwise and demand for this parking would be low due to provision of off-street parking within industrial, retail, and residential uses in the surrounding area. There is no designated parking within the enhancement site.

### 4.4.2 RAIL NETWORK

The Main South Line runs through the Greater Hume - Lockhart precinct from Culcairn to The Rock and features seven rail crossings (one grade separated and six active level crossings) in the vicinity of the enhancement sites

The Greater Hume - Lockhart precinct includes the heritage-listed Culcairn, Henty, and The Rock railway stations. The stations each generally feature commuter parking and passenger drop-off areas. Pedestrian access to the stations is provided via the unsealed roads to the stations, with continuous pedestrian footpaths generally not provided to the station buildings.

The Main South Line that runs through the Greater Hume - Lockhart precinct carries the passenger rail services connecting Melbourne, Sydney, Canberra, and Griffith. Additionally, the rail line is an important freight corridor. Table 4.28 shows the average daily passenger and freight rail services that operate through the area.

Table 4.28 Existing passenger and rail freight services - Greater Hume - Lockhart precinct

|  | PASSENGER | FREIGHT | TOTAL |
| :--- | :---: | :---: | :---: |
| Average daily two-way services | 4 | 12 | 16 |

Source: $\quad$ https://transportnsw.info/trip\#/departures? depart $=26501$ \& type $=$ platform\&accessible=false
The rail line, stations, and crossings are illustrated in Figure 4.28 below.
The existing road/rail interfaces in the Greater Hume - Lockhart precinct including rail level crossings, road bridges and underpasses are described below in Table 4.29.

Table 4.29 Existing rail crossings - Greater Hume - Lockhart precinct

| ENHANCEMENT SITE | ROAD NAME | ROAD TYPE | CROSSING TYPE |
| :--- | :--- | :--- | :--- |
| Culcairn | Gamble Street | Two-way, one lane | Grade-separated - rail over road |
|  | Balfour Street | Two-way, two lanes | Level Crossing - Active |
| Henty | Rosler Parade | Two-way, two lanes | Level Crossing - Active |
|  | Sladen Street | Two-way, two lanes | Level Crossing - Active |
| Yerong Creek | Plunkett Street | Two-way, two lanes | Level Crossing - Active |
| The Rock | Urana Street | Two-way, two lanes | Level Crossing - Active |
|  | Yerong Street | Two lane - two way | Level Crossing - Active |



### 4.4.3 HEAVY VEHICLES ROUTES

Figure 4.29 shows the heavy vehicle routes that operate through the Greater Hume - Lockhart precinct. Heavy vehicle routes are located along the proposed haulage routes within the Greater Hume - Lockhart precinct on the following key road links:

- Olympic Highway / Melville Street
- Balfour Street
- Railway Parade.
- Sladen Street
- Yankee Crossing Road.
- Urana Street
- Mangoplah Road.

In addition to these routes the Regional Freight Transport Plan 2019 (RFTP) by Riverina Eastern Regional Organisation of Councils (REROC) identifies the Hume Highway (from Albury to Olympic Highway interchange) and the Olympic Highway from Hume Highway to Illabo as a REROC Strategic Highways.


### 4.4.4 TRAVELLING STOCK RESERVES

Figure 4.30 shows that there are Livestock Highways within the Greater Hume - Lockhart precinct the along the Olympic Highway from Henty through Yerong Creek and The Rock, and along Lockhart - The Rock Road to The Rock. Moving stock on public roads outside of Travelling Stock Reserves is possible with the necessary permits and so stock may at times require limited use of rail crossings within the proposal.


### 4.4.5 PUBLIC TRANSPORT NETWORKS

### 4.4.5.1 PUBLIC BUSES

Public bus services are provided by Regional Buses and are operated in collaboration with TfNSW under their Rural and Regional On Demand Public Transport pilot program. Services are booked by the passenger and offer door-to-door transfers and as such service routes vary. Table 4.30 below shows the services and frequency offered.

Table 4.30 Public transport on-demand bus services - Greater Hume - Lockhart

| SERVICE | DAYS OFFERED |
| :--- | :--- |
| Holbrook, Morven, Culcairn, Gerogery, Gerogery West and Albury | Mondays and Wednesdays |
| Holbrook, Morven, Culcairn, Henty, Yerong Creek, The Rock, Uranquinty and Wagga | Tuesdays |
| Henty, Culcairn, Gerogery and Albury | Thursdays |
| Holbrook, Woomargama, Mullengandra and Albury | Fridays |

### 4.4.5.2 SCHOOL BUSES

The school bus routes in the Greater Hume - Lockhart precinct are run by several private bus companies. The routes identified in the vicinity of the enhancement sites are detailed in Table 4.31.

Table $4.31 \quad$ Existing school bus services - Greater Hume - Lockhart

| SERVICE | SERVICE RUNNING AREA |
| :--- | :--- |
| N0766 - Henty to Merri Meric, N1141 - Henty to Edgehill, <br> N1198 - Henty to Mundawadra Primary Service, <br> N585 - Henty to Bucki | Uses Olympic Highway in Henty, stops on Sladen <br> Street. |
| N2839 - Yerong Creek to Mangoplah Road | Uses Olympic Highway through Henty and Yerong <br> Creek. |
| N1200 - Henty to Culcairn | Uses Olympic Highway through Culcairn and Henty. |
| Bus 7 - Jindera and Walla, Bus 8 - Walbundrie, Bus 9 - Eden <br> Valley, Bus 10 - Gerogery East and West, Bus 11 - Gerogery <br> and Walla | Uses Olympic Highway through Culcairn and stops <br> on Balfour Street. |
| N1102 Culcairn to The Pines, N317 - Culcairn to Holbrook Rt 1 | Uses Olympic Highway through Culcairn and Henty <br> and Railway Parade in Culcairn. Stops on Balfour <br> Street in Culcairn. |
| N1196 - Mundawadra, Henty and Culcairn | Uses Olympic Highway through Culcairn and Henty <br> and Railway Parade in Culcairn. Stops on Balfour <br> Street in Culcairn and Sladen Street in Henty. |
| N1197 - Yerong Creek, Henty, and Culcairn | Uses Olympic Highway through Culcairn, Henty, <br> Yerong Creek, and The Rock. Stops on Plunkett <br> Street and Finlayson Street in Yerong Creek. |
| N1243 - The Rock to French Park | Uses Olympic Highway through Yerong Creek and <br> The Rock. Stops on Plunkett Street, Yerong Creek. |
| N1172 - The Rock to Bourkes Creek | Uses the Olympic Highway through The Rock. |

### 4.4.6 ACTIVE TRANSPORT NETWORKS

### 4.4.6.1 CYCLING NETWORK

Figure 4.31 and Figure 4.32 show the designated cycle infrastructure that TfNSW has classified in the Greater Hume Lockhart precinct for the Yerong Creek Yard clearances and The Rock Yard clearances enhancement sites. Some cycle infrastructure is located on streets adjacent to the access routes for the Henty enhancement site. In all areas the existing road lanes or shoulders may be used by cyclists.

### 4.4.6.2 PEDESTRIAN NETWORK

Footpaths and formal road crossings are generally only present in the vicinity of enhancement sites in urban areas. Where present they are generally on one side of the street and consist of concrete paths with kerb ramps. Streets through central commercial areas such as Balfour Street in Culcairn, Sladen Street in Henty, Plunkett Street in Yerong Creek, and Urana Street in The Rock feature concrete paths on both sides of the street.

There are several designated opportunities to cross the rail line at level crossings and one closed pedestrian overpass in Culcairn as described in Table 4.32.

Table 4.32 Pedestrian rail crossing opportunities - Greater Hume - Lockhart

| WORK SITE | ROAD NAME | CROSSING TYPE |
| :--- | :--- | :--- |
| Culcairn | Balfour Street | Pedestrian overpass (closed) |
|  | Balfour Street | Level Crossing - Active |
| Henty | Sladen Street | Level Crossing - Active |
| Yerong Creek | Plunkett Street | Level Crossing - Active |
| The Rock | Urana Street | Level Crossing - Active |

Figure 4.33 shows existing opportunities to cross the rail line in the in Greater Hume - Lockhart precinct.

Albury to Illabo Figure 4.32 Cycling infrastructure - The Rock Yard clearances enhancement site



### 4.5 WAGGA WAGGA PRECINCT

Wagga Wagga precinct includes the following enhancement sites:

- Uranquinty Yard clearances
- Pearson Street bridge
- Cassidy Parade pedestrian bridge
- Edmondson Street bridge
- Wagga Wagga Station pedestrian bridge
- Wagga Wagga Yard Clearances
- Bomen Yard clearances.
- Due to their proximity Cassidy Parade pedestrian bridge, Edmondson Street bridge, Wagga Wagga Station pedestrian bridge, and Wagga Wagga Yard clearances were considered collectively (referred to as Wagga Wagga Station and surrounds).

The existing traffic and transport network relevant to Albury precinct is discussed in the following sections.

### 4.5.1 ROAD NETWORK

The Uranquinty Yard clearances enhancement site is connected to Wagga Wagga by the Olympic Highway running north-south between them. The Bomen Yard clearance enhancement site is located on Byrnes Road, which runs northsouth adjacent to the railway line between Wagga Wagga and Junee. The enhancement sites and main road links within the precinct are shown below in Figure 4.34.


### 4.5.1.1 URANQUINTY ENHANCEMENT SITE

The key road links and intersections that support the construction or operational movements related to the proposal for the Uranquinty enhancement site are depicted below in Figure 4.35. Key road characteristics are described in Table 4.33 and key intersection configurations are shown in Appendix C.

Table $4.33 \quad$ Key road links - Uranquinty enhancement site

| ROAD NAME | ROAD DESCRIPTION |
| :--- | :--- |
| Olympic Highway | Two-way, two lane state-controlled highway that runs from the Hume Highway 18km north of <br> Albury (23km north of the Murray River) to the Mid-Western Highway at Cowra. <br> In the vicinity of the Uranquinty enhancement site the highway is generally rural and features <br> 3.7 m wide lanes, areas of sealed and unsealed shoulders, and has a posted speed limit of 50, <br> residential accesses and a school zone and subsequently has a lower speed limit than outside of <br> the Uranquinty area. |
| Yarragundry Street/ <br> Uranquinty Cross <br> Road | Two-way, two lane locally controlled urban road that generally runs north-south and provides <br> access to Uranquinty town centre, the Uranquinty power station, and provides cross connectivity <br> within Uranquinty via a rail level crossing north of Olympic Highway. <br> In the vicinity of the Uranquinty enhancement site the road generally features 3.4m wide lanes, <br> areas of sealed and unsealed shoulders, and has a posted speed limit of 50km $/ \mathrm{h}$ through the <br> Uranquinty urban area and 100km/h in the rural area. |
| Hanging Rock Road | Two-way, one lane locally controlled rural road that generally runs northwest from Uranquinty <br> Cross Road and provides rural residential access. <br> In the vicinity of the Uranquinty enhancement site the road generally features a 4.4 m sealed <br> width (approx.) and unsealed shoulders, and has a posted speed limit of $100 \mathrm{~km} / \mathrm{h}$. |

## TRAFFIC VOLUMES

Observed traffic volumes for the roads expected support the construction or operational movements related to the proposal for the Uranquinty enhancement site are shown in Table 4.34. Where published AADT data was not available or considered inappropriate, estimations based on comparable locations, as detailed in the methodology, are presented.

Table $4.34 \quad$ Uranquinty enhancement site observed traffic volumes

| ROAD NAME | COUNT YEAR | DAILY (TWO- <br> WAY) VOLUME | HV <br> PROPORTION |
| :--- | :---: | :---: | :---: |
| Olympic Highway $^{1}$ |  | 3,646 | $17 \%$ |
| Uranquinty Street | 2010 | 434 | $9 \%$ |
| Yarragundry Street | 2017 | 507 | $8 \%$ |
| Hanging Rock Road $^{2}$ | N/A | $50-100$ | Not available |

(1) No data available, volumes estimated as average of Olympic Highway - Ashmont, 95065 and Olympic Highway The Rock, 9551 with equivalent HV proportion
(2) Estimated traffic volume based on road type and surrounding land uses


## ROAD SAFETY

Figure 4.36 shows the crashes that occurred in the data collection period in the vicinity of the Uranquinty enhancement site, with the following observations:

- Olympic Highway - four crashes (an average of less than one crash per year)
- no fatal crashes are noted in the vicinity of this enhancement site.

It is noted that the areas with a greater occurrence of crashes are also roads carrying a high volume of vehicles (relative to the rest of the network), increasing the overall crash exposure risk.


Source: https://roadsafety.transport.nsw.gov.au/statistics/interactivecrashstats
Figure $4.36 \quad$ Crash data (2015-2019) Uranquinty enhancement site

## PARKING

On-street kerbside parking is generally allowed on the urban road network in the vicinity of the Uranquinty enhancement site unless signed otherwise and demand for this parking would be low due to provision of off-street parking within industrial, retail, and residential uses in the surrounding area. There is no designated parking within the enhancement site. Further detail around parking on key links is provided below in Table 4.35.

Table $4.35 \quad$ Parking provisions - Uranquinty enhancement site

| LOCATION | PARKING | TIME OF DAY RESTRICTIONS |
| :--- | :--- | :--- |
| Olympic Highway | Kerbside parking within urban area <br> Uranquinty Rest Area | Kerbside: Restrictions at pedestrian <br> crossing south of Yarragundry Street <br> Rest Area: Heavy vehicles restricted |
| Yarragundry Street/Uranquinty Cross <br> Road | Kerbside and angle parking | No Restrictions |
| Hanging Rock Road | Kerbside parking | No Restrictions |

### 4.5.1.2 PEARSON STREET BRIDGE ENHANCEMENT SITE

The key road links and intersections expected to support the construction or operational movements related to the proposal for the Pearson Street bridge enhancement site are depicted below in Figure 4.37. Key road characteristics are described in Table 4.36 and key intersection configurations are shown in Appendix C.

Table 4.36 Key road links - Pearson Street bridge enhancement site

| ROAD NAME | ROAD DESCRIPTION |
| :---: | :---: |
| Moorong Street (Olympic <br> Highway) | Two-way, four lane divided state controlled road running north-south from Edward Street and forms part of the Olympic Highway. <br> In the vicinity of the Pearson Street bridge enhancement site the road generally features 3.4 m wide lanes, sealed shoulders, and has a posted speed limit of $60 \mathrm{~km} / \mathrm{h}$ approaching the intersection with Pearson Street and $80 \mathrm{~km} / \mathrm{h}$ exiting the work site. |
| Edward Street (Sturt Highway) | Two-way, two-lane state-controlled highway that generally runs east-west and connects the Northern Expressway in South Australia and the Hume Highway in NSW. <br> In the vicinity of the Pearson Street bridge enhancement site the road generally features 3.4 m wide lanes, sealed shoulders with parking, and has a posted speed limit of $80 \mathrm{~km} / \mathrm{h}$ outside and $60 \mathrm{~km} / \mathrm{h}$ through Wagga Wagga. |
| Pearson Street | Two-way, four lane urban locally controlled road that provides north-south cross-connectivity through western Wagga Wagga, running from the Sturt Highway and provides access to commercial districts in south Wagga Wagga. The road crosses the rail line via a grade-separated road bridge north of Urana Street. <br> In the vicinity of the Pearson Street bridge enhancement site the road generally features 3.3 m wide lanes, sealed shoulders with parking, and has a posted speed limit of $60 \mathrm{~km} / \mathrm{h}$. |
| Cheshire Street | Two-way, two lane urban locally controlled street that runs east-west from Pearson street and provides access to commercial and industrial areas adjacent to the northern side of the rail line. <br> In the vicinity of the Pearson Street bridge enhancement site the road generally features a 12.2 m sealed width, limited line marking, shoulders with parking, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |
| Urana Street | Two-way, two lane urban locally controlled street that runs generally east-west from Pearson Street, crossing Bourke Street and provides access to the Showgrounds, residential areas, and access to the rail line from the south. <br> In the vicinity of the Pearson Street bridge enhancement site the road generally features an 8.8 m sealed width, unsealed shoulders, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |
| Fernleigh Road | Two-way, two lane urban locally controlled road that runs east-west, crossing Glenfield Road, Bourke Street, and Mitchelmore Street, and provides access to The Rules Club sports field, and residential areas. The road crosses the rail line via an at-grade rail level crossing west of the work site. <br> In the vicinity of the Pearson Street bridge enhancement site the road generally features 3.3 m wide lanes, sealed shoulders with parking, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. West of Glenfield Road, Fernleigh Road also features a median turning lane for property access. |
| Alan Turner <br> Depot Access <br> Road | Two-way, two lane urban locally controlled street that runs generally north-south, from Fernleigh Road, and provides access to The Alan Turner Depot. <br> In the vicinity of the Pearson Street bridge enhancement site the road generally features an 8.1 m sealed width, limited road marking, and has a posted speed limit of $40 \mathrm{~km} / \mathrm{h}$. |



## TRAFFIC VOLUMES

Observed traffic volumes for the roads expected support the construction or operational movements related to the proposal for the Pearson Street bridge enhancement site are shown below in Table 4.37.

Table 4.37 Pearson Street bridge enhancement site observed traffic volumes

| ROAD NAME | COUNT YEAR | DAILY <br> (TWO-WAY) <br> VOLUME | HV PROPORTION |
| :--- | :---: | :---: | :---: |
| Edward Street (Sturt Highway) $^{1}$ | 2021 | 6,907 | $12 \%$ |
| Moorong Street (Olympic Highway) $^{1}$ | 2021 | 12,663 | $5 \%$ |
| Pearson Street $^{1}$ | 2021 | 9,814 | $5 \%$ |
| Urana Street $^{1}$ | 2021 | 4,758 | $2 \%$ |
| Cheshire Street $^{2}$ | 2021 | 491 | $5 \%$ |
| Alan Turner Depot Access Road ${ }^{3}$ | N/A | $50-100$ | Not available |

(1) 10 -hour ( 5 am to 10 am and 2 pm to 7 pm ) traffic survey volumes
(2) No data available, volumes estimated as $5 \%$ of Pearson Street 10 -hour with equivalent HV proportion
(3) Estimate traffic volume based on road type and surrounding land uses

## ROAD SAFETY

Figure 4.38 shows the crashes that occurred in the data collection period in the vicinity of the Pearson Street bridge enhancement site, with the following observations:

- Edward Street/Pearson Street (key road links and intersection) - Crash cluster at the intersection
- Pearson Street/Dobney Avenue (key road links and intersection) - Crash cluster at the intersection.
- Edward Street (key road link) - One fatal crash occurring in 2018.

It is noted that the areas with a greater occurrence of crashes are also roads carrying a high volume of vehicles (relative to the rest of the network), increasing the overall crash exposure risk.


Source: https://roadsafety.transport.nsw.gov.au/statistics/interactivecrashstats
Figure $4.38 \quad$ Crash data (2015-2019) Pearson Street bridge enhancement site

## PARKING

On-street kerbside parking is generally allowed on the urban road network in the vicinity of the Pearson Street bridge enhancement site unless signed otherwise and demand for this parking would be low due to provision of off-street parking within commercial, industrial, retail, and residential uses in the surrounding area. There is no designated parking within the enhancement site. Further detail of on street parking on key roads expected to support construction or operational activities related to the proposal is provided in Table 4.38.

Table $4.38 \quad$ Parking provisions - Pearson

| LOCATION | PARKING | TIME OF DAY RESTRICTIONS |
| :--- | :--- | :--- |
| Moorong Street (Olympic <br> Highway) | Kerbside parking | No restrictions |
| Sturt Highway/Edward Street | Kerbside parking | No restrictions |
| Pearson Street | Kerbside parking | Areas of 1P ${ }^{1}$ parking restrictions north of <br> Dobney Avenue |
| Cheshire Street | Kerbside parking | No restrictions |
| Urana Street | Kerbside parking east of Peacock Drive | No restrictions |
| Fernleigh Road | Kerbside parking | No restrictions |
| Alan Turner Depot Access Road | No parking | N/A |

(1) One-hour parking

### 4.5.1.3 WAGGA WAGGA STATION AND SURROUNDS

The enhancement sites in the vicinity of the Wagga Wagga Station share the same road network and have been combined in the following section, for:

- Cassidy Parade pedestrian bridge enhancement site
- Edmondson Street bridge enhancement site
- Wagga Wagga Station pedestrian bridge enhancement site
- Wagga Wagga Yard clearances enhancement site.

The key road links and intersections expected to support the construction or operational movements related to the proposal for the Wagga Wagga Wagga Station and surrounds are depicted below in Figure 4.39 and Figure 4.40. Key road characteristics are described in Table 4.39 and key intersection configurations are shown in Appendix C.

Table 4.39 Key road links - Wagga Station and surrounds

| ROAD NAME | ROAD DESCRIPTION |
| :--- | :--- |
| Edward Street <br> (Sturt Highway) | Two-way, four lane state-controlled road that runs east-west through Wagga Wagga. It is <br> alternately named Edward Street and Hammond Avenue and forms part of the Sturt Highway. The <br> road crosses the rail line via a grade-separated rail bridge west of Lake Albert Road. |
| In the vicinity of the Wagga Wagga Station and surrounds the highway is generally urban and <br> features 3.4m wide lanes, sealed shoulders with parking, and has a posted speed limit of $60 \mathrm{~km} / \mathrm{h}$. |  |


| ROAD NAME | ROAD DESCRIPTION |
| :---: | :---: |
| Docker Street and Bourke Street | Two-way, four lane urban locally controlled street that crosses Edward Street and provides northsouth cross-connectivity through western Wagga Wagga. It provides access to the Wagga Wagga Base Hospital, showgrounds, and Henschke Primary school. The road crosses the rail line via an at-grade rail level crossing in the work site. <br> In the vicinity of the Wagga Wagga Station and surrounds the road generally features 3.3 m wide lanes, sealed shoulders with parking, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |
| Brookong Avenue | Two-way, two lane urban locally controlled road that runs between Docker Street and Edward Street and provides access to residential areas and the Wagga Wagga Base Hospital. <br> In the vicinity of the Wagga Wagga Station and surrounds the road generally features 3.9 m wide lanes, and sealed shoulders with parking and a cycle lane, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |
| Fox Street | Two-way, two lane urban locally controlled street that runs north-south from Edward Street, connecting to Best Street via Donnelly Street and Little Best Street and provides access to residential areas and the Wagga Wagga McDonalds. <br> In the vicinity of the Wagga Wagga Station and surrounds the road generally features a 17.9 m sealed width, no line marking, shoulders with parking, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |
| Edmondson Street and Mitchelmore Street | Two-way, four lane urban locally controlled road that provides north-south cross-connectivity through central Wagga Wagga crossing Edward Street, Coleman Street, and Urana Street. It provides access to the Wagga Wagga High School, Kildare Catholic College, The Bidgee School, and passes adjacent to the South Wagga Wagga Public School. The road crosses the rail line via a grade-separated road bridge north of Erin Street. <br> In the vicinity of the Wagga Wagga Station and surrounds the road generally features 3.1 m wide lanes, sealed shoulders with parking, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{hr}$ and a $40 \mathrm{~km} / \mathrm{h}$ school zone. |
| Norman Street | Two-way, two lane urban locally controlled street that runs north-south from Coleman Street, connecting to Cassidy Parade provides access to a residential area. <br> In the vicinity of the Wagga Wagga Station and surrounds the road generally features a 16.6 m sealed width, limited line marking, shoulders with parking, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |
| Coleman Street | Two-way, two lane urban locally controlled street that runs generally east-west from Docker Street, crossing Edmondson Street and provides access to Wagga Wagga TAFE and residential areas. <br> In the vicinity of the Wagga Wagga Station and surrounds the road generally features 3.6 m wide lanes, sealed shoulders with parking and a cycle lane, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |
| Cassidy Parade | Two-way, two lane urban locally controlled street that runs generally east west between Bimbeen Street and Kildare Street, running adjacent to the south side of the rail line. It provides access to the rail line, Kildare Catholic College via Kildare Street, and residential areas. <br> In the vicinity of the Wagga Wagga Station and surrounds the road generally features a 4.5 m sealed width, limited line marking, unsealed shoulders, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |
| Erin Street | Two-way, two lane urban locally controlled street that runs east-west from Edmondson Street and provides access to Macleay Street. <br> The road features a 12 m sealed width, limited line marking, sealed shoulders with parking, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |


| ROAD NAME | ROAD DESCRIPTION |
| :--- | :--- |
| Macleay Street | Two-way, two lane urban locally controlled street that runs north-south from Railway Street, <br> crosses Coleman Avenue, and provides access to Wagga Wagga TAFE and residential areas. <br> In the vicinity of the Wagga Wagga Station and surrounds the road generally features a 21m sealed <br> width, limited line marking, shoulders with parking, and has a posted speed limit of 50km/h. |
| Railway Street | Two-way, two lane urban locally controlled street that runs east-west from Macleay Street to Lake <br> Albert Road and provides access to the rail line, industrial and residential areas. The Wagga Rail <br> Heritage Museum Rest House is located adjacent to Railway Street. |
| In the vicinity of the Wagga Wagga Station and surrounds the road generally features a 12m sealed <br> width, sealed shoulders with parking, and a posted speed limit of 50km/h. |  |
| Station Place | Two-way, two lane urban locally controlled street that runs north-south from Edward Street and <br> provides access to the heritage-listed Wagga Wagga Railway Station, the Multicultural Council of <br> Wagga Wagga, and other private business. |
| In the vicinity of the Wagga Wagga Station and surrounds the road generally features 3.4m wide |  |
| lanes, sealed shoulders with parking, and has a posted speed limit of 50km/h. |  |\(\left|\begin{array}{l}Two-way, four lane urban locally controlled road that runs north-south through eastern Wagga <br>

Wagga from Edward Street, intersecting with Railway Street and providing external connection to <br>
the suburb of Kooringal. <br>
The road generally features 3.3m wide lanes, sealed shoulders with parking and a cycle lane, and <br>

has a posted speed limit of 60km/h.\end{array}\right|\)| Urana Street |
| :--- |
| Two-way, two lane urban locally controlled street that provides east-west cross-connectivity <br> through Wagga Wagga south of the rail line running from Pearson Street, crossing Bourke, <br> Mitchelmore, and Macleay Streets and provides access to the Showgrounds, residential areas, and <br> continues on to Kooringal in the east. <br> In the vicinity of the Wagga Wagga Station and surrounds the road generally features an 8.3m <br> sealed width, sealed shoulders with parking, and has a posted speed limit of 50km/h. |



Albury to Illabo
Figure 4.39 Key road links and intersections - Wagga Wagga Station and surrounds

| $\begin{aligned} & 0 \\ & 0 \\ & \hline \end{aligned}$ | Proposal site | gUNEE |  |
| :---: | :---: | :---: | :---: |
| Coordinate System: GDA 1994 MGA Zone 55 ARTC makes no representason or warranty and assumes no | Existing railway | mart waga wagca | INLAND AR |
| 边 | - Main road |  | RAIL ANTC |
|  | - Local road |  |  |
|  | - Key intersection |  |  |
|  |  | 8ROOK | The Australan Government s selivering rimand Rail |
| Date: 8/1222021 $\quad$ Paper: A3 <br> Author. WSP <br> Data Sources: ARTC, NSWSS | Key road link | - HOWLONG albury | in parnership with the private sector. |




## TRAFFIC VOLUMES

Observed traffic volumes for the roads expected to support the construction or operational movements related to the proposal for the Wagga Wagga Station and surrounds are shown below in Table 4.40.

Table 4.40 Wagga Wagga Station and surrounds observed traffic volumes

| ROAD NAME | COUNT YEAR | DAILY (TWO- <br> WAY) VOLUME <br> PROPORTION |  |
| :--- | :---: | :---: | :---: |
| Edward Street (Sturt Highway) $^{1}$ | 2021 | 12,151 | $8 \%$ |
| Docker Street/Bourke Street $^{1}$ | 2021 | 8,957 | $2 \%$ |
| Fox Street $^{2}$ | 2021 | 332 | $3 \%$ |
| Mitchelmore Street $^{1}$ | 2021 | 8,044 | $1 \%$ |
| Edmondson Street $^{1}$ | 2021 | 10,448 | $2 \%$ |
| Norman Street $^{3}$ | 2021 | 332 | $3 \%$ |
| Coleman Street $^{1}$ | 2021 | 3,318 | $3 \%$ |
| Cassidy Parade $^{4}$ | 2021 | 664 | $3 \%$ |
| Erin Street ${ }^{5}$ | 2021 | 476 | $2 \%$ |
| Macleay Street ${ }^{6}$ | 2020 | 3,230 | $9 \%$ |
| Railway Street ${ }^{7}$ | 2020 | 3,230 | $9 \%$ |
| Station Place ${ }^{8}$ | 2021 | 472 | $3 \%$ |
| Lake Albert Road ${ }^{9}$ | 2020 | 14,477 | $5 \%$ |
| Urana Street ${ }^{1}$ | 2021 | 4,758 | $1 \%$ |
| Brookong Avenue ${ }^{10}$ | 2021 | 1,215 | $8 \%$ |

(1) 10 -hour ( 5 am to 10 am and 2 pm to 7 pm ) traffic survey volumes
(2) No data available, volumes estimated as Norman Street 10-hour with equivalent HV proportion
(3) No data available, volumes estimated as $50 \%$ of Cassidy Street 10 -hour with equivalent HV proportion
(4) No data available, volumes estimated as $20 \%$ of Coleman Street 10 -hour with equivalent HV proportion
(5) No data available, volumes estimated as $10 \%$ of Urana Street 10 -hour with equivalent HV proportion
(6) No data available, volumes estimated as Railway Street with equivalent HV proportion
(7) Railway Street between Lake Albert Road and Beauty Point Road
(8) No data available, volumes estimated as Smollett Street, Albury 10-hour with equivalent HV proportion
(9) Lake Albert Road between Hammond Avenue and Railway Street
(10) No data available, volumes estimated as $10 \%$ of Edward Street 10 -hour with equivalent HV proportion

## ROAD SAFETY

Figure 4.41 shows the crashes that occurred in the data collection period in the vicinity of the Wagga Station and surrounds, with the following observations:

- Sturt Highway/Edward Street (key road link) - a higher concentration than surrounding areas
- Docker Street (key road link) - a higher concentration than surrounding areas
- Sturt Highway/Edward Street/Docker Street intersection (key intersection) - a higher concentration than surrounding areas
- Coleman Street (key road link) - one fatal crash occurring in 2017.

It is noted that the areas with a greater occurrence of crashes are also roads carrying a high volume of vehicles (relative to the rest of the network), increasing the overall crash exposure risk.


Source: https://roadsafety.transport.nsw.gov.au/statistics/interactivecrashstats
Figure 4.41 Crash data (2015-2019) Wagga Station and surrounds

## PARKING

On-street kerbside parking is generally allowed on the urban road network in the vicinity of the Wagga Wagga Station and surrounds unless signed otherwise. Off street parking is present within commercial, industrial and retail uses within the surrounding area. Engagement with the school has revealed that the limited on-site parking and drop-off facilities combined with restricted adjacent roadside parking results in Railway Street being an important location for the drop off of students who use the Wagga Wagga Station pedestrian bridge and Edmondson Street to access the school. Off street designated parking is present within commercial, industrial and retail areas. Further detail around parking on key links is provided below in Table 4.41.

Table $4.41 \quad$ Parking provisions - Wagga Station and surrounds

| LOCATION | PARKING | TIME OF DAY RESTRICTIONS |
| :---: | :---: | :---: |
| Edward Street (Sturt Highway) | Kerbside parking west of Edmondson Street | No restrictions |
| Docker Street/Bourke Street | Kerbside parking | 2P adjacent Wagga Wagga Base Hospital <br> 8:30am - 6pm Monday - Friday; <br> 8:30am - 12:30pm |
| Brookong Avenue | Kerbside parking | No restrictions |
| Fox Street | Kerbside parking | No restrictions |
| Little Best Street | Kerbside parking and informal verge parking | No restrictions |
| Edmondson Street/ <br> Mitchelmore Street | Kerbside parking south of Erin Street | School bus zones $8 \mathrm{am}-9: 30 \mathrm{am} ; 3 \mathrm{pm}-4 \mathrm{pm}$ |
| Norman Street | Kerbside parking | No restrictions |
| Coleman Street | Kerbside parking | No parking adjacent Kildare Catholic College 8:00am - 9:30pm, 3:00pm - 4:00pm school days <br> 2P Monday - Friday between Invenary and Kildare Street |
| Cassidy Parade | Kerbside parking | No restrictions |
| Erin Street | Kerbside parking | No restrictions |
| Macleay Street | Kerbside parking | No restrictions |
| Railway Street | Kerbside parking | Areas of restricted parking 8:00am -9:30pm, 2:30pm $-4: 00 \mathrm{pm}$ school days |
| Station Place (Wagga Wagga Railway Station) | Short-term kerbside parking: 10 spaces <br> Public station off-street carpark: <br> 47 spaces (including two disabled spaces) <br> Access to private off-street local business parking: Quantity unknown <br> Long-distance coach parking: three bays Taxi zone: One bay | Short-term kerbside parking: 1P on Station Place <br> Public station off-street carpark: Unsigned Off-street local business parking: Unknown Long-distance coach parking: Unsigned Taxi zone: Unsigned |
| Lake Albert Road | No Parking | N/A |
| Urana Street | Kerbside parking east of Peacock Drive | No restrictions |
| Mt Erin Heritage Centre | Private off-street parking (no formal road markings) | Restricted to customers of the Mt Erin Heritage Centre |

### 4.5.1.4 BOMEN YARD CLEARANCES ENHANCEMENT SITE

The key road links and intersections expected to support the construction or operational movements related to the proposal for the Bomen Yard clearances enhancement site are depicted below in Figure 4.42. Key road characteristics are described in Table 4.42 and key intersection configurations are shown in Appendix C.

Table 4.42 Key road links - Bomen Yard clearances enhancement site

| ROAD NAME | ROAD DESCRIPTION |
| :--- | :--- |
| Olympic Highway | Two-way, two-lane state-controlled highway that runs from the Hume Highway 18 km north of <br> Albury (23km north of the Murray River) to the Mid-Western Highway at Cowra. <br> In the vicinity of the Bomen Yard clearances enhancement site the highway is generally rural <br> and features 3.4m wide lanes, areas of sealed and unsealed shoulders and a posted speed limit of <br> $100 \mathrm{~km} / \mathrm{h}$. |
| Byrnes Road | Two-way, two lane rural locally controlled road running generally north-south between Oura <br> Road and the Olympic Highway at Junee, connecting Bomen, Junee, and Harefield and <br> providing access to the Harefield Intermodal Terminal. <br> In the vicinity of the Bomen Yard clearances enhancement site the road generally features 3.5m <br> wide lanes, sealed shoulders, and has a posted speed limit of 80km/h. |
| Merino Street | Two-way, four lane rural locally controlled street that runs north-south through Wagga Wagga <br> from Edward Street, intersecting with Railway street and providing access to the suburb of <br> Kuringal. The road crosses the rail line via a grade-separated rail bridge north of Byrnes Road. <br> In the vicinity of the Bomen Yard clearances enhancement site the road generally features 3.5m <br> wide lanes, sealed shoulders, and has a posted speed limit of $60 \mathrm{~km} / \mathrm{h}$ between Byrnes Road and <br> Dorset Drive, and 80km/h between Dorset Drive and the Olympic Highway. |



## TRAFFIC VOLUMES

Observed traffic volumes for the roads expected support the construction or operational movements related to the proposal for the Bomen Yard clearances enhancement site are shown below in Table 4.43. Where published AADT data was not available or considered inappropriate, estimations based on comparable locations, as detailed in the methodology, are presented.

Table $4.43 \quad$ Bomen Yard clearances enhancement site observed traffic volumes

| ROAD NAME | COUNT YEAR | DAILY (TWO-WAY) <br> VOLUME | HV PROPORTION |
| :--- | :---: | :---: | :---: |
| Olympic Highway $^{1}$ | 2010 | 3,646 | $17 \%$ |
| Byrnes Road | 2021 | 2,503 | $31 \%$ |
| Merino Drive - between Olympic and Dorsett | 2019 | 926 | $33 \%$ |
| Merino Drive - between Byrnes and Dorsett | 2019 | 2,115 | $37 \%$ |
| East Bomen Road ${ }^{2}$ | 2019 | 529 | Not Available |

(1) No data available, volumes estimated as average of Olympic Highway - Ashmont, 95065 and Olympic Highway The Rock, 9551 with equivalent HV proportion
(2) No data available, volumes estimated as $25 \%$ of Merino Street - Between Byrnes Road and Dorset Drive with equivalent HV proportion

## ROAD SAFETY

Figure 4.43 shows the crashes that occurred in the data collection period in the vicinity of the Bomen Yard clearances enhancement site, with the following observations noted:

- Olympic Highway (key road link) - 13 crashes in the vicinity of this enhancement site
- no fatal crashes are noted in the vicinity of this enhancement site.

It is noted that the areas with a greater occurrence of crashes are also roads carrying a high volume of vehicles (relative to the rest of the network), increasing the overall crash exposure risk.


Source: https://roadsafety.transport.nsw.gov.au/statistics/interactivecrashstats
Figure $4.43 \quad$ Crash data (2015-2019) Bomen Yard clearances enhancement site

## PARKING

Within the rural areas in the vicinity of the Bomen Yard clearances enhancement site there is limited provision of on street parking and demand for this parking would be low due to provision of off-street parking within commercial and industrial uses in the surrounding area. There is no designated parking within the enhancement site.

### 4.5.2 RAIL NETWORK

The Main South Line runs through the Wagga Wagga Work precinct from Uranquinty to Bomen and features eight road crossings (four grade-separated crossings, three active level crossings, and one closed level crossing) in the vicinity of the enhancement sites.

The heritage-listed Wagga Wagga Railway Station located on Station Place is the one operating Railway Station in the Wagga Wagga precinct and is adjacent to the South Wagga Wagga Public School. The station features commuter parking, a regional coach stop, passenger drop-off and taxi staging areas. The station also houses the Wagga Rail Heritage Museum and the Multicultural Council of Wagga Wagga and ARTC Interstate Network Division - South Corridor office are adjacent to the station.

Pedestrian access to the station from Edward Street is provided via footpaths on Station Place. Footpaths also connect to Wagga Wagga Station pedestrian bridge over the rail line to Railway Street.

Through Albury the Main South Line carries the passenger rail services connecting Melbourne, Sydney, Canberra, and Griffith. Additionally, the rail line is an important freight corridor. Table 4.44 shows the average daily passenger and freight rail services that currently operate through the area.

Table $4.44 \quad$ Existing passenger services - Wagga Wagga Railway Station

|  | PASSENGER | FREIGHT | TOTAL |
| :--- | :---: | :---: | :---: |
| Average daily two-way services | 4 | 12 | 16 |

Source: $\quad$ https://transportnsw.info/trip\#/departures? depart $=26501$ \& type $=$ platform\&accessible=false
The rail line, station, and road/rail interfaces are illustrated in Figure 4.44 below.
The existing road/rail interfaces in the Wagga Wagga work precinct including rail level crossings, road bridges and underpasses are described below in Table 4.45.

Table $4.45 \quad$ Existing rail crossings - Wagga Wagga work precinct

| WORK SITE | ROAD NAME | ROAD TYPE | CROSSING TYPE |
| :--- | :--- | :--- | :--- |
| Uranquinty Yard <br> clearances | Yarragundry Street | Two-way, two lanes | Level Crossing - Active |
| Pearson Street bridge | Fernleigh Road | Two-way, two lanes | Level Crossing - Active |
|  | Pearson Street | Two-way, two lanes | Grade-separated - road over rail |
| Wagga Station and <br> surrounds | Bourke Street | Two-way, four lanes | Level Crossing - Active |
|  | Edmondson Street | Two-way, four lanes | Grade-separated - road over rail |
|  | Edward Street | Two-way, four lanes | Grade-separated - rail over road |
| Bomen Yard clearances | Dampier Street | Two lane - two way | Closed Level Crossing |
|  | Merino Street | Two lane - two way | Grade-separated - rail over road |



### 4.5.3 HEAVY VEHICLES ROUTES

Figure 4.45 shows the heavy vehicle routes that operate through the Wagga Wagga precinct. Heavy vehicle routes are located along the proposed construction access routes for the Uranquinty Yard clearances, Pearson Street bridge, Wagga Wagga Yard clearances and Bomen Yard enhancement sites on the following key road links:

- Olympic Highway
- Pearson Street
- Cheshire Street
- Fernleigh Road
- Edward Street
- Fox Street
- Byrnes Road
- Merino Road.

In addition to these routes, the Regional Freight Transport Plan 2019 (RFTP) by Riverina Eastern Regional Organisation of Councils (REROC) identifies the Olympic Highway from Hume Highway to Illabo as a REROC Strategic Highway and the Federal Department of Infrastructure, Transport, Regional Development and Communications identifies the Sturt Highway as a key national freight route.


### 4.5.4 TRAVELLING STOCK RESERVES

Figure 4.46 shows Travelling stock routes within the Wagga Wagga precinct. It is noted that there are livestock highways along the Olympic Highway through Uranquinty, along the Sturt Highway through Wagga Wagga and Bourke Street/ Docker Street through central Wagga Wagga to the intersection of Sturt Highway/Docker Street.


### 4.5.5 PUBLIC TRANSPORT NETWORKS

### 4.5.5.1 PUBLIC BUSES

Figure 4.47 shows the public bus routes that operate within the vicinity of the Wagga Wagga precinct enhancement sites.
Table 4.46 shows all bus services accessible within Wagga Wagga as shown in Figure 4.47.
Table $4.46 \quad$ Existing public bus services - Wagga Wagga work precinct

| SERVICE | DESTINATION | SERVICES PER DAY MON- FRI | SERVICES <br> PER DAY <br> SATURDAY | SERVICES PER DAY SUNDAY AND PUBLIC HOLIDAYS |
| :---: | :---: | :---: | :---: | :---: |
| 921 | Junee | 2 | - | - |
| 922 | Junee | 2 | - | - |
| 930 | Ganmian | 2 | - | - |
| 931 | Coolamon | 2 | - | - |
| 960 | Lake Albert to Charles Sturt University | 17 | 15 | 10 |
| 961 | Bourkelands | 16 | 14 | 8 |
| 962 | Glenfield Park | 17 | 13 | 5 |
| 963 | Glenfield Park | 14 | 14 | 5 |
| 965 | Forest Hill | 10 | 6 | 4 |
| 966 | Estella | 9 | 7 | 5 |
| 969 | Tatton | 15 | 13 | 5 |
| $\begin{aligned} & 702 \\ & \text { (TrainLink) } \end{aligned}$ | Queanbeyan (Mondays and Fridays only) | 1 | - | - |
| $\begin{aligned} & 704 \\ & \text { (TrainLink) } \end{aligned}$ | Queanbeyan (Tuesdays and Thursdays only) | 1 | 1 | - |
| 727 | Tumbarumba (Mondays, Wednesdays, and Fridays only) | 1 | - | - |
| 731 | Griffith | 1 | - | - |
| 733 | Echuca (Mondays, Wednesday, Fridays, and Sundays only) | 1 | - | 1 |
| 735 | Griffith (Mondays and Saturdays only) | 1 | 1 |  |



The public buses services operating on roads expected to support proposal construction or operational movements within the Wagga Wagga precinct are described below in Table 4.47.

Table 4.47 Existing public bus routes on key road links- Wagga Wagga

| SERVICE | ENHANCEMENT SITES | KEY ROAD LINKS | KEY BUS STOP (NAME / NUMBER) |
| :---: | :---: | :---: | :---: |
| Route 1W - Coolamon via Downside, Route 931 Coolamon to Wagga Wagga, Route 930 - Ganmain, 921 Junee to Wagga Wagga | Edmondson Street bridge <br> Pearson Street bridge <br> Harefield Yard clearances | Uses Edmondson Street, Coleman Street, Edward Street, and has stops on Edmondson Street Uses Harefield Road | Kildare Catholic College / 2650107 and 265098 <br> Pearson Street before Edward Street / 265078 |
| Route 969 - Tatton to Wagga <br> Wagga, 965 - Forest Hill | Edmondson Street bridge | Uses Edmondson Street and has stops on Edmondson Street and Railway Street | Railway Street at Collins Street / 2650305 <br> Kildare Catholic College / <br> 2650107 and 265098 |
| 961 - Wagga Wagga - <br> Bourkelands | Edmondson Street bridge | Uses and stops on Docker/ Bourke Street | Docker Street opposite Meurant Ave / 2650250 <br> Henschke Primary School / 2650100 |
| 970 - Bomen via Wagga CBD | Pearson Street bridge | Uses Fernleigh Road | No stops on key links |
| 923 - Junee to Wagga Wagga via Junee Station | Bomen | Uses Byrnes Road | No stops on key links |
| 998 - Wagga Wagga <br> Marketplace | Edmondson Street bridge | Uses Station Place | Wagga Wagga Station / 26502 |

### 4.5.5.2 SCHOOL BUSES

There are wide variety of school bus routes in Wagga Wagga which service numerous schools within the area and the surrounding region. The majority of the school bus routes use or cross Edward Street as part of their routes, as a number of schools are located near The Wagga Wagga Station and on Edmondson Street and Mitchelmore Street. The school bus routes identified in the area are shown below in Table 4.48.

Table $4.48 \quad$ Existing school bus routes on key road links - Wagga Wagga

| BUS ROUTE | ENHANCEMENT <br> SITES | KEY ROAD LINKS | KEY SCHOOL BUS STOPS <br> (NAME / NUMBER) |
| :--- | :--- | :--- | :--- |
| S100 - Mount Austin Public <br> School, S120 - Wagga Wagga <br> HS, S122 - Gobbagombalin, <br> S123 - Sturt PS, S150 - The <br> Riverina College, S159 - | Edmondson Street <br> bridge | Uses and stops on <br> Edmondson Street | - Kildare Catholic College / |
| Ashmont, S171 - South Wagga |  |  |  |
| PS, S179 - South Wagga PS, |  |  | South Wagga Public School / <br> S199 - North Wagga Wagga, <br> S210 - Marrar, S215 - Lockhart, |
|  |  |  |  |
| S216 - Currawarna, S243 - |  |  |  |
| Wagga to Gundagai, S188 - |  |  |  |
| North Wagga PS, |  |  |  |


| BUS ROUTE | ENHANCEMENT SITES | KEY ROAD LINKS | KEY SCHOOL BUS STOPS (NAME / NUMBER) |
| :---: | :---: | :---: | :---: |
| S203 - TRAC to Lloyd, S197Estella to Wagga Wagga High School, S191 - The Riverina Anglican College to Kooringal via Uranquinty, S185 - South Wagga Wagga Primary to Estella, S173 - North Wagga Wagga Primary to Henschke Primary, S172 - Wagga Wagga Primary to Tarcutta, S167 - Estella to Lake Albert Primary, S162 - Glenfield Park to Kildare, S149 - The Riverina Anglican College to Mangoplah, S144 - Estella to Turvey Park Primary, S134 North Wagga Wagga to Wagga Wagga Primary, S124 - Wagga Wagga Primary to Ashmont via The Rock |  |  |  |
| S103 - South Wagga PS | Edmondson Street bridge | Uses and stops on Edmondson Street and Railway Street | - Kildare Catholic College / |
| S109 - Wagga Wagga Primary, <br> S121 - South Wagga Primary, <br> S138 - Forest Hill, S163 - <br> Wagga Wagga Primary, S190 - <br> Uranquinty to Wagga Wagga Primary | Edmondson Street bridge <br> Uranquinty | Uses and stops on Railway Street | $\begin{aligned} & -\quad \text { Railway Street at Collins } \\ & \text { Street / } 2650305 \text { \&265073 } \end{aligned}$ |
| S126 - Lake Albert, S187Gumly Gumly, S196 - Ladysmith | Edmondson Street bridge | Uses Erin and Edmondson Street. Stops on Edmondson Street | $\begin{aligned} & \text { - Railway Street at Collins } \\ & \text { Street / } 2650305 \text { \&265073 } \end{aligned}$ |
| S129 - Glenfield Park, S250 San Isidore, S130 - Mater Dei College, S143 - South Wagga Wagga Primary | Edmondson Street bridge | Uses Erin and Edmondson <br> Street. Stops on Edmondson Street and Railway Street | $\begin{array}{r} \text { - Kildare Catholic College / } \\ 2650107 \text { and } 265098 \\ -\quad \text { Railway Street at Collins } \\ \text { Street / } 2650305 \text { \&265073 } \end{array}$ |
| S148 - Holy Trinity Primary, <br> S155 - South Wagga Wagga, <br> S151 - Forest Hill, S174 - Forest <br> Hill to Wagga Wagga High | Edmondson Street bridge | Uses Erin, Railway, Coleman, and Edmondson Street. Stops on Edmondson Street | - Kildare Catholic College / <br>  2650107 and 265098 <br> - MacLeay Street at Erin Street <br>  $/ 2650220$ and 2650358 <br> - Kildare Catholic College, <br>  Coleman Street / 2650340 |

### 4.5.6 ACTIVE TRANSPORT NETWORKS

### 4.5.6.1 CYCLING NETWORK

Figure 4.48 shows the designated cycle infrastructure that TfNSW has classified in Wagga Wagga. No dedicated cycle infrastructure is provided in Uranquinty or Bomen. In all areas the existing road lanes or shoulders may be used by cyclists.

Additionally, Wagga Wagga City Council are planning and constructing a 56 km network of shared and cycle paths across Wagga Wagga, referred to as the Wagga Wagga Active Travel Plan, which aims to provide active transport alternatives to car travel. One of the links in this plan crosses the rail corridor at the Cassidy Parade pedestrian bridge connecting to Brookong Avenue and Murray Street to the north and Cassidy Parade and Norman Street to the south of the rail corridor (Wagga Wagga City Council, 2021).

### 4.5.6.2 PEDESTRIAN NETWORK

Footpaths are present on most roads within the urban area of the Wagga Wagga precinct and pedestrian crossings are provided at most signalised intersections, and many unsignalised intersections. Typically, there is not provision of connected pedestrian infrastructure in the vicinity of enhancement sites in rural areas such as in Bomen.

There are also several opportunities to cross the rail line at grade separated and level crossings and pedestrian overpasses as detailed in Table 4.49 and Figure 4.49.

Table $4.49 \quad$ Pedestrian rail crossing opportunities - Wagga Wagga work precinct

| ENHANCEMENT SITE | LOCATION | CROSSING TYPE |
| :---: | :---: | :---: |
| Uranquinty Yard clearances | Yarragundry Street | Railway Level Crossing |
| Pearson Street bridge | Fernleigh Road | Railway Level Crossing |
|  | Pearson Street | Grade-separated - road over rail |
| Wagga Wagga Station and surrounds | Bourke/Docker Street | Railway Level Crossing |
|  | Cassidy Parade | Pedestrian overpass |
|  | Edmondson Street | Grade-separated - road over rail |
|  | Wagga Wagga Station pedestrian bridge | Pedestrian overpass |
|  | Edward Street | Rail bridge over road/footpath |

Engagement with the South Wagga Public School has revealed Wagga Wagga Station pedestrian bridge connecting to Railway Street and Edmondson Street pedestrian path is particularly important to the community as the limited on-site parking and drop-off facilities combined with restricted adjacent roadside parking results in many people using Railway Street to drop off students who subsequently use the Edmondson Street pedestrian path and Wagga Wagga Station pedestrian bridge ( 250 m east of Edmondson Street) to access the school. Figure 4.49 shows existing opportunities to cross the rail line in the Wagga Wagga precinct.



### 4.6 JUNEE PRECINCT

Junee precinct includes the following enhancement sites:

- Harefield Yard clearances
- Kemp Street bridge
- Junee Station pedestrian bridge
- Junee Yard clearances
- Olympic Highway underbridge
- Junee to Illabo clearances.

Due to their proximity Kemp Street bridge, Junee Station pedestrian bridge and Junee Yard clearances were considered collectively (referred to as Junee Station and surrounds).

The existing traffic and transport network relevant to the Junee precinct is discussed in the following sections.

### 4.6.1 ROAD NETWORK

The Harefield and Junee sites are connected by Byrnes Road running north-south between them and adjacent to the railway line. The sites from Junee to Illabo are connected by the Olympic Highway running north-south between them. The precinct includes a number of key railway crossings. The enhancement sites and main road links within the precinct are shown below in Figure 4.50.


### 4.6.1.1 HAREFIELD YARD CLEARANCES ENHANCEMENT SITE

The key road links and intersections expected to support the construction or operational movements related to the proposal for the Harefield Yard clearances enhancement site are depicted below in Figure 4.51. Key road characteristics are described in Table 4.50 and key intersection configurations are shown in Appendix C.

Table 4.50 Key road links - Harefield Yard clearances enhancement site

| ROAD | ROAD DESCRIPTION |
| :--- | :--- |
| NAME |  |$\quad$| Harefield |
| :--- |
| Road | | Two-way, one lane rural locally controlled arterial that runs from the Olympic Highway to Byrnes Road |
| :--- |
| at Harefield and provides access to surrounding rural properties and the Harefield Railway Station. |
| In the vicinity of the Harefield Yard clearances enhancement site the highway generally features a 6.2 m |
| sealed width, unsealed shoulders, and has a posted speed limit of 100km/h. |$|$| Byrnes Road |
| :--- |
|  |
| Two-way, two lane rural locally controlled road running generally north-south between Oura Road and <br> the Olympic Highway at Junee, connecting Bomen, Junee, and Harefield and providing access to the <br> Harefield Intermodal Terminal. <br> In the vicinity of the Harefield Yard clearances enhancement site the main north-south movement has <br> been rerouted to separate Pattersons Road from the Harefield Road/Byrnes Road intersection, with the <br> original road alignment also retained to provide access to the Rural Fire Service. On the main alignment <br> the road generally features 3.5m wide lanes, sealed shoulders, and has a posted speed limit of 100km$/ \mathrm{h}$. <br> The access road features a 4.4m sealed width (approx.) and unsealed shoulders. No speed limit signs <br> were noted. |
| Harefield <br> Railway <br> Access Road |
| Two-way, one lane rural locally controlled road that generally runs southwest from Harefield Road and <br> provides access to the Harefield railway yard. <br> In the vicinity of the Harefield Yard clearances enhancement site the road generally features a 4.4m <br> sealed width (approx.) and unsealed shoulders. No speed limit signs were noted. |

Albury to Illabo
Figure 4.51 Key road links and intersections - Harefield Yard clearances enhancement site

| $\begin{gathered} 0 \\ \hline \end{gathered}$ | Proposal site | ILABO <br> UNEE |
| :---: | :---: | :---: |
| Coordinate System: GDA 1994 MGA Zone 55 <br>  | Existing railway | sawaga |
|  | Main road |  |
| Nomen | - Local road |  |
|  | Key intersection | Brook |
| Date: 11/11/2021 $\quad$ Paper: A3 Author: WSP Sata Sources: ARTC, NSWSS | y road lin | albury |

## TRAFFIC VOLUMES

Observed traffic volumes for the roads expected support the construction or operational movements related to the proposal for the Harefield Yard clearances enhancement site are shown in Table 4.51. Where published AADT data was not available or considered inappropriate, estimations based on comparable locations, as detailed in the methodology, are presented.

Table 4.51 Harefield Yard clearances enhancement sites observed traffic volumes

| ROAD NAME | COUNT YEAR | DAILY <br> (TWO-WAY) <br> VOLUME | HV PROPORTION |
| :--- | :---: | :---: | :---: |
| Harefield Road | 2016 | 173 | $38 \%$ |
| Byrnes Road $^{1}$ | 2018 | 2,590 | $33 \%$ |
| Harefield Railway Access Road $^{2}$ | N/A | $50-100$ | Not available |

(1) Byrnes Road, north of Harefield Road
(2) No data available, traffic volume estimated based on road type and surrounding land uses

ROAD SAFETY
Figure 4.52 shows that an insufficient number of crashes were recorded for any significant observations in in the vicinity of the Harefield Yard clearances enhancement site


Source: https://roadsafety.transport.nsw.gov.au/statistics/interactivecrashstats
Figure 4.52 Crash data (2015-2019) Harefield Yard clearances enhancement site

## PARKING

Within the rural areas in the vicinity of the Harefield Yard clearances enhancement site there is limited provision of on street parking and demand for this parking would be low due to provision of off-street parking within industrial land uses in the surrounding area. There is no designated parking within the enhancement site.

### 4.6.1.2 JUNEE STATION AND SURROUNDS

The Junee Station and surrounds share the same road network and have been combined in the following section, consisting of:

- Kemp Street bridge enhancement site
- Junee Station pedestrian bridge enhancement site
- Junee Yard clearances enhancement site.

The key road links and intersections expected to support the construction or operational movements related to the proposal for the Junee Station and surrounds are depicted below in Figure 4.53. Key road characteristics are described in Table 4.52 and key intersection configurations are shown in Appendix C.

Table $4.52 \quad$ Key road links - Junee Station and surrounds

| ROAD NAME | ROAD DESCRIPTION |
| :---: | :---: |
| Kemp Street Olympic Highway | Two-way, two lane state-controlled highway that generally runs east-west and connects the Northern Expressway in South Australia and the Hume Highway in NSW. Kemp Street runs eastwest and serves as a key cross-rail connectivity corridor via a rail overpass from Ducker Street and connects to the Olympic Highway at the Seignior Street intersection. <br> In the vicinity of the Junee Station and surrounds the highway is generally urban and features 3.3 m wide lanes, sealed shoulders with parking, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |
| Seignior Street | Two-way, two lane urban state-controlled road running generally north-south between the Olympic Highway/Kemp Street intersection and Broadway Street, forming part of the Olympic Highway and providing access through central Junee west of the rail line. <br> In the vicinity of the Junee Station and surrounds the road generally features 3.5 m wide lanes, sealed shoulders with areas of angle parking, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |
| Humphreys Street | Two-way, two lane urban locally controlled street running east-west between Peel Street and Main Street and providing access to Junee Railway Station and central Junee east of the rail line. <br> In the vicinity of the Junee Station and surrounds the road generally features 5.5 m wide lanes, sealed shoulders with angle parking, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |
| Main Street (Olympic Highway) | Two-way, two lane urban street that forms part of the state-controlled highway Olympic highway running generally north-south from Railway Square and providing access to residential areas of Junee and the Junee Memorial Park. The Olympic Highway crosses the rail line via an at-grade rail level crossing between Seignior Street and Main Street and via a rail overpass north of Cedric Street. <br> In the vicinity of the Junee Station and surrounds the road generally features 3.5 m wide lanes, sealed shoulders with parking, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |
| Lorne Street/Peel Street/Ducker Street | Two-way, two lane urban locally controlled road running north-south through Junee from Cox Street and providing access to the Junee Public School, Junee Junction Recreation \& Aquatic Centre, Junee Skate Park, and commercial areas in central Junee east of the rail line. <br> In the vicinity of the Junee Station and surrounds the road generally features 3.5 m wide lanes, sealed shoulders with parking, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |
| Hill Street | Two-way, two lane urban locally controlled street that crosses Lorne Street and runs east-west from the railway line and provides access to residential areas in east Junee. <br> In the vicinity of the Junee Station and surrounds the road generally features 6 m wide lanes, sealed shoulders, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |


| ROAD NAME | ROAD DESCRIPTION |
| :---: | :---: |
| Joffre Street | Two-way, two lane urban locally controlled street that runs north-south from the Olympic Highway to Crawley Street and provides access to residential areas in west Junee. <br> In the vicinity of the Junee Station and surrounds the road generally features a 7.1 m sealed width, unsealed shoulders, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |
| Harold Street | Two-way, two lane urban locally controlled street that crosses Thomas Street and runs north-south from the Olympic Highway and provides access to residential areas in west Junee. <br> In the vicinity of the Junee Station and surrounds the road generally features a 10.2 m sealed width, sealed shoulders with parking, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |
| Thomas Street | Two-way, two lane urban locally controlled street that crosses Railway Lane and runs east-west from the railway line and provides access to residential areas in west Junee. <br> In the vicinity of the Junee Station and surrounds the road generally features a 6 m sealed width, sealed shoulders, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |
| Railway Lane | Two-way, two lane urban locally controlled street that crosses Thomas Street and runs north-south from the Olympic Highway and provides access to residential areas in west Junee. <br> In the vicinity of the Junee Station and surrounds the road generally features a 3.8 m sealed width, unsealed shoulders with parking, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |
| Railway Parade | Two-way, two lane urban locally controlled street that crosses Thomas Street and runs north-south from the Olympic Highway and provides access to residential areas in west Junee. <br> In the vicinity of the Junee Station and surrounds the road generally features a 7.6 m sealed width, sealed shoulders with parking, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |
| William Street | Two-way, two lane urban locally controlled street that crosses Lorne Street and runs east-west from the railway line and provides access to residential areas in east Junee. <br> In the vicinity of the Junee Station and surrounds the road generally features a 12 m sealed width, sealed shoulders, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |
| Edgar Street/ <br> Byrnes Road | Two-way, two lane rural locally controlled street running generally north-south between Oura Road and the Olympic Highway at Junee, connecting Bomen, Junee, and Harefield and providing access to the Harefield Intermodal Terminal. <br> In the vicinity of the Junee Station and surrounds the road generally features 3.5 m wide lanes, sealed shoulders, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |
| Pretoria Avenue | Two-way, two lane urban locally controlled street that crosses Joffre Street and runs east-west from the seignior Street and provides access to residential areas in west Junee. <br> In the vicinity of the Junee Station and surrounds the road generally features a 7.2 m sealed width, sealed shoulders with parking, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |




## TRAFFIC VOLUMES

Observed traffic volumes for the roads expected support the construction or operational movements related to the proposal for the Junee Station and surrounds are shown below in Table 4.53.

Table 4.53 Junee Station and surrounds enhancement sites observed traffic volumes

| ROAD NAME | COUNT YEAR | DAILY (TWO-WAY) VOLUME | $\begin{gathered} \text { HV } \\ \text { PROPORTION } \end{gathered}$ |
| :---: | :---: | :---: | :---: |
| Olympic Highway (west of Seignior Street) ${ }^{1}$ | 2021 | 3,271 | 3\% |
| Kemp Street ${ }^{1}$ | 2021 | 2,905 | 2\% |
| Seignior Street ${ }^{1}$ | 2021 | 2,856 | 4\% |
| Broadway Street ${ }^{1}$ | 2021 | 3,363 | 2\% |
| Olympic Highway Level Crossing ${ }^{1}$ | 2021 | 2,292 | 4\% |
| Humphrys Street ${ }^{2}$ | 2021 | 1,146 | 4\% |
| Main Street (Olympic Highway) ${ }^{2}$ | 2021 | 1,146 | 3\% |
| Lorne Street | 2016 | 2,315 | 8\% |
| Hill Street ${ }^{3}$ | 2016 | 926 | 8\% |
| Joffre Street ${ }^{4}$ | $2016{ }^{5}$ | 451 | 8\% |
| Harold Street ${ }^{6}$ | 2016 | 1,158 | 8\% |
| Thomas Street ${ }^{7}$ | $2016{ }^{5}$ | 338 | 8\% |
| Railway Lane ${ }^{1}$ | 2021 | 341 | 3\% |
| Railway Parade ${ }^{8}$ | 2021 | 341 | 3\% |
| William Street ${ }^{9}$ | 2016 | 518 | 8\% |
| Edgar Street | 2018 | 1,436 | 8\% |
| Byrnes Road | 2014 | 2,299 | 8\% |
| Pretoria Avenue ${ }^{7}$ | $2016^{5}$ | 338 | 8\% |

(1) 10 -hour ( 5 am to 10 am and 2 pm to 7 pm ) traffic survey volumes
(2) No data available, volumes estimated as $50 \%$ of Olympic Highway Level Crossing 10 -hour with equivalent HV proportion
(3) No data available, volumes estimated as $40 \%$ of Lorne Street with equivalent HV proportion
(4) No data available, volumes estimated as Crawley Street with equivalent HV proportion
(5) No data available, assume count occurred in 2016 with equivalent HV proportion
(6) No data available, volumes estimated as $50 \%$ of Lorne Street with equivalent HV proportion
(7) No data available, volumes estimated as $75 \%$ of Joffre Street with equivalent HV proportion
(8) No data available, volumes estimated as Railway Lane with equivalent HV proportion
(9) No data available, volumes estimated as $60 \%$ of the difference between Byrnes Road and Edgar Street with equivalent HV proportion.

## ROAD SAFETY

Figure 4.54 shows the crashes that occurred in the data collection period in the vicinity of the Junee Station and surrounds, with the following observations noted:

- Olympic Highway/Seignior Street/Kemp Street (key road links and intersection) - two crashes
- Seignior Street (key road link) - three crashes
- no fatal crashes are noted in the vicinity of these enhancement sites.

It is noted that the areas with a greater occurrence of crashes are also roads carrying a high volume of vehicles (relative to the rest of the network), increasing the overall crash exposure risk.


Source: https://roadsafety.transport.nsw.gov.au/statistics/interactivecrashstats
Figure $4.54 \quad$ Crash data (2015-2019) Junee Station and surrounds

## PARKING

Within the urban areas of Junee, on-street kerbside parking is generally allowed unless signed otherwise and demand for this parking would be low due to provision of off-street parking within commercial, industrial, retail, and residential uses in the surrounding area. There is no designated parking within the enhancement site. Further detail around parking on key links is provided below in Table 4.54.

Table 4.54 Parking provisions -Junee Station and surrounds

| LOCATION | PARKING | TIME OF DAY <br> RESTRICTIONS |
| :--- | :--- | :--- |
| Kemp Street | Kerbside parking | No restrictions |
| Seignior Street | Kerbside parking <br> Angle parking north of Anzac Avenue | $1 P^{1}$ for angle parking in <br> central Junee |
| Humphreys Street | Kerbside parking | No restrictions |
| Railway Square (Junee <br> Railway Station) | Junee Station Parking: 13 spaces. One PWD space | No restrictions |
| Main Street (Olympic <br> Highway) | Kerbside parking | No restrictions |


| LOCATION | PARKING | TIME OF DAY <br> RESTRICTIONS |
| :--- | :--- | :--- |
| Lorne Street/Peel Street/ <br> Ducker Street | Kerbside parking <br> Designated commercial parking behind train station: 60 car <br> spaces (approximately) | No restrictions |
| Hill Street | Kerbside parking | No restrictions |
| Thomas Street | Kerbside parking | No restrictions |
| Railway Lane | Kerbside parking | No restrictions |
| Railway Parade | Kerbside parking | No restrictions |
| William Street | Kerbside parking | No restrictions |
| Edgar Street/Byrnes Road | Kerbside parking permitted where space allows | No restrictions |
| Joffre Street | Kerbside parking | No restrictions |
| Pretoria Avenue | Kerbside parking | No restrictions |

(1) One-hour parking

### 4.6.1.3 OLYMPIC HIGHWAY UNDERBRIDGE ENHANCEMENT SITE

The key road links and intersections expected to support the construction or operational movements related to the proposal for the Olympic Highway under bridge enhancement site are depicted below in Figure 4.55. Key road characteristics are described in Table 4.55 and key intersection configurations are shown in Appendix C.

Table 4.55 Key road links - Olympic Highway under bridge enhancement site

| ROAD <br> NAME | ROAD DESCRIPTION |
| :--- | :--- |
| Main Street <br> (Olympic <br> Highway) | Two-way, two lane state-controlled highway running generally north-south from Railway Square, <br> forming part of the Olympic Highway and providing access to northern residential areas of Junee and <br> the Junee Memorial Park, extending north and connecting to Illabo. The Olympic Highway crosses the <br> rail line via an at-grade rail level crossing between Seignior Street and Main Street and via a rail <br> overpass north of Cedric Street. |
| Illabo Road <br> (Olympic <br> Highway) | Two-way, two lane local road that runs north-south between Regent Street and Olympic Highway, <br> providing access to residential areas and the Highway. <br> In the vicinity of the enhancement site the road generally features a 13.2 m sealed width, minimal road <br> marking, shoulders with parking, and has a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. |



Albury to Illabo

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Proposal site
Existing railway
Main road
Local road
Key intersection
Key road links

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## TRAFFIC VOLUMES

Observed traffic volumes for the roads expected support the construction or operational movements related to the proposal for the Olympic Highway under bridge enhancement site are shown below in Table 4.56. Where published AADT data was not available or considered inappropriate, estimations based on comparable locations, as detailed in the methodology, are presented.

Table 4.56 Olympic Highway under bridge enhancement site observed traffic volumes

| ROAD NAME | COUNT YEAR | DAILY (TWO- <br> WAY) VOLUME | HV <br> PROPORTION |
| :--- | :---: | :---: | :---: |
| Main Street (Olympic Highway) ${ }^{1}$ | 2011 | 1,718 | $16 \%^{3}$ |
| Illabo Road $^{2}$ | 2015 | 592 | $6 \%$ |

(1) Olympic Highway - 90m North of Illabo Road, Junee
(2) No data available, volumes estimated as John Potts Drive, Junee with equivalent HV proportion
(3) No data available, heavy vehicles estimated as Cox Street, Junee with equivalent HV proportion.

## ROAD SAFETY

Figure 4.56 shows the crashes that occurred in the data collection period in the vicinity of the Olympic Highway underbridge enhancement site, with the following observations:

- Main Street (key road link) - two crashes
- Regent Street (key road link) - three crashes
- no fatal crashes are noted in the vicinity of this enhancement site.

It is noted that the areas with a greater occurrence of crashes are also roads carrying a high volume of vehicles (relative to the rest of the network), increasing the overall crash exposure risk.


[^0]Figure 4.56 Crash data (2015-2019) Olympic Highway under bridge enhancement site

## PARKING

On-street kerbside parking is generally allowed on the urban road network in the vicinity of the Olympic Highway underbridge enhancement site unless signed otherwise and demand for this parking would be low due to provision of offstreet parking within commercial, industrial, retail, and residential uses in the surrounding area. There is no designated parking within the enhancement site.

### 4.6.1.4 JUNEE TO ILLABO CLEARANCES ENHANCEMENT SITE

The key road links and intersections expected to support the construction or operational movements related to the proposal for the Junee to Illabo clearances enhancement site are depicted below in Figure 4.57 and Figure 4.58. Key road characteristics are described in Table 4.57 and key intersection configurations are shown in Appendix C.

Table $4.57 \quad$ Key road links - Junee to Illabo clearances enhancement site

| ROAD NAME | ROAD DESCRIPTION |
| :--- | :--- |
| Olympic Highway | Two-way, two lane state-controlled highway that runs from the Hume Highway l8km north of <br> Albury (23km north of the Murray River) to the Mid-Western Highway at Cowra. <br> In the vicinity of the Junee to Illabo clearances enhancement site the highway generally features <br> 3.5 m wide lanes, partially sealed shoulders, and has a posted speed limit of 100km/h. |
| Brabins Road | Two-way, one lane locally controlled road that generally runs north-south from the Olympic <br> Highway and provides access to surrounding rural properties. The road crosses the rail line via an <br> at-grade rail level crossing. <br> In the vicinity of the Junee to Illabo clearances enhancement site the road generally features a 6.2m <br> sealed width, unsealed shoulders, and a 100km/h speed limit. |
| Waterworks Road | Two-way, one lane locally controlled road running generally north-south between Ballengorrah <br> Lane and Main Street in Junee, rural properties in Wantiool with the Olympic Highway and Junee. <br> In the vicinity of the Junee to Illabo clearances enhancement site the road is generally unsealed and <br> features unsealed shoulders and a 100km/h speed limit. |
| Marinna Station <br> Access Road | Two-way, one lane locally controlled road that provides access to Marinna Station and silo. <br> In the vicinity of the Junee to Illabo clearances enhancement site the road is generally unsealed and <br> features unsealed shoulders and a 100km/h speed limit. |
| Marinna Station <br> Cross Road | Two-way, one lane locally controlled road that connects Waterworks Road and the Olympic <br> Highway. <br> In the vicinity of the Junee to Illabo clearances enhancement site the road is generally unsealed and <br> features unsealed shoulders and a 100km/h speed limit. |
| Lawford Street/ <br> Junee Street | Two-way, one lane locally controlled road that connects Brabins Road and Morris Street and <br> provides access to the silo on Junee Street. <br> In the vicinity of the Junee to Illabo clearances enhancement site the road is generally unsealed and <br> features unsealed shoulders and a 100km/h speed limit. |




## TRAFFIC VOLUMES

Observed traffic volumes for the roads expected support the construction or operational movements related to the proposal for the Junee to Illabo Yard clearances enhancement site are shown below in Table 4.58. Where published AADT data was not available or considered inappropriate, estimations based on comparable locations, as detailed in the methodology, are presented.

Table 4.58 Junee to Illabo Yard clearances enhancement site observed traffic volumes

| ROAD NAME | COUNT YEAR | DAILY (TWO- <br> WAY) <br> VOLUME | HV <br> PROPORTION |
| :--- | :---: | :---: | :---: |
| Olympic Highway $^{1}$ | 2011 | 1,718 | $16 \%$ |
| Brabins Road | 2014 | 44 | Not available |
| Waterworks Road | 2014 | 241 | Not available |
| Marinna Station Access Road | N/A | 10 | Not available |
| Marinna Station Cross Road ${ }^{2}$ | 2014 | 44 | Not available |
| Lawford Street/ Junee Street N/A | 10 | Not available |  |

(1) Olympic Highway - 90m North of Illabo Road, Junee
(2) No data available, volumes estimated as Brabins Road, Illabo with equivalent HV proportion
(3) Estimated traffic volume based on road type and surrounding land uses.

## ROAD SAFETY

Figure 4.59 shows that an insufficient number of crashes were recorded to identify any significant observations in the vicinity of the Junee to Illabo clearances enhancement site.


Source: https://roadsafety.transport.nsw.gov.au/statistics/interactivecrashstats
Figure 4.59 Crash data (2015-2019) Junee to Illabo clearances enhancement site

## PARKING

Within the rural areas in the vicinity of the Junee to Illabo clearances enhancement site, site there is limited provision or demand of on street parking and demand for this parking would be low due to provision of off-street parking within industrial land uses in the surrounding area. There is no designated parking within the enhancement site. There is no designated parking within the enhancement site.

### 4.6.2 RAIL NETWORK

The Main South Line runs through the Junee precinct from Harefield to Illabo and features eight road crossings (2 gradeseparated, 6 active) in the vicinity of the enhancement sites.

The heritage-listed Junee Railway Station located on Railway Square is the one operating railway station in the Junee precinct and is adjacent to the Junee station enhancement site. The station features commuter parking, passenger dropoff, and public bus stops and services The Main South Line.

Pedestrian access to the station is provided via footpaths on Station Square, Lorne Street, and Main Street. Footpaths also connect to the rail level crossing on the Olympic Highway.

Through Junee the Main South Line carries the passenger rail services connecting Melbourne, Sydney, Canberra, and Griffith. Additionally, the rail line is an important freight corridor. Table 4.59 shows the average daily passenger and freight rail services that currently operate through the area.

Table $4.59 \quad$ Existing passenger services - Wagga Wagga Railway Station

|  | PASSENGER | FREIGHT | TOTAL |
| :--- | :---: | :---: | :---: |
| Average daily two-way services | 4 | 12 | 16 |

Source: https://transportnsw.info/trip\#/departures? depart $=26501$ \& type $=$ platform\&accessible=false
The rail line, station, and road/rail interfaces are illustrated in Figure 4.60 below.
The existing road/rail interfaces in the Junee precinct including rail level crossings, road bridges and underpasses are described below in Table 4.60.

Table $4.60 \quad$ Existing rail crossings - Junee precinct

| ENHANCEMENT SITE | ROAD NAME | ROAD TYPE | CROSSING TYPE |
| :--- | :--- | :--- | :--- |
| Harefield | Harefield Road | Two-way, two lanes | Level Crossing - Active |
| Kemp Street bridge and <br> Junee Station | Kemp Street | Two-way, two lanes | Grade-separated - road over rail |
|  | Junee Station pedestrian <br> overpass | Pedestrian bridge | Pedestrian bridge |
|  | Olympic Highway (between <br> Seignior Street and Main Street | Two-way, two lanes | Level Crossing - Active |
| Olympic Highway <br> underbridge | Main Street | Two-way, two lanes | Grade-separated - rail over road |
| Illabo | Unnamed Road (near <br> Waterworks Road at Marinna) | Two lane, two way | Level Crossing - Active |
|  | Brabins Road | Two lane, two way | Level Crossing - Active |
|  | Olympic Highway | Two lane, two way | Level Crossing - Active |



### 4.6.3 HEAVY VEHICLES ROUTES

Figure 4.61 shows the heavy vehicle routes that operate through the Junee precinct. Heavy vehicle routes are located along the proposed haulage routes within the Junee precinct on the following key road links:

- Byrnes Road
- Harefield Road.
- Olympic Highway
- Seignior Street
- Edgar Street
- Harold Street
- Brabins Road.

In addition to these routes The Regional Freight Transport Plan 2019 (RFTP) by Riverina Eastern Regional Organisation of Councils (REROC) identifies the Olympic Highway from Hume Highway to Illabo as a REROC Strategic Highway.



### 4.6.4 TRAVELLING STOCK RESERVES

Figure 4.62 shows that there are no Livestock Highways in the vicinity of enhancement sites within the Junee precinct. Moving stock on public roads outside of Travelling Stock Reserves is possible with the necessary permits and so stock may at times require limited use of rail crossings within the proposal.


### 4.6.5 PUBLIC TRANSPORT NETWORKS

### 4.6.5.1 PUBLIC BUSES

Figure 4.63 shows the public bus routes that operate within the Junee precinct in the vicinity of the Kemp Street bridge, Junee Station pedestrian bridge, Junee Yard clearances and Olympic Highway underbridge enhancement sites.

Table 4.61 details the public bus routes shown in Figure 4.63.
Table 4.61 Existing public bus services - Junee precinct

| SERVICE | DESTINATION | SERVICES PER DAY MON-FRI | SERVICES PER DAY SATURDAY | SERVICES PER DAY <br> SUNDAY AND PUBLIC HOLIDAYS |
| :---: | :---: | :---: | :---: | :---: |
| 921 | Wagga Wagga | 2 | - | - |
| 922 | Wagga Wagga | 2 | - | - |
| 923 | Wagga Wagga | 1 | - | - |
| 924 | Wagga Wagga | 1 (Thursdays only) | - | - |
| 925 | Wagga Wagga | 1 | - | - |
| 704 (TrainLink) | Queanbeyan (Tuesdays and Thursdays only) | 1 | 1 | - |



The public buses services operating on roads expected to support proposal construction or operational within the Junee precinct are detailed in Table 4.62.

Table $4.62 \quad$ Existing public bus routes on key road links- Junee

| SERVICE | ENHANCEMENT SITES | KEY ROAD LINKS | KEY BUS STOPS (NAME / NUMBER) |
| :---: | :---: | :---: | :---: |
| Wagga, 922 - Junee to Wagga Wagga, 924 Junee to Wagga Wagga via Jail Break Inn, Wallacetown and Brucedale Dr | $\begin{aligned} &- \text { Junee Station and } \\ & \text { surrounds } \\ &- \text { Olympic Highway } \\ & \text { underbridge } \end{aligned}$ | - Uses and stops on Kemp Street, Seignior Street, Harold Street, and Lorne Street | $\begin{array}{ll} - & \text { Kemp Street after Joffre Street / } 2663127 \\ - & \text { Junee Public School / } 266315 \\ - & \text { Junee Station / } 26632 \\ - & \text { Harold Street after Thomas Street / } 26631 \\ - & \text { Lorne Street opposite Belmore Street / } \\ & 266340 \\ - & \text { Illabo Road opposite Marquis Street / } \\ 266341 \end{array}$ |
| 921 - Junee to Wagga via Harefield | $\begin{aligned} &- \text { Junee Station and } \\ & \text { surrounds } \\ &- \text { Olympic Highway } \\ & \text { underbridge } \\ &- \begin{array}{l} \text { Harefield Yard } \\ \text { clearances } \end{array} \end{aligned}$ | - Uses Kemp Street <br> - Uses and stops on <br>  Lorne Street <br> - Harefield Road | - Junee Public School, Lorne Street / 266315 <br> - George Street before Edgar Street / 266339 <br> - Lorne Street opposite Belmore Street / <br>  266340 <br> - Illabo Road opposite Marquis Street / <br>  266341 <br> - Harefield Rd at Byrnes Rd / 2650504 |
| 923 - Junee to Wagga Wagga via Junee Station | - Junee Station and surrounds | - Uses Hill Street and Kemp Street | $\begin{array}{ll} - & \text { Junee Public School, Lorne Street / } 266315 \\ - & \text { Lorne Street opposite Belmore Street / } \\ 266340 \end{array}$ |
| 925 - Junee to Wagga Wagga | - Junee Station and surrounds | - Uses and stops on Lorne Street | - Junee Public School, Lorne Street / 266315 |

### 4.6.5.2 SCHOOL BUSES

The school bus routes identified in the Junee precinct are shown below in Table 4.63.
Table $4.63 \quad$ Existing school bus services on key road links - Junee

| SERVICE | ENHANCEMENT <br> SITES | KEY ROAD LINKS | KEY STOPS (NAME / |
| :--- | :--- | :--- | :--- |
| NUMBER) |  |  |  |$|$| S221 - Junee Schools | Junee Station and <br> surrounds | Uses Olympic Highway and Kemp <br> Street and stops on Olympic Highway | Kemp Street after Joffre <br> Street / 2663127 |
| :--- | :--- | :--- | :--- |
| S226 - Junee Reef to <br> Junee Schools via Marinna <br> Road | Junee Station and <br> surrounds Olympic <br> Highway <br> underbridge | Uses Olympic Highway, Main Street, <br> Regent Street, Broadway Street, Kemp <br> Street, Lorne Street, and Peel Street. <br> Stops on Lorne Street and Peel Street. | Lorne Street opposite <br> Belmore Street / 266340 |
| S242 - Illabo to <br> Cootamundra Schools via <br> Eurongilly and Bethungra | Junee to Illabo <br> Yard clearances | Uses Olympic Highway and Brabins <br> Road. Stops on Olympic Highway. | No stops on key links |

### 4.6.6 ACTIVE TRANSPORT NETWORKS

### 4.6.6.1 CYCLING NETWORK

Figure 4.64 shows the designated cycle infrastructure that TfNSW has classified in Junee. No cycle infrastructure is provided in the Illabo or Harefield work sites. In all areas the existing road lanes or shoulders may be used by cyclists.

### 4.6.6.2 PEDESTRIAN NETWORK

Footpaths are present on some of the major roads within the urban area of the Junee precinct. Typically, there is not provision of connected pedestrian infrastructure in the vicinity of enhancement sites in rural areas such as Harefield and Illabo. There are also several opportunities to cross the rail line at level crossings and one pedestrian overpass to the Junee Railway Station platform (closed), and these locations are described in Table 4.64.

Table $4.64 \quad$ Pedestrian rail crossing opportunities - Junee

| ENHANCEMENT SITE | LOCATION | CROSSING TYPE |
| :--- | :--- | :--- |
| Harefield Yard clearances | Harefield Road | Railway Level Crossing |
| Junee Station and surrounds | Kemp Street | Grade-separated - road over rail |
|  | Olympic Highway (between Seignior <br> Street and Main Street) | Railway Level Crossing |
| Olympic Highway underbridge | Olympic Highway | Rail bridge over road/footpath |
| Junee to Illabo Yard clearances | Unnamed Road (near Waterworks <br> Road at Marinna) | Railway Level Crossing |
| ${\text { Brabins Road }} &{\text { Railway Level Crossing }} \\ {\hline}$ |  |  |

Figure 4.65 shows existing opportunities to cross the rail line in the Junee precinct.




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## 5 IMPACT ASSESSMENT CONSTRUCTION

An impact assessment of the transport networks has been undertaken in accordance with the SEARs to assess the expected impacts of the proposal during construction and to guide the development of mitigation measures to minimise the consequence and/or likelihood of these impacts.

### 5.1 ALBURY PRECINCT

### 5.1.1 CONSTRUCTION PROFILE

This section outlines the construction profile for the proposal within the Albury precinct. This includes all vehicle routes, as shown in section 5.1.1.2, and all volumes of heavy and light vehicles required for construction of the proposal, as shown in section 5.1.1.3, which includes the vehicles required for the import and export of fill material. It also outlines other construction requirements, such as temporary road closures and diversions, and parking requirements for each enhancement site.

### 5.1.1.1 CONSTRUCTION PROGRAM

Key construction stages and work durations at each enhancement site within the Albury precinct are summarised in Table 5.1 and Figure 5.1.

Table 5.1 Summary of construction stages - Albury precinct
$\left.\begin{array}{|l|l|c|c|c|c|}\hline \begin{array}{l}\text { ENHANCEMENT } \\ \text { SITES }\end{array} & \begin{array}{l}\text { CONSTRUCTION STAGES } \\ \text { UNDERTAKEN }\end{array} & \text { START } & \text { FINISH } & \begin{array}{c}\text { DURATION } \\ \text { OF WORKS } \\ \text { (MONTHS) }\end{array} & \begin{array}{c}\text { RAIL } \\ \text { POSSESSION } \\ \text { REQUIRED }\end{array} \\ \hline \begin{array}{l}\text { Murray River } \\ \text { bridge }\end{array} & - \text { Site establishment } \\ \text { Rail bridge structure } \\ \text { modifications } \\ \text { Demobilisation and landscaping }\end{array}\right)$
$\left.\begin{array}{|l|l|c|c|c|c|}\hline \begin{array}{l}\text { ENHANCEMENT } \\ \text { SITES }\end{array} & \begin{array}{l}\text { CONSTRUCTION STAGES } \\ \text { UNDERTAKEN }\end{array} & \text { START } & \text { FINISH } & \begin{array}{c}\text { DURATION } \\ \text { OF WORKS } \\ \text { (MONTHS) }\end{array} & \begin{array}{c}\text { RAIL } \\ \text { POSSESSION } \\ \text { REQUIRED }\end{array} \\ \hline \begin{array}{l}\text { Billy Hughes } \\ \text { bridge }\end{array} & - \text { Site establishment } \\ \hline- \text { Track lowering } \\ \text { Track realignment }(>300 \mathrm{~m} \\ \text { and/or track formation } \\ \text { replacement) }\end{array}\right)$


Figure $5.1 \quad$ Albury precinct construction programme

### 5.1.1.2 CONSTRUCTION AND DIVERSION ROUTES

Proposed construction routes and accesses to enhancement sites in the Albury precinct are shown in Figure 5.2 to Figure 5.5. No vehicle diversions are required in the Albury precinct.

Construction routes have been selected to minimise the use of local roads where possible. However, use of local roads is generally required to facilitate access to enhancement sites. As shown in section 5.1.1.3, construction vehicle volumes using construction routes and accesses on local roads are generally low.

Mitigations for the use of all road types, including local roads are provided in section 8.2. In addition, mitigation measures have been identified for other assessments, including noise and vibration, visual and social, to address potential impacts from the use of construction and diversion routes.

Where diversions are required for active travel routes, the selected diversion route has considered where pedestrian infrastructure is present. Where cyclists utilise diversion routes, and an existing cycle or shared path is not present, cyclists would be required to cycle on-road. To facilitate access to the rail corridor and surrounds for construction vehicles, including surrounding residences, diversion of pedestrians and cyclists within the proposal site would also be required. Detailed consideration of the management of pedestrian and cyclist safety within the proposal site will be completed prior to and during construction. Mitigation measures, including the requirements for a Traffic Management Plan (TMP), are provided in section 8.2.



Albury to Illabo

| ${ }^{50}{ }^{50}$ |  |
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|  | Scale: 1: |

Figure 5.4 Construction routes, diversions and site accesses (Billy Hughes bridge)

|  |  | INLAND RAIL <br> ART̄C <br> The Australian Government is delivering Inland Rail through the Australian Rail Track Corporation (ARTC), in partnership with the private sector. |
| :---: | :---: | :---: |



Vehicle and pedestrian diversions proposed within the Albury precinct during construction include:

- Albury Station pedestrian bridge - pedestrian diversion during construction along Harold Mair Bridge to the north and along Young street.

No vehicle diversions are proposed in the Albury precinct.

### 5.1.1.3 VEHICLE TYPE AND QUANTITY

Table 5.2 shows the peak construction, peak hour vehicle movements at each enhancement site as identified from construction scenario data shown in Chapter 8: Construction of the proposal of the EIS. To provide a worst-case assessment, the highest traffic generating work element for these enhancement sites, typically during a possession period has been adopted for assessment.
Table 5.2 Peak hour construction movements - Albury precinct enhancement sites

| ENHANCEMENT SITES | VEHICLE TYPE | PEAK HOUR MOVEMENTS | CONSTRUCTION VEHICLE PARKING AND LAYDOWN |
| :---: | :---: | :---: | :---: |
| Murray River bridge | Light vehicles | 27 in (am) / out (pm) | Internal to Proposal site |
|  | Heavy vehicles | 2 in and out |  |
| Albury Station pedestrian bridge | Light vehicles | $13^{1}$ in (am) / out (pm) | Internal to Proposal site |
|  | Heavy vehicles | 8 in and out |  |
| Albury Yard clearances | Light vehicles | $27^{2}$ in (am) / out (pm) | Internal to Proposal site |
|  | Heavy vehicles | 8 in and out |  |
| Riverina Highway bridge | Light vehicles | $40^{2}$ in (am) / out (pm) | Internal to Proposal site |
|  | Heavy vehicles | 10 in and out |  |
| Billy Hughes bridge | Light vehicles | $47^{2}$ in (am) / out (pm) | Internal to Proposal site |
|  | Heavy vehicles | 10 in and out |  |
| Table Top Yard clearances | Light vehicles | 7 in (am) / out (pm) | Internal to Proposal site |
|  | Heavy vehicles | 2 in and out |  |

(1) Three-day possession peak (typically only 7 vehicle movements in a peak period)
(2) Three-day possession peak (typically only 13 vehicle movements in a peak period) Road Network Operation

### 5.1.2 ROAD NETWORK OPERATION

### 5.1.2.1 MURRAY RIVER BRIDGE ENHANCEMENT SITE

## ROAD PERFORMANCE

The link LOS assessment for the Murray River bridge Enhancement Site component of the proposal is shown in Table 5.3. This assessment shows that with construction traffic all road links are expected to operate at LOS B or better, which is considered stable flow conditions as per the Guide to Traffic Generating Developments (RTA 2002). Furthermore, the assessment shows no change in LOS as a result of the construction generated traffic and subsequently no significant impacts to road operation and performance are expected.

Table 5.3 Murray River bridge enhancement site, construction route Road performance

| ROAD NAME | ROAD TYPE | 2024 PEAK HOUR |  | 2024 WITH CONSTRUCTION PEAK HOUR |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: |
|  |  | Volume - one <br> way | LOS | Construction <br> volume - one <br> way | Combined <br> volume - one <br> way | LOS |
| East Street $^{1}$ | Urban | 1,231 | B | 29 | 1,260 | B |
| Atkins Street $^{1}$ | Urban | 310 | B | 29 | 339 | B |
| Hume Highway $^{2}$ | Highway | 620 | B | 31 | 651 | B |
| Macauley Street $^{3}$ | Urban | 31 | A | 29 | 60 | A |
| Panmure Street $^{3}$ | Urban | 31 | A | 29 | 60 | A |
| Abercorn Street $^{3}$ | Urban | 31 | A | 29 | 60 | A |
| Kiewa Street $^{4}$ | Urban | 93 | A | 29 | 122 | A |
| Townsend Street $^{3}$ | Urban | 31 | A | 29 | 60 | A |
| Olive Street $^{4}$ | Urban | 93 | A | 29 | 122 | A |

(1) Traffic survey volumes
(2) Hume Highway - 120m East of Olive Street, South Albury 2640
(3) No data available, volumes estimated as $10 \%$ of Atkins Street 10 hour
(4) No data available, volumes estimated as $30 \%$ of Atkins Street 10 hour

Note, construction peak hour volumes are higher on Hume Highway than on the other roads under assessment as the road performance assessment for highways requires assessment of PCUs which effectively doubles the count of heavy vehicles required for construction.

## INTERSECTION PERFORMANCE

An assessment of the performance of the highest trafficked (on a per lane basis) construction route intersection in the Albury precinct during peak construction activities was undertaken and presented in section 5.1.2.2. The intersection assessment assessed peak hour construction traffic in conjunction with peak hour background traffic as a worst-case scenario for construction movements, as expected construction start and finish times end outside of typical peak periods.

This assessment showed that the expected performance of the highest trafficked intersection with construction traffic in the precinct was LOS C which is considered an acceptable LOS as per the Guide to Traffic Generating Developments (RTA 2002). Further, the assessment shows no change in LOS as a result of the construction generated traffic and subsequently no significant impacts to intersection operation and performance are expected. Furthermore, $95^{\text {th }}$ queuing does not extend into any additional adjacent intersections as a result of the construction vehicles. As such, it is not considered that construction vehicles would impact the performance of any other lesser trafficked construction route intersection within the precinct. Therefore, no additional construction route intersection analysis has been undertaken for the Murray River bridge enhancement site.

## TEMPORARY CLOSURES AND DIVERSIONS

No road closures or diversions are proposed for the Murray River bridge enhancement site.

## PARKING

Parking for construction workers and laydown areas for unloading of heavy vehicles at the Murray River bridge enhancement site would be provided within the proposal site and so would have minimal impact to existing on-street parking or public parking facilities. Any minor impacts to parking due to traffic control or site accesses on the local road network would be managed in line with the Traffic Management Plan (TMP).

No disabled parking spaces would be impacted by the proposal.

### 5.1.2.2 ALBURY STATION AND SURROUNDS ENHANCEMENT SITES

The enhancement sites in the vicinity of Albury Station share the same road network and have been combined in the following section, consisting of:

- Albury Station pedestrian bridge enhancement site
- Albury Yard clearances enhancement site
- Riverina Highway bridge enhancement site.


## ROAD PERFORMANCE

The link LOS assessment for the Albury Station and surrounds enhancement sites component of the proposal is shown in Table 5.4. This assessment shows that with construction traffic all road links are expected to operate at LOS C or better, which is considered stable flow conditions as per the Guide to Traffic Generating Developments (RTA 2002). Furthermore, the assessment shows no change in LOS as a result of the construction generated traffic and subsequently no significant impacts to road operation and performance are expected.
Table 5.4 Albury Station and surrounds enhancement sites, construction route road performance

| ROAD NAME | ROAD TYPE | 2024 PEAK HOUR |  | 2024 WITH CONSTRUCTION PEAK HOUR |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: |
|  |  | Volume - one <br> way | LOS | Construction <br> volume - one <br> way | Combined <br> volume - one <br> way | LOS |
| ${\text { Young Street }{ }^{1}}^{2}$ | Urban | 658 | A | 50 | 708 | A |
| Smollet Street <br> Railway Place) $^{1}$ | Urban | 41 | A | 50 | 91 | A |
| Borella Road $^{1}$ | Highway | 1,202 | C | 60 | 1,262 | C |
| Hume Highway <br> Northbound Off <br> Ramps | Highway | 620 | B | 60 | 680 | B |
| Schubach Street | Urban | 310 | B | 50 | 360 | B |

## (1) Traffic survey volumes

Note, construction peak hour volumes are higher on Hume Highway and Borella Road than on the other roads under assessment as the road performance assessment for highways requires assessment of PCUs which effectively doubles the count of heavy vehicles required for construction.

## INTERSECTION PERFORMANCE

The intersection of Borella Road and Hume Highway Northbound Off Ramp, used as part of the construction route to the Albury Yard clearances enhancement site, has the highest traffic volumes of available data within the Albury precinct on a per lane basis. Therefore, the Borella Road/Hume Highway Northbound Off Ramp intersection has been assessed in SIDRA to determine the highest level of construction vehicle impact at an intersection, within the Albury precinct. The intersection assessment assessed peak hour construction traffic in conjunction with peak hour background traffic as a worst-case scenario for construction movements as expected construction start and finish times end outside of typical peak periods.

Figure 5.6 shows the layout of the Borella Road/Hume Highway Northbound Off Ramp intersection as modelled in SIDRA and Figure 5.7 shows the signal phasing arrangement assumed for the analysis.

Hourly turning volumes for each approach at the Borella Road/Hume Highway Northbound Off Ramp intersection have been taken from a traffic survey at the intersection in 2021 and forecast 2024 volumes have been derived using a 3 per cent per year compounding growth rate. The traffic survey determined that the PM peak hour was the highest trafficked peak period at this intersection, as such the PM peak hour is the subject of this intersection assessment.


Figure 5.6 Borella Road/Hume Highway Northbound Off Ramp SIDRA intersection layout


Figure 5.7 Borella Road/Hume Highway Northbound Off Ramp SIDRA modelled signal phasing
Table 5.5 shows the SIDRA results for the Borella Road / Hume Highway Northbound Off Ramp intersection during a 2024 peak hour with and without construction vehicles. The results show the performance of the intersection is not significantly impacted by construction vehicles: LOS continues to operate at an acceptable level (LOS C), DOS only increases from $0.708-0.779$, intersection delay only increases by three seconds, and $95^{\text {th }}$ percentile queue lengths only increases by 27 m (approx. five vehicles). $95^{\text {th }}$ queuing does not extend into any additional adjacent intersections as a result of the construction vehicles.

It is noted that the West approach transitions from LOS B to LOS C, however this is the result of an increase in average delay of four seconds. It is also noted that the southern approach currently operates at LOS D and remains at LOS D (with the same amount of delay) with the proposal. The overall intersection performance remains at LOS C with the proposal.

Table 5.5 Borella Road/Hume Highway Northbound Off Ramp, 2024 construction route intersection capacity PM Peak

\left.|  | 2024 PM PEAK HOUR |  |  |  | 2024 PM PEAK HOUR WITH |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CONSTRUCTION |  |  |  |  |  |  |  |$\right]$

The Borella Road/Hume Highway Northbound Off Ramp intersection is reflective of the 'worst case' expected construction vehicle impacts to intersection performance, being the highest trafficked intersection on a per lane basis. Based on the results of this assessment it is not expected that the performance of any other construction route intersection within the Albury precinct would be significantly impacted by construction vehicle movements.

## TEMPORARY CLOSURES AND DIVERSIONS

No road closures or vehicle diversions are proposed for the Albury Station and surrounds enhancement sites.

## PARKING

During the 5-month program for the Albury Station pedestrian bridge enhancement site the informal car park to the north of Albury bridge and part of the designated station car parking is expected to be closed due to the establishment of a site access and equipment set up in this location. Estimated impacts are shown in Table 5.6.

Table $5.6 \quad$ Impacts to car parking - Albury Station and surrounds precinct

| LOCATION | CARPARK CAPACITY | IMPACTED AREA | REMAINING AREA |
| :--- | :--- | :--- | :--- |
| Albury Station parking on <br> Smollett Street and Railway <br> Place | 128 designated spaces | 13 informal spaces | 14 designated spaces |
| 13 informal spaces | 114 designated spaces |  |  |
| 0 informal spaces |  |  |  |

During the closure period described in section 5.1.1, users of these car parks would need to seek alternative locations to park. It is noted that there is on-street parking on Young Street within approximately 200 m of the station, which is within the 200 - 500m acceptable walking distance to public transport noted in RTA 2002.

Except for the parking impacts described above, parking for construction workers and laydown areas for unloading of heavy vehicles at the Albury Station and surrounds enhancement sites will be provided within the enhancement site and so would have minimal impact to existing parking facilities. No impact to existing parking facilities is expected from construction worker parking. Any minor impacts to parking due to traffic control or site accesses on the local road network would be managed in line with the TMP.

No disabled parking spaces would be impacted by the proposal.

### 5.1.2.3 BILLY HUGHES BRIDGE ENHANCEMENT SITE

## ROAD PERFORMANCE

The link LOS assessment for the Billy Hughes bridge enhancement site component of the proposal is shown in Table 5.7. This assessment shows that with construction traffic all road links are expected to operate at LOS C or better, which is considered stable flow conditions and an acceptable LOS as per the Guide to Traffic Generating Developments (RTA 2002). Furthermore, the assessment shows no change in LOS as a result of the construction generated traffic and subsequently no significant impacts to road operation and performance are expected.

## Table 5.7 Billy Hughes bridge Clearances enhancement site - construction route road performance

| ROAD NAME | ROAD TYPE | 2024 PEAK HOUR |  | 2024 WITH CONSTRUCTION PEAK HOUR |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: |
|  |  | Volume - <br> one way | LOS | Construction volume - <br> one way | Combined volume <br> - one way | LOS |
| Wagga Road $^{1}$ | Rural | 385 | B | 57 | 442 | B |
| Hume Highway $^{2}$ | Highway | 906 | C | 67 | 973 | C |
| R W Henry <br> Drive $^{3}$ | Rural | 39 | A | 57 | 96 | A |

(1) No data available, volumes estimated as Wagga Road - 110m South of Waldner Court, Lavington
(2) No data available, volumes estimated as Hume Highway - 200m North of Ford Lane, Table Top
(3) No data available, volumes estimated as 10\% of Wagga Road - 110m South of Waldner Court, Lavington

Note, construction peak hour volumes are higher on Hume Highway than on the other roads under assessment as the road performance assessment for highways requires assessment of PCUs which effectively doubles the count of heavy vehicles required for construction.

## INTERSECTION PERFORMANCE

An assessment of the performance of the highest trafficked (on a per lane basis) construction route intersection in the Albury precinct during peak construction activities was undertaken and presented in section 5.1.2.2. The intersection assessment assessed peak hour construction traffic in conjunction with peak hour background traffic as a worst-case scenario for construction movements, as expected construction start and finish times end outside of typical peak periods.

This assessment showed that the expected performance of the highest trafficked intersection in the precinct was LOS C, which is considered stable flow conditions and an acceptable LOS as per the Guide to Traffic Generating Developments (RTA 2002). The assessment shows no change in LOS as a result of the construction generated traffic and subsequently no significant impacts to intersection operation and performance are expected. Furthermore, $95^{\text {th }}$ queuing does not extend into any additional adjacent intersections as a result of the construction vehicles. As such, it is not considered that construction vehicles would impact the performance of any other lesser trafficked construction route intersection within the precinct. Therefore, no additional construction route intersection analysis has been undertaken for the Billy Hughes bridge enhancement site.

## TEMPORARY CLOSURES AND DIVERSIONS

No road closures or diversions are proposed for the Billy Hughes bridge enhancement site.

## PARKING

Parking for construction workers and laydown areas for unloading of heavy vehicles at the Billy Hughes bridge enhancement site would be provided within the construction site area and so would have minimal impact to existing parking facilities. Any minor impacts to parking due to traffic control or site accesses on the local road network would be managed in line with the TMP.

No disabled parking spaces would be impacted by the proposal.

### 5.1.2.4 TABLE TOP YARD CLEARANCE ENHANCEMENT SITE

## ROAD PERFORMANCE

The link LOS assessment for the Table Top Yard clearances enhancement site component of the proposal is shown in Table 5.8. This assessment shows that with construction traffic all road links are expected to operate at LOS C or better, which is considered stable flow conditions and an acceptable LOS as per the Guide to Traffic Generating Developments (RTA 2002). Furthermore, the assessment shows no change in LOS as a result of the construction generated traffic and subsequently no significant impacts to road operation and performance are expected.

Table $5.8 \quad$ Table Top, construction route road performance

| ROAD NAME | ROAD TYPE | 2024 PEAK HOUR |  | 2024 WITH CONSTRUCTION PEAK HOUR |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: |
|  |  | Volume - <br> one way | LOS | Construction volume - <br> one way | Combined volume <br> - one way | LOS |
| Perryman Lane $^{1}$ | Rural | 32 | B | 9 | 41 | B |
| Tynan Road $^{2}$ | Rural | 41 | B | 9 | 50 | B |
| Hume Highway $^{3}$ | Highway | 906 | C | 11 | 917 | C |

(1) No data available, volumes estimated as $5 \%$ of Hume Highway
(2) Tynan Road - between Gerogery Road and Perryman Lane, Table Top
(3) Hume Highway - 200m North of Ford Lane, Table Top

Note, construction peak hour volumes are higher on Hume Highway than on the other roads under assessment as the road performance assessment for highways requires assessment of PCUs which effectively doubles the count of heavy vehicles required for construction.

## INTERSECTION PERFORMANCE

An assessment of the performance of the highest trafficked (on a per lane basis) construction route intersection in the Albury precinct during peak construction activities was undertaken and presented in section 5.1.2.2. The intersection assessment assessed peak hour construction traffic in conjunction with peak hour background traffic as a worst-case scenario for construction movements as expected construction start and finish times end outside of typical peak periods.

This assessment showed that the expected performance of the highest trafficked intersection in the precinct was LOS C or better, which is considered stable flow conditions as per the Guide to Traffic Generating Developments (RTA 2002). The assessment shows no change in LOS as a result of the construction generated traffic and subsequently no significant impacts to intersection operation and performance are expected. Furthermore, $95^{\text {th }}$ queuing does not extend into any additional adjacent intersections as a result of the construction vehicles. As such, it is not considered that construction vehicles would impact the performance of any other lesser trafficked construction route intersection within the precinct. Therefore, no additional construction route intersection analysis has been undertaken for the Table Top Yard clearances enhancement site.

## TEMPORARY CLOSURES AND DIVERSIONS

No road closures or diversions are proposed for the Table Top Yard clearance enhancement site.

## PARKING

Parking for construction workers and laydown areas for unloading of heavy vehicles at the Table Top Yard clearances enhancement site would generally be provided within the proposal site and so would have minimal impact to existing parking facilities. Some parking may occur on Perryman Road, however any minor impacts to parking due to traffic control or site accesses on the local road network would be managed in line with the TMP.

No disabled parking spaces would be impacted by the proposal.

### 5.1.3 CONSTRUCTION SITE ACCESS

A turn warrant assessment for each enhancement site access in the Albury precinct have been undertaken based on The Guide to Traffic Management - Part 6 Intersection, Interchanges and Crossings (Austroads 2020). This assessment has analysed a worst-case scenario, assuming all peak generated construction traffic is distributed to each access during the road network peak period. The results of this assessment are shown in Table 5.9.

Table 5.9 Albury precinct enhancement site access turn warrant assessment

| ENHANCEMENT SITE | ACCESS POINTS NUMBER / ROAD | $\begin{aligned} & \text { ROAD } \\ & \text { TYPE } \end{aligned}$ | ASSESSMENT OUTCOME <br> (TURN <br> TREATMENT) | CONSIDERATIONS |
| :---: | :---: | :---: | :---: | :---: |
| Murray River bridge | 36 / <br> Townsend St | Two-way | N/A ${ }^{1}$ | Through movement into site. <br> No opposing movements on public road. <br> Low speed environment ( $\leq 60 \mathrm{~km} / \mathrm{h}$ ). <br> Minimal impact to existing traffic movements expected. |
|  | 35 / Olive Street | Two-way | $\mathrm{N} / \mathrm{A}^{1}$ | Through movement into site. <br> No opposing movements on public road. Low speed environment ( $\leq 60 \mathrm{~km} / \mathrm{h}$ ). <br> Minimal impact to existing traffic movements expected |
|  | 37 / Hume <br> Highway on ramp | One way | N/A ${ }^{1}$ | Left turn into and out of site. <br> Opposing movements on public road. <br> High speed environment ( $\geq 80 \mathrm{~km} / \mathrm{h}$ ). <br> High traffic volume highway. |
| Albury Station and surrounds | 38 / Railway <br> Parade | One way | N/A ${ }^{1}$ | Through movement into site. <br> No opposing movements on public road. <br> Low speed environment ( $\leq 60 \mathrm{~km} / \mathrm{h}$ ). <br> Minimal impact to existing traffic movements expected. |
|  | 72 / <br> Kenilworth Street | One way | N/A ${ }^{1}$ | Through movement into site. <br> No opposing movements on public road. <br> Low speed environment ( $\leq 60 \mathrm{~km} / \mathrm{h}$ ). <br> Minimal impact to existing traffic movements expected. |
|  | 39 / Borella <br> Road off ramp | One way | N/A ${ }^{1}$ | Left turn into and out of site. <br> Opposing movements on public road. <br> High speed environment ( $\geq 80 \mathrm{~km} / \mathrm{h}$ ). <br> High traffic volume highway. |


| ENHANCEMENT SITE | ACCESS POINTS NUMBER / ROAD | $\begin{aligned} & \text { ROAD } \\ & \text { TYPE } \end{aligned}$ | ASSESSMENT <br> OUTCOME <br> (TURN <br> TREATMENT) | CONSIDERATIONS |
| :---: | :---: | :---: | :---: | :---: |
| Billy Hughes bridge | 43 / Wagga <br> Road | Two-way | Channelised <br> Right-Turn / <br> Auxiliary Left- <br> Turn | Left and right turn into and out of site. Opposing movements on public road. High speed environment $(\geq 80 \mathrm{~km} / \mathrm{h})$. Current configuration does not meet turn warrant guidance, Road Safety Audit would investigate the need for traffic management of this access. |
|  | 42 / Wagga <br> Road | Two-way | Channelised Right-Turn / Auxiliary LeftTurn | Left and right turn into and out of site. Opposing movements on public road High speed environment ( $\geq 80 \mathrm{~km} / \mathrm{h}$ ). <br> Potential for impacts from construction vehicles movements or implementation of traffic management. <br> Current configuration does not meet turn warrant guidance, Road Safety Audit would investigate the need for traffic management of this access. |
|  | 74 / R W <br> Henry Drive | Two-way | Channelised Right-Turn / BAL | Left and right turn into and out of site. <br> Opposing movements on public road <br> High speed environment ( $\geq 80 \mathrm{~km} / \mathrm{h}$ ). <br> Potential for impacts from construction vehicles movements or implementation of traffic management. <br> Current configuration does not meet turn warrant guidance, Road Safety Audit would investigate the need for traffic management of this access. |
| Table Top Yard clearances | 44 / Perryman Lane | Two-way | Basic Right-Turn <br> / Basic Left-Turn | Left and right turn into and out of site. Opposing movements on public road. High speed environment $(\geq 80 \mathrm{~km} / \mathrm{h})$. <br> Potential for impacts from construction vehicles movements or implementation of traffic management. <br> Current configuration does not meet turn warrant guidance, Road Safety Audit would investigate the need for traffic management of this access. |

(1) Turn warrant assessment not required due to access intersection configuration (no opposing flows on public road or left in left out only)

Basic Left-Turn/ Basic Right-Turn and Auxiliary Left-Turn/ Channelised Right-Turn treatments are required by the intersection turn warrant assessment for some site accesses in this precinct. However, this may not be required given the temporary nature of accesses during the construction phase and the conservative nature of the assessment (peak construction vehicles assessed during the background peak hour, when peak construction vehicles are expected outside the background peak hour).

Where the turn warrant assessment methodology is unsuitable for the assessment of the enhancement site access the access arrangements as per the current road network would not have a significant impact as they are either a through movement from the end of a street, or they are impacting limited traffic movements.

The proposed accesses located on the Hume Highway entry ramp and Hume Highway exit ramps are on one-way roads and not suitable for turn warrant assessment. These proposed enhancement site accesses would potentially have a greater impact on the performance and safe operation of critical highway infrastructure due to their location on or adjacent to:

- high speed environment ( $110 \mathrm{~km} / \mathrm{h}$ posted speed limit)
- high traffic environment
- limited shoulder width to provide space for turning construction vehicles to slow down without impacting other vehicles

More detailed assessment of the accesses will be undertaken as part of the Road Safety Audits and appropriate Construction Traffic Transport and Access Management Plans will be developed by the contractor prior to commencement of construction activities on site to moderate any potential safety issues. Design of any access treatments or modifications to roads would be undertaken in accordance with appropriate design standards and with approvals from the relevant local or state road authorities. Works Authorisation Deeds or other suitable consent or agreement with TfNSW will be made prior to undertaking any relevant works on a State Controlled Road.

### 5.1.4 ROAD SAFETY

During construction there would be changes to road conditions within the Albury precinct consisting of increased traffic volumes due to construction vehicles and new access points to the enhancement sites from the public road network. This assessment has primarily considered the operation and capacity of the road network rather than the appropriateness of use of certain roads by construction vehicles

It is noted that the construction activities at enhancement sites within the Albury precinct are expected to generate a maximum peak hour flow of 57 vehicles (during a three day possession peak period), and an appropriate LOS is maintained on all of the enhancement site access routes as discussed in section 5.1.1. Access intersections to the enhancement sites within the Albury precinct would be designed or have traffic control measures implemented to provide suitable safe access to public roads in accordance with relevant standards and guidelines.

To manage any construction impacts resulting in potential road safety issues, Road Safety Audits and Construction Traffic Transport and Access Management Plans would be required to be undertaken by the contractor prior to commencement of construction activities and the safety of all road users should be taken into account.

### 5.1.5 HEAVY VEHICLE ROUTES

As an appropriate LOS is maintained on roads used for construction activities at enhancement sites within the Albury precinct, it is not expected that construction heavy vehicle and workforce movements generated by the proposal, as shown in section 5.1.1.3, would impact the operations of existing heavy vehicles movements, including agricultural transport, on the routes discussed in section 4.3.3.

There is potential for construction heavy vehicles to impact road pavement conditions along haul routes. To determine the extent of the impact a road dilapidation report would be prepared for all haul routes within the precinct.

### 5.1.6 TRAVELLING STOCK RESERVES

As discussed in section 4.3.4, there are no Livestock Highways or TSRs in the vicinity of enhancement sites within the Albury precinct. It is expected that prior to the commencement of works that Local Land Services would be notified of temporary closures of rail level crossings in the Albury precinct so that stock handlers, including walking permit holders, can be notified of the impacts to stock movements.

### 5.1.7 PUBLIC TRANSPORT ROUTES

### 5.1.7.1 ROAD

Although there would be increased traffic resulting from construction activities at enhancement sites within the Albury precinct, it is expected to have a minimal impact on the operation of public or school bus services or bus stops due to the low traffic volumes generated by the construction activities (stable flow conditions are maintained on all of the enhancement site access routes). It is noted that the heaviest period of construction workforce movements at the start and end of construction hours ( 6 am to 6 pm ) outside peak bus service periods (e.g. school times). There may be minor delays to buses passing near enhancement sites from reduced speed limits and traffic control. These impacts would be managed in accordance with the traffic management plan to ameliorate impacts to the safe and efficient travel of bus services through the affected areas. Albury station includes a bus interchange, access would be maintained through traffic management, and no impact to these services are expected as a result of the construction activities.

### 5.1.7.2 RAIL

Construction activities requiring possessions would occur during either:

- existing scheduled weekend rail corridor possession periods (typically 72 hours) when trains along the rail corridor are stopped for maintenance as part of operation of the existing rail line; or
- track work authorisations periods, which enable works that impact rail operations to occur outside scheduled rail possessions, but within available time windows in which train services are not scheduled.

Work during these periods would be undertaken in consultation with passenger rail operators. However, it is not expected that proposal construction works would impact upon the rail services and train station platforms will not be impacted by the enhancement sites. Impacts to pedestrian access from construction works on the Albury Station pedestrian bridge are discussed in the following section.

### 5.1.8 ACTIVE TRANSPORT ROUTES

Given the surrounding land uses in the vicinity of the Murray River bridge, Billy Hughes bridge and Table Top Yard clearances enhancement sites the demand for cycling and pedestrian travel in the area is likely to be low. Although there would be increased traffic from construction vehicles, the increase is minor with all road links with stable flow conditions and minimal change in LOS (LOS A to B) expected as a result of construction generated traffic with no impact to existing active transport movements expected. The largest hourly construction movements would occur outside peak traffic periods and would have minimal impact to pedestrians and cyclists.

As part of the Albury Station and surrounds Enhancement sites construction activities, the Albury Station pedestrian bridge (which does not currently cater for cyclists) replacement would require closure of the bridge. During the closure period of approximately six months, pedestrians would be diverted to the two nearest crossings; the Harold Mair Bridge located 160m ( 2 minutes' walk) north, and the Amatex Street bridge located 460 m ( 6 minutes' walk) south.

Footpaths provide full pedestrian connectivity between Albury Station and Kenilworth Street (the location of the western landing of the Albury Station pedestrian bridge) via the Harold Mair Bridge and the Amatex Street Bridge. Due to the high level of connectivity of active transport infrastructure in the Albury Station area and the proximity of alternative facilities, it is expected that the impacts to pedestrians and cyclists due to diversions would be relatively minor and can be effectively managed and minimised.

There may be minor disruptions to cyclists using roads near the enhancement sites as a result of traffic control. These impacts although expected to be minimal would be managed in accordance with the TMP.

### 5.1.9 PROPERTY ACCESS IMPACTS

Although there may be some minor, temporary disruptions, property access is expected to be maintained throughout the duration of the construction activities in the area. Any changes to arrangements would need to be undertaken in consultation with the relevant stakeholders and in line with the TMP.

### 5.1.10 RAIL FREIGHT

Section 5.1.7.2 notes when construction activities requiring possessions will occur.
Work during these periods would be undertaken in consultation with freight operators. However, it is not expected that proposal construction works would impact upon the rail freight network. Note, there are no other impacts to freight operations.

### 5.1.11 WATER BASED TRANSPORT

As stated in section 4.3.7, the Murray River in the vicinity of the Albury precinct enhancement sites does not support public transport, trade, or shipping freight routes, and water-based transport is generally limited to recreational activities. However, the Murray River provides through access for water-based emergency services. Any changes to the access arrangement of the waterway under the Murray River bridge during construction activities (approximately 12 months) would:

- maintain the river as navigable by the provision of a channel under the bridge to maintain access for watercraft
- be undertaken in consultation with TfNSW Maritime and the relevant stakeholders (such as commercial operators, local businesses, and water-based emergency services) in line with the TMP
- observe appropriate maritime permit requirements and safety notice periods.


### 5.1.12 EMERGENCY VEHICLE ACCESS

Construction of the proposal would result in temporary impacts to traffic and an increase in vehicle movements on the road network. As shown in the link and intersection performance assessments, there is no significant impact to the performance of the road network due to the construction generated traffic within the Albury precinct, and there is not expected to be a significant impact to emergency vehicles movements. The traffic and access management plan would be developed in consultation with TfNSW, Albury City Council, and State emergency services and would consider and effectively manage any impacts to emergency vehicles seeking to use roads in the vicinity of the enhancement sites.

### 5.1.13 SEASONAL VARIATION

Temporary local events such as festivals, shows, and markets may result in minor localised traffic variations, particularly in urban environments such as Albury.

Localised seasonal traffic variation may also be experienced at enhancement sites that share land with agricultural infrastructure (grain silos, livestock loading facilities etc.) as the infrastructure will likely generate additional heavy or farm vehicle movements during harvest seasons. A review of aerial imagery of enhancement sites in the Albury precinct did not identify any agriculture infrastructure co-located with enhancement sites. The seasonal variation in traffic movements identified in section 4.2.2 is expected to be representative of enhancement sites across the Albury precinct.

More detailed assessment of the enhancement site accesses, which would consider seasonal variation due to social events and agricultural movements, will be undertaken by the contractor prior to commencement of construction activities on site. These would include Road Safety Audits and appropriate Construction Traffic Transport and Access Management Plans to moderate any potential safety issues.

### 5.2 GREATER HUME, LOCKHART

### 5.2.1 CONSTRUCTION PROFILE

This section outlines the construction profile for the proposal within the Greater Hume, Lockhart precinct. This includes all vehicle routes, as shown in section 5.2.1.2, and all volumes of heavy and light vehicles required for construction of the proposal, as shown in section 5.2.1.3, which includes the vehicles required for the import and export of fill material. It also outlines other construction requirements, such as temporary road closures and diversions, and parking requirements for each enhancement site.

### 5.2.1.1 CONSTRUCTION PROGRAM

Key construction stages and work durations at each enhancement site within the Greater Hume/Lockhart precinct are summarised in Table 5.10 and Figure 5.8.

Table 5.10 Summary of construction stages - Greater Hume - Lockhart enhancement sites

| ENHANCEMENT SITES | CONSTRUCTION STAGES UNDERTAKEN | START | FINISH | DURATION OF WORKS (MONTHS) | RAIL POSSESSION REQUIRED |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Culcairn Yard clearance and Culcairn pedestrian bridge | - Site establishment <br> - Gantry modification <br> - Pedestrian bridge removal/relocation with crane <br> - Demobilisation and landscaping | $\begin{gathered} 15 \text { January } \\ 2024 \end{gathered}$ | 1 April 2024 | 3 | Yes |
| Henty Yard clearances | - Site establishment <br> - Track realignment ( $<300 \mathrm{~mm}$ ) <br> - Gantry modifications <br> - Level crossing modification <br> - Demobilisation and landscaping | $\begin{gathered} 15 \text { January } \\ 2024 \end{gathered}$ | 8 April 2024 | 3 | No |
| Yerong Creek Clearances | - Site establishment <br> - Track realignment ( $<300 \mathrm{~mm}$ ) <br> - Track realignment ( $>300 \mathrm{~mm}$ and/or track formation replacement) <br> - Level crossing modification <br> - Demobilisation and landscaping | $\begin{gathered} 15 \text { January } \\ 2024 \end{gathered}$ | 5 April 2024 | 3 | Yes |
| The Rock Yard clearances | - Site establishment <br> - Track lowering <br> - Gantry modifications <br> - Demobilisation and landscaping | 1 February 2024 | $\begin{gathered} 25 \text { February } \\ 2024 \end{gathered}$ | $<1$ | No |



Figure 5.8 Greater Hume - Lockhart precinct construction programme

### 5.2.1.2 CONSTRUCTION AND DIVERSION ROUTES

Proposed construction routes and accesses to enhancement sites in the Greater Hume - Lockhart precinct are shown below in Figure 5.9 to Figure 5.12.

Construction routes have been selected to minimise the use of local roads where possible. However, use of local roads is generally required to facilitate access to enhancement sites. As shown in section 5.2.1.3, construction vehicle volumes using construction routes and accesses on local roads are generally low.

Diversion routes have been selected on roads of the same order where possible. In the instances where diversion routes have been required on roads of a lower order, the requirement for mitigation has been considered.

Mitigations for the use of all road types, including local roads are provided in section 8.2. In addition, mitigation measures have been identified for other assessments, including noise and vibration, visual and social, to address potential impacts from the use of construction and diversion routes.

Where diversions are required for active travel routes, the selected diversion route has considered where pedestrian infrastructure is present. Where cyclists utilise diversion routes, and an existing cycle or shared path is not present, cyclists would be required to cycle on-road. To facilitate access to the rail corridor and surrounds for construction vehicles, including surrounding residences, diversion of pedestrians and cyclists within the proposal site would also be required. Detailed consideration of the management of pedestrian and cyclist safety within the proposal site will be completed prior to and during construction. Mitigation measures, including the requirements for a Traffic Management Plan (TMP), are provided in section 8.2.






Vehicle and pedestrian diversions proposed during construction are as follows:

- Henty Yard clearances
- Sladen Street level crossing closure (five days) - vehicle traffic to be diverted via Rosler Parade/Yankee Crossing Road level crossing. Pedestrian access would be maintained.


### 5.2.1.3 VEHICLE TYPE AND QUANTITY

Table 5.11 shows the peak hour two-way movements at each site as identified from construction scenario data shown in Chapter 8: Construction of the proposal of the EIS. To provide a worst-case assessment, the highest traffic generating work element for these enhancement sites, typically during a possession period has been adopted.
Table 5.11 Peak hour construction movements - Greater Hume - Lockhart precinct

| ENHANCEMENT SITES | VEHICLE TYPE | PEAK HOUR <br> MOVEMENTS | CONSTRUCTION <br> VEHICLE PARKING AND <br> LAYDOWN |
| :--- | :--- | :--- | :--- |
| Culcairn Station (Yard Clearance and <br> pedestrian bridge) | Light vehicles | $40^{1}$ in $(\mathrm{am}) /$ out $(\mathrm{pm})$ | Internal to Proposal site |
| Henty Yard clearances | Heavy vehicles | 8 in and out |  |
| Yerong Creek Clearances | Light vehicles | $40^{1}$ in $(\mathrm{am}) /$ out $(\mathrm{pm})$ | Internal to Proposal site |
|  | Heavy vehicles | 8 in and out |  |
|  | Light vehicles | $40^{1}$ in $(\mathrm{am}) /$ out $(\mathrm{pm})$ | Internal to Proposal site |
|  | Heavy vehicles | 8 in and out |  |

(1) Three-day possession peak (typically only 20 vehicle movements in a peak period)

### 5.2.2 ROAD NETWORK OPERATION

### 5.2.2.1 CULCAIRN ENHANCEMENT SITES

ROAD PERFORMANCE
The link LOS assessment for the Culcairn enhancement sites component of the proposal is shown in Table 5.12. This assessment shows that with construction traffic all road links are expected to operate at LOS C or better, which is considered stable flow conditions as per the Guide to Traffic Generating Developments (RTA 2002). Furthermore, the assessment shows no change in LOS as a result of the construction generated traffic and subsequently no significant impacts to road operation and performance are expected.

Table 5.12
Culcairn enhancement site, construction route road performance

| ROAD NAME | ROAD <br> TYPE | 2024 PEAK HOUR | 2024 WITH CONSTRUCTION |  |
| :--- | :--- | :--- | :---: | :---: | :---: | :---: | :---: |
| PEAK HOUR |  |  |  |  |$|$

(1) Olympic Highway - 290m North of Calool Lane, Culcairn
(2) Railway Parade (Olympic Highway) - 80m South of Balfour Street, Culcairn
(3) Estimated conservatively as $25 \%$ of Railway Parade (south of Balfour Street) traffic volume as Railway Parade (north of Balfour Street) does not form part of the Olympic Highway, as Railway Parade (south of Balfour Street) does.
Note, construction peak hour volumes are higher on Melville Street (Olympic Highway) than on the other roads under assessment as the road performance assessment for highways requires assessment of PCUs which effectively doubles the count of heavy vehicles (8) required for construction.

## INTERSECTION PERFORMANCE

Table 5.12 shows that Balfour Street and Railway Parade have the highest traffic volumes within the Greater Hume Lockhart precinct on a per lane basis. Therefore, the Balfour Street/Railway Parade intersection has been assessed in SIDRA, to determine the highest level of construction vehicle impact at an intersection within the Greater Hume Lockhart precinct. The intersection assessment assessed peak hour construction traffic in conjunction with peak hour background traffic as a worst-case scenario for construction movements, as expected construction start and finish times end outside of typical peak periods.

Hourly turning volumes for each approach at the Balfour Street/ Railway Parade intersection have been calculated based on:

- AADT volumes factored to peak hour (10\%)
- approach proportions of total intersection volume to determine turn movement volumes.

Figure 5.13 shows the layout of the Balfour Street / Railway Parade intersection as modelled in SIDRA.


Figure 5.13 Balfour Street/Railway Parade SIDRA intersection layout
Table 5.13 shows the SIDRA results for the Balfour Street/Railway Parade intersection during a 2024 peak hour with and without construction vehicles. The results show the performance of the intersection is not significantly impacted by construction vehicles: LOS continues operates at an acceptable level (LOS A), DOS only increases from 0.446-0.487, intersection delay does not increase, and $95^{\text {th }}$ percentile queue lengths only increases by 3 m (approx. one vehicle). $95^{\text {th }}$ queuing does not extend into any additional adjacent intersections as a result of the construction vehicles.

Table 5.13 Balfour Street/Railway Parade, 2024 peak hour without construction vehicles - 10\% of AADT

|  | 2024 PEAK HOUR (10\% AADT) |  |  |  | 2024 PEAK HOUR (10\% AADT) WITH CONSTRUCTION |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | DOS | Delay (s) | LOS | $95^{\text {th }} \%$ ile queue (m) | DOS | Delay (s) | LOS | $95^{\text {th }} \%$ ile queue (m) |
| South: Railway Parade (Olympic Highway) | 0.362 | 8 | LOS A | 21 | 0.418 | 8 | LOS A | 25 |
| East: Balfour Street | 0.442 | 6 | LOS A | 27 | 0.481 | 6 | LOS A | 31 |
| North: Railway Parade | 0.114 | 9 | LOS A | 6 | 0.128 | 8 | LOS A | 6 |
| West: Balfour Street | 0.446 | 7 | LOS A | 28 | 0.487 | 8 | LOS A | 31 |
| Intersection | 0.446 | 7 | LOS A | 28 | 0.487 | 7 | LOS A | 31 |

The Balfour Street/Railway Parade intersection is reflective of the 'worst case' expected construction vehicle impacts to intersection performance, being the highest trafficked intersection on a per lane basis. Based on the results of this assessment it is not expected that the performance of any other construction route intersection within the Greater Hume Lockhart precinct would be significantly impacted by construction vehicle movements.

## TEMPORARY CLOSURES AND DIVERSIONS

No road closures or diversions are proposed for the Culcairn enhancement site.

## PARKING

Parking for construction workers and laydown areas for unloading of heavy vehicles at the Culcairn pedestrian bridge and Yard clearances enhancement sites would be provided within the construction site area and so would have minimal impact to existing parking facilities. Any minor impacts to parking due to traffic control or site accesses on the local road network would be managed in line with the TMP.

No disabled parking spaces would be impacted by the proposal.

### 5.2.2.2 HENTY YARD CLEARANCES ENHANCEMENT SITE

## ROAD PERFORMANCE

The link LOS assessment for the Henty Yard clearances enhancement site component of the proposal is shown in Table 5.14. This assessment shows that with construction traffic all road links are expected to operate at LOS A or better, which is considered stable flow conditions as per the Guide to Traffic Generating Developments (RTA 2002).
Furthermore, the assessment shows no change in LOS as a result of the construction generated traffic and subsequently no significant impacts to road operation and performance are expected.

Table 5.14 Henty, construction route road performance

| ROAD NAME | $\begin{array}{l}\text { ROAD } \\ \text { TYPE }\end{array}$ | $\begin{array}{c}\text { 2024 PEAK } \\ \text { HOUR }\end{array}$ |  | 2024 WITH CONSTRUCTION |  |
| :--- | :--- | :--- | :--- | :---: | :---: | :---: | :---: |
| PEAK HOUR |  |  |  |  |  |$]$

(1) No data available, volumes estimated as Olympic Highway - 290m North of Calool Lane, Culcairn
(2) No data available, volumes estimated as $50 \%$ of Sladen Street
(3) No data available, volumes estimated as $20 \%$ of Railway Parade

Note, construction peak hour volumes are higher on Railway Parade (Olympic Highway) than on the other roads under assessment as the road performance assessment for highways requires assessment of PCUs which effectively doubles the count of heavy vehicles required for construction.

## INTERSECTION PERFORMANCE

An assessment of the performance of the highest trafficked (on a per lane basis) construction route intersection in the Greater Hume - Lockhart precinct during peak construction activities was undertaken for the Culcairn enhancement sites in section 5.2.2.1. The intersection assessment assessed peak hour construction traffic in conjunction with peak hour background traffic as a worst-case scenario for construction movements as expected construction start and finish times end outside of typical peak periods.

This assessment showed that the expected performance of the highest trafficked intersection in the precinct was LOS A, which is considered an acceptable LOS as per the Guide to Traffic Generating Developments (RTA 2002). Further, the assessment shows no change in LOS as a result of the construction generated traffic and subsequently no significant impacts to intersection operation and performance are expected. Furthermore, $95^{\text {th }}$ queuing does not extend into any additional adjacent intersections as a result of the construction vehicles. As such, it is not considered that construction vehicles would impact the performance of any other lesser trafficked construction route intersection within the precinct. Therefore, no additional construction route intersection analysis has been undertaken for the Henty Yard clearances enhancement site.

## TEMPORARY CLOSURES AND DIVERSIONS

The Sladen Street rail level crossing would require a road closure as shown in Figure 5.14, for five days during the construction activities. Based on AADT data from 2014 extrapolated to 2024 (at a 3 per cent compounding per annum growth rate) this diversion is expected to impact 997 vehicles per day.

The closure requires vehicles to be diverted to the rail level crossing on Rosler Parade via the Olympic Highway on the western side of the rail line and via Allan Street on the eastern side of the railway line. Crossing the rail line with the diversion in place incurs up to a maximum 2.2 km travel distance than without the diversion. As this diversion is implemented for a relatively short period (five days) the additional travel distance and time are not considered a significant impact.

Road Safety Audits and Construction Traffic Transport and Access Management Plans would be undertaken by the contractor prior to commencement of diversionary routes. Particular attention should be paid the type and size of vehicle using the level crossing on Rosler Parade so that appropriate clearance to the rail line can be maintained when giving way to vehicles on the Olympic Highway.


## ROAD PERFORMANCE

Traffic volumes for Rosler Parade and Allen Street were not available at the time of analysis. Traffic volumes for Sladen Street have been used to assess the road performance of diverted traffic on Rosler Parade and Allen Street. This provides a conservative assessment of the potential impacts as Sladen Street is expected to have higher traffic volumes than Rosler Parade or Allen Street, as it provides connection through the main retail area of Henty. Table 5.15 shows that Rosler Parade and Allen Street (Sladen Street) would operate at LOS A in a 2024 peak hour and that diversion related vehicles (Sladen Street traffic volumes) using these roads during a 2024 peak hour would have no impact to the LOS.

Note, Allan Street is not part of construction vehicle routes in Henty, as such construction vehicles have not been included in the assessment of diversion route link capacities.

Table $5.15 \quad$ Henty, diversion route road performance

| ROAD NAME | ROAD <br> TYPE | 2024 PEAK HOUR VEHICLES <br> (ONE-WAY) |  |  | DIVERSION PEAK HOUR VEHICLES <br> (ONE-WAY) |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Volume | LOS | Construction <br> volume | Diversion <br> volume | Combined <br> volume | LOS |
| Rosler Parade/ <br> Yankee Crossing <br> Road | Urban | 10 | A | 48 | 51 | 109 | A |
| Allan Street | Urban | 36 | A | - | 51 | 87 | A |

## INTERSECTION PERFORMANCE

A 'worst case' assessment of construction route intersection performance was undertaken for the precinct in section 5.2.2.1. The analysis showed no impact to intersection performance as a result of the 39 construction vehicles. As such, it is not considered that an additional 51 diverted vehicles per hour would impact the performance of other intersections with lower traffic volumes, such as in Henty. Therefore, no additional intersection analysis has been undertaken to assess the impact of diverted vehicles to intersections during the Sladen Street closure.

## TRAVEL TIME

Figure 5.15 shows that the longest potential diversion would take a maximum of approximately five minutes of additional travel time in a vehicle. As the diversion is temporary (for a five day period), an additional four minutes travel time during the diversion is not considered a significant impact.

## PARKING

Parking for construction workers and laydown areas for unloading of heavy vehicles at the Henty Yard clearances enhancement site would be provided within the construction site area and so would have minimal impact to existing parking facilities. Any minor impacts to parking due to traffic control or site accesses on the local road network would be managed in line with the TMP.

No disabled parking spaces would be impacted by the proposal.


Albury to Illabo
Figure 5.15 Henty diversion travel time impacts


### 5.2.2.3 YERONG CREEK YARD CLEARANCES ENHANCEMENT SITE

## ROAD PERFORMANCE

The link LOS assessment for the Yerong Creek Yard clearances enhancement site component of the proposal is shown in Table 5.16. This assessment shows that with construction traffic all road links are expected to operate at LOS A or better, which is considered stable flow conditions as per the Guide to Traffic Generating Developments (RTA 2002). Further, the assessment shows no change in LOS as a result of the construction generated traffic and subsequently no significant impacts to road operation and performance are expected.

Table 5.16 Yerong Creek, construction route road performance

| ROAD NAME | ROAD TYPE | 2024 PEAK HOUR |  | 2024 WITH CONSTRUCTION PEAK HOUR |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Volume - one <br> way | LOS | Construction <br> volume - one way | Combined volume <br> - one way | LOS |  |
| Cox Street <br> (Olympic <br> Highway) | Highway | 275 | A | 56 | 331 | A |
| Plunkett Street $^{1}$ | Urban | 51 | A | 48 |  |  |
| Finlayson Lane $^{3}$ | Urban | 13 | A | 48 | 99 | A |

(1) No data available, volumes estimated as Olympic Highway - 50m East of Mangoplah Road, The Rock 2655
(2) No data available, volumes estimated as Sladen Street, Henty (East-West road through town)
(3) No data available, volumes estimated as $25 \%$ of Plunkett St

Note, construction peak hour volumes are higher on Cox Street (Olympic Highway) than on the other roads under assessment as the road performance assessment for highways requires assessment of PCUs which effectively doubles the count of heavy vehicles required for construction.

## INTERSECTION PERFORMANCE

An assessment of the performance of the highest trafficked (on a per lane basis) construction route intersection in the Greater Hume - Lockhart precinct during peak construction activities was undertaken for the Culcairn enhancement sites in section 5.2.2.1. The intersection assessment assessed peak hour construction traffic in conjunction with peak hour background traffic as a worst-case scenario for construction movements as expected construction start and finish times end outside of typical peak periods.

This assessment showed that the expected performance of the highest trafficked intersection in the precinct was LOS A, which is considered an acceptable LOS as per the Guide to Traffic Generating Developments (RTA 2002). Furthermore, the assessment shows no change in LOS as a result of the construction generated traffic and subsequently no significant impacts to intersection operation and performance are expected. Furthermore, $95^{\text {th }}$ queuing does not extend into any additional adjacent intersections as a result of the construction vehicles. As such, it is not considered that construction vehicles would impact the performance of any other lesser trafficked construction route intersection within the precinct. Therefore, no additional construction route intersection analysis has been undertaken for the Yerong Creek Yard clearances enhancement site.

## TEMPORARY CLOSURES AND DIVERSIONS

No road closures or diversions are proposed for the Yerong Creek Yard clearances enhancement site.

## PARKING

Parking for construction workers and laydown areas for unloading of heavy vehicles at the Yerong Creek Yard clearances enhancement site would be provided within the construction site area and so would have minimal impact to existing parking facilities. Any minor impacts to parking due to traffic control or site accesses on the local road network would be managed in line with the TMP.

No disabled parking spaces would be impacted by the proposal.

### 5.2.2.4 THE ROCK YARD CLEARANCES ENHANCEMENT SITE

## ROAD PERFORMANCE

The link LOS assessment for The Rock Yard clearances enhancement site component of the proposal is shown in Table 5.17. This assessment shows that with construction traffic all road links are expected to operate at LOS A or better, which is considered stable flow conditions as per the Guide to Traffic Generating Developments (RTA 2002). Furthermore, the assessment shows no change in LOS as a result of the construction generated traffic and subsequently no significant impacts to road operation and performance are expected.

Table 5.17 The Rock Yard clearances enhancement site, construction route road performance

| ROAD NAME | ROAD TYPE | 2024 PEAK HOUR |  | 2024 WITH CONSTRUCTION PEAK HOUR |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: |

(1) No data available, volumes estimated as Olympic Highway - 50m East of Mangoplah Road, The Rock 2655
(2) No data available, volumes estimated as Sladen Street, Henty

Note, construction peak hour volumes are higher on Melville Street (Olympic Highway) than on the other roads under assessment as the road performance assessment for highways requires assessment of PCUs which effectively doubles the count of heavy vehicles required for construction.

## INTERSECTION PERFORMANCE

An assessment of the performance of the highest trafficked (on a per lane basis) construction route intersection in the Greater Hume - Lockhart precinct during peak construction activities was undertaken for the Culcairn enhancement sites in section 5.2.2.1. The intersection assessment assessed peak hour construction traffic in conjunction with peak hour background traffic as a worst-case scenario for construction movements as expected construction start and finish times end outside of typical peak periods.

This assessment showed that the expected performance of the highest trafficked intersection in the precinct was LOS A, which is considered an acceptable LOS as per the Guide to Traffic Generating Developments (RTA 2002). Furthermore, the assessment shows no change in LOS as a result of the construction generated traffic and subsequently no significant impacts to intersection operation and performance are expected. Furthermore, $95^{\text {th }}$ queuing does not extend into any additional adjacent intersections as a result of the construction vehicles. As such, it is not considered that construction vehicles would impact the performance of any other lesser trafficked construction route intersection within the precinct. Therefore, no additional construction route intersection analysis has been undertaken for The Rock Yard clearances enhancement site.

## TEMPORARY CLOSURES AND DIVERSIONS

No road closures or diversions are proposed for The Rock enhancement site.

## PARKING

Parking for construction workers and laydown areas for unloading of heavy vehicles at The Rock Yard clearances enhancement site would be provided within the construction site area and so would have minimal impact to existing parking facilities. Any minor impacts to parking due to traffic control or site accesses on the local road network would be managed in line with the TMP.

No disabled parking spaces would be impacted by the proposal.

### 5.2.3 CONSTRUCTION SITE ACCESS

A turn warrant assessment for each enhancement site access in the Greater Hume - Lockhart precinct have been undertaken based on The Guide to Traffic Management - Part 6 Intersection, Interchanges and Crossings (Austroads 2020). This assessment has analysed a worst case scenario, assuming all peak generated construction traffic is distributed to each access during the road network peak period. The results of this assessment are shown in Table 5.18.

Table 5.18 Greater Hume - Lockhart precinct enhancement site access turn warrant assessment
\(\left.$$
\begin{array}{|l|l|l|l|l|}\hline \text { ENHANCEMENT } & \begin{array}{l}\text { ACCESS } \\
\text { NUMBER / } \\
\text { ROAD }\end{array} & \begin{array}{l}\text { ROAD } \\
\text { TYPE }\end{array}
$$ \& \begin{array}{l}ASSESSMENT <br>
OUTCOME <br>
(TURN <br>

TREATMENT)\end{array} \& CONSIDERATIONS\end{array}\right]\)| Street |
| :--- |
| Culcairn |


| ENHANCEMENT <br> SITE | ACCESS <br> NUMBER / <br> ROAD | ROAD <br> TYPE | ASSESSMENT <br> OUTCOME <br> (TURN <br> TREATMENT) | CONSIDERATIONS |
| :--- | :--- | :--- | :--- | :--- |
| The Rock | $46 /$ Urana <br> Street | Two-way | Basic Right-Turn <br> / Basic Left-Turn | Left and right turn into and out of site. <br> Opposing movements on public road. <br> Low speed environment $(\leq 60 \mathrm{~km} / \mathrm{h})$. <br> Current configuration does not meet turn warrant <br> guidance, Road Safety Audit would investigate the <br> need for traffic management of this access. |

Basic Right-Turn and Auxiliary Left-Turn / Channelised Right-Turn / Channelised Left-Turn treatments are required by the intersection turn warrant assessment for some site accesses in this precinct. However, this may not be required given the temporary nature of accesses during the construction phase and the conservative nature of the assessment (peak construction vehicles assessed during the background peak hour, when peak construction vehicles are expected outside the background peak hour).

More detailed assessment of the accesses will be undertaken as part of the Road Safety Audits and appropriate Construction Traffic Transport and Access Management Plans will be developed by the contractor prior to commencement of construction activities on site to moderate any potential safety issues. Design of any access treatments or modifications to roads would be undertaken in accordance with appropriate design standards and with approvals from the relevant local or state road authorities. Works Authorisation Deeds or other suitable consent or agreement with TfNSW will be made prior to undertaking any relevant works on a State Controlled Road.

### 5.2.4 ROAD SAFETY

During construction there would be changes to road conditions within the Greater Hume - Lockhart precinct consisting of increased traffic volumes due to construction vehicles, temporary diversions and new access points to the enhancement sites from the public road network. This study has primarily considered the operation and capacity of the road network rather than the appropriateness of use of certain roads by construction vehicles.

It is noted that the construction activities at enhancement sites within the Greater Hume - Lockhart precinct, are expected to generate a maximum peak hour flow of 48 vehicles (during a three-day possession peak period) and an appropriate LOS is maintained on all of the enhancement site access routes as discussed in section 5.2.2. Access intersections to the enhancement sites within the precinct would be designed or have traffic control measures implemented to provide suitable safe access to public roads in accordance with relevant standards and guidelines.

To moderate any construction impacts to potential safety issues, Road Safety Audits and Construction Traffic Transport and Access Management Plans would be required to be undertaken by the contractor prior to commencement of construction activities on site and the safety of all road users should be considered. Particular attention should be paid the type and size of vehicle using the level crossing on Rosler Parade during the five-day Sladen Street closure so that appropriate clearance to the rail line can be maintained when giving way to vehicles on the Olympic Highway.

### 5.2.5 HEAVY VEHICLE ROUTES

As there are no changes to background LOS resulting from the traffic generated by the construction activities at enhancement sites the within the Greater Hume - Lockhart precinct, it is not expected that construction heavy vehicle and workforce movements generated by the proposal, as shown in section 5.2.1.3, would impact the current operations of existing heavy vehicles movements, including agricultural transport, on the routes discussed in section 4.4.3.

The Henty Yard clearances enhancement site works would require Sladen Street, which forms part of the Heavy Vehicle route network, to be closed for a five-day period. This closure would require vehicles using this route to be diverted to an alternative heavy vehicle route across the southern level crossing on Rosler Parade via the Olympic Highway and Allan Street (a residential area), a diversion of approximately 2 km . Rosler Parade is designated as a heavy vehicle route in only the westbound direction. Due to the short duration of the diversion, Rosler Parade may be able to be used as a two-way heavy vehicle route. A Road Safety Audit, Construction Traffic Transport and Access Management Plans, in consultation with National Heavy Vehicle Regulator and TfNSW would need to be undertaken by the contractor prior to the closure of Sladen Street to minimise the impacts of diverted heavy vehicles to the surrounding road uses. Particular attention should be paid the type and size of vehicle using the level crossing on Rosler Parade during the five-day Sladen Street closure so that appropriate clearance to the rail line can be maintained when giving way to vehicles on the Olympic Highway.

There is potential for construction heavy vehicles to impact road pavement conditions along haul routes. To determine the extent of the impact a road dilapidation report would be prepared for all haul routes within the precinct.

Beyond the increased distance and travel times (a maximum of approximately five minutes), it is not expected that heavy vehicle movements would be impacted as a result of the diversion.

### 5.2.6 TRAVELLING STOCK RESERVES

Travelling Stock Reserves are located on the following roads expected to support construction access for The Rock Yard clearances enhancement site:

- Olympic Highway
- Urana Street.

Based on the low traffic volumes generated by the construction activities it is not expected that heavy vehicle and workforce movements would impact the operation of these Travelling Stock Reserves. It is noted that the additional construction traffic does not result in a change of LOS on any of the construction access routes within the Greater Hume - Lockhart precinct.

It is expected that prior to the commencement of works that Local Land Services would be notified of increased vehicle movements along the TSRs and temporary closures of rail level crossings in the Greater Hume - Lockhart precinct so that stock handlers, including walking permit holders, can be notified of the impacts to stock movements.

### 5.2.7 PUBLIC TRANSPORT ROUTES

### 5.2.7.1 ROAD

Bus routes are located along the proposed construction access routes to enhancement sites within the Greater Hume Lockhart precinct on the following road links:

- Olympic Highway
- Railway Parade
- Balfour Street
- Plunkett Street
- Finlayson Street
- Sladen Street
- Olympic Highway
- Urana Street.

Construction activities at enhancement sites within the Greater Hume - Lockhart precinct will generate increased traffic on these roads. Resulting impact on the operation of public or school bus services or bus stops are expected to be minimal due to the low traffic volumes generated by the construction activities (which do not result in a change in LOS from current operation). It is noted that the heaviest period of construction workforce movements at the start and end of construction hours ( 6 am to 6 pm ) outside peak bus service periods (e.g. school times). There may be minor delays to buses passing near the enhancement sites from reduced speed limits and traffic control.

These impacts would be managed in accordance with the traffic management plan to ameliorate impacts to the safe and efficient travel of bus services through the affected areas.

The level crossing works on Sladen Street would require the road to be closed which would require existing traffic to be diverted to the southern level crossing on Rosler Parade via Allan Street. This diversion is expected to have a minimal impact on the operation of these bus services due to the on-demand nature of bus services through Henty with non-fixed routes and the limited time of the diversion (five days).

### 5.2.7.2 RAIL

Construction activities requiring possessions would occur during either:

- existing scheduled weekend rail corridor possession periods (typically 72 hours) when trains along the rail corridor are stopped for maintenance as part of operation of the existing rail line; or
- track work authorisations periods, which enable works that impact rail operations to occur outside scheduled rail possessions, but within available 9-hour windows in which train services are not scheduled.

Work during these periods would be undertaken in consultation with passenger rail operators. However, it is not expected that proposal construction works would impact upon the rail services and train station platforms will not be impacted by the enhancement sites.

### 5.2.8 ACTIVE TRANSPORT ROUTES

As shown in section 4.3.6, provision of active transport infrastructure within the Greater Hume - Lockhart precinct is minimal, and although road lanes may be used for cycling, given the surrounding land uses the demand for cycling and pedestrian travel in the area is likely to be low. Although there would be increased traffic resulting from construction activities at enhancement sites within the Greater Hume - Lockhart precinct it is expected to have a minimal impact on cycling or pedestrian movements due to the low traffic volumes generated by the construction activities (which do not result in a change in LOS from current operation).

The removal of the pedestrian overpass on Balfour Street in Culcairn will not impact pedestrian connectivity as the overpass is already closed and the pedestrian crossing facility at the level crossing adjacent to the overpass would remain open.

The level crossing works on Sladen Street in Henty would require the road to be closed temporarily (five days), however pedestrian connectivity would be maintained through the closure's duration and would be managed in accordance with the TMP.

There may be minor disruptions to cyclists using roads near the enhancement sites as a result of traffic control. These impacts although expected to be minimal would be managed in accordance with the TMP.

### 5.2.9 PROPERTY ACCESS IMPACTS

It is not expected that there would be disruptions to property access associated with construction activities within the Greater Hume - Lockhart precinct. Any changes to arrangements would need to be undertaken in consultation with the relevant stakeholders and in line with the TMP.

### 5.2.10 RAIL FREIGHT

Section 5.2.7.2 notes when construction activities requiring possessions will occur.
Work during these periods would be undertaken in consultation with freight operators. However, it is not expected that proposal construction works would impact upon the rail freight network. Note, there are no other impacts to freight operations.

### 5.2.11 EMERGENCY VEHICLE ACCESS

Construction of the proposal would result in temporary impacts to traffic and an increase in vehicle movements on the road network. As shown in the link and intersection performance assessments, there is no significant impact to the performance of the road network due to the construction generated traffic within the Greater Hume - Lockhart precinct, and so there is not expected to be a significant impact to emergency vehicles movements. It is expected that the traffic and access management plan would be developed in consultation with TfNSW, Greater Hume and Lockhart Councils, and State emergency services and would consider and effectively manage any impacts to emergency vehicles seeking to use roads in the vicinity of the enhancement sites.

### 5.2.12 SEASONAL VARIATION

Temporary local events such as festivals, shows, and markets may result in minor localised traffic variations, particularly in urban environments. The Greater Hume - Lockhart precinct is generally less urbanised than other precincts, featuring more rural and agricultural land uses.

Localised seasonal traffic variation may be experienced at enhancement sites that share land with agricultural infrastructure (grain silos, livestock loading facilities etc.) as the infrastructure will likely generate additional heavy or farm vehicle movements during harvest seasons as discussed in section 4.2.2.

A review of aerial imagery of enhancement sites in the Greater Hume - Lockhart precinct identified grain silos in the vicinity of the following enhancement sites:

- Culcairn Yard clearances
- Yerong Creek Yard clearances
- Henty Yard clearances
- The Rock Yard clearances.

However, it is not anticipated that seasonal variation would significantly impact the outcomes of the traffic assessment as background and construction vehicle traffic volumes are low.

More detailed assessment of the enhancement site accesses, which would consider seasonal variation due to social events and agricultural movements, will be undertaken by the contractor prior to commencement of construction activities on site. These would include Road Safety Audits and appropriate Construction Traffic Transport and Access Management Plans to moderate any potential safety issues.

### 5.3 WAGGA WAGGA PRECINCT

### 5.3.1 CONSTRUCTION PROFILE

This section outlines the construction profile for the proposal within the Wagga Wagga precinct. This includes all vehicle routes, as shown in section 5.3.1.2, and all volumes of heavy and light vehicles required for construction of the proposal, as shown in section 5.3.1.3, which includes the vehicles required for the import and export of fill material. It also outlines other construction requirements, such as temporary road closures and diversions, and parking requirements for each enhancement site.

### 5.3.1.1 CONSTRUCTION PROGRAM

Key construction stages and work durations at each enhancement site within the Wagga Wagga precinct are summarised in Table 5.19 and Figure 5.16.

Table 5.19 Summary of construction stages - Wagga Wagga enhancement sites

| ENHANCEMENT SITES | CONSTRUCTION STAGES UNDERTAKEN | START | FINISH | DURATION OF WORKS (MONTHS) | RAIL POSSESSION REQUIRED |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Uranquinty Yard clearances | - Site establishment <br> - Track realignment ( $>300 \mathrm{~mm}$ and/or track formation replacement) <br> - Level crossing modification <br> - Rail underbridge modifications <br> - Gantry removal <br> - Demobilisation and landscaping | 15 July 2024 | $\begin{gathered} 24 \text { September } \\ 2024 \end{gathered}$ | 2 | Yes |
| Pearson Street bridge | - Site establishment <br> - Track lowering <br> - Demobilisation and landscaping | $\begin{gathered} 15 \text { January } \\ 2024 \end{gathered}$ | 10 April 2025 | 16 | Yes |
| Cassidy Parade pedestrian bridge | - Site establishment <br> - Pedestrian bridge replacement works <br> - Demobilisation and landscaping | 1 February $2024$ | 17 July 2024 | 6 | Yes |
| Edmondson Street bridge | - Site establishment <br> - Track realignment ( $<300 \mathrm{~mm}$ ) <br> - Road bridge replacement <br> - Demobilisation and landscaping | $\begin{gathered} 20 \text { February } \\ 2024 \end{gathered}$ | $\begin{gathered} 23 \text { December } \\ 2024 \end{gathered}$ | 11 | Yes |


| ENHANCEMENT SITES | CONSTRUCTION STAGES UNDERTAKEN | START | FINISH | DURATION OF WORKS (MONTHS) | RAIL POSSESSION REQUIRED |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Wagga Wagga Station pedestrian bridge | - Site establishment <br> - Gantry works <br> - Pedestrian replacement works <br> - Demobilisation and landscaping | $\begin{aligned} & 15 \text { January } \\ & 2025 \end{aligned}$ | 1 July 2025 | 6 | Yes |
| Wagga Wagga Yard clearances | - Site establishment <br> - Track realignment ( $>300 \mathrm{~mm}$ and/or track formation replacement) <br> - Gantry replacement <br> - Demobilisation and landscaping | 1 February $2024$ | 16 April 2024 | 3 | Yes |
| Bomen Yard clearances | - Site establishment <br> - Track realignment ( $>300 \mathrm{~mm}$ and/or track formation replacement) <br> - Demobilisation and landscaping | 15 July 2024 | $\begin{aligned} & 24 \text { September } \\ & 2024 \end{aligned}$ | 2 | Yes |



Figure 5.16 Wagga Wagga precinct construction programme

### 5.3.1.2 CONSTRUCTION AND DIVERSION ROUTES

Proposed construction routes and accesses to enhancement sites in the Wagga Wagga precinct are shown below in Figure 5.17 to Figure 5.21.

Vehicle and pedestrian diversions proposed during construction are as follows:

- Uranquinty Yard clearances
- level crossing works to be completed under traffic control
- pedestrian access to be maintained.
- Cassidy Parade pedestrian bridge:
- Cassidy Parade closure. A small area of Cassidy Parade would be closed for a lift pad. No vehicle detour is proposed as access to properties would be maintained.
- pedestrian detours via Wagga Wagga Station pedestrian bridge (Mothers Bridge) and the Bourke/Docker Street level crossing.
- Edmondson Street bridge
- Erin Street closure: vehicle detour via Macleay and Coleman streets.
- Edmondson Street closure: vehicle detour via Docker Street to the west and Lake Albert Road to the east.
- pedestrian detours via Cassidy Parade pedestrian bridge (when completed) and Wagga Wagga Station pedestrian bridge (Mothers Bridge).
- Wagga Wagga Station pedestrian bridge
- pedestrian detour via Edmondson Street bridge.

Construction routes have been selected to minimise the use of local roads where possible. However, use of local roads is generally required to facilitate access to enhancement sites. As shown in section 5.3.1.3, construction vehicle volumes using construction routes and accesses on local roads are generally low.

Diversion routes have been selected on roads of the same order where possible. In the instances where diversion routes have been required on roads of a lower order, the requirement for mitigation has been considered.

Mitigations for the use of all road types, including local roads are provided in section 8.2. In addition, mitigation measures have been identified for other assessments, including noise and vibration, visual and social, to address potential impacts from the use of construction and diversion routes.

Where diversions are required for active travel routes, the selected diversion route has considered where pedestrian infrastructure is present. Where cyclists utilise diversion routes, and an existing cycle or shared path is not present, cyclists would be required to cycle on-road. To facilitate access to the rail corridor and surrounds for construction vehicles, including surrounding residences, diversion of pedestrians and cyclists within the proposal site would also be required. Detailed consideration of the management of pedestrian and cyclist safety within the proposal site will be completed prior to and during construction. Mitigation measures, including the requirements for a Traffic Management Plan (TMP), are provided in section 8.2.




## INLAND <br> RAIL $=$





### 5.3.1.3 VEHICLE TYPE AND QUANTITY

Table 5.20 shows the peak hour two-way movements at each site as identified from construction scenario data shown in Chapter 8: Construction of the proposal of the EIS.

Table 5.20 Peak hour construction movements - Wagga Wagga precinct

| ENHANCEMENT SITES | VEHICLE TYPES | PEAK HOUR MOVEMENTS | CONSTRUCTION VEHICLE PARKING AND LAYDOWN |
| :---: | :---: | :---: | :---: |
| Uranquinty Yard clearances | Light Vehicle | $27^{1}$ in (am) / out (pm) | Internal to Proposal site |
|  | Heavy Vehicle | 8 in and out |  |
| Pearson Street bridge | Light Vehicle | $33^{1}$ in (am) / out (pm) | Internal to Proposal site |
|  | Heavy Vehicle | 3 in and out |  |
| Cassidy Parade pedestrian bridge | Light Vehicle | $13^{2}$ in (am) / out (pm) | Internal to Proposal site |
|  | Heavy Vehicle | 3 in and out |  |
| Edmondson Street bridge | Light Vehicle | $20^{1}$ in (am) / out (pm) | Internal to Proposal site |
|  | Heavy Vehicle | 5 in and out |  |
| Wagga Wagga Station pedestrian bridge | Light Vehicle | $13^{2}$ in (am) / out (pm) | Internal to Proposal site |
|  | Heavy Vehicle | 3 in and out |  |
| Wagga Wagga Yard clearances | Light Vehicle | $27^{1}$ in (am) / out (pm) | Internal to Proposal site |
|  | Heavy Vehicle | 10 in and out |  |
| Wagga Wagga Yard clearances - Docker Street Gantry | Light Vehicle | 8 in (am) / out (pm) | Internal to Proposal site |
|  | Heavy Vehicle | 2 in and out |  |
| Bomen Yard clearances | Light Vehicle | $27^{1}$ in (am) / out (pm) | Internal to Proposal site |
|  | Heavy Vehicle | 8 in and out |  |

(1) Possession peak (typically only 13 vehicle movements in a peak period)
(2) Possession peak (typically only 7 vehicle movements in a peak period)

### 5.3.2 ROAD NETWORK OPERATION

### 5.3.2.1 URANQUINTY YARD CLEARANCES ENHANCEMENT SITE

## ROAD PERFORMANCE

The link LOS assessment for the Uranquinty Yard clearances enhancement site component of the proposal is shown in Table 5.21. This assessment shows that with construction traffic all road links are expected to operate at LOS B or better, which is considered stable flow conditions as per the Guide to Traffic Generating Developments (RTA 2002).
Furthermore, the assessment shows no change in LOS as a result of the construction generated traffic and subsequently no significant impacts to road operation and performance are expected.

Table $5.21 \quad$ Uranquinty enhancement site, construction route road performance

| ROAD | 2024 PEAK HOUR |  | 2024 WITH CONSTRUCTION PEAK HOUR |  |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: |
| Road name | Road type | Volume - one <br> way | LOS | Construction <br> volume - one <br> way | Combined <br> volume - one <br> way | LOS |
| Olympic <br> Highway |  |  |  |  |  |  |
| Uranquinty Street | Urban | 323 | A | 43 | 366 | A |
| Yarragundry <br> Street | Urban | 27 | A | 35 | 62 | A |
| Hanging Rock <br> Road | Rural | 4 | A | 35 | 66 | A |

(1) No data available, volumes estimated as average of Olympic Highway - Ashmont, 95065 and Olympic Highway The Rock, 9551
(2) Estimated traffic volume based on road type and surrounding land uses

Note, construction peak hour volumes are higher on Olympic Highway than on the other roads under assessment as the road performance assessment for highways requires assessment of PCUs which effectively doubles the count of heavy vehicles required for construction.

## INTERSECTION PERFORMANCE

An assessment of the performance of the highest trafficked, on a per lane basis, construction route intersection in the Wagga Wagga precinct (excluding the Wagga Wagga Station enhancement sites intersections, which are assessed as part of the Edmondson Street bridge diversion assessment) during peak construction activities was undertaken for the Pearson Street bridge enhancement sites in section 5.3.2.2.

This assessment showed that the expected performance of the intersection with construction traffic was LOS B, which is considered an acceptable LOS as per the Guide to Traffic Generating Developments (RTA 2002). Furthermore, the assessment shows no change in LOS as a result of the construction generated traffic and subsequently no significant impacts to intersection operation and performance are expected. Furthermore, $95^{\text {th }}$ queuing does not extend into any additional adjacent intersections as a result of the construction vehicles. As such, it is not considered that construction vehicles would impact the performance of any other lesser trafficked construction route intersection within the precinct. Therefore, with the exception of the Wagga Wagga Station enhancement sites diversion assessment, no additional construction route intersection analysis has been undertaken for the Wagga Wagga precinct enhancement sites.

## TEMPORARY CLOSURES AND DIVERSIONS

No road closures or diversions are proposed for the Uranquinty Yard clearances enhancement site.

## PARKING

Parking for construction workers and laydown areas for unloading of heavy vehicles at the Uranquinty Yard clearances enhancement site would be provided within the construction site area and so would have minimal impact to existing parking facilities. Any minor impacts to parking due to traffic control or site accesses on the local road network would be managed in line with the TMP.

No disabled parking spaces would be impacted by the proposal.

### 5.3.2.2 PEARSON STREET BRIDGE ENHANCEMENT SITE

## ROAD PERFORMANCE

The link LOS assessment for the Pearson Street bridge enhancement site component of the proposal is shown in Table 5.22. This assessment shows no change in LOS as a result of the construction generated traffic and subsequently no significant impacts to road operation and performance are expected. With construction traffic, road links are expected to operate at LOS C or better, which is considered stable flow conditions as per the Guide to Traffic Generating Developments (RTA 2002), with the exception of Fernleigh Road, which operates at LOS D (close to the limit of stable flow). However, the assessment shows that this condition would occur both with and without construction traffic, and that no significant impacts to road operation and performance from the existing are expected as a result of construction activities.

Table 5.22 Pearson Street bridge, construction route road performance

| ROAD |  | 2024 PEAK HOUR |  | 2024 WITH CONSTRUCTION PEAK HOUR |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Road name | Road type | Volume - one way | LOS | Construction volume - one way | Combined volume - one way | LOS |
| Edward Street (Sturt Highway) ${ }^{1}$ | Urban | 1,013 | B | 36 | 1,049 | B |
| Moorong Street (Olympic Highway) ${ }^{1}$ | Highway | 1,003 | C | 39 | 1,042 | C |
| Pearson Street ${ }^{1}$ | Urban | 954 | B | 36 | 990 | B |
| Urana Street ${ }^{1}$ | Urban | 518 | C | 36 | 554 | C |
| Cheshire Street ${ }^{2}$ | Urban | 48 | A | 36 | 84 | A |
| Alan Turner Depot Access Road ${ }^{3}$ | Urban | 101 | A | 36 | 137 | A |
| Fernleigh Road ${ }^{1}$ | Urban | 665 | D | 36 | 701 | D |

(1) 10-hour traffic volumes ( $5 \mathrm{am}-10 \mathrm{am}$ and $2 \mathrm{pm}-7 \mathrm{pm}$ )
(2) No data available, volumes estimated as $5 \%$ of Pearson Street 10 -hour
(3) Estimate traffic volume based on road type and surrounding land uses

Note, construction peak hour volumes are higher on Moorong Street (Olympic Highway) than on the other roads under assessment as the road performance assessment for highways requires assessment of PCUs which effectively doubles the count of heavy vehicles required for construction.

## INTERSECTION PERFORMANCE

The intersection of Edward Street and Pearson Street have the highest traffic volumes in the Wagga Wagga precinct on a per lane basis (excluding the Wagga Wagga Station enhancement sites, which are assessed as part of the Edmondson Street bridge diversion assessment).

Therefore, the Edward Street/Pearson Street intersection has been assessed in SIDRA to reflect a 'worst-case' scenario of construction vehicle impact at an intersection within the Wagga Wagga precinct. The intersection assessment assessed peak hour construction traffic in conjunction with peak hour background traffic as a worst-case scenario for construction movements as expected construction start and finish times end outside of typical peak periods.

Figure 5.22 shows the layout of the Edward Street and Pearson Street intersection as modelled in SIDRA.
The highest peak hour turning volumes at the Edward Street and Pearson Street intersection have been taken from a traffic survey at the intersection in 2021 and forecast 2024 volumes have been derived using a 3 per cent per year compounding growth rate. The traffic survey determined that the AM peak hour was the highest trafficked peak period at this intersection, as such the AM peak hour is the subject of this intersection assessment.


Figure 5.22 Edward Street and Pearson Street
Table 5.23 shows the SIDRA results for the Edward Street and Pearson Street intersection during a 2024 peak hour with and without construction vehicles. The results show the performance of the intersection is not significantly impacted by construction vehicles: LOS continues operates at an acceptable level (LOS B), DOS only increases from $0.682-0.701$, intersection delay only increases by one second, and $95^{\text {th }}$ percentile queue lengths only increases by 2 m (approx. one vehicle). $95^{\text {th }}$ queuing does not extend into any additional adjacent intersections as a result of the construction vehicles.

Table 5.23
Edward Street and Pearson Street, 2024 construction route intersection capacity - AM Peak

|  | 2024 AM PEAK HOUR |  |  |  | 2024 AM PEAK HOUR WITH CONSTRUCTION |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | DOS | Delay <br> (s) | LOS | 95 ${ }^{\text {th }} \%$ ile queue ( m ) | DOS | Delay <br> (s) | LOS | $95^{\text {th }} \%$ ile queue ( m ) |
| South: Pearson Street (S) | 0.576 | 10 | LOS B | 32 | 0.579 | 10 | LOS B | 33 |
| East: Edward Street (E) | 0.368 | 10 | LOS B | 17 | 0.386 | 10 | LOS B | 18 |
| North: Moorong Street (Olympic Highway)(N) | 0.682 | 13 | LOS B | 47 | 0.701 | 13 | LOS B | 49 |
| West: Sturt Highway (W) | 0.563 | 12 | LOS B | 29 | 0.578 | 12 | LOS B | 30 |
| Intersection | 0.682 | 11 | LOS B | 47 | 0.701 | 12 | LOS B | 49 |

As the Edward Street and Pearson Street intersection is reflective of the 'worst case' construction vehicle impact at a construction route intersection without diversion traffic in the Wagga Wagga precinct, it is not considered that the performance of any other construction route intersection within the precinct would be significantly impacted by construction vehicles alone. Further intersection analysis is presented as component of the Edmondson Street bridge closure diversions assessment to understand the impacts of diverted traffic flows on the surrounding road network.

## TEMPORARY CLOSURES AND DIVERSIONS

No road closures or diversions are proposed for the Pearson Street bridge work site.

## PARKING

Parking for construction workers and laydown areas for unloading of heavy vehicles at the Pearson Street bridge enhancement site would be provided within the construction site area or unused parts of the Wagga Wagga Showgrounds and so would have minimal impact to existing parking facilities. Any minor impacts to parking due to traffic control or site accesses on the local road network would be managed in line with the TMP.

No disabled parking spaces would be impacted by the proposal.

### 5.3.2.3 WAGGA WAGGA WAGGA STATION AND SURROUNDS ENHANCEMENT SITES

The enhancement sites in the vicinity of the Wagga Wagga Station share the same road network and have been combined in the following section, for:

- Cassidy Parade pedestrian bridge enhancement site
- Edmondson Street bridge enhancement site
- Wagga Wagga Station pedestrian bridge enhancement site
- Wagga Wagga Yard clearances enhancement site.


## ROAD PERFORMANCE

The link LOS assessment for the Wagga Wagga Wagga Station and surrounds enhancement sites component of the proposal is shown in Table 5.24. This road performance assessment excludes road links expected to be used as diversion routes during the Edwardson Street Bridge closure (addressed within the Edmondson Street bridge closure diversion assessment for cumulative construction and the diversion traffic). As the enhancement sites within this area are likely to use similar access routes, the combined highest construction traffic volumes generated by Cassidy Parade pedestrian bridge, Edmondson Street bridge and Wagga Wagga Yard clearances enhancement sites during possessions has been used to assess potential impacts to construction access routes. This assessment shows that with construction traffic all road links are expected to operate at LOS C or better, which is considered stable flow conditions as per the Guide to Traffic Generating Developments (RTA 2002).

The assessment shows a change in LOS as a result of the construction generated traffic on Brookong Street and Fox Street from LOS A to LOS B. However, it is noted that these streets are short streets serving a local access function with limited through traffic potential, LOS B still represents stable traffic flow with drivers having reasonable freedom to choose their desired speed, and that the change does not suggest that a significant impact to road operation and performance is expected.

Table 5.24 Wagga Wagga Wagga Station and surrounds enhancement sites, construction route road performance

| ROAD NAME | ROAD TYPE | 2024 PEAK HOUR VEHICLES - ONE-WAY |  | 2024 PEAK HOUR WITH CONSTRUCTION VEHICLES - ONE WAY |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Volume | LOS | Construction volume | Combined volume | LOS |
| Edward Street (Sturt Highway) ${ }^{1}$ | Urban | 1,096 | B | 100 | 1,196 | B |
| Fox Street ${ }^{2}$ | Urban | 895 | A | 100 | 995 | B |
| Mitchelmore Street ${ }^{1}$ | Urban | 38 | A | 100 | 138 | A |
| Edmondson Street ${ }^{1}$ | Urban | 563 | A | 100 | 663 | A |
| Norman Street ${ }^{3}$ | Urban | 795 | A | 100 | 895 | A |
| Coleman Street ${ }^{1}$ | Urban | 38 | A | 100 | 138 | A |
| Cassidy Parade ${ }^{4}$ | Urban | 382 | C | 100 | 482 | C |
| Erin Street ${ }^{5}$ | Urban | 76 | A | 100 | 176 | A |
| Station Place ${ }^{6}$ | Urban | 52 | A | 100 | 152 | A |
| Brookong Avenue ${ }^{7}$ | Urban | 182 | A | 100 | 282 | B |

(1) 10 -hour ( 5 am to 10 am and 2 pm to 7 pm ) traffic survey volumes
(2) No data available, volumes estimated as Norman Street 10 -hour
(3) No data available, volumes estimated as $50 \%$ of Cassidy Street 10 -hour
(4) No data available, volumes estimated as $20 \%$ of Coleman Street 10 -hour
(5) No data available, volumes estimated as $10 \%$ of Urana Street 10-hour
(6) No data available, volumes estimated as Smollett Street, Albury 10-hour
(7) No data available, volumes estimated as $10 \%$ of Edward Street 10 -hour

## INTERSECTION PERFORMANCE

SIDRA intersection analysis was undertaken as a component of the diversion assessment associated with the Edmondson Street bridge Closure to assess the cumulative impact of diverted vehicles and construction vehicles to intersection performance in central Wagga.

As vehicle diversions are proposed to be in place for the majority of the construction period in this area (nine months closure of Edmondson Street bridge out of 11 months of construction activities at the enhancement site), it has not been deemed necessary to assess the impact of solely construction vehicles on intersection performance when diversions would not be in place. It is expected that during this period the impact to intersection performance within Wagga Wagga would be minimal (a total of 100 construction vehicles during a peak hour).

The intersection assessment assessed peak hour construction traffic in conjunction with peak hour background and diversion traffic as a worst-case scenario as is considered a worst case scenario as construction start and finish times end outside of typical peak periods. The results of the assessment are discussed in the sections below.

## TEMPORARY CLOSURES AND DIVERSIONS

The reconstruction of the Edmondson Street bridge would require a road closure on both Edmondson Street and Erin Street for a nine month period. Based on traffic counts procured as part of this study and extrapolated to the construction year of 2024 (at a 3 per cent compounding per annum growth rate) this diversion is expected to impact over 11,000 vehicles per day travelling on Edmondson Street. The road closures would require traffic diversions (as shown in Figure 5.23) for:

- Mitchelmore Street/Edmondson Street traffic:
- traffic to/from the west and 50 per cent of the through movements on Edmondson Street assumed to be rerouted to the west via Urana Street, Docker Street, Bourke Street, and Edward Street
- traffic to/from the east and 50 per cent of the through movements on Edmondson Street assumed to be rerouted to the east via Urana Street, MacLeay Street, Railway Street and Lake Albert Road.

It is noted that in the absence of origin-destination data for the area, the assessment of this diversion has assumed a worstcase scenario where all traffic rerouted from Edmondson Street would use the specified diversion routes.

Local traffic that currently uses Erin Street would be diverted via Coleman Street or Railway Street. Based on surrounding land uses and network connectivity, this traffic and associated impacts are expected to be minimal as only a few houses are located on the street, and as such it has not been assessed.

The assumed diversion routes have been selected to minimise impacts to the road network by using higher order roads for diverted traffic. The diversion routes have also been selected based on the shortest route available and the lowest amount of turning movements required. Road Safety Audits and Construction Traffic Transport and Access Management Plans would be undertaken by the contractor prior to commencement of diversionary routes. Note, use of diversionary routes cannot be completely controlled and would be subject to road user decisions.


## ROAD PERFORMANCE

The link LOS assessment for the Edmondson Street bridge diversion is shown in Table 5.25 which details a worst case assessment of road performance during the AM peak hour (the heaviest traffic peak period) including both peak construction vehicles (where applicable) and peak hour diverted vehicles.

The assessment shows that a change in link LOS is seen on all roads under assessment as a result of the diversions and construction traffic. However, impacts outside of the peak hours are anticipated to be less. Moreover, the diversionary period is temporary. LOS is expected to be restored to existing levels following the end of the diversionary period. Furthermore, it is noted that, as the diversions are proposed to occur over a ten-month (231 working days) period it is expected that a proportion of diverted vehicles may seek alternative routes to the proposed diversions across the broader network, particularly for those trips that would travel on diversion routes but that do not cross the rail line. This potential redistribution of diverted vehicles would likely reduce the impact to link LOS shown in Table 5.25 and distribute the impacts of diverted traffic more proportionally across Wagga Wagga. This effect is discussed further in Summary of diversion impacts. Moreover, as discussed in section 8.2 traffic mitigation measures will be put in place to reduce the impact of the diversions during this temporary period, including consideration of temporary changes to signal phasing to improve LOS.

Table 5.25 Edmondson Street bridge, diversion routes road performance assessment

| ROAD | $\begin{array}{c}\text { 2024 PEAK HOUR } \\ \text { ONE-WAY }\end{array}$ |  | 2024 WITH DIVERSION PEAK HOUR |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ONE-WAY |  |  |  |  |  |$]$

(1) one-lane in each direction (lower capacity than two lane roads)
(2) highest traffic volume on Edmondson Street (northbound) to be diverted to the west (one-way)
(3) highest traffic volume on Edmondson Street (northbound) to be diverted to the east (one-way)

## INTERSECTION PERFORMANCE

The traffic diversions assumed for the replacement of the Edmondson Street bridge uses several intersections through Wagga Wagga. To identify intersections where significant impacts may occur as a result of the diversions and where further analysis was required, a qualitative assessment was undertaken based on changes to traffic volumes and opposing traffic flows from the diversions at each intersection. The results are shown in Table 5.26.

Table 5.26 Diversion intersection impacts - Edmondson Street bridge enhancement site

| INTERSECTION | DESCRIPTION OF TRAFFIC FLOW CHANGE DURING DIVERSION | EXPECTED TRAFFIC IMPACT |
| :---: | :---: | :---: |
| Edward Street / <br> Best Street / Edmondson Street | Changed turn movement proportions, reduced vehicles travelling to/from Edmondson Street | Minimal impact/improvement expected due to overall vehicle volumes at the intersection remaining constant/potentially reducing. |
| Edward Street <br> Docker Street | Significant increased turning movements | Potential for significant delays for vehicles turning in/out of Docker Street |
| Docker Street/Coleman Street/ Bourke Street | Increased through movements on Docker Street | Potential delays for vehicles turning in/ out of Coleman Street. |
| Bourke Street/Urana Street | Significant increased turning movements | Potential significant delays for vehicles turning in/out of Urana Street and Bourke Street. |
| Urana Street/Mitchelmore Street | Redistributed turn movements but no increase to overall traffic volumes at the intersection. | Minimal impact expected due to overall vehicle volumes at the intersection remaining constant. |
| Coleman Street/Edmondson Street/ Mitchelmore Street | Decreased through movements. | Potential increase in intersection performance. |
| Urana Street/MacLeay Street | Significant increased turning movements | Potential significant delays for vehicles turning in/out of Urana Street and MacLeay. |
| MacLeay Street/Coleman Street | Increased through movements on MacLeay Street | Potential delays for vehicles on MacLeay Street. |
| Lake Albert Road/Railway Street | Significant increased turning movements | Potential significant delays for vehicles turning in/out of Lake Albert Road and Railway Street. |
| Edward Street <br> Lake Albert Road | Significant increased turning movements | Potential significant delays for vehicles turning in/out of Lake Albert Road and Railway Street. |

As a result of the qualitative assessment in Table 5.26, some intersections are expected to perform adequately during the diversion period, while the following intersections were identified as the most likely to be significantly impacted by the proposal:

- Edward Street/Docker Street intersection
- Bourke Street/Urana Street intersection
- Urana Street/MacLeay Street intersection
- Lake Albert Road/Railway Street intersection
- Edward Street/Lake Albert Road intersection.

These intersections have been assessed in SIDRA to determine the impacts of the proposal to intersection performance. Traffic surveys undertaken in 2021 have been used to determine the highest peak hour turning volumes at these intersections. The peak hour turning volumes have been forecast to 2024 volumes using a 3 per cent per year compounding growth rate for the without proposal analysis. The peak hour diverted traffic volumes (those currently crossing Edmondson Street bridge) and construction vehicles, were allocated to the appropriate turn movements on the diversionary routes for the with proposal analysis. The traffic survey determined that the AM peak hour was the highest trafficked peak period at these intersections, as such the AM peak hour is the subject of this intersection assessment.

## EDWARD STREET / DOCKER STREET INTERSECTION

Figure 5.24 shows the layout of the Edward Street/Docker Street intersection as modelled in SIDRA.


Figure 5.24 Edward Street/Docker Street SIDRA intersection layout

Table 5.27 shows the SIDRA results for the Edward Street/Docker Street intersection during a 2024 peak hour with and without diversions or construction vehicles. The results show that the intersection would operate at a DOS of ( 0.924 ) without construction or diverted vehicles. With the construction and diverted vehicles the DOS of the intersection increases from 0.924 to 1.034 , and average delay increases by approximately 1 minute per vehicle, increasing the LOS from an LOS D to LOS F. $95^{\text {th }}$ percentile queue lengths are also shown to increase (a maximum of 452 m ) as a result of the diversion. These increases to queue lengths would potentially impact the performance of adjacent intersections on Docker Street and Edward Street.

Table 5.27 Edward Street/Docker Street, 2024 SIDRA analysis - AM Peak

\left.|  | 2024 AM PEAK HOUR |  |  |  | 2024 AM PEAK HOUR WITH |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CONSTRUCTION + DIVERSION |  |  |  |  |  |  |  |$\right]$

Note, this assessment of intersection performance with construction and diverted vehicles is considered to be a 'worstcase' assessment and it is expected that a proportion of vehicles would seek alternative routes to avoid this congested intersection, particularly for those trips that would travel on diversion routes but that do not cross the rail line. This potential redistribution of diverted vehicles would likely reduce the impact to intersection performance shown in Table 5.27 and distribute the impact of diversions more proportionally across the broader network.

Moreover, the assessment of a peak hour is not reflective of intersection performance across a day, which during off-peak periods, is likely to operate more optimally with lower vehicle volumes than seen during a peak hour. Furthermore, to provide a conservative assessment, peak construction vehicles have been assessed during the background peak hour, when peak construction vehicles are expected outside the background peak hour.

Furthermore, as discussed in section 8.2 traffic mitigation measures will be put in place to reduce the impact of the diversions during this temporary period, including consideration of temporary changes to signal phasing to improve LOS.

It should be noted that the diversionary period is temporary, and that LOS is expected to be restored to existing levels following the end of the diversionary period.

## BOURKE STREET / URANA STREET INTERSECTION

Figure 5.25 shows the layout of the Bourke Street/Urana Street intersection as modelled in SIDRA.


Figure 5.25
Bourke Street/Urana Street SIDRA intersection layout

Table 5.28 shows the SIDRA results for the Bourke Street/Urana Street intersection during a during a 2024 peak hour with and without construction and diverted vehicles. The results show that the intersection operates at LOS A and with $95^{\text {th }}$ percentile queues up to 30 m without construction or diverted vehicles. With construction and diverted vehicles, the intersection operates at a DOS over 1. Most roads do not see a significant increase in LOS, delay or queuing, in some instances delay decreases. However, the Bourke Street south approach increases from LOS A to LOS F, with 102 seconds of increased delay and significant increases in queuing due to the large increase in diverted traffic on the east approach which has priority. The increases in $95^{\text {th }}$ queue lengths on the south, east and north approaches will potentially impact the performance of adjacent intersections on Bourke Street and Urana Street.
This changes the overall intersection LOS from LOS A to LOS D. The high DOS, delay, and queue length suggests that the south approach will incur the greatest impact.
Table 5.28 Bourke Street/Urana Street, 2024 construction route intersection capacity - AM Peak

|  | 2024 AM PEAK HOUR |  |  | 2024 AM PEAK HOUR WITH <br> CONSTRUCTION + DIVERSION |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | DOS | Delay (s) | LOS | Queue <br> (m) | DOS | Delay (s) | LOS | Queue <br> (m) |
| South: Bourke Street | 0.501 | 9 | LOS A | 30 | 1.039 | 111 | LOS F | 296 |
| East: Urana Street | 0.478 | 7 | LOS A | 20 | 0.911 | 19 | LOS B | 140 |
| North: Bourke Street | 0.213 | 7 | LOS A | 10 | 0.375 | 7 | LOS A | 20 |
| West: Urana Street | 0.426 | 8 | LOS A | 17 | 0.621 | 16 | LOS B | 30 |
| Intersection | 0.501 | 8 | LOS A | 30 | 1.039 | 41 | LOS D | 296 |

Note, this assessment of intersection performance with construction and diverted vehicles is considered to be a worstcase assessment and it is expected that a proportion of vehicles would seek alternative routes to avoid the Bourke Street south approach, particularly for those trips that would travel on diversion routes but that do not cross the rail line. This potential redistribution of diverted vehicles would likely reduce the impact to intersection performance shown in Table 5.28 and distribute the impact of diversions more proportionally across the broader network.

Moreover, the assessment of a peak hour is not reflective of intersection performance across a day, which during off-peak periods, is likely to operate more optimally with lower vehicle volumes than seen during a peak hour. Furthermore, to provide a conservative assessment, peak construction vehicles have been assessed during the background peak hour, when peak construction vehicles are expected outside the background peak hour.
It should be noted that the diversionary period is temporary, and that LOS is expected to be restored to existing levels following the end of the diversionary period.

## URANA STREET / MACLEAY STREET INTERSECTION

Figure 5.26 shows the layout of the Urana Street/MacLeay Street intersection as modelled in SIDRA.


Figure 5.26
Urana Street/MacLeay Street SIDRA intersection layout
Table 5.29 shows the SIDRA results for the Urana Street/MacLeay Street intersection during a 2024 peak hour with and without diversions or construction vehicles. The results show that the intersection would operate at LOS A and with low levels of queuing and delay with and without construction and diverted vehicles. The increases in $95^{\text {th }}$ queue lengths do not extend into any adjacent intersections on Bourke Street or MacLeay Street.

Table 5.29
Urana Street/MacLeay Street, 2024 SIDRA analysis - AM Peak

\left.|  | 2024 AM PEAK HOUR |  |  |  | 2024 AM PEAK HOUR WITH |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CONSTRUCTION + DIVERSION |  |  |  |  |  |  |  |$\right]$

## LAKE ALBERT ROAD / RAILWAY STREET INTERSECTION

Figure 5.27 shows the layout of the Lake Albert Road/Railway Street intersection as modelled in SIDRA.


Figure 5.27 Lake Albert Road/Railway Street SIDRA intersection layout
Figure 5.28 shows the phasing modelled for the Lake Albert Road/Railway Street intersection in SIDRA. This phasing has been adopted in the with and without construction traffic to provide a comparative assessment of impacts.


Figure 5.28 Lake Albert Road/Railway Street SIDRA phasing
Table 5.30 shows the SIDRA results for the Lake Albert Road/ Railway Street intersection during a 2024 peak hour with and without construction and diversion vehicles.

The results show that the intersection LOS would increase from LOS B to LOS E, and average delay would increase by 51 seconds with the addition of construction and diversion vehicles. There would also be increases to queuing on all approaches with additional construction vehicles and diverted vehicles, particularly on Railway Street where $95^{\text {th }}$ percentile queues increase by almost 300 metres. The increases in $95^{\text {th }}$ queue lengths do not extend into any adjacent intersections on Lake Albert Street/ Railway Street.

Table 5.30
Lake Albert Street/ Railway Street, 2024 SIDRA analysis - AM Peak

|  | 2024 AM PEAK HOUR |  |  |  | 2024 AM PEAK HOUR WITH CONSTRUCTION + DIVERSION |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | DOS | Delay <br> (s) | LOS | Queue (m) | DOS | Delay (s) | LOS | Queue <br> (m) |
| South: Lake Albert Road | 0.738 | 18 | LOS B | 87 | 1.004 | 79 | LOS E | 239 |
| North: Lake Albert Road | 0.564 | 12 | LOS B | 23 | 0.914 | 31 | LOS C | 81 |
| West: Railway St | 0.748 | 29 | LOS C | 46 | 1.004 | 82 | LOS F | 345 |
| Intersection | 0.748 | 18 | LOS B | 87 | 1.004 | 69 | LOS E | 345 |

Note, this assessment of intersection performance with construction and diverted vehicles is considered to be a 'worstcase' and it is expected that a proportion of vehicles would seek alternative routes to avoid this congested intersection, particularly for those trips that would travel on diversion routes but that do not cross the rail line. This potential redistribution of diverted vehicles would likely reduce the impact to intersection performance shown in Table 5.30 and distribute the impact of diversions more proportionally across the broader network.

Moreover, the assessment of a peak hour is not reflective of intersection performance across a day, which during off-peak periods, is likely to operate more optimally with lower vehicle volumes than seen during a peak hour. Furthermore, to provide a conservative assessment, peak construction vehicles have been assessed during the background peak hour, when peak construction vehicles are expected outside the background peak hour.

Furthermore, as discussed in section 8.2 traffic mitigation measures will be put in place to reduce the impact of the diversions during this temporary period, including consideration of temporary changes to signal phasing to improve LOS.

It should be noted that the diversionary period is temporary, and that LOS is expected to be restored to existing levels following the end of the diversionary period.

## EDWARD STREET / LAKE ALBERT ROAD INTERSECTION

Figure 5.29 shows the layout of the Edward Street/Lake Albert Road intersection as modelled in SIDRA.


Figure 5.29
Edward Street/Lake Albert Road SIDRA intersection layout
Table 5.31 shows the SIDRA results for the Edward Street/Lake Albert Road intersection during a 2024 peak hour with and without construction and diversion vehicles. Other than the change of LOS from C to D on Edward Street, the results show that the intersection would operate with the same LOS (D) with and without construction and diversion vehicles. There are some increases to queuing and delay on all approaches.

Table 5.31 Edward Street/Lake Albert Road, 2024 SIDRA analysis - AM Peak

|  | 2024 AM PEAK HOUR |  |  |  | 2024 AM PEAK HOUR WITH CONSTRUCTION + DIVERSION |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | DOS | Delay (s) | LOS | Queue (m) | DOS | Delay (s) | LOS | Queue <br> (m) |
| South: Lake Albert Road | 0.71 | 36 | LOS D | 102 | 0.903 | 49 | LOS D | 178 |
| East: Edward Street | 0.65 | 33 | LOS C | 99 | 0.733 | 38 | LOS D | 109 |
| North: Tarcutta Street | 0.661 | 41 | LOS D | 61 | 0.691 | 41 | LOS D | 70 |
| West: Edward Street | 0.745 | 37 | LOS D | 119 | 0.841 | 45 | LOS D | 135 |
| Intersection | 0.745 | 36 | LOS D | 119 | 0.903 | 44 | LOS D | 178 |

Figure 5.30 shows the daily ( 24 hr ) vehicle profile of the Edmonson Street/Mitchelmore Street/Coleman Street intersection in Wagga Wagga. The daily profile has two distinctive peaks; 08:00-09:00 (AM peak) and 15:00-16:00 (PM peak).


Figure 5.30 Daily ( 24 hr ) traffic profile - Edmondson Street/Mitchelmore Street/Coleman Street intersection
The traffic profile is representative of a typical intersection in an urban environment. The AM peak aligns with typical travel to work and school drop off times and the PM peak aligns with typical school pick-up times. All intersections assessed for the Wagga Wagga diversion are located in the vicinity of this intersection. As such, the daily profile is considered representative of all daily traffic profiles within the Wagga Wagga diversionary area, including diverted vehicle volumes.

Figure 5.30 shows the hourly volumes between the AM and PM peaks are approximately 60 per cent of the peak hour volumes. Hourly volumes prior to the AM peak and post the PM peak rapidly diminish to relatively low volumes. Therefore, it is not expected that the levels of link and intersection performance shown during the peak hour (temporary) diversions would be experienced outside of the peak hours.

## TRAVEL TIME

Figure 5.31 shows that the western diversion would take approximately six minutes of additional travel time under existing road conditions. As shown in Table 5.27 and Table 5.28, with the proposed diversions and construction vehicles, there is a potential three minutes of additional delay along this route. As a result, the potential increase in travel time on the western diversion route is approximately nine minutes during the heaviest trafficked peak period. This additional travel time is a worst case scenario assuming an origin and destination immediately adjacent to the Edmondson Bridge closure. It is noted that outside of peak hours, intersection delay would be less, and that this assessment of additional diversion travel time represents a worst-case assessment.

Figure 5.32 shows that the eastern diversion would take approximately eight minutes of additional travel time under existing road conditions. As shown in Table 5.29 and Table 5.30, with the proposed diversions and construction vehicles, there is a potential one minute of additional delay along this route. As a result, the potential increase in travel time on the eastern diversion route is approximately nine minutes during the heaviest trafficked peak period. This additional travel time is a worst-case scenario assuming an origin and destination immediately adjacent to the Edmondson bridge closure. It is noted that outside of peak hours, intersection delay would be less, and that this assessment of additional diversion travel time represents a worst-case assessment.



| Proposal site $\quad$ Travel time impacts (distance, time delay) Existing railway Main road Local road Waterways Waterbodies |  |
| :---: | :---: |

## SUMMARY OF DIVERSION IMPACTS

The assessment of Edmondson Street bridge traffic diversions has shown that some intersections are significantly impacted, whilst others are not.

It should be noted that the assessment of intersection performance is a worst-case assessment, and it is expected that a proportion of vehicles would seek alternative routes away from significantly impacted intersections, particularly for residents of suburbs south of the rail line such as Tolland and Mount Austin who may divert via Red Hill Road or Kooringal Road to access the Sturt Highway. This potential redistribution of vehicles would likely reduce the effects of diversions on the most heavily impacted intersections and spread the impact more proportionally across the broader network. Furthermore, as noted in section 8.2 , consideration will be given to temporary changes to signal phasing at intersections along the traffic diversion routes, to mitigate performance impacts during the Edmondson Road bridge closure.

There are only a limited number of rail crossing opportunities in Wagga Wagga through which the diverted vehicles can cross the rail line, and as such these crossings will see an increase in traffic volume during the diversion period. Note that all rail crossings in Wagga Wagga that have not been assessed for diversion impacts are free-flowing infrastructure such as underpasses or overpasses and as such there will be no additional delay encountered at these rail crossings due to diverted traffic. Furthermore, the conservative approach to the road performance assessment of diversion routes (applying peak construction traffic numbers to peak background traffic numbers) has shown that most links in the study area perform acceptably during the diversion period.

Note, the assessment of a peak hour is not reflective of intersection performance across a day, which during off-peak periods is likely to operate more optimally with lower vehicle volumes than seen during a peak hour. Furthermore, following the end of the construction period, intersection performance will return to pre-construction levels.

## PARKING

Parking for construction workers and laydown areas for unloading of heavy vehicles at the Wagga Wagga Station precinct enhancement sites within the proposal site and so would have minimal impact to existing parking facilities.

During the nine-month closure of Edmondson Street, existing school drop off areas on Edmondson Street adjacent to Kildare Catholic College would remain viable as parents would be able to drop off their children and undertake a U turn movement at the closure on the east and west side of Edmondson Street controlled by onsite traffic management. Access to the Mt Erin Heritage Centre car park would be maintained during construction.

Parking on Edmondson Street between Edward Street and Erin Street is largely restricted and so the Edmondson Street closure would have minimal impact on parking in this area. The closure of Erin Street would remove approximately two kerbside parking spaces on Erin Street for the nine-month duration of closure of the Edmondson Street bridge. Informal parking on the verge of the eastern side and kerbside parking on the western side of Little Best Street will also be subject to temporary disruption during this period. Review of aerial imagery of the area suggests that demand for on-street parking would be relatively low in the surrounding streets, as residences in the area have space for private off-street parking, and there is kerbside parking capacity nearby to absorb the temporary parking losses.

Access to parking for the Multicultural Council of Wagga Wagga, located adjacent to the Wagga Wagga Railway Station will be closed for approximately two days for lifting of construction materials during the replacement of the Wagga Wagga Station pedestrian bridge (Mothers Bridge), as shown in section 5.3.9. Pedestrian access to the Multicultural Council of Wagga Wagga would be maintained under escort during this time. This impact is expected to be managed in consultation with stakeholders and in line with the TMP.

Expected parking impacts on key roads is detailed in Table 5.32.
No disabled parking spaces would be impacted by the proposal.

Table 5.32
Parking impacts - Wagga Station enhancement sites

| LOCATION | PARKING <br> TYPE | TIME OF DAY <br> RESTRICTIONS | EXPECTED IMPACTS | DURATION |
| :--- | :--- | :--- | :--- | :--- |
| Edmondson Street/ <br> Mitchelmore <br> Street | Kerbside parking <br> south of Erin <br> Street | School bus zones <br> $8 \mathrm{am}-9: 30 \mathrm{am} ;$ <br> $3 \mathrm{pm}-4 \mathrm{pm}$ | Impacts managed with <br> onsite traffic control | Nine months (duration of <br> Edmondson Street bridge <br> closure) |
| Little Best Street | Kerbside parking | No restrictions | Temporary disruption to <br> kerbside parking and <br> informal verge parking <br> Impacts managed with <br> onsite traffic control | Nine months (duration of <br> Edmondson Street bridge <br> closure) |
| Erin Street | Kerbside parking | No restrictions | Removal of approximately <br> two spaces | Nine months (duration of <br> Edmondson Street bridge <br> closure) |
| Station Place | Kerbside parking <br> Public commuter <br> carpark | Kerbside: 1P on Station | Access to local business <br> parking will be impacted by <br> construction activities | Approximately two days |

### 5.3.2.4 BOMEN YARD CLEARANCES ENHANCEMENT SITE

## ROAD PERFORMANCE

The link LOS assessment for the Bomen Yard clearances enhancement site component of the proposal is shown in Table 5.33. This assessment shows that with construction traffic all road links are expected to operate at LOS A or better, which is considered stable flow conditions as per the Guide to Traffic Generating Developments (RTA 2002).
Furthermore, the assessment shows no change in LOS as a result of the construction generated traffic and subsequently no significant impacts to road operation and performance are expected.

Table 5.33 Bomen Yard clearances enhancement site construction route road performance

| ROAD NAME | ROAD TYPE | 2024 PEAK HOUR |  | 2024 WITH CONSTRUCTION PEAK HOUR |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Volume - one way | LOS | Construction volume one way | Combined volume one way | LOS |
| Olympic Highway | Highway | 323 | A | 43 | 366 | A |
| Byrnes Road | Urban | 137 | A | 35 | 172 | A |
| Merino Drive - between Olympic and Dorsett | Urban | 54 | A | 35 | 89 | A |
| Merino Drive - between Byrnes and Dorsett | Urban | 123 | A | 35 | 158 | A |
| E Bomen Road ${ }^{1}$ | Urban | 31 | A | 35 | 66 | A |

(1) No data available, volumes estimated as average of Olympic Highway - Ashmont, 95065 and Olympic Highway The Rock, 9551
Note, construction peak hour volumes are higher on Olympic Highway than on the other roads under assessment as the road performance assessment for highways requires assessment of PCUs which effectively doubles the count of heavy vehicles required for construction.

## INTERSECTION PERFORMANCE

An assessment of the performance of the highest trafficked, on a per lane basis, construction route intersection in the Wagga Wagga precinct (excluding the Wagga Wagga Station and surrounds, which is assessed as part of the Edmondson Street bridge diversion assessment) during peak construction activities was undertaken for the Pearson Street bridge enhancement sites in section 5.3.2.2.

This assessment showed that the expected performance of the highest trafficked intersection in the precinct was LOS B, which is considered an acceptable LOS as per the Guide to Traffic Generating Developments (RTA 2002). Furthermore, the assessment shows no change in LOS as a result of the construction generated traffic and subsequently no significant impacts to intersection operation and performance are expected. Furthermore, $95^{\text {th }}$ queuing does not extend into any additional adjacent intersections as a result of the construction vehicles. As such, it is not considered that construction vehicles would impact the performance of any other lesser trafficked construction route intersection within the precinct. Therefore, with the exception of the Wagga Wagga Station enhancement sites Edmondson Street bridge closure diversion assessment, no additional construction route intersection analysis has been undertaken for the Wagga Wagga precinct enhancement sites.

## TEMPORARY CLOSURES AND DIVERSIONS

No road closures or diversions are proposed for the Bomen Yard clearances enhancement site.

## PARKING

Parking for construction workers and laydown areas for unloading of heavy vehicles at the Bomen Yard clearances enhancement site would be provided within the construction site area and so would have minimal impact to existing parking facilities. Any minor impacts to parking due to traffic control or site accesses on the local road network would be managed in line with the TMP.

No disabled parking spaces would be impacted by the proposal.

### 5.3.3 CONSTRUCTION SITE ACCESS

A turn warrant assessment for each enhancement site access in the Wagga Wagga precinct have been undertaken based on The Guide to Traffic Management - Part 6 Intersection, Interchanges and Crossings (Austroads 2020). This assessment has analysed a worst case scenario, assuming all peak generated construction traffic is distributed to each access during the road network peak period. The results of this assessment are shown in Table 5.34.
Table 5.34 Wagga Wagga precinct enhancement site access turn warrant assessment

| ENHANCEMENT SITE | ACCESS <br> NUMBER I <br> ROAD | ROAD <br> TYPE | ASSESSMENT OUTCOME (TURN TREATMENT) | CONSIDERATIONS |
| :---: | :---: | :---: | :---: | :---: |
| Uranquinty Yard clearances | 2 / Hanging <br> Rock Road | One lane two way | N/A ${ }^{1}$ | Through movement into site. <br> No opposing movements on public road. <br> Low speed environment ( $\leq 60 \mathrm{~km} / \mathrm{h}$ ). <br> Minimal impact to existing traffic movements expected. |
| Uranquinty Yard clearances | 3 / Olympic Highway* | Two-way | Channelised Right- <br> Turn/Basic Left-Turn | Left and right turn into and out of site. Opposing movements on public road. Current configuration does not meet turn warrant guidance, Road Safety Audit would investigate the need for traffic management of this access. |


| ENHANCEMENT <br> SITE | ACCESS <br> NUMBER <br> ROAD | ROAD <br> TYPE | ASSESSMENT <br> OUTCOME (TURN <br> TREATMENT) | CONSIDERATIONS |
| :--- | :--- | :--- | :--- | :--- |
| Uranquinty Yard <br> clearances | $1 /$ <br> Yarragundry <br> Street | Two-way | Basic Left-Turn/Basic <br> Right-Turn | Left and right turn into and out of site. <br> Opposing movements on public road. |
| Low speed environment ( $\leq 60 \mathrm{~km} / \mathrm{h})$. |  |  |  |  |


| ENHANCEMENT SITE | ACCESS <br> NUMBER / <br> ROAD | ROAD TYPE | ASSESSMENT OUTCOME (TURN TREATMENT) | CONSIDERATIONS |
| :---: | :---: | :---: | :---: | :---: |
| Wagga Wagga Station And surrounds | 8 / Fox/ <br> Donnelly <br> Avenue | Two-way | Basic Left-Turn/Basic Right-Turn | Left and right turn into and out of site. Opposing movements on public road. Low speed environment ( $\leq 60 \mathrm{~km} / \mathrm{h}$ ). Current configuration does not meet turn warrant guidance, Road Safety Audit would investigate the need for traffic management of this access. |
| Wagga Wagga Station And surrounds | 17 / <br> Edmondson <br> Street north | Two-way | N/A ${ }^{3}$ | Left and right turn into and out of site. Opposing movements on public road. <br> Low speed environment ( $\leq 60 \mathrm{~km} / \mathrm{h}$ ). Minimal impact to existing traffic movements expected. |
| Wagga Wagga Station And surrounds | 16 / <br> Edmondson <br> Street south <br> (Erin Street) | Two-way | N/A ${ }^{1}$ | Through movement into site. <br> No opposing movements on public road. <br> Low speed environment ( $\leq 60 \mathrm{~km} / \mathrm{h}$ ). <br> Minimal impact to existing traffic movements expected. |
| Wagga Wagga Station And surrounds | 11 and 18 / <br> Railway Street | Two-way | N/A ${ }^{1}$ | Through movement into site. <br> No opposing movements on public road. <br> Low speed environment ( $\leq 60 \mathrm{~km} / \mathrm{h}$ ). <br> Minimal impact to existing traffic movements expected. |
| Wagga Wagga Station And surrounds | 10 / Station Place | Two-way | N/A ${ }^{1}$ | Through movement into site. <br> No opposing movements on public road. <br> Low speed environment ( $\leq 60 \mathrm{~km} / \mathrm{h}$ ). <br> Minimal impact to existing traffic movements expected. |
| Wagga Wagga Station and surrounds | 73 / Docker Street (Chaston Street) | Two-way | N/A ${ }^{1}$ | Left turn into and out of site. ${ }^{2}$ <br> Opposing movements on public road. <br> Low speed environment ( $\leq 60 \mathrm{~km} / \mathrm{h}$ ). <br> Close proximity to existing intersection. <br> Potential for impacts from construction vehicles movements or implementation of traffic management. |


| ENHANCEMENT <br> SITE | ACCESS <br> NUMBER / <br> ROAD | ROAD <br> TYPE | ASSESSMENT <br> OUTCOME (TURN <br> TREATMENT) | CONSIDERATIONS |
| :--- | :--- | :--- | :--- | :--- |
| Bomen Yard <br> clearances | 19 / Station <br> Place | Two-way | Basic Left-Turn/Basic <br> Right-Turn | Left and right turn into and out of site. <br> Opposing movements on public road. <br> High speed environment ( $\geq 80 \mathrm{~km} / \mathrm{h}$ ). |
|  |  |  | Current configuration does not meet turn <br> warrant guidance, Road Safety Audit would <br> investigate the need for traffic management of <br> this access. |  |

(1) Turn warrant methodology not suitable for assessment due to access intersection configuration
(2) Cannot be right turn in, right turn out
(3) Existing traffic to be diverted, auxiliary lanes already in place at signalised intersection

Basic Right-Turn and Auxiliary Left-Turn / Channelised Right-Turn / Channelised Left-Turn treatments are required by the intersection turn warrant assessment for some site accesses in this precinct. However, this may not be required given the temporary nature of accesses during the construction phase and the conservative nature of the assessment (peak construction vehicles assessed during the background peak hour, when peak construction vehicles are expected outside the background peak hour).

Where the turn warrant assessment methodology is unsuitable for the assessment of the enhancement site access the access arrangements as per the current road network would not have a significant impact as they are either a through movement from the end of a street, or they are impacting limited traffic movements.

The accesses off Cheshire Street to the Pearson Street bridge enhancement site, and the access off Chaston Street to the Wagga Wagga Yard clearances enhancement site require special consideration due to their proximity to adjacent intersections (Pearson Street/Cheshire Street and Docker Street/Chaston Street, respectively). It is recommended that these accesses be designated as left in, left out turning movements only to limit any performance or safety impacts to the surrounding road network.

More detailed assessment of the accesses will be undertaken as part of the Road Safety Audits and appropriate Construction Traffic Transport and Access Management Plans will be developed by the contractor prior to commencement of construction activities on site to moderate any potential safety issues. Design of any access treatments or modifications to roads would be undertaken in accordance with appropriate design standards and with approvals from the relevant local or state road authorities. Works Authorisation Deeds or other suitable consent or agreement with TfNSW will be made prior to undertaking any relevant works on a State Controlled Road.

### 5.3.4 ROAD SAFETY

During construction there would be changes to road conditions within the Wagga Wagga precinct consisting of increased traffic volumes due to construction vehicles, temporary diversions and new access points to the enhancement sites from the public road network. This study has primarily considered the operation and capacity of the road network rather than the appropriateness of use of certain roads by construction vehicles. The suitability of access and diversion routes has not been assessed with respect to road safety.

It is noted that the construction activities at Uranquinty Yard clearances, Pearson Street bridge. Wagga Wagga Yard clearances and Bomen Yard clearances enhancement sites within the Wagga Wagga precinct, are expected to generate relatively low volumes of traffic, and an appropriate LOS is maintained on all of these enhancement site access routes as discussed in section 5.3.2. Access intersections to the enhancement sites within the Wagga Wagga precinct would be designed or have traffic control measures implemented to provide suitable safe access to public roads in accordance with relevant standards and guidelines.

Construction vehicles at Cassidy Parade pedestrian bridge, Edmondson Street bridge and Wagga Wagga Station pedestrian bridge are not expected to create significant impacts. However, the traffic diversions in place for the Edmondson Street bridge enhancement site bridge closure re-routes vehicles crossing the rail line on Edmondson Street via Lake Albert and Docker Streets, significantly increasing the traffic volumes on the diversion routes as discussed in section 5.3.2.3. Traffic management for these diversion routes would be provided for safe movements along public roads in accordance with relevant standards and guidelines. It is noted that the additional traffic on these routes impact the link and intersection LOS to LOS E and F which does not meet stable flow conditions or the acceptable performance standard, respectively.

To moderate any construction impacts to existing or potential safety issues associated with either construction vehicle movements or the additional traffic on local roads from diversions, Road Safety Audits and Construction Traffic Transport and Access Management Plans would be required to be undertaken by the contractor prior to commencement of construction activities on site or the implementation of diversionary routes and the safety of all road users should be taken into account.

### 5.3.5 HEAVY VEHICLE ROUTES

There are no changes to background LOS resulting from the traffic generated by the construction activities at these enhancement sites enhancement sites and it is not expected that construction heavy vehicle and workforce movements generated by the proposal, as shown in section 5.3.1.3, would impact the current operations of existing heavy vehicles movements on the routes detailed in section 4.5.3.

During the Edmondson Street closure diversion period, although no heavy vehicle routes will be directly affected by road closures, additional diverted traffic is expected on the following heavy vehicle routes:

- Sturt Highway
- Lake Albert Road.

The additional traffic at the Docker Street/Edwards Street and Lake Albert Road/Edward Street intersections is expected to increase average delay by one minute during a peak period, as shown in Table 5.27 and Table 5.30 respectively, which is not considered a significant impact to the heavy vehicle route passing though these intersections. Lake Albert Road and the Sturt Highway are not expected to be significantly impacted by the increased traffic volumes resulting from the diversion traffic. However, there may be minor delays to heavy vehicles from reduced speed limits and traffic control. Construction Traffic Transport and Access Management Plans would be developed to ameliorate impacts to safe and efficient travel of heavy vehicles through this diversionary route.

There is potential for construction heavy vehicles to impact road pavement conditions along haul routes. To determine the extent of the impact a road dilapidation report will be prepared for all haul routes within the precinct.

### 5.3.6 TRAVELLING STOCK RESERVES

Travelling Stock Reserves are located along the proposed construction access routes for the Uranquinty Yard clearances enhancement site, and a Livestock Highway on Bourke Street in Wagga Wagga, a diversion route during the Edmondson Street bridge closure.

Based on the low traffic volumes generated by the construction activities in Uranquinty it is not expected that heavy vehicle and workforce movements would impact the operation of the Travelling Stock Reserves here. It is noted that the additional construction traffic does not result in a change of LOS on any of the construction access routes for the Uranquinty Yard clearances enhancement site.

It is expected that prior to the commencement of this traffic diversion Local Land Services should be notified of increased vehicle movements along the TSR through Uranquinty and the Livestock Highway on Bourke Street during the construction phase to advise stock handlers, including walking permit holders, of potential impacts.

### 5.3.7 PUBLIC TRANSPORT ROUTES

### 5.3.7.1 ROAD

Construction vehicle movements are expected to have a minimal impact on the operation of bus services or bus stops along construction access routes due to the low traffic volumes generated by the construction activities (which do not result in a change in LOS from current operation) for the following enhancement sites:

- Uranquinty Yard clearances
- Pearson Street bridge
- Cassidy Parade pedestrian bridge
- Wagga Wagga Station pedestrian bridge
- Wagga Wagga Yard clearances
- Bomen Yard clearances.

It is noted that the heaviest period of construction workforce movements at the start and end of construction hours (6am to 6 pm ) outside peak bus service periods (e.g. school times). Other routes on the detour roads may be affected by additional diversion traffic on these roads and impacted performance at intersections. Average delays at impacted intersections will increase by one minute or less. There may be minor delays to buses passing near the enhancement sites from reduced speed limits and traffic control. These impacts would be managed in accordance with the traffic management plan to ameliorate impacts to the safe and efficient travel of bus services through the affected areas. The closure of Edmondson and Erin Streets for a nine-month period as part of the Edmondson Street bridge enhancement site and the associated changes to road network connectivity is expected to directly impact the operation of public and school bus services bus services in the area through delays, as well as direct impact to the routes and existing bus stops. These impacts are detailed in Table 5.35 and Table 5.36.

Table 5.35 Public bus route impacts - Wagga Wagga precinct

| SERVICE | IMPACT |
| :--- | :--- |
| Route 1W - Coolamon via | -Directly impacted by the Edmondson Street bridge closure, would require <br> rerouting and alternative stops (Kildare Catholic College / 2650107 and <br> Downside, Route 930 - Ganmain |
|  | 265098) or stopping patterns during the closure period. |


| BUS ROUTE | IMPACT |
| :---: | :---: |
| S100 - Mount Austin Public School <br> S120 - Wagga Wagga High School <br> S122 - Gobbagombalin <br> S123 - South Wagga Primary School <br> S150 - The Riverina College <br> S159 - Ashmont <br> S171 - South Wagga Primary School <br> S179 - South Wagga Primary School <br> S199 - North Wagga Wagga <br> S210 - Marrar, S215 - Lockhart <br> S216 - Currawarna <br> S243 - Wagga to Gundagai <br> S188 - North Wagga Primary School <br> S203 - TRAC to Lloyd <br> S197 - Estella to Wagga Wagga High School <br> S191 - The Riverina Anglican College to <br> Kooringal via Uranquinty <br> S185 - South Wagga Wagga Primary to Estella <br> S173 - North Wagga Wagga Primary to Henschke Primary, S172 - Wagga Wagga Primary to Tarcutta <br> S167 - Estella to Lake Albert Primary <br> S162 - Glenfield Park to Kildare <br> S149 - The Riverina Anglican College to <br> Mangoplah <br> S144 - Estella to Turvey Park Primary <br> S134 - North Wagga Wagga to Wagga Wagga Primary <br> S124 - Wagga Wagga Primary to Ashmont via The Rock | - Directly impacted by Edmondson Street and Erin Street closures as part of Edmondson Street bridge Closure, would require rerouting and alternative stops (Kildare Catholic College / 2650107 and 265098) or stopping patterns during the closure period. |
| S103 - South Wagga Primary | - Directly impacted by Edmondson Street and Erin Street closures as part of Edmondson Street bridge Closure, would require rerouting and alternative stops (Kildare Catholic College / 2650107 and 265098) or stopping patterns during the closure period. <br> - Impact to train station connectivity for patrons during pedestrian bridge replacement works. <br> - May require temporary stop location (Railway Street at Collins Street / 2650305 \& 265073) during footpath works on Railway Street. |


| BUS ROUTE | IMPACT |
| :---: | :---: |
| $\begin{aligned} & \text { S109 - Wagga Wagga Primary } \\ & \text { S121 - South Wagga Primary } \\ & \text { S138 - Forest Hill } \\ & \text { S163 - Wagga Wagga Primary } \\ & \text { S190 - Uranquinty to Wagga Wagga Primary } \end{aligned}$ | - Impact to train station connectivity for patrons during pedestrian bridge replacement works. <br> - May require temporary stop location (Railway Street at Collins Street / 2650305 \& 265073) during footpath works on Railway Street. |
| S126 - Lake Albert, S187 - Gumly Gumly <br> S196 - Ladysmith | - Directly impacted by Edmondson Street and Erin Street closures as part of Edmondson Street bridge Closure, would require rerouting and alternative stops (Kildare Catholic College / 2650107 and 265098) or stopping patterns during the closure period. |
| $\begin{aligned} & \text { S129 - Glenfield Park } \\ & \text { S250 - San Isidore } \\ & \text { S130 - Mater Dei College } \\ & \text { S143 - South Wagga Wagga Primary } \end{aligned}$ | - Directly impacted by Edmondson Street and Erin Street closures as part of Edmondson Street bridge Closure, would require rerouting and alternative stops (Kildare Catholic College / 2650107 and 265098) or stopping patterns during the closure period. <br> - Impact to train station connectivity for patrons during pedestrian bridge replacement works. <br> - May require temporary stop location (Railway Street at Collins Street / 2650305 \& 265073) during footpath works on Railway Street. |
| S148 - Holy Trinity Primary S155 - South Wagga Wagga S151 - Forest Hill S174 - Forest Hill to Wagga Wagga High | - Directly impacted by Erin Street closures as part of Edmondson Street bridge Closure, would require rerouting and alternative stops/stopping patterns during the closure period. <br> - Impact to train station connectivity for patrons during pedestrian bridge replacement works. <br> - May require temporary stop location (Railway Street at Collins Street / 2650305 \& 265073) during footpath works on Railway Street. |

Changes to bus routes and bus stops to mitigate these impacts, including establishing temporary stops, would need to be planned in consultation with the relevant stakeholders to minimise the impact on community, public transport users, and service providers.

### 5.3.7.2 RAIL

Construction activities requiring possessions would occur during either:

- existing scheduled weekend rail corridor possession periods (typically 72 hours) when trains along the rail corridor are stopped for maintenance as part of operation of the existing rail line; or
- track work authorisations periods, which enable works that impact rail operations to occur outside scheduled rail possessions, but within available 9-hour windows in which train services are not scheduled.

Work during these periods would be undertaken in consultation with passenger rail operators. However, it is not expected that proposal construction works would impact upon the rail services and train station platforms will not be impacted by the enhancement sites. Impacts to pedestrian access to the Wagga Wagga Station are discussed in the following section.

### 5.3.8 ACTIVE TRANSPORT ROUTES

As shown in section 4.5.6, provision of infrastructure for active transport in the vicinity of the Uranquinty and Bomen Yard Clearance enhancement sites is minimal, and given the surrounding land uses the demand for cycling and pedestrian travel in the area is likely to be low. Footpaths are provided on key roads in the vicinity of the Pearson enhancement site with minimal provision of dedicated cycling infrastructure on key roads. Although there would be increased traffic from construction vehicles in the vicinity of these enhancement sites, there is expected to be a minimal impact to active transport movements as there is no change in LOS expected as a result of construction generated traffic. There may be minor disruptions to cyclists using roads near access points to these enhancement sites as a result of reduced speed limits and traffic management. It is noted that during the Edmondson Street bridge closure, additional traffic would be diverted to the surrounding road network impacting the LOS of road links and intersections. These impacts, although expected to be minimal to active transport movements, would be managed in accordance with the TMP.

Dedicated cycling infrastructure is provided on some key roads in the vicinity of the Wagga Wagga Station and surrounds. Although there would be increased traffic from construction vehicles in the vicinity of these enhancement sites the increase is minor with no change in LOS expected as a result of construction generated traffic.

The closures of the Wagga Wagga Station pedestrian bridge (Mothers Bridge), Cassidy Parade pedestrian bridge, and Edmondson Street bridge would impact active transport connectivity to transport facilities (bus stops and the Wagga Wagga Railway Station) and land uses in the surrounding area. The additional distance and travel time to cross the rail line during construction of each of the bridges is shown below in Table 5.37. The distances reflect a trip to reach each side of a closed bridge via the nearest rail crossing and represents a worst-case scenario for active transport impact as actual distance would vary by individual origin and destination. Paved pedestrian footpaths provide full connectivity between each of the crossing points shown in the table.

The Edmondson Street bridge, Wagga Wagga Station pedestrian bridge (Mothers Bridge), and Cassidy Parade pedestrian bridge closures are not scheduled to all close simultaneously and so pedestrian connectivity is maintained in this area via at least one of these three bridges, throughout the construction activities in the Wagga Wagga Station and surrounds enhancement sites. During closure of the Cassidy Parade pedestrian bridge, diversion via the Bourke/Docker Street level crossing would also be possible.

Table 5.37 Bridge closure active transport impacts -Wagga Station and Surrounds

| EXISTING CROSSING POINT | DURATION OF CLOSURE | NEW CROSSING POINT | DISTANCE / TIME |
| :---: | :---: | :---: | :---: |
| Cassidy Parade pedestrian bridge | 6 months | Wagga Wagga Station pedestrian bridge (Mothers Bridge) | Walking: $2 \mathrm{~km} / 26$ minutes <br> Cycling: 2km / 8 minutes |
|  |  | Bourke/Docker Street level crossing | Walking: $1.8 \mathrm{~km} / 22$ minutes <br> Cycling: $1.8 \mathrm{~km} / 7$ minutes |
| Edmondson Street bridge | 9 months | Cassidy Parade pedestrian bridge | Walking: 1.6km / 20 minutes Cycling: 1.6km / 7 minutes |
|  |  | Wagga Wagga Station pedestrian bridge (Mothers Bridge) | Walking: $850 \mathrm{~m} / 10$ minutes Cycling: $850 \mathrm{~m} / 3$ minutes |
| Wagga Wagga Station pedestrian bridge (Mothers Bridge) | 6 months | Edmondson Street bridge | Walking: 850m / 10 minutes Cycling: 850m / 3 minutes |

The Cassidy Parade pedestrian bridge is an existing link in the Wagga Wagga Active Travel Plan. The proposed bridge design includes a ramp on the southern side of the rail corridor. Discussions are ongoing with Wagga Wagga City Council to align plans and minimise potential impacts on the final configuration of the future infrastructure.

### 5.3.9 PROPERTY ACCESS IMPACTS

Some impacts to property access are expected as a result of the implementation of the Wagga Wagga Station and surrounds enhancement sites as shown in Figure 5.33.

As shown in Figure 5.33 the driveway from Station Place that gives access to the Multicultural Council of Wagga Wagga at the Wagga Wagga Station pedestrian bridge enhancement site would be used for construction activities and would require temporary closure for up to two days.

The driveway of one residential property located on Erin Street but accessed via Railway Street will be impacted, however, it is expected that this would be intermittent in response to construction activities and alternative arrangements for access would be provided for the duration of construction. Other accesses to residential properties in this area are located outside the expected construction impact zone and would not be impacted. It is expected that pedestrian access to the residential properties would be maintained during construction

It is expected that access to properties along Little Best Street would be maintained and that residents would continue to have the option of using private off-street parking, as described in section 5.3.2.3.

The proposal will utilise the Mt Erin Heritage Centre driveway off Edmondson Street for access to the Edmondson Street bridge enhancement site. This access arrangement would need to be undertaken in consultation with Mt Erin Heritage Centre. It is expected that access to the Mt Erin Heritage Centre would be maintained through the duration of construction.

Impacts to accesses for private residences and businesses would be minimised in consultation with relevant stakeholders and managed in line with the TMP.


| Proposal site <br> Existing railway | $\diamond$ Site access points Construction area | JUNEE FILLABO |
| :---: | :---: | :---: |
| Main road | $\square$ Proposed lift pad | lockhart wagga wagga |
| Local road | Proposed laydown |  |
| Multicultural Council of Wagga Wagga | Proposed laydown and site access compound | - HOLBROOK |
| Informal parking |  | HomLong |

## INLAND <br> RAIL $=$

### 5.3.10 RAIL FREIGHT

Section 5.3.7.2 notes when construction activities requiring possessions will occur.
Work during these periods would be undertaken in consultation with freight operators. However, it is not expected that proposal construction works would impact upon the rail freight network. Note, there are no other impacts to freight operations.

### 5.3.11 EMERGENCY VEHICLE ACCESS

Construction of the proposal would result in temporary impacts to traffic and an increase in vehicle movements on the road network. As shown in the link and intersection performance assessments, there is no significant impact to the performance of the road network due to the construction generated traffic within the Wagga precinct except for the Edmondson Street bridge diversions. There is not expected to be a significant impact to emergency vehicles movements for the following enhancement areas:

- Uranquinty Yard clearances
- Pearson Street bridge
- Cassidy Parade pedestrian bridge
- Wagga Wagga Station pedestrian bridge
- Wagga Wagga Yard clearances
- Bomen Yard clearances.

As a result of the closure of the Edmondson Street bridge and the increase in vehicle movements on the diversionary route, emergency vehicles may incur some additional travel time. The maximum theoretical increase in delay was calculated at nine-minutes in the AM peak period for a trip originating from Best Street with a destination at Erin Street. This is a highly unlikely origin and destination for emergency services and so this level of delay would be highly unlikely to occur, noting that emergency services would also be able to use Coleman Street rather than Urana to shorten the distance. The actual additional travel time experienced when responding to an emergency would vary depending on the origin and destination of the emergency services vehicles, noting that emergency vehicles have priority right of way and should incur less delay at intersections than general traffic.

From Fire and Rescue NSW Wagga Wagga on The Esplanade, responding to an emergency on Erin Street would incur up to an additional 3.5 minutes due to a combination of additional distance travelled and road congestion. For the same emergency from the Wagga Wagga Base Hospital, the additional delay due to the diversions would be expected to be minimal, if any. A Traffic and Access Management Plan will be developed in consultation with TfNSW, Wagga Wagga City Council, and State emergency services and would consider and effectively manage any impacts to emergency vehicles seeking to use roads in the vicinity of the enhancement sites or diversion routes.

### 5.3.12 SEASONAL VARIATION

Temporary local events such as festivals, shows, and markets may result in minor localised traffic variations, particularly in urban environments such as Wagga Wagga. The Uranquinty and Bomen enhancement sites are less urbanised than Wagga Wagga, featuring more rural and agricultural land uses.

Localised seasonal traffic variation may be experienced at enhancement sites that share land with agricultural infrastructure (grain silos, livestock loading facilities etc.) as the infrastructure will likely generate additional heavy or farm vehicle movements during harvest seasons as discussed in section 4.2.2.

A review of aerial imagery of enhancement sites in the Wagga Wagga precinct identified agricultural infrastructure such as grain silos or livestock loading facilities in the vicinity of the following enhancement sites:

- Uranquinty Yard clearances
- Bomen Yard clearances.

However, it is not anticipated that seasonal variation would significantly impact the outcomes of the traffic assessment as background and construction vehicle traffic volumes are low.

More detailed assessment of the enhancement site accesses, which would consider seasonal variation due to social events and agricultural movements, will be undertaken by the contractor prior to commencement of construction activities on site. These would include Road Safety Audits and appropriate Construction Traffic Transport and Access Management Plans to moderate any potential safety issues.

### 5.4 JUNEE PRECINCT

### 5.4.1 CONSTRUCTION PROFILE

This section outlines the construction profile for the proposal within the Junee precinct. This includes all vehicle routes, as shown in section 5.4.1.2, and all volumes of heavy and light vehicles required for construction of the proposal, as shown in section 5.4.1.3, which includes the vehicles required for the import and export of fill material. It also outlines other construction requirements, such as temporary road closures and diversions, and parking requirements for each enhancement site.

### 5.4.1.1 CONSTRUCTION PROGRAM

Key construction stages and work durations at each enhancement site within the Junee precinct are summarised below in Table 5.38 and Figure 5.34.

Table 5.38 Summary of construction stages - Junee enhancement sites

| ENHANCEMENT SITES | CONSTRUCTION STAGES UNDERTAKEN | START | FINISH | DURATION OF WORKS (MONTHS) | RAIL POSSESSION REQUIRED |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Harefield Yard clearances | - Site establishment <br> - Track realignment ( $>300 \mathrm{~mm}$ and/or track formation replacement) <br> - Gantry removal <br> - Demobilisation and landscaping | 1 February 2024 | 2 April 2024 | 2 | Yes |
| Kemp Street bridge | - Site establishment <br> - Traffic diversion works <br> - Road bridge replacement <br> - Demobilisation and landscaping | 1 February 2024 | 14 November 2024 | 10 | Yes |
| Junee Station pedestrian bridge | - Site establishment <br> - Pedestrian bridge removal or relocation works <br> - Demobilisation and landscaping | 1 February 2024 | 14 March 2024 | 1 | Yes |
| Junee Yard clearances | - Site establishment <br> - Track realignment ( $>300 \mathrm{~mm}$ and/or track formation replacement) <br> - Gantry removal <br> - Demobilisation and landscaping | 1 February 2024 | 2 April 2024 | 2 | Yes |


| ENHANCEMENT SITES | CONSTRUCTION STAGES UNDERTAKEN | START | FINISH | DURATION OF WORKS (MONTHS) | RAIL POSSESSION REQUIRED |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Olympic Highway underbridge | - Site establishment <br> - Track realignment ( $<300 \mathrm{~mm}$ ) <br> - Rail bridge track work <br> - Demobilisation and landscaping | 15 January 2024 | 3 April 2024 | 3 | Yes |
| Junee to Illabo clearances | - Site establishment <br> - Track realignment <br>  $(<300 \mathrm{~mm})$ <br> - Track realignment <br>  $(>300 \mathrm{~mm}$ and $/ \mathrm{or}$ <br>  track formation <br>  replacement $)$ <br> - Level crossing <br>  modification <br> - Extension or <br>  replacement of <br>  culverts <br> - Demobilisation and <br>  landscaping | 15 January 2024 | 6 November 2024 | 10 | Yes |



Figure 5.34 Junee precinct construction programme

### 5.4.1.2 CONSTRUCTION AND DIVERSION ROUTES

Proposed construction routes and diversion routes for each work site in the Junee precinct are shown in Figure 5.35 to Figure 5.38.

Vehicle and pedestrian diversions proposed within the Junee precinct during construction are:

- Kemp Street bridge
- Kemp Street bridge traffic diverted via Joffre Street, Pretoria Avenue, Seignior Street, Lorne Street, Ducker Street, Hill Street, George Street, and Edgar Street
- local access to Railway Lane and Railway Parade would be via Harold Street and Thomas Street
- Junee to Illabo clearances
- upgrade of private and public level crossings. Access will be managed with local traffic control and sidetracking, with minor diversions required.

Construction routes have been selected to minimise the use of local roads where possible. However, use of local roads is generally required to facilitate access to enhancement sites. As shown in section 5.4.1.3, construction vehicle volumes using construction routes and accesses on local roads are generally low.

Diversion routes have been selected on roads of the same order where possible. In the instances where diversion routes have been required on roads of a lower order, the requirement for mitigation has been considered.

Mitigations for the use of all road types, including local roads are provided in section 8.2. In addition, mitigation measures have been identified for other assessments, including noise and vibration, visual and social, to address potential impacts from the use of construction and diversion routes.

Where diversions are required for active travel routes, the selected diversion route has considered where pedestrian infrastructure is present. Where cyclists utilise diversion routes, and an existing cycle or shared path is not present, cyclists would be required to cycle on-road. To facilitate access to the rail corridor and surrounds for construction vehicles, including surrounding residences, diversion of pedestrians and cyclists within the proposal site would also be required. Detailed consideration of the management of pedestrian and cyclist safety within the proposal site will be completed prior to and during construction. Mitigation measures, including the requirements for a Traffic Management Plan (TMP), are provided in section 8.2.





Figure 5.38 Construction routes, diversions and site accesses (Junee to Illabo clearances)


### 5.4.1.3 VEHICLE TYPE AND QUANTITY

Table 5.39 shows the peak hour two-way movements at each enhancement site as identified from construction scenario data shown in Chapter 8: Construction of the proposal of the EIS.

Table $5.39 \quad$ Peak hour construction movements - Junee Work precinct enhancement sites

| ENHANCEMENT SITES | VEHICLE TYPES | PEAK HOUR MOVEMENTS | CONSTRUCTION VEHICLE PARKING AND LAYDOWN |
| :---: | :---: | :---: | :---: |
| Harefield | Light Vehicle | $47^{1}$ in (am) / out (pm) | Internal to Proposal site |
|  | Heavy Vehicle | 8 |  |
| Kemp Street bridge | Light Vehicle | $20^{1}$ in (am) / out (pm) | Internal to Proposal site |
|  | Heavy Vehicle | 8 |  |
| Junee Station pedestrian bridge | Light Vehicle | 7 in (am) / out (pm) | Internal to Proposal site |
|  | Heavy Vehicle | 1 |  |
| Junee Yard clearances | Light Vehicle | $23^{1}$ in (am) / out (pm) | Internal to Proposal site |
|  | Heavy Vehicle | 8 |  |
| Olympic Highway underbridge | Light Vehicle | $53^{1}$ in (am) / out (pm) | During possession peak some on-street parking may be utilised |
|  | Heavy Vehicle | 8 |  |
| Junee to Illabo clearances | Light Vehicle | $60^{2}$ in (am) / out (pm) | During possession peak some on-street parking may be utilised |
|  | Heavy Vehicle | 8 |  |

(1) Three-day possession peak (typically only 13 vehicle movements in a peak period)
(2) Three-day possession peak (typically only 20 vehicle movements in a peak period)

### 5.4.2 ROAD NETWORK OPERATION

### 5.4.2.1 HAREFIELD YARD CLEARANCES ENHANCEMENT SITE

## ROAD PERFORMANCE

The link LOS assessment for the Harefield Yard clearances enhancement site component of the proposal is shown in Table 5.40. This assessment shows that with construction traffic all road links are expected to operate at LOS B or better, which is considered stable flow conditions and an acceptable LOS as per the Guide to Traffic Generating Developments (RTA 2002). Furthermore, the assessment shows no change in LOS as a result of the construction generated traffic and subsequently no significant impacts to road operation and performance are expected.

Table 5.40
Harefield, construction route road performance

| ROAD | 2024 PEAK HOUR |  | 2024 WITH CONSTRUCTION PEAK HOUR |  |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: |
| Road name | Road type | Volume - one <br> way | LOS | Construction <br> volume - one <br> way | Combined <br> volume - one <br> way | LOS |
| Harefield Road | Rural | 9 | B | 28 | 37 | B |
| Byrnes Road $^{1}$ | Rural | 146 | B | 28 | 174 | B |
| Harefield <br> Railway Access <br> Road $^{2}$ | Rural | 135 | B | 28 | 163 | B |

(1) Byrnes Road, north of Harefield Road
(2) No data available, traffic volume estimated based on road type and surrounding land uses

## INTERSECTION PERFORMANCE

An assessment of the performance of the expected highest trafficked (on a per lane basis) construction route intersection in the Junee precinct was undertaken for the Junee Station and surrounds. This assessment is presented in section 5.4.2.2. The intersection assessment assessed combined peak hour construction traffic in conjunction with peak hour diversion and background traffic as a worst-case scenario for construction movements as expected construction start and finish times end outside of typical peak periods.

This assessment showed that the expected performance of the highest trafficked intersection in the precinct was LOS A, which is considered an acceptable LOS as per the Guide to Traffic Generating Developments (RTA 2002). Furthermore, the assessment shows no change in LOS as a result of the construction and diversion generated traffic and subsequently no significant impacts to intersection operation and performance are expected. As such, it is not considered that construction vehicles would impact the performance of any other lesser trafficked construction route intersection within the precinct. Therefore, no additional construction route intersection analysis has been undertaken for the Harefield Yard clearances enhancement site.

## TEMPORARY CLOSURES AND DIVERSIONS

No road closures or diversions are proposed for the Harefield site.

## PARKING

Parking for construction workers and laydown areas would be provided for unloading of heavy vehicles at the Harefield Yard clearances enhancement site within the construction site area and so would have minimal impact to existing parking facilities. There may be minor isolated impacts to parking due to traffic control and the increase of heavy vehicles on the local road network, which would be managed in line with the TMP.

No disabled parking spaces would be impacted by the proposal.

### 5.4.2.2 JUNEE STATION AND SURROUNDS

The enhancement sites in the vicinity of the Junee Station share the same road network and have been combined in the following section, for:

- Kemp Street bridge enhancement site
- Junee Station pedestrian bridge enhancement site
- Junee Yard clearances enhancement site.


## ROAD PERFORMANCE

The link LOS assessment for construction traffic from the combined Junee Station and surrounds enhancement sites component (occurring concurrently and utilising the same construction access routes) of the proposal is shown in Table 5.41. This road performance assessment excludes road links expected to be used as diversion routes during the Kemp Street Bridge closure (addressed within the Kemp Street bridge closure diversion assessment for cumulative construction and the diversion traffic).

This assessment shows that with construction traffic all road links are expected to operate at LOS B or better, which is considered stable flow conditions as per the Guide to Traffic Generating Developments (RTA 2002).

The assessment shows a change in LOS as a result of the construction generated traffic on the Olympic Highway Level Crossing from LOS A to LOS B. However, it is noted that the forecast traffic volume was approaching the upper limit of the LOS A band, LOS B still represents stable traffic flow with drivers having reasonable freedom to choose their desired speed and, that the change does not suggest that a significant impact to road operation and performance is expected.

Table 5.41 Junee Station and surrounds enhancement sites construction route road performance

| ROAD NAME | ROAD TYPE | 2024 PEAK HOUR VEHICLES ONE WAY |  | 2024 PEAK HOUR WITH CONSTRUCTION VEHICLES ONE WAY |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Volume | LOS | Construction volume | Combined volume | LOS |
| Olympic Highway (west of Seignior Street) ${ }^{1}$ | Highway | 212 | A | 45 | 257 | A |
| Seignior Street ${ }^{1}$ | Urban | 235 | B | 36 | 271 | B |
| Broadway Street ${ }^{1}$ | Urban | 291 | B | 36 | 327 | B |
| Olympic Highway Level Crossing ${ }^{1}$ | Urban | 198 | A | 36 | 234 | B |
| Humphrys Street ${ }^{2}$ | Urban | 99 | A | 36 | 135 | A |
| Main Street (Olympic Highway) ${ }^{2}$ | Urban | 99 | A | 36 | 135 | A |
| Lorne Street | Urban | 136 | A | 36 | 172 | A |
| Hill Street ${ }^{3}$ | Urban | 54 | A | 36 | 90 | A |
| Joffre Street ${ }^{4}$ | Urban | 24 | A | 36 | 60 | A |
| Harold Street ${ }^{5}$ | Urban | 68 | A | 36 | 104 | A |
| Thomas Street ${ }^{6}$ | Urban | 18 | A | 36 | 54 | A |
| Railway Lane ${ }^{1}$ | Urban | 24 | A | 36 | 60 | A |
| Railway Parade ${ }^{7}$ | Urban | 24 | A | 36 | 60 | A |
| George Street ${ }^{8}$ | Urban | 37 | A | 36 | 73 | A |
| Edgar Street | Urban | 79 | A | 36 | 115 | A |


| ROAD NAME | ROAD TYPE | 2024 PEAK HOUR VEHICLES ONE WAY |  | 2024 PEAK HOUR WITH CONSTRUCTION VEHICLES ONE WAY |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Volume | LOS | Construction volume | Combined volume | LOS |
| Byrnes Road | Urban | 140 | A | 36 | 176 | A |
| Pretoria Avenue ${ }^{6}$ | Urban | 18 | A | 36 | 54 | A |

(1) Traffic survey volumes
(2) No data available, volumes estimated as $50 \%$ of Olympic Highway Level Crossing 10-hour
(3) No data available, volumes estimated as $40 \%$ of Lorne Street
(4) No data available, volumes estimated as Crawley Street
(5) No data available, volumes estimated as $50 \%$ of Lorne Street
(6) No data available, volumes estimated as $75 \%$ of Joffre Street
(7) No data available, volumes estimated as Railway Lane
(8) No data available, volumes estimated as $60 \%$ of the difference between Byrnes Road and Edgar Street

Note, construction peak hour volumes are higher on Olympic Highway than on the other roads under assessment as the road performance assessment for highways requires assessment of PCUs which effectively doubles the count of heavy vehicles required for construction.

## INTERSECTION PERFORMANCE

SIDRA intersection analysis was undertaken as a component of the diversion assessment associated with the Kemp Street bridge Closure to assess the cumulative impact of diverted vehicles and construction vehicles to intersection performance in Junee.

As vehicle diversions are proposed to occur over the majority of the construction period in this area, it has not been deemed necessary to assess the impact of solely construction vehicles on intersection performance during the limited period of time when diversions would not be in place. It is expected that during this limited period the impact to intersection performance within Junee would be minimal (a total of 27 construction vehicles during a peak hour).

The intersection assessment assessed peak hour construction traffic in conjunction with peak hour background and diversion traffic and is considered a worst case scenario as construction start and finish times end outside of typical road traffic peak periods. The results of the assessment are shown in the following sections.

## TEMPORARY CLOSURES AND DIVERSIONS

As shown in section 5.4.1, the replacement of Kemp Street bridge would require approximately 11 months of construction activity. The Kemp Street road closure would be in effect for approximately eight months during the reconstruction of the bridge and surrounding intersections. This road closure would include the Kemp Street bridge and the adjacent intersections of Olympic Highway/Seignior Street/Kemp Street to the west of the bridge and the Kemp Street/Edgar Street overpass to the east of the rail line as shown in Figure 5.39. Based on traffic data provided by Junee Shire council for 2018 and extrapolated to 2024 (at a 1 per cent compounding per annum growth rate) this diversion is expected to impact 2,903 vehicles per day.


The intersection closure on the western side and the Kemp Street bridge closure requires diversions for:

- Olympic Highway traffic - rerouted via Joffre Street and Pretoria Avenue. It is expected that the intersection of Joffre Street and Pretoria Avenue would be managed under traffic control to give priority to the major movement of Joffre Street to/from Pretoria Avenue
- Kemp Street bridge traffic - eastbound traffic rerouted via the level crossing on Olympic Highway to the north, and be diverted via Joffre Street, Pretoria Avenue, Seignior Street, Main Street, Humphries Street and Lorne Street
- local traffic that currently turns right on Railway Parade would be diverted via Harold Street.

The intersection closure on the eastern side of Kemp Street bridge requires diversions for:

- north-south traffic at Edgar Street to be diverted via William Street and Lorne Street
- Kemp Street bridge traffic - westbound traffic rerouted via the level crossing on Olympic Highway to the north, and be diverted via Joffre Street, Pretoria Avenue, Seignior Street Main Street, Humphries Street and Lorne Street.

The diversion routes have been selected to minimise impact to the surrounding residential and open space park land uses. These diversion routes would be designed to provide suitable safe movements along public roads in accordance with relevant standards and guidelines.

## ROAD PERFORMANCE

The link LOS assessment for the Kemp Street bridge and Junee Station pedestrian bridge enhancement site components of the proposal is shown in Table 5.42. The table details a worst-case assessment including both expected peak construction traffic and diverted traffic applied to the highest peak hour traffic volume for each link. The assessment shows that with diversions in place all road links are expected to operate at LOS C or better, which is considered stable flow conditions as per the Guide to Traffic Generating Developments (RTA 2002). A change in LOS as a result of the diversions and construction traffic is seen on the following roads:

- Seignior Street (LOS B to LOS C)
- Olympic Highway Level Crossing (LOS A to LOS C)
- Humphrys Street (LOS A to LOS B)
- Joffre Street (LOS A to LOS B)
- Pretoria Avenue (LOS A to LOS B).

Table 5.42 Kemp Street bridge, diversion route road performance

| ROAD | 2024 PEAK HOUR |  | 2024 WITH DIVERSION PEAK HOUR |  |  |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Road name | Road type | Volume - <br> one way | LOS | Construction <br> volume - one <br> way | Diverted <br> volume - <br> one way <br> volume - one <br> way | Combined | LOS |
| Seignior Street | Urban | 235 | B | 27 | 173 | 435 | C |
| Olympic <br> Highway Level <br> Crossing | Urban | 198 | A | 27 | 173 | 398 | C |
| Humphrys Street | Urban | 99 | A | 27 | 173 | 299 | B |
| Lorne Street | Urban | 99 | A | 27 | 0 | 126 | A |
| Joffre Street | Urban | 24 | A | 27 | 173 | 224 | B |
| Harold Street | Urban | 68 | A | 27 | 14 | 109 | A |
| Thomas Street | Urban | 18 | A | 27 | 14 | 59 | A |
| William Street | Urban | 37 | A | 27 | 79 | 143 | A |
| Pretoria Avenue | Urban | 18 | A | 27 | 173 | 218 | B |

It is noted that the level crossing on the Olympic Highway in Junee closes more regularly and for a longer duration than other level crossings in the study area due to rail operations at the rail yard to the south of the crossing.

Data for the crossing in August 2021 (31 days) has been used to determine the number and frequency of level crossing closures during the peak traffic period (3:15PM to $4: 15 \mathrm{PM})$. The data showed the following:

- the average closure time during the traffic peak hour was under 3 minutes
- the average number of closures was less than one in a peak traffic hour.

To provide a conservative assessment of additional (diverted and construction) vehicles impacted by the crossing closures, it has been assumed that the crossing closes once during the peak hour for a duration of three minutes.

Three minutes is equivalent to $5 \%$ of the peak hour. Therefore, it is assumed that $5 \%$ of peak hour road traffic is affected by the crossing closure. The total number of vehicles two-way (with and without the diversion) is shown in Table 5.43.

Table $5.43 \quad$ Olympic Highway Junee level crossing impacts (two-way)

|  | WITHOUT <br> DIVERSIONS - <br> TWO WAY | CONSTRUCTION <br> VOLUME - <br> TWO WAY | DIVERTED <br> VOLUME - <br> TWO WAY | COMBINED <br> VOLUME - <br> TWO WAY |
| :--- | :---: | :---: | :---: | :---: |
| Number of vehicles forecast (2024) | 394 | 54 | 173 | 398 |
| $5 \%$ of vehicles impacted by closure | 20 | 3 | 13 | 36 |

Table 5.43 presents a worst-case scenario, where all diverted traffic use the level crossing. This would result in the number of vehicles experiencing delay during the peak period increase from 20 to 36 vehicles. This is not considered a significant impact. Furthermore, the assessment was undertaken for a peak hour and at other times of the day even fewer vehicles are expected to be affected by the level crossing closures.

Moreover, it is expected that locals, with knowledge of the road network and the frequency of crossing closures, would elect to avoid the crossing and use an alternative diversion route via Broadway, Regent Street, and Illabo Road, reducing the total number of vehicles impacted by the Kemp Street bridge works diversion. Table 5.44 shows the additional travel time incurred by this alternative route for northbound and southbound traffic. Although this represents a significant additional travel time for southbound vehicles, some drivers may prefer to take this route to avoid being stationary at the level crossing.

Table 5.44 Travel times for alternative diversion route

|  | EXISTING <br> TRAVEL TIME | DETOUR TRAVEL TIME | TOTAL ADDITIONAL <br> TRAVEL TIME |
| :--- | :---: | :---: | :---: |
| Northbound traffic | 2 mins | 4 mins <br> (via Broadway, Regent Street, and Illabo Road) | 2 mins |
| Southbound traffic | 0 mins | 5 mins <br> (via Broadway, Regent Street, and Illabo Road) | 5 mins |

## INTERSECTION PERFORMANCE

As stated above, the traffic diversion required for the Kemp Street bridge Enhancement Site uses several intersections through Junee. To identify intersection(s) likely to be impacted, a qualitative assessment was undertaken based on intersection layouts and opposing traffic flows at each intersection. The results are shown in Table 5.45.

Table 5.45 Diversion intersection impacts - Kemp Street bridge enhancement site

| INTERSECTION | DESCRIPTION OF TRAFFIC FLOW | EXPECTED TRAFFIC IMPACT |
| :--- | :--- | :--- |
| Olympic Highway/Joffre <br> Street | Diverted traffic flows unopposed. Left-and right <br> turn movements to/from Joffre Street are the only <br> significant movement during diversion | Minimal impacts due to diversions <br> expected. |
| Joffre Street/Pretoria <br> Avenue | Most traffic unopposed. Left-and right turn <br> movements to/from Pretoria Avenue would be <br> given priority under traffic control | Minimal impacts due to diversions <br> expected. |
| Seignior Street/Pretoria <br> Avenue | Traffic flows unopposed. Left-and right turn <br> movements to/from Seignior Street are the only <br> significant movements during diversion | Minimal impacts due to diversions <br> expected. |
| Seignior Street/Olympic <br> Highway/ Broadway | Diverted traffic has the potential to create <br> queuing issues due to proximity to level crossing | Minimal impacts due to diversions <br> expected. |
| Main Street/Olympic | Kemp street diversion traffic expected on the <br> south approach left turn and West approach left <br> Highway | Minimal impacts due to diversions <br> expected. |
| existing intersection configuration |  |  |
| Street |  |  |

The Seignior Street/Olympic Highway/Broadway roundabout was identified as the most critical to traffic operations in Junee due to:

- road hierarchy and location on the highly trafficked Olympic Highway
- opposing traffic flow volumes to major movements
- close proximity to the railway level crossing on the Olympic Highway, and potential queuing issues at this location.

Therefore, the Seignior Street/Olympic Highway/Broadway intersection has been assessed in SIDRA to reflect a 'worstcase' scenario of construction vehicle impact at an intersection during diversions within the Junee precinct. Figure 5.40 shows the layout of the roundabout as modelled in SIDRA.


Figure 5.40 Seignior Street/Olympic Highway/Broadway SIDRA intersection configuration

Traffic counts procured for the assessment show the highest hourly volumes are during the PM peak. Table 5.46 shows the background and diverted vehicle numbers during this peak period at the intersection.

Table 5.46 Seignior Street/Olympic Highway/Broadway roundabout diversion traffic volumes - PM Peak

| ROUNDABOUT | PM PEAK <br> APPROACH | DIVERTED <br> VEHICLES | CONSTRUCTION <br> VEHICLES | TOTAL VEHICLES <br> DURING <br> DIVERSION |
| :--- | :---: | :---: | :---: | :---: |
| South: Seignior Street | 179 | 83 | $27 \mathrm{lv}+9 \mathrm{hv}$ | 298 |
| East: Olympic <br> Highway | 193 | 178 | $27 \mathrm{lv}+9 \mathrm{hv}$ | 407 |
| North: Broadway | 291 | 0 | 0 | 291 |

Table 5.47 shows the SIDRA results for the Seignior Street/Olympic Highway/Broadway intersection during a 2024 peak hour with and without construction vehicles. The results show the performance of the intersection is not significantly impacted by construction vehicles: LOS continues operates at an acceptable level (LOS A), DOS only increases from $0.102-0.207$, intersection delay does not increase, and $95^{\text {th }}$ percentile queue lengths only increases by 5 m (approx. one vehicle). $95^{\text {th }}$ queuing does not extend into any additional adjacent intersections as a result of the construction vehicles.

Table 5.47 Seignior Street/Olympic Highway/Broadway, 2024 construction route intersection capacity - PM Peak

|  | 2024 PM PEAK HOUR |  |  |  | 2024 PM PEAK HOUR WITH CONSTRUCTION |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | DOS | Delay (s) | LOS | Queue (m) | DOS | Delay (s) | LOS | Queue (m) |
| South: Seignior Street | 0.08 | 6 | LOS A | 3 | 0.129 | 8 | LOS A | 6 |
| East: Olympic Highway | 0.081 | 6 | LOS A | 3 | 0.207 | 4 | LOS A | 9 |
| North: Broadway | 0.102 | 4 | LOS A | 4 | 0.113 | 5 | LOS A | 5 |
| Intersection | 0.102 | 5 | LOS A | 4 | 0.207 | 5 | LOS A | 9 |

As the Seignior Street/Olympic Highway/Broadway intersection is reflective of the 'worst case' impact resulting from diversion and construction route intersection in the Junee precinct, it is not considered that the performance of any other intersections forming part of the diversion routes would be significantly impacted by the proposal.

## TRAVEL TIME

Figure 5.41 shows that the longest potential diversion would take approximately three-to-four minutes of additional travel time in a vehicle. As the diversion is temporary, a maximum (depending on origin and destination) four minutes travel time is not considered a significant impact.


## PARKING

Parking for construction workers and laydown areas would be provided for unloading of heavy vehicles at the Kemp Street bridge enhancement site within the construction site area and so would have minimal impact to existing parking facilities.

During the two-month program for the Junee Station pedestrian bridge enhancement site a portion of the Lorne Street carpark and kerbside parking on Railway Square is expected to be impacted due to the establishment of a site access and equipment set up in these locations. Table 5.48 shows the impact to car parking in the area.

Table $5.48 \quad$ Impacts to car parking - Junee Station and surrounds

| LOCATION | CARPARK <br> CAPACITY | IMPACTED AREA | REMAINING | DURATION |
| :--- | :---: | :---: | :---: | :---: |
| Junee Station and surrounds <br> (off Lorne Street) | 60 spaces | 27 spaces | 33 spaces | Two months |
| Railway Square (Junee <br> Railway Station) | 13 spaces <br> One disabled parking <br> space | Up to 2 spaces <br> (including one <br> disabled parking <br> space) | 11 spaces | $1-2$ days |

One kerbside disabled parking space on Railway Square is likely to be temporarily impacted by works at Junee Station taking place on the overhead signal cables. These works are expected to last only for 1-2 days. Any user requiring this space would be accommodated in the TMP.

There may be other minor isolated impacts to parking due to traffic control and the increase of heavy vehicles on the local road network as listed in Table 5.49. Review of aerial imagery of the area suggests that in all locations demand for on-street parking would be relatively low in the surrounding streets, as the areas feature low-density residential premises with space for private off-street parking. There is also kerbside parking capacity nearby to absorb the temporary parking losses.

Table 5.49 Impacts to on-street parking - Junee Station and surrounds

| LOCATION | IMPACTED AREA | DURATION |
| :--- | :--- | :--- |
| Kemp Street | 19 on road spaces |  |
| Seignior Street | 18 on road spaces |  |
| Railway Lane | 13 on road spaces | Eight months (duration of Kemp Street bridge <br> closure) |
| Railway Parade | 3 on road spaces |  |
| William Street | 16 on road spaces |  |
| Joffre Street | 16 on road spaces |  |
| Pretoria Avenue | 27 on road spaces |  |

Any on-street parking impacts would be managed in line with the TMP.

### 5.4.2.3 OLYMPIC HIGHWAY UNDERBRIDGE ENHANCEMENT SITE

## ROAD PERFORMANCE

The link LOS assessment for the Olympic Highway underbridge enhancement site component of the proposal is shown in Table 5.50. This assessment shows that with construction traffic all road links are expected to operate at LOS A, which is considered stable flow conditions as per the Guide to Traffic Generating Developments (RTA 2002). Furthermore, the assessment shows no change in LOS as a result of the construction generated traffic and subsequently no significant impacts to road operation and performance are expected.

Table 5.50 Olympic Highway underbridge enhancement site, construction route road performance

| ROAD | 2024 PEAK HOUR |  | 2024 WITH CONSTRUCTION PEAK HOUR |  |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: |
| Road name | Road type | Volume - one <br> way | LOS | Construction <br> volume - one <br> way | Combined <br> volume - one <br> way | LOS |
| Main Street <br> (Olympic <br> Highway ${ }^{1}$ | Highway | 113 | A | 71 | 184 | A |
| Illabo Road $^{2}$ | Urban | 35 | A | 61 |  |  |

(1) Olympic Highway - 90 m North of Illabo Road, Junee
(2) No data available, volumes estimated as John Potts Drive, Junee with equivalent HV proportion

Note, construction peak hour volumes are higher on Main Street (Olympic Highway) than on the other roads under assessment as the road performance assessment for highways requires assessment of PCUs which effectively doubles the count of heavy vehicles required for construction.

## INTERSECTION PERFORMANCE

An assessment of the performance of the expected highest trafficked (on a per lane basis) construction route intersection in the Junee precinct was undertaken for the Junee Station and surrounds. This assessment is presented in section 5.4.2.2. The intersection assessment assessed combined peak hour construction traffic in conjunction with peak hour diversion and background traffic as a worst-case scenario for construction movements as expected construction start and finish times end outside of typical peak periods.

This assessment showed that the expected performance of the highest trafficked intersection in the precinct was LOS A, which is considered an acceptable LOS as per the Guide to Traffic Generating Developments (RTA 2002). Furthermore, the assessment shows no change in LOS as a result of the construction generated traffic and subsequently no significant impacts to intersection operation and performance are expected. Furthermore, $95^{\text {th }}$ queuing does not extend into any additional adjacent intersections as a result of the construction vehicles. As such, it is not considered that construction vehicles would impact the performance of any other lesser trafficked construction route intersection within the precinct. Therefore, no additional construction route intersection analysis has been undertaken for the Olympic Highway underbridge enhancement site.

## TEMPORARY CLOSURES AND DIVERSIONS

No road closures or diversions are proposed for the Olympic Highway underbridge enhancement site.

## PARKING

Parking for construction workers and laydown areas would be provided for unloading of heavy vehicles at the Olympic Highway underbridge enhancement site within the construction site area and so would have minimal impact to existing parking facilities. There may be minor isolated impacts to parking due to traffic control and the increase of heavy vehicles on the local road network, which would be managed in line with the TMP.

No disabled parking spaces would be impacted by the proposal.

### 5.4.2.4 JUNEE TO ILLABO CLEARANCES ENHANCEMENT SITE

## ROAD PERFORMANCE

The link LOS assessment for the Junee to Illabo Yard clearances enhancement site component of the proposal is shown in Table 5.51. This assessment shows that with construction traffic all road links are expected to operate at LOS B or better, which is considered stable flow conditions and an acceptable LOS as per the Guide to Traffic Generating Developments (RTA 2002). Furthermore, the assessment shows no change in LOS as a result of the construction generated traffic and subsequently no significant impacts to road operation and performance are expected.

Table 5.51 Junee to lllabo clearances enhancement site, construction route road performance

| ROAD | 2024 PEAK HOUR |  | 2024 WITH CONSTRUCTION PEAK HOUR |  |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: |
| Road name | Road <br> type | Volume - one <br> way | LOS | Construction <br> volume - one <br> way | Combined <br> volume - one <br> way | LOS |
| Olympic Highway $^{1}$ | Highway | 113 | A | 90 | 203 | A |
| Brabins Road $^{\text {Rural }}$ | 2 | B | 85 | 87 | B |  |
| Waterworks Road | Rural | 15 | B | 85 | 100 | B |
| Marinna Station Cross <br> Road $^{2}$ | Rural | 2 | B | 85 | 87 | B |

(1) Olympic Highway - 90 m North of Illabo Road, Junee
(2) No data available, volumes estimated as Brabins Road, Illabo

Note, construction peak hour volumes are higher on Olympic Highway than on the other roads under assessment as the road performance assessment for highways requires assessment of PCUs which effectively doubles the count of heavy vehicles required for construction.

## INTERSECTION PERFORMANCE

An assessment of the performance of the expected highest trafficked (on a per lane basis) construction route intersection in the Junee precinct was undertaken for the Junee Station and surrounds. This assessment is presented in section 5.4.2.2. The intersection assessment assessed combined peak hour construction traffic in conjunction with peak hour diversion and background traffic as a worst-case scenario for construction movements as expected construction start and finish times end outside of typical peak periods.

This assessment showed that the expected performance of the highest trafficked intersection in the precinct was LOS A, which is considered an acceptable LOS as per the Guide to Traffic Generating Developments (RTA 2002). Furthermore, the assessment shows no change in LOS as a result of the construction generated traffic and subsequently no significant impacts to intersection operation and performance are expected. Furthermore, $95^{\text {th }}$ queuing does not extend into any additional adjacent intersections as a result of the construction vehicles. As such, it is not considered that construction vehicles would impact the performance of any other lesser trafficked construction route intersection within the precinct. Therefore, no additional construction route intersection analysis has been undertaken for the Junee to Illabo Yard clearances enhancement site.

## TEMPORARY CLOSURES AND DIVERSIONS

The Junee to Illabo clearances enhancement site includes amendments to one public level crossing and three private level crossings. Table 5.52 shows the crossings to be closed, the duration of closure, and alternative access options that will be made available.

Table 5.52 Level crossing closures and diversions - Junee to Illabo clearances

| LEVEL |  |  |
| :--- | :--- | :--- |
| CROSSING | DURATION <br> OF <br> CLOSURE | ALTERNATIVE ACCESS OPTION |
| Waterworks Road <br> level crossing <br> (LX604) | Three days | Motorists would need to use Waterworks Road to travel to/from the Olympic <br> Highway. |
| Wornes Gate Road <br> level crossing <br> (LX1472) | Five days | Alternative route using Hazeldene Road would need to be used. |
| Shire and Carter <br> property level <br> crossing (LX605) | Three days | For the Junee Shire Council property, alternative access is not available but <br> Council has advised that access to this property is infrequent. Alternative access is <br> available for the private Carter property via Hazeldene Road to travel west (via <br> Ballengaoarrah Lane and Waterworks Road), or east (via Brabins Road). The <br> number of vehicles accessing the property via the level crossing is likely low but <br> may increase during harvest periods. The timing of this closure would be <br> coordinated in consultation with the Junee Shire Council and the private property <br> owner. |

The public level crossing between Waterworks Road and the Olympic Highway will be closed for enhancements as part of the proposal for three days. However, other connection points from Waterworks Road to the Olympic Highway are available via:

- Main Street in Junee, 1km to the west
- Wornes Gates Road in Illabo, 9km to the east
- Brabins Road in Illabo, 17 km to the east.

Table 5.53 shows the additional travel time required to access the Olympic Highway via these locations and the additional travel time required to travel to the location on the Olympic Highway adjacent to Waterworks Road to represent a worst-case detour.

Table 5.53
Additional travel time and number of vehicles impacted

| ROUTE FROM WATERWORKS ROAD | EXISTING <br> TRAVEL TIME | DETOUR <br> TRAVEL TIME | TOTAL ADDITIONAL <br> TRAVEL TIME |
| :--- | :---: | :---: | :---: |
| Main Street, Junee | 6 mins | 6 mins | 0 mins |
| Wornes Gate Road, Illabo | 4 mins | 10 mins | 6 mins |
| Brabins Road, Illabo | 9 mins | 15 mins | 6 mins |
| Olympic Highway adjacent to Waterworks Road | $<1 \mathrm{~min}$ | 11 mins | 10 mins |

Table 5.53 shows that for vehicles travelling:

- west to Junee there is no additional travel time
- east to Illabo there is an additional six-minute travel time via either Wornes Gate Road or Brabins Road
- north to Olympic Highway adjacent to Waterworks Road, there is an additional 10-minute travel time.

Table 5.51 shows that during a peak hour, only 15 vehicles (one way) are present on Waterworks Road during a peak hour. 15 vehicles being impacted by the additional travel time shown in Table 5.53 is not considered significant. Noting vehicles heading west will not experience any additional travel time because of the level crossing closure. Moreover, only a small percentage of vehicles would experience the maximum additional delay of 10 minutes as most vehicles will be travelling east or west.

Other level crossing closures are expected to have minimal traffic impacts as they are for a short duration, affect single property accesses, roads that carry minimal traffic, or sufficient alternative routes are available to minimise impacts.

## PARKING

Parking for construction workers and laydown areas would be provided for unloading of heavy vehicles at the Junee to Illabo clearances enhancement site within the construction site area and so would have minimal impact to existing parking facilities. There may be minor isolated impacts to parking due to traffic control and the increase of heavy vehicles on the local road network, which would be managed in line with the TMP.

No disabled parking spaces would be impacted by the proposal.

### 5.4.3 CONSTRUCTION SITE ACCESS

A turn warrant assessment for each enhancement site access in the Junee precinct have been undertaken based on The Guide to Traffic Management - Part 6 Intersection, Interchanges and Crossings (Austroads 2020). This assessment has analysed a worst-case scenario, assuming all peak generated construction traffic is distributed to each access during the road network peak period. The results of this assessment are shown in Table 5.54.

Table 5.54 Junee precinct enhancement site access turn warrant assessment

| ENHANCEMENT <br> SITE | ACCESS <br> NUMBER / <br> ROAD | ROAD <br> DESCRIPTION | ASSESSMENT <br> OUTCOME (TURN <br> TREATMENT) | CONSIDERATIONS |
| :--- | :--- | :--- | :--- | :--- |
| Harefield | $26 /$ <br> Harefield <br> Road | Two-way | Basic Left-Turn / <br> Basic Right-Turn | Left and right turn into and out of site. <br> Opposing movements on public road. |
|  |  |  | High speed environment ( $\geq 80 \mathrm{~km} / \mathrm{h}$ ). <br> Current configuration does not meet turn <br> warrant guidance, Road Safety Audit would <br> investigate the need for traffic management <br> of this access. |  |


| ENHANCEMENT SITE | ACCESS <br> NUMBER / <br> ROAD | $\begin{aligned} & \text { ROAD } \\ & \text { DESCRIPTION } \end{aligned}$ | ASSESSMENT OUTCOME (TURN TREATMENT) | CONSIDERATIONS |
| :---: | :---: | :---: | :---: | :---: |
| Harefield | 25 / Byrnes <br> Road (south <br> of Harefield <br> Road) | Two-way | Basic Left-Turn / Basic Right-Turn | Left and right turn into and out of site. Opposing movements on public road High speed environment ( $\geq 80 \mathrm{~km} / \mathrm{h}$ ). <br> Current configuration does not meet turn warrant guidance, Road Safety Audit would investigate the need for traffic management of this access. |
| Junee Station and surrounds | 30 / Seignior Street | Two-way | Channelised Right- <br> Turn / Auxiliary <br> Left-Turn | Left and right turn into and out of site. Opposing movements on public road. <br> Low speed environment ( $\leq 60 \mathrm{~km} / \mathrm{h}$ ). <br> Current configuration does not meet turn warrant guidance, Road Safety Audit would investigate the need for traffic management of this access. |
| Junee Station and surrounds | 27 / Edgar <br> Street / Hill <br> Street | Two-way | Basic Left-Turn / Basic Right-Turn | Left and right turn into and out of site. Opposing movements on public road. Low speed environment ( $\leq 60 \mathrm{~km} / \mathrm{h}$ ). Current configuration does not meet turn warrant guidance, Road Safety Audit would investigate the need for traffic management of this access. |
| Junee Station and surrounds | 29 / <br> Commercial carpark off Lorne Street | Two-way | N/A ${ }^{1}$ | Through movement into site. <br> No opposing movements on public road. <br> Low speed environment ( $\leq 60 \mathrm{~km} / \mathrm{h}$ ). <br> Minimal impact expected. |
| Olympic Highway underbridge | 31 / Regent Street | One lane twoway | N/A ${ }^{1}$ | Through movement into site. <br> No opposing movements on public road. <br> Low speed environment $(\leq 60 \mathrm{~km} / \mathrm{h})$. <br> Minimal impact expected. |
| Olympic Highway underbridge | 49 / Illabo <br> Road | Two-way | Basic Left-Turn / Basic Right-Turn | Left and right turn into and out of site. Opposing movements on public road. High speed environment ( $\geq 80 \mathrm{~km} / \mathrm{h}$ ). <br> Current configuration does not meet turn warrant guidance, Road Safety Audit would investigate the need for traffic management of this access. |


| ENHANCEMENT SITE | ACCESS <br> NUMBER / ROAD | $\begin{aligned} & \text { ROAD } \\ & \text { DESCRIPTION } \end{aligned}$ | ASSESSMENT OUTCOME (TURN TREATMENT) | CONSIDERATIONS |
| :---: | :---: | :---: | :---: | :---: |
| Olympic Highway underbridge | 32 / Main <br> Street | Two-way | Basic Left-Turn / <br> Basic Right-Turn | Left and right turn into and out of site. Opposing movements on public road High speed environment ( $\geq 80 \mathrm{~km} / \mathrm{h}$ ). <br> Current configuration does not meet turn warrant guidance, Road Safety Audit would investigate the need for traffic management of this access. |
| Olympic Highway underbridge | 48 / <br> Olympic <br> Highway | Two-way | Basic Left-Turn Basic Right-Turn | Left and right turn into and out of site. Opposing movements on public road. High speed environment $(\geq 80 \mathrm{~km} / \mathrm{h})$. Current configuration does not meet turn warrant guidance, Road Safety Audit would investigate the need for traffic management of this access. |
| Junee to Illabo | $\begin{aligned} & 33,34,53, \\ & 47,54,55, \\ & 56,57,58, \\ & 70,59,60, \\ & 71,62,63, \\ & 64,65,66 \text { / } \\ & \text { Olympic } \\ & \text { Highway } \end{aligned}$ | Two-way | Basic Left-Turn / <br> Basic Right-Turn | Left and right turn into and out of site. <br> Opposing movements on public road. <br> High speed environment $(\geq 80 \mathrm{~km} / \mathrm{h})$. <br> Current configuration does not meet turn warrant guidance, Road Safety Audit would investigate the need for traffic management of this access. |
| Junee to Illabo | $\begin{aligned} & 51,52,68, \\ & 69, / \end{aligned}$ <br> Waterworks <br> Road | One lane twoway | Basic Left-Turn / <br> Basic Right-Turn | Left and right turn into and out of site. Opposing movements on public road. High speed environment $(\geq 80 \mathrm{~km} / \mathrm{h})$. Current configuration does not meet turn warrant guidance, Road Safety Audit would investigate the need for traffic management of this access. |
| Junee to Illabo | 61 / Brabins Road | One lane twoway | N/A ${ }^{1}$ | Through movement into site. <br> No opposing movements on public road. <br> Low speed environment ( $\leq 60 \mathrm{~km} / \mathrm{h}$ ). <br> Minimal impact expected. |

(1) Turn warrant methodology not suitable for assessment due to access intersection configuration

Basic Left-Turn/Basic Right-Turn and Channelised Right-Turn / Auxiliary Left-Turn treatments are required by the intersection turn warrant assessment for some site accesses in this precinct. However, this may not be required given the temporary nature of accesses during the construction phase and the conservative nature of the assessment (peak construction vehicles assessed during the background peak hour, when peak construction vehicles are expected outside the background peak hour).

Where the turn warrant assessment methodology is unsuitable for the assessment of the enhancement site access, access arrangements as per the current road network are not expected to have a significant impact as they are either a through movement from the end of a street or impacting limited traffic movements.

More detailed assessment of the accesses will be undertaken as part of the Road Safety Audits and appropriate Construction Traffic Transport and Access Management Plans will be developed by the contractor prior to commencement of construction activities on site to moderate any potential safety issues. Design of any access treatments or modifications to roads would be undertaken in accordance with appropriate design standards and with approvals from the relevant local or state road authorities. Works Authorisation Deeds or other suitable consent or agreement with TfNSW will be made prior to undertaking any relevant works on a State Controlled Road.

### 5.4.4 ROAD SAFETY

During construction there would be changes to road conditions within the Junee precinct consisting of increased traffic volumes due to construction vehicles, temporary diversions and new access points to the enhancement sites from the public road network. This study has primarily considered the operation and capacity of the road network rather than the appropriateness of use of certain roads by construction vehicles. The suitability of access and diversion routes has not been assessed with respect to road safety.

It is noted that the construction activities at enhancement sites within the Junee precinct, are expected to generate a maximum peak hour flow of 65 vehicles (for a three-day peak possession period), which does not result in a change of LOS on any of the enhancement site access routes as discussed in section 5.4.1. Access intersections to the enhancement sites within the Junee precinct would be designed or have traffic control measures implemented to provide suitable safe access to public roads in accordance with relevant standards and guidelines.

Additionally, there would be traffic diversions in place for the Kemp Street bridge work site that re-route vehicles on the state-controlled Olympic Highway to Joffre Street and Pretoria Street. The diversion of Traffic from the Kemp Street bridge results in a change of LOS, but all road links still operate at LOS C or better, which is considered stable flow conditions as per the Guide to Traffic Generating Developments (RTA 2002). Traffic management for these diversion routes would be designed to provide suitable safe access to public roads in accordance with relevant standards and guidelines.

To moderate any construction impacts to existing or potential safety issues associated with either construction vehicle movements or the additional traffic on local roads from diversions, Road Safety Audits and Construction Traffic Transport and Access Management Plans would be required to be undertaken by the contractor prior to commencement of construction activities on site or the implementation of diversionary routes and the safety of all road users should be taken into account.

### 5.4.5 HEAVY VEHICLE ROUTES

As there are no significant changes to background LOS resulting from the traffic generated by the construction activities at enhancement sites or diversions within the Junee precinct, it is not expected that construction heavy vehicle and workforce movements generated by the proposal, as shown in section 5.4.1.3, would impact the current operations of existing heavy vehicles movements, including agricultural transport, on the routes discussed in section 4.6.3

The Kemp Street bridge enhancement site works would require diverting of part of the Olympic Highway in southern Junee. Heavy vehicle diversionary signage would be implemented to divert traffic outside of Junee on existing heavy vehicle routes via Goldfields way and Old Junee Road resulting in an additional travel distance of 4 km to reduce impact associated with heavy vehicle movements on Pretoria Street. For heavy vehicles that this diversionary route is not appropriate, a diversion on local roads within Junee via Joffre Street and Pretoria Avenue would be in place. This diversion does not represent a significant change in distance travelled. However, there may be minor delays to heavy vehicles passing through the enhancement site from reduced speed limits and traffic control. The Construction Traffic Transport and Access Management Plans would be developed to ameliorate impacts to safe and efficient travel of heavy vehicles through this diversionary route.

There is potential for construction heavy vehicles to impact road pavement conditions along haul routes. To determine the extent of the impact a road dilapidation report would be prepared for all haul routes within the precinct. Joffre Street and Pretoria Avenue would be monitored for damage during construction and any necessary repairs attended to immediately.

### 5.4.6 TRAVELLING STOCK RESERVES

No Travelling Stock Reserves are located on roads expected to support construction movements in the Junee precinct. A small Travelling Stock Reserve is located near the eastern end of the Junee to Illabo clearances enhancement site, which is not expected be significantly impacted as it does not cross the enhancement site. It is expected that prior to the commencement of works that Local Land Services would be notified of increased vehicle movements along the TSRs and temporary closures of rail level crossings in the Junee precinct so that stock handlers, including walking permit holders, can be notified of the impacts to stock movements.

### 5.4.7 PUBLIC TRANSPORT ROUTES

### 5.4.7.1 ROAD

Although there would be increased traffic resulting from construction activities within the Junee precinct, it is expected to have a minimal impact on the operation of public or school bus services or bus stops due to the low traffic volumes generated by the construction activities (with diversions in place all road links are expected to operate at LOS C or better, which is considered stable flow conditions as per the Guide to Traffic Generating Developments (RTA 2002)). It is noted that the heaviest period of construction movements during a day is expected to occur outside peak bus service periods (e.g. school times). There may be minor delays to buses passing near the enhancement sites from reduced speed limits and traffic control. These impacts would be managed in accordance with the traffic management plan to ameliorate impacts to the safe and efficient travel of bus services through the affected areas.

The road closures associated with the Kemp Street bridge enhancement site and the associated changes in road network connectivity for eight months is expected to directly impact public and school bus services as described below in Table 5.55 and Table 5.56.

Table 5.55 Public bus route impacts - Kemp Street bridge

| SERVICE | IMPACTS |
| :--- | :--- |
| Wagga, 922 - Junee to Wagga Wagga, 924 <br> - Junee to Wagga Wagga via Jail Break <br> Inn, Wallacetown and Brucedale Dr | These services use Kemp Street and are directly impacted by Kemp Street <br> bridge closure. Would require rerouting and alternative stops (Kemp Street <br> after Joffre Street / 2663127) or stopping patterns during the closure period. |
| 921 - Junee to Wagga | These services use Kemp Street and are directly impacted by Kemp Street <br> bridge closure. Would require rerouting during the closure period. |
| 923 - Junee to Wagga Wagga via Junee <br> Station | These services use Byrnes Road and are directly impacted by Kemp Street <br> bridge closure. Would require rerouting during the closure period. |

## Table $5.56 \quad$ School bus route impacts - Kemp Street bridge

| SERVICE | IMPACTS |
| :--- | :--- |
| S221 - Junee Schools | This service uses Kemp Street and is directly impacted by Kemp Street bridge closure. <br> Would require rerouting and alternative stops (Kemp Street after Joffre Street / <br> 2663127) or stopping patterns during the closure period. |
| S226 - Junee Reef to Junee <br> Schools via Marinna Road | These services use Kemp Street and are directly impacted by Kemp Street bridge <br> closure. Would require rerouting during the closure period. |

Changes to bus routes and bus stops would be planned in consultation with the relevant stakeholders to minimise the impact on community, public transport users, and service providers.

Further to the above impacts due to diversions, there may be minor delays to buses passing near enhancement sites from reduced speed limits and traffic control. These impacts would be managed in accordance with the traffic management plan to ameliorate impacts to the safe and efficient travel of bus services through the affected areas.

### 5.4.7.2 RAIL

Track works would be required for following enhancement sites:

- Harefield Yard clearances
- Junee Yard clearances
- Olympic Highway underbridge
- Junee to Illabo clearances.

These works would occur during either:

- existing scheduled weekend rail corridor possession periods (typically 72 hours) when trains along the rail corridor are stopped for maintenance as part of operation of the existing rail line; or
- track work authorisations periods, which enable works that impact rail operations to occur outside scheduled rail possessions, but within available 9-hour windows in which train services are not scheduled.

Work during these periods would be undertaken in consultation with passenger rail operators. However, it is not expected that proposal construction works would impact upon the passenger rail network. A portion of the train station platform at Junee station will be temporarily impacted during the pedestrian overpass removal works. During the works the platform will remain open and the remaining unimpacted length of platform (approximately 130 m ) is expected to provide sufficient capacity to operate without impact to passengers.

### 5.4.8 ACTIVE TRANSPORT ROUTES

As shown in section 4.6.6, provision for active transport in the vicinity of the Harefield and Junee to Illabo Yard clearances enhancement sites is minimal, and given the surrounding land uses the demand for cycling and pedestrian travel in the area is likely to be low. Although there would be increased traffic from construction vehicles, it is expected to have a minimal impact on cycling or pedestrian movements due to the low traffic volumes generated by the construction activities (with diversions in place all road links are expected to operate at LOS C or better, which is considered stable flow conditions as per the Guide to Traffic Generating Developments (RTA 2002)).

The closure of the Kemp Street bridge for approximately eight months will impact active transport connectivity. During the closure period, cross-rail pedestrian and cyclist movements would be diverted to the alternative rail crossing on Olympic Highway located 700 m north. This is a potential additional diversion distance of 1.4 km as a worst-case scenario as actual impacts would vary by individual origin and destination. Footpaths provide full pedestrian connectivity for the diversion route between Kemp Street and Ducker Street (the location of western landing of the Kemp Street bridge) via Seignior Street and Lorne Street. Cyclists would be required to travel on-road via the diversion route. Pretoria Avenue and Joffre Street do not have full pedestrian connectivity for the diversion route between Kemp Street and Ducker Street (as there are no formalised footpaths). The existing shared path located within the enhancement site through Endeavour Park (as shown in Figure 4.64) would remain available until it is closed for construction. At this point, pedestrians would be detoured onto Pretoria Avenue and Joffre Street. Construction staging will be planned to account for continued active transport connectivity during construction.

The Olympic Highway underbridge would require the closure of the pedestrian path under the bridge for approximately five days. Works are planned during rail possession periods when the demand for pedestrian and cyclist movement in this area is expected to be low. The nearest alternative crossing represents a detour of approximately 3.5 km and so it is expected that pedestrians would be managed by on-site traffic management during this period. Cyclists would be required to travel on-road via the diversion route.

### 5.4.9 PROPERTY ACCESS IMPACTS

Although there may be some minor temporary disruptions, property access is expected to be maintained for the duration of the construction activities in the area, including to houses on Pretoria Avenue. Properties located adjacent to the Kemp Street bridge enhancement site on the Olympic Highway between Railway Lane and Harold Street have rear lane access, which would be maintained throughout construction. Pedestrian access to these properties would be maintained via Olympic Highway. One property on Railway Lane may be impacted by the closure of this street, however alternative access arrangements are expected to be provided.

Access to an approved development at the rear of the Locomotive Hotel off Kemp Street would be maintained via Edgar Street. More detailed assessment of this access requirement would be undertaken by the contractor prior to commencement of construction activities on site. These would include Road Safety Audits and appropriate Construction Traffic Transport and Access Management Plans to moderate any potential safety issues.

Any changes to the existing access arrangements would need to be undertaken in consultation with the relevant stakeholders and in line with the TMP.

### 5.4.10 RAIL FREIGHT

Track works would be required for the following enhancement sites:

- Harefield Yard clearances
- Junee Yard clearances
- Olympic Highway underbridge
- Junee to Illabo clearances.

These works would occur during either:

- existing scheduled weekend rail corridor possession periods (typically 72 hours) when trains along the rail corridor are stopped for maintenance as part of operation of the existing rail line; or
- track work authorisations periods, which enable works that impact rail operations to occur outside scheduled rail possessions, but within available 9-hour windows in which train services are not scheduled.

Work during these periods would be undertaken in consultation with freight operators. However, it is not expected that proposal construction works would impact upon the rail freight network.

### 5.4.11 EMERGENCY VEHICLE ACCESS

Construction of the proposal would result in temporary impacts to access and traffic with the establishment of diversions due to closure of the Kemp Street bridge, and an increase in vehicle movements on the road network. As shown in the link and intersection performance assessments, all road links are expected to operate at LOS C or better within the Junee precinct, and so there is not expected to be a significant impact to emergency vehicles. It is expected that the traffic and access management plan would be developed in consultation with TfNSW, Junee Shire Council, and State emergency services and would consider and effectively manage any impacts to emergency vehicles seeking to use roads in the vicinity of the enhancement sites or diversion routes.

### 5.4.12 SEASONAL VARIATION

Temporary local events such as festivals, shows, and markets may result in minor localised traffic variations, particularly in urban environments such as Junee. The Harefield and Junee to Illabo Yard clearances enhancement sites are less urbanised than those located closer to Junee, featuring more rural and agricultural land uses.

Localised seasonal traffic variation may be experienced at enhancement sites that share land with agricultural infrastructure (grain silos, livestock loading facilities etc.) as the infrastructure will likely generate additional heavy or farm vehicle movements during harvest seasons.

A review of aerial imagery of enhancement sites in the Junee precinct identified grain silos and agricultural transport facilities that may generate seasonal agricultural vehicle or machinery movements in the vicinity of the Junee to Illabo clearances enhancement site. The following rail level crossings provide access to the enhancement site and were identified as the most likely to have agricultural movements.

- LX604 - Brabins Road
- LX605 - Shire and Carter property level crossing
- LX1472 - Wornes Gate Lane
- LX606 - Waterworks Road.

However, it is not anticipated that any seasonal variation would significantly impact the outcomes of the traffic assessment as background and construction vehicle traffic volumes are low. More detailed assessment of the enhancement site accesses, which would consider seasonal variation due to social events and agricultural movements, will be undertaken by the contractor prior to commencement of construction activities on site. These would include Road Safety Audits and appropriate Construction Traffic Transport and Access Management Plans to moderate any potential safety issues.

## 6 IMPACT ASSESSMENT - OPERATION

In accordance with the SEARs, an impact assessment of the transport network during the operation of the proposal has been undertaken. Mitigation measures have been developed to minimise the consequence and/or likelihood of the impacts.

### 6.1 OPERATIONAL CONTEXT

The operational assessment of the proposal has been undertaken for the horizon years of 2025 (year of opening) and 2040 (15-year design horizon). Between 2025-2040 the expected number of Inland Rail services between Albury and Illabo is expected to increase. The number of freight trains movements between Albury and Illabo will increase from up to 12 per day in 2021 to up to 18 per day in 2025, further increasing to up to 20 per day in 2040.

To provide a conservative assessment of the operational period, it has been assumed that all expected growth in services (passenger and rail) after 2025 are attributed to the proposal. This methodology results in an increase of up to two daily services from 2025 to 2040 . Conservatively, its assumed that a maximum of two services would operate in any one hour in 2040.

These trains would be diesel powered, and would be a mix of passenger trains, bulk freight, and containerised freight trains of up to $1,800 \mathrm{~m}$ in length with train speeds ranging from 60 to $115 \mathrm{~km} / \mathrm{hr}$. The maximum length of trains operating between Albury and Illabo would not increase due to the proposal, as trains up to $1,800 \mathrm{~m}$ in length currently operate. The existing freight train speed limits between Albury and Illabo would apply to the Inland Rail freight trains therefore no changes to current freight train speeds are expected as a result of the proposal. The possible future use of the railway between Albury and Illabo by freight trains up to $3,600 \mathrm{~m}$ long would be subject to separate assessment.

An Inland Rail freight train of $1,800 \mathrm{~m}$ in length would generally travel through any given location at the same speed a $1,800 \mathrm{~m}$ in length freight train would under current operations. Using a level crossing as an example, the total closure time for a $1,800 \mathrm{~m}$ in length freight train would be the same with the operation of the proposal as it would under current operations. However, as the proposal would increase the number of freight trains and particularly those up to $1,800 \mathrm{~m}$ in length, the likelihood of experiencing the maximum delay associated with a level crossing closure for a $1,800 \mathrm{~m}$ freight train would increase.

As the proposal only provides enhancements to the existing rail line and crossings, the potential operational impacts would be associated with:

- increased daily train services resulting in an increased frequency of closures per day at level crossings
- increased delay where level crossings on private accesses have been upgraded from passive to active.


### 6.2 ROAD NETWORK OPERATION

There is not expected to be any significant impact to road network performance during the operation of the proposal.
The proposal would not generate additional traffic during operation, as there would be no changes to track maintenance activities and rolling stock staffing. As such, no impacts to the road network performance during operation of the proposal from vehicle movements would occur.

Furthermore, the number of road-based freight movements utilising the wider road network may reduce as a result of the operation of the Inland Rail program as a whole. Moreover, as there are no proposed increases to passenger train services as a result of the proposal it is not expected that any additional traffic would be generated by passengers accessing existing railway stations.

It is noted that some realignment and modification of the road network occurs as a result of enhancements at the Edmondson Street bridge site in Wagga Wagga and the Kemp Street bridge site in Junee. No significant change to the geometry and functionality of the road network adjacent to the Edmondson Street bridge is expected. Therefore, no associated impacts to traffic capacity or intersection performance are expected either. The intersection of Railway Parade/ Kemp Street / Olympic Highway in Junee will be reconfigured from close-set staggered T-intersections to a four-way priority intersection, maintaining all existing traffic movements. Due to the low volumes on Railway Parade, this permanent change to the road network is not expected to have any significant impacts to intersection delay, capacity, or Level of Service.

### 6.3 RAIL INTERFACE OPERATION

### 6.3.1 APPROACH

The approach ARTC has used for considering level crossing options is outlined in Appendix A. It has taken into account relevant NSW and Australian level crossing policies, which emphasise the need to minimise the number of level crossings, as far as reasonably practicable.

The treatment options for the interaction of public roads and the rail corridor consist of:

- grade-separated crossings (via a road or rail bridge)
- level crossings.

Level crossings would be provided with warning signage, line marking, and other relevant controls, in accordance with the relevant ARTC and Australian standards, incorporating either:

- passive crossings, which involve static warning signs
- active crossings, which involve flashing lights, warning bells and boom barriers for motorists. These devices are activated prior to and during the movement of a train through the level crossing.


### 6.3.2 SIGHT LINES

The vegetation and topography near level crossings must be assessed for its potential to obscure visibility of signals, other transport and sight lines to the track from vehicle stop lines at level crossings (to meet ALCAM distances). Sight lines were reviewed for all modified level crossings. Sight lines at one level crossing being LX 604 (Brabins Road) were identified to be insufficient.

The deficiency is attributed to vegetation on the western side of the Brabins Road reserve. Permanent removal of the vegetation would restore the sighting distance and resolve the sight line failure. Although this option involves some limited biodiversity impacts associated with the removal of the vegetation, it provides a permanent solution that does not require the substantial upgrade of the level crossing to resolve the sight line deficiency. The upgrade of the level crossing to have additional controls would require a prolonged period of temporary level crossing closure during construction which would cause additional traffic impacts for road users.

### 6.3.3 CLOSURE OF LEVEL CROSSINGS

No level crossings are proposed to be closed at this stage, however ARTC are consulting with relevant stakeholders on the potential closure of LX 1472. Located in the Junee to Illabo clearances enhancement site, LX 1472 (Wornes Gate Lane) is currently a public, passive level crossing between the Olympic Highway and Wornes Gate Lane which is an unsealed road and expected to have minimal to no use by the public or for landowner access. All property adjacent to LX 1472 have primary access points elsewhere.

### 6.3.4 PREFERRED OPTIONS

The preferred option for public road interactions across the proposal site, based on the considerations described in section 3.3 and Appendix A involves a mix of active and passive level crossings. ARTC would continue consultation with relevant road managers during detailed design, to finalise preferred treatments at each location. The appropriate treatment would be assessed on a case-by-case basis for design purposes, with consideration given to the results of consultation; current and future usage of the asset; its location relative to other crossings of the rail corridor; and the road and rail geometry at the crossing location.

Three level crossings would be upgraded as part of the proposal:

- Henty Yard clearances: Sladen Street (LX625). At this location the pedestrian crossing would be upgraded from a passive to an active level crossing. The existing active vehicular crossing would be modified to accommodate the proposal.
- Junee to Illabo clearances: Wornes Gate Lane (LX 1472) would be upgraded from a passive to active vehicular level crossing.
- Junee to Illabo clearances: Shire and Carter Property access road (LX605) would be upgraded from a passive to active vehicular level crossing.

Elsewhere, adjustments to five open active level crossings and one closed level crossing would be required to accommodate the realigned track, or to address short stacking issues at some level crossings. Further detail is provided in the proceeding sections.

### 6.3.5 LEVEL CROSSINGS - SHORT STACKING ASSESSMENT

Higher train numbers in future years may present safety risks to motorists due to potential collisions with trains at level crossings. In accordance with the safety measures outlined within the ALCAM assessment process (Appendix A), where works have been carried out on level crossings, all crossing points would be designed to ensure that adequate safety measures are implemented to mitigate the likelihood of incidents between passing trains and passenger vehicles. A review of the existing level crossings has been undertaken to identify locations in the enhancement sites where short stacking may be an issue and is presented in Table 6.1.

Table 6.1 Review of Short stacking at level crossings

| PRECINCT | CROSSING ROAD | $\begin{aligned} & \text { ROAD } \\ & \text { TYPE } \end{aligned}$ | DISTANCE TO CONTROL POINT | LENGTH ${ }^{1}$ <br> (DESIGN <br> VEHICLE ${ }^{2}$ <br> $+5 \mathrm{~m})$ | COMMENT |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Albury | Tynan Road | Public Road | 36 m | 24 m | No short stacking issue |
| Greater <br> Hume - <br> Lockhart | Balfour Street | Public Road | 70 m | 31 m | No short stacking issue |
|  | Sladen Street (LX625) | Public Road | 20m | 31 m | ARTC is continuing to consult with TfNSW to determine a suitable solution to the short stacking issue which will be confirmed during the detailed design stage (further detail is provided below). |
|  | Rosler Parade | Public Road | 29 m | $24 \mathrm{~m}^{3}$ | No short stacking issue |
|  | Plunkett Street (LX622) | Public Road | 30 | 24 m | No short stacking issue |
|  | Yerong Street | Public Road | 33 m | 24 m | No short stacking issue |
|  | Urana Street | Public Road | 50 m | 31 m | No short stacking issue |


| PRECINCT | CROSSING ROAD | ROAD TYPE | DISTANCE TO CONTROL POINT | LENGTH ${ }^{1}$ <br> (DESIGN <br> VEHICLE ${ }^{2}$ <br> $+5 \mathrm{~m})$ | COMMENT |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Wagga Wagga | Yarragundry Street (LX619) | Public Road | 70 m | 24 m | No short stacking issue |
|  | Fernleigh Road | Public Road | 240 m | 24 m | No short stacking issue |
|  | Bourke/Docker Street | Public Road | $>400 \mathrm{~m}$ | 24 m | No short stacking issue |
| Junee | Harefield Road | Public Road | 150 m | 31 m | No short stacking issue |
|  | Olympic Highway <br> (Junee) | Public Road | 45 m | 31 m | No short stacking issue |
|  | Waterworks Road (LX606) | Public Road | 24 m | 24 m | Intersection priorities at Waterworks Road will be changed as part of construction works. Vehicles on Waterworks Road will give way to southbound vehicles crossing the rail line, eliminating a short stacking deficiency. The proposed changes to intersection priority are not expected to introduce any negative safety outcomes as vehicles will now have to slow down on the approach to the intersection, reducing the likelihood of a collision with a vehicle queued through the intersection. Furthermore, traffic counts completed for this assessment indicate vehicle volumes are low on Waterworks Road. <br> ARTC is continuing to consult with Junee Council in regards to mitigation at this level crossing. |
|  | Private level crossing (LX605) | Private <br> Access off Olympic <br> Highway | 16 m | 31 m | A storage lane will be provided on the Olympic Highway with the capacity to store heavy vehicles clear of the rail line without impacting on the Olympic Highway traffic movements. A concrete island would be established on the level crossing approach from the Olympic Highway to limit movements to left-in and left-out. |

$\left.\begin{array}{|l|l|l|c|c|l|}\hline \text { PRECINCT } & \text { CROSSING ROAD } & \begin{array}{l}\text { ROAD } \\ \text { TYPE }\end{array} & \begin{array}{c}\text { DISTANCE } \\ \text { TO } \\ \text { CONTROL } \\ \text { POINT }\end{array} & \begin{array}{c}\text { LENGTH } \\ \text { (DESIGN } \\ \text { VEHICLE }\end{array} & \text { COMMENT } \\ \mathbf{+ 5 m} \text { ) }\end{array}\right]$
(1) As per Crossing Assessment Handbook, Australian Level Crossing Assessment Model, Applicable to Road Model v 2.1.1.1, Pedestrian Model v 1.2 (2017)
(2) The design vehicle is taken as a 19 m articulated vehicle except where the level crossing is located on a designated 25 m Bdouble Route, where the design vehicle is taken as a 25 m B-double
(3) Rosler Parade is a designated heavy vehicle route only in the westbound direction. In the eastbound direction, the design vehicle length is taken at 19 m .

An existing potential short stacking deficiency has been identified at the Sladen Street level crossing as the give way line for the west approach to the intersection with Olympic Highway is set back from the conflict point to allow space for heavy vehicles to turn right into Sladen Street from the Olympic Highway. A review of the crash history from 2015 to 2019 show no crashes recorded at this level crossing (refer to section 4.4.1.2). The level crossing configuration exists with and without the proposal and that works associated with the proposal do not include any deficiencies. ARTC is continuing to consult with TfNSW to determine a suitable solution to the short stacking issue which will be confirmed during the detailed design stage.

### 6.3.6 LEVEL CROSSINGS - UPGRADES

The ALCAM assessment identified the need for two level crossings within the Junee to Illabo clearances enhancement site to be upgraded from passive to active for road traffic. The level crossings are:

- LX1472 (Wornes Gate Lane) - Wornes Gate Lane is a Junee Shire Council unsealed road, providing access to rural areas south of the Olympic Highway and is currently a passively controlled crossing
- LX605 (Shire and Carter property level crossing - provides access to a Junee Shire Council unsealed road, providing local access to a low intensity extractive industry site south of the Olympic Highway and is currently a passively controlled crossing.

Due to the very low daily and hourly demand expected at these level crossings, and the relatively low frequency of trains (conservatively, its assumed that a maximum of two services would operate in any one hour in 2040), the number of vehicles expected to be impacted by the proposed level crossing upgrades at these sites is low.

### 6.3.7 LEVEL CROSSINGS - CLOSURE TIME

An Inland Rail freight train of $1,800 \mathrm{~m}$ in length would generally travel through any given location at the same speed a $1,800 \mathrm{~m}$ in length freight train would under current operations. Using a level crossing as an example, the total closure time for a $1,800 \mathrm{~m}$ in length freight train would be the same with the operation of the proposal as it would under current operations. However, as the proposal would increase the number of freight trains and particularly those up to $1,800 \mathrm{~m}$ in length, the likelihood of experiencing the maximum closure time associated with a level crossing closure for a $1,800 \mathrm{~m}$ freight train would increase.

Notwithstanding, where an existing level crossing is upgraded from passive to active controls, a delay from additional closure time for boom gates to close, and reopen, may be introduced. As discussed in section 6.3.6, two level crossings would be upgraded from passive to active controls as part of the proposal. To understand the relative increase in delay at a level crossing from this change, the expected closure times for both passive and active level crossings have been calculated. The following operational assumptions at a passive and active level crossing have been adopted, as shown in Table 6.2.

Table 6.2 Passive and active level crossing delay calculation

| ASSUMPTIONS | PASSIVE | ACTIVE | DIFFERENCE |
| :--- | :--- | :--- | :--- |
| Train length | $1,800 \mathrm{~m}$ | $1,800 \mathrm{~m}$ | - |
| Train speed | $80 \mathrm{~km} / \mathrm{h}$ | $80 \mathrm{~km} / \mathrm{h}$ | - |
| Before train | 20 seconds - traffic stops | 30 seconds - traffic stops <br> Flashing lights and closing boom gates | 10 seconds |
| Train pass-by | 81 seconds | 81 seconds | - |
| After train | 5 seconds - traffic recommences | 10 seconds - traffic recommences <br> Flashing lights and opening boom gates | 5 seconds |
| Total duration | 106 seconds | 121 seconds | 15 seconds |

It is noted that train speeds would range from 60 to $115 \mathrm{~km} / \mathrm{h}$ for the proposal, however the typical train speed is $80 \mathrm{~km} / \mathrm{h}$ which has been used in this assessment. At any location, an active crossing has a 15 second longer closure time compared to a passive crossing, regardless of train speed. This is due to the duration of time that is programmed for the flashing lights and closing of the boom gates prior to the train pass-by and for the flashing lights and opening of the boom gates when the train has passed.

After a level crossing is upgraded from passive to active, road users would experience an additional 15 seconds of closure time during a level crossing closure. Given the increase in rail services between 2025 and 2040 of up to two daily services, level crossing closures would also be more frequent and as such road users would be more likely to encounter a level crossing closure.

### 6.3.8 LEVEL CROSSINGS - TRAFFIC

### 6.3.8.1 TRAFFIC VOLUMES

During operation of the proposal it is expected that there will be more daily rail services than at present. The increase in daily rail service numbers will increase both the number of level crossing activations per day and the likelihood that a level crossing activation may occur during a peak hour. This would therefore increase the number of vehicles stopping during the activation of a level crossing. There are 15 existing active level crossings on public roads and two existing passive level crossings on private accesses in operation along the rail line within the proposal site.

The road characteristics, applied growth rates, and extrapolated peak hour traffic volumes for the 2025 and 2040 operational horizons on the public roads with level crossings are shown in Table 6.3. It is noted that the growth rate of 3 per cent compounding per annum applied in some areas for the duration of the operational assessment period ( 15 years) may be considered relatively high considering land use and growth forecasting.

Table 6.3
Future traffic volumes at level crossings

| PRECINCT | CROSSING ROAD | ROAD <br> DESCRIPTION | GROWTH <br> RATE <br> (PER | 2 WAY 2025 <br> PEAK HOUR <br> TRAFFIC <br> RONNU) | 2 WAY 2040 <br> PEAK HOUR <br> TRAFFIC <br> VOLUMES |
| :--- | :--- | :--- | :---: | :---: | :---: |
| Albury |  |  | Two-way, two lanes | $3 \%$ | 93 |

(1) Calculated as $10 \%$ of AADT
(2) Peak hour intersection count

### 6.3.8.2 IMPACTED VEHICLES

The closure time calculations show that the total closure time for vehicles at level crossings would be 121 seconds. It is noted that the closure time at a level crossing not subject to upgrade from passive to active controls would be constant with or without the proposal, with the only increase being the frequency of closures occurring.

The average number of vehicles predicted to stop during a level crossing closure in a peak hour during the 2025 and 2040 operational horizons are presented in Table 6.4. Note, the number of impacted vehicles during a level crossing closure in a peak hour would be equivalent for the with and without the proposal scenarios in both 2025 and 2040.

Table 6.4 Operational horizon active level crossing impacted vehicles during peak hour closures

| PRECINCT | ROAD WITH LEVEL CROSSING | 2025 IMPACTED <br> VEHICLES (AVG PER <br> PEAK HOUR CLOSURE) | 2040 IMPACTED VEHICLES (AVG PER PEAK HOUR CLOSURE) |
| :---: | :---: | :---: | :---: |
| Albury | Tynan Road | 3 vehicles | 5 vehicles |
| Greater Hume <br> - Lockhart | Balfour Street | 29 vehicles | 45 vehicles |
|  | Sladen Street | 4 vehicles | 6 vehicles |
|  | Rosler Parade | 4 vehicles | 6 vehicles |
|  | Plunkett Street | 4 vehicles | 6 vehicles |
|  | Yerong Street | 1 vehicles | 1 vehicles |
|  | Urana Street | 3 vehicles | 5 vehicles |
| Wagga Wagga | Yarragundry Street | 2 vehicles | 3 vehicles |
|  | Fernleigh Road | 44 vehicles | 68 vehicles |
|  | Bourke/Docker Street | 57 vehicles | 72 vehicles |
| Junee | Harefield Road | 1 vehicles | 1 vehicles |
|  | Olympic Highway (between Seignior Street and Main Street | 14 vehicles | 17 vehicles |
|  | Waterworks Road | 1 vehicles | 1 vehicle |
|  | Brabins Road | $<1$ vehicle | $<1$ vehicle |
|  | Shire and Carter property level crossing | $<1$ vehicle | $<1$ vehicle |
|  | Wornes Gate Lane | $<1$ vehicle | $<1$ vehicle |
|  | Olympic Highway (Illabo) | 7 vehicles | 8 vehicles |

It is noted that the number of impacted vehicles during a level crossing closure in a peak hour would be equivalent for the with and without the proposal scenarios. However, due to the increase in rail services (up to two daily services from 2025 to 2040) a level crossing closure is more likely to be encountered during a peak hour as a result of the proposal (conservatively, its assumed that a maximum of two services would operate in any one hour in 2040).

### 6.3.8.3 ROAD PERFORMANCE

LOS, average queue lengths and average delay on public roads at level crossings during a peak hour have been assessed using SIDRA intersection software with outcomes shown in Table 6.5. For this assessment it has been assumed that two rail services would pass through the level crossing during a peak hour. The SIDRA modelling has used a 3,600 second, 4-phase signal plan with two 121 second phases for train movements and all remaining time given to the road crossing. Where the directionality of traffic flows is known (at locations where traffic counts were undertaken for this study), queues modelled on the approach with the highest volume from the highest trafficked peak period have been reported. It is expected that queues at all other times will be less than those reported, however a conservative approach has been adopted that reports the longest expected queue length. Where the directionality of traffic flows is not known, the oneway approach volume has been taken as half of the two-way peak volume and equivalent queues would be expected on both approaches.

Table 6.5 Road performance at level crossings

| PRECINCT | ROAD WITH LEVEL CROSSING | 2025 |  |  | 2040 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | LOS | Average delay (s) | Average queue (m) | LOS | Average delay (s) | Average queue (m) |
| Albury | Tynan Road ${ }^{1}$ | A | 5 | 4 | A | 5 | 22 |
| Greater Hume Lockhart | Balfour Street ${ }^{1}$ | A | 6 | 156 | A | 7 | 294 |
|  | Sladen Street ${ }^{1}$ | A | 5 | 16 | A | 5 | 25 |
|  | Rosler Parade ${ }^{1}$ | A | 5 | 16 | A | 5 | 25 |
|  | Plunkett Street ${ }^{1}$ | A | 5 | 16 | A | 5 | 25 |
|  | Yerong Street ${ }^{1}$ | A | 5 | 4 | A | 5 | 5 |
|  | Urana Street ${ }^{1}$ | A | 5 | 13 | A | 5 | 20 |
| Wagga Wagga | Yarragundry Street ${ }^{1}$ | A | 5 | 10 | A | 5 | 15 |
|  | Fernleigh Road ${ }^{2}$ | A | 7 | 304 | A | 11 | 724 |
|  | Bourke/Docker Street ${ }^{2}$ | A | 3 | 238 | A | 4 | 348 |
| Junee | Harefield Road ${ }^{1}$ | A | 5 | 3 | A | 5 | 4 |
|  | Olympic Highway (between Seignior Street and Main Street ${ }^{2}$ | A | 5 | 62 | A | 8 | 80 |
|  | Waterworks Road ${ }^{1}$ | A | 5 | 4 | A | 5 | 4 |
|  | Brabins Road ${ }^{1}$ | A | 5 | 1 | A | 5 | 1 |
|  | Olympic Highway (Illabo) ${ }^{1}$ | A | 5 | 28 | A | 5 | 33 |

(1) Calculated as $5 \%$ of AADT / half of the two-way peak volume (which is $10 \%$ of AADT).
(2) Peak hour intersection count

As LOS is typically a measure of average delay over an hour. All level crossings operate at LOS A due to the relatively low frequency of closures and proportion of vehicles stopped during a closure. Some significant queues are noted at Balfour Street and Fernleigh Road. However, due to the expected time between closures these queues are likely to disperse prior to the next level crossing activation. It is noted that the delay and queues calculated by SIDRA for a peak hour closure would occur with or without the proposal. However, due to the growth in rail services (up to two daily services from 2025 to 2040) there is an increase to the likelihood of these occurring.

Potential impacts (with or without the proposal) to adjacent intersections associated with queueing from level crossing closures are shown below in Table 6.6 for the operational horizons. Queue lengths at the level crossings have been adopted from the SIDRA assessment detailed above.

Table 6.6
Adjacent intersection impacts

| PRECINCT | ROAD WITH LEVEL CROSSING | DISTANCE TO ADJACENT INTERSECTIONS FROM LEVEL CROSSING APPROACHES | $2025$ <br> AVERAGE QUEUE (M) ON LEVEL CROSSING APPROACHES | $2040$ <br> AVERAGE QUEUE (M) ON LEVEL CROSSING APPROACHES |
| :---: | :---: | :---: | :---: | :---: |
| Albury | Tynan Road ${ }^{1}$ | East approach: 40m to Hume Highway West approach: 70m to Perryman Road | 4 | 22 |
| Greater <br> Hume - <br> Lockhart | Balfour Street ${ }^{1}$ | East approach: 60m to Melville Street West approach: 70m to Olympic | 156 | 294 |
|  | Sladen Street ${ }^{1}$ | East approach: 30m to Railway Parade West approach: 43m to Ivor St | 16 | 25 |
|  | Rosler Parade ${ }^{1}$ | East approach: 30m to Railway Parade West approach: 25 m to Henty Walla Rd | 16 | 25 |
|  | Plunkett Street ${ }^{1}$ | East approach: 25 m to Olympic <br> West approach: 30m to Finlayson lane | 16 | 25 |
|  | Yerong Street ${ }^{1}$ | North approach: 175 m to Nicholas Street South approach: 220 m to Olympic | 4 | 5 |
|  | Urana Street ${ }^{1}$ | East approach: 50m to Olympic Highway West approach: 15 m to Draper Smissen | 13 | 20 |
| Wagga <br> Wagga | Yarragundry Street ${ }^{1}$ | East approach: 70m to Olympic West approach 50m to Pearson | 10 | 15 |
|  | Fernleigh Road ${ }^{2}$ | East approach: 100 m to Barrima West approach: 60 m Bulolo | 304 | 724 |
|  | Bourke/Docker Street ${ }^{2}$ | North approach 20m to Chaston Street South approach 10m to Colman Street | 238 | 348 |
| Junee | Harefield Road ${ }^{1}$ | East approach: 120 m to Byrnes Road | 3 | 4 |
|  | Olympic Highway (between Seignior Street and Main Street ${ }^{2}$ | East approach: 20m to Main Street West approach: 35 m to Broadway | 62 | 80 |
|  | Waterworks Road ${ }^{1}$ | East approach: 20m to Waterworks Road West approach: 60 to Olympic Highway | 4 | 4 |
|  | Brabins Road ${ }^{1}$ | East approach: 155m o Morris Street West approach: 40 m to Olympic | 1 | 1 |
|  | Olympic Highway (Illabo) ${ }^{1}$ | West approach: 50 m to Warrens lane | 28 | 33 |

(1) Calculated as $5 \%$ of AADT / half of the two-way peak volume (which is $10 \%$ of AADT).
(2) Peak hour intersection count

Based on the average queue lengths calculated by SIDRA at public road level crossings, impacts to adjacent intersections during a level crossing closure may occur at the following level crossings.

- Balfour Street
- Urana Street
- Fernleigh Road
- Bourke/Docker Street
- Olympic Highway (Junee).

It is noted that these impacts to adjacent intersections would occur with or without the proposal. However, due to the increase in rail services (up to two daily services from 2025 to 2040) it would be more likely to occur.

### 6.4 RAIL NETWORK OPERATION

The proposal would not result in any change in operation of the existing rail network.

### 6.5 PARKING

As discussed in section 6.2, there would be no increases to road traffic as a result of the proposal.
At the Albury Station pedestrian bridge enhancement site, two parking spaces will not be re-instated after construction. These parking spaces would make way for a new DDA compliant ramp and associated adjustments to the existing pedestrian zebra crossing that together provide upgraded connectivity and accessibility between the station building and the pedestrian bridge. Engagement with TfNSW will be ongoing through subsequent design stages to investigate opportunities to ameliorate residual impacts to parking.

At the Wagga Wagga Station pedestrian bridge, three private parking spaces at the Multicultural Council of Wagga Wagga would be removed as the northern ramp would extend over these spaces. Opportunities to reinstate the parking spaces under the ramp would be investigated during detailed design.

### 6.6 ROAD SAFETY

As discussed in section 6.2 it is likely there would be no increases in road traffic as a result proposal.
The minor change to the intersection configuration at Railway Parade / Kemp Street / Olympic Highway in Junee is not expected to impact on the safety of road users at this location.

### 6.7 HEAVY VEHICLE ROUTES

As discussed in section 6.2, there would be no increases to road traffic as a result of the proposal.
Heavy vehicles would have a greater chance of being stopped at a level crossing, due to the increased frequency of level crossing closures as a result of the proposal. As outlined in section 6.3.7, under existing operations an activated level crossing would be closed for approximately two minutes during a $1,800 \mathrm{~m}$ train pass by at a typical speed of $80 \mathrm{~km} / \mathrm{h}$. This occurs under current operations and would not change with the operation of the proposal. As such, heavy vehicles are not expected to experience additional delay at existing, activated level crossings. However, due to the increased services (up to two daily services from 2025 to 2040) a level crossing closure is more likely to be encountered.

Potential short stacking issues at level crossings for heavy vehicles has been assessed and detailed in section 6.3.

### 6.8 TRAVELLING STOCK RESERVES

As discussed in section 6.3, movements on the road, such as stock movements, would have a greater chance of being stopped at a level crossing, due to the increased frequency of level crossing closures as a result of the proposal. This would result in minimal impact to the movement of stock across the corridor.

### 6.9 PUBLIC TRANSPORT ROUTES

As discussed in section 6.2, there would be no increases to road traffic as a result of the proposal.
Any changes to bus routes or bus stop infrastructure temporarily implemented during construction would be reinstated to the original configurations before the commencement of proposal operation.

Buses would have a greater chance of being stopped at a level crossing, due to the increased frequency of level crossing closures as a result of the proposal. Most of the bus services that may use level crossings within the study area are school bus services operating twice a day, and therefore the likelihood of being impacted by a passing train is minimal. However, if a bus is stopped at an active level crossing the level crossing closure time would be approximately two minutes for a $1,800 \mathrm{~m}$ train to pass by at a typical speed of $80 \mathrm{~km} / \mathrm{h}$. This occurs under current operations and would not change with the operation of the proposal for existing, activated level crossings.

### 6.10 ACTIVE TRANSPORT ROUTES

As discussed in section 6.2, there would be no increases to road traffic as a result of the proposal.
Enhancements of pedestrian rail crossings provide additional connectivity and Disability Discrimination Act (DDA) compliance for pedestrians and cyclists through the enhancement of active transport infrastructure at locations shown in Table 6.7. These enhancements may also help local councils achieve objectives for improving active transport infrastructure, such as those outlined in the Wagga Wagga Active Travel Plan.

Table 6.7 Active transport enhancements

| PRECINCT | ENHANCEMENT SITE | ACTIVE TRANSPORT ENHANCEMENT |
| :--- | :--- | :--- |
| Albury | Albury Station pedestrian bridge | Ramps to be provided at the eastern and western landings, <br> improving accessibility for a range of users, DDA compliance |
| Greater Hume - <br> Lockhart | Henty Yard clearances | Upgrade of Sladen Street level crossing with activated gated <br> pedestrian enclosure |
| Wagga Wagga | Cassidy Parade pedestrian bridge | Improved safety and quality of footpaths, DDA compliance |
|  | Wagga Wagga Station pedestrian <br> bridge | Improved safety and quality of footpaths, DDA compliance |
|  | Improved safety and quality of infrastructure with shared paths <br> provided on both sides of the road. Due to the road gradient, the <br> paths integrated on the bridge structure would not be DDA <br> compliant. ARTC is committed to revising the existing design <br> to achieve DDA compliance. To achieve this, it is expected that <br> a pedestrian bridge independent of the road bridge may be <br> required as a substitute for the footpath on one side of the road <br> bridge. |  |


| PRECINCT | ENHANCEMENT SITE | ACTIVE TRANSPORT ENHANCEMENT |
| :--- | :--- | :--- |
| Junee | Kemp Street bridge | Improved safety and quality of infrastructure. A shared path <br> would be provided on the northern side of Kemp Street from <br> Ducker Street to the Olympic Highway. No path would be <br> provided on the southern side, the path on the northern side of <br> bridge improves amenity and connectivity with footpath <br> network. Due to the road gradient, the paths integrated on the <br> bridge structure would not be DDA compliant. ARTC is <br> committed to revising the existing design to achieve DDA <br> compliance. To achieve this, it is expected that a pedestrian <br> bridge independent of the road bridge may be required as a <br> substitute for the footpath on one side of the road bridge. |

Pedestrians and cyclists would have a greater chance of being stopped at a level crossing, due to the increased frequency of level crossing closures as a result of the proposal.

The Cassidy Parade pedestrian bridge is an existing link in the Wagga Wagga Active Travel Plan. The proposed bridge design includes a ramp on the southern side of the rail corridor. Discussions are ongoing with Wagga Wagga City Council to align plans and minimise potential impacts on the final configuration of the future infrastructure.

As part of the enhancement works, existing pedestrian rail overpasses in Culcairn (adjacent to Balfour Street), and Junee (providing access to a station platform) are being removed, however, both are no longer used and their removal is not expected to have any impact to pedestrian connectivity.

### 6.11 PROPERTY ACCESS

Access to all properties in all precincts would be re-established post construction. There would be no ongoing operational impacts to properties, except for the Junee to Illabo clearances enhancement site, which will feature an upgraded (from passive to active) level crossing that provides access to the Shire and Carter private properties.

As discussed in section 6.3.6, an increase of 15 seconds in delay is expected at level crossing that are upgraded from passive to active. Furthermore, the increase of up to two daily services between 2025 and 2040 represents a minor increase in the likelihood of level crossing closures occurring at the property access. Due to the very low daily and hourly demand expected on the access, and the relatively low frequency of trains (conservatively, its assumed that a maximum of two services would operate in any one hour in 2040), the expected impact to property access, due to the proposed level crossing upgrade, is low.

## 7 CUMULATIVE IMPACTS

For an EIS, cumulative impacts can be defined as the successive, incremental, and combined effect of multiple impacts, which may in themselves be minor but could become significant when considered together. These impacts may result from multiple unrelated projects under construction concurrently that each add traffic to the road network and include:

- impacts to rail services
- additional delay at intersections
- additional queueing at intersections and level crossings
- reduction in road LOS performance.

The assessment of potential cumulative impacts has been undertaken in accordance with the SEARs, as detailed in the EIS, and considers the potential for impacts from other projects in the study area. The following tasks were undertaken to assess the potential for cumulative impacts:

- identifying potentially relevant projects in the study area (either proposed or approved) based on information available in the public domain
- screening identified projects for their potential to interact with the proposal
- identifying and assessing (quantitatively or qualitatively) the significance of potential cumulative impacts.

Additionally, the methodology used to assess road performance during construction and operation of the proposal assumes traffic growth factors for the background network that account for uplift in traffic due to traffic-generating developments in the area.

Potentially relevant projects in the study area were identified based on a search of the following data sources in May 2020:

- The Department of Planning, Industry and Environment's Major Projects register
- The NSW Independent Planning Commission project registers for the Albury City, Great Hume, Lockhart, Wagga Wagga City and Junee local government areas
- The NSW Southern Regional Planning Panel planning register
- proponent websites
- local council websites/DA tracking databases.

The projects identified were screened in relation to their potential for cumulative impacts with the proposal, based on:

- development size
- expected construction and operational periods
- potential to generate traffic during construction and operational periods
- proximity to the proposal site
- likelihood of sharing roads with the proposal.

Projects in the study area considered to have the potential for cumulative impacts with the proposal are shown on
Figure 7.1 and detailed in Table 7.1.


Figure 7-1 Major projects in the vicinity of the proposal

Table 7.1 Projects with the potential for cumulative impacts with the proposal

| PROJECT | DESCRIPTION | SITE LOCATION | POTENTIAL OVERLAP |
| :---: | :---: | :---: | :---: |
| Inland Rail - <br> Tottenham to <br> Albury (Victoria) | Upgrade of 305 km of existing rail corridor between the Victoria-NSW border at Albury and Melbourne. | Adjacent to Murray River bridge | Unlikely to share local road network. Construction routes may overlap on major highways. <br> Traffic assessment assumes a growth rate on the roads used by the proposal that accounts for traffic increases due to such developments. |
| Thurgoona Link Road | Construction of a new road that would provide connectivity to the Hume Freeway at Davey Road, plus an east-west link from Elizabeth Mitchell Drive to Kerr Road. | Adjacent to Billy Hughes bridge | Stage 2 adjacent to Billy Hughes bridge enhancement site is complete. Traffic assessment assumes a growth rate on the roads used by the proposal that accounts for traffic increases. |
| Nexus Industrial precinct | A 450ha site zoned to support large or heavy industrial development. | Adjacent to Billy Hughes bridge | Operational traffic likely to use Wagga Road and Hume Highway. <br> Traffic assessment assumes a growth rate on the roads used by the proposal that accounts for traffic increases due to such developments. |
| Jindera Solar Farm | 120 Megawatt (MW) solar farm with energy storage and associated infrastructure. | About 10km north west of Table Top Yard clearances | Construction of the Jindera Solar Farm is expected to be finished by start of construction of the proposal. Not expected share roads with proposal. |
| Glenellen Solar Farm | 200MW solar farm with energy storage and associated infrastructure. | About 14km north west of Table Top Yard clearances | Construction of the Glenellen Solar Farm is expected to be finished by start of construction of the proposal. Not expected share roads with proposal. |
| Walla Walla Solar Farm | A 300 (MW) solar farm and associated infrastructure. | About 6km south west of Culcairn Yard clearances | Construction of the Walla Walla Solar Farm is expected to be finished by start of construction of the proposal. During operation it is expected to generate up to 32 vehicle movements per day potentially using Olympic Highway. <br> Traffic assessment assumes a growth rate on the roads used by the proposal that accounts for traffic increases due to such developments. |


| PROJECT | DESCRIPTION | SITE LOCATION | POTENTIAL OVERLAP |
| :---: | :---: | :---: | :---: |
| Culcairn Solar Farm | 400MW solar farm with energy storage and associated infrastructure. | About 10 kilometres south west of Culcairn Yard clearances | Construction of the Culcairn Solar Farm is expected to be finished by start of construction of the proposal. During operation it is expected to generate up to 10 vehicle movements per day potentially using Olympic Highway. <br> Traffic assessment assumes a growth rate on the roads used by the proposal that accounts for traffic increases due to such developments. |
| Uranquinty Solar Farm | 5MW solar farm, battery storage and associated infrastructure. | About 2km southeast of Uranquinty Yard clearances | Expected traffic generation likely to use the Olympic Highway but is very low ( 15 vehicles per day). <br> Traffic assessment assumes a growth rate on the roads used by the proposal that accounts for traffic increases due to such developments. |
| Uranquinty Solar Farm | 200MW solar farm including, battery storage and associated infrastructure. | About 14 km north west of Uranquinty Yard clearances | Expected traffic generation not available. <br> May use Uranquinty level crossing and Olympic Highway. <br> Traffic assessment assumes a growth rate on the roads used by the proposal that accounts for traffic increases due to such developments. |
| Sandy Creek Solar Farm | 17MW solar farm including connection to the existing 22 kV line along the Olympic Highway, via a new switching station. | Directly north of Uranquinty Yard clearances | Expected to generate less than 50 daily vehicle movements during construction using Uranquinty level crossing and Olympic Highway. <br> Traffic assessment assumes a growth rate on the roads used by the proposal that accounts for traffic increases due to such developments. |
| Gregadoo Solar <br> Farm | 47MW solar farm and associated infrastructure. | About 12 km east of Uranquinty Yard clearances | Not expected share roads with proposal. |


| PROJECT | DESCRIPTION | SITE LOCATION | POTENTIAL OVERLAP |
| :---: | :---: | :---: | :---: |
| Wagga Wagga Special Activation precinct | The Wagga Wagga precinct covers an area of approximately 4,500 hectares, including 300 hectares already developed as part of the Bomen Industrial precinct. The precinct would focus on advanced manufacturing, agribusiness, and freight and logistics. | Surrounding Bomen Yard clearances | Promotes industrial and freight growth in the Bomen area north of Wagga Wagga. Increase in traffic may be seen on Olympic Highway, Byrnes Road, and Merino Road in vicinity of proposal. <br> Traffic assessment assumes a growth rate on the roads used by the proposal that accounts for traffic increases due to such developments. |
| Riverina Intermodal <br> Freight and <br> Logistics Hub | Construction of approximately 4.9-kilometre rail siding off the Main South Line and the intermodal freight terminal. | About 1 km north of the Bomen Yard clearances | Part of the Wagga Wagga Special Activation precinct. This assessment assumes a growth rate on the roads used by the proposal that accounts for traffic increases due to such developments. |
| Olympic Highway intersection upgrades | Upgrade of the Olympic Highway intersections at Old Narrandera Road and Travers Street, Wagga Wagga | About 3 km to the west of Bomen Yard clearances. About 4 km north of Wagga Wagga Station and Yard clearances | Construction may overlap with construction of the proposal. At peak, up to 120 heavy vehicles and 60 light vehicles would access the project each day. <br> Likely to cause additional construction traffic on the Olympic Highway. <br> Traffic assessment assumes a growth rate on the roads used by the proposal that accounts for traffic increases due to such developments. |
| Solar Farm - <br> Bomen | 5MW solar farm and associated infrastructure. | About 2 km south west of Bomen yard clearances | No vehicle volumes provided but noted as minor increases in traffic due to the proposal during construction. <br> Traffic assessment assumes a growth rate on the roads used by the proposal that accounts for traffic increases due to such developments. |
| Project <br> EnergyConnect (NSW - Eastern Section) | Development of a new transmission line ( 330 kV minimum) connecting Buronga Substation and Wagga Wagga Substation, and construction of the new Dinawan Substation (170km west of Wagga Wagga). | About seven kilometres south of Wagga Wagga station and yard clearances. <br> About 3 km to the south-west of Uranquinty Yard clearances. | Minimal overlap with the study area expected. <br> Likely to cause additional construction traffic on the Olympic Highway, Sturt Highway, Edward Street. <br> Traffic assessment assumes a growth rate on the roads used by the proposal that accounts for traffic increases due to such developments. |


| PROJECT | DESCRIPTION | SITE LOCATION | POTENTIAL OVERLAP |
| :---: | :---: | :---: | :---: |
| Humelink | Construction of a new 500 kV transmission line which will connect Wagga Wagga, Bannaby and Maragle. | About 14 km south of Wagga Wagga Station and Yard clearances <br> About 18 km to the south west of Uranquinty Yard clearances. | Expected traffic generation not available. Minimal overlap with the study area expected. <br> Likely to cause additional construction traffic on the Olympic Highway, Sturt Highway, Edward Street. <br> Construction is anticipated to commence in 2024. <br> Traffic assessment assumes a growth rate on the roads used by the proposal that accounts for traffic increases due to such developments. |
| Junee Station Upgrade | Upgrades to Junee Station to improve accessibility for those with a disability or limited mobility. | At Junee Station | The Junee Station Upgrade is expected to be finished by start of construction of the proposal. <br> No operational impacts. |
| Junee to Griffith Line Upgrade | Line upgrade work between Junee and Griffith to allow for increased train speeds to improve efficiency for freight carriers as part of the Fixing Country Rail program. | Adjacent to Junee Station | Construction of the Junee to Griffith Line Upgrade is expected to be finished by start of construction of the proposal. <br> Increased train numbers during operation are accounted for in the operational impact assessment. |
| Illabo Solar Farm | 80MW solar farm and associated on-site infrastructure, including a 132 kV substation and overhead transmission lines. | About six <br> kilometres south east of Junee to Illabo clearances | Traffic generation details not available. Will likely use Olympic Highway which is expected to have ample spare capacity based on similar solar farm projects. <br> Traffic assessment assumes a growth rate on the roads used by the proposal that accounts for traffic increases due to such developments. |
| Inland Rail - Illabo to Stockinbingal | Construction and operation of new rail and associated facilities to accommodate double stack freight trains up to 1800 metres long. | Adjacent to Junee to Illabo clearance | Unlikely to share local road network. Construction routes may overlap on major highways. <br> Traffic assessment assumes a growth rate on the roads used by the proposal that accounts for traffic increases due to such developments. |


| PROJECT | DESCRIPTION | SITE LOCATION | POTENTIAL OVERLAP |
| :--- | :--- | :--- | :--- |
| Grade separating <br> road interfaces | TfNSW is currently in the early <br> planning stages to grade separate <br> road and rail interfaces at four <br> locations where Inland Rail crosses <br> the NSW road network. | Intersects with the <br> Junee to Illabo <br> clearances | Details of construction timing and <br> traffic generation details not available. |
|  | The nearest grade separation <br> proposal is the Olympic Highway at <br> Harris Gates, located north of <br> Illabo. |  |  |

### 7.1 CONSTRUCTION

The proposal will connect into two other Inland Rail projects (Illabo to Stockinbingal and Tottenham to Albury). Both projects involve the upgrade of the existing rail lines. The generated construction traffic from these projects would be distributed over the length of the Illabo to Stockinbingal and the Tottenham to Albury project alignments, respectively. Shared construction access routes between these projects and the proposal would only be expected on highways and arterial roads. Cumulative impacts, such as additional delay and queuing, are expected to be minor due to the relatively low traffic generated by the proposal and the capacity of highways and arterial roads.

Proposed resource, logistics and infrastructure developments in the surrounding region would potentially be under construction in the same timeframe as the proposal. Due to the spatial separation of the majority of these developments and the enhancement sites, it is expected that any of the shared haulage routes are likely to be highways and arterial roads.

Based on the low traffic generation associated with the construction of the proposal, these arterial roads and highways would be appropriate to accommodate traffic movements for multiple projects. If any local roads are to be shared for construction access for adjacent sites, this would be managed through the approval process of the TMP.

The highest level of impacts during construction of the proposal result from the diversion of traffic within the Wagga Wagga urban area associated with the Edmondson Street bridge closure. Due to the unlikeliness of any concurrent project(s) construction movements significantly utilising the local streets supporting the diversions (Urana Street, Bourke Street, and Railway Street), it is not expected that there would be any cumulative impacts in this area. Project EnergyConnect is expected to use Edward Street, however Edward Street is a high capacity road that forms part of the Sturt Highway, and is expected to have ample capacity to accommodate additional traffic associated with the construction of Project EnergyConnect, even when diversionary routes are in place.

The grade separating road interfaces project by TfNSW is in its early stages of planning and the construction program is unknown. ARTC will continue to consult with TfNSW to be aware of the proposed construction timeframe to minimise cumulative impacts with works at the Junee to Illabo clearances enhancement site

Additionally, the methodology used to assess road performance assumes traffic growth factors that account for uplift in traffic due to traffic-generating developments in the area. The cumulative impacts of multiple projects are therefore not expected to cause additional delay, queuing, or other performance impacts beyond what has been assessed in Chapter 5 .

### 7.2 OPERATION

The proposal is not expected to generate any significant additional traffic during operation. Additionally, the Inland Rail program has the potential to reduce the overall number of trucks along the north south road corridors in the region by shifting freight movements from road-based transport to the rail corridor. The potential benefits that may accrue as a result of this modal shift include:

- fewer trucks on the road would reduce the impacts to road capacity and potentially delay the need for road capacity improvements
- fewer trucks on the road would reduce the impacts to the pavement on the roads and the overall maintenance costs required on these roads
- the reduction of long-haul truck movements on the road network has potential safety improvements for the local areas near the proposal and the wider road network
- the reduction of long-haul truck movements reduces the likelihood of an incident due to driver fatigue.

The operation of other transport infrastructure projects located in the vicinity of the proposal, are not expected to generate any operational traffic beyond that already included in growth estimates used to forecast traffic volumes. Therefore, operation of the proposal is not expected to have any cumulative impact.

Renewable energy projects located in the vicinity of the Albury to Illabo section of the Inland Rail corridor may generate daily light vehicle movement (staff movements) associated with each project. It is expected that any of the shared operational access routes between the proposal and these renewable energy developments would likely be on arterial roads and highways. Similar to the operation of the proposal, the renewable energy projects are not anticipated to generate a significant number of vehicle movements once operational and therefore are anticipated to have a negligible cumulative impact on the operation of the wider road network.

Industrial and logistics developments located in the vicinity of the Albury to Illabo section of the Inland Rail corridor are likely to generate daily light vehicle movements (staff movements) and freight related heavy vehicle trips associated with each project. The staff movements generated by these developments are expected to be dispersed across the road network and heavy vehicle trips generated by the industrial and logistics developments are expected to be primarily on highways. The proposal would not generate additional traffic during operation; as such, no impacts to the road network performance during operation of the proposal from vehicle movements would occur.

Additionally, the methodology used to assess road performance assumes traffic growth factors that account for uplift in traffic due to traffic-generating developments in the area. The cumulative impacts of multiple projects are therefore not expected to cause additional delay, queuing, or other performance impacts beyond what has been assessed in Chapter 6 .

The proposal includes upgrades to existing active transport infrastructure. These upgrades improve active transport accessibility and connectivity for a range of users. These upgrades may also help local councils achieve objectives for improving active transport infrastructure, such as those outlined in the Wagga Wagga Active Travel Plan.

As part of the grade separating road interfaces project, TfNSW propose to modify the Olympic Highway at Illabo, including removal of the existing level crossing (LX603). The proposal includes minor modification to the level crossing to accommodate the realigned track. The removal of a level crossing would provide a positive impact for road users utilising the Olympic Highway. ARTC will continue to consult with TfNSW to be aware of the final design solution of the grade separation project at the Olympic Highway level crossing (LX 603) to minimise cumulative impacts with works at the Junee to Illabo clearances enhancement site.

## 8 RECOMMENDED MITIGATION AND MANAGEMENT MEASURES

### 8.1 APPROACH TO MITIGATION AND MANAGEMENT

Environmental management for the proposal would be carried out in accordance with the environmental management approach as detailed in Chapter 27: Approach to mitigation and management of the EIS.

This would include a Traffic Management Plan (TMP) sub-plan, prepared as part of the Construction Environmental Management Plan (CEMP).

The TMP sub-plan would include (but is not limited to) the following management measures for impacts to the transport network (Table 8.1).

Table 8.1 Traffic management plan sub-plan

## TRAFFIC MANAGEMENT SUB-PLAN OUTLINE

| Objectives | - Ensure appropriate controls and procedures are implemented to minimise potential traffic, transport and access impacts. <br> - Identify appropriate traffic management measures and establish a framework for coordinating their implementation. <br> - Maintain network safety, journey times and congestion at acceptable levels. <br> - Ensure access to properties are maintained. |
| :---: | :---: |
| Purpose and requirements | - The plan will detail processes and responsibilities to minimise traffic and access delays and disruptions, and identify and respond to changes in road safety. <br> - The plan will be prepared in consultation with Transport for NSW; relevant councils; and public transport/bus operators (as relevant). <br> The plan will include measures to: <br> - identify haulage routes and access points <br> - identify and manage diversionary routes for motorists, cyclists and pedestrians, maintain access to individual residences, public transport services and infrastructure, services and businesses, and for livestock across the proposal site identify alternative routes for construction traffic activities in the event roads are closed by relevant authorities <br> - communicate changes in traffic conditions and access arrangements with relevant stakeholders provide safe routes for pedestrians and cyclists during construction <br> - minimise the number of changes to road users' travel paths <br> - manage the movements of construction-related traffic to minimise traffic and access disruptions in the public road network <br> - manage temporary access arrangements where required <br> _ provide a mechanism for the monitoring, review and amendment of the plan. |


| TRAFFIC MANAGEMENT SUB-PLAN OUTLINE |  |
| :---: | :---: |
| Relevant guidelines and standards | The plan will be prepared in accordance with relevant legislation, guidelines and standards, including: <br> - Roads act 1993 <br> - traffic control at work sites (roads and maritime services, 2018b) <br> - As 1742.3-2009: manual of uniform traffic control devices - traffic control for works on Roads. |
| Example management measures | Management measures to be included in the plan and implemented during construction will include (but not be limited to): <br> - adequate road signage will be provided to inform drivers and pedestrians of the work, timing and alternative access arrangements <br> - heavy vehicle movements will be minimised during peak traffic times <br> - measures to manage traffic flows around the area affected by construction will be provided, including required regulatory and directional signposting, line marking, variable message signs, and all other necessary traffic control devices <br> - consultation with relevant road authorities regarding the potential for preventative road improvements to be undertaken prior to construction to minimise potential road damage <br> - adequate signage for road and pedestrian diversions will be provided, clearly articulating alternative routes <br> - designated queuing and idling areas will be determined near work areas to minimise disruption to the local community <br> - appropriate controls will be established where vehicles are required to cross footpaths to access construction sites. This may include manual supervision, physical barriers or temporary traffic signals as required <br> - construction vehicles will park within the construction compound where practicable <br> - the timing of deliveries accessing the site will be programmed to ensure there is sufficient space within the proposal site to accommodate deliveries. |
| Related strategies, plans or requirements | - Road safety audits <br> - Road dilapidation report <br> - TMP s for each enhancement site. |

### 8.2 SUMMARY OF MITIGATION AND MANAGEMENT MEASURES

The mitigation measures to manage impacts to transport from the proposal during pre-construction, construction and operations are outlined in Table 8.2.

Table 8.2 Pre-construction, construction and operational mitigation measures

| IMPACT | MITIGATION MEASURE | TIMING |
| :---: | :---: | :---: |
| Road operations | Early consultation will be undertaken with road authorities (local councils and Transport for NSW) and public transport service providers for aspects of the proposal that may require changes to the road network. This includes consideration of temporary changes to signal phasing at intersections along the traffic diversion routes in Wagga Wagga during the Edmondson Street bridge closure. | Detailed design/ pre-construction |
| Bus services | Changes to bus routes and bus stops to mitigate impacts to bus services, including establishing temporary stops, would need to be planned in consultation with TfNSW, bus operators, and other key stakeholders such as schools to minimise the impact on community, public transport users, and service providers. | Detailed design/ pre-construction |
| Emergency Services | Consultation will be undertaken with emergency services to plan alternative routes that avoid the heaviest impacted areas of the road network during the Edmondson Street bridge and Kemp Street bridge closures and associated diversions to minimise travel time delay experienced by emergency service vehicles. <br> Consultation will also be undertaken with emergency services regarding the disruption to access on the Murray River. | Detailed design/ pre-construction |
| Stock movements | Prior to the commencement of works, Local Land Services will be notified of increased vehicle movements along the TSRs and temporary closures of any level crossings during the construction phase so that stock handlers, including walking permit holders, can be notified of the impacts to stock movements. | Detailed design/ pre-construction |
| Water based transport | Restrictions on navigation of the Murray River beneath and in the vicinity of the Murray River bridge site as result of the construction will be planned prior to commencing construction and handled in accordance with the Marine Safety Act 1998 (NSW). Transport for NSW will be notified of the proposed works and will be consulted in regard to Navigational marks, signage and marine notices. | Detailed design/ pre-construction |
| Impacts on existing roads | Consultation with Junee Shire Council will be undertaken regarding the potential for preventative road works, prior to road diversions in Junee on Joffre Street and Pretoria Avenue, to offset impacts from higher than typical traffic and heavy vehicle movements on some local roads due to diverted traffic. | Detailed design/ pre-construction |


| IMPACT | MITIGATION MEASURE | TIMING |
| :---: | :---: | :---: |
| Road safety | Development of Road Safety Audits (RSAs) and risk assessments, prior to commencement of construction, for each enhancement site where changes to the road network are required or where increased traffic movements or diversions during the construction phase may present an increased crash risk. These will be undertaken by the contractor and developed in accordance with the Austroads guidelines to provide for safe movements of construction vehicles on public roads, and will consider the safety of all road users. A safe system approach will be adopted to minimise harm caused to all road users through the use of appropriate road design features and speeds. | Detailed design/ pre-construction |
| Active transport connectivity | Construction staging will be planned to account for continued active transport connectivity during construction. | Detailed design/ pre-construction |
| Active transport integration | ARTC will continue to work with Wagga Wagga City Council on the integration of the new Cassidy Parade pedestrian bridge to align and minimise impacts to the Wagga Wagga Active Travel Plan. <br> Further work with Wagga Wagga City Council and Junee Shire Council will pursue and adopt, an alternative design that will provide DDA compliant access for pedestrians at Edmondson Street bridge and Kemp Street bridge. | Detailed design/ pre-construction/ construction |
| Impacts on existing roads | Appropriate signage and warnings, including variable messaging signs, will be considered in the Construction Traffic Transport and Access Management Plans. These will be deployed as considered appropriate in the vicinity of the enhancement sites to provide early warning for road users of disruptions due to construction activities and road closures. | Pre-construction/ construction |
| Road pavement | A Road Dilapidation Report will be prepared for all haul routes within each precinct. Should damage to the road occur as a result of construction, the damage will be rectified to restore the road to the pre-work condition as identified in the road dilapidation report or as otherwise agreed with the relevant road authority. Joffre Street and Pretoria Avenue will be monitored for damage during construction and any necessary repairs attended to as soon as possible. | Pre-construction/ <br> Construction |
| Impacts on existing roads | Heavy vehicle diversionary signage will be implemented to encourage the diversion of heavy vehicle traffic outside of Junee on the existing heavy vehicle routes via Goldfields Way and Old Junee Road during closure of the Kemp Street bridge. | Construction |


| IMPACT | MITIGATION MEASURE | TIMING |
| :---: | :---: | :---: |
| Access | Communication with relevant stakeholders will be undertaken regularly to minimise congestion and inconvenience to road users in areas affected by diversions, such as during the works for the replacement of the Edmondson Street Bridge in Wagga Wagga and Kemp Street Bridge in Junee, or level crossing closures (including full or partial closure). Stakeholders will include the relevant local council, bus operators, state government departments, emergency services and affected property owners/occupants. <br> The community will be notified in advance of pedestrian bridge closures and any proposed road or pedestrian network closures and diversions through signage, the local media and other appropriate forms of communication. <br> Appropriate wayfinding signage for road and pedestrian diversions will be provided, clearly articulating alternative routes. Consultation would also discuss opportunities for broader diversions away from congested roads. Additional measures identified as an outcome of consultation would be implemented during construction where practicable. | Construction |
| Road operations | The construction access off Cheshire Street to the Pearson Bridge enhancement site and Chaston Street to Wagga Wagga Station and surrounds will be designated a left in, left out turning movement only to limit any performance or safety impacts to the surrounding road network. | Pre-construction/ construction |
| Access | Where changes to access arrangements to businesses and residences are required as part of the proposal construction activities, ARTC will advise property owners/occupants and consult with them in advance regarding temporary disruption to existing accesses. Temporary changes to access arrangements during construction will include (but not limited to): <br> - Edmondson Street bridge <br> - Wagga Wagga station and surrounds <br> - Kemp Street bridge. | Pre-construction/ construction |
| Seasonal/ agricultural impacts | Special consideration would be given to enhancement sites that are located on land with agricultural storage or transportation infrastructure, such as grain silos, due to the high localised seasonal freight movements accessing them. <br> Detailed assessment of the site accesses will be undertaken as part of the Road Safety Audits and appropriate Construction Traffic Transport and Access Management Plans will be developed by the contractor in consultation with the site operator prior to commencement of construction activities on site to moderate any potential safety issues. | Pre-construction/ construction |
| Active travel | ARTC will continue to work with Wagga Wagga City Council on the integration of the new Cassidy Parade pedestrian bridge to align and minimise impacts to the Wagga Wagga Active Travel Plan. | Detailed design/ pre-construction/ construction |
| Level crossing safety | In accordance with national and state rail safety law requirements, public road crossings would be subject to an Interface Agreement with the relevant road manager in order to identify and minimise safety risks as far as practicable during operations. | Operation |


| IMPACT | MITIGATION MEASURE | TIMING |
| :--- | :--- | :--- |
| Level crossing <br> safety | Opportunities to consolidate low use level crossings will be progressed with key <br> stakeholders as per the Transport for NSW Level crossing closure policy where <br> appropriate. Any closures will be progressed in accordance with the requirements <br> of the Transport Administration Act 1988. | Pre-construction/ <br> construction |
| Parking | All parking impacted by the construction phase will be re-instated and lines <br> remarked to previous condition or better where necessary, with the exception of <br> Albury Station pedestrian bridge and the Wagga Wagga Station pedestrian bridge <br> enhancement site. <br> At the Albury Station pedestrian bridge enhancement site, two parking spaces <br> will not be re-instated after construction. These parking spaces will make way for <br> a new DDA compliant ramp. Engagement with TfNSW will be ongoing through <br> subsequent design stages to investigate opportunities to ameliorate residual <br> impacts to parking. | Operation |
| At the Wagga Wagga Station pedestrian bridge enhancement site, three private <br> parking spaces will not be re-instated after construction. Opportunities to reinstate <br> the parking spaces under the ramp would be investigated during detailed design. |  |  |
| Cumulative <br> impacts | ARTC will continue to consult with TfNSW to be aware of the final design <br> solution of the grade separation project at the Olympic Highway level crossing <br> (LX 603) and proposed construction timeframe to minimise cumulative impacts <br> with works at the Junee to Illabo clearances enhancement site. | Detailed design/ <br> pre-construction |

### 8.3 EFFECTIVENESS OF PROPOSED MITIGATION MEASURES

The mitigation measures specified above are anticipated to reduce the likelihood and/or consequence of the identified risks.

Transport elements with the potential for residual impact to transport users, local businesses and residents during the construction phase are:

- Wagga Wagga urban road network during the diversion of traffic associated with the Edmondson Street bridge closure
- cross rail active transport network connectivity in Wagga Wagga and Junee during closures of pedestrian rail crossing facilities.

If any issues are unable to be mitigated through the design, construction or operational process such as intersection performance during diversions or reduced pavement condition following the construction process (heavy vehicle activity), further consultation would be required to develop management measures to limit impacts as far as is practicable.

During operation of the proposal no residual impacts are expected.

## 9 CONCLUSION

The proposed Albury to Illabo section of Inland involves enhancement works to provide the increased vertical and horizontal clearances required for double-stacked freight trains. The proposal is generally within the existing active rail corridor between the towns of Albury and Illabo. Works are proposed at 24 locations along the 'Main South Line' corridor, described as 'enhancement sites' within four precincts aligned with the local government areas of Albury, Greater Hume and Lockhart, Wagga Wagga and Junee.

This report has provided a description of the existing conditions on the transport network, detailed expected construction activities and timeframes and presented an assessment of the impact of the construction and operation of the proposal.

It has found that the proposal would have different impacts during construction and operation as discussed below. The recommended mitigations have sought to identify and eliminate or minimise risks so far as is reasonably practicable during the construction and operational phases.

### 9.1 CONSTRUCTION IMPACTS

During construction, the movement of construction vehicles is expected to have minimal impact on the transport network. Although unlikely to occur, a conservative approach was taken in the assessment of construction vehicle impact on the road network by assuming that peak hour construction vehicle trips would occur during the existing network peak hour. The assessment found that an adequate level of service was maintained on the assessed roads and intersections affected by the additional traffic generated during construction in 2024. Due to the low construction traffic volumes generated by the proposal, impacts to other transport facilities such as public transport, heavy vehicle and active transport routes and Traveling Stock Reserves are not expected.

Road closures to facilitate construction in Henty, Wagga Wagga, and Junee would result in temporary localised road and intersection performance and travel time impacts, particularly in the denser urban area of Wagga Wagga. The traffic diversions associated with the Edmondson Street bridge closure would result in inappropriate LOS for E and F for some intersections and travel time impacts of up to nine minutes. In addition, this bridge closure would impact public and school bus routes requiring rerouting and alternative stop locations.

### 9.2 OPERATIONAL IMPACTS

Expected operational impacts would results from:

- increased daily train services resulting in an increased frequency of closures per day at level crossings
- increased delay where level crossings on private accesses have been upgraded from passive to active.

There would be no increases to road traffic as a result of the proposal.
The maximum rail service increase between 2025 and 2040 is up to two daily services. It is anticipated that the maximum closure time encountered at an active level crossing (with or without the proposal) would be 121 seconds. An assessment of active level crossing LOS was undertaken and found that all level crossings on public roads would operate at a delaybased LOS of A.

Amendments to the road network as part of the permanent works would not remove any existing turn movements and are not expected to impact on the current capacity or level of service of any intersections.

Short stacking deficiencies at the existing level crossings were assessed and potential deficiencies identified at two of the level crossings.

It is noted that all operational impacts would be expected to occur both with and without the proposal, however the likelihood of these impacts occurring is expected to increase due to the larger number of rail services per day.

### 9.3 MITIGATIONS

During construction of the proposal a Traffic Management Plan (TMP) sub-plan will be prepared as part of the Construction Environmental Management Plan (CEMP) detailing construction sites activities and impacted transport facilities and specify the mitigation measure to reduce the impacts. Key mitigation measures that will be undertaken include:

- road safety audits where changes to the road network are required or increased traffic movements during the construction phase may present an increased crash risk
- consultation with relevant stakeholders (state, local government, emergency services transport service providers and impacted property owners)
- heavy vehicle diversionary signage would be implemented to divert Heavy vehicle traffic outside of Junee on the existing heavy vehicle routes via Goldfields Way and Old Junee Road
- community notification of any proposed road or pedestrian network closures and diversions and provision of appropriate wayfinding signage for road and pedestrian diversions will be provided, clearly articulating alternative routes.
- rectification of pavement where necessary to support diversion of vehicles from the Olympic Highway to local roads in Junee
- restricted access to level crossings for oversize vehicles that may present a short-stacking risk

With these mitigation measures in place the proposal construction activities are expected to have minimal impact on the transport network. Residual traffic impacts are likely to be experienced during construction of the proposal, particularly associated with road closures and diversions in Wagga Wagga and Junee. The post-construction operation of the proposal has been shown to have no significant impact to the transport network in this assessment.

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## TECHNICAL PAPER <br> 

## Traffic and transport

## Appendix A Public level crossing treatment methodology

## Public level crossing treatment methodology

## Introduction

The key principles guiding the decision-making process for determining treatments at public road-rail interfaces includes:

- Using a risk-based decision-making process focused on minimising risk So Far As Is Reasonably Practicable (SFAIRP)
- Consistency in the determination of road-rail interface treatments across the projects of the Inland Rail Program
- Applying a consistent methodology to determine if the cost of the potential available treatment is grossly disproportionate to the level of risk to safety and the projected benefits
- Ensuring the feasibility of the Inland Rail Program by proposing cost-effective solutions.

An overview of the process followed in the assessment of road-rail interfaces across the proposal and the methodology followed in the development of road-rail interface treatments is outlined below.

## Process overview—determination of road rail interface treatments

## Identification of all potential road-rail interfaces within the proposal site

An important objective of level crossing investigations is the clear and accurate identification of all road-rail interfaces within the proposal site. The list of identified road-rail interfaces is then provided to the relevant road manager for review in order to ensure that all interfaces and the associated road infrastructure managers have been correctly identified.

## Identify opportunities to minimise the number of proposed road-rail interfaces

Initial consideration will be given to the elimination of level crossing risks by assessing all road-rail interfaces for closure. This is in line with the Transport for New South Wales (TfNSW) Level Crossing Closures Policy (n.d.), which notes that:
'in order to manage the risks to safety associated with road and rail interfaces, the closure of public and private level crossings in NSW is to be pursued, where it is practical and cost effective to do so'.

Road closures will only be progressed if endorsed by the relevant road manager.

## Review whether the road-rail interfaces meet the criteria for automatic grades separation

ARTC's policy is that road-rail interfaces will be automatically grade separated in the following three instances:

1. Road-rail interfaces with four rail tracks (current)
2. Road-rail interfaces of freeways and highways of four or more lanes (current and committed future plans)
3. Where grade separation is the logical option for topographical or other technical engineering reasons.

All other crossings will be assessed using the Inland Rail Level Crossing Risk Tool.

## Inland Rail Level Crossing Risk Tool

Where a road-rail interface is required, a methodology has been developed to identify what risk treatments should be implemented at individual road-rail interfaces as part of the Inland Rail project scope. This methodology is in the form of a formalised Level Crossing Risk Tool that identifies risk treatments and assists ARTC in being able to demonstrate that risks to safety would be managed SFAIRP for both new and existing road-rail interfaces.

The Australian Transport Council, in May 2003, agreed to adopt the Australian Level Crossing Assessment Model (ALCAM) as the only comprehensive level crossing assessment model in Australia. ALCAM is an assessment tool used to identify key potential risks at level crossings and assess the overall effects of proposed treatments. It does not specify what treatment is warranted at level road-rail crossing sites nor attempt to define a 'safe' or acceptable level of risk. This is a decision for each rail infrastructure manager.

In line with Office of the National Rail Safety Regulator (ONRSR) recommendation around the use of quantitative risk assessment techniques, a tool was developed which moved from a 'warrant' approach (e.g. decisions around control types based on basic metrics such as road type or traffic volumes) to a cost benefit analysis (CBA) approach for safety risk management. The approach uses ALCAM as one of the main inputs into the decision process for the recommended level of control at Inland Rail level crossings.

ARTC use a consistent methodology to develop all proposed road-rail interface treatments across the Inland Rail Program. In June 2020, the ONRSR finalised an audit of the Inland Rail Road-Rail Crossing Strategy, which included a number of the TfNSW level crossing interfaces on the N2N project. The audit recognised a consistent, systematic and comprehensive process for the assessment of level crossings is applied to determine adequate treatments, noting that the approach ensures level crossing safety risks are eliminated or minimised, SFAIRP. There were no findings or recommendations identified by the audit requiring action by ARTC.

Section 10 of ONRSR's Policy on Level Crossings (ONRSR, 2019) provides support for the use of ALCAM as follows:

> 'ONRSR accepts the use of ALCAM as a tool to help prioritise investment (when used in conjunction with other relevant factors, such as recent occurrence history). This tool has been endorsed by state and territory ministers.'

Consideration of factors other than ALCAM that may influence the recommended level of control are also taken into account, where relevant, on a case-by-case basis, including:

- Collision and near-collision history
- Traffic and transport impacts
- Local knowledge of driver or pedestrian behaviour.

The assessment incorporates a compliance check against AS1742.7-2016 Manual of uniform traffic control devices, Part 7: Railway crossings (Standards Australia, 2016).

Level crossing treatment (control) options considered as part of the process include:

- Installation of passive (stop sign) level crossings—compliant with AS1742.7-2016
- Installation of active level crossings (flashing lights and boom barriers)
- Grade separation
- Other treatments identified based on-site specific risks.

Active controls are where a device, such as flashing lights or boom barriers, is activated prior to and during the passage of a train through the level crossing.

## Cost benefit analysis

Part of the test as to whether risks have been managed SFAIRP is to determine whether the cost of the additional control is grossly disproportionate to the benefit gained via a CBA. From a financial perspective, three key inputs are required for the CBA:

1. The avoided cost if an additional risk control is implemented-the risk tool relies on ALCAM, which provides a quantitative measure of risk, which also enables the modelling of risk reduction generated by changing the controls at the level crossing. Risk reduction (benefits) can be calculated by comparing two risk scores for two scenarios, e.g. one level crossing with stop signs and one with flashing lights and boom barriers.
2. The cost of implementing the additional risk control-this is a combination of the capital cost of the additional control and the annual maintenance and repair cost over the life of the additional control.
3. What would be considered grossly disproportionate-from a legal perspective, the ONRSR Meaning of Duty to Ensure Safety So Far As Is Reasonably Practicable Guideline provides some guidance on what would be considered grossly disproportionate-the 'Grossly Disproportionate Factor' or GDF. The guideline suggests that the GDF may be dependent on the likelihood and consequence, with low risks having a factor of 2 and high risks having a factor of 10 .

## The use of ALCAM assessments in the determination of level crossing treatments

ALCAM assessments are undertaken for all proposed public road level crossings in the proposal site, thus providing a baseline risk score. The proposal functionality in the ALCAM system is used to model what the ALCAM risk score would be, assuming the introduction of Inland Rail. This incorporates forecast train speeds, volumes and train lengths. Updated road traffic counts, including a breakdown between light are heavy vehicles, are also collected for all public roads and included in this analysis.

If a crossing is assessed as being non-compliant for a passive stop sign control, the next level of control is applied. For example, if, based on the updated train speeds, sufficient sighting distance for a stop sign crossing as per AS 1742.7-2016 Manual of uniform traffic control devices Part 7: Railway crossings (Standards Australia, 2016) cannot be achieved, then the minimum control is flashing lights and boom barriers.

Even when a crossing is compliant for a passive stop sign control, the next level of control is modelled in ALCAM and a cost benefit/GDF analysis is undertaken, until the risk factor is reduced and a cost-effective level of crossing protection is established. For example, a passive control would be compared to a boom barrier control, which would then be compared to a grade separated control.

## Preliminary design

A preliminary level of design is first undertaken to confirm that a level crossing with the proposed control, which complies with the relevant standards, can be constructed. This design incorporates any road design standards that have been provided by the relevant road infrastructure manager.

Site-specific level crossing treatments are then reviewed with the respective road infrastructure managers as the project progresses through the design process.

## Interface agreements

In accordance with National and State Rail Safety Law requirements, all current and proposed public road crossings will be subject to an Interface Agreement.

## Conclusion

The objective is to develop a consistent methodology in the selection of level crossing treatments that is acceptable to key stakeholders and minimises risk SFAIRP.

## TECHNICAL PAPER <br> 

## Traffic and transport

## Appendix B Traffic counts

ALBURY TO ILLABO ENVIRONMENTAL IMPACT STATEMENT
$\pm=$


| $\begin{aligned} & \text { Time } \\ & \text { Period } \end{aligned}$ | Lgat | Ham | Toot |  |  |  |  |  |  |  |  |  |  |  | Hovere |  |  | Toot |  |  |  |  |  | \|anoumano |  |  | $\mid$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | enemome | $\frac{1}{\text { amomement }}$ |  | Peak hour volum |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5．00．51／15 | 1 | $\bigcirc$ | 1 | ${ }^{26}$ | 0 | ${ }^{26}$ | 2 | 1 | 2 | － | － | 0 | 2 | 1 | 3 | 5 | 4 | 8 | 4 | 1 | 5 | 0 |  | 2 | 7 | － | 7 | 5 | 0 | 5 |  | $\bigcirc$ | 1 | 0 | － | 0 | 4 | $\bigcirc$ | 4 | 7 | － | ${ }^{13}$ | $\bigcirc$ | － | 0 | 0 | － | 0 | ${ }_{78}$ | 00．6．00 |  |
| 5．15．530 | － | － | － | ${ }^{27}$ | － | ${ }^{28}$ | 3 | － | 3 | － | － | － | － | 1 | 1 | 5 | 4 | 10 | － | 1 | 10 | － | － | － | 10 | 1 | 11 | ${ }^{19}$ | － | 19 | 5 | 1 | 5 | － | － | － | 7 | $\bigcirc$ | 7 | 13 | 2 | 15 | 0 | － | － | － | － | $\bigcirc$ | ${ }^{109}$ | 5.15 .6 .6 |  |
| 53.3 | ， | ， | 2 | 51 | 1 | ${ }_{52}$ | 4 | ， | 5 | － | － | 。 |  | － |  | － | ${ }^{6}$ | ${ }^{14}$ | ${ }^{14}$ | 1 | ${ }^{14}$ | － | － |  | ${ }^{\prime}$ |  | ${ }^{18}$ | ${ }^{20}$ |  | ${ }^{20}$ | 10 |  | ${ }^{10}$ | － |  | 。 | ${ }^{14}$ |  | ${ }_{15}$ | ${ }^{18}$ | ${ }^{3}$ | ${ }^{20}$ | 1 | ， | 2 | － | － | － | ${ }^{173}$ |  |  |
| ${ }^{5455.600}$ | 1 | － | 2 | ${ }^{39}$ | 2 | 41 | 6 | 2 | 8 | － | － | － | 2 | － | 2 | － | 9 | 17 | 10 | 1 | 11 | － | － | 1 | ${ }^{21}$ | － | 22 | 19 | 1 | ${ }^{19}$ | 8 | 1 | 9 | － | － | － | ${ }^{12}$ | 4 | ${ }^{16}$ | 15 | 4 | ${ }^{19}$ | － | $\bigcirc$ | － | － | － | 0 | ${ }^{166}$ | S4．6．64 |  |
| 6．00．6．615 | 2 | － | 2 | 30 | 2 | 32 | 7 | ， | － | － | － | － | 5 | 1 | 6 | 12 | 8 | ${ }^{20}$ | ${ }^{14}$ | 1 | ${ }^{14}$ | － | ， |  | ${ }^{18}$ |  | 19 | ${ }^{24}$ | 2 | ${ }^{26}$ | 10 | 1 | 11 | － | － | 。 | 12 |  | ${ }^{13}$ | 11 | 2 | 14 | 1 | － | ， | － | － | 0 | ${ }^{167}$ |  | \％ |
| 6．15．6．30 | 2 | 1 | 3 | 42 | 2 | 4 | 5 | 1 | 5 | － | － | $\bigcirc$ | 5 | － | － | 16 | 6 | ${ }^{21}$ | 17 | 1 | ${ }^{18}$ | 1 | － | 1 | ${ }^{23}$ | 1 | ${ }^{23}$ | ${ }^{34}$ | 2 | ${ }^{36}$ | ${ }^{14}$ | 1 | ${ }^{16}$ | － | － | － | － | 3 | 12 | 19 | 4 | ${ }^{23}$ | 1 | 1 | 2 | － | － | 0 | ${ }^{21}$ | 6．15．7．15 | ${ }^{1364}$ |
| 6，30．645 | 5 | － | 5 | ${ }^{61}$ | 6 | ${ }^{67}$ | ${ }^{14}$ | 2 | ${ }^{15}$ | ， | － | 1 | － | 2 | 7 | ${ }^{19}$ | 10 | ${ }^{29}$ | ${ }^{2}$ | 5 | ${ }^{28}$ | 1 | ， | 2 | ${ }^{41}$ | 2 | ${ }^{43}$ | 51 | 2 | ${ }_{5}$ | ${ }^{18}$ | ， | ${ }^{19}$ | － | 。 | － | ${ }^{13}$ | 4 | ${ }^{17}$ | ${ }^{32}$ | 3 | ${ }_{3}$ | 1 | － | 2 | － | 。 | － | ${ }^{324}$ | 6．30，7：30 |  |
| ${ }_{6,455}$－7，00 | 5 | － | ${ }^{6}$ | ${ }^{25}$ | 4 | ${ }^{89}$ | ${ }^{21}$ | 4 | ${ }^{25}$ | － | － | － | － | 1 | 10 | 22 | － | ${ }^{28}$ | ${ }^{34}$ | 4 | ${ }^{38}$ | 2 | ＇ | 3 | ${ }^{48}$ | 2 | 49 | 75 | 2 | 7 | 2 | 3 | ${ }^{24}$ | － | － | － | ${ }^{25}$ | 1 | ${ }^{27}$ | 4 | 5 | 49 | 4 | 2 | ${ }^{-}$ | － | － | － | ${ }^{42}$ | ${ }^{6} 4.45 .745$ | ${ }^{178}$ |
| 7：00，7：15 | 8 | － | ${ }^{8}$ | ${ }^{73}$ | 9 | ${ }^{82}$ | 2 | 3 | ${ }^{25}$ | 0 | － | － | 10 | ${ }^{3}$ | ${ }^{13}$ | ${ }^{28}$ | 12 | 40 | ${ }^{26}$ | 4 | ${ }^{30}$ | 1 | $\bigcirc$ | 1 | ${ }^{33}$ | 1 | ${ }_{3}$ | ${ }^{6}$ | ${ }^{6}$ | ${ }^{69}$ | ${ }^{26}$ | 3 | ${ }^{27}$ | － | － | － | ${ }^{21}$ | ${ }^{3}$ | ${ }^{24}$ | ${ }^{3}$ | 4 | ${ }_{38}$ | 2 | 1 | ${ }^{3}$ | － | $\bigcirc$ | － | ${ }^{397}$ | 200．80 | 200 |
| r：15，－3， 30 | 4 | 1 | ${ }^{5}$ | ${ }^{82}$ | ${ }^{\circ}$ | ${ }_{87}$ | ${ }^{24}$ | 5 | ${ }^{29}$ | － | － | － | ${ }^{8}$ | 2 | 10 | ${ }^{25}$ | 5 | ${ }_{30}$ | ${ }^{30}$ | 2 | ${ }^{32}$ | 2 | － | 2 | ${ }^{47}$ | 2 | 49 | ${ }^{63}$ | 3 | ${ }^{66}$ | ${ }^{27}$ | 0 | ${ }^{28}$ | － | － | － | ${ }^{28}$ | 5 | ${ }^{32}$ | 4 | 4 | ${ }_{4}$ | 3 | － | 3 | － | － | 0 | 419 | 715．8．15 |  |
| ${ }^{7} 38.3$－7，45 | 7 | 1 | － | ${ }_{88}$ | － | ${ }^{4}$ | ${ }^{31}$ | 4 | ${ }^{34}$ | 1 | － | ， | ${ }^{10}$ | 2 | 12 | ${ }^{30}$ | 8 | ${ }_{38}$ | ${ }^{2}$ | 2 | ${ }^{30}$ | 1 | － | 1 | ${ }_{53}$ | 2 | ${ }_{5}$ | 80 | 5 | ${ }^{85}$ | ${ }^{24}$ | 3 | ${ }^{27}$ | － | － | － | ${ }^{34}$ | 4 | ${ }_{3}$ | 56 | 7 | ${ }_{6}$ | 3 | － | 3 | － | － | － | ${ }^{488}$ | 30．80 | 281 |
| ${ }_{7} 74.45$ | 7 | 3 | 10 | ${ }^{120}$ | 8 | ${ }^{128}$ | ${ }^{51}$ | 4 | ${ }_{55}$ | 2 | － | 2 | ${ }_{18}$ | 3 | ${ }^{21}$ | ${ }^{29}$ | 7 | ${ }_{36}$ | ${ }^{39}$ | 3 | 42 | 4 | 1 | 5 | 74 | 2 | 76 | 102 | 2 | 104 | ${ }^{21}$ | 5 | ${ }^{26}$ | － | － | － | ${ }^{35}$ | 3 | ${ }^{38}$ | ${ }^{7}$ | 5 | ${ }^{78}$ | 5 | ， | ${ }^{\circ}$ | － | － | 0 | ${ }^{626}$ | 7．45．845 |  |
| ${ }^{\text {8．00．} 8.15}$ | 7 | 2 | ， | ${ }^{125}$ | 7 | ${ }^{132}$ | ${ }^{53}$ | 5 | ${ }_{57}$ | 2 | － | 2 | ${ }^{21}$ | 3 | ${ }^{24}$ | 32 | 7 | ${ }^{39}$ | ${ }^{34}$ | 3 | ${ }_{3}$ | － | ， | 7 | 70 | 3 | ${ }^{7}$ | ${ }^{102}$ | 3 | ${ }^{105}$ | ${ }^{2}$ | 3 | ${ }^{29}$ | － | － | － | ${ }^{35}$ | 3 | ${ }^{38}$ | 7 | 7 | ${ }^{80}$ | ： | ， | － | － | － | － | ${ }^{00}$ | 800.900 |  |
| 8：15．830 | － | 1 | 7 | ${ }_{132}$ | 5 | ${ }^{137}$ | 7 | 3 | ${ }^{7}$ | 1 | － | 1 | ${ }^{26}$ | 2 | ${ }^{28}$ | ${ }^{30}$ | 8 | ${ }^{38}$ | ${ }^{38}$ | 3 | 40 | 5 | － | 5 | ${ }^{\circ}$ | 4 | 72 | ${ }^{124}$ | 5 | ${ }^{129}$ | ${ }^{32}$ | 7 | 40 | 0 | － | 0 | 50 | 5 | ${ }^{54}$ | ${ }^{\circ}$ | ， | ${ }^{9}$ | 7 | ＇ | ${ }^{8}$ | － | － | － | ${ }^{127}$ | 8．15．9．975 |  |
| ${ }^{830} \mathbf{0 , 8 4 5}$ | － | 2 | 10 | ${ }_{149}$ | 5 | ${ }^{158}$ | ${ }^{13}$ | 4 | $\pi$ | 3 | － | 3 | ${ }^{21}$ | 3 | ${ }^{24}$ | ${ }^{3}$ | 8 | 41 | ${ }^{47}$ | 4 | 50 | 4 | 1 | 5 | ${ }^{8}$ | 1 | ${ }_{82}$ | 104 | 5 | ${ }^{109}$ | ${ }^{28}$ | 3 | ${ }^{3}$ | － | － | － | 49 | 4 | ${ }_{5} 5$ | 7 | 7 | ${ }^{78}$ | 5 | ， | 5 | － | － | － | ${ }^{73}$ | 430．930 |  |
| 8．45．900 | 8 | 2 | 10 | ${ }^{125}$ | － | ${ }^{131}$ | ${ }^{58}$ | 8 | ${ }_{6}$ | ＇ | － | 1 | ${ }^{18}$ | 3 | ${ }^{21}$ | ${ }^{34}$ | 8 | ${ }_{4}$ | ${ }^{35}$ | 2 | ${ }^{37}$ | 5 | ＇ | 7 | ${ }^{6}$ | 4 | 70 | ${ }^{112}$ | 5 | ${ }^{117}$ | ${ }^{34}$ | 5 | ${ }^{38}$ | － | － | － | ${ }^{47}$ | 7 | ${ }_{5}$ | ${ }^{73}$ | 7 | ${ }^{\text {so }}$ | 3 | 1 | 4 | － | － | － | ${ }^{679}$ | ${ }^{\text {8，45 945 }}$ |  |
| 9.00 | 8 | 2 | 10 | 97 | 6 | ${ }^{103}$ | ${ }^{56}$ | 5 | ${ }^{62}$ | 2 | － | 2 | ${ }^{28}$ | 5 | ${ }^{32}$ | ${ }^{40}$ | 6 | ${ }^{46}$ | ${ }^{37}$ | 5 | ${ }_{4}$ | 8 | 1 | $\stackrel{ }{ }$ | ${ }_{53}$ | 3 | ${ }_{56}$ | 95 | 4 | 98 | ${ }^{17}$ | 5 | 22 | － | － | － | ${ }^{37}$ | 3 | 40 | ${ }_{6}$ | 5 | ${ }^{71}$ | 8 | － | $\stackrel{1}{8}$ | － | － | 0 | ${ }^{603}$ | 9．000－10．00 |  |
| 9，15．930 | 7 | 1 | ： | ${ }^{8}$ | 7 | so | 4 | 5 | 52 | 1 | ， | 2 | ${ }^{27}$ | 4 | ${ }^{31}$ | ${ }^{39}$ | 7 | 46 | ${ }^{35}$ | 2 | ${ }^{37}$ | 10 | 1 | 11 | 51 | 2 | 53 | 79 | 5 | ${ }^{83}$ | ${ }^{25}$ | 5 | ${ }^{30}$ | － | － | － | ${ }_{3}$ | 5 | 42 | ${ }_{5}$ | － | ${ }^{65}$ | 5 | ， | 7 | － | － | － | ${ }_{57}$ | ${ }^{\text {m Paei }}$ |  |
| 930 | － | 2 | 10 | 82 | 2 | ${ }^{84}$ | ${ }_{4}$ | － | ${ }_{5} 5$ | ， | ， | 2 | ${ }^{30}$ | 3 | ${ }^{33}$ | ${ }^{39}$ | 5 | ${ }^{4}$ | ${ }^{24}$ | 4 | ${ }^{38}$ | 7 | － | 7 | 45 | 2 | 47 | 72 | 5 | ${ }^{76}$ | 13 | － | ${ }^{19}$ | － | － | 0 | ${ }^{24}$ | － | ${ }^{30}$ | ${ }^{6}$ | － | 71 | 7 | ＇ | \％ | － | － | $\bigcirc$ | ${ }^{521}$ |  |  |
| 9， 4 5－10．00 | － | 1 | 10 | ${ }^{82}$ | 5 | ${ }_{8}$ | ${ }^{54}$ | 3 | ${ }_{5}$ | ， | － | 1 | ${ }^{31}$ | 4 | ${ }_{3}$ | ${ }_{3}$ | 5 | ${ }^{43}$ | ${ }^{26}$ | 4 | ${ }^{30}$ | 7 | － | 7 | ${ }_{4}$ | 2 | 50 | ${ }^{78}$ | 3 | ${ }^{82}$ | ${ }^{18}$ | 4 | 2 | － | － | － | ${ }^{27}$ | 4 | ${ }^{32}$ | ${ }^{2}$ | － | ${ }_{68}$ | － | ＇ | 7 | － | － | $\bigcirc$ | 51 |  |  |
| ${ }^{\text {an }}$ | ${ }^{107}$ | ${ }^{21}$ | ${ }^{128}$ | 1801 | ${ }^{8}$ | 1689 | ${ }_{6} 6$ | ${ }^{64}$ | 712 | 16 | 2 | 18 | ${ }^{27}$ | ${ }^{43}$ | ${ }^{320}$ | ${ }_{4}^{49}$ | ${ }^{139}$ | ${ }^{630}$ | ${ }^{533}$ | 51 | ${ }^{54}$ | ${ }^{6}$ | 12 | 7 | ${ }^{876}$ | ${ }^{34}$ | 910 | 1320 | ${ }^{60}$ | 1380 | ${ }^{37}$ | ${ }^{58}$ | ${ }^{435}$ | 1 | $\bigcirc$ | 1 | ${ }^{520}$ | ${ }^{6}$ | ${ }^{565}$ | 91 | ${ }^{106}$ | 1017 | 70 | ${ }^{14}$ | ${ }^{85}$ | $\bigcirc$ | 1 | 1 | 357 |  |  |
| ${ }^{\text {an Peak }}$ | 30 | 7 | ${ }^{37}$ | ${ }_{52}$ | 22 | ${ }_{554}$ | 255 | ${ }^{20}$ | 275 | 7 | $\bigcirc$ | 7 | ${ }^{6}$ | 0 | ${ }^{96}$ | ${ }^{128}$ | ${ }^{31}$ | 160 | 153 | 12 | 18 | 21 | 4 | 25 | ${ }^{287}$ | 11 | ${ }^{298}$ | 44 | ${ }^{18}$ | 460 | ${ }^{11}$ | 19 | ${ }^{138}$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | ${ }^{181}$ | ${ }^{18}$ | 199 | 300 | 30 | 330 | 2 | 3 | 26 | － | $\bigcirc$ | $\bigcirc$ | 278 |  |  |
| Tonr Toasi | ${ }^{28}$ | ${ }_{3}$ | ${ }^{336}$ | 339 | 132 | 392 | 1431 | ${ }^{108}$ | 1539 | ${ }_{3}$ | 2 | 38 | ${ }_{68} 8$ | 65 | ${ }^{75}$ | 1775 | 248 | ${ }_{198}$ | 153 | 79 | 1613 | 190 | 18 | 208 | 1138 | ${ }_{6}$ | ${ }^{1773}$ | ${ }^{3311}$ | ${ }^{128}$ | 339 | 1960 | ${ }_{14}$ | ${ }^{1222}$ | 4 | $\bigcirc$ | 4 | 1071 | ${ }_{13}$ | ${ }^{1207}$ | ${ }^{1788}$ | 236 | 199 | 152 | 30 | ${ }_{182}$ | 1 | － | 2 | ${ }_{18982}$ |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Period | Ligh | Hear | Toala | Light | Hasy | Tout | Ligh | Hamy | Toat | Ligh | Haxy | Toba | Light | Heany | To | Leg | Heary | Toal | Lagt | Ham | Toal | Ligh | Hany | Tobal | Ligh | Heany | Total | mt | Heary | Tom | ， | Hamy | Toat | Light | Hamy | Tobal | Light | Heay | T | Lght | Heary |  | 号 | Haay | Total | Light | Haxy | Total | Toteren |  |  |
| 14：00－14．15 | 8 | 2 | 10 | ${ }^{67}$ | 5 | 72 | ${ }_{5}$ | 4 | ${ }^{57}$ | ${ }^{1}$ | － | 1 | ${ }^{33}$ | 1 | ${ }^{34}$ | ${ }^{6}$ | 5 | ${ }^{71}$ | ${ }^{35}$ | 1 | ${ }^{37}$ | ${ }^{8}$ | $\bigcirc$ | ${ }^{8}$ | ${ }^{32}$ | 3 | ${ }_{35}$ | ${ }^{75}$ | 4 | ${ }^{78}$ | ${ }^{23}$ | ${ }^{6}$ | ${ }^{29}$ | 0 | － | $\bigcirc$ | ${ }^{23}$ | 3 | ${ }^{26}$ | ${ }^{43}$ | 7 | ${ }_{50}$ | ${ }^{6}$ | － | ${ }^{6}$ | $\bigcirc$ | － | $\bigcirc$ | 516 | ${ }^{14.400-1500}$ |  |
| 14.45 | ${ }^{14}$ | 1 | 15 | ${ }^{65}$ | 3 | ${ }^{68}$ | ${ }^{45}$ | 3 | ${ }^{47}$ | － | $\bigcirc$ | － | ${ }^{26}$ | 1 | ${ }^{27}$ | ${ }^{6}$ | 5 | ${ }^{69}$ | 4 | ${ }^{3}$ | ${ }^{47}$ | ${ }^{11}$ | 1 | ${ }^{11}$ | ${ }^{34}$ | 3 | ${ }_{3}$ | ${ }^{82}$ | 6 | ${ }^{88}$ | ${ }^{27}$ | 4 | ${ }^{30}$ | － | － | － | ${ }^{18}$ | 5 | ${ }^{22}$ | ${ }^{42}$ | 11 | ${ }_{53}$ | 5 | ＇ | ${ }^{6}$ | － | $\bigcirc$ | － | ${ }^{521}$ | 15－15：15 |  |
| 14330.14 .45 | 10 | 1 | 11 | ${ }^{73}$ | 3 | ${ }^{76}$ | ${ }_{50}$ | 2 | ${ }^{52}$ | 2 | － | 2 | ${ }_{3}$ | ${ }^{4}$ | ${ }^{39}$ | ${ }^{65}$ | ${ }^{6}$ | ${ }^{71}$ | 45 | 3 | ${ }^{48}$ | ${ }^{8}$ | 1 | $\stackrel{ }{ }$ | ${ }_{3}^{6}$ | 2 | ${ }^{38}$ | ${ }^{6}$ | 5 | 91 | ${ }^{27}$ | ${ }^{6}$ | ${ }^{32}$ | － | － | － | ${ }^{24}$ | 3 | ${ }^{27}$ | ${ }^{40}$ | 8 | ${ }_{48}$ | 7 | ＇ | 8 | $\bigcirc$ | － | $\bigcirc$ | ${ }^{553}$ |  |  |
| 14.455 .1500 | ${ }^{12}$ | 1 | ${ }^{14}$ | ${ }^{82}$ | 4 | ${ }_{8} 8$ | 43 | 3 | ${ }^{47}$ | 2 | － | 2 | ${ }^{29}$ | － | ${ }^{29}$ | 50 | 5 | ${ }_{55}$ | 4 | 3 | ${ }^{47}$ | － | － | $\stackrel{ }{ }$ | ${ }^{4}$ | 2 | 46 | ${ }^{9}$ | 4 | ${ }_{9}$ | ${ }^{26}$ | 6 | ${ }^{32}$ | － | － | － | ${ }^{24}$ | 6 | ${ }_{30}$ | ${ }^{45}$ | $\stackrel{8}{8}$ | ${ }_{54}$ | 7 | 1 | ${ }^{8}$ | $\bigcirc$ | － | － | ${ }^{553}$ | 14.45 .15 .45 |  |
| 155001515 | 10 | 3 | ${ }^{13}$ | ${ }_{95}$ | 5 | 100 | ${ }^{54}$ | 5 | ${ }_{5} 9$ | 2 | － | 2 | ${ }_{31}$ | 2 | 34 | ${ }^{\circ}$ | 7 | ${ }^{67}$ | 4 | 1 | 46 | $\stackrel{ }{ }$ | $\bigcirc$ | $\stackrel{ }{ }$ | ${ }^{43}$ | 1 | 44 | ${ }^{130}$ | 4 | ${ }^{135}$ | ${ }^{35}$ | 5 | 40 | － | － | 0 | ${ }^{33}$ | 4 | ${ }^{37}$ | 51 | 11 | ${ }^{62}$ | 5 | ， | ${ }^{-}$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | ${ }_{62}$ |  |  |
| 15.15 .15 .350 | ${ }^{12}$ | 1 | ${ }^{13}$ | ${ }_{9}$ | 5 | 101 | ${ }^{50}$ | ${ }^{3}$ | ${ }_{5}$ | 1 | $\bigcirc$ | 1 | ${ }^{27}$ | 2 | ${ }^{28}$ | ${ }^{68}$ | ${ }^{5}$ | ${ }^{73}$ | ${ }^{47}$ | 2 | ${ }^{49}$ | ${ }^{6}$ | $\bigcirc$ | 7 | 4 | ${ }^{6}$ | 50 | ${ }^{129}$ | 5 | ${ }^{133}$ | 40 | 5 | 4 | － | $\bigcirc$ | $\bigcirc$ | ${ }^{31}$ | 3 | ${ }^{34}$ | ${ }_{4}$ | ${ }^{8}$ | ${ }^{57}$ | 5 | 2 | 7 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | ${ }^{651}$ |  |  |
| $14350.15,45$ | 16 | $\bigcirc$ | ${ }^{16}$ | ${ }^{113}$ | 2 | ${ }_{115}$ | ${ }^{57}$ | 3 | ${ }^{60}$ | ， | － | 1 | ${ }^{27}$ | 1 | ${ }^{29}$ | 5 | 5 | ${ }^{62}$ | 70 | ${ }_{4}$ | ${ }^{74}$ | ${ }^{8}$ | － | ${ }^{8}$ | ${ }_{38}$ | 2 | ${ }_{4}$ | ${ }^{113}$ | 7 | ${ }^{120}$ | ${ }_{37}$ | 5 | ${ }_{4}$ | － | － | － | ${ }^{33}$ | 5 | ${ }^{38}$ | 52 | 9 | ${ }^{61}$ | 4 | 1 | 5 | － | － | $\bigcirc$ | ${ }^{672}$ | 15350.1830 |  |
| 15.45 .16 .00 | ${ }^{12}$ | 1 | ${ }^{13}$ | ${ }^{102}$ | 2 | ${ }^{104}$ | ${ }^{53}$ | ${ }^{3}$ | ${ }_{56}$ | 1 | $\bigcirc$ | 1 | ${ }^{27}$ | 1 | ${ }^{28}$ | ${ }^{6}$ | ${ }^{6}$ | 72 | 59 | 4 | ${ }^{6}$ | ${ }^{8}$ | $\bigcirc$ | 8 | ${ }^{39}$ | ${ }^{2}$ | ${ }^{4}$ | ${ }^{106}$ | ${ }^{6}$ | ${ }^{113}$ | ${ }^{39}$ | 5 | 4 | － | $\bigcirc$ | $\bigcirc$ | 41 | ${ }^{3}$ | ${ }^{45}$ | 56 | 10 | ${ }^{66}$ | 5 | ${ }^{2}$ | 7 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | ${ }^{663}$ |  |  |
| 18.0001615 | 11 | 2 | ${ }^{13}$ | ${ }^{120}$ | 2 | ${ }^{122}$ | ${ }^{52}$ | ${ }^{4}$ | ${ }_{56}$ | 3 | $\bigcirc$ | ${ }^{3}$ | ${ }^{30}$ | 2 | 32 | 70 | ${ }^{4}$ | ${ }^{74}$ | ${ }^{5}$ | 1 | ${ }_{5}$ | ${ }^{\circ}$ | ${ }^{1}$ | 10 | ${ }^{4}$ | 2 | ${ }^{45}$ | ${ }^{121}$ | 5 | ${ }^{126}$ | ${ }^{47}$ | 3 | ${ }^{\text {so }}$ | － | － | － | ${ }^{24}$ | 5 | ${ }^{29}$ | ${ }^{49}$ | ${ }^{8}$ | ${ }_{57}$ | 5 | 1 | ${ }^{6}$ | － | － | $\bigcirc$ | ${ }^{67}$ | 18.00 －1700 |  |
| 16，15． 16.50 | ${ }^{13}$ | － | ${ }^{13}$ | ${ }^{105}$ | 1 | ${ }^{106}$ | ${ }^{40}$ | 2 | 42 | 1 | $\bigcirc$ | 1 | 22 | 2 | ${ }^{24}$ | 71 | $\stackrel{ }{ }$ | ${ }^{81}$ | ${ }^{48}$ | ＇ | so | $\cdot$ | ＇ | 7 | 47 | 1 | ${ }_{48}$ | ${ }^{118}$ | 2 | ${ }^{120}$ | 4 | ${ }^{4}$ | ${ }^{48}$ | － | $\bigcirc$ | － | ${ }^{32}$ | 3 | ${ }_{3}$ | ${ }^{48}$ | 8 | ${ }_{56}$ | 5 | ${ }^{\prime}$ | ${ }^{\circ}$ | － | － | $\bigcirc$ | ${ }^{637}$ | 517 |  |
| 18330.184 .4 | 13 | 1 | 15 | ${ }^{112}$ | 3 | ${ }_{115}$ | ${ }^{50}$ | 1 | ${ }_{51}$ | 1 | $\bigcirc$ | 1 | 21 | $\bigcirc$ | 21 | ${ }^{3}$ | ${ }^{6}$ | ${ }^{69}$ | ${ }^{67}$ | 1 | ${ }^{6}$ | － | $\bigcirc$ | 6 | ${ }_{46}$ | 1 | ${ }_{4}^{47}$ | ${ }^{118}$ | 4 | ${ }^{121}$ | ${ }_{4}^{4}$ | 3 | 51 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | ${ }^{33}$ | 4 | ${ }^{37}$ | ${ }_{4}$ | 4 | ${ }_{50}$ | 5 | $\bigcirc$ | 5 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | ${ }_{6} 68$ | 18350.1730 |  |
| 18.45 .1700 | 12 | 1 | ${ }^{13}$ | ${ }^{13}$ | 1 | ${ }^{114}$ | ${ }^{43}$ | ${ }^{3}$ | ${ }^{46}$ | 1 | $\bigcirc$ | 1 | ${ }^{20}$ | 2 | 22 | ${ }^{81}$ | ${ }^{\circ}$ | ${ }^{87}$ | ${ }^{67}$ | 1 | ${ }^{68}$ | $\stackrel{ }{ }$ | $\bigcirc$ | $\stackrel{ }{ }$ | 50 | 1 | 51 | ${ }^{128}$ | 2 | ${ }^{131}$ | 43 | 5 | ${ }^{48}$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | ${ }^{26}$ | ${ }^{3}$ | 30 | ${ }^{47}$ | ${ }^{8}$ | ${ }_{55}$ | 5 | 1 | ${ }^{6}$ | 0 | $\bigcirc$ | $\bigcirc$ | ${ }^{681}$ | 16.45 －1745 |  |
| 17700－77．15 | 11 | 1 | 12 | ${ }^{115}$ | 1 | ${ }^{116}$ | ${ }^{33}$ | 3 | ${ }_{36}$ | 1 | － | 1 | ${ }^{17}$ | － | ${ }^{17}$ | ${ }^{\circ}$ | 3 | ${ }^{99}$ | 59 | $\bigcirc$ | 59 | 4 | $\bigcirc$ | 4 | ${ }^{45}$ | 1 | 46 | ${ }^{119}$ | 5 | ${ }^{124}$ | 57 | ${ }^{6}$ | ${ }^{6}$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | ${ }^{28}$ | 4 | ${ }^{32}$ | 4 | 8 | ${ }^{49}$ | 4 | ${ }^{1}$ | 5 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | ${ }_{684} 6$ | 18.00 |  |
| 17：15，17：30 | 9 | $\bigcirc$ | 9 | ง | 1 | ${ }^{101}$ | ${ }^{40}$ | 2 | ${ }^{42}$ | 1 | 0 | 1 | 19 | ${ }^{3}$ | 21 | ${ }^{82}$ | 7 | ${ }^{89}$ | ${ }_{6}$ | ＇ | ${ }^{67}$ | 4 | $\bigcirc$ | 4 | 52 | $\bigcirc$ | 52 | 127 | 2 | ${ }^{129}$ | ${ }^{54}$ | 4 | ${ }^{57}$ | ＇ | － | 1 | ${ }^{38}$ | 2 | 40 | 41 | ${ }^{8}$ | 49 | 4 | $\bigcirc$ | 4 | 0 | 0 | $\bigcirc$ | ${ }_{688}$ |  |  |
| 1730． 17.45 | $\stackrel{ }{ }$ | $\bigcirc$ | $\stackrel{ }{ }$ | ${ }^{109}$ | 1 | ${ }^{109}$ | ${ }^{3}$ | 2 | ${ }^{36}$ | $\bigcirc$ | － | $\bigcirc$ | ${ }^{19}$ | $\bigcirc$ | ${ }^{19}$ | $\pi$ | 7 | ${ }^{84}$ | ${ }^{6}$ | $\bigcirc$ | 61 | ${ }^{\circ}$ | $\bigcirc$ | ${ }^{6}$ | ${ }^{39}$ | 1 | ${ }^{41}$ | ${ }^{117}$ | 3 | ${ }^{120}$ | 4 | ${ }^{4}$ | ${ }^{48}$ | － | $\bigcirc$ | $\bigcirc$ | ${ }^{29}$ | 4 | ${ }^{33}$ | ${ }_{36}$ | 5 | ${ }^{40}$ | 2 | ${ }^{1}$ | ${ }^{3}$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | ${ }^{609}$ | 17330 －1830 |  |
| 17，45．18，00 | 4 | － | 5 | ${ }_{88}$ | $\bigcirc$ | ${ }^{88}$ | ${ }^{25}$ | 0 | 25 | 1 | － | 1 | 7 | － | 7 | 59 | 4 | ${ }^{63}$ | 4 | 0 | 4 | ${ }^{3}$ | － | 3 | ${ }^{28}$ | 1 | ${ }^{28}$ | ${ }^{25}$ | 1 | ${ }^{\text {s5 }}$ | ${ }^{24}$ | 3 | ${ }^{27}$ | $\bigcirc$ | $\bigcirc$ | － | ${ }^{30}$ | 4 | ${ }^{34}$ | ${ }^{3}$ | 4 | ${ }^{38}$ | 1 | ${ }^{1}$ | 1 | － | － | $\bigcirc$ | ${ }^{451}$ | 17.45 | 148 |
| 18.00 －18：15 | 3 | $\bigcirc$ | 3 | ${ }^{62}$ | 0 | ${ }^{62}$ | ${ }^{20}$ | $\bigcirc$ | 20 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | 8 | $\bigcirc$ | 8 | ${ }^{48}$ | 5 | ${ }^{53}$ | ${ }^{39}$ | $\bigcirc$ | ${ }^{39}$ | 2 | $\bigcirc$ | 2 | ${ }^{30}$ | $\bigcirc$ | 30 | ${ }^{7}$ | 1 | ${ }^{80}$ | 20 | 3 | ${ }^{23}$ | 1 | $\bigcirc$ | 1 | ${ }^{25}$ | 2 | ${ }^{27}$ | ${ }^{30}$ | 8 | ${ }^{39}$ | 2 | $\bigcirc$ | ${ }^{3}$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | ${ }^{39}$ | $18.00 \cdot 1900$ |  |
| 18：15－1830 | ${ }_{4}$ | $\bigcirc$ | 5 | ${ }^{54}$ | $\bigcirc$ | ${ }^{54}$ | 16 | 1 | ${ }^{16}$ | － | － | 0 | ${ }^{4}$ | 1 | 4 | ${ }^{39}$ | 3 | ${ }^{42}$ | ${ }^{3}$ | 0 | ${ }_{3}$ | 2 | － | ${ }^{3}$ | ${ }^{27}$ | － | ${ }^{27}$ | ${ }^{6}$ | 1 | ${ }^{62}$ | 2 | 2 | 25 | － | － | － | ${ }^{23}$ | 4 | ${ }^{27}$ | ${ }^{28}$ | 5 | ${ }^{34}$ | ${ }^{3}$ | － | ${ }^{3}$ | － | － | 0 | ${ }^{36}$ | ${ }^{\text {mp }}$ Pax |  |
| 1830．18，45 | ${ }_{4}$ | － | ${ }^{4}$ | ${ }^{52}$ | 1 | ${ }^{53}$ | ${ }^{12}$ | 1 | ${ }^{13}$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | ${ }^{6}$ | － | ${ }^{6}$ | ${ }_{36}$ | 4 | ${ }^{40}$ | 40 | $\bigcirc$ | ${ }^{4}$ | ${ }^{4}$ | $\bigcirc$ | ${ }^{4}$ | ${ }^{21}$ | 1 | 22 | ${ }^{54}$ | 1 | ${ }_{5}$ | ${ }^{13}$ | 2 | ${ }^{16}$ | $\bigcirc$ | $\bigcirc$ | 0 | ${ }^{19}$ | ${ }^{2}$ | ${ }^{21}$ | ${ }^{26}$ | ${ }^{4}$ | ${ }_{30}$ | 2 | 0 | ${ }^{2}$ | 0 | $\bigcirc$ | $\bigcirc$ | ${ }^{366}$ |  |  |
| 18.45 19000 | 2 | － | 3 | ${ }^{39}$ | 2 | ${ }^{4}$ | ${ }^{14}$ | － | ${ }^{14}$ | － | $\bigcirc$ | $\bigcirc$ | 2 | － | 2 | ${ }^{24}$ | 5 | ${ }^{29}$ | ${ }^{28}$ | $\bigcirc$ | ${ }^{28}$ | 2 | $\bigcirc$ | 2 | ${ }^{21}$ | 1 | 22 | 51 | 1 | 51 | 15 | ${ }^{3}$ | ${ }^{18}$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | 15 | 4 | 19 | ${ }^{22}$ | 7 | ${ }^{29}$ | 1 | $\bigcirc$ | 1 | 0 | － | － | ${ }^{261}$ |  |  |
| ${ }^{\text {PM Toatal }}$ | ${ }^{192}$ | ${ }^{16}$ | ${ }^{208}$ | 1759 | ${ }^{4}$ | ${ }^{183}$ | ${ }^{784}$ | ${ }^{4}$ | ${ }^{828}$ | 20 | $\bigcirc$ | ${ }^{20}$ | 409 | 22 | 431 | 124 | ${ }^{109}$ | 1353 | 102 | ${ }^{28}$ | 122 | 124 | 7 | ${ }^{131}$ | 761 | ${ }^{32}$ | ${ }^{733}$ | 1991 | ${ }^{68}$ | 259 | ${ }^{63}$ | ${ }^{84}$ | 767 | 5 | $\bigcirc$ | 3 | ${ }_{5} 51$ | 7 | ${ }^{62}$ | ${ }^{827}$ | ${ }_{150}$ | ${ }^{97}$ | ${ }^{8}$ | ${ }^{15}$ | 97 | 1 | － | ， | ${ }^{1122}$ |  |  |
| ${ }^{\text {pum Paxk }}$ | 50 | 3 | 53 | 49 | $\bigcirc$ | 458 | ${ }^{233}$ | 12 | 215 | ${ }^{5}$ | $\bigcirc$ | 5 | 101 | ${ }^{6}$ | 107 | ${ }^{295}$ | ${ }^{24}$ | ${ }^{39}$ | ${ }^{233}$ | 7 | ${ }^{240}$ | 29 | 2 | ${ }^{31}$ | ${ }^{176}$ | 8 | 184 | 486 | ${ }^{12}$ | 498 | ${ }^{179}$ | ${ }^{14}$ | ${ }^{193}$ | 0 | 0 | $\bigcirc$ | ${ }^{123}$ | 18 | ${ }^{141}$ | 210 | 30 | 239 | ${ }^{21}$ | 4 | ${ }^{25}$ | $\bigcirc$ | $\bigcirc$ | － | 2298 |  |  |



| Tme Perioo | Lapt Heay Toal |  |  |  |  |  | Lgot Heary Tool |  |  |  |  |  | Light Heam Toal |  |  |  |  |  | $$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $L_{\text {Light }}^{\text {Morenems } 10}$ Toata |  |  | Light Homem Toual |  |  |  |  |  | Laght Heany Tooal |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Light | Hamy | Toal |  |  |  | Ligh | Heany | Toal |  |  |  | Ligm | Hamy | Toal |  |  |  | Lignt | Hoan | Toot |  |  |  | L．gnt | Heany | Toal | Ligh | Hamy |  | Lght |  | Toal |  |  |  | Legt | Hamy | Tota |  |  |  |
| 500． 6.00 | 3 | 1 | 4 |  |  |  | ${ }^{143}$ | 3 | ${ }^{146}$ | 14 | 3 | ${ }^{18}$ | 。 | － | － | 5 | 2 | － | ${ }^{26}$ | ${ }^{23}$ | 49 | ${ }^{37}$ | 3 | 4 | 1 | 2 | 3 | ${ }_{56}$ | 2 | ${ }_{58}$ | ${ }^{\text {® }}$ | 1 | ${ }^{6}$ | ${ }^{23}$ | 2 | ${ }^{25}$ | 0 | － | － |  |  |  | ${ }^{37}$ | 6 | ${ }^{4}$ | ${ }^{53}$ | 14 | ${ }^{6}$ | 2 | 1 | 3 | 0 | － | － | ${ }^{464}$ | ${ }^{6}$ | ${ }^{26}$ |
| ${ }^{5} / 15.56 .15$ | 5 | 1 | － | ${ }_{17}$ | 5 | ${ }^{133}$ | 20 | 4 | ${ }^{24}$ | 。 | － | － | 7 | 2 | － | 3 | ${ }^{27}$ | ${ }^{6}$ | ${ }_{4}^{47}$ | 3 | so | 1 | ， | 2 | ${ }^{67}$ | 3 | 70 | ${ }^{81}$ | 3 | ${ }^{84}$ | 32 | 3 | ${ }_{3}$ | － | － | 0 | 4 | 7 | 51 | 5 | 11 | ${ }^{6}$ | 2 | 2 | 4 | 0 | － | － | ${ }_{545}$ | 71 | 615 |
| ${ }_{5} 530.630$ | 7 | $=$ | － | ${ }_{162}$ | 7 | 169 | 2 | 4 | ${ }^{26}$ | 。 | － | － | 12 | 1 | 14 | 4 | ${ }^{28}$ | 72 | ${ }^{54}$ | 4 | ${ }_{58}$ | 1 | 1 | 2 | ${ }_{80}$ | 3 | ${ }^{82}$ | 9 | 5 | 101 | ${ }_{4}$ | 4 | 45 | 0 | － | － | 47 | 10 | 56 | ${ }^{6}$ | 14 | ${ }^{76}$ | ${ }^{3}$ | 2 | 5 | 0 | － | － | ${ }^{63}$ | ${ }^{84}$ | 77 |
| 5454.645 | 11 | 1 | ${ }^{13}$ | ${ }^{122}$ | 12 | 184 | ${ }^{32}$ | 5 | ${ }_{3}$ | 1 | － | 1 | 17 | 3 | 20 | 55 | 32 | ${ }^{87}$ | ${ }^{6}$ | 8 | 72 | 2 | 2 | 4 | 104 | 4 | 107 | ${ }^{128}$ | 7 | ${ }^{34}$ | so | 4 | ${ }^{4}$ | 0 | － | － | ${ }^{46}$ | 12 | ${ }^{58}$ | $\pi$ | 14 | $\because$ | 3 | 2 | 5 | 。 | － | － | ${ }^{6} 2$ | ${ }^{106}$ | ${ }_{668}$ |
| ${ }^{6000} 7.700$ | 15 | 1 | 17 | 219 | 14 | 232 | ${ }^{47}$ | 7 | ${ }^{54}$ | 2 | － | 2 | ${ }^{24}$ | 4 | 29 | ${ }_{8}$ | ${ }^{30}$ | $\stackrel{ }{8}$ | ${ }^{87}$ | 11 | ${ }^{8}$ | 4 | 3 | $\cdot$ | ${ }^{130}$ | 5 | ${ }^{135}$ | ${ }^{184}$ | 8 | 192 | ${ }^{6}$ | 6 | 70 | － | $\bigcirc$ | $\bigcirc$ | 59 | $\stackrel{ }{ }$ | ${ }^{9}$ | ${ }^{106}$ | 15 | ${ }^{121}$ | 7 | 4 | 11 | － | － | － | ${ }^{1016}$ | ${ }^{118}$ | ${ }^{138}$ |
| ${ }^{6} 145.57 .15$ | ${ }^{21}$ | 2 | ${ }^{23}$ | ${ }_{26} 2$ | ${ }^{21}$ | ${ }^{233}$ | ${ }^{62}$ | － | ${ }^{11}$ | 2 | － | 2 | 30 | － | ${ }_{3}$ | ${ }^{4}$ | 34 | ${ }^{119}$ | 100 | 14 | 114 | 5 | 2 | 7 | 145 | 5 | 150 | ${ }^{223}$ | 12 | ${ }^{235}$ | 79 | 8 | ${ }^{87}$ | 0 | － | － | ${ }^{6}$ | 11 | ${ }^{\text {so }}$ | ${ }^{128}$ | 17 | ${ }^{146}$ | 8 | 4 | ${ }^{12}$ | － | － | － | ${ }^{1218}$ | ${ }^{146}$ | ${ }^{136}$ |
| ${ }^{630} \mathbf{3} \cdot 7.30$ | ${ }^{23}$ | 2 | 24 | ${ }^{301}$ | 24 | ${ }^{326}$ | ${ }_{81}$ | ${ }^{13}$ | ${ }_{94}$ | 1 | － | 2 | 32 | 8 | 4 | ${ }^{9}$ | ${ }^{34}$ | 127 | ${ }^{113}$ | 15 | ${ }^{128}$ | 6 | 2 | － | ${ }_{169}$ | 7 | 176 | 232 | 13 | 265 | 92 | 7 | 9 | － | － | － | ${ }_{87}$ | 13 | ${ }^{100}$ | 151 | 17 | 188 | 10 | 4 | 14 | － | － | － | ${ }^{1412}$ | 180 | 1572 |
|  | ${ }^{24}$ | 3 | ${ }^{27}$ | ${ }^{32}$ | 24 | ${ }_{3} 38$ | ＊ | 15 | ${ }^{113}$ | 1 | － | 2 | ${ }_{3}$ | 8 | ${ }^{45}$ | ${ }^{105}$ | ${ }^{31}$ | ${ }^{136}$ | ${ }^{118}$ | 12 | ${ }^{130}$ | 。 | 1 | 7 | ${ }^{181}$ | － | ${ }_{187}$ | ${ }^{231}$ | 16 | ${ }_{2} 27$ | ${ }_{97}$ | s | ${ }^{106}$ | － | － | － | ${ }^{108}$ | 13 | ${ }^{120}$ | ${ }^{175}$ | 20 | 195 | 12 | 3 | 15 | － | － | $\bigcirc$ | ${ }^{1572}$ | ${ }^{164}$ | ${ }^{1736}$ |
| 7．00．8．800 | ${ }^{26}$ | 5 | 31 | ${ }^{36}$ | 29 | 392 | ${ }^{128}$ | 15 | ${ }^{143}$ | 3 | － | 3 | 46 | 10 | ${ }_{56}$ | ${ }^{112}$ | ${ }^{32}$ | ${ }^{14}$ | ${ }^{123}$ | 11 | ${ }^{134}$ | 8 | 1 | $\stackrel{ }{ }$ | 207 | 7 | 214 | ${ }^{39}$ | 16 | ${ }^{325}$ | ${ }^{97}$ | 11 | ${ }^{108}$ | 0 | － | － | ${ }^{117}$ | 15 | ${ }^{132}$ | 204 | 20 | ${ }^{224}$ | ${ }^{14}$ | 2 | ${ }^{16}$ | 0 | － | － | ${ }^{1757}$ | ${ }^{173}$ | ${ }^{1930}$ |
| ${ }^{7} 195.8 .15$ | ${ }^{25}$ | 7 | 32 | 415 | ${ }^{27}$ | ${ }_{4} 4$ | ${ }_{158}$ | 17 | 175 | 4 | － | 5 | 57 | 10 | ${ }_{6}$ | ${ }^{116}$ | ${ }^{27}$ | 142 | 130 | 10 | 141 | ${ }^{13}$ | $=$ | 15 | ${ }^{24}$ | 9 | ${ }_{23} 5$ | ${ }^{38}$ | 13 | ${ }^{36}$ | s | 12 | 109 | 0 | － | － | ${ }^{131}$ | 14 | 146 | 242 | 23 | 265 | 19 | 2 | 21 | 0 | － | － | 2001 | ${ }^{173}$ | 2774 |
| 7，30．8．30 | ${ }^{27}$ | 7 | ${ }^{4}$ | ${ }_{46} 6$ | ${ }^{26}$ | 49 | 206 | 15 | 220 | 5 | － | － | 75 | 9 | ${ }_{8} 8$ | ${ }^{121}$ | ${ }^{30}$ | 151 | ${ }^{138}$ | 11 | ${ }^{19}$ | ${ }_{16}$ | 2 | 18 | 268 | 10 | 27 | ${ }^{408}$ | 15 | ${ }^{423}$ | ${ }^{103}$ | 19 | ${ }^{121}$ | － | － | － | ${ }_{153}$ | 14 | 188 | ${ }^{235}$ | ${ }^{28}$ | ${ }^{313}$ | ${ }^{23}$ | 3 | ${ }^{26}$ | 0 | － | － | ${ }^{2232}$ | ${ }^{189}$ | ${ }^{288}$ |
| ${ }_{7} 7458.845$ | ${ }^{28}$ | 8 | ${ }^{36}$ | ${ }^{527}$ | 25 | 551 | 248 | 15 | 238 | 7 | － | 7 | ${ }_{86}$ | 11 | ${ }^{6}$ | ${ }^{124}$ | ${ }^{30}$ | ${ }^{154}$ | 157 | 12 | 169 | ${ }^{20}$ | 3 | ${ }^{23}$ | 24 | 10 | ${ }^{304}$ | ${ }_{4} 3$ | 15 | ${ }^{47}$ | 107 | 19 | ${ }^{126}$ | 0 | － | － | ${ }_{168}$ | 14 | ${ }^{183}$ | 330 | ${ }^{28}$ | ${ }^{328}$ | ${ }^{24}$ | 4 | ${ }^{28}$ | － | － | － | ${ }^{2523}$ | ${ }^{193}$ | 276 |
| ${ }^{8000.900}$ | 30 | 7 | ${ }^{37}$ | ${ }^{32}$ | 2 | ${ }_{554}$ | 255 | 20 | ${ }^{275}$ | 7 | $\bigcirc$ | 7 | ${ }^{8}$ | 10 | ${ }^{6}$ | ${ }^{128}$ | ${ }^{31}$ | ${ }_{180}$ | ${ }_{153}$ | 12 | 14 | ${ }^{21}$ | 4 | ${ }^{25}$ | ${ }^{237}$ | 11 | ${ }^{298}$ | 41 | ${ }^{18}$ | 450 | 119 | 19 | ${ }^{138}$ | － | － | $\bigcirc$ | ${ }^{181}$ | ${ }^{18}$ | ${ }^{199}$ | ${ }^{300}$ | ${ }^{30}$ | ${ }^{33}$ | 2 | 3 | ${ }^{26}$ | 。 | － | － | ${ }_{2562}$ | ${ }^{207}$ | 276 |
| 8．159．9，15 | 31 | 8 | ${ }^{38}$ | 504 | ${ }^{21}$ | ${ }_{5} 5$ | 259 | 20 | 279 | 7 | 1 | 7 | ${ }^{9}$ | 12 | 105 | ${ }^{137}$ | ${ }^{31}$ | 16 | ${ }_{156}$ | 13 | 169 | ${ }_{2} 2$ | 3 | ${ }^{26}$ | 289 | 11 | 280 | ${ }^{44}$ | 19 | ${ }_{45}$ | 11 | 21 | 132 | － | － | － | ${ }^{183}$ | 18 | 201 | ${ }^{238}$ | ${ }^{28}$ | ${ }^{321}$ | 23 | 3 | ${ }^{25}$ | － | － | － | ${ }^{2522}$ | ${ }^{299}$ | ${ }^{2371}$ |
| ${ }^{830} 0.930$ | ${ }^{32}$ | 7 | 39 | 455 | ${ }^{24}$ | ${ }^{478}$ | 235 | 22 | 257 | 7 | 1 | 8 | ${ }^{93}$ | 15 | ${ }^{108}$ | ${ }^{46}$ | 29 | ${ }^{175}$ | ${ }^{154}$ | 12 | 186 | ${ }^{28}$ | 4 | 32 | 251 | 10 | 261 | ${ }^{39}$ | 19 | ${ }^{40}$ | ${ }^{103}$ | 19 | ${ }^{122}$ | － | － | $\bigcirc$ | ${ }^{170}$ | 19 | ${ }^{188}$ | 288 | ${ }^{26}$ | ${ }^{23}$ | ${ }^{21}$ | 3 | ${ }^{24}$ | 。 | － | $\bigcirc$ | ${ }^{2351}$ | 210 | 2562 |
| ${ }^{8.45 .945}$ | 32 | 7 | ${ }^{39}$ | ${ }_{38} 8$ | ${ }^{21}$ | 409 | 207 | ${ }^{24}$ | 231 | 5 | 2 | 7 | ${ }_{102}$ | 15 | ${ }^{17}$ | 152 | ${ }^{26}$ | 178 | 141 | 12 | 154 | ${ }_{30}$ | 3 | ${ }^{34}$ | 215 | 10 | 225 | ${ }^{357}$ | 19 | ${ }^{376}$ | 8 | 21 | 110 | － | － | － | ${ }^{45}$ | ${ }^{21}$ | 186 | 239 | ${ }^{28}$ | 287 | 23 | 3 | ${ }^{27}$ | 。 | － | － | ${ }^{2146}$ | 214 | 2350 |
| 9．00 10．00 | ${ }^{33}$ | ${ }^{6}$ | 39 | ${ }^{34}$ | ${ }^{20}$ | 364 | ${ }^{204}$ | 19 | 22 | ${ }^{5}$ | 2 | $\cdot$ | ${ }^{116}$ | 17 | ${ }_{132}$ | 156 | 23 | 180 | ${ }^{13}$ | 14 | 147 | ${ }^{32}$ | 2 | ${ }^{34}$ | 197 | 9 | 205 | ${ }^{323}$ | ${ }^{17}$ | 330 | ${ }^{73}$ | ${ }^{20}$ | 94 | 。 | 0 | $\bigcirc$ | 125 | 18 | 143 | 249 | ${ }^{26}$ | 275 | ${ }^{26}$ | 4 | 30 | 0 | 0 | $\bigcirc$ | ${ }^{2014}$ | ${ }^{198}$ | 2212 |


|  | ， |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | tuemmar |  |  | Light Heomemet Toat |  |  | Moements |  |  | Movement |  |  | Moverenem 9 A <br> Light <br> Heary <br> Toata |  |  | Movement 10 |  |  | Movenemen |  |  | $$ |  |  |  |  |  | Grand Toat |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Ligh | Heay | Tool | Light | Heary | Toat | Light | Heary | Toal | Light | Heary | Toal | Light | Heay | Tool | Light | Heary | Toal | Light | Heary | Toal | Light | Heax | Toal |  |  |  | Light | Haxy | Toas | Light | Heany | Toal |  |  |  | Lght | Heany | Toal |  |  |  | Light | Heay | Total |  |  |  |
| 14000 1500 | 45 | 5 | so | ${ }^{226}$ | 15 | 302 | ${ }_{19} 1$ | ${ }^{13}$ | ${ }^{203}$ | 5 | － | 5 | ${ }^{122}$ | 6 | ${ }^{129}$ | 246 | ${ }^{20}$ | 268 | ${ }_{188}$ | ${ }^{11}$ | ${ }^{179}$ | ${ }_{36}$ | 2 | ${ }^{38}$ | ${ }^{146}$ | 10 | 157 | ${ }^{335}$ | 19 | ${ }^{354}$ | 102 | ${ }^{21}$ | ${ }^{123}$ | － | － | － | ${ }_{8} 9$ | 17 | ${ }^{106}$ | ${ }_{169}$ | ${ }^{35}$ | 204 |  |  |  | 25 | 4 | ${ }^{28}$ | 。 | － | － | ${ }^{1955}$ | ${ }^{178}$ | ${ }^{2143}$ |
| ${ }^{14.45 \text {－1515 }}$ | 4 | 5 | ${ }^{53}$ | ${ }^{314}$ | 15 | ${ }^{32}$ | ${ }_{192}$ | 13 | 205 | 5 | － | 5 | ${ }^{121}$ | 7 | ${ }^{128}$ | 239 | 23 | 262 | 17 | 11 | ${ }^{188}$ | ${ }_{36}$ | 2 | ${ }^{38}$ | ${ }^{158}$ | 8 | 166 | 391 | 19 | 410 | 114 | 20 | 134 | 。 | － | － | ${ }^{9}$ | 17 | 116 | ${ }^{178}$ | 39 | 27 | ${ }^{24}$ | 4 | ${ }^{28}$ | 0 | － | － | ${ }^{2006}$ | ${ }^{184}$ | 2280 |
| 1433017530 | 45 | 5 | 50 | ${ }^{36}$ | 17 | ${ }^{323}$ | ${ }_{198}$ | 13 | 211 | 6 | － | － | ${ }^{122}$ | 8 | 130 | ${ }^{24}$ | ${ }^{23}$ | ${ }^{226}$ | ${ }^{181}$ | ง | 190 | ${ }^{32}$ | 2 | 34 | ${ }^{168}$ | 10 | ${ }^{179}$ | ${ }^{437}$ | 18 | 455 | 127 | 21 | 148 | － | － | － | ${ }^{112}$ | 15 | ${ }^{128}$ | ${ }^{186}$ | ${ }^{35}$ | 22 | ${ }^{24}$ | 4 | ${ }^{28}$ | － | － | － | ${ }^{2227}$ | ${ }_{182}$ | 200 |
| 14.45 －1545 | 50 | 5 | ${ }_{55}$ | ${ }_{3} 35$ | 16 | ${ }^{40}$ | 205 | 14 | ${ }^{219}$ | 6 | － | － | 114 | 6 | 120 | 235 | ${ }^{23}$ | ${ }^{25}$ | 205 | 10 | 215 | ${ }_{3}$ | ， | ${ }^{32}$ | 170 | ${ }^{11}$ | 181 | 44 | ${ }^{20}$ | 484 | ${ }^{138}$ | ${ }^{20}$ | ${ }^{158}$ | － | － | － | ${ }^{122}$ | 17 | ${ }^{139}$ | ${ }_{198}$ | ${ }^{36}$ | ${ }^{234}$ | ${ }^{21}$ | 5 | ${ }^{26}$ | 1 | － | 1 | ${ }^{245}$ | ${ }_{183}$ | 2528 |
| 15.50016800 | 50 | 5 | ${ }_{55}$ | ${ }^{405}$ | 15 | ${ }^{20}$ | 214 | 13 | ${ }^{228}$ | 5 | － | 5 | ${ }^{113}$ | 6 | ${ }^{119}$ | 252 | ${ }^{24}$ | ${ }^{275}$ | ${ }^{221}$ | 11 | 231 | ${ }^{31}$ | 1 | ${ }_{32}$ | 185 | 11 | 176 | 479 | 22 | ${ }^{501}$ | ${ }^{151}$ | 19 | 170 | － | － | － | ${ }^{139}$ | 14 | ${ }^{133}$ | 298 | ${ }^{37}$ | ${ }^{246}$ | ${ }^{19}$ | 6 | ${ }^{25}$ | － | － | $\bigcirc$ | ${ }^{2453}$ | ${ }^{185}$ | ${ }_{268}$ |
| ${ }^{151515} 518.15$ | 51 | 4 | ${ }_{55}$ | ${ }^{41}$ | 12 | 43 | 212 | 13 | 224 | － | － | － | ${ }^{11}$ | － | ${ }^{117}$ | 262 | ${ }^{20}$ | ${ }^{232}$ | 231 | 10 | 24 | ${ }^{31}$ | 2 | ${ }^{33}$ | 165 | ${ }^{12}$ | 17 | 469 | ${ }^{23}$ | ${ }^{49}$ | 163 | ${ }_{18}$ | ${ }^{181}$ | － | － | － | ${ }^{130}$ | 16 | ${ }^{146}$ | 207 | ${ }^{34}$ | 241 | 19 | 6 | ${ }^{25}$ | － | － | － | ${ }^{2487}$ | ${ }^{176}$ | 2683 |
| 15530.183 .30 | 52 | 3 | 56 | ${ }_{3} 3$ | 8 | $4{ }^{48}$ | 201 | 12 | 213 | 6 | － | － | ${ }^{107}$ | － | ${ }^{13}$ | 265 | ${ }^{24}$ | 239 | 232 | 10 | 242 | ${ }^{31}$ | 3 | 33 | 167 | 8 | 175 | 459 | ${ }^{20}$ | 479 | ${ }^{68}$ | ${ }^{17}$ | ${ }^{185}$ | － | － | － | ${ }^{130}$ | ${ }_{16}$ | 147 | 205 | ${ }^{34}$ | ${ }^{240}$ | 19 | 5 | ${ }^{24}$ | 。 | － | － | 2482 | 167 | ${ }^{263}$ |
| 15.45 －1645 | 50 | 4 | ${ }_{54}$ | ${ }^{239}$ | 9 | 48 | ${ }_{194}$ | 10 | 204 | 6 | － | － | 101 | 5 | ${ }^{105}$ | ${ }^{271}$ | 25 | 236 | 22 | 7 | 236 | ${ }^{29}$ | 3 | ${ }^{32}$ | ${ }^{175}$ | ${ }^{6}$ | 181 | 443 | 17 | 480 | ${ }^{178}$ | 16 | ${ }^{193}$ | 1 | － | 1 | ${ }^{130}$ | 16 | ${ }^{146}$ | ${ }_{19} 9$ | ${ }^{30}$ | ${ }^{29}$ | 20 | 4 | ${ }^{24}$ | － | － | － | ${ }^{2889}$ | ${ }^{151}$ | 2285 |
| 16000 | 50 | 4 | ${ }_{54}$ | 450 | 8 | ${ }_{4}^{45}$ | ${ }^{184}$ | ， | 194 | 6 | － | － | ${ }^{4}$ | 5 | \％ | 286 | ${ }_{26}$ | ${ }^{31}$ | ${ }^{237}$ | 4 | 242 | ${ }^{3}$ | 3 | ${ }^{33}$ | ${ }^{186}$ | 5 | 191 | 485 | ${ }^{13}$ | ${ }^{498}$ | ${ }_{182}$ | 15 | ${ }^{197}$ | － | － | － | 115 | 16 | ${ }^{131}$ | 190 | ${ }^{28}$ | ${ }^{218}$ | ${ }^{20}$ | 2 | 22 | － | － | － | ${ }^{2514}$ | ${ }^{139}$ | 2653 |
| 16：158．77：75 | 50 | 3 | 53 | 445 | － | 441 | ${ }_{165}$ | 9 | ${ }^{174}$ | 4 | － | 4 | ${ }^{81}$ | 4 | ${ }^{85}$ | ${ }^{31}$ | 25 | 336 | 212 | 4 | 246 | 25 | 2 | ${ }^{27}$ | ${ }^{189}$ | 4 | ${ }^{192}$ | 483 | 13 | 496 | ${ }_{192}$ | 18 | 210 | － | － | － | ${ }_{19}$ | 15 | ${ }^{133}$ | ${ }_{181}$ | 29 | 210 | 19 | 2 | 22 | － | － | － | 2507 | ${ }^{133}$ | 240 |
| 16380 1730 | 45 | 4 | 4 | 439 | － | 46 | ${ }_{16} 6$ | 8 | ${ }^{174}$ | 4 | － | 4 | $\pi$ | 5 | 82 | 322 | 23 | ${ }^{3} 5$ | 239 | 3 | 263 | ${ }_{2}$ | － | ${ }^{24}$ | ${ }^{198}$ | 3 | ${ }^{197}$ | 482 | 13 | ${ }_{505}$ | 201 | ${ }^{18}$ | ${ }^{219}$ | 1 | － | 1 | ${ }^{125}$ | 13 | ${ }^{139}$ | 175 | 29 | 204 | ${ }^{18}$ | 2 | ${ }^{20}$ | － | － | － | 2842 | ${ }^{128}$ | 2850 |
| ${ }^{18,455}$－17，45 | 40 | 2 | ${ }^{4}$ | ${ }_{46}$ | 4 | 40 | ${ }_{150}$ | 10 | 180 | 4 | － | 4 | ${ }_{7}$ | 5 | ${ }^{79}$ | ${ }^{336}$ | ${ }^{24}$ | ${ }_{3} 5$ | 233 | 2 | 255 | ${ }^{24}$ | － | ${ }^{24}$ | 187 | 3 | ${ }^{190}$ | ${ }_{4} 9$ | 12 | ${ }_{503}$ | ${ }_{197}$ | 19 | 216 | 1 | － | 1 | ${ }^{122}$ | 13 | ${ }^{135}$ | ${ }_{165}$ | 29 | 194 | 15 | 3 | ${ }^{18}$ | － | － | － | 2995 | ${ }^{126}$ | 2221 |
| 17：000 18：00 | ${ }^{33}$ | 1 | ${ }^{34}$ | 41 | 3 | 414 | ${ }^{132}$ | 7 | ${ }_{140}$ | 4 | － | 4 | ${ }^{61}$ | 3 | ${ }^{64}$ | ${ }^{314}$ | 22 | 335 | 230 | 2 | 231 | ${ }^{18}$ | － | 18 | 164 | 3 | 188 | 447 | 10 | 458 | ${ }^{178}$ | ${ }^{17}$ | ${ }^{195}$ | 1 | － | 1 | ${ }^{126}$ | ${ }^{13}$ | ${ }^{139}$ | 152 | 25 | ${ }^{17}$ | 11 | 3 | ${ }^{13}$ | － | － | － | ${ }^{2281}$ | ${ }^{110}$ | ${ }^{2391}$ |
| 17：15，81：75 | 25 | 1 | ${ }^{26}$ | ${ }_{3} 3$ | 3 | ${ }^{31}$ | ${ }^{119}$ | 4 | ${ }^{123}$ | 3 | － | 3 | 52 | 3 | ${ }^{55}$ | 266 | 23 | 239 | 210 | 1 | ${ }^{211}$ | 16 | － | 16 | 149 | 3 | 151 | 407 | 7 | 414 | 141 | 14 | 155 | 2 | － | 2 | ${ }^{123}$ | 11 | ${ }^{34}$ | ${ }_{1} 12$ | 25 | 166 | － | 2 | 11 | － | － | － | ${ }^{2020}$ | ${ }^{6}$ | 2117 |
| 17300．1830 | ${ }^{21}$ | 1 | ${ }^{21}$ | ${ }^{312}$ | 1 | 314 | ${ }^{9}$ | 3 | 9 | 2 | － | 2 | ${ }^{37}$ | 1 | ${ }^{38}$ | ${ }^{23}$ | 19 | ${ }^{212}$ | ${ }_{182}$ | － | 182 | 14 | － | $\cdots$ | ${ }^{124}$ | 3 | 126 | 32 | 6 | ${ }_{3} 37$ | 110 | 13 | ${ }^{123}$ | 1 | － | 1 | ${ }^{108}$ | 13 | ${ }^{120}$ | ${ }^{29}$ | 22 | 151 | 8 | 2 | 10 | － | － | － | 1705 | 84 | 1789 |
| 174，45－18：45 | 16 | 1 | ${ }^{17}$ | 235 | 2 | 257 | ${ }^{7}$ | 1 | ${ }^{74}$ | 1 | － | 1 | ${ }^{24}$ | 1 | 25 | ${ }_{182}$ | 17 | 198 | ${ }^{161}$ | 1 | 162 | 11 | 1 | 12 | ${ }^{106}$ | 2 | 108 | 279 | 4 | ${ }^{233}$ | ${ }^{80}$ | 11 | ${ }^{20}$ | 1 | － | 1 | ${ }^{8}$ | 11 | ${ }^{108}$ | ${ }^{119}$ | 22 | 141 | 7 | 1 | － | － | － | － | ${ }^{1413}$ | ${ }^{73}$ | 1486 |
| 18800 19000 | ${ }^{14}$ | 1 | 15 | 206 | 3 | 210 | ${ }^{2}$ | 1 | ${ }^{6}$ | － | － | － | ${ }^{19}$ | 1 | ${ }^{20}$ | 147 | 18 | 165 | ${ }^{46}$ | $\circ$ | 146 | 10 | 1 | 11 | 9 | 2 | 102 | 245 | 4 | ${ }^{29}$ | 70 | 11 | 8 | 1 | 。 | 1 | ${ }_{8} 8$ | 11 | ${ }^{4}$ | 107 | 25 | 132 | 7 | 1 | 8 | － | 。 | － | ${ }^{1218}$ | ${ }^{78}$ | ${ }^{1296}$ |

austraffic




[^1]


 1430.1530 2acs















|  |  | many | Tout |  | maxy | Toat | Lom | mav | Toal | Lom | mave | Toon | Lom | my | Toos | Lemm | 1 maxy | Toun | Lom | mavy | Toun | Lem | mow | Toat | Lom | max | Toal |  | navy | Tool | Lom | mavy | Toal |  |  | Toest |  | mavy | Toul |  | namy | Toon |  |  | Tool |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $14.400 \cdot 1500$ | ${ }^{3}$ | ． | \％ | ${ }^{273}$ | 10 | ${ }^{22}$ | ${ }^{3}$ | － | ${ }^{4}$ |  | $0$ | － |  |  | 32 | ${ }^{116}$ |  |  | $9$ | 2 | 4 | $0$ | － | － | 70 |  | ＂ | ${ }_{36}$ | 15 | ${ }^{37}$ | ${ }^{25}$ | ． | 235 | 2 | － | 3 | ${ }^{178}$ | 10 | ${ }^{188}$ | ${ }^{146}$ | ． | ${ }_{150}$ | 12 | 5 | ${ }^{108}$ |  |  | 5 | ${ }^{1700}$ | ${ }^{6}$ | ${ }^{1764}$ |
| 1415 －12 | ${ }^{\circ}$ | 5 | $\because$ | 238 | ＂ | ${ }^{30}$ | ${ }^{39}$ | ㅇ | 3 | ㅇ | $0$ |  | $35$ |  | $36$ | 123 |  | 125 | 4 |  | $47$ |  |  |  | ${ }^{74}$ |  |  | ${ }^{20}$ |  |  | ${ }_{20} 8$ |  | ${ }^{268}$ | 2 |  |  | 187 |  | 197 | ${ }_{180}$ |  | ${ }^{164}$ | 19 |  | ${ }^{14}$ |  |  |  | ${ }_{182}$ | \％ | ${ }^{180}$ |
| 14.30 | ${ }^{89}$ | － | \％ | ${ }^{31}$ | 1s | 33 | ${ }^{13}$ | 。 | ＊ | 。 | 。 | － | $97$ |  | 4 | 135 | ． | ${ }^{13}$ | 52 |  | ss |  |  |  | 7 |  | ${ }^{\circ}$ | 430 |  | ${ }^{46}$ | ${ }^{27}$ |  | 231 |  |  |  | ${ }^{215}$ | 10 | ${ }^{215}$ | ${ }^{168}$ |  | ${ }^{174}$ | ${ }^{126}$ |  | ${ }^{31}$ |  |  |  | ${ }^{1984}$ | ＂ | ${ }^{209}$ |
| 12.45 .1845 | $\infty$ | ． | ${ }^{100}$ | ${ }^{326}$ | 12 | 37 | ${ }^{45}$ | 。 | ${ }^{4}$ | 。 | 。 | － | ${ }^{\circ}$ |  | ${ }^{\circ}$ | 152 |  | ${ }_{158}$ | 5 |  | ${ }^{5}$ |  |  |  | 2 |  | $\cdots$ | ${ }^{45}$ |  | ${ }^{88}$ | ${ }^{20}$ |  | ${ }^{30}$ |  |  |  | ${ }^{207}$ |  | 218 | 162 |  | ${ }^{68}$ | ${ }^{134}$ |  | ${ }^{17}$ |  |  | 10 | ${ }^{212}$ | ${ }^{\circ}$ |  |
| 15500．18500 | ${ }^{5}$ | 7 | ${ }^{102}$ | ${ }^{312}$ | 12 | ${ }^{32}$ | ${ }^{3}$ | － | ${ }^{3}$ | 。 | － | － | 8 | ， | \％ | ${ }_{158}$ | 。 | ${ }_{162}$ | 53 | ， | 5 | － | － | － | ＊ |  | $\because$ | 51 | 13 | ${ }^{52}$ | ${ }^{39}$ | 10 | ${ }^{16}$ | 2 | － | 2 | 212 | ， | ${ }^{219}$ | 145 | 5 | ${ }^{170}$ | 145 | 2 | 147 | ． |  | ． | ${ }^{2182}$ | ${ }^{\circ}$ |  |
|  | $\stackrel{ }{*}$ | 5 | $\sim$ | ${ }^{288}$ | ． | 30 | ${ }^{8}$ | － | ${ }^{8}$ | 。 | 。 | － | 8 | ， | $\because$ | ${ }_{157}$ | ． | ${ }^{160}$ | 5 | ， | $\stackrel{ }{ }$ | 。 | － | － | 2 | ， | 3 | ${ }^{59}$ | ＂ | 55 | ${ }^{32}$ | － | ${ }^{35}$ | ， | － | ， | ${ }^{20}$ | 5 | 212 | ${ }_{180}$ | 5 | ${ }^{105}$ | 158 | 2 | ${ }^{18}$ | ． | － | 10 | ${ }^{2218}$ | 5 |  |
| 1530． 18.3 | $\cdots$ | 3 | $\because$ | 309 | 7 | ${ }^{11}$ | 3 | － | ${ }^{4}$ | 。 | 。 | － | 8 | ， | $\because$ | 132 | ， | ${ }^{15}$ | ${ }_{8}$ | ， | 4 | 。 | － | － | $\because$ | ， | $\because$ | 557 | 10 | ${ }_{58} 8$ | 32 | ． | 31 | ， | － | ， | 197 | ， | 202 | 153 | 2 | ${ }^{155}$ | 14 | 3 | ${ }^{19}$ | ， | ， | ， | ${ }^{2195}$ | ${ }^{4}$ |  |
| ${ }_{15} 54.5$ | ${ }^{4}$ | 2 | ${ }^{86}$ | 298 | － | 300 | ${ }^{3}$ | － | ${ }^{3}$ | 。 | － | － | ${ }^{75}$ | ， | ${ }^{6}$ | ${ }_{14} 1$ | － | 151 | 4 | ， | 4 | － | － | － | 3 |  | $\because$ | ${ }_{568}$ | ， | ${ }^{57}$ | ${ }^{303}$ | 4 | ${ }^{30}$ | ， | － |  | ${ }^{198}$ | 3 | ${ }^{20}$ | 157 |  | 158 | 145 |  | 147 | 5 |  |  | ${ }^{214}$ | ${ }^{2}$ |  |
| 18500. | $\infty$ |  | \％ | ${ }^{293}$ | － | ${ }^{29}$ | ${ }^{33}$ | － | ${ }^{3}$ | 。 | － | － | ${ }^{74}$ | 。 | $75$ | ${ }^{129}$ | ， | ${ }^{150}$ | 4 | ， | ${ }^{*}$ | － | － | － | $\because$ |  | ${ }_{96}$ | 573 |  | 50 | ${ }^{32}$ | 3 | 36 |  | 。 |  | ${ }_{192}$ |  | ${ }^{198}$ | 142 |  | $163$ | ${ }^{139}$ | 3 | 142 | 5 | ， | － | 2151 | 27 | 212 |
| 18：515．17 | $\stackrel{1}{4}$ | ， | ${ }^{5}$ | 292 | 7 | 29 | ${ }^{33}$ | － | ${ }^{3}$ | 。 | － | － | ${ }^{7}$ | 。 | ${ }^{6}$ | 154 | ， | 155 | 45 | ， | 4 | － | － | － | 107 | － | 107 | ${ }_{580}$ | 7 | ${ }_{58}$ | 22 | 3 | ${ }^{25}$ | ， | － | ， | ${ }^{180}$ | 2 | 182 | ${ }^{163}$ | 。 | ${ }^{163}$ | 135 | 3 | 137 | 5 | － | s | ${ }^{2157}$ | 25 | 210 |
| $14.50 \cdot 17.30$ | $\sim$ | 1 | 100 | ${ }^{288}$ | 5 | 292 | ${ }^{36}$ | － | ${ }^{4}$ | 。 | － | － | ${ }^{76}$ | ， | ＂ | 155 | ， | ${ }_{156}$ | ${ }^{4}$ | 。 | 4 | － | － | － | 107 | ， | ${ }^{107}$ | ${ }_{609}$ |  | ${ }^{17}$ | 28 |  | ${ }_{30}$ |  | － |  | ${ }^{75}$ |  | ${ }^{176}$ | 162 | 。 | 162 | ${ }^{10}$ |  | ${ }^{14}$ | ¢ |  | － | ${ }^{2194}$ | 21 |  |
| $18.45 \cdot 17$ | ${ }^{109}$ | ， | ${ }^{108}$ | ${ }^{23}$ | 4 | 28 | ${ }_{3}$ | － | 3 | 。 | － | － | 8 | ， | 8 | 159 | ， | ${ }^{60}$ | 4 | 。 | 4 | － | － | － | ${ }^{103}$ | ， | ${ }^{104}$ | 680 | ， | ${ }^{68}$ | 38 | 2 | 30 | ， | － | ， | ${ }_{162}$ | ， | ${ }^{65}$ | ${ }^{187}$ | － | ${ }^{18}$ | ${ }^{136}$ | ， | ${ }^{19}$ | － | － | － | ${ }^{2216}$ | 21 |  |
| 17800．18：00 | ${ }^{16}$ | ， | ${ }^{17}$ | 278 | 3 | 276 | 3 | － | 3 | ， | － | ． | 75 | ， | ${ }_{7}$ | ${ }_{188}$ | ＇ | 158 | 48 | 。 | 4 | － | － | － | $\because$ | ， | $\because$ | ${ }_{66}$ | 7 | ${ }^{613}$ | 28 | 2 | 300 | ， | － | ， | 132 | ， | 153 | 149 | － | ${ }^{19}$ | 138 | ， | 134 | 7 | － | 7 | 2138 | 19 | ${ }^{215}$ |
|  | ${ }^{114}$ | － | ${ }^{14}$ | 237 | 2 | 200 | ${ }^{30}$ | － | 30 | ＇ | － | ． | ${ }^{82}$ | － | ${ }^{6}$ | 150 | ＇ | 150 | ${ }^{39}$ | 。 | 39 | － | － | － | ${ }^{7}$ | ， | ＂ | ${ }_{59}$ | － | sts | ${ }^{24}$ | ， | 238 | ， | － | ， | 147 | ， | ${ }^{148}$ | 140 | － | 140 | 128 | ， | ${ }^{12}$ | 7 | － | ， | ${ }_{197}$ | 15 | 190 |
| 173．0．180 | ${ }^{109}$ | $\bigcirc$ | ${ }^{109}$ | 215 | 3 | 217 | ${ }^{29}$ | $\bigcirc$ | \％ |  | $\bigcirc$ | 1 | 5 | $\bigcirc$ | 5 | ${ }^{137}$ | － | ${ }^{38}$ | ${ }^{36}$ | － | ${ }^{3}$ | － | － | － | ${ }^{6}$ | ， | ${ }^{68}$ | 452 | － | $4{ }^{4}$ | ${ }^{238}$ | ， | ${ }^{254}$ | ， | － | － | ${ }^{187}$ | $\bigcirc$ | ${ }^{37}$ | ${ }^{13}$ | － | ${ }^{131}$ | ${ }^{109}$ |  | ${ }^{10}$ | ． |  |  | ${ }_{173}$ | ${ }^{13}$ | 1750 |
| 17：45，18，45 | \％ |  | $\because$ | ${ }_{102}$ |  | 194 | ${ }^{25}$ |  | ${ }^{25}$ |  | － | $\stackrel{1}{ }$ | ${ }^{3}$ |  | ${ }^{3}$ | ${ }^{123}$ | 。 | ${ }^{123}$ | ${ }^{29}$ | － | ${ }^{20}$ | － |  | － | 50 |  | 5 | ${ }_{3}^{36}$ | ． | ${ }_{38}$ | 218 |  | ${ }^{219}$ |  | － |  | 129 | 。 | ${ }^{29}$ | ${ }_{12}$ | 。 | ${ }^{121}$ | 105 | ， | 107 | 5 | 。 |  | 198 | ＂ | ${ }_{100}$ |
| 13000．1300 |  | － | 7 | 184 | 2 | 18 | ${ }^{24}$ | － | ${ }^{4}$ | ， | 0 | 1 | ${ }^{28}$ | 。 | ${ }^{26}$ | 103 | 。 | 103 | ${ }^{23}$ | － | ${ }^{24}$ | 1 | 。 | 1 | 49 | 。 | 4 | ${ }^{309}$ | 4 | 3 | 192 | ， | 132 | － | 0 | － | 122 | 1 | ${ }^{22}$ | 10 | 。 | 10 | ${ }^{9}$ | ， | $\because$ | 4 |  |  | 1302 | 。 |  |







 1425.18455 $1515 \cdot-16,545$
 ${ }_{1350-1850}$ 2034 $1545.10455^{2027}$
 4000.100 ${ }_{1830-1730}$ 2055


 $4000-12000170$ pureak $30{ }^{302}$




|  | ${ }^{\text {bmm }}$ | nany | Toat |  |  | Tomat |  |  | Toat |  |  | Toul |  |  | Tout |  |  | Tout |  | man | Toan |  | many | Tom |  | nowy | Tooll |  | mavy | Toon |  | man | Toum |  |  | Toal | 4 mm | maxy | Tom |  | many | Tool |  | max | Toal |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $14.40 \cdot 1580$ | 6 | 2 | ${ }^{\circ}$ | ${ }^{31}$ | 4 | ${ }^{323}$ | ${ }_{12}$ | 4 | 145 | 。 | － | － | ${ }_{14}$ | 7 | ${ }_{150}$ | 586 | 45 | 51 | ${ }_{78}$ | 2 | ${ }^{\circ}$ | 。 |  | － | ${ }_{107}$ |  | ${ }^{11}$ | ${ }^{318}$ |  | ${ }^{32}$ | ${ }^{27}$ |  | ${ }^{238}$ | － |  | － | ${ }^{127}$ |  | ${ }^{12}$ | ${ }_{39}$ | 97 | ${ }^{4} 8$ | ${ }^{63}$ |  | ${ }^{5}$ |  |  | － | ${ }_{2652}$ | ${ }^{17}$ | ${ }^{278}$ |
| 14.45 | ＊ | 1 | ${ }^{\circ}$ | ${ }_{35}$ |  | ${ }^{30}$ | ${ }^{51}$ | 4 | 155 | 。 | － | － | ，45 |  | 132 | ${ }^{17}$ | 4 | ${ }^{56}$ | 8 | ， | ${ }^{\circ}$ | － |  | － | ${ }^{\text {\％88 }}$ |  | ＂＇ | ${ }^{36}$ |  | 31 | 274 |  | ${ }^{29}$ | － |  |  | ${ }^{186}$ |  | ${ }^{18}$ | ${ }^{468}$ | ${ }^{102}$ | ${ }^{50}$ | ＂ |  | ${ }^{18}$ | － |  | － | 2886 | 185 | 222 |
| 14230.12 | ${ }^{6}$ | 2 | ${ }^{8}$ | ${ }_{35}$ |  | ${ }^{34}$ | 147 |  | 150 | ㅇ | － |  | ${ }^{138}$ |  | ${ }^{14}$ | 58 | 4 | 572 | 9 |  | $\because$ | － |  | － | ${ }^{16}$ |  | ${ }^{19}$ | ${ }^{374}$ |  | 378 | 27 |  | ${ }^{275}$ |  |  |  | ${ }^{18}$ |  | «1 | ${ }^{41}$ | ss | 48 | ${ }^{87}$ |  | ${ }^{8}$ |  |  |  | ${ }^{273}$ | ${ }^{134}$ |  |
| 14.45 | ${ }_{7}$ | 2 | ＂ | ${ }_{36}$ |  | 102 | 188 | 2 | 157 | 。 | 。 | $0$ | ${ }^{140}$ |  | ${ }^{14}$ | ${ }_{535}$ | 45 | Sso | ${ }^{103}$ |  | ${ }^{106}$ |  |  | － | ${ }^{118}$ |  | ＂9 | ${ }_{37}$ |  | 39 | ${ }^{29}$ |  | ${ }^{27}$ |  |  |  | ${ }^{14}$ |  | ${ }^{13}$ | ${ }^{436}$ |  | 40 | \％ |  | ${ }^{5}$ |  |  |  | ${ }^{2386}$ | ${ }^{129}$ |  |
| 15500 | ${ }^{7}$ | 2 | 8 | 4 | － | ${ }^{25}$ | 132 | 3 | 156 |  | － | － | ${ }^{14}$ |  | ${ }^{14}$ | ${ }^{655}$ | 4 | ${ }^{61}$ | 107 |  | ${ }^{108}$ |  |  | － | ＂＇ |  | 112 | ${ }^{405}$ |  | 407 | 278 |  | ${ }^{23}$ | － | － |  | ${ }^{198}$ |  | ${ }^{112}$ | ${ }^{29}$ |  | 48 | ${ }^{97}$ |  | \％ | ． |  | 。 | ${ }^{290}$ | 130 |  |
| 18，58， | 8 | 2 | ${ }^{\circ}$ | ${ }^{47}$ | ， | ${ }^{25}$ | ${ }^{19}$ | ． | 182 | － | － | － | 146 | 2 | ${ }^{188}$ | s5 | 4 | as | ${ }^{12}$ | ， | ${ }^{13}$ | － | 。 | － | 108 | ， | ${ }^{10}$ | ${ }^{6} 5$ |  | 407 | ${ }^{200}$ | ＋ | ${ }^{29}$ | － | － | － | ${ }^{18}$ | 5 | ${ }^{14}$ | ${ }^{39}$ | 4 | ${ }^{48}$ | ${ }^{5}$ | 2 | \％ | － |  | － | 295 | ＂8 |  |
| 15830.1630 | 8 | 1 | ${ }^{2}$ | ${ }_{4} 4$ | ， | ${ }^{22}$ | 180 | 3 | 153 | － | 。 | － | 155 | － | 158 | ${ }_{59}$ | 42 | ${ }^{87}$ | 110 | 。 | ${ }^{10}$ | 。 | 。 | － | ${ }^{105}$ | ， | ${ }^{100}$ | $3{ }^{30}$ | 2 | 33 | 27 | 3 | 27 | － | 。 | － | ${ }^{13}$ | 3 | ${ }^{13}$ | 4 | so | 49 | ${ }_{85}$ | 2 | 8 | 。 |  | 。 | 2294 | ＂19 |  |
|  | 7 | ， | ＂ | 392 | 7 | 30 | 132 | 3 | 156 | － | － | － | 13 | － | ${ }^{158}$ | ${ }_{5} 8$ | 4 | ${ }^{23}$ | ${ }^{107}$ | － | 107 | 。 | － | － | ${ }^{188}$ | ， | ${ }^{10}$ | ${ }^{37}$ | ， | ${ }^{38}$ | ${ }^{27}$ | 3 | ${ }^{20}$ | － | － | － | ${ }^{129}$ | 2 | ${ }^{13}$ | ${ }^{28}$ | ${ }^{4}$ | ${ }^{47}$ | ${ }^{87}$ | 3 | $\sim$ | － | 。 | － | ${ }^{2682}$ | 110 |  |
| 18.50 | ${ }^{68}$ | － | ${ }^{6}$ | ${ }^{376}$ | － | 32 | ${ }^{14}$ | 3 | 14 | － | － | － | ${ }^{2}$ | 5 | ${ }^{138}$ | 59 | 40 | ${ }^{\circ}$ | 109 | － | 106 | － | － | － | ${ }^{104}$ | 2 | ${ }^{106}$ | 33 | ， | $3{ }^{3}$ | ${ }^{27}$ | 3 | 230 | － | － | － | ${ }^{130}$ | 2 | ${ }^{13}$ | ${ }^{42}$ | ${ }^{3}$ | 48 | ${ }^{87}$ | 2 | \％ | － |  | － | ${ }^{295}$ | 19 |  |
| 18.45 | ${ }^{\circ}$ | － | ${ }^{\circ}$ | ${ }_{369}$ | 5 | ${ }^{38}$ | 142 |  | 14 | － | － | － | ${ }^{197}$ |  | 138 | 576 | 38 | 64 | \％ | 。 | $\because$ | － | － | － | ${ }^{107}$ |  | $108$ | 81 |  | 403 | ${ }_{20}^{20}$ |  | 29 |  |  |  | ${ }^{120}$ |  | ${ }^{121}$ | ${ }^{468}$ | ${ }^{\circ}$ | 4 | ${ }^{101}$ |  | ${ }^{106}$ |  |  |  | ${ }^{2033}$ | 100 |  |
| 18：30． 17 F | 6 | － | 6 | 355 | 5 | 350 | 145 | 2 | 147 | － | － | － | 146 | ． | 150 | ${ }_{586}$ | ${ }^{6}$ | ${ }^{621}$ | ${ }^{105}$ | － | ${ }^{105}$ | － | 。 | － | ＂＇ | ， | ${ }_{12}$ | 418 |  | 419 | 29 | 2 | 235 | － | － | － | ${ }^{19}$ | ＇ | ${ }^{20}$ | ${ }_{38}$ | ＊ | 432 | ${ }^{118}$ | 2 | 120 | － |  | 。 | ${ }^{2684}$ | ${ }^{89}$ |  |
| 12045.1745 | ${ }^{\circ}$ | 。 | ${ }^{\circ}$ | 354 | 4 | 388 | ${ }^{31}$ | 2 | ${ }^{13}$ | 。 | 。 | － | 182 | 3 | ${ }^{14}$ | ${ }^{574}$ | 33 | \％8 | ${ }^{\circ}$ | － | $\sim$ | 。 | 。 | － | 100 |  | 101 | ${ }^{43}$ |  | ${ }^{33}$ | ${ }^{288}$ |  | 20 | － | － | － | ${ }^{17}$ | 3 | 19 | ${ }^{37}$ | ${ }^{8}$ | 41 | ${ }^{118}$ |  | ${ }^{19}$ |  |  | － | ${ }^{2001}$ | ${ }^{87}$ |  |
| 17：00，18：00 | 5 | － | 5 | ${ }^{320}$ | 2 | 32 | ${ }^{18}$ | 2 | 120 | － | － | － | 182 | 3 | 155 | ${ }_{36}$ | ${ }^{29}$ | s65 | 82 | － | ${ }^{3}$ | － | － | － | 138 | － | ${ }^{103}$ | ${ }_{48}$ | － | 43 | ${ }^{288}$ | ， | 260 | － | － | － | ${ }^{102}$ | 2 | 104 | 361 | 3 | 33 | ${ }^{126}$ | ， | 127 | － | － | 。 | ${ }^{287}$ | 75 |  |
| 17：45，［1：15 | 54 | － | ${ }_{54}$ | ${ }^{295}$ | 2 | ${ }^{29}$ | 107 | 3 | 10 | － | － | － | 158 | 2 | 160 | 468 | 3 | 48 | ${ }^{4}$ | － | ${ }^{4}$ | － | － | － | ${ }^{8}$ | － | ${ }^{8}$ | 39 | － | 33 | ${ }^{27}$ | － | ${ }^{23}$ | － | $\bigcirc$ | － | \％ | 1 | ${ }^{\circ}$ | ${ }_{36}$ | 29 | ${ }_{35}$ | 114 | ， | ${ }^{14}$ | － | － | － | 2280 | 70 | 20 |
| ${ }^{17380.1830}$ | ${ }^{48}$ | － | 4 | 280 | ， | 261 | \％ | 2 | os | － | － | － | ${ }_{14}$ | 2 | 147 | ${ }^{0} 5$ | ${ }^{25}$ | 430 | ${ }_{5}$ | 。 | ${ }^{5}$ | － | － | － | $\pi$ | － | $\pi$ | $3{ }^{39}$ | － | $3{ }^{3}$ | 201 | － | 201 | － | － | － | ${ }_{85}$ | 2 | ${ }^{66}$ | ${ }_{28}^{236}$ | 20 | ${ }^{325}$ | ${ }^{2}$ | ， | 3 | 。 | － | 。 | ${ }^{217}$ | 8 | 278 |
| 17．45．1845 | 4 |  | 45 | 220 |  | ${ }^{21}$ | ${ }^{6}$ |  | 87 | － | － | － | ${ }^{12}$ | 2 | ${ }^{123}$ | 355 | ${ }^{24}$ | ${ }^{378}$ | 55 | － | ${ }^{5}$ | － | － | － | ${ }^{3}$ | ， | ${ }^{7}$ | ${ }^{308}$ | － | 308 | ${ }^{169}$ | － | 14 | － | $\bigcirc$ | － | ＂ | 1 | $\because$ | ${ }^{27} 4$ | 25 | ${ }^{288}$ | ${ }^{8}$ | － | ${ }^{4}$ |  | － |  | ${ }_{\text {Lss }}$ | 55 |  |
|  | 4 | － | 4 | ${ }^{207}$ | ， | ${ }^{20}$ | 8 | ， | ： |  |  |  | ${ }^{12}$ | 。 | ${ }^{112}$ | ${ }^{317}$ | 23 | 30 | so | － | 5 | 。 | － | － | ＊ |  | ${ }^{64}$ | ${ }^{24}$ | 。 | ${ }_{24} 4$ | ${ }^{135}$ | 。 | ${ }_{18}$ | 。 | 。 | － | ${ }^{6}$ |  | ${ }^{6}$ | 281 | ${ }^{27}$ | 280 | ${ }^{7}$ |  | ${ }^{73}$ | － |  | － | 189 | ${ }_{55}$ |  |





| Peros | Lem | Nateme | Tool | ${ }^{\text {Lomm }}$ | ，nembenema | Thomen | Leme | many | Toot | Lom | many | Toal | Lomt | neary | Toan | Lome | Heary | Toan 1 | Lom | maxy | Toan | Lbom mas | maxy | Tome | Lom | many Tomer | Tout | Lum | neay T |  |  | $\operatorname{man}$ | Tool | Lesemem | $\frac{n o m e m e m e x ~}{n}$ |  | Lem |  |  |  | many | Toal |  | maxy | Toal | Homen |  | $\begin{aligned} & \text { rMovement } \\ & \hline \text { Total } \\ & \hline \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5．00．5．15 | 1 | － | 1 | 1 | $\bigcirc$ | ＇ | 2 | － | 2 | $\circ$ | 0 | － | $\bigcirc$ | － | $\bigcirc$ | $\stackrel{\square}{\circ}$ | ， | ${ }^{16}$ | $\bigcirc$ | － | 1 | $\bigcirc$ | － | $\bigcirc$ | $\circ$ | $\bigcirc$ | $\bigcirc$ | $\circ$ | $\bigcirc$ | $\bigcirc$ | 。 | $\bigcirc$ | － | $\bigcirc$ | $\bigcirc$ | － | 1 | $\bigcirc$ | 1 | ${ }^{16}$ | 5 | ${ }^{21}$ | 1 | － |  | 。 | $\bigcirc$ | － | ${ }^{45}$ |
| 5185，53． | 2 | － | 2 | 5 | － | 5 | ${ }^{3}$ | － | 3 | － | － | － | ， | － | ， | 10 | 5 | 15 | － | － | － | － | － | － | － | － | ， | 2 | － | 2 | － | － | － | － | － | － | － | $\bigcirc$ | － | ${ }^{25}$ | － | 29 | － | － | 。 | － | $\bigcirc$ | － | ${ }^{\circ}$ |
|  | 2 | － | 2 | ＂ | － | ＂ | － | $\bigcirc$ | 7 | － | － | － | ， | － | ， | 19 | 10 | ${ }^{29}$ | － | － | － | － | － | － | ， | 。 | ， | ， | $\bigcirc$ | 1 | 3 | － | 3 | － | － | － | 3 | $\bigcirc$ | 3 | 40 | － | 45 | 2 | － |  | － | $\bigcirc$ | － | ${ }^{104}$ |
| 54.5 .600 | , | － | ， | ＂ | － | ＂ | ${ }^{8}$ | － | ： | － | 。 | － | － | － | ， | ${ }^{21}$ | ＂ | ${ }^{32}$ |  | － | ， | － |  | － | ， | － |  | 2 | 。 | 2 |  | 。 | 1 | － | － | － |  | － | 3 | ${ }^{12}$ |  | ${ }^{50}$ |  |  |  | － | $\bigcirc$ | － | ${ }^{113}$ |
| 8.00 | 3 | － | 3 | 5 | ， | － | － | － | － | － | $\bigcirc$ | － | 3 |  | ${ }^{3}$ | ${ }^{35}$ | 10 | ${ }^{4}$ |  |  |  |  |  | － |  | － |  | ${ }^{3}$ | － | 3 |  |  | ， | － |  | － | 2 | － | 2 | 3 | 5 | ${ }^{4}$ |  | － |  | － | $\bigcirc$ | － | ${ }^{15}$ |
| 6.45 | － | － | 4 | － | － | － | － | － | 10 | － | － | － | 3 | － | 3 | 36 | 10 | ${ }^{4}$ | － | － | － | $\bigcirc$ | － | － | ， | － | ， | 3 |  | － | 5 | － | 5 | － | $\bigcirc$ | － | ${ }^{3}$ | $\bigcirc$ | 3 | ${ }^{4}$ | 5 | ${ }^{5}$ | 3 | － | ${ }^{3}$ | － | － | － | ${ }^{14}$ |
| 6．30．6．45 | － | － | － | ${ }^{13}$ | － | 13 | ${ }^{\prime \prime}$ | － | ＂ | － | － | － | 3 | － | 3 | 50 | 18 | ${ }^{\circ}$ | 2 | － | 2 | － |  | $\bigcirc$ | － | － | 4 | － | $\bigcirc$ | － |  | $\bigcirc$ | 7 | － | 。 | － | ${ }^{3}$ | $\bigcirc$ | 3 | ${ }^{\circ}$ | － | ${ }^{6}$ | 4 | － | － | － | － | － | ${ }^{194}$ |
| 644． 730 |  | － | ${ }^{10}$ | 23 | － | 23 | ${ }^{\prime}$ | $\bigcirc$ | ${ }^{\prime \prime}$ | － | － | － | 5 | － | $\cdot$ | ${ }^{6}$ | 14 | ${ }^{5}$ | 2 | － | 2 | － |  | $\bigcirc$ | － | － | 4 | 13 | $\bigcirc$ | 13 | 4 | $\bigcirc$ | ． | － | － | － | 5 | $\bigcirc$ | 5 | ${ }^{\circ}$ | 13 | 97 | 5 | － | 5 | － | $\bigcirc$ | $\bigcirc$ | ${ }^{29}$ |
| 7．00，77．75 |  |  | ， | ${ }^{24}$ | $\bigcirc$ | ${ }^{24}$ | ＂ | ＇ | ${ }^{12}$ | － | － | $\bigcirc$ | － | － | 4 | ${ }_{5}$ | 17 | ${ }^{5}$ | － | － | $\cdot$ | $\bigcirc$ | 。 | $\bigcirc$ | $\checkmark$ | $\bigcirc$ | $\checkmark$ | ${ }^{13}$ | $\bigcirc$ | ${ }^{13}$ | 12 | ＇ | ${ }^{13}$ | $\bigcirc$ | － | － | － | $\bigcirc$ | 4 | ${ }^{68}$ | － | ${ }^{7}$ | 5 | － | 5 | － | $\bigcirc$ | － | ${ }^{26}$ |
| 2：15，730 | - | － | － | 3 | 1 | ${ }^{23}$ | 10 | $\bigcirc$ | 10 | $\bigcirc$ | $\bigcirc$ | － | ， | 1 | 8 | 79 | ${ }^{4}$ | $\stackrel{ }{4}$ | 4 | － | $\checkmark$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | 3 | $\bigcirc$ | 3 | ＂ | $\bigcirc$ | ${ }^{\prime \prime}$ | － | $\bigcirc$ | － | － | $\bigcirc$ | － | － | $\bigcirc$ | $\bigcirc$ | $\because$ | － | ${ }^{100}$ | 5 | － | － | － | $\bigcirc$ | － | ${ }^{20}$ |
| 7300.745 | 12 | ， | 12 | ${ }_{3}$ | $\bigcirc$ | ${ }_{36}$ | ${ }^{16}$ | $\bigcirc$ | ${ }^{16}$ | $\bigcirc$ | － | － | $\bigcirc$ | $\bigcirc$ | 8 | 8 | ${ }^{17}$ | ${ }^{9}$ | 5 | － | 5 | － | － | $\bigcirc$ | 2 | $\bigcirc$ | 2 | ${ }^{20}$ | 1 | 21 | ${ }^{18}$ | $\cdot$ | ${ }^{19}$ | － | － | － | － | $\bigcirc$ | － | $\because$ | 12 | 108 | 10 |  | ＂ | － | － | $\bigcirc$ | ${ }^{20}$ |
| ${ }^{248.5800}$ | ${ }^{19}$ | 2 | 20 | ${ }^{3}$ | － | ${ }^{63}$ | ${ }^{19}$ | $\bigcirc$ | ${ }^{19}$ | － | $\bigcirc$ | － | ${ }^{10}$ | 1 | ＂ | ${ }^{6}$ | 19 | 14 | 5 | － | 5 | － | － | － | 4 | $\bigcirc$ | ${ }^{4}$ | ${ }^{4}$ |  | ${ }^{38}$ | ＂ | $\bigcirc$ | ＂ | － | － | － | ${ }^{13}$ | $\bigcirc$ | ${ }^{13}$ | ${ }^{115}$ | 10 | ${ }^{125}$ | ${ }^{18}$ |  | ${ }^{18}$ | － | $\bigcirc$ |  |  |
| 8000．8．45 | ${ }^{28}$ | $\bigcirc$ | ${ }^{28}$ | ${ }^{6}$ | － | ${ }^{65}$ | s | 1 | 3 | $\bigcirc$ | － | － | ${ }^{\prime \prime}$ | $\bigcirc$ | ＂ | ${ }^{\circ}$ | ${ }^{17}$ | ${ }^{14}$ | ＂ | － | ${ }^{\prime \prime}$ | $\bigcirc$ | － | － | $\bigcirc$ | $\bigcirc$ | 8 | ${ }^{37}$ | 3 | 40 | ${ }^{10}$ | ＇ | ＂ | － | － | － | ${ }^{15}$ | ， | ${ }^{18}$ | 102 | ${ }^{15}$ | ${ }^{18}$ | ${ }^{13}$ |  | ${ }^{4}$ | － |  |  |  |
| ${ }^{315.85 .30}$ | 26 | － | ${ }^{3}$ | ${ }_{12}$ | 3 | ${ }^{11}$ | $\sim$ | $\bigcirc$ | 40 | － | － | $\bigcirc$ | ＂ | ， | 13 | ${ }^{107}$ | 16 | ${ }^{123}$ | － | ， | － | － | － | － | 5 | － | 5 | ${ }^{57}$ | 3 | $\infty$ | ${ }^{17}$ | ， | ${ }^{18}$ | － | － | － | ${ }^{18}$ |  | ${ }^{19}$ | ${ }^{105}$ | ${ }^{13}$ | ＂ | ${ }^{18}$ |  | ${ }^{19}$ | － | － | － | ${ }_{58}$ |
| 830 | 4 | 2 | ${ }^{8}$ | ${ }^{13}$ | ， | ${ }^{135}$ | 4 |  | 5 | － | 。 | － | 12 | 。 | 15 | ${ }^{8}$ | 18 | ${ }^{114}$ | ＂ | － | ＂ | － | － | － | － | － | － | 7 | － | 74 | ${ }^{20}$ | － | 2 | － | － | － | ${ }^{16}$ |  | ${ }^{17}$ | ${ }^{128}$ | ${ }^{12}$ | ${ }^{188}$ | ${ }^{18}$ | 2 | ${ }^{20}$ | － | － | － | ${ }^{\text {as }}$ |
| 845．900 | 4 | 2 | ${ }^{4}$ | ${ }^{129}$ | ， | ${ }^{12}$ | 5 | － | 5 | － | 。 | － | ${ }^{18}$ | 3 | 17 | ${ }^{113}$ | 17 | ${ }^{30}$ | ＂ | ， | 12 | － | － | － | ${ }^{10}$ | － | ＂ | ${ }^{6}$ |  | \％ | ${ }^{30}$ | ， | ${ }^{30}$ | － | － | － | ${ }^{13}$ | ， | ${ }^{14}$ | ${ }^{14}$ | 17 | 188 | 17 | ， | ${ }^{18}$ | － | － | 。 | ${ }^{\text {ar }}$ |
| 200 | ${ }^{26}$ | － | ${ }^{27}$ | $\infty$ | － | 8 | ${ }^{36}$ | － | ${ }^{36}$ | － | － | － | 13 | 。 | 13 | ${ }^{120}$ | ${ }^{18}$ | ${ }^{13}$ | ${ }^{13}$ | － | ${ }^{13}$ | － | － | － | ＇ | － | ， | ${ }^{*}$ | － | ${ }^{4}$ | ${ }^{22}$ | ， | 2 | 。 | － | － | ${ }^{26}$ | ， | ${ }^{26}$ | ${ }^{128}$ | ${ }^{13}$ | ${ }^{14}$ | ${ }^{14}$ | － | ${ }^{14}$ | － | － | － | ${ }^{56}$ |
| 2.45 | 12 | － | 12 | ${ }^{\circ}$ | 2 | $"$ | ${ }^{24}$ | － | ${ }^{24}$ | － | － | － | 14 | － | 14 | ${ }^{19}$ | 12 | ${ }^{13}$ | 10 | － | 10 | － | － | － | ， | － | ， | 4 | － | 4 | ${ }^{27}$ | － | ${ }^{27}$ | － | － | － | 19 | 3 | ${ }^{2}$ | 12 | 15 | ${ }^{18}$ | － | － | － | － | $\bigcirc$ | － |  |
| 0.30 | ${ }^{\circ}$ | － | ${ }^{16}$ | 4 | ＇ | 5 | ${ }^{28}$ | $\bigcirc$ | ${ }^{28}$ | － | － | － | ＂ | 1 | 12 | ＂ | 18 | ${ }^{12}$ | ＂ | － | 12 | － | － | － | － | ， | － | ${ }^{6}$ | 2 | 8 | ${ }^{24}$ | － | ${ }^{24}$ | － | － | － | ${ }^{19}$ | 1 | ${ }^{20}$ | 131 | 15 | ${ }^{14}$ | － | ， | 7 | － | － | － | 41 |
| 0．45 1.000 | 15 | 1 | ${ }^{16}$ | 5 | － | \％ | ${ }^{26}$ | 1 | ${ }^{27}$ | $\bigcirc$ | － | － | ＂ | $\bigcirc$ | ${ }^{\prime \prime}$ | ${ }_{12}$ | 18 | ${ }^{128}$ | ${ }^{13}$ | － | ${ }^{13}$ | － | $\bigcirc$ | $\bigcirc$ | － | $\bigcirc$ | $\cdot$ | 5 | 2 | ${ }^{2}$ | 32 | 1 | 32 | － | $\bigcirc$ | $\bigcirc$ | 14 | 1 | 15 | ${ }^{18}$ | 13 | ${ }^{138}$ | 10 | ， | ＂ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | ${ }_{522}$ |
| Toat | $230$ | ${ }^{4}$ | ${ }^{30}$ | ${ }^{27}$ | 15 | ${ }^{12}$ | ${ }^{\circ}$ |  | ${ }^{14}$ | － | $\bigcirc$ | － | ${ }^{112}$ | 12 | 15 | 130 |  |  | ${ }^{119}$ | ． | ${ }^{12}$ |  |  |  | ${ }^{7}$ |  |  | ${ }^{17}$ | ${ }^{8}$ |  | ${ }^{25}$ |  | ${ }^{28}$ |  |  |  |  |  | 20 |  | ${ }^{24}$ |  |  |  |  |  |  |  |  |
| ${ }_{\text {a }}^{\text {ampreak }}$ | ${ }^{145}$ |  |  | 45 |  | ${ }^{45}$ | ${ }^{178}$ |  | ${ }^{180}$ | $\bigcirc$ |  |  |  |  | ${ }^{5}$ |  |  | ${ }^{505}$ |  | $\stackrel{2}{2}$ | － |  | $\bigcirc$ | $\bigcirc$ | ${ }^{2}$ |  | － | ${ }^{23}$ |  | ${ }^{245}$ | $\stackrel{8}{9}$ | 2 | $\because$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | － | 4 | ${ }^{6}$ | soo | ${ }^{\text {ss }}$ | ${ }_{5}{ }^{\text {ss }}$ | ${ }^{8}$ | 3 | ${ }^{1}$ | ， | $\bigcirc$ | $\bigcirc$ | ${ }^{264}$ |
| $\stackrel{\mathrm{fmex}}{\mathrm{~mm}}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1400.4 | ${ }^{14}$ | － | ${ }^{14}$ | ${ }^{40}$ | ＇ | ${ }^{4}$ | ${ }^{22}$ | － | ${ }^{2}$ | $\circ$ | $\bigcirc$ | $\bigcirc$ | ${ }^{28}$ | 1 | ${ }^{29}$ | ${ }^{148}$ | ${ }^{\prime \prime}$ | ${ }_{10} 8$ | ${ }^{10}$ | － | 10 | $\circ$ | $\bigcirc$ | $\circ$ | 8 | 1 | $\therefore$ | ${ }_{6} 5$ | － | ${ }^{65}$ | ${ }^{3}$ | － | ${ }^{4}$ | － | － | － | ${ }^{21}$ | － | 22 | ${ }_{18} 8$ | ${ }^{13}$ | 178 | 8 | ， | ${ }^{10}$ | － | － | － |  |
| 14.45 ， 14 | 12 | － | 12 | 4 | 2 | 4 | ${ }^{22}$ | $\bigcirc$ | ${ }^{23}$ | － | － | － | ${ }^{28}$ | $\bigcirc$ | ${ }^{28}$ | ${ }^{128}$ | 14 | ${ }^{12}$ | $\bigcirc$ | $\bigcirc$ | ， | － | － | $\bigcirc$ | － | ， | － | 6 | － | ＊ | ${ }^{12}$ | ＇ | ${ }^{4}$ | － | － | － | 15 | 1 | ${ }_{1}$ | ${ }^{129}$ | ${ }^{16}$ | 145 | ${ }^{10}$ | － | 10 | － | － | － |  |
| 1430.14 | 12 | － | 12 | 40 | $\bigcirc$ | 40 | ${ }^{26}$ | ＇ | ${ }^{27}$ | － | － | － | ${ }^{25}$ | ＝ | ${ }^{27}$ | ${ }^{14}$ | 13 | 158 | ${ }^{14}$ | $\bigcirc$ | 15 | $\bigcirc$ | － | － | ＂ | － | ＂ | ${ }^{\circ}$ | ＇ | ${ }^{6}$ | 4 | － | ${ }^{4}$ | － | － | $\bigcirc$ | ${ }^{16}$ | － | ${ }^{16}$ | ${ }^{125}$ | ${ }^{16}$ | $1{ }^{1 / 2}$ | 15 | － | 15 | － | $\bigcirc$ | － |  |
| 14.45 | ${ }^{14}$ | $\bigcirc$ | ${ }^{14}$ | 5 | 2 | 53 | ${ }^{19}$ | $\bigcirc$ | 20 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | 2 | 1 | 22 | ${ }^{138}$ | 12 | ${ }^{150}$ | ${ }^{1}$ | $\bigcirc$ | ${ }^{\prime \prime}$ | － | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | 8 | 70 | 2 | ${ }^{3}$ | 40 | $\bigcirc$ | 40 | $\bigcirc$ | － | $\bigcirc$ | 20 | $\bigcirc$ | ${ }^{20}$ | 14 | 15 | ${ }^{188}$ | ${ }^{13}$ | － | ${ }^{13}$ | $\bigcirc$ | $\bigcirc$ | － | ${ }^{51}$ |
| 1550 | 2 | $\bigcirc$ | ${ }^{22}$ | 5 | ＇ | ${ }_{5}$ | ${ }^{23}$ | $\cdot$ | ${ }^{23}$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | 2 | 1 | 2 | ${ }^{123}$ | ${ }^{14}$ | ${ }^{137}$ | ${ }^{15}$ | $\bigcirc$ | ${ }^{15}$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\stackrel{\square}{\circ}$ | $\bigcirc$ | $\because$ | ${ }^{8}$ | ${ }^{1}$ | ${ }^{35}$ | ${ }^{3}$ | ＋ | ${ }^{35}$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | ${ }^{18}$ | $\bigcirc$ | ${ }^{18}$ | 14 | ${ }^{18}$ | ${ }^{188}$ | ${ }^{16}$ |  | ${ }^{16}$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | ${ }^{60}$ |
| ${ }^{18,15}$ | ${ }^{37}$ | $\bigcirc$ | ${ }^{37}$ | ${ }^{6}$ | ＇ | ${ }^{6}$ | 30 |  | 30 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | 30 | 5 | ${ }^{35}$ | 138 | 12 | ${ }^{155}$ | ＂ | ＇ | 12 | － | － | $\bigcirc$ | － | $\bigcirc$ | 8 | ${ }^{\text {w9 }}$ | 2 | ＂${ }^{\prime}$ | ${ }^{4}$ | $\bigcirc$ | 43 | － | $\bigcirc$ | $\bigcirc$ | 20 | 1 | ${ }^{21}$ | 14 | ${ }^{14}$ | ${ }^{155}$ | ${ }^{13}$ |  | ${ }^{13}$ | － | $\bigcirc$ | － | a¢ |
|  | ${ }^{4}$ |  | 50 | ${ }^{108}$ |  | ${ }^{116}$ | 12 |  | ${ }^{3}$ |  | － | － | ${ }^{26}$ |  | ${ }^{36}$ | ${ }^{156}$ | 12 | ${ }^{168}$ | ${ }^{16}$ | $\bigcirc$ | ${ }^{14}$ | － |  | － | 8 | － |  | 12 |  | ${ }^{5}$ | ${ }^{37}$ |  | ${ }^{37}$ | $\bigcirc$ |  |  | 2 |  |  | ${ }^{19}$ |  | ${ }^{18}$ |  |  |  |  |  |  | ${ }^{12}$ |
| 11845.1850 | 21 | ， | 2 | ${ }^{4}$ | ， | ${ }^{85}$ | ${ }_{36}$ | － | ${ }^{6}$ | － | － | － | ${ }^{26}$ | － | 26 | 156 | ＂ | 187 | ${ }^{17}$ | ， | ${ }^{18}$ | － | － | － | 10 | $\bigcirc$ | 10 | 8 | － | 8 | ${ }^{38}$ | － | ${ }_{3}$ | － | － | － | ${ }^{17}$ | － | 17 | ${ }^{136}$ | ${ }^{13}$ | ${ }^{\text {ra }}$ | ＂ | ＇ | 12 | － | $\bigcirc$ | － | ${ }_{650}$ |
| 1850.188 .4 | ${ }^{21}$ | － | ${ }^{21}$ | ${ }^{54}$ | ， | ${ }_{5}$ | ${ }^{25}$ | － | ${ }^{25}$ | － | － | － | ${ }^{37}$ | $\bigcirc$ | ${ }^{37}$ | 145 | － | ${ }^{174}$ | 12 | － | 12 | － | － | － | 8 | － | 8 | ${ }^{82}$ | $\bigcirc$ | ＊ | ${ }^{5}$ | － | 5 | － | － | － | 19 | $\bigcirc$ | ${ }^{19}$ | ${ }^{184}$ | ${ }^{13}$ | ${ }^{187}$ | 10 | － | 10 | － | $\bigcirc$ | － | ${ }_{6}$ |
| ${ }^{16,565.6 .430}$ | ${ }^{16}$ | － | ${ }^{16}$ | ${ }^{55}$ | $\bigcirc$ | ${ }^{55}$ | ${ }^{24}$ | $\bigcirc$ | ${ }^{24}$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | ${ }^{4}$ | $\bigcirc$ | ${ }^{34}$ | 145 | 14 | ${ }^{15}$ | ${ }^{13}$ | － | 13 | $\bigcirc$ | － | $\bigcirc$ | － | $\bigcirc$ | $\cdot$ | 9 | $\bigcirc$ | $\%$ | ${ }^{37}$ | $\bigcirc$ | ${ }^{37}$ | － | $\bigcirc$ | － | ${ }^{14}$ | $\bigcirc$ | ${ }^{15}$ | ${ }^{14}$ | ${ }^{13}$ | ${ }^{18}$ | ${ }^{12}$ | － | ${ }^{13}$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | ${ }^{688}$ |
| ${ }^{16} 8.30 .1645$ | ${ }^{24}$ | － | ${ }^{24}$ | ${ }^{55}$ | ＇ | ${ }_{5}$ | ${ }^{28}$ | ＇ | ${ }^{29}$ | $\bigcirc$ | － | － | ${ }^{25}$ | 1 | ${ }^{26}$ | ${ }^{132}$ | 10 | ${ }_{12}$ | － | $\bigcirc$ | $\bullet$ | $\bigcirc$ | － | $\bigcirc$ | 13 | $\bigcirc$ | 13 | ${ }^{12}$ | － | ${ }_{12}$ | ${ }^{1}$ | ， | ${ }^{4}$ | － | － | － | ${ }^{18}$ | ， | ${ }^{19}$ | ${ }^{159}$ | － | ${ }^{165}$ | ${ }^{16}$ | － | ${ }^{17}$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | ${ }^{66}$ |
| 14.45 .1780 | ${ }^{16}$ | － | 17 | ${ }_{58}$ | $\bigcirc$ | 59 | ${ }^{32}$ | － | ${ }^{32}$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | ${ }^{3}$ | $\bigcirc$ | ${ }^{35}$ | ${ }^{129}$ | ＂ | ${ }^{150}$ | 17 | ＇ | 18 | － | － | － | ＂ | $\bigcirc$ | ＂ | ${ }^{118}$ | $\bigcirc$ | ${ }^{116}$ | 4 | － | 47 | $\bigcirc$ | － | $\bigcirc$ | ${ }^{19}$ | $\bigcirc$ | 19 | ${ }^{13}$ | ＂ | ${ }^{1 / 2}$ | ${ }^{16}$ | $\bigcirc$ | ${ }^{16}$ | － | $\bigcirc$ | － | ${ }^{60}$ |
| 1720．077： | ${ }^{14}$ | － | ${ }^{14}$ | ${ }^{4}$ | $\bigcirc$ | 4 | 26 | － | 26 | － | $\bigcirc$ | $\bigcirc$ | 45 | － | 45 | 157 | － | ${ }^{168}$ | 15 | $\bigcirc$ | ${ }^{15}$ | － | － | － | 12 | － | 12 | ня | $\bigcirc$ | 150 | 59 | － | ${ }^{\circ}$ | － | － | － | 15 | － | 15 | ${ }^{134}$ | ＂ | ${ }^{1 / 5}$ | ${ }^{16}$ | $\bigcirc$ | ${ }^{16}$ | － | $\bigcirc$ | $\bigcirc$ | ${ }^{70}$ |
| 18.5 | ${ }^{2}$ | $\bigcirc$ | ${ }^{23}$ | ${ }^{4}$ | $\bigcirc$ | ${ }^{4}$ | ${ }^{27}$ | $\bigcirc$ | ${ }^{27}$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | ${ }^{48}$ | $\bigcirc$ | 48 | ${ }^{49}$ | $\bigcirc$ | 158 | ＂ | $\bigcirc$ | ＂ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | 10 | $\circ$ | 10 | ${ }^{135}$ | $\bigcirc$ | ${ }^{135}$ | 50 | － | so | $\bigcirc$ | $\bigcirc$ | － | ${ }^{17}$ | ＇ | ${ }^{18}$ | ${ }^{13}$ | － | $1 / 2$ | 2 |  | 2 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | ${ }^{\text {e9 }}$ |
| 173：0， 71745 | 16 | $\bigcirc$ | ${ }^{16}$ | ${ }^{37}$ | － | ${ }^{37}$ | ， | $\bigcirc$ | ${ }^{24}$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | ${ }^{36}$ | 1 | ${ }^{37}$ | 12 | $\bigcirc$ | ${ }^{131}$ | 8 | － | 8 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | 7 | $\bigcirc$ | 7 | ＂18 | $\bigcirc$ | ${ }_{18}$ | 50 | － | 50 | $\bigcirc$ | － | － | － | $\bigcirc$ | 8 | ${ }^{120}$ | 10 | ${ }^{129}$ | 12 |  | 12 | － | $\bigcirc$ |  | so |
| 17245，1800 | 13 | － | ${ }^{13}$ | ${ }^{4}$ | － | 43 | ${ }^{30}$ | $\bigcirc$ | 3 |  | － |  | 28 |  | 28 | ${ }^{17}$ | $\cdot$ | ${ }^{123}$ | 13 | $\bigcirc$ | 13 | － | － | － | ， | － | \％ | ${ }^{8}$ |  | ${ }^{23}$ | ${ }^{30}$ | － | 30 | － | － | $\bigcirc$ | ${ }^{14}$ | － | 14 | ＂5 | 4 | ${ }^{119}$ | 10 | － | 10 | － |  |  | ${ }^{54}$ |
| $1800 \cdot 1884$ | － | － | － | ${ }^{29}$ | 。 | ${ }^{29}$ | ${ }^{18}$ | － | ${ }^{18}$ | － | 。 | － | ${ }^{28}$ | 。 | ${ }^{28}$ | ${ }^{25}$ | － | ${ }^{10}$ | ， | $\bigcirc$ | $\bigcirc$ | － | － | $\bigcirc$ | － | $\bigcirc$ | 4 | 12 | － | 12 | ${ }^{29}$ | － | 2 | － | $\bigcirc$ | $\bigcirc$ | ${ }^{14}$ | $\bigcirc$ | ${ }^{14}$ | \％ | － | ${ }^{107}$ | 10 | － | 10 | － | $\bigcirc$ | － | ${ }^{42}$ |
| 8， 15. | 10 | 。 | 10 | ${ }^{37}$ | 。 | ${ }^{37}$ | ${ }^{18}$ | － | 19 | － | 0 | － | ${ }^{20}$ | － | ${ }^{30}$ | ${ }^{4}$ | － | ${ }^{39}$ | ${ }^{13}$ | $\bigcirc$ | ${ }^{13}$ | － | $\bigcirc$ | － | 4 | $\bigcirc$ | 4 | ${ }_{5}$ | － | ${ }_{58}$ | 30 | － | 3 | － | － | － | ＂ | － | ＂ | ${ }^{85}$ | － | $\because$ | 10 | － | 10 | － | $\bigcirc$ | － | ${ }^{43}$ |
| 18380.1845 | 7 | － | 7 | ${ }^{4}$ | － | ${ }^{34}$ | 22 | － | 22 | － | － | － | ${ }^{23}$ | ， | ${ }^{24}$ | 7 | － | $\pi$ | ＂ | $\bigcirc$ | ＂ | － | $\bigcirc$ | $\bigcirc$ | － | － | － | ${ }_{58}$ | － | ${ }_{58}$ | ${ }^{28}$ | － | ${ }^{28}$ | － | － | － | 7 | － | 7 | ${ }^{83}$ | － | ${ }^{8}$ | － | － | － | － | $\bigcirc$ | － | ${ }^{368}$ |
| 18455 1900 | 8 | － | 8 | ${ }^{23}$ | $\bigcirc$ | ${ }^{23}$ | 19 | － | ${ }^{19}$ | － | － | － | ${ }^{18}$ | － | 18 | ${ }^{8}$ | 5 | ${ }^{3}$ | － | － | $\bigcirc$ | － | － | － | 5 | $\bigcirc$ | 5 | 45 | － | 45 | ${ }^{23}$ | － | ${ }^{23}$ | － | － | － | － | 0 | － | 8 | ， | ${ }^{88}$ | 7 | － | 7 | － | － |  | ${ }^{328}$ |



|  | neav |  | Ioun | Momemen |  | Toat | ${ }^{\text {a momememe }}$ |  | Toal |  |  | rom | ${ }^{\text {ame mamen }}$ |  | Toul | Lemm Hemers |  | Toest |  |  | Toat | $\begin{array}{c\|} \hline \text { Movement } \epsilon \\ \text { ht Heavy } \end{array}$ |  | Toun | Somment |  | Toot | $\begin{aligned} & \text { Hovem } \\ & \text { neom } \end{aligned}$ |  | out | Heavement |  | Toom |  | many | Toas | \％om | ＂v | remer |  |  | Toat | $\begin{aligned} & \text { lovement } \\ & \hline \text { Heavy } \end{aligned}$ |  | obl |  |  | Tout | ， |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $14.00 \cdot 1500$ | 52 | 1 | ${ }_{52}$ | ${ }^{12}$ | 4 | ${ }^{176}$ | 9 |  | $\because$ | － | 。 | 。 | ${ }^{106}$ | 3 | 107 | ${ }_{500}$ | 50 | \％10 | ${ }^{4}$ | ， | ${ }^{4}$ | 。 | 。 | － | ${ }^{35}$ | 1 | ${ }^{6}$ | 265 | 4 | 28 | ${ }^{168}$ | 2 | 188 | 。 | 。 | － | ${ }^{12}$ | 2 | ${ }^{7}$ | ${ }_{59} 9$ | \％ | 59 | ${ }^{46}$ | ， | 48 | 。 | － | － | ${ }^{2135}$ | ${ }^{131}$ | 2265 |
| ${ }_{1} 415$ | ${ }^{6}$ | ， | $\because$ | ${ }^{185}$ | 5 | ${ }^{180}$ | $\%$ | 2 | $\because$ | － | 。 | － | ${ }^{9}$ | 3 | ${ }^{100}$ | ${ }^{53}$ | 5 | sir | 49 | ， | 4 | 。 | － | － | ${ }^{37}$ |  | ${ }^{3}$ | ${ }^{238}$ |  | ${ }^{28}$ | 157 | 2 | 159 | － | － | － | ${ }^{6}$ | 2 | 70 | ${ }_{56} 6$ | 6 | ${ }^{\text {612 }}$ | ${ }_{5}$ | － | $s$ | － |  | － | ${ }_{2159}$ | ${ }^{14}$ |  |
| 14.30 | ${ }^{85}$ | ， | ${ }^{6}$ | 208 | ¢ | ${ }^{213}$ | 9 | 2 | 100 | － | － | － | ${ }^{8}$ | － | 107 | ${ }_{59} 9$ | 51 | \％o | 5 | ， | 5 | － | － | － | ${ }^{26}$ |  | ${ }^{6}$ | ${ }^{33}$ |  | ${ }_{37}$ | ${ }^{188}$ | ， | ${ }^{15}$ | 。 | － | 。 | ${ }^{74}$ |  | ${ }^{5}$ | ${ }_{58} 5$ | ${ }^{\circ}$ | ${ }^{62}$ | 5 | － | $\because$ | － | － | － | ${ }^{203}$ | ${ }^{14}$ |  |
| 14.45 .154 .4 | ${ }^{122}$ |  | ${ }^{124}$ | ${ }^{27}$ |  | ${ }^{28}$ | 114 |  | ${ }^{16}$ | － | 。 | － | ${ }^{101}$ | 1 | ${ }^{115}$ | ${ }_{500}$ | 50 | \％10 | 5 | ， | 32 |  |  | － | ${ }^{3}$ |  | ${ }^{3}$ | ${ }_{38}$ |  | ${ }^{34}$ | 158 |  | ${ }^{155}$ | － |  |  | \％ |  | 8 | ${ }_{3} 8$ |  | 8 |  |  | ss |  |  |  | ${ }^{2684}$ | ${ }^{151}$ |  |
| 15：50，16：00 | ${ }^{29}$ | 2 | 13 | ${ }^{39}$ | ＂ | 320 | ${ }^{130}$ | 2 | 132 |  | 。 | － | ${ }^{105}$ |  | ${ }^{19}$ | ${ }^{57}$ | ${ }^{4}$ | ${ }^{62}$ | 5 |  | 5 | 。 | － |  | ${ }^{35}$ |  | ${ }^{5}$ | 35 |  | ${ }^{351}$ | ${ }^{51}$ |  | ${ }^{152}$ |  |  |  | ${ }^{7}$ |  | 7 | ${ }_{57}$ | 5 | ${ }^{63}$ | 52 |  | 54 |  |  |  | ${ }^{236}$ | 147 |  |
| 15.518 .14 .15 | ${ }^{128}$ | s | 130 | ${ }_{3} 3$ | ＂ | ${ }^{32}$ | ${ }^{13}$ | ， | ${ }^{13}$ | 。 | － | － | ${ }^{20}$ | ， | ${ }^{3}$ | ${ }^{80}$ | ${ }^{3}$ | ${ }^{68}$ | 5 | 2 | 5 | 。 | － | － | 3 |  | ${ }^{3}$ | ${ }_{34}$ |  | 39 | ${ }_{188}$ |  | 14 | ． | － |  | 7 |  | \％ | 50 | 5 | ${ }^{63}$ | 4 |  | 4 |  |  | － | ${ }^{2615}$ | ${ }^{138}$ |  |
|  | ${ }^{107}$ | 3 | 110 | ${ }^{30}$ | 10 | 31 | ${ }^{126}$ | ， | ${ }^{127}$ | － | － | － | ${ }^{124}$ | ． | ${ }^{13}$ | ${ }^{62}$ | ${ }^{4}$ | ${ }_{6}$ | 56 | ， | 5 | 。 | － | － | 32 | － | ${ }^{3}$ | ${ }_{30}$ | 3 | 33 | ${ }_{182}$ | － | 153 | － | － | － | ${ }^{3}$ | － | ${ }^{3}$ | ${ }_{88} 8$ | 5 | ${ }^{\text {es8 }}$ | 45 | 2 | 4 | 。 |  | 。 | ${ }^{2568}$ | ${ }^{125}$ |  |
| 15.45. | 8 | 2 | ${ }^{8}$ | ${ }^{24} 8$ | 3 | ${ }^{251}$ | ${ }^{113}$ | ， | ${ }^{14}$ | － | － | － | 122 | ， | ${ }^{123}$ | ${ }^{618}$ | ${ }^{4}$ | ${ }_{6}$ | 51 | ， | 52 | － | － | － | ${ }^{37}$ | － | ${ }^{37}$ | ${ }^{370}$ | ， | 370 | ${ }^{188}$ | ， | 160 | － | － | － | ${ }^{6}$ | ， | 70 | ${ }_{597}$ | 45 | ${ }_{6}$ | 4 | 2 | 5 | － | － | － | ${ }^{233}$ | 102 |  |
| 18000 | ＂ | 1 | ${ }^{8}$ | 22 | 2 | ${ }^{225}$ | ${ }^{109}$ | ， | ${ }^{109}$ | － | － | － | 130 | ＋ | ${ }^{32}$ | 6 | ${ }^{4}$ | ws | 5 | ， | 52 | － | － | － | 38 | － | ${ }^{3}$ | ${ }^{80}$ | ． | ${ }^{407}$ | ${ }^{17}$ | ＋ | ${ }^{178}$ | － | － | － | 70 | ， | $\stackrel{ }{\prime \prime}$ | ${ }_{5} 5$ | ${ }^{4}$ | ${ }^{68}$ | ${ }^{54}$ | ， | ${ }^{5}$ | － | 。 | － | 259 | ${ }^{9}$ |  |
| 18.45 | 70 | ， | ${ }^{7}$ | ${ }^{212}$ | ， | ${ }^{213}$ | 198 | ， | ${ }^{10}$ | － | － | － | ${ }^{138}$ | 1 | 140 | ${ }_{593}$ | 4 | ${ }^{65}$ | ${ }^{54}$ | 1 | ${ }^{\text {ss }}$ | － | － | － | 4 | － | 4 | 47 | － | ． | ${ }^{185}$ | ， | ${ }^{186}$ | － | － | － | ${ }^{6}$ | 1 | $\square$ | $5{ }_{5}$ | ${ }^{4}$ | ${ }^{613}$ | ${ }^{6}$ | ， | ${ }^{2}$ | － | 。 | － | 258 | $\because$ |  |
| $18.30 \cdot 173$ | ${ }^{76}$ |  | ＂ | 201 |  | ${ }^{23}$ | 13 |  | 14 | － |  | － | ${ }^{132}$ |  | 184 | ${ }_{597}$ | ${ }^{37}$ | ${ }^{\text {es }}$ | ${ }^{5}$ |  | ss |  |  |  | 4 |  | 4 | ${ }^{512}$ |  | 512 | ${ }^{188}$ |  | ${ }^{20}$ |  |  |  | ${ }^{6}$ |  | 70 | ${ }_{57}$ |  | ${ }^{59}$ |  |  | $\because$ |  |  |  | ${ }^{264}$ | 8 |  |
| 18.45 .578 .45 | ${ }^{6}$ | ， | ${ }^{\circ}$ | ${ }^{183}$ | ， | ${ }^{184}$ | 19 | － | 19 | － | － | － | ${ }^{163}$ | 2 | 14 | 587 | ${ }^{6}$ | ${ }^{603}$ | 5 | ， | 5 | － | － | － | 40 |  | 4 | ${ }^{518}$ |  | 518 | 226 |  | ${ }^{207}$ | 。 | － | － | 59 |  | $\cdots$ | ${ }^{18}$ | ${ }^{\prime}$ | ${ }_{5} 5$ | ${ }_{6}$ | 。 | ${ }_{6}$ |  |  |  | ${ }^{259}$ | ${ }^{8}$ |  |
| 17200．18000 | ${ }^{5}$ | － | ${ }^{6}$ | ${ }^{188}$ | － | ${ }^{188}$ | ${ }^{108}$ | － | ${ }^{108}$ | － | － | － | 157 | 2 | 139 | ${ }_{5}$ | 3 | sr | ${ }^{47}$ | $\bigcirc$ | 4 | － | － | － | ${ }^{5}$ | 。 | ${ }^{6}$ | 485 | 。 | 485 | ${ }^{180}$ | － | 190 | － | － | － | ${ }_{5}$ |  | ${ }_{5}$ | ${ }^{50}$ | ${ }^{4}$ | ${ }^{56}$ | ${ }^{6}$ | － | ${ }^{\circ}$ | － | － | 。 | ${ }^{246}$ | ＂ |  |
| 17：75，18：75 | $\infty$ | － | ${ }^{\circ}$ | ${ }_{13} 18$ | ， | 158 | ${ }^{180}$ | ， | 100 | － | － | － | ${ }^{14}$ | 2 | ${ }^{14}$ | ${ }^{483}$ | 3 | ${ }^{14}$ | 4 | － | ${ }^{4}$ | － | － | － | ${ }^{28}$ | － | ${ }^{28}$ | 407 | － | 407 | ${ }^{159}$ | － | 159 | － | － | － | ${ }_{5}$ | ， | ${ }^{5}$ | 46 | 32 | 488 | ${ }_{5}$ | － | ${ }^{4}$ | － | － | － | 22.5 | ${ }^{6}$ |  |
| 1730．1830 | 4 | － | 4 | 14 | ， | 146 | $\because$ | ， | 2 | － | － | － | ${ }^{123}$ | 2 | ${ }^{125}$ | 48 | ${ }^{27}$ | 45 | 43 | － | ${ }^{4}$ | － | － | － | 2 | － | 22 | 330 | － | 330 | ${ }^{138}$ | － | ${ }^{139}$ | － | － | － | ${ }^{47}$ | － | 4 | 418 | 29 | 47 | 4 | － | 4 | － | － | 。 | ${ }_{188} 8$ | 8 |  |
| 178.5 －1845 | ${ }^{38}$ | － | ${ }^{38}$ | 12 | ， | 14 | ${ }^{8}$ | ， | $\because$ | － | － | － | ${ }^{109}$ | 2 | ＂ | ${ }^{387}$ | ${ }^{24}$ | ${ }^{39}$ | 4 | $\bigcirc$ | 4 | － | － | － | 20 | 。 | ${ }^{20}$ | ${ }^{27}$ | － | 270 | ${ }^{16}$ | $\bigcirc$ | ${ }^{17}$ | － | － | － | 4 | － | 4 | ${ }_{31}$ | 25 | 46 | ${ }^{8}$ | － | ${ }^{8}$ | － | － | － | ${ }_{168}$ | 53 |  |
|  |  |  |  | ${ }^{22}$ |  | ${ }^{23}$ | 7 |  | ${ }^{5}$ |  |  |  | \％ |  | 100 | ${ }^{318}$ | 23 | ${ }^{34}$ | 4 | $0$ | 4 | $0$ | $0$ |  | ${ }^{18}$ |  | ${ }^{18}$ | 232 |  | 22 | 10 |  | 10 |  |  |  | 4 |  | 4 | ${ }^{36}$ | ${ }^{28}$ | ${ }^{37}$ | ${ }^{35}$ |  | ${ }^{35}$ |  |  | 。 | ${ }^{1775}$ |  |  |






$=4=1$












$\pm=$


| mep | 4 | many | Toat | Lom | namy | Toom | Lom | many | Toat | ${ }^{\text {Lomm }}$ | maxy | Toun | Lom | nmaxy | Toat | Lomm | neay | Tout | Lom | many | Toat | Lom | maxy | Toon | 4 | maxy | Toat | Lom | neay | Tout | Lom | many | Toon | Lomm | maxy | Tout | ${ }^{\text {Lomm }}$ | neaxy | Toon | Lomm | neasy | Tool | ${ }^{\text {Lomm }}$ | maxy | Toon | ${ }^{\text {bomm }}$ | many | Toat | Lem | max |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5．00．6．00 | － | － | ， | ${ }^{2}$ | 1 | $\stackrel{ }{ }$ | － | － | 5 | 。 | $\bigcirc$ | － | 1 | $\bigcirc$ | 1 | ${ }^{16}$ | － | ${ }^{17}$ | ${ }^{26}$ | $\bigcirc$ | 25 | － | － | － | 5 | － | － | 14 | 1 | 15 | 3 | $\bigcirc$ | 3 | － | $\bigcirc$ | － | 19 |  | ${ }^{20}$ | 24 | － | ${ }^{25}$ | 2 | － | 2 | 。 |  | － | ${ }^{298}$ | ＊ | ${ }^{2123}$ |
| 5．15．6．48 | ， | － | ， | ${ }^{109}$ | 2 | ${ }^{106}$ | － | － | － | － | $\bigcirc$ | － | 2 | － | 2 | ${ }^{24}$ |  | ${ }^{26}$ | ${ }^{29}$ | $\bigcirc$ | ${ }^{29}$ | － | － | － | － | － |  | ${ }^{16}$ |  | ＂ | 4 | 。 | － | 0 |  | － | ${ }^{29}$ |  | ${ }^{29}$ | 32 |  | 32 |  | － |  |  |  | － | ${ }^{288}$ | 5 |  |
| 550.650 | 2 | 1 | 2 | ＂1 | 3 | ${ }^{114}$ | － | － | － | － | － | － | 3 |  | 3 | 32 |  | ${ }^{3}$ | ${ }^{4}$ | $\bigcirc$ | 4 |  |  | － |  |  | － | ${ }^{21}$ |  | ${ }^{24}$ |  | － | ， |  |  |  | 40 |  | 4 | ${ }^{6}$ |  | ${ }^{37}$ |  |  |  |  | － | $\bigcirc$ | ${ }^{312}$ | $\stackrel{ }{ }$ |  |
| 5．4．5．44 | 3 | ， | 4 | ${ }^{151}$ | 3 | 154 | ＂ | － | ＂ | － | － | － | 4 | － | 4 | ${ }^{39}$ |  | 40 | 60 | $\bigcirc$ | ¢ |  |  | － | ＂ | 0 | ＂ | ${ }^{30}$ |  | ${ }^{4}$ |  |  | 10 |  |  | ， | ${ }^{55}$ |  | ${ }_{5}$ | 45 |  | 4 | ¢ | － |  | 。 | $\bigcirc$ | － | ${ }^{42}$ | 12 |  |
| 600．7．700 | 4 | ， | 5 | ${ }^{22}$ | 4 | ${ }^{21}$ | ${ }^{14}$ |  | ${ }^{14}$ | － | － | － | － | 1 | $\checkmark$ | － |  | － | － | ＇ | ${ }^{7}$ | － | ． | － | ${ }^{13}$ | － | ${ }^{13}$ | ${ }^{5}$ |  | ${ }^{\text {sf }}$ | ${ }^{16}$ |  | ${ }^{16}$ | ， |  |  | 79 |  | 8 | 53 |  | s | 4 |  |  | 。 | － | － | ${ }^{59}$ | － |  |
| 6．15．7．715 | 8 | 1 | － | ${ }^{266}$ | 5 | ${ }^{27}$ | ${ }^{18}$ | ， | ${ }^{18}$ | － | $\bigcirc$ | － | 7 | 1 | － | 5 | 1 | 52 | ${ }^{3}$ | ， | ${ }^{*}$ | － | － | － | ${ }^{16}$ | ， | ${ }^{16}$ | 7 | 5 | ＂ | ${ }^{20}$ | ， | ${ }^{21}$ | 2 | 。 | 2 | ${ }^{8}$ | ＝ | ${ }^{3}$ | ${ }^{6}$ |  | ${ }^{8}$ | 5 | ， | － | － | － | － | ${ }^{705}$ | ${ }^{20}$ |  |
| ${ }^{6.300 .730}$ | ， | $\bigcirc$ | － | ${ }^{323}$ | 4 | ${ }^{32}$ | ${ }^{21}$ | ， | 2 | － | $\bigcirc$ | 1 | － | 1 | － | ${ }^{68}$ | 2 | 70 | ${ }^{108}$ | 1 | ${ }^{109}$ | － | － | － | ${ }^{20}$ | 1 | ${ }^{21}$ | ${ }^{3}$ | 5 | 9 | ${ }^{24}$ | ， | 25 | 4 |  | 4 | ${ }^{87}$ | ＊ | $\because$ | $\pi$ | 3 | 8 | 5 | 1 |  | － |  |  | ${ }^{\text {as }}$ | ${ }^{25}$ |  |
|  | ＂ | － | ＂ | ${ }^{371}$ | 4 | ${ }^{375}$ | 2 | ， | ${ }^{23}$ | － | $\bigcirc$ | 1 | 10 | 1 | ${ }^{11}$ |  |  | ${ }^{8}$ | ${ }^{20}$ | ， | ${ }^{121}$ | － | － | － | ${ }^{23}$ | 1 | ${ }^{24}$ | ${ }^{19}$ | 5 | ${ }^{123}$ | ${ }^{32}$ | ， | ${ }^{3}$ | 5 | － | 5 | ${ }^{25}$ | － | $\cdots$ | \％ | 5 | $\because$ | － | 1 |  | － |  | － | ${ }^{97}$ | 26 |  |
| 2000．800 | ${ }^{17}$ | － | ${ }^{17}$ | ${ }^{41}$ | 5 | 45 | ${ }^{26}$ | 1 | 2 | － | $\bigcirc$ | 1 | 12 | 0 | ${ }^{13}$ | ${ }^{5}$ | 2 | $\because$ | ${ }^{14}$ | 1 | ${ }^{19}$ | － | － | － | 25 | ， | ${ }^{26}$ | 113 | 5 | ${ }^{18}$ | ${ }^{34}$ | 2 | ${ }^{37}$ | － | － | － | ${ }^{10}$ |  | ${ }^{14}$ | 107 |  | ${ }^{11}$ | － | － |  | － | － | － | ${ }^{13}$ | ${ }^{27}$ |  |
| 2715．8．15 | ${ }^{18}$ | － | ${ }^{18}$ | 49 | 5 | ${ }_{504}$ | ${ }^{33}$ | 1 | ${ }^{3}$ | － | $\bigcirc$ | － | 14 | － | 14 | 13 | 2 | ${ }^{15}$ | ${ }^{188}$ | － | 16 | － | － | － | ${ }^{30}$ | 1 | 3 | ${ }^{129}$ | 5 | ${ }^{134}$ | ${ }^{38}$ | 3 | 4 | － | － | － | ${ }^{150}$ | 5 | 135 | ${ }^{125}$ | ¢ | ${ }^{128}$ | － | － | － | ， | － | ， | ${ }^{133}$ | ${ }^{26}$ |  |
| ${ }^{7} 300.830$ | ${ }^{26}$ | 1 | ${ }^{27}$ | ${ }^{601}$ | － | ${ }^{600}$ | ${ }^{12}$ | $\bigcirc$ | 4 | ＇ | － | 1 | ${ }^{19}$ | 1 | ${ }^{20}$ | ${ }^{13}$ | 3 | 134 | ${ }^{188}$ | － | ${ }^{197}$ | － | － | － | ${ }^{34}$ | － | ${ }^{34}$ | ${ }^{61}$ | 5 | ${ }^{167}$ | 4 | 3 | 5 | 10 | ， | 11 | ${ }^{203}$ | － | ${ }_{207}$ | ${ }^{132}$ | ＊ | ${ }^{156}$ | $\checkmark$ | ， | － | ， | － | ， | ${ }^{163}$ | ${ }^{32}$ |  |
| $7_{7} 7.45 .845$ | ${ }^{4}$ | 1 | ${ }_{3}$ | ${ }^{678}$ | 12 | ${ }^{61}$ | ${ }^{0}$ | 1 | ${ }^{\circ}$ | 2 | － | 2 | ${ }^{30}$ | 1 | 32 | 158 | 3 | ${ }^{48}$ | 216 | 2 | 218 | － | － | － | 4 | 1 | 45 | ${ }^{198}$ | 5 | 198 | ${ }^{6}$ | 4 | 6 | ${ }^{15}$ | ＇ | ${ }_{15}$ | 246 | 3 | 230 | ${ }^{17}$ | 3 | ${ }^{130}$ | 10 | ＇ | ＂ | ＇ | － | ， | ${ }_{182}$ | ${ }^{38}$ |  |
| 800．900 | ${ }^{39}$ | 2 | 4 | ${ }^{67}$ | ${ }^{4}$ | ${ }^{71}$ | ${ }^{63}$ | 1 | ${ }^{6}$ | 2 | $\bigcirc$ | 2 | ${ }^{38}$ | 1 | ${ }^{39}$ | 170 | 5 | ${ }^{175}$ | ${ }^{23}$ | 2 | 240 | － | － | － | ${ }^{6}$ | 2 | 6 | ${ }^{227}$ | 5 | 22 | ${ }^{74}$ | 3 | ${ }^{6}$ | ${ }^{18}$ | ＇ | ${ }^{18}$ | 24 | 3 | ${ }^{250}$ | ${ }^{193}$ | 3 | 196 | 12 | ， | ${ }^{3}$ | 2 | － | 2 | 2200 | 4 |  |
| 8.15 .915 | ${ }^{8}$ | 2 | － | ${ }^{\text {ass }}$ | 14 | \％ | ${ }^{\circ}$ | ， | ${ }^{\circ}$ | 3 | － | 3 | 4 | ， | ${ }^{6}$ | ${ }^{185}$ | 5 | ${ }^{18}$ | ${ }^{28}$ | 2 | ${ }^{28}$ | － | － | － | ＂ | 2 | ${ }^{3}$ | ${ }^{26}$ | s | ${ }^{25}$ | 8 | 2 | 8 | ${ }^{20}$ | － | ${ }^{20}$ | ${ }^{24}$ | 3 | ${ }^{27}$ | 190 | 3 | ${ }^{193}$ | ${ }^{4}$ | ， | 15 | ， | － | ， | 2210 | 12 |  |
| ${ }^{8.30 .930}$ | ${ }^{23}$ | 1 | ${ }_{3}$ | ${ }^{598}$ | 12 | ถ0 | ${ }^{57}$ |  | ${ }^{58}$ | ， | $\bigcirc$ |  | 48 | 1 | 4 | ${ }^{167}$ | 4 | 170 | 210 | 1 | 212 | － | － | － | ， | 2 | ， | ${ }^{238}$ | 5 | ${ }^{210}$ | \％ | 2 | － | ${ }^{17}$ | － | 17 | ${ }_{1} 8$ | 3 | ${ }^{198}$ | ${ }^{178}$ | 2 | 180 | 14 | － | ${ }^{4}$ | ＇ | － | － | 195 | ${ }^{3}$ |  |
| 8，45．945 | 25 | ， | ${ }^{25}$ | 42 | － | 50 | 40 | ， | 40 | － | $\bigcirc$ | ， | ${ }^{38}$ | 1 | ${ }^{39}$ | ${ }^{14}$ | 4 | 150 | ${ }^{176}$ | ， | 176 | － | － | － | ${ }^{3}$ | 2 | ${ }^{5}$ | ${ }^{268}$ | 4 | ${ }^{210}$ | 6 | ， | ${ }^{\circ}$ | ${ }^{14}$ | － | 14 | ${ }^{154}$ | 3 | 188 | 185 | 2 | 137 | ${ }^{12}$ | － | 12 | ， | $\bigcirc$ | ， | ${ }^{1584}$ | ${ }^{28}$ |  |
|  |  |  |  |  |  | 410 |  |  |  |  |  |  | 29 |  |  | ${ }^{123}$ |  |  |  |  |  |  |  |  | ${ }^{2}$ |  |  |  |  |  |  |  | ${ }^{6}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| Twe feroo | ${ }^{\text {Lom }}$ | maxy | Tout | Lome | maxy | Tout | Lom | mox | Toot | Lom | mavy | Toas | 4 | may | Toul | Lom | many | Toma | ${ }^{\text {Lom }}$ | many | Toal | Lom max | Tour | Lom | maxy | Toul | 4 mm | mavy | Tout | Lom | mavy | Tom | L9m | many | Tool | Lom | mavy | Tout | ${ }^{\text {Lomm }}$ | many | Toos | Lom | man | Toan | Lom max | Toun | ${ }^{\text {Lomm }}$ | max | Tome |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $14000 \cdot 1500$ | 10 | 1 | 10 | 35 | － | ${ }^{320}$ | ${ }^{28}$ | 。 | ${ }^{28}$ | 2 | － | 2 | 40 | 1 | 4 | 110 | 1 | ${ }^{11}$ | $\because$ | 2 | ${ }^{2}$ | － 0 | － | ${ }^{69}$ | 1 | \％ | ${ }^{36}$ | － | 332 | 102 | 2 | ${ }^{104}$ | ${ }^{17}$ | 。 | ${ }^{17}$ | ${ }^{123}$ | 4 | ${ }^{127}$ | ${ }^{136}$ | 1 | ${ }^{37}$ | ${ }^{14}$ | ， | ${ }^{15}$ | － 0 | 。 | ${ }_{130}$ | ${ }^{26}$ | 1408 |
| ${ }^{14.45 \cdot 5 \cdot 15: 4}$ | ． | ， | 10 | ${ }^{15}$ | － | ${ }^{32}$ | 3 | 。 | 3 | ， | － | ， | ${ }^{4}$ |  | 4 | ${ }^{113}$ | ， | ${ }^{11}$ | $\stackrel{3}{ }$ | ， | $\because$ | － 0 | － | ${ }^{2}$ |  | ${ }^{6}$ | ${ }^{370}$ |  | 376 | ${ }^{112}$ |  | 115 | 17 |  | ${ }^{17}$ | ${ }^{13}$ | 3 | ${ }^{18}$ | 188 |  | ${ }^{19}$ | ${ }^{18}$ |  | ${ }^{18}$ | ， |  | ${ }^{1503}$ | 25 |  |
| 14380 | ${ }^{20}$ | ， | ${ }^{21}$ | ${ }_{37} 8$ | － | ${ }_{3} 3$ | ${ }^{4}$ | 。 | ${ }^{48}$ | 4 | － | 4 | ${ }^{2}$ |  | ${ }^{3}$ | ${ }^{121}$ | ， | 122 | 100 | ， | ${ }^{101}$ | $\cdots$ |  | \％ |  | ${ }^{\circ}$ | ${ }_{4} 4$ |  | $4{ }^{4}$ | ${ }^{128}$ |  | ${ }^{28}$ | ${ }^{16}$ | 。 | ${ }^{16}$ | 149 | 2 | ${ }^{51}$ | ${ }_{182}$ |  | ${ }^{18}$ | 19 |  | 20 |  | ， | ${ }^{1733}$ | 27 |  |
| 19.45 ． | 25 | 3 | ${ }^{28}$ | ${ }^{45}$ | － | ${ }^{23}$ | ${ }_{56}$ | ， | ${ }^{58}$ | 4 | － | 4 | 5 |  | 57 | ${ }^{149}$ | 3 | 151 | ${ }^{12}$ | ， | ${ }^{30}$ | ，。 |  | ${ }^{12}$ |  | ${ }^{104}$ | 48 |  | s6 | ${ }^{14}$ |  | ${ }^{19}$ | ${ }^{21}$ | － | ${ }^{21}$ | 147 |  | 150 | ${ }^{193}$ |  | ${ }^{202}$ | ${ }^{2}$ |  | 23 |  |  | ${ }^{1955}$ | 4 |  |
| 15500 | ${ }^{26}$ | 3 | ${ }^{28}$ | ${ }^{49}$ | 10 | ${ }^{29}$ | ${ }^{6}$ | ， | 6 | 4 | $\bigcirc$ | 4 | ${ }^{58}$ | ， | 5 | 183 | 4 | 187 | ${ }^{139}$ | 2 | 14 | －。 | ， | ${ }^{108}$ | 2 | 110 | ${ }_{58}$ | － | ${ }_{\text {sto }}$ | ${ }^{184}$ | 3 | 157 | ${ }^{27}$ | － | ${ }^{27}$ | ${ }^{14}$ | 2 | ${ }^{18}$ | ${ }^{19}$ |  | 200 | ${ }^{2}$ | 3 | 24 | 1. |  | ${ }^{2354}$ | 4 |  |
| $15: 18.18$ | 2 | 2 | 3 | ${ }^{23}$ | 10 | ${ }^{48}$ | ${ }^{6}$ |  | ${ }^{\circ}$ | 5 |  | 5 | s | － | ss | ${ }^{189}$ |  | ${ }^{13}$ | ${ }^{139}$ | 2 | 14 | － 0 |  | ${ }^{104}$ | 2 | 106 | 53 | － | ${ }^{58}$ | 158 | 3 | 137 | 20 | 。 | ${ }^{2}$ | 12 | 2 | ${ }^{14}$ | ${ }^{190}$ | － | 18 | ${ }^{18}$ |  | ${ }^{2}$ |  | ， | ${ }^{2076}$ | ${ }^{4}$ |  |
| ${ }_{15350.1530}$ | ${ }^{20}$ | 2 | 22 | ${ }_{3} 3$ | ＂ | 4 | 4 | ， | 4 | 3 | － | 3 | 5 | － | 5 | ${ }^{17}$ | 4 | ${ }^{17}$ | ${ }^{140}$ | 2 | 112 | － | － | ${ }^{108}$ | 2 | ＂ | ${ }^{535}$ | 7 | ${ }_{512}$ | ${ }^{143}$ | 2 | 145 | ${ }^{30}$ | － | 30 | ${ }^{131}$ |  | ${ }^{13}$ | ${ }^{180}$ | 7 | ${ }^{18}$ | ${ }^{19}$ | 3 |  |  |  | ${ }^{1973}$ | ${ }^{4}$ |  |
| 15.585 .1845 | ${ }^{18}$ | － | ${ }^{18}$ | ${ }^{361}$ | ： | ${ }^{36}$ | ${ }^{3}$ | － | ${ }^{3}$ | 3 | － | 3 | 50 | － | so | ${ }^{1} 8$ | 2 | 150 | ${ }^{19}$ | 2 | ${ }^{11}$ | 1. | ， | ${ }^{105}$ | － | ${ }^{105}$ | ${ }^{53}$ | 5 | 528 | ${ }^{132}$ | ， | ${ }^{13}$ | ${ }^{26}$ | － | 25 | ${ }^{125}$ | － | ${ }^{25}$ | ${ }^{181}$ | 3 | ${ }^{184}$ | ${ }^{17}$ | 2 | ${ }^{\circ}$ | 1. | ， | ${ }^{180} 0$ | 25 |  |
| 18.80 | ${ }^{18}$ | 1 | 19 | ${ }_{3}^{35}$ | ， | ${ }^{36}$ | ${ }^{38}$ | $\bigcirc$ | 3 | 2 | － | 2 | ${ }_{5}$ | － | ${ }^{\text {ss }}$ | ${ }_{180}$ | ， | ${ }_{12}$ | ${ }^{2}$ | ， | 3 | － 0 | － | ${ }^{105}$ | － | ${ }^{105}$ | 548 | 5 | sss | ${ }^{120}$ | ， | ${ }^{31}$ | ${ }^{19}$ | － | 10 | ${ }^{124}$ | － | ${ }^{124}$ | ${ }^{185}$ | 2 | ${ }^{18}$ | ${ }^{19}$ | ， | 20 | 1. | － | ${ }_{188}$ | ${ }^{19}$ |  |
| 18.45 .11 | ${ }^{21}$ | ， | ${ }^{21}$ | 352 | － | ${ }_{38}$ | ${ }_{3}$ | － | ${ }^{3}$ | 2 | － | 2 | ${ }^{3}$ | 。 | ${ }^{6}$ | 112 | ， | 143 | ${ }^{6}$ | － | ${ }^{8}$ | 10 | ， | ${ }^{125}$ | － | ${ }^{125}$ | 578 | 4 | ${ }_{38}$ | ${ }^{13}$ | ， | ${ }^{135}$ | ${ }^{18}$ | $\bigcirc$ | ${ }^{18}$ | ${ }^{12}$ | $\bigcirc$ | ${ }^{12}$ | ${ }^{198}$ | ， | ${ }^{195}$ | ${ }^{25}$ | ， | 26 | － 0 | － | ${ }^{1887}$ | 15 |  |
| 1838.1730 | ${ }^{21}$ | 1 | 2 | 339 | 4 | ${ }_{35}$ | ${ }^{3}$ | － | ${ }^{3}$ | 1 | $\bigcirc$ | $\cdot$ | 70 | － | ${ }^{\prime}$ | 14 | 1 | ${ }^{1 / 2}$ | ${ }^{6}$ | － | ${ }^{7}$ | 1. | ， | ${ }^{126}$ | 。 | ${ }^{126}$ | 619 | 2 | ${ }^{62}$ | ${ }^{138}$ | ， | 139 | ${ }^{18}$ | $\bigcirc$ | ${ }^{18}$ | ${ }^{18}$ | 1 | ＂1 | ${ }^{189}$ | － | ${ }^{189}$ | ${ }^{30}$ | ， | 3 | － 0 | － | ${ }^{1931}$ | 12 |  |
| 18.455 .774 | ${ }^{21}$ | 1 | ${ }^{2}$ | 329 | ． | ${ }_{32}$ | ${ }^{37}$ | － | ${ }^{3}$ | ＋ | － | $\cdot$ | 72 | ＋ | ${ }^{3}$ | ${ }^{139}$ | 1 | ${ }^{10}$ | ＂ | － | ＂ | $\bigcirc$ | ， | ${ }^{129}$ | － | ${ }^{129}$ | ${ }^{631}$ | 2 | ${ }^{63}$ | ${ }^{129}$ | ＋ | ${ }^{130}$ | ${ }^{17}$ | － | 17 | 15 | ， | ${ }^{16}$ | ${ }^{178}$ | － | 178 | 3 |  | 32 | － 0 | 。 | ${ }_{1087}$ | 10 |  |
| 17200，1850 | ${ }^{18}$ | － | ${ }^{18}$ | ${ }^{39}$ | ， | ${ }^{31}$ | ${ }^{37}$ | － | ${ }^{3}$ | ， | － | $\cdot$ | ${ }^{\infty}$ |  | ${ }^{5}$ | ${ }^{13}$ | 1 | ${ }^{138}$ | ${ }^{3}$ | $\bigcirc$ | ${ }^{74}$ | $\bigcirc$ | ， | ${ }^{126}$ | － | ${ }^{126}$ | 59 | 2 | 60 | ${ }^{124}$ |  | ${ }^{124}$ | ${ }^{18}$ | $\bigcirc$ | ${ }^{16}$ | ${ }^{105}$ |  | ${ }^{106}$ | 188 | － | 14 | ${ }^{28}$ |  | 20 | － 0 | － | ${ }_{7} 786$ | 10 |  |
| 1725：1818．5 | 13 | － | ${ }^{13}$ | ${ }^{27}$ | 2 | 29 | ${ }^{36}$ | － | ${ }^{6}$ | ， | － | ， | ${ }_{53}$ |  | ${ }^{4}$ | ${ }^{120}$ | ， | ${ }^{120}$ | ${ }^{8}$ | － | ${ }^{\circ}$ | $\bigcirc$ | － | ${ }^{104}$ | 。 | ${ }^{104}$ | ${ }^{53}$ | 3 | ${ }_{26}$ | ${ }^{104}$ |  | 104 | 15 | － | 15 | 9 |  | ${ }^{100}$ | ${ }^{126}$ | － | ${ }^{127}$ | ${ }^{23}$ | － | ${ }^{23}$ | － | 。 | ${ }_{1} 158$ | － |  |
| 1730．1830 | 10 | － | 10 | 273 | ， | 275 | ${ }^{6}$ | － | ${ }^{6}$ | 2 | － | 2 | 4 | ， | 4 | $\cdots$ | $\bigcirc$ | $\because$ | ${ }_{5}$ | － | ${ }_{\text {ss }}$ | － 0 | － | ${ }^{87}$ | － | ${ }^{8}$ | 48 | 3 | 48 | ${ }^{8}$ | － | ${ }^{8}$ | ＂ | － | ＂ | ${ }^{87}$ | － | ${ }^{8}$ | ${ }^{109}$ | － | ${ }^{108}$ | 15 | － | 15 | － | － | ${ }^{1357}$ | 7 |  |
| 77．45，1845 | 7 | － | 7 | 232 | 2 | 25 | 32 | － | 32 | 2 | － | 2 | ${ }^{36}$ | $\bigcirc$ | 37 | ${ }_{8}$ | － | ${ }^{8}$ | 50 | 1 | ${ }_{50}$ | $\cdots$ | － | ${ }^{3}$ | － | 73 | ${ }_{382}$ | 3 | ${ }^{36}$ | ＂ | － | ＂ | 8 | － | － | ${ }_{78}$ | － | ${ }^{8}$ | $\because$ | － | $\because$ | $\because$ | － | ＂ | － | － | ${ }^{1771}$ | － |  |
| 13800 12300 |  |  | － |  |  | ${ }^{23}$ |  |  | 29 |  | － |  | ${ }^{32}$ | － | 32 | ${ }^{7}$ | $\bigcirc$ | ${ }^{6}$ |  | － | 4 | － | － | ${ }^{65}$ | － | ${ }^{65}$ | ${ }^{30}$ | ， | 302 | ${ }^{6}$ | $\bigcirc$ | ${ }^{\circ}$ |  | － | － | ${ }_{74}$ | $\bigcirc$ | ${ }^{4}$ |  |  |  | 10 |  |  |  |  | ${ }^{1021}$ |  |  |







austraffic
…


| Twe eraoo |  | themen | Toan |  |  | Toent | ${ }_{\text {Lomo }}$ |  | Ton | ${ }^{\text {and }}$ | Toen | Hoem | Seme | Tem | Hovemen en |  |  |  | Tom |  | ${ }^{18}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 500．600 |  |  |  | ${ }^{14}$ |  | ${ }^{2}$ |  |  |  | ${ }_{37}^{37}$ | ${ }^{4}$ | 50 |  | ${ }_{5}$ | $\bigcirc$ |  | ${ }^{23}$ |  | ${ }^{25}$ | 4 |  |  |  |  | ${ }^{129}$ |  | ${ }^{153}$ |
| 5．15．6．45 | ． |  | ， | ${ }^{18}$ |  | 3 |  |  |  | 46 |  | ${ }_{6}$ |  | \％ | 。 |  | ${ }^{27}$ |  | ${ }^{29}$ | ． |  |  |  |  | 159 |  | ${ }^{18}$ |
| ${ }_{5350.630}$ |  |  |  |  |  | 3 |  |  |  |  | ${ }_{72}^{51}$ | ${ }^{6}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5．45，64， | ， |  |  | ${ }_{3}^{23}$ | ${ }_{21}$ | ${ }_{5 s}$ |  |  |  | ${ }^{8}$ | ${ }^{12}$ | ${ }_{97}$ |  | ${ }^{103}$ | 2 |  | S |  | \％ | ． |  |  |  |  | ${ }^{200}$ |  | ${ }^{23}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | ， |
| 600．780 | 2 |  | 2 | ${ }^{5}$ | ${ }^{2}$ | ${ }^{75}$ |  |  |  | ${ }^{125}$ | ${ }^{13}$ | ${ }^{122}$ |  | ${ }^{198}$ | s |  | 5 |  | ＊ | ＂ | ${ }^{2}$ |  |  |  | ${ }^{39}$ | 12 | ${ }^{46}$ |
| 6．15，7175 | 2 |  | 3 | 12 | ${ }_{24}$ | ${ }^{\circ}$ | 。 |  |  | 158 | ${ }^{4}$ | ${ }^{163}$ |  | ${ }^{12}$ | 2 |  | ${ }^{8}$ |  | 9 | ${ }^{14}$ | ${ }^{14}$ |  |  |  | 480 | 52 | s2 |
| 6，30．730 | － |  | 5 | ${ }^{7}$ | ${ }^{24}$ | 102 | 。 |  |  | ${ }^{17} \quad 11$ | ${ }^{18}$ | ${ }^{198}$ |  | ${ }^{208}$ | ＝ |  | ${ }^{103}$ |  | ＂＇ | ${ }^{13}$ | ${ }^{14}$ |  |  |  | ${ }^{57}$ | ${ }_{5}$ | so |
| 6．45．74， | 5 |  |  | 180 | ${ }^{29}$ | ${ }^{12}$ | 。 |  |  | 174 | ${ }^{15}$ | ${ }^{26}$ | 10 | ${ }^{256}$ | ＝ |  | ${ }^{125}$ |  | ${ }^{13}$ | ＂ | 12 | 。 |  |  | ${ }_{68} 6$ | ${ }^{6}$ | ${ }^{75}$ |
| 7：00，8， 80 | ， |  | 10 | 109 | ${ }_{3}$ | ${ }^{14}$ | 。 |  |  | 178 | ${ }^{19}$ | ${ }^{291}$ |  | 22 | 2 |  | 159 |  | ${ }^{6}$ | 10 | ＂ | ， |  |  | ${ }^{30}$ | ＂ | ${ }^{82}$ |
| 2，15．8．15 | ， |  | ＂ | ＂＇1 | 32 | ${ }^{14}$ |  |  |  | ${ }^{183}$ | ${ }^{188}$ | ${ }^{43}$ | ＂ | 4 | ${ }^{3}$ |  | ${ }_{185}$ |  | ${ }^{13}$ | ＂ | 12 | ， |  |  | ${ }^{206}$ | ${ }^{6}$ | ${ }^{975}$ |
| 7：30， 3.30 | ＂ |  | 12 | ${ }^{30}$ | ${ }_{32}$ | 162 |  |  |  | ${ }^{222}$ | ${ }^{22}$ | ${ }^{565}$ | ＂ | 59 | 3 |  | 22 |  | 22 | ＂ | ${ }^{13}$ | ＇ |  |  | 1.175 | 75 | ，2， |
| 7．45， 8.45 | ， |  | ＂ | ${ }^{123}$ | ${ }^{3}$ | ${ }_{154}$ |  |  |  | ${ }^{222} \quad 28$ | 230 | ${ }^{78}$ | ${ }^{3}$ | 76 | 3 |  | ${ }^{29}$ |  | 30 | ${ }^{13} 2$ | ${ }^{15}$ | － |  |  | 1.410 | ${ }^{4}$ | 1.48 |
| 800．980 | 7 |  |  | ${ }^{125}$ | ${ }^{26}$ | 132 |  |  |  | 236 | ${ }^{26}$ | ${ }^{881}$ |  | ${ }^{82}$ | 2 |  | ${ }^{38}$ |  | ${ }^{3}$ | ${ }^{4}$ | ＂ |  |  |  | 1.802 | ${ }^{4}$ | 1.188 |
| 881．9．95 | － |  | ${ }^{12}$ | ${ }^{126}$ | 29 | 145 | 。 |  |  | ${ }^{28} \quad 38$ | ${ }^{261}$ | ${ }^{\text {a，8 }}$ |  | ${ }^{55}$ | 2 |  | 350 |  | ${ }^{35}$ | 14. | ＂ | 。 |  |  | 1.59 | ${ }^{89}$ | 1.68 |
| 830．930 | － |  | ${ }^{10}$ | ${ }^{120}$ |  | 132 | 。 |  |  | 20135 | ${ }^{25}$ | ${ }^{713}$ |  | ${ }^{73}$ | ＝ |  | ${ }^{36}$ |  | ${ }^{28}$ | ${ }^{15}$ | ${ }^{18}$ | ， |  |  | 1335 | ${ }^{9}$ | ，1，980 |
| 845． 24.4 | ${ }^{10}$ |  | ${ }^{13}$ | 114 | ${ }^{3}$ | ${ }^{17}$ | 。 |  |  | ${ }^{173} \quad 34$ | ${ }^{207}$ | s6 |  | ${ }^{54}$ | 2 |  | ${ }^{25}$ |  | ${ }^{30}$ | ${ }^{15}{ }^{3}$ | ${ }^{18}$ | ＇ |  |  | ${ }^{1,77}$ | 4 | 12.20 |
| 200， 10.00 |  |  |  | ${ }_{102}$ |  | ${ }^{18}$ | 。 |  |  | 4，3 ${ }^{34}$ |  | ${ }^{43}$ |  | ${ }^{42}$ |  |  |  |  | ${ }_{26} 6$ | $12 \quad 2$ |  |  |  |  | \％ |  | ${ }_{2} .105$ |


| Tue ereao | ${ }^{\text {comememem }}$ | Toen | ， | movenem | Tout | ${ }_{\text {Nomemem }}$ | ${ }_{\text {Tomi }}$ | ${ }_{\text {den }}$ | Tomb | ${ }^{\text {Lemm }}$ | ， | Toast | ${ }^{\text {Nomomemema }}$ | ＋ | ${ }^{\text {w }}$ |  | Tom |  |  | Ioal |  |  | Toen |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 14000.1500 | 12. | ${ }_{1}$ | ${ }^{147}$ | ${ }^{25}$ | ${ }^{17}$ | 。 |  | ${ }^{114}$ | ${ }^{4} 5$ | ${ }_{36}^{386}$ |  | ${ }^{39}$ | ＝ | 2 | 480 |  | 49 | ${ }^{16}$ | ${ }^{4} \cdot$ | ＂ |  |  | 3 | ${ }_{1}^{1,58}$ | ${ }^{8}$ | ， |
| 1414.5 ，19，15 | ${ }^{19}$ | ＂ | ${ }^{153}$ | ${ }^{26}$ | 189 | 。 | 。 | ${ }_{18}{ }^{33}$ | 151 | ${ }_{36}^{36}$ |  | ${ }_{39} 9$ | 2 |  | ${ }^{575}$ |  | ${ }_{54}$ |  |  | ${ }^{16}$ |  |  | 2 | 1273 | ${ }_{8}$ | ${ }_{1,389}$ |
| 14350.1530 | 15 | ＂ | ${ }^{179}$ | ${ }^{25}$ | ${ }^{205}$ | － | 。 | 1238 | ${ }_{4}{ }^{\text {a }}$ | ${ }^{36}$ |  | ${ }^{39}$ | 2 | 2 | ${ }^{63}$ |  | ${ }^{6}$ | ${ }^{13}$ |  | ${ }^{\circ}$ |  |  | ， | 1,380 | ${ }^{3}$ | ${ }_{1,43}$ |
| 124.45 .14 .45 | ${ }^{17}$ | ${ }^{19}$ | ${ }^{206}$ | ${ }^{66}{ }^{28}$ | ${ }^{23}$ | ， |  | ${ }^{129}$ | ${ }^{15}$ | ${ }^{39}$ |  | ${ }^{088}$ | 2 |  | ${ }^{65}$ |  | ${ }^{8}$ |  |  | ${ }^{*}$ |  |  |  | 1,43 | ${ }^{5}$ | ${ }_{1.58}$ |
| 1550，1600 | 17 | 19 | ${ }^{211}$ | ${ }^{25}$ | ${ }^{25}$ | ， |  | ${ }^{135} 83$ | ${ }^{6}$ | ${ }^{41}$ |  | 416 | 。 |  | 7 |  | ${ }^{24}$ | ${ }^{13}$ |  | ${ }^{*}$ | 2 |  |  | ${ }_{1589}$ | 80 | ${ }_{\text {4，533 }}$ |
|  | ${ }^{17}$ | ${ }^{18}$ | ${ }^{211}$ | $1{ }^{21}$ | ${ }^{23}$ | ， |  | ${ }^{14}$ | ＂ | ${ }_{4} 4$ |  | 43 | － | 。 | ${ }^{\text {® }}$ |  | ${ }^{687}$ | ${ }^{13}$ |  | ${ }^{15}$ | ${ }^{3}$ |  |  | ${ }_{1,513}$ | 7 | ${ }_{1,58}$ |
| 1330．1430 | ${ }^{16}$ | ${ }^{18}$ | ${ }^{215}$ | ${ }^{515}$ | ${ }^{27}$ | ， |  | ${ }^{151}{ }^{33}$ | ${ }^{18}$ | ${ }^{46}$ |  | ${ }^{43}$ | － |  | в6 |  | ${ }^{65}$ | ${ }^{15}$ |  | ${ }^{16}$ | 2 |  |  | 1.594 | ${ }^{3}$ | ${ }_{1,687}$ |
|  | ${ }^{15}$ | ${ }^{15}$ | ${ }^{218}$ | ${ }^{18} 8$ | ${ }^{28}$ | ， |  | ${ }^{19}$ | ${ }^{181}$ | 45 |  | $4{ }^{64}$ | 10 | 10 | ${ }^{708}$ |  | ${ }^{75}$ | ${ }^{5}$ |  | ${ }^{15}$ | ${ }^{3}$ |  |  | 1.975 | ${ }_{6} 6$ | ${ }^{164}$ |
| 1850．17，00 | ${ }^{16}$ | ${ }^{16}$ | ${ }^{24}$ | ${ }^{4} 4$ | 22 | ， |  | ${ }^{157}$ | ${ }^{18}$ | 45 |  | 48 | － | － | ${ }^{73}$ |  | ${ }^{76}$ | ${ }^{16}$ |  | ${ }^{15}$ | 2 |  |  | 1.510 | ${ }^{1}$ | 1.60 |
| 16：15－77：75 | ${ }^{16}$ | ${ }^{16}$ | ${ }^{238}$ | ${ }^{28} 17$ | ${ }^{265}$ | － |  | 159 | ${ }^{18}$ | 49 |  | 45 | － | 。 | 789 |  | ${ }^{73}$ | ＂ |  | 12 | 2 |  |  | 1.880 | $s$ | 1，73 |
| 18380.1730 | 17 | $\square$ | ${ }_{200}$ | $0{ }^{15}$ | ${ }^{275}$ |  |  | ${ }^{148}$ | ＂1 | ${ }^{21}$ |  | ${ }^{24}$ | 。 |  | 81 |  | ${ }^{84}$ |  | 。 | ${ }^{\circ}$ |  |  |  | 1,78 | ${ }_{4}$ | ．77 |
| 16，45－7745 | ${ }^{17}$ | ＂ | ${ }^{26}$ | ${ }^{13}$ | ${ }^{29}$ |  |  | 1418 | ${ }_{182}$ | ${ }^{49}$ |  | ${ }^{43}$ | 。 |  | ${ }_{87}$ |  | \％00 |  | 。 | 10 |  |  |  | ${ }_{127}$ | ${ }^{4}$ | ${ }^{1,768}$ |
| 1780，18800 | ${ }^{15}$ | ${ }^{15}$ | ${ }^{227}$ | 27 | ${ }^{29}$ |  |  | ${ }^{125}$ | ${ }^{14}$ | ${ }^{33}$ |  | ${ }_{37}^{37}$ | ， | ， | ${ }_{87}$ |  | ${ }^{87}$ |  | 。 | 10 |  |  |  | 1,46 | ${ }^{38}$ | 1．681 |
| 77：15，12：45 | ${ }^{13}$ | ${ }^{13}$ | ${ }^{180}$ | \％ | ${ }^{22}$ |  |  | ${ }^{103}$ | ${ }^{19}$ | ${ }^{37}$ |  | ${ }_{30}$ | ${ }^{4}$ |  | ${ }^{74}$ |  | m |  | 。 | 10 | ， |  |  | 1.44 | ${ }^{35}$ | ${ }_{1} / 4.76$ |
| 1730．1830 | ＂ | ＂ | 155 | ${ }^{15}$ | ${ }^{19}$ |  |  |  | ${ }^{105}$ | ${ }^{32}$ |  | 33 | 2 | ＝ | ${ }_{6} 5$ |  | ${ }^{69}$ |  |  | ． | ， |  |  | ${ }_{122}$ | ${ }^{35}$ | ${ }_{12,26}$ |
| 172，5－1845 | ${ }^{10}$ | ${ }^{10}$ | ${ }^{123}$ | ${ }^{2}$ | ${ }^{13}$ |  |  |  | \％ | ${ }^{266}$ |  | ${ }^{25}$ | 2 | 2 | 521 |  | ${ }^{54}$ |  | ，。 | ， | ， |  | ， | ${ }_{1}^{1,207}$ | ${ }^{30}$ | ${ }_{1}^{1.087}$ |
| 1880.1800 | ${ }^{8} \cdot$ | $\cdot$ | ${ }^{10}$ | 12 | ${ }^{13}$ |  |  | ${ }^{6}$ 10 | $\stackrel{7}{1}$ | ${ }^{231}$ |  | ${ }^{23}$ | ， | 1 | ${ }^{437}$ |  | 43 |  | s | 5 | ， |  | $\cdot$ | ${ }^{\text {a／}}$ | ${ }^{27}$ | ${ }^{83}$ |




| Tue ereao | 4 Lom | max | Tool | ${ }^{\text {Lomo }}$ | neay | Toon | ${ }^{\text {Lomo }}$ | many | Toot | Lomt nama | Tool | Lomt | Tout | Loyt max | Tout | Lomt naver | Tout | $L^{\text {Lem }}$ Hemax | Tout | Lomm nemar | Tout | Lomm | tomy | Toout | Lomm | Toat | ${ }^{\text {Lomm }}$ | maxy | Tout | Lomm | namy | Tout | Lomm | maxy | Toon | ${ }^{\text {Lomm }}$ | mave | Tout | Lbom | maxy | Tout | Lsm | $\xrightarrow{\text { and }}$ | Tout |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5．00．600 | 1 |  |  | ${ }^{38}$ |  | ${ }^{4}$ |  |  |  |  |  | $\bigcirc$ |  | － | － | 2 | ${ }^{2}$ |  |  | ${ }^{3}$ | ， | ${ }^{27}$ |  | ${ }^{29}$ | － 1 | ${ }^{10}$ |  |  |  | ＂ |  | 12 | 2 |  | 2 | ， |  |  |  |  |  | ${ }^{9}$ |  |  |
| 5．15，6，45 | － |  |  | ${ }^{4}$ |  | ＂ | 。 |  | 。 |  |  | 1 |  | －。 | ， | 20 | 2 |  |  | － | － | ${ }^{33}$ |  | ${ }^{35}$ | ${ }^{19} 2$ | ${ }^{21}$ | ， |  |  | 18 |  | 15 | ， |  |  | ， |  |  |  |  |  | ${ }^{120}$ |  |  |
| 53．30．630 | $\square$ |  |  | ${ }^{4}$ |  | ${ }^{4}$ | － |  | － |  |  | 1 |  | － |  | 3 。 | 3 | － | 。 | － | 。 | ${ }^{4}$ |  | ${ }^{4}$ | ${ }^{27} 2$ | ${ }^{30}$ | ＇ |  |  | ${ }^{13}$ |  | ${ }^{15}$ | ， |  |  | ， |  | ， |  |  |  | ${ }^{145}$ | 13 |  |
| 5445．44 | － |  |  | 5 |  | ${ }_{5}$ | 。 |  | ， |  |  | 1 |  | 1. |  | 4 | s | 。 | － | 5 | s | ${ }^{46}$ |  | ${ }^{4}$ | ${ }^{39}=$ | ${ }^{\prime}$ | ， |  |  | 14 |  | ${ }^{15}$ | ， |  |  | ， |  | ， |  |  |  | ${ }^{17}$ | 15 |  |
| 600．7．700 | ${ }^{13}$ |  | ${ }^{13}$ | $\square$ |  | ${ }^{3}$ | ， |  |  |  |  | 1. |  | 20 |  | 4 ＇ |  | － |  | － |  | ${ }^{\circ}$ |  | ${ }^{65}$ | ${ }^{6}$－ | ${ }^{65}$ | ， |  |  | ${ }^{16}$ |  | ${ }^{18}$ | ， |  |  | 3 |  |  |  |  |  | ${ }^{25}$ | ${ }^{20}$ |  |
| 6．15，715 | ${ }^{16}$ |  | ${ }^{16}$ | ${ }^{79}$ |  | ${ }^{8}$ | ， |  | ， |  |  | $\cdots$ |  | 2 |  | 4 － |  | － |  | 5 |  | ${ }^{75}$ |  | ${ }^{79}$ | ${ }^{64}{ }^{3}$ | ${ }^{\circ}$ |  |  |  | ${ }^{18}$ |  | ${ }^{22}$ | 3 |  |  | 4 |  |  |  |  |  | ${ }^{27}$ | ${ }^{21}$ |  |
| 830．7．730 | ${ }^{21}$ |  | ${ }^{23}$ | ${ }^{86}$ |  | $\because$ | ， | － | ， |  |  | 1. |  | 2 |  | 4. | － | ． |  | － |  | ${ }^{3}$ |  | ${ }^{85}$ | ${ }^{6}$ ． | ＂ | 。 |  |  | 2 |  | ${ }^{24}$ | 3 |  |  | ， |  |  |  |  |  | ${ }^{27}$ | ${ }_{24}$ |  |
| 6．45－74． | ${ }^{3}$ |  | ${ }^{3}$ | 12 | 10 | ＂＇ | ， |  | ＋ |  |  | － | － | 3 | 3 | 3 | ${ }^{3}$ | ． |  | 7 | 7 | $\because$ |  | ${ }^{6}$ | $\infty$－ | ${ }^{\text {as }}$ | 。 |  |  | ${ }^{26}$ |  | ${ }^{20}$ | ${ }^{4}$ |  |  | ＂ |  | ${ }^{12}$ |  |  |  | ${ }^{359}$ | ${ }^{27}$ |  |
| ${ }^{2} 8.00 .800$ | ${ }^{2}$ |  | ＂ | ${ }^{17}$ | 10 | ${ }^{127}$ | ， |  | ＇ |  |  | － | － | 4 | － | － | － | － | － | 8 |  | ${ }^{105}$ |  | ${ }^{10}$ | ${ }^{55} 5$ | ${ }^{100}$ | ， |  |  | ${ }^{36}$ |  | ${ }^{3}$ | 5 |  |  | ${ }^{14}$ |  | ${ }^{15}$ |  |  |  | ${ }^{43}$ | ${ }^{26}$ |  |
| 2715．8．45 | ${ }^{6}$ |  | ${ }^{6}$ | 153 |  | ${ }^{165}$ | ， |  | ＋ | ． |  | $\bigcirc$ | － | 5 | 5 | － 0 | － | － | － | － | 10 | 109 |  | ${ }^{116}$ | ${ }^{25}$ | ${ }_{132}$ | ， |  |  | ${ }^{4}$ |  | ${ }^{2}$ | ${ }^{4}$ |  |  | ${ }^{20}$ |  |  |  |  |  | ${ }_{56} 6$ | 3 |  |
| 7，30．830 | ${ }^{\circ}$ |  | $\cdots$ | 219 |  | ${ }^{23}$ | ， |  | ， |  |  | 1 |  | ， |  | ＂ | 12 | － |  | ${ }^{12}$ | 12 | ${ }^{155}$ |  | 14 | ${ }_{182}$ | ${ }^{188}$ | ， |  |  | ${ }^{58}$ |  | ${ }^{2}$ | 5 |  |  | ${ }^{24}$ |  |  |  |  |  | ${ }^{75}$ | ${ }^{32}$ |  |
| $7^{2}$ ，4， 8.84 | ${ }^{127}$ |  | ${ }^{128}$ | 232 |  | ${ }^{23}$ | 2 |  | 2 |  |  | 3 |  | 10 | 10 | 14 | ${ }^{15}$ | ， |  | ${ }^{15}$ | ${ }^{16}$ | ${ }^{18} 8$ |  | ${ }^{188}$ | ${ }^{216}$ | ${ }^{23}$ | ＝ |  |  | ${ }^{7}$ |  | 8 | 7 |  |  | ${ }^{4}$ |  | ${ }^{4}$ |  |  |  | ${ }^{93}$ | ${ }_{38}$ |  |
| 800．900 | ${ }^{50}$ |  | 15 | ${ }^{37}$ | ， | ${ }_{35}$ | 2 |  | $=$ |  |  | 3 |  | 10 | ＂ | ${ }^{18}$ | ${ }^{19}$ | － |  | ${ }^{20}$ | ${ }^{21}$ | ${ }_{182}$ |  | ${ }^{13}$ | 232 | ${ }^{23}$ | ， |  |  | $\because$ |  | 19 | 10 |  |  | ${ }^{4}$ |  | ${ }^{4}$ |  |  |  | 1.100 | ${ }_{5}$ |  |
| 8， 8.9 .94 | ${ }^{15}$ |  | 184 | ${ }^{388}$ |  | 37 | ＝ |  | 3 |  |  | 5 |  | ＂ | ${ }^{12}$ | 18 | ${ }^{19}$ | － |  | ${ }^{21}$ | 2 | 200 |  | 22 | ${ }^{28}$ | ${ }^{27}$ | ， |  |  | $\because$ |  | 19 | 12 |  | ${ }^{13}$ | ${ }^{45}$ |  | ${ }^{48}$ |  |  |  | 1.159 | 52 | ${ }^{121}$ |
| 330．930 | ${ }^{127}$ |  | 130 | ${ }^{30}$ | 0 | ${ }_{36}$ | ＊ |  | ${ }^{4}$ |  |  | 5 |  | 12 | 13 | 9 | ${ }^{20}$ | － | － | ${ }^{18}$ | ${ }^{20}$ | ${ }^{20}$ |  | 220 | 216 | ${ }^{28}$ | ， |  |  | ${ }^{113}$ |  | 12 | ${ }^{13}$ |  | ${ }^{4}$ | ${ }^{46}$ |  | 4 |  |  |  | 1，06 | ${ }^{55}$ | 1，55 |
| 8045．945 | ${ }^{103}$ |  | ${ }^{106}$ | 24 | 4 | ${ }^{31}$ | 3 |  | 3 | $\bigcirc$ |  | 3 |  | 10 | ${ }^{10}$ | ${ }^{20}$ | ${ }^{20}$ |  |  | ${ }^{17}$ | ${ }^{18}$ | ${ }_{17}$ |  | ${ }^{28}$ | ${ }^{198}$ | ${ }^{28}$ | ， |  |  | ${ }^{118}$ |  | ${ }^{126}$ | 12 |  | ${ }^{13}$ | ${ }^{35}$ |  | ${ }^{38}$ |  |  |  | 1.012 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  | ＂ |  |  |  |  |  |  |  |  |  |  | ${ }_{182} 6$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | ${ }^{29}$ |  |  |






austraffic



| tweremao | ${ }^{\text {Lomm }}$ | Heme | Toom | ${ }^{\text {Lomo }}$ | nomy | Toun | ${ }^{\text {Lomm }}$ | maxy | Toen |  | thay | Toob | ${ }^{\text {Lbom }}$ | neay | Toom | ${ }_{\text {Lomo }}$ | namy | Toom | Lom | max | Toen | ${ }^{\text {Lbomo }}$ | many | Toob | Lomo | namy | Toat | ${ }^{\text {Lemem }}$ | Hemy | Toas |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5.000 .600 | ${ }^{31}$ |  | ${ }^{2}$ | ， |  |  |  |  |  | － |  |  | ${ }^{13}$ |  | ${ }^{\circ}$ |  |  |  | － |  | 。 | ${ }^{22}$ |  | ${ }^{23}$ | 2 |  |  | $\%$ |  | ＊ |
| 5．15．6．15 | 4 |  | ${ }^{\prime}$ | 10 |  | 10 | 。 |  | 。 | ${ }^{10}$ |  | ${ }^{10}$ | ${ }^{21}$ |  | ${ }^{2}$ |  |  |  | ＂ |  | ＂ | ${ }^{20}$ |  | ${ }^{20}$ | － |  |  | ${ }^{17}$ |  | ${ }^{120}$ |
| 5.50 .650 | 4 |  | 50 | ${ }^{12}$ |  | ${ }^{13}$ | 。 |  | 。 | ${ }^{13}$ |  | ${ }^{13}$ | ${ }^{23}$ |  | ${ }^{25}$ |  |  |  | ${ }^{16}$ |  | $\square$ | ${ }^{24}$ |  | ${ }^{25}$ | － |  |  | ${ }_{12}$ |  | ${ }^{169}$ |
| 5.45 .645 | ${ }_{55}$ |  | ${ }^{5}$ | ${ }^{15}$ |  | ${ }^{16}$ | 。 |  |  | 15 |  | ${ }^{4}$ | ${ }^{25}$ |  | ${ }^{27}$ |  |  |  | ${ }^{19}$ |  | ${ }^{20}$ | ${ }^{3}$ |  | ${ }^{32}$ | ， |  |  | ${ }^{167}$ |  | ${ }^{75}$ |
| 8000．730 | ${ }_{52}$ |  | ${ }^{5}$ | 16 |  | ＂ | 。 |  | － | ${ }^{21}$ |  | ${ }^{2}$ | ${ }^{30}$ |  | ${ }^{3}$ |  |  |  | 2 |  | ${ }^{23}$ | ${ }^{3}$ |  | ${ }^{39}$ | ， |  |  | ${ }^{189}$ |  | ${ }^{18}$ |
| 6，15，715 | ${ }_{50}$ |  | ${ }_{5}$ | ${ }^{7}$ |  | ${ }^{18}$ | － |  |  | ${ }^{26}$ |  | ${ }^{26}$ | ${ }^{3}$ |  | ${ }^{39}$ |  |  |  | ${ }^{3}$ |  | ${ }^{33}$ | ${ }^{48}$ |  | ${ }^{50}$ | ， |  |  | ${ }^{213}$ |  | ${ }^{27}$ |
| 6，30．730 | ${ }_{54}$ |  | $s$ | 2 |  | ${ }^{23}$ |  |  |  | ${ }^{32}$ |  | ${ }^{35}$ | ${ }^{39}$ |  | ${ }^{4}$ |  |  |  | ${ }^{3}$ |  | ${ }^{3}$ | ${ }^{53}$ |  | $s$ | 8 |  |  | ${ }^{23}$ |  | ${ }^{25}$ |
| 8445．745 | ${ }^{55}$ |  | ${ }^{5}$ | ${ }^{2}$ |  | ${ }^{27}$ |  |  |  | ${ }^{34}$ |  | ${ }^{3}$ | ${ }^{4}$ |  | 5 | 。 |  |  | ${ }^{37}$ |  | ${ }^{3}$ | ${ }^{6}$ |  | ${ }^{65}$ | 8 |  |  | ${ }^{287}$ | ${ }^{11}$ | ${ }^{288}$ |
| 7：00．8．00 | ${ }^{70}$ |  | ${ }^{75}$ | ${ }^{26}$ |  | 3 |  |  |  | ${ }^{3}$ |  | ${ }^{36}$ | ${ }_{50}$ |  | ${ }^{5}$ | ， |  |  | ${ }^{39}$ |  | ＂ | ${ }^{6}$ |  | ${ }^{6}$ | － |  |  | ${ }^{255}$ | ${ }^{26}$ | ${ }^{30}$ |
| 2：15．8．15 | ＂ |  | ${ }^{85}$ | ${ }^{30}$ |  | ${ }^{3}$ |  | 。 | － | ${ }^{36}$ |  | ${ }^{\circ}$ | 5 |  | ${ }^{\text {s }}$ | ， |  |  | ${ }^{12}$ |  | ${ }^{*}$ | ${ }^{6}$ |  | ${ }^{65}$ | － |  |  | ${ }^{303}$ | ${ }^{26}$ | ${ }_{330}$ |
| 7300．830 | ${ }^{85}$ |  | $\because$ | ${ }^{3}$ |  | 4 | 。 | 。 |  | ${ }^{3}$ |  | ${ }^{36}$ | ${ }^{\text {s8 }}$ |  | ${ }^{6}$ | ， |  |  | ${ }_{5}$ |  | s | ${ }^{6}$ |  | ${ }^{6}$ | $\bigcirc$ |  |  | ${ }_{3}^{32}$ | ${ }^{27}$ | ${ }^{35}$ |
| Ti45， 8.45 | ${ }^{88}$ |  | \％ | ${ }^{5}$ |  | ${ }^{\text {s5 }}$ | 。 | 。 |  | ${ }^{52}$ |  | ${ }^{55}$ | ${ }^{65}$ |  | ${ }^{\circ}$ | ， |  |  | ${ }^{6}$ |  | ${ }^{2}$ | ${ }^{6}$ |  | ${ }^{\circ}$ | － |  |  | ${ }^{39}$ | ${ }^{24}$ | ${ }_{48}$ |
| 8．00，980 | ${ }^{9}$ |  | $\%$ | ＊ |  | ${ }^{6}$ | － |  | － | ${ }^{6}$ |  | $"$ | 70 |  | ${ }^{7}$ | ， |  |  | ${ }^{6}$ |  | ${ }^{8}$ | ${ }^{7}$ |  | ${ }^{7}$ | － |  |  | ${ }^{42}$ | ${ }^{27}$ | ${ }^{48}$ |
| 845．9．15 | ${ }^{8}$ |  | ${ }^{102}$ | ＊ |  | ${ }^{\circ}$ | ， |  |  | ${ }^{70}$ |  | ${ }^{74}$ | ＂ |  | ${ }^{8}$ | ， |  |  | $\cdots$ |  | $\stackrel{3}{ }$ | ${ }^{7}$ |  | ${ }^{80}$ | － |  |  | ${ }^{485}$ | ${ }^{26}$ | ${ }^{50}$ |
| 830．930 | \％ |  | 101 | $\infty$ |  | ${ }^{6}$ | ， |  |  | ${ }^{73}$ |  | ＂ | ${ }^{7}$ |  | ＊ | ， |  |  | ＊ |  | － | ${ }^{8}$ |  | ${ }^{\circ}$ | ＂ |  | ＂ | 48 | 2 | ${ }^{515}$ |
| 8，45，945 | ${ }^{4}$ |  | $\stackrel{ }{ }$ | ${ }^{45}$ |  | ${ }^{5}$ | ， |  |  | ${ }^{56}$ |  | ${ }^{\circ}$ | ＂ |  | ${ }^{7}$ | － |  |  | ${ }^{8}$ |  | ${ }^{8}$ | ${ }^{7}$ |  | ${ }_{80}$ | 12 |  | ${ }^{12}$ | ${ }^{48}$ | ${ }^{2}$ | ${ }^{42}$ |
| 2000．10：00 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | ${ }^{42}$ |  | ${ }_{42}$ |


| тwe ereoo | Lom | maxy | Toon | 4 | max | Toat | Lom | maxy | Tout | Lom | mavy | Toat | ${ }^{\text {Lomm }}$ | many | Toat | ${ }^{\text {Lomm }}$ | many | Toon | 4 mm |  | Toat | Lom | mam | Toum |  | Lom | many | Toou | ${ }^{\text {Lsmm}}$ | maxy | Toat |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $14.80 \cdot 1500$ | ${ }^{2}$ |  | $\because$ | ${ }^{2}$ | 1 | 4 | 2 | ＝ |  | ${ }^{48}$ |  | 4 | \％ |  | $\because$ | ， |  |  | ${ }^{108}$ |  | ${ }^{12}$ | ${ }^{10}$ | ， |  | ${ }^{104}$ | ＂ |  | ＂ | ${ }^{194}$ | ${ }^{13}$ | ${ }^{507}$ |
| 14．15，［1：15 | $\cdots$ |  | $\because$ | ¢ | 9 | 5 | ， | ， |  | 5 |  | \％ | ${ }^{2}$ |  | \％ | ， |  |  | ${ }^{113}$ |  | ${ }^{17}$ |  |  |  | 102 | ${ }^{12}$ |  | ${ }^{13}$ | 599 | ＂ | ${ }^{86}$ |
| 1430．1530 | ${ }^{9}$ |  | ${ }^{8}$ | \％ | 3 | ${ }_{6}$ | ， | ， |  | ${ }^{68}$ |  | ${ }_{7}$ | ${ }^{103}$ |  | ${ }^{106}$ | ， |  |  | ${ }^{19}$ |  | ${ }_{12}$ |  | 5 |  | ${ }^{100}$ | 12 |  | ${ }^{13}$ | 890 | 2 | 59 |
| $14.45 .15,45$ | ${ }^{8}$ |  | ${ }^{100}$ | 6 | ， | ${ }^{65}$ |  | ， |  | ${ }^{7}$ |  | ${ }^{\circ}$ | 109 |  | ＂1 | ， |  |  | ${ }^{121}$ |  | ${ }^{12}$ | ${ }^{12}$ |  |  | ${ }^{12}$ | ＂ |  | ${ }^{12}$ | 59 | ${ }^{24}$ | ${ }^{63}$ |
| 15500．16：00 | ${ }^{8}$ |  | ${ }^{10}$ | － |  | ＊ |  | ， |  | ${ }^{7}$ |  | ${ }^{23}$ | ${ }^{103}$ |  | 105 | ， |  |  | ${ }^{123}$ |  | ${ }^{12}$ | ${ }^{12}$ | 4 |  | ${ }^{128}$ | ${ }^{10}$ |  | ＂ | ${ }_{52}$ | ${ }^{25}$ | ${ }^{66}$ |
|  | ${ }^{10}$ |  | ${ }^{113}$ | ， |  | $\cdots$ |  | ， |  | $\square$ |  | ＂ | ${ }^{109}$ |  | ${ }^{10}$ | ＝ |  |  | ${ }^{125}$ |  | ${ }^{12}$ | ${ }^{14}$ | 3 |  | 146 | 。 |  |  | ${ }^{23}$ | ${ }^{24}$ | ${ }^{\text {ac }}$ |
| 1530．14．30 | ${ }^{110}$ |  | ${ }^{12}$ | 1 |  | ${ }^{4}$ |  | ＇ |  | ${ }^{56}$ |  | ${ }^{\text {w }}$ | ${ }^{103}$ |  | ${ }^{105}$ | ， |  |  | ${ }^{123}$ |  | ${ }^{125}$ |  |  |  | ${ }^{15}$ | 10 |  | ＂ | ${ }^{60}$ | ${ }^{20}$ | ${ }^{624}$ |
| 15.45 .16 .45 | ${ }^{14}$ |  | ${ }^{17}$ | ${ }^{45}$ | ${ }^{5}$ | ${ }^{4}$ |  | ， |  | ${ }^{54}$ |  | ${ }^{\circ}$ | 12 |  | ${ }^{103}$ | ， |  |  | ${ }^{12}$ |  | ${ }^{126}$ | ${ }^{14}$ | 0 |  | ${ }_{12}$ | ${ }^{12}$ |  | 12 | 59 | 20 | ${ }^{611}$ |
| 18500．7．7．00 | ${ }^{120}$ |  | ${ }^{12}$ | 2 | 2 | $\cdots$ |  | ， |  | 50 |  | ${ }_{5}$ | ${ }^{105}$ |  | ${ }^{106}$ | ， |  |  | 19 |  | ${ }^{123}$ |  | 6 |  | ${ }^{4}$ | ${ }^{15}$ |  | ${ }^{15}$ | ${ }_{58} 8$ | ＂ | ${ }^{615}$ |
| 18：15．57：715 | ${ }^{17}$ |  | － | － |  | ${ }^{4}$ |  | ， |  | ${ }^{51}$ |  | ${ }^{5}$ | ${ }^{8}$ |  | $\cdots$ | 。 |  |  | ${ }^{19}$ |  | ${ }^{12}$ |  | \％ |  | ${ }^{18}$ | ${ }^{16}$ |  | ${ }^{16}$ | 82 | ${ }^{14}$ | ${ }^{56}$ |
| 18530．7．730 | ${ }^{12}$ |  | ${ }^{123}$ | \％ |  | ${ }^{4}$ |  | ， |  | 50 |  | 5 | ${ }^{2}$ |  | ${ }^{3}$ | ， |  |  | ＂5 |  | ${ }^{18}$ |  | O |  | ${ }^{13}$ | ${ }^{13}$ |  | ${ }^{13}$ | ${ }_{568}$ | 13 | ${ }_{58}$ |
| 10．4． 7 7， 7.5 | ${ }^{19}$ |  | ${ }^{121}$ | 45 |  | ${ }^{4}$ |  | ， |  | ${ }^{48}$ |  | ${ }^{49}$ | ${ }^{\circ}$ |  | $\because$ | 。 |  |  | 10 |  | ${ }^{12}$ |  | 8 |  | ${ }^{128}$ | ＂ |  | ＂ | 556 |  | ${ }_{56}$ |
| ${ }^{17200.18500}$ | ${ }^{123}$ |  | ${ }^{124}$ | 4 |  | ${ }^{9}$ |  |  |  | ${ }^{45}$ |  | 4 | ${ }^{82}$ |  | 8 |  |  |  | ${ }^{100}$ |  | ${ }^{12}$ |  |  |  | ${ }^{19}$ | － |  |  | ${ }^{59}$ |  | ${ }_{56}$ |
| tres．18：1．： | ${ }^{17}$ |  | ${ }^{18}$ | \％ |  | ${ }^{39}$ |  |  |  | ${ }^{3}$ |  | ${ }^{3}$ | ${ }^{2}$ |  | 70 | 。 |  |  | ${ }^{8}$ |  | ${ }^{3}$ |  | 8 |  | ${ }^{108}$ | ＂ |  | ＂ | 46 |  | ${ }^{40}$ |
| ${ }^{1730.18,30}$ | ${ }^{106}$ |  | ${ }^{107}$ | ${ }^{3}$ |  | ${ }^{32}$ |  | s |  | ${ }^{29}$ |  | ${ }^{29}$ | ${ }^{63}$ |  | ${ }^{63}$ | 。 |  |  | ${ }^{76}$ |  | ＂ |  | 8 |  | ${ }^{108}$ | ${ }^{12}$ |  | ${ }^{12}$ | ${ }^{22}$ |  | ${ }^{48}$ |
| ${ }^{173,5.18,4.4}$ | ${ }^{23}$ |  | ＊ | 2 | 2 | ${ }^{24}$ |  | ， |  | ${ }^{25}$ |  | ${ }^{25}$ | 4 |  | $\because$ | ， |  |  | ${ }^{65}$ |  | ${ }^{6}$ |  | 0 |  | ${ }^{101}$ | ${ }^{13}$ |  | ${ }^{13}$ | ${ }_{33}$ | 3 | ${ }^{37}$ |
| 18300．1930 | ${ }^{7}$ |  | $\stackrel{7}{7}$ | 4 | ${ }^{6}$ 2 | ${ }^{18}$ |  | － |  | ${ }^{23}$ |  | ${ }^{24}$ | ${ }^{42}$ |  | 4 | ＇ |  |  | ${ }_{5}$ |  | $s$ |  | 0 |  | $\because$ | 12 |  | ${ }^{12}$ | ${ }^{317}$ | ${ }^{4}$ | ${ }^{321}$ |

# TECHNICAL PAPER <br>  

## Traffic and transport

## Appendix C Key intersection configurations

## A. 1 ALBURY PRECINCT

A.1.1 MURRAY RIVER BRIDGE ENHANCEMENT SITE


1. Atkins Street / East Street

2. Panmure Street / Olive Street

3. Atkins Street / Macauley Street

4. Atkins Street / Kiewa Street

5. Abercorn Street / Kiewa Street

6. Abercorn Street / Townsend Street

## A.1.2 ALBURY STATION ENHANCEMENT SITES



1. Young Street / Smollett Street / Railway Place

2. Young Street / Dean Street

3. Young Street / Wilson Street

4. Young Street / Guinea Street / Riverina Highway


5. Schubach Street / Kenilworth Street
A.1.3

This section is intentionally left blank

## A.1.4 BILLY HUGHES BRIDGE ENHANCEMENT SITE



1. Wagga Road / Hume Highway Northbound Ramps

2. Wagga Road / Hume Highway Southbound Ramps

## A.1.5 TABLE TOP CLEARANCES ENHANCEMENT SITE



1. Tynan Road / Perryman Lane

2. Tynan Road / Hume Highway

## A. 2 GREATER HUME - LOCKHART PRECINCT

A.2.1 CULCAIRN ENHANCEMENT SITE


## A.2.2 HENTY YARD CLEARNACES ENHANCEMENT SITE



1. Olympic Highway / Sladen Street and;
2. Ivor Street / Sladen Street

3. Rosler Street / Allan Street

4. Sladen Street / Allan Street

5. Rosler Street / Yankee Crossing Road / Railway Parade

## A.2.3 YERONG CREEK YARD CLEAREANCES ENHANCEMENT SITE



1. Olympic Highway / Plunkett Street / Cole Street

2. Plunkett Street / Finlayson Street

## A.2.4 THE ROCK YARD CLEARANCES ENHANCEMENT SITE



1. Olympic Highway / Urana Street / Mangoplah Road

## A. 3 WAGGA WAGGA PRECINCT

A.3.1 URANQUINTY YARD CLEARANCES ENHANCEMENT SITE


1. Olympic Highway / Yarragundry Street

## A.3.2 PEARSON STREET BRIDGE ENAHANCEMENT SIET



1. Pearson Street / Edward Street / Moorong Street

2. Pearson Street / Urana Street
3. Fernleigh Road / Alan Turner Depot Access Road


4. Pearson Street / Cheshire Street

5. Pearson Street / Fernleigh Road / Glenfield Road

## A.3.3 WAGGA WAGGA STATION ENHANCEMENT SITES



1. Edward Street / Docker Street

2. Edward Street / Fox Street


3. Edward Street / Brookong Avenue

4. Edward Street / Edmondson Street



5. Erin Street / Macleay Street

6. Bourke Street / Urana Street

7. Coleman Street / Kildare Street

8. Edmondson Street / Erin Street

9. Michelmore Street / Urana Street

10. Docker Street / Chaston Street

11. Macleay / Urana Street

## A.3.4 BOMEN YARD CLEARANCES ENHANCEMENT SITE



1. Merino Street / Byrnes Road / East Bomen Road

## A. 4 JUNEE PRECINCT

## A.4.1 HAREFIELD YARD CLEARANCES ENHANCEMENT SITE



1. Harefield Road / Railway Access Road / Byrnes Road (stub)

2. Byrnes Road / Pattersons Road

## A.4.2 KEMP STREET BRIDGE AND JUNEE STATION ENHANCEMENT SITES



5. Lorne Street / Peel Street / Humpreys Street

6. Lorne Street / Belmore Street / Access

7. Lorne Street / Hill Street / Ducker Street

## A.4.3 OLYMPIC HIGHWAY UNDERBRIDGE ENHANCEMENT SITE



1. Illabo Road / Regent Street / Access Road

2. Byrnes Road / Pattersons Road

3. Main Street / Olympic Highway

## A.4.4 JUNEE TO ILLABO CLEARANCES ENAHNCEMENT SITE



1. Olympic Highway / Waterworks Road

2. Olympic Highway / Brabins Road

3. Olympic Highway / Marinna Railway Station Access Road

4. Brabins Road / Lawford Street

# TECHNICAL PAPER <br>  

## Traffic and transport

## Appendix D SIDRA results

ALBURY TO ILLABO ENVIRONMENTAL IMPACT STATEMENT

## SITE LAYOUT

## 目 Site: [Borella Road / Hume Highway NB off ramp - Base - PM

 Peak (Site Folder: Albury)]Site Category: Base Year
Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


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## PHASING SUMMARY

## 目 Site: [Borella Road / Hume Highway NB off ramp - Base - PM

Peak (Site Folder: Albury)]

Site Category: Base Year
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=90$ seconds (Site User-Given Cycle Time)
Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Leading Right Turn
Reference Phase: Phase B
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

| Phase Timing Summary |
| :--- |
| Phase A B C <br> Phase Change Time (sec) 38 0 14 <br> Green Time (sec) 46 8 18 <br> Phase Time (sec) 52 14 24 <br> Phase Split $58 \%$ $16 \%$ $27 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase

| Normal Movement | Permitted/Opposed |
| :---: | :---: |
| $\Rightarrow$ Slip/Bypass-Lane Movement | Opposed Slip/Bypass-Lane |
| Stopped Movement | $\checkmark$ Turn On Red |
| Other Movement Class (MC) Running | $\Rightarrow$ Undetected Movement |
| $\checkmark$ Mixed Running \& Stopped MCs | $\Rightarrow$ Continuous Movement |
| $\checkmark$ Other Movement Class (MC) Stopped | - Phase Transition Applied |

## MOVEMENT SUMMARY

## 目 Site: [Borella Road / Hume Highway NB off ramp - Base - PM Peak (Site Folder: Albury)]

Site Category: Base Year
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=90$ seconds (Site User-Given Cycle Time)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INP } \\ & \text { vOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | UT HV ] veh/h |  |  | Deg. Satn v/c | Aver. Delay sec | Level of Service |  | $\begin{aligned} & \text { CK OF } \\ & \text { UE } \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. Que | Effective <br> Stop <br> Rate | Aver. No. Cycles | Aver. Speed km/h |
| South: Hume Highway NB Off ramp (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 253 | 1 | 266 | 0.4 | * 0.708 | 43.8 | LOS D | 11.5 | 80.6 | 0.99 | 0.86 | 1.05 | 27.1 |
| 2 T1 | 1 | 0 | 1 | 0.0 | 0.608 | 36.5 | LOS D | 9.0 | 66.7 | 0.96 | 0.82 | 0.96 | 38.4 |
| 3 R2 | 207 | 14 | 218 | 6.8 | 0.608 | 41.9 | LOS D | 9.0 | 66.7 | 0.96 | 0.82 | 0.96 | 26.1 |
| Approach | 461 | 15 | 485 | 3.3 | 0.708 | 42.9 | LOS D | 11.5 | 80.6 | 0.98 | 0.84 | 1.01 | 26.7 |
| East: Borella Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 T1 | 854 | 5 | 899 | 0.6 | 0.643 | 13.4 | LOS B | 21.1 | 148.4 | 0.66 | 0.72 | 0.66 | 25.0 |
| 6 R2 | 64 | 2 | 67 | 3.1 | * 0.643 | 48.3 | LOS D | 6.0 | 42.7 | 1.00 | 0.83 | 1.07 | 26.4 |
| Approach | 918 | 7 | 966 | 0.8 | 0.643 | 15.8 | LOS B | 21.1 | 148.4 | 0.68 | 0.73 | 0.69 | 25.2 |
| West: Borella Road (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 343 | 5 | 361 | 1.5 | 0.705 | 21.6 | LOS C | 23.2 | 164.0 | 0.82 | 0.79 | 0.82 | 39.3 |
| 11 T1 | 995 | 6 | 1047 | 0.6 | * 0.705 | 18.0 | LOS B | 23.9 | 168.0 | 0.82 | 0.76 | 0.82 | 20.8 |
| Approach | 1338 | 11 | 1408 | 0.8 | 0.705 | 18.9 | LOS B | 23.9 | 168.0 | 0.82 | 0.77 | 0.82 | 27.5 |
| All <br> Vehicles | 2717 | 33 | 2860 | 1.2 | 0.708 | 21.9 | LOS C | 23.9 | 168.0 | 0.80 | 0.76 | 0.81 | 26.7 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline \multicolumn{12}{|l|}{Pedestrian Movement Performance} \\
\hline \[
\begin{aligned}
\& \text { Mov } \\
\& \text { ID }
\end{aligned}
\] \& \begin{tabular}{l}
Input Vol. \\
ped/h
\end{tabular} \& Dem. Flow ped/h \& Aver. Delay sec \& \multicolumn{3}{|l|}{Level of AVERAGE BACK OF Service QUEUE} \& \multicolumn{2}{|l|}{Prop. Effective
Que
Stop

Rate} \& Travel Time sec \& \begin{tabular}{l}
Travel Dist. <br>
m

 \& 

Aver. <br>
Speed <br>
$\mathrm{m} / \mathrm{sec}$
\end{tabular} <br>

\hline \multicolumn{12}{|l|}{South: Hume Highway NB Off ramp (S)} <br>
\hline P1 Full \& 50 \& 53 \& 39.3 \& LOS D \& 0.1 \& 0.1 \& 0.94 \& 0.94 \& 200.2 \& 209.2 \& 1.04 <br>
\hline \multicolumn{12}{|l|}{North: Hume Highway NB On ramp (N)} <br>
\hline P3 Full \& 50 \& 53 \& 39.3 \& LOS D \& 0.1 \& 0.1 \& 0.94 \& 0.94 \& 200.1 \& 209.0 \& 1.04 <br>
\hline \multicolumn{12}{|l|}{West: Borella Road (W)} <br>
\hline P4 Full \& 50 \& 53 \& 39.3 \& LOS D \& 0.1 \& 0.1 \& 0.94 \& 0.94 \& 207.7 \& 219.0 \& 1.05 <br>

\hline | All |
| :--- |
| Pedestrians | \& 150 \& 158 \& 39.3 \& LOS D \& 0.1 \& 0.1 \& 0.94 \& 0.94 \& 202.7 \& 212.4 \& 1.05 <br>

\hline
\end{tabular}

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## PHASING SUMMARY

目 Site: [Borella Road / Hume Highway NB Off ramps - PM Peak with Construction Traffic (Site Folder: Albury)]

Site Category: Future Conditions 1
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=90$ seconds (Site User-Given Cycle Time)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Leading Right Turn
Reference Phase: Phase B
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C
Phase Timing Summary

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Phase Change Time (sec) | 38 | 0 | 14 |
| Green Time (sec) | 46 | 8 | 18 |
| Phase Time (sec) | 52 | 14 | 24 |
| Phase Split | $58 \%$ | $16 \%$ | $27 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement
Other Movement Class (MC) Running

## MOVEMENT SUMMARY

Site: [Borella Road / Hume Highway NB Off ramps - PM Peak with Construction Traffic (Site Folder: Albury)]

Site Category: Future Conditions 1
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=90$ seconds (Site User-Given Cycle Time)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | JT MES HV ] veh/h |  | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \mathrm{m} \end{gathered}$ | Prop. Que | Effective Stop Rate |  | Aver. Speed <br> $\mathrm{km} / \mathrm{h}$ |
| South: Hume Highway NB Off ramp (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 253 | 1 | 266 | 0.4 | * 0.708 | 43.8 | LOS D | 11.5 | 80.6 | 0.99 | 0.86 | 1.05 | 27.1 |
| $2 \quad \mathrm{~T} 1$ | 1 | 0 | 1 | 0.0 | 0.608 | 36.5 | LOS D | 9.0 | 66.7 | 0.96 | 0.82 | 0.96 | 38.4 |
| 3 R2 | 207 | 14 | 218 | 6.8 | 0.608 | 41.9 | LOS D | 9.0 | 66.7 | 0.96 | 0.82 | 0.96 | 26.1 |
| Approach | 461 | 15 | 485 | 3.3 | 0.708 | 42.9 | LOS D | 11.5 | 80.6 | 0.98 | 0.84 | 1.01 | 26.7 |
| East: Borella Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 T1 | 854 | 5 | 899 | 0.6 | 0.643 | 13.4 | LOS B | 21.1 | 148.4 | 0.66 | 0.72 | 0.66 | 25.0 |
| 6 R2 | 64 | 2 | 67 | 3.1 | * 0.643 | 48.3 | LOS D | 6.0 | 42.7 | 1.00 | 0.83 | 1.07 | 26.4 |
| Approach | 918 | 7 | 966 | 0.8 | 0.643 | 15.8 | LOS B | 21.1 | 148.4 | 0.68 | 0.73 | 0.69 | 25.2 |
| West: Borella Road (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 360 | 9 | 379 | 2.5 | 0.726 | 21.9 | LOS C | 24.2 | 171.8 | 0.84 | 0.80 | 0.84 | 38.9 |
| 11 T1 | 1012 | 10 | 1065 | 1.0 | * 0.726 | 18.3 | LOS B | 24.9 | 176.1 | 0.84 | 0.77 | 0.84 | 20.6 |
| Approach | 1372 | 19 | 1444 | 1.4 | 0.726 | 19.3 | LOS B | 24.9 | 176.1 | 0.84 | 0.78 | 0.84 | 27.4 |
| All <br> Vehicles | 2751 | 41 | 2896 | 1.5 | 0.726 | 22.1 | LOS C | 24.9 | 176.1 | 0.81 | 0.77 | 0.82 | 26.7 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID Crossing | Input Vol. ped/h | Dem. Flow ped/h | Aver. Delay sec | Level of AVERAGE BACK OF Service QUEUE |  |  | Prop. EffectiveQueStop <br>  <br>  <br>  <br> Rate |  | Travel Time sec | Travel Dist. <br> m | Aver. Speed m/sec |
| South: Hume Highway NB Off ramp (S) |  |  |  |  |  |  |  |  |  |  |  |
| P1 Full | 50 | 53 | 39.3 | LOS D | 0.1 | 0.1 | 0.94 | 0.94 | 200.2 | 209.2 | 1.04 |
| North: Hume Highway NB On ramp (N) |  |  |  |  |  |  |  |  |  |  |  |
| P3 Full | 50 | 53 | 39.3 | LOS D | 0.1 | 0.1 | 0.94 | 0.94 | 200.1 | 209.0 | 1.04 |
| West: Borella Road (W) |  |  |  |  |  |  |  |  |  |  |  |
| P4 Full | 50 | 53 | 39.3 | LOS D | 0.1 | 0.1 | 0.94 | 0.94 | 207.7 | 219.0 | 1.05 |
| All <br> Pedestrians | 150 | 158 | 39.3 | LOS D | 0.1 | 0.1 | 0.94 | 0.94 | 202.7 | 212.4 | 1.05 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## SITE LAYOUT

$\square$ Site: [Olympic Highway / Balfour Street - Base - Peak Hour (Site Folder: Culcairn, Greater Hume Lockhart)]
New Site
Site Category: Base Year
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


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## MOVEMENT SUMMARY

## $\nabla$ Site: [Olympic Highway / Balfour Street - Base - Peak Hour (Site Folder: Culcairn, Greater Hume Lockhart)]

New Site
Site Category: Base Year
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { INP } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { UT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ | $\begin{array}{r} \text { DEN } \\ \text { FLC } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{aligned} & \text { AND } \\ & \text { WS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service | $\begin{aligned} & 95 \% \text { B } \\ & \text { QU } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver No. Cycles | Aver. Speed <br> km/h |
| South: Railway Parade / Olympic Hwy |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 130 | 28.0 | 137 | 28.0 | 0.362 | 6.0 | LOSA | 2.4 | 20.5 | 0.62 | 0.69 | 0.62 | 45.0 |
| 2 T1 | 48 | 28.0 | 51 | 28.0 | 0.362 | 5.9 | LOS A | 2.4 | 20.5 | 0.62 | 0.69 | 0.62 | 46.0 |
| 3 R2 | 130 | 28.0 | 137 | 28.0 | 0.362 | 9.9 | LOS A | 2.4 | 20.5 | 0.62 | 0.69 | 0.62 | 45.8 |
| Approach | 308 | 28.0 | 324 | 28.0 | 0.362 | 7.6 | LOS A | 2.4 | 20.5 | 0.62 | 0.69 | 0.62 | 45.5 |
| East: Balfour Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 160 | 28.0 | 168 | 28.0 | 0.442 | 5.6 | LOSA | 3.1 | 27.2 | 0.59 | 0.61 | 0.59 | 45.6 |
| 5 T1 | 217 | 28.0 | 228 | 28.0 | 0.442 | 5.5 | LOS A | 3.1 | 27.2 | 0.59 | 0.61 | 0.59 | 46.7 |
| 6 R2 | 40 | 28.0 | 42 | 28.0 | 0.442 | 9.5 | LOS A | 3.1 | 27.2 | 0.59 | 0.61 | 0.59 | 46.5 |
| Approach | 417 | 28.0 | 439 | 28.0 | 0.442 | 5.9 | LOS A | 3.1 | 27.2 | 0.59 | 0.61 | 0.59 | 46.2 |
| North: Railway Parade |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 22 | 28.0 | 23 | 28.0 | 0.114 | 7.4 | LOS A | 0.6 | 5.6 | 0.67 | 0.71 | 0.67 | 44.7 |
| 8 T1 | 33 | 28.0 | 35 | 28.0 | 0.114 | 7.3 | LOS A | 0.6 | 5.6 | 0.67 | 0.71 | 0.67 | 45.7 |
| 9 R2 | 22 | 28.0 | 23 | 28.0 | 0.114 | 11.3 | LOS B | 0.6 | 5.6 | 0.67 | 0.71 | 0.67 | 45.5 |
| Approach | 77 | 28.0 | 81 | 28.0 | 0.114 | 8.5 | LOS A | 0.6 | 5.6 | 0.67 | 0.71 | 0.67 | 45.4 |
| West: Balfour Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 40 | 28.0 | 42 | 28.0 | 0.446 | 5.6 | LOS A | 3.2 | 27.7 | 0.60 | 0.64 | 0.60 | 45.1 |
| 11 T1 | 217 | 28.0 | 228 | 28.0 | 0.446 | 5.5 | LOS A | 3.2 | 27.7 | 0.60 | 0.64 | 0.60 | 46.1 |
| 12 R 2 | 160 | 28.0 | 168 | 28.0 | 0.446 | 9.6 | LOS A | 3.2 | 27.7 | 0.60 | 0.64 | 0.60 | 45.9 |
| Approach | 417 | 28.0 | 439 | 28.0 | 0.446 | 7.1 | LOS A | 3.2 | 27.7 | 0.60 | 0.64 | 0.60 | 45.9 |
| All <br> Vehicles | 1219 | 28.0 | 1283 | 28.0 | 0.446 | 6.9 | LOS A | 3.2 | 27.7 | 0.61 | 0.65 | 0.61 | 45.9 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\nabla$ Site: [Olympic Highway / Balfour Street - Peak Hour with Construction Traffic (Site Folder: Culcairn, Greater Hume <br> Lockhart)]

New Site
Site Category: Future Conditions 1
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{array}{r} \text { IN } \\ \text { VOL } \\ \text { [ Total } \\ \text { veh/h } \\ \hline \end{array}$ | $\begin{gathered} \text { JT } \\ \text { VES } \\ \text { HV] } \\ \% \\ \hline \end{gathered}$ |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \\ & \hline \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{aligned} & \text { CK OF } \\ & \text { UE } \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Railway Parade / Olympic Hwy |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 130 | 28.0 | 137 | 28.0 | 0.418 | 6.4 | LOSA | 2.9 | 24.8 | 0.68 | 0.73 | 0.68 | 44.9 |
| 2 T1 | 82 | 28.0 | 86 | 28.0 | 0.418 | 6.3 | LOSA | 2.9 | 24.8 | 0.68 | 0.73 | 0.68 | 45.9 |
| 3 R2 | 130 | 28.0 | 137 | 28.0 | 0.418 | 10.4 | LOS B | 2.9 | 24.8 | 0.68 | 0.73 | 0.68 | 45.7 |
| Approach | 342 | 28.0 | 360 | 28.0 | 0.418 | 7.9 | LOSA | 2.9 | 24.8 | 0.68 | 0.73 | 0.68 | 45.4 |
| East: Balfour Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 160 | 28.0 | 168 | 28.0 | 0.481 | 5.7 | LOS A | 3.6 | 31.0 | 0.62 | 0.63 | 0.62 | 45.4 |
| 5 T1 | 217 | 28.0 | 228 | 28.0 | 0.481 | 5.6 | LOS A | 3.6 | 31.0 | 0.62 | 0.63 | 0.62 | 46.5 |
| 6 R2 | 74 | 28.0 | 78 | 28.0 | 0.481 | 9.6 | LOS A | 3.6 | 31.0 | 0.62 | 0.63 | 0.62 | 46.2 |
| Approach | 451 | 28.0 | 475 | 28.0 | 0.481 | 6.3 | LOS A | 3.6 | 31.0 | 0.62 | 0.63 | 0.62 | 46.0 |
| North: Railway Parade |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 26 | 28.0 | 27 | 28.0 | 0.128 | 7.4 | LOS A | 0.7 | 6.4 | 0.69 | 0.72 | 0.69 | 44.7 |
| 8 T1 | 37 | 28.0 | 39 | 28.0 | 0.128 | 7.3 | LOSA | 0.7 | 6.4 | 0.69 | 0.72 | 0.69 | 45.7 |
| 9 R2 | 22 | 28.0 | 23 | 28.0 | 0.128 | 11.4 | LOS B | 0.7 | 6.4 | 0.69 | 0.72 | 0.69 | 45.5 |
| Approach | 85 | 28.0 | 89 | 28.0 | 0.128 | 8.4 | LOS A | 0.7 | 6.4 | 0.69 | 0.72 | 0.69 | 45.4 |
| West: Balfour Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 40 | 28.0 | 42 | 28.0 | 0.487 | 6.4 | LOSA | 3.5 | 30.5 | 0.69 | 0.72 | 0.69 | 44.7 |
| 11 T1 | 217 | 28.0 | 228 | 28.0 | 0.487 | 6.3 | LOSA | 3.5 | 30.5 | 0.69 | 0.72 | 0.69 | 45.8 |
| 12 R 2 | 160 | 28.0 | 168 | 28.0 | 0.487 | 10.3 | LOS B | 3.5 | 30.5 | 0.69 | 0.72 | 0.69 | 45.6 |
| Approach | 417 | 28.0 | 439 | 28.0 | 0.487 | 7.8 | LOSA | 3.5 | 30.5 | 0.69 | 0.72 | 0.69 | 45.6 |
| All <br> Vehicles | 1295 | 28.0 | 1363 | 28.0 | 0.487 | 7.4 | LOSA | 3.6 | 31.0 | 0.66 | 0.69 | 0.66 | 45.7 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## SITE LAYOUT

$\nabla$ Site: [Peak Hour Base - 2024 (Site Folder: Uranquinty,
Wagga)]
New Site
Site Category: (None)
Give-Way (Two-Way)

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.
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## MOVEMENT SUMMARY

$\nabla$ Site: [Peak Hour Base - 2024 (Site Folder: Uranquinty,
Wagga)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INP } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay $\qquad$ <br> sec | Level of Service | $\begin{gathered} \text { 95\% B B } \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Yarragundry Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 14 | 8.0 | 15 | 8.0 | 0.051 | 4.6 | LOS A | 0.2 | 1.3 | 0.48 | 0.64 | 0.48 | 37.3 |
| 2 T1 | 3 | 8.0 | 3 | 8.0 | 0.051 | 6.5 | LOSA | 0.2 | 1.3 | 0.48 | 0.64 | 0.48 | 37.3 |
| 3 R2 | 14 | 8.0 | 15 | 8.0 | 0.051 | 9.2 | LOSA | 0.2 | 1.3 | 0.48 | 0.64 | 0.48 | 37.0 |
| Approach | 31 | 8.0 | 33 | 8.0 | 0.051 | 6.9 | LOS A | 0.2 | 1.3 | 0.48 | 0.64 | 0.48 | 37.2 |
| East: Olympic Hwy |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 16 | 17.0 | 17 | 17.0 | 0.199 | 5.8 | LOSA | 0.2 | 1.8 | 0.08 | 0.05 | 0.08 | 48.7 |
| 5 T1 | 290 | 17.0 | 305 | 17.0 | 0.199 | 0.1 | LOSA | 0.2 | 1.8 | 0.08 | 0.05 | 0.08 | 49.5 |
| 6 R2 | 16 | 17.0 | 17 | 17.0 | 0.199 | 6.5 | LOS A | 0.2 | 1.8 | 0.08 | 0.05 | 0.08 | 48.2 |
| Approach | 322 | 17.0 | 339 | 17.0 | 0.199 | 0.7 | NA | 0.2 | 1.8 | 0.08 | 0.05 | 0.08 | 49.4 |
| North: Yarragundry Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 14 | 8.0 | 15 | 8.0 | 0.051 | 4.6 | LOSA | 0.2 | 1.3 | 0.48 | 0.64 | 0.48 | 37.3 |
| 8 T1 | 3 | 8.0 | 3 | 8.0 | 0.051 | 6.5 | LOSA | 0.2 | 1.3 | 0.48 | 0.64 | 0.48 | 37.3 |
| 9 R2 | 14 | 8.0 | 15 | 8.0 | 0.051 | 9.2 | LOSA | 0.2 | 1.3 | 0.48 | 0.64 | 0.48 | 37.0 |
| Approach | 31 | 8.0 | 33 | 8.0 | 0.051 | 6.9 | LOSA | 0.2 | 1.3 | 0.48 | 0.64 | 0.48 | 37.2 |
| West: Olympic Hwy |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 16 | 17.0 | 17 | 17.0 | 0.199 | 5.8 | LOSA | 0.2 | 1.8 | 0.08 | 0.05 | 0.08 | 48.7 |
| 11 T1 | 290 | 17.0 | 305 | 17.0 | 0.199 | 0.1 | LOS A | 0.2 | 1.8 | 0.08 | 0.05 | 0.08 | 49.5 |
| 12 R 2 | 16 | 17.0 | 17 | 17.0 | 0.199 | 6.5 | LOSA | 0.2 | 1.8 | 0.08 | 0.05 | 0.08 | 48.2 |
| Approach | 322 | 17.0 | 339 | 17.0 | 0.199 | 0.7 | NA | 0.2 | 1.8 | 0.08 | 0.05 | 0.08 | 49.4 |
| All <br> Vehicles | 706 | 16.2 | 743 | 16.2 | 0.199 | 1.3 | NA | 0.2 | 1.8 | 0.11 | 0.11 | 0.11 | 48.0 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\nabla$ Site: [Peak Hour Base w/ construction - 2024 (Site Folder: Uranquinty, Wagga)]

New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INP } \\ & \text { VOLu } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { JT } \\ & \text { VES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { WD } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | $\begin{aligned} & \text { Aver. } \\ & \text { No. } \\ & \text { Cycles } \end{aligned}$ | Aver. Speed <br> km/h |
| South: Yarragundry Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 14 | 8.0 | 15 | 8.0 | 0.054 | 4.6 | LOS A | 0.2 | 1.3 | 0.49 | 0.65 | 0.49 | 37.2 |
| 2 T1 | 3 | 8.0 | 3 | 8.0 | 0.054 | 7.4 | LOS A | 0.2 | 1.3 | 0.49 | 0.65 | 0.49 | 37.2 |
| 3 R2 | 14 | 8.0 | 15 | 8.0 | 0.054 | 9.8 | LOSA | 0.2 | 1.3 | 0.49 | 0.65 | 0.49 | 36.9 |
| Approach | 31 | 8.0 | 33 | 8.0 | 0.054 | 7.2 | LOSA | 0.2 | 1.3 | 0.49 | 0.65 | 0.49 | 37.0 |
| East: Olympic Hwy |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 16 | 17.0 | 17 | 17.0 | 0.233 | 6.6 | LOS A | 0.6 | 5.2 | 0.20 | 0.11 | 0.20 | 48.1 |
| 5 T1 | 290 | 17.0 | 305 | 17.0 | 0.233 | 0.5 | LOS A | 0.6 | 5.2 | 0.20 | 0.11 | 0.20 | 48.9 |
| 6 R2 | 50 | 17.0 | 53 | 17.0 | 0.233 | 6.9 | LOS A | 0.6 | 5.2 | 0.20 | 0.11 | 0.20 | 47.6 |
| Approach | 356 | 17.0 | 375 | 17.0 | 0.233 | 1.7 | NA | 0.6 | 5.2 | 0.20 | 0.11 | 0.20 | 48.7 |
| North: Yarragundry Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 18 | 8.0 | 19 | 8.0 | 0.068 | 4.7 | LOS A | 0.2 | 1.7 | 0.50 | 0.66 | 0.50 | 37.1 |
| 8 T1 | 3 | 8.0 | 3 | 8.0 | 0.068 | 7.2 | LOS A | 0.2 | 1.7 | 0.50 | 0.66 | 0.50 | 37.1 |
| 9 R2 | 18 | 8.0 | 19 | 8.0 | 0.068 | 10.1 | LOS B | 0.2 | 1.7 | 0.50 | 0.66 | 0.50 | 36.8 |
| Approach | 39 | 8.0 | 41 | 8.0 | 0.068 | 7.3 | LOS A | 0.2 | 1.7 | 0.50 | 0.66 | 0.50 | 37.0 |
| West: Olympic Hwy |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 50 | 17.0 | 53 | 17.0 | 0.221 | 5.2 | LOS A | 0.2 | 2.0 | 0.08 | 0.10 | 0.08 | 48.5 |
| 11 T1 | 290 | 17.0 | 305 | 17.0 | 0.221 | 0.1 | LOS A | 0.2 | 2.0 | 0.08 | 0.10 | 0.08 | 49.2 |
| 12 R 2 | 16 | 17.0 | 17 | 17.0 | 0.221 | 6.6 | LOSA | 0.2 | 2.0 | 0.08 | 0.10 | 0.08 | 48.0 |
| Approach | 356 | 17.0 | 375 | 17.0 | 0.221 | 1.2 | NA | 0.2 | 2.0 | 0.08 | 0.10 | 0.08 | 49.1 |
| All <br> Vehicles | 782 | 16.2 | 823 | 16.2 | 0.233 | 1.9 | NA | 0.6 | 5.2 | 0.17 | 0.15 | 0.17 | 47.5 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## SITE LAYOUT

$\nabla$ Site: [Edward Street / Pearson Street - AM Peak (Site Folder:
Wagga Wagga)]
Site Category: Base Year
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


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## MOVEMENT SUMMARY

© Site: [Edward Street / Pearson Street - AM Peak (Site Folder:
Wagga Wagga)]
Site Category: Base Year
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | JT MES HV ] veh/h |  | $\begin{aligned} & \text { AND } \\ & \text { WS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay $\qquad$ <br> sec | Level of Service | $\begin{gathered} 95 \% \text { B } \\ \text { QU } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \mathrm{m} \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Pearson Street (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 40 | 8 | 42 | 20.0 | 0.576 | 8.7 | LOS A | 4.4 | 32.2 | 0.76 | 0.86 | 0.89 | 49.9 |
| 2 T1 | 605 | 24 | 637 | 4.0 | 0.576 | 8.2 | LOS A | 4.4 | 32.2 | 0.76 | 0.88 | 0.90 | 51.4 |
| 3 R2 | 300 | 21 | 316 | 7.0 | 0.576 | 13.7 | LOS B | 4.3 | 31.6 | 0.77 | 0.96 | 0.92 | 45.9 |
| 3 u U | 7 | 0 | 7 | 0.0 | 0.576 | 15.6 | LOS B | 4.3 | 31.6 | 0.77 | 0.96 | 0.92 | 48.1 |
| Approach | 952 | 53 | 1002 | 5.6 | 0.576 | 10.0 | LOS B | 4.4 | 32.2 | 0.76 | 0.91 | 0.91 | 49.7 |
| East: Edward Street (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 105 | 11 | 111 | 10.5 | 0.368 | 7.4 | LOS A | 2.1 | 17.0 | 0.75 | 0.79 | 0.76 | 48.4 |
| 5 T1 | 174 | 34 | 183 | 19.5 | 0.368 | 7.9 | LOS A | 2.1 | 17.0 | 0.75 | 0.81 | 0.76 | 51.7 |
| 6 R2 | 180 | 13 | 189 | 7.2 | 0.368 | 12.8 | LOS B | 2.1 | 15.9 | 0.75 | 0.91 | 0.77 | 48.9 |
| 6 u U | 27 | 4 | 28 | 14.8 | 0.368 | 15.3 | LOS B | 2.1 | 15.9 | 0.75 | 0.91 | 0.77 | 45.7 |
| Approach | 486 | 62 | 512 | 12.8 | 0.368 | 10.0 | LOS B | 2.1 | 17.0 | 0.75 | 0.85 | 0.77 | 49.6 |
| North: Moorong Street ( N ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 325 | 12 | 342 | 3.7 | 0.682 | 11.5 | LOS B | 6.4 | 46.5 | 0.88 | 1.06 | 1.21 | 48.2 |
| 8 T1 | 502 | 20 | 528 | 4.0 | 0.682 | 12.2 | LOS B | 6.4 | 46.5 | 0.88 | 1.07 | 1.23 | 48.2 |
| 9 R2 | 150 | 20 | 158 | 13.3 | 0.682 | 18.2 | LOS B | 6.1 | 45.0 | 0.88 | 1.08 | 1.25 | 49.0 |
| 9 u U | 1 | 0 | 1 | 0.0 | 0.682 | 19.6 | LOS B | 6.1 | 45.0 | 0.88 | 1.08 | 1.25 | 50.4 |
| Approach | 978 | 52 | 1029 | 5.3 | 0.682 | 12.9 | LOS B | 6.4 | 46.5 | 0.88 | 1.07 | 1.23 | 48.4 |
| West: Sturt Highway (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 217 | 20 | 228 | 9.2 | 0.563 | 10.8 | LOS B | 3.8 | 29.0 | 0.86 | 1.00 | 1.09 | 50.3 |
| 11 T1 | 361 | 33 | 380 | 9.1 | 0.563 | 11.9 | LOS B | 3.8 | 29.0 | 0.85 | 1.00 | 1.10 | 49.1 |
| 12 R 2 | 28 | 4 | 29 | 14.3 | 0.563 | 17.7 | LOS B | 3.5 | 26.8 | 0.85 | 1.00 | 1.11 | 46.6 |
| 12u U | 1 | 0 | 1 | 0.0 | 0.563 | 19.0 | LOS B | 3.5 | 26.8 | 0.85 | 1.00 | 1.11 | 51.4 |
| Approach | 607 | 57 | 639 | 9.4 | 0.563 | 11.8 | LOS B | 3.8 | 29.0 | 0.86 | 1.00 | 1.10 | 49.5 |
| All <br> Vehicles | 3023 | 224 | 3182 | 7.4 | 0.682 | 11.3 | LOS B | 6.4 | 46.5 | 0.82 | 0.97 | 1.03 | 49.2 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^2]
## MOVEMENT SUMMARY

- Site: [Edward Street / Pearson Street - AM Peak with Construction Traffic (Site Folder: Wagga Wagga)]

Site Category: Future Conditions 1
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | JT <br> MES HV ] veh/h |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. <br> Satn <br> v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{aligned} & \text { CK OF } \\ & \text { UE } \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Pearson Street (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| L2 | 40 | 8 | 42 | 20.0 | 0.579 | 8.7 | LOS A | 4.4 | 32.5 | 0.76 | 0.86 | 0.90 | 49.8 |
| 2 T1 | 605 | 24 | 637 | 4.0 | 0.579 | 8.3 | LOSA | 4.4 | 32.5 | 0.76 | 0.89 | 0.90 | 51.3 |
| 3 R 2 | 300 | 21 | 316 | 7.0 | 0.579 | 13.8 | LOS B | 4.3 | 31.8 | 0.77 | 0.96 | 0.93 | 45.9 |
| 3 u U | 7 | 0 | 7 | 0.0 | 0.579 | 15.6 | LOS B | 4.3 | 31.8 | 0.77 | 0.96 | 0.93 | 48.0 |
| Approach | 952 | 53 | 1002 | 5.6 | 0.579 | 10.1 | LOS B | 4.4 | 32.5 | 0.76 | 0.91 | 0.91 | 49.7 |
| East: Edward Street (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 117 | 12 | 123 | 10.3 | 0.386 | 7.7 | LOS A | 2.3 | 18.3 | 0.77 | 0.83 | 0.80 | 48.3 |
| $5 \quad \mathrm{~T} 1$ | 174 | 34 | 183 | 19.5 | 0.386 | 8.2 | LOS A | 2.3 | 18.3 | 0.77 | 0.84 | 0.80 | 51.4 |
| 6 R2 | 180 | 13 | 189 | 7.2 | 0.386 | 13.2 | LOS B | 2.3 | 17.1 | 0.77 | 0.93 | 0.81 | 48.7 |
| 6 u U | 27 | 4 | 28 | 14.8 | 0.386 | 15.7 | LOS B | 2.3 | 17.1 | 0.77 | 0.93 | 0.81 | 45.5 |
| Approach | 498 | 63 | 524 | 12.7 | 0.386 | 10.3 | LOS B | 2.3 | 18.3 | 0.77 | 0.88 | 0.80 | 49.4 |
| North: Moorong Street ( N ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 325 | 12 | 342 | 3.7 | 0.701 | 11.9 | LOS B | 6.8 | 49.1 | 0.89 | 1.08 | 1.26 | 47.8 |
| 8 T1 | 514 | 21 | 541 | 4.1 | 0.701 | 12.8 | LOS B | 6.8 | 49.1 | 0.89 | 1.09 | 1.28 | 47.8 |
| 9 R2 | 150 | 20 | 158 | 13.3 | 0.701 | 18.7 | LOS B | 6.4 | 47.3 | 0.89 | 1.10 | 1.29 | 48.7 |
| 9 u U | 1 | 0 | 1 | 0.0 | 0.701 | 20.1 | LOS C | 6.4 | 47.3 | 0.89 | 1.10 | 1.29 | 50.0 |
| Approach | 990 | 53 | 1042 | 5.4 | 0.701 | 13.4 | LOS B | 6.8 | 49.1 | 0.89 | 1.09 | 1.27 | 48.0 |
| West: Sturt Highway (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 217 | 20 | 228 | 9.2 | 0.578 | 11.0 | LOS B | 4.0 | 30.1 | 0.86 | 1.01 | 1.11 | 50.2 |
| 11 T1 | 361 | 33 | 380 | 9.1 | 0.578 | 12.1 | LOS B | 4.0 | 30.1 | 0.86 | 1.01 | 1.12 | 48.8 |
| 12 R 2 | 41 | 5 | 43 | 12.2 | 0.578 | 17.8 | LOS B | 3.7 | 27.8 | 0.85 | 1.01 | 1.13 | 46.6 |
| 12 u U | 1 | 0 | 1 | 0.0 | 0.578 | 19.2 | LOS B | 3.7 | 27.8 | 0.85 | 1.01 | 1.13 | 51.0 |
| Approach | 620 | 58 | 653 | 9.4 | 0.578 | 12.1 | LOS B | 4.0 | 30.1 | 0.86 | 1.01 | 1.12 | 49.2 |
| All <br> Vehicles | 3060 | 227 | 3221 | 7.4 | 0.701 | 11.6 | LOS B | 6.8 | 49.1 | 0.82 | 0.98 | 1.05 | 49.0 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## SITE LAYOUT

$\nabla$ Site: [Glenfield Road / Pearson Street / Fernleigh Road (Site
Folder: Wagga Wagga)]
Site Category: Base Year
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


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## MOVEMENT SUMMARY

- Site: [Glenfield Road / Pearson Street / Fernleigh Road (Site Folder: Wagga Wagga)]

Site Category: Base Year
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | JT <br> VES <br> HV ] <br> veh/h |  | $\begin{gathered} \text { AND } \\ \text { WS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. <br> Satn <br> v/c | Aver. Delay sec | Level of Service |  | $\begin{aligned} & \text { CK OF } \\ & \text { UE } \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. Que | Effective Stop Rate | Aver. No. Cvcles | Aver. Speed <br> km/h |
| South: Glenfield Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| L2 | 122 | 5 | 128 | 4.1 | 0.719 | 10.8 | LOS B | 9.3 | 66.0 | 0.87 | 0.91 | 1.10 | 49.9 |
| 2 T1 | 651 | 12 | 685 | 1.8 | 0.719 | 10.6 | LOS B | 9.3 | 66.0 | 0.87 | 0.91 | 1.10 | 50.4 |
| 3 R2 | 77 | 1 | 81 | 1.3 | 0.117 | 11.7 | LOS B | 0.6 | 4.3 | 0.59 | 0.75 | 0.59 | 50.3 |
| 3 u U | 1 | 1 | 1 | 100.0 | 0.117 | 18.3 | LOS B | 0.6 | 4.3 | 0.59 | 0.75 | 0.59 | 47.4 |
| Approach | 851 | 19 | 896 | 2.2 | 0.719 | 10.7 | LOS B | 9.3 | 66.0 | 0.84 | 0.89 | 1.05 | 50.3 |
| East: Fernleigh Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 37 | 3 | 39 | 8.1 | 0.069 | 9.9 | LOS A | 0.4 | 2.7 | 0.69 | 0.74 | 0.69 | 50.3 |
| 5 T1 | 137 | 8 | 144 | 5.8 | 0.234 | 8.2 | LOS A | 1.6 | 11.5 | 0.73 | 0.76 | 0.73 | 51.8 |
| 6 R2 | 67 | 2 | 71 | 3.0 | 0.234 | 11.9 | LOS B | 1.6 | 11.5 | 0.73 | 0.76 | 0.73 | 50.8 |
| 6 u U | 1 | 0 | 1 | 0.0 | 0.234 | 13.6 | LOS B | 1.6 | 11.5 | 0.73 | 0.76 | 0.73 | 52.4 |
| Approach | 242 | 13 | 255 | 5.4 | 0.234 | 9.5 | LOS A | 1.6 | 11.5 | 0.73 | 0.75 | 0.73 | 51.3 |
| North: Pearson Street (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 81 | 1 | 85 | 1.2 | 0.368 | 6.9 | LOS A | 2.7 | 19.5 | 0.68 | 0.69 | 0.68 | 51.0 |
| 8 T1 | 301 | 13 | 317 | 4.3 | 0.368 | 6.9 | LOSA | 2.7 | 19.5 | 0.68 | 0.69 | 0.68 | 52.3 |
| 9 R2 | 204 | 13 | 215 | 6.4 | 0.256 | 11.2 | LOS B | 1.6 | 11.8 | 0.65 | 0.77 | 0.65 | 49.6 |
| 9 u U | 1 | 0 | 1 | 0.0 | 0.256 | 12.9 | LOS B | 1.6 | 11.8 | 0.65 | 0.77 | 0.65 | 49.7 |
| Approach | 587 | 27 | 618 | 4.6 | 0.368 | 8.4 | LOS A | 2.7 | 19.5 | 0.67 | 0.71 | 0.67 | 51.1 |
| West: Fernleigh Road (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 257 | 11 | 271 | 4.3 | 0.432 | 10.0 | LOS A | 2.7 | 19.5 | 0.79 | 0.94 | 0.88 | 49.4 |
| 11 T1 | 216 | 12 | 227 | 5.6 | 0.481 | 9.7 | LOS A | 3.3 | 24.2 | 0.81 | 0.96 | 0.93 | 50.9 |
| 12 R2 | 99 | 5 | 104 | 5.1 | 0.481 | 13.5 | LOS B | 3.3 | 24.2 | 0.81 | 0.96 | 0.93 | 50.6 |
| 12 u U | 11 | 0 | 12 | 0.0 | 0.481 | 15.1 | LOS B | 3.3 | 24.2 | 0.81 | 0.96 | 0.93 | 51.4 |
| Approach | 583 | 28 | 614 | 4.8 | 0.481 | 10.6 | LOS B | 3.3 | 24.2 | 0.80 | 0.95 | 0.91 | 50.2 |
| All <br> Vehicles | 2263 | 87 | 2382 | 3.8 | 0.719 | 10.0 | LOS A | 9.3 | 66.0 | 0.78 | 0.85 | 0.88 | 50.6 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^3]
## MOVEMENT SUMMARY

© Site: [Glenfield Road / Pearson Street / Fernleigh Road - AM Peak with Construction Traffic (Site Folder: Wagga Wagga)]

Site Category: Future Conditions 1
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INF } \\ & \text { VOLし } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | UT MES HV] veh/h | $\begin{array}{r} \text { DEM } \\ \text { FLC } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service | $\begin{aligned} & 95 \% \text { Bt } \\ & \text { QUI } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \mathrm{m} \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| South: Glenfield Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 122 | 5 | 128 | 4.1 | 0.741 | 12.0 | LOS B | 10.2 | 72.8 | 0.91 | 0.97 | 1.21 | 49.2 |
| 2 T1 | 651 | 12 | 685 | 1.8 | 0.741 | 11.8 | LOS B | 10.2 | 72.8 | 0.91 | 0.97 | 1.21 | 49.5 |
| 3 R2 | 77 | 1 | 81 | 1.3 | 0.122 | 12.0 | LOS B | 0.6 | 4.5 | 0.61 | 0.76 | 0.61 | 50.1 |
| 3 u U | 2 | 1 | 2 | 50.0 | 0.122 | 16.2 | LOS B | 0.6 | 4.5 | 0.61 | 0.76 | 0.61 | 49.0 |
| Approach | 852 | 19 | 897 | 2.2 | 0.741 | 11.8 | LOS B | 10.2 | 72.8 | 0.88 | 0.95 | 1.15 | 49.5 |
| East: Fernleigh Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 37 | 3 | 39 | 8.1 | 0.071 | 10.3 | LOS B | 0.4 | 2.9 | 0.71 | 0.75 | 0.71 | 50.0 |
| 5 T1 | 137 | 8 | 144 | 5.8 | 0.242 | 8.5 | LOS A | 1.7 | 12.2 | 0.76 | 0.77 | 0.76 | 51.6 |
| 6 R2 | 67 | 2 | 71 | 3.0 | 0.242 | 12.2 | LOS B | 1.7 | 12.2 | 0.76 | 0.77 | 0.76 | 50.6 |
| 6 u U | 1 | 0 | 1 | 0.0 | 0.242 | 14.0 | LOS B | 1.7 | 12.2 | 0.76 | 0.77 | 0.76 | 52.2 |
| Approach | 242 | 13 | 255 | 5.4 | 0.242 | 9.8 | LOS A | 1.7 | 12.2 | 0.75 | 0.77 | 0.75 | 51.1 |
| North: Pearson Street ( N ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 81 | 1 | 85 | 1.2 | 0.369 | 6.9 | LOS A | 2.7 | 19.5 | 0.68 | 0.69 | 0.68 | 51.0 |
| 8 T1 | 301 | 13 | 317 | 4.3 | 0.369 | 6.9 | LOS A | 2.7 | 19.5 | 0.68 | 0.69 | 0.68 | 52.3 |
| 9 R2 | 240 | 16 | 253 | 6.7 | 0.293 | 11.3 | LOS B | 1.9 | 14.0 | 0.66 | 0.77 | 0.66 | 49.6 |
| 9 u U | 1 | 0 | 1 | 0.0 | 0.293 | 12.9 | LOS B | 1.9 | 14.0 | 0.66 | 0.77 | 0.66 | 49.7 |
| Approach | 623 | 30 | 656 | 4.8 | 0.369 | 8.6 | LOS A | 2.7 | 19.5 | 0.67 | 0.72 | 0.67 | 51.0 |
| West: Fernleigh Road (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 257 | 11 | 271 | 4.3 | 0.436 | 10.0 | LOS B | 2.7 | 19.8 | 0.80 | 0.94 | 0.89 | 49.4 |
| 11 T1 | 216 | 12 | 227 | 5.6 | 0.485 | 9.8 | LOS A | 3.4 | 24.6 | 0.82 | 0.96 | 0.94 | 50.9 |
| 12 R 2 | 99 | 5 | 104 | 5.1 | 0.485 | 13.5 | LOS B | 3.4 | 24.6 | 0.82 | 0.96 | 0.94 | 50.6 |
| 12 u U | 11 | 0 | 12 | 0.0 | 0.485 | 15.2 | LOS B | 3.4 | 24.6 | 0.82 | 0.96 | 0.94 | 51.4 |
| Approach | 583 | 28 | 614 | 4.8 | 0.485 | 10.6 | LOS B | 3.4 | 24.6 | 0.81 | 0.95 | 0.92 | 50.2 |
| All <br> Vehicles | 2300 | 90 | 2421 | 3.9 | 0.741 | 10.4 | LOS B | 10.2 | 72.8 | 0.79 | 0.87 | 0.92 | 50.3 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^4]
## SITE LAYOUT

## 目 Site: [Edward Street / Docker Street - Base - AM Peak (Site

 Folder: Wagga Wagga)]Site Category: Base Year
Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


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## PHASING SUMMARY

目 Site: [Edward Street / Docker Street - Base - AM Peak (Site
Folder: Wagga Wagga)]

Site Category: Base Year
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=90$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Leading Right Turn
Reference Phase: Phase B
Input Phase Sequence: A, B, C, D
Output Phase Sequence: A, B, C, D

Phase Timing Summary

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 75 | 0 | 27 | 55 |
| Green Time (sec) | 9 | 21 | 22 | 14 |
| Phase Time (sec) | 15 | 27 | 28 | 20 |
| Phase Split | $17 \%$ | $30 \%$ | $31 \%$ | $22 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase

| $\Rightarrow$ Normal Movement | $\Rightarrow$ Permitted/Opposed |
| :---: | :---: |
| $\Rightarrow$ Slip/Bypass-Lane Movement | Opposed Slip/Bypass-Lane |
| Stopped Movement | $\checkmark$ Turn On Red |
| Other Movement Class (MC) Running | $\Rightarrow$ Undetected Movement |
| $\Rightarrow$ Mixed Running \& Stopped MCs | $\Rightarrow$ Continuous Movement |
| $\checkmark$ Other Movement Class (MC) Stopped | - Phase Transition Applied |

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## MOVEMENT SUMMARY

## 目 Site: [Edward Street / Docker Street - Base - AM Peak (Site <br> Folder: Wagga Wagga)]

Site Category: Base Year
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 90 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | UT <br> MES HV ] veh/h |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay $\qquad$ sec | Level of Service $\qquad$ | 95\% <br> QU <br> [ Veh. veh | $\begin{aligned} & \text { CK OF } \\ & \text { UE } \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. Que | Effective Stop Rate |  | Aver. Speed $\mathrm{km} / \mathrm{h}$ |
| South: Docker Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 65 | 3 | 68 | 4.6 | 0.102 | 16.8 | LOS B | 1.1 | 8.4 | 0.71 | 0.71 | 0.71 | 43.3 |
| 2 T1 | 654 | 7 | 688 | 1.1 | * 0.924 | 53.0 | LOS D | 24.1 | 171.2 | 1.00 | 1.14 | 1.42 | 31.9 |
| 3 R2 | 177 | 4 | 186 | 2.3 | 0.924 | 59.2 | LOS E | 24.1 | 171.2 | 1.00 | 1.14 | 1.42 | 29.7 |
| Approach | 896 | 14 | 943 | 1.6 | 0.924 | 51.6 | LOS D | 24.1 | 171.2 | 0.98 | 1.10 | 1.37 | 32.1 |
| East: Edward Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 107 | 10 | 113 | 9.3 | 0.719 | 39.7 | LOS D | 13.2 | 101.9 | 0.97 | 0.87 | 1.03 | 34.5 |
| 5 T1 | 473 | 66 | 498 | 14.0 | 0.719 | 35.9 | LOS D | 13.2 | 101.9 | 0.97 | 0.88 | 1.04 | 33.4 |
| 6 R2 | 94 | 5 | 99 | 5.3 | 0.556 | 48.7 | LOS D | 4.4 | 32.2 | 1.00 | 0.78 | 1.01 | 31.1 |
| Approach | 674 | 81 | 709 | 12.0 | 0.719 | 38.3 | LOS D | 13.2 | 101.9 | 0.98 | 0.86 | 1.03 | 33.2 |
| North: Docker Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 112 | 4 | 118 | 3.6 | 0.202 | 29.5 | LOS C | 3.8 | 27.2 | 0.76 | 0.75 | 0.76 | 37.6 |
| 8 T1 | 284 | 8 | 299 | 2.8 | 0.893 | 52.2 | LOS D | 13.5 | 97.0 | 1.00 | 1.06 | 1.42 | 32.2 |
| 9 R2 | 206 | 7 | 217 | 3.4 | 0.893 | 58.2 | LOS E | 13.2 | 95.1 | 1.00 | 1.04 | 1.43 | 29.4 |
| Approach | 602 | 19 | 634 | 3.2 | 0.893 | 50.0 | LOS D | 13.5 | 97.0 | 0.96 | 0.99 | 1.30 | 32.0 |
| West: Edward Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 226 | 6 | 238 | 2.7 | * 0.919 | 55.3 | LOS E | 22.0 | 162.5 | 1.00 | 1.19 | 1.41 | 29.9 |
| 11 T1 | 562 | 60 | 592 | 10.7 | * 0.919 | 52.6 | LOS D | 22.0 | 162.5 | 1.00 | 1.18 | 1.42 | 29.0 |
| 12 R 2 | 152 | 4 | 160 | 2.6 | * 0.873 | 57.6 | LOS E | 8.1 | 58.2 | 1.00 | 1.03 | 1.46 | 29.1 |
| Approach | 940 | 70 | 989 | 7.4 | 0.919 | 54.1 | LOS D | 22.0 | 164.6 | 1.00 | 1.16 | 1.42 | 29.2 |
| All <br> Vehicles | 3112 | 184 | 3276 | 5.9 | 0.924 | 49.1 | LOS D | 24.1 | 171.2 | 0.98 | 1.05 | 1.30 | 31.4 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }_{\text {ID }}^{\text {Mov }} \text { Crossing }$ | Input Vol. <br> ped/h | Dem. Flow <br> ped/h | Aver. Delay sec $\qquad$ | Level of Service | $\begin{gathered} \text { VERAG } \\ \text { Q } \\ \text { [ Ped } \\ \text { ped } \end{gathered}$ | $\begin{gathered} \text { ACK OF } \\ \text { E } \\ \text { Dist ] } \\ m \end{gathered}$ | Prop. Que | Effective Stop Rate | Travel Time sec | Travel Dist. $\qquad$ m | Aver. Speed <br> $\mathrm{m} / \mathrm{sec}$ |
| South: Docker Street |  |  |  |  |  |  |  |  |  |  |  |
| P1 Full | 50 | 53 | 39.3 | LOS D | 0.1 | 0.1 | 0.94 | 0.94 | 211.6 | 224.0 | 1.06 |
| East: Edward Street |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 50 | 53 | 39.3 | LOS D | 0.1 | 0.1 | 0.94 | 0.94 | 208.2 | 219.6 | 1.05 |


| North: Docker Street |  |  |  |  |  |  |  |  |  |  |
| :--- | :---: | ---: | ---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| P3 | Full | 50 | 53 | 39.3 | LOS D | 0.1 | 0.1 | 0.94 | 0.94 | 208.9 |
| 220.5 | 1.06 |  |  |  |  |  |  |  |  |  |
| West: Edward | Street |  |  |  |  |  |  |  |  |  |
| P4 Full | 50 | 53 | 39.3 | LOS D | 0.1 | 0.1 | 0.94 | 0.94 | 209.6 | 221.4 |
| All | 200 | 211 | 39.3 | LOS D | 0.1 | 0.1 | 0.94 | 0.94 | 209.6 | 221.4 |
|  | 1.06 |  |  |  |  |  |  |  |  |  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## PHASING SUMMARY

目 Site: [Edward Street / Docker Street - AM Peak with
Construction \& Diversion Traffic (Site Folder: Wagga Wagga)]
Site Category: Future Conditions 1
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=130$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Leading Right Turn
Reference Phase: Phase B
Input Phase Sequence: A, B, C, D
Output Phase Sequence: A, B, C, D

Phase Timing Summary

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 106 | 0 | 35 | 82 |
| Green Time (sec) | 18 | 29 | 41 | 18 |
| Phase Time (sec) | 24 | 35 | 47 | 24 |
| Phase Split | $18 \%$ | $27 \%$ | $36 \%$ | $18 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


| $\Rightarrow$ Normal Movement | $\Rightarrow$ Permitted/Opposed |
| :---: | :---: |
| $\Rightarrow$ Slip/Bypass-Lane Movement | Opposed Slip/Bypass-Lane |
| Stopped Movement | $\checkmark$ Turn On Red |
| Other Movement Class (MC) Running | $\Rightarrow$ Undetected Movement |
| $\Rightarrow$ Mixed Running \& Stopped MCs | $\Rightarrow$ Continuous Movement |
| $\checkmark$ Other Movement Class (MC) Stopped | - Phase Transition Applied |

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## MOVEMENT SUMMARY

目 Site: [Edward Street / Docker Street - AM Peak with Construction \& Diversion Traffic (Site Folder: Wagga Wagga)]

Site Category: Future Conditions 1
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 130 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | MES HV ] veh/h | DEMAND FLOWS |  | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% BACK OF QUEUE <br> [ Veh. Dist] <br> veh m |  | Prop. Que | Effective Stop Rate | Aver. Aver. <br> No. Speed <br> Cycles <br> km/h |  |
| South: Docker Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 231 | 12 | 243 | 5.2 | 0.278 | 17.9 | LOS B | 5.5 | 40.4 | 0.66 | 0.75 | 0.66 | 42.7 |
| 2 T 1 | 905 | 11 | 953 | 1.2 | 1.034 | 119.2 | LOS F | 63.8 | 452.4 | 1.00 | 1.37 | 1.67 | 20.1 |
| 3 R2 | 177 | 4 | 186 | 2.3 | 1.034 | 122.5 | LOS F | 63.8 | 452.4 | 1.00 | 1.34 | 1.64 | 19.5 |
| Approach | 1313 | 27 | 1382 | 2.1 | 1.034 | 101.8 | LOS F | 63.8 | 452.4 | 0.94 | 1.26 | 1.49 | 22.1 |
| East: Edward Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 375 | 19 | 395 | 5.1 | * 1.042 | 130.1 | LOS F | 52.5 | 389.9 | 1.00 | 1.28 | 1.71 | 18.3 |
| 5 T1 | 473 | 66 | 498 | 14.0 | 1.042 | 128.0 | LOS F | 52.5 | 389.9 | 1.00 | 1.43 | 1.76 | 18.0 |
| 6 R2 | 94 | 5 | 99 | 5.3 | 0.401 | 60.8 | LOS E | 5.9 | 42.8 | 0.96 | 0.78 | 0.96 | 28.2 |
| Approach | 942 | 90 | 992 | 9.6 | 1.042 | 122.1 | LOS F | 52.5 | 389.9 | 1.00 | 1.30 | 1.66 | 18.8 |
| North: Docker Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 112 | 4 | 118 | 3.6 | 0.201 | 39.6 | LOS D | 5.4 | 38.7 | 0.76 | 0.76 | 0.76 | 34.1 |
| 8 T1 | 284 | 8 | 299 | 2.8 | * 1.056 | 139.5 | LOS F | 27.6 | 198.8 | 1.00 | 1.34 | 1.90 | 17.9 |
| 9 R2 | 206 | 7 | 217 | 3.4 | 1.056 | 144.5 | LOS F | 27.6 | 198.8 | 1.00 | 1.29 | 1.88 | 17.1 |
| Approach | 602 | 19 | 634 | 3.2 | 1.056 | 122.6 | LOS F | 27.6 | 198.8 | 0.96 | 1.21 | 1.68 | 19.3 |
| West: Edward Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 226 | 6 | 238 | 2.7 | 0.913 | 71.1 | LOS E | 27.7 | 204.7 | 1.00 | 1.13 | 1.28 | 26.5 |
| 11 T1 | 486 | 57 | 512 | 11.7 | 0.913 | 68.7 | LOS E | 27.7 | 204.7 | 1.00 | 1.12 | 1.30 | 25.7 |
| 12 R 2 | 249 | 13 | 262 | 5.2 | * 1.052 | 140.5 | LOS F | 26.7 | 195.4 | 1.00 | 1.29 | 1.87 | 17.3 |
| Approach | 961 | 76 | 1012 | 7.9 | 1.052 | 87.9 | LOS F | 27.7 | 204.7 | 1.00 | 1.17 | 1.44 | 23.0 |
| All <br> Vehicles | 3818 | 212 | 4019 | 5.6 | 1.056 | 106.6 | LOS F | 63.8 | 452.4 | 0.97 | 1.24 | 1.55 | 20.9 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }_{\text {ID }}^{\text {Mov }} \text { Crossing }$ | Input Vol. <br> ped/h | Dem. Flow ped/h | Aver. Delay sec | Level of AVERAGE BACK OF Service QUEUE |  |  | Prop. EffectiveQue $\begin{gathered}\text { Stop } \\ \text { Rate }\end{gathered}$ |  | Travel Time sec | Travel Dist. | Aver. Speed <br> $\mathrm{m} / \mathrm{sec}$ |
| South: Docker Street |  |  |  |  |  |  |  |  |  |  |  |
| P1 Full | 50 | 53 | 59.3 | LOSE | 0.2 | 0.2 | 0.96 | 0.96 | 231.6 | 224.0 | 0.97 |
| East: Edward Street |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 50 | 53 | 59.3 | LOS E | 0.2 | 0.2 | 0.96 | 0.96 | 228.2 | 219.6 | 0.96 |


| North: Docker Street |  |  |  |  |  |  |  |  |  |  |
| :--- | :---: | ---: | ---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| P3 | Full | 50 | 53 | 59.3 | LOS E | 0.2 | 0.2 | 0.96 | 0.96 | 228.9 |
| 220.5 | 0.96 |  |  |  |  |  |  |  |  |  |
| West: Edward | Street |  |  |  |  |  |  |  |  |  |
| P4 Full | 50 | 53 | 59.3 | LOS E | 0.2 | 0.2 | 0.96 | 0.96 | 229.6 | 221.4 |
| All | 200 | 211 | 59.3 | LOS E | 0.2 | 0.2 | 0.96 | 0.96 | 229.6 | 221.4 |
|  | 0.96 |  |  |  |  |  |  |  |  |  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## SITE LAYOUT

目 Site: [Railway Street/ Lake Albert Road - Base - AM Peak (Site
Folder: Wagga Wagga)]
Site Category: Base Year
Signals - EQUISAT (Fixed-Time/SCATS) Isolated
Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.

## Q



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## PHASING SUMMARY

Site: [Railway Street/ Lake Albert Road - Base - AM Peak (Site Folder: Wagga Wagga)]

Site Category: Base Year
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=50$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Leading Right Turn
Reference Phase: Phase B
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

Phase Timing Summary

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Phase Change Time (sec) | 35 | 0 | 23 |
| Green Time (sec) | 9 | 17 | 6 |
| Phase Time (sec) | 15 | 23 | 12 |
| Phase Split | $30 \%$ | $46 \%$ | $24 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement
Other Movement Class (MC) Running

## MOVEMENT SUMMARY

## Site: [Railway Street/ Lake Albert Road - Base - AM Peak (Site Folder: Wagga Wagga)]

Site Category: Base Year
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 50 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{gathered} \text { IN } \\ \text { VOL } \\ \text { [ Total } \\ \text { veh/h } \end{gathered}$ | UT <br> MES HV ] veh/h | $\begin{gathered} \text { DEM } \\ \text { FLC } \\ \text { [ Total } \\ \text { veh/h } \end{gathered}$ | $\begin{gathered} \text { ND } \\ \text { VS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. Satn v/c | Aver. Delay $\qquad$ sec | Level of Service | 95\% B QU [ Veh. veh | $\begin{aligned} & \text { CK OF } \\ & \text { UE } \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed $\qquad$ km/h |
| South: Lake Albert Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 113 | 9 | 119 | 8.0 | 0.738 | 23.4 | LOS C | 12.0 | 86.7 | 0.94 | 0.89 | 1.04 | 42.0 |
| 2 T1 | 864 | 20 | 909 | 2.3 | * 0.738 | 17.8 | LOS B | 12.2 | 87.4 | 0.94 | 0.88 | 1.04 | 46.1 |
| Approach | 977 | 29 | 1028 | 3.0 | 0.738 | 18.4 | LOS B | 12.2 | 87.4 | 0.94 | 0.88 | 1.04 | 45.6 |
| North: Lake Albert Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 297 | 11 | 313 | 3.7 | 0.142 | 5.2 | LOS A | 1.8 | 12.6 | 0.48 | 0.40 | 0.48 | 55.3 |
| 9 R2 | 113 | 9 | 119 | 8.0 | * 0.564 | 30.3 | LOS C | 3.0 | 22.6 | 0.99 | 0.80 | 1.05 | 37.1 |
| Approach | 410 | 20 | 432 | 4.9 | 0.564 | 12.1 | LOS B | 3.0 | 22.6 | 0.62 | 0.51 | 0.64 | 48.7 |
| West: Railway Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 113 | 9 | 119 | 8.0 | 0.748 | 28.7 | LOS C | 6.1 | 46.0 | 0.98 | 0.93 | 1.22 | 37.4 |
| 12 R 2 | 113 | 9 | 119 | 8.0 | * 0.748 | 28.7 | LOS C | 6.1 | 46.0 | 0.98 | 0.93 | 1.22 | 37.4 |
| Approach | 226 | 18 | 238 | 8.0 | 0.748 | 28.7 | LOS C | 6.1 | 46.0 | 0.98 | 0.93 | 1.22 | 37.4 |
| All <br> Vehicles | 1613 | 67 | 1698 | 4.2 | 0.748 | 18.3 | LOS B | 12.2 | 87.4 | 0.87 | 0.79 | 0.96 | 44.9 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov <br> ID Crossing | Input Vol. ped/h | Dem. <br> Flow <br> ped/h | Aver. Delay sec | Level of Service | $\begin{gathered} \text { VERAC } \\ \text { Q } \\ \text { [ Ped } \\ \text { ped } \end{gathered}$ | $\begin{aligned} & \text { ACK OF } \\ & \text { E } \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. Que | Effective Stop Rate | Travel Time sec | Travel Dist. m | Aver. Speed |
| South: Lake Albert Road |  |  |  |  |  |  |  |  |  |  |  |
| P1 Full | 50 | 53 | 19.4 | LOS B | 0.1 | 0.1 | 0.88 | 0.88 | 188.8 | 220.2 | 1.17 |
| West: Railway Street |  |  |  |  |  |  |  |  |  |  |  |
| P4 Full | 50 | 53 | 19.4 | LOS B | 0.1 | 0.1 | 0.88 | 0.88 | 181.7 | 211.0 | 1.16 |
| All <br> Pedestrians | 100 | 105 | 19.4 | LOS B | 0.1 | 0.1 | 0.88 | 0.88 | 185.2 | 215.6 | 1.16 |

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## PHASING SUMMARY

## 慁ite: [Railway Street/ Lake Albert Road - AM Peak with Construction \& Diversion Traffic (Site Folder: Wagga Wagga)]

## Site Category: Future Conditions 1

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=80$ seconds (Site User-Given Cycle Time)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Leading Right Turn
Reference Phase: Phase B
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C
Phase Timing Summary

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Phase Change Time (sec) | 43 | 0 | 26 |
| Green Time (sec) | 31 | 20 | 11 |
| Phase Time (sec) | 37 | 26 | 17 |
| Phase Split | $46 \%$ | $33 \%$ | $21 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.

## Output Phase Sequence



REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement
Oermitted/Opposed
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs
Other Movement Class (MC) Stopped

## MOVEMENT SUMMARY

## 目 Site: [Railway Street/ Lake Albert Road - AM Peak with Construction \& Diversion Traffic (Site Folder: Wagga Wagga)]

Site Category: Future Conditions 1
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=80$ seconds (Site User-Given Cycle Time)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{array}{r} \text { INP } \\ \text { VOLU } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | UT MES HV] veh/h |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay sec $\qquad$ | Level of Service | $\begin{aligned} & \text { 95\% B B } \\ & \text { QU } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed $\mathrm{km} / \mathrm{h}$ |
| South: Lake Albert Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 113 | 9 | 119 | 8.0 | 1.004 | 84.3 | LOS F | 32.9 | 237.1 | 1.00 | 1.42 | 1.85 | 24.7 |
| 2 T1 | 864 | 20 | 909 | 2.3 | * 1.004 | 78.5 | LOS E | 33.5 | 239.1 | 1.00 | 1.42 | 1.85 | 26.0 |
| Approach | 977 | 29 | 1028 | 3.0 | 1.004 | 79.1 | LOS E | 33.5 | 239.1 | 1.00 | 1.42 | 1.85 | 25.9 |
| North: Lake Albert Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 297 | 11 | 313 | 3.7 | 0.177 | 13.5 | LOS B | 3.6 | 25.7 | 0.62 | 0.51 | 0.62 | 49.1 |
| 9 R2 | 204 | 25 | 215 | 12.3 | 0.914 | 57.6 | LOS E | 10.5 | 81.2 | 1.00 | 1.05 | 1.60 | 29.0 |
| Approach | 501 | 36 | 527 | 7.2 | 0.914 | 31.4 | LOS C | 10.5 | 81.2 | 0.77 | 0.73 | 1.02 | 38.3 |
| West: Railway Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 560 | 15 | 589 | 2.7 | * 1.004 | 82.1 | LOS F | 47.8 | 345.2 | 1.00 | 1.27 | 1.78 | 24.2 |
| 12 R 2 | 113 | 9 | 119 | 8.0 | 1.004 | 82.1 | LOS F | 47.8 | 345.2 | 1.00 | 1.27 | 1.78 | 24.2 |
| Approach | 673 | 24 | 708 | 3.6 | 1.004 | 82.1 | LOS F | 47.8 | 345.2 | 1.00 | 1.27 | 1.78 | 24.2 |
| All <br> Vehicles | 2151 | 89 | 2264 | 4.1 | 1.004 | 69.0 | LOS E | 47.8 | 345.2 | 0.95 | 1.21 | 1.63 | 27.3 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Input Vol. <br> ped/h | Dem. Flow ped/h | Aver. Delay sec | Level of AVERAGE BACK OF Service QUEUE |  |  | Prop. EffectiveQueStop <br> Rate |  | Travel Time sec | Travel Dist. <br> m | Aver. <br> Speed <br> $\mathrm{m} / \mathrm{sec}$ |
| South: Lake Albert Road |  |  |  |  |  |  |  |  |  |  |  |
| P1 Full | 50 | 53 | 34.3 | LOS D | 0.1 | 0.1 | 0.93 | 0.93 | 203.7 | 220.2 | 1.08 |
| West: Railway Street |  |  |  |  |  |  |  |  |  |  |  |
| P4 Full | 50 | 53 | 34.3 | LOS D | 0.1 | 0.1 | 0.93 | 0.93 | 196.6 | 211.0 | 1.07 |
| All Pedestrians | 100 | 105 | 34.3 | LOS D | 0.1 | 0.1 | 0.93 | 0.93 | 200.1 | 215.6 | 1.08 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

Project: \Icorp.pbwan.net\ANZ\ProposalsAU\PP123xxx\PP123740_ILR_P2_RDEIS_Albul4_WIP\Master_Doc\RFT\Traffic\Temp working for Project195PercentlSIDRAITraffic count intersections.sip9

## SITE LAYOUT

© Site: [Urana Street / Bourke Street - Base - AM Peak (Site
Folder: Wagga Wagga)]
Site Category: Base Year
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


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## MOVEMENT SUMMARY

$\nabla$ Site: [Urana Street / Bourke Street - Base - AM Peak (Site Folder: Wagga Wagga)]

Site Category: Base Year
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | INPUT VOLUMES |  | DEMAND FLOWS |  |  | Aver. Delay $\qquad$ | Level of Service | 95\% BACK OF QUEUE |  | Prop. Que | Effective Stop Rate |  | Aver. Speed km/h |
| South: Bourke Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| L2 | 44 | 2 | 46 | 4.5 | 0.501 | 8.4 | LOSA | 4.2 | 30.1 | 0.81 | 0.81 | 0.87 | 48.1 |
| 2 T1 | 764 | 16 | 804 | 2.1 | 0.501 | 8.7 | LOSA | 4.2 | 30.1 | 0.81 | 0.84 | 0.88 | 52.4 |
| 3 R 2 | 70 | 1 | 74 | 1.4 | 0.501 | 13.7 | LOS B | 4.0 | 28.6 | 0.81 | 0.88 | 0.91 | 48.7 |
| $3 \mathrm{u} \quad \mathrm{U}$ | 3 | 0 | 3 | 0.0 | 0.501 | 15.6 | LOS B | 4.0 | 28.6 | 0.81 | 0.88 | 0.91 | 52.7 |
| Approach | 881 | 19 | 927 | 2.2 | 0.501 | 9.1 | LOS A | 4.2 | 30.1 | 0.81 | 0.84 | 0.88 | 51.9 |
| East: Urana Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 50 | 1 | 53 | 2.0 | 0.089 | 6.3 | LOS A | 0.4 | 2.5 | 0.52 | 0.65 | 0.52 | 49.0 |
| $5 \quad \mathrm{~T} 1$ | 207 | 5 | 218 | 2.4 | 0.478 | 5.1 | LOS A | 2.9 | 20.4 | 0.61 | 0.71 | 0.63 | 46.0 |
| 6 R2 | 260 | 2 | 274 | 0.8 | 0.478 | 9.4 | LOSA | 2.9 | 20.4 | 0.61 | 0.71 | 0.63 | 48.9 |
| $6 \mathrm{u} \quad \mathrm{U}$ | 1 | 0 | 1 | 0.0 | 0.478 | 12.7 | LOS B | 2.9 | 20.4 | 0.61 | 0.71 | 0.63 | 49.6 |
| Approach | 518 | 8 | 545 | 1.5 | 0.478 | 7.4 | LOS A | 2.9 | 20.4 | 0.60 | 0.71 | 0.62 | 47.7 |
| North: Bourke Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 80 | 2 | 84 | 2.5 | 0.213 | 5.7 | LOSA | 1.4 | 9.7 | 0.52 | 0.57 | 0.52 | 49.3 |
| 8 T1 | 274 | 6 | 288 | 2.2 | 0.213 | 5.7 | LOSA | 1.4 | 9.7 | 0.53 | 0.60 | 0.53 | 53.7 |
| 9 R2 | 89 | 2 | 94 | 2.2 | 0.213 | 10.3 | LOS B | 1.3 | 9.3 | 0.54 | 0.65 | 0.54 | 49.4 |
| 9 u U | 22 | 0 | 23 | 0.0 | 0.213 | 12.3 | LOS B | 1.3 | 9.3 | 0.54 | 0.65 | 0.54 | 53.5 |
| Approach | 465 | 10 | 489 | 2.2 | 0.213 | 6.9 | LOSA | 1.4 | 9.7 | 0.53 | 0.61 | 0.53 | 52.0 |
| West: Urana Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 259 | 3 | 273 | 1.2 | 0.400 | 7.5 | LOS A | 2.3 | 16.0 | 0.79 | 0.91 | 0.86 | 48.2 |
| 11 T1 | 211 | 4 | 222 | 1.9 | 0.426 | 8.4 | LOS A | 2.3 | 16.6 | 0.79 | 0.91 | 0.90 | 45.6 |
| 12 R 2 | 17 | 1 | 18 | 5.9 | 0.426 | 12.9 | LOS B | 2.3 | 16.6 | 0.79 | 0.91 | 0.90 | 48.3 |
| 12u U | 1 | 0 | 1 | 0.0 | 0.426 | 16.0 | LOS B | 2.3 | 16.6 | 0.79 | 0.91 | 0.90 | 49.3 |
| Approach | 488 | 8 | 514 | 1.6 | 0.426 | 8.1 | LOS A | 2.3 | 16.6 | 0.79 | 0.91 | 0.88 | 47.0 |
| All <br> Vehicles | 2352 | 45 | 2476 | 1.9 | 0.501 | 8.1 | LOS A | 4.2 | 30.1 | 0.70 | 0.78 | 0.75 | 49.9 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: [Urana Street / Bourke Street - AM Peak with Construction \& Diversion Traffic (Site Folder: Wagga Wagga)]

Site Category: Future Conditions 1
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | UT MES HV ] veh/h |  | $\begin{gathered} \text { HD } \\ \text { NS } \\ \text { HV] } \\ \% \\ \hline \end{gathered}$ | Deg. <br> Satn <br> v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \mathrm{m} \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> $\mathrm{km} / \mathrm{h}$ |
| South: Bourke Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 44 | 2 | 46 | 4.5 | 1.039 | 108.9 | LOS F | 41.4 | 295.8 | 1.00 | 2.41 | 4.51 | 20.9 |
| 2 T1 | 764 | 16 | 804 | 2.1 | 1.039 | 110.8 | LOS F | 41.4 | 295.8 | 1.00 | 2.33 | 4.40 | 21.5 |
| 3 R 2 | 70 | 1 | 74 | 1.4 | 1.039 | 118.2 | LOS F | 32.5 | 231.3 | 1.00 | 2.21 | 4.25 | 20.5 |
| $3 \mathrm{u} \quad \mathrm{U}$ | 3 | 0 | 3 | 0.0 | 1.039 | 120.1 | LOS F | 32.5 | 231.3 | 1.00 | 2.21 | 4.25 | 21.2 |
| Approach | 881 | 19 | 927 | 2.2 | 1.039 | 111.3 | LOS F | 41.4 | 295.8 | 1.00 | 2.32 | 4.40 | 21.4 |
| East: Urana Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 50 | 1 | 53 | 2.0 | 0.091 | 6.5 | LOS A | 0.4 | 2.8 | 0.55 | 0.66 | 0.55 | 48.8 |
| 5 T1 | 207 | 5 | 218 | 2.4 | 0.911 | 16.1 | LOS B | 19.6 | 139.9 | 1.00 | 1.29 | 1.73 | 40.4 |
| 6 R2 | 678 | 16 | 714 | 2.4 | 0.911 | 20.4 | LOS C | 19.6 | 139.9 | 1.00 | 1.29 | 1.73 | 42.6 |
| 6 u U | 1 | 0 | 1 | 0.0 | 0.911 | 23.7 | LOS C | 19.6 | 139.9 | 1.00 | 1.29 | 1.73 | 43.2 |
| Approach | 936 | 22 | 985 | 2.4 | 0.911 | 18.7 | LOS B | 19.6 | 139.9 | 0.98 | 1.25 | 1.67 | 42.4 |
| North: Bourke Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 425 | 15 | 447 | 3.5 | 0.375 | 5.9 | LOS A | 2.8 | 20.0 | 0.60 | 0.63 | 0.60 | 49.3 |
| 8 T1 | 274 | 6 | 288 | 2.2 | 0.375 | 6.2 | LOS A | 2.8 | 20.0 | 0.61 | 0.66 | 0.61 | 53.0 |
| 9 R2 | 89 | 2 | 94 | 2.2 | 0.375 | 10.6 | LOS B | 2.6 | 18.9 | 0.62 | 0.66 | 0.62 | 49.6 |
| 9 u U | 22 | 0 | 23 | 0.0 | 0.375 | 12.6 | LOS B | 2.6 | 18.9 | 0.62 | 0.66 | 0.62 | 53.8 |
| Approach | 810 | 23 | 853 | 2.8 | 0.375 | 6.7 | LOS A | 2.8 | 20.0 | 0.61 | 0.65 | 0.61 | 50.7 |
| West: Urana Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 259 | 3 | 273 | 1.2 | 0.548 | 14.1 | LOS B | 3.8 | 27.1 | 0.92 | 1.07 | 1.22 | 44.3 |
| 11 T1 | 211 | 4 | 222 | 1.9 | 0.621 | 18.0 | LOS B | 4.2 | 29.8 | 0.91 | 1.10 | 1.33 | 40.8 |
| 12 R 2 | 17 | 1 | 18 | 5.9 | 0.621 | 22.6 | LOS C | 4.2 | 29.8 | 0.91 | 1.10 | 1.33 | 42.9 |
| 12u U | 1 | 0 | 1 | 0.0 | 0.621 | 25.6 | LOS C | 4.2 | 29.8 | 0.91 | 1.10 | 1.33 | 43.7 |
| Approach | 488 | 8 | 514 | 1.6 | 0.621 | 16.1 | LOS B | 4.2 | 29.8 | 0.91 | 1.08 | 1.27 | 42.7 |
| All Vehicles | 3115 | 72 | 3279 | 2.3 | 1.039 | 41.4 | LOS D | 41.4 | 295.8 | 0.88 | 1.37 | 2.10 | 34.3 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## SITE LAYOUT

## $\nabla$ Site: [Urana Street /MacLeay Street - Base - AM Peak (Site

Folder: Wagga Wagga)]
Site Category: Base Year
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


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## MOVEMENT SUMMARY

$\square$ Site: [Urana Street /MacLeay Street - Base - AM Peak (Site Folder: Wagga Wagga)]

Site Category: Base Year
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | JT MES HV ] veh/h |  | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. <br> Satn <br> v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate |  | Aver. Speed <br> $\mathrm{km} / \mathrm{h}$ |
| South: MacLeay Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| L2 | 11 | 1 | 12 | 9.1 | 0.221 | 5.8 | LOS A | 1.2 | 8.8 | 0.39 | 0.56 | 0.39 | 48.8 |
| 2 T1 | 196 | 16 | 206 | 8.2 | 0.221 | 5.9 | LOS A | 1.2 | 8.8 | 0.39 | 0.56 | 0.39 | 53.2 |
| 3 R 2 | 18 | 1 | 19 | 5.6 | 0.221 | 9.1 | LOS A | 1.2 | 8.8 | 0.39 | 0.56 | 0.39 | 49.5 |
| 3 u U | 1 | 0 | 1 | 0.0 | 0.221 | 10.6 | LOS B | 1.2 | 8.8 | 0.39 | 0.56 | 0.39 | 53.7 |
| Approach | 226 | 18 | 238 | 8.0 | 0.221 | 6.2 | LOSA | 1.2 | 8.8 | 0.39 | 0.56 | 0.39 | 52.7 |
| East: Lord Baden Powell Drive |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 12 | 0 | 13 | 0.0 | 0.129 | 4.9 | LOS A | 0.7 | 5.0 | 0.41 | 0.59 | 0.41 | 48.2 |
| 5 T1 | 51 | 1 | 54 | 2.0 | 0.129 | 4.9 | LOS A | 0.7 | 5.0 | 0.41 | 0.59 | 0.41 | 46.0 |
| 6 R2 | 66 | 1 | 69 | 1.5 | 0.129 | 8.1 | LOS A | 0.7 | 5.0 | 0.41 | 0.59 | 0.41 | 48.7 |
| 6 u U | 1 | 0 | 1 | 0.0 | 0.129 | 10.9 | LOS B | 0.7 | 5.0 | 0.41 | 0.59 | 0.41 | 49.2 |
| Approach | 130 | 2 | 137 | 1.5 | 0.129 | 6.6 | LOS A | 0.7 | 5.0 | 0.41 | 0.59 | 0.41 | 47.5 |
| North: MacLeay St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 39 | 3 | 41 | 7.7 | 0.195 | 5.2 | LOS A | 1.1 | 8.4 | 0.27 | 0.53 | 0.27 | 48.9 |
| 8 T1 | 133 | 11 | 140 | 8.3 | 0.195 | 5.3 | LOS A | 1.1 | 8.4 | 0.27 | 0.53 | 0.27 | 53.3 |
| 9 R2 | 44 | 4 | 46 | 9.1 | 0.195 | 8.6 | LOSA | 1.1 | 8.4 | 0.27 | 0.53 | 0.27 | 49.6 |
| 9 u U | 11 | 1 | 12 | 9.1 | 0.195 | 10.2 | LOS B | 1.1 | 8.4 | 0.27 | 0.53 | 0.27 | 53.4 |
| Approach | 227 | 19 | 239 | 8.4 | 0.195 | 6.2 | LOS A | 1.1 | 8.4 | 0.27 | 0.53 | 0.27 | 51.8 |
| West: Urana Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 65 | 1 | 68 | 1.5 | 0.132 | 5.5 | LOS A | 0.7 | 5.0 | 0.49 | 0.58 | 0.49 | 48.8 |
| 11 T1 | 53 | 1 | 56 | 1.9 | 0.132 | 5.4 | LOS A | 0.7 | 5.0 | 0.49 | 0.58 | 0.49 | 46.5 |
| 12 R 2 | 4 | 0 | 4 | 0.0 | 0.132 | 8.6 | LOS A | 0.7 | 5.0 | 0.49 | 0.58 | 0.49 | 49.4 |
| 12u U | 1 | 0 | 1 | 0.0 | 0.132 | 11.4 | LOS B | 0.7 | 5.0 | 0.49 | 0.58 | 0.49 | 49.9 |
| Approach | 123 | 2 | 129 | 1.6 | 0.132 | 5.6 | LOS A | 0.7 | 5.0 | 0.49 | 0.58 | 0.49 | 47.8 |
| All <br> Vehicles | 706 | 41 | 743 | 5.8 | 0.221 | 6.2 | LOS A | 1.2 | 8.8 | 0.37 | 0.56 | 0.37 | 50.5 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: [Urana Street /MacLeay Street - AM Peak with Construction \& Diversion Traffic (Site Folder: Wagga Wagga)]

Site Category: Future Conditions 1
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | MES HV ] veh/h |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \hline \end{aligned}$ | Deg. <br> Satn <br> v/c | Aver. Delay <br> sec | Level of Service | 95\% B QU [ Veh. veh | $\begin{aligned} & \text { CK OF } \\ & \text { UE } \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. Que | Effective Stop Rate |  | Aver. <br> Speed <br> km/h |
| South: MacLeay Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| L2 | 11 | 1 | 12 | 9.1 | 0.235 | 6.3 | LOSA | 1.3 | 9.4 | 0.45 | 0.60 | 0.45 | 48.6 |
| 2 T1 | 196 | 16 | 206 | 8.2 | 0.235 | 6.4 | LOSA | 1.3 | 9.4 | 0.45 | 0.60 | 0.45 | 52.9 |
| 3 R 2 | 18 | 1 | 19 | 5.6 | 0.235 | 9.5 | LOSA | 1.3 | 9.4 | 0.45 | 0.60 | 0.45 | 49.3 |
| 3 u U | 1 | 0 | 1 | 0.0 | 0.235 | 11.0 | LOS B | 1.3 | 9.4 | 0.45 | 0.60 | 0.45 | 53.4 |
| Approach | 226 | 18 | 238 | 8.0 | 0.235 | 6.6 | LOS A | 1.3 | 9.4 | 0.45 | 0.60 | 0.45 | 52.4 |
| East: Lord Baden Powell Drive |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 12 | 0 | 13 | 0.0 | 0.137 | 5.3 | LOSA | 0.8 | 5.3 | 0.48 | 0.62 | 0.48 | 48.0 |
| 5 T1 | 51 | 1 | 54 | 2.0 | 0.137 | 5.4 | LOSA | 0.8 | 5.3 | 0.48 | 0.62 | 0.48 | 45.8 |
| 6 R2 | 66 | 1 | 69 | 1.5 | 0.137 | 8.5 | LOSA | 0.8 | 5.3 | 0.48 | 0.62 | 0.48 | 48.4 |
| 6 u U | 1 | 0 | 1 | 0.0 | 0.137 | 11.3 | LOS B | 0.8 | 5.3 | 0.48 | 0.62 | 0.48 | 49.0 |
| Approach | 130 | 2 | 137 | 1.5 | 0.137 | 7.0 | LOSA | 0.8 | 5.3 | 0.48 | 0.62 | 0.48 | 47.3 |
| North: MacLeay Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 39 | 3 | 41 | 7.7 | 0.248 | 5.2 | LOSA | 1.6 | 11.9 | 0.29 | 0.56 | 0.29 | 48.6 |
| 8 T1 | 133 | 11 | 140 | 8.3 | 0.248 | 5.4 | LOSA | 1.6 | 11.9 | 0.29 | 0.56 | 0.29 | 52.9 |
| 9 R2 | 107 | 12 | 113 | 11.2 | 0.248 | 8.6 | LOSA | 1.6 | 11.9 | 0.29 | 0.56 | 0.29 | 49.2 |
| 9 u U | 11 | 1 | 12 | 9.1 | 0.248 | 10.2 | LOS B | 1.6 | 11.9 | 0.29 | 0.56 | 0.29 | 53.0 |
| Approach | 290 | 27 | 305 | 9.3 | 0.248 | 6.7 | LOSA | 1.6 | 11.9 | 0.29 | 0.56 | 0.29 | 50.9 |
| West: Urana Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 512 | 7 | 539 | 1.4 | 0.597 | 7.2 | LOSA | 5.4 | 37.9 | 0.72 | 0.75 | 0.78 | 48.0 |
| 11 T1 | 53 | 1 | 56 | 1.9 | 0.597 | 7.2 | LOSA | 5.4 | 37.9 | 0.72 | 0.75 | 0.78 | 45.7 |
| 12 R 2 | 4 | 0 | 4 | 0.0 | 0.597 | 10.3 | LOS B | 5.4 | 37.9 | 0.72 | 0.75 | 0.78 | 48.5 |
| 12 u U | 1 | 0 | 1 | 0.0 | 0.597 | 13.1 | LOS B | 5.4 | 37.9 | 0.72 | 0.75 | 0.78 | 49.0 |
| Approach | 570 | 8 | 600 | 1.4 | 0.597 | 7.2 | LOSA | 5.4 | 37.9 | 0.72 | 0.75 | 0.78 | 47.7 |
| All <br> Vehicles | 1216 | 55 | 1280 | 4.5 | 0.597 | 7.0 | LOS A | 5.4 | 37.9 | 0.54 | 0.66 | 0.57 | 49.2 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## SITE LAYOUT

© Site: [Seignior Street / Broadway / Olympic Highway - Base -
PM Peak (Site Folder: Junee)]

## Peak

Site Category: Base Year
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.
$q^{N}$


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## MOVEMENT SUMMARY

$\square$ Site: [Seignior Street / Broadway / Olympic Highway - Base -
PM Peak (Site Folder: Junee)]

Peak<br>Site Category: Base Year<br>Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | UT MES HV ] veh/h |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay sec $\qquad$ | Level of Service | $\begin{aligned} & 95 \% \text { B } \\ & \text { QU } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | CK OF UE Dist] m | Prop. Que | Effective Stop Rate | $\begin{aligned} & \text { Aver. } \\ & \text { No. } \\ & \text { Cycles } \end{aligned}$ | Aver. Speed $\mathrm{km} / \mathrm{h}$ |
| South: Seignior Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 118 | 3 | 124 | 2.5 | 0.081 | 4.2 | LOSA | 0.5 | 3.3 | 0.30 | 0.39 | 0.30 | 42.7 |
| 3 R 2 | 64 | 3 | 67 | 4.7 | 0.056 | 9.8 | LOSA | 0.3 | 2.2 | 0.32 | 0.60 | 0.32 | 30.6 |
| 3 u U | 1 | 0 | 1 | 0.0 | 0.056 | 12.0 | LOS B | 0.3 | 2.2 | 0.32 | 0.60 | 0.32 | 34.6 |
| Approach | 183 | 6 | 193 | 3.3 | 0.081 | 6.2 | LOS A | 0.5 | 3.3 | 0.31 | 0.46 | 0.31 | 38.0 |
| East: Olympic Highway |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 81 | 11 | 85 | 13.6 | 0.072 | 2.8 | LOSA | 0.4 | 2.8 | 0.33 | 0.45 | 0.33 | 42.7 |
| 6 R2 | 116 | 2 | 122 | 1.7 | 0.081 | 7.5 | LOS A | 0.4 | 3.0 | 0.30 | 0.62 | 0.30 | 33.4 |
| 6 u U | 2 | 0 | 2 | 0.0 | 0.081 | 9.8 | LOSA | 0.4 | 3.0 | 0.30 | 0.62 | 0.30 | 27.6 |
| Approach | 199 | 13 | 209 | 6.5 | 0.081 | 5.6 | LOS A | 0.4 | 3.0 | 0.31 | 0.55 | 0.31 | 36.1 |
| North: Broadway |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 130 | 2 | 137 | 1.5 | 0.097 | 4.1 | LOS A | 0.5 | 3.6 | 0.21 | 0.44 | 0.21 | 37.4 |
| 8 T1 | 151 | 3 | 159 | 2.0 | 0.102 | 3.9 | LOS A | 0.6 | 3.9 | 0.20 | 0.39 | 0.20 | 43.4 |
| 9 u U | 9 | 0 | 9 | 0.0 | 0.102 | 11.6 | LOS B | 0.6 | 3.9 | 0.20 | 0.39 | 0.20 | 41.0 |
| Approach | 290 | 5 | 305 | 1.7 | 0.102 | 4.2 | LOSA | 0.6 | 3.9 | 0.21 | 0.41 | 0.21 | 41.1 |
| All <br> Vehicles | 672 | 24 | 707 | 3.6 | 0.102 | 5.2 | LOS A | 0.6 | 3.9 | 0.27 | 0.47 | 0.27 | 38.7 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

$\forall$ Site: [Seignior Street / Broadway / Olympic Highway - PM
Peak with Construction \& Diversion Traffic (Site Folder: Junee)]

## Peak

Site Category: Future Conditions 1
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { INF } \\ & \text { VOL } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | UT MES HV] veh/h |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay sec $\qquad$ | Level of Service | $\begin{aligned} & \text { 95\% B B } \\ & \text { QU } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed $\mathrm{km} / \mathrm{h}$ |
| South: Seignior Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 T 1 | 118 | 3 | 124 | 2.5 | 0.098 | 4.4 | LOS A | 0.6 | 4.0 | 0.33 | 0.41 | 0.33 | 42.3 |
| 3 R2 | 183 | 15 | 193 | 8.2 | 0.129 | 9.7 | LOS A | 0.8 | 5.8 | 0.32 | 0.60 | 0.32 | 30.5 |
| 3 u U | 1 | 0 | 1 | 0.0 | 0.129 | 11.9 | LOS B | 0.8 | 5.8 | 0.32 | 0.60 | 0.32 | 34.6 |
| Approach | 302 | 18 | 318 | 6.0 | 0.129 | 7.6 | LOS A | 0.8 | 5.8 | 0.32 | 0.52 | 0.32 | 34.8 |
| East: Olympic Highway |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 294 | 23 | 309 | 7.8 | 0.207 | 2.7 | LOS A | 1.2 | 9.3 | 0.35 | 0.46 | 0.35 | 43.2 |
| 6 R2 | 116 | 2 | 122 | 1.7 | 0.106 | 7.9 | LOS A | 0.6 | 4.0 | 0.35 | 0.63 | 0.35 | 33.2 |
| 6 u U | 2 | 0 | 2 | 0.0 | 0.106 | 10.1 | LOS B | 0.6 | 4.0 | 0.35 | 0.63 | 0.35 | 27.4 |
| Approach | 412 | 25 | 434 | 6.1 | 0.207 | 4.2 | LOS A | 1.2 | 9.3 | 0.35 | 0.51 | 0.35 | 39.1 |
| North: Broadway |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 130 | 2 | 137 | 1.5 | 0.109 | 4.6 | LOSA | 0.6 | 4.1 | 0.37 | 0.50 | 0.37 | 35.7 |
| 8 T1 | 151 | 3 | 159 | 2.0 | 0.113 | 4.4 | LOS A | 0.6 | 4.5 | 0.35 | 0.45 | 0.35 | 41.6 |
| 9 u U | 10 | 1 | 11 | 10.0 | 0.113 | 12.1 | LOS B | 0.6 | 4.5 | 0.35 | 0.45 | 0.35 | 38.9 |
| Approach | 291 | 6 | 306 | 2.1 | 0.113 | 4.7 | LOSA | 0.6 | 4.5 | 0.36 | 0.47 | 0.36 | 39.3 |
| All <br> Vehicles | 1005 | 49 | 1058 | 4.9 | 0.207 | 5.4 | LOS A | 1.2 | 9.3 | 0.35 | 0.50 | 0.35 | 37.6 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Project: \Icorp.pbwan.net\ANZ\ProposalsAU\PP123xxx\PP123740_ILR_P2_RDEIS_Albul4_WIP\Master_Doc\RFT\TrafficITemp working for Project195Percent|SIDRAITraffic count intersections.sip9

## SITE LAYOUT

© Site: [Peak Hour Base - 2024 (Site Folder: Bomen, Wagga)]
Site Category: (None)
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


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## MOVEMENT SUMMARY

## 8 Site: [Peak Hour Base - 2024 (Site Folder: Bomen, Wagga)]

Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | INPUT VOLUMES |  | DEMAND FLOWS |  | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% BACK OF QUEUE |  | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed |
| SouthEast: E Bomen Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 8 | 37.0 | 8 | 37.0 | 0.029 | 4.3 | LOS A | 0.1 | 1.3 | 0.33 | 0.46 | 0.33 | 53.7 |
| 2 T1 | 14 | 37.0 | 15 | 37.0 | 0.029 | 4.2 | LOS A | 0.1 | 1.3 | 0.33 | 0.46 | 0.33 | 55.8 |
| 3 R2 | 8 | 37.0 | 8 | 37.0 | 0.029 | 10.5 | LOS B | 0.1 | 1.3 | 0.33 | 0.46 | 0.33 | 55.5 |
| Approach | 30 | 37.0 | 32 | 37.0 | 0.029 | 5.9 | LOS A | 0.1 | 1.3 | 0.33 | 0.46 | 0.33 | 55.1 |
| NorthEast: Byrnes Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 32 | 31.0 | 34 | 31.0 | 0.124 | 4.2 | LOS A | 0.6 | 5.7 | 0.33 | 0.47 | 0.33 | 53.9 |
| 5 T1 | 72 | 31.0 | 76 | 31.0 | 0.124 | 4.1 | LOSA | 0.6 | 5.7 | 0.33 | 0.47 | 0.33 | 56.0 |
| 6 R2 | 32 | 31.0 | 34 | 31.0 | 0.124 | 10.4 | LOS B | 0.6 | 5.7 | 0.33 | 0.47 | 0.33 | 55.9 |
| Approach | 136 | 31.0 | 143 | 31.0 | 0.124 | 5.6 | LOS A | 0.6 | 5.7 | 0.33 | 0.47 | 0.33 | 55.4 |
| NorthWest: Merino Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 32 | 37.0 | 34 | 37.0 | 0.113 | 4.2 | LOSA | 0.6 | 5.3 | 0.31 | 0.46 | 0.31 | 53.8 |
| 8 T1 | 58 | 37.0 | 61 | 37.0 | 0.113 | 4.1 | LOS A | 0.6 | 5.3 | 0.31 | 0.46 | 0.31 | 55.9 |
| 9 R2 | 32 | 37.0 | 34 | 37.0 | 0.113 | 10.4 | LOS B | 0.6 | 5.3 | 0.31 | 0.46 | 0.31 | 55.6 |
| Approach | 122 | 37.0 | 128 | 37.0 | 0.113 | 5.8 | LOS A | 0.6 | 5.3 | 0.31 | 0.46 | 0.31 | 55.2 |
| SouthWest: Byrnes Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 32 | 31.0 | 34 | 31.0 | 0.112 | 3.8 | LOS A | 0.6 | 5.1 | 0.21 | 0.42 | 0.21 | 54.4 |
| 11 T1 | 72 | 31.0 | 76 | 31.0 | 0.112 | 3.6 | LOS A | 0.6 | 5.1 | 0.21 | 0.42 | 0.21 | 56.5 |
| 12 R 2 | 32 | 31.0 | 34 | 31.0 | 0.112 | 9.9 | LOSA | 0.6 | 5.1 | 0.21 | 0.42 | 0.21 | 56.4 |
| Approach | 136 | 31.0 | 143 | 31.0 | 0.112 | 5.2 | LOSA | 0.6 | 5.1 | 0.21 | 0.42 | 0.21 | 56.0 |
| All Vehicles | 424 | 33.2 | 446 | 33.2 | 0.124 | 5.5 | LOS A | 0.6 | 5.7 | 0.29 | 0.45 | 0.29 | 55.5 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

$\square$ Site: [Peak Hour Base w/ construction - 2024 (Site Folder: Bomen, Wagga)]

Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{array}{r} \text { INF } \\ \text { VOLI } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | MES <br> HV ] <br> \% |  | $\begin{aligned} & \text { AND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \mathrm{m} \end{gathered}$ | Prop. Que | Effective Stop Rate |  | Aver. Speed <br> km/h |
| SouthEast: E Bomen Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 8 | 37.0 | 8 | 37.0 | 0.030 | 4.7 | LOSA | 0.1 | 1.4 | 0.40 | 0.49 | 0.40 | 53.4 |
| 2 T1 | 14 | 37.0 | 15 | 37.0 | 0.030 | 4.6 | LOSA | 0.1 | 1.4 | 0.40 | 0.49 | 0.40 | 55.5 |
| 3 R2 | 8 | 37.0 | 8 | 37.0 | 0.030 | 10.9 | LOS B | 0.1 | 1.4 | 0.40 | 0.49 | 0.40 | 55.2 |
| Approach | 30 | 37.0 | 32 | 37.0 | 0.030 | 6.3 | LOS A | 0.1 | 1.4 | 0.40 | 0.49 | 0.40 | 54.8 |
| NorthEast: Byrnes Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 32 | 31.0 | 34 | 31.0 | 0.133 | 4.7 | LOSA | 0.7 | 6.2 | 0.42 | 0.51 | 0.42 | 53.6 |
| 5 T1 | 72 | 31.0 | 76 | 31.0 | 0.133 | 4.6 | LOSA | 0.7 | 6.2 | 0.42 | 0.51 | 0.42 | 55.6 |
| $6 \quad \mathrm{R} 2$ | 32 | 31.0 | 34 | 31.0 | 0.133 | 10.9 | LOS B | 0.7 | 6.2 | 0.42 | 0.51 | 0.42 | 55.5 |
| Approach | 136 | 31.0 | 143 | 31.0 | 0.133 | 6.1 | LOSA | 0.7 | 6.2 | 0.42 | 0.51 | 0.42 | 55.0 |
| NorthWest: Merino Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 32 | 37.0 | 34 | 37.0 | 0.173 | 4.3 | LOSA | 0.9 | 8.6 | 0.33 | 0.53 | 0.33 | 52.7 |
| 8 T1 | 58 | 37.0 | 61 | 37.0 | 0.173 | 4.1 | LOSA | 0.9 | 8.6 | 0.33 | 0.53 | 0.33 | 54.7 |
| 9 R2 | 100 | 37.0 | 105 | 37.0 | 0.173 | 10.5 | LOS B | 0.9 | 8.6 | 0.33 | 0.53 | 0.33 | 54.5 |
| Approach | 190 | 37.0 | 200 | 37.0 | 0.173 | 7.5 | LOS A | 0.9 | 8.6 | 0.33 | 0.53 | 0.33 | 54.2 |
| SouthWest: Byrnes Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 40 | 31.0 | 42 | 31.0 | 0.118 | 3.8 | LOSA | 0.6 | 5.5 | 0.21 | 0.42 | 0.21 | 54.5 |
| 11 T1 | 72 | 31.0 | 76 | 31.0 | 0.118 | 3.6 | LOSA | 0.6 | 5.5 | 0.21 | 0.42 | 0.21 | 56.6 |
| 12 R 2 | 32 | 31.0 | 34 | 31.0 | 0.118 | 9.9 | LOSA | 0.6 | 5.5 | 0.21 | 0.42 | 0.21 | 56.5 |
| Approach | 144 | 31.0 | 152 | 31.0 | 0.118 | 5.1 | LOSA | 0.6 | 5.5 | 0.21 | 0.42 | 0.21 | 56.0 |
| All <br> Vehicles | 500 | 33.6 | 526 | 33.6 | 0.173 | 6.3 | LOS A | 0.9 | 8.6 | 0.32 | 0.49 | 0.32 | 55.0 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.


[^0]:    Source: https://roadsafety.transport.nsw.gov.au/statistics/interactivecrashstats

[^1]:    
    
    
     S45. 645 ${ }^{668}$
    
    
    
    
    
    800.500
    
    
    

[^2]:    SIDRA INTERSECTION 9.0 | Copyright © 2000-2020 Akcelik and Associates Pty Ltd \| sidrasolutions.com
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[^3]:    SIDRA INTERSECTION 9.0 | Copyright © 2000-2020 Akcelik and Associates Pty Ltd \| sidrasolutions.com
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[^5]:    Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
    Pedestrian movement LOS values are based on average delay per pedestrian movement.
    Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

