## APPENDIX H. 1 TRAFFIC IMPACT ASSESSMENT ADDENDUM REPORT



# Hills of G old Wind Farm <br> Traffic and Transport Addendum 

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## Hills of Gold Wind Farm

## Traffic and Transport Addendum

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## Table of Contents

1 Introduction ..... 1
1.1 Stakeholder Submissions ..... 1
1.2 Report Structure ..... 4
2 Overview ..... 5
2.1 Updated Oversized Over Mass Route Refinement ..... 6
2.2 Traffic Generation .....  7
2.3 Traffic Modelling ..... 8
2.4 Devil's Elbow Alignment ..... 8
3 OSOM Routes ..... 9
3.1 OSOM Vehicles ..... 9
3.1.1 Altemate Route Options in Muswellbrook Local Govemment Area ..... 9
3.1.2 Revised Route in Tamworth Regional Council ..... 10
3.1.3 OSOM Traffic Generated ..... 11
4 Traffic Generation Assumptions ..... 14
4.1 Peak Period Traffic Generation ..... 14
4.1.1 Plant and Equipment and Materials ..... 14
4.1.2 Water. ..... 14
4.1.3 Construction Workers Access ..... 14
4.1.4 Bulk Earthworks ..... 15
4.2 Traffic Generation ..... 15
4.3 Site Establishment ..... 16
4.4 Construction Period ..... 16
4.5 Operational Phase ..... 17
4.6 Traffic Distribution ..... 18
5 Traffic Analysis ..... 21
5.1 Modelling ..... 21
5.2 Modelling Results ..... 10
5.3 Midblock Capacity ..... 11
5.4 Tum Treatment Analysis. ..... 14
6 Mitigation Measures ..... 17
6.1 Updated Routes ..... 17
6.2 Car Pooling ..... 17
6.3 Dedicated Construction Carpark ..... 17
transport planning
6.4 School Hours ..... 17
6.5 Additional Laybys ..... 18
6.6 Voluntary Temporary Parking Restrictions ..... 18
6.7 Pedestrian C rossing in Nundle ..... 19
6.8 Mitigation of Risks for OSOM and Heavy Vehicles ..... 20
6.9 Public Road Modific ations and Dila pidation ..... 20
6.10 Traffic Management ..... 23
7 Tamworth Regional Council ..... 26
7.1 Access During Operational Period ..... 26
7.2 Decommissioning ..... 26
7.3 Impacts on Amenity ..... 26
7.4 Project Design ..... 30
8 Muswellbrook Shire Council ..... 31
8.1 Overview ..... 31
8.2 Road Safety ..... 31
8.3 Updated Route Development. ..... 33
8.3.1 Loads Description ..... 33
8.3.2 Proposed Routes Muswellbrook ..... 35
8.3.3 Route Usage ..... 37
8.4 Existing Road Transport Environment ..... 38
8.4.1 Road Network ..... 38
8.4.2 Intersections ..... 40
8.4.3 Traffic Survey Program ..... 41
8.4.4 Midblock Traffic Volumes ..... 42
8.4.5 Traffic Contributions by the Project ..... 43
8.5 Impacts on Road Infrastructure ..... 44
8.5.1 Muswellbrook Mine Affect Roads Network Plan (Muswellbrook MARNP) ..... 44
8.5.2 Thomas Mitchell Drive Contributions Study ..... 46
8.5.3 Relevance to Hills of Gold Wind Farm ..... 46
9 Road Projects ..... 48
9.1 Overview ..... 48
9.2 Golden Highway Upgrades ..... 48
9.2.1 Belford to Golden Highway ..... 48
9.2.2 Mudies Creek Bridge ..... 50
9.3 New England Highway ..... 50
9.3.1 Camberwall ..... 50
transport planning
9.3.2 Muswellbrook Bypass ..... 50
9.4 Mitigation Strategies. ..... 51
Conclusion ..... 52
Tables
Table 1.1: Submission Responses ..... 0
Table 3.1: Proposed Oversized and Over Mass Vehicles ..... 12
Table 4.1: Site Establishment Trip Generation ..... 16
Table 4.2: Peak Construction Period (through Nundle to the Project Site) ..... 17
Table 4.3: Peak Construction Period (with shuttle service to the Project Site from Nundle) ..... 17
Table 4.4: Typical Operational Period ..... 17
Table 4.5: Higher Activity Periods ..... 18
Table 4.6: Moming Peak Traffic Distribution - Workforce and Heavy Vehic le Traffic Flows ..... 19
Table 4.7: Evening Peak Traffic Distribution - Workforce and Heavy Vehic le Traffic Flows ..... 20
Table 5.1: Levels of Service ..... 21
Table 5.2: Sidra Model Results. ..... 10
Table 5.3: Rural Road Level of Service ..... 12
Table 5.4: Environmental Capacity ..... 12
Table 5.5: Peak Construction Period Generation and V/C Ratio ..... 13
Table 5.6: Peak Construction Period Rural Road Level of Service ..... 14
Table 6.1: Summary of Proposed Road Modifications. ..... 20
Table 6.2: Muswellbrook Stakeholders Consultation ..... 25
Table 7.1: Updated Traffic Generation Estimates ..... 27
Table 8.1: Traffic by Type of Load ..... 34
Table 8.2: Estimated Route Usage ..... 37
Table 8.3: Existing Traffic Volumes (vehicles per day) ..... 42
Table 8.4: Surveyed Daily Traffic Classific ation (vehicles perday) ..... 43
Table 8.5: Comparison of Traffic Volumes (vehic les perday) ..... 43
Figures
Figure 2.1: Devil's Elbow Concept ..... 8
Figure 3.1: Proposed Route New England Highway to Project Area ..... 11
transport planning
Figure 4.1: Construction Traffic Routes from New England Highway to the Project Area ..... 18
Figure 5.1: Modelled Intersections (Tamworth ..... 22
Figure 5.2: Modelled Intersections (Nundle) ..... 23
Figure 5.3: Moming Peak Modelled Traffic Volumes (7:00am - 8:00am) Goonoo Goonoo Road and Scott Road ..... 0
Figure 5.4: Moming Peak Modelled Traffic Volumes (7:00am - 8:00am) Marius Street and Murray Street. .....  1
Figure 5.5: Moming Peak Modelled Traffic Volumes (7:00am - 8:00am) New England Highway and Nundle Road ..... 2
Figure 5.6: Moming Peak Modelled Traffic Volumes (7:00am - 8:00am) Lindsays Gap Road and Nundle Road ..... 3
Figure 5.7: Moming Peak Modelled Traffic Volumes (7:00am - 8:00am) Oa kenville Street and J enkins Street ..... 4
Figure 5.8: Evening Peak Modelled Traffic Volumes (5:00pm - 6:00pm) Goonoo Goonoo Road and Scott Road ..... 5
Figure 5.9: Evening Peak Modelled Traffic Volumes (5:00pm - 6:00pm) Murray Street and Ma rius Street ..... 6
Figure 5.10: Evening Peak Modelled Traffic Volumes(5:00pm - 6:00pm) New England Highway and Nundle Road ..... 7
Figure 5.11: Evening Peak Modelled Traffic Volumes(5:00pm - 6:00pm) New England Highway and Nundle Road ..... 8
Figure 5.12: Evening Peak Modelled Traffic Volumes (5:00pm - 6:00pm) Oakenville Street and J enkin Street. ..... 9
Figure 5.13: Morisons Gap Road and Bamy Road ..... 15
Figure 5.14: Austroads Tum Treatment Warrant ..... 16
Figure 5.15: Basic Right Tum ..... 16
Figure 6.1: Nundle Key Services. ..... 19
Figure 6.2: Road Upgrades Newcastle Port to Lindsays Gap Road ..... 22
Figure 6.3: Road Upgrade Locations LindsaysGap Road to Project Area ..... 23
Figure 7.1: Project Program ..... 28
Figure 7.2: Project Activity ..... 29
Figure 8.1: Crashes Wybong Road and Bengalla Road (2015-2020) ..... 32
Figure 8.2: Crashes Denman Road (2015 - 2020) ..... 32
Figure 8.3: Crashes Thomas Mitchell Drive (2015-2020) ..... 33
Figure 8.4: OSOM Routes ..... 36
Figure 8.5: Muswellbrook MARNP ..... 45
Figure 9.1: Golden Highway Upgrades ..... 49
Figure 9.2: Muswellbrook Bypass ..... 51

## APPENDICES

A. REXJ ANDREWS ROUTE ASSESSMENT
B. SIDRA MODEШNG OUTPUTS
C. MUSWELBROOK COUNCIL MEETING MINUTES
D. SUMMARY OF CONSULTATION AND COMMTMENTS
E. MUSWEயBRO OK SHIRE COUNCIL ASSET USTFOR ASSESSMENT
F. MUSWE BRRO OK SHIRE COUNCIL LETIER OF OFFER
transport planning

## 1 Introduction

The Transport Planning Partnership (TTPP) has been commissioned by Hills of Gold Wind Fa m Pty Ltd to prepare a response to the submissions on the Environmental Impact Statement (EIS) for the Hills of Gold Wind Farm Project (the 'Project'). This report responds directly to the submissions from key sta keholders a ddressing the issues raised and presenting revised transport routes, opportunities to minimise impacts revised traffic conditions and residual traffic impacts. It should be considered an addendum to the Traffic and Transport Impact Assessment (TTPP, 2020) presented in the EIS.

This report is also intended to be read in conjunction with:

- The updated Route Assessment prepared by RexJ Andrews (RJ A, 2021) for the transportation of the over sized and over mass vehic les (OSOM) and the Amended Project Report (ERM, 2021).
- Concept designs provided by Tumbull Eng ineering.


### 1.1 Stakeholder Submissions

Key submissions that related to traffic and transport were received from three key agency stakeholders. These were:

- Transport for NSW
- Tamworth Regional Council
- Muswellbrook Shire Council

In addition, concems raised by the Nundle and Hanging Rock communities and organisations including Nundle Business a nd Tourism Marketing Group and the Hills of Gold Preservation Inc. through their submissions and subsequent consultation held has been addressed.

The key submissions a nd the responses a re summa rised in Ta ble 1.1.

## Table 1.1: Submission Responses

| Stakeholder | Comment | Response |
| :---: | :---: | :---: |
| Muswellbrook Shire Council Submission | Traffic and Transport Study should consider the Thomas Mitc hell Drive Contributions Study and the Muswellbrook Mine Affected Roads Network Plan Review. | See Section 8 |
|  | Traffic and Transport Study should look at road safety and crashes within Muswellb rook Shire. | See Section 8 |
|  | Roads proposed are used by existing businesses including minutes and horse studs and camy high volumes of traffic during peak hour. | See Annexure D - Summary of Consultation and Commitments |
| Muswellbrook Shire Council - Issues raised in Meeting held on 31 March 2021 - Minutes provided in Annexure C. | Council requires that the Project must demonstrate diligently the full measures being taken to ensure that safety is not impacted along the proposed transport route. | Section 8 |
|  | There was deemed to be not enough information on traffic volumes and movements with the EIS. Data and information required for both the construction and operational phases. <br> Council suggested that the Mt Pleasant mine traffic data, recently published, would be a useful resource for the Project as it is the most up to date data collated on traffic movements and volumes on proposed roads. | Section 8 |
|  | Blade movements and blade volumesto be included in updated reports and issued to council for review. | Section 8 |
|  | Council expressed concem over the proposed use of Bell St Rd, citing the presence of the school at the top of the hill accommodating over 1500 students. | The Project confimed that road usage outside of restricted times such as School bus hours would all be included in the Traffic Management Plan. See Section 4 for OSOM Routes and Section 8. |
|  | Council expressed an initial preference that a single route option would be preferable for both blades and tower components. The Project discussed investigating splitting traffic to reduce impact on Bell St, Victoria St and Market St. | Section 8 |
|  | Council noted that ARTC also intend on building 3 new bridges over rail line in a similar timesc ale creating potential works conflicts. | Section 8 |


| Stakeholder | Comment | Response |
| :---: | :---: | :---: |
|  | Council noted that MACH energy also intend on camying out road upgrades at a similar time to the Projects proposed upgradescreating the possibility of works conflicts. | Section 8 |
|  | Council confirmed that they would like to see a proposed Term Sheet on road usage as well as a statement of commitments provided by the Project for review. | Appendix D |
|  | Altemative Route via Tamworth, suggested altemative to the proposal to widen bridges on Lindsays Gap Road. | Tamworth route no longer being considered. |
| Transport for NSW | Removal of signage, repositioning of light poles, erection of hard stand must be replaced or made good at Project completion. | See Section 6 |
|  | Commitment that any damage to the state road assets should be made good upon Project completion. | See Section 6 |
|  | Fig 3.12 of the TTA states that a section of median safety barier is to be removed at the intersection of MR316 and HW10. Est replacement delivery wind ow of 9 months. Provide further details of how this safety component is to be maintained due to long lead times for replacement. | Arangements for this have changed see the Rex J Andrews Route assessment report. |
|  | Further justific ation required to understand Fig 3.13 of the TTA proposing to construct a new crossover of HEX median instead of utilising existing. | Arrangements for this have changed see the Rex J Andrews Route assessment report. |
|  | Section 3.3.2 of the TTA addressing traffic generation and staff movements has not considered carpooling by staff. To be reviewed based on this option. | See Section 4 |
|  | Fig 3.2 detailing traffic routes does not appropriately labelled and connections to the New England highway to not match the description of the vehicle movements. | Figure has been corrected see Figure 4.1. |
|  | Route Assessment needsto be refreshed to take into account new road and upgrades proposed in the same time as the Projects construction. | See Section 9 |
|  | No intersection a nalysis undertaken for the indic ated routes at key loc ations on the classified roadsfor the traffic generated by the Project. All referencesto intersection a nalysis throughout the EIS and TTA are in relation to the transportation of the OSOM movements only. | See Section 5 |


| Stakeholder | Comment | Response |
| :---: | :---: | :---: |
|  | Development Application refers to roads having been previously used for other wind farm developments, however, the largest blade movement in NSW to date has been for 67 m long blades. The proposed trailer combination, extending to 92 m in length therefore has not been tested in NSW previously. | See Section 6 |
|  | If Head of the Peel road is used to camy a signific ant portion of the traffic, this road should be committed to be tarred aswell. | Head of Peel Road no longer being considered. |
| Tamworth Regional Council | There is no mention of the needs for RAV vehicle movements during operation where a blade may be needed to transport and the impact this will have had on the rehabilitation committed. | See Section 7.1 |
|  | Decommissioning would require RAV access. | See Section 7.2 |
|  | Nundle Traffic will quadruple during construction phase which will make Nundle feel busier, noisier, than the baseline environment. | See updated traffic generation in section 5 impacts on a menity in Section 7 |
|  | There is a potential for accelerated deterioration of council roadways and associated infrastructure. Project to provide commitments to make good through dila pidation surveys, management plans and use of performance bonds. | The Project hascommitted to undertake dila pidation surveys prior to use of roads a nd a nnually thereafter and post construction. The Project has committed to provide performance bonds as per the letter of offer to Ta mworth Regional Council attached in Appendix E. |
|  | There are concems around the engineering of the upgrades required to facilitate blade movement. The concem stems from a "plan-view" geometry and understates the extend of the impacted areas where there are cuttings and batters. The assessment does not consider the mec hanism for achieving the extra clearing, infrastructure relocations and land acquisition. | See Section 7. |
|  | The Head of the Peel Road upgrades require private land for upgrades and the landowner is opposed to the Project. | Head of Peel Road no longer being considered. |
|  | Provide a realistic breakdown of the percentage of traffic each of the proposed six routes is estimated to camy on a daily basis during construction and operational period. | Section 4 |
| Hills of Gold Preservation Inc (HoGPI) | Provide intersection modelling to enable the local community to understand the transport impact of the proposal on their main street. | Section 5 |


| Stakeholder | Comment | Response |
| :---: | :---: | :---: |
|  | Request to do a detailed assessment on traffic and transport based on different terrain levels. | Section 5 |
|  | Consultation held with Nundle Business and Tourism Marketing Group on the 4th of May raised concem overtraffic congestion and impacts to existing businesses, tourists and locals as a result of expected construction traffic. | Section 5 for Traffic Generation and Section 6 for Project Commitments including a parking restriction placed on construction traffic in Nundle. |
| Nundle Business and Tourism Marketing Group | Safety was raised for pedestria ns in Nundle. | Section 3 for overview of OSOM Route changes in Nundle. <br> Section 4 for Traffic generation changes on account of carpooling and reduced trucks. dedicated carpark in Nundle. <br> Section 6 for Project Commitments inc luding greater clarity on communication protocols in the Traffic Management Plan, a proposed dedicated construction carpark and temporary parking restrictions in Nundle to preserve local residents' and tourists' a menity, <br> And further safety mitigation measures including commitments to add a pedestrian crossing in Nundle, subject to a pproval of Council. |
|  | Congestion on Lindsays Gap Road into Nundle. | See updated Project Ccmmitments including adding a layby on Lindsays Gap Road. |

### 1.2 Report Structure

This report is struc tured as follows:

- Section 2-Overview of key changes to the submission.
- Section 3 - Updated Oversized and over mass vehic les routes.
- Section 4-The revised traffic generation assumptions.
- Section 5 - Revised traffic analysis and modelling results.
- Section 6 - Traffic impact mitigation measures.
- Section 7- Addresses issues raised by Tamworth Regional Council.
- Section 8 - Addresses issues raised by Muswellbrook Shire Council.
- Section 9-Identifies road upgrade Project along the OSOM routes that may impact the Project.
- Section 10-Conclusion.
transport planning


## 2 Overview

The Project has made substantial changes in response to submissions received from agencies, notably Tamworth Regional Council and Muswelbrook Shire Council) a nd key stakeholders groups, Hills of Gold Preservation Inc (HOGPI) and Nundle Business and Tourism Marketing Group through public submissions and subsequent enga gement.

The changes proposed aim to provide certainty to proposed routes, further assessment as requested and additional mitigation of residual impacts detemined through consultation. This Traffic and Transport Addendum should be read in conjunction with the Traffic and Transport Assessment (TTPP 2020) with those changes proposed in this report to supersede any conflicts.

The key updates of the Project include:

- The proposed number of wind turbine generators has been reduced from 70 to 68, however this tra ffic assessment has been based on a 'worst case' 70 wind turbine generators.
- Removal of the option to transport Oversized Overmass deliveries via Ta mworth a nd Nundle Road.
- Removal of options to transport Oversized Overmass equipment deliveries and for construction access to site via Head of the Peel Road and Crawney Road and associated transport options through Nundle residential streets including Happy Valley Road, J enkins St, Herron Street North, Gill St a nd Innes St.
- Altemate Route Options a round Muswellbrook for Oversized Ovemass equipment deliveries and greater Project commitment towards struc tural a ssessment of council a ssets a nd community safety.
- 2 xadditional laybys along Lindsay Gap Road and Morisons Gap Road for reduced tourism and commuterimpacts entering Nundle.
- Volunta ry temporary parking restrictions for construc tion workers on streets within Nundle providing key services to tourists a nd residents.
- Commitment to create a dedicated construction staff carpark prior to entering Nundle town centre which can enable the introduction of temporary parking restrictions without reducing the benefits of accessing local content for the Project, a nd could a ssist the introduction of a shuttle service for peak hour "last mile" site access to reduce traffic through Nundle, on Bamy Road and Morrison's Gap Road, if practicable.
- Improved safety commitments in Nundle with a proposed pedestrian c rossing on the comers of Oa kenville St a nd J enkins St, subject to a greement from Tamworth Regional Council.
- Greater clarity on Traffic Management Plan commitments including for residents a long Shearers Road and Morisons Gap Road for safe ingress and egress, broadercommunity
transport planning
communication initiatives, escorts for some OSOM movements along along the proposed OSOM route including Morisons Gap Road, IVMS for regular vehicles accessing the Project Site, and traffic management systems during public road upgrades.
- Geophysic al assessment, realignment and construction method consideration for the Devils Elbow Upgrade.
- Revision of the traffic generation a ssumptions and traffic management strategy to include car pooling as an initiative.
- Additional assessment and traffic modelling on key intersections in Tamworth Regional Council.
- Additional assessment and traffic modelling for Muswelbrook Oversize Overmass route options.
- Project commitments for assessment and upgrades of Muswellbrook Shire Council and Tamworth Regional Council road assets where required, subject to additional consultation.
- Inclusion of key stakeholders and communication protocols in the Traffic Management Plan for residents along the transport routes.
- The Project will provide UHF radios (given mobile phone reception can be intermittent) to residents along Morisons Gap Road and Shearers Road to communic ate any emergency or travel plans to site staff along with a protocol for reaching the site manager.
- Project Commitments to road usage fees, dila pidation surveys, and/or performance bonds for remediation works.


### 2.1 Updated Oversized Over Mass Route Refinement

The EIS assessment provided access options for oversized and over mass (OSOM) vehic les from the Port of Newcastle to the Project Area. These routes provided contingency to allow for flexibility with equipment procurement and transport contractors and due to the need for potential upgrades identified in the Route Assessment to access the Project Area.

A revised Route Assessment was undertaken by RexJ Andrews detailing the refined OSOM transport routes proposed with commentary on suitability of route and required upgrades.

The key refinements are:

- Removal of the option to transport OSOM deliveries via Tamworth and Nundle Road.
- Removal of options to transport OSOM equipment deliveries a nd for construction access to site via Head of the Peel Road and Crawney Road and associated transport options through Nundle residential streets including Happy Valley Road, J enkins St, Gill St and Innes St.
transport planning
- Altemate Route Options around Muswellbrook for OSOM equipment deliveries and greater Project commitment to wa rds struc tural assessment of council a ssets and community sa fety.

In addition, Intersection and Road Upgrade Design was undertaken in areas where signific ant upgrades were required to facilitate Project OSOM deliveries inc luding:

- The Kayuga and Wybong Road intersection in Muswellbrook Shire Council
- The Devils Elbow Upgrade on Bary Road in Ta mworth Regional Council
- The Barry Road and Morisons Gap Road intersection in Tamworth Regional Council
- The upgrades proposed along Morisons Gap Road.

These updated routes respond to consultation with Tamworth Regional Council, Transport for NSW and Muswellbrook Shire Council.

### 2.2 Traffic Generation

The generation and distribution assumptions for the Project have been updated to capture:

- Altemate routes around Muswellbrook following consultation with Muswelbrook Shire Council.
- Removal of construction access via Head of the Peel Road reducing construction related traffic to Head of Peel presented in the previous assessment.
- Traffic generation for new access a rangements a round Nundle, Hanging Rock and affected areas of Tamworth.

Despite all traffic accessing the Project Area through Bary Road and Morisons Gap Road additional mitigation commitments offera $36 \%$ reduction in forec ast daily traffic volumes compared to the previous assessment.

Revised a ssessment on routes within Muswellbrook Shire Council roads offers flexibility to select a combination of routes that respond to results of committed structural a assessments on council assets and ongoing consultation with Muswellbrook Shire following equipment selection and detailed Traffic Management Plan. For the purposes of impact assessment this report assesses the most conservative of these route options. The updated assessment is provided in Section 4 of this report.

Traffic has been estimated based on project with 70 turbines.. This has been revised to 65 turbines in the project amendment report. Traffic generated remains as a worst case without changes to account for reduced construction traffic or OSOM traffic. These volumescan be expected to be reduced but have not been updated to continue to present worst case.

### 2.3 Traffic Modelling

Further a na lysis of intersection performance has been undertaken using Sidra intersection modelling. The intersection modelling and road network a nalysis is provided in Section 5 of this report.

### 2.4 Devil's Elbow Alignment

The Devil's Elbow alignment will be subject to final detail design, following selection of construction contractor's and final Project technology and equipment. Following geophysical assessment to a ssess potential for subsurface voids relating to abandoned mine workings in the vicinity of the proposed Devil's Elbow upgrades, Tumbull Engineering have redesigned and realigned the road such that the expected void locationsidentified in the geophysic al assessment are in undisturbed a reas or a reas of fill, reducing the risk of removing earth support. The realigned road is presented in Figure 2.1.

Figure 2.1: Devil's Elbow Concept

transport planning

## 3 OSOM Routes

### 3.1 OSOM Vehicles

The EIS assessment provided access options for OSOM vehicles from the Port of Newcastle to the Project Area. These routes provided contingency to allow for flexibility with equipment procurement and transport contractors and due to the need forpotential upgrades identified in the Route Assessment to access the Project Area.

A revised Route Assessment was undertaken by RexJ Andrews detailing the refined OSOM transport routes proposed with commentary on suitability of route and required upgrades.

The key refinements are:

- Removal of the option to transport Oversized Overmass deliveries via Tamworth and Nundle Road.
- Removal of options to transport Oversized Overmassequipment deliveries a nd for construction access to site via Head of the Peel Road and Crawney Road and associated transport options through Nundle residential streets including Happy Valley Road, J enkins Street, G ill Street a nd Innes Street.
- Altemate Route Options a round Muswellbrook for Oversized Ovemass equipment deliveries and greater Project commitment towards struc tural a ssessment of council a ssets and community sa fety.

These updated routes respond to consultation with Ta mworth Regional Council, Transport for NSW and Muswellbrook Shire Council.

In addition, intersection and road upgrade design was undertaken by Tumbull Engineering in a reas where signific a nt upgrades were required including:

- The Kayuga and Wybong Road intersection in Muswelbrook Shire Council
- The Devils Elbow Upgrade on Bary Road in Ta mworth Regional Council
- The Bamy Road and MonisonsGap Road intersection in Tamworth Regional Council
- The upgrades proposed along Morrison's Gap Road.


### 3.1.1 Altemate Route Options in Muswellbrook Local Govemment Area

Following consulta tion with Muswellbrook Shire Council, a list of Council assets a long the proposed routes (provided in Appendix E Muswellbrook Shire C ouncil Asset List for Assessment) was provided to the Project. In addition, structural assessments were provided to the Project on some of these assets where available. RJ A have conducted a route survey on these route options in Muswellbrook LGA and visually inspected these assets, see Appendix A,
transport planning
and have confimed that they have used a combination of these routes in the past to transport loads in excess of those required to deliver this Project.

The Project has committed to assessing the relevant assets from the list of C ouncil Assets for safety and structural a dequacy upon final turbine equipment selection and associated transport contractor and vehic les being proposed. Any Council Asset a ssessed requiring modific ation to allow the safe transportation of Project components, including works such as strengthening, monitoring during passage, or upgrading, will be undertaken in accordance with Austroads standards and in consultation with Muswellbrook Shire Council for relevant S138 a pprovals.

Concems around traffic volumes on the Altemate Heavy Vehic le Route using Bell Street, Vic toria Street and Market Street were also raised.

Based on this feedback the Project has undertaken additional route a nalysis to create possible options to split OSOM traffic based on final volumes proposed and their frequency. This is addressed in Section 8.

### 3.1.2 Revised Route in Tamworth Regional Council

The final proposed route for OSOM movementsthrough Tamworth Regional Council is updated in Figure 3.1.

The route has been updated to remove the option to transport Oversized Overmass deliveries via Tamworth and Nundle Road. This has the benefit of reduced impact to communities to the south of Tamworth and along Nundle Road including townships such as Nemingha, Piallamore, Dungowan and Woolomin.

Figure 3.1: Proposed Route New England Highway to Project Area


The existing proposed Lindsays Gap Road forblades is now proposed for other OSOM movements.

In addition the option to transport 20\% of the Oversized Ovemass equipment deliveries and for construction access to site via Head of the Peel Road and Crawney Road and associated transport options through Nundle residential streets inc luding Happy Valley Road, J enkins St, Gill St and Innes St has been removed. This change has signific a nt benefits to residents in Nundle reducing traffic through residential streets in the town and the resident living on Head of the Peel Road.

The traffic generated due to this change is assessed in Section 4 with additional mitigation for existing road users addressed in Section 6.

These changes are a result of consultation and submissions from Ta mworth Regional Council, Transport for NSW a nd residents of Nundle a nd Hanging Rock.

### 3.1.3 OSOM Traffic Generated

An exhaustive review of the OSOM vehic le routes from the Port of Newcastle to the Project Area was undertaken by RJ A, a logistic scompany with experience in transporting wind turbine blades and components and with local experience on the proposed routes. This is
provided as a supporting document in Appendix A and should be referred to with regards to deta ils of truck dimensions and routes assessment as well as deta ils of a ditional road works required. A summary of the changes to proposed road modific ations is provided in Table 6.1 in Section 6.9.

A summary of the proposed equipment a nd vehicle types proposed from the Port of Newcastle to the Project Area is shown in in Table 3.1.

Table 3.1: Proposed Oversized and Over Mass Vehicles

| Component Type | Vehicle Types | No. of Trips to Site | Daily No. of Trips to site | Duration of Deliveries |
| :---: | :---: | :---: | :---: | :---: |
| Blades (root section) | Prime mover with $1 \times 4$ dolly with $4 \times 4$ extendable blade trailer | 210 | $0.9 \text { (2 }$ <br> WTGs/week) | 35 weeks |
| Blades (tip section)* | Prime mover with $2 \times 4-4 \times 4$ platform trailer | 70 | 0.3 | 35 weeks |
| Nacelles | Prime mover with $8 \times 8$ Platform trailer | 70 | 0.3 | 35 weeks |
| Drivetra in | Prime mover with $2 \times 8-4 \times 8$ Platform Low loader | 70 | 0.3 | 35 weeks |
| Hubs | Prime mover with $2 \times 84 \times 8$ Low Loader | 70 | 0.3 | 35 weeks |
| Tower Sections | Prime mover with 10x8 platform trailer (lower sections) <br> Prime mover with $3 \times 4-2 \times 8$ Dolly jinker (upper sections) | 490 (7 section tower) | 2.0 | 35 weeks |
| Other <br> ( $2 \times 40 f t$ Shipping Conta iner per WTG) | Prime mover with $1 \times 4-3 \times 4$ platform trailer | 140 (2 per WTG ) | 0.6 | 35 weeks |
| Sub station | Prime moverwith $1 \times 4-3 \times 4$ platform trailer | 20 | 0.1 | 10-19 months |
| Switching Station | Prime mover with $1 \times 4-3 \times 4$ platform trailer | 20 | 0.1 | 10-19 months |
| Overhead cabling | Prime mover with $1 \times 4-3 \times 4$ platform trailer | 120 | 0.5 | 10-19 months |
| Underground cabling | Prime mover with $1 \times 4-3 \times 4$ platform trailer | 20 | 0.1 | 10-19 months |
| Battery System | Standard Semi - Trailer | 158 | 2 | 35 weeks |
| Mobile concrete Batch Plant | Standard Semi - Trailer | 2 | 1 | 1 Week |
| Transformers | $2 \times$ Low Loaders | 2 | 1 | 2 Weeks |

*Blade (tip section) - these movement would only occur if bladesare split into two units. Note: Three tipscan be transported on one truck.
*The proposed number of Wind Turbine Generators has been reduced from 70 to 65 however the assessment has continued to be based on 70 Wind Turbine Generators.
transport planning
Transportation of the components isforecast to be undertaken over a period of approximately 9 months. This equates to a total of 1250-1320 OSOM movements over 9 months or an average of 5.6 movements perday assuming 6 available transport days per week.. These volumes are applicable for traffic generated for OSOM movements on parts of the New England Highway (not proposed to be detoured), Lindsay Gap Road, Nundle Road, Bary Road and Morison's Gap Road.

It should be noted that existing logging truckscreate 72 movements one-way perday and the additional impact to traffic volumes as a result of the Project's OSOM movements is not signific ant from the New England Highway to the Project Area. To provide the community with greater comfort and benefits for all road users, the Project hascommitted to three new layby passing bayson Lindsays Gap Road, Bary Road and Morisons Gap Road to further reduce impacts.

Traffic generated in Muswellbrook LGA is expected to only occuras a result of the Project OSOM movements and not general construction traffic. An updated assessment of road safety, traffic generation, consultation undertaken and the existing road transport environment is provided in Section 8.
transport planning

## 4 Traffic Generation Assumptions

### 4.1 Peak Period Traffic Generation

The following are the updated assumptions used to estimate traffic generation around the Project Area from general construction activities.

### 4.1.1 Plant and Equipment and Materials

Plant and equipment and materials are those items not included in the OSOM assessment and are carried with more commonly used transport units such as B-Doubles or Semi-trailers. Travel to the Project Area from the New England Highway is via Lindsays Gap Road, Nundle Road and then Bary Road to Morisons Gap Road.

### 4.1.2 Water

It is a ssumed that water would be transported from Tamworth on the basis that it likely represents the worst case for water transport. All trips would use Momisons Gap Road.

### 4.1.3 Construction Workers Access

It is a ssumed that the majority of construction workforce would be coming from Tamworth with a smaller percentage from otherareas. The directional plait for this assessment assumed that the routes and percentage of workers to access the Project Area would be:

- 68\%-Nundle Road from Tamworth
- 20\%-New England Highway from Tamworth, Garoo Road and Lindsay Gap Road (20\%)
- 10\% - New England Highway from the south (10\%) and Lindsay Gap Road
- $2 \%$ - Crawney Road from the Upper Hunter LGA .

Use of light vehic les would be reduced through the implementation of car pooling which is assumed to increase the average caroccupancy to 2.5 workers pervehicle.

There is little literature on the effectiveness of car pooling initiatives and each case would be different based on location and type of organisation. Given that most construction workforce are estimated to be travelling from Tamworth and the moderate commuting times it could be expected the take up of carpooling would be significant.

The Project is investigating the creation of a dedicated construction staff car park prior to entering Nundle town centre which can enable the introduction of temporary parking restrictions without reducing the benefits of accessing local content for the Project, and could assist the introduction of a shuttle service for peak hour "last mile" site access to reduce
transport planning
traffic through Nundle, on Barry Road and Morrison's Gap Road, if practicable. For more information on the proposed construction car park see Section 6.3.

### 4.1.4 Bulk Earthworks

It is assumed that earthworks would be balanced on site and there would be no need to transport soil to or from the Project Area. If not balanced, any excess spoil will likely be reused on site and thus assume no transport of spoil to or from the Project Area.

Importation of quarm material: Construction materials including gravel, aggregate and sand will be required for the construction of hardstands and turbine foundations to support Project infrastructure, including intemal ac cess roads, wind turbine generators (WTG) hardstands, laydown areas and installation of electric al cabling.

Gravel, aggregate and sand have been assumed to be sourced extemally from existing operating qua mies. There are a number of existing qua mies located within approximately 80km of the Project Area, inc luding quaries located at Tamworth, Willow Tree, Currabubula, Ardglen and on Crawney Road.

It is a ntic ipated that material from excavations will be recycled where suitable which will reduce the estimated traffic volumes upon confirmed geotechnical testing and construction procurement.

The Traffic and Transport Impact Assessment hasconsidered vehicle transport of aggregates from roads in these localities for the purposes of the traffic assessment. Construction materials will be transported to the Project Area by trucks.

### 4.2 Traffic Generation

For the purpose of this a ssessment, a vehicle trip is defined in accordance with the RTA Guide to Traffic Generating as a movement to or from the Project Area. For example a watertruck a miving at the Project Area and then leaving is two trips (one ariving and one leaving). For each of the stages identified above the estimated vehicle trips and these are provided below. Note this does not include OSOM vehicles which are considered separately.

Typic al hours are to be:

- Monday to Friday 7 am to 6 pm
- Saturday 8 am to 1 pm
- No work on Sundays or public holidays.

A traffic management plan for the Project will a lso stipulate that movement of heavy vehic les is to avoid school peaks in Nundle from 8:00am - 9:00am and 2:30pm-4:00pm weekdays. Any changes to the school bus routes ortimes will be incorporated into the latest Traffic Management Plan.

It is assumed that the evening peak traffic generation is the inverse of the moming peak. There are no expected construction traffic impacts associated with the Muswellbrook Shire Council LGA other than OSOM movements described in Section 4.

### 4.3 Site Establishment

The estimate for traffic generation during site establishment is shown in Table 4.1. A car occupancy of 2.5 people pervehicle is assumed based on the commitment to provide a car pooling scheme for the Project.

Table 4.1: Site Establishment Trip Generation

| Table Heading | Units | Moming to Site <br> (trips) | Moming from site <br> (trips) | Moming total <br> (trips) | Daily <br> (trips) |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Light vehicles | 125 workers | 50 | 0 | 50 | 100 |
| Buses | - | - | - | - | - |
| Water trucks | 11 perday | 2 | 2 | 4 | 22 |
| Trucks | 20 perday | 3 | 2 | 5 | 40 |

### 4.4 Construction Period

The following assumptions have been applied to the traffic a nd transport impact assessment:

- the peak construction workforce of 174 staff;
- that there are some people coming and going from the Project Area throughout the day however this would be substantia lly lower tha $n$ the commuter peaks.

A carpooling initiative would further reduce the number of light vehic les by a ssuming a resulting caroccupancy of 2.5 people per vehicle. Table 4.2 shows the peak construction period traffic generated through Nundle to the Project Site. Based on the proposed program the peak would occur only from month 6 to month 14. The peak trips a nd daily trips have reduced from what was presented in the EIS due to the lower estimate of workers and the car pooling initiativesthat are proposed.

Table 4.2: Peak Construction Period (through Nundle to the Project Site)

| Table Heading | Units | Moming to Site <br> (trips) | Moming from site <br> (trips) | Moming total <br> (trips) | Daily <br> (trips) |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Light vehic les | 174 workers | 70 | 15 | 85 | 155 |
| Buses | - | - | - | - | - |
| Water trucks | 15 per day | 3 | 3 | 6 | 30 |
| Trucks | 63 per day | 7 | 7 | 14 | 126 |
| Total | - | 80 | 25 | 105 | 311 |

The proposed temporary dedicated construction carpark in Nundle could facilitate the implementation of a shuttle bus service at peak times which would reduce the traffic generated from Nundle to the Project Area. The implementation of a shuttle bus service at peak times is subject to further consultation with Project stakeholders including tho rough risk a ssessments and will only be introduced if practicable. For information purposes, Table 4.3 shows the expected reduced peakconstruction period traffic generated from Nundle to the Project site if a shuttle service was implemented.

Table 4.3: Peak Construction Period (with shuttle service to the Project Site from Nundle)

| Table Heading | Units | Moming to Site <br> (trips) | Moming from site <br> (trips) | Moming total <br> (trips) | Daily <br> (trips) |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Light vehic les | 104 workers | 42 | 10 | 52 | 94 |
| Buses | 70 workers | 3 | 3 | 0 | 6 |
| Water trucks | 15 per day | 3 | 3 | 6 | 30 |
| Trucks | 63 perday | 7 | 7 | 14 | 126 |
| Total | - | 55 | 23 | 72 | 256 |

### 4.5 Operational Phase

During operations, it is estimated that there would be 14 permanent full time staff. The estimated number of trips in a typical operational period is shown in Table 4.4.

Table 4.4: Typical Operational Period

| Table Heading | Units | Moming to Site <br> (trips) | Moming from site <br> (trips) | Moming total <br> (trips) | Daily <br> (trips) |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Light vehicles | 14 workers | 14 | 0 | 14 | 28 |
| Heavy Vehic les | 2 perday | 2 | 1 | - | 4 |

At timesthere may be more staff on site formajormaintenance. Conservatively we have based the assessment on a higher activity period when there would be up to 33 staff during peak operational periods.

Table 4.5: Higher Activity Periods

| Table Heading | Units | Moming to Site <br> (trips) | Moming from site <br> (trips) | Moming total <br> (trips) | Daily <br> (trips) |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Light vehicles | 33 workers | 33 | 0 | 33 | 66 |
| Heavy Vehicles | 4 perday | 2 | 1 | - | 8 |

### 4.6 Traffic Distribution

All traffic is to access the site via Barry Road and Morisons Gap Road. The assumed traffic routes are shown in Figure 4.1. It is a ssumed that:

- $68 \%$ of traffic would use Nundle Road
- $20 \%$ of traffic would use New England Highway (from the North)
- $10 \%$ of traffic would use New England Highway (from the South)

A small proportion of $2 \%$ light vehic les are assumed to use C rawney Road south of Nundle.

Figure 4.1: Construction Traffic Routes from New England Highway to the ProjectArea


The volumes of traffic on each route are shown in Table 4.6 a nd Table 4.7 for the moming and evening peaks respectively.

Table 4.6: Moming Peak Traffic Distribution - Workforce and Heavy Vehicle Traffic Rows

| Route | Split | To Nundle (vph) | From Project Area <br> (vph) | Total (vph) |
| :--- | :---: | :---: | :---: | :---: |
| Route via Nundle <br> Road (from <br> Tamworth) | $68 \%$ |  |  |  |

Table 4.7: Evening Peak Traffic Distribution - Workforce and Heavy Vehic le Traffic Rows

| Route | Split | To Site (vph) | From Site (vph) | Total (vph) |
| :--- | :---: | :---: | :---: | :---: |
| Route via Nundle <br> Road | $68 \%$ |  |  |  |

## 5 Traffic Analysis

Transport for NSW (TfNSW) and HoGPI requested an a nalysis at key intersections. The key intersections have been modelled using the Sidra Intersection a nalysis software. Sidra modelling provides several useful indic ators to determine the level of intersection performance.

TfNSW uses the performance measure level of service (LoS), to determine how effic ient an intersection/network is operating undergiven prevailing traffic conditions. Level of service is directly related to the delays experienced by traffic tra velling through the intersection.
SIDRA's level of service ranges from Los A to Los F, with LoSA indic ating that the intersection is operating with spare capacity and LoS F indicating the intersection is operating over capacity. LoSD is the long term desirable level of service.

The criteria that Sidra intersection adopts in assessing the level of service is shown in Table 5.1.

## Table 5.1: Levels of Service

| Level of Senvice (LoS) | Average Delay per vehicle (secs/veh) | Traffic Signals, Roundabout | Give Way \& Stop Sign |
| :---: | :---: | :---: | :---: |
| A | Less than 14 | Good operation | Good operation |
| B | 15 to 28 | Good with acceptable delays and spare capacity | Acceptable delays and spare capacity |
| C | 29 to 42 | Satisfa c tory | Satisfactory, but accident study required |
| D | 43 to 56 | Nearcapacity | Nearcapacity, accident study required |
| E | 57 to 70 | At capacity; at signals inc idents would cause excessive delays. Roundabouts require other control mode | At capacity, requires other control mode |
| F | Greaterthan 70 | Unsa tisfac tory, requires additional capac ity | Unsa tisfac tory, requires other control mode ormajor treatment |

Source: RMS Guide to Traffic Generating Developments, 2002

### 5.1 Modelling

The key intersections in Ta mworth modelled included:

- Goonoo Goonoo Road (NEH) / Scott Road / Vera Street
- Murray Street / Marius Street
- New England Highway / Nundle Road

These locationshave been selected based on the volume of traffic proposed to be moving through these key intersections a nd input from TFNSW. These loc ations a re shown in Figure 5.1.

Figure 5.1: Modelled Intersections (Tamworth


In addition to these the local intersectionsat:

- Lindsays Gap Road and Nundle Road (Nundle)
- Oa kenville Street and Jenkins Street (Nundle)

These intersections are show in Figure 5.2. Both these intersections have low traffic volumes that would not normally wa rant traffic modelling and Tamworth Regional Council acknowledging in their response to the EIS that traffic volumes generated would not impact the operation of the roads.

Figure 5.2: Modelled Intersections (Nundle)


Additional traffic was added to the key intersections in accordance with the traffic distribution assumptions. The model periods were:

- 7:00am-8:00am
- 5:00pm - 6:00pm

The moming peak forconstruction traffic is expected to occurearlier than 7:00am however 7:00am - 8:00am hour waschosen in orderto be more conservative astraffic volumes before 7:00am are very low. The existing and forecast traffic volumes are shown in Figure 5.3 to Figure 5.12 for key intersections for the moming and evening peaks.

Figure 5.3: Moming Peak Modelled Traffic Volumes (7:00am - 8:00am) Goonoo Goonoo Road and Scott Road

Existing


Forecast Traffic Volumes


Figure 5.4: Moming Peak Modelled Traffic Volumes (7:00am - 8:00am) Marius Street and Muray Street


Construction Traffic


Forecast Traffic Volumes


Figure 5.5: Moming Peak Modelled Traffic Volumes (7:00am - 8:00am) New England Highway and Nundle Road

Existing


Construction Traffic


Forecast Traffic Volumes


Figure 5.6: Moming Peak Modelled Traffic Volumes (7:00am - 8:00am) Lindsays Gap Road and Nundle Road

Existing


Construction Traffic


Forecast Traffic Volumes


Figure 5.7: Moming Peak Modelled Traffic Volumes (7:00am - 8:00am) Oakenville Street and Jenkins Street
Existing


Construction Traffic


Forecast Traffic Volumes


Figure 5.8: Evening Peak Modelled Traffic Volumes (5:00pm - 6:00pm) Goonoo Goonoo Road and Scott Road


Construction Traffic


Forecast Traffic Volumes


Figure 5.9: Evening Peak Modelled Traffic Volumes (5:00pm - 6:00pm) Muray Street and Marius Street


Construction Traffic


Forecast Traffic Volumes


Figure 5.10: Evening Peak Modelled Traffic Volumes (5:00pm - 6:00pm) New England Highway and Nundle Road

Existing


Construction Traffic


Forecast Traffic Volumes


Figure 5.11: Evening Peak Modelled Traffic Volumes (5:00pm - 6:00pm) New England Highway and Nundle Road

Existing


Construction Traffic


Forecast Traffic Volumes


Figure 5.12: Evening Peak Modelled Traffic Volumes (5:00pm - 6:00pm) Oakenville Street and Jenkin Street

Existing


Construction Traffic


Forecast Traffic Volumes


### 5.2 Modelling Results

The modelling results are shown in Table 5.2. In each case the delay a nd level of service for the worst performing movement is presented as the intersection result in accordance with standard practice stipulated in the RTA Guide to Traffic Generating Developments for priority and roundabout intersections.

Table 5.2: Sidra Model Results

| Intersection | Period | Existing |  | Existing + Construction Traffic |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Ave. Delay (sec) | LoS | Ave. Delay (sec) | LoS |
| Goonoo Goonoo Road, Vera Street, Sc ott Street | Moming Peak | 13 | A | 12 | A |
|  | Evening Peak | 15 | B | 16 | B |
| Muray Street, Ma rius Street | Moming Peak | 10 | A | 10 | A |
|  | Evening Peak | 11 | A | 12 | A |
| New England Highway, Nundle Road | Moming Peak | 15 | B | 18 | B |
|  | Evening Peak | 38 | C | 44 | D |
| Lindsays Gap Road, Nundle Road | Moming Peak | 7 | A | 7 | A |
|  | Evening Peak | 7 | A | 8 | A |
| Oakenville Street, J enkins Street | Moming Peak | 6 | A | 7 | A |
|  | Evening Peak | 6 | A | 7 | A |

The modelling shows that each of the intersections modelled would perform acceptably with and without the construction traffic from the Hills of Gold Wind Farm. The poorest performing intersection was the New England Highway and Nundle Road. At this intersection the movement with the highest average delay was from the north on Railway Street. This is a minorstreet with 12 vehicles an hour on approach the average delay forthe through movement was 38 seconds in the existing case and 44 seconds in the case with the construction vehicles. The $95^{\text {th }}$ percentile queue would be less than 1 vehicle on all approaches.

Queueing at all intersections modelled was modest with $95^{\text {th }}$ percentile queues of less than 20 m at all intersections. The largest queues were modelled at the intersection of Murray Street and Marius Street.

TFNSW were partic ula ly requested the review of the impacts at the intersection of New England Highway and Nundle Road and the right tum from the New England Highway to Nundle Road in the moming peak. Modelling indic ates that the $95^{\text {th }}$ percentile queue for this right tum would increase from 1 m to 4 m (i.e. less than 1 vehic le at all times). While the queue from the worst performing approach, Railway Street, would also be less than 1 vehicle.

The modelling shows that the construction traffic would have minimal impact on the road network operation in both the moming and evening peaks.

### 5.3 Midblock Capacity

The assessment of traffic capacity has been based on the volume capacity ratio (V/C), rural road level of service and the Environmental Capacity for urban areas based on the RTA (2002) Guide to Traffic Generating Development.

The V/C ratio indic ates the level of congestion by comparing the forecast traffic volumes to the theoretical lane capacity. For this assessment, the rural roads are assumed to have a capacity of 1000 vehicles/ hour/ lane. AsV/C ratios approach 0.9 it should be expected that flow would become signific antly intemupted.

To account for overtaking, the level of service can be estimated based on the RTA Guide to Traffic Generating Developmentstable forthe rural roads this is shown in Table 5.3. This is generally applicable fortwo-way two lane rural roads with a $100 \mathrm{~km} / \mathrm{h}$ speed limit.

Table 5.3: Rural Road Level of Service

| Terrain | Level of Service | Percent of Heavy Vehicles |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 0 | 5 | 10 | 15 |
| Level | B | 630 | 590 | 560 | 530 |
|  | C | 1030 | 970 | 920 | 870 |
|  | D | 1630 | 1550 | 1480 | 1410 |
|  | E | 2630 | 2500 | 2390 | 2290 |
| Rolling | B | 500 | 420 | 360 | 310 |
|  | C | 920 | 760 | 650 | 570 |
|  | D | 1370 | 1140 | 970 | 700 |
|  | E | 2420 | 2000 | 1720 | 1510 |
| Mountainous | B | 340 | 230 | 180 | 150 |
|  | C | 600 | 410 | 320 | 260 |
|  | D | 1050 | 680 | 500 | 400 |
|  | E | 2160 | 1400 | 1040 | 820 |

Source: RTA Guide to Traffic Generating Developments
The desirable Level of Service as recommended by the RTA Guide to Traffic Generating Developments is Level of Service C.

The environmental capacity is an assessment of the impact on the a menity of an environment. The environmental capacities are estimated by considering a range of differing perceptions of traffic impacts in a particulararea. The assessment has used the tables provided in the RTA Guide to Traffic Generating Developments as shown in Ta ble 5.4.

Table 5.4: Environmental Capacity

| Road Class | Road Type | Maximum Speed <br> $(\mathbf{k m} / \mathrm{hr})$ | Maximum peak hour <br> volume <br> $(\mathrm{veh} / \mathrm{hr})$ |
| :--- | :---: | :---: | :---: |
|  | Accessway | 25 | 100 |
|  | Street | 40 | 200 environmental goal |
| Collector | Street | 50 | 300 maximum |

Source: RTA Guide to Traffic Generating Developments

The traffic impacts during construction have been analysed based on a scena rio without the proposed carpark and shuttle bus. The results of the analysis are shown in Table 5.5. The table presents the existing traffic volumes and corresponding Volume Capacity (V/C) ratio and the forecast traffic volumes and V/C during the construction period. The V/C ratio is the comparison of the traffic volumes to the theoretic al capacity. This a ssumes all traffic would go to Morisons Gap Road.

Table 5.5: Peak Construction Period Generation and V/C Ratio

| Road | Period | Direction | Existing Volumes |  | With Construction Volumes |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Volume (vph) | V/C | Project Generated traffic (vph) | Total Volume (vph) | V/C |
| Nundle Road (north of LindsaysGap Road) | Moming Peak | Northbound | 19 | 0.019 | 17 | 36 | 0.036 |
|  |  | Southbound | 13 | 0.013 | 54 | 67 | 0.067 |
|  | Evening Peak | Northbound | 6 | 0.006 | 54 | 60 | 0.060 |
|  |  | Southbound | 9 | 0.009 | 17 | 26 | 0.026 |
| Lindsays Gap Road | Moming Peak | Northbound | 3 | 0.003 | 24 | 27 | 0.027 |
|  |  | Southbound | 9 | 0.009 | 8 | 17 | 0.017 |
|  | Evening Peak | Northbound | 13 | 0.013 | 8 | 21 | 0.021 |
|  |  | Southbound | 5 | 0.005 | 24 | 29 | 0.029 |
| Nundle Road (between Lindsay Gap Road and Nundle) | Moming Peak | Westbound | 20 | 0.02 | 25 | 45 | 0.045 |
|  |  | Eastbound | 30 | 0.03 | 78 | 108 | 0.108 |
|  | Evening Peak | Westbound | 16 | 0.016 | 78 | 94 | 0.094 |
|  |  | Eastbound | 17 | 0.017 | 25 | 42 | 0.042 |
| From Nundle to Project Area (Oakenville Street, Ba my Rd, Momions Gap Road) | Moming Peak | Westbound | 21 | 0.021 | 25 | 46 | 0.046 |
|  |  | Eastbound | 19 | 0.019 | 80 | 99 | 0.099 |
|  | Evening Peak | Westbound | 24 | 0.024 | 80 | 104 | 0.104 |
|  |  | Eastbound | 27 | 0.027 | 25 | 52 | 0.052 |

The a nalysis indicates that the forec ast volumes would not have a signific a nt impact on the road network effic iency with V/C ratios less than 0.2 on all roads that were assessed.

The Level of Service based on the criteria in Table 5.3 is shown in Table 5.6. This is based on assuming $15 \%$ heavy vehic les, rolling terrain or mounta inous for O akenville Street (Bamy Road).

Table 5.6: Peak Construction Period Rural Road Level of Senvice

| Road | Period | Existing Volumes |  | With Construction Volumes |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Volume (vph) | Level of Service | Total Volume (vph) | Level of Service |
| Nundle Road North of Lindsays Gap Road | Moming | 32 | A | 103 | A |
|  | Evening | 15 | A | 86 | A |
| Lindsays Gap Road | Moming | 32 | A | 44 | A |
|  | Evening | 15 | A | 50 | A |
| Nundle Road | Moming | 50 | A | 153 | A |
|  | Evening | 33 | A | 136 | A |
| Oakenville Street (Bamy Road) | Moming | 40 | A | 145 | A |
|  | Evening | 51 | A | 156 | B |

The assessment shows that almost all the roads would operate at Level of Service A during the peak of construction. If we consider Oakenville Street as mountainous and includes Bary Road, then this would be revised to Level of Service B. In all cases the level of service is equal or better than the Level of Service B which is better than the recommended desirable Level of Service C.

In terms of environmental capacity, the forecast volumes would be less than the maximum 300 vehic les for collector roads and less than 200 vehicles per hour for local roads. Thus, the Project related traffic would operate within environmental capacity guidelines.

As raised in the submission by HOGPI and understood through consultation since the Nundle and Hanging Rock communities have sought to understand how the Project can commit to reduced traffic impact and increased safety. Further details are addressed in Section 6.

### 5.4 Tum Treatment Analysis

The intersection of Bary Road and Morisons Gap Road has been checked against the tum treatment wa rants provided in Austroads. Other intersections along the route are already used by heavy vehic les including the forestry trucks and assumed to be sufficiently safe. The existing intersection is shown in Figure 5.13.

Figure 5.13: Morisons Gap Road and Bamy Road


The wa rrants for tum treatments are based on the volume of traffic tuming and the conflicting movements. In the case of right tum on an undivided road the flow $Q m$ is the sum of the through movements on the major road and the left tum from the major road to the minor road. The Austroads tum wa rants are shown in Figure 5.14.

Figure 5.14: Austroads Tum Treatment Warrant


In accordance with the Austroadsa right tum bay would not be required as the right tum volumes a re estimated to be some 80 vehic les per hour and the major road traffic volumes $(Q m)$ are 5 vehic les an hour. However, any intersection requires a (BAR) basic right tum treatment.

A BAR is simply providing additional sea led shoulder at the intersection. Where the major road is sealed it is preferable that the shoulder is sealed also. As additional hard stand would be required at this intersection for the transport of the turbine blades, additional hard stand could be provided in the shoulder to facilitate a BAR treatment. The a rrangement for a typic al BAR treatment is shown in Figure 5.15.

Figure 5.15: Basic Right Tum

transport planning

## 6 Mitigation Mea sures

### 6.1 Updated Routes

Asdiscussed in this paper routes have been removed for the option to transport OSOM deliveries via Tamworth and Nundle Road and removal of options to transport OSOM equipment deliveries and for construction access to site via Head of the Peel Road and Crawney Road and associated transport options through Nundle residential streets including Happy Valley Road, J enkins Street, G ill Street and Innes Street.

### 6.2 CarPooling

The Project commits to providing that the future contractors will instigate a car pooling system for the construction workforce travelling to the Project Area. Provision of an electronic system such asa mobile phone application to match drivers with passengers would encourage this behaviour. This could be similarto a ride share applications. The benefits of a carpooling scheme would be that it reducestraffic while also benefiting workseconomically.

Car pooling is estimated to be an effective way of reducing traffic for this Project given that most workers are forecast to be travelling from Tamworth to the Project Area where there are common origins and destinations and the distances make if financially benefic ial.

### 6.3 Dedicated Construction Carpark

The Project has committed to creating a dedicated construction staff carpark prior to entering Nundle town centre. This will enable the introduction of the proposed temporary parking restrictions, detailed in Section 6.6, without reduc ing the benefits of accessing local content for the Project. This carpark could also assist the introduction of a shuttle service for peak hour "last mile" site access to reduce traffic through Nundle, on Barry Road and Morrison's Gap Road, if practicable. The location of this carpark is proposed to be within walking distance to the village of Nundle to ensure the township benefits from increased demand for loc al content services.

### 6.4 School Hours

The Traffic Management Plan for the Project will include special consideration to travelling outside school peaks. This will be for the route through Nundle and the Muswellbrook route that travels adjacent to Muswellbrook High School as well as identified school bus routes to be confirmed in the Traffic Management Plan. Nominally the hours to be avoided for heavy vehic les are 8:00am - 9:30am and 2:30pm-4:00pm around schools and at the times of school buses use routes for school pickup and drop-off.
transport planning

### 6.5 Additional Laybys

Additional laybys, one along Lindsay Gap Road and anotheron Morisons Gap Road, have been proposed to allow forpassing of slower OSOM movements. Consultation with Nundle Business and Tourism Marketing Group raised concems impacting to urist traffic entering Nundle. These measures should support reduced impact.

### 6.6 Voluntary Temporary Parking Restrictions

In the Traffic Management Plan a Code of Conduct will include temporary parking restrictions for construction workers on streets within Nundle providing key servic es to tourists a nd local residents in order to preserve the current amenity. The loc ation of these restrictions will be determined in consultation with the Nundle Business and Tourism Marketing Group and Tamworth Regional Council, but should consider the services accessed by tourists and local community on J enkins Street. The nominal times for parking restrictions in these loc ations will be 8:00am to 5:00pm Monday to Friday, subject to further consultation. An image of key services is shown in Figure 6.1.

Figure 6.1: Nundle Key Senvices


Temporary signage will be considered subject to further consultation with Ta mworth Regional Counc il and local business owners indicating no "Wind Farm Construction Parking, customers only".

### 6.7 Pedestrian C rossing in Nundle

Within Nundle, the Project commits to providing a pedestrian crossing on the comer of Oakenville Street and Jenkins Street, subject to further consultation with and approval from

Tamworth Regional Council. It is noted that there are existing pedestrian refuges at this location and a pedestrian crossing at this location will not meet the normal IfNSW warrants required for pedestrian crossings.

### 6.8 Mitigation of Risks for OSOM and Heavy Vehicles

It is acknowledged that this Project will use the largest turbine bladesto date in this area and previous bladesto use this route were 62 m . However, the state govemments policy is forthe New England area of NSW to become a Renewable Energy Zone (REZ). This means that the Hills of Gold Wind Farm is one of many Projects in this area that will contemplate using similar sized blades, or larger.

As the routes has not been used for this sized blades it is proposed that before the transportation of 'live' loads that test runs of each of the routes are completed using simulated loads that have the same height width and length. Once the route is demonstrated to be safe fortransportation, then the transport of the loads could commence.

### 6.9 Public Road Modifications and Dilapidation

The following table summarises the public road modific ations proposed in the RJ A Transport Route Assessment. The key proposed road modific ations are listed in Table 6.1.

Table 6.1: Summary of Proposed Road Modifications

| ID | Type* | Location | Work |
| :---: | :---: | :---: | :---: |
| Port to Lindsays Gap Road |  |  |  |
| $\begin{aligned} & 1- \\ & 2,14-15 \end{aligned}$ | RU | Mayfield \# 4 Port Storage Area; Mayfield \# 4 Berth; Mayfield \# 4 onto Selwyn Street | Additional hardstand required and fence relocated. |
| 27 | RU | Selwyn Street onto Industrial Drive (via George Street) | Signs need to be made removable, traffic signals relocated and additional hardstand. |
| 37 | RU | Industrial Drive onto Maitland Road | Minor alteration to concrete median strip. |
| 38 | RU | John Renshaw Drive onto the Hunter Expressway | May require additional hardstand on the Hunter Expressway. |
| 39 | RU | New England Highway onto Golden Highway at Whittingham | Modific ationsto the centre island and removable signs. |
| 40-41 | RU | Golden Highway through Jemys Pla ins village | Signs need to be made removable and additional hardstand required. |
| 42 | RU | Golden Highway to Denman Road | Additional hardstand required and signs made removable. |
| 43-44 | RU | Denman Road onto Bengalla Road | Additional hardstand required and signsmade removable. |

transport planning

| ID | Type* | Location | Work |
| :--- | :---: | :--- | :--- |
| 16 | RU | Wybong Road <br> onto Kayuga Road | Signs to be ma de remova ble, additional ha rdstand and <br> adjustment of fences on private la nd. See Tumbull <br> Engineering Report in Appendix P of the <br> Amendment Report. |
| $17-18$ | RU | Invemmein Street onto <br> Dartbrook Mine Access Road | Signs made removable and additional ha rdstand <br> inc luding culvert extension required. |
| 19 | RU | Dartbrook Road | Additional hardstand required, and signs made <br> removable. |
| 20 | RU | Dartbrook Road to New <br> England Highway | Signsto be made remova ble a nd some hardstand <br> added. |

New England Highway to Nundle via Lindsays Gap Road

| 21 | RU | New England Highway <br> and Lindsays Gap Road | Widening of hardstand a rea a nd make signs removable <br> to allow vehiclesto tum from the New England Highway. |
| :--- | :---: | :--- | :--- |
| 3 | BU | Goonoo Goonoo Creek <br> Bridge | Bridge needs widening a nd upgrading for loads with axles <br> exceeding 3.5 m. |
| 4 | RU | Middlebrook Creek Bridge | 4.5 m clearance, bridge may need upgrading. |
| 22 | Lindsays Gap Road to Nundle <br> Road | Requires some intersection widening and additional <br> hardstand, signs made removable and a power pole <br> relocation. |  |

Nundle to the Project Area via Morisons Gap Road (preferred access, 'Northern Route')

| 23 | RU | Oakenville Street and Old Hanging Rock Road | Requires fence relocation, additional hardstand removable signage and guardrail relocation. <br> Bamy Road Layover - It has been identified that an area at the base of the hill where additional road shoulder may need to be constructed to provide a staging area for trucks about to negotiate the gradient up to Hanging Rock. This would be used if multiple prime movers are required. |
| :---: | :---: | :---: | :---: |
| $24 / 25$ | RU | Nundle to Hanging Rock via Barrys Road | Bamys Road has a section of road known as the Devils Elbows. The existing hairpin comers are impassable for the blades, towers and motors. A detour of the Devils Elbow has been assessed and amended alignment proposed for all loads. The proposed concept alignment for Devil's Elbow is detailed in Appendix $P$ of the Amendment Report. <br> To the west and east of the Devils Elbows the road will need to be widened on a few comers, this would installation of laybys. <br> Bary Road Layover - It has been identified that an area at the base of the hill where additional road shoulder may need to be constructed to provide a staging area for trucks about to negotiate the gradient up to Hanging Rock. This would be used if multiple prime movers are required. |
| 26 | RU | Ba mys Road onto Momisons Gap Road | Requires additional widening and hardstand, fence relocation and removal of trees. See Tumbull Engineering Report in Appendix P of the Amendment Report. |
| 28 | RU | Morisons Gap Road | Requires upgrade with widening 5.5 m width and widening on bends and clearing vegetation on bends. The Proponent is also proposing to seal Morisons Gap Road to |


| ID | Type* | Location | Work |
| :---: | :--- | :--- | :--- |
|  |  |  | improve road safety a nd the amenity of local <br> residents. See Tumbull Engineering Report in Appendix P of <br> the Amendment Report. |

[^0]The locations of the upgrades are shown in Figure 6.2 and Figure 6.3.
Figure 6.2: Road Upgrades Newcastle Port to Lindsays Gap Road


Figure 6.3: Road Upgrade Locations Lindsays Gap Road to Project Area


In addition, the Project has committed to further assessment of Muswellbrook Shire Council listed a ssets a s per Appendix E ba sed on final equipment dimensions a nd transport contra ctor selection. Structural a ssessments will be und erta ken by the Project as required, through consultation with Muswellbrook Shire Council, and where required for safe transport. Any assets that the Project determines the need to upgrade, will be upgraded in accordance with the Austroadsdesign requirements.

The Project committed to dila pidation surveys, road usa ge fees, a nd/orperformance bonds for remedial works through Offer Letters sent to Ta mworth Regional Council and Muswellbrook Shire Council. These commitments are included in the RTS Report.

Any removal of signage, repositioning of light poles and temporary changes along the OSOM route and damage caused as a direct result of the OSOM movements will be made good as agreed with the local authority. A dilapidation survey will be undertaken along the route prior to a nd at completion of OSOM movements.

### 6.10 Traffic Management

The Project has increased its commitment to safety for ingress a nd egress to residents a long Morisons Gap Road. The Project will include a commitment in the Traffic Management Plan
(TMP) to provide escortsfor the majority of OSOM loadsalong Momisons Gap Road, including police escorts for the higher risk OSOM loads, to ensure residents a long Shearers Road and Morisons Gap Road have safe passage. A further layby has been introduced on Momisons Gap Road to manage these traffic impacts. The TMP Driver's Code of Conduct will also include a commitment that all vehicles regularly accessing the Project Area during construction are required to have In -Vehicle Monitoring Systems installed.

In addition, the Project will provide UHF radios (given mobile phone reception can be intermittent) to residents along Morisons Gap Road and Shearers Road to communic ate any emergency or travel plans to site staff along with a protocol for reaching the site manager.

Prior to OSOM component deliveries commencing on the Project, community information sessions will be held to provide information about the types of components that will be delivered to the Project Area. These will create opportunities to expla in the Project and update the community on Project delivery schedules.

Communic ation of the latest delivery schedules including expected component types, days and times and duration of deliveries will be provided to the local community. This will oc cur through:

- Website updates including fact sheets.
- Community information boards within Nundle and Hanging Rock.
- A text message service for those registered.
- A permanent community hub will be established in Nundle during construction and a local person (from within the LGA where possible) will be employed to assist in providing information about the Project inc luding transport delivery times to the community.
- Provision of major activity notices to residents a long Shearers Road and Monisons Gap Road, one week in advance.

Consultation was undertaken with businesses within Muswellbrook Shire Council based on the OSOM route proposed and input from Muswellbrook Shire Council. The Project commits to include these businesses in communic ation protocols as shown in Table 6.1.

Table 6.2: Muswellbrook Stakeholders Consultation

| Landowner | Status |
| :---: | :---: |
| Maxwell Underground Mine | Consulted |
| Mt Arthur Mine | Consulted |
| Bengalla Mine | Consulted |
| J emys Pla ins Resident | Consulted |
| Mt Pleasant Mine | Consulted |
| Mangoola Mine | Consulted |
| Dartbrook Underground Mine | Consulted |
| Coolmore Stud | Consulted |
| Da rey Wood la nds Stud | Consulted |
| J emys pla ins resident | Consulted |
| J emys pla ins resid ent | Consulted |
| J emys pla ins resident | Consulted |
| Edenglassie Stud | Consulted |
| Balmoral | Consulted |
| Tilt Renewables | Consulted |

transport planning

## 7 Tamworth Regional Council

### 7.1 Access During Operational Period

After completion of construction, there may be a requirement to transport additional blades or infrastructure to the Project Area for maintenance activities. To facilitate this, it is intended that the infrastructure that wascreated or modified to transport components to the Project Area during construction would be left available so that it can easily be reinstated if needed. This would be particularly important for the Devil's Elbow bypass which is intended to be maintained by the Project as a private road during the operation of the Project.

Maintenance of the Devils Elbow bypass would be undertaken by the Project to ensure that the infrastructure would be available if needed consistent with private landowner a greements for use of land on the transport route.

The need for additional transportation during the operational phase is assumed to be less than once a yearand more likely in the first few years of operation. Additional strategic stoc kpiling of components within the Project Area would allow further flexibility in the timing of transporting components.

### 7.2 Decommissioning

At this stage, at the end of the Project's design life, there is the possibility for the Project to have either a life extension, undergo reconditioning, or be removed as part of a decommissioning program. In the event of decommissioning, the Proponent will prepare a decommissioning management plan in consultation with DPIE. The decommissioning plan will take into consideration the status of roads and method for dismantling the turbines, noting that blades are likely to be broken into parts on site for ease of removal with standard vehic les. The Project land agreements include the provision of bank guarantees in order to sec ure the cost of removal of wind turbines and associated infrastructure at the end of the land tenure.

### 7.3 Impacts on Amenity

Additional Project commitments, inc luding reducing the number of transport options for OSOM vehic les to avoid residential streets in Nundle and Head of the Peel Road, have reduced traffic through Nundle from the earlier assessment in the EIS. See below table for details.

Estimated reduction in Peak Construction Moming and Evening Traffic and Daily traffic, through Nundle and Hanging Rock are shown in Table 7.1.

Table 7.1: Updated Traffic Generation Estimates

|  | Units | ES <br> Assessed Peak Moming and Evening to Site (tuips) | Updated Peak Moming and Evening to Site <br> (trips) | Reduction | ES <br> Assessed Daily to Site <br> (trips) | Updated Daily to Site <br> (trips) | Reduction |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Light vehicles | 174 workers | 87 | 70 | -20\% | 210 | 155 | -26\% |
| Buses |  | 4 | 0 | -100\% | 12 | 0 | -100\% |
| Water trucks | 15 perday | 3 | 3 | 0\% | 40 | 30 | -25\% |
| Trucks | 63 perday | 14 | 7 | -50\% | 240 | 126 | -48\% |
| Total | - | 108 | 80 | -26\% | 502 | 311 | -38\% |

In addition, proposal for a dedicated construction carpark and temporary construction parking restrictions in Nundle would significantly reduce the impacts to local residents and tourists on access to key services and tourist attractions. These measures are proposed in direct response to issues raised during Counciland community consultation to preserve amenity in Nundle.

The traffic analysis in Section 5 shows that the additional traffic generated by the Project would have minimal impact on the road network effic iency. In addition, the volumes forecast for the local streets would be less than the environmental capacities presented within the RTA Guide to Traffic Generating developments.

Notwithstanding the construction period will increase traffic volumes in Nundle forthe period of the construction. The a nalysis provided is for the peak of construction and not for the full construction period. Based on the program shown in Figure 7.1 the estimated peak construction a ctivity is shown in Figure 7.2. It shows that the peak construction activity is likely to last for a pproximately 6 months with periods before and after this having much lower traffic generation.

Figure 7.1: Project Program

transport planning
Figure 7.2: Project Activity

transport planning

### 7.4 Project Design

Engineering design of the Project Area and the Devils Elbow upgrade wascompleted prior to the a ssessment of biodiversity and heritage and lodgement of the EIS. The a ssessment was completed by Tumbull Engineering and undertaken in 12D (a 3D civil engineering software) to show the expected worst case development impact of earthworks and associated drainage. It is uncommon for a Project to undertake this level of assessment at this stage of the Project but given assessed complexities at Devils Elbow and on parts of the Project Area, concept design wascompleted in order to present greater detail to likely impacts and address fea sibility.

Devils Elbow bypass upgrades have since been modified slightly following site visits by short listed construc tion contractors a nd feedback from logistic s providers. It has been confirmed suitable for the types of loads being proposed.

Aspart of consultation with Ta mworth Regional Council the original engineering files were provided for assessment. An updated set of designs are including Devils Elbow, Momisons Gap Road and the intersection of Morisons Gap Road and Bamy Road.

The updated RJ A Transport assessment has optimised swept path to reduce the number of affected private landowners along the route. This has resulted in a reduction of properties affected. All works along Morisons Gap Road stay within the existing road reserve with the exception of the Barry Road intersection upgrade.

The Project has consulted all la ndowners a long the transport route and upon final equipment selection and design will seek lic enses or ea sements as required for either ha rdsta nd works or temporary blade overhang.

## 8 Muswellbrook Shire Council

### 8.1 Overview

Muswellbrook Shire Council have objected to the Project on the groundsthat the Project is to use local roads within the Muswellbrook LGA to transport the wind turbine components.

The key concemswere:

- Road Safety
- Impacts on road infrastructure
- Impact to local businesses along the proposed route.


### 8.2 Road Safety

Local roads in the Muswellbrook LGA will be used only for transporting OSOM loads to the Project Area and will not include typic al construction traffic including water trucks, aggregate trucks, and construction workers in light vehicles.

A review of the 5 yearcrash history (2015-2020) from the Centre for Road Safety identified that there have been two fatal crashesalong the route to be used for the bladesand vehic les over 5.2m. These occurred at the intersection of Bengalla Road and Wybong Road and on Denman Road.

The location of c rashes is shown in Figure 8.1, Figure 8.2 and Figure 8.3.

Figure 8.1: Crashes Wybong Road and Bengalla Road (2015-2020)


Figure 8.2: Crashes Denman Road (2015-2020)


There have also been eight crashes associated with the intersection of Thomas Mitchell Drive and the New England Highway of which three were serious and two moderate injury crashes.

Figure 8.3: Crashes Thomas Mitc hell Drive (2015-2020)


To minimise risk to road safety, all OSOM loads to be transported through Muswellbrook LGA are to be transported under traffic controllers and police escort, or as required by the relevant NHVR transport permit. Typically, these vehic les will be travelling at low speed and with advance waming given to drivers on approach. The volume of traffic generated is expected to be low on a daily basis so that risk of crashes is minimised.

It is also proposed that the Traffic Management Plan forthe transportation of OSOM will be developed to restrict the use of local roads within Muswellbrook LGA to hours outside the typic al school times and restricted to outside the hours of 10pm to 5am a long Bell Street, Market and Vic toria Street.

### 8.3 Updated Route Development

The following providesa description of the type of loads and routes to be used through Muswellbrook LGA. Asthe details of type of blades and nacelles to be used for the Project have not been fina lised, his a ssessment has considered different combinations of infrastructure that would need to be transported.

### 8.3.1 Loads Description

For this description of loads the following teminology has been adopted.

Blades- The blades being considered include single section blades and potential split blades. Split blades can be split so that the root section is transported by one truck each while three tipscan be transported on one truck.

Nacelles-Nacelles are the housing that sits on top of the towers and conta ins the power generating equipment and brakes. There are two options for nacelles to be transported. The first would be to transport the nacelle attached to the drivetra in which would reduce the number of trips but these loads are greater than 4.9 m high which will affect the a vailable routes. Altematively, they can be transported separately reducing the height and weight but doubling the number of vehicles.

Due to the restrictions in travelling through Muswellbrook the OSOM loads have been separated in three categories:

- Route 1 - Turbine Blades and heavy loads over 5.2m
- Route 2 Heavy Loadsunder 5.2m in height (excluding blades)
- Route 3 Heavy Loads over 5.2m in height (excluding blades)
- Standard loads up to 3.5 m wide and 5.2 m in height.

The estimated number of trips is desc ribed in Section 3.1.3. A further breakdown of the type of loads by categories are shown in Table 8.1.

Table 8.1: Traffic by Type of Load

|  | Turbine Blades | Heavy Loads over 5.2m in height | Heavy Loads under 5.2 m in height | Standard loads up to 3.5 m wide and 5.2 m in height |
| :---: | :---: | :---: | :---: | :---: |
| OSOM Components | Blades (root section) <br> Blades (tip section) | Hubs <br> Tower Sections <br> Transformers <br> Nacelles with Drivetrain in | Nacelle with Drivetra in Out Drivetra in | Other ( $2 \times 40 f t$ <br> Shipping <br> Conta iner per <br> WTG ) <br> Sub station <br> Switc hing Station <br> Overhead cabling <br> Underground cabling <br> Battery System <br> Mobile concrete <br> Batch Plant |
| Total Trips | 280 (210¹) | 650 (580²) | 1403 | 320 |
| Weekly Trips | 8 (6) | 18 (16) | 4 | 9 |

## Notes:

1. Reduced numbers if blades are transported as a single unit.
2. Reduced number if nacelles and drivetrains are transported separately trips are moved to the under 5.2 m category.
3. Only if na celles a nd drivetra ins are transported separately.
transport planning
It should be noted that if the nacelles are transported as single units that this would inc rease their height and require the use of the over 5.2 m route. Otherwise, they can use the under 5.2 m vehic le heights.

### 8.3.2 Proposed Routes Muswellbrook

The proposed routes through Muswellbrook are shown in Figure 8.4.
Route 1-Via Golden Highway, Denman Road, Bengalla Road, Wybong Road, Kyuga Road, Invermein Street, Stair Street, Dartbrook Road to New England Highway

Route 2 - Via New England Highway, Bell Street, Vic toria Street, New England Highway
Route 3-Via Golden Highway, Denman Road, Thomas Mitchell Drive, New England Highway, Bell Street, Vic toria Street, New England Highway

Route 4-Standard loads via New England Highway.
The Project is considering three options for route selection:

- All OSOM loads via Route 1 with standard loads using Route 4 the New England Highway.
- $100 \%$ of loads(other than blades) on Route 2 and 3 with blades using Route 1 and standard loads on Route 4.
- Splitting the loads 50/50 between Route 1 and Route 2 and 3, all blades using Route 1 and standard loads using Route 4.

Figure 8.4: OSOM Routes


### 8.3.3 Route Usage

The routes selected have been assessed and confimed suitable with the stated upgrades in the RJ A Transport Assessment for the proposed wind farm.

The final traffic volumes generated on these routes will be subject to the structural load assessment of Council Assets and further consultation with Muswellbrook Shire Council on required upgrades. This will be based on final turbine equipment, transport logistic soperators, proposed vehicles and associated weights.

The estimated worst-case traffic predictions are presented based on a range of possible scenarios including a scena rio which reduces impacts to Bell Street, Vic toria Street and Market Street by splitting the volumes between routes:

Table 8.2: Estimated Route Usage

| Option | Route 1 | Route 2 <br> (Includes <br> Bell St) | Route 3 <br> (includes <br> Bell St) | Route 4 | Totals |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Previous ElS | Total Trips | 280 | - | 1110 | 0 | 1390 |
|  | Average Weekly | 8 | - | 32 | 0 |  |
| All Heavy Loads <br> on Route 1 with <br> nomal loadson <br> Route 4. | Total Trips | 1070 | - | - | 320 | 1390 |
|  | Average Weekly | 31 | - | - | 9 | 1303 |
| 100\% Heavy Loads <br> on Route 2 and 3 | Tota I Thips | 280 | $650^{2}$ | $140^{3}$ | 320 | 1390 |
|  | Average Weekly | 8 | 192 | 43 | 9 | $140^{3}$ |

Notes:

1. Reduced numbers if blades are transported as a single unit.
2. Reduced number if nacelles and drivetrains are transported separately trips a re moved to the under 5.2 m category.
3. Only if na celles a nd drivetra ins are transported sepa rately

The transportation period for the turbine components has been forecast to occurover approximately 9 months or 35 weeks.

All route options reduce traffic proposed on the Bells St Heavy Vehicle Altemate route (Route 2 and 3) by taking advantage of the updated route 4 option for vehicles under 3.5 m wide
and 5.2 m high and options to use Route 1 for some or all of the heavy vehicles. The range in reduced volume is between 11 and 32 movements per week from the previously submitted EIS.

All trucks retuming to the Port of Newcastle would travel as standard loadsalong the New England Highway.

### 8.4 Existing Road Transport Environment

### 8.4.1 Road Network

Muswellbrook Shire Council recommended the Project assess information provided in the Mount Pleasant Optimisation Project Road Transport Assessment of December 2020 by TIPP. The following information is relevant for the Project and has been assessed in response to the Muswellbrook Shire Council submission.

The existing road network through Muswellbrook Shire Council that is proposed to be used by the Project is shown in Figure 8.5, and the key roads in the road network surrounding the site are described below.

New England Highway (Highway 9, Route A15) is a major State road and forms part of the National Land Transport Network, a defined national network of road and rail infrastructure links for which Commonwealth funding is provided to assist national and regional economic and social development. New England Highway is the main north-south link through the Hunter Region and connects Muswellbrook and Newcastle as part of its route between Hexham and the Queensland border. It is an altemative to the Pacific Highway forthe northsouth vehic ular link between Brisbane and Sydney, and as such ca mies a signific ant proportion of regional and interstate traffic movements.

Outside of the urban areas, New England Highway is generally a two-lane high standard rural highway with regular overtaking lanes, wide sealed shoulders, designated tuming lanes and a posted speed limit of 100 kilometres per hour (km/h). New England Highway is an approved B-double route. The New England Highway bypass of Scone wasopened to traffic in early 2020.

Golden Highway (Highway 27, Route B84) is also known as Meriwa Road, Jemys Pla ins Road, Putty Road and Mitchell Line of Road, and is a State road under the control of TFNSW. Golden Highway provides a road link between New England Highway at Minimbah and Newell Highway at Dubbo. It is generally a two-lane rural highway with a posted speed limit of 100 $\mathrm{km} / \mathrm{h}$ outside of urban areas. Golden Highway is an approved $B$-double route.

Denman Road (Main Road 209) is a State road that is funded by the RMS but maintained by Muswellbrook Shire Council. Denman Road forms the primary connection between the township of Denman and Muswellbrook and provides a road link between Golden Highway
and New England Highway. Outside of the urban areas, Denman Road is a two-lane rural road, with a 7 metre ( m ) wide sealed camiageway, additional sealed shoulders, and a posted speed limit of $100 \mathrm{~km} / \mathrm{h}$, reducing to $80 \mathrm{~km} / \mathrm{h}$ west of Bengalla Road. Denman Road is a designated B-double route.

Denman Road providesaccess to a number of existing mining operations via local roads such as Edderton Road and Thomas Mitchell Drive. As a result, Denman Road camies a signific a nt proportion of mine-related traffic, partic ula rly employee traffic accessing the mining operations.

Bengalla Road is a localroad under the control of Muswellbrook Shire Council and is an approved B-double route between Denman Road and the entry to Bengalla Mine. It is a sealed road, with a single travel lane in each direction and sealed shoulders. The speed limit on Bengalla Road is 100 km/h. Together with Wybong Road, Bengalla Road providesa link between Denman Road south of Muswellbrook and Meriwa Road (Golden Highway) at Sandy Hollow. It provides vehic ular access to Bengalla Mine, and crosses the MuswellbrookUlan Rail Line at a road over rail crossing approximately 4 km from Denman Road. At the T intersection formed with Wybong Road, Bengalla Road and Wybong Road west are the priority main road, and Wybong Road north-east is the minor road.

Wybong Road is a local road under the control of Muswellbrook Shire Council, which provides a link between Kayuga Road north-west of Muswellbrook and Meriwa Road (Golden Highway) at Sandy Hollow. The speed limit on Wybong Road is $100 \mathrm{~km} / \mathrm{h}$, reducing to $80 \mathrm{~km} / \mathrm{h}$ for approximately 750 m on approach to Kayuga Road. The vehicularaccess for the Mount Pleasant Operation is provided from Wybong Road, approximately 8 km from Kayuga Road and 1.5 km from Bengalla Road. East of the Mount Pleasant Operation access, Wybong Road is subject to a gross load limit of 12 tonnes $(\mathrm{t})$ a nd hascentre linemarking a nd no edgelines. West of the Mount Pleasa nt Operation access, Wybong Road has centre linemarking, solid edgelines and sealed shoulders. Signage indicates the road is subject to flooding in the vic inity of the Rosebrook Bridge east of Logues Lane. The owner of the Mount Plea sant Mine (MACH Energy) is currently resurfacing Wybong Road between the Mount Pleasant Operation Mine Road and Overton Road aspart of the Stage 2 (Modification 4) rail spur constuction. Rosebrook Bridge is outside of the upgrades being undertaken by the Mount Plea sant Mine and is included in the Muswellbrook Council list of a ssets to be assessed as part of the final route selection.

Kayuga Road is a local road underthe control of Muswellbrook Shire Council, which provides a link between Aberdeen Street on the westem side of the Main Northem Railway Muswellbrook, and the locality of Kayuga. It is a sealed road with a single travel lane in each direction, with the exception of at Kayuga Bridge over the Hunter River immediately west of Aberdeen Street, which is a single lane bridge, at which westbound vehicles must give way to vehic les on the bridge. Kayuga Road hascentre linemarking east of Wybong Road and no linemarking to the north-west of Wybong Road. The speed limit on Kayuga Road is $80 \mathrm{~km} / \mathrm{h}$ from Aberdeen Street to a pproximately 1.5 km north-west of Wybong Road, $100 \mathrm{~km} / \mathrm{h}$ over the next approximately 3.5 km , then reduces to $80 \mathrm{~km} / \mathrm{h}$ through Kayuga.

Thomas Mitchell Drive is a local road under the control of Muswellbrook Shire Council and is an approved B-Double route. It provides a link between Denman Road and New England Highway to the south of Muswellbrook township, thus providing a bypass of Muswellbrook for some traffic and is signposted as an altemative route to Singleton from Denman Road. It is a 7 $m$ wide sealed road, and providesaccess to the Mt Arthur Coal Mine, the Muswellbrook Industrial Area, and the Maxwell Infrastructure. Thomas Mitc hell Drive crosses the Antiene Rail Spur at rail over road crossings at two locations approximately 3 km and 4.8 km west of New England Highway. The speed limit on Thomas Mitc hell Drive is $80 \mathrm{~km} / \mathrm{h}$ through a nd to the west of the Industrial Area, a nd between the Maxwell Infrastructure access and New England Highway. The remainder has a speed limit of 100 km/h.

The NSW Department of Planning and Environment (now the Department of Planning, Industry and Environment [DPIE]) produced the Thomas Mitchell Drive Contributions Study (GHD, 2015), with a supplementary report (GHD, 2018). These establish a contributions framework for the allocation of funding to upgrade and mainta in Thomas Mitchell Drive. Currently, Mangoola Coal, Bengalla Mine, Mt Arthur Coal Mine and the Mount Pleasant Operation contribute funding.

### 8.4.2 Intersections

The key intersections in the road network of relevance to the Project are described below.

The intersection of Wybong Road and Mount Pleasant Operation Mine Access Road is a prionity-c ontrolled T-intersection with a channelised left tum deceleration lane in Wybong Road forvehiclesentering the access road, and wide sealed shoulders and a wire rope barier on the southem side of Wybong Road over approximately 300 m past the intersection. The site access road has a single approach and single departure lane at the intersection. The Project does not propose to use this intersection but acknowledges it will be required to be included in the Traffic Management Plan and include consultation with Mach Energy, the owner of the Mount Plea sant Mine.

The intersection of Wybong Road and Bengalla Road is a priority-c ontrolled T-intersection with a channelised left tum deceleration lane in Wybong Road west and a channelised right tum deceleration lane in Bengalla Road. Wybong Road north is the minorapproach to the intersection, and has a single approach and single departure lane, separated by a concrete median island. The RJ A Route Assessment (see Table 6.1 for summary of upgrades) for proposed loads.

The intersection of Bengalla Road and Denman Road is a priority-controlled T-intersection, with channelised left and right tum deceleration lanes in Denman Road, and an eastbound acceleration lane in Denman Road for those vehic les that have tumed left from Bengalla Road. Bengalla Road hasa single approach and single departure lane at the intersection, separated by a concrete median island. Overhead lighting is provided at the intersection. Proposed upgrades in the RJ A Route Assessment (see Table 6.1 for summary of upgrades) for
proposed loadsand have determined with the recommended escorts proposed forall OSOM loads safety will not be compromised.

The intersection of Wybong Road and Kayuga Road is a basic rural prio rity-c ontrolled Tintersection, with single approach and departure lanes on all legs, and no auxiliary tum lanes. Kayuga Road is the majorroad at the intersection, and Wybong Road is the minorroad, with "give way" signs. Wybong Road meets Kayuga Road at approximately 75 degrees, and both roads follow a straight and level a lignment in the immediate vicinity of the intersection, such that sight lines are good.

The intersection of Thomas Mitchell Drive and Denman Road has a left tum deceleration lane and short left tum acceleration lane in Denman Road, and widening of the northbound camiageway that allows northbound vehic les to pass a round vehic les waiting to tum right into Thomas Mitchell Drive. Separate left and right tum lanes are provided in Thomas Mitchell Drive on the approach to the intersection. A single departure lane is provided in Thomas Mitchell Drive, which widens to two eastbound lanes before merging to a single lane over a pproximately 300 m .

The intersection of Thomas Mitc hell Drive and New England Highway is a sea gull intersection with channelised deceleration lanes for vehic les tuming into Thomas Mitchell Drive, and acceleration lanes for vehicles tuming into New England Highway in both directions. Vehicles tuming right into Thomas Mitchell Drive have priority over those tuming left into Thomas Mitchell Drive, which approach via a slip lane with "give way" control. Vehicles turning right from Thomas Mitchell Drive have a "stop" control prior to crossing the northbound lane of New England Highway.

As with any road or intersection TTPP cannot guarantee that a road is completely 'safe'. However, the RJ A route assessment and the traffic management plan that would be put in place to manage the transportation of OSOM has been designed to identify and minimise road safety risks. Loads would be transported with escorts and at slower speeds then general traffic and are therefore estimated to be saferthan general traffic.

### 8.4.3 Traffic Survey Program

To quantify existing traffic conditions as a baseline against which future conditions can be assessed, a program of traffic surveys was undertaken on roads and intersections of relevance to the Project. The traffic survey program was developed to quantify the existing characteristics of the traffic generated along the proposed OSOM routes, and the contribution to traffic by the OSOM traffic generated assummarised in this Section.

It is considered that the main constraint on the capacity of the road network proposed is the operation of the intersections in the network during peak hours rather than the midblock capacity of the roads. This is due to the need forvehicles in opposing directions to occupy the same road space at intersections. While the traffic survey program includes midblock traffic volumes, and the assessment which follows considers the midblock capacity at the
surveyed locations, the intersection operating characteristic sare considered to be the more critical and relevant criteria.

The survey program included mid-block surveys using ATC s of classified vehicle volumes by direction over one week between Tuesday 11 February and Monday 17 February 2020 (inclusive) on:

- Bengalla Road south-east of Wybong Road; and
- Wybong Road between Bengalla Road and Mount Pleasant Operation Road.

To examine the distribution of traffic, vehic le tuming movement surveys were undertaken between 6:00 am and 6:00 pm on Wednesday 27 November 2019 at the intersections of:

- Wybong Road and Kayuga Road;
- Wybong Road and Bengalla Road; and
- Bengalla Road and Denman Road.


### 8.4.4 Midblock Traffic Volumes

Table 8.3 presents a summary of the daily traffic volumes surveyed at the midblocklocations during February 2020 as part of the Mount Pleasant Mine Optimisation.

Table 8.3: Existing Traffic Volumes (vehic les per day)

| Site | Road | Monday | Tuesday | Wednesday | Thurday | Friday | Saturday | Sunday |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| B | Bengalla Road <br> south-east of <br> Wybong Road | 1,913 | 1,943 | 2,111 | 2,128 | 1,958 | 948 | 900 |
| C | Wybong Road <br> north of <br> Bengalla Road | 1,164 | 1,362 | 1,460 | 1,448 | 1,314 | 683 | 661 |

The results demonstrate that the weekday volumes are distinctly different from those on weekend days at all the surveyed locations. Overthe surveyed week, Mount Pleasant Operation generated an average of 888 vehic les perweekday, and 362 vehic les per weekend day.

The surveys included classification of the vehicles based on the Austroads Vehicle Classification System. Light vehic les include motorc ycles, cars, vans, 4-wheel drives (4WDs), and utes (including those towing a trailer or caravan). Heavy vehic les include single unit rigid trucks a nd buses with two, three or four axles and up to 14.5 m long, as well as a rtic ulated vehic les (which include semi-trailers a nd rigid trucks with trailers, B-Doubles and road trains where permitted). The surveyed average weekday daily classified traffic volumesare summarised in Table 8.4.

Table 8.4: Surveyed Daily Traffic Classification (vehicles per day)

| Site | Road | Light | Rigid | Artic ulated | Total | Percentage <br> Heavy |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| B | Bengalla Road <br> south-east of <br> Wybong Road | 1,635 | 331 | 44 | 2,010 | 18.7 |
| C | Wybong Road north <br> of Bengalla Road | 1,146 | 181 | 22 | 1,349 | 15.0 |

It is noted that, of the rigid vehicles on the Mount Pleasant Operation Road in Table 4.2, the significant majority are "Class 3 " vehicles under the Austroads system, which include longer wheelbase utilities and 4WDs (such as Ford Rangers and RAM 1500 utilities), which are commonly used in mining operations, and which would otherwise be considered as light vehic les. The reported percent heavy vehic les in Table 4.2 assume that these vehic les are all heavy vehicles, and is therefore considered to overestimate the actual number of rigid heavy vehicles.

### 8.4.5 Traffic Contributions by the Project

The Project will not contribute to an inc rease in light vehic les through the shire as most of the work force is antic ipated to be coming from Tamworth. However, heavy vehicles including OSOM vehic les will use routes through Tamworth Shire as discussed above. The OSOM vehic les would be travelling under controlled conditions with escort traffic controllers or police at slower speed.

While it is generally not relevant to compare the number of OSOM vehicles with background traffic the Project's contribution to existing traffic volumes is shown in Table 8.5.

Table 8.5: Comparison of Traffic Volumes (vehic les per day)

| Road | Survey Date | Existing <br> Average <br> Weekday | Existing <br> Average <br> Daily | Data Source | Project Weekly <br> Contribution <br> (Loads per <br> week) |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Denman Road <br> west of Benga lla Road | 2012 | - | 2,993 | GHD, 2017 | $8-31$ |
| Denman Road <br> north of Golden Highway | October 2013 | 2,371 | 2,094 | TTPP, 2019 | $8-31$ |
| Denman Road <br> between Golden Highway and <br> Edderton Road | November 2013 | 2,446 | 2,219 | Cardno, 2013 | $8-31$ |
| Thomas Mitchell Drive east of <br> Industrial Area | February 2013 | 3,993 | 3,191 | Hyder, 2013 | $0-19$ |

As shown the number of OSOM vehic les is relatively low compared to the existing traffic volumes and would only contribute a small volume to the existing traffic. The impacts of the vehic les would also be less as the loads would generally travel outside commuter peaks.

### 8.5 Impacts on Road Infrastructure

Muswellbrook Shire Council has requested that our assessment make reference to:

- Muswellbrook Mine Affected Roads Network Plan, Bitzios C onsulting, Ap ril 2020.
- Thomas Mitc hell Drive C ontributions Study, GHD May 2015.


### 8.5.1 Muswellbrook Mine Affect Roads Network Plan (Muswellbrook MARNP)

The Muswellbrook MARNP is a document prepared by Bitzios Consulting (2020) that identifies road upgrades and new road Projects to address access for mine related traffic and transport. It is an update of a similarstudy undertaken in 2015 with the aim of providing a road network plan that can work with mining activity and support other industry and community needs.

An outline of the recommendations of this study are shown in Figure 8.5.

Figure 8.5: Muswellbrook MARNP


[^1]transport planning

The plan identified a number of road network upgrades including a westem comidor connecting the Golden Highway to New England Highway and an inner link road. The plan also makes reference to the Muswellbrook Bypass that is proposed by TfNSW.

It is noted that none of the proposed Projects have any commitment at this stage and it is understood that Muswellbrook Shire Council is in a process of developing an apportionment plan for the construction and upgrade of these roads. It is unlikely that these roads will be con

It is unlikely that these roads will be constructed and be operational within the timeframe of the Project construction. The Project should consult with the Muswellbrook Shire Council as part of the preparation of the TMP for any proposed road works likely to affect the timing of the proposed routes.

### 8.5.2 Thomas Mitc hell Drive Contributions Study

The Thomas Mitc hell Drive Contributions Study (GHD May 2015) was commissioned by the NSW Department of Planning and Environment to establish a framework for the allocation of funding for the upgrade and maintenance of Thomas Mitc hell Drive.

Thomas Mitchell Drive is a local road and is funded by Muswellbrook Shire Council. This means that Council is responsible for the maintenance and upgrade of the road. However, the road is heavily used by the mining industry with local mines using the road to transport heavy equipment and by workers commuting to site.

Assuch the study suggests that the road should be declared aseither a state road or regional road which would allow funding from the state govemment.

However, the study considered models forfunding that included a user pay model where the mines pay for their use of the road and allocates the funding for the road to different road users.

### 8.5.3 Relevance to Hills of Gold Wind Farm

The studies reviewed do not indicate any clear commitment to partic ular infrastructure upgrades or the relative timing. However, it is clear from the studies that Muswellbrook Shire Council is managing how their roads are used for heavy industries such as mining and considering how users would contribute to the use of the local roads.

OSOM vehicles will need to use local roads through Muswellbrook due to the existing constraints on the New England Highway. However, the contribution of the Project on the Thomas Mitchell Drive is between 0-19 times per week in addition to the estimated 4000 daily users of the road and is deemed negligible in comparison to other road users.

The Project will work with Council to develop a contributions plan for the fair use of local roads within the Muswellbrook LGA given its relative use. In addition, dilapidation of the roads is to be managed in conjunction with Muswellbrook Shire Council to ensure that any signific ant damage directly attributable to the Project is made good without cost to the council.
transport planning

## 9 Road Projects

### 9.1 Overview

It is noted that the route for OSOM vehic les is likely to pass a number of road upgrade Projects that are either planned or in construction. The following outlinesthe key road Projects that have been identified.

### 9.2 Golden Highway Upgrades

IfNSW have developed a plan for road upgradesalong the Golden Highway from the New England Highway to Dunedoo. These Projects may have an impact on the OSOM movements through the area. The Projects are shown in Figure 9.1 noting that the Ogilvies Hill and Winery Hill Projects have now been completed.

### 9.2.1 Belford to Golden Highway

The Belford to Golden Highway Project is one of the key upgrades that could impact the Project. The upgrade includes:

- widening the New England Highway to provide a divided road with two lanes in each direction between Belford and the Golden Highway.
- replacing the existing right tum movement from the Golden Highway to the New England Highway with a flyover
- a roundabout on the Golden Highway with a connection to the New England Highway improves safety for motorists tuming left onto the New England Highway towards Singleton and provides safer access to adjoining properties.

Particular attention will need to be considered given that construction of the Belford to Golden Highway Project is likely to begin soon. The transport analysis has included an assessment of the route when completed and before completion. Work is scheduled to begin in late 2021 and be completed within three years.

Figure 9.1: Golden Highway Upgrades

transport planning

### 9.2.2 Mudies Creek Bridge

It is proposed to upgrade the bridge over Mudies Creek on the Golden Highway. The proposal involves:

- Building a new road crossing at MudiesCreek to withstand a one in 100 year flood. The new 30 metre long bridge would be three metres higher than the curent road level to improve travel reliability along the highway during flood events.
- Upgrading a six kilometre section of highway between Whittingham and Mount Thorley. Improvements include providing a smoother road surface, wider road shoulders and five metre clearzones, safety bariers, and overtaking lanes in both directionsto improve safety and traffic flow.


### 9.3 New England Highway

Potential road upgrade Projects on the New England Highway have also been identified.

### 9.3.1 Camberwall

## The Project involves:

- installing a one metre wide painted centreline along a 350 metre section of the highway between 50 metres east of Lethbridge Street and 80 metres west of $G$ lennie Street. The introduction of the centreline will improve safety by providing greater separation between vehicles travelling in opposite directions.
- widening the highway on approach to Glennie Street to improve safety for motorists tuming left.
- installing audio-tactile line marking along the edge and centrelines.
- upgrading drainage on both sides of the highway.
- installing a roadside safety bamier on the northem approach of the bridge over Glennies Creek.
- improving line markings and installing new signage.

This Project is expected to have minimal impact on the Project.

### 9.3.2 Muswellbrook Bypass

The Muswellbook Bypass will feature:

- A 9.1 kilometres of new highway with a single lane in each direction.
- A refined alignment south of Coal Road, with the bypass shifted further to the east to reduce environmental impacts and improve the road alignment.
- Full southem and northem connections with the existing New England Highway which provide for all traffic movements.

While the Muswellbrook Bypass Project could potentia lly have signific ant benefits for the Project, the bypass Project is in early planning phase and is unlikely to begin construction within the timelines of the Hills of G old Wind Farm Project.

Figure 9.2: Muswellbrook Bypass


### 9.4 Mitigation Strategies

The Belford to Golden Highway Project is likely to be the most signific a nt impact on the Project. As part of the Traffic Management Plan, it is recommended that the Project mainta ins a communic ation with TFNSW Project mana gers to identify potential impacts. This will include notific ation of the times when trucks will be travelling through the construction sites.
transport planning

## 10 Conclusion

The Transport Planning Partnership (TTPP) has been commissioned to prepare a response to stakeholder submissions for the Hills of G old Wind Farm Project. The Project will see the construction of 65 wind turbines some 10km south east of Nundle.

The key updates of the Project include:

- The proposed number of wind turbine generators has been reduced from 70 to 65 , however this traffic assessment has been based on a 'worst case' 70 wind turbine generators.
- Removal of the option to transport O versized Overmass deliveries via Tamworth and Nundle Road.
- Removal of options to transport Oversized Overmass equipment deliveries and for construction access to site via Head of the Peel Road and Crawney Road and associated transport options through Nundle residential streets inc luding Happy Valley Road, J enkins St, Herron Street North, G ill Street and Innes Street.
- Altemate Route Options a round Muswellbrook for Oversized Overmass equipment deliveries and greater Project commitment towards structural assessment of council a ssets and community sa fety.
- 2 xadditional laybysalong Lindsay Gap Road and Morisons Gap Road for reduced tourism and commuter impacts entering Nundle.
- Voluntary temporary parking restrictions for construction workers on streets within Nundle providing key services to tourists a nd residents.
- Commitment to create a dedicated construction staff carpark prior to entering Nundle town centre which can enable the introduction of temporary parking restrictions without reducing the benefits of accessing local content for the Project, and could assist the introduction of a shuttle service for peak hour "last mile" site access to reduce traffic through Nundle, on Barry Road and Morrison's Gap Road, if practicable.
- Improved safety commitments in Nundle with a proposed pedestrian crossing on the comers of Oakenville St and Jenkins St, subject to agreement from Tamworth Regional Council.
- Greater clarity on Traffic Management Plan commitments including for residents along Shearers Road and Morisons Gap Road forsafe ingress and egress, broadercommunity communication initiatives, escorts for some OSOM movements along along the proposed OSOM route including Momisons Gap Road, IVMS for regular vehicles accessing the Project Site, and traffic management systems during public road upgrades.
- Geophysic al assessment, realignment and construction method consideration for the Devils Elbow Upgrade.
transport planning
- Revision of the traffic generation assumptions and traffic management strategy to include carpooling as an initiative.
- Additional assessment and traffic modelling on key intersections in Tamworth Regional Council.
- Additional assessment and traffic modelling for Muswelbrook Oversize Overmass route options.
- Project commitments for assessment and upgrades of Muswellbrook Shire Council and Tamworth Regional Council road assets where required, subject to additional consultation.
- Inclusion of key stakeholders and communication protocols in the Traffic Management Plan for residents along the transport routes.
- The Project will provide UHF radios (given mobile phone reception can be intermittent) to residents along Morisons Gap Road and Shearers Road to communicate any emergency or travel plans to site staff along with a protocol for reaching the site manager.
- Project Commitments to road usage fees, dilapidation surveys, and/or performance bonds for remediation works.

The Project has committed to a numbermeasures to minimise the traffic and transport impacts of the Project working with stakeholders throughout the process. Since the submission of the EIS the transport aspects of the Project ha ve been signific antly refined to address issues raised by stakeholders. The revised traffic and transport plan includes:

- All construction traffic to access the site via Morrison's Gap Road - no constructionrelated traffic will use the Head of Peel Road or any residential streets in Nundle as presented in the EIS.
- The Project is committed to upgrading two bridges on Lindsays Gap Road in order to accept the widest loads for the Project, unless other suita ble transport a rangements for the Project can be implemented in consultation with Tamworth Regional Council. This will negate the need to transport loads via Tamworth as previously presented in the EIS.
- The Devils Elbow upgrade has been refined based on further design analysis
- Routes around Muswellbrook have been updated to reduce impacts on the town. The Project will work with Muswellbrook Shire Council to develop a suitable contribution plan for the usage of local roads in the shire.
- Commitment to create a dedic ated construction staff carpark prior to entering Nundle town centre which can enable the introduction of temporary parking restrictions without reducing the benefits of accessing local content for the Project. A policy of car pooling will be implemented by the Project team to further reduce the need for local vehicles to access the site.
transport planning
This revised assessment has included the modelling of intersections in Tamworth and further a nalysis of traffic given the revised traffic routes. The analysis shows that:
- Construction traffic will not have an adverse effect on the operation of the road network. Queueing and delay within Tamworth and surrounding intersections will not be signific antly impacted by the additional traffic for the short period of peak traffic .
- Volumes of traffic forecast will be lower that the environmental ca pacity for loc al streets in Nundle.
- The revised traffic volumes will operate at Levels of Service B or better.

The Project will work with the relevant road authorities, Transport for NSW, Tamworth Regional Council and Muswellbrook Shire Council to ensure that the roads are maintained and there is fair compensation for the use of local roads. The Project will consult with Tamworth Regional Council on the need to undertake dilapidation surveys before and after construction.

Traffic management options described in the EIS have not changed except for including a policy forcarpooling.

During construction it has been identified that there may be road upgrade Projects that will coincide with the period that the oversized and over mass loads will be transported from Newc astle port to site. The key Projects identified are the upgrade of the intersection of the New England Highway and Golden Highway and the new bridge at Mudies Creek on the Golden Highway. The Project team proposes to liaise with the relevant Project managers for these Projectsto ensure that the impacts to the Project and the road network are minimised.

At the completion of the Project infrastructure that wascreated for the Project transportation of OSOM will closed but maintained to the degree that they can be used in the future should additional blades need to be transported to site.

To minimise the effects on local streets in Muswellbrook and Nundle it is proposed that the traffic management plan will include limitations on trips during school peak hours from 8:00am - 9:30am and 2:30pm-4:00pm.

The project involves associated road works including the upgrade of two bridges along Lindsays Gap Road and otherenabling works and road upgrades. The project will work with Musewellbrook Shire Council and Tamworth Regional Council to ensure that the road infrastructure are not degraded and contribute to the maintenance and upgrade of the roads. The upgrade of infrastructure would continue to be of beneift community in terms of road safety, maintence of the public assets and support local businesses beyond the construction period of the project.
transport planning

## References

Roads and Traffic Authority - Guide to Traffic Generating Developments, 2002
The Transport Planning Partnership (TTPP) - Hills of Gold Wind Farm, Traffic a nd Tra nsport Assessment 2020.

Rex J Andrews - Route Study: Someva Hills of G old Windfarm Ex Port Newcastle (Revision 4) 2021.

Bitzios Consulting - Muswellbrook Mine Affected Roads Network Pla n, April 2020.

GHD Thomas Mitc hell Drive Contributions Study, May 2015

## AppendixA

## RexJ Andrews Route Assessment

## REX J ANDREWS

ENGINEERED TRANSPORTATION

ROUTE STUDY: SOMEVA P/L
PROJECT: HILLS OF GOLD WINDFARM
EX PORT OF NEWCASTLE.

08/04/2021 REV 04


## Index:

INDEX: ..... 2
INDEX: ..... 2
1.0 Introduction ..... 3
2.0 Evaluation ..... 4
3.0 Project data ..... 5
4.0 Transport combinations (EXAMPLES). ..... 6
5.0 Transport drawings (EXAMPLES) ..... 7
6.0 SIte Location. ..... 19
7.0 WINDFARM SITE MAP. ..... 20
8.0 PORT OF IMPORT. ..... 21
9.0 TRANSPORT SUMMARY. ..... 25
10.0 Route Survey A: Newcastle port to Hills of Gold WF Via the Golden Hwy. (Blade route) ..... 26
11.0 Route Survey B: Newcastle port to Hills of Gold WF for loads up to 5.2 metres in height. ..... 93
12.0 Route Survey C: Newcastle port to Hills of Gold WF for loads over 5.2 metres in height. ..... 98
13.0 Route Survey D: Newcastle port to Hills of Gold WF for standard loads. ..... 104
14.0 Conclusion: ..... 108
15.0 References: ..... 114

### 1.0 Introduction

This document describes observations and previous experience on route and explains the Transport of Wind turbine equipment from Newcastle to Hills of Gold Windfarm.

This Route survey took place on 17-06-19.

### 2.0 Evaluation

| $\mathbf{1}$ | No Cost |
| :---: | :--- |
| $\mathbf{2}$ | Some Work |
| $\mathbf{3}$ | Moderate Amount of Work |
| $\mathbf{4}$ | Extreme Amount of Work |

(Mark below boxes with an X)

|  |  | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ |
| :--- | :--- | :---: | :---: | :---: | :---: |
| A | Harbour |  | $\mathbf{X}$ |  |  |
| B | Road Modification |  |  |  | $\mathbf{X}$ |
| C | Road Furnishings |  |  |  | $\mathbf{X}$ |
| D | Trees |  |  | $\mathbf{X}$ |  |
| E | Site Entrance |  |  |  | $\mathbf{X}$ |
| F | Bridge Calculations |  |  | $\mathbf{X}$ |  |
| G | Traffic Control |  | $\mathbf{X}$ |  |  |

### 3.0 Project data.

Date of latest Route Assessment. 17/06/2019
Survey undertaken by. (Rex J Andrews P/L)
Project name. White Hills of Gold windfarm
Location. Newcastle port (NSW) to Nundle (NSW)
Turbine type (Example)
Rotor size 170 metre with a hub height of up to 165 Metres.
Rotor size 158 metre with a hub height of up to 165 Metres.

### 4.0 Transport combinations (Examples).

Nacelle with drivetrain out (12l $\times 4.2 \mathrm{w} \times 4.2 \mathrm{~h} \times 70 \mathrm{~T}$ )
Possible transport configuration. Prime mover with $8 \times 8$ Platform trailer.
Overall length: $30.01 \times 4.2 w \times 4.9 h \times 122.0 \mathrm{~T}$.

Drivetrain (7l x 3.5w x 3.5h x 68T)
Possible transport configuration. Prime mover with $2 \times 8-4 \times 8$ Platform Low loader.
Overall length: $30.01 \times 4.2 \mathrm{w} \times 4.9 \mathrm{~h} \times 122.0 \mathrm{~T}$.

Nacelle with drivetrain in (12l $\times 4.2 \mathrm{w} \times 4.2 \mathrm{~h} \times 125 \mathrm{~T}$ )
Possible transport configuration. Prime mover with $11 \times 8$ Platform trailer.
Overall length: $49.01 \times 4.2 w \times 5.2 h \times 195.0 T$.

Hubs (4.0l x $3.5 \mathrm{w} \times 3.8 \mathrm{~h} \times 50.0 \mathrm{~T}$ )
Possible transport configuration. Prime mover with $2 \times 84 \times 8$ Low Loader.
Overall length: $28.01 \times 5.1 w \times 5.9 h \times 92.5 T$.

Blade 170 rotor ( $82.01 \times 4.5 \mathrm{w} \times 4.0 \mathrm{~h} \times 35 \mathrm{~T}$ )
Possible transport configuration. Prime mover with $2 \times 8$ dolly with $2 \times 8$ jinker.
Overall length: $92.01 \times 5.6 \mathrm{w} \times 5.3 \mathrm{~h} \times 86.5 \mathrm{~T}$.

Blade 158 rotor ( $65.4 \mathrm{l} \times 4.7 \mathrm{w} \times 3.4 \mathrm{~h} \times 24 \mathrm{~T}$ )
Possible transport configuration. Prime mover with $1 \times 4$ dolly with $4 \times 4$ extendable blade trailer.
Overall length: $92.01 \times 5.6 \mathrm{w} \times 5.3 \mathrm{~h} \times 86.5 \mathrm{~T}$.

Bottom section (16.21 x $4.8 \times 4.5 \times 100 \mathrm{~T}$ )
Possible transport configuration. Prime mover with $8 \times 8$ Platform trailer.
Overall length: $30.01 \times 4.8 w \times 5.5 h \times 108.5 \mathrm{~T}$.

Mid lower section ( $21.8 \mathrm{l} \times 4.5 \times 4.5 \times 95.2 \mathrm{~T}$ )
Possible transport configuration. Prime mover with $10 \times 8$ platform trailer.
Overall length: $32.01 \times 4.5 w \times 5.5 h \times 157.5 \mathrm{~T}$.

Mid section ( $21.81 \times 4.5 \times 4.5 \times 72.5 \mathrm{~T}$ )
Possible transport configuration. Prime mover with $10 \times 8$ platform trailer.
Overall length: $32.0 \mathrm{l} \times 4.5 \mathrm{w} \times 5.5 \mathrm{~h} \times 137.5 \mathrm{~T}$.

Mid upper section ( $28.81 \times 4.5 \times 4.5 \times 52.3 \mathrm{~T}$ )
Possible transport configuration. Prime mover with $3 \times 4-2 \times 8$ Dolly jinker
Overall length: $40.01 \times 4.5 \mathrm{w} \times 5.5 \mathrm{~h} \times 92.5 \mathrm{~T}$.

Top section ( $30.81 \times 4.5 \times 3.4 \mathrm{~h} \times 50.0 \mathrm{~T}$ )
Possible transport configuration. Prime mover with $3 \times 4-2 \times 8$ Dolly jinker
Overall length: $40.01 \times 4.5 \mathrm{w} \times 5.5 \mathrm{~h} \times 90.5 \mathrm{~T}$.

### 5.0 Transport drawings (Examples)

## Blade diagram (170 rotor):



ROUIE STUDY

Blade diagram (158 rotor):



## Hub trailer:



Newc astle to Hills of Gold

## Nacelle Drivetrain in:



## Nacelle drivetrain out:



ROUIE STUDY

## Drivetrain:



## Tower trailer 10x8:



ROUIE STUDY

## Tower trailer 8x8:



## Mid tower trailer 10x8:



## Top tower trailer:



Newc astle to Hills of Gold

## Bookend tower trailer:



ROUTE STUDY<br>Newc astle to Hills of Gold<br>Windfarm

### 6.0 Site Location.

The Hill of Gold wind farm is located 8 Km's south of Nundle NSW and 300 Kilometres by road from the Port of Newcastle.


## ROUIE STUDY Newc astle to Hills of Gold Windfarm

### 7.0 Windfarm site map.



ROUIE STUDY Newc astle to Hills of Gold<br>Windfarm

### 8.0 Port of Import.

The wind turbine equipment will be imported from various countries and will arrive on ships into the Port of Newcastle. The client may alternately source local towers. The ideal berth for these shipments is the Mayfield \#4 Berth. This facility has a hardstand storage area of roughly $100,000 \mathrm{~s} / \mathrm{q}$ meters, adjacent to the berth.

Access from the storage to the Public roads, is via a port operated road onto Selwyn Street. There will need to be a small amount of road modifications within the port.

Image 1: Port overview.


ROUTE STUDY<br>Newc astle to Hills of Gold<br>Windfarm

Image 2: Mayfield \#4 Berth


Image 3: Mayfield \#4 Port storage area.


## ROUIE STUDY <br> Newc astle to Hills of Gold <br> Windfarm

Image 4: Mayfield \#4 Port storage area.
 Newc astle to Hills of Gold

### 9.0 Transport Summary.

We have based this study on the turbine components, and towers entering Australia via the Port of Newcastle. The following shows the blade route and 3 additional routes depending on the size of the load.

ROUTE A: PORT OF NEWCASTLE TO HILLS OF GOLD WF, BLADE ROUTE: (326.0
kilometres): After completing this route survey, we believe the following is the most suitable option for the blades, and possibly the towers and motors.
This route took us via Selwyn Street, George Street, Industrial Drive, Maitland Road, New England Highway, John Renshaw Drive, Hunter Expressway, New England Highway, Golden Highway, Denman Road, (Muswellbrook bypass via Bengalla Road, Wybong Road, Kayuga Road, Ivermein Street, Dartbrook mine access Road), New England Highway, Lindsays Gap Road, Nundle Road, Crosby Street, Oakenville Street, Old Hanging Rock Road, Barry Road, Morrisons Gap Road.
GPS Link: https://goo.gl/maps/NrA7rYBLwoV6PE7n7

## ROUTE B: PORT OF NEWCASTLE TO HILLS OF GOLD WF, LOADS UP TO 5.2

METRES HIGH: (284.0 kilometres): After completing this route survey, we believe the following is the most suitable option for loads up to 5.2 metres in height, except the blades. This route took us via Selwyn Street, George Street, Industrial Drive, Maitland Road, New England Highway, John Renshaw Drive, Hunter Expressway, New England Highway, Bell Street, Victoria Street, Market Street, New England Highway, Lindsays Gap Road, Nundle Road, Crosby Street, Oakenville Street, Old Hanging Rock Road, Barry Road, Morrisons Gap Road.
GPS Link: https://goo.gl/maps/rouAWyxLZ53pMB3v7

ROUTE C: PORT OF NEWCASTLE TO HILLS OF GOLD WF, LOADS OVER 5.2 METRES HIGH: ( 328.0 kilometres): After completing this route survey, we believe the following is the most suitable option for loads over 5.2 metres in height, except the blades.
This route took us via Selwyn Street, George Street, Industrial Drive, Maitland Road, New England Highway, John Renshaw Drive, Hunter Expressway, New England Highway, Golden Highway, Denman Road, Thomas Mitchell Drive, New England Highway, Bell Street, Victoria Street, Market Street, New England Highway, Lindsays Gap Road, Nundle Road, Crosby Street, Oakenville Street, Old Hanging Rock Road, Barry Road, Morrisons Gap Road.
GPS Link: https://goo.gl/maps/tMkKEEQKNL7azUDi7

ROUTE D: PORT OF NEWCASTLE TO HILLS OF GOLD WF, STANDARD LOADS:
(284.0 kilometres): After completing this route survey, we believe the following is the most suitable option for standard loads up to 3.5 metres wide, and 5.2 metres in height.
This route took us via Selwyn Street, George Street, Industrial Drive, Maitland Road, New England Highway, John Renshaw Drive, Hunter Expressway, New England Highway, Lindsays Gap Road, Nundle Road, Crosby Street, Oakenville Street, Old Hanging Rock Road, Barry Road, Morrisons Gap Road.
GPS Link: https://goo.gl/maps/rd4SwBkQqnga1RjY7

ROUIE STUDY<br>Newc astle to Hills of Gold<br>Windfarm

### 10.0 Route Survey A: Newcastle port to Hills of Gold WF Via the Golden Hwy. (Blade route)

Distance: (326.0 Kilometres).
Via: Selwyn Street, George Street, Industrial Drive, Maitland Road, New England Highway, John Renshaw Drive, Hunter Expressway, New England Highway, Golden Highway, Denman Road, (Muswellbrook bypass via Bengalla Road, Wybong Road, Kayuga Road, Ivermein Street, Dartbrook mine access Road), New England Highway, Lindsays Gap Road, Nundle Road, Crosby Street, Oakenville Street, Old Hanging Rock Road, Barry Road, Morrisons Gap Road.
GPS Link: https://goo.gl/maps/NrA7rYBLwoV6PE7n7


| KEY |  |
| :---: | :---: |
| MODIFICATIONS REQUIRED |  |
| MINOR WORKS OR CAUTION |  |
| PARKING |  |


| $\begin{gathered} \text { KM } \\ \text { index } \end{gathered}$ | Location | Section of road | Critical <br> Measurement | Procedure | Comments 170.0 m rotor | Comments 158.0 m rotor |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.0 | Mayfield | Mayfield \#4 berth onto Selwyn Street GPS link: <br> https://goo.gl/maps/afLwPYKuNdm | Clearance: <br> Length: 70.0 metres | Right hand turn | Both options will require the fence to be relocated on the left-hand side. Some hardstand will need to be added to the left side entering the corner and while exiting the corner. | Fence may need to be modified. |
| 0.4 | Mayfield | Selwyn Street rail crossing <br> GPS link: <br> https://goo.gl/maps/AmohE54hKSz | Clearance: <br> Width: 9.0 metres | Travel directly ahead | Loads to travel over the crossing in the center of the road. Approval required crossing this line, likely cross with caution. | Loads to travel over the crossing in the center of the road. Approval required crossing this line, likely cross with caution. |
| 1.3 | Mayfield | Selwyn Street onto George Street GPS link: <br> https://goo.gl/maps/gXeHvBtCp4D2 | Clearance: <br> Length: 70.0 metres | Right hand turn | The sign on the inside of the corner will need to be made removable. | No problem with this section of road. |
| 1.4 | Mayfield | George Street onto Industrial Drive https://goo.gl/maps/s4ayrsuoAsD2 | Clearance: <br> Length: 70.0 metres | Moderate righthand turn | Load to travel across to the correct side to the correct side. The traffic signal in the middle of the intersection will need to be relocated. Additionally, hardstand will need to be placed on the south side of the intersection. | Load to travel across to the correct side to the correct side. Hardstand will need to be placed on the south side of the intersection. |

# Newc astle to Hills of Gold <br> Windfarm 

| 4.9 | Mayfield | Industrial Drive under traffic signals GPS link: <br> https://goo.gl/maps/YmqhiS2iR582 | Clearance: <br> Height: 5.4 <br> Metres | Travel directly ahead | The lowest traffic signal on route is at the intersection of Steel River Blvd. Trucks that exceed 5.3 meters will need to travel in the right-hand lane. | The lowest traffic signal on route is at the intersection of Steel River Blvd. Trucks that exceed 5.3 meters will need to travel in the right hand lane. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5.5 | Mayfield West | Industrial Drive onto Maitland Road GPS link: <br> https://goo.gl/maps/Kn49dhWG2qG2 | Clearance: <br> Length: 70.0 metres | Moderate right hand turn | The blades will need to cross to the incorrect side 150 metres prior to the intersection, then return to the correct side 120 metres past the intersection. <br> No road modifications required. | The blades will need to cross to the incorrect side 150 metres prior to the intersection, then return to the correct side 120 metres past the intersection. <br> No road modifications required. |
| 13.9 | Hexham | New England Highway under gantry GPS link: <br> https://goo.gl/maps/YTMoFe7Aick | Clearance: <br> Height: 5.95 Metres | Travel directly ahead | This is the lowest structure on route. There is no bypass around the gantry. A maximum loaded height of 5.8 metres should not be exceeded. | This is the lowest structure on route. There is no bypass around the gantry. A maximum loaded height of 5.8 metres should not be exceeded. |
| 17.4 | Tarro | New England Highway onto John Renshaw Drive GPS link: <br> https://goo.gl/maps/SRDr5JigkBp | Clearance: <br> Width: 12.0 metres | Left hand merge | No problems with this section of road. | No problems with this section of road. |
| 18.4 | Beresfield | John Renshaw Drive through M1 intersection GPS link: https://goo.gl/maps/N19vJih1Fgr | Clearance: <br> Width: 9.0 metres <br> Height: 5.9 metres | Travel directly ahead | No problems with this section of road. | No problems with this section of road. |
| 28.7 | Buchanan | John Renshaw Drive onto the Hunter Expressway <br> GPS link: <br> https://goo.gl/maps/FH5DqHBXwSkntAmz9 | Clearance: <br> Length: 65.0 metres | Right hand turn | The blades will need to cross to the incorrect side than down the off-ramp onto the incorrect side of the expressway. Approx 600 metres along the expressway there is a break in the road, which will allow the blades to cross back to the correct side of the expressway, this may require additional hardstand. Traffic control and or police will be required to perform this procedure. | Travel around the roundabout and take the third exit onto the Hunter Expressway onramp. <br> A sign will need to be made removable. Spotter to guide load through this pinchpoint. |


| 58.9 | Branxton | The Hunter Expressway onto New England Highway <br> GPS link: <br> https://goo.gl/maps/7rauNuxzqiq | Clearance: <br> Width: 9.0 metres | Travel directly ahead | No problems with this section of road. | No problems with this section of road. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 67.3 | Whittingham | The New England Highway onto the Golden Highway GPS link: https://goo.gl/maps/nAnfkYfeUn42 | Clearance: <br> Width: 12.0 metres | Left Hand turn | The NSW Government is currently upgrading this intersection. The intersection in its current form has a number of signs that would need to be made removable, but no modifications are required on the existing corner. <br> At this stage the data that is available for the upgrades shows that the section of road that we would need to access does not change considerably. However, it is recommended that you monitor the progress of the upgrades, and that any changes are thoroughly looked at. | The NSW Government is currently upgrading this intersection. The intersection in its current form has a number of signs that would need to be made removable, but no modifications are required on the existing corner. <br> At this stage the data that is available for the upgrades shows that the section of road that we would need to access does not change considerably. However, it is recommended that you monitor the progress of the upgrades, and that any changes are thoroughly looked at. |
| 67.4 | Whittingham | Golden Highway <br> GPS link: <br> https://goo.gl/maps/R86RFuPnmFU2 | Clearance: $115.0 \times 9.0$ <br> metres | Parking Bay | Suitable parking for Fatigue breaks. | Suitable parking for Fatigue breaks. |
| 77.3 | Whittingham | Golden Highway intersection with the Putty Road <br> GPS link: <br> https://goo.gl/maps/7hQdEmK1EgE2 | Clearance: <br> Length: 85.0 metres | Left hand turn | Blades to cross from the incorrect side to the incorrect side. Some signs will need to be made removable. | Blades to cross from the incorrect side to the incorrect side. Some signs will need to be made removable. |
| 77.4 | Mount Thorley | Golden Highway <br> GPS link: <br> https://goo.gl/maps/zGvdupDuixx | Clearance: $100.0 \times 10.0$ <br> metres | Parking Bay | Suitable parking for Fatigue breaks. | Suitable parking for Fatigue breaks. |
| 80.8 | Mount Thorley | Golden Highway intersection with the Putty Road <br> GPS link: <br> https://goo.gl/maps/VyA42n1CqZx | Clearance: <br> Length: 85.0 metres | Right hand turn | Blades to cross from the incorrect side and cross back to the correct side approx. 500 metres west of the intersection. | Blades to cross from the incorrect side and cross back to the correct side approx. 500 metres west of the intersection. |

Windfarm

| 98.0 | Warkworth | Golden Highway <br> GPS link: <br> https://goo.gl/maps/Y6V6EXaCwxq | Clearance: $100.0 \times 8.0$ <br> metres | Parking Bay | Suitable parking for Fatigue breaks. | Suitable parking for Fatigue breaks. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 107.0 | Jerrys Plains | Golden Highway through Jerrys Plains village <br> GPS link: <br> https://goo.gl/maps/AiuT8MMVTh5crs348 | Clearance: <br> Length: 70.0 metres | Dogleg | Blades to cross from the incorrect side to the incorrect side. Some hardstand will need to be added to the outside of the right hand corner. <br> The swept path will stay within the road reserve. | No problems with this section of road. |
| 126.0 | Ogilvy | Golden Highway <br> GPS link: <br> https://goo.gl/maps/ShT4hrj8WQeMcris7 | 6\% gradient | Travel directly ahead | This section of road has a steep mountain range that will require additional pull trucks to assists loads that exceed 80T gross weight. <br> Additionally, the NSW Government is currently upgrading this section of road. It is recommended that you monitor the progress of the upgrades, and that any changes are thoroughly looked at. | This section of road has a steep mountain range that will require additional pull trucks to assists loads that exceed 80T gross weight. <br> Additionally, the NSW Government is currently upgrading this section of road. <br> It is recommended that you monitor the progress of the upgrades, and that any changes are thoroughly looked at. |
| 141.9 | Denman | Golden Highway onto Denman Road GPS link: <br> https://goo.gl/maps/sf4PNnycxB32 | Clearance: <br> Length: 60.0 metres | Right hand turn | The blades will travel around the corner from correct side onto the correct side. The existing corner will require hardstand to be added and signs made removable. <br> The swept path will stay within the road reserve. | The blades will travel around the corner from correct side onto the correct side. The existing corner will require hardstand to be added and signs made removable. |
| 149.0 | Muswellbrook | Denman Road onto Bengalla Road GPS link: <br> https://goo.gl/maps/CJYMtSMTttJ2 | Clearance: <br> Length: 65.0 metres | Left hand turn | Blades to cross from the incorrect side to the incorrect side. Some signs will need to be made removable and some hardstand added to the inside and outside of the corner. The swept path will enter a landowner's boundaries on the inside of the corner. | Blades to cross from the incorrect side to the incorrect side. <br> No works required on this intersection. |


| 158.5 | Muswellbrook | Bengalla Road onto Wybong Road GPS link: <br> https://goo.gl/maps/vibQtvHkxXE2 | Clearance: <br> Length: 70.0 metres | Right hand turn | Blades to cross from the correct side to the correct side. Some signs will need to be made removable. | Blades to cross from the correct side to the correct side. Some signs will need to be made removable. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 168.1 | Muswellbrook | Wybong Road onto Kayuga Road OPTION 1: <br> GPS link: <br> https://goo.gl/maps/xVscKUT1isJ2 | Clearance: <br> Length: 40.0 metres | Left hand turn | Blades to cross from the incorrect side to the incorrect side. Some signs will need to be relocated or made removable. Permission will be required from the landowner to travel over the private land. This will require removal and realigning the fence, and adding hardstand. | Blades to cross from the incorrect side to the incorrect side. Some signs will need to be relocated or made removable. Permission will be required from the landowner to travel over the private land. This will require removal and realigning the fence, and adding hardstand. |
| 173.3 | Muswellbrook | Kayuga Road onto Ivermein Street GPS link: <br> https://goo.gl/maps/JpTfmcsZ6Sk | Clearance: <br> Length: 85.0 metres | Travel directly ahead | No problems with this section of road. | No problems with this section of road. |
| 174.0 | Muswellbrook | Ivermein Street onto Dartbrook mine access Road <br> GPS link: <br> https://goo.gl/maps/ddMHa4CmXK32 | Clearance: <br> Length: 50.0 metres | Right hand turn | Blades to cross from the correct side to the correct side. Some signs will need to be made removable and some hardstand added to the inside and outside of the corner. Additionally, a drainage pipe will need to be extended on the inside of the corner. | Blades to cross from the correct side to the correct side. Some signs will need to be made removable and some hardstand added to the inside and outside of the corner. Additionally, a drainage pipe will need to be extended on the inside of the corner. |
| 174.8 | Muswellbrook | Dartbrook Road <br> GPS link: <br> https://goo.gl/maps/u9vSXiSV7Jt | Clearance: <br> Length: 60.0 metres | Right hand turn | Blades to cross from the correct side to the correct side but cut across the inside of the corner. Some signs will need to be made removable and some hardstand added to the inside of the corner. | Blades to cross from the correct side to the correct side but cut across the inside of the corner. Some signs will need to be made removable and some hardstand added to the inside of the corner. |
| 177.0 | Muswellbrook | Dartbrook Road onto New England Highway GPS link: <br> https://goo.gl/maps/twTsmUKaED82 | Clearance: <br> Length: 60.0 metres | Left hand turn | Blades to cross from the incorrect side to the incorrect side. Some signs will need to be made removable on the corner and some hardstand added. | Blades to cross from the incorrect side to the incorrect side. Some signs will need to be made removable on the corner and some hardstand added. |
| 240.8 | Murrurundi | New England highway (Township) GPS link: <br> https://goo.gl/maps/Sj3ixAkhujt | Clearance: $60.0 \times 5.0$ metres | Parking Bay | Suitable parking for Fatigue breaks. | Suitable parking for Fatigue breaks. |


| 245.4 | Murrurundi Hill | New England highway Nowlands Gap GPS link: <br> https://goo.gl/maps/R5yufobPeMG2 | Clearance: $120.0 \times 12.0$ <br> metres | Parking Bay | Emergency parking only. | Emergency parking only. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 251.3 | Willow Tree | New England highway <br> GPS link: <br> https://goo.gl/maps/XLTg7CRV7EU2 | Clearance: <br> Width: 7.0 m <br> Length: 35 m <br> Height: 5.2 m | Kankool weighbridge | It is likely that the towers and defiantly the blades will not fit into this facility. Engineered documentation showing correct weights for all loads will be required. | It is likely that the towers and defiantly the blades will not fit into this facility. Engineered documentation showing correct weights for all loads will be required. |
| 257.9 | Willow Tree Township | New England highway <br> GPS link: <br> https://goo.gl/maps/gw38qmvVfTC2 | Clearance: $60.0 \times 5.0$ metres | Parking Bay | Suitable parking for Fatigue breaks. | Suitable parking for Fatigue breaks. |
| 259.5 | Willow Tree Truck Stop N | New England highway <br> GPS link: <br> https://goo.gl/maps/RRdPVHupGCs | Clearance: $120.0 \times 12.0$ <br> metres | Parking Bay | Suitable parking for Fatigue breaks for small loads only. | Suitable parking for Fatigue breaks for small loads only. |
| 269.0 | Wallabadah | New England highway <br> GPS link: <br> https://goo.gl/maps/QWCyeHQSohS2 | Clearance: $80.0 \times 5.0$ metres | Parking Bay (side of road) | Suitable parking for Fatigue breaks. | Suitable parking for Fatigue breaks. |
| 276.0 | Wallabadah | New England highway onto Lindsay's Gap Road GPS link: $\qquad$ | Clearance: <br> Length: 50.0 metres | Right hand turn | Blades to cross from the correct side to the correct side but cut across the inside of the corner. Some signs will need to be made removable and some hardstand added to the inside of the corner. | Blades to cross from the correct side to the correct side but cut across the inside of the corner. Some signs will need to be made removable on the inside of the corner. |
| 287.7 | Garoo | Lindsay's Gap Road over Goonoo Goonoo Creek <br> GPS link: <br> https://goo.gl/maps/9ELSk5ZLRWnf14tm7 | Clearance: <br> Axle width: 3.60 m <br> Overall width: <br> 6.20m <br> Guard rail height: <br> 850mm | Travel directly ahead over bridge in the centre of the road. | The blades will fit over the structure in its current condition. <br> Loads that are been carried on trailers with an axle width exceeding 3.5 meters will not fit over this structure in its current form. <br> This bridge will need to be replaced or modified before the towers or motors can be delivered on this route. <br> A trafficable deck width of at least 4.6 meters is required for these heavier loads. | The blades will fit over the structure in its current condition. <br> Loads that are been carried on trailers with an axle width exceeding 3.5 meters will not fit over this structure in its current form. <br> This bridge will need to be replaced or modified before the towers or motors can be delivered on this route. |


|  |  |  |  |  |  | A trafficable deck width of at least 4.6 meters is required for these heavier loads. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 295.7 | Garoo | Lindsay's Gap Road over Middlebrook Creek GPS link: | Clearance: <br> Axle width: 4.50 m <br> Overall width: <br> 6.10 m <br> Guard rail height: <br> 750mm | Travel directly ahead over bridge in the centre of the road. | The blades will fit over the structure in its current condition. <br> This bridge will need to be modified or replaced before the towers or motors can be delivered on this route. <br> A trafficable deck width of at least 4.6 meters is required for these heavier loads. | The blades will fit over the structure in its current condition. <br> This bridge will need to be modified or replaced before the towers or motors can be delivered on this route. <br> A trafficable deck width of at least 4.6 meters is required for these heavier loads. |
| 301.2 | Garoo | Lindsay's Gap Road through Lindsay's Gap GPS link: | Clearance: <br> Length: 90.0 metres | Travel directly ahead | Load to travel in the centre of the road, escorts to warn traffic 500 metres to the east of the gap. | Load to travel in the centre of the road, escorts to warn traffic 500 metres to the east of the gap. |
| 306.8 | Nundle | Lindsay's Gap Road onto Nundle Road GPS link: <br> https://goo.gl/maps/FX4ZRx2YG9i2BsXMA | Clearance: <br> Length: 50.0 metres | Right hand turn | Blades to cross from the correct side to the correct side but cut across the inside of the corner. Some signs will need to be made removable and some hardstand added to the inside of the corner. A power pole will also need to be relocated. | Blades to cross from the correct side to the correct side but cut across the inside of the corner. Some signs will need to be made removable. |
| 310.3 | Nundle | Nundle Road onto Crosby Street GPS link: <br> https://goo.g1/maps/uVvcN9QkPyTDP1YR6 | Clearance: <br> Width: 8.0 metres | Travel directly ahead | No problems with this section of road. | No problems with this section of road. |
| 310.6 | Nundle | Crosby Street onto Oakenville Street GPS link: <br> https://goo.gl/maps/aZNDKURdSBERedMr9 | Clearance: <br> Width: 8.0 metres | Travel directly ahead | No problems with this section of road. | No problems with this section of road. |
| 311.0 | Nundle | Oakenville Street and Jenkins Street intersection <br> GPS link: <br> https://goo.gl/maps/7YM56hQq8bnCSoZy8 | 5.0 metres width clearance |  | Blades to travel directly ahead on the correct side of the road. A no parking exclusion zone will need to be placed on the left-hand side while travelling through this intersection. Two signs will also need to be made removable. | Blades to travel directly ahead on the correct side of the road. A no parking exclusion zone will need to be placed on the left-hand side while travelling through this intersection. Two signs will also need to be made removable. |


| 312.0 | Nundle | Oakenville Street onto Old Hanging Rock <br> GPS link: <br> https://goo.gl/maps/1UMr2EwZetiE76Ey9 | 35.0 metres length clearance | Left hand turn | Blades to turn left from the incorrect side to the incorrect side of the road. The swept path will have the blades travel through a landowner's boundaries. This will require a fence to be relocated and hardstand added. Additionally, while travelling over the bridge some signs will need to be relocated and some sections of guardrail relocated. | Blades to turn left from the incorrect side to the incorrect side of the road. The swept path will have the blades travel through a landowner's boundaries. This will require a fence to be relocated and hardstand added. Additionally, while travelling over the bridge some signs will need to be relocated. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 313.0 | Nundle | Old Hanging Rock Road onto Barry Road <br> GPS link: <br> https://goo.gl/maps/ve9zvmdJnLBYtQSz5 | 90.0 metres clearance | Right hand bend | No problems with this section of road. | No problems with this section of road. |
| $\begin{aligned} & 313.0 \text { to } \\ & 323.0 \\ & \mathrm{Km} \text { 's } \end{aligned}$ | Nundle to Hanging Rock | Barrys Road <br> https://goo.gl/maps/BUBe2MCfoQ215qKE6 | 25.0 metres length clearance | Travel directly ahead through multiple tight turns and steep terrain | Barrys Road has a section of road known as the Devils Elbows. The existing hairpin corners are impassable for the blades, towers and motors. A detour of the Devils Elbow has been looked at and will likely be the best solution for all loads. <br> To the west and east of the Devils Elbows the road will need to be widened on a few corners, this would include hardstand and tree removal. | Barrys Road has a section of road known as the Devils Elbows. The existing hairpin corners are impassable for the blades, towers and motors. A detour of the Devils Elbow has been looked at and will likely be the best solution for all loads. <br> To the west and east of the Devils Elbows the road will need to be widened on a few corners, this would include hardstand and tree removal. |
| 323.0 | Hanging Rock | Barrys Road onto Morrisons Gap <br> Road <br> GPS link: <br> https://goo.gl/maps/CLZDJSjENx8rifAg7 | 35.0 metres length clearance | Right hand turn | Blades to turn right from the correct side to the correct side of the road. The swept path will have the blades travel through a landowner's boundaries on the inside of the corner. This will require a fence to be relocated and hardstand added. Additionally, some trees will need to be removed. | Blades to turn right from the correct side to the correct side of the road. The swept path will have the blades travel through a landowner's boundaries on the inside of the corner. This will require a fence to be relocated and hardstand added. Additionally, some trees will need to be removed. |

ENGINEERED TRANSPORTATION

| 323.0 to 326.0 Km's | Hanging Rock | Morrisons Gap Road GPS link: <br> https://goo.gl/maps/kLtYYnmhTgvE6ZPFA | 25.0 metres length clearance | Travel around several sweeping bends on a gravel road | This section of road is gravel for the entirety. The road will need to be widened for the majority of the road. Typically, the road will need to be widened to 5.5 meters in all straight sections and made wider on the corners depending on the radius. A swept path analysis of this section of road, shows that the corridor would be able to stay within the road reserve. Additionally, there will need to be trees removed. The vertical curve will also need to be checked for the entirety of this road. | This section of road is gravel for the entirety. The road will need to be widened for the majority of the road. Typically, the road will need to be widened to 5.5 meters in all straight sections and made wider on the corners depending on the radius. A swept path analysis of this section of road, shows that the corridor would be able to stay within the road reserve. Additionally, there will need to be trees removed. The vertical curve will also need to be checked for the entirety of this road. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 326.0 \\ & \text { Km's } \end{aligned}$ | Hanging Rock | Morrisons Gap Road into Hills of Gold windfarm GPS link: |  | Travel directly ahead into site entrance | Windfarm to supply suitable access for the dimensions and swept path of all loads. | Windfarm to supply suitable access for the dimensions and swept path of all loads. |

### 0.0 Km's: Mayfield \#4 onto Selwyn Street at Mayfield. <br> 170 Metre rotor:



PROCEDURE: Right hand turn.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/afLwPYKuNdm
COMMENTS: Some hardstand will need to be added to the left entry up to but not past the culvert and also the exit of the corner. Some signs will need to be relocated and or made removable and some fence will need to be relocated.
A spotter will need to keep the driver informed throughout the procedure. Police and escorts to control local traffic either side of the intersection.
ROAD MODIFICATIONS: Yes, moderate amounts of work are required.

### 0.0 Km's: Mayfield \#4 onto Selwyn Street at Mayfield. 158 Metre rotor:



PROCEDURE: Right hand turn.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/afLwPYKuNdm
COMMENTS: Fence may need to be modified.
A spotter will need to keep the driver informed throughout the procedure. Police and escorts to control local traffic either side of the intersection.
ROAD MODIFICATIONS: Yes small amounts of work are required.

ROUTE STUDY Newc astle to Hills of Gold<br>Windfarm

### 0.4 Km's: Rail crossing over Selwyn Street at Mayfield.



PROCEDURE: Travel directly ahead over the crossing.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/864FhMSaF9P2
COMMENTS: Large width clearance and good ground clearance over this crossing.
Police and escorts to control local traffic either side of the crossing. ARTC approval will need to be obtained to travel over this crossing. Likely to cross with caution, no escort required.
ROAD MODIFICATIONS: No works required.

## ROUIE STUDY Newc astle to Hills of Gold <br> Windfarm

### 1.3 Km's: Selwyn Street onto Industrial Drive, via George Street at Mayfield. <br> 170 Metre rotor:



PROCEDURE: Right hand turn from Selwyn Street through George Street and onto Industrial Drive.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/brPRAckLr572
COMMENTS: The first right hand turn through George Street will need a sign made removable. Entering Industrial Drive the loads will cross from the correct side to the correct side. The traffic signal in the centre median will need to be relocated. Some hardstand will need to be placed on the south side of the intersection. spotter would need to help the load through this intersection.
ROAD MODIFICATIONS: Yes, large amounts of works are required.

## ROUIE STUDY Newc astle to Hills of Gold Windfarm

## 158 Metre rotor:



PROCEDURE: Right hand turn from Selwyn Street through George Street and onto Industrial Drive.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/brPRAckLr572
COMMENTS: Entering Industrial Drive the loads will cross from the correct side to the correct side. Some hardstand will need to be placed on the south side of the intersection. A spotter would need to help the load through this intersection.
ROAD MODIFICATIONS: Yes, moderate amounts of works are required.

ROUTE STUDY<br>Newc astle to Hills of Gold<br>Windfarm

### 4.9 Km's: Standard overhanging Traffic signals Mayfield to Hunter Expressway.



PROCEDURE: Overhanging signals while travelling through the intersection.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/5DpD3b7KnT72
COMMENTS: The lowest traffic signal on route has 5.4 metres clearance. This signal is on the corner of Steel River Blvd at Mayfield West. Loads with an overall height of 5.3 or higher, can avoid this signal by travelling in the centre lane. Loads to slow down while doing this manoeuvre. All other signals exceed 5.6 metres high on this section of road.
ROAD MODIFICATIONS: No works are required.

ROUIE STUDY Newc astle to Hills of Gold<br>Windfarm

### 5.5 Km's: Industrial Drive onto Maitland Road at Mayfield West.

170 Metre rotor:


PROCEDURE: Right hand turn from Industrial Drive onto Maitland Road.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/Kn49dhWG2qG2
COMMENTS: The loads will need to cross to the incorrect side of the intersection, before crossing back over 200 metres to the north.
Spotter to keep the driver informed throughout the procedure.
Police and escorts to control local traffic either side of the intersection.
ROAD MODIFICATIONS: Nil.

ROUIE STUDY Newc astle to Hills of Gold<br>Windfarm

158 Metre rotor:


PROCEDURE: Right hand turn from Industrial Drive onto Maitland Road.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/Kn49dhWG2qG2
COMMENTS: The loads will need to cross to the incorrect side of the intersection, before crossing back over 200 metres to the north. The centre median strip will need to be modified so the trucks can cross over safely.
Spotter to keep the driver informed throughout the procedure.
Police and escorts to control local traffic either side of the intersection.
ROAD MODIFICATIONS: Nil.

ROUIE STUDY Newc astle to Hills of Gold Windfarm

13.9 Km's: Lowest structure (Bridge or Sign) between Mayfield and the Hunter Expressway.
Image 1:


PROCEDURE: Travel directly ahead in the centre lane.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/YTMoFe7Aick
COMMENTS: This is the lowest structure on route. There is no bypass around the gantry. A maximum loaded height of 5.8 metres should not be exceeded.
ROAD MODIFICATIONS: No works are required.

ROUIE STUDY Newc astle to Hills of Gold Windfarm

18.4 Km's: Intersection of John Renshaw Drive and M1 at Beresfield.
170 Metre rotor and 158 Metre rotor:


PROCEDURE: Travel directly ahead in the centre lane.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/MYSBciVvcwB2
COMMENTS: The roundabout has been demolished. The new intersection has 2 lanes
directly ahead with a width clearance of 9.0 metres.
ROAD MODIFICATIONS: No works are required.
28.7 Km's: John Renshaw Drive onto the Hunter Expressway at Buchanan.

170 Metre rotor:


## ROUIE STUDY Newc astle to Hills of Gold Windfarm

## 170 Metre rotor:



PROCEDURE: Right hand turn onto the incorrect side of the Motorway, before crossing back onto the correct side at the crossover bay.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/FH5DqHBXwSkntAmz9
COMMENTS: Cross to the incorrect side than down the off-ramp onto the incorrect side of the expressway. Approx 600 metres along the expressway there is a break in the road, which will allow the blades to cross back to the correct side of the expressway. Traffic control and or police will be required to perform this procedure.
ROAD MODIFICATIONS: No works required.

ROUIE STUDY Newc astle to Hills of Gold Windfarm

## 158 Metre rotor:



PROCEDURE: Travel around the roundabout and take the third exit onto the Hunter
Expressway onramp.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/cEnuC5th1p52
COMMENTS: A sign will need to be made removable. Spotter to guide load through this pinchpoint.
ROAD MODIFICATIONS: No works required.

ROUTE STUDY<br>Newc astle to Hills of Gold Windfarm

67.3 Km's: New England Highway onto Golden Highway at Whittingham.
Image 1: Proposed upgrades


## 170 Metre rotor:



PROCEDURE: Left hand turn from the New England Highway onto the Golden Highway. GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/GZ3VbkLrKf42
COMMENTS: Loads to turn from the incorrect side to the incorrect side. The signs in the center median will need to be made removable.
ROAD MODIFICATIONS: NOTE: This intersection is currently in line to be upgraded.
The details on image 1 shows that the changes should not affect the swept path, however it is recommended that this is monitored.

# ROUIE STUDY Newc astle to Hills of Gold <br> Windfarm 

## 158 Metre rotor:



PROCEDURE: Left hand turn from the New England Highway onto the Golden Highway.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/GZ3VbkLrKf42
COMMENTS: Loads to turn from the incorrect side to the incorrect side. The signs in the center median will need to be made removable.

ROAD MODIFICATIONS: NOTE: This intersection is currently in line to be upgraded.
The details on image 1 shows that the changes should not affect the swept path, however it is recommended that this is monitored.

ROUTE STUDY Newc astle to Hills of Gold Windfarm

77.3 Km's: Golden Highway intersection with Putty Road at Whittingham.
170 Metre rotor:


# ROUIE STUDY Newc astle to Hills of Gold <br> Windfarm 

## 158 Metre rotor:



PROCEDURE: Left hand turn from the Golden Highway at the intersection of the Putty Road.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/esuS6TUUwQ92
COMMENTS: Loads to turn from the incorrect side to the incorrect side. Spotter to keep the driver informed throughout the procedure.
Police and escorts to control local traffic either side of the intersection.
ROAD MODIFICATIONS: No works required.

## ROUIE STUDY Newc astle to Hills of Gold Windfarm

80.8 Km's: Golden Highway intersection with Putty Road at Mount Thorley.
170 Metre rotor:


Image 2:


PROCEDURE: Right hand turn from the Putty Road onto the Golden Highway.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/Qj4tjSSjN932
COMMENTS: Loads to turn from the incorrect side to the incorrect side. Blades to cross to the incorrect side prior to the intersection, and return to the correct side when the lanes remerge. Spotter to keep the driver informed throughout the procedure.
Police and escorts to control local traffic either side of the intersection.
NOTE: Towers and general loads will travel under the overpass and stay on the correct side of the road. The overpass is 5.6 in the center of the road. Loads that exceed 5.6 high will need to take the blade detour.
ROAD MODIFICATIONS: No works required.

## 158 Metre rotor



PROCEDURE: Right hand turn from the Putty Road onto the Golden Highway.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/Qj4tjSSjN932
COMMENTS: Loads to turn from the incorrect side to the incorrect side. Blades to cross to the incorrect side prior to the intersection, and return to the correct side when the lanes remerge. Spotter to keep the driver informed throughout the procedure.
Police and escorts to control local traffic either side of the intersection.
NOTE: Towers and general loads will travel under the overpass and stay on the correct side of the road. The overpass is 5.6 in the center of the road. Loads that exceed 5.6 high will need to take the blade detour.
ROAD MODIFICATIONS: No works required.

ROUIE STUDY Newc astle to Hills of Gold Windfarm

107.0 Km's: Golden Highway through Jerrys Plains.

170 Metre rotor:


ROUIE STUDY Newc astle to Hills of Gold Windfarm

## 170 Metre rotor:



PROCEDURE: Right and left hand turn through the village.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/AiuT8MMVTh5crs348
COMMENTS: Blades to cross from the incorrect side to the incorrect side. Some hardstand needs to be added to the outside of the corner for the right-hand turn. The swept path will stay within the existing road reserve.
Police and escorts to control local traffic either side of the intersection.
ROAD MODIFICATIONS: Moderate amounts of work are required.

## ROUIE STUDY Newc astle to Hills of Gold Windfarm

158 Metre rotor:


ROUIE STUDY Newc astle to Hills of Gold Windfarm

158 Metre rotor:


PROCEDURE: Right and left hand turn through the village.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/AiuT8MMVTh5crs348
COMMENTS: Blades to cross from the incorrect side to the incorrect side. Police and escorts to control local traffic either side of the intersection.
ROAD MODIFICATIONS: No works required.

ROUIE STUDY Newc astle to Hills of Gold Windfarm

### 141.9 Km's: Golden Highway intersection with Denman Road at Denman.

170 Metre rotor:


PROCEDURE: Right hand turn from the Golden Highway at the intersection of Denman Road.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/T4m46bBNuro
COMMENTS: Blades to cross from the correct side to the correct side. Some signs will need to be made removable and some hardstand added to the outside exit of the turn. Police and escorts to control local traffic either side of the intersection. Loads swept path will stay within the road reserve.

ROAD MODIFICATIONS: Moderate amounts of work are required.

Newc astle to Hills of Gold Windfarm

## 158 Metre rotor:



PROCEDURE: Right hand turn from the Golden Highway at the intersection of Denman
Road.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/T4m46bBNuro
COMMENTS: Blades to cross from the correct side to the correct side. Some signs will need to be made removable. Police and escorts to control local traffic either side of the intersection.
ROAD MODIFICATIONS: Small amounts of work are required.

ROUIE STUDY Newc astle to Hills of Gold<br>Windfarm

### 149.0 Km's: Denman Road onto Bengalla Road at Muswellbrook.

170 Metre rotor:


PROCEDURE: Left hand turn from Denman Road onto Bengalla Road.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/CJYMtSMTttJ2
COMMENTS: Blades to cross from the incorrect side to the incorrect side. Some signs will need to be made removable and some hardstand added to the inside of the corner as well as a fence removed. Loads swept path will enter a landowner's boundaries on the inside of the corner.
Police and escorts to control local traffic either side of the intersection.
ROAD MODIFICATIONS: Moderate amounts of work are required.

# ROUIE STUDY Newc astle to Hills of Gold Windfarm 

## 158 Metre rotor:



PROCEDURE: Left hand turn from Denman Road onto Bengalla Road.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/CJYMtSMTttJ2
COMMENTS: Blades to cross from the incorrect side to the incorrect side. Police and escorts to control local traffic either side of the intersection.

ROAD MODIFICATIONS: No works required.

Newc astle to Hills of Gold<br>Windfarm

### 158.5 Km's: Bengalla Road onto Wybong Road at Muswellbrook.

170 Metre rotor:


PROCEDURE: Right hand turn from Bengalla Road onto Wybong Road.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/vibQtvHkxXE2
COMMENTS: Blades to cross from the correct side to the correct side. Some signs will need to be made removable. Police and escorts to control local traffic either side of the intersection.

ROAD MODIFICATIONS: Small amounts of work are required.

ROUIE STUDY Newc astle to Hills of Gold Windfarm

158 Metre rotor:


PROCEDURE: Right hand turn from Bengalla Road onto Wybong Road.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/vibQtvHkxXE2
COMMENTS: Blades to cross from the correct side to the correct side. Some signs will need to be made removable. Police and escorts to control local traffic either side of the intersection.

ROAD MODIFICATIONS: Small amounts of work are required.

ROUTE STUDY Newc astle to Hills of Gold<br>Windfarm

### 168.1 Km's: Wybong Road onto Kayuga Road at Muswellbrook. OPTION 1 <br> 170 Metre rotor:



PROCEDURE: Left hand turn from Wybong Road onto Kayuga Road.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/xVscKUT1isJ2
COMMENTS: Blades to cross from the incorrect side to the incorrect side with the load travelling across the inside of the telegraph pole and through private land.
Permission will be required from the landowner to travel over the private land. This will require removal and realigning the fence and adding hardstand.
Police and escorts to control local traffic either side of the intersection.
ROAD MODIFICATIONS: Large amounts of work are required.

## 158 Metre rotor:



PROCEDURE: Left hand turn from Wybong Road onto Kayuga Road.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/xVscKUT1isJ2
COMMENTS: Blades to cross from the incorrect side to the incorrect side. Permission will be required from the landowner to travel over the private land. This will require removal and realigning the fence and adding hardstand. Police and escorts to control local traffic either side of the intersection.

ROAD MODIFICATIONS: Large amounts of work are required.

ROUIE STUDY Newc astle to Hills of Gold Windfarm

### 174.0 Km's: Ivermein Street onto Dartbrook access Road at Muswellbrook.

170 Metre rotor:


PROCEDURE: Right hand turn from Ivermain Street onto the Dartbrook mine access Road.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/ddMHa4CmXK32
COMMENTS: Blades to cross from the correct side to the correct side. Some signs will need to be made removable and some hardstand added to the inside and outside of the corner.
Additionally, a drainage pipe will need to be extended on the inside of the corner.
Police and escorts to control local traffic either side of the intersection.
ROAD MODIFICATIONS: Moderate amounts of work are required.

ROUIE STUDY Newc astle to Hills of Gold<br>Windfarm

158 Metre rotor:


PROCEDURE: Right hand turn from Ivermain Street onto the Dartbrook mine access Road. GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/ddMHa4CmXK32
COMMENTS: Blades to cross from the correct side to the correct side. Some signs will need to be made removable and some hardstand added to the inside and outside of the corner. Additionally, a drainage pipe will need to be extended on the inside of the corner. Police and escorts to control local traffic either side of the intersection.

ROAD MODIFICATIONS: Moderate amounts of work are required.

### 174.8 Km's: Dartbrook access Road at Muswellbrook.

## 170 Metre rotor:



PROCEDURE: Right hand turn on the Dartbrook mine access Road.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/u9vSXiSV7Jt
COMMENTS: Blades to cross from the correct side to the correct side, but cut across the inside of the corner. Some signs will need to be made removable and some hardstand added to the inside of the corner. Police and escorts to control local traffic either side of the intersection.
ROAD MODIFICATIONS: Moderate amounts of work are required.

158 Metre rotor:


PROCEDURE: Right hand turn on the Dartbrook mine access Road.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/u9vSXiSV7Jt
COMMENTS: Blades to cross from the correct side to the correct side, but cut across the inside of the corner. Some signs will need to be made removable and some hardstand added to the inside of the corner. Police and escorts to control local traffic either side of the intersection.
ROAD MODIFICATIONS: Small amounts of work are required.

ROUIE STUDY Newc astle to Hills of Gold<br>Windfarm

### 177.0 Km's: Dartbrook access Road onto the New England Highway at Muswellbrook. <br> 170 Metre rotor:



PROCEDURE: Left hand turn from the Dartbrook mine access Road onto the New England Highway.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/twTsmUKaED82
COMMENTS: Blades to cross from the incorrect side to the incorrect side. Some signs will need to be made removable on the corner and some hardstand added. Police and escorts to control local traffic either side of the intersection.
ROAD MODIFICATIONS: Moderate amounts of work are required.

ROUIE STUDY<br>Newc astle to Hills of Gold<br>Windfarm

158 Metre rotor:


PROCEDURE: Left hand turn from the Dartbrook mine access Road onto the New England Highway.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/twTsmUKaED82
COMMENTS: Blades to cross from the incorrect side to the incorrect side. Some signs will need to be made removable on the corner and some hardstand added. Police and escorts to control local traffic either side of the intersection.
ROAD MODIFICATIONS: Moderate amounts of work are required.

ROUIE STUDY<br>Newc astle to Hills of Gold<br>Windfarm

276.0 Km's: New England Highway onto Lindsay’s Gap Road at Wallabadah.
170 Metre rotor:


PROCEDURE: Right hand turn from the New England Highway onto Lindsay's Gap Road. GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/ePbYctjJootkBZiM9
COMMENTS: Blades to cross from the correct side to the correct side but cut across the inside of the corner. Some signs will need to be made removable and some hardstand added to the inside of the corner.
ROAD MODIFICATIONS: Moderate amounts of work are required.

## ROUTE STUDY <br> Newc astle to Hills of Gold <br> Windfarm

## 158 Metre rotor:



PROCEDURE: Right hand turn from the New England Highway onto Lindsay's Gap Road. GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/ePbYctjJootkBZiM9 COMMENTS: Blades to cross from the correct side to the correct side but cut across the inside of the corner. Some signs will need to be made removable.
ROAD MODIFICATIONS: Small amounts of work are required.

ROUIE STUDY Newc astle to Hills of Gold Windfarm

### 287.7 Km's: Lindsay’s Gap Road over Goonoo Goonoo Creek at Garoo.

Image 1:


PROCEDURE: Travel directly ahead in the centre of the bridge.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/9ELSk5ZLRWnf14tm7
COMMENTS: The blades will fit over the structure in its current condition.
Loads that are been carried on trailers with an axle width exceeding 3.5 meters will not fit over this structure in its current form.
This bridge will need to be replaced or modified before the towers or motors can be delivered on this route.
A trafficable deck width of at least 4.6 meters is required for these heavier loads. And possibly turn the bridge into dual lane.
ROAD MODIFICATIONS: Yes, a large amount of works is required.

ROUIE STUDY
295.7 Km's: Lindsay’s Gap Road over Middlebrook Creek at Garoo.
Image 1:


ROUIE STUDY Newc astle to Hills of Gold Windfarm

Image 2:


PROCEDURE: Travel directly ahead in the centre of the bridge before entering a right-hand bend.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/DyxGUid9JucoAHhHA COMMENTS: The blades will fit over the structure in its current condition.
Loads that are been carried on trailers with an axle width exceeding 3.5 meters will not fit over this structure in its current form.
This bridge will need to be replaced or modified before the towers or motors can be delivered on this route. A trafficable deck width of at least 4.6 meters is required for these heavier loads. And possibly turn the bridge into dual lane.
ROAD MODIFICATIONS: Yes, a large amount of works is required.

ROUIE STUDY Newc astle to Hills of Gold Windfarm

306.8 Km's: Lindsay's Gap Road onto Nundle Road at Nundle.

170 Metre rotor:


PROCEDURE: Right hand turn from Lindsay's Gap Road onto Nundle Road.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/FX4ZRx2YG9i2BsXMA
COMMENTS: Blades to cross from the correct side to the correct side but cut across the inside of the corner. Some signs will need to be made removable and some hardstand added to the inside of the corner. A power pole will also need to be relocated.
ROAD MODIFICATIONS: Large amounts of work are required.

## ROUIE STUDY Newc astle to Hills of Gold Windfarm

## 158 Metre rotor:



PROCEDURE: Right hand turn from Lindsay's Gap Road onto Nundle Road.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/FX4ZRx2YG9i2BsXMA COMMENTS: Blades to cross from the correct side to the correct side but cut across the inside of the corner. Some signs will need to be made removable.
ROAD MODIFICATIONS: Small amounts of work are required.

ROUIE STUDY<br>Newc astle to Hills of Gold<br>Windfarm

### 311.0 Km's: Oakenville Street at Nundle.

170 Metre rotor and 158 Metre rotor:


PROCEDURE: Travel directly ahead on Oakenville Street.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/7YM56hQq8bnCSoZy8
COMMENTS: Blades to travel directly ahead on the correct side of the road. A no parking exclusion zone will need to be placed on the left-hand side while travelling through this intersection. Two signs will also need to be made removable.
ROAD MODIFICATIONS: Small amounts of work are required.

ROUTE STUDY<br>Newc astle to Hills of Gold<br>Windfarm

### 312.0 Km's: Oakenville Street onto Hanging Rock Road at Nundle. <br> 170 Metre rotor:



PROCEDURE: Left hand turn from Oakenville Street onto Old Hanging Rock Road. GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/dTVzsVzuaY1qvLHd7 COMMENTS: Blades to turn left from the incorrect side to the incorrect side of the road. The swept path will have the blades travel through a landowner's boundaries. This will require a fence to be relocated and hardstand added. Additionally, while travelling over the bridge some signs will need to be relocated and some sections of guardrail relocated.
ROAD MODIFICATIONS: Large amounts of work are required.

# Newc astle to Hills of Gold <br> Windfarm 

## 313.0 to 323.0 Km's: Barry’s Gap Road from Nundle to Hanging Rock.

170 Metre rotor:
Image 1: Looking east towards Devils Elbow.


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Image 2: (Proposed bypass of Devils Elbow).


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Image 3: (Upgrades on Barrys Road).


PROCEDURE: Travel directly ahead on Barrys Road.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/BUBe2MCfoQ215qKE6
COMMENTS: Barrys Road has a section of road known as the Devils Elbows. The existing hairpin corners are impassable for the blades, towers and motors. A detour of the Devils Elbow as per Image 3 has been looked at and will likely be the best solution for all loads. If the gradient of this new detour exceeds $14 \%$ than it will need to be sealed.
To the west and east of the Devils Elbows the road will need to be widened on a few corners, this would include hardstand and tree removal.
ROAD MODIFICATIONS: Large amounts of work are required.

ROUIE STUDY Newc astle to Hills of Gold<br>Windfarm

### 323.0 Km’s: Barrys Road onto Morrisons Gap Road.

## 170 Metre rotor:



PROCEDURE: Right hand turn from Barrys Road onto Morrisons Gap Road.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/CLZDJSjENx8rjfAg7
COMMENTS: Blades to turn left from the correct side to the correct side of the road. The swept path will have the blades travel through a landowner's boundaries on the inside of the corner. This will require a fence to be relocated and hardstand added. Additionally, some trees will need to be removed.
ROAD MODIFICATIONS: Large amounts of work are required.

ROUIE STUDY
Newc astle to Hills of Gold
Windfarm

## 158 Metre rotor:



PROCEDURE: Right hand turn from Barrys Road onto Morrisons Gap Road.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/CLZDJSjENx8rjfAg7
COMMENTS: Blades to turn left from the correct side to the correct side of the road. The swept path will have the blades travel through a landowner's boundaries on the inside of the corner. This will require a fence to be relocated and hardstand added. Additionally, some trees will need to be removed.
ROAD MODIFICATIONS: Large amounts of work are required.

ROUIE STUDY Newc astle to Hills of Gold Windfarm

323.0 to 326.0 Km's: Morrisons Gap Road at Hanging Rock. 170 Metre rotor and 158 Metre rotor: Image 1: (Looking along Morrisons Gap Road from Barry Road)


Image 2: (Swept path staying within the road reserve)


REX JANDREWS
ENGINEERED TRANSPORTATION

Image 3: (Swept path staying within the road reserve)


Image 4: (Swept path staying within the road reserve)


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Image 5: (Swept path staying on existing road).


Image 6: (Swept path staying on existing road).


ROUIE STUDY Newc astle to Hills of Gold<br>Windfarm

Image 7: (Swept path staying on existing road).


PROCEDURE: Travel directly ahead on Morrisons Gap Road.
GPS LINK FOR SECTION OF ROAD: https://goo.gl/maps/kLtYYnmhTgvE6ZPFA COMMENTS: This section of road is gravel for the entirety. The road will need to be widened for the majority of the road. Typically, the road will need to be widened to 5.5 meters in all straight sections and made wider on the corners depending on the radius. A swept path analysis of this section of road, shows that the corridor would be able to stay within the road reserve. Additionally, there will need to be trees removed. The vertical curve will also need to be checked for the entirety of this road.
ROAD MODIFICATIONS: Large amounts of work are required.

NOTE: From this point on all access roads through to final delivery points will need to be made suitable for the swept path of the largest items. These access roads will also need to be made with suitable gradients and vertical curves.

ROUTE STUDY<br>Newc astle to Hills of Gold<br>Windfarm

### 11.0 Route Survey B: Newcastle port to Hills of Gold WF for loads up to 5.2 metres in height.

Distance: (284.0 Kilometres).
Via: Selwyn Street, George Street, Industrial Drive, Maitland Road, New England Highway, John Renshaw Drive, Hunter Expressway, New England Highway, Bell Street, Victoria Street, Market Street, New England Highway, Lindsays Gap Road, Nundle Road, Crosby Street, Oakenville Street, Old Hanging Rock Road, Barry Road, Morrisons Gap Road. GPS Link: https://goo.gl/maps/rouAWyxLZ53pMB3v7


ROUIE STUDY

| KEY |  |
| :---: | :---: |
| MODIFICATIONS REQUIRED |  |
| MINOR WORKS OR CAUTION |  |
| PARKING |  |


| $\begin{gathered} \text { KM } \\ \text { index } \end{gathered}$ | Location | Section of road | Critical Measurement | Procedure | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Route Index |  |  |  |  |  |
| 0.0 | Mayfield | Mayfield \#4 berth onto Selwyn Street GPS link: <br> https://goo.gl/maps/afLwPYKuNdm | Clearance: <br> Length: 70.0 metres <br> Width: 8.0 metres | Right hand turn | No problems with this section of road. |
| 0.4 | Mayfield | Selwyn Street rail crossing GPS link: https://goo.gl/maps/AmohE54hKSz | Clearance: <br> Width: 9.0 metres | Travel directly ahead | Loads to travel over the crossing in the center of the road. Approval required crossing this line, likely cross with caution. |
| 1.3 | Mayfield | Selwyn Street onto George Street GPS link: <br> https://goo.gl/maps/gXeHvBtCp4D2 | Clearance: <br> Length: 70.0 metres <br> Width: 8.0 metres | Right hand turn | No problems with this section of road. |
| 1.4 | Mayfield | George Street onto Industrial Drive https://goo.gl/maps/s4ayrsuoAsD2 | Clearance: <br> Length: 70.0 metres <br> Width: 8.0 metres | Moderate right hand turn | No problems with this section of road. |
| 4.9 | Mayfield | Industrial Drive under traffic signals GPS link: <br> https://goo.gl/maps/YmqhiS2iR582 | Clearance: <br> Height: 5.4 Metres | Travel directly ahead | The lowest traffic signal on route is at the intersection of Steel River Blvd. Trucks that exceed 5.3 metres will need to travel in the right hand lane. |
| 5.5 | Mayfield West | Industrial Drive onto Maitland Road GPS link: <br> https://goo.gl/maps/Kn49dhWG2qG2 | Clearance: <br> Length: 50.0 metres <br> Width: 10.0 metres | Right hand turn | No problems with this section of road. |
| 13.9 | Hexham | New England Highway under gantry GPS link: https://goo.gl/maps/YTMoFe7Aick | Clearance: <br> Height: 5.95 Metres | Travel directly ahead | This is the lowest structure on route. There is no bypass around the gantry. A maximum loaded height of 5.8 metres should not be exceeded. |
| 17.4 | Tarro | New England Highway onto John Renshaw Drive GPS link: https://goo.gl/maps/SRDr5JigkBp | Clearance: <br> Width: 12.0 metres | Left hand merge | No problems with this section of road. |
| 18.4 | Beresfield | John Renshaw Drive GPS link: https://goo.gl/maps/N19vJih1Fgr | Clearance: <br> Width: 9.0 metres <br> Height: 5.9 metres | Travel directly ahead | No problems with this section of road. |
| 28.7 | Buchanan | John Renshaw Drive onto the Hunter Expressway <br> GPS link: <br> https://goo.gl/maps/1STJ1PfQt9E2 | Clearance: <br> Length: 65.0 metres <br> Width: 7.0 metres | Right hand turn | No problems with this section of road. |

# ROUIE STUDY Newc astle to Hills of Gold <br> Windfarm 

| $\begin{gathered} \text { KM } \\ \text { index } \end{gathered}$ | Location | Section of road | Critical Measurement | Procedure | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 59.0 | Branxton | The Hunter Expressway onto The New England Highway <br> GPS link: <br> https://goo.gl/maps/7rauNuxzqja | Clearance: <br> Width: 9.0 metres | Travel directly ahead | No problems with this section of road. |
| 124.5 | Muswellbrook | New England Highway onto Bell Street GPS link: <br> https://goo.gl/maps/H94bMYQMeSHay7918 | Clearance: <br> Length: 40.0 metres <br> Width: 6.0 metres | Right hand turn | No problems with this section of road. |
| 125.0 | Muswellbrook | Bell Street onto Victoria Street GPS link: $\qquad$ | Clearance: <br> Length: 40.0 metres <br> Width: 7.0 metres | Left hand corners | Tight left-hand bend over a rail bridge before another tight left hand bend. <br> Spotter to guide loads through this section of road, and approval from rail required to cross this structure. |
| 125.5 | Muswellbrook | Victoria Street onto Market Street GPS link: <br> https://goo.gl/maps/pyiTUH25bANG3m9n9 | Clearance: <br> Width: 7.0 metres | Travel directly ahead | No problems with this section of road. |
| 126.0 | Muswellbrook | Market Street onto New England Highway GPS link: <br> https://goo.gl/maps/3kpU6XdCBmCW75gM7 | Clearance: <br> Length: 30.0 metres <br> Width: 7.0 metres | Right hand turn at roundabout | Loads may need to cross to the incorrect side of the roundabout if they exceed 30.0 meters in length, and do not exceed 42 meters in length. |
| 201.8 | Murrurundi | New England highway (Township) GPS link: <br> https://goo.gl/maps/Sj3ixAkhujt | Clearance: $60.0 \times 5.0$ metres | Parking Bay | Suitable parking for Fatigue breaks. |
| 206.4 | Murrurundi Hill | New England highway Nowlands Gap GPS link: <br> https://goo.gl/maps/R5yufobPeMG2 | Clearance: <br> $120.0 \times 12.0$ metres | Parking Bay (small ) | Emergency parking only. |
| 203.0 | Willow Tree | New England highway <br> GPS link: <br> https://goo.gl/maps/XLTg7CRV7EU2 | Clearance: <br> Width: 7.0 metres <br> Length: 35 metres <br> Height: 5.2 metres | Kankool weighbridge | It is likely that the towers and defiantly the blades will not fit into this facility. We have engineered documentation showing correct weights for all loads. |
| 208.9 | Willow Tree Township | New England highway <br> GPS link: <br> https://goo.gl/maps/gw38qmvVfTC2 | Clearance: $60.0 \times 5.0$ metres | Parking Bay | Suitable parking for Fatigue breaks. |
| 210.5 | Willow Tree Truck Stop N | New England highway <br> GPS link: <br> https://goo.gl/maps/RRdPVHupGCs | Clearance: <br> $120.0 \times 12.0$ metres | Parking Bay ( small ) | Suitable parking for Fatigue breaks for small loads only. |
| 230.0 | Wallabadah | New England highway GPS link: <br> https://goo.gl/maps/QWCyeHQSohS2 | Clearance: $80.0 \times 5.0$ metres | Parking Bay (side of road) | Suitable parking for Fatigue breaks. |
| 235.0 | Wallabadah | New England highway onto Lindsay's Gap Road GPS link: <br> https://goo.gl/maps/ePbYctjJootkBZiM9 | Clearance: <br> Length: 50.0 metres | Right hand turn | If the upgrades are completed for the blades than this corner will be suitable for the remaining components. |

## ROUIE STUDY Newc astle to Hills of Gold Windfarm

| $\begin{gathered} \text { KM } \\ \text { index } \end{gathered}$ | Location | Section of road | Critical Measurement | Procedure | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 245.7 | Garoo | Lindsay's Gap Road over Goonoo Goonoo Creek GPS link: $\qquad$ | Clearance: <br> Axle width: 3.60 m <br> Overall width: 6.20 m <br> Guard rail height: 850 mm | Travel directly ahead over bridge in the centre of the road. | Loads that are been carried on trailers with an axle width exceeding 3.5 meters will not fit over this structure in its current form. <br> This bridge will need to be replaced or modified before the towers or motors can be delivered on this route. <br> A trafficable deck width of at least 4.6 meters is required for these heavier loads. |
| 253.7 | Garoo | Lindsay's Gap Road over Middlebrook Creek GPS link: https://goo.gl/maps/DyxGUid9JucoAHhHA | Clearance: <br> Axle width: 4.50 m <br> Overall width: 6.10 m <br> Guard rail height: <br> 750 mm | Travel directly ahead over bridge in the centre of the road. | Loads that are been carried on trailers with an axle width exceeding 3.5 meters will not fit over this structure in its current form. <br> This bridge will need to be replaced or modified before the towers or motors can be delivered on this route. |
| 259.2 | Garoo | Lindsay's Gap Road through Lindsay's Gap <br> GPS link: <br> https://goo.gl/maps/GGKmqemziKdth8wH9 | Clearance: <br> Length: 90.0 metres | Travel directly ahead | Load to travel in the centre of the road, escorts to warn traffic 500 metres to the east of the gap. |
| 264.8 | Nundle | Lindsay's Gap Road onto Nundle Road GPS link: <br> https://goo.gl/maps/FX4ZRx2YG9i2BsXMA | Clearance: <br> Length: 50.0 metres | Right hand turn | If the upgrades are completed for the blades than this corner will be suitable for the remaining components. |
| 268.3 | Nundle | Nundle Road onto Crosby Street GPS link: <br> https://goo.gl/maps/uVvcN9QkPyTDP1YR6 | Clearance: <br> Width: 8.0 metres | Travel directly ahead | No problems with this section of road. |
| 268.6 | Nundle | Crosby Street onto Oakenville Street GPS link: <br> https://goo.gl/maps/aZNDKURdSBERedMr9 | Clearance: <br> Width: 8.0 metres | Travel directly ahead | No problems with this section of road. |
| 269.0 | Nundle | Oakenville Street and Jenkins Street intersection <br> GPS link: <br> https://goo.gl/maps/7YM56hQq8bnCSoZy8 | 5.0 metres width clearance |  | A no parking exclusion zone will need to be placed on the lefthand side while travelling through this intersection. Two signs will also need to be made removable. |
| 270.0 | Nundle | Oakenville Street onto Old Hanging Rock GPS link: <br> https://goo.gl/maps/1UMr2EwZetiE76Ey9 | 35.0 metres length clearance | Left hand turn | If the upgrades are completed for the blades than this corner will be suitable for the remaining components. |
| 271.0 | Nundle | Old Hanging Rock Road onto Barry Road GPS link: <br> https://goo.gl/maps/ve9zvmdJnLBYtQSz5 | 90.0 metres clearance | Right hand bend | No problems with this section of road. |


| $\begin{gathered} \text { KM } \\ \text { index } \end{gathered}$ | Location | Section of road | Critical Measurement | Procedure | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 271.0 \text { to } \\ & 281.0 \\ & \text { Km's } \end{aligned}$ | Nundle to Hanging Rock | Barrys Road <br> https://goo.gl/maps/BUBe2MCfoQ215qKE6 | 25.0 metres length clearance | Travel directly ahead through multiple tight turns and steep terrain | As per the blades Barrys Road has a section of road known as the Devils Elbows. The existing hairpin corners are impassable for the blades, towers and motors. A detour of the Devils Elbow has been looked at and will likely be the best solution for all loads. <br> To the west and east of the Devils Elbows the road will need to be widened on a few corners, this would include hardstand and tree removal. |
| 281.0 | Hanging Rock | Barrys Road onto Morrisons Gap Road GPS link: <br> https://goo.gl/maps/CLZDJSjENx8rifAg7 | 35.0 metres length clearance | Right hand turn | Blades to turn right from the correct side to the correct side of the road. The swept path will have the blades travel through a landowner's boundaries on the inside of the corner. This will require a fence to be relocated and hardstand added. <br> Additionally, some trees will need to be removed. |
| $\begin{aligned} & 281.0 \text { to } \\ & 284.0 \\ & \text { Km's } \end{aligned}$ | Hanging Rock | Morrisons Gap Road GPS link: <br> https://goo.gl/maps/kLtYYnmhTgvE6ZPFA | 25.0 metres length clearance | Travel around several sweeping bends on a gravel road | This section of road is gravel for the entirety. The road will need to be widened for the majority of the road. Typically, the road will need to be widened to 5.5 meters in all straight sections and made wider on the corners depending on the radius. A swept path analysis of this section of road, shows that the corridor would be able to stay within the road reserve. <br> Additionally, there will need to be trees removed. The vertical curve will also need to be checked for the entirety of this road. |
| $\begin{aligned} & 284.0 \\ & \text { Km's } \end{aligned}$ | Hanging Rock | Morrisons Gap Road into Hills of Gold windfarm <br> GPS link: <br> https://goo.gl/maps/5VFMQCB3drgXcjyU8 |  | Travel directly ahead into site entrance | Windfarm to supply suitable access for the dimensions and swept path of all loads. |

ROUTE STUDY<br>Newc astle to Hills of Gold<br>Windfarm

### 12.0 Route Survey C: Newcastle port to Hills of Gold WF for loads over 5.2 metres in height.

Distance: (328.0 Kilometres).
Via: Selwyn Street, George Street, Industrial Drive, Maitland Road, New England Highway, John Renshaw Drive, Hunter Expressway, New England Highway, Golden Highway, Denman Road, Thomas Mitchell Drive, New England Highway, Bell Street, Victoria Street, Market Street, New England Highway, Lindsays Gap Road, Nundle Road, Crosby Street, Oakenville Street, Old Hanging Rock Road, Barry Road, Morrisons Gap Road.
GPS Link: https://goo.gl/maps/tMkKEEQKNL7azUDi7


ROUIE STUDY

| KEY |  |
| :---: | :---: |
| MODIFICATIONS REQUIRED |  |
| MINOR WORKS OR CAUTION |  |
| PARKING |  |


| $\begin{gathered} \text { KM } \\ \text { index } \end{gathered}$ | Location | Section of road | Critical <br> Measurement | Procedure | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Route Index |  |  |  |  |  |
| 0.0 | Mayfield | Mayfield \#4 berth onto Selwyn Street GPS link: <br> https://goo.gl/maps/afLwPYKuNdm | Clearance: <br> Length: 70.0 metres <br> Width: 8.0 metres | Right hand turn | No problems with this section of road. |
| 0.4 | Mayfield | Selwyn Street rail crossing GPS link: https://goo.gl/maps/AmohE54hKSz | Clearance: <br> Width: 9.0 metres | Travel directly ahead | Loads to travel over the crossing in the center of the road. Approval required crossing this line, likely cross with caution. |
| 1.3 | Mayfield | Selwyn Street onto George Street GPS link: https://goo.gl/maps/gXeHvBtCp4D2 | Clearance: <br> Length: 70.0 metres <br> Width: 8.0 metres | Right hand turn | No problems with this section of road. |
| 1.4 | Mayfield | George Street onto Industrial Drive https://goo.gl/maps/s4ayrsuoAsD2 | Clearance: <br> Length: 70.0 metres <br> Width: 8.0 metres | Moderate right hand turn | No problems with this section of road. |
| 4.9 | Mayfield | Industrial Drive under traffic signals GPS link: https://goo.gl/maps/YmqhiS2iR582 | Clearance: <br> Height: 5.4 Metres | Travel directly ahead | The lowest traffic signal on route is at the intersection of Steel River Blvd. Trucks that exceed 5.3 metres will need to travel in the right hand lane. |
| 5.5 | Mayfield West | Industrial Drive onto Maitland Road GPS link: https://goo.gl/maps/Kn49dhWG2qG2 | Clearance: <br> Length: 50.0 metres <br> Width: 10.0 metres | Right hand turn | No problems with this section of road. |
| 13.9 | Hexham | New England Highway under gantry GPS link: https://goo.gl/maps/YTMoFe7Aick | Clearance: <br> Height: 5.95 Metres | Travel directly ahead | This is the lowest structure on route. There is no bypass around the gantry. A maximum loaded height of 5.8 metres should not be exceeded. |
| 17.4 | Tarro | New England Highway onto John Renshaw Drive GPS link: <br> https://goo.gl/maps/SRDr5JigkBp | Clearance: <br> Width: 12.0 metres | Left hand merge | No problems with this section of road. |
| 18.4 | Beresfield | John Renshaw Drive GPS link: https://goo.gl/maps/N19vJih1Fgr | Clearance: <br> Width: 9.0 metres <br> Height: 5.9 metres | Travel directly ahead | No problems with this section of road. |
| 28.7 | Buchanan | John Renshaw Drive onto the Hunter Expressway <br> GPS link: https://goo.gl/maps/1STJ1PfQt9E2 | Clearance: <br> Length: 65.0 metres <br> Width: 7.0 metres | Right hand turn | No problems with this section of road. |


| $\begin{gathered} \text { KM } \\ \text { index } \end{gathered}$ | Location | Section of road | Critical Measurement | Procedure | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 59.0 | Branxton | The Hunter Expressway onto The New England Highway <br> GPS link: <br> https://goo.gl/maps/7rauNuxzqjq | Clearance: <br> Width: 9.0 metres | Travel directly ahead | No problems with this section of road. |
| 67.3 | Whittingham | The New England Highway onto the Golden Highway GPS link: https://goo.gl/maps/nAnfkYfeUn42 | Clearance: <br> Width: 12.0 metres | Left Hand turn | No problems with this section of road. |
| 67.4 | Whittingham | Golden Highway <br> GPS link: <br> https://goo.gl/maps/R86RFuPnmFU2 | Clearance: <br> $115.0 \times 9.0$ metres | Parking Bay | Suitable parking for Fatigue breaks. |
| 77.3 | Whittingham | Golden Highway intersection with the Putty Road GPS link: https://goo.gl/maps/7hQdEmK1EgE2 | Clearance: <br> Length: 85.0 metres <br> Width: 12.0 metres | Left hand turn | No problems with this section of road. |
| 77.4 | Mount Thorley | Golden Highway <br> GPS link: <br> https://goo.gl/maps/zGvdupDuixx | Clearance: <br> $100.0 \times 10.0$ metres | Parking Bay | Suitable parking for Fatigue breaks. |
| 80.8 | Mount Thorley | Golden Highway intersection with Mt Thorley Road. <br> GPS link: <br> https://goo.gl/maps/VyA42n1CqZx | Clearance: <br> Length: 45.0 metres <br> Width: 8.0 metres <br> Height: 5.6 metres | Right hand turn | Loads over the listed clearances will need to travel along the incorrect side of the road. Loads will need to cross to the incorrect side 100 metres prior to the Mt Thorley Road underpass. |
| 98.0 | Warkworth | Golden Highway <br> GPS link: <br> https://goo.gl/maps/Y6V6EXaCwxq | Clearance: <br> $100.0 \times 8.0$ metres | Parking Bay | Suitable parking for Fatigue breaks. |
| 107.0 | Jerrys Plains | Golden Highway through Jerrys Plains village GPS link: https://goo.gl/maps/WgSCRsJ9ZGt | Clearance: <br> Length: 70.0 metres <br> Width: 9.0 metres | Dogleg | No problems with this section of road. |
| 126.0 | Ogilvy | Golden Highway GPS link: <br> https://goo.gl/maps/ShT4hrj8WQeMcris7 | 6\% gradient | Travel directly ahead | This section of road has a steep mountain range that will require additional pull trucks to assists loads that exceed 80T gross weight. <br> Additionally, the NSW Government is currently upgrading this section of road. It is recommended that you monitor the progress of the upgrades, and that any changes are thoroughly looked at. |
| 141.9 | Denman | Golden Highway onto Denman Road GPS link: <br> https://goo.gl/maps/sf4PNnycxB32 | Clearance: <br> Length: 60.0 metres <br> Width: 10.0 metres | Right hand turn | No problems with this section of road. |

ROUTE STUDY Newc astle to Hills of Gold Windfarm

| $\begin{gathered} \text { KM } \\ \text { index } \end{gathered}$ | Location | Section of road | Critical Measurement | Procedure | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 150.0 | Muswellbrook | Denman Road onto Thomas Mitchell Drive GPS link: <br> https://goo.gl/maps/XxZcg2MKqAgURuGu8 | Clearance: <br> Length: 65.0 metres <br> Width: 12.0 metres | Right hand turn | No problems with this section of road. |
| 160.6 | Muswellbrook | Thomas Mitchell onto New England Highway GPS link: <br> https://goo.gl/maps/3SyWufXF3gXqxaAt5 | Clearance: <br> Length: 70.0 metres <br> Width: 10.0 metres | Left hand turn | No problems with this section of road. |
| 169.5 | Muswellbrook | New England Highway onto Bell Street GPS link: <br> https://goo.gl/maps/H94bMYQMeSHay7918 | Clearance: <br> Length: 40.0 metres <br> Width: 6.0 metres | Right hand turn | No problems with this section of road. |
| 170.0 | Muswellbrook | Bell Street onto Victoria Street GPS link: $\qquad$ | Clearance: <br> Length: 40.0 metres <br> Width: 7.0 metres | Left hand corners | Tight left-hand bend over a rail bridge before another tight left hand bend. <br> Spotter to guide loads through this section of road, and approval from rail required to cross this structure. |
| 170.5 | Muswellbrook | Victoria Street onto Market Street GPS link: <br> https://goo.gl/maps/pyiTUH25bANG3m9n9 | Clearance: <br> Width: 7.0 metres | Travel directly ahead | No problems with this section of road. |
| 171.0 | Muswellbrook | Market Street onto New England Highway GPS link: <br> https://goo.gl/maps/3kpU6XdCBmCW75gM7 | Clearance: <br> Length: 30.0 metres Width: 7.0 metres | Right hand turn at roundabout | Loads may need to cross to the incorrect side of the roundabout if they exceed 30.0 meters in length, and do not exceed 42 meters in length. |
| 246.8 | Murrurundi | New England highway (Township) GPS link: <br> https://goo.gl/maps/Sj3ixAkhujt | Clearance: $60.0 \times 5.0$ metres | Parking Bay | Suitable parking for Fatigue breaks. |
| 251.4 | Murrurundi Hill | New England highway Nowlands Gap GPS link: <br> https://goo.gl/maps/R5yufobPeMG2 | Clearance: <br> $120.0 \times 12.0$ metres | Parking Bay (small ) | Emergency parking only. |
| 248.0 | Willow Tree | New England highway <br> GPS link: <br> https://goo.gl/maps/XLTg7CRV7EU2 | Clearance: <br> Width: 7.0 metres <br> Length: 35 metres <br> Height: 5.2 metres | Kankool weighbridge | It is likely that the towers and defiantly the blades will not fit into this facility. We have engineered documentation showing correct weights for all loads. |
| 253.9 | Willow Tree Township | New England highway GPS link: <br> https://goo.gl/maps/gw38qmvVfTC2 | Clearance: $60.0 \times 5.0$ metres | Parking Bay | Suitable parking for Fatigue breaks. |
| 255.5 | Willow Tree Truck Stop N | New England highway <br> GPS link: <br> https://goo.gl/maps/RRdPVHupGCs | Clearance: <br> $120.0 \times 12.0$ metres | Parking Bay ( small ) | Suitable parking for Fatigue breaks for small loads only. |
| 275.0 | Wallabadah | New England highway <br> GPS link: <br> https://goo.gl/maps/QWCyeHQSohS2 | Clearance: $80.0 \times 5.0$ metres | Parking Bay (side of road) | Suitable parking for Fatigue breaks. |

## ROUIE STUDY Newc astle to Hills of Gold Windfarm

| $\begin{gathered} \text { KM } \\ \text { index } \end{gathered}$ | Location | Section of road | Critical Measurement | Procedure | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 282.0 | Wallabadah | New England highway onto Lindsay's <br> Gap Road <br> GPS link: <br> https://goo.gl/maps/ePbYctjJootkBZiM9 | Clearance: <br> Length: 50.0 metres | Right hand turn | If the upgrades are completed for the blades than this corner will be suitable for the remaining components. |
| 289.7 | Garoo | Lindsay's Gap Road over Goonoo Goonoo Creek GPS link: $\qquad$ | Clearance: <br> Axle width: 3.60 m <br> Overall width: 6.20 m <br> Guard rail height: <br> 850 mm | Travel directly ahead over bridge in the centre of the road. | Loads that are been carried on trailers with an axle width exceeding 3.5 meters will not fit over this structure in its current form. <br> This bridge will need to be replaced or modified before the towers or motors can be delivered on this route. <br> A trafficable deck width of at least 4.6 metres is required. |
| 297.7 | Garoo | Lindsay's Gap Road over Middlebrook Creek GPS link: https://goo.gl/maps/DyxGUid9JucoAHhHA | Clearance: <br> Axle width: 4.50 m <br> Overall width: 6.10 m <br> Guard rail height: <br> 750 mm | Travel directly ahead over bridge in the centre of the road. | Loads that are been carried on trailers with an axle width exceeding 3.5 meters will not fit over this structure in its current form. <br> This bridge will need to be replaced or modified before the towers or motors can be delivered on this route. |
| 303.2 | Garoo | Lindsay's Gap Road through Lindsay's Gap <br> GPS link: <br> https://goo.gl/maps/GGKmqemziKdth8wH9 | Clearance: <br> Length: 90.0 metres | Travel directly ahead | Load to travel in the centre of the road, escorts to warn traffic 500 metres to the east of the gap. |
| 308.8 | Nundle | Lindsay's Gap Road onto Nundle Road GPS link: <br> https://goo.gl/maps/FX4ZRx2YG9i2BsXMA | Clearance: <br> Length: 50.0 metres | Right hand turn | If the upgrades are completed for the blades than this corner will be suitable for the remaining components. |
| 311.3 | Nundle | Nundle Road onto Crosby Street GPS link: <br> https://goo.gl/maps/uVvcN9QkPyTDP1YR6 | Clearance: <br> Width: 8.0 metres | Travel directly ahead | No problems with this section of road. |
| 312.6 | Nundle | Crosby Street onto Oakenville Street GPS link: <br> https://goo.gl/maps/aZNDKURdSBERedMr9 | Clearance: <br> Width: 8.0 metres | Travel directly ahead | No problems with this section of road. |
| 313.0 | Nundle | Oakenville Street and Jenkins Street intersection <br> GPS link: <br> https://goo.gl/maps/7YM56hQq8bnCSoZy8 | 5.0 metres width clearance |  | A no parking exclusion zone will need to be placed on the lefthand side while travelling through this intersection. Two signs will also need to be made removable. |
| 314.0 | Nundle | Oakenville Street onto Old Hanging Rock GPS link: <br> https://goo.gl/maps/1UMr2EwZetiE76Ey9 | 35.0 metres length clearance | Left hand turn | If the upgrades are completed for the blades than this corner will be suitable for the remaining components. |


| KM index | Location | Section of road | Critical Measurement | Procedure | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 315.0 | Nundle | Old Hanging Rock Road onto Barry Road GPS link: <br> https://goo.gl/maps/ve9zvmdJnLBYtQSz5 | 90.0 metres clearance | Right hand bend | No problems with this section of road. |
| $\begin{aligned} & 315.0 \text { to } \\ & 325.0 \\ & \text { Km's } \end{aligned}$ | Nundle to Hanging Rock | Barrys Road <br> https://goo.gl/maps/BUBe2MCfoQ215qKE6 | 25.0 metres length clearance | Travel directly ahead through multiple tight turns and steep terrain | As per the blades Barrys Road has a section of road known as the Devils Elbows. The existing hairpin corners are impassable for the blades, towers and motors. A detour of the Devils Elbow has been looked at and will likely be the best solution for all loads. <br> To the west and east of the Devils Elbows the road will need to be widened on a few corners, this would include hardstand and tree removal. |
| 325.0 | Hanging Rock | Barrys Road onto Morrisons Gap Road GPS link: https://goo.gl/maps/CLZDJSjENx8rjfAg7 | 35.0 metres length clearance | Right hand turn | Loads to turn right from the correct side to the correct side of the road. The swept path will have the longer loads travel through a landowner's boundaries on the inside of the corner. This will require a fence to be relocated and hardstand added. Additionally, some trees will need to be removed. |
| $\begin{aligned} & 325.0 \text { to } \\ & 328.0 \\ & \text { Km's } \end{aligned}$ | Hanging Rock | Morrisons Gap Road GPS link: <br> https://goo.gl/maps/kLtYYnmhTgvE6ZPFA | 25.0 metres length clearance | Travel around several sweeping bends on a gravel road | This section of road is gravel for the entirety. The road will need to be widened for the majority of the road. Typically, the road will need to be widened to 5.5 meters in all straight sections and made wider on the corners depending on the radius. A swept path analysis of this section of road, shows that the corridor would be able to stay within the road reserve. <br> Additionally, there will need to be trees removed. The vertical curve will also need to be checked for the entirety of this road. |
| $\begin{aligned} & 328.0 \\ & \text { Km's } \end{aligned}$ | Hanging Rock | Morrisons Gap Road into Hills of Gold windfarm <br> GPS link: <br> https://goo.gl/maps/5VFMQCB3drgXcjyU8 |  | Travel directly ahead into site entrance | Windfarm to supply suitable access for the dimensions and swept path of all loads. |

### 13.0 Route Survey D: Newcastle port to Hills of Gold WF for standard loads.

Distance: (284.0 Kilometres).
Via: Selwyn Street, George Street, Industrial Drive, Maitland Road, New England Highway, John Renshaw Drive, Hunter Expressway, New England Highway, Lindsays Gap Road, Nundle Road, Crosby Street, Oakenville Street, Old Hanging Rock Road, Barry Road, Morrisons Gap Road.
GPS Link: https://goo.gl/maps/rouAWyxLZ53pMB3v7


ROUIE STUDY

| KEY |  |
| :---: | :---: |
| MODIFICATIONS REQUIRED |  |
| MINOR WORKS OR CAUTION |  |
| PARKING |  |


| $\begin{gathered} \text { KM } \\ \text { index } \end{gathered}$ | Location | Section of road | Critical <br> Measurement | Procedure | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Route Index |  |  |  |  |  |
| 0.0 | Mayfield | Mayfield \#4 berth onto Selwyn Street GPS link: <br> https://goo.gl/maps/afLwPYKuNdm | Clearance: <br> Length: 70.0 metres <br> Width: 8.0 metres | Right hand turn | No problems with this section of road. |
| 0.4 | Mayfield | Selwyn Street rail crossing GPS link: https://goo.gl/maps/AmohE54hKSz | Clearance: <br> Width: 9.0 metres | Travel directly ahead | Loads to travel over the crossing in the center of the road. Approval required crossing this line, likely cross with caution. |
| 1.3 | Mayfield | Selwyn Street onto George Street GPS link: https://goo.gl/maps/gXeHvBtCp4D2 | Clearance: <br> Length: 70.0 metres <br> Width: 8.0 metres | Right hand turn | No problems with this section of road. |
| 1.4 | Mayfield | George Street onto Industrial Drive https://goo.gl/maps/s4ayrsuoAsD2 | Clearance: <br> Length: 70.0 metres <br> Width: 8.0 metres | Moderate right-hand turn | No problems with this section of road. |
| 4.9 | Mayfield | Industrial Drive under traffic signals GPS link: https://goo.gl/maps/YmqhiS2iR582 | Clearance: <br> Height: 5.4 Metres | Travel directly ahead | The lowest traffic signal on route is at the intersection of Steel River Blvd. Trucks that exceed 5.3 metres will need to travel in the right hand lane. |
| 5.5 | Mayfield West | Industrial Drive onto Maitland Road GPS link: https://goo.gl/maps/Kn49dhWG2qG2 | Clearance: <br> Length: 50.0 metres <br> Width: 10.0 metres | Right hand turn | No problems with this section of road. |
| 13.9 | Hexham | New England Highway under gantry GPS link: https://goo.gl/maps/YTMoFe7Aick | Clearance: <br> Height: 5.95 Metres | Travel directly ahead | This is the lowest structure on route. There is no bypass around the gantry. A maximum loaded height of 5.8 metres should not be exceeded. |
| 17.4 | Tarro | New England Highway onto John Renshaw Drive GPS link: <br> https://goo.gl/maps/SRDr5JigkBp | Clearance: <br> Width: 12.0 metres | Left hand merge | No problems with this section of road. |
| 18.4 | Beresfield | John Renshaw Drive GPS link: https://goo.gl/maps/N19vJih1Fgr | Clearance: <br> Width: 9.0 metres <br> Height: 5.9 metres | Travel directly ahead | No problems with this section of road. |
| 28.7 | Buchanan | John Renshaw Drive onto the Hunter Expressway <br> GPS link: https://goo.gl/maps/1STJ1PfQt9E2 | Clearance: <br> Length: 65.0 metres <br> Width: 7.0 metres | Right hand turn | No problems with this section of road. |

ROUIE STUDY Newc astle to Hills of Gold
Windfarm

| $\begin{gathered} \text { KM } \\ \text { index } \end{gathered}$ | Location | Section of road | Critical Measurement | Procedure | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 59.0 | Branxton | The Hunter Expressway onto The New England Highway <br> GPS link: <br> https://goo.gl/maps/7rauNuxzqjq | Clearance: <br> Width: 9.0 metres | Travel directly ahead | No problems with this section of road. |
| 125.0 | Muswellbrook | New England Highway intersection of Sydney Road GPS link: <br> https://goo.gl/maps/HMs11pkPQWqQbJny7 | Clearance: <br> Length: 40.0 metres <br> Width: 6.0 metres | Right hand turn | No problems with this section of road. |
| 125.3 | Muswellbrook | New England Highway under rail overpass GPS link: <br> https://goo.gl/maps/2kU2zsFJrJamDe2a7 | Clearance: <br> Height: 5.1 metres <br> Width: 4.0 metres | Travel directly ahead | Loads over the listed critical measurement are not to travel under this structure. |
| 201.8 | Murrurundi | New England highway (Township) GPS link: https://goo.gl/maps/Sj3ixAkhujt | Clearance: $60.0 \times 5.0$ metres | Parking Bay | Suitable parking for Fatigue breaks. |
| 206.4 | Murrurundi Hill | New England highway Nowlands Gap GPS link: <br> https://goo.gl/maps/R5yufobPeMG2 | Clearance: <br> $120.0 \times 12.0$ metres | Parking Bay (small ) | Emergency parking only. |
| 203.0 | Willow Tree | New England highway <br> GPS link: <br> https://goo.gl/maps/XLTg7CRV7EU2 | Clearance: <br> Width: 7.0 metres <br> Length: 35 metres <br> Height: 5.2 metres | Kankool weighbridge | No problems with this section of road. |
| 208.9 | Willow Tree Township | New England highway GPS link: <br> https://goo.gl/maps/gw38qmvVfTC2 | Clearance: $60.0 \times 5.0$ metres | Parking Bay | Suitable parking for Fatigue breaks. |
| 210.5 | Willow Tree Truck Stop N | New England highway GPS link: <br> https://goo.gl/maps/RRdPVHupGCs | Clearance: <br> $120.0 \times 12.0$ metres | Parking Bay ( small ) | Suitable parking for Fatigue breaks for small loads only. |
| 230.0 | Wallabadah | New England highway <br> GPS link: <br> https://goo.gl/maps/QWCyeHQSohS2 | Clearance: $80.0 \times 5.0$ metres | Parking Bay (side of road) | Suitable parking for Fatigue breaks. |
| 235.0 | Wallabadah | New England highway onto Lindsay's Gap Road GPS link: <br> https://goo.gl/maps/ePbYctjJootkBZiM9 | Clearance: <br> Length: 50.0 metres | Right hand turn | No problems with this section of road. |
| 245.7 | Garoo | Lindsay's Gap Road over Goonoo Goonoo Creek GPS link: <br> https://goo.gl/maps/9ELSk5ZLRWnf14tm7 | Clearance: <br> Axle width: 3.60 m <br> Overall width: 6.20 m <br> Guard rail height: <br> 850mm | Travel directly ahead over bridge in the centre of the road. | No problems with this section of road. |
| 253.7 | Garoo | Lindsay's Gap Road over Middlebrook Creek GPS link: | Clearance: <br> Axle width: 4.50 m <br> Overall width: 6.10 m <br> Guard rail height: <br> 750mm | Travel directly ahead over bridge in the centre of the road. | No problems with this section of road. |

ROUIE STUDY Newc astle to Hills of Gold Windfarm

| $\begin{gathered} \text { KM } \\ \text { index } \end{gathered}$ | Location | Section of road | Critical Measurement | Procedure | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 259.2 | Garoo | Lindsay's Gap Road through Lindsay's Gap GPS link: <br> https://goo.gl/maps/GGKmqemziKdth8wH9 | Clearance: <br> Length: 90.0 metres | Travel directly ahead | No problems with this section of road. |
| 264.8 | Nundle | Lindsay's Gap Road onto Nundle Road GPS link: <br> https://goo.gl/maps/FX4ZRx2YG9i2BsXMA | Clearance: <br> Length: 50.0 metres | Right hand turn | No problems with this section of road. |
| 268.3 | Nundle | Nundle Road onto Crosby Street GPS link: <br> https://goo.gl/maps/uVvcN9QkPyTDP1YR6 | Clearance: <br> Width: 8.0 metres | Travel directly ahead | No problems with this section of road. |
| 268.6 | Nundle | Crosby Street onto Oakenville Street GPS link: <br> https://goo.gl/maps/aZNDKURdSBERedMr9 | Clearance: <br> Width: 8.0 metres | Travel directly ahead | No problems with this section of road. |
| 269.0 | Nundle | Oakenville Street and Jenkins Street intersection <br> GPS link: <br> https://goo.gl/maps/7YM56hQq8bnCSoZy8 | 5.0 metres width clearance |  | No problems with this section of road. |
| 270.0 | Nundle | Oakenville Street onto Old Hanging Rock GPS link: <br> https://goo.gl/maps/1UMr2EwZetiE76Ey9 | 35.0 metres length clearance | Left hand turn | No problems with this section of road. |
| 271.0 | Nundle | Old Hanging Rock Road onto Barry Road GPS link: <br> https://goo.gl/maps/ve9zvmdJnLBYtQSz5 | 90.0 metres clearance | Right hand bend | No problems with this section of road. |
| 271.0 to 281.0 <br> Km's | Nundle to Hanging Rock | Barrys Road <br> https://goo.gl/maps/BUBe2MCfoQ215qKE6 | 25.0 metres length clearance | Travel directly ahead through multiple tight turns and steep terrain | No problems with this section of road. |
| 281.0 | Hanging Rock | Barrys Road onto Morrisons Gap <br> Road <br> GPS link: <br> https://goo.gl/maps/CLZDJSjENx8rjfAg7 | 35.0 metres length clearance | Right hand turn | No problems with this section of road. |
| $\begin{aligned} & 281.0 \text { to } \\ & 284.0 \\ & \text { Km's } \end{aligned}$ | Hanging Rock | Morrisons Gap Road GPS link: <br> https://goo.gl/maps/kLtYYnmhTgvE6ZPFA | 25.0 metres length clearance | Travel around several sweeping bends on a gravel road | This section of road is gravel for the entirety. The road will need upgrades for standard loads to pass through. |
| $\begin{aligned} & 284.0 \\ & \text { Km's } \end{aligned}$ | Hanging Rock | Morrisons Gap Road into Hills of Gold windfarm GPS link: <br> https://goo.gl/maps/5VFMQCB3drgXciyU8 |  | Travel directly ahead into site entrance | Windfarm to supply suitable access for the dimensions and swept path of all loads. |

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### 14.0 Conclusion:

## ROUTE SELECTION:

After studying all options and undertaking a route survey, it was observed that the components would need to be transported on several different routes through to the Hill of Gold project as listed in the report.

Route A: Suitable for all loads if modifications are undertaken.
Route B: Suitable for Towers and motors up to 5.2 metres in height, but not blades.
Route C: Suitable for Towers and motors over 5.2 metres in height, but not blades.
Route D: Suitable for standard loads up to 3.5 metres wide, and no higher than 5.2 metres in overall height.

## NEWCASTLE:

The intersection of George Street and Industrial Drive at Mayfield looks to be the most difficult corner. Relocation of the traffic signal in the centre of the intersection would be necessary to allow the 83-metre blade to traverse the bend. The 65 Metre blade will not require traffic signals to be removed. However, both blades will require some hardstand to be added to the outside of the corner.

The corner from Industrial Drive onto Maitland Road will require the centre median strips to be lowered while the blades traverse the corner on the incorrect side of the road for both blade options.

## HUNTER EXPRESSWAY:

The 83-metre blades will not make it around the roundabout from John Renshaw Drive onto the Hunter Expressway. The 65 Metre blade can travel around the roundabout.

For the 83-metre blade traffic control/Police would be required to block the eastbound lanes of the Hunter expressway while the blades travel down the incorrect side before crossing over at the centre crossover point.

## NEW ENGLAND HIGHWAY ONTO THE GOLDEN HIGHWAY:

This corner is currently in the design stage of modifications. The existing corner would need only a small amount of works to allow the blades a suitable swept path. It is recommended that the project keep a close eye on any potential changes that may affect the blades swept path around the corner.

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## THE GOLDEN HIGHWAY:

Several corners would need to have a moderate number of modifications.
Additionally, the blades will need to travel onto the incorrect side of the Golden Highway for approx. 400 metres. This will require the police escorts to hold all eastbound traffic on the Golden Highway. Roadwork's are programmed to take place on this route over the next year, so it is recommended that the client discuss any upcoming road projects with Transport NSW.

## MUSWELLBROOK:

Several different routes are required to travel through Muswellbrook, listed below is a summary of these routes.

- ROUTE A VIA: New England Highway, Golden Highway, Denman Road, Bengalla Road, Wybong Road, Kayuga Road, Ivermein Street, Dartbrook Mine access Road, New England Highway.
This route will require a large number of upgrades; these include large amounts of hard standing, relocating of power poles and approvals from Muswellbrook Shire Council, Private landowners and Dartbrook Mine. The 65 metre blade requires around $50 \%$ of the upgrades that the 83 metre blade would require.
- ROUTE B \& C VIA: New England Highway, Golden Highway, Denman Road, Thomas Mitchell Drive, New England Highway, Bell Street, Victoria street, Market Street, New England Highway.
This route is suitable in its current form for loads up to 40 metres long and 5.6 metres in height. Approval required from Muswellbrook Shire Council and rail.
- ROUTE D VIA: New England Highway.


## LINDSAY'S GAP ROAD THROUGH TO NUNDLE:

Loads to turn right from the New England Highway onto Lindsay's Gap Road, travelling across to Nundle Road before entering Nundle via Crosby Street and Oakenville Road.

- The section of Lindsay's Gap Road between the New England Highway and Nundle Road has several bridges that will need to be checked for axle loadings.
The bridge over Goonoo Goonoo creek has a maximum axle width of 3.5 metres. The bridge over Middlebrook Creek also has axle width restrictions. These bridges will require replacement or upgrades before the towers or motors could be delivered to the project. A deck width of at least 4.6 metres is required for the heavier loads.
- Upgrades required on the turn off from the New England Highway onto Lindsay's Gap Road, and also from Lindsay's Gap Road onto Nundle Road.


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The 85 metre blade will require a large amount of upgrades on this section of road, whereas the 65 metre blades only have a moderate amount of works.

- Oakenville Street would require no parking areas put in place throughout the deliveries, these locations are listed in the survey.


## BARRY ROAD:

- Barry Road will not accommodate either size blade or the towers and motors. The section of road through the Devils elbows will need to be detoured via a new alignment to the south of Devil's Elbow. This new alignment will need to be sealed if the gradient exceeds $14 \%$.
- Either side of the Devil's Elbow the road has tight sections that would need upgrades, these would include tree removal and hardstand.


## MORRISON GAP ROAD:

- Barry Road onto Morrison's Gap Road would require extensive modifications with the swept path currently entering a landowner's boundaries on the inside of the corner.
- Morrison's Gap Road is gravel for the entirety and would need to be made suitable for all weather travel.
The swept path of this road is tight in several sections and would need to be widened to at least 5.5 metres of road width and wider on the corners. A swept path analysis has been undertaken on Morrison's Gap Road, and the blades would stay within the existing road reserve with some modifications required to the existing alignment.
- Morrison's Gap Road also has several Crests that would also need to be surveyed. This will allow us to determine if the largest trailers have adequate clearance to pass through them without the need for additional road works.
- Morrison's Gap Road has a number of trees that will need to be removed and or trimmed to allow a suitable swept path for the largest loads.


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## GENERAL ROAD ACCESS:

## BRIDGE CROSSINGS:

This route from Newcastle to Tamworth has been used in the past for items up to 100T. Further investigations would be required if item mass exceeds this. Additionally, once the loads turn off the New England Highway all structures that require the loads to travel over them, will need to be assessed for axle loads.

## OVERHEAD STRUCTURES:

The lowest structure on this route is the Liddell overpass. This bridge is 5.2 metres in the centre carriageway and 5.3 metres in the far-right lane. Loads that exceed 5.2 metres in overall height will need to bypass the bridge via the Golden Highway. A maximum height of 5.8 metres than would be the lowest structure that cannot be avoided. This structure is on the New England Highway at Hexham.

## OVERHEAD WIRES:

This route would need to be assessed to handle a loaded height of up to 5.8 metres. It is likely that there are wires that will need to be raised.

## RAIL ASSETS:

There are a number of rail overbridges and crossings on route that will require approval from authorities before loads can access the routes.

## FLOODWAYS:

There are a number of floodway's on the access roads that will need to be raised and widened. These floodway's vary considerably, and some would need moderate to large amount of works, where others would only need minor upgrades. Each floodway should be assessed on its own merit.

## CRESTS:

There are number of crests on Morrison's Gap Road that will need to be surveyed. Hydraulic lift trailers could overcome these obstacles without the need for additional road works.

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## PAVEMENT:

The Pavement up to Morrison's Gap Road is of suitable highway grade. Morrison's Gap Road is gravel and would need widening as well as upgrading to an all-weather surface.

## ROADWORKS:

Roadworks are likely to be continuous on any route within NSW, as this is common practice. Some roads will just have general maintenance, and resealing, while other sections will have complete realignment. It is recommended that the project discuss any major works well in advance with the authorities.

## PORT:

The port has an excellent Break bulk berth that runs at approximately $60 \%$ berth occupancy.
The berth has axle and crane loadings well above what is required for this project.
The storage area is asphalt hardstand with a current area of $100,000 \mathrm{~s} / \mathrm{q}$ metres available, all level. It is adjacent to the port, and within 300 metres of the berth, all within the Port grounds. No local roads need to be used during the discharge.
Access to the local roads from the port is while require some upgrades, including adding hardstand and relocating fences.

## APPROVALS:

At a minimum the following are required for approval to access these routes.

- NHVR
- RMS
- Newcastle Council
- Muswellbrook Council
- Tamworth Regional Council
- NSW Police
- Ausgrid
- Essential Energy
- Telstra
- CRN JHG (Rail)
- ARTC (Rail)


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## SUMMARY OF ROUTES:

After reviewing all routes, we are under the opinion that the loads could be delivered through to the Hill of Gold windfarm project with a large number of upgrades.
The 83 metre and the 65 metre blades would require a detour around Muswellbrook via Route $A$ and approvals would still need to be sought to confirm that this is possible. The Towers and motors could use Route A if the upgrades are completed, and if the bridges have the capacity on the detour.
Access to the Hill of Gold windfarm once the loads arrive at Nundle has considerable road modifications that would need to take place before it could become a reality for both blade types.
The additional routes based on the height, allows the project to source larger towers if required. We recommend however that a loaded height of 5.8 metres is not exceeded. In saying that we believe a 5.6 metre flange could be delivered to site but would require bookends to keep the height under 5.8 metres.
We also recommend that a Blade dry run is undertaken once all road modifications have been completed, and prior to the first blade movement.

### 15.0 References:

Rex Andrews Engineered Transportation Pty. Ltd.
Someva Renewables
Engie
Rex J Andrews P/L Route Survey LL273 REV02.
Google Earth/Maps
Nearmaps
Sixmaps
NHVAS Maintenance Management (NHVAS21193)
NHVAS Basic Fatigue Management (NHVAS21193)

Disclaimer: This route study is a guide only; government approvals would be required before these routes could be deemed suitable for transporting the components over the listed routes.

This study was undertaken using data supplied by Rex J Andrews P/L. Equipment and swept paths might vary if using transport methodology other than the data supplied by Rex J Andrews.
transport planning

## Appendix B

Sidra Modelling Outputs

## SITE LAYOUT

S Site: 101 [2021 AM Scott St-New England Hwy (Site Folder:
Existing)]
New Site
Site Category: (None)
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


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Project: X:I18289 Hills of Gold Wind Farm Nundlel07 Modelling Files\18289-Hills of Gold model-210603.sip9

## MOVEMENT SUMMARY

$\forall$ Site: 101 [2021 AM Scott St-New England Hwy (Site Folder:

## Existing)]

New Site
Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | JT MES HV ] veh/h | $\begin{gathered} \text { DEM } \\ \text { FLO } \\ \text { [ Total } \\ \text { veh/h } \end{gathered}$ | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service | $\begin{gathered} 95 \% \text { B } \\ \text { QU } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver No. Cycles | Aver. Speed <br> km/h |
| South: New England Higway (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 19 | 0 | 20 | 0.0 | 0.226 | 4.4 | LOSA | 1.3 | 9.4 | 0.17 | 0.41 | 0.17 | 54.6 |
| 2 T1 | 642 | 31 | 676 | 4.8 | 0.226 | 4.5 | LOS A | 1.3 | 9.4 | 0.18 | 0.41 | 0.18 | 55.9 |
| 3 R2 | 2 | 0 | 2 | 0.0 | 0.226 | 9.0 | LOSA | 1.3 | 9.4 | 0.18 | 0.41 | 0.18 | 55.9 |
| Approach | 663 | 31 | 698 | 4.7 | 0.226 | 4.5 | LOS A | 1.3 | 9.4 | 0.18 | 0.41 | 0.18 | 55.9 |
| East: Scott Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 1 | 0 | 1 | 0.0 | 0.002 | 6.4 | LOSA | 0.0 | 0.0 | 0.44 | 0.53 | 0.44 | 53.5 |
| 5 T1 | 4 | 0 | 4 | 0.0 | 0.015 | 5.3 | LOSA | 0.1 | 0.4 | 0.38 | 0.62 | 0.38 | 53.0 |
| 6 R2 | 12 | 0 | 13 | 0.0 | 0.015 | 9.8 | LOSA | 0.1 | 0.4 | 0.38 | 0.62 | 0.38 | 52.9 |
| Approach | 17 | 0 | 18 | 0.0 | 0.015 | 8.5 | LOS A | 0.1 | 0.4 | 0.38 | 0.62 | 0.38 | 52.9 |
| North: New England Highway (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 1 | 0 | 1 | 0.0 | 0.143 | 4.3 | LOS A | 0.7 | 5.3 | 0.14 | 0.40 | 0.14 | 54.7 |
| 8 T1 | 349 | 28 | 367 | 8.0 | 0.143 | 4.4 | LOS A | 0.7 | 5.3 | 0.14 | 0.42 | 0.14 | 55.8 |
| 9 R2 | 30 | 0 | 32 | 0.0 | 0.143 | 8.9 | LOS A | 0.7 | 5.2 | 0.14 | 0.45 | 0.14 | 55.6 |
| Approach | 380 | 28 | 400 | 7.4 | 0.143 | 4.8 | LOS A | 0.7 | 5.3 | 0.14 | 0.43 | 0.14 | 55.8 |
| West: Vera Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 126 | 3 | 133 | 2.4 | 0.130 | 6.0 | LOS A | 0.5 | 3.6 | 0.49 | 0.68 | 0.49 | 53.5 |
| 11 T1 | 1 | 0 | 1 | 0.0 | 0.060 | 7.6 | LOS A | 0.2 | 1.6 | 0.53 | 0.80 | 0.53 | 50.8 |
| 12 R 2 | 31 | 3 | 33 | 9.7 | 0.060 | 12.6 | LOS A | 0.2 | 1.6 | 0.53 | 0.80 | 0.53 | 50.4 |
| Approach | 158 | 6 | 166 | 3.8 | 0.130 | 7.3 | LOS A | 0.5 | 3.6 | 0.50 | 0.70 | 0.50 | 52.8 |
| All <br> Vehicles | 1218 | 65 | 1282 | 5.3 | 0.226 | 5.0 | LOS A | 1.3 | 9.4 | 0.21 | 0.45 | 0.21 | 55.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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10:02:21 PM
Project: X:\18289 Hills of Gold Wind Farm Nundlel07 Modelling Files\18289-Hills of Gold model-210603.sip9

## MOVEMENT SUMMARY

$\forall$ Site: 101 [2021 PM Scott St-New England Hwy (Site Folder:
Existing)]
New Site
Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { INF } \\ & \text { VOL } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | UT MES HV] veh/h | $\begin{gathered} \text { DEM } \\ \text { FLO } \\ \text { [ Total } \\ \text { veh/h } \end{gathered}$ | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay sec $\qquad$ | Level of Service | $\begin{aligned} & \text { 95\% BA } \\ & \text { QUE } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed $\mathrm{km} / \mathrm{h}$ |
| South: New England Higway (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 86 | 0 | 91 | 0.0 | 0.347 | 5.7 | LOS A | 2.4 | 17.4 | 0.57 | 0.58 | 0.57 | 52.8 |
| 2 T1 | 389 | 13 | 409 | 3.3 | 0.347 | 5.9 | LOS A | 2.4 | 17.4 | 0.57 | 0.59 | 0.57 | 53.9 |
| 3 R2 | 302 | 8 | 318 | 2.6 | 0.347 | 10.7 | LOSA | 2.3 | 16.6 | 0.59 | 0.71 | 0.59 | 51.8 |
| Approach | 777 | 21 | 818 | 2.7 | 0.347 | 7.8 | LOSA | 2.4 | 17.4 | 0.58 | 0.64 | 0.58 | 53.0 |
| East: Scott Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 374 | 23 | 394 | 6.1 | 0.474 | 7.9 | LOS A | 3.0 | 21.8 | 0.75 | 0.91 | 0.84 | 52.3 |
| 5 T1 | 153 | 1 | 161 | 0.7 | 0.340 | 7.6 | LOS A | 1.7 | 12.0 | 0.70 | 0.80 | 0.71 | 52.7 |
| 6 R2 | 68 | 1 | 72 | 1.5 | 0.340 | 12.2 | LOSA | 1.7 | 12.0 | 0.70 | 0.80 | 0.71 | 52.6 |
| Approach | 595 | 25 | 626 | 4.2 | 0.474 | 8.3 | LOS A | 3.0 | 21.8 | 0.73 | 0.87 | 0.79 | 52.4 |
| North: New England Highway (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 174 | 3 | 183 | 1.7 | 0.521 | 9.5 | LOSA | 4.2 | 29.7 | 0.80 | 0.89 | 0.93 | 51.2 |
| 8 T1 | 545 | 13 | 574 | 2.4 | 0.521 | 9.9 | LOSA | 4.2 | 29.7 | 0.80 | 0.91 | 0.94 | 51.9 |
| 9 R2 | 95 | 2 | 100 | 2.1 | 0.521 | 14.8 | LOS B | 4.0 | 28.7 | 0.80 | 0.93 | 0.95 | 51.3 |
| Approach | 814 | 18 | 857 | 2.2 | 0.521 | 10.4 | LOS A | 4.2 | 29.7 | 0.80 | 0.91 | 0.93 | 51.7 |
| West: Vera Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 69 | 1 | 73 | 1.4 | 0.138 | 8.3 | LOSA | 0.5 | 3.8 | 0.61 | 0.81 | 0.61 | 52.0 |
| 11 T1 | 209 | 8 | 220 | 3.8 | 0.401 | 7.0 | LOSA | 2.1 | 15.3 | 0.67 | 0.78 | 0.71 | 52.7 |
| 12 R 2 | 132 | 4 | 139 | 3.0 | 0.401 | 11.5 | LOSA | 2.1 | 15.3 | 0.67 | 0.78 | 0.71 | 52.6 |
| Approach | 410 | 13 | 432 | 3.2 | 0.401 | 8.7 | LOSA | 2.1 | 15.3 | 0.66 | 0.79 | 0.69 | 52.5 |
| All <br> Vehicles | 2596 | 77 | 2733 | 3.0 | 0.521 | 8.9 | LOS A | 4.2 | 29.7 | 0.69 | 0.80 | 0.76 | 52.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 101 [2021 AM + Cons. Scott St-New England Hwy (Site
Folder: Project Scenario)]
New Site
Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | JT MES HV ] veh/h | $\begin{gathered} \text { DEM } \\ \text { FLO } \\ \text { [ Total } \\ \text { veh/h } \end{gathered}$ | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service | $\begin{gathered} 95 \% \text { B } \\ \text { QU } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver No. Cycles | Aver. Speed <br> km/h |
| South: New England Higway (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 22 | 0 | 23 | 0.0 | 0.240 | 4.4 | LOSA | 1.4 | 10.1 | 0.17 | 0.41 | 0.17 | 54.5 |
| 2 T1 | 679 | 31 | 715 | 4.6 | 0.240 | 4.5 | LOS A | 1.4 | 10.1 | 0.18 | 0.41 | 0.18 | 55.9 |
| 3 R2 | 2 | 0 | 2 | 0.0 | 0.240 | 9.0 | LOSA | 1.4 | 10.1 | 0.19 | 0.41 | 0.19 | 55.9 |
| Approach | 703 | 31 | 740 | 4.4 | 0.240 | 4.5 | LOS A | 1.4 | 10.1 | 0.18 | 0.41 | 0.18 | 55.9 |
| East: Scott Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 1 | 0 | 1 | 0.0 | 0.002 | 6.6 | LOSA | 0.0 | 0.0 | 0.46 | 0.53 | 0.46 | 53.4 |
| 5 T1 | 4 | 0 | 4 | 0.0 | 0.015 | 5.4 | LOSA | 0.1 | 0.4 | 0.39 | 0.63 | 0.39 | 52.9 |
| 6 R2 | 12 | 0 | 13 | 0.0 | 0.015 | 9.9 | LOSA | 0.1 | 0.4 | 0.39 | 0.63 | 0.39 | 52.8 |
| Approach | 17 | 0 | 18 | 0.0 | 0.015 | 8.6 | LOS A | 0.1 | 0.4 | 0.40 | 0.62 | 0.40 | 52.9 |
| North: New England Highway (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 1 | 0 | 1 | 0.0 | 0.156 | 4.4 | LOS A | 0.8 | 5.8 | 0.16 | 0.40 | 0.16 | 54.6 |
| 8 T1 | 377 | 28 | 397 | 7.4 | 0.156 | 4.5 | LOS A | 0.8 | 5.8 | 0.16 | 0.43 | 0.16 | 55.7 |
| 9 R2 | 32 | 0 | 34 | 0.0 | 0.156 | 8.9 | LOS A | 0.8 | 5.7 | 0.16 | 0.45 | 0.16 | 55.5 |
| Approach | 410 | 28 | 432 | 6.8 | 0.156 | 4.8 | LOS A | 0.8 | 5.8 | 0.16 | 0.43 | 0.16 | 55.7 |
| West: Vera Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 133 | 3 | 140 | 2.3 | 0.139 | 6.1 | LOS A | 0.5 | 3.9 | 0.50 | 0.69 | 0.50 | 53.5 |
| 11 T1 | 1 | 0 | 1 | 0.0 | 0.069 | 7.4 | LOS A | 0.2 | 1.8 | 0.54 | 0.80 | 0.54 | 51.0 |
| 12 R 2 | 39 | 3 | 41 | 7.7 | 0.069 | 12.2 | LOS A | 0.2 | 1.8 | 0.54 | 0.80 | 0.54 | 50.7 |
| Approach | 173 | 6 | 182 | 3.5 | 0.139 | 7.5 | LOS A | 0.5 | 3.9 | 0.51 | 0.72 | 0.51 | 52.8 |
| All <br> Vehicles | 1303 | 65 | 1372 | 5.0 | 0.240 | 5.0 | LOS A | 1.4 | 10.1 | 0.22 | 0.46 | 0.22 | 55.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 101 [2021 PM + Cons. Scott St-New England Hwy (Site
Folder: Project Scenario)]
New Site
Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | JT MES HV] veh/h |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay sec $\qquad$ | Level of Service | $\begin{gathered} 95 \% \text { B } \\ \text { QU } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed $\mathrm{km} / \mathrm{h}$ |
| South: New England Higway (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 97 | 0 | 102 | 0.0 | 0.377 | 5.9 | LOS A | 2.7 | 19.6 | 0.60 | 0.59 | 0.60 | 52.7 |
| 2 T1 | 419 | 13 | 441 | 3.1 | 0.377 | 6.0 | LOSA | 2.7 | 19.6 | 0.60 | 0.61 | 0.60 | 53.8 |
| $3 \quad \mathrm{R} 2$ | 318 | 8 | 335 | 2.5 | 0.377 | 10.9 | LOS A | 2.6 | 18.6 | 0.62 | 0.72 | 0.62 | 51.8 |
| Approach | 834 | 21 | 878 | 2.5 | 0.377 | 7.9 | LOS A | 2.7 | 19.6 | 0.61 | 0.65 | 0.61 | 52.9 |
| East: Scott Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 394 | 23 | 415 | 5.8 | 0.518 | 8.4 | LOS A | 3.4 | 25.3 | 0.78 | 0.94 | 0.91 | 51.9 |
| 5 T1 | 161 | 1 | 169 | 0.6 | 0.373 | 8.1 | LOS A | 2.0 | 13.9 | 0.73 | 0.85 | 0.77 | 52.5 |
| 6 R2 | 72 | 1 | 76 | 1.4 | 0.373 | 12.7 | LOSA | 2.0 | 13.9 | 0.73 | 0.85 | 0.77 | 52.4 |
| Approach | 627 | 25 | 660 | 4.0 | 0.518 | 8.8 | LOS A | 3.4 | 25.3 | 0.76 | 0.91 | 0.86 | 52.1 |
| North: New England Highway (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 183 | 3 | 193 | 1.6 | 0.572 | 10.8 | LOS A | 5.1 | 36.3 | 0.85 | 0.96 | 1.05 | 50.3 |
| 8 T1 | 576 | 13 | 606 | 2.3 | 0.572 | 11.3 | LOS A | 5.1 | 36.3 | 0.84 | 0.98 | 1.06 | 51.0 |
| 9 R2 | 100 | 2 | 105 | 2.0 | 0.572 | 16.2 | LOS B | 4.9 | 34.7 | 0.84 | 1.00 | 1.07 | 50.3 |
| Approach | 859 | 18 | 904 | 2.1 | 0.572 | 11.7 | LOSA | 5.1 | 36.3 | 0.85 | 0.98 | 1.06 | 50.8 |
| West: Vera Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 73 | 1 | 77 | 1.4 | 0.150 | 8.5 | LOS A | 0.6 | 4.2 | 0.63 | 0.81 | 0.63 | 51.9 |
| 11 T1 | 220 | 8 | 232 | 3.6 | 0.439 | 7.4 | LOS A | 2.5 | 17.7 | 0.70 | 0.82 | 0.77 | 52.5 |
| 12 R 2 | 142 | 4 | 149 | 2.8 | 0.439 | 11.9 | LOSA | 2.5 | 17.7 | 0.70 | 0.82 | 0.77 | 52.4 |
| Approach | 435 | 13 | 458 | 3.0 | 0.439 | 9.0 | LOS A | 2.5 | 17.7 | 0.69 | 0.82 | 0.75 | 52.3 |
| All <br> Vehicles | 2755 | 77 | 2900 | 2.8 | 0.572 | 9.5 | LOS A | 5.1 | 36.3 | 0.73 | 0.84 | 0.83 | 51.9 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## SITE LAYOUT

Site: 101 [2021 AM Murray St-New England Hwy (Site Folder:
Existing)]
New Site
Site Category: (None)
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


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## MOVEMENT SUMMARY

$\square$ Site: 101 [2021 AM Murray St-New England Hwy (Site Folder:
Existing)]
New Site
Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{array}{r} \text { INP } \\ \text { VOLU } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | UT MES HV] veh/h |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay sec $\qquad$ | Level of Service | $\begin{aligned} & \text { 95\% BA } \\ & \text { QUE } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed $\mathrm{km} / \mathrm{h}$ |
| South: New England Highway (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 88 | 0 | 93 | 0.0 | 0.141 | 4.3 | LOS A | 0.8 | 5.6 | 0.21 | 0.43 | 0.21 | 54.7 |
| 2 T1 | 301 | 14 | 317 | 4.7 | 0.141 | 4.4 | LOS A | 0.8 | 5.6 | 0.22 | 0.42 | 0.22 | 56.0 |
| 3 R2 | 13 | 5 | 14 | 38.5 | 0.141 | 9.7 | LOSA | 0.8 | 5.7 | 0.22 | 0.42 | 0.22 | 54.4 |
| Approach | 402 | 19 | 423 | 4.7 | 0.141 | 4.6 | LOS A | 0.8 | 5.7 | 0.22 | 0.42 | 0.22 | 55.6 |
| East: Murray Street (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 7 | 0 | 7 | 0.0 | 0.060 | 4.9 | LOS A | 0.2 | 1.6 | 0.35 | 0.57 | 0.35 | 53.2 |
| 5 T1 | 33 | 0 | 35 | 0.0 | 0.060 | 5.1 | LOSA | 0.2 | 1.6 | 0.35 | 0.57 | 0.35 | 54.6 |
| 6 R2 | 19 | 0 | 20 | 0.0 | 0.060 | 9.9 | LOS A | 0.2 | 1.6 | 0.35 | 0.57 | 0.35 | 54.6 |
| Approach | 59 | 0 | 62 | 0.0 | 0.060 | 6.6 | LOS A | 0.2 | 1.6 | 0.35 | 0.57 | 0.35 | 54.4 |
| North: New England Highway (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 9 | 0 | 9 | 0.0 | 0.095 | 4.3 | LOS A | 0.4 | 3.1 | 0.17 | 0.41 | 0.17 | 54.8 |
| 8 T1 | 206 | 30 | 217 | 14.6 | 0.095 | 4.5 | LOS A | 0.4 | 3.1 | 0.17 | 0.43 | 0.17 | 55.8 |
| 9 R2 | 19 | 0 | 20 | 0.0 | 0.095 | 9.1 | LOS A | 0.4 | 3.1 | 0.18 | 0.45 | 0.18 | 55.7 |
| Approach | 234 | 30 | 246 | 12.8 | 0.095 | 4.8 | LOS A | 0.4 | 3.1 | 0.17 | 0.43 | 0.17 | 55.7 |
| West: Murray Street (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 3 | 0 | 3 | 0.0 | 0.017 | 5.6 | LOS A | 0.1 | 0.4 | 0.39 | 0.51 | 0.39 | 53.8 |
| 11 T1 | 11 | 0 | 12 | 0.0 | 0.017 | 5.6 | LOS A | 0.1 | 0.4 | 0.39 | 0.51 | 0.39 | 55.3 |
| 12 R 2 | 38 | 1 | 40 | 2.6 | 0.034 | 9.8 | LOS A | 0.1 | 0.9 | 0.36 | 0.65 | 0.36 | 52.2 |
| Approach | 52 | 1 | 55 | 1.9 | 0.034 | 8.7 | LOS A | 0.1 | 0.9 | 0.37 | 0.61 | 0.37 | 52.9 |
| All <br> Vehicles | 747 | 50 | 786 | 6.7 | 0.141 | 5.1 | LOS A | 0.8 | 5.7 | 0.22 | 0.45 | 0.22 | 55.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 101 [2021 PM Murray St-New England Hwy (Site Folder:

## Existing)]

New Site
Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INP } \\ & \text { VOLu } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | UT <br> MES HV ] veh/h |  | $\begin{aligned} & \text { WD } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: New England Highway (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 181 | 25 | 191 | 13.8 | 0.197 | 5.2 | LOSA | 1.1 | 9.0 | 0.41 | 0.52 | 0.41 | 53.5 |
| 2 T1 | 269 | 36 | 283 | 13.4 | 0.197 | 5.4 | LOSA | 1.1 | 9.0 | 0.43 | 0.52 | 0.43 | 54.7 |
| 3 R2 | 13 | 0 | 14 | 0.0 | 0.197 | 9.9 | LOS A | 1.1 | 8.7 | 0.43 | 0.52 | 0.43 | 54.9 |
| Approach | 463 | 61 | 487 | 13.2 | 0.197 | 5.4 | LOS A | 1.1 | 9.0 | 0.42 | 0.52 | 0.42 | 54.2 |
| East: Murray Street (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 24 | 0 | 25 | 0.0 | 0.183 | 6.6 | LOS A | 0.8 | 5.6 | 0.59 | 0.72 | 0.59 | 52.5 |
| 5 T1 | 85 | 0 | 89 | 0.0 | 0.183 | 6.8 | LOS A | 0.8 | 5.6 | 0.59 | 0.72 | 0.59 | 53.8 |
| 6 R2 | 26 | 0 | 27 | 0.0 | 0.183 | 11.6 | LOS A | 0.8 | 5.6 | 0.59 | 0.72 | 0.59 | 53.8 |
| Approach | 135 | 0 | 142 | 0.0 | 0.183 | 7.7 | LOSA | 0.8 | 5.6 | 0.59 | 0.72 | 0.59 | 53.6 |
| North: New England Highway (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 47 | 1 | 49 | 2.1 | 0.299 | 6.1 | LOS A | 1.4 | 10.5 | 0.59 | 0.62 | 0.59 | 52.8 |
| 8 T1 | 369 | 17 | 388 | 4.6 | 0.299 | 6.3 | LOS A | 1.4 | 10.5 | 0.59 | 0.67 | 0.59 | 53.8 |
| 9 R2 | 109 | 0 | 115 | 0.0 | 0.299 | 11.2 | LOSA | 1.4 | 10.0 | 0.60 | 0.73 | 0.60 | 53.1 |
| Approach | 525 | 18 | 553 | 3.4 | 0.299 | 7.3 | LOS A | 1.4 | 10.5 | 0.59 | 0.68 | 0.59 | 53.5 |
| West: Murray Street (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 38 | 4 | 40 | 10.5 | 0.378 | 5.7 | LOS A | 2.0 | 14.4 | 0.49 | 0.54 | 0.49 | 53.0 |
| 11 T1 | 379 | 4 | 399 | 1.1 | 0.378 | 5.5 | LOS A | 2.0 | 14.4 | 0.49 | 0.54 | 0.49 | 54.8 |
| 12 R 2 | 222 | 17 | 234 | 7.7 | 0.257 | 10.6 | LOSA | 1.2 | 8.9 | 0.47 | 0.73 | 0.47 | 51.6 |
| Approach | 639 | 25 | 673 | 3.9 | 0.378 | 7.3 | LOS A | 2.0 | 14.4 | 0.49 | 0.61 | 0.49 | 53.5 |
| All <br> Vehicles | 1762 | 104 | 1855 | 5.9 | 0.378 | 6.8 | LOS A | 2.0 | 14.4 | 0.51 | 0.61 | 0.51 | 53.7 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\square$ Site: 101 [2021 AM + Cons. Murray St-New England Hwy (Site
Folder: Project Scenario)]
New Site
Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{array}{r} \text { INP } \\ \text { VOLU } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | UT MES HV] veh/h |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay sec $\qquad$ | Level of Service | $\begin{gathered} 95 \% \text { B } \\ \text { QU } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed $\mathrm{km} / \mathrm{h}$ |
| South: New England Highway (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 93 | 0 | 98 | 0.0 | 0.156 | 4.4 | LOS A | 0.9 | 6.3 | 0.22 | 0.43 | 0.22 | 54.6 |
| 2 T1 | 329 | 14 | 346 | 4.3 | 0.156 | 4.5 | LOSA | 0.9 | 6.3 | 0.23 | 0.43 | 0.23 | 55.8 |
| 3 R2 | 19 | 5 | 20 | 26.3 | 0.156 | 9.6 | LOSA | 0.9 | 6.4 | 0.24 | 0.43 | 0.24 | 54.7 |
| Approach | 441 | 19 | 464 | 4.3 | 0.156 | 4.7 | LOSA | 0.9 | 6.4 | 0.23 | 0.43 | 0.23 | 55.5 |
| East: Murray Street (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 21 | 0 | 22 | 0.0 | 0.082 | 5.1 | LOS A | 0.3 | 2.2 | 0.38 | 0.59 | 0.38 | 53.3 |
| 5 T1 | 37 | 0 | 39 | 0.0 | 0.082 | 5.3 | LOS A | 0.3 | 2.2 | 0.38 | 0.59 | 0.38 | 54.7 |
| 6 R2 | 20 | 0 | 21 | 0.0 | 0.082 | 10.1 | LOSA | 0.3 | 2.2 | 0.38 | 0.59 | 0.38 | 54.7 |
| Approach | 78 | 0 | 82 | 0.0 | 0.082 | 6.5 | LOS A | 0.3 | 2.2 | 0.38 | 0.59 | 0.38 | 54.3 |
| North: New England Highway (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 9 | 0 | 9 | 0.0 | 0.115 | 4.3 | LOSA | 0.5 | 3.8 | 0.19 | 0.41 | 0.19 | 54.7 |
| 8 T1 | 257 | 30 | 271 | 11.7 | 0.115 | 4.5 | LOSA | 0.5 | 3.8 | 0.19 | 0.43 | 0.19 | 55.8 |
| 9 R2 | 20 | 0 | 21 | 0.0 | 0.115 | 9.1 | LOSA | 0.5 | 3.7 | 0.19 | 0.45 | 0.19 | 55.7 |
| Approach | 286 | 30 | 301 | 10.5 | 0.115 | 4.8 | LOS A | 0.5 | 3.8 | 0.19 | 0.43 | 0.19 | 55.8 |
| West: Murray Street (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 3 | 0 | 3 | 0.0 | 0.019 | 5.7 | LOS A | 0.1 | 0.5 | 0.41 | 0.52 | 0.41 | 53.7 |
| 11 T1 | 12 | 0 | 13 | 0.0 | 0.019 | 5.7 | LOSA | 0.1 | 0.5 | 0.41 | 0.52 | 0.41 | 55.2 |
| 12 R 2 | 40 | 1 | 42 | 2.5 | 0.036 | 9.9 | LOSA | 0.1 | 1.0 | 0.38 | 0.66 | 0.38 | 52.1 |
| Approach | 55 | 1 | 58 | 1.8 | 0.036 | 8.7 | LOSA | 0.1 | 1.0 | 0.39 | 0.62 | 0.39 | 52.9 |
| All <br> Vehicles | 860 | 50 | 905 | 5.8 | 0.156 | 5.1 | LOS A | 0.9 | 6.4 | 0.24 | 0.46 | 0.24 | 55.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

B Site: 101 [2021 PM + Cons. Murray St-New England Hwy (Site
Folder: Project Scenario)]
New Site
Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { INP } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | UT MES HV] veh/h |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay sec $\qquad$ | Level of Service | $\begin{gathered} \text { 95\% B B } \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | CK OF Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: New England Highway (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 191 | 25 | 201 | 13.1 | 0.229 | 5.3 | LOSA | 1.4 | 10.6 | 0.43 | 0.53 | 0.43 | 53.4 |
| 2 T1 | 323 | 36 | 340 | 11.1 | 0.229 | 5.4 | LOSA | 1.4 | 10.6 | 0.45 | 0.54 | 0.45 | 54.6 |
| 3 R2 | 23 | 0 | 24 | 0.0 | 0.229 | 10.0 | LOSA | 1.3 | 10.1 | 0.45 | 0.54 | 0.45 | 54.7 |
| Approach | 537 | 61 | 565 | 11.4 | 0.229 | 5.6 | LOS A | 1.4 | 10.6 | 0.44 | 0.53 | 0.44 | 54.2 |
| East: Murray Street (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 32 | 0 | 34 | 0.0 | 0.207 | 6.8 | LOSA | 0.9 | 6.5 | 0.62 | 0.74 | 0.62 | 52.4 |
| 5 T1 | 89 | 0 | 94 | 0.0 | 0.207 | 7.0 | LOSA | 0.9 | 6.5 | 0.62 | 0.74 | 0.62 | 53.8 |
| 6 R2 | 27 | 0 | 28 | 0.0 | 0.207 | 11.8 | LOS A | 0.9 | 6.5 | 0.62 | 0.74 | 0.62 | 53.8 |
| Approach | 148 | 0 | 156 | 0.0 | 0.207 | 7.8 | LOS A | 0.9 | 6.5 | 0.62 | 0.74 | 0.62 | 53.5 |
| North: New England Highway ( N ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 49 | 1 | 52 | 2.0 | 0.329 | 6.3 | LOSA | 1.6 | 11.9 | 0.62 | 0.64 | 0.62 | 52.7 |
| 8 T1 | 398 | 17 | 419 | 4.3 | 0.329 | 6.5 | LOSA | 1.6 | 11.9 | 0.62 | 0.68 | 0.62 | 53.6 |
| 9 R2 | 115 | 0 | 121 | 0.0 | 0.329 | 11.4 | LOSA | 1.6 | 11.4 | 0.63 | 0.76 | 0.63 | 52.9 |
| Approach | 562 | 18 | 592 | 3.2 | 0.329 | 7.5 | LOSA | 1.6 | 11.9 | 0.62 | 0.69 | 0.62 | 53.4 |
| West: Murray Street (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 44 | 4 | 46 | 9.1 | 0.417 | 5.9 | LOSA | 2.3 | 16.3 | 0.54 | 0.57 | 0.54 | 52.8 |
| 11 T1 | 399 | 4 | 420 | 1.0 | 0.417 | 5.7 | LOS A | 2.3 | 16.3 | 0.54 | 0.57 | 0.54 | 54.5 |
| 12 R2 | 234 | 17 | 246 | 7.3 | 0.283 | 10.9 | LOSA | 1.3 | 9.8 | 0.52 | 0.76 | 0.52 | 51.5 |
| Approach | 677 | 25 | 713 | 3.7 | 0.417 | 7.5 | LOSA | 2.3 | 16.3 | 0.53 | 0.64 | 0.53 | 53.3 |
| All <br> Vehicles | 1924 | 104 | 2025 | 5.4 | 0.417 | 7.0 | LOS A | 2.3 | 16.3 | 0.54 | 0.63 | 0.54 | 53.6 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## SITE LAYOUT

## $\nabla$ Site: 101 [2021 AM Nundle Rd-New England Hwy (Site Folder:

## Existing)]

New Site
Site Category: (None)
Give-Way (Two-Way)

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


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## MOVEMENT SUMMARY

$\nabla$ Site: 101 [2021 AM Nundle Rd-New England Hwy (Site Folder:
Existing)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { INF } \\ & \text { VOLI } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | UT MES HV ] veh/h |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay $\qquad$ <br> sec | Level of Service | $\begin{gathered} \text { 95\% B B } \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Nundle Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 105 | 1 | 111 | 1.0 | 0.102 | 6.5 | LOS A | 0.4 | 2.7 | 0.31 | 0.59 | 0.31 | 52.6 |
| 2 T1 | 1 | 0 | 1 | 0.0 | 0.021 | 9.7 | LOSA | 0.1 | 0.5 | 0.53 | 0.70 | 0.53 | 49.6 |
| 3 R2 | 6 | 1 | 6 | 16.7 | 0.021 | 12.4 | LOSA | 0.1 | 0.5 | 0.53 | 0.70 | 0.53 | 48.6 |
| Approach | 112 | 2 | 118 | 1.8 | 0.102 | 6.8 | LOS A | 0.4 | 2.7 | 0.32 | 0.60 | 0.32 | 52.4 |
| East: New England Highway (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 33 | 2 | 35 | 6.1 | 0.020 | 5.6 | LOSA | 0.0 | 0.0 | 0.00 | 0.57 | 0.00 | 53.4 |
| 5 T1 | 189 | 20 | 199 | 10.6 | 0.109 | 0.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 59.9 |
| 6 R2 | 1 | 0 | 1 | 0.0 | 0.001 | 6.0 | LOS A | 0.0 | 0.0 | 0.25 | 0.53 | 0.25 | 52.5 |
| Approach | 223 | 22 | 235 | 9.9 | 0.109 | 0.9 | NA | 0.0 | 0.0 | 0.00 | 0.09 | 0.00 | 58.8 |
| North: Railway St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 4 | 1 | 4 | 25.0 | 0.032 | 6.5 | LOSA | 0.1 | 0.8 | 0.44 | 0.66 | 0.44 | 48.6 |
| 8 T1 | 1 | 0 | 1 | 0.0 | 0.032 | 10.0 | LOSA | 0.1 | 0.8 | 0.44 | 0.66 | 0.44 | 50.0 |
| 9 R2 | 7 | 1 | 7 | 14.3 | 0.032 | 14.5 | LOS B | 0.1 | 0.8 | 0.44 | 0.66 | 0.44 | 49.0 |
| Approach | 12 | 2 | 13 | 16.7 | 0.032 | 11.5 | LOS A | 0.1 | 0.8 | 0.44 | 0.66 | 0.44 | 49.0 |
| West: New England Highway (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 8 | 0 | 8 | 0.0 | 0.013 | 5.5 | LOSA | 0.0 | 0.0 | 0.00 | 0.21 | 0.00 | 56.2 |
| 11 T1 | 121 | 29 | 127 | 24.0 | 0.067 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.03 | 0.00 | 59.7 |
| 12 R 2 | 34 | 3 | 36 | 8.8 | 0.033 | 6.7 | LOSA | 0.1 | 1.0 | 0.34 | 0.58 | 0.34 | 52.5 |
| Approach | 163 | 32 | 172 | 19.6 | 0.067 | 1.7 | NA | 0.1 | 1.0 | 0.07 | 0.15 | 0.07 | 57.9 |
| All <br> Vehicles | 510 | 58 | 537 | 11.4 | 0.109 | 2.7 | NA | 0.4 | 2.7 | 0.10 | 0.23 | 0.10 | 56.7 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 101 [2021 PM Nundle Rd-New England Hwy (Site Folder:
Existing)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { INF } \\ & \text { VOLI } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | UT MES HV ] veh/h |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay $\qquad$ <br> sec | Level of Service | $\begin{gathered} \text { 95\% B B } \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | CK OF Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Nundle Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 93 | 9 | 98 | 9.7 | 0.101 | 6.9 | LOS A | 0.4 | 2.8 | 0.36 | 0.62 | 0.36 | 52.1 |
| 2 T1 | 5 | 1 | 5 | 20.0 | 0.164 | 27.2 | LOS B | 0.5 | 4.1 | 0.84 | 0.93 | 0.85 | 39.1 |
| 3 R2 | 16 | 3 | 17 | 18.8 | 0.164 | 32.1 | LOS C | 0.5 | 4.1 | 0.84 | 0.93 | 0.85 | 38.8 |
| Approach | 114 | 13 | 120 | 11.4 | 0.164 | 11.4 | LOS A | 0.5 | 4.1 | 0.45 | 0.68 | 0.45 | 49.0 |
| East: New England Highway (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 31 | 3 | 33 | 9.7 | 0.019 | 5.7 | LOSA | 0.0 | 0.0 | 0.00 | 0.57 | 0.00 | 53.2 |
| 5 T1 | 219 | 63 | 231 | 28.8 | 0.140 | 0.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 59.9 |
| 6 R2 | 3 | 0 | 3 | 0.0 | 0.003 | 7.2 | LOS A | 0.0 | 0.1 | 0.44 | 0.59 | 0.44 | 51.8 |
| Approach | 253 | 66 | 266 | 26.1 | 0.140 | 0.8 | NA | 0.0 | 0.1 | 0.01 | 0.08 | 0.01 | 58.9 |
| North: Railway St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 5 | 0 | 5 | 0.0 | 0.069 | 7.4 | LOSA | 0.2 | 1.7 | 0.75 | 0.81 | 0.75 | 42.7 |
| 8 T1 | 4 | 2 | 4 | 50.0 | 0.069 | 37.6 | LOS C | 0.2 | 1.7 | 0.75 | 0.81 | 0.75 | 42.0 |
| 9 R2 | 3 | 0 | 3 | 0.0 | 0.069 | 29.8 | LOS C | 0.2 | 1.7 | 0.75 | 0.81 | 0.75 | 42.8 |
| Approach | 12 | 2 | 13 | 16.7 | 0.069 | 23.0 | LOS B | 0.2 | 1.7 | 0.75 | 0.81 | 0.75 | 42.5 |
| West: New England Highway (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 13 | 0 | 14 | 0.0 | 0.037 | 5.5 | LOSA | 0.0 | 0.0 | 0.00 | 0.12 | 0.00 | 57.3 |
| 11 T1 | 382 | 22 | 402 | 5.8 | 0.185 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.02 | 0.00 | 59.8 |
| 12 R 2 | 133 | 5 | 140 | 3.8 | 0.134 | 7.0 | LOSA | 0.6 | 4.0 | 0.40 | 0.63 | 0.40 | 52.2 |
| Approach | 528 | 27 | 556 | 5.1 | 0.185 | 1.9 | NA | 0.6 | 4.0 | 0.10 | 0.17 | 0.10 | 57.6 |
| All <br> Vehicles | 907 | 108 | 955 | 11.9 | 0.185 | 3.1 | NA | 0.6 | 4.1 | 0.13 | 0.22 | 0.13 | 56.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [2021 AM + Cons. Nundle Rd-New England Hwy <br> (Site Folder: Project Scenario)]

New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | JT MES HV ] veh/h |  | $\begin{gathered} \text { HD } \\ \text { NS } \\ \text { HV] } \\ \% \\ \hline \end{gathered}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Nundle Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 128 | 5 | 135 | 3.9 | 0.128 | 6.6 | LOS A | 0.5 | 3.5 | 0.32 | 0.60 | 0.32 | 52.4 |
| 2 T1 | 1 | 0 | 1 | 0.0 | 0.025 | 11.1 | LOS A | 0.1 | 0.6 | 0.59 | 0.76 | 0.59 | 48.3 |
| 3 R 2 | 6 | 1 | 6 | 16.7 | 0.025 | 14.6 | LOS B | 0.1 | 0.6 | 0.59 | 0.76 | 0.59 | 47.3 |
| Approach | 135 | 6 | 142 | 4.4 | 0.128 | 7.0 | LOS A | 0.5 | 3.5 | 0.34 | 0.61 | 0.34 | 52.2 |
| East: New England Highway (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 35 | 2 | 37 | 5.7 | 0.021 | 5.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.57 | 0.00 | 53.4 |
| 5 T1 | 199 | 20 | 209 | 10.1 | 0.114 | 0.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 59.9 |
| 6 R2 | 1 | 0 | 1 | 0.0 | 0.001 | 6.0 | LOS A | 0.0 | 0.0 | 0.25 | 0.53 | 0.25 | 52.4 |
| Approach | 235 | 22 | 247 | 9.4 | 0.114 | 0.9 | NA | 0.0 | 0.0 | 0.00 | 0.09 | 0.00 | 58.8 |
| North: Railway St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $7 \quad$ L2 | 4 | 1 | 4 | 25.0 | 0.039 | 6.5 | LOS A | 0.1 | 1.0 | 0.49 | 0.70 | 0.49 | 47.2 |
| 8 T1 | 1 | 0 | 1 | 0.0 | 0.039 | 11.5 | LOS A | 0.1 | 1.0 | 0.49 | 0.70 | 0.49 | 48.5 |
| 9 R2 | 7 | 1 | 7 | 14.3 | 0.039 | 18.1 | LOS B | 0.1 | 1.0 | 0.49 | 0.70 | 0.49 | 47.6 |
| Approach | 12 | 2 | 13 | 16.7 | 0.039 | 13.7 | LOS A | 0.1 | 1.0 | 0.49 | 0.70 | 0.49 | 47.5 |
| West: New England Highway (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 8 | 0 | 8 | 0.0 | 0.014 | 5.5 | LOS A | 0.0 | 0.0 | 0.00 | 0.20 | 0.00 | 56.3 |
| 11 T1 | 127 | 29 | 134 | 22.8 | 0.070 | 0.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.02 | 0.00 | 59.7 |
| 12 R 2 | 92 | 23 | 97 | 25.0 | 0.101 | 7.2 | LOSA | 0.4 | 3.5 | 0.38 | 0.62 | 0.38 | 52.2 |
| Approach | 227 | 52 | 239 | 22.9 | 0.101 | 3.1 | NA | 0.4 | 3.5 | 0.16 | 0.27 | 0.16 | 56.3 |
| All <br> Vehicles | 609 | 82 | 641 | 13.5 | 0.128 | 3.3 | NA | 0.5 | 3.5 | 0.14 | 0.28 | 0.14 | 56.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^2]
## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [2021 PM + Cons. Nundle Rd-New England Hwy <br> (Site Folder: Project Scenario)]

New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | JT MES HV] veh/h |  | $\begin{aligned} & \text { HD } \\ & \text { NS } \\ & \text { HV] } \\ & \% \\ & \hline \end{aligned}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Nundle Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 152 | 9 | 160 | 5.9 | 0.165 | 7.1 | LOS A | 0.6 | 4.6 | 0.39 | 0.64 | 0.39 | 52.2 |
| 2 T1 | 5 | 1 | 5 | 20.0 | 0.200 | 32.4 | LOS C | 0.6 | 5.0 | 0.87 | 0.95 | 0.91 | 36.9 |
| 3 R 2 | 17 | 3 | 18 | 17.6 | 0.200 | 37.9 | LOS C | 0.6 | 5.0 | 0.87 | 0.95 | 0.91 | 36.6 |
| Approach | 174 | 13 | 183 | 7.5 | 0.200 | 10.8 | LOS A | 0.6 | 5.0 | 0.45 | 0.68 | 0.45 | 49.5 |
| East: New England Highway (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 33 | 3 | 35 | 9.1 | 0.020 | 5.7 | LOSA | 0.0 | 0.0 | 0.00 | 0.57 | 0.00 | 53.2 |
| 5 T1 | 239 | 63 | 252 | 26.4 | 0.151 | 0.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 59.9 |
| 6 R2 | 3 | 0 | 3 | 0.0 | 0.004 | 7.4 | LOS A | 0.0 | 0.1 | 0.45 | 0.59 | 0.45 | 51.7 |
| Approach | 275 | 66 | 289 | 24.0 | 0.151 | 0.8 | NA | 0.0 | 0.1 | 0.00 | 0.08 | 0.00 | 58.9 |
| North: Railway St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 5 | 0 | 5 | 0.0 | 0.085 | 7.5 | LOS A | 0.3 | 2.0 | 0.79 | 0.84 | 0.79 | 40.5 |
| 8 T1 | 4 | 2 | 4 | 50.0 | 0.085 | 44.3 | LOS D | 0.3 | 2.0 | 0.79 | 0.84 | 0.79 | 39.9 |
| 9 R2 | 3 | 0 | 3 | 0.0 | 0.085 | 39.0 | LOS C | 0.3 | 2.0 | 0.79 | 0.84 | 0.79 | 40.6 |
| Approach | 12 | 2 | 13 | 16.7 | 0.085 | 27.7 | LOS B | 0.3 | 2.0 | 0.79 | 0.84 | 0.79 | 40.3 |
| West: New England Highway (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 14 | 0 | 15 | 0.0 | 0.039 | 5.5 | LOS A | 0.0 | 0.0 | 0.00 | 0.12 | 0.00 | 57.3 |
| 11 T1 | 402 | 22 | 423 | 5.5 | 0.195 | 0.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.02 | 0.00 | 59.7 |
| 12 R 2 | 157 | 5 | 165 | 3.2 | 0.162 | 7.2 | LOSA | 0.7 | 4.9 | 0.43 | 0.65 | 0.43 | 52.2 |
| Approach | 573 | 27 | 603 | 4.7 | 0.195 | 2.1 | NA | 0.7 | 4.9 | 0.12 | 0.19 | 0.12 | 57.4 |
| All <br> Vehicles | 1034 | 108 | 1088 | 10.4 | 0.200 | 3.5 | NA | 0.7 | 5.0 | 0.15 | 0.25 | 0.15 | 56.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^3]
## SITE LAYOUT

$\nabla$ Site: 101 [2021 AM Nundle Rd - Lindsays Gap Rd (Site
Folder: Existing)]
New Site
Site Category: (None)
Give-Way (Two-Way)

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings


Nundle Road

## MOVEMENT SUMMARY

$\nabla$ Site: 101 [2021 AM Nundle Rd - Lindsays Gap Rd (Site
Folder: Existing)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INF } \\ & \text { VOLI } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay $\qquad$ <br> sec | Level of Service | $\begin{gathered} \text { 95\% B B } \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Nundle Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 15 | 15.0 | 16 | 15.0 | 0.018 | 7.2 | LOSA | 0.0 | 0.0 | 0.00 | 0.32 | 0.00 | 64.3 |
| 2 T1 | 15 | 15.0 | 16 | 15.0 | 0.018 | 0.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.32 | 0.00 | 74.3 |
| Approach | 30 | 15.0 | 32 | 15.0 | 0.018 | 3.6 | NA | 0.0 | 0.0 | 0.00 | 0.32 | 0.00 | 68.9 |
| North: Nundle Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 8 | 15.0 | 8 | 15.0 | 0.008 | 0.1 | LOSA | 0.0 | 0.2 | 0.08 | 0.24 | 0.08 | 75.2 |
| 9 R2 | 5 | 15.0 | 5 | 15.0 | 0.008 | 7.0 | LOSA | 0.0 | 0.2 | 0.08 | 0.24 | 0.08 | 64.2 |
| Approach | 13 | 15.0 | 14 | 15.0 | 0.008 | 2.7 | NA | 0.0 | 0.2 | 0.08 | 0.24 | 0.08 | 70.6 |
| West: Linsays Gap Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 6 | 15.0 | 6 | 15.0 | 0.008 | 7.3 | LOS A | 0.0 | 0.2 | 0.07 | 0.61 | 0.07 | 60.4 |
| 12 R2 | 4 | 15.0 | 4 | 15.0 | 0.008 | 7.0 | LOSA | 0.0 | 0.2 | 0.07 | 0.61 | 0.07 | 59.8 |
| Approach | 10 | 15.0 | 11 | 15.0 | 0.008 | 7.2 | LOS A | 0.0 | 0.2 | 0.07 | 0.61 | 0.07 | 60.2 |
| All <br> Vehicles | 53 | 15.0 | 56 | 15.0 | 0.018 | 4.1 | NA | 0.0 | 0.2 | 0.03 | 0.36 | 0.03 | 67.5 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 101 [2021 PM Nundle Rd - Lindsays Gap Rd (Site
Folder: Existing)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INF } \\ & \text { vOL } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service | $\begin{gathered} 95 \% \text { B } \\ \text { QU } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \mathrm{m} \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Nundle Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 3 | 15.0 | 3 | 15.0 | 0.010 | 7.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.11 | 0.00 | 66.9 |
| 2 T 1 | 14 | 15.0 | 15 | 15.0 | 0.010 | 0.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.11 | 0.00 | 77.9 |
| Approach | 17 | 15.0 | 18 | 15.0 | 0.010 | 1.3 | NA | 0.0 | 0.0 | 0.00 | 0.11 | 0.00 | 75.7 |
| North: Nundle Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 6 | 15.0 | 6 | 15.0 | 0.005 | 0.0 | LOSA | 0.0 | 0.1 | 0.04 | 0.16 | 0.04 | 76.9 |
| 9 R2 | 2 | 15.0 | 2 | 15.0 | 0.005 | 7.0 | LOSA | 0.0 | 0.1 | 0.04 | 0.16 | 0.04 | 65.4 |
| Approach | 8 | 15.0 | 8 | 15.0 | 0.005 | 1.8 | NA | 0.0 | 0.1 | 0.04 | 0.16 | 0.04 | 73.7 |
| West: Linsays Gap Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 1 | 15.0 | 1 | 15.0 | 0.012 | 7.3 | LOSA | 0.0 | 0.3 | 0.08 | 0.62 | 0.08 | 60.6 |
| 12 R2 | 13 | 15.0 | 14 | 15.0 | 0.012 | 7.0 | LOSA | 0.0 | 0.3 | 0.08 | 0.62 | 0.08 | 60.0 |
| Approach | 14 | 15.0 | 15 | 15.0 | 0.012 | 7.0 | LOS A | 0.0 | 0.3 | 0.08 | 0.62 | 0.08 | 60.0 |
| All <br> Vehicles | 39 | 15.0 | 41 | 15.0 | 0.012 | 3.4 | NA | 0.0 | 0.3 | 0.04 | 0.30 | 0.04 | 68.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 101 [2021 AM Nundle Rd - Lindsays Gap Rd (Site
Folder: Project Scenario)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INF } \\ & \text { VOLI } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay $\qquad$ <br> sec | Level of Service | $\begin{gathered} \text { 95\% B B } \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Nundle Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 23 | 15.0 | 24 | 15.0 | 0.033 | 7.2 | LOSA | 0.0 | 0.0 | 0.00 | 0.27 | 0.00 | 64.9 |
| 2 T1 | 32 | 15.0 | 34 | 15.0 | 0.033 | 0.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.27 | 0.00 | 75.2 |
| Approach | 55 | 15.0 | 58 | 15.0 | 0.033 | 3.0 | NA | 0.0 | 0.0 | 0.00 | 0.27 | 0.00 | 70.5 |
| North: Nundle Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 62 | 15.0 | 65 | 15.0 | 0.040 | 0.0 | LOSA | 0.0 | 0.3 | 0.03 | 0.05 | 0.03 | 78.9 |
| 9 R2 | 5 | 15.0 | 5 | 15.0 | 0.040 | 7.1 | LOSA | 0.0 | 0.3 | 0.03 | 0.05 | 0.03 | 66.9 |
| Approach | 67 | 15.0 | 71 | 15.0 | 0.040 | 0.5 | NA | 0.0 | 0.3 | 0.03 | 0.05 | 0.03 | 77.9 |
| West: Linsays Gap Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 6 | 15.0 | 6 | 15.0 | 0.032 | 7.3 | LOS A | 0.1 | 0.8 | 0.16 | 0.61 | 0.16 | 60.2 |
| 12 R2 | 28 | 15.0 | 29 | 15.0 | 0.032 | 7.4 | LOS A | 0.1 | 0.8 | 0.16 | 0.61 | 0.16 | 59.6 |
| Approach | 34 | 15.0 | 36 | 15.0 | 0.032 | 7.4 | LOS A | 0.1 | 0.8 | 0.16 | 0.61 | 0.16 | 59.8 |
| All <br> Vehicles | 156 | 15.0 | 164 | 15.0 | 0.040 | 2.9 | NA | 0.1 | 0.8 | 0.05 | 0.25 | 0.05 | 70.6 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 101 [2021 PM Nundle Rd - Lindsays Gap Rd (Site
Folder: Project Scenario)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INP } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | MES <br> HV ] <br> \% |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay sec | Level of Service |  | $\mathrm{CK} \text { OF }$ UE Dist ] m | Prop. Que | Effective <br> Stop <br> Rate | Aver. No. Cycles | Aver. Speed km/h |
| South: Nundle Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 27 | 15.0 | 28 | 15.0 | 0.057 | 7.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.18 | 0.00 | 66.0 |
| 2 T1 | 68 | 15.0 | 72 | 15.0 | 0.057 | 0.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.18 | 0.00 | 76.6 |
| Approach | 95 | 15.0 | 100 | 15.0 | 0.057 | 2.1 | NA | 0.0 | 0.0 | 0.00 | 0.18 | 0.00 | 73.3 |
| North: Nundle Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 23 | 15.0 | 24 | 15.0 | 0.015 | 0.0 | LOS A | 0.0 | 0.1 | 0.04 | 0.05 | 0.04 | 78.8 |
| 9 R2 | 2 | 15.0 | 2 | 15.0 | 0.015 | 7.2 | LOS A | 0.0 | 0.1 | 0.04 | 0.05 | 0.04 | 66.8 |
| Approach | 25 | 15.0 | 26 | 15.0 | 0.015 | 0.6 | NA | 0.0 | 0.1 | 0.04 | 0.05 | 0.04 | 77.6 |
| West: Linsays Gap Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 1 | 15.0 | 1 | 15.0 | 0.021 | 7.5 | LOS A | 0.1 | 0.5 | 0.20 | 0.61 | 0.20 | 60.1 |
| 12 R 2 | 21 | 15.0 | 22 | 15.0 | 0.021 | 7.4 | LOS A | 0.1 | 0.5 | 0.20 | 0.61 | 0.20 | 59.5 |
| Approach | 22 | 15.0 | 23 | 15.0 | 0.021 | 7.4 | LOS A | 0.1 | 0.5 | 0.20 | 0.61 | 0.20 | 59.6 |
| All Vehicles | 142 | 15.0 | 149 | 15.0 | 0.057 | 2.6 | NA | 0.1 | 0.5 | 0.04 | 0.23 | 0.04 | 71.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## SITE LAYOUT

$\nabla$ Site: 101 [2021 AM Oakenville Rd - Jenkins St (Site Folder:
Existing)]
New Site
Site Category: (None)
Give-Way (Two-Way)

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.

## 1 N



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## MOVEMENT SUMMARY

$\nabla$ Site: 101 [2021 AM Oakenville Rd - Jenkins St (Site Folder:
Existing)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { INF } \\ & \text { VOLI } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay sec $\qquad$ | Level of Service | $\begin{gathered} \text { 95\% B B } \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Oakenville Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 11 | 2.0 | 12 | 2.0 | 0.009 | 5.6 | LOS A | 0.0 | 0.2 | 0.05 | 0.55 | 0.05 | 53.4 |
| 2 T1 | 13 | 2.0 | 14 | 2.0 | 0.022 | 4.9 | LOSA | 0.1 | 0.6 | 0.15 | 0.50 | 0.15 | 53.9 |
| 3 R2 | 8 | 2.0 | 8 | 2.0 | 0.022 | 5.9 | LOSA | 0.1 | 0.6 | 0.15 | 0.50 | 0.15 | 53.6 |
| Approach | 32 | 2.0 | 34 | 2.0 | 0.022 | 5.4 | LOS A | 0.1 | 0.6 | 0.11 | 0.52 | 0.11 | 53.7 |
| East: Oakenville Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 3 | 2.0 | 3 | 2.0 | 0.002 | 5.6 | LOSA | 0.0 | 0.0 | 0.00 | 0.58 | 0.00 | 53.5 |
| 5 T1 | 10 | 15.0 | 11 | 15.0 | 0.010 | 0.0 | LOSA | 0.0 | 0.3 | 0.04 | 0.22 | 0.04 | 57.7 |
| 6 R2 | 6 | 2.0 | 6 | 2.0 | 0.010 | 5.6 | LOS A | 0.0 | 0.3 | 0.04 | 0.22 | 0.04 | 55.8 |
| Approach | 19 | 8.8 | 20 | 8.8 | 0.010 | 2.7 | NA | 0.0 | 0.3 | 0.04 | 0.28 | 0.04 | 56.4 |
| North: Oakenville Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 9 | 2.0 | 9 | 2.0 | 0.007 | 5.6 | LOSA | 0.0 | 0.2 | 0.03 | 0.56 | 0.03 | 53.4 |
| 8 T1 | 7 | 2.0 | 7 | 2.0 | 0.018 | 4.9 | LOSA | 0.1 | 0.5 | 0.15 | 0.52 | 0.15 | 53.8 |
| 9 R2 | 9 | 2.0 | 9 | 2.0 | 0.018 | 6.0 | LOSA | 0.1 | 0.5 | 0.15 | 0.52 | 0.15 | 53.1 |
| Approach | 25 | 2.0 | 26 | 2.0 | 0.018 | 5.5 | LOS A | 0.1 | 0.5 | 0.11 | 0.53 | 0.11 | 53.4 |
| West: Oakenville Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 8 | 2.0 | 8 | 2.0 | 0.005 | 5.6 | LOSA | 0.0 | 0.0 | 0.00 | 0.58 | 0.00 | 53.5 |
| 11 T1 | 4 | 15.0 | 4 | 15.0 | 0.008 | 0.0 | LOS A | 0.0 | 0.2 | 0.06 | 0.37 | 0.06 | 56.2 |
| 12 R2 | 8 | 2.0 | 8 | 2.0 | 0.008 | 5.6 | LOSA | 0.0 | 0.2 | 0.06 | 0.37 | 0.06 | 54.9 |
| Approach | 20 | 4.6 | 21 | 4.6 | 0.008 | 4.5 | NA | 0.0 | 0.2 | 0.04 | 0.45 | 0.04 | 54.6 |
| All <br> Vehicles | 96 | 3.9 | 101 | 3.9 | 0.022 | 4.7 | NA | 0.1 | 0.6 | 0.08 | 0.46 | 0.08 | 54.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 101 [2021 PM Oakenville Rd - Jenkins St (Site Folder:
Existing)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INF } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. <br> Satn <br> v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver Speed km/h |
| South: Oakenville Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 11 | 2.0 | 12 | 2.0 | 0.009 | 5.6 | LOSA | 0.0 | 0.2 | 0.05 | 0.55 | 0.05 | 53.4 |
| 2 T1 | 13 | 2.0 | 14 | 2.0 | 0.022 | 4.9 | LOSA | 0.1 | 0.6 | 0.15 | 0.50 | 0.15 | 53.9 |
| 3 R2 | 8 | 2.0 | 8 | 2.0 | 0.022 | 5.9 | LOSA | 0.1 | 0.6 | 0.15 | 0.50 | 0.15 | 53.6 |
| Approach | 32 | 2.0 | 34 | 2.0 | 0.022 | 5.4 | LOS A | 0.1 | 0.6 | 0.11 | 0.52 | 0.11 | 53.7 |
| East: Oakenville Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 3 | 2.0 | 3 | 2.0 | 0.002 | 5.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.58 | 0.00 | 53.5 |
| 5 T1 | 10 | 15.0 | 11 | 15.0 | 0.010 | 0.0 | LOSA | 0.0 | 0.3 | 0.04 | 0.22 | 0.04 | 57.7 |
| 6 R2 | 6 | 2.0 | 6 | 2.0 | 0.010 | 5.6 | LOSA | 0.0 | 0.3 | 0.04 | 0.22 | 0.04 | 55.8 |
| Approach | 19 | 8.8 | 20 | 8.8 | 0.010 | 2.7 | NA | 0.0 | 0.3 | 0.04 | 0.28 | 0.04 | 56.4 |
| North: Oakenville Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 9 | 2.0 | 9 | 2.0 | 0.007 | 5.6 | LOSA | 0.0 | 0.2 | 0.03 | 0.56 | 0.03 | 53.4 |
| 8 T1 | 7 | 2.0 | 7 | 2.0 | 0.018 | 4.9 | LOSA | 0.1 | 0.5 | 0.15 | 0.52 | 0.15 | 53.8 |
| 9 R2 | 9 | 2.0 | 9 | 2.0 | 0.018 | 6.0 | LOSA | 0.1 | 0.5 | 0.15 | 0.52 | 0.15 | 53.1 |
| Approach | 25 | 2.0 | 26 | 2.0 | 0.018 | 5.5 | LOSA | 0.1 | 0.5 | 0.11 | 0.53 | 0.11 | 53.4 |
| West: Oakenville Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 8 | 2.0 | 8 | 2.0 | 0.005 | 5.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.58 | 0.00 | 53.5 |
| 11 T1 | 4 | 15.0 | 4 | 15.0 | 0.008 | 0.0 | LOSA | 0.0 | 0.2 | 0.06 | 0.37 | 0.06 | 56.2 |
| 12 R 2 | 8 | 2.0 | 8 | 2.0 | 0.008 | 5.6 | LOSA | 0.0 | 0.2 | 0.06 | 0.37 | 0.06 | 54.9 |
| Approach | 20 | 4.6 | 21 | 4.6 | 0.008 | 4.5 | NA | 0.0 | 0.2 | 0.04 | 0.45 | 0.04 | 54.6 |
| All <br> Vehicles | 96 | 3.9 | 101 | 3.9 | 0.022 | 4.7 | NA | 0.1 | 0.6 | 0.08 | 0.46 | 0.08 | 54.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 101 [2021 AM Oakenville Rd - Jenkins St (Site Folder:
Project Scenario)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { INF } \\ & \text { VOLI } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay sec $\qquad$ | Level of Service | $\begin{gathered} \text { 95\% B B } \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Oakenville Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 11 | 2.0 | 12 | 2.0 | 0.009 | 5.7 | LOS A | 0.0 | 0.2 | 0.11 | 0.54 | 0.11 | 53.2 |
| 2 T1 | 13 | 2.0 | 14 | 2.0 | 0.026 | 5.8 | LOSA | 0.1 | 0.7 | 0.31 | 0.53 | 0.31 | 53.4 |
| 3 R2 | 8 | 2.0 | 8 | 2.0 | 0.026 | 6.9 | LOSA | 0.1 | 0.7 | 0.31 | 0.53 | 0.31 | 53.0 |
| Approach | 32 | 2.0 | 34 | 2.0 | 0.026 | 6.0 | LOS A | 0.1 | 0.7 | 0.24 | 0.54 | 0.24 | 53.2 |
| East: Oakenville Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 3 | 2.0 | 3 | 2.0 | 0.002 | 5.6 | LOSA | 0.0 | 0.0 | 0.00 | 0.58 | 0.00 | 53.5 |
| 5 T1 | 35 | 15.0 | 37 | 15.0 | 0.026 | 0.1 | LOS A | 0.0 | 0.3 | 0.07 | 0.09 | 0.07 | 58.8 |
| 6 R2 | 6 | 2.0 | 6 | 2.0 | 0.026 | 5.9 | LOS A | 0.0 | 0.3 | 0.07 | 0.09 | 0.07 | 56.9 |
| Approach | 44 | 12.3 | 46 | 12.3 | 0.026 | 1.2 | NA | 0.0 | 0.3 | 0.06 | 0.12 | 0.06 | 58.2 |
| North: Oakenville Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 9 | 2.0 | 9 | 2.0 | 0.008 | 5.9 | LOSA | 0.0 | 0.2 | 0.18 | 0.54 | 0.18 | 53.0 |
| 8 T1 | 7 | 2.0 | 7 | 2.0 | 0.021 | 5.7 | LOSA | 0.1 | 0.6 | 0.32 | 0.55 | 0.32 | 53.3 |
| 9 R2 | 9 | 2.0 | 9 | 2.0 | 0.021 | 6.9 | LOSA | 0.1 | 0.6 | 0.32 | 0.55 | 0.32 | 52.6 |
| Approach | 25 | 2.0 | 26 | 2.0 | 0.021 | 6.2 | LOSA | 0.1 | 0.6 | 0.27 | 0.54 | 0.27 | 52.9 |
| West: Oakenville Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 8 | 2.0 | 8 | 2.0 | 0.005 | 5.6 | LOSA | 0.0 | 0.0 | 0.00 | 0.58 | 0.00 | 53.5 |
| 11 T1 | 82 | 15.0 | 86 | 15.0 | 0.055 | 0.0 | LOS A | 0.1 | 0.4 | 0.02 | 0.05 | 0.02 | 59.3 |
| 12 R2 | 8 | 2.0 | 8 | 2.0 | 0.055 | 5.7 | LOSA | 0.1 | 0.4 | 0.02 | 0.05 | 0.02 | 57.9 |
| Approach | 98 | 12.9 | 103 | 12.9 | 0.055 | 0.9 | NA | 0.1 | 0.4 | 0.02 | 0.09 | 0.02 | 58.7 |
| All <br> Vehicles | 199 | 9.6 | 209 | 9.6 | 0.055 | 2.5 | NA | 0.1 | 0.7 | 0.10 | 0.23 | 0.10 | 56.9 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 101 [2021 PM Oakenville Rd - Jenkins St (Site Folder:
Project Scenario)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { INF } \\ & \text { VOLI } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay sec $\qquad$ | Level of Service | $\begin{gathered} \text { 95\% B B } \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Oakenville Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 11 | 2.0 | 12 | 2.0 | 0.009 | 5.7 | LOS A | 0.0 | 0.2 | 0.11 | 0.54 | 0.11 | 53.2 |
| 2 T1 | 13 | 2.0 | 14 | 2.0 | 0.029 | 5.8 | LOSA | 0.1 | 0.8 | 0.32 | 0.54 | 0.32 | 53.3 |
| 3 R2 | 10 | 2.0 | 11 | 2.0 | 0.029 | 6.9 | LOSA | 0.1 | 0.8 | 0.32 | 0.54 | 0.32 | 53.0 |
| Approach | 34 | 2.0 | 36 | 2.0 | 0.029 | 6.1 | LOS A | 0.1 | 0.8 | 0.25 | 0.54 | 0.25 | 53.2 |
| East: Oakenville Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 4 | 2.0 | 4 | 2.0 | 0.002 | 5.6 | LOSA | 0.0 | 0.0 | 0.00 | 0.58 | 0.00 | 53.5 |
| 5 T1 | 35 | 15.0 | 37 | 15.0 | 0.026 | 0.1 | LOS A | 0.0 | 0.3 | 0.07 | 0.09 | 0.07 | 58.8 |
| 6 R2 | 6 | 2.0 | 6 | 2.0 | 0.026 | 5.9 | LOS A | 0.0 | 0.3 | 0.07 | 0.09 | 0.07 | 56.9 |
| Approach | 45 | 12.1 | 47 | 12.1 | 0.026 | 1.3 | NA | 0.0 | 0.3 | 0.06 | 0.13 | 0.06 | 58.1 |
| North: Oakenville Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 9 | 2.0 | 9 | 2.0 | 0.008 | 5.9 | LOSA | 0.0 | 0.2 | 0.18 | 0.54 | 0.18 | 53.0 |
| 8 T1 | 7 | 2.0 | 7 | 2.0 | 0.021 | 5.7 | LOSA | 0.1 | 0.6 | 0.32 | 0.55 | 0.32 | 53.3 |
| 9 R2 | 9 | 2.0 | 9 | 2.0 | 0.021 | 6.9 | LOSA | 0.1 | 0.6 | 0.32 | 0.55 | 0.32 | 52.6 |
| Approach | 25 | 2.0 | 26 | 2.0 | 0.021 | 6.2 | LOSA | 0.1 | 0.6 | 0.27 | 0.54 | 0.27 | 52.9 |
| West: Oakenville Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 8 | 2.0 | 8 | 2.0 | 0.005 | 5.6 | LOSA | 0.0 | 0.0 | 0.00 | 0.58 | 0.00 | 53.5 |
| 11 T1 | 82 | 15.0 | 86 | 15.0 | 0.055 | 0.0 | LOS A | 0.1 | 0.4 | 0.03 | 0.05 | 0.03 | 59.3 |
| 12 R2 | 8 | 2.0 | 8 | 2.0 | 0.055 | 5.7 | LOSA | 0.1 | 0.4 | 0.03 | 0.05 | 0.03 | 57.9 |
| Approach | 98 | 12.9 | 103 | 12.9 | 0.055 | 0.9 | NA | 0.1 | 0.4 | 0.02 | 0.09 | 0.02 | 58.7 |
| All <br> Vehicles | 202 | 9.5 | 213 | 9.5 | 0.055 | 2.5 | NA | 0.1 | 0.8 | 0.10 | 0.23 | 0.10 | 56.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^4]
## Appendix C

## Muswellbrook Council Meeting Minutes

## Muswellbrook Shire Council - Hills Of Gold Wind Farm

Meeting to discuss key points from Council Submission

| Date | $31 / 03 / 2021$ |  |  |  |
| :--- | :--- | :--- | :--- | :--- |
| Time | 11am AET |  |  |  |
| Meeting Subject | Hills Of Gold Wind Farm - Key Council Concerns |  |  |  |
| Venue | Council Offices | - Muswellbrook |  |  |
| Attendees $(\checkmark) /$ | In attendance | Name | Company |  |
| Apologies $(\times)$ |  | Jamie Chivers | Someva | JC |
|  |  | Alex Henderson | Someva | AH |
|  |  | Liam Edgeworth | Someva | LE |
|  |  | Aref Taleb | Someva | AT |
|  |  | Fiona Plesman | MSC | FP |
|  |  | Sharon Pope | MSC | SP |
|  |  | Derek Finnegan | MSC | DF |
|  |  | Peter Chambers | MSC | PC |
|  |  | Kellie Scholes | MSC | KS |
|  |  | Meredith Andrews | Engie | MA |
|  |  | Jody Doran | Engie | JD |
|  |  | Warrick Andrews | RJA | WA |
|  |  | Stephen Read | TTPP | SR |
|  |  | Amanda Antcliff | ERM | AA |
|  |  |  |  |  |


| Item | Subject | Action By Who | Due Date |
| :---: | :---: | :---: | :---: |
| 1 | Traffic and Transport |  |  |
| 1.1 | The Projects proposal of a road usage fee was deemed acceptable following proposal review. Someva to issue |  |  |
| 1.2 | The project offered to include a statement to commit to structural assessment being carried out on a list of council assets to determine integrity and impact on design life. If the project is approved this would need to be undertaken as part of S138 approvals with council. |  |  |
| 1.3 | Council confirmed that as a requirement, structural assessments and bridge load analysis would need to be conducted on all affected/used structures along the proposed project route - Council to issue asset list | MSC | 20/04/21 |
| 1.4 | Council also confirmed that not all these assets are council owned, and that individual landowners would need to be approached to carry out the assessments as well. It estimated that approx. 20 structures in total may need to be assessed |  |  |

## Muswellbrook Shire Council - Hills Of Gold Wind Farm

Meeting to discuss key points from Council Submission

| Item | Subject | Action By Who | Due Date |
| :---: | :---: | :---: | :---: |
| 1.5 | Council noted that the box culvert on Wybong road would need to be replaced |  |  |
| 1.6 | Council requires that the project must demonstrate diligently the full measures being taken to ensure that safety is not impacted along the proposed transport route |  |  |
| 1.7 | There was deemed to be not enough information on traffic volumes and movements with the EIS. Data and information required for both the construction and operational phases | Someva | May 2021 |
| 1.8 | Traffic data should include areas out with the immediate project area |  |  |
| 1.9 | Blade movements and blade volumes to be included in updated reports and issued to council for review |  |  |
| 1.10 | Council expressed concern over the proposed use of Bell St Rd, citing the presence of the school at the top of the hill accommodating over 1500 students. |  |  |
| 1.11 | The project confirmed that road usage outside of restricted times such as School bus hours would all be included in the Traffic and Transport Management Management Plan (TTMP) |  |  |
| 1.12 | The Muswellbrook bypass was signalled as a possible preferred option to avoid local roads however the timing of this was raised as not viable for the projects timelines |  |  |
| 1.13 | Council expressed an initial preference that a single route option would be preferable for both blades and tower components |  |  |
| 1.14 | The project discussed investigating splitting traffic to reduce impact on Bell St, Victoria St and Market St. |  |  |
| 1.15 | The project confirmed that traffic management plans for the Kyuga/Wybong intersection, Bollards would be used to restrict non project use and that the project would intend to retain a right to use over the intersection upgrade throughout the projects operational phases |  |  |
| 1.16 | Council noted that ARTC also intend on building 3 new bridges over rail line in a similar timescale creating potential works conflicts |  |  |
| 1.17 | Council suggested that the Mt Pleasant mine traffic data, recently published, would be a useful resource for the project as it is the most up to date data collated on traffic movements and volumes |  |  |
| 1.18 | Council expressed a desire to arrange a further meeting once new route options have been finalised and issued. |  |  |

## Muswellbrook Shire Council - Hills Of Gold Wind Farm

Meeting to discuss key points from Council Submission

| Item | Subject | Action By Who | Due Date |
| :---: | :---: | :---: | :---: |
| 1.19 | Council noted that MACH energy also intend on carrying out road upgrades at a similar time to the projects proposed upgrades creating the possibility of works conflicts. |  |  |
| 2 | Community Engagement |  |  |
| 2.1 | The Project issued a stakeholder engagement list in hard copy to all attendees that detailed all engagements to date with the local community. This included local businesses, studs and landowners |  |  |
| 2.2 | The project confirmed that local Mines had also been approached and received a generally positive response |  |  |
| 2.3 | The project confirmed that we are committed to working with the mines and to continue to consult as part of the TTMP. |  |  |
| 3 | General |  |  |
| 3.1 | Council confirmed that they would like to see a proposed Term Sheet on road usage as well as a statement of commitments provided by the project for review |  |  |
| 3.2 | Council believed it unlikely that they would be ready to offer an audience with councillors before the May Councillors meeting |  |  |
| 4 | Key Actions |  |  |
| 4.1 | Someva to issue Term Sheet on road usage to Council for review by the next Council meeting at the end of April. | Someva | 31/04/21 |
| 4.2 | Council to Issue asset list for inclusion into the structural assessments to be committed by the project for structural assessment and design life impact | MSC | 20/04/21 |
| 4.3 | Council to confirm whether the project is to meet with Councillors at the April or May meeting | MSC | 16/04/21 |
| 4.4 | Someva to issue Road Usage Contribution Voluntary Planning Agreement proposal for review | Someva | 31/04/21 |
| 4.5 | Someva to provide greater detail on traffic types, volumes and movements, including beyond the immediate project area | Someva | May 2021 |
| 4.6 | Someva to contact MACH energy and ARTC to confirm their programme of proposed upgrades and ensure no works conflicts exist | Someva | 31/04/21 |

## Someva Presentation

Someva presented a powerpoint presentation to address the points as detailed above. This is provided separately.
transport planning

## Appendix D

Summary of Consultation and Commitments

### 6.1 DRAFT VOLUNTARY PLANNING AGREEMENT BETWEEN HILLS OF GOLD WIND FARM PTY LTD AND MUSWELLBROOK SHIRE COUNCIL

Attachments:<br>A. Hills of Gold - Council submission<br>B. Hills of Gold - Letter of Offer<br>Responsible Officer:<br>Author:<br>Community Plan Issue:<br>Community Plan Goal:<br>Community Plan Strategy:<br>Derek Finnigan - Deputy General Manager<br>Michelle Sandell-Hay - PA to the General Manager<br>A Council that is well managed, efficient and properly resourced and that is responsive to its communities and stakeholders<br>Maintain a strong focus on financial discipline to enable Council to properly respond to the needs of the communities it serves.<br>Appropriate matters are reported to Council in a timely manner in accordance with the Financial Control and Reporting Policy.

## PURPOSE

To consider the Letter of Offer from Hills of Gold to Muswellbrook Shire Council for use of local roads in the Shire.

## OFFICER'S RECOMMENDATION

## The Committee:

1. Notes the Letter of Offer from Hills of Gold Wind Farm Pty Ltd and concerns of staff;
2. Resolves that the preferred option for transport of long, heavy and otherwise oversize components is Option 1 as outlined in the Letter of Offer from Hills of Gold Wind Farm Pty Ltd;
3. Authorises staff to continue to negotiate with Hills of Gold Wind Farm Pty Ltd on a road usage fee, Indemnity Deed and Bond for asset failure that exceeds general dilapidation, and the need for dilapidation surveys; and
4. Authorises staff to remove Council's objection to SSD 9679 staff are satisfied with the results of negotiations with Hills of Gold Wind Farm Pty Ltd.

Moved: $\qquad$ Seconded: $\qquad$

## REPORT

Hills of Gold Wind Farm Pty Ltd (Hills of Gold) lodged a State Significant Development Application for a wind farm and associated infrastructure located 50 km south-east of Tamworth and 8 km south of Nundle, comprising up to 70 wind turbines, battery storage and grid connection with the Department of Planning, Industry and Environment in 2019. Council made a submission objecting to the proposed use of local roads in the Shire for the transportation of the over-size elements of the towers. A copy of the submission is provided in Attachment A.
Hills of Gold has offered a package of infrastructure works and funding to enable them to use the Shire's local road network (subject only to the execution of a voluntary planning agreement or similar agreement by the parties to formalise these matters on terms acceptable to each party and to the approval of the Development Application). A copy of the offer is provided in Attachment B. A summary is provided below:

1. Route Assessment and Upgrade Works:
(a) Hills of Gold will consult with MSC to determine those Council Assets which require a detailed structural assessment to be undertaken to assess their structural suitability for use by Project OSOM traffic and will engage a suitably qualified, independent expert acceptable to MSC to undertake that structural assessment. Such engagement would be at Hills of Gold cost, however, may require assistance from MSC to facilitate the assessment, in particular the provision of any existing data on, or previously completed assessment of, those Council Assets.
(b) If any Council Asset is found to be structurally inadequate for the transport of the expected equipment loads, Hills of Gold will, at its cost:
(1) upgrade each such Council Asset to the extent reasonably required to ensure it is structurally adequate and suitable for the expected Project loads and consult with MSC to incorporate any reasonable requirements of MSC in respect of such upgrade, and
(2) provide, or have its contractor provide, a performance bond in favour of MSC in the form of a letter of credit or bank guarantee to secure its performance of such upgrade works, with such bond to be for a reasonable amount having regard to the cost of the upgrade works and to be provided prior to the commencement of the upgrade works. Any such performance bond would be released upon completion of the upgrade works.

## Council staff comment

This aspect of the offer is generally acceptable; however, the performance bond should also cover key assets that were assessed to not require upgrade to cover the potential for the assessment to have been incorrect and subsequent failure of the assets.

## 2. Road Usage Fee

Hills of Gold will pay a one-off, road usage fee of $\$ 70,000$ to MSC upon the commencement of construction of the Project to compensate MSC for any dilapidation which may be caused by the general use of roads within the MSC by traffic associated with the Project. Due to the volume of traffic which already uses roads within the MSC, it will likely be impractical to commission a dilapidation survey which can identify only that dilapidation attributable to Project traffic. Accordingly, the one-off, road usage fee is proposed as an alternative to a dilapidation survey to provide greater certainty to MSC.

## Council staff comment

The less adequate sections of road identified as part of Option 1 for the transport of long, heavy and otherwise oversize components are primarily Wybong Road and Kayuga Road. These roads are not subject to high volumes of truck traffic and Council has conditions limiting the use of these roads by traffic related to Mt Pleasant, Bengalla and Mangoola mines. Historical information on approvals for OSOM vehicles to use these roads supports this position. As a result, it will be likely that any dilapidation observed during the 9 months that components are transported along this road can be attributed to the Hills of Gold project.

Staff consider that having a dilapidation survey completed at the beginning of the project and every 3 months to the end of the project will be an objective assessment of dilapidation. The $\$ 70,000$ offered for general dilapidation is low and would only really cover cost of staff time involved in monitoring impacts of traffic movements on the road network.

Finally, Hills of Gold have nominated three options for routes to transport the long, heavy or otherwise oversize components. Option 1 relies on the local roads to the west of the Hunter River and the New England Highway. Option 2 and Option 3 include some loads using Bell Street. Option 1 is the preference of staff.

## CONCLUSION

Council staff do not consider that the Letter of Offer is acceptable, however it does demonstrate a willingness by Hills of Gold to discuss a way forward.

It is recommended that Hills of Gold be advised that the preferred option for transport of long, heavy and otherwise oversize components is Option 1 but that the current Offer is inadequate. Council staff should be authorised to negotiate with Hills of Gold Wind Farm Pty Ltd on a road usage fee, Indemnity Deed and Bond for asset failure that exceeds general dilapidation, and the need for dilapidation surveys.

If staff are satisfied with the results of negotiations with Gold Wind Farm Pty Ltd there is no need for Council to maintain an objection to SSD 9679.

## FINANCIAL IMPLICATIONS

The VPA proposes a one-off payment of $\$ 70,000$ for road usage fees in lieu of attempting to assess road dilapidation. This is considered inadequate.

## RISK MANAGEMENT IMPLICATIONS

The VPA proposes a one-off payment of $\$ 70,000$ for road usage fees in lieu of attempting to assess road dilapidation. Once the Asset structural assessment is completed it may be easier to determine the likely risk to Council.
transport planning

## AppendixE

Muswellb rook Shire Council Asset List for Assessment

Measurements start at Denman Road and finish at the end of the shire marker
Distances are calculated from a desk top exercise as Wybong Road east is currently closed due to road works.

| Road | Chainage m | Pipe Info |  | Size mm | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Pipe/ RCBC | No |  |  |
| Bengalla Road | 350 | RCBC | 5 | $2100 \times 400$ | Major Culvert |
|  | 695 | Pipe | 1 | 300 |  |
|  | 1470-1670 | Keys Bridge |  |  | Bridge |
|  | 2340 | RCBC | 1 | $3400 \times 1800$ |  |
|  | 3000 | Pipe | 1 | 400 |  |
|  | 3420 | Pipe | 1 | 400 |  |
|  | 3830 | RCBC | 5 | $3400 \times 1800$ | Major Culvert |
|  | 4260 | Rail Overpass |  |  |  |
|  | 4820 | Pipe | 1 | 900 |  |
|  | 5131 | RCBC | 1 | $800 \times 500$ |  |
|  | 5440 | RCBC | 1 | $2100 \times 500$ |  |
|  | 5830 | Pipe | 2 | $500 \times 500$ |  |
|  | 6200 | RCBC | 1 | $1200 \times 770$ |  |
|  | 6410 | Pipe | 4 | $1650 \times 1650$ | Major Culvert |
|  | 6650 | Rail Bridge |  |  | Bridge - Mt Pleasant loop |
|  | 6770 | Pipe | 1 | 670 |  |
|  | 8550 | Pipe | 1 | 600 |  |
|  | 8900 | Pipe | 1 | 600 |  |
|  | 9421 | Pipe | 1 | 300 |  |
|  |  |  |  |  | Intersection Bengalla Road and Wybong Road |
| Wybong Road East | 9910 | Pipe | 1 | 450 |  |
|  | 10140 | Pipe | 1 | 450 |  |
|  | 11145 | Pipe | 1 | 450 |  |
|  | 11375 | Pipe | 1 | 900 |  |
|  | 11869 | Pipe | 1 | 450 |  |
|  | 12035 | Pipe | 1 | 450 |  |
|  | 12315 | RCBC | 2 | 600 |  |
|  | 12955 | Pipe | 1 | 1500 |  |
|  | 13120 | Pipe | 3 | 1500 |  |
|  | 13440 | Pipe | 1 | 450 |  |
|  | 13820 | Pipe | 1 | 450 |  |
|  | 14515 | Pipe | 1 | 450 |  |
|  | 15045 | Pipe | 1 | 600 |  |
|  | 15245 | Pipe | 1 | 600 |  |
|  | 15580 | Pipe | 1 | 450 |  |
|  | 15905 | Pipe | 1 | 450 |  |
|  | 16365 | RCBC | 3 | $2400 \times 1200$ | Major Culvert |
|  | 16525 | RCBC | 1 | $1200 \times 350$ |  |
|  | 16683 | RCBC | 4 | $1200 \times 350$ |  |
|  | 16905 |  |  |  | Rosebrook Bridge |
|  | 17090 | RCBC | 4 | $1200 \times 350$ |  |
|  | 17965 |  |  |  | Floodway |
|  | 18570 | Pipe | 1 | 450 |  |
|  |  |  |  |  | Intersection Wybong Road and Kayuga Road |
| Kayuga Road | 19085 | Pipe | 1 | 450 | Pipe (only) runs parallel to pavement - gully pit system across intersection |
|  | 19085 | Pipe | 1 | 375 | Gully pit system |
|  | 19145 | Pipe | 1 | 450 | Pipe (only) runs parallel to pavement - gully pit system |
|  | 19255 | Pipe | 1 | 450 | pipe back flow valve - gully pit system |
|  | 19265 | RCBC | 8 | 300 | Major Culvert |
|  | 19545 | RCBC | 2 | 300 |  |
|  | 20790 | RCBC | 2 | 300 |  |
|  | 20995 | RCBC | 3 | $1200 \times 600$ |  |
|  | 21005 | RCBC | 1 | $1200 \times 600$ |  |
|  | 21745 | Pipe | 1 | 450 |  |
|  | 21855 | Pipe | 2 | 1200 |  |
|  | 22460 | Pipe | 1 | 450 |  |
|  | 22950 | Pipe | 1 | 450 |  |
|  | 23135 | RCBC | 2 | 600 |  |
|  | 23475 | Pipe | 1 | 450 |  |
|  | 23655 | Pipe | 1 | 450 |  |
|  | 24395 | RCBC | 2 | 300 |  |
|  | 24710 | RCBC | 7 | 2400 | Major Culvert |
|  | 25210 | Pipe | 1 | 450 |  |
|  | 25445 | Pipe | 1 | 450 |  |
|  |  |  |  |  | Dartbrook Mine Entrance Road |
|  | 25565 | Pipe | 1 | 450 |  |
|  | 25700 | Pipe | 1 | 450 |  |
|  | 25815 | Pipe | 4 | 1200 |  |
|  | 26230 | Pipe | 1 | 450 |  |
|  |  |  |  |  | end of shire |
|  |  |  |  |  |  |
|  |  |  |  |  |  |

## Appendix F

Muswellbrook Shire Council Letter of Offer

Fiona Plesman
General Manager
Muswellbrook Shire Council
Via email

2 June 2021

Dear Fiona,

## Voluntary Contribution from Hills of Gold Wind Farm Pty Ltd

Thank you for your and your team's time on 31 March 2021 to discuss Muswellbrook Shire Council's (MSC) concerns regarding the proposed use of council roads and assets by traffic associated with the Hills of Gold Wind Farm (the "Project") which is the subject of Development Application Number SSD-9679 (the "Development Application").

We appreciated the constructive suggestion of your team to progress an agreement with MSC to address those concerns, specifically those in respect of the proposed use of those council roads and council-owned assets set out in the subsequently provided list in Annexure A (Council Assets).

We confirm we have undertaken further assessment on the alternate route options available based on feedback from MSC. The Project, via its Response to Submission Report, will propose new route options for heavy, oversize / overmass (OSOM) vehicles which will reduce impacts on existing traffic volumes as compared to the initial route proposed. To provide some further detail in this respect, Annexure B provides a summary of estimated OSOM traffic type and volumes by route, as well as a map showing the additional route options. We will continue to engage with MSC as we progress final turbine selection, selection of a logistics contractor and assess the Council Assets to determine the most suitable route option(s).

In the meantime and further to our recent discussions, we confirm that the Project proponent, Hills of Gold Wind Farm Pty Ltd (ACN 145173 324) ("HOGWFPL"), is also willing to make the following offer to MSC in respect of the proposed use of any Council Assets as part of the final route selection (subject only to the execution of a voluntary planning agreement or similar agreement by the parties to formalise these matters on terms acceptable to each party and to the approval of the Development Application):

## eNGie

## 1. Route Assessment and Upgrade Works:

(a) HOGWFPL will consult with MSC to determine those Council Assets which require a detailed structural assessment to be undertaken to assess their structural suitability for use by Project OSOM traffic and will engage a suitably qualified, independent expert acceptable to MSC to undertake that structural assessment. Such engagement would be at HOGWFPL's cost, however, we may require reasonable assistance from MSC to facilitate the assessment, in particular, the provision of any existing data on, or previously completed assessment of, those Council Assets.
(b) If any Council Asset is found by the independent expert to be structurally inadequate for the transport of the expected equipment loads for the Project and that Council Asset is proposed to be used as part of the final transport route for the Project, HOGWFPL will, at its cost (1) upgrade each such Council Asset to the extent reasonably required to ensure it is structurally adequate and suitable for the expected Project loads and consult with MSC to incorporate any reasonable requirements of MSC in respect of such upgrade, and (2) provide, or have its contractor provide, a performance bond in favour of MSC in the form of a letter of credit or bank guarantee to secure its performance of such upgrade works, with such bond to be for a reasonable amount having regard to the cost of the upgrade works and to be provided prior to the commencement of the upgrade works. Any such performance bond would be released upon completion of the upgrade works.
2. Road Usage Fee: In addition, HOGWFPL will pay a one-off, road usage fee of $\$ 70,000$ to MSC upon the commencement of construction of the Project to compensate MSC for any dilapidation which may be caused by the general use of roads within the MSC by traffic associated with the Project. Due to the volume of traffic which already uses roads within the MSC, it will likely be impractical to commission a dilapidation survey which can identify only that dilapidation attributable to Project traffic. Accordingly, the one-off, road usage fee is proposed as an alternative to a dilapidation survey to provide greater certainty to MSC.

If the above offer is acceptable to MSC, please sign where indicated below to confirm such acceptance. Once signed, a copy will be provided to the Department of Planning for inclusion of the relevant commitments by HOGWFPL in the Project's Statement of Commitments.

We look forward to hearing from you and would welcome any further discussion in respect of any remaining queries.

Yours sincerely,
DocuSigned by:
Herlul

General Manager - Asset Development

## ACCEPTANCE BY MUSWELLBROOK SHIRE COUNCIL:

Subject only to the execution of a voluntary planning agreement or similar agreement by the parties to formalise these matters (and to the approval of the Development Application), Muswellbrook Shire Council hereby confirms its acceptance of the terms contained in this letter.

Signed for and on behalf of Muswellbrook Shire Council by:

## Signature

Name (please print)

Position (please print)

## ENGIE

## APPENDIX A - List of Council Assets

| Road | Chainage m | Pipe Info |  | Size mm | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Pipe/ RCBC | No |  |  |
| Bengalla Road | 350 | RCBC | 5 | $2100 \times 400$ | Major Culvert |
|  | 695 | Pipe | 1 | 300 |  |
|  | 1470-1670 | Keys Bridge |  |  | Bridge |
|  | 2340 | RCBC | 1 | $3400 \times 1800$ |  |
|  | 3000 | Pipe | 1 | 400 |  |
|  | 3420 | Pipe | 1 | 400 |  |
|  | 3830 | RCBC | 5 | $3400 \times 1800$ | Major Culvert |
|  | 4260 | Rail Overpass |  |  |  |
|  | 4820 | Pipe | 1 | 900 |  |
|  | 5131 | RCBC | 1 | $800 \times 500$ |  |
|  | 5440 | RCBC | 1 | $2100 \times 500$ |  |
|  | 5830 | Pipe | 2 | $500 \times 500$ |  |
|  | 6200 | RCBC | 1 | $1200 \times 770$ |  |
|  | 6410 | Pipe | 4 | $\begin{gathered} 1650 x \\ 1650 \\ \hline \end{gathered}$ | Major Culvert |
|  | 6650 | Rail Bridge |  |  | Bridge - Mt Pleasant loop |
|  | 6770 | Pipe | 1 | 670 |  |
|  | 8550 | Pipe | 1 | 600 |  |
|  | 8900 | Pipe | 1 | 600 |  |
|  | 9421 | Pipe | 1 | 300 |  |
|  |  |  |  |  | Intersection Bengalla Road and Wybong Road |
| Wybong Road East | 9910 | Pipe | 1 | 450 |  |
|  | 10140 | Pipe | 1 | 450 |  |
|  | 11145 | Pipe | 1 | 450 |  |
|  | 11375 | Pipe | 1 | 900 |  |
|  | 11869 | Pipe | 1 | 450 |  |
|  | 12035 | Pipe | 1 | 450 |  |
|  | 12315 | RCBC | 2 | 600 |  |
|  | 12955 | Pipe | 1 | 1500 |  |
|  | 13120 | Pipe | 3 | 1500 |  |
|  | 13440 | Pipe | 1 | 450 |  |
|  | 13820 | Pipe | 1 | 450 |  |
|  | 14515 | Pipe | 1 | 450 |  |
|  | 15045 | Pipe | 1 | 600 |  |
|  | 15245 | Pipe | 1 | 600 |  |
|  | 15580 | Pipe | 1 | 450 |  |


|  | 15905 | Pipe | 1 | 450 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 16365 | RCBC | 3 | $\begin{gathered} 2400 x \\ 1200 \\ \hline \end{gathered}$ | Major Culvert |
|  | 16525 | RCBC | 1 | $1200 \times 350$ |  |
|  | 16683 | RCBC | 4 | $1200 \times 350$ |  |
|  | 16905 |  |  |  | Rosebrook Bridge |
|  | 17090 | RCBC | 4 | $1200 \times 350$ |  |
|  | 17965 |  |  |  | Floodway |
|  | 18570 | Pipe | 1 | 450 |  |
|  |  |  |  |  | Intersection Wybong Road and Kayuga Road |
| Kayuga Road | 19085 | Pipe | 1 | 450 | Pipe (only) runs parallel to pavement - gully pit system across intersection |
|  | 19085 | Pipe | 1 | 375 | Gully pit system |
|  | 19145 | Pipe | 1 | 450 | Pipe (only) runs parallel to pavement - gully pit system |
|  | 19255 | Pipe | 1 | 450 | pipe back flow valve - gully pit system |
|  | 19265 | RCBC | 8 | 300 | Major Culvert |
|  | 19545 | RCBC | 2 | 300 |  |
|  | 20790 | RCBC | 2 | 300 |  |
|  | 20995 | RCBC | 3 | $1200 \times 600$ |  |
|  | 21005 | RCBC | 1 | $1200 \times 600$ |  |
|  | 21745 | Pipe | 1 | 450 |  |
|  | 21855 | Pipe | 2 | 1200 |  |
|  | 22460 | Pipe | 1 | 450 |  |
|  | 22950 | Pipe | 1 | 450 |  |
|  | 23135 | RCBC | 2 | 600 |  |
|  | 23475 | Pipe | 1 | 450 |  |
|  | 23655 | Pipe | 1 | 450 |  |
|  | 24395 | RCBC | 2 | 300 |  |
|  | 24710 | RCBC | 7 | 2400 | Major Culvert |
|  | 25210 | Pipe | 1 | 450 |  |
|  | 25445 | Pipe | 1 | 450 |  |
|  |  |  |  |  | Dartbrook Mine Entrance Road |
|  | 25565 | Pipe | 1 | 450 |  |
|  | 25700 | Pipe | 1 | 450 |  |
|  | 25815 | Pipe | 4 | 1200 |  |
|  | 26230 | Pipe | 1 | 450 |  |
|  |  |  |  |  | end of shire |


| Road Name | Chainage m | Pipe Info |  | Size mm | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Pipe/ RCBC | No |  |  |
| Bengalla Road | 350 | RCBC | 5 | $2100 \times 400$ | Major Culvert |
|  | 695 | Pipe | 1 | 300 |  |
|  | 1470-1670 | Keys Bridge |  |  | Bridge |
|  | 2340 | RCBC | 1 | $3400 \times 1800$ |  |
|  | 3000 | Pipe | 1 | 400 |  |
|  | 3420 | Pipe | 1 | 400 |  |
|  | 3830 | RCBC | 5 | $3400 \times 1800$ | Major Culvert |
|  | 4260 | Rail Overpass |  |  |  |
|  | 4820 | Pipe | 1 | 900 |  |
|  | 5131 | RCBC | 1 | $800 \times 500$ |  |
|  | 5440 | RCBC | 1 | $2100 \times 500$ |  |
|  | 5830 | Pipe | 2 | $500 \times 500$ |  |
|  | 6200 | RCBC | 1 | $1200 \times 770$ |  |
|  | 6410 | Pipe | 4 | $\begin{gathered} 1650 \mathrm{x} \\ 1650 \\ \hline \end{gathered}$ | Major Culvert |
|  | 6650 | Rail Bridge |  |  | Bridge - Mt Pleasant loop |
|  | 6770 | Pipe | 1 | 670 |  |
|  | 8550 | Pipe | 1 | 600 |  |
|  | 8900 | Pipe | 1 | 600 |  |
|  | 9421 | Pipe | 1 | 300 |  |
|  |  |  |  |  | Intersection Bengalla Road and Wybong Road |
| Wybong Road East | 9910 | Pipe | 1 | 450 |  |
|  | 10140 | Pipe | 1 | 450 |  |
|  | 11145 | Pipe | 1 | 450 |  |
|  | 11375 | Pipe | 1 | 900 |  |
|  | 11869 | Pipe | 1 | 450 |  |
|  | 12035 | Pipe | 1 | 450 |  |
|  | 12315 | RCBC | 2 | 600 |  |
|  | 12955 | Pipe | 1 | 1500 |  |
|  | 13120 | Pipe | 3 | 1500 |  |
|  | 13440 | Pipe | 1 | 450 |  |
|  | 13820 | Pipe | 1 | 450 |  |
|  | 14515 | Pipe | 1 | 450 |  |
|  | 15045 | Pipe | 1 | 600 |  |
|  | 15245 | Pipe | 1 | 600 |  |
|  | 15580 | Pipe | 1 | 450 |  |
|  | 15905 | Pipe | 1 | 450 |  |


|  | 16365 | RCBC | 3 | $\begin{gathered} 2400 \mathrm{x} \\ 1200 \\ \hline \end{gathered}$ | Major Culvert |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 16525 | RCBC | 1 | $1200 \times 350$ |  |
|  | 16683 | RCBC | 4 | $1200 \times 350$ |  |
|  | 16905 |  |  |  | Rosebrook Bridge |
|  | 17090 | RCBC | 4 | $1200 \times 350$ |  |
|  | 17965 |  |  |  | Floodway |
|  | 18570 | Pipe | 1 | 450 |  |
|  |  |  |  |  | Intersection Wybong Road and Kayuga Road |
| Kayuga Road | 19085 | Pipe | 1 | 450 | Pipe (only) runs parallel to pavement - gully pit system across intersection |
|  | 19085 | Pipe | 1 | 375 | Gully pit system |
|  | 19145 | Pipe | 1 | 450 | Pipe (only) runs parallel to pavement - gully pit system |
|  | 19255 | Pipe | 1 | 450 | pipe back flow valve - gully pit system |
|  | 19265 | RCBC | 8 | 300 | Major Culvert |
|  | 19545 | RCBC | 2 | 300 |  |
|  | 20790 | RCBC | 2 | 300 |  |
|  | 20995 | RCBC | 3 | $1200 \times 600$ |  |
|  | 21005 | RCBC | 1 | $1200 \times 600$ |  |
|  | 21745 | Pipe | 1 | 450 |  |
|  | 21855 | Pipe | 2 | 1200 |  |
|  | 22460 | Pipe | 1 | 450 |  |
|  | 22950 | Pipe | 1 | 450 |  |
|  | 23135 | RCBC | 2 | 600 |  |
|  | 23475 | Pipe | 1 | 450 |  |
|  | 23655 | Pipe | 1 | 450 |  |
|  | 24395 | RCBC | 2 | 300 |  |
|  | 24710 | RCBC | 7 | 2400 | Major Culvert |
|  | 25210 | Pipe | 1 | 450 |  |
|  | 25445 | Pipe | 1 | 450 |  |
|  |  |  |  |  | Dartbrook Mine Entrance Road |
|  | 25565 | Pipe | 1 | 450 |  |
|  | 25700 | Pipe | 1 | 450 |  |
|  | 25815 | Pipe | 4 | 1200 |  |
|  | 26230 | Pipe | 1 | 450 |  |
|  |  |  |  |  | end of shire |

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APPENDIX B - Updated OSOM Route Through Muswellbrook Shire Council
Map of Updated Route Option


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Traffic By Type and Total Volume to be Transported

|  | Turbine Blades | Heavy Loads over 5.2 m in height | 2 Heavy Loads under 5.2 m in height | Standard loads up to 3.5 m wide and 5.2 m in height |
| :---: | :---: | :---: | :---: | :---: |
| Example of Equipment | - Blades (root section) <br> - Blades (tip section) | - Hubs <br> - Tower Sections <br> - Transformers <br> - Nacelles with Drivetrain in | - Nacelle with Drivetrain Out <br> - Drivetrain | - Other (2 x 40ft Shipping Container per WTG) <br> - Sub station <br> - Switching Station <br> - Overhead cabling <br> - Underground cabling <br> - Battery System <br> - Mobile concrete Batch Plant |
| Total Trips | $280(210){ }^{1}$ | 650 (580) ${ }^{2}$ | $140^{3}$ | 320 |
| Weekly Trips | 8 (6) | 18 (16) | 4 | 9 |

The final traffic volumes generated on these routes will be subject to the structural load assessment of Council Assets and further consultation with MSC on required upgrades. This will be based on the final turbine equipment and the transport logistics operators' proposed vehicles and associated weights.

The estimated worst-case traffic predictions are presented based on a range of possible scenarios including a scenario which reduces impacts to Bell St/Victoria St and Market St by splitting the volumes between routes.

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## Comparison of Traffic Generated by Routes Options

| Scenario (all blades always <br> travel on route 1) | Route 1 | Route 2 <br> (includes <br> Bell St) | Route 3 <br> (includes <br> Bell St) | Route <br> $\mathbf{4}$ | Totals |
| :--- | ---: | :--- | :--- | ---: | ---: |
| Previous EIS Scenario | 280 |  | 1110 | 0 | 1390 |
| Average Weekly | $\mathbf{8}$ | $\mathbf{0}$ | $\mathbf{3 2}$ | $\mathbf{0}$ |  |
| Option 1 - All Heavy Loads on <br> Route 1 with normal loads on <br> Route 4 | $1070^{1}$ |  |  | 320 | 1390 |
| Average Weekly | $\mathbf{3 1}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{9}$ |  |
| Option 2 - 100\% Heavy Loads <br> on Route 2 and 3 | $280^{1}$ | $650^{2}$ | $140^{3}$ | 320 | 1390 |
| Average Weekly | $\mathbf{8}^{1}$ | $\mathbf{1 9}$ | $\mathbf{4}^{\mathbf{3}}$ | $\mathbf{9}$ |  |
| Example of Option 3 - 50\% <br> Heavy between Route 1 and <br> Routes 2 and 3 | $605^{1}$ | $325^{2}$ | $140^{3}$ | 320 | 1390 |
| Average Weekly | $\mathbf{1 7}^{1}$ | $\mathbf{9}^{\mathbf{2}}$ | $\mathbf{4}^{\mathbf{3}}$ | $\mathbf{9}$ |  |

Notes:

1. Reduced numbers if blades are transported as a single unit.
2. This will be reduced if nacelles and drivetrains are transported separately as presented in the next column with both nacelle and drivetrains being under 5.2 m and able to use Route 3 .
3. This will not be required if nacelles and drivetrains are transported together

The transportation period for the turbine components has been forecast to occur over approximately a 9month period, or 35 weeks.

All route options reduce traffic proposed on the Bells St Heavy Vehicle Alternate route (Route 2 and 3) by taking advantage of the updated Route 4 option for vehicles under 3.5 m wide and 5.2 m high and options to use Route 1 for some or all of the heavy vehicles. The range in reduced volume is between 11 and 32 movements per week from the previously submitted EIS.

The Transport Planning Partnership Suite 402 Level 4, 22 Atc hison Street

St Leonards NSW 2065
P.O. Box 237

St Leonards NSW 1590

0284377800
info@ttpp.net.au
www.ttpp.net.au

## APPENDIX H. 2 LETTERS OF OFFER

Gina Vereker<br>Tamworth Regional Council<br>Ray Walsh House, 437 Peel Street<br>Tamworth NSW 2340<br>Via email

14 July 2021

Dear Gina

## Revised Offer - Voluntary Contributions from Hills of Gold Wind Farm Pty Ltd for Annual Community Enhancement Funds

Thank you to you and your colleagues for your time on 30 June 2021 to discuss our letter dated 19 May 2021 regarding a voluntary contribution to a proposed community enhancement fund in respect of the Hills of Gold Wind Farm (the "Project"), which is the subject of Development Application Number SSD-9679 (the "Development Application").

Further to our discussions, we confirm that the Project proponent, Hills of Gold Wind Farm Pty Ltd (ACN 145173 324) ("HOGWFPL"), is willing to accept the suggested amendments to the community enhancement fund and to make the following revised offer to Tamworth Regional Council in respect of the Project (subject only to the execution of a voluntary planning agreement or similar agreement acceptable to the parties to formalise these matters, on terms acceptable to each party, and to the approval of the Development Application):

## 1. Community Enhancement Fund:

(a) HOGWFPL will establish a dedicated community enhancement fund to be administered by the Tamworth Regional Council for the benefit of members of the community who may be impacted by the Project ("Community Enhancement Fund").
(b) HOGWFPL will maintain its previous offer to increase the amount of funds per turbine to be provided to the Community Enhancement Fund administered by, and shared on a merit basis to applicants within, the Tamworth Regional Council by contributing AUD\$3,000 per turbine, per annum, in respect of those Project turbines within the Tamworth Regional Council Local Government Area, with such amounts to be payable to the Community Enhancement Fund on an annual basis on and from the date on which
the first wind turbine commissioned on the Project site becomes commercially operational and continue each year thereafter for the life of the Project.

For indicative purposes only, the current list of proposed turbines is set forth in Annexure A and includes the coordinates and the LGA in respect of the location of each proposed turbine.
(c) Following consultation with the Tamworth Regional Council, the funds to be contributed to the Community Enhancement Fund by HOGWFPL will be administered in accordance with the following principles:
(i) Tamworth Regional Council will nominate a respected local person with neutral views on the Project to act as the independent chairperson of the Community Enhancement Fund for the first 5 years of the administration of the Community Enhancement Fund;
(ii) a suitable governance framework will be primarily adapted from existing Section 355 Community Committee guidelines and the operating manual (where relevant), or other appropriate guidelines as agreed between the parties. The framework will otherwise be consistent with the Tamworth Regional Council's Community Committee Operating Manual 2020 and will utilise its existing administrative and finance templates already in use in respect of other community committees;
(iii) HOGWFPL will provide all reasonable assistance to the Tamworth Regional Council in respect of the establishment and early operation of the Community Enhancement Fund to ensure committee roles and responsibilities, committee establishment and voting rules are customised to ensure the simple and effective operation of the Community Enhancement Fund;
(iv) a Community Enhancement Fund Committee will be established prior to the first wind turbine commissioned on the Project site becoming commercially operational to ensure a committee consisting of Tamworth Regional Council, HOGWFPL and volunteer community representatives can be formed that meets the Tamworth Regional Council's requirements for transparency, accountability and probity in respect of the use and dissemination of the funds;
(v) the community representatives of the Community Enhancement Fund will be elected volunteers from the community;
(vi) HOGWFPL will provide an additional, fixed contribution of (i) \$10,000 for the first year upon establishing the Community Enhancement Fund, and thereafter (ii) $\$ 5,000$ per annum, to cover the costs incurred in respect of the appointment of an independent chairperson, annual auditing and administration of the Community Engagement Fund (the "Administrative Funds"), with such Administrative Funds to be payable at the same time as the other HOGWFPL contributions to the Community Engagement Fund; and
(vii) the Community Enhancement Fund Committee will determine the finer details of project eligibility, community representation and other mechanics following the approval of the Development

Application, however, it will be acknowledged that consideration must be given to both the cost of any long-term obligations on Tamworth Regional Council and the opportunity to fund long-term strategic initiatives brought forward by the community.
(d) The amount of the contributions by HOGWFPL to the Community Enhancement Fund and the additional Administrative Funds will be adjusted on an annual basis to reflect any change in the Consumer Price Index from the Consumer Price Index in effect as at the date of approval of the Development Application.
2. Construction Community Funding: HOGWFPL commits to establishing a one-off fund of $\$ 150,000$ upon the commencement of construction of the Project to provide funds to communities who may be impacted by the construction activities of the Project (including the Upper Hunter Shire Council and Tamworth Regional Council communities) to put towards HOGWFPL-initiated community projects, including support for sports and academic scholarships to local schools to support interstate trips and competitions and community engagement days associated with Project construction milestones (for example, upon delivery of the first turbine blade), with the application of such funds to be applied by HOGWFPL in its direction during the construction phase of the Project.
3. External Legal Fees: HOGWFPL will cover the cost of external legal fees that are incurred by Tamworth Regional Council in negotiating the voluntary planning or similar agreement (as contemplated by this letter of offer), up to a maximum of $\$ 10,000$ (excluding GST).

We look forward to hearing from you and would welcome any further discussion in respect of any remaining queries.

Yours sincerely
-DocuSigned by:
Herlers

General Manager - Asset Development

## ACCEPTANCE BY TAMWORTH REGIONAL COUNCIL:

Subject only to the execution of a voluntary planning agreement or similar agreement by the parties to formalise these matters and to the approval of the Development Application, Tamworth Regional Council hereby confirms its acceptance of the terms contained in this letter.

## eNGie

Signed for and on behalf of Tamworth Regional Council by:

Signature

Name (please print)

Position (please print)

1 July 2021

Engie
Level 33, Rialto South Tower
525 Collins Street
MELBOURNE VIC 3000
Attention: Andrew Kerley

Dear Andrew,
Hills of Gold Wind Farm - Offer to enter into Voluntary Planning Agreement
We refer to your letter dated 19 May 2021 regarding your revised offer to enter into a Voluntary Planning Agreement (VPA) with Upper Hunter Shire Council.

Council, at its meeting held on 28 June 2021, considered your revised offer and resolved the following:

That Council accept the offer from Hills of Gold Wind Farm Pty Ltd to enter into a Voluntary Planning Agreement (VPA) based on an annual contribution of \$3,000 per turbine (indexed to CPI) towards a Community Enhancement Fund and a fixed contribution of $\$ 5,000$ per annum (indexed to CPI) to cover administrative costs.

Please find attached, the signed acceptance of your offer.
Should you have any questions, or wish to discuss this matter further, please contact Council's Director Environmental \& Community Services, Mathew Pringle, on

Yours faithfully


Mathew Pringle
DIRECTOR ENVIRONMENTAL \& COMMUNITY SERVICES

# muswellbrook shire council 

Enquiries Direct<br>Our reference<br>Your reference

Please ask for Peter Chambers

29 August 2021

Alex Henderson<br>Team Leader Energy Assessments Hills of Gold<br>Dear Mr Henderson,

## Hills of Gold Windfarm Project - Muswellbrook Shire Council Route requirements

Further to our recent discussions I confirm that the preferred route for all proposed OSOM loads is via Thomas Mitchell Drive, Bengalla Link Road, Wybong Road East and Kayuga Road.

Given Wybong Road East and Kayuga Road were not constructed to contemplate these types of loads and vehicles Council will require the applicant for the Hills of Gold wind farm to complete the following:

## 1. Route Assessment

A portion of the requested proposed route along Wybong Road East is currently load limited to 12 tonnes and is not currently part of the Shire's Mine Affected Road Network. A Detailed Route Analysis considering road furniture, geometry, load limits, safe sight distance, private property and Council road impacts, turning circles by a suitably experienced and practicing consultant is to be provided to Council, including:

- Written consent of the private property owners along the route in the case where their land will be impacted, including any written correspondence between parties and contact information;
- A joint dilapidation survey with Council is to be conducted in accordance with the requirements detailed on Annexure A (below) and submitted for Council's acceptance, for the route including inspection of all drainage structures and road surfaces; and
- Structural assessment of all drainage structures along the proposed route that has not had a recent condition assessment with proposed design loads exceeding existing load compliant traffic along the proposed road route.


## 2. Transport Management Plan

In order to assess the proposal, Council requires further details relating to the timing, frequency and proposed size and loading of vehicles, and the overall time frame for completion of movements. Council also requires the proposed starting date for transport movements through the Shire.

A Transport Management Plan is to be submitted to Council for the route by a suitably experienced and practicing consultant showing:
i. Distribution and number of loads, including frequency per week, expected time of travel, standard axle design loads, total vehicle widths and lengths, proposed route;
ii. Traffic Management Plan for the route, including use of wide swept paths across private property, movement and replacement of identified road
furniture to prevent short-cuts by the community, pull-over bays for road furniture interchanging;
iii. Proposals for any details of any intersection upgrades through private property;
iv. Consider and determine any impacts to existing school bus routes;
v. The current plans for replacement of Rosebrook Bridge and how timing of this re-construction may coincide with the wind farm, and the ability of OSOM vehicles to utilize the intended side-track that will be in place during construction;
vi. Vertical geometry for clearances of long loads to be considered, including any side-track;
vii. Details of the pilots to be provided as part of the S138 permit stage; and
viii. Applicant to fund the cost of hiring a Council Traffic Observer for the duration of the project to follow OSOM transport through Council's municipality during operations.

## 3. Road Improvements

Wybong Road East from the intersection of Overton Rd to the intersection with Kayuga Rd is currently unsuitable for OSOM loads and requires upgrades to the road and structures along the route to support the proposed movements. This portion of road is to be upgraded to the below standard:
i. Road widths - RS2M Standard requirement, which means $2 \times 3.5 \mathrm{~m}$ lanes, $2 \times 1.0 \mathrm{~m}$ sealed shoulder and $2 \times 2.0 \mathrm{~m}$ unsealed shoulder ( 3.12 km length), pavement design to be provided and accepted to Council's satisfaction.
ii. Under the S138, road pavement design to be provided based on 22.32 x $10^{\wedge} 6$ axle, CBR $\min 4 \%$

Any works or maintenance on Council Public Roads is subject to application for an S138 of the Roads Act permit and will be required to be prepared and delivered in accordance with the conditions of the S138 permit.

Any works or maintenance on State or Federal Public Roads to be prepared and delivered in accordance with an ROL permit with TfNSW.

## 4. Road Maintenance

The applicant will need to enter a formal maintenance management plan as part of the S138 permit for Council roads along the route for the entire duration of the project, to Council's written satisfaction including:

1. The maintenance management plan will be based on TfNSW M3 Maintenance Plan (see proforma example attached);
2. Maintenance work will be coordinated to Council's satisfaction including timing and day/night work;
3. Dilapidation survey of the route to be undertaken every twelve weeks of the project and provided to Council;
4. A Bank Guarantee will be required for the period of the project plus six months to cover any damage determined by Council's reasonable opinion, and dilapidation surveys, to have occurred as a result of the OSOM transported loads for the project; and
5. An Indemnity Deed Poll to be provided for emergency works to any assets that may suffer damage during the project.

## 5. Communication

The applicant will need to enter a formal community consultation management plan for the entire duration of the project, to Council's written satisfaction including:

The community consultation management plan is to be developed in consultation with Council including but not limited to:
i. Monthly meetings with Council staff to discuss progress, issues and community feedback;
ii. Complaints and incident handling procedure including contact details of the applicant;
Identifying residents, businesses, emergency services, school bus and mines (shift change times) and key contacts in these operations and necessary liaising with these road users;
iii. Details of the Transport Management Plan and progress to be included and updated on both the applicant's website as well as Council's website;
iv. Applicant to provide updates to Council with regards to any planned maintenance works and/or upgrades and replacements.

Council staff would be pleased to provide additional information if requested.
I also advise that staff have recently held a meeting with another wind farm proponent who wishes to use the same route for their OSOM vehicles, and that there be further projects in the period up to the opening of the Muswellbrook Bypass. Council staff consider that there would be benefits in a more strategic approach to managing this construction traffic. You may be contacted by another wind farm proponent soon to compile information that Council would put before a number of State Government agencies to initiate discussion this strategic approach.

Yours faithfully


Sharon Pope
Executive Manager Environment and Planning.

## Annexure A

Road Dilapidation Survey Requirements
Liaison is to occur with MSC Staff as to what is to be included in the dilapidation survey. This will require a s. 138 Roads Act 1993 approval through MSC. The following matters (at a minimum) need to be addressed in the pre dilapidation survey:
Minimum requirement

1. Visual Condition Assessment (Automated Road Analyser - ARAN) - The visual pavement assessment is to be undertaken by an experienced pavement engineer who will:
a) Record video of the relevant road section using a GPS camera to document the condition of the existing pavement;
b) Use the footage to record the location, type and extent of pavement defects and other environmental factors (e.g. drainage) that may be impacting the existing pavement.

The results of the visual assessment will be provided in a section of the pavement assessment report and summarised in table format and to include the following factors:

- Roughness
- Rutting
- Structural Cracking
- Environmental Cracking
- Pot holes
- Pot Patch
- Heavy Patching
- Ravelling
- California Bearing Ratio (CBR)
- Deflection
- Curvature
- AC overlay (mm)
- Granular Overlay (mm)
- Structural Deficiency (mm)
- Pavement Condition Index (PCI)
- Surface Curvature Index (SCI)

The assessment of the existing pavement is to be conducted in accordance with the following design standards and guidelines:

- Austroad Guide to Pavement Technology (AGPT)- Part 2: Pavement Structural Design (2017)
- Austroad Guide to Pavement Technology (AGPT) -Part 5 Pavement Evaluation and Treatment Design (2011)
- Applicable AUSPEC and TfNSW specifications
- Other applicable design standards.

2. Falling Weight Deflectometer (FWD) - Specifically loading 40 kN and 70 kN need to be applied to the existing pavement at 20 m intervals in alternating wheel paths. Subsurface investigations_sufficient number of 300 mm (at a minimum) diameter pavement holes would be required to sufficiently assess the pavement and underlying subgrade. Dynamic cone penetrometer (DCP) testing to be performed at each test pit location to assess in-situ density or consistency of subsurface material. The test locations are to be recorded by a GPS unit with typical accuracy
of $+/-10 \mathrm{~m})$ in MGA format, together with description of locations relative to the pavement.

Samples of pavement and subgrade are to be tested at a NATA registered laboratory for the following geotechnical testing:

- Subgrade
i) 3 No. Standard compaction and CBR
- 3 No. moisture content pavement
i) 6 No. Modified compaction and CBR
ii) 6 No. PSD
iii) 6 No. moisture content
iv) 6 No. Atterberg Limits

The above 2 methods are standard investigations to determine the current surface and pavement condition prior to use of the road by construction traffic.

Fiona Plesman
General Manager
Muswellbrook Shire Council
Via email

2 June 2021

Dear Fiona,

## Voluntary Contribution from Hills of Gold Wind Farm Pty Ltd

Thank you for your and your team's time on 31 March 2021 to discuss Muswellbrook Shire Council's (MSC) concerns regarding the proposed use of council roads and assets by traffic associated with the Hills of Gold Wind Farm (the "Project") which is the subject of Development Application Number SSD-9679 (the "Development Application").

We appreciated the constructive suggestion of your team to progress an agreement with MSC to address those concerns, specifically those in respect of the proposed use of those council roads and council-owned assets set out in the subsequently provided list in Annexure A (Council Assets).

We confirm we have undertaken further assessment on the alternate route options available based on feedback from MSC. The Project, via its Response to Submission Report, will propose new route options for heavy, oversize / overmass (OSOM) vehicles which will reduce impacts on existing traffic volumes as compared to the initial route proposed. To provide some further detail in this respect, Annexure B provides a summary of estimated OSOM traffic type and volumes by route, as well as a map showing the additional route options. We will continue to engage with MSC as we progress final turbine selection, selection of a logistics contractor and assess the Council Assets to determine the most suitable route option(s).

In the meantime and further to our recent discussions, we confirm that the Project proponent, Hills of Gold Wind Farm Pty Ltd (ACN 145173 324) ("HOGWFPL"), is also willing to make the following offer to MSC in respect of the proposed use of any Council Assets as part of the final route selection (subject only to the execution of a voluntary planning agreement or similar agreement by the parties to formalise these matters on terms acceptable to each party and to the approval of the Development Application):

## eNGie

## 1. Route Assessment and Upgrade Works:

(a) HOGWFPL will consult with MSC to determine those Council Assets which require a detailed structural assessment to be undertaken to assess their structural suitability for use by Project OSOM traffic and will engage a suitably qualified, independent expert acceptable to MSC to undertake that structural assessment. Such engagement would be at HOGWFPL's cost, however, we may require reasonable assistance from MSC to facilitate the assessment, in particular, the provision of any existing data on, or previously completed assessment of, those Council Assets.
(b) If any Council Asset is found by the independent expert to be structurally inadequate for the transport of the expected equipment loads for the Project and that Council Asset is proposed to be used as part of the final transport route for the Project, HOGWFPL will, at its cost (1) upgrade each such Council Asset to the extent reasonably required to ensure it is structurally adequate and suitable for the expected Project loads and consult with MSC to incorporate any reasonable requirements of MSC in respect of such upgrade, and (2) provide, or have its contractor provide, a performance bond in favour of MSC in the form of a letter of credit or bank guarantee to secure its performance of such upgrade works, with such bond to be for a reasonable amount having regard to the cost of the upgrade works and to be provided prior to the commencement of the upgrade works. Any such performance bond would be released upon completion of the upgrade works.
2. Road Usage Fee: In addition, HOGWFPL will pay a one-off, road usage fee of $\$ 70,000$ to MSC upon the commencement of construction of the Project to compensate MSC for any dilapidation which may be caused by the general use of roads within the MSC by traffic associated with the Project. Due to the volume of traffic which already uses roads within the MSC, it will likely be impractical to commission a dilapidation survey which can identify only that dilapidation attributable to Project traffic. Accordingly, the one-off, road usage fee is proposed as an alternative to a dilapidation survey to provide greater certainty to MSC.

If the above offer is acceptable to MSC, please sign where indicated below to confirm such acceptance. Once signed, a copy will be provided to the Department of Planning for inclusion of the relevant commitments by HOGWFPL in the Project's Statement of Commitments.

We look forward to hearing from you and would welcome any further discussion in respect of any remaining queries.

Yours sincerely,
DocuSigned by:
Herlul

General Manager - Asset Development

## ACCEPTANCE BY MUSWELLBROOK SHIRE COUNCIL:

Subject only to the execution of a voluntary planning agreement or similar agreement by the parties to formalise these matters (and to the approval of the Development Application), Muswellbrook Shire Council hereby confirms its acceptance of the terms contained in this letter.

Signed for and on behalf of Muswellbrook Shire Council by:

## Signature

Name (please print)

Position (please print)

## ENGIE

## APPENDIX A - List of Council Assets

| Road | Chainage m | Pipe Info |  | Size mm | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Pipe/ RCBC | No |  |  |
| Bengalla Road | 350 | RCBC | 5 | $2100 \times 400$ | Major Culvert |
|  | 695 | Pipe | 1 | 300 |  |
|  | 1470-1670 | Keys Bridge |  |  | Bridge |
|  | 2340 | RCBC | 1 | $3400 \times 1800$ |  |
|  | 3000 | Pipe | 1 | 400 |  |
|  | 3420 | Pipe | 1 | 400 |  |
|  | 3830 | RCBC | 5 | $3400 \times 1800$ | Major Culvert |
|  | 4260 | Rail Overpass |  |  |  |
|  | 4820 | Pipe | 1 | 900 |  |
|  | 5131 | RCBC | 1 | $800 \times 500$ |  |
|  | 5440 | RCBC | 1 | $2100 \times 500$ |  |
|  | 5830 | Pipe | 2 | $500 \times 500$ |  |
|  | 6200 | RCBC | 1 | $1200 \times 770$ |  |
|  | 6410 | Pipe | 4 | $\begin{gathered} 1650 x \\ 1650 \\ \hline \end{gathered}$ | Major Culvert |
|  | 6650 | Rail Bridge |  |  | Bridge - Mt Pleasant loop |
|  | 6770 | Pipe | 1 | 670 |  |
|  | 8550 | Pipe | 1 | 600 |  |
|  | 8900 | Pipe | 1 | 600 |  |
|  | 9421 | Pipe | 1 | 300 |  |
|  |  |  |  |  | Intersection Bengalla Road and Wybong Road |
| Wybong Road East | 9910 | Pipe | 1 | 450 |  |
|  | 10140 | Pipe | 1 | 450 |  |
|  | 11145 | Pipe | 1 | 450 |  |
|  | 11375 | Pipe | 1 | 900 |  |
|  | 11869 | Pipe | 1 | 450 |  |
|  | 12035 | Pipe | 1 | 450 |  |
|  | 12315 | RCBC | 2 | 600 |  |
|  | 12955 | Pipe | 1 | 1500 |  |
|  | 13120 | Pipe | 3 | 1500 |  |
|  | 13440 | Pipe | 1 | 450 |  |
|  | 13820 | Pipe | 1 | 450 |  |
|  | 14515 | Pipe | 1 | 450 |  |
|  | 15045 | Pipe | 1 | 600 |  |
|  | 15245 | Pipe | 1 | 600 |  |
|  | 15580 | Pipe | 1 | 450 |  |


|  | 15905 | Pipe | 1 | 450 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 16365 | RCBC | 3 | $\begin{gathered} 2400 x \\ 1200 \\ \hline \end{gathered}$ | Major Culvert |
|  | 16525 | RCBC | 1 | $1200 \times 350$ |  |
|  | 16683 | RCBC | 4 | $1200 \times 350$ |  |
|  | 16905 |  |  |  | Rosebrook Bridge |
|  | 17090 | RCBC | 4 | $1200 \times 350$ |  |
|  | 17965 |  |  |  | Floodway |
|  | 18570 | Pipe | 1 | 450 |  |
|  |  |  |  |  | Intersection Wybong Road and Kayuga Road |
| Kayuga Road | 19085 | Pipe | 1 | 450 | Pipe (only) runs parallel to pavement - gully pit system across intersection |
|  | 19085 | Pipe | 1 | 375 | Gully pit system |
|  | 19145 | Pipe | 1 | 450 | Pipe (only) runs parallel to pavement - gully pit system |
|  | 19255 | Pipe | 1 | 450 | pipe back flow valve - gully pit system |
|  | 19265 | RCBC | 8 | 300 | Major Culvert |
|  | 19545 | RCBC | 2 | 300 |  |
|  | 20790 | RCBC | 2 | 300 |  |
|  | 20995 | RCBC | 3 | $1200 \times 600$ |  |
|  | 21005 | RCBC | 1 | $1200 \times 600$ |  |
|  | 21745 | Pipe | 1 | 450 |  |
|  | 21855 | Pipe | 2 | 1200 |  |
|  | 22460 | Pipe | 1 | 450 |  |
|  | 22950 | Pipe | 1 | 450 |  |
|  | 23135 | RCBC | 2 | 600 |  |
|  | 23475 | Pipe | 1 | 450 |  |
|  | 23655 | Pipe | 1 | 450 |  |
|  | 24395 | RCBC | 2 | 300 |  |
|  | 24710 | RCBC | 7 | 2400 | Major Culvert |
|  | 25210 | Pipe | 1 | 450 |  |
|  | 25445 | Pipe | 1 | 450 |  |
|  |  |  |  |  | Dartbrook Mine Entrance Road |
|  | 25565 | Pipe | 1 | 450 |  |
|  | 25700 | Pipe | 1 | 450 |  |
|  | 25815 | Pipe | 4 | 1200 |  |
|  | 26230 | Pipe | 1 | 450 |  |
|  |  |  |  |  | end of shire |


| Road Name | Chainage m | Pipe Info |  | Size mm | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Pipe/ RCBC | No |  |  |
| Bengalla Road | 350 | RCBC | 5 | $2100 \times 400$ | Major Culvert |
|  | 695 | Pipe | 1 | 300 |  |
|  | 1470-1670 | Keys Bridge |  |  | Bridge |
|  | 2340 | RCBC | 1 | $3400 \times 1800$ |  |
|  | 3000 | Pipe | 1 | 400 |  |
|  | 3420 | Pipe | 1 | 400 |  |
|  | 3830 | RCBC | 5 | $3400 \times 1800$ | Major Culvert |
|  | 4260 | Rail Overpass |  |  |  |
|  | 4820 | Pipe | 1 | 900 |  |
|  | 5131 | RCBC | 1 | $800 \times 500$ |  |
|  | 5440 | RCBC | 1 | $2100 \times 500$ |  |
|  | 5830 | Pipe | 2 | $500 \times 500$ |  |
|  | 6200 | RCBC | 1 | $1200 \times 770$ |  |
|  | 6410 | Pipe | 4 | $\begin{gathered} 1650 x \\ 1650 \\ \hline \end{gathered}$ | Major Culvert |
|  | 6650 | Rail Bridge |  |  | Bridge - Mt Pleasant loop |
|  | 6770 | Pipe | 1 | 670 |  |
|  | 8550 | Pipe | 1 | 600 |  |
|  | 8900 | Pipe | 1 | 600 |  |
|  | 9421 | Pipe | 1 | 300 |  |
|  |  |  |  |  | Intersection Bengalla Road and Wybong Road |
| Wybong Road East | 9910 | Pipe | 1 | 450 |  |
|  | 10140 | Pipe | 1 | 450 |  |
|  | 11145 | Pipe | 1 | 450 |  |
|  | 11375 | Pipe | 1 | 900 |  |
|  | 11869 | Pipe | 1 | 450 |  |
|  | 12035 | Pipe | 1 | 450 |  |
|  | 12315 | RCBC | 2 | 600 |  |
|  | 12955 | Pipe | 1 | 1500 |  |
|  | 13120 | Pipe | 3 | 1500 |  |
|  | 13440 | Pipe | 1 | 450 |  |
|  | 13820 | Pipe | 1 | 450 |  |
|  | 14515 | Pipe | 1 | 450 |  |
|  | 15045 | Pipe | 1 | 600 |  |
|  | 15245 | Pipe | 1 | 600 |  |
|  | 15580 | Pipe | 1 | 450 |  |
|  | 15905 | Pipe | 1 | 450 |  |


|  | 16365 | RCBC | 3 | $\begin{gathered} 2400 \mathrm{x} \\ 1200 \\ \hline \end{gathered}$ | Major Culvert |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 16525 | RCBC | 1 | $1200 \times 350$ |  |
|  | 16683 | RCBC | 4 | $1200 \times 350$ |  |
|  | 16905 |  |  |  | Rosebrook Bridge |
|  | 17090 | RCBC | 4 | $1200 \times 350$ |  |
|  | 17965 |  |  |  | Floodway |
|  | 18570 | Pipe | 1 | 450 |  |
|  |  |  |  |  | Intersection Wybong Road and Kayuga Road |
| Kayuga Road | 19085 | Pipe | 1 | 450 | Pipe (only) runs parallel to pavement - gully pit system across intersection |
|  | 19085 | Pipe | 1 | 375 | Gully pit system |
|  | 19145 | Pipe | 1 | 450 | Pipe (only) runs parallel to pavement - gully pit system |
|  | 19255 | Pipe | 1 | 450 | pipe back flow valve - gully pit system |
|  | 19265 | RCBC | 8 | 300 | Major Culvert |
|  | 19545 | RCBC | 2 | 300 |  |
|  | 20790 | RCBC | 2 | 300 |  |
|  | 20995 | RCBC | 3 | $1200 \times 600$ |  |
|  | 21005 | RCBC | 1 | $1200 \times 600$ |  |
|  | 21745 | Pipe | 1 | 450 |  |
|  | 21855 | Pipe | 2 | 1200 |  |
|  | 22460 | Pipe | 1 | 450 |  |
|  | 22950 | Pipe | 1 | 450 |  |
|  | 23135 | RCBC | 2 | 600 |  |
|  | 23475 | Pipe | 1 | 450 |  |
|  | 23655 | Pipe | 1 | 450 |  |
|  | 24395 | RCBC | 2 | 300 |  |
|  | 24710 | RCBC | 7 | 2400 | Major Culvert |
|  | 25210 | Pipe | 1 | 450 |  |
|  | 25445 | Pipe | 1 | 450 |  |
|  |  |  |  |  | Dartbrook Mine Entrance Road |
|  | 25565 | Pipe | 1 | 450 |  |
|  | 25700 | Pipe | 1 | 450 |  |
|  | 25815 | Pipe | 4 | 1200 |  |
|  | 26230 | Pipe | 1 | 450 |  |
|  |  |  |  |  | end of shire |

## eNGie

APPENDIX B - Updated OSOM Route Through Muswellbrook Shire Council
Map of Updated Route Option


## ENGIE

Traffic By Type and Total Volume to be Transported

|  | Turbine Blades | Heavy Loads over 5.2 m in height | 2 Heavy Loads under 5.2 m in height | Standard loads up to 3.5 m wide and 5.2 m in height |
| :---: | :---: | :---: | :---: | :---: |
| Example of Equipment | - Blades (root section) <br> - Blades (tip section) | - Hubs <br> - Tower Sections <br> - Transformers <br> - Nacelles with Drivetrain in | - Nacelle with Drivetrain Out <br> - Drivetrain | - Other (2 x 40ft Shipping Container per WTG) <br> - Sub station <br> - Switching Station <br> - Overhead cabling <br> - Underground cabling <br> - Battery System <br> - Mobile concrete Batch Plant |
| Total Trips | $280(210){ }^{1}$ | $650(580){ }^{2}$ | $140^{3}$ | 320 |
| Weekly Trips | 8 (6) | 18 (16) | 4 | 9 |

The final traffic volumes generated on these routes will be subject to the structural load assessment of Council Assets and further consultation with MSC on required upgrades. This will be based on the final turbine equipment and the transport logistics operators' proposed vehicles and associated weights.

The estimated worst-case traffic predictions are presented based on a range of possible scenarios including a scenario which reduces impacts to Bell St/Victoria St and Market St by splitting the volumes between routes.

## ENGIE

## Comparison of Traffic Generated by Routes Options

| Scenario (all blades always <br> travel on route 1) | Route 1 | Route 2 <br> (includes <br> Bell St) | Route 3 <br> (includes <br> Bell St) | Route <br> $\mathbf{4}$ | Totals |
| :--- | ---: | :--- | :--- | ---: | ---: |
| Previous EIS Scenario | 280 |  | 1110 | 0 | 1390 |
| Average Weekly | $\mathbf{8}$ | $\mathbf{0}$ | $\mathbf{3 2}$ | $\mathbf{0}$ |  |
| Option 1 - All Heavy Loads on <br> Route 1 with normal loads on <br> Route 4 | $1070^{1}$ |  |  | 320 | 1390 |
| Average Weekly | $\mathbf{3 1}$ | $\mathbf{0}$ | $\mathbf{0}$ | $\mathbf{9}$ |  |
| Option 2 - 100\% Heavy Loads <br> on Route 2 and 3 | $280^{1}$ | $650^{2}$ | $140^{3}$ | 320 | 1390 |
| Average Weekly | $\mathbf{8}^{1}$ | $\mathbf{1 9}$ | $\mathbf{4}^{\mathbf{3}}$ | $\mathbf{9}$ |  |
| Example of Option 3 - 50\% <br> Heavy between Route 1 and <br> Routes 2 and 3 | $605^{1}$ | $325^{2}$ | $140^{3}$ | 320 | 1390 |
| Average Weekly | $\mathbf{1 7}^{1}$ | $\mathbf{9}^{\mathbf{2}}$ | $\mathbf{4}^{\mathbf{3}}$ | $\mathbf{9}$ |  |

Notes:

1. Reduced numbers if blades are transported as a single unit.
2. This will be reduced if nacelles and drivetrains are transported separately as presented in the next column with both nacelle and drivetrains being under 5.2 m and able to use Route 3 .
3. This will not be required if nacelles and drivetrains are transported together

The transportation period for the turbine components has been forecast to occur over approximately a 9month period, or 35 weeks.

All route options reduce traffic proposed on the Bells St Heavy Vehicle Alternate route (Route 2 and 3) by taking advantage of the updated Route 4 option for vehicles under 3.5 m wide and 5.2 m high and options to use Route 1 for some or all of the heavy vehicles. The range in reduced volume is between 11 and 32 movements per week from the previously submitted EIS.

Sharon Pope
Executive Manager Environment and Planning
Muswellbrook Shire Council
Via email

18 October 2021

Dear Sharon,

## Hills of Gold Wind Farm Project - Revised Letter of Offer to Muswellbrook Shire Council

Thank you for your time in the meeting on 16 July 2021 to further discuss the Hills of Gold Wind Farm (the "Project"), and your subsequent letter of 29 August 2021 detailing the Council's route requirements. We appreciate the time taken by your team and the constructive discussions regarding the use of Council roads and assets for the Project.

We acknowledge the need to preserve the condition of Council's roads and assets through transport of turbine components to the Project site, and believe this can be achieved through a combination of best practise industry mechanisms outlined in this letter. On this basis the Project proponent, Hills of Gold Wind Farm Pty Ltd (ACN 145 173 324) ("HOGWFPL"), makes the following revised counteroffer to Muswellbrook Shire Council (MSC) in respect of the use of proposed Council managed roads (subject only to the execution of a voluntary planning agreement or similar agreement by the parties to formalise these matters on terms acceptable to each party and to the approval of the Development Application SSD 9679).

This offer supersedes the previous offer to Council set out in the Letter of Offer dated 2 June 2021.

| Council's letter 29 August 2021 | Proponent response and revised offer |
| :--- | :--- |
| General Comment | We note that this is Council's preferred route option for <br> OSOM project traffic. HOGWFPL would like to retain |
| Further to our recent discussions I confirm that the preferred |  |
| route for all proposed OSOM loads is via Thomas Mitchell | flexibility in the proposed OSOM routes through <br> Muswellbrook Shire, detailed in Annexure B of our 2 June <br> Drive, Bengalla Link Road, Wybong Road East and <br> Kayuga Road. |
| 2021 letter, in order to select the most suitable route option <br> for each load type subject to final turbine selection, |  |


|  | engagement of final logistics contractor, and structural assessment of Council assets. HOGWFPL will continue to engage with MSC throughout this process and in preparation of the Project's traffic management plan. |
| :---: | :---: |
| 1. Route Assessment <br> Detailed Route Analysis considering road furniture, geometry, load limits, safe sight distance, private property and Council road impacts, turning circles by a suitably experienced and practicing consultant is to be provided to Council, including: <br> - Written consent of the private property owners along the route in the case where their land will be impacted, including any written correspondence between parties and contact information; <br> - A joint dilapidation survey with Council is to be conducted in accordance with the requirements detailed on Annexure A (below) and submitted for Council's acceptance, for the route including inspection of all drainage structures and road surfaces; and <br> - Structural assessment of all drainage structures along the proposed route that has not had a recent condition assessment with proposed design loads exceeding existing load compliant traffic along the proposed road route. | A Route Survey has been completed by Rex Andrews for the Project and can be found in Annexure C. A Traffic and Transport Addendum has been prepared for the Project is available in Annexure D. Further route analysis will be completed for the final transport routes and be detailed in the Project's Traffic Management Plan, in consultation with MSC. <br> Written consent will be provided from all private property owners along the Project transport routes whose private land requires modifications for the Project transport. This has been achieved with all landowners on the transport route in MSC LGA with the exception of Mach Energy. <br> As discussed further below, a Road Usage Fee has been offered to MSC as an alternative to road dilapidation surveys and remains HOGWFPL's strong preference to provide both parties with greater certainty. However, should road dilapidation surveys ultimately be conditioned for the Project, an independent dilapidation survey will be undertaken in consultation with MSC to assess the existing condition of road pavement and drainage structures along the final transport routes within Muswellbrook Shire. Note the dilapidation survey would not include item 2 of Annexure A in Council's letter, Falling Weight Deflectometer. Suitable QA testing will be agreed in consultation with Council for any pavement modifications required on the transport route. <br> We request that Council provide all recent condition assessments for drainage structures undertaken along the proposed Project transport routes. Following this, HOGWFPL will consult with MSC to determine those Council Assets (listed in Annexure A of our 2 June 2021 letter) which require a detailed structural assessment to be undertaken to assess their structural suitability for use by Project OSOM traffic. HOGWFPL will then engage a suitably qualified, independent expert acceptable to MSC to undertake that structural assessment. <br> If any Council Asset is found by the independent expert to be structurally inadequate for the transport of the expected equipment loads for the Project and that Council Asset is |

$\left.\begin{array}{|c|l|}\hline & \begin{array}{l}\text { proposed to be used as part of the final transport route for } \\ \text { the Project, HOGWFPL will, at its cost, upgrade each } \\ \text { Council Asset to the extent reasonably required to ensure it } \\ \text { is structurally adequate and suitable for the expected Project } \\ \text { loads and consult with MSC to incorporate any reasonable } \\ \text { requirements of MSC in respect of such upgrade. }\end{array} \\ \hline \text { 2. Transport Management Plan } & \begin{array}{l}\text { A number of these items have been assessed in the Traffic } \\ \text { and Transport Addendum or Route Survey. HOGWFPL will } \\ \text { prepare a Traffic Management Plan post approval in } \\ \text { consultation with MSC which will assess the requirements } \\ \text { set out in Council's letter. }\end{array} \\ \text { All OSOM traffic will be transported in accordance with } \\ \text { Heavy Vehicle National Law and Regulations, and will be } \\ \text { permitted in consultation with local road authorities. These } \\ \text { permits will include details for requirements of OSOM } \\ \text { escort/pilot vehicles (including Police escorts) as applicable } \\ \text { to each load to ensure safe transport. This approach is } \\ \text { common for all wind farms of this scale in NSW. For this } \\ \text { reason, HOGWFPL does not agree to funding the cost of } \\ \text { hiring a Council Traffic Observer for the duration of the }\end{array}\right\}$

Any works or maintenance on Council Public Roads is subject to application for an S138 of the Roads Act permit and will be required to be prepared and delivered in accordance with the conditions of the S138 permit.

Any works or maintenance on State or Federal Public Roads to be prepared and delivered in accordance with an ROL permit with TfNSW.

## 4. Road Maintenance

The applicant will need to enter a formal maintenance management plan as part of the S138 permit for Council roads along the route for the entire duration of the project, to Council's written satisfaction including:

1. The maintenance management plan will be based on TfNSW M3 Maintenance Plan (see proforma example attached);
2. Maintenance work will be coordinated to Council's satisfaction including timing and day/night work;
3. Dilapidation survey of the route to be undertaken every twelve weeks of the project and provided to Council;
4. A Bank Guarantee will be required for the period of the project plus six months to cover any damage determined by Council's reasonable opinion, and dilapidation surveys, to have occurred as a result of the OSOM transported loads for the project; and
5. An Indemnity Deed Poll to be provided for emergency works to any assets that may suffer damage during the project.
either a Road Usage Fee or dilapidation surveys,, and a Bank Guarantee.

Noted. HOGWFPL will consult with MSC to obtain S138 permits for any works or maintenance performed on Council roads.

Noted. HOGWFPL will consult with TfNSW for any requirements when performing works or maintenance on State or Federal Public Roads.

The Projects Traffic Management Plan will detail requirements for any emergency repair or maintenance on Council roads along the final transport routes. This plan will be prepared in consultation with MSC.

If road dilapidation surveys are ultimately conditioned for the Project within Muswellbrook Shire, HOGWFPL will undertake a dilapidation survey along the final transport routes prior to commencement and following the completion of the OSOM delivery phase for construction. This survey will be provided to Council. If dilapidation surveys identify that any Council roads have been damaged during as a result of Project usage, HOGWFPL will repair this damage.

However we note a one-off Road Usage Fee of \$70,000 upon the commencement of construction was previously offered to MSC in our letter dated 2 June 2021 as an alternative to performing road dilapidation surveys and to provide greater certainty to MSC. The fee is proposed to compensate MSC for any dilapidation which may be caused by the general use of roads within the Muswellbrook Shire by traffic associated with the Project. Due to the volume of traffic which already uses roads within the Muswellbrook Shire, it will likely be impractical to commission a dilapidation survey which can identify only that dilapidation attributable to Project traffic, noting that OSOM loads for the Project are estimated to be less than 6 trips per day on average. To further support this, TTPP assessed the impact of estimated Project vehicles using Thomas Mitchell Drive and concluded that the Project impact is deemed negligible in comparison to other road users (Section 8.5.3 - Hills of Gold Wind Farm Traffic and Transport Addendum). Accordingly, this proposed approach of a Road Usage Fee as an alternative to road dilapidation surveys remains HOGWFPL's strong

|  | preference to provide both parties with greater certainty, and we ask that MSC further considers this and reverts on the offer. This offer is not intended to avoid HOGWFPL's obligation for repair if damage was made to roads by the Project that is not consistent with standard wear and tear. <br> HOGWFPL is accepting of providing a performance bond in favour of MSC in the form of a letter of credit or bank guarantee to secure its performance of any Council Asset upgrade works or general maintenance and repair of roads. HOGWFPL will negotiate these terms with MSC in good faith following selection of the final transport routes, with such bond to be for a reasonable amount having regard to the cost of any required modification works. The bond would be provided prior to the earlier of: (1) commencement of any modification works, or (2) commencement of OSOM deliveries. Any such performance bond would be released upon completion of Project OSOM deliveries plus 6 months. <br> On the basis of HOGWFPL offering: <br> - a performance bond throughout the duration of Project OSOM deliveries to protect MSC road assets; <br> - a Road Usage Fee (in lieu of road dilapidation surveys); <br> - a structural assessment of all drainage structures along the proposed route; and <br> - emergency repair or maintenance commitments in the TMP, <br> it is HOGWFPL's view that the risk to damage and repair of Council's assets during construction of the Project is well mitigated and therefore we do not agree to the request to also provide MSC an Indemnity Deed Poll. |
| :---: | :---: |
| 5. Communication <br> The applicant will need to enter a formal community consultation management plan for the entire duration of the project, to Council's written satisfaction including: <br> The community consultation management plan is to be developed in consultation with Council including but not limited to: <br> i. Monthly meetings with Council staff to discuss progress, issues and community feedback; <br> ii. Complaints and incident handling procedure including contact details of the applicant; | HOGWFPL commits to consulting with MSC on all these requests. |

$$
\begin{array}{l|l}
\hline \text { iii. Identifying residents, businesses, emergency services, } \\
\text { school bus and mines (shift change times) and key contacts } \\
\text { in these operations and necessary liaising with these road } \\
\text { users; } & \\
\text { iv. Details of the Transport Management Plan and progress } \\
\text { to be included and updated on both the applicant's website } \\
\text { as well as Council's website; }
\end{array} \quad \begin{aligned}
& \\
& \text { v. Applicant to provide updates to Council with regards to } \\
& \text { any planned maintenance works and/or upgrades and } \\
& \text { replacements. }
\end{aligned}
$$

HOGWFPL welcomes any feedback or further discussions with Muswellbrook Shire Council on the revised offer above or any further matters relating to the Project. If the above revised offer is acceptable to Muswellbrook Shire Council, we would greatly appreciate written confirmation of this from Council. A copy of this letter will be provided to the Department of Planning for inclusion of the relevant commitments by HOGWFPL in the Project's Statement of Commitments.

We respectfully request Council withdraw their objection to the project and confirm in writing by 3 November 2021.

Yours sincerely,


[^5]
## eNGie

APPENDIX A - Hills of Gold Windfarm Project - Muswellbrook Shire Council Route requirements - Letter 29 August 2021

## eNGie

APPENDIX B - Voluntary Contribution from Hills of Gold Wind Farm Pty Ltd - Letter 2 June 2021

## ENGie

APPENDIX C - Hills of Gold Wind Farm Route Survey v7 - Rex J Andrews


[^0]:    * Type Abbreviations: GU: General Upgrade; RU: Road Upgrade; BU: Bridge Upgrade; TTPP: TTPP Swept Path Design; CC: Creek Crossing

[^1]:    Source: Bitzios Consulting, 2020

[^2]:    SIDRA INTERSECTION 9.0 | Copyright © 2000-2020 Akcelik and Associates Pty Ltd | sidrasolutions.com
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[^3]:    SIDRA INTERSECTION 9.0 | Copyright © 2000-2020 Akcelik and Associates Pty Ltd | sidrasolutions.com
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    Project: X:118289 Hills of Gold Wind Farm Nundlel07 Modelling Files\18289-Hills of Gold model-210603.sip9

[^5]:    Andrew Kerley
    General Manager - Asset Development

