## asongroup

# Traffic Impact Assessment 

State Significant Development Application
Mamre South Precinct - Warehouse \& Logistics Hub 657-703 Mamre Road, Kemps Creek
Ref: 0584r02v06
13/05/2019

## Table of Contents

1 INTRODUCTION ..... 4
1.1 OVERVIEW ..... 4
1.2 Response to SEARs ..... 5
1.3 Objectives ..... 6
1.4 Methodology ..... 6
1.5 ReFERENCES ..... 7
1.6 REPORT StRUCTURE ..... 8
2 OVERVIEW OF PROPOSAL ..... 9
2.1 Proposed Development Characteristics ..... 9
2.2 Potential Future Master Plan (not part of this application) ..... 10
3 EXISTING CONDITIONS ..... 12
3.1 Site Location ..... 12
3.2 Existing Site Traffic Generation ..... 12
3.3 ROAD Network ..... 12
3.4 KEY INTERSECTIONS ..... 15
3.5 Existing Network Traffic Volumes ..... 18
3.6 Mid-block Traffic Volumes ..... 18
3.7 Intersection Performance - Existing Baseline (May 2018) ..... 19
3.8 PUBLIC TRANSPORT ..... 21
3.9 CYCLING ..... 23
4 FUTURE CONTEXT (WITHOUT PROPOSAL) ..... 24
4.1 PLANNED UpGRADES ..... 24
4.2 Background Growth - Future Base Case Traffic Projections ..... 27
4.3 Future Mid-block Capacity Analysis ..... 27
4.4 FUTURE INTERSECTION ANALYSIS ..... 28
4.5 IMPACT Mitigation ..... 30
5 OPERATIONAL TRAFFIC IMPACTS ..... 32
5.1 Traffic Generation Rates ..... 32
5.2 SSDA Traffic Generation ..... 33
5.3 SSDA Traffic Distribution ..... 33
5.4 SSDA INTERSECTION TRAFFIC INCREASE ..... 34
5.5 SSDA INTERSECTION ANALYSIS ..... 35
6 SSDA PARKING ANALYSIS ..... 39
6.1 Car Parking Rates ..... 39
6.2 CAR Parking Requirements ..... 39
6.3 Accessible Parking Rates ..... 41
6.4 SSDA Service Bay Requirement ..... 43
7 FUTURE SCENARIO WITH POTENTIAL MASTER PLAN ..... 45
7.1 TraFFIC GENERATION ..... 45
7.2 Traffic Distribution ..... 45
7.3 Mid-block Capacity Analysis ..... 46
7.4 TRAFFIC IMPACT ..... 47
8 CONCLUSIONS ..... 49
8.1 General Notes ..... 49
8.2 EXISTING \& FUTURE CONDITIONS (WITHOUT PROPOSAL) ..... 49
8.3 SSDA AsSESSMENTS ..... 50
8.4 InDICATIVE FUTURE MASTER PLAN (CONTEXT ONLY - NOT PART OF THIS APPLICATION)50

## Appendices

## Appendix A: SEARs (Ref: SSD 9522)

Appendix B: Reduced Architectural Plans
Appendix C: Traffic Volumes
Appendix D: SIDRA Results

## 1 Introduction

### 1.1 Overview

Ason Group has been commissioned by Altis Property Partners (Altis) and Frasers Property Australia (FPA) to undertake a Traffic Impact Assessment (TIA) in relation to a development at 657-753 Mamre Road in Kemps Creek (to be known as the Mamre South Precinct - MSP), within the Penrith City Council (PCC) Local Government Area. As a State Significant Development Application (SSDA), the application - for construction and operation of a warehouse, industrial and logistics hub (refer Figure 1) - is to be submitted to NSW Department of Planning \& Environment (DP\&E). The SSDA comprises two precincts to be located on either side of Bakers Lane as shown in below figure.


Figure 1: MSP SSDA Plan
A Response to the Secretary's Environmental Assessment Requirements is provided in the following section.

## 0584r02v06

Mamre South Precinct; 657 - 703 Mamre Rd, Kemps Creek | SSDA Traffic Impact Assessment

### 1.2 Response to SEARs

The Secretary's Environmental Assessment Planning Requirements (SEARs) for the preparation of an Environmental Impact Statement (EIS) is included in Appendix A.

A summary of relevant SEARs requirements relating to the traffic and transport related aspects is presented in Table 1. This also includes reference to the relevant sections of the TIA where each requirement is addressed.

Table 1: Response to SEARs

## Requirement

Relevant Section of TIA

A quantitative Traffic Impact Assessment prepared in accordance with relevant Penrith City Council, Austroads and Roads and Maritime Services guidelines.

Details of all daily and peak traffic and transport movements likely to be generated by the development (vehicle type, public transport) during construction and indicative operation.

Impacts on the safety and capacity of the surrounding road network and access points, using SIDRA or similar modelling, to assess impacts from current traffic counts and cumulative traffic from existing and proposed development

Demonstrate that sufficient loading/unloading, car parking and pedestrian and cyclist facilities have been provided for the development.

Details and a justification of access to, from and within the site (vehicular and pedestrian).

Details of road upgrades, new roads or access points required for the development, if necessary.

Consideration of the western connection of the Southern Link Road and road widening requirements for Mamre Road, in consultation with RMS

This Traffic Impact Assessment (TIA), covers all critical expectations of the Council, Austroads and RMS for traffic reporting and is in line with the TIA structure and checklist suggested by TfNSW (TfNSW, Draft Guide to Transport Impact Assessments, 2018).

Daily and peak hour traffic generation figures for the SSDA is provided in Section 5.2 which provides context on the anticipated traffic volumes of the Proposal on the surrounding road network. It is expected that separate Construction Traffic Management(s) would be prepared for each Lot which will discuss the anticipated construction traffic volumes.

SIDRA analysis for relevant modelling scenarios have been undertaken and included in Appendix D. Essentially the SIDRA performance reviews for the "Existing + SSDA" scenario is addressed in Section 5.5.

Relevant parking rates based on Roads and Maritime Services (RMS) Guide to Traffic Generating Developments, are included in Section 6.1. These rates are sought for the SSDA and addressed in Section 6.2.

Details SSDA access arrangements are provided in Section 2.

A number of road / intersection upgrades are envisaged in this vicinity. Identified upgrades to support nondevelopment traffic is discussed in Section 4. Additional upgrades (or required connections to the regional road network) are discussed in this section.

Reference should be made to the above Sections with regard to future road upgrades both "with" and "without" development of this Site.

Requirement

Consideration of the proposed Western Sydney Freight Line, including the width of the corridor and how this will be considered in the layout of the proposal, in consultation with TfNSW.

Details of how the proposal would allow connection to future land uses to the south of the site.

## Relevant Section of TIA

It is our understanding that some initial consultation has been undertaken with TfNSW and, in response, the Proposal sets aside land along the northern boundary to allow for the possible future freight rail corridor.

No connection is deemed necessary due to individual sites developing and having their own access to Mamre Road.

It is anticipated that the construction vehicles will access to/from the Proposal via Mamre Road. However, it is noted that a detail Construction Traffic Management Plan (CTMP) for the Proposal is not part of the scope of this TIA.

It is expected that a CTMP will be prepared for the SSDA development prior to issue of the Construction Certificate (CC). That CTMP will have detailed information regarding the construction work and its associated traffic impact on the surrounding road network.

### 1.3 Objectives

The key objectives of this TIA are:

- To assess the impact of the proposal on the performance of the road network in the proximity of the Site; and
- Where required, identify necessary upgrades to mitigate any adverse impacts.


### 1.4 Methodology

To achieve the above objectives, Ason Group has undertaken the following tasks:

- Commissioned and reviewed traffic data for the key intersections in the locality. The existing traffic volumes were surveyed to assist with developing a Base Case.
- Reviewed the planned future road network to establish context for any required road infrastructure improvements.
- Obtained EMME model future traffic volume forecasts from RMS to establish Future (Year 2036) Base Case network volumes.
- Undertaken a detailed assessment of the traffic generation and distribution characteristics of the project.
- Undertaken a detailed review of the mid-block capacity on the surrounding road network under the following scenarios:
- Existing - May 2018.
- Future (Year 2036) Base Case based on RMS upgrade plans for the locality.
- An alternative Future Base Case (Project Case) which is developed based on the outcome of this TIA.
- Existing Base Case + SSDA. This scenario also considers the traffic generation from Stage 1 of MWP.
- Project Case + A possible future built form on the MSP.
- Assessed the performance of the key intersections, using SIDRA Network, for the above-mentioned scenarios. In this regard, the key intersections have been identified as those intersection along Mamre Road between Mandalong Close and Bakers Lane (inclusive).


### 1.5 References

In preparing this report, Ason Group has referenced the following documents:

- Mamre West Land Investigation Area, Planning Proposal Mamre Road, Western Sydney Priority Growth Area, prepared by Ason Group (ref: 0124r03v3) and dated 23 February 2016 (MWP TIA).
- Stage 1 SSDA, Proposed Warehouse and Logistics Hub; 585-649 Mamre Road, Orchard Hills, Western Sydney Priority Growth Area (the SSD TIA), prepared by Ason Group (ref: 0124r04v2) and dated 5 April 2016. This report was submitted as a State Significant Development (SSD) application for Stage 1 (Lots 7, 8 and internal roads) of the Mamre West Precinct.
- Mamre Road Upgrades Kerrs Road to M4 Motorway, prepared by Roads and Maritime Services (RMS) and dated November 2017.

In addition, this TIA also refers to the following general guidelines and Standards:

- Roads and Maritime Services (RMS), Guide to Traffic Generating Developments, 2002 (RMS Guide).
- Roads and Maritime Services (RMS), Guide to Traffic Generating Developments Updated Traffic Surveys, 2013.


### 1.6 Report Structure

The remainder of this report is structured as follows:

- Section 2 Provides a detailed overview of the Project.
- Section 3 Describes existing conditions including the road network and accessibility to alternate (non-car transport modes).
- Section 4 Provides the future context for the Site and surrounding area and outlines future traffic volumes and planned upgrades.
- Section 5 Assesses the impacts of the SSDA traffic volumes.
- Section 6 Assesses the car parking demand and supply for the proposed SSDA.
- Section 7 Assesses the impacts of a possible future built form on the entire MSP site and identifies necessary upgrades and relevant controls applicable to subsequent stages of the development such as parking rates and access provisions. It is noteworthy that any further development stages will be subject to separate applications.
- Section 8 Presents the study conclusions.


## 2 Overview of Proposal

A detailed description of the proposal is provided in the planning submissions prepared by Willowtree Planning. Reference should also be made to the relevant plan included in Appendix B. Nevertheless, a summary of the key aspects relevant to this traffic and transport assessment are provided below.

### 2.1 Proposed Development Characteristics

An overview of the proposed SSDA access strategy is presented in below figure. The SSDA will comprises:

- A total of $163,671 \mathrm{~m}^{2}$ of building floor area, comprising:
- $155,411 \mathrm{~m}^{2}$ warehouse GFA; and
- $8,260 \mathrm{~m}^{2}$ of ancillary office.
- Primary access from Bakers Lane (west) to the existing signalised intersection of Mamre Road / Bakers Lane, with appropriate upgrades to the Bakers Lane (west) approach and broader signal operations.
- A secondary LILO access from Mamre Road is also proposed at the southern end of the subject development.


Figure 2: SSDA Access Strategy

### 2.2 Potential Future Master Plan (not part of this application)

Whilst not part of this application but for the purpose of future traffic assessments included in this TIA, we have been advised for a possible overall built form scheme and future access strategy for the entire Site. The future built form is broadly expected to include:

- A total of $511,871 \mathrm{~m}^{2}$ of warehouse building floor area, comprising:
- $486,361 \mathrm{~m}^{2}$ warehouse GFA; and
- $25,510 \mathrm{~m}^{2}$ of ancillary office.
- New internal roads.
- A new connection to the (future) external road network, being a new signalised connection to Southern Link Road, if to be extended west of Mamre Road by RMS / DPE in the future, and
- Upon construction of the Southern Link Road, the Bakers Lane / Mamre Road intersection would be closed, and access would instead be provided by the (signalised) intersection of Southern Link Road / Mamre Road (yet to be determined by the State and Local Government agencies).

It is important to note that this additional scope for modelling associated with this Master Plan does not relate to this SSDA - future stages being subject to subsequent DAs - and is only provided for context to inform the required future upgrades on the surrounding road network.

## 3 Existing Conditions

### 3.1 Site Location

The Site is located within the Penrith City Council LGA and is bordered by Mamre Road to the east; the Sydney Water Warragamba Pipeline to the north; South Creek to the west; and rural land to the south. Properties included within the Site are as follows:

```
| Lot 34 in DP1118173
- Lot Y in DP421633
- Lot 22 in DP258414
- Lot X in DP421633
- Lot 1 in DP1018318
```


### 3.2 Existing Site Traffic Generation

The Site does not currently generate any significant traffic volumes. As such, and for the purposes of a conservative assessment, the additional traffic associated with the development is considered as a NET increase in traffic to the surrounding road network.

### 3.3 Road Network

With reference to Figure 3, the key local roads influenced by the application include:

- Mamre Road - an arterial road servicing traffic between the Great Western Highway and M4 to the north and Elizabeth Drive to the south. In the vicinity of the MSP, Mamre Road generally provides 2 lanes for two-way traffic, with additional through movement and turning infrastructure at key intersections, specifically at Erskine Park Road and James Erskine Drive. Mamre Road has a posted speed limit of $80 \mathrm{~km} / \mathrm{h}$.
- Erskine Park Road - a sub-arterial road servicing traffic between the Great Western Highway and M4 to the north, Mamre Road to the south-west, as well as linking Lenore Drive (Erskine Park Link Road) to the M7 to the east. Erskine Park Road provides 4 lanes for two-way traffic north-east from the intersection of Mamre Road. Erskine Park Road has a posted speed limit of $70 \mathrm{~km} / \mathrm{h}$.
- James Erskine Drive - a local industrial access road, providing local access for the Erskine Park Industrial Precinct, which lies to the east of Mamre Road, northeast of the Precinct. James Erskine Drive provides 4 lanes for two-way traffic and provides additional turning infrastructure on the approach to Mamre Road. On-street parking is permitted; however, demand for this parking is low and therefore rarely used.
- Bakers Lane (East) - a two lane undivided Local Road which operates under a $60 \mathrm{~km} / \mathrm{hr}$ sign posted speed limit. Bakers Lane (East) provides primary access to a number of local schools and colleges in the area, with School Zone speed limit restrictions (40km/h) in operation during school peak periods. At discussed previously, at present, Bakers Lane (East) forms a Signalised T intersection with Mamre


Figure 3: Existing Road Network

### 3.4 Key Intersections

The key intersection in the vicinity of the MSP is the existing Signalised intersection of Mamre Road / Bakers Lane which is shown in Figure 4.


Figure 4: Existing Intersection of Mamre Road / Bakers Lane

At present this intersection effectively operates as a Signalised T intersection, with the Mamre Road and Bakers Lane (East) approaches under signal control, while the minor Bakers Lane (West) approach operates under priority (Stop) control. It is noted that Bakers Lane (West) currently provides for a minimal amount of construction traffic only, with less than 3 veh/hour in both the AM and PM peak periods.

The intersection currently provides the following turning infrastructure: -currently offers:

- A short left-turn lane, Mamre Road to Bakers Lane (East)
- A short right turn lane, Mamre Road to Bakers Lane (East).
- A short-left turn lane, Bakers Lane (East) to Mamre Road.

It Is noted that there are currently no restrictions to movements to or from Bakers Lane (West).

The performance of this intersection during the AM and PM peak periods have been assessed further to on-site observations and using SIDRA Network software.

In general, the on-site observations confirm a significant school traffic demand through the intersection, particularly during the PM peak period. The SIDRA results for the existing scenario will be discussed in further details in Section 3.5.

Other key intersections in this vicinity which have been reviewed as part of this TIA are shown in Figure 5 and are as follows:

1. T-intersection of Mamre Road / Mandalong Close.
2. Signalised intersection of Mamre Road / Erskine Park Road.
3. Signalised intersection of Mamre Road / James Erskine Drive.
4. Signalised intersection of Mamre Road / Mamre West Precinct.


Figure 5:Key intersections in the vicinity of the Site

### 3.5 Existing Network Traffic Volumes

The existing traffic volumes at key intersections in this vicinity were surveyed during weekday AM and PM peak periods, on a typical weekday in May 2018. The results of the traffic surveys are detailed in

## Appendix C1.

### 3.6 Mid-block Traffic Volumes

To get a better appreciation of the average weekday mid-block traffic volumes on Mamre Road (between Bakers Lane and James Erskine Drive) Ason Group undertook a 7-day (tube count) surveys. A summary of the existing 2018 directional mid-block traffic volumes in Mamre Road and Bakers Lane (East) in the immediate vicinity of the Site is provided below. This includes the applicable Level of Service (LoS) for each period, based on the RMS Guide criteria, noting again that Mamre Road is a two-lane undivided road with central line-marking in the vicinity of the Site.

Table 2: Existing Mid-block Traffic Volumes

| Road Section | Period | Existing Traffic Volumes (AWT) | LoS |
| :---: | :---: | :---: | :---: |
| Mamre Road north of Bakers Lane | AM | $\begin{gathered} 2,215 \\ \mathrm{NB}=1,094 \\ \mathrm{SB}=1,121 \end{gathered}$ | $\begin{aligned} & \mathrm{NB}=\mathrm{E} \\ & \mathrm{SB}=\mathrm{E} \end{aligned}$ |
|  | PM | $\begin{gathered} 2,085 \\ \mathrm{NB}=1,114 \\ \mathrm{SB}=971 \end{gathered}$ | $\begin{aligned} & \mathrm{NB}=\mathrm{E} \\ & \mathrm{SB}=\mathrm{E} \end{aligned}$ |
| Mamre Road south of Bakers Lane | AM | $\begin{gathered} 1,391 \\ N B=782 \\ S B=609 \end{gathered}$ | $\begin{aligned} & \mathrm{NB}=\mathrm{D} \\ & \mathrm{SB}=\mathrm{D} \end{aligned}$ |
|  | PM | $\begin{gathered} 1,541 \\ N B=678 \\ S B=863 \end{gathered}$ | $\begin{aligned} & \mathrm{NB}=\mathrm{D} \\ & \mathrm{SB}=\mathrm{D} \end{aligned}$ |
| Bakers Lane East of Mamre Road | AM | $\begin{gathered} 1,085 \\ W B=413 \\ E B=672 \end{gathered}$ | $\begin{gathered} W B=C \\ E B=D \end{gathered}$ |
|  | PM | $\begin{gathered} 734 \\ W B=536 \\ E B=198 \end{gathered}$ | $\begin{gathered} W B=C \\ E B=A \end{gathered}$ |

[^0]The above table indicates that:

- Mamre Road mid-block traffic volumes during the AM and PM peak hours are essentially already at capacity. This strongly suggests that the (planned) duplication of Mamre Road may need to be investigated sooner than envisaged based on current planning / timing.
- The above analysis of Mamre Road nearing capacity was confirmed by on-site observations during AM and PM peak hours. Extensive queues were observed on Mamre Road in this vicinity of the MSP, particularly during the PM peak period.


### 3.7 Intersection Performance - Existing Baseline (May 2018)

The performance of the key intersections in the vicinity of the MPS has been analysed using the SIDRA Network Intersection computer program. SIDRA modelling outputs a range of performance measures, in particular:

- Average Vehicle Delay (AVD) - The AVD (or average delay per vehicle in seconds) for intersections also provides a measure of the operational performance of an intersection and is used to determine an intersection's Level of Service (see below). For signalised intersections, the AVD reported relates to the average of all vehicle movements through the intersection. For priority (Give Way, Stop \& Roundabout controlled) intersections, the AVD reported is that for the movement with the highest AVD.
- Level of Service (LOS) - This is a comparative measure that provides an indication of the operating performance, based on AVD.

The following table provides a recommended baseline for assessment as per the RMS Guide:

Table 3 : Level of Service Criteria for Intersections

| Level of <br> Service | Average Delay per <br> Vehicle (secs/veh) | Traffic Signals, Roundabout | Give Way and Stop Signs |
| :---: | :---: | :---: | :---: |
| A less than 14 | 15 to 28 | Good with acceptable delays \& spare |  |
| capacity |  |  |  |$\quad$ Acceptable delays \& spare capacity

The results of the SIDRA Network analysis are summarised in Table 4.

Table 4: SIDRA Network Results - Existing Baseline (May 2018)


Notes 1: The traffic associated with the signalised intersection of Mamre Road / MWP access was not fully settled at the time of preparation of this TIA and as such the existing baseline does not allow for assessment of this intersection.

2: The intersection of Mamre Road / Mandalong Close has is an existing intersection. It is important to note that this intersection is proposed for LI/LO in future and will operate satisfactorily under future scenarios (refer Table 21).

3: Figure in brackets () reflects average intersection performance for unsignalised intersection.

It can be seen from above that a number of intersections "fail" under existing conditions, with a LoS F in one or more periods. A number of upgrades have been identified for the road network to address these issues and support further growth, as discussed in Section 4.

### 3.8 Public Transport

### 3.8.1 Existing Bus Services

The existing bus services in the vicinity of the MSP are shown in Figure 6.


Figure 6: Public Transport Services \& Cycling Routes

It is evident that the MSP is not directly serviced by public transport operations at this time. Notwithstanding, opportunities for future connections have been identified and are discussed further below.

### 3.8.2 Future Bus Service Opportunities

While it is apparent that the MSP will be well served by a future road network, it is nonetheless important that people have the opportunity to use public transport, which requires significantly improved connectivity to the broader area in the first instance. This could be possible through an extension of the 779-bus route to include stops within the future internal road network of the MSP. This route would provide a direct connection to St Mary's railway station and to the broader transport network.

The planning of bus services in Sydney is governed by the NSW Service Planning Guidelines, which aims to establish Strategic Transport Corridors and a hierarchy of bus route types that:

- link to Regional centres (such as Penrith and Mt Druitt).
- pass through patronage generators such as district centres, TAFE colleges, hospitals and universities.
- connect with other transport modes (trains, ferries and other buses).
- are multifunctional (serving journeys to work, education, shopping and recreation).
- are direct and frequent.
- meet the network planning principles.

It is also the case that the establishment of public transport services as early as possible in the development stages of the area is important to achieve a culture of public transport use from the outset. To make public transport a viable choice in the study area, the services should ideally:

- integrate with existing bus services in the area.
- connect to regional centres of Penrith, Mt Druitt and Blacktown.
- in the long term connect to areas such as Leppington in the South West Growth Centre, Prairiewood and the Liverpool to Parramatta T-Way.


### 3.9 Cycling

There are existing opportunities and infrastructure for cyclists to access the Site via Mamre Road. Bicycle lanes are provided along Erskine Park Road and sections of Mamre Road, in addition to carriageway shoulders that could also be utilised by cyclists. Notwithstanding, there are opportunities to improve cycling infrastructure through the provision of shared paths along Mamre Road fronting the MSP that could be connected to paths along Erskine Park Road.

## 4 Future Context (Without Proposal)

### 4.1 Planned Upgrades

It is known that the road network in the general vicinity of the Site is due to receive significant road upgrades in future as part of the Mamre Road Upgrade strategy. It is therefore crucial to develop a future "Base Case' that includes those planned road and intersection upgrades (and of course the forecast additional traffic flows) so as to appropriately measure the (potential) impacts of the traffic likely to be generated by the potential development yield on the entire site.

Accordingly, the modelling assumptions made for the major proposed road upgrades in the immediate vicinity of the Site are extracted from Mamre Road Upgrade document prepared by RMS in November 2017 and also reference has been made to the RMS website.


Figure 7: Mamre Road Upgrade Concept Design

In February 2019, the NSW Government announced \$220M funding for a 3.8-kilometre section of the Mamre Road Upgrade between M4 Motorway and Erskine Park Road to:
"...transform the existing two-lane undivided road into a four-lane divided road, providing a safer, highercapacity link. The Mamre Road upgrade will also be future proofed, allowing another two lanes to be added down the track,"

With reference to above, the following figures provide more detail in regard to the RMS future intersection layouts.


Figure 8: Mamre Road Upgrade - Intersection Configurations


Figure 9: Mamre Road Upgrade - Intersection Configurations

### 4.2 Background Growth - Future Base Case Traffic Projections

The future base case scenario has considered the year 2036. As such, EMME model traffic volumes for the vicinity of the Site for 2036 were obtained from RMS during the course of this study, with data provided for the following three (3) intersections:

- Mamre Road / Southern Link Road (EMME inputs assume a four-way intersection),
- Mamre Road / James Erskine Drive (EMME inputs assume a T-intersection), and
- Mamre Road / Erskine Park Road (EMME inputs assume a T-intersection).

These volumes form the basis of the Future Base Case scenario. However, to also incorporate the extent of the assumed future road upgrades envisaged in this TIA, further assumptions have been made which are as follows:

- Mamre Road / James Erskine Drive will be a four-way signalised intersection. The traffic volumes on the fourth leg (the western leg) were obtained from MWP TIA prepared by Ason Group.
- The EMME outputs provided by the RMS did not include traffic projections on Mandalong Close. Accordingly, a 5\% traffic growth per annum was conservatively assumed for this road in order to provide a robust traffic assessment. It is noted that the intersection of Mamre Road / Mandalong Road is expected to provide Left In/Left Out only by 2036.

Further to the above, a copy of the base case traffic volumes (year 2036) are attached in Appendix C2.

### 4.3 Future Mid-block Capacity Analysis

Future Base Case mid-block capacities and Level of Service have been determined with reference to the 2036 forecast traffic volumes and are summarised in Table 5.

Table 5: Future Base Case Mid-block Traffic Volumes

| Road Section | Period | Projected 2036 Traffic Volumes | LoS |
| :---: | :---: | :---: | :---: |
| Mamre Rd | AM | $\begin{gathered} 4,076 \\ \mathrm{NB}=1,908 \\ \mathrm{SB}=2,168 \end{gathered}$ | $\begin{aligned} & N B=D \\ & S B=D \end{aligned}$ |
| (north of SLR) | PM | $\begin{gathered} 3,689 \\ N B=1,582 \\ S B=2,107 \end{gathered}$ | $\begin{aligned} & \mathrm{NB}=\mathrm{C} \\ & \mathrm{SB}=\mathrm{D} \end{aligned}$ |
| Mamre Rd (south of SLR) | AM | $\begin{gathered} 3,961 \\ N B=2,109 \\ S B=1,852 \end{gathered}$ | $\begin{aligned} & \mathrm{NB}=\mathrm{D} \\ & \mathrm{SB}=\mathrm{D} \end{aligned}$ |
|  | PM | $\begin{gathered} 3,598 \\ \mathrm{NB}=1,626 \\ \mathrm{SB}=1,972 \end{gathered}$ | $\begin{aligned} & \mathrm{NB}=\mathrm{C} \\ & \mathrm{SB}=\mathrm{D} \end{aligned}$ |
| Southern Link Rd (East of Mamre Rd) | AM | $\begin{gathered} 2,251 \\ W B=577 \\ E B=1,674 \end{gathered}$ | $\begin{aligned} & W B=A \\ & E B=C \end{aligned}$ |
|  | PM | $\begin{gathered} 2,525 \\ W B=1,785 \\ E B=740 \end{gathered}$ | $\begin{gathered} W B=C \\ E B=A \end{gathered}$ |

Notes 1): NB = North Bound direction \& SB = Southbound direction
2): Mid-block LoS criteria is obtained from Table 4.4 of RMS Guide to Traffic Generating Documents.
3): Future Base Case allows for two lane traffic flow on Mamre Road and Southern Link Road plus turning lanes.

According to the above table, the following outcomes are noteworthy:

- While the future road upgrades envisaged for Mamre Road - and specifically carriageway widening to provide a 4-lane road - would accommodate the projected traffic flows, there is little if any spare capacity available north of the Southern Link Road (and then through the other key intersections to the north. Notwithstanding, it is noted that a wide-median treatment is proposed for the upgraded Mamre Road, which would facilitate further widening in the future.
- The capacity assessment undertaken for the Southern Link Road confirms that the proposed 4lane carriageway (two-lanes per direction) can accommodate future demands with significant spare capacity.


### 4.4 Future Intersection Analysis

The Future Base Case (Year 2036) - with the identified intersection layouts outlined in Section 4 above and EMME traffic volumes obtained from RMS - has been assessed using SIDRA Network software to establish the performance of the future network without the proposed development. Details of the SIDRA outputs are attached in Appendix D2 and a summary of the results provided in Table 6.

Table 6: Network Performance - Future Base Case (with Mamre Road Upgrades)

| Intersection | Scenario | Period | Intersection Delay | Level of Service |
| :---: | :---: | :---: | :---: | :---: |
| Mamre Road/ Southern Link | Future Baseline | AM | 77.1 | F |
|  |  | PM | 45.3 | D |
| Mamre Road/ Mamre West Precinct Access | Future Baseline | AM | $\begin{aligned} & 13.7 \\ & (0.4) \end{aligned}$ | A |
|  |  | PM | $\begin{aligned} & 18.2 \\ & (1.0) \end{aligned}$ | B |
| Mamre Road / James Erskine Drive | Future Baseline | AM | 39.0 | C |
|  |  | PM | 47.6 | D |
| Mamre Road / Erskine Park Road | Future Baseline | AM | 50.0 | D |
|  |  | PM | 25.0 | B |
| Mamre Road / Mandalong Close | Future Baseline | AM | $\begin{aligned} & 10.6 \\ & (0.8) \end{aligned}$ | A |
|  |  | PM | $\begin{aligned} & 17.2 \\ & (0.6) \end{aligned}$ | B |

Note 1) All pedestrian crossings at the signals are modelled with $20 \%$ pedestrian calls in SIDRA to reflect the low levels of pedestrian activity in the locality.
2) The proposed Mamre Road intersections with the MWP southern access, and with Mandalong Close, will be in the form of LILO intersections.

From the above, the following is noteworthy:

- It is apparent that the future intersection upgrades envisaged for Mamre Road will NOT achieve the RMS desirable design LoS.
- The intersection of Mamre Road / Southern Link Road will operate at a LoS "F and D" during AM and PM peak periods, respectively. A further review of the SIDRA Network Lane summary results confirm that the Mamre Road approaches to the Southern Link Road intersection will operate with excessive delays and queues (refer Appendix D2 for details).
- The degree of saturation for a number of movements at numerous Mamre Road intersections exceeds $100 \%$, which strongly suggests the potential for future capacity constraints.


### 4.5 Impact Mitigation

Having regard for above, it is concluded that the recommended road and intersection upgrades envisaged for Mamre Road (at this time) do not adequately accommodate the future demand for this regional corridor.

Accordingly, this TIA has undertaken some 'option testing' to identify further upgrades that could be considered to mitigate these capacity issues. It is emphasised that the 'options' presented in this TIA will require further consultation with RMS prior to adoption.

### 4.5.1 Alternative Upgrade Option - Project Future Case

An alternative design option examined to resolve the Mamre Road mid-block capacity issues provides for an additional (third) lane in Mamre Road through the study area. As previously stated, the current Mamre Road Upgrade planning provides for a wide central median in Mamre Road to allow for future widening. As such, implementation of this option would primarily be in the form of reducing the central median width.

The results of the intersection performance analysis undertaken for this option (along with the revised intersection layouts) are detailed in Appendix D3 and summarised in Table 7 below.

Table 7: Network Performance - Future Base Case with Improvements

| Intersection | Scenario | Period | Intersection Delay | Level of Service |
| :---: | :---: | :---: | :---: | :---: |
| Mamre Road / Southern Link | Project Future Case | AM | 37.0 | C |
|  |  | PM | 36.7 | C |
| Mamre Road / Mamre West Precinct Access | Project Future Case | AM | $\begin{gathered} 9.2 \\ (0.3) \end{gathered}$ | A |
|  |  | PM | $\begin{aligned} & 10.2 \\ & (0.4) \end{aligned}$ | A |
| Mamre Road / James Erskine Drive | Project Future Case | AM | 30.2 | C |
|  |  | PM | 35.1 | C |
| Mamre Road/ Erskine Park Road | Project Future Case | AM | 24.1 | B |
|  |  | PM | 24.5 | B |

## 0584r02v06

Mamre South Precinct; 657 - 703 Mamre Rd, Kemps Creek | SSDA Traffic Impact Assessment

| Intersection | Scenario | Period | Intersection Delay | Level of Service |
| :---: | :---: | :---: | :---: | :---: |
| Mamre Road / Mandalong Close | Project Future Case | AM | $\begin{gathered} 9.7 \\ (0.4) \end{gathered}$ | A |
|  |  | PM | $\begin{aligned} & 12.5 \\ & (0.5) \end{aligned}$ | A |

Note 1) As per Base Case, all pedestrian crossing at the signals are modelled with $20 \%$ pedestrian calls in SIDRA to reflect the low levels of pedestrian activity in the locality.
2) The proposed Mamre Road intersections with the southern MWP access and Mandalong Close will be in the form of LILO intersections.

It is evident from comparison between Table 6 and Table 7 that:

- The alternative design option with three (3) lanes in each direction in Mamre Road will significantly improve the performance of all key intersections.
- More importantly, a review of the SIDRA Network Lane Summary results confirms that no approach movements (at any of the Mamre Road intersection) would operate at LoS "F". As such, the operation of Mamre Road - an important future regional corridor - will be improved significantly, with no excessive queues or delays through 2036.

Accordingly, it is expected that Mamre Road should be upgraded to 3 lanes in each direction in the longer term to support the general background growth in traffic volumes, regardless of the MSP proposal. As such, the remainder of TIA relies on this option (Future Base Case with Improvements) as basis to compare the Project Future Case scenario (Future Base Case + Development).

## 5 Operational Traffic Impacts

### 5.1 Traffic Generation Rates

The traffic generation rates adopted for this assessment reference Appendix E of the RMS Technical Direction TDT 2013/04a. Specifically, Ason Group has referenced the surveyed rates for vehicle trips during adjacent road AM and PM peak periods for the following three (3) industrial sites:

- Site 1: Erskine Park Industrial Estate, Erskine Park;
- Site 3: Wonderland Business Park, Eastern Creek; and
- Site 4: Riverwood Business Park, Riverwood.

These Sydney sites all exhibit similar attributes to those proposed for this TIA, including land-use and size of development. It is noted that the other Sydney and non-metropolitan sites reported in the RMS Technical Direction TDT 2013/04a are much smaller than the MSP and/or have a significantly higher office component that that proposed for the MSP.

The MWP TIA adopted the trip generation rates surveyed for Site 1 (Erskine Park Industrial Estate) which was entirely reasonable given that the MWP lies directly opposite the Erskine Park Industrial Estate. The rates surveyed at the Erskine Park Industrial Estate (and applied to the MWP) are:

- AM Rate $\quad 0.134$ trip per $100 \mathrm{~m}^{2}$ of GFA.
- PM Rate 0.139 trip per $100 \mathrm{~m}^{2}$ of GFA.

While it would be equally appropriate to apply these same rates to the MSP assessment, for the purposes of a worst-case assessment, this TIA has adopted rates which reflect the average rate of the 3 Sydney warehouse sites. These (significantly higher) MSP assessment trip rates are as follows:

- AM Rate $\quad 0.247$ trip per $100 \mathrm{~m}^{2}$ of GFA.
- PM Rate 0.182 trip per $100 \mathrm{~m}^{2}$ of GFA.
- Daily Rate 2.64 trip per $100 \mathrm{~m}^{2}$ of GFA.

Accordingly, the results of the assessments presented in this TIA are more conservative than what was undertaken for MWP. This conservative approach provides flexibility for latter development to reflect minor changes that may occur over the life of the MSP.

### 5.2 SSDA Traffic Generation

Application of the traffic generation rates discussed in Section 5.1 above to the SSDA yield results in the following $\mathrm{AM}, \mathrm{PM}$ and daily traffic volumes.

Table 8: SSDA Estimated Traffic Generation

| Site | GFA (m2) | AM Peak <br> (veh/hr) | PM Peak <br> (veh/hr) |
| :---: | :---: | :---: | :---: |
| Site 1 <br> (North of Bakers lane - <br> Lots 1, 2 and 3) | 66,135 | 164 | 120 |
| Site 2 <br> (South of Bakers Lane- <br> Lots 4, 5 and 6) | 97,536 | 241 | 177 |
| Total | 163,671 | 405 | 297 |

### 5.3 SSDA Traffic Distribution

The adopted trip distribution for the SSDA is summarised in below Table 9:

Table 9: Traffic Distribution - SSDA

| Peak Period | Land Use | Total Generation (veh/hr) | \%Inbound | \%outbound | Inbound Movements (veh/hr) | Outbound <br> Movements (veh/hr) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM | Warehouse | 385 | 70\% | 30\% | 270 | 115 |
|  | Office | 20 | 70\% | 30\% | 14 | 6 |
| PM | Warehouse | 282 | 30\% | 70\% | 85 | 197 |
|  | Office | 15 | 30\% | 70\% | 4 | 11 |

The resultant traffic distribution of the proposed SSDA development on the surrounding road network is shown in Appendix C3 and the Existing + SSDA traffic is attached in Appendix C4.

### 5.4 SSDA Intersection Traffic Increase

For context, below Table 10 summarises the total existing traffic volumes at key intersections during the AM and PM peak periods and the additional traffic increase as a result of the proposed SSDA development.

Table 10: SSDA Contribution to the Existing and Future Traffic Volumes

| Intersection | Period | Traffic Volumes (\% Increase) |  |
| :---: | :---: | :---: | :---: |
|  |  | Existing | SSDA Traffic (\%Increase) |
| Mamre Road/ Bakers Lane (Signal Control) | AM | 2,365 | $\begin{gathered} 401 \\ (+16.9 \%) \end{gathered}$ |
|  | PM | 2,202 | $\begin{gathered} 297 \\ (+13.5 \%) \end{gathered}$ |
| Mamre Road / <br> Mamre West Precinct Access (Signal Control) | AM | na | 247 |
|  | PM | na | 178 |
| Mamre Road/ James Erskine Drive (Signal Control) | AM | 2,557 | $\begin{gathered} 247 \\ (+9.7 \%) \end{gathered}$ |
|  | PM | 2,349 | $\begin{gathered} 178 \\ (+7.6 \%) \end{gathered}$ |
| Mamre Road/ Erskine Park Road (Signal Control) | AM | 3,113 | $\begin{gathered} 247 \\ (+7.9 \%) \end{gathered}$ |
|  | PM | 2,878 | $\begin{gathered} 178 \\ (+6.2 \%) \end{gathered}$ |
| Mamre Road / Mandalong Close (Stop Control) | AM | 2,119 | $\begin{gathered} 92 \\ (+4.3 \%) \end{gathered}$ |
|  | PM | 1,798 | $\begin{gathered} 100 \\ (+5.6 \%) \end{gathered}$ |

Note: (1) The existing Mamre Road West Precinct traffic has not been settled at the time of preparation of this report and as such the assessment of this intersection for existing scenario is not undertaken.

As indicated in the above table:

- The additional traffic added to Mamre Road / Bakers Lane intersection in the interim scenario are in the order of $13 \%$ to $17 \%$ during the road network peak hour periods.
- Following construction of the SSDA, the additional AM and PM peak traffic on all other intersections (other than the signalised intersection of Mamre Road / Bakers Lane) is estimated to be in the order of less than $10 \%$.
- Typically, an increase in traffic of less than $10 \%$ does not warrant detailed intersection assessment (i.e. SIDRA intersection analysis). Notwithstanding, in order for a robust assessment, the performance of these intersections have been modelled using SIDRA Network for both AM and PM peak hours as part of this assessment, as detailed below Sections.


### 5.5 SSDA Intersection Analysis

The SIDRA analysis assumes that in the interim, prior to Mamre Road Upgrade works:

- The configuration of the Mamre Road / Bakers Lane is as shown in Figure 10. This includes:
- Provision of a new right turn bay from Mamre Road southbound into the proposed development;
- Provision of a new left turn bay from Mamre Road northbound into the proposed development;
- Provision of dedicated short left and right turn lanes from the Bakers Lane (West) approach to Mamre Road, and
- Provision of full signalised pedestrian crossings in accordance with standard RMS practice for new signalised intersections.
- Other key intersection configurations will be as per the existing network (refer Figure 5).

It is again noted that this intersection upgrade will only be temporary and is provided only to facilitate the development traffic. Bakers Lane is proposed to be disconnected from Mamre Road and be realigned with the proposed Southern Link Road in the longer term. It is noteworthy that the traffic modelling (SIDRA analysis) undertaken for "Existing + SSDA" refers to an earlier scheme of the project with greater assumed yield of $165,187 \mathrm{~m}^{2}$. Accordingly, the modelled AM and PM peak hour vehicle trips of 408 and $300 \mathrm{veh} / \mathrm{hr}$ respectively modelled in SIDRA are actually higher than assessed above. Whilst these modelled figures 3 veh/hr greater than the estimated peak hour traffic generation of the SSDA - as per the current scheme - the change is not expected to have any material impact on the outcome of the modelling which is more conservative.


Figure 10: Signalised Intersection of Mamre Road / Bakers Lane - Interim Scenario
The SIDRA results are summarised in below table.

Table 11: Local Network Performance Comparison (Existing and Existing + SSDA)

| Intersection | Scenario | Period | Intersection Delay | Level of Service |
| :---: | :---: | :---: | :---: | :---: |
| Mamre Road / Bakers Lane (Signal Control) | Baseline | AM | 29.6 | C |
|  |  | PM | 139.5 | F |
|  | Existing + SSD | AM | 42.0 | C |
|  |  | PM | 85 | F |
| Mamre Road/ Mamre West Precinct Access (Signal Control) | Baseline | AM | na | na |
|  |  | PM | na | na |
|  | Existing + SSD | AM | 13.5 | A |
|  |  | PM | 16.5 | B |
| Mamre Road/ James Erskine Drive (Signal Control) | Baseline | AM | 10.6 | A |
|  |  | PM | 18.1 | B |
|  | Existing + SSDA | AM | 13.8 | A |
|  |  | PM | 14.9 | B |
| Mamre Road/ Erskine Park Road (Signal Control) | Baseline | AM | 23.9 | B |
|  |  | PM | 29 | C |
|  | Existing + SSD | AM | 31.4 | C |
|  |  | PM | 30.0 | C |
| Mamre Road / Mandalong Close (Stop Control) | Baseline | AM | $\begin{aligned} & 1,083 \\ & (23.7) \end{aligned}$ | F |
|  |  | PM | $\begin{aligned} & 235 \\ & (2.2) \end{aligned}$ | F |
|  | Existing + SSD | AM | $\begin{gathered} 2,519.2 \\ (22.4) \end{gathered}$ | F |
|  |  | PM | $\begin{gathered} 629.8 \\ (4.3) \end{gathered}$ | F |

Note: 1) Figure in brackets () reflects average intersection performance for unsignalised intersection.
2) Full pedestrian crossing is assumed for the proposed design of Mamre Road / Bakers Lane signal in Existing + SSDA scenario, however, the pedestrian phase call is set at 20\% in SIDRA.
3) The intersection of Mamre Road / Mandalong Close is an existing intersection. It is important to note that this intersection is proposed for LI/LO in future and will operate satisfactorily under future scenarios (refer Table 21).

## 0584r02v06

Mamre South Precinct; 657 - 703 Mamre Rd, Kemps Creek | SSDA Traffic Impact Assessment

According to the SIDRA results:

- The proposed SSDA will not have material impact on the surrounding road network as the average delays and LoS as a result of the "Existing + SSDA" traffic are similar to the existing baseline. In this instance considerations should be given to the significant improvements as a result of the upgraded intersection of Mamre Road / Bakers Lane. This intersection has been reported to operate with significantly less average delay ( 54.5 seconds) during PM peak hour when compared to the existing baseline. This demonstrates a significant improvement to the existing vehicular traffic operation at this signal.
- With respect to the intersection of Mamre Road / Bakers Lane it is noteworthy that this intersection is currently a signalised intersection with a stop sign control on the western leg and without pedestrian crossing facility. However, the proposal includes significant upgrades to this intersection with appropriate signalised pedestrian crossings. In this regard the upgrades proposed for Mamre Road / Bakers Lane will improve the pedestrian crossing opportunities, which is considered as a significant positive outcome for the locality.
- Furthermore, the existing configuration of this signal does not provide right and left turn bays into the Site to/from Mamre Road of which the proposed upgrades intend to implement these additional upgrades.
- Accordingly, the proposed upgrades at the Mamre Road / Bakers Lane signal can improve the vehicular and pedestrian movements at this signal when compared to the existing baseline.
- Further review of the SIDRA results for the Mamre Road / Bakers Lane signal suggests that the estimated overall queue distance at this intersection will be reduced by approximately 260 metres as a result of the additional improvements.
- Furthermore, SIDRA results confirm that the additional upgrades at the intersection of Mamre Road / Bakers Lane will improve the overall degree of saturation for the post development scenario which is also deemed to be a positive outcome.
- Regardless of the above, it is again emphasised that this arrangement will only be temporarily as the proposed regional upgrades in the vicinity will supersede this arrangement, and Bakers Lane will ultimately be closed off with no connection to Mamre Road.

In summary, the SSDA traffic can be accommodated by the surrounding road network and intersections without any material traffic impact, subject to the localised improvements to the Bakers Lane intersection.

## 6 SSDA Parking Analysis

### 6.1 Car Parking Rates

There is evidence that Council's warehouse parking requirement ( 1 space per $100 \mathrm{~m}^{2} \mathrm{GFA}$ ) is more than actual parking demands for warehouse developments, specifically as a factor of lower warehouse employee numbers. Amongst other factors, significant technological advances have also resulted in lower employee densities within warehouse developments, with the 2012 Employment Typology Study for the WSEA indicating employment densities of less than 20 employees per hectare across much of western Sydney. Consequently, many warehouse sites now provide car parking significantly in excess of the actual parking requirements of end users.

This position is further supported by the warehouse rates adopted by other controls, all of which return parking requirements significantly less than the numbers required based on the application of Council's DCP rates.

In response to the above, the minimum parking rates sought for the proposal, based on the RMS Guide rates for warehouse car parking, are:

- 1 space per $300 \mathrm{~m}^{2}$ of warehouse GFA
- 1 space per $40 \mathrm{~m}^{2}$ of ancillary office GFA

These proposed (minimum) rates would enable the required flexibility in the design of future developments whilst still ensuring sufficient parking to accommodate both the current and future parking requirements of tenants.

### 6.2 Car Parking Requirements

Having regard for the RMS parking rates suggested above, the required parking spaces for the SSDA and the supply of parking for this development is assessed in the following tables.

Table 12: Car Parking Provisions for Site 1 (to the north of Bakers Lane)

| Lot | $\begin{aligned} & \text { GFA m² } \\ & \text { (land-Use) } \end{aligned}$ | Car Parking Requirement | Total Parking Requirement | Car Parking Provided | Surplus (+)/ <br> Shortfall (-) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Lot 1 | $22,750 \mathrm{~m}^{2}$ <br> (warehouse) | 76 | 103 | $102{ }^{1}$ | (-) 1 |
|  |  |  |  |  |  |
|  | $\begin{aligned} & 1,100 m^{2} \\ & \text { (office) } \end{aligned}$ | 27 |  |  |  |
| Lot 2 | $21,995 \mathrm{~m}^{2}$ <br> (warehouse) | 73 | 102 | 105 | (+) 3 |
|  |  |  |  |  |  |
|  | $\begin{aligned} & 1,150 m^{2} \\ & \text { (office) } \end{aligned}$ | 29 |  |  |  |
| Lot 3 | $\begin{gathered} 18,040 \mathrm{~m}^{2} \\ \text { (warehouse) } \end{gathered}$ | 60 | 88 | 86 | (-) 2 |
|  |  |  |  |  |  |
|  | $\begin{aligned} & 1,100 m^{2} \\ & \text { (office) } \end{aligned}$ | 28 |  |  |  |
| Total | $\begin{gathered} 62,785 \mathrm{~m}^{2} \\ \text { (warehouse) } \end{gathered}$ | 209 | 293 | 2931 | 0 |
|  |  |  |  |  |  |
|  | $\begin{aligned} & 3,350 \mathrm{~m}^{2} \\ & \text { (office) } \end{aligned}$ | 84 |  |  |  |

Notes (1) Lot 1 provides a total of 93 onsite parking bays +9 provisional bays at the hardstand area.

According to the above table, the site 1 will provide a total of 284 car parking bays within the proposed car parking areas associated with all Lots plus 9 additional provisional bays for Lot 1 which sum up to a total of 293 car parking provision in total.

Despite minor shortfall of parking in Lots 1 and 3, the above table indicates that the overall parking across site 1 will provide enough car parking spaces to satisfy the RMS requirements.

It is important to note that the RMS parking rate of 1 space per $300 \mathrm{~m}^{2}$ - by itself - assumes a level of contingency for ancillary uses (office use in this instance) of up to $20 \%$. As such, adopting the 1 space per $300 \mathrm{~m}^{2}$ for the warehouse and office uses across site 1, it will result in sufficient number of bays proposed for this site.

A car parking assessment for site 2 is provided below.

Table 13: Car Parking Provisions for Site 2 (to the south of Bakers Lane)

| Lot | GFA m2 <br> (land-Use) | Car Parking <br> Requirement | Total Parking <br> Requirement | Car Parking <br> Provided |
| :---: | :---: | :---: | :---: | :---: |
| $18,480 m^{2}$ <br> (warehouse) | 62 | Surplus (+)/ <br> Shortfall (-) |  |  |
| $890 m^{2}$ <br> (office) | 22 | 84 | $(+) 8$ |  |

According to the above table the proposed site 2 will provide total of 461 car parking bays.

As indicated above, site 2 will provide more than enough car parking spaces to satisfy the RMS requirements for all three (3) Lots (with an overall surplus of 29 spaces).

### 6.2.1 Total Car Parking Provision

According to the above, the proposal will provide a total of 745 car parking bays within the car parking areas for all Lots plus 9 provisional bays (provided at Lot 1) which increases the parking provision to a total of 754 car parking bays.

In summary, the car parking provision for the entire Site is deemed sufficient in accordance with RMS requirements.

### 6.3 Accessible Parking Rates

Council's DCP at Part C10 - Transport, Access and Parking, Table C10.2 - requires accessible parking to be provided in accordance with the Disability (Access to Premises - Buildings) Standards 2010 from the Building Code of Australia. This standard requires accessible parking for industrial developments to be provided at a rate of:

- 1 space for every 100 car parking spaces or part thereof (rounded up).

The provision of accessible parking in accordance with these Standards would be adopted for the SSDA.

### 6.3.1 SSDA Accessible Car Parking Requirements

As discussed above, each individual Lot is to provide accessible car parking at a rate of $1 \%$ of the total parking provision (rounded up). Applicable accessible parking requirements are summarised in the following tables.

Table 14: Accessible Car Parking Provision for Site 1

| Lot | Car Parking Provided | Accessible Car Parking Requirement |
| :---: | :---: | :---: |
| Lot 1 | $102^{1}$ | 2 |
| Lot 2 | 105 | 2 |
| Lot 3 | 86 | 1 |
| Total | 293 | 5 |

Notes (1) 93 onsite parking bays +9 provisional bays at the hardstand area.

Table 15: Accessible Car Parking Provision for Site 2

| Lot | Car Parking Provided | Accessible Car Parking Requirement |
| :---: | :---: | :---: |
| Lot 4 | 92 | 1 |
| Lot 5 6 | 135 | 2 |
| Total | 234 | 3 |

Accessible spaces should ideally be located within close proximity to building entrances.

### 6.4 SSDA Service Bay Requirement

Separate hardstand areas are proposed for each warehouse development which is expected to accommodate their proposed site-specific demand. However, in the absence of known operational requirements, the RMS Guide suggests the following service bay requirements for industrial land-uses:

- 1 space per $800 \mathrm{~m}^{2}$ for development with a GFA $<8,000 \mathrm{~m}^{2}$, and
- 10 spaces +1 space per $1,000 m^{2}$ over $8,000 m^{2}$.

It is noted that (based on experience on similar projects) the strict application of RMS Guides service bay rates leads to a significant on-site service bay requirement which in most cases is higher than the actual tenant demands for such facilities.

In this regard, a review of the similar site-specific plans for developments within the Mamre West Precinct has been undertaken to review current practice with regard to provision of service bays for such developments.

Details of this analysis are outlined in below table.

Table 16: Service Bay Rates - Subdivision Lots at Mamre West Precinct

| Lot | Warehouse GFA ( $\mathrm{m}^{2}$ ) | Number of service bays provided | Service Bay Rate |
| :---: | :---: | :---: | :---: |
| Lot 6A | 5,000 | 6 | 1 space per $833 \mathrm{~m}^{2}$ |
| Lot 6B | 4,575 | 4 | 1 space per $1,144 \mathrm{~m}^{2}$ |
| Lot 6C | 13,950 | 6 | 1 space per $2,325 \mathrm{~m}^{2}$ |
| Lot 8A | 21,000 | 25 | 1 space per $840 \mathrm{~m}^{2}$ |
| Lot 8B1 | 7,000 | 9 | 1 space per $778 \mathrm{~m}^{2}$ |
| Lot 8B2 | 11,734 | 13 | 1 space per $903 \mathrm{~m}^{2}$ |

From the above Table it can be understood that the actual service bay provision varies within the range of (1 space per 2,325 to 1 space per 778) m²of warehouse GFA.

### 6.4.1 SSDA Loading Dock Requirements

Application of the recommended rates for the provision of service bays, discussed in above section the minimum and maximum range has been applied to each individual warehouse development at sites 2 and 5. The resultant service bay requirements are outlined in the following two tables:

Table 17: Service Bay Requirements for Site 1

| Lot | Warehouse GFA <br> $\left(\mathrm{m}^{2}\right)$ | Service Bay Requirement <br> (Lower Rate) | Service Bay Requirement <br> (Upper Rate) |
| :---: | :---: | :---: | :---: |
| Lot 1 | 22,750 | 10 | 29 |
| Lot 2 3 | 21,995 | 10 | 28 |
| Total | 18,040 | 8 | 23 |

Table 18: Service Bay Requirements for Site 2

| Lot | Warehouse GFA <br> $\left(\mathbf{m}^{2}\right)$ | Service Bay Requirement <br> (Lower Rate) | Service Bay Requirement <br> (Upper Rate) |
| :---: | :---: | :---: | :---: |
| Lot 4 | 18,480 | 8 | 24 |
| Lot 5 | 25,805 | 11 | 33 |
| Lot 6 | 48,341 | 21 | 62 |

The SSDA site plans currently shows large hardstand areas for each individual Lot. It is can be suggested that the proposed loading dock requirement would be between the upper and lower range of the above table.

It is also important to note that the above service bay requirements are generally more than actual operational requirements of large format industrial uses.

## 7 Future Scenario with Potential Master Plan

As outlined above, the below is provided for context and the full Master Plan does not form part of this application.

### 7.1 Traffic Generation

Further to the application of the trip rates described in Section 5.1 to the assumed yield of the entire MSP, below indicative future trip generations have been estimated for the purpose of the modelling:

| - | AM Peak: | $1,266 \mathrm{vph}$ |
| :--- | :--- | ---: |
| - | PM Peak | 931 vph |
| - | Daily: | $13,581 \mathrm{vpd}$ |

### 7.2 Traffic Distribution

The adopted trip distribution for the MSP is summarised in the below Table.

Table 19: Traffic Distribution - Potential Future Master Plan

| Peak Period | Land Use | Total Generation (veh/hr) | \%Inbound | \%outbound | Inbound <br> Movements (veh/hr) | Outbound <br> Movements (veh/hr) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM | Warehouse | 1,203 | 70\% | 30\% | 842 | 361 |
|  | Office | 63 | 70\% | 30\% | 44 | 19 |
| PM | Warehouse | 883 | 30\% | 70\% | 265 | 618 |
|  | Office | 46 | 30\% | 70\% | 14 | 32 |

The resultant MSP traffic distribution to the surrounding road network is shown in Appendix C5 and the 2036 projected background traffic volumes + the assumed future built-form traffic are attached in Appendix C6.

### 7.3 Mid-block Capacity Analysis

The resultant Mid-block capacity analysis is summarised in Table 20.

Table 20: Project Future Mid-block Traffic Volumes

| Road Section | Period | Project Future Case Built Form | Approach Capacity (Nominal capacity) | Volume / capacity (VoC) |
| :---: | :---: | :---: | :---: | :---: |
| Mamre Road north of Southern Link Road | AM | $\begin{gathered} 4,633 \\ \mathrm{NB}=2,049 \\ \mathrm{SB}=2,584 \end{gathered}$ | $\begin{aligned} & \mathrm{NB}=3,000 \\ & \mathrm{SB}=3,000 \end{aligned}$ | $\begin{aligned} & \mathrm{NB}=0.68 \\ & \mathrm{SB}=0.86 \end{aligned}$ |
|  | PM | $\begin{gathered} 4,102 \\ \mathrm{NB}=2,344 \\ \mathrm{SB}=1,758 \end{gathered}$ | $\begin{aligned} & \mathrm{NB}=3,000 \\ & \mathrm{SB}=3,000 \end{aligned}$ | $\begin{aligned} & \mathrm{NB}=0.78 \\ & \mathrm{SB}=0.59 \end{aligned}$ |
| Mamre Road south of Southern Link Road | AM | $\begin{gathered} 4,333 \\ \mathrm{NB}=2,375 \\ \mathrm{SB}=1,958 \end{gathered}$ | $\begin{aligned} & \mathrm{NB}=3,000 \\ & \mathrm{SB}=3,000 \end{aligned}$ | $\begin{aligned} & \mathrm{NB}=0.79 \\ & \mathrm{SB}=0.65 \end{aligned}$ |
|  | PM | $\begin{gathered} 3,808 \\ \mathrm{NB}=1,673 \\ \mathrm{SB}=2,135 \end{gathered}$ | $\begin{aligned} & \mathrm{NB}=3,000 \\ & \mathrm{SB}=3,000 \end{aligned}$ | $\begin{aligned} & \mathrm{NB}=0.56 \\ & \mathrm{SB}=0.71 \end{aligned}$ |
| Southern Link Road East of Mamre Road | AM | $\begin{gathered} 2,577 \\ \mathrm{WB}=781 \\ \mathrm{~EB}=1,796 \end{gathered}$ | $\begin{gathered} W B=2,000 \\ E B=2,000 \end{gathered}$ | $\begin{aligned} \mathrm{WB} & =0.39 \\ \mathrm{~EB} & =0.9 \end{aligned}$ |
|  | PM | $\begin{gathered} 2,745 \\ W B=1,841 \\ E B=905 \end{gathered}$ | $\begin{gathered} W B=2,000 \\ E B=2,000 \end{gathered}$ | $\begin{aligned} & W B=0.92 \\ & E B=0.45 \end{aligned}$ |

Note (1): NB = Northbound direction \& SB = Southbound direction
Note (2): Table 4.4 of RMS Guides does not provide LoS for three lanes. Therefore, VoC has been adopted to assess the capacity.

As reported in above table, the future traffic generated by the assumed development yield at the MSP is well accommodated further to the proposed road upgrades on Mamre Road and Southern Link Road, with spare capacity on all links during both the AM and PM peak periods.

### 7.4 Traffic Impact

The 'impact' of the MSP under the assumed modelling scenario is best considered by comparing changes in modelled performance between 'Future Base Case with Improvements' and 'Project Future Case' scenarios. A summary of the intersection performance under each of these scenarios is provided in Table 21 below.

Table 21: Network Performance - Project Future Case

| Intersection | Scenario | Period | Intersection Delay | Level of Service |
| :---: | :---: | :---: | :---: | :---: |
| Mamre Road/ Southern Link | Future Base Case | AM | 37.0 | C |
|  |  | PM | 36.7 | C |
|  | Project Future Case + the assumed future built form | AM | 47.1 | D |
|  |  | PM | 51.6 | D |
| Mamre Road/ Mamre West Precinct Access | Future Base Case | AM | $\begin{gathered} 9.2 \\ (0.3) \end{gathered}$ | A |
|  |  | PM | $\begin{aligned} & 10.2 \\ & (0.4) \end{aligned}$ | A |
|  | Project Future Case + assumed future built form | AM | $\begin{aligned} & 10.7 \\ & (0.3) \end{aligned}$ | A |
|  |  | PM | $\begin{aligned} & 11.7 \\ & (0.4) \end{aligned}$ | A |
| Mamre Road / James Erskine Drive | Future Base Case | AM | 30.2 | C |
|  |  | PM | 35.1 | C |
|  | Project Future Case + assumed future built form | AM | 32.4 | C |
|  |  | PM | 33.6 | C |
| Mamre Road/ Erskine Park Road | Future Base Case | AM | 24.1 | B |
|  |  | PM | 24.5 | B |
|  | Project Future Case + assumed future built form | AM | 26.1 | B |
|  |  | PM | 31.6 | C |
| Mamre Road / Mandalong Close | Future Base Case | AM | $\begin{gathered} 9.7 \\ (0.5) \end{gathered}$ | A |
|  |  | PM | $\begin{aligned} & 12.5 \\ & (0.5) \end{aligned}$ | A |

## 0584r02v06

Mamre South Precinct; 657 - 703 Mamre Rd, Kemps Creek | SSDA Traffic Impact Assessment

| Intersection | Scenario | Period | Intersection <br> Delay |
| :---: | :---: | :---: | :---: |
|  | AM | Level of Service |  |
|  | Project Future Case + |  |  |
| assumed future built form |  |  |  |$\quad$ PM | 9.8 |
| :---: |

Note: 1) Figures in brackets () reflects average intersection performance for unsignalised intersection.

The SIDRA Network results show that:

- With the exception of the Mamre Road / Southern Link Road intersections, the traffic generation of the MSP has no significant impact on the key Mamre Road intersections, each of which report the same Level of Service as determined under the Base Case analysis.
" Although the LoS for the proposed Mamre Road / Southern Link Road will change from "C" to "D" the average delay increases at the intersection is reported to be in the order of 10 to 15 seconds during the AM and PM peak hours respectively.

In summary, our assessment of the road network providing for the assumed MSP ultimate yield has determined that the likely traffic generated by the MSP can be accommodated further to upgrades of the road network in line with the upgrades required to accommodate (future) background traffic flows without any significant changes in Levels of Service at key intersections.

## 8 Conclusions

### 8.1 General Notes

- Ason Group has been commissioned by Altis Property Partners (Altis) and Frasers Property Australia (FPA) to undertake a Traffic Impact Assessment (TIA) for a proposed warehouse development at 657-753 Mamre Road in Kemps Creek (known as Mamre South Precinct - MSP) within the Penrith City Council Local Government.
- The proposal generally seeks construction of warehouse developments with ancillary office uses as part of a State Significant Development Application for the MSP.


### 8.2 Existing \& Future Conditions (Without Proposal)

- Existing Mamre Road Mid-block traffic volumes during AM and PM peak hours confirm that Mamre Road already operates at capacity; as such, an upgrade of Mamre Road to provide three lanes in each direction may need to be investigated sooner than envisaged based on current planning / timing.
- The SIDRA analysis undertaken for the key intersections in the vicinity of the MSP for the Baseline (May 2018) confirm the intersection of Mamre Road / Bakers Lane currently operate at a LoS 'F' during the PM peak hour with a modelled average intersection delay of 139.5 seconds.
- Mamre Road in this vicinity is proposed to be upgraded to two (2) lanes in each direction as part of the RMS Mamre Road Upgrade project.
- The Future Base Case intersection analysis included in this TIA adopts the future intersection upgrades envisaged by the Mamre Road Upgrade document prepared by Road and Maritime Services (RMS).
- Future year (2036) traffic volumes from the strategic EMME model were obtained from RMS during the course of this study.
- The Mid-block capacity assessment and the SIDRA analysis undertaken for the Future Base Case with RMS identified upgrades suggest that Mamre Road will operate at and, in some instances, in excess of capacity in the future, and that key intersections will not achieve the desirable target Level of Services, with resulting capacity constraints and queue distance issues.
- This situation suggests that the identified road and intersection upgrades envisaged by RMS may not be sufficient to accommodate the regional traffic growth regardless of the MSP proposal.
- Notwithstanding, it is noted that the Mamre Road Upgrade includes a wide median treatment to accommodate future widening in the future.
- Accordingly, this TIA has undertaken a review of future network performance on the basis that this additional widening (to 3 lanes in each direction) is required to support future background traffic volumes even without the Project.
- The results of the SIDRA analysis show that the upgrade of Mamre Road to three (3) lanes in each direction will significantly improve network performance and satisfactorily accommodate future traffic demands. Therefore, this scenario has been considered as the Project Future Baseline.


### 8.3 SSDA Assessments

- It is proposed that SSDA will be accessed via the western leg of the existing Mamre Road / Bakers Lane signalised intersection.
- The SSDA is anticipated to generate approximately $405 \mathrm{veh} / \mathrm{hr}$ during the AM and $297 \mathrm{veh} / \mathrm{hr}$ during the PM peak hour. The estimated daily traffic generation of the proposed SSDA is 4,322 veh/day.
- With reference to the SIDRA Network results for the proposal, it is concluded that the proposed SSDA traffic volumes can be accommodated through the existing intersections in the locality and that the proposed indicative signal layout envisaged for the Mamre Road / Bakers Lane can cater the additional traffic volumes.
- A review of the parking requirements for the SSDA confirms that each land parcel will generally provide sufficient car parking spaces to satisfy the RMS parking requirements.


### 8.4 Indicative Future Master Plan (context only - not part of this application)

- To allow for the future modelling assessment we have assumed indicative development yield for the entire MSP site. Accordingly, the traffic generation of the indicative built form has been estimated to be 1,266 and 931 veh/hr during the road network AM and PM peak hours respectively. The likely daily traffic generation of the future possible built form is estimated to be 13,518 veh/day.
- Mid-block capacity analysis for the 'Project Future Baseline' was then expanded to consider the impact of this built form. The outcome of the assessment confirmed that the proposed traffic from the built form can be accommodated within the recommended future upgrades.
- The results of the SIDRA analysis confirm that the indicative future built form traffic can be accommodated by the proposed future upgrades of the key Mamre Road intersections.
- In summary, our assessment of the road network providing for the MSP has determined that the traffic generated by the MSP can be accommodated subject to upgrades of the road network in line with the upgrades required to accommodate (future) background traffic flows without any significant changes in Levels of Service at key intersections.


## Appendix A <br> SEARs

Mr Andrew Gowan
Director, Willowtree Planning
Suite 4, Level 7, 100 Walker Street
NORTH SYDNEY NSW 2060
Email: acowan@willowtp.com.au

## Dear Mr Cowan

## State Significant Development - Planning Secretary's Environmental Assessment Requirements Kemps Creek Warehouse and Logistics Hub (SSD 9522)

Please find attached the Planning Secretary's Environmental Assessment Requirements (SEARs) for the preparation of an Environmental Impact Statement (EIS) for the above-mentioned development. Attachment 1 provides guidelines which may assist in the preparation of the EIS.

The attached SEARs have been prepared in consultation with the relevant government agencies and Penrith City Council (see Attachment 2). The SEARs are based on the scoping report prepared by Willowtree Planning, dated 15 August 2018.

Please note the Planning Secretary may alter the SEARs at any time. You must consult further with the Department if you do not lodge a development application (DA) and EIS for the development within two years of the date of issue of these SEARs.

I wish to emphasise the importance of effective and genuine community consultation and the need for the proposal to proactively respond to the community's concerns. A comprehensive, detailed and genuine community consultation and engagement process must be undertaken during the preparation of the EIS. This process must ensure the community is informed of the development and engaged with issues of concern to it. Sufficient information must be provided to the community to enable a good understanding of the development and any potential impacts.

If the proposal is likely to have a significant impact on matters of National Environmental Significance, it may require an approval under the Commonwealth Environment Protection and Biodiversity Conservation Act 1999 (EPBC Act). If an EPBC Act approval is required, please advise accordingly, as the Commonwealth approval process may be integrated into the NSW approval process, and supplementary SEARs may need to be issued.

Please contact the Department at least two weeks before you lodge the EIS and any associated documentation for the development. This will enable the Department to confirm:

- the applicable fee (see Division 1AA, Part 15 of the Environmental Planning and Assessment Regulation 2000)
- consultation and public exhibition arrangements.

If you have any enquiries, please contact Bianca Thornton on the details above.

## Yours sincerely



## Planning Secretary's Environmental Assessment Requirements

Section 4.12(8) of the Environmental Planning and Assessment Act 1979 Schedule 2 of the Environmental Planning and Assessment Regulation 2000

| Application Number | SSD 9522 |
| :---: | :---: |
| Project Name | Kemps Creek Warehouse and Logistics Hub |
| Development | Establishment of a warehouse and logistics hub, comprising: <br> - site-wide earthworks, infrastructure and internal road network <br> - construction and operation of 11 warehouses comprising 165,186 square metres ( $\mathrm{m}^{2}$ ) of floor space ( $152,485 \mathrm{~m}^{2}$ warehouse and $7,700 \mathrm{~m}^{2}$ office) <br> - 816 parking spaces <br> - subdivision. |
| Location | 657-769 Mamre Road, Kemps Creek in the Penrith Local Government Area (Lot 34 DP1118173, Lot X DP421633, Lot 1 DP1018318, Lot Y DP421633 and Lot 22 DP258414) |
| Applicant | Frasers Property Industrial Construction Pty Ltd and Altis Property Partners Pty Ltd |
| Date of Issue | 14 September 2018 |
| General Requirements | The environmental impact statement (EIS) must be prepared in accordance with, and meet the minimum requirements of, clauses 6 and 7 of Schedule 2 of the Environmental Planning and Assessment Regulation 2000 (the Regulation). In addition, the EIS must include: <br> - a detailed description of the development, including: <br> - the need for the proposed development <br> - justification for the proposed development <br> - likely staging of the development <br> - likely interactions between the development and existing, approved and proposed operations in the vicinity of the site <br> - plans of any proposed building works <br> - consideration of all relevant environmental planning instruments, including identification and justification of any inconsistencies with these instruments <br> - a risk assessment of the potential environmental impacts of the development, identifying the key issues for further assessment <br> - a detailed assessment of the key issues specified below, and any other significant issues identified in this risk assessment, which includes: <br> - a description of the existing environment, using sufficient baseline data <br> - an assessment of the potential impacts of all stages of the development, including any cumulative impacts, taking into consideration relevant guidelines, policies, plans and statutes <br> - a description of the measures that would be implemented to avoid, minimise, mitigate and if necessary, offset the potential impacts of the development, including proposals for adaptive management and/ or contingency plans to manage significant risks to the environment <br> a consolidated summary of all the proposed environmental management and monitoring measures, highlighting commitments included in the EIS. <br> The EIS must also be accompanied by a report from a qualified quantity surveyor providing: <br> - a detailed calculation of the capital investment value (CIV) (as defined in clause 3 of the Regulation) of the proposal, including details of all assumptions and |


|  | prepared on company letterhead and indicate applicable GST component of the CIV <br> - an estimate of jobs that will be created during the construction and operational phases of the proposed development <br> - certification that the information provided is accurate at the date of preparation. |
| :---: | :---: |
| Key issues | The EIS must address the following specific matters: <br> - Statutory and Strategic Context - including: <br> - detailed justification that the proposed land use is permissible, taking into consideration the State Environmental Planning Policy (Western Sydney Employment Area) 2009 <br> - details of any proposed consolidation or subdivision of land <br> - demonstration that the proposal is consistent with all relevant planning strategies, environmental planning instruments, adopted precinct plans, draft district plan(s) and adopted management plans and justification for any inconsistencies. The following must be addressed: <br> - State Environmental Planning Policy (Western Sydney Employment Area) 2009 <br> - A Metropolis of Three Cities <br> - Western City District Plan <br> - Western Sydney Aerotropolis - Land Use and Infrastructure Implementation Plan - Stage 1: Initial Precincts Western Sydney Freight Line corridor. <br> - Planning Agreement/Development Contributions - demonstration that satisfactory arrangements have been or would be made to provide, or contribute to the provision of, necessary local and regional infrastructure required to support the development. <br> - Suitability of the Site - including: <br> - an analysis of site constraints, such as flooding impacts and future road and road corridors <br> - a detailed justification that the site is suitable for the scale of the proposal and any constraints identified, having regard to the site's surrounds and the potential visual impact of the development. <br> - Community and Stakeholder Engagement - including: <br> - a detailed community and stakeholder participation strategy which identifies who in the community has been consulted and a justification for their selection, other stakeholders consulted and the form(s) of consultation, including a justification for this approach <br> - a report on the results of the implementation of the strategy including issues raised by the community and surrounding land owners and occupiers that may be impacted by the proposal <br> - details of how issues raised during community and stakeholder consultation have been addressed and whether they have resulted in changes to the proposal <br> - details of the proposed approach to future community and stakeholder engagement based on the results of consultation. <br> - Urban Design and Visual - including: <br> - a visual impact assessment (including photomontages and perspectives) of the development layout and design (buildings and storage areas), including height, colour, scale, building materials and finishes, signage and lighting, having regard to surrounding residential receivers and clause 23 of the State Environmental Planning Policy (Western Sydney Employment Area) 2009, particularly in terms of potential impacts on: <br> - nearby public and private receivers <br> - significant vantage points in the broader public domain including Mamre Road <br> - consideration of the layout and design of the development having regard to the surrounding vehicular, pedestrian and cycling networks |

- detailed plans showing suitable landscaping which incorporates endemic species
- a design report that establishes design guidelines and development parameters, and includes diagrams, illustrations and drawings to clarify the design intent of the proposal and which clearly demonstrates how design quality will be achieved in accordance with Clause 31 Design Principles of the State Environmental Planning Policy (Western Sydney Employment Area) 2009
Traffic and Transport - including:
- a quantitative Traffic Impact Assessment prepared in accordance with relevant Penrith City Council, Austroads and Roads and Maritime Services guidelines
- details of all daily and peak traffic and transport movements likely to be generated by the development (vehicle type, public transport) during construction and indicative operation
- impacts on the safety and capacity of the surrounding road network and access points, using SIDRA or similar modelling, to assess impacts from current traffic counts and cumulative traffic from existing and proposed development
- demonstrate that sufficient loading/unloading, car parking and pedestrian and cyclist facilities have been provided for the development
- details and a justification of access to, from and within the site (vehicular and pedestrian)
- details of road upgrades, new roads or access points required for the development, if necessary
- consideration of the western connection of the Southern Link Road and road widening requirements for Mamre Road, in consultation with RMS
- consideration of the proposed Western Sydney Freight Line, including the width of the corridor and how this will be considered in the layout of the proposal, in consultation with TfNSW
- details of how the proposal would allow connection to future land uses to the south of the site.
- Flooding - a detailed hydrological and hydraulic assessment which includes the following:
- a comprehensive assessment of the impact of flooding on the development for the full range of flood events up to the probable maximum flood. This assessment should address any relevant provisions of the NSW Floodplain Development Manual (2005) including the potential effects of climate change, sea level rise and an increase in rainfall intensity
- consideration of current flooding behaviour and impacts, including on flood detention areas, how flood behaviour and impacts will change due to the proposal and how these changes will be mitigated
- assessment of the impact of the development on flood behaviour (i.e., levels, velocities and duration of flooding) and on adjacent, downstream and upstream areas
- detail proposed floor levels for all proposed habitable structures on the site having considered the full range of flood events up to the probable maximum flood
- detail an emergency response plan for the site, which includes consideration of a flood-free access to or from the development site in extreme flood events.
- Soils and Water - including:
- a description of how the proposal takes into consideration the South Creek corridor strategy and the land use vision for the South Creek Precinct, in consultation with Infrastructure NSW and the Greater Sydney Commission
- measures to protect the Warragamba Pipelines corridor from any works or activities associated with the development

|  | - details of how access to the Warragamba Piplines corridor would be maintained, in consultation with WaterNSW <br> - a description of the water demands and a breakdown of water supplies, including a detailed site water balance <br> - identification of any water licensing requirements under the Water Act 1912 or Water Management Act 2000 <br> - details of proposed erosion and sediment controls during construction <br> - a description of the surface and stormwater management system designed in accordance with Penrith City Council's Water Sensitive Urban Design Policy, including drainage design, on site detention, and measures to treat or re-use water <br> - characterisation of the nature and extent of any contamination on the site and surrounding area <br> - an assessment of potential impacts on surface and groundwater resources, drainage patterns, soil (stability, salinity and acid sulfate soils), related infrastructure, watercourses and riparian land and proposed mitigation, management and monitoring measures. <br> Biodiversity - including: <br> - an assessment of the proposal's biodiversity impacts in accordance with the Biodiversity Conservation Act 2016, including the preparation of a Biodiversity Development Assessment Report (BDAR) where required under the Act, except where a waiver for preparation of a BDAR has been granted <br> - describe how impacts upon critical vegetation and endangered species on site will be avoided and minimised. <br> Infrastructure Requirements - including: <br> - a detailed written and/or geographical description of infrastructure required on the site <br> - identification of any infrastructure upgrades required off-site to facilitate the development, and describe any arrangements to ensure that the upgrades will be implemented in a timely manner and maintained <br> - an infrastructure delivery and staging plan, including a description of how infrastructure on and off-site will be co-ordinated and funded to ensure it is in place prior to the commencement of construction <br> - an assessment of the impacts of the development (construction and operation) on existing infrastructure surrounding the site. <br> - Heritage - including: <br> - an Aboriginal Cultural Heritage Assessment Report prepared in consultation with Aboriginal people and in accordance with Office of Environment and Heritage guidelines <br> - an assessment of European Heritage including potential impacts on the surrounding site and surrounding area, including any built landscape items, conservation areas, views and settings. <br> - Noise and Vibration- including: <br> - a quantitative noise and vibration impact assessment undertaken by a suitably qualified person in accordance with the relevant Environment Protection Authority guidelines and including an assessment of nearby sensitive receivers <br> - cumulative impacts of other developments <br> - details of proposed mitigation, management and monitoring measures. <br> - Hazards and Risk - including: <br> - a preliminary risk screening completed in accordance with State Environmental Planning Policy No. 33 - Hazardous and Offensive Development and Applying SEPP 33 (DoP, 2011), with a clear indication of class, quantity and location of all dangerous goods and hazardous materials associated with the development. Should preliminary screening indicate that the project is "potentially hazardous" a preliminary hazard analysis (PHA) must be prepared in accordance with Hazardous Industry Planning Advisory |
| :---: | :---: |


|  | Paper No. 6 - Guidelines for Hazard Analysis (DoP, 2011) and Multi-Level Risk Assessment (DoP, 2011). <br> - Bushfire - including: <br> - details of the storage of any flammable materials <br> - an assessment against the requirements of Planning for Bushfire Protection 2006, particularly access and provision of water supply for firefighting purposes <br> - a description of measures to ensure the proposal will not increase the bushfire risk to adjoining lands. <br> - Waste - including: <br> - details of the quantities and classification of all waste streams to be generated on site during construction and operation <br> - details of waste storage, handling and disposal during construction and operation <br> - details of the measures that would be implemented to ensure that the development is consistent with the aims, objectives and guidance in the NSW Waste Avoidance and Resource Recovery Strategy 2014-2021. <br> - Air Quality - including: <br> - an assessment of the air quality impacts (including dust) during construction and operation of the development, in accordance with the relevant Environment Protection Authority guidelines <br> - details of proposed mitigation, management and monitoring measures. <br> - Social - including the preparation of a social impact assessment, which: <br> - identifies and analyses the potential social impacts of the development, from the points of view of the affected community/ies and other relevant stakeholders, i.e. how they expect to experience the project <br> - considers how potential environmental changes in the locality may affect people's: way of life; community; access to and use of infrastructure, services, and facilities; culture; health and wellbeing; surroundings; personal and property rights; decision-making systems; and fears and aspirations, as relevant and considering how different groups may be disproportionately affected <br> - assesses the significance of positive, negative, and cumulative social impacts considering likelihood, extent, duration, severity/scale, sensitivity/importance, and level of concern/interest <br> - includes mitigation measures for likely negative social impacts, and any proposed enhancement measures <br> - details how social impacts will be adaptively monitored and managed over time. |
| :---: | :---: |
| Plans and Documents | The EIS must include all relevant plans, architectural drawings, diagrams and relevant documentation required under Schedule 1 of the Regulation. You should provide these as part of the EIS rather than as separate documents. |
| Consultation | During the preparation of the EIS, you must consult with the relevant local, State or Commonwealth Government authorities, service providers, community groups and affected landowners. <br> In particular you must consult with: <br> - Penrith City Council <br> - Greater Sydney Commission <br> - Roads and Maritime Services <br> - Transport for NSW <br> - Office of Environment and Heritage <br> - Environment Protection Authority <br> - Fire and Rescue NSW <br> - Rural Fire Service <br> - Department of Industry - Crown Lands and Water <br> - Sydney Water |


|  | - WaterNSW <br> e <br> a <br> surrounding local residents and stakeholders <br> any other public transport or community service providers. <br> The EIS must describe the consultation process and the issues raised, and identify <br> where the design of the development has been amended in response to these <br> issues. Where amendments have not been made to address an issue, a short <br> explanation should be provided. |
| :--- | :--- |
| Further <br> consultation <br> after 2 years | If you do not lodge a Development Application and EIS for the development within <br> 2 years of the issue date of these SEARs, you must consult further with the <br> Secretary in relation to the preparation of the EIS. |
| References | The assessment of the key issues listed above must take into account relevant <br> guidelines, policies, and plans as identified. While not exhaustive, the following <br> attachment contains a list of some of the guidelines, policies, and plans that may <br> be relevant to the environmental assessment of this proposal. |

## Appendix B

## Reduced Architectural Plan



## Appendix C

## Traffic Volumes

## Appendix C1

## Existing Traffic Volumes



## Appendix C2

## 2036 Projected Background Traffic



## Appendix C3

## SSDA Traffic Only



## Appendix C4

## Existing + SSDA Traffic



## Appendix C5

## Future Built Form Traffic Only



## Appendix C6

2036 Background Traffic + Future Built Form


## Appendix D

## SIDRA Outputs and Results

## Appendix D1

## Existing Baseline SIDRA Output

## SITE LAYOUT

## Site: 104 [[Existing] Mamre Road x Bakers Lane_AM]

Mamre Road x Bakers Lane
2018 Existing
Signals - Fixed Time Coordinated


SIDRA INTERSECTION 7.0 | Copyright © 2000-2017 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: ASON GROUP PTY LTD | Created: Thursday, 24 May 2018 8:47:14 AM
Project: C: \Users\Alireza Rasouli\Ason Group\Ason Group Team Site - 0584\Projects\Modelling\SIDRAIExisting - Base Case 2018\AG0584m01
Mamre_Existing.sip7

## Mamre Road x Bakers Lane

2018 Existing
Signals - Fixed Time Coordinated Cycle Time $=130$ seconds (User-Given Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | $\begin{gathered} \text { Demand Flows } \\ \text { Total HV } \\ \text { veh/h } \end{gathered}$ |  | Arrival FlowsTotal HV |  | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back of Queue Vehicles Distance |  | Prop. Queued | Effective Average |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  | \% |  |  |  |  | m |  | Rate | km/h |
| South: Mamre Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 1 | 0.0 | 1 | 0.0 | 0.707 | 23.5 | LOS B | 29.7 | 229.7 | 0.70 | 0.64 | 51.1 |
| 2 | T1 | 743 | 12.2 | 743 | 12.2 | 0.707 | 16.6 | LOS B | 29.7 | 229.7 | 0.70 | 0.64 | 46.5 |
| 3 | R2 | 80 | 0.0 | 80 | 0.0 | 0.800 | 80.2 | LOS F | 5.5 | 38.8 | 1.00 | 0.86 | 26.2 |
| Appr | ach | 824 | 11.0 | 824 | 11.0 | 0.800 | 22.8 | LOS B | 29.7 | 229.7 | 0.72 | 0.66 | 41.2 |
| East: Bakers Lane ( 440 m ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 43 | 0.0 | 43 | 0.0 | 0.060 | 32.1 | LOS C | 1.7 | 11.8 | 0.66 | 0.70 | 40.4 |
| 5 | T1 | 1 | 0.0 | 1 | 0.0 | 0.789 | 47.5 | LOS D | 22.3 | 156.4 | 0.92 | 0.87 | 31.1 |
| 6 | R2 | 392 | 0.3 | 392 | 0.3 | 0.789 | 53.0 | LOS D | 22.3 | 156.4 | 0.92 | 0.87 | 20.4 |
| Appr | ach | 436 | 0.2 | 436 | 0.2 | 0.789 | 50.9 | LOS D | 22.3 | 156.4 | 0.90 | 0.85 | 22.5 |
| North: Mamre Road (750m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 627 | 0.2 | 624 | 0.2 | 0.394 | 9.1 | LOS A | 8.5 | 59.4 | 0.24 | 0.70 | 60.5 |
| 8 | T1 | 598 | 18.3 | 595 | 18.4 | 0.909 | 45.1 | LOS D | 36.6 | 296.3 | 0.79 | 0.87 | 44.6 |
| 9 | R2 | 3 | 0.0 | 3 | 0.0 | 0.909 | 51.7 | LOS D | 36.6 | 296.3 | 0.79 | 0.87 | 40.6 |
| Appr | ach | 1228 | 9.0 | $1222^{\mathrm{N} 1}$ | 9.0 | 0.909 | 26.7 | LOS B | 36.6 | 296.3 | 0.51 | 0.78 | 51.3 |
| West: Bakers lane |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 3 | 0.0 | 3 | 0.0 | 0.003 | 5.5 | LOS A | 0.0 | 0.0 | 0.00 | 0.47 | 52.5 |
| 11 | T1 | 1 | 0.0 | 1 | 0.0 | 0.003 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.47 | 55.7 |
| 12 | R2 | 1 | 0.0 | 1 | 0.0 | 0.003 | 5.5 | LOSA | 0.0 | 0.0 | 0.00 | 0.47 | 54.2 |
| Approach |  | 5 | 0.0 | 5 | 0.0 | 0.003 | 4.4 | LOS A | 0.0 | 0.0 | 0.00 | 0.47 | 53.8 |
| All Ve | icles | 2494 | 8.1 | $2487^{\mathrm{N} 1}$ | 8.1 | 0.909 | 29.6 | LOS C | 36.6 | 296.3 | 0.65 | 0.75 | 43.5 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement. Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 0.0 \% Number of Iterations: 7 (maximum specified: 10)

N1 Arrival Flow value is reduced due to capacity constraint at oversaturated upstream lanes.

[^1]MOVEMENT SUMMARY
Site: 104 [[Existing] Mamre Road x Bakers Lane_PM]

Mamre Road x Bakers Lane
2018 Existing
Signals - Fixed Time Coordinated Cycle Time = 130 seconds (User-Given Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Demand Total veh/h | $\begin{aligned} & \text { Flows } \\ & \text { HV } \\ & \% \end{aligned}$ | Arriva Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Mamre Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 1 | 0.0 | 1 | 0.0 | 0.792 | 35.8 | LOS C | 35.4 | 274.4 | 0.89 | 0.81 | 43.6 |
| 2 | T1 | 687 | 12.4 | 687 | 12.4 | 0.792 | 28.8 | LOS C | 35.4 | 274.4 | 0.89 | 0.81 | 35.6 |
| 3 | R2 | 26 | 0.0 | 26 | 0.0 | 0.307 | 75.8 | LOS F | 1.7 | 12.1 | 1.00 | 0.71 | 27.1 |
| Appro |  | 715 | 11.9 | 715 | 11.9 | 0.792 | 30.6 | LOS C | 35.4 | 274.4 | 0.89 | 0.80 | 34.9 |
| East: Bakers Lane (440m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 52 | 0.0 | 52 | 0.0 | 0.055 | 22.5 | LOS B | 1.6 | 11.3 | 0.53 | 0.68 | 45.5 |
| 5 | T1 | 1 | 0.0 | 1 | 0.0 | 0.897 | 45.5 | LOS D | 32.6 | 229.0 | 0.91 | 0.93 | 31.7 |
| 6 | R2 | 513 | 0.4 | 513 | 0.4 | 0.897 | 51.0 | LOS D | 32.6 | 229.0 | 0.91 | 0.93 | 20.9 |
| Appro |  | 565 | 0.4 | 565 | 0.4 | 0.897 | 48.4 | LOS D | 32.6 | 229.0 | 0.88 | 0.91 | 23.1 |
| North: Mamre Road (750m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 180 | 1.2 | 180 | 1.2 | 0.113 | 8.4 | LOS A | 1.7 | 12.0 | 0.16 | 0.67 | 61.1 |
| 8 | T1 | 857 | 12.9 | 857 | 12.9 | 1.287 | 318.5 | LOS F | 145.1 | 1127.5 | 1.00 | 2.17 | 11.8 |
| 9 | R2 | 1 | 0.0 | 1 | 0.0 | 1.287 | 325.1 | LOS F | 145.1 | 1127.5 | 1.00 | 2.17 | 11.5 |
| Appro |  | 1038 | 10.9 | 1038 | 10.9 | 1.287 | 264.7 | LOS F | 145.1 | 1127.5 | 0.85 | 1.91 | 13.7 |
| West: Bakers lane |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 1 | 0.0 | 1 | 0.0 | 0.002 | 5.5 | LOS A | 0.0 | 0.0 | 0.00 | 0.45 | 52.9 |
| 11 | T1 | 1 | 0.0 | 1 | 0.0 | 0.002 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.45 | 56.0 |
| 12 | R2 | 2 | 0.0 | 2 | 0.0 | 0.002 | 5.5 | LOS A | 0.0 | 0.0 | 0.00 | 0.45 | 54.4 |
| Approach |  | 4 | 0.0 | 4 | 0.0 | 0.002 | 4.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.45 | 54.6 |
| All Vehicles |  | 2322 | 8.6 | 2322 | 8.6 | 1.287 | 139.5 | LOS F | 145.1 | 1127.5 | 0.87 | 1.32 | 16.6 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 2.0 \%
Number of Iterations: 10 (maximum specified: 10)

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Project: C:\Users\Alireza Rasouli\Ason Group\Ason Group Team Site - 0584\Projects\Modelling\SIDRAIExisting - Base Case 2018\AG0584m01 Mamre_Existing.sip7

## SITE LAYOUT

## Site: 103 [[Existing] Mamre Road x James Erskine Drive_AM]

Mamre Road x James Erskine Drive
2018 Existing
Signals - Fixed Time Isolated


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Project: C:\Users\Alireza Rasouli\Ason Group\Ason Group Team Site - 0584\Projects\Modelling\SIDRA\Existing - Base Case 2018\AG0584m01
Mamre Existing.sip7

## MOVEMENT SUMMARY

Site: 103 [[Existing] Mamre Road x James Erskine

Mamre Road x James Erskine Drive
2018 Existing
Signals - Fixed Time Isolated Cycle Time $=60$ seconds (User-Given Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Demand Total veh/h | Flows HV \% | Arrival <br> Total <br> veh/h | Flows HV \% | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles <br> veh | of Queue Distance | Prop. Queued | Effective Stop Rate per veh | verage speed <br> km/h |
| South: Mamre Road (520m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | T1 | 997 | 7.1 | 997 | 7.1 | 0.542 | 4.3 | LOS A | 10.0 | 74.3 | 0.48 | 0.43 | 67.8 |
| 3 | R2 | 86 | 22.0 | 86 | 22.0 | 0.538 | 37.8 | LOS C | 2.7 | 22.1 | 0.99 | 0.78 | 33.7 |
| Appro | ach | 1083 | 8.3 | 1083 | 8.3 | 0.542 | 7.0 | LOS A | 10.0 | 74.3 | 0.52 | 0.46 | 61.5 |
| East: James Erskine Drive (170m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 33 | 54.8 | 33 | 54.8 | 0.183 | 12.9 | LOS A | 0.8 | 8.5 | 0.71 | 0.70 | 26.2 |
| 6 | R2 | 87 | 54.2 | 87 | 54.2 | 0.435 | 27.7 | LOS B | 1.8 | 18.0 | 0.89 | 0.73 | 16.7 |
| Appr |  | 120 | 54.4 | 120 | 54.4 | 0.435 | 23.7 | LOS B | 1.8 | 18.0 | 0.84 | 0.72 | 18.5 |
| North: Mamre Road (300m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 276 | 17.9 | 274 | 18.0 | 0.222 | 8.9 | LOS A | 1.5 | 12.2 | 0.32 | 0.68 | 49.7 |
| 8 | T1 | 1213 | 7.4 | 1206 | 7.4 | 0.737 | 12.9 | LOS A | 16.8 | 125.0 | 0.80 | 0.73 | 42.0 |
| Approach |  | 1488 | 9.3 | $1480{ }^{\mathrm{N} 1}$ | 9.4 | 0.737 | 12.1 | LOS A | 16.8 | 125.0 | 0.71 | 0.72 | 43.8 |
| All Vehicles |  | 2692 | 10.9 | $2683{ }^{\mathrm{N} 1}$ | 10.9 | 0.737 | 10.6 | LOS A | 16.8 | 125.0 | 0.64 | 0.61 | 50.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 0.0 \% Number of Iterations: 7 (maximum specified: 10)

N1 Arrival Flow value is reduced due to capacity constraint at oversaturated upstream lanes.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Back <br> Pedestrian <br> ped | of Queue Distance $\square$ | Prop. Queued | Effective <br> Stop Rate per ped |
| P1 | South Full Crossing | 1 | 24.3 | LOS C | 0.0 | 0.0 | 0.90 | 0.90 |
| P2 | East Full Crossing | 1 | 13.3 | LOS B | 0.0 | 0.0 | 0.67 | 0.67 |
| All Pedestrians |  | 2 | 18.8 | LOS B |  |  | 0.78 | 0.78 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

## MOVEMENT SUMMARY

Site: 103 [[Existing] Mamre Road x James Erskine Drive_PM]

Mamre Road x James Erskine Drive
2018 Existing
Signals - Fixed Time Isolated Cycle Time $=80$ seconds (User-Given Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Demand Total veh/h | $\begin{gathered} =\text { lows } \\ \text { HV } \\ \% \end{gathered}$ | Arriva Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Mamre Road (520m) mer mill |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | T1 | 906 | 9.6 | 906 | 9.6 | 0.560 | 8.6 | LOS A | 14.4 | 109.2 | 0.58 | 0.51 | 59.0 |
| 3 | R2 | 25 | 58.3 | 25 | 58.3 | 0.257 | 49.2 | LOS D | 1.0 | 10.7 | 0.98 | 0.72 | 29.2 |
| Appr |  | 932 | 11.0 | 932 | 11.0 | 0.560 | 9.7 | LOS A | 14.4 | 109.2 | 0.59 | 0.52 | 56.9 |
| East: James Erskine Drive (170m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 101 | 8.3 | 101 | 8.3 | 0.254 | 11.8 | LOS A | 2.7 | 20.5 | 0.62 | 0.70 | 27.0 |
| 6 | R2 | 285 | 17.3 | 285 | 17.3 | 0.603 | 30.3 | LOS C | 8.0 | 64.4 | 0.87 | 0.79 | 15.5 |
| Appr | ach | 386 | 15.0 | 386 | 15.0 | 0.603 | 25.5 | LOS B | 8.0 | 64.4 | 0.81 | 0.77 | 17.5 |
| North: Mamre Road ( 300 m ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 133 | 56.3 | 133 | 56.3 | 0.121 | 8.9 | LOS A | 0.5 | 5.4 | 0.19 | 0.64 | 49.5 |
| 8 | T1 | 1022 | 15.1 | 1022 | 15.1 | 0.689 | 16.9 | LOS B | 17.8 | 140.9 | 0.80 | 0.71 | 36.5 |
| Approach |  | 1155 | 19.9 | 1155 | 19.9 | 0.689 | 16.0 | LOS B | 17.8 | 140.9 | 0.73 | 0.70 | 38.2 |
| All Vehicles |  | 2473 | 15.8 | 2473 | 15.8 | 0.689 | 15.1 | LOS B | 17.8 | 140.9 | 0.69 | 0.64 | 41.6 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement. Intersection and Approach LOS values are based on average delay for all vehicle movements. SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 2.0 \%
Number of Iterations: 10 (maximum specified: 10)

Movement Performance - Pedestrians

| Mov ID | Description | Demand | Average | Level of | Average Ba | f Queue | Prop. | Effective |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Flow ped/h | Delay sec | Service | Pedestrian ped | Distance m | Queued | Stop Rate per ped |
| P1 | South Full Crossing | 1 | 34.2 | LOS D | 0.0 | 0.0 | 0.93 | 0.93 |
| P2 | East Full Crossing | 1 | 16.9 | LOS B | 0.0 | 0.0 | 0.65 | 0.65 |
| All Pedestrians |  | 2 | 25.6 | LOS C |  |  | 0.79 | 0.79 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

## SITE LAYOUT

Site: 102 [[Existing] Mamre Road x Erskine Park Road_AM]
Mamre Road x Erskine Park Road
2018 Existing
Signals - Fixed Time Isolated


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Project: C:\Users\Alireza Rasouli\Ason Group\Ason Group Team Site - 0584\Projects\Modelling\SIDRAIExisting - Base Case 2018\AG0584m01
Mamre_Existing.sip7

## MOVEMENT SUMMARY

Site: 102 [[Existing] Mamre Road x Erskine Park Road_AM]
Mamre Road x Erskine Park Road
2018 Existing
Signals - Fixed Time Isolated Cycle Time = 80 seconds (User-Given Cycle Time)

| Mov OD <br> ID Mov | Demand Flows Arrival Flows Total HV Total HV |  |  |  | Deg. <br> Satn <br> v/c | Average Delay sec | Level of Service | 95\% Back of Queue Vehicles Distance |  | Prop. Queued | Effective Average Stop Speed |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | veh/h | \% | veh/h | \% |  |  |  | veh | m |  | per veh | km/h |
| South: Mamre Road (300m) 0 |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 518 | 9.8 | 518 | 9.8 | 0.396 | 4.9 | LOS A | 8.0 | 60.8 | 0.43 | 0.38 | 59.5 |
| 3 R 2 | 557 | 13.4 | 557 | 13.4 | 0.773 | 43.5 | LOS D | 11.3 | 88.4 | 1.00 | 0.89 | 35.5 |
| Approach | 1075 | 11.7 | 1075 | 11.7 | 0.773 | 24.9 | LOS B | 11.3 | 88.4 | 0.73 | 0.65 | 39.4 |
| East: Erskine Park Road (590m) |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 594 | 13.1 | 594 | 13.1 | 0.827 | 35.1 | LOS C | 23.5 | 183.3 | 0.95 | 0.93 | 35.1 |
| 6 R2 | 187 | 14.0 | 187 | 14.0 | 0.811 | 49.8 | LOS D | 8.1 | 63.6 | 1.00 | 0.91 | 28.4 |
| Approach | 781 | 13.3 | 781 | 13.3 | 0.827 | 38.6 | LOS C | 23.5 | 183.3 | 0.96 | 0.92 | 33.2 |
| North: Mamre Road (200m) |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 553 | 4.4 | 547 | 4.4 | 0.712 | 13.6 | LOS A | 17.6 | 128.6 | 0.71 | 0.77 | 56.3 |
| 8 T1 | 868 | 6.4 | 860 | 6.4 | 0.712 | 15.7 | LOS B | 18.4 | 135.8 | 0.82 | 0.78 | 28.8 |
| Approach | 1421 | 5.6 | $1407{ }^{\text {N1 }}$ | 5.6 | 0.712 | 14.9 | LOS B | 18.4 | 135.8 | 0.78 | 0.77 | 43.9 |
| All Vehicles | 3277 | 9.4 | $3263{ }^{\text {N1 }}$ | 9.5 | 0.827 | 23.9 | LOS B | 23.5 | 183.3 | 0.81 | 0.77 | 38.9 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 0.0 \%
Number of Iterations: 7 (maximum specified: 10)
N1 Arrival Flow value is reduced due to capacity constraint at oversaturated upstream lanes.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Bac Pedestrian ped | Queue Distance m | Prop. Queued | Effective Stop Rate per ped |
| P1 | South Full Crossing | 1 | 34.2 | LOS D | 0.0 | 0.0 | 0.93 | 0.93 |
| P2 | East Full Crossing | 1 | 20.3 | LOS C | 0.0 | 0.0 | 0.71 | 0.71 |
| P3 | North Full Crossing | 1 | 34.2 | LOS D | 0.0 | 0.0 | 0.93 | 0.93 |
| All Pedestrians |  | 3 | 29.6 | LOS C |  |  | 0.85 | 0.85 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

[^2]
## MOVEMENT SUMMARY

Site: 102 [[Existing] Mamre Road x Erskine Park Road_PM]
审审 Network: N101 [Existing -

Mamre Road x Erskine Park Road
2018 Existing
Signals - Fixed Time Isolated Cycle Time = 100 seconds (User-Given Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Arriva Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Mamre Road (300m) mill |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | T1 | 598 | 8.5 | 598 | 8.5 | 0.588 | 16.0 | LOS B | 19.2 | 144.4 | 0.72 | 0.64 | 37.7 |
| 3 | R2 | 643 | 11.1 | 643 | 11.1 | 0.748 | 47.1 | LOS D | 15.3 | 117.4 | 0.98 | 0.88 | 34.4 |
| Appr |  | 1241 | 9.8 | 1241 | 9.8 | 0.748 | 32.1 | LOS C | 19.2 | 144.4 | 0.85 | 0.76 | 35.2 |
| East: Erskine Park Road (590m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 649 | 24.8 | 649 | 24.8 | 0.646 | 19.2 | LOS B | 19.3 | 164.1 | 0.66 | 0.82 | 47.4 |
| 6 | R2 | 436 | 7.7 | 436 | 7.7 | 0.754 | 41.1 | LOS C | 19.8 | 147.6 | 0.95 | 0.88 | 31.9 |
| Appr |  | 1085 | 17.9 | 1085 | 17.9 | 0.754 | 28.0 | LOS B | 19.8 | 164.1 | 0.78 | 0.84 | 39.7 |
| North: Mamre Road (200m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 195 | 10.8 | 195 | 10.8 | 0.653 | 21.3 | LOS B | 9.9 | 76.3 | 0.87 | 0.79 | 48.6 |
| 8 | T1 | 508 | 12.4 | 508 | 12.4 | 0.653 | 27.0 | LOS B | 12.7 | 98.0 | 0.92 | 0.80 | 20.4 |
| Approach |  | 703 | 12.0 | 703 | 12.0 | 0.653 | 25.4 | LOS B | 12.7 | 98.0 | 0.90 | 0.80 | 31.0 |
| All Vehicles |  | 3029 | 13.2 | 3029 | 13.2 | 0.754 | 29.1 | LOS C | 19.8 | 164.1 | 0.84 | 0.80 | 36.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 2.0 \%
Number of Iterations: 10 (maximum specified: 10)

Movement Performance - Pedestrians

| Mov ID | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Back Pedestrian ped | queue Distance m | Prop. Queued | Effective Stop Rate per ped |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P1 | South Full Crossing | 1 | 32.0 | LOS D | 0.0 | 0.0 | 0.80 | 0.80 |
| P2 | East Full Crossing | 1 | 37.8 | LOS D | 0.0 | 0.0 | 0.87 | 0.87 |
| P3 | North Full Crossing | 1 | 32.0 | LOS D | 0.0 | 0.0 | 0.80 | 0.80 |
| All Pedestrians |  | 3 | 33.9 | LOS D |  |  | 0.82 | 0.82 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

## SITE LAYOUT

STOF Site: 101 [[Existing] Mamre Road x Mandalong Close_AM]
Mamre Road x Mandalong Close
2018 Existing
Stop (Two-Way)


## MOVEMENT SUMMARY

รT0F Site: 101 [[Existing] Mamre Road x Mandalong Close_AM]
Mamre Road x Mandalong Close
2018 Existing
Stop (Two-Way)


Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 0.0 \%
Number of Iterations: 7 (maximum specified: 10)

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Project: C:IUsers\Alireza Rasouli\Ason Group\Ason Group Team Site - 0584\Projects\ModellingISIDRA\Existing - Base Case 2018\AG0584m01
Mamre_Existing.sip7

## MOVEMENT SUMMARY

Site: 101 [[Existing] Mamre Road x Mandalong Close_PM]
Mamre Road x Mandalong Close
2018 Existing
Stop (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Deman Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Arriva Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Mamre Road ( 200 m ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 24 | 8.7 | 24 | 8.7 | 0.014 | 7.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.63 | 60.4 |
| 2 | T1 | 1134 | 7.5 | 1134 | 7.5 | 0.610 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 79.5 |
| Appr |  | 1158 | 7.5 | 1158 | 7.5 | 0.610 | 0.2 | NA | 0.0 | 0.0 | 0.00 | 0.01 | 79.2 |
| North: Mamre Road (1245m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 | T1 | 672 | 12.4 | 672 | 12.4 | 0.372 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 79.8 |
| 9 | R2 | 26 | 0.0 | 26 | 0.0 | 0.098 | 19.9 | LOS B | 0.3 | 2.3 | 0.83 | 0.94 | 58.4 |
| Appr | ach | 698 | 11.9 | 698 | 11.9 | 0.372 | 0.9 | NA | 0.3 | 2.3 | 0.03 | 0.04 | 78.2 |
| West: Mandalong Close ( 720 m ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 26 | 8.0 | 26 | 8.0 | 0.169 | 31.4 | LOS C | 0.5 | 3.9 | 0.89 | 1.01 | 53.3 |
| 12 | R2 | 11 | 0.0 | 11 | 0.0 | 0.551 | 283.5 | LOS F | 1.5 | 10.6 | 0.99 | 1.03 | 8.1 |
| Approach |  | 37 | 5.7 | 37 | 5.7 | 0.551 | 103.4 | LOS F | 1.5 | 10.6 | 0.92 | 1.01 | 31.0 |
| All Vehicles |  | 1893 | 9.1 | 1893 | 9.1 | 0.610 | 2.5 | NA | 1.5 | 10.6 | 0.03 | 0.04 | 76.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 2.0 \%
Number of Iterations: 10 (maximum specified: 10)

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Mamre_Existing.sip7

## Appendix D2

## 2036 Baseline SIDRA Output - With RMS identified improvements

## SITE LAYOUT

Site: 104 [[2036 Base] Mamre Road x Southern Link_AM]
Mamre Road x Bakers Lane
2036 Base
Signals - Fixed Time Isolated


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Project: C:IUsers\Alireza RasouliAson Group\Ason Group Team Site - 0584|ProjectsIModellingISIDRAI2036 Base Casel2036 Base Case - With $20 \%$ ped callIAG0584m05 Mamre_2036 Basecase - Two lanes on Mamre.sip7

## MOVEMENT SUMMARY

Site: 104 [[2036 Base] Mamre Road x Southern Link_AM]

Mamre Road x Bakers Lane
2036 Base
Signals - Fixed Time Isolated Cycle Time $=150$ seconds (Practical Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Demano Total veh/h | Flows HV \% | Arrival Total veh/h | Flows HV \% | Deg Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | verage Speed km/h |
| South: Mamre Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 1 | 0.0 | 1 | 0.0 | 0.590 | 33.7 | LOS C | 27.7 | 214.0 | 0.72 | 0.66 | 49.6 |
| 2 | T1 | 1613 | 12.2 | 1613 | 12.2 | 0.590 | 24.6 | LOS B | 27.9 | 215.9 | 0.71 | 0.64 | 39.3 |
| 3 | R2 | 607 | 0.0 | 607 | 0.0 | 1.022 | 134.1 | LOS F | 31.9 | 223.4 | 1.00 | 1.09 | 19.2 |
| Appr | ach | 2221 | 8.8 | 2221 | 8.8 | 1.022 | 54.6 | LOS D | 31.9 | 223.4 | 0.79 | 0.76 | 27.5 |
| East: Bakers Lane (440m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 342 | 0.0 | 342 | 0.0 | 0.392 | 33.6 | LOS C | 15.0 | 105.1 | 0.69 | 0.83 | 43.6 |
| 5 | T1 | 181 | 0.0 | 181 | 0.0 | 0.240 | 55.0 | LOS D | 5.6 | 39.2 | 0.89 | 0.70 | 35.9 |
| 6 | R2 | 84 | 0.3 | 84 | 0.3 | 0.262 | 78.2 | LOS F | 3.0 | 20.8 | 0.97 | 0.74 | 16.9 |
| Appr |  | 607 | 0.0 | 607 | 0.0 | 0.392 | 46.1 | LOS D | 15.0 | 105.1 | 0.79 | 0.78 | 36.8 |
| North: Mamre Road ( 760 m ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 524 | 0.2 | 524 | 0.2 | 1.019 | 81.1 | LOS F | 69.3 | 517.2 | 1.00 | 1.09 | 25.7 |
| 8 | T1 | 1607 | 18.3 | 1607 | 18.3 | 1.019 | 104.6 | LOS F | 82.4 | 667.6 | 1.00 | 1.24 | 26.9 |
| 9 | R2 | 151 | 0.0 | 151 | 0.0 | 0.608 | 84.5 | LOS F | 5.6 | 39.5 | 1.00 | 0.78 | 32.3 |
| Appr |  | 2282 | 12.9 | 2282 | 12.9 | 1.019 | 97.9 | LOS F | 82.4 | 667.6 | 1.00 | 1.18 | 26.9 |
| West: Site Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 280 | 0.0 | 280 | 0.0 | 0.972 | 101.9 | LOS F | 31.4 | 219.8 | 1.00 | 1.10 | 15.8 |
| 11 | T1 | 631 | 0.0 | 631 | 0.0 | 0.972 | 100.5 | LOS F | 31.4 | 219.8 | 1.00 | 1.09 | 24.5 |
| 12 | R2 | 1 | 0.0 | 1 | 0.0 | 0.007 | 83.5 | LOS F | 0.0 | 0.3 | 0.97 | 0.57 | 28.4 |
| Approach |  | 912 | 0.0 | 912 | 0.0 | 0.972 | 100.9 | LOS F | 31.4 | 219.8 | 1.00 | 1.09 | 22.1 |
| All Vehicles |  | 6022 | 8.2 | 6022 | 8.2 | 1.022 | 77.1 | LOS F | 82.4 | 667.6 | 0.90 | 0.97 | 27.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement. Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: $13.8 \%$
Number of Iterations: 10 (maximum specified: 10)

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Back Pedestrian ped | Queue Distance m | Prop. Queued | Effective Stop Rate per ped |
| P11 | South Stage 1 | 11 | 69.2 | LOS F | 0.0 | 0.0 | 0.96 | 0.96 |
| P12 | South Stage 2 | 11 | 69.2 | LOS F | 0.0 | 0.0 | 0.96 | 0.96 |
| P2 | East Full Crossing | 11 | 37.5 | LOS D | 0.0 | 0.0 | 0.71 | 0.71 |
| P31 | North Stage 1 | 11 | 65.4 | LOS F | 0.0 | 0.0 | 0.93 | 0.93 |
| P32 | North Stage 2 | 11 | 60.8 | LOS F | 0.0 | 0.0 | 0.90 | 0.90 |
| P4 | West Full Crossing | 11 | 28.2 | LOS C | 0.0 | 0.0 | 0.61 | 0.61 |
| All Pedestrians |  | 63 | 55.0 | LOS E |  |  | 0.85 | 0.85 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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With 20\% ped call\2036 Base Case with 2 lanes on Mamre Rd\AG0584m05 Mamre_2036 Basecase - Two lanes on Mamre.sip7

## MOVEMENT SUMMARY

Site: 104 [[2036 Base] Mamre Road x Southern Link_PM]

Mamre Road x Bakers Lane
2036 Base
Signals - Fixed Time Isolated Cycle Time $=75$ seconds (Practical Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Demano Total veh/h | Flows <br> HV <br> \% | Arrival Total veh/h | Flows <br> HV <br> \% | Deg Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | verage peed <br> km/h |
| South: Mamre Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 1 | 0.0 | 1 | 0.0 | 0.913 | 52.3 | LOS D | 21.8 | 167.7 | 1.00 | 1.10 | 39.9 |
| 2 | T1 | 1391 | 11.5 | 1391 | 11.5 | 0.913 | 44.5 | LOS D | 21.8 | 167.7 | 1.00 | 1.10 | 27.9 |
| 3 | R2 | 321 | 0.0 | 321 | 0.0 | 0.589 | 41.4 | LOS C | 5.8 | 40.5 | 0.98 | 0.81 | 39.8 |
| Appr | ach | 1713 | 9.3 | 1713 | 9.3 | 0.913 | 43.9 | LOS D | 21.8 | 167.7 | 1.00 | 1.04 | 30.6 |
| East: Bakers Lane (440m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 751 | 0.0 | 751 | 0.0 | 0.793 | 29.9 | LOS C | 20.0 | 140.1 | 0.76 | 0.97 | 42.1 |
| 5 | T1 | 631 | 0.0 | 631 | 0.0 | 0.793 | 34.9 | LOS C | 20.0 | 140.1 | 0.96 | 0.95 | 41.3 |
| 6 | R2 | 498 | 0.5 | 498 | 0.5 | 0.776 | 41.9 | LOS C | 9.7 | 68.0 | 1.00 | 0.92 | 24.0 |
| Appr |  | 1879 | 0.1 | 1879 | 0.1 | 0.793 | 34.8 | LOS C | 20.0 | 140.1 | 0.89 | 0.95 | 37.7 |
| North: Mamre Road ( 760 m ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 132 | 0.3 | 132 | 0.3 | 0.980 | 71.4 | LOS F | 28.6 | 223.5 | 1.00 | 1.26 | 35.6 |
| 8 | T1 | 1325 | 18.5 | 1325 | 18.5 | 0.980 | 65.3 | LOS E | 28.6 | 223.5 | 1.00 | 1.27 | 37.4 |
| 9 | R2 | 208 | 0.0 | 208 | 0.0 | 0.383 | 38.2 | LOS C | 3.6 | 25.2 | 0.95 | 0.77 | 42.3 |
| Appr |  | 1665 | 14.7 | 1665 | 14.7 | 0.980 | 62.4 | LOS E | 28.6 | 224.4 | 0.99 | 1.21 | 37.9 |
| West: Site Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 236 | 0.0 | 236 | 0.0 | 0.774 | 29.8 | LOS C | 8.2 | 57.4 | 0.99 | 0.96 | 32.3 |
| 11 | T1 | 326 | 0.0 | 326 | 0.0 | 0.774 | 37.2 | LOS C | 8.2 | 57.4 | 1.00 | 0.91 | 39.5 |
| 12 | R2 | 1 | 0.0 | 1 | 0.0 | 0.004 | 40.6 | LOS C | 0.0 | 0.1 | 0.93 | 0.56 | 38.4 |
| Approach |  | 563 | 0.0 | 563 | 0.0 | 0.774 | 34.1 | LOS C | 8.2 | 57.4 | 0.99 | 0.93 | 37.1 |
| All Vehicles |  | 5820 | 7.0 | 5820 | 7.0 | 0.980 | 45.3 | LOS D | 28.6 | 224.4 | 0.96 | 1.05 | 36.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement. Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 2.0 \% Number of Iterations: 10 (maximum specified: 10)

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \hline \text { ID } \end{aligned}$ | Description | Demand Flow ped/h | Average Delay $\qquad$ sec | Level o Service | Average Back Pedestrian ped | of Queue Distance $\qquad$ m | Prop. Queued | Effective Stop Rate per ped |
| P11 | South Stage 1 | 11 | 31.8 | LOS D | 0.0 | 0.0 | 0.92 | 0.92 |
| P12 | South Stage 2 | 11 | 31.8 | LOS D | 0.0 | 0.0 | 0.92 | 0.92 |
| P2 | East Full Crossing | 11 | 31.8 | LOS D | 0.0 | 0.0 | 0.92 | 0.92 |
| P31 | North Stage 1 | 11 | 31.8 | LOS D | 0.0 | 0.0 | 0.92 | 0.92 |
| P32 | North Stage 2 | 11 | 31.8 | LOS D | 0.0 | 0.0 | 0.92 | 0.92 |
| P4 | West Full Crossing | 11 | 31.8 | LOS D | 0.0 | 0.0 | 0.92 | 0.92 |
| All Pedestrians |  | 63 | 31.8 | LOS D |  |  | 0.92 | 0.92 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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With 20\% ped call\2036 Base Case with 2 lanes on Mamre Rd\AG0584m05 Mamre_2036 Basecase - Two lanes on Mamre.sip7

## SITE LAYOUT

Site: 105vv [[2036 Base] Mamre Road x Mamre west precicnt
Mamre Road x Mamre west precicnt 2018 Base
Giveway / Yield (Two-Way)


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## MOVEMENT SUMMARY

$\nabla$ Site: 105vv [[2036 Base] Mamre Road x Mamre west
 Case - AM - IMPORVED EPR] precicnt _AM]

Mamre Road x Mamre west precicnt
2018 Base
Giveway / Yield (Two-Way)

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline \multicolumn{13}{|l|}{Movement Performance - Vehicles} <br>
\hline $$
\begin{array}{ll}
\text { Mov } & \text { OD } \\
\text { ID } & \text { Mov }
\end{array}
$$ \& Demand Total veh/h \& Demand Flows Arrival Flows Total HV Total HV \& Arriva Total veh/h \& ows
HV

$\%$ \& Deg. Satn v/c \& | Average Delay |
| :--- |
| sec | \& Level of Service \& \multicolumn{2}{|l|}{95\% Back of Queue Vehicles Distance veh} \& Prop. Queued \& \multicolumn{2}{|l|}{} <br>

\hline \multicolumn{13}{|l|}{South: Mamre Road (760m) min min} <br>
\hline 1 L2 \& 112 \& 0.0 \& 112 \& 0.0 \& 0.060 \& 7.0 \& LOS A \& 0.0 \& 0.0 \& 0.00 \& 0.63 \& 67.9 <br>
\hline 2 T 1 \& 1865 \& 7.6 \& 1865 \& 7.6 \& 0.502 \& 0.1 \& LOS A \& 0.0 \& 0.0 \& 0.00 \& 0.00 \& 79.7 <br>
\hline Approach \& 1977 \& 7.2 \& 1977 \& 7.2 \& 0.502 \& 0.5 \& NA \& 0.0 \& 0.0 \& 0.00 \& 0.04 \& 78.5 <br>
\hline \multicolumn{13}{|l|}{North: Mamre Road (520m)} <br>
\hline 8 T1 \& 2282 \& 7.7 \& 2282 \& 7.7 \& 0.614 \& 0.1 \& LOS A \& 0.0 \& 0.0 \& 0.00 \& 0.00 \& 79.5 <br>
\hline Approach \& 2282 \& 7.7 \& 2282 \& 7.7 \& 0.614 \& 0.1 \& NA \& 0.0 \& 0.0 \& 0.00 \& 0.00 \& 79.5 <br>
\hline \multicolumn{13}{|l|}{West: Mamre west preciont Site Access} <br>
\hline 10 L2 \& 32 \& 0.0 \& 32 \& 0.0 \& 0.082 \& 13.7 \& LOSA \& 0.3 \& 1.9 \& 0.73 \& 0.88 \& 41.6 <br>
\hline Approach \& 32 \& 0.0 \& 32 \& 0.0 \& 0.082 \& 13.7 \& LOS A \& 0.3 \& 1.9 \& 0.73 \& 0.88 \& 41.6 <br>
\hline All Vehicles \& 4291 \& 7.4 \& 4291 \& 7.4 \& 0.614 \& 0.4 \& NA \& 0.3 \& 1.9 \& 0.01 \& 0.02 \& 78.5 <br>
\hline
\end{tabular}

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 13.8 \%
Number of Iterations: 10 (maximum specified: 10)

[^3]
## MOVEMENT SUMMARY

$\nabla$ Site: 105vv [[2036 Base] Mamre Road x Mamre west

Mamre Road x Mamre west precicnt
2018 Base
Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{ll} \text { Mov OD } \\ \text { ID } & \text { Mov } \end{array}$ | Demand Flows Total HV veh/h \% |  | Arrival FlowsTotal HV |  | Deg. Satn v/c | Average Delay <br> sec | Level of Service | 95\% Back of Queue Vehicles Distance veh |  | Prop. Queued | Effective Average Stop Speed Rate per veh km/h |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 38 | 0.0 | 38 | 0.0 | 0.020 | 6.9 | LOSA | 0.0 | 0.0 | 0.00 | 0.63 | 67.9 |
| 2 T 1 | 2086 | 6.8 | 2086 | 6.8 | 0.821 | 0.9 | LOSA | 0.0 | 0.0 | 0.00 | 0.00 | 78.0 |
| Approach | 2124 | 6.6 | 2124 | 6.6 | 0.821 | 1.0 | NA | 0.0 | 0.0 | 0.00 | 0.01 | 77.7 |
| North: Mamre Road (520m) |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 1665 | 13.7 | 1665 | 13.7 | 0.465 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 79.7 |
| Approach | 1665 | 13.7 | 1665 | 13.7 | 0.465 | 0.1 | NA | 0.0 | 0.0 | 0.00 | 0.00 | 79.7 |
| West: Mamre west preciont Site Access |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 94 | 0.0 | 94 | 0.0 | 0.396 | 18.2 | LOS B | 1.1 | 7.6 | 0.79 | 0.97 | 37.7 |
| Approach | 94 | 0.0 | 94 | 0.0 | 0.396 | 18.2 | LOS B | 1.1 | 7.6 | 0.79 | 0.97 | 37.7 |
| All Vehicles | 3883 | 9.5 | 3883 | 9.5 | 0.821 | 1.0 | NA | 1.1 | 7.6 | 0.02 | 0.03 | 76.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 2.0 \%
Number of Iterations: 10 (maximum specified: 10)

[^4]
## SITE LAYOUT

Site: 103 [[2036 Base] Mamre Road x James Erskine Drive_AM]
Mamre Road x James Erskine Drive 2036 Base
Signals - Fixed Time Isolated


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Project: C:IUsers\Alireza Rasouli\Ason Group\Ason Group Team Site - 0584\Projects\Modelling\SIDRAI2036 Base Casel2036 Base Case - With 20\% ped call\AG0584m05 Mamre_2036 Basecase - Two lanes on Mamre.sip7

## MOVEMENT SUMMARY

E Site: 103 [[2036 Base] Mamre Road x James Erskine
审审 Network: N101 [2036 Base Drive_AM] Case - AM - IMPORVED EPR]

Mamre Road x James Erskine Drive
2036 Base
Signals - Fixed Time Isolated Cycle Time = 150 seconds (Practical Cycle Time)


Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 13.8 \%
Number of Iterations: 10 (maximum specified: 10)

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Back Pedestrian ped | Queue Distance m | Prop. Queued | Effective Stop Rate per ped |
| P1 | South Full Crossing | 1 | 69.1 | LOS F | 0.0 | 0.0 | 0.96 | 0.96 |
| P2 | East Full Crossing | 1 | 16.3 | LOS B | 0.0 | 0.0 | 0.47 | 0.47 |
| P3 | North Full Crossing | 53 | 69.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 |
| P4 | West Full Crossing | 53 | 15.4 | LOS B | 0.1 | 0.1 | 0.45 | 0.45 |
| All Pedestrians |  | 107 | 42.4 | LOS E |  |  | 0.71 | 0.71 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.

Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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Organisation: ASON GROUP PTY LTD | Processed: Friday, 25 May 2018 12:39:52 PM
Project: C:IUsers\Alireza Rasouli\Ason Group\Ason Group Team Site - 0584\Projects\Modelling\SIDRAI2036 Base Casel2036 Base Case With $20 \%$ ped call\2036 Base Case with 2 lanes on Mamre Rd\AG0584m05 Mamre_2036 Basecase - Two lanes on Mamre.sip7

## MOVEMENT SUMMARY

Site: 103 [[2036 Base] Mamre Road x James Erskine
审审 Network: N101 [2036 Base Case - PM - IMPROVED EPR]
Drive_PM] $\qquad$
Mamre Road x James Erskine Drive
2036 Base
Signals - Fixed Time Isolated Cycle Time $=150$ seconds (Practical Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \hline \text { ID } \end{gathered}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Demand Total veh/h | Flows HV <br> \% | Arrival Total veh/h | Flows HV \% | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance | Prop. Queued | Effective Stop Rate per veh | verage Speed km/h |
| South: Mamre Road (520m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 1 | 0.0 | 1 | 0.0 | 0.001 | 7.2 | LOS A | 0.0 | 0.1 | 0.18 | 0.56 | 53.1 |
| 2 | T1 | 2136 | 10.3 | 2136 | 10.3 | 0.966 | 58.9 | LOS E | 94.2 | 713.6 | 1.00 | 1.09 | 23.3 |
| 3 | R2 | 60 | 58.3 | 60 | 58.3 | 0.264 | 80.2 | LOS F | 2.1 | 22.5 | 0.97 | 0.74 | 21.7 |
| Appr | ach | 2197 | 11.6 | 2197 | 11.6 | 0.966 | 59.4 | LOS E | 94.2 | 713.6 | 1.00 | 1.08 | 23.3 |
| East: James Erskine Drive (170m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 172 | 8.3 | 172 | 8.3 | 0.225 | 10.4 | LOS A | 3.6 | 27.3 | 0.39 | 0.63 | 28.8 |
| 5 | T1 | 1 | 0.0 | 1 | 0.0 | 0.225 | 6.0 | LOS A | 3.6 | 27.3 | 0.39 | 0.63 | 46.0 |
| 6 | R2 | 221 | 17.3 | 221 | 17.3 | 0.926 | 98.7 | LOS F | 9.5 | 76.5 | 1.00 | 1.06 | 6.2 |
| Appr | ach | 394 | 13.4 | 394 | 13.4 | 0.926 | 60.0 | LOS E | 9.5 | 76.5 | 0.73 | 0.87 | 9.5 |
| North: Mamre Road ( 300 m ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 127 | 56.3 | 127 | 56.3 | 0.432 | 30.5 | LOS C | 15.2 | 131.9 | 0.60 | 0.66 | 34.4 |
| 8 | T1 | 1379 | 15.1 | 1379 | 15.1 | 0.558 | 22.3 | LOS B | 25.5 | 201.5 | 0.67 | 0.63 | 31.1 |
| 9 | R2 | 63 | 0.0 | 63 | 0.0 | 0.425 | 86.5 | LOS F | 2.4 | 16.9 | 1.00 | 0.72 | 21.5 |
| Appr | ach | 1569 | 17.9 | 1569 | 17.9 | 0.558 | 25.5 | LOS B | 25.5 | 201.5 | 0.68 | 0.64 | 30.2 |
| West: RoadName |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 94 | 0.0 | 94 | 0.0 | 0.169 | 37.0 | LOS C | 4.5 | 31.2 | 0.73 | 0.73 | 27.6 |
| 11 | T1 | 1 | 0.0 | 1 | 0.0 | 0.169 | 31.4 | LOS C | 4.5 | 31.2 | 0.73 | 0.73 | 31.8 |
| 12 | R2 | 115 | 0.0 | 115 | 0.0 | 0.842 | 88.6 | LOS F | 9.1 | 63.9 | 1.00 | 0.93 | 15.8 |
| Approach |  | 209 | 0.0 | 209 | 0.0 | 0.842 | 65.2 | LOS E | 9.1 | 63.9 | 0.88 | 0.84 | 19.6 |
| All Vehicles |  | 4369 | 13.5 | 4369 | 13.5 | 0.966 | 47.6 | LOS D | 94.2 | 713.6 | 0.85 | 0.89 | 23.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 2.0 \%
Number of Iterations: 10 (maximum specified: 10)

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Bac Pedestrian ped | Queue Distance m | Prop. Queued | Effective Stop Rate per ped |
| P1 | South Full Crossing | 1 | 69.1 | LOS F | 0.0 | 0.0 | 0.96 | 0.96 |
| P2 | East Full Crossing | 1 | 21.3 | LOS C | 0.0 | 0.0 | 0.53 | 0.53 |
| P3 | North Full Crossing | 53 | 69.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 |
| P4 | West Full Crossing | 53 | 69.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 |
| All Pedestrians |  | 107 | 68.8 | LOS F |  |  | 0.96 | 0.96 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.

Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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Project: C:IUsers\Alireza Rasouli\Ason Group\Ason Group Team Site - 0584\Projects\Modelling\SIDRAI2036 Base Casel2036 Base Case With $20 \%$ ped call\2036 Base Case with 2 lanes on Mamre Rd\AG0584m05 Mamre_2036 Basecase - Two lanes on Mamre.sip7

## SITE LAYOUT

## Site: 102 [[2036 Base] Mamre Road x Erskine Park Road_PM - IMPROVED]

Mamre Road x Erskine Park Road
2036 Base
Signals - Fixed Time Isolated


## MOVEMENT SUMMARY

Site: 102 [[2036 Base] Mamre Road x Erskine Park
审审 Network: N101 [2036 Base Case - AM - IMPORVED EPR] Road_AM - IMPROVED] $\qquad$
Mamre Road x Erskine Park Road
2036 Base
Signals - Fixed Time Coordinated Cycle Time = 100 seconds (Network Cycle Time - User-Given)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov OD ID Mov | Demand Total veh/h | Flows HV \% | Arrival Total veh/h | Flows HV \% | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance | Prop. Queued | Effective Stop Rate per veh | verage Speed km/h |
| South: Mamre Road (300m) |  |  |  |  |  |  |  |  |  |  |  |  |
| $2 \quad \mathrm{~T} 1$ | 748 | 9.8 | 748 | 9.8 | 0.249 | 2.1 | LOS A | 4.0 | 30.6 | 0.24 | 0.21 | 69.7 |
| 3 R2 | 951 | 13.4 | 951 | 13.4 | 0.825 | 45.9 | LOS D | 23.6 | 184.4 | 0.98 | 0.92 | 35.0 |
| Approach | 1699 | 11.8 | 1699 | 11.8 | 0.825 | 26.6 | LOS B | 23.6 | 184.4 | 0.66 | 0.61 | 39.3 |
| East: Erskine Park Road (590m) |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 1017 | 13.1 | 1017 | 13.1 | 0.899 | 41.8 | LOS C | 31.3 | 243.6 | 0.91 | 0.92 | 31.9 |
| 6 R2 | 12 | 14.0 | 12 | 14.0 | 0.057 | 57.7 | LOS E | 0.3 | 2.2 | 0.97 | 0.65 | 25.8 |
| Approach | 1028 | 13.1 | 1028 | 13.1 | 0.899 | 42.0 | LOS C | 31.3 | 243.6 | 0.91 | 0.92 | 31.8 |
| North: Mamre Road (200m) |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 222 | 4.4 | 222 | 4.4 | 0.717 | 25.6 | LOS B | 18.3 | 134.2 | 0.84 | 0.86 | 47.6 |
| 8 T1 | 1432 | 6.4 | 1432 | 6.4 | 1.043 | 87.4 | LOS F | 44.2 | 326.4 | 0.95 | 1.26 | 8.1 |
| Approach | 1654 | 6.1 | 1654 | 6.1 | 1.043 | 79.1 | LOS F | 44.2 | 326.4 | 0.94 | 1.21 | 11.6 |
| All Vehicles | 4381 | 10.0 | 4381 | 10.0 | 1.043 | 50.0 | LOS D | 44.2 | 326.4 | 0.82 | 0.91 | 24.5 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 13.8 \%
Number of Iterations: 10 (maximum specified: 10)

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Bac Pedestrian ped | Queue Distance m | Prop. Queued | Effective Stop Rate per ped |
| P1 | South Full Crossing | 1 | 44.2 | LOS E | 0.0 | 0.0 | 0.94 | 0.94 |
| P2 | East Full Crossing | 1 | 23.8 | LOS C | 0.0 | 0.0 | 0.69 | 0.69 |
| P2S | East Slip/Bypass Lane | 53 | 19.3 | LOS B | 0.1 | 0.1 | 0.62 | 0.62 |
|  | Crossing |  |  |  |  |  |  |  |
| P3 | North Full Crossing | 1 | 44.2 | LOS E | 0.0 | 0.0 | 0.94 | 0.94 |
| All Pedestrians |  | 56 | 20.3 | LOS C |  |  | 0.63 | 0.63 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

[^5]
## MOVEMENT SUMMARY

Site: 102 [[2036 Base] Mamre Road x Erskine Park
审审 Network: N101 [2036 Base Case - PM - IMPROVED EPR] Road_PM - IMPROVED] $\qquad$
Mamre Road x Erskine Park Road
2036 Base
Signals - Fixed Time Coordinated Cycle Time = 100 seconds (Network Cycle Time - User-Given)


Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 2.0 \% Number of Iterations: 10 (maximum specified: 10)

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Bac Pedestrian ped | Queue Distance m | Prop. Queued | Effective Stop Rate per ped |
| P1 | South Full Crossing | 1 | 44.2 | LOS E | 0.0 | 0.0 | 0.94 | 0.94 |
| P2 | East Full Crossing | 1 | 41.4 | LOS E | 0.0 | 0.0 | 0.91 | 0.91 |
| P2S | East Slip/Bypass Lane | 53 | 35.4 | LOS D | 0.1 | 0.1 | 0.84 | 0.84 |
|  | Crossing |  |  |  |  |  |  |  |
| P3 | North Full Crossing | 1 | 44.2 | LOS E | 0.0 | 0.0 | 0.94 | 0.94 |
| All Pedestrians |  | 56 | 35.8 | LOS D |  |  | 0.85 | 0.85 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

[^6]
## SITE LAYOUT

SsT0F Site: 101 [[2036 Base] Mamre Road x Mandalong Close_AM]
Mamre Road x Mandalong Close
2036 Base
Stop (Two-Way)


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Organisation: ASON GROUP PTY LTD | Created: Thursday, 24 May 2018 11:58:05 AM
Project: C:\Users\Alireza Rasouli\Ason Group\Ason Group Team Site - 0584\Projects\Modelling\SIDRA\2036 Base Casel2036 Base Case - With 20\% ped call\AG0584m05 Mamre_2036 Basecase - Two lanes on Mamre.sip7

## MOVEMENT SUMMARY

Site: 101 [[2036 Base] Mamre Road x Mandalong Close_AM]
神审 Network: N101 [2036 Base Case - AM - IMPORVED EPR]
Mamre Road x Mandalong Close
2036 Base
Stop (Two-Way)


Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 13.8 \%
Number of Iterations: 10 (maximum specified: 10)

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Project: C:\Users\Alireza Rasouli\Ason Group\Ason Group Team Site - 0584\Projects\Modelling\SIDRA\2036 Base Case\2036 Base Case -
With 20\% ped call\2036 Base Case with 2 lanes on Mamre Rd\AG0584m05 Mamre_2036 Basecase - Two lanes on Mamre.sip7

## MOVEMENT SUMMARY

Site: 101 [[2036 Base] Mamre Road x Mandalong Close_PM]
它审 Network: N101 [2036 Base Case - PM - IMPROVED EPR]
Mamre Road x Mandalong Close
2036 Base
Stop (Two-Way)

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline \multicolumn{13}{|l|}{Movement Performance - Vehicles} \\
\hline \begin{tabular}{cc} 
Mov OD \\
ID \& Mov
\end{tabular} \& Demand Total veh/h \& Flows HV \% \& Arriva Total veh/h \& HV l (

$\%$ \& Deg. Satn v/c \& | Average Delay |
| :--- |
| sec | \& Level of Service \& 95\% Back Vehicles veh \& | of Queue Distance |
| :--- |
| m | \& Prop. Queued \& Effective Stop Rate per veh \& | Average Speed |
| :--- |
| km/h | <br>

\hline \multicolumn{13}{|l|}{} <br>
\hline 1 L2 \& 58 \& 8.7 \& 58 \& 8.7 \& 0.033 \& 7.1 \& LOS A \& 0.0 \& 0.0 \& 0.00 \& 0.63 \& 60.4 <br>
\hline 2 T1 \& 1639 \& 7.5 \& 1639 \& 7.5 \& 0.441 \& 0.0 \& LOS A \& 0.0 \& 0.0 \& 0.00 \& 0.00 \& 79.8 <br>
\hline Approach \& 1697 \& 7.6 \& 1697 \& 7.6 \& 0.441 \& 0.3 \& NA \& 0.0 \& 0.0 \& 0.00 \& 0.02 \& 79.2 <br>
\hline \multicolumn{13}{|l|}{North: Mamre Road (1245m)} <br>
\hline 8 T1 \& 865 \& 12.4 \& 865 \& 12.4 \& 0.240 \& 0.1 \& LOS A \& 0.0 \& 0.0 \& 0.00 \& 0.00 \& 79.9 <br>
\hline Approach \& 865 \& 12.4 \& 865 \& 12.4 \& 0.240 \& 0.1 \& NA \& 0.0 \& 0.0 \& 0.00 \& 0.00 \& 79.9 <br>
\hline \multicolumn{13}{|l|}{West: Mandalong Close ( 720 m )} <br>
\hline 10 L2 \& 63 \& 8.0 \& 63 \& 8.0 \& 0.170 \& 17.2 \& LOS B \& 0.6 \& 4.5 \& 0.72 \& 1.00 \& 59.5 <br>
\hline Approach \& 63 \& 8.0 \& 63 \& 8.0 \& 0.170 \& 17.2 \& LOS B \& 0.6 \& 4.5 \& 0.72 \& 1.00 \& 59.5 <br>
\hline All Vehicles \& 2625 \& 9.2 \& 2625 \& 9.2 \& 0.441 \& 0.6 \& NA \& 0.6 \& 4.5 \& 0.02 \& 0.04 \& 78.5 <br>
\hline
\end{tabular}

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 2.0 \%
Number of Iterations: 10 (maximum specified: 10)

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Organisation: ASON GROUP PTY LTD | Processed: Friday, 25 May 2018 12:44:21 PM
Project: C:\Users\Alireza Rasouli\Ason Group\Ason Group Team Site - 0584\Projects\Modelling\SIDRAl2036 Base Case\2036 Base Case -
With 20\% ped call\2036 Base Case with 2 lanes on Mamre Rd\AG0584m05 Mamre 2036 Basecase - Two lanes on Mamre.sip7

## Appendix D3

## 2036 Project Future Baseline SIDRA Results - Three Lanes on Mamre Road

## SITE LAYOUT

## Site: 104 [[2036 Base] Mamre Road x Southern Link_AM]

Mamre Road x Bakers Lane
2036 Base
Signals - Fixed Time Isolated


## MOVEMENT SUMMARY

Site: 104 [[2036 Base] Mamre Road x Southern Link_AM]

Mamre Road x Bakers Lane
2036 Base
Signals - Fixed Time Isolated Cycle Time $=105$ seconds (Practical Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Demand Total veh/h | Flows HV \% | Arrival Total veh/h | Flows HV \% | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate | Average Speed <br> km/h |
| South: Mamre Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 1 | 0.0 | 1 | 0.0 | 0.001 | 7.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.60 | 66.5 |
| 2 | T1 | 1623 | 12.8 | 1623 | 12.8 | 0.637 | 22.8 | LOS B | 20.8 | 160.9 | 0.82 | 0.73 | 40.9 |
| 3 | R2 | 607 | 0.0 | 607 | 0.0 | 0.858 | 60.6 | LOS E | 17.2 | 120.2 | 1.00 | 0.95 | 32.7 |
| Appr | ach | 2232 | 9.3 | 2232 | 9.3 | 0.858 | 33.1 | LOS C | 20.8 | 160.9 | 0.87 | 0.79 | 37.1 |
| East: Bakers Lane (440m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 342 | 0.0 | 342 | 0.0 | 0.328 | 16.7 | LOS B | 8.3 | 57.9 | 0.55 | 0.75 | 55.2 |
| 5 | T1 | 181 | 0.0 | 181 | 0.0 | 0.257 | 40.3 | LOS C | 4.0 | 28.3 | 0.90 | 0.71 | 42.3 |
| 6 | R2 | 84 | 0.3 | 84 | 0.3 | 0.398 | 62.7 | LOS E | 2.2 | 15.7 | 1.00 | 0.73 | 20.2 |
| Appr | ach | 607 | 0.0 | 607 | 0.0 | 0.398 | 30.1 | LOS C | 8.3 | 57.9 | 0.72 | 0.73 | 45.0 |
| North: Mamre Road (760m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 524 | 0.2 | 524 | 0.2 | 0.283 | 7.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.60 | 68.0 |
| 8 | T1 | 1607 | 18.3 | 1607 | 18.3 | 0.897 | 49.3 | LOS D | 31.7 | 256.6 | 1.00 | 1.05 | 43.2 |
| 9 | R2 | 151 | 0.0 | 151 | 0.0 | 0.608 | 62.8 | LOS E | 4.0 | 28.3 | 1.00 | 0.78 | 38.1 |
| Appr | ach | 2282 | 12.9 | 2282 | 12.9 | 0.897 | 40.6 | LOS C | 31.7 | 256.6 | 0.77 | 0.93 | 46.6 |
| West: Site Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 280 | 0.0 | 280 | 0.0 | 0.151 | 7.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.60 | 61.4 |
| 11 | T1 | 631 | 0.0 | 631 | 0.0 | 0.893 | 57.6 | LOS E | 18.6 | 130.4 | 1.00 | 1.01 | 35.2 |
| 12 | R2 | 1 | 0.0 | 1 | 0.0 | 0.005 | 59.0 | LOS E | 0.0 | 0.2 | 0.96 | 0.57 | 35.1 |
| Approach |  | 912 | 0.0 | 912 | 0.0 | 0.893 | 42.2 | LOS C | 18.6 | 130.4 | 0.69 | 0.88 | 38.4 |
| All V | icles | 6033 | 8.3 | 6033 | 8.3 | 0.897 | 37.0 | LOS C | 31.7 | 256.6 | 0.79 | 0.85 | 42.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement. Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 0.0 \% Number of Iterations: 5 (maximum specified: 10)

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Description | Demand Flow ped $/ \mathrm{h}$ | Average Delay sec $\qquad$ | Level of Service | Average Back Pedestrian ped | of Queue Distance $\qquad$ | Prop. Queued | Effective Stop Rate per ped |
| P11 | South Stage 1 | 11 | 46.7 | LOS E | 0.0 | 0.0 | 0.94 | 0.94 |
| P12 | South Stage 2 | 11 | 43.0 | LOS E | 0.0 | 0.0 | 0.91 | 0.91 |
| P21 | East Stage 1 | 11 | 20.8 | LOS C | 0.0 | 0.0 | 0.63 | 0.63 |
| P22 | East Stage 2 | 11 | 19.5 | LOS B | 0.0 | 0.0 | 0.61 | 0.61 |
| P31 | North Stage 1 | 11 | 35.2 | LOS D | 0.0 | 0.0 | 0.82 | 0.82 |
| P32 | North Stage 2 | 11 | 32.8 | LOS D | 0.0 | 0.0 | 0.79 | 0.79 |
| P41 | West Stage 1 | 11 | 13.4 | LOS B | 0.0 | 0.0 | 0.50 | 0.50 |
| P42 | West Stage 2 | 11 | 12.4 | LOS B | 0.0 | 0.0 | 0.49 | 0.49 |


| All Pedestrians | 84 | 28.0 | LOS C | 0.71 | 0.71 |
| :--- | :--- | :--- | :--- | :--- | :--- |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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\AG0584m05v01 Mamre_2036 Basecase - Final - With Improvements.sip7

## MOVEMENT SUMMARY

Site: 104 [[2036 Base] Mamre Road x Southern Link_PM]

Mamre Road x Bakers Lane
2036 Base
Signals - Fixed Time Isolated Cycle Time $=85$ seconds (Practical Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Demano Total veh/h | Flows HV \% | Arrival Total veh/h | lows HV \% | Deg Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | verage peed km/h |
| South: Mamre Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 1 | 0.0 | 1 | 0.0 | 0.001 | 7.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.60 | 66.5 |
| 2 | T1 | 1401 | 12.1 | 1401 | 12.1 | 0.804 | 33.1 | LOS C | 19.5 | 149.6 | 0.98 | 0.93 | 33.5 |
| 3 | R2 | 321 | 0.0 | 321 | 0.0 | 0.816 | 54.1 | LOS D | 7.4 | 51.7 | 1.00 | 0.91 | 34.9 |
| Appr | ach | 1723 | 9.9 | 1723 | 9.9 | 0.816 | 37.0 | LOS C | 19.5 | 149.6 | 0.98 | 0.92 | 33.9 |
| East: Bakers Lane (440m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 751 | 0.0 | 751 | 0.0 | 0.404 | 5.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.53 | 54.6 |
| 5 | T1 | 631 | 0.0 | 631 | 0.0 | 0.916 | 52.3 | LOS D | 16.2 | 113.1 | 1.00 | 1.11 | 34.9 |
| 6 | R2 | 498 | 0.5 | 498 | 0.5 | 0.880 | 54.2 | LOS D | 12.1 | 84.8 | 1.00 | 1.03 | 20.5 |
| Appr |  | 1879 | 0.1 | 1879 | 0.1 | 0.916 | 34.2 | LOS C | 16.2 | 113.1 | 0.60 | 0.86 | 37.2 |
| North: Mamre Road ( 760 m ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 132 | 0.3 | 132 | 0.3 | 0.071 | 7.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.60 | 68.0 |
| 8 | T1 | 1325 | 18.5 | 1325 | 18.5 | 0.899 | 45.9 | LOS D | 22.2 | 180.1 | 1.00 | 1.07 | 44.7 |
| 9 | R2 | 208 | 0.0 | 208 | 0.0 | 0.795 | 53.9 | LOS D | 4.8 | 33.8 | 1.00 | 0.90 | 37.2 |
| Appr |  | 1665 | 14.7 | 1665 | 14.7 | 0.899 | 43.9 | LOS D | 22.2 | 180.1 | 0.92 | 1.01 | 44.7 |
| West: Site Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 236 | 0.0 | 236 | 0.0 | 0.127 | 5.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.53 | 51.4 |
| 11 | T1 | 326 | 0.0 | 326 | 0.0 | 0.474 | 34.9 | LOS C | 6.3 | 43.9 | 0.95 | 0.77 | 41.4 |
| 12 | R2 | 1 | 0.0 | 1 | 0.0 | 0.002 | 38.2 | LOS C | 0.0 | 0.1 | 0.86 | 0.57 | 39.6 |
| Approach |  | 563 | 0.0 | 563 | 0.0 | 0.474 | 22.6 | LOS B | 6.3 | 43.9 | 0.55 | 0.67 | 43.8 |
| All Vehicles |  | 5831 | 7.2 | 5831 | 7.2 | 0.916 | 36.7 | LOS C | 22.2 | 180.1 | 0.80 | 0.90 | 39.7 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 0.0 \%
Number of Iterations: 5 (maximum specified: 10)

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Description | $\begin{aligned} & \text { Demand } \\ & \text { Flow } \\ & \text { ped/h } \end{aligned}$ | Average Delay sec | Level of Service | Average Back Pedestrian ped | Queue Distance m | Prop. Queued | Effective Stop Rate per ped |
| P11 | South Stage 1 | 11 | 31.4 | LOS D | 0.0 | 0.0 | 0.86 | 0.86 |
| P12 | South Stage 2 | 11 | 26.4 | LOS C | 0.0 | 0.0 | 0.79 | 0.79 |
| P21 | East Stage 1 | 11 | 15.3 | LOS B | 0.0 | 0.0 | 0.60 | 0.60 |
| P22 | East Stage 2 | 11 | 14.1 | LOS B | 0.0 | 0.0 | 0.58 | 0.58 |
| P31 | North Stage 1 | 11 | 23.4 | LOS C | 0.0 | 0.0 | 0.74 | 0.74 |
| P32 | North Stage 2 | 11 | 21.2 | LOS C | 0.0 | 0.0 | 0.71 | 0.71 |
| P41 | West Stage 1 | 11 | 13.6 | LOS B | 0.0 | 0.0 | 0.56 | 0.56 |
| P42 | West Stage 2 | 11 | 12.5 | LOS B | 0.0 | 0.0 | 0.54 | 0.54 |


| All Pedestrians | 84 | 19.7 | LOS B | 0.67 |
| :--- | :--- | :--- | :--- | :--- | :--- |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## SITE LAYOUT

## Site: 105vv [[2036 Base] Mamre Road x Mamre west precicnt <br> AM]

Mamre Road x Mamre west precicnt 2018 Base
Giveway / Yield (Two-Way)


## MOVEMENT SUMMARY

$\nabla$ Site: 105vv [[2036 Base] Mamre Road x Mamre west
 Case - AM - IMPORVED EPR] precicnt _AM]

Mamre Road x Mamre west precicnt
2018 Base
Giveway / Yield (Two-Way)

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline \multicolumn{13}{|l|}{Movement Performance - Vehicles} <br>
\hline $$
\begin{array}{ll}
\text { Mov } & \text { OD } \\
\text { ID } & \text { Mov }
\end{array}
$$ \& Demand Total veh/h \& Demand Flows Arrival Flows Total HV Total HV \& Arriva Total veh/h \& ows
HV

$\%$ \& Deg. Satn v/c \& | Average Delay |
| :--- |
| sec | \& Level of Service \& \multicolumn{2}{|l|}{95\% Back of Queue Vehicles Distance veh} \& Prop. Queued \& \multicolumn{2}{|l|}{Effective Average Stop Speed Rate per veh km/h} <br>

\hline \multicolumn{13}{|l|}{South: Mamre Road (760m) mil} <br>
\hline 1 L2 \& 112 \& 0.0 \& 112 \& 0.0 \& 0.060 \& 7.0 \& LOS A \& 0.0 \& 0.0 \& 0.00 \& 0.63 \& 67.9 <br>
\hline 2 T 1 \& 1865 \& 7.6 \& 1865 \& 7.6 \& 0.335 \& 0.1 \& LOS A \& 0.0 \& 0.0 \& 0.00 \& 0.00 \& 79.8 <br>
\hline Approach \& 1977 \& 7.2 \& 1977 \& 7.2 \& 0.335 \& 0.5 \& NA \& 0.0 \& 0.0 \& 0.00 \& 0.04 \& 78.6 <br>
\hline \multicolumn{13}{|l|}{North: Mamre Road (520m)} <br>
\hline 8 T1 \& 2282 \& 7.7 \& 2282 \& 7.7 \& 0.410 \& 0.1 \& LOS A \& 0.0 \& 0.0 \& 0.00 \& 0.00 \& 79.8 <br>
\hline Approach \& 2282 \& 7.7 \& 2282 \& 7.7 \& 0.410 \& 0.1 \& NA \& 0.0 \& 0.0 \& 0.00 \& 0.00 \& 79.8 <br>
\hline \multicolumn{13}{|l|}{West: Mamre west preciont Site Access} <br>
\hline 10 L2 \& 32 \& 0.0 \& 32 \& 0.0 \& 0.048 \& 9.2 \& LOSA \& 0.2 \& 1.2 \& 0.54 \& 0.74 \& 46.3 <br>
\hline Approach \& 32 \& 0.0 \& 32 \& 0.0 \& 0.048 \& 9.2 \& LOS A \& 0.2 \& 1.2 \& 0.54 \& 0.74 \& 46.3 <br>
\hline All Vehicles \& 4291 \& 7.4 \& 4291 \& 7.4 \& 0.410 \& 0.3 \& NA \& 0.2 \& 1.2 \& 0.00 \& 0.02 \& 78.8 <br>
\hline
\end{tabular}

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 0.0 \%
Number of Iterations: 5 (maximum specified: 10)

[^7]
## MOVEMENT SUMMARY

$\nabla$ Site: 105vv [[2036 Base] Mamre Road x Mamre west

Mamre Road x Mamre west precicnt
2018 Base
Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{ll} \text { Mov } & \text { OD } \\ \text { ID } & \text { Mov } \end{array}$ | Demand Flows Total veh/h \% |  | Arrival FlowsTotal HV |  | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back of Queue Vehicles Distance veh |  | Prop. Queued | Effective Average Stop Speed Rate per veh km/h |  |
| South: Mamre Road (760m) min min |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 38 | 0.0 | 38 | 0.0 | 0.020 | 6.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.63 | 67.9 |
| 2 T 1 | 2086 | 6.8 | 2086 | 6.8 | 0.372 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 79.8 |
| Approach | 2124 | 6.6 | 2124 | 6.6 | 0.372 | 0.2 | NA | 0.0 | 0.0 | 0.00 | 0.01 | 79.4 |
| North: Mamre Road (520m) |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 1665 | 13.7 | 1665 | 13.7 | 0.310 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 79.9 |
| Approach | 1665 | 13.7 | 1665 | 13.7 | 0.310 | 0.0 | NA | 0.0 | 0.0 | 0.00 | 0.00 | 79.9 |
| West: Mamre west precicnt Site Access |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 94 | 0.0 | 94 | 0.0 | 0.155 | 10.2 | LOSA | 0.6 | 4.0 | 0.59 | 0.83 | 45.1 |
| Approach | 94 | 0.0 | 94 | 0.0 | 0.155 | 10.2 | LOS A | 0.6 | 4.0 | 0.59 | 0.83 | 45.1 |
| All Vehicles | 3883 | 9.5 | 3883 | 9.5 | 0.372 | 0.4 | NA | 0.6 | 4.0 | 0.01 | 0.03 | 78.5 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 0.0 \%
Number of Iterations: 5 (maximum specified: 10)

[^8]
## SITE LAYOUT

## Site: 103 [[2036 Base] Mamre Road x James Erskine Drive_AM]

Mamre Road x James Erskine Drive
2036 Base
Signals - Fixed Time Isolated


## MOVEMENT SUMMARY

E Site: 103 [[2036 Base] Mamre Road x James Erskine
审审 Network: N101 [2036 Base Drive_AM] Case - AM - IMPORVED EPR]

Mamre Road x James Erskine Drive
2036 Base
Signals - Fixed Time Isolated Cycle Time = 95 seconds (Practical Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Demand Total veh/h | Flows HV <br> \% | Arriva Total veh/h | lows <br> HV <br> \% | Deg. Satn v/c | Average Delay | Level of Service | 95\% Back Vehicles veh | of Queue Distance | Prop. Queued | Effective Stop Rate per veh | verage peed <br> km/h |
| South: Mamre Road (520m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 1 | 0.0 | 1 | 0.0 | 0.001 | 8.7 | LOS A | 0.0 | 0.1 | 0.30 | 0.56 | 52.0 |
| 2 | T1 | 1580 | 8.1 | 1580 | 8.1 | 0.648 | 23.2 | LOS B | 19.1 | 141.7 | 0.85 | 0.75 | 40.9 |
| 3 | R2 | 147 | 22.0 | 147 | 22.0 | 0.727 | 60.7 | LOS E | 3.8 | 31.3 | 1.00 | 0.84 | 26.2 |
| Appr | ach | 1728 | 9.3 | 1728 | 9.3 | 0.727 | 26.4 | LOS B | 19.1 | 141.7 | 0.86 | 0.76 | 38.5 |
| East: James Erskine Drive (170m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 62 | 54.8 | 62 | 54.8 | 0.110 | 13.4 | LOS A | 1.2 | 12.5 | 0.52 | 0.64 | 26.1 |
| 5 | T1 | 1 | 0.0 | 1 | 0.0 | 0.110 | 8.2 | LOS A | 1.2 | 12.5 | 0.52 | 0.64 | 44.0 |
| 6 | R2 | 88 | 54.2 | 88 | 54.2 | 0.531 | 56.5 | LOS D | 2.2 | 22.6 | 1.00 | 0.77 | 10.1 |
| Appr | ach | 152 | 54.1 | 152 | 54.1 | 0.531 | 38.5 | LOS C | 2.2 | 22.6 | 0.80 | 0.71 | 13.7 |
| North: Mamre Road ( 300 m ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 429 | 17.9 | 429 | 17.9 | 0.652 | 26.4 | LOS B | 16.9 | 133.5 | 0.77 | 0.87 | 34.8 |
| 8 | T1 | 2182 | 7.4 | 2182 | 7.4 | 0.843 | 30.9 | LOS C | 31.3 | 233.2 | 0.95 | 0.94 | 25.2 |
| 9 | R2 | 183 | 0.0 | 183 | 0.0 | 0.781 | 59.3 | LOS E | 4.7 | 32.9 | 1.00 | 0.88 | 27.0 |
| Appr | ach | 2795 | 8.5 | 2795 | 8.5 | 0.843 | 32.0 | LOS C | 31.3 | 233.2 | 0.93 | 0.92 | 26.9 |
| West: RoadName |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 31 | 0.0 | 31 | 0.0 | 0.040 | 11.8 | LOS A | 0.5 | 3.2 | 0.49 | 0.64 | 43.8 |
| 11 | T1 | 1 | 0.0 | 1 | 0.0 | 0.040 | 6.2 | LOSA | 0.5 | 3.2 | 0.49 | 0.64 | 46.9 |
| 12 | R2 | 38 | 0.0 | 38 | 0.0 | 0.323 | 54.7 | LOS D | 1.8 | 12.6 | 0.99 | 0.73 | 22.1 |
| Approach |  | 69 | 0.0 | 69 | 0.0 | 0.323 | 35.1 | LOS C | 1.8 | 12.6 | 0.76 | 0.69 | 28.5 |
| All Vehicles |  | 4744 | 10.1 | 4744 | 10.1 | 0.843 | 30.2 | LOS C | 31.3 | 233.2 | 0.90 | 0.85 | 30.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 0.0 \%
Number of Iterations: 5 (maximum specified: 10)

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Back Pedestrian ped | queue Distance m | Prop. Queued | Effective Stop Rate per ped |
| P1 | South Full Crossing | 1 | 41.7 | LOS E | 0.0 | 0.0 | 0.94 | 0.94 |
| P2 | East Full Crossing | 1 | 24.3 | LOS C | 0.0 | 0.0 | 0.72 | 0.72 |
| P3 | North Full Crossing | 53 | 41.8 | LOS E | 0.1 | 0.1 | 0.94 | 0.94 |
| P4 | West Full Crossing | 53 | 23.0 | LOS C | 0.1 | 0.1 | 0.70 | 0.70 |
| All Pedestrians |  | 107 | 32.4 | LOS D |  |  | 0.82 | 0.82 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.

Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## MOVEMENT SUMMARY

Site: 103 [[2036 Base] Mamre Road x James Erskine
审审 Network: N101 [2036 Base Case - PM - IMPROVED EPR]
Drive_PM] $\qquad$
Mamre Road x James Erskine Drive
2036 Base
Signals - Fixed Time Isolated Cycle Time $=100$ seconds (Practical Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Demand Flows Total HV veh/h \% |  | Arriva Total veh/h | Flows HV $\%$ | Deg. Satn v/c | Average Delay <br> sec | Level of Service | 95\% Back of Queue Vehicles Distance veh |  | Prop. Queued | Effective Average <br> Stop Speed <br> Rate <br> per veh km/h |  |
| South: Mamre Road (520m) mil |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 1 | 0.0 | 1 | 0.0 | 0.001 | 7.8 | LOS A | 0.0 | 0.1 | 0.25 | 0.56 | 52.7 |
| 2 | T1 | 2136 | 10.3 | 2136 | 10.3 | 0.880 | 37.7 | LOS C | 37.3 | 282.9 | 0.98 | 1.00 | 31.3 |
| 3 | R2 | 60 | 58.3 | 60 | 58.3 | 0.176 | 51.8 | LOS D | 1.4 | 14.3 | 0.92 | 0.73 | 28.8 |
| Appr | ach | 2197 | 11.6 | 2197 | 11.6 | 0.880 | 38.1 | LOS C | 37.3 | 282.9 | 0.98 | 0.99 | 31.2 |
| East: James Erskine Drive (170m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 172 | 8.3 | 172 | 8.3 | 0.190 | 8.6 | LOS A | 2.4 | 18.2 | 0.38 | 0.62 | 31.0 |
| 5 | T1 | 1 | 0.0 | 1 | 0.0 | 0.190 | 3.8 | LOS A | 2.4 | 18.2 | 0.38 | 0.62 | 47.6 |
| 6 | R2 | 221 | 17.3 | 221 | 17.3 | 0.849 | 63.0 | LOS E | 6.1 | 49.4 | 1.00 | 0.99 | 9.2 |
| Appr | ach | 394 | 13.4 | 394 | 13.4 | 0.849 | 39.1 | LOS C | 6.1 | 49.4 | 0.73 | 0.83 | 13.3 |
| North: Mamre Road ( 300 m ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 127 | 56.3 | 127 | 56.3 | 0.475 | 33.3 | LOS C | 9.3 | 83.6 | 0.77 | 0.79 | 32.3 |
| 8 | T1 | 1379 | 15.1 | 1379 | 15.1 | 0.613 | 27.4 | LOS B | 16.1 | 127.2 | 0.86 | 0.76 | 27.3 |
| 9 | R2 | 63 | 0.0 | 63 | 0.0 | 0.283 | 57.3 | LOS E | 1.6 | 11.0 | 0.99 | 0.72 | 27.5 |
| Appr | ach | 1569 | 17.9 | 1569 | 17.9 | 0.613 | 29.1 | LOS C | 16.1 | 127.2 | 0.86 | 0.76 | 27.8 |
| West: RoadName |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 94 | 0.0 | 94 | 0.0 | 0.124 | 16.2 | LOS B | 2.1 | 14.8 | 0.55 | 0.69 | 39.6 |
| 11 | T1 | 1 | 0.0 | 1 | 0.0 | 0.124 | 10.6 | LOS A | 2.1 | 14.8 | 0.55 | 0.69 | 43.2 |
| 12 | R2 | 115 | 0.0 | 115 | 0.0 | 0.772 | 59.9 | LOS E | 6.1 | 42.5 | 1.00 | 0.89 | 20.8 |
| Approach |  | 209 | 0.0 | 209 | 0.0 | 0.772 | 40.1 | LOS C | 6.1 | 42.5 | 0.80 | 0.80 | 26.5 |
| All V | hicles | 4369 | 13.5 | 4369 | 13.5 | 0.880 | 35.1 | LOS C | 37.3 | 282.9 | 0.91 | 0.89 | 28.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 0.0 \%
Number of Iterations: 5 (maximum specified: 10)

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Back Pedestrian ped | queue Distance m | Prop. Queued | Effective Stop Rate per ped |
| P1 | South Full Crossing | 1 | 44.2 | LOS E | 0.0 | 0.0 | 0.94 | 0.94 |
| P2 | East Full Crossing | 1 | 29.6 | LOS C | 0.0 | 0.0 | 0.77 | 0.77 |
| P3 | North Full Crossing | 53 | 44.3 | LOS E | 0.1 | 0.1 | 0.94 | 0.94 |
| P4 | West Full Crossing | 53 | 44.3 | LOS E | 0.1 | 0.1 | 0.94 | 0.94 |
| All Pedestrians |  | 107 | 44.1 | LOS E |  |  | 0.94 | 0.94 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.

Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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Project: C:IUsers\Alireza RasoulilDesktoplCopies of SIDRA for Mamrel290518\Finals\2036 Base Casel2036 Base Case - Three Lanes VAG0584m05v01 Mamre_2036 Basecase - Final - With Improvements.sip7

## SITE LAYOUT

## Site: 102 [[2036 Base] Mamre Road x Erskine Park Road_AM - IMPROVED]

Mamre Road x Erskine Park Road
2036 Base
Signals - Fixed Time Isolated


## MOVEMENT SUMMARY

日 Site： 102 ［［2036 Base］Mamre Road x Erskine Park

审审 Network：N101［2036 Base Case－AM－IMPORVED EPR］ Road AM－IMPROVED］ $\qquad$
Mamre Road x Erskine Park Road
2036 Base
Signals－Fixed Time Coordinated Cycle Time＝ 100 seconds（Network Cycle Time－User－Given）


Site Level of Service（LOS）Method：Delay（RTA NSW）．Site LOS Method is specified in the Network Data dialog（Network tab）． Vehicle movement LOS values are based on average delay per movement．
Intersection and Approach LOS values are based on average delay for all vehicle movements．
SIDRA Standard Delay Model is used．Control Delay includes Geometric Delay．
Gap－Acceptance Capacity：SIDRA Standard（Akçelik M3D）．
HV（\％）values are calculated for All Movement Classes of All Heavy Vehicle Model Designation．
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations： 0.0 \％ Number of Iterations： 5 （maximum specified：10）

| Movement Performance－Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | Description | Demand Flow ped／h | Average Delay sec | Level of Service | Average Bac Pedestrian ped | of Queue Distance m | Prop． Queued | Effective Stop Rate per ped |
| P1 | South Full Crossing | 1 | 44.2 | LOS E | 0.0 | 0.0 | 0.94 | 0.94 |
| P2 | East Full Crossing | 1 | 36.1 | LOS D | 0.0 | 0.0 | 0.85 | 0.85 |
| P2S | East Slip／Bypass Lane | 53 | 30.5 | LOS D | 0.1 | 0.1 | 0.78 | 0.78 |
|  | Crossing |  |  |  |  |  |  |  |
| P3 | North Full Crossing | 1 | 44.2 | LOS E | 0.0 | 0.0 | 0.94 | 0.94 |
| All Pedestrians |  | 56 | 31.1 | LOS D |  |  | 0.79 | 0.79 |

Level of Service（LOS）Method：SIDRA Pedestrian LOS Method（Based on Average Delay）
Pedestrian movement LOS values are based on average delay per pedestrian movement．
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements．

[^9]
## MOVEMENT SUMMARY

Site: 102 [[2036 Base] Mamre Road x Erskine Park
审审 Network: N101 [2036 Base Case - PM - IMPROVED EPR] Road_PM - IMPROVED] $\qquad$
Mamre Road x Erskine Park Road
2036 Base
Signals - Fixed Time Coordinated Cycle Time = 100 seconds (Network Cycle Time - User-Given)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Arrival Total veh/h | Flows HV \% | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles <br> veh | of Queue Distance | Prop. Queued | Effective Stop Rate per veh | lerage peed <br> km/h |
| South: Mamre Road (300m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | T1 | 1355 | 8.5 | 1355 | 8.5 | 0.317 | 3.7 | LOS A | 6.6 | 49.4 | 0.33 | 0.29 | 63.8 |
| 3 | R2 | 1080 | 11.1 | 1080 | 11.1 | 0.551 | 21.9 | LOS B | 16.4 | 125.7 | 0.68 | 0.80 | 47.7 |
| Appr | ach | 2435 | 9.6 | 2435 | 9.6 | 0.551 | 11.8 | LOS A | 16.4 | 125.7 | 0.48 | 0.52 | 51.7 |
| East: Erskine Park Road (590m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 728 | 24.8 | 728 | 24.8 | 0.370 | 12.4 | LOS A | 7.4 | 63.0 | 0.37 | 0.71 | 55.7 |
| 6 | R2 | 342 | 7.7 | 342 | 7.7 | 0.888 | 66.7 | LOS E | 9.7 | 72.7 | 1.00 | 0.97 | 23.4 |
| Appr | ach | 1071 | 19.3 | 1071 | 19.3 | 0.888 | 29.8 | LOS C | 9.7 | 72.7 | 0.57 | 0.79 | 38.7 |
| North: Mamre Road (200m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 24 | 10.8 | 24 | 10.8 | 0.621 | 38.1 | LOS C | 6.6 | 50.8 | 0.98 | 0.82 | 39.3 |
| 8 | T1 | 841 | 12.4 | 841 | 12.4 | 0.904 | 54.3 | LOS D | 13.2 | 102.6 | 1.00 | 0.98 | 12.4 |
| Approach |  | 865 | 12.4 | 865 | 12.4 | 0.904 | 53.9 | LOS D | 13.2 | 102.6 | 1.00 | 0.98 | 13.3 |
| All Vehicles |  | 4371 | 12.6 | 4371 | 12.6 | 0.904 | 24.5 | LOS B | 16.4 | 125.7 | 0.61 | 0.68 | 38.1 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 0.0 \% Number of Iterations: 5 (maximum specified: 10)

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Bac Pedestrian ped | queue Distance m | Prop. Queued | Effective Stop Rate per ped |
| P1 | South Full Crossing | 1 | 44.2 | LOS E | 0.0 | 0.0 | 0.94 | 0.94 |
| P2 | East Full Crossing | 1 | 44.2 | LOS E | 0.0 | 0.0 | 0.94 | 0.94 |
| P2S | East Slip/Bypass Lane Crossing | 53 | 40.6 | LOS E | 0.1 | 0.1 | 0.90 | 0.90 |
| P3 | North Full Crossing | 1 | 44.2 | LOS E | 0.0 | 0.0 | 0.94 | 0.94 |
| All Pedestrians |  | 56 | 40.8 | LOS E |  |  | 0.90 | 0.90 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

[^10]
## SITE LAYOUT

STOF Site: 101 [[2036 Base] Mamre Road x Mandalong Close_AM]
Mamre Road x Mandalong Close
2036 Base
Stop (Two-Way)
4N

## MOVEMENT SUMMARY

Site: 101 [[2036 Base] Mamre Road x Mandalong Close_AM]
蚄 Network: N101 [2036 Base Case - AM - IMPORVED EPR]
Mamre Road x Mandalong Close
2036 Base
Stop (Two-Way)


Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 0.0 \%
Number of Iterations: 5 (maximum specified: 10)

## MOVEMENT SUMMARY

Site: 101 [[2036 Base] Mamre Road x Mandalong Close_PM]
它审 Network: N101 [2036 Base Case - PM - IMPROVED EPR]
Mamre Road x Mandalong Close
2036 Base
Stop (Two-Way)


Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 0.0 \%
Number of Iterations: 5 (maximum specified: 10)

## Appendix D4

## Existing + SSDA SIDRA Results

## SITE LAYOUT

Site: 104 [[Existing+Dev] Mamre Road x Bakers Lane_AM]
Mamre Road x Bakers Lane
2018 Existing + Dev
Signals - Fixed Time Coordinated

## 2 N



Project: C:IUsers\Alireza Rasouli\Downloads\AG0584m03 Mamre_Existing+SSDA1 Dev.sip7

MOVEMENT SUMMARY
Site: 104 [[Existing+Dev] Mamre Road x Bakers Lane_AM]
Mamre Road x Bakers Lane
2018 Existing + Dev
Signals - Fixed Time Coordinated Cycle Time = 140 seconds (Practical Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Demano Total veh/h | $\begin{gathered} \text { =lows } \\ \text { HV } \\ \% \end{gathered}$ | Arrival Total veh/h | $\begin{aligned} & \text { Flows } \\ & \text { HV } \\ & \% \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Mamre Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 115 | 0.0 | 115 | 0.0 | 0.085 | 11.3 | LOS A | 2.2 | 15.4 | 0.31 | 0.65 | 49.5 |
| 2 | T1 | 778 | 11.6 | 778 | 11.6 | 0.897 | 36.4 | LOS C | 49.5 | 381.3 | 0.92 | 0.91 | 31.1 |
| 3 | R2 | 80 | 0.0 | 80 | 0.0 | 0.431 | 72.5 | LOS F | 5.2 | 36.2 | 0.96 | 0.77 | 27.7 |
| Appr |  | 973 | 9.3 | 973 | 9.3 | 0.897 | 36.4 | LOS C | 49.5 | 381.3 | 0.85 | 0.86 | 33.0 |
| East: Bakers Lane ( 440 m ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 43 | 0.0 | 43 | 0.0 | 0.142 | 58.7 | LOS E | 2.6 | 18.0 | 0.89 | 0.73 | 30.8 |
| 5 | T1 | 1 | 0.0 | 1 | 0.0 | 0.142 | 53.2 | LOS D | 2.6 | 18.0 | 0.89 | 0.73 | 29.7 |
| 6 | R2 | 392 | 0.3 | 392 | 0.3 | 0.907 | 69.0 | LOS E | 28.4 | 199.2 | 1.00 | 0.96 | 17.0 |
| Appr |  | 436 | 0.2 | 436 | 0.2 | 0.907 | 68.0 | LOS E | 28.4 | 199.2 | 0.99 | 0.94 | 18.6 |
| North: Mamre Road (750m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 627 | 0.2 | 624 | 0.2 | 0.462 | 15.1 | LOS B | 17.0 | 119.2 | 0.44 | 0.76 | 55.9 |
| 8 | T1 | 609 | 18.0 | 607 | 18.0 | 0.726 | 31.0 | LOS C | 32.7 | 264.2 | 0.86 | 0.78 | 51.8 |
| 9 | R2 | 191 | 0.0 | 190 | 0.0 | 1.021 | 127.7 | LOS F | 18.5 | 129.4 | 1.00 | 1.10 | 22.0 |
| Appr |  | 1427 | 7.7 | $1420{ }^{\text {N1 }}$ | 7.8 | 1.021 | 36.9 | LOS C | 32.7 | 264.2 | 0.70 | 0.81 | 44.9 |
| West: Bakers lane |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 78 | 0.0 | 78 | 0.0 | 0.242 | 59.0 | LOS E | 4.7 | 32.6 | 0.90 | 0.76 | 20.7 |
| 11 | T1 | 1 | 0.0 | 1 | 0.0 | 0.242 | 53.4 | LOS D | 4.7 | 32.6 | 0.90 | 0.76 | 29.6 |
| 12 | R2 | 54 | 0.0 | 54 | 0.0 | 0.121 | 44.5 | LOS D | 2.7 | 18.6 | 0.82 | 0.73 | 34.2 |
| Approach |  | 133 | 0.0 | 133 | 0.0 | 0.242 | 53.1 | LOS D | 4.7 | 32.6 | 0.87 | 0.75 | 26.8 |
| All V | icles | 2968 | 6.8 | $2961{ }^{\text {N1 }}$ | 6.8 | 1.021 | 42.0 | LOS C | 49.5 | 381.3 | 0.80 | 0.85 | 36.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 0.0 \%
Number of Iterations: 7 (maximum specified: 10)
N1 Arrival Flow value is reduced due to capacity constraint at oversaturated upstream lanes.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Back Pedestrian ped | of Queue Distance m | Prop. Queued | Effective Stop Rate per ped |
| P1 | South Full Crossing | 11 | 64.2 | LOS F | 0.0 | 0.0 | 0.96 | 0.96 |
| P2 | East Full Crossing | 11 | 22.9 | LOS C | 0.0 | 0.0 | 0.57 | 0.57 |
| P3 | North Full Crossing | 11 | 64.2 | LOS F | 0.0 | 0.0 | 0.96 | 0.96 |
| P4 | West Full Crossing | 11 | 22.9 | LOS C | 0.0 | 0.0 | 0.57 | 0.57 |


| All Pedestrians | 42 | 43.5 | LOS E | 0.76 |
| :--- | :--- | :--- | :--- | :--- |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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日 Site： 104 ［［Existing＋Dev］Mamre Road x Bakers Lane＿PM］
Mamre Road x Bakers Lane
2018 Existing＋Dev
Signals－Fixed Time Coordinated Cycle Time $=140$ seconds（Practical Cycle Time）

| Movement Performance－Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Demand Total veh／h | Flows HV \％ | Arriva Total veh／h | Flows HV \％ | Deg． Satn v／c | Average Delay sec | Level of Service | 95\％Back Vehicles <br> veh | of Queue Distance m | Prop． Queued | Effective Stop Rate per veh | verage peed <br> km／h |
| South：Mamre Road（500m） |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 16 | 0.0 | 16 | 0.0 | 0.033 | 46.7 | LOS D | 0.8 | 5.6 | 0.78 | 0.69 | 33.4 |
| 2 | T1 | 687 | 12.4 | 687 | 12.4 | 0.784 | 25.0 | LOS B | 33.2 | 257.0 | 0.78 | 0.71 | 38.4 |
| 3 | R2 | 26 | 0.0 | 26 | 0.0 | 0.331 | 81.5 | LOS F | 1.8 | 12.9 | 0.99 | 0.71 | 25.8 |
| Appr | ach | 729 | 11.7 | 729 | 11.7 | 0.784 | 27.5 | LOS B | 33.2 | 257.0 | 0.78 | 0.71 | 37.0 |
| East：Bakers Lane（440m） |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 52 | 0.0 | 52 | 0.0 | 0.231 | 65.5 | LOS E | 3.3 | 23.0 | 0.94 | 0.75 | 29.0 |
| 5 | T1 | 1 | 0.0 | 1 | 0.0 | 0.231 | 60.0 | LOS E | 3.3 | 23.0 | 0.94 | 0.75 | 28.0 |
| 6 | R2 | 513 | 0.4 | 513 | 0.4 | 0.947 | 77.1 | LOS F | 40.9 | 287.2 | 1.00 | 1.01 | 15.7 |
| Appr | ach | 565 | 0.4 | 565 | 0.4 | 0.947 | 76.0 | LOS F | 40.9 | 287.2 | 0.99 | 0.98 | 17.1 |
| North：Mamre Road（750m） |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 180 | 1.2 | 180 | 1.2 | 0.270 | 30.3 | LOS C | 7.8 | 55.1 | 0.69 | 0.78 | 46.7 |
| 8 | T1 | 893 | 12.4 | 893 | 12.4 | 1.095 | 157.6 | LOS F | 112.1 | 867.7 | 1.00 | 1.57 | 20.9 |
| 9 | R2 | 81 | 0.0 | 81 | 0.0 | 1.018 | 125.8 | LOS F | 7.7 | 53.7 | 1.00 | 1.09 | 22.2 |
| Appr |  | 1154 | 9.8 | 1154 | 9.8 | 1.095 | 135.5 | LOS F | 112.1 | 867.7 | 0.95 | 1.42 | 22.9 |
| West：Bakers lane |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 111 | 0.0 | 111 | 0.0 | 0.493 | 68.1 | LOS E | 7.3 | 51.3 | 0.98 | 0.79 | 18.8 |
| 11 | T1 | 2 | 0.0 | 2 | 0.0 | 0.493 | 62.5 | LOS E | 7.3 | 51.3 | 0.98 | 0.79 | 27.5 |
| 12 | R2 | 223 | 0.0 | 223 | 0.0 | 0.423 | 42.9 | LOS D | 11.4 | 79.6 | 0.87 | 0.80 | 34.7 |
| Approach |  | 336 | 0.0 | 336 | 0.0 | 0.493 | 51.3 | LOS D | 11.4 | 79.6 | 0.90 | 0.80 | 29.6 |
| All Vehicles |  | 2784 | 7.2 | 2784 | 7.2 | 1.095 | 85.0 | LOS F | 112.1 | 867.7 | 0.91 | 1.07 | 24.1 |

Site Level of Service（LOS）Method：Delay（RTA NSW）．Site LOS Method is specified in the Network Data dialog（Network tab）． Vehicle movement LOS values are based on average delay per movement． Intersection and Approach LOS values are based on average delay for all vehicle movements．
SIDRA Standard Delay Model is used．Control Delay includes Geometric Delay．
Gap－Acceptance Capacity：SIDRA Standard（Akçelik M3D）．
HV（\％）values are calculated for All Movement Classes of All Heavy Vehicle Model Designation．
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations： 0.9 \％
Number of Iterations： 9 （maximum specified：10）

| Movement Performance－Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | Description | Demand Flow ped／h | Average Delay sec | Level of Service | Average Back Pedestrian ped | f Queue Distance m | Prop． Queued | Effective Stop Rate per ped |
| P1 | South Full Crossing | 53 | 64.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 |
| P2 | East Full Crossing | 53 | 22.3 | LOS C | 0.1 | 0.1 | 0.57 | 0.57 |
| P3 | North Full Crossing | 11 | 64.2 | LOS F | 0.0 | 0.0 | 0.96 | 0.96 |
| P4 | West Full Crossing | 11 | 22.3 | LOS C | 0.0 | 0.0 | 0.56 | 0.56 |
| All Pedestrians |  | 126 | 43.3 | LOS E |  |  | 0.76 | 0.76 |

Level of Service（LOS）Method：SIDRA Pedestrian LOS Method（Based on Average Delay）
Pedestrian movement LOS values are based on average delay per pedestrian movement．

Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## SITE LAYOUT

Site: 105v [[Existing+Dev] Mamre Road x Mamre west precicnt _PM]
Mamre Road x Mamre west precicnt
2018 Existing
Signals - Fixed Time Isolated


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Project: C:\Users\Alireza Rasouli\Downloads\AG0584m03 Mamre_Existing+SSDA1 Dev.sip7

## MOVEMENT SUMMARY

B Site: 105v
[[Existing+Dev] Mamre Road x Mamre west precicnt_AM] $\qquad$ +Dev - AM]

Mamre Road x Mamre west precicnt 2018 Existing
Signals - Fixed Time Isolated Cycle Time = 50 seconds (Practical Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Demand Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \\ \hline \end{gathered}$ | Arrival Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \end{gathered}$ | $\begin{aligned} & \text { Deg. } \\ & \text { Satn } \\ & \text { v/c } \end{aligned}$ | Average Delay sec | Level of Service | 95\% Back <br> Vehicles <br> veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed $\mathrm{km} / \mathrm{h}$ |
| South: Mamre Road ( 750 m ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 35 | 0.0 | 35 | 0.0 | 0.836 | 28.8 | LOS C | 17.0 | 126.6 | 0.96 | 0.99 | 52.1 |
| 2 | T1 | 1213 | 7.6 | 1213 | 7.6 | 0.836 | 21.3 | LOS B | 17.0 | 126.6 | 0.97 | 0.99 | 49.1 |
| Appr |  | 1247 | 7.3 | 1247 | 7.3 | 0.836 | 21.5 | LOS B | 17.0 | 126.6 | 0.97 | 0.99 | 49.3 |
| North: Mamre Road (520m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 | T1 | 1433 | 7.5 | 1425 | 7.5 | 0.634 | 5.7 | LOS A | 11.3 | 84.2 | 0.63 | 0.57 | 64.5 |
| 9 | R2 | 57 | 0.0 | 57 | 0.0 | 0.254 | 30.0 | LOS C | 1.3 | 9.4 | 0.94 | 0.74 | 43.3 |
| Appr |  | 1489 | 7.2 | $1482{ }^{\text {N1 }}$ | 7.2 | 0.634 | 6.7 | LOS A | 11.3 | 84.2 | 0.64 | 0.57 | 62.3 |
| West: Mamre west precicnt Site Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 18 | 0.0 | 18 | 0.0 | 0.089 | 15.3 | LOS B | 0.4 | 2.5 | 0.84 | 0.70 | 40.2 |
| 12 | R2 | 12 | 0.0 | 12 | 0.0 | 0.089 | 15.2 | LOS B | 0.4 | 2.5 | 0.84 | 0.70 | 40.2 |
| Approach |  | 29 | 0.0 | 29 | 0.0 | 0.089 | 15.3 | LOS B | 0.4 | 2.5 | 0.84 | 0.70 | 40.2 |
| All Vehicles |  | 2766 | 7.2 | $2759{ }^{\text {N1 }}$ | 7.2 | 0.836 | 13.5 | LOS A | 17.0 | 126.6 | 0.79 | 0.76 | 54.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 0.0 \%
Number of Iterations: 7 (maximum specified: 10)
N1 Arrival Flow value is reduced due to capacity constraint at oversaturated upstream lanes.

Movement Performance - Pedestrians

| Mov <br> ID | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Back Pedestrian ped | queue Distance m | Prop. Queued | Effective Stop Rate per ped |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P3 | North Full Crossing | 11 | 19.4 | LOS B | 0.0 | 0.0 | 0.88 | 0.88 |
| P4 | West Full Crossing | 11 | 5.3 | LOS A | 0.0 | 0.0 | 0.46 | 0.46 |
| All P | estrians | 21 | 12.3 | LOS B |  |  | 0.67 | 0.67 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

## MOVEMENT SUMMARY

B Site: 105v [[Existing+Dev] Mamre Road x Mamre west precicnt PM] $\qquad$ +Dev - PM]

Mamre Road x Mamre west precicnt
2018 Existing
Signals - Fixed Time Isolated Cycle Time $=50$ seconds (Practical Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Demand Flows Total HV veh/h eh/h \% |  | Arrival FlowsTotal HV |  | Deg. Satn v/c | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Average Stop Speed Rate |  |
|  |  |  |  | Vehicles | Distance |  |  |  |  |  |  |
|  |  |  |  |  | \% |  |  |  | veh | m |  | Rate oer veh | km/h |
| South: Mamre Road (750m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 12 | 0.0 |  |  | 12 | 0.0 | 0.884 | 33.9 | LOS C | 20.5 | 151.4 | 0.99 | 1.08 | 49.4 |
| 2 | T1 | 1311 | 6.7 | 1311 | 6.7 | 0.884 | 26.2 | LOS B | 20.5 | 151.4 | 0.99 | 1.08 | 45.2 |
| Appr |  | 1322 | 6.6 | 1322 | 6.6 | 0.884 | 26.3 | LOS B | 20.5 | 151.4 | 0.99 | 1.08 | 45.3 |
| North: Mamre Road (520m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 | T1 | 1203 | 13.6 | 1203 | 13.6 | 0.615 | 5.6 | LOS A | 8.6 | 66.9 | 0.62 | 0.55 | 64.7 |
| 9 | R2 | 20 | 0.0 | 20 | 0.0 | 0.090 | 29.2 | LOS C | 0.5 | 3.2 | 0.92 | 0.70 | 43.7 |
| Appr | ch | 1223 | 13.3 | 1223 | 13.3 | 0.615 | 6.0 | LOS A | 8.6 | 66.9 | 0.62 | 0.55 | 63.7 |
| West: Mamre west precicnt Site Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 58 | 0.0 | 58 | 0.0 | 0.303 | 16.2 | LOS B | 1.3 | 8.9 | 0.89 | 0.75 | 39.5 |
| 12 | R2 | 36 | 0.0 | 36 | 0.0 | 0.303 | 16.1 | LOS B | 1.3 | 8.9 | 0.89 | 0.75 | 39.5 |
| Approach |  | 94 | 0.0 | 94 | 0.0 | 0.303 | 16.2 | LOS B | 1.3 | 8.9 | 0.89 | 0.75 | 39.5 |
| All V | icles | 2639 | 9.5 | 2639 | 9.5 | 0.884 | 16.5 | LOS B | 20.5 | 151.4 | 0.82 | 0.82 | 50.7 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 0.9 \%
Number of Iterations: 9 (maximum specified: 10)

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Back Pedestrian ped | Queue Distance m | Prop. Queued | Effective Stop Rate per ped |
| P3 | North Full Crossing | 11 | 19.4 | LOS B | 0.0 | 0.0 | 0.88 | 0.88 |
| P4 | West Full Crossing | 11 | 5.3 | LOS A | 0.0 | 0.0 | 0.46 | 0.46 |
| All Pedestrians |  | 21 | 12.3 | LOS B |  |  | 0.67 | 0.67 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

## SITE LAYOUT

## Site: 103 [[Existing+Dev] Mamre Road x James Erskine Drive_PM]

Mamre Road x James Erskine Drive
2018 Existing + Dev
Signals - Fixed Time Isolated


## MOVEMENT SUMMARY

日 Site： 103 ［［Existing＋Dev］Mamre Road x James Erskine


Mamre Road x James Erskine Drive
2018 Existing＋Dev
Signals－Fixed Time Isolated Cycle Time $=60$ seconds（User－Given Cycle Time）

| Movement Performance－Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | $\begin{aligned} & \text { Demand } \\ & \text { Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Arrival Total veh／h | $\begin{aligned} & \text { Flows } \\ & \text { HV } \\ & \% \end{aligned}$ | Deg． Satn v／c | Average Delay sec | Level of Service | 95\％Back Vehicles veh | of Queue Distance m | Prop． Queued | Effective Stop Rate per veh | Average Speed km／h |
| South：Mamre Road（520m） |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | T1 | 1089 | 6.5 | 1089 | 6.5 | 0.590 | 4.5 | LOS A | 11.6 | 85.5 | 0.50 | 0.45 | 67.4 |
| 3 | R2 | 86 | 22.0 | 86 | 22.0 | 0.538 | 37.8 | LOS C | 2.7 | 22.1 | 0.99 | 0.78 | 33.7 |
| Appr |  | 1176 | 7.6 | 1176 | 7.6 | 0.590 | 7.0 | LOS A | 11.6 | 85.5 | 0.54 | 0.48 | 61.6 |
| East：James Erskine Drive（170m） |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 33 | 54.8 | 33 | 54.8 | 0.181 | 14.9 | LOS B | 1.0 | 10.7 | 0.74 | 0.70 | 24.3 |
| 6 | R2 | 87 | 54.2 | 87 | 54.2 | 0.429 | 28.2 | LOS B | 1.7 | 17.8 | 0.90 | 0.73 | 16.5 |
| Appr |  | 120 | 54.4 | 120 | 54.4 | 0.429 | 24.6 | LOS B | 1.7 | 17.8 | 0.85 | 0.73 | 18.1 |
| North：Mamre Road（300m） |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 276 | 17.9 | 274 | 18.0 | 0.223 | 8.9 | LOS A | 1.5 | 12.3 | 0.32 | 0.68 | 49.7 |
| 8 | T1 | 1457 | 6.1 | 1449 | 6.2 | 0.879 | 19.5 | LOS B | 28.2 | 208.0 | 0.89 | 0.89 | 33.8 |
| Approach |  | 1733 | 8.0 | $1724{ }^{\text {N1 }}$ | 8.0 | 0.879 | 17.8 | LOS B | 28.2 | 208.0 | 0.80 | 0.86 | 36.4 |
| All Vehicles |  | 3028 | 9.7 | $3019{ }^{\text {N1 }}$ | 9.7 | 0.879 | 13.8 | LOS A | 28.2 | 208.0 | 0.70 | 0.71 | 45.0 |

Site Level of Service（LOS）Method：Delay（RTA NSW）．Site LOS Method is specified in the Network Data dialog（Network tab）． Vehicle movement LOS values are based on average delay per movement．
Intersection and Approach LOS values are based on average delay for all vehicle movements．
SIDRA Standard Delay Model is used．Control Delay includes Geometric Delay．
Gap－Acceptance Capacity：SIDRA Standard（Akçelik M3D）．
HV（\％）values are calculated for All Movement Classes of All Heavy Vehicle Model Designation．
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations： 0.0 \％
Number of Iterations： 7 （maximum specified：10）
N1 Arrival Flow value is reduced due to capacity constraint at oversaturated upstream lanes．

Movement Performance－Pedestrians

| Mov ID | Description | Demand Flow ped／h | Average Delay sec | Level of Service | Average Back Pedestrian ped | queue Distance $\qquad$ | Prop． Queued | Effective Stop Rate per ped |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P1 | South Full Crossing | 1 | 24.3 | LOS C | 0.0 | 0.0 | 0.90 | 0.90 |
| P2 | East Full Crossing | 1 | 13.3 | LOS B | 0.0 | 0.0 | 0.67 | 0.67 |
| All Pedestrians |  | 2 | 18.8 | LOS B |  |  | 0.78 | 0.78 |

Level of Service（LOS）Method：SIDRA Pedestrian LOS Method（Based on Average Delay） Pedestrian movement LOS values are based on average delay per pedestrian movement． Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements．

## MOVEMENT SUMMARY

Site: 103 [[Existing+Dev] Mamre Road x James Erskine

Mamre Road x James Erskine Drive
2018 Existing + Dev
Signals - Fixed Time Isolated Cycle Time $=80$ seconds (User-Given Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Demand Flows Total HV veh/h eh/h \% |  | Arrival FlowsTotal HV |  | Deg. Satn v/c | Average Delay | Level of Service | 95\% Back of Queue |  | Prop. Queued | Effective Average Stop Speed |  |
|  |  |  |  | Vehicles | Distance |  |  |  |  |  |  |
|  |  |  |  |  | \% |  |  |  | veh | m |  | Rate | km/h |
| South: Mamre Road (520m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | T1 | 1075 | 8.1 |  |  | 1075 | 8.1 | 0.645 | 8.7 | LOS A | 18.2 | 136.5 | 0.61 | 0.55 | 58.7 |
| 3 | R2 | 25 | 58.3 | 25 | 58.3 | 0.257 | 49.2 | LOS D | 1.0 | 10.7 | 0.98 | 0.72 | 29.2 |
| Appro |  | 1100 | 9.3 | 1100 | 9.3 | 0.645 | 9.7 | LOS A | 18.2 | 136.5 | 0.62 | 0.55 | 57.0 |
| East: James Erskine Drive (170m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 101 | 8.3 | 101 | 8.3 | 0.266 | 12.5 | LOS A | 2.9 | 22.7 | 0.63 | 0.71 | 26.3 |
| 6 | R2 | 285 | 17.3 | 285 | 17.3 | 0.632 | 31.3 | LOS C | 8.1 | 65.3 | 0.88 | 0.80 | 15.2 |
| Appro |  | 386 | 15.0 | 386 | 15.0 | 0.632 | 26.4 | LOS B | 8.1 | 65.3 | 0.82 | 0.78 | 17.1 |
| North: Mamre Road (300m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 133 | 56.3 | 133 | 56.3 | 0.121 | 8.9 | LOS A | 0.5 | 5.4 | 0.19 | 0.64 | 49.5 |
| 8 | T1 | 1122 | 13.8 | 1122 | 13.8 | 0.732 | 16.9 | LOS B | 20.1 | 157.2 | 0.81 | 0.73 | 36.6 |
| Approach |  | 1255 | 18.3 | 1255 | 18.3 | 0.732 | 16.0 | LOS B | 20.1 | 157.2 | 0.75 | 0.72 | 38.1 |
| All Ve | icles | 2741 | 14.2 | 2741 | 14.2 | 0.732 | 14.9 | LOS B | 20.1 | 157.2 | 0.70 | 0.66 | 42.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 0.9 \%
Number of Iterations: 9 (maximum specified: 10)

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Description | Demand Flow ped $/ \mathrm{h}$ | Average Delay $\qquad$ sec | Level of Service | Average Back Pedestrian $\qquad$ | of Queue Distance $\qquad$ m | Prop. Queued | Effective Stop Rate per ped |
| P1 | South Full Crossing | 1 | 34.2 | LOS D | 0.0 | 0.0 | 0.93 | 0.93 |
| P2 | East Full Crossing | 1 | 16.3 | LOS B | 0.0 | 0.0 | 0.64 | 0.64 |
| All Pedestrians |  | 2 | 25.2 | LOS C |  |  | 0.78 | 0.78 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

## SITE LAYOUT

Site: 102 [[Existing+Dev] Mamre Road x Erskine Park Road_PM]
Mamre Road x Erskine Park Road
2018 Existing + Dev
Signals - Fixed Time Isolated


SIDRA INTERSECTION 7.0 | Copyright © 2000-2017 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: ASON GROUP PTY LTD | Created: Tuesday, 29 May 2018 8:45:20 AM
Project: C:IUsers\Alireza Rasouli\Downloads\AG0584m03 Mamre_Existing+SSDA1 Dev.sip7

## MOVEMENT SUMMARY

Site: 102 [[Existing+Dev] Mamre Road x Erskine Park
$\qquad$
Mamre Road x Erskine Park Road
2018 Existing + Dev
Signals - Fixed Time Isolated Cycle Time $=80$ seconds (User-Given Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Deman Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Arrival Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Mamre Road (300m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | T1 | 547 | 9.2 | 547 | 9.2 | 0.418 | 5.0 | LOS A | 8.7 | 65.4 | 0.44 | 0.39 | 59.1 |
| 3 | R2 | 621 | 12.0 | 621 | 12.0 | 0.764 | 41.5 | LOS C | 12.4 | 95.6 | 0.99 | 0.89 | 36.4 |
| Appr |  | 1168 | 10.7 | 1168 | 10.7 | 0.764 | 24.4 | LOS B | 12.4 | 95.6 | 0.73 | 0.66 | 40.1 |
| East: Erskine Park Road (590m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 739 | 10.5 | 739 | 10.5 | 0.956 | 60.1 | LOS E | 42.2 | 321.8 | 1.00 | 1.07 | 25.0 |
| 6 | R2 | 187 | 14.0 | 187 | 14.0 | 0.811 | 49.8 | LOS D | 8.1 | 63.6 | 1.00 | 0.91 | 28.4 |
| Appr |  | 926 | 11.3 | 926 | 11.3 | 0.956 | 58.0 | LOS E | 42.2 | 321.8 | 1.00 | 1.03 | 25.6 |
| North: Mamre Road (200m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 553 | 4.4 | 548 | 4.4 | 0.811 | 19.1 | LOS B | 21.3 | 155.6 | 0.83 | 0.89 | 51.4 |
| 8 | T1 | 978 | 5.7 | 969 | 5.7 | 0.811 | 21.4 | LOS B | 23.4 | 171.6 | 0.91 | 0.90 | 23.9 |
| Approach |  | 1531 | 5.2 | $1517{ }^{\text {N1 }}$ | 5.2 | 0.811 | 20.5 | LOS B | 23.4 | 171.6 | 0.88 | 0.90 | 37.5 |
| All Vehicles |  | 3625 | 8.5 | $3611{ }^{\text {N1 }}$ | 8.6 | 0.956 | 31.4 | LOS C | 42.2 | 321.8 | 0.86 | 0.86 | 33.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 0.0 \%
Number of Iterations: 7 (maximum specified: 10)
N1 Arrival Flow value is reduced due to capacity constraint at oversaturated upstream lanes.

Movement Performance - Pedestrians

| Mov ID | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Back Pedestrian ped | of Queue Distance m | Prop. Queued | Effective Stop Rate per ped |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P1 | South Full Crossing | 1 | 34.2 | LOS D | 0.0 | 0.0 | 0.93 | 0.93 |
| P2 | East Full Crossing | 1 | 21.8 | LOS C | 0.0 | 0.0 | 0.74 | 0.74 |
| P3 | North Full Crossing | 1 | 34.2 | LOS D | 0.0 | 0.0 | 0.93 | 0.93 |
| All P | estrians | 3 | 30.1 | LOS D |  |  | 0.86 | 0.86 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

## MOVEMENT SUMMARY

日 Site： 102 ［［Existing＋Dev］Mamre Road x Erskine Park

Mamre Road x Erskine Park Road
2018 Existing＋Dev
Signals－Fixed Time Isolated Cycle Time $=100$ seconds（User－Given Cycle Time）

| Movement Performance－Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov OD ID Mov | Demand Total <br> veh／h | Flows HV \％ | Arrival Total | Flows HV $\%$ | Deg． Satn v／c | Average Delay | Level of Service | 95\％Back Vehicles | of Queue Distance | Prop． Queued | Effective Stop Rate | erage peed km／h |
| South：Mamre Road（300m） |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 694 | 7.3 | 694 | 7.3 | 0.654 | 15.7 | LOS B | 23.0 | 171.0 | 0.74 | 0.67 | 38.0 |
| 3 R2 | 716 | 10.0 | 716 | 10.0 | 0.794 | 48.7 | LOS D | 17.7 | 134.5 | 0.99 | 0.90 | 34.0 |
| Approach | 1409 | 8.7 | 1409 | 8.7 | 0.794 | 32.5 | LOS C | 23.0 | 171.0 | 0.87 | 0.79 | 34.9 |
| East：Erskine Park Road（590m） |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 707 | 22.8 | 707 | 22.8 | 0.706 | 20.6 | LOS B | 22.9 | 191.4 | 0.72 | 0.84 | 46.0 |
| 6 R2 | 436 | 7.7 | 436 | 7.7 | 0.803 | 45.5 | LOS D | 21.2 | 158.4 | 0.98 | 0.90 | 30.0 |
| Approach | 1143 | 17.0 | 1143 | 17.0 | 0.803 | 30.1 | LOS C | 22.9 | 191.4 | 0.82 | 0.86 | 38.2 |
| North：Mamre Road（200m） |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 195 | 10.8 | 195 | 10.8 | 0.668 | 21.3 | LOS B | 9.7 | 74.8 | 0.88 | 0.80 | 48.7 |
| 8 T1 | 542 | 11.7 | 542 | 11.7 | 0.668 | 26.8 | LOS B | 13.5 | 104.2 | 0.92 | 0.81 | 20.6 |
| Approach | 737 | 11.4 | 737 | 11.4 | 0.668 | 25.3 | LOS B | 13.5 | 104.2 | 0.91 | 0.81 | 30.8 |
| All Vehicles | 3289 | 12.2 | 3289 | 12.2 | 0.803 | 30.0 | LOS C | 23.0 | 191.4 | 0.86 | 0.82 | 35.3 |

Site Level of Service（LOS）Method：Delay（RTA NSW）．Site LOS Method is specified in the Network Data dialog（Network tab）． Vehicle movement LOS values are based on average delay per movement．
Intersection and Approach LOS values are based on average delay for all vehicle movements．
SIDRA Standard Delay Model is used．Control Delay includes Geometric Delay．
Gap－Acceptance Capacity：SIDRA Standard（Akçelik M3D）．
HV（\％）values are calculated for All Movement Classes of All Heavy Vehicle Model Designation．
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations： 0.9 \％ Number of Iterations： 9 （maximum specified：10）

| Movement Performance－Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | Description | Demand Flow ped／h | Average Delay sec | Level of Service | Average Bac Pedestrian ped | of Queue Distance m | Prop． Queued | Effective Stop Rate per ped |
| P1 | South Full Crossing | 1 | 33.6 | LOS D | 0.0 | 0.0 | 0.82 | 0.82 |
| P2 | East Full Crossing | 1 | 37.0 | LOS D | 0.0 | 0.0 | 0.86 | 0.86 |
| P3 | North Full Crossing | 1 | 33.6 | LOS D | 0.0 | 0.0 | 0.82 | 0.82 |
| All Pedestrians |  | 3 | 34.7 | LOS D |  |  | 0.83 | 0.83 |

Level of Service（LOS）Method：SIDRA Pedestrian LOS Method（Based on Average Delay）
Pedestrian movement LOS values are based on average delay per pedestrian movement．
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements．

## SITE LAYOUT

ST0F Site: 101 [[Existing+Dev] Mamre Road x Mandalong Close_PM]
Mamre Road x Mandalong Close
2018 Existing + Dev
Stop (Two-Way)


## MOVEMENT SUMMARY

ST0Fi Site: 101 [[Existing+Dev] Mamre Road x Mandalong
Close_AM]

Mamre Road x Mandalong Close
2018 Existing + Dev
Stop (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | $\begin{aligned} & \text { Demand } \\ & \text { Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Arriva Total veh/h | $\begin{aligned} & \text { Flows } \\ & \text { HV } \\ & \% \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Mamre Road (200m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 19 | 11.1 | 19 | 11.1 | 0.011 | 7.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.63 | 59.3 |
| 2 | T1 | 741 | 10.1 | 741 | 10.1 | 0.405 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 79.8 |
| Appr |  | 760 | 10.1 | 760 | 10.1 | 0.405 | 0.2 | NA | 0.0 | 0.0 | 0.00 | 0.02 | 79.4 |
| North: Mamre Road (1245m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 | T1 | 1508 | 5.2 | 1508 | 5.2 | 0.800 | 0.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 78.8 |
| 9 | R2 | 43 | 2.4 | 43 | 2.4 | 0.076 | 12.0 | LOS A | 0.3 | 2.0 | 0.62 | 0.84 | 62.5 |
| Appr |  | 1552 | 5.1 | 1552 | 5.1 | 0.800 | 1.1 | NA | 0.3 | 2.0 | 0.02 | 0.02 | 78.0 |
| West: Mandalong Close ( 720 m ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 27 | 7.7 | 27 | 7.7 | 0.067 | 15.5 | LOS B | 0.2 | 1.7 | 0.66 | 1.00 | 60.3 |
| 12 | R2 | 20 | 5.3 | 20 | 5.3 | 3.333 | 2519.2 | LOS F | 16.0 | 117.3 | 1.00 | 1.30 | 0.9 |
| Approach |  | 47 | 6.7 | 47 | 6.7 | 3.333 | 1072.6 | LOS F | 16.0 | 117.3 | 0.80 | 1.13 | 4.1 |
| All V | icles | 2359 | 6.7 | 2359 | 6.7 | 3.333 | 22.4 | NA | 16.0 | 117.3 | 0.03 | 0.04 | 56.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 0.0 \%
Number of Iterations: 7 (maximum specified: 10)

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## MOVEMENT SUMMARY

ST0F Site: 101 [[Existing+Dev] Mamre Road x Mandalong

Mamre Road x Mandalong Close
2018 Existing + Dev
Stop (Two-Way)


Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 0.9 \%
Number of Iterations: 9 (maximum specified: 10)

## Appendix D5 <br> 2036 Project Future Baseline + Future Built Form SIDRA Results

## SITE LAYOUT

## Site: 104 [[2036 Base + Dev] Mamre Road x Southern Link_AM]

Mamre Road x Bakers Lane
2036 Base
Signals - Fixed Time Isolated


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## MOVEMENT SUMMARY

⿴ Site： 104 ［［2036 Base＋Dev］Mamre Road x Southern
审审 Network：N101［2036 Base Link＿AM］

Mamre Road x Bakers Lane
2036 Base
Signals－Fixed Time Isolated Cycle Time $=115$ seconds（Practical Cycle Time）

| Movement Performance－Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Demand Flows Total HV veh／h \％ |  | Arrival FlowsTotal HV |  | Deg． Satn v／c | Average Delay sec | Level of Service | 95\％Back of Queue Vehicles Distance |  | Prop． Queued | Effective Average Stop Speed Rate |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | $\mathrm{veh} / \mathrm{h}$ | \％ |  |  |  | veh | m |  | per veh | km／h |
| South：Mamre Road（500m） |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 1 | 10.0 | 1 | 10.0 | 0.001 | 7.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.60 | 60.8 |
| 2 | T1 | 1628 | 12.6 | 1628 | 12.6 | 0.881 | 49.3 | LOS D | 33.1 | 255.9 | 1.00 | 1.01 | 26.1 |
| 3 | R2 | 607 | 10.0 | 607 | 10.0 | 0.876 | 67.0 | LOS E | 19.1 | 145.5 | 1.00 | 0.96 | 30.3 |
| Appr | ach | 2237 | 11.9 | 2237 | 11.9 | 0.881 | 54.1 | LOS D | 33.1 | 255.9 | 1.00 | 0.99 | 27.6 |
| East：Southern Link Rd－E |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 342 | 20.0 | 342 | 20.0 | 0.210 | 7.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.59 | 58.9 |
| 5 | T1 | 408 | 20.0 | 408 | 20.0 | 0.619 | 46.9 | LOS D | 10.7 | 88.0 | 0.97 | 0.81 | 25.2 |
| 6 | R2 | 84 | 20.0 | 84 | 20.0 | 0.497 | 69.8 | LOS E | 2.5 | 20.5 | 1.00 | 0.74 | 18.7 |
| Appr |  | 835 | 20.0 | 835 | 20.0 | 0.619 | 33.2 | LOS C | 10.7 | 88.0 | 0.58 | 0.71 | 31.4 |
| North：Mamre Road（760m） |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 524 | 20.0 | 524 | 20.0 | 0.323 | 7.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.59 | 63.4 |
| 8 | T1 | 1607 | 18.3 | 1607 | 18.3 | 0.884 | 49.7 | LOS D | 33.1 | 268.4 | 1.00 | 1.02 | 33.3 |
| 9 | R2 | 615 | 18.3 | 615 | 18.3 | 0.897 | 70.3 | LOSE | 20.1 | 162.9 | 1.00 | 0.98 | 26.9 |
| Appr |  | 2746 | 18.6 | 2746 | 18.6 | 0.897 | 46.4 | LOS D | 33.1 | 268.4 | 0.81 | 0.93 | 36.2 |
| West：Southern Link Rd－W |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 448 | 20.0 | 339 | 22.7 | 0.212 | 7.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.59 | 61.4 |
| 11 | T1 | 766 | 20.0 | 580 | 22.7 | 0.892 | 62.5 | LOS E | 18.8 | 157.0 | 1.00 | 1.02 | 33.6 |
| 12 | R2 | 119 | 20.0 | 90 | 22.7 | 0.540 | 70.4 | LOS E | 2.7 | 22.5 | 1.00 | 0.75 | 21.1 |
| Approach |  | 1334 | 20.0 | $1009{ }^{\text {N1 }}$ | 22.7 | 0.892 | 44.9 | LOS D | 18.8 | 157.0 | 0.66 | 0.85 | 36.0 |
| All V | icles | 7152 | 16.9 | $6827{ }^{\text {N1 }}$ | 17.7 | 0.897 | 47.1 | LOS D | 33.1 | 268.4 | 0.82 | 0.91 | 32.9 |

Site Level of Service（LOS）Method：Delay（RTA NSW）．Site LOS Method is specified in the Network Data dialog（Network tab）．
Vehicle movement LOS values are based on average delay per movement．
Intersection and Approach LOS values are based on average delay for all vehicle movements．
SIDRA Standard Delay Model is used．Control Delay includes Geometric Delay．
Gap－Acceptance Capacity：SIDRA Standard（Akçelik M3D）．
HV（\％）values are calculated for All Movement Classes of All Heavy Vehicle Model Designation．
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations： 1.6 \％
Number of Iterations： 10 （maximum specified：10）
N1 Arrival Flow value is reduced due to capacity constraint at oversaturated upstream lanes．

| Movement Performance－Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Description | Demand Flow ped／h | Average Delay sec | Level of Service | Average Back Pedestrian ped | of Queue Distance m | Prop． Queued | Effective Stop Rate per ped |
| P11 | South Stage 1 | 11 | 27.1 | LOS C | 0.0 | 0.0 | 0.69 | 0.69 |
| P12 | South Stage 2 | 11 | 23.2 | LOS C | 0.0 | 0.0 | 0.64 | 0.64 |
| P21 | East Stage 1 | 11 | 22.5 | LOS C | 0.0 | 0.0 | 0.63 | 0.63 |
| P22 | East Stage 2 | 11 | 21.3 | LOS C | 0.0 | 0.0 | 0.61 | 0.61 |
| P31 | North Stage 1 | 11 | 48.0 | LOS E | 0.0 | 0.0 | 0.91 | 0.91 |
| P32 | North Stage 2 | 11 | 45.3 | LOS E | 0.0 | 0.0 | 0.89 | 0.89 |


| P41 | West Stage 1 | 11 | 23.2 | LOS C | 0.0 | 0.0 | 0.64 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| P42 | West Stage 2 | 11 | 21.9 | LOS C | 0.0 | 0.0 | 0.62 |
| All Pedestrians | 84 | 29.1 | LOS C |  |  | 0.64 |  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## MOVEMENT SUMMARY

Site: 104 [[2036 Base + Dev] Mamre Road x Southern

审审 Network: N101 [2036 Base Case + Dev - PM - IMPROVED EPR]
Mamre Road x Bakers Lane
2036 Base
Signals - Fixed Time Isolated Cycle Time = 130 seconds (Practical Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | OD Mov | Deman <br> Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Arrival Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Mamre Road ( 500 m ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 1 | 20.0 | 1 | 20.0 | 0.001 | 18.2 | LOS B | 0.0 | 0.2 | 0.44 | 0.61 | 45.5 |
| 2 | T1 | 1401 | 12.1 | 1401 | 12.1 | 0.897 | 61.5 | LOS E | 33.0 | 253.4 | 1.00 | 1.02 | 22.3 |
| 3 | R2 | 321 | 11.5 | 321 | 11.5 | 0.810 | 75.0 | LOS F | 10.9 | 83.6 | 1.00 | 0.90 | 28.2 |
| Appro |  | 1723 | 12.0 | 1723 | 12.0 | 0.897 | 64.0 | LOS E | 33.0 | 253.4 | 1.00 | 0.99 | 23.8 |
| East: Southern Link Rd-E |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 751 | 10.0 | 751 | 10.0 | 0.433 | 5.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.52 | 50.0 |
| 5 | T1 | 693 | 20.0 | 693 | 20.0 | 0.902 | 66.9 | LOS E | 31.2 | 256.0 | 1.00 | 1.08 | 18.0 |
| 6 | R2 | 498 | 10.0 | 498 | 10.0 | 0.479 | 45.7 | LOS D | 12.9 | 98.1 | 0.87 | 0.81 | 22.9 |
| Appro |  | 1941 | 13.6 | 1941 | 13.6 | 0.902 | 37.8 | LOS C | 31.2 | 256.0 | 0.58 | 0.80 | 25.8 |
| North: Mamre Road (760m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 132 | 20.0 | 132 | 20.0 | 0.081 | 7.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.59 | 63.4 |
| 8 | T1 | 1325 | 18.5 | 1325 | 18.5 | 0.892 | 61.1 | LOS E | 31.3 | 253.4 | 1.00 | 1.02 | 29.4 |
| 9 | R2 | 208 | 18.5 | 208 | 18.5 | 0.864 | 81.8 | LOS F | 8.0 | 65.0 | 1.00 | 1.00 | 22.0 |
| Appro |  | 1665 | 18.6 | 1665 | 18.6 | 0.892 | 59.5 | LOS E | 31.3 | 253.4 | 0.92 | 0.98 | 30.1 |
| West: Southern Link Rd - W |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 598 | 20.0 | 220 | 28.8 | 0.143 | 5.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.51 | 51.3 |
| 11 | T1 | 508 | 20.0 | 187 | 28.8 | 0.493 | 60.1 | LOS E | 5.8 | 50.2 | 0.98 | 0.77 | 32.0 |
| 12 | R2 | 181 | 20.0 | 67 | 28.8 | 0.156 | 60.1 | LOS E | 1.9 | 16.5 | 0.92 | 0.72 | 21.5 |
| Approach |  | 1287 | 20.0 | $473{ }^{\text {N1 }}$ | 28.8 | 0.493 | 34.9 | LOS C | 5.8 | 50.2 | 0.52 | 0.65 | 34.8 |
| All Vehicles |  | 6617 | 15.7 | $5802{ }^{\text {N1 }}$ | 17.9 | 0.902 | 51.6 | LOS D | 33.0 | 256.0 | 0.80 | 0.90 | 27.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 10.2 \%
Number of Iterations: 10 (maximum specified: 10)
N1 Arrival Flow value is reduced due to capacity constraint at oversaturated upstream lanes.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Bac Pedestrian ped | Queue Distance m $\qquad$ | Prop. Queued | Effective Stop Rate per ped |
| P11 | South Stage 1 | 11 | 27.8 | LOS C | 0.0 | 0.0 | 0.65 | 0.65 |
| P12 | South Stage 2 | 11 | 40.8 | LOS E | 0.0 | 0.0 | 0.79 | 0.79 |
| P21 | East Stage 1 | 11 | 25.2 | LOS C | 0.0 | 0.0 | 0.62 | 0.62 |


| P22 | East Stage 2 | 11 | 38.5 | LOS D | 0.0 | 0.0 | 0.77 | 0.77 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| P31 | North Stage 1 | 11 | 20.2 | LOS C | 0.0 | 0.0 | 0.77 | 0.77 |
| P32 | North Stage 2 | 11 | 40.8 | LOS E | 0.0 | 0.0 | 0.79 | 0.79 |
| P41 | West Stage 1 | 11 | 12.5 | LOS B | 0.0 | 0.0 | 0.44 | 0.44 |
| P42 | West Stage 2 | 11 | 38.5 | LOS D | 0.0 | 0.0 | 0.77 | 0.77 |
| All Pedestrians | 84 | 30.5 | LOS D |  |  | 0.70 | 0.70 |  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## SITE LAYOUT

Site: 105vv [[2036 Base + Dev] Mamre Road x Mamre west precicnt
Mamre Road x Mamre west precicnt 2018 Base
Giveway / Yield (Two-Way)



## MOVEMENT SUMMARY

$\nabla$ Site: 105vv [[2036 Base + Dev] Mamre Road x Mamre west
precicnt_AM]

虫审 Network: N101 [2036 Base
Case + Dev - AM - With Imporved EPR]
Mamre Road x Mamre west precicnt 2018 Base
Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov OD  <br> ID Mov | Demand Total veh/h | Flows HV \% | Arrival Total <br> veh/h | Flows <br> HV <br> \% | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles <br> veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | verage Speed km/h |
| South: Mamre Road (760m) |  |  |  |  |  |  |  |  |  |  |  |  |
| L2 | 112 | 20.0 | 106 | 20.1 | 0.065 | 7.3 | LOS A | 0.0 | 0.0 | 0.00 | 0.63 | 62.4 |
| $2 \quad \mathrm{~T} 1$ | 2056 | 7.6 | 1957 | 7.7 | 0.351 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 79.8 |
| Approach | 2167 | 8.3 | $2063{ }^{\text {N1 }}$ | 8.3 | 0.351 | 0.4 | NA | 0.0 | 0.0 | 0.00 | 0.03 | 78.0 |
| North: Mamre Road (520m) |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 2178 | 7.7 | 2178 | 7.7 | 0.391 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 79.8 |
| Approach | 2178 | 7.7 | 2178 | 7.7 | 0.391 | 0.1 | NA | 0.0 | 0.0 | 0.00 | 0.00 | 79.8 |
| West: Mamre west precient Site Access |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 32 | 20.0 | 32 | 20.0 | 0.059 | 10.7 | LOS A | 0.2 | 1.7 | 0.57 | 0.78 | 44.9 |
| Approach | 32 | 20.0 | 32 | 20.0 | 0.059 | 10.7 | LOS A | 0.2 | 1.7 | 0.57 | 0.78 | 44.9 |
| All Vehicles | 4377 | 8.1 | $4273{ }^{\text {N1 }}$ | 8.3 | 0.391 | 0.3 | NA | 0.2 | 1.7 | 0.00 | 0.02 | 78.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 1.6 \%
Number of Iterations: 10 (maximum specified: 10)
N1 Arrival Flow value is reduced due to capacity constraint at oversaturated upstream lanes.

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## MOVEMENT SUMMARY

$\nabla$ Site: 105vv [[2036 Base + Dev] Mamre Road x Mamre west
precicnt _PM]

Mamre Road x Mamre west precicnt
2018 Base
Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{ll} \text { Mov } & \text { OD } \\ \text { ID } & \text { Mov } \end{array}$ | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Arrival Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles <br> veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Mamre Road (760m) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 38 | 20.0 | 32 | 19.4 | 0.020 | 7.3 | LOS A | 0.0 | 0.0 | 0.00 | 0.63 | 62.6 |
| 2 T1 | 2448 | 6.8 | 2102 | 6.5 | 0.375 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 79.8 |
| Approach | 2486 | 7.0 | $2135{ }^{\text {N1 }}$ | 6.7 | 0.375 | 0.2 | NA | 0.0 | 0.0 | 0.00 | 0.01 | 79.3 |
| North: Mamre Road (520m) |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 1665 | 13.7 | 1665 | 13.7 | 0.310 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 79.9 |
| Approach | 1665 | 13.7 | 1665 | 13.7 | 0.310 | 0.0 | NA | 0.0 | 0.0 | 0.00 | 0.00 | 79.9 |
| West: Mamre west precicnt Site Access |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 94 | 20.0 | 94 | 20.0 | 0.187 | 11.7 | LOS A | 0.7 | 5.6 | 0.64 | 0.84 | 43.7 |
| Approach | 94 | 20.0 | 94 | 20.0 | 0.187 | 11.7 | LOS A | 0.7 | 5.6 | 0.64 | 0.84 | 43.7 |
| All Vehicles | 4245 | 9.9 | $3894{ }^{\text {N1 }}$ | 10.8 | 0.375 | 0.4 | NA | 0.7 | 5.6 | 0.02 | 0.03 | 78.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: $10.2 \%$
Number of Iterations: 10 (maximum specified: 10)
N1 Arrival Flow value is reduced due to capacity constraint at oversaturated upstream lanes.

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## SITE LAYOUT

## Site: 103 [[2036 Base + Dev] Mamre Road x James Erskine Drive_AM]

Mamre Road x James Erskine Drive
2036 Base
Signals - Fixed Time Isolated


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## MOVEMENT SUMMARY

日 Site： 103 ［［2036 Base＋Dev］Mamre Road x James Erskine
审审 Network：N101［2036 Base Drive＿AM］

Mamre Road x James Erskine Drive
2036 Base
Signals－Fixed Time Isolated Cycle Time $=120$ seconds（Practical Cycle Time）

| Movement Performance－Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Demand Total veh／h | Flows HV \％ | Arrival Total <br> veh／h | lows HV \％ | Deg． Satn v／c | Average Delay sec | Level of Service | 95\％Back Vehicles veh | of Queue Distance m | Prop． Queued | Effective Stop Rate per veh | verage Speed km／h |
| South：Mamre Road（520m） |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 1 | 0.0 | 1 | 0.0 | 0.001 | 8.2 | LOS A | 0.0 | 0.1 | 0.25 | 0.56 | 52.3 |
| 2 | T1 | 1898 | 6.7 | 1809 | 6.8 | 0.597 | 20.7 | LOS B | 23.6 | 173.9 | 0.74 | 0.67 | 43.3 |
| 3 | R2 | 180 | 18.0 | 171 | 18.1 | 0.781 | 74.2 | LOS F | 5.5 | 44.3 | 1.00 | 0.86 | 23.1 |
| Appr | ach | 2079 | 7.7 | $1981{ }^{\text {N1 }}$ | 7.8 | 0.781 | 25.4 | LOS B | 23.6 | 173.9 | 0.76 | 0.68 | 39.3 |
| East：James Erskine Drive（170m） |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 62 | 54.8 | 62 | 54.8 | 0.134 | 20.3 | LOS B | 1.9 | 19.3 | 0.59 | 0.67 | 20.7 |
| 5 | T1 | 1 | 0.0 | 1 | 0.0 | 0.134 | 15.1 | LOS B | 1.9 | 19.3 | 0.59 | 0.67 | 39.2 |
| 6 | R2 | 88 | 54.2 | 88 | 54.2 | 0.671 | 72.8 | LOS F | 2.9 | 29.3 | 1.00 | 0.83 | 8.2 |
| Appr |  | 152 | 54.1 | 152 | 54.1 | 0.671 | 50.9 | LOS D | 2.9 | 29.3 | 0.83 | 0.76 | 11.1 |
| North：Mamre Road（300m） |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 429 | 17.9 | 429 | 17.9 | 0.690 | 28.2 | LOS B | 25.9 | 202.8 | 0.75 | 0.85 | 34.2 |
| 8 | T1 | 2646 | 7.4 | 2646 | 7.4 | 0.891 | 34.4 | LOS C | 52.3 | 389.2 | 0.88 | 0.91 | 23.4 |
| 9 | R2 | 183 | 0.0 | 183 | 0.0 | 0.740 | 70.4 | LOS E | 5.7 | 40.1 | 1.00 | 0.85 | 24.5 |
| Appr |  | 3259 | 8.4 | 3259 | 8.4 | 0.891 | 35.6 | LOS C | 52.3 | 389.2 | 0.87 | 0.90 | 24.9 |
| West：RoadName |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 31 | 0.0 | 31 | 0.0 | 0.045 | 13.2 | LOSA | 0.5 | 3.8 | 0.50 | 0.64 | 42.5 |
| 11 | T1 | 1 | 0.0 | 1 | 0.0 | 0.045 | 7.6 | LOSA | 0.5 | 3.8 | 0.50 | 0.64 | 45.7 |
| 12 | R2 | 38 | 0.0 | 38 | 0.0 | 0.408 | 69.4 | LOSE | 2.3 | 16.1 | 1.00 | 0.73 | 18.9 |
| Approach |  | 69 | 0.0 | 69 | 0.0 | 0.408 | 43.8 | LOS D | 2.3 | 16.1 | 0.77 | 0.69 | 25.3 |
| All Vehicles |  | 5559 | 9.3 | $5461{ }^{\mathrm{N} 1}$ | 9.4 | 0.891 | 32.4 | LOS C | 52.3 | 389.2 | 0.83 | 0.81 | 29.4 |

Site Level of Service（LOS）Method：Delay（RTA NSW）．Site LOS Method is specified in the Network Data dialog（Network tab）．
Vehicle movement LOS values are based on average delay per movement．
Intersection and Approach LOS values are based on average delay for all vehicle movements．
SIDRA Standard Delay Model is used．Control Delay includes Geometric Delay．
Gap－Acceptance Capacity：SIDRA Standard（Akçelik M3D）．
HV（\％）values are calculated for All Movement Classes of All Heavy Vehicle Model Designation．
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations： 1.6 \％
Number of Iterations： 10 （maximum specified：10）
N1 Arrival Flow value is reduced due to capacity constraint at oversaturated upstream lanes．

| Movement Performance－Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Description | Demand Flow ped／h | Average Delay sec | Level of Service | Average Back Pedestrian ped | of Queue Distance m | Prop． Queued | Effective Stop Rate per ped |
| P1 | South Full Crossing | 1 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P2 | East Full Crossing | 1 | 20.4 | LOS C | 0.0 | 0.0 | 0.58 | 0.58 |
| P3 | North Full Crossing | 53 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 |
| P4 | West Full Crossing | 53 | 19.3 | LOS B | 0.1 | 0.1 | 0.57 | 0.57 |
| All P | estrians | 107 | 36.8 | LOS D |  |  | 0.76 | 0.76 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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审审 Network: N101 [2036 Base Case + Dev - PM - IMPROVED EPR]

Mamre Road x James Erskine Drive
2036 Base
Signals - Fixed Time Isolated Cycle Time = 115 seconds (Practical Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \hline \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \\ \hline \end{gathered}$ | Arrival Total veh/h | $\begin{gathered} =\text { lows } \\ \mathrm{HV} \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles <br> veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Mamre Road (520m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 1 | 0.0 | 1 | 0.0 | 0.001 | 7.5 | LOS A | 0.0 | 0.1 | 0.22 | 0.56 | 52.9 |
| 2 | T1 | 2702 | 8.1 | 2368 | 8.3 | 0.860 | 33.1 | LOS C | 42.6 | 318.1 | 0.95 | 0.92 | 33.8 |
| 3 | R2 | 95 | 36.8 | 83 | 37.0 | 0.251 | 60.0 | LOS E | 2.2 | 20.5 | 0.95 | 0.74 | 26.4 |
| Appr | ch | 2798 | 9.1 | $2452^{\mathrm{N} 1}$ | 9.2 | 0.860 | 34.0 | LOS C | 42.6 | 318.1 | 0.95 | 0.92 | 33.4 |
| East: James Erskine Drive (170m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 186 | 7.7 | 186 | 7.7 | 0.222 | 9.4 | LOS A | 3.2 | 23.7 | 0.39 | 0.63 | 29.9 |
| 5 | T1 | 1 | 0.0 | 1 | 0.0 | 0.222 | 4.6 | LOS A | 3.2 | 23.7 | 0.39 | 0.63 | 46.8 |
| 6 | R2 | 259 | 14.8 | 259 | 14.8 | 0.902 | 75.1 | LOS F | 8.5 | 67.4 | 1.00 | 1.06 | 8.0 |
| Appr |  | 446 | 11.8 | 446 | 11.8 | 0.902 | 47.6 | LOS D | 8.5 | 67.4 | 0.75 | 0.88 | 11.5 |
| North: Mamre Road (300m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 127 | 56.3 | 127 | 56.3 | 0.458 | 33.6 | LOS C | 11.5 | 102.0 | 0.73 | 0.75 | 32.3 |
| 8 | T1 | 1575 | 15.1 | 1575 | 15.1 | 0.592 | 26.3 | LOS B | 19.4 | 153.6 | 0.81 | 0.73 | 28.1 |
| 9 | R2 | 63 | 0.0 | 63 | 0.0 | 0.326 | 66.1 | LOS E | 1.8 | 12.8 | 1.00 | 0.72 | 25.4 |
| Approach |  | 1765 | 17.6 | 1765 | 17.6 | 0.592 | 28.3 | LOS B | 19.4 | 153.6 | 0.81 | 0.73 | 28.2 |
| West: RoadName |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 94 | 0.0 | 94 | 0.0 | 0.136 | 18.7 | LOS B | 2.5 | 17.7 | 0.57 | 0.70 | 37.6 |
| 11 | T1 | 1 | 0.0 | 1 | 0.0 | 0.136 | 13.1 | LOS A | 2.5 | 17.7 | 0.57 | 0.70 | 41.4 |
| 12 | R2 | 115 | 0.0 | 115 | 0.0 | 0.710 | 64.9 | LOS E | 6.7 | 47.1 | 1.00 | 0.85 | 19.8 |
| Approach |  | 209 | 0.0 | 209 | 0.0 | 0.710 | 44.0 | LOS D | 6.7 | 47.1 | 0.81 | 0.78 | 25.1 |
| All Vehicles |  | 5219 | 11.8 | $4873{ }^{\text {N1 }}$ | 12.7 | 0.902 | 33.6 | LOS C | 42.6 | 318.1 | 0.87 | 0.84 | 29.1 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 10.2 \%
Number of Iterations: 10 (maximum specified: 10)
N1 Arrival Flow value is reduced due to capacity constraint at oversaturated upstream lanes.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\stackrel{M}{\mathrm{Mov}}$ | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Back Pedestrian ped | of Queue Distance $\qquad$ | Prop. Queued | Effective Stop Rate per ped |
| P1 | South Full Crossing | 1 | 51.7 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 |
| P2 | East Full Crossing | 1 | 27.1 | LOS C | 0.0 | 0.0 | 0.69 | 0.69 |
| P3 | North Full Crossing | 53 | 51.8 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 |


| P4 West Full Crossing | 53 | 51.8 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :--- |
| All Pedestrians | 107 | 51.5 | LOS E |  | 0.95 | 0.95 |  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## SITE LAYOUT

Site: 102 [[2036 Base + Dev] Mamre Road x Erskine Park Road_AM - IMPROVED]
Mamre Road x Erskine Park Road 2036 Base
Signals - Fixed Time Isolated


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## MOVEMENT SUMMARY

B Site: 102 [[2036 Base + Dev] Mamre Road x Erskine Park Road_AM - IMPROVED]

Network: N101 [2036 Base
Case + Dev - AM - With Imporved EPR]
Mamre Road x Erskine Park Road
2036 Base
Signals - Fixed Time Coordinated Cycle Time $=100$ seconds (Network Cycle Time - User-Given)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Demand Flows Total HV veh/h \% |  | Arrival FlowsTotal HV |  | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back of Queue Vehicles Distance |  | Prop. Queued | Effective Average |  |
|  |  |  |  | Stop | peed |  |  |  |  |  |  |
|  |  |  |  | $\mathrm{veh} / \mathrm{h}$ | \% |  |  |  | veh | m |  | per veh | km/h |
| South: Mamre Road (300m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | T1 | 820 | 9.8 |  |  | 784 | 10.0 | 0.174 | 2.0 | LOS A | 2.6 | 19.9 | 0.22 | 0.19 | 70.4 |
| 3 | R2 | 1069 | 13.4 | 1024 | 13.7 | 0.658 | 30.1 | LOS C | 19.3 | 151.4 | 0.83 | 0.84 | 42.2 |
| Appro |  | 1889 | 11.8 | $1808{ }^{\mathrm{N1}}$ | 12.1 | 0.658 | 17.9 | LOS B | 19.3 | 151.4 | 0.57 | 0.56 | 46.1 |
| East: Erskine Park Road (590m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 1283 | 13.1 | 1283 | 13.1 | 0.800 | 24.2 | LOS B | 28.1 | 219.1 | 0.75 | 0.84 | 42.8 |
| 6 | R2 | 12 | 14.0 | 12 | 14.0 | 0.057 | 57.8 | LOS E | 0.3 | 2.2 | 0.97 | 0.65 | 25.9 |
| Appro |  | 1295 | 13.1 | 1295 | 13.1 | 0.800 | 24.5 | LOS B | 28.1 | 219.1 | 0.75 | 0.84 | 42.6 |
| North: Mamre Road (200m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 222 | 4.4 | 222 | 4.4 | 0.585 | 19.2 | LOS B | 12.9 | 94.5 | 0.82 | 0.79 | 52.1 |
| 8 | T1 | 1432 | 6.4 | 1432 | 6.4 | 0.850 | 39.1 | LOS C | 24.8 | 183.1 | 0.97 | 0.95 | 16.1 |
| Approach |  | 1654 | 6.1 | 1654 | 6.1 | 0.850 | 36.4 | LOS C | 24.8 | 183.1 | 0.95 | 0.93 | 21.5 |
| All Ve | icles | 4838 | 10.2 | $4757^{\mathrm{N} 1}$ | 10.4 | 0.850 | 26.1 | LOS B | 28.1 | 219.1 | 0.75 | 0.77 | 36.7 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement. Intersection and Approach LOS values are based on average delay for all vehicle movements. SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: $1.6 \%$
Number of Iterations: 10 (maximum specified: 10)
N1 Arrival Flow value is reduced due to capacity constraint at oversaturated upstream lanes.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Back Pedestrian ped | of Queue Distance m | Prop. Queued | Effective Stop Rate per ped |
| P1 | South Full Crossing | 1 | 44.2 | LOS E | 0.0 | 0.0 | 0.94 | 0.94 |
| P2 | East Full Crossing | 1 | 32.8 | LOS D | 0.0 | 0.0 | 0.81 | 0.81 |
| P2S | East Slip/Bypass Lane Crossing | 53 | 27.4 | LOS C | 0.1 | 0.1 | 0.74 | 0.74 |
| P3 | North Full Crossing | 1 | 44.2 | LOS E | 0.0 | 0.0 | 0.94 | 0.94 |
| All Pedestrians |  | 56 | 28.2 | LOS C |  |  | 0.75 | 0.75 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

## MOVEMENT SUMMARY

Site: 102 [[2036 Base + Dev] Mamre Road x Erskine Park Road_PM - IMPROVED]

审审 Network: N101 [2036 Base Case + Dev - PM - IMPROVED EPR]

Mamre Road x Erskine Park Road
2036 Base
Signals - Fixed Time Coordinated Cycle Time = 140 seconds (Network Cycle Time - Program)


Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 10.2 \%
Number of Iterations: 10 (maximum specified: 10)
N1 Arrival Flow value is reduced due to capacity constraint at oversaturated upstream lanes.

| Movement Performance - Pedestrians |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Back Pedestrian ped | of Queue Distance m | Prop. Queued | Effective Stop Rate per ped |
| P1 | South Full Crossing | 1 | 64.1 | LOS F | 0.0 | 0.0 | 0.96 | 0.96 |
| P2 | East Full Crossing | 1 | 53.2 | LOS E | 0.0 | 0.0 | 0.87 | 0.87 |
| P2S | East Slip/Bypass Lane Crossing | 53 | 47.3 | LOS E | 0.2 | 0.2 | 0.82 | 0.82 |
| P3 | North Full Crossing | 1 | 64.1 | LOS F | 0.0 | 0.0 | 0.96 | 0.96 |
| All Pedestrians |  | 56 | 48.1 | LOS E |  |  | 0.83 | 0.83 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## SITE LAYOUT

STof Site: 101 [[2036 Base + Dev] Mamre Road x Mandalong Close_AM]
Mamre Road x Mandalong Close
2036 Base
Stop (Two-Way)
$1 N$


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ST0F Site: 101 [[2036 Base + Dev] Mamre Road x Mandalong Close_AM]

Mamre Road x Mandalong Close
2036 Base
Stop (Two-Way)

| Mov OD <br> ID Mov | Demand Flows Arrival Flows Total HV Total HV |  |  |  | Deg. <br> Satn <br> v/c | Average Delay <br> sec | Level of Service | $95 \%$ Back of Queue Vehicles Distance |  | Prop. Queued | Effective Average Stop Speed |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | veh/h | \% | veh/h | \% |  |  |  | veh | m |  | per veh | km/h |
| South: Mamre Road (200m) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 45 | 11.1 | 43 | 11.4 | 0.025 | 7.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.63 | 59.2 |
| 2 T1 | 786 | 10.5 | 753 | 10.8 | 0.138 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 80.0 |
| Approach | 832 | 10.5 | $796{ }^{\text {N1 }}$ | 10.8 | 0.138 | 0.4 | NA | 0.0 | 0.0 | 0.00 | 0.03 | 79.0 |
| North: Mamre Road (1245m) |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 1852 | 5.5 | 1852 | 5.5 | 0.328 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 79.9 |
| Approach | 1852 | 5.5 | 1852 | 5.5 | 0.328 | 0.1 | NA | 0.0 | 0.0 | 0.00 | 0.00 | 79.9 |
| West: Mandalong Close (720m) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 66 | 7.7 | 66 | 7.7 | 0.075 | 9.8 | LOS A | 0.3 | 2.2 | 0.36 | 0.88 | 63.0 |
| Approach | 66 | 7.7 | 66 | 7.7 | 0.075 | 9.8 | LOS A | 0.3 | 2.2 | 0.36 | 0.88 | 63.0 |
| All Vehicles | 2749 |  | $2714{ }^{\text {N1 }}$ | 7.2 | 0.328 | 0.4 | NA | 0.3 | 2.2 | 0.01 | 0.03 | 78.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 1.6 \%
Number of Iterations: 10 (maximum specified: 10)
N1 Arrival Flow value is reduced due to capacity constraint at oversaturated upstream lanes.

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## MOVEMENT SUMMARY

| sTof Site: 101 [[2036 Base + Dev] Mamre Road x Mandalong | 中审 Network: N101 [2036 Base <br> Close_PM] <br> Case + Dev - PM - IMPROVED |
| :--- | ---: |

Mamre Road x Mandalong Close
2036 Base
Stop (Two-Way)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{ll} \text { Mov } & \text { OD } \\ \text { ID } & \text { Mov } \end{array}$ | Demand Total veh/h | Flows HV $\%$ | Arrival Total veh/h | $\begin{gathered} \text { =lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Mamre Road (200m) |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 58 | 8.7 | 53 | 8.8 | 0.030 | 7.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.63 | 60.3 |
| 2 T1 | 1878 | 7.5 | 1710 | 7.6 | 0.307 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 79.9 |
| Approach | 1936 | 7.6 | $1763{ }^{\text {N1 }}$ | 7.7 | 0.307 | 0.2 | NA | 0.0 | 0.0 | 0.00 | 0.02 | 79.4 |
| North: Mamre Road (1245m) |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 943 | 12.4 | 943 | 12.4 | 0.186 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 79.9 |
| Approach | 943 | 12.4 | 943 | 12.4 | 0.186 | 0.1 | NA | 0.0 | 0.0 | 0.00 | 0.00 | 79.9 |
| West: Mandalong Close ( 720 m ) |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 63 | 8.0 | 63 | 8.0 | 0.110 | 12.8 | LOS A | 0.4 | 3.1 | 0.56 | 0.97 | 61.6 |
| Approach | 63 | 8.0 | 63 | 8.0 | 0.110 | 12.8 | LOS A | 0.4 | 3.1 | 0.56 | 0.97 | 61.6 |
| All Vehicles | 2942 | 9.1 | $2769{ }^{\text {N1 }}$ | 9.7 | 0.307 | 0.5 | NA | 0.4 | 3.1 | 0.01 | 0.03 | 78.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
Largest change in Average Back of Queue or Degree of Saturation for any lane during the last three iterations: 10.2 \%
Number of Iterations: 10 (maximum specified: 10)
N1 Arrival Flow value is reduced due to capacity constraint at oversaturated upstream lanes.

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[^0]:    Note (1): NB = North Bound direction \& SB = Southbound direction
    Note (2): Mid-block LoS criteria obtained from Table 4.4 of RMS Guide to Traffic Generating Documents.

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