

Macksville Hospital Development

Structural Report

Revision: 3

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Report Amendment Register

Rev. No.	Issue/Amendment	Author	Reviewer	Date
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1. EXECUTIVE SUMMARY

Structural Works

This structural report has been prepared by Bonacci Group (NSW) Pty Ltd to describe the structural works associated with the State Significant Development Application (SSDA) for the new Level 3 Rural Hospital in North Macksville.

A new multi-storey concrete and steel framed building is to be constructed to the north of an old precast yard, and adjacent to the new Pacific Highway alignment. The new hospital building contains a basement level, ground level and first floor level. Single-storey in patient units (IPUs) are to be of lightweight construction.

The column grid for the new structure is generally in accordance with the Health Infrastructure (HI) guidelines, spaced at 8.4 metres in each direction. The columns are to be supported on shallow footings that bear on highly weathered Phyllite or via piles socketed into the Phyllite. The ground level raft slab and basement raft slab can bear on natural residual soil (clay) and highly weathered Phyllite respectively. This structure can likely be supported on a raft slab.

The suspended slabs are proposed to be post-tensioned banded slabs with the bands orientated to suit the reticulation of major ductwork where possible. The floors have been designed to accommodate all the design requirements in the HI guidelines with respect to vibration performance and future flexibility (creation of set downs and additional risers adjacent to columns). No vertical expansion has been allowed for in the design, however, future horizontal expansion have been identified.

Lateral loads are to be resisted by in situ concrete shear walls and the central lift and stair cores. The structure is considered to be Importance Level 4 for the determination of design return periods.

2. EXISTING CONDITIONS

2.1. Location

The proposed development is located in North Macksville NSW. The development site is part of the old pre-cast yard for the construction of the Pacific Highway upgrade project. The site is bordered by the Pacific Highway to the west, farmland fronting Watt Creek to the east, farmland fronting Mattick Road to the north, and vacant lots fronting a new road providing access to Letitia Close to the south.



Figure 2.1 – Aerial view of the proposed Macksville Hospital site.

The location for the site is to the north of an old precast yard, and adjacent to the new Pacific Highway alignment. This northern site option comprises an elevated hillside area, which has been used for temporary stockpiling of earthfill. This hillside slopes away towards the north at approximately 10 degrees. The fill in this area is up to 3m in depth. The central portion of the site contains an existing farm house, and the southern portion contains a site compound.

2.2. Geotechnical

2.2.1. Geology

A geotechnical investigation for the site has been undertaken by Regional Geotechnical Solutions with the findings presented in the Geotechnical and Phase 1 Site Contamination and Assessment Report on 17th November 2017 (Report No. RGS31237.1 – AE). Refer Appendix C.

The subsurface conditions comprise:

- 0.2m -1.4m fill (gravelly silty clay); overlying
- Residual soil (very stiff to hard clay); overlying
- Extremely weathered Phyllite.

2.2.2. Soil Contamination

Based on the results of the soil contamination assessment (Refer Appendix C), no soil contamination was identifiable and therefore no remedial works are likely to be required.

2.2.3. Groundwater

As noted in the Geotechnical and Phase 1 Site Contamination and Assessment Report (Report No. RGS31237.1 – AE), no groundwater was encountered during the excavation of the test pits. It should be noted however that no long term monitoring of groundwater was carried out. Ground water levels may fluctuate seasonally due to periods of heavy rainfall.

3. PROPOSED DEVELOPMENT

3.1. General Description

The proposed development comprises the construction of a new multi-level regional hospital building on a predominantly greenfield site. As part of the development, an access road will need to be constructed from Letitia Rd to the south, which is subject to a separate planning approval (DA).

3.2. Structural Works

3.2.1. Foundations

Based on the advice provided within the Geotechnical and Phase 1 Site Contamination and Assessment Report on 17th November 2017 (Report No. RGS31237.1 – AE), the columns for the main building are to be supported on shallow footings that bear on highly weathered Phyllite, which provides a bearing capacity of 300kPa. The ground level raft slab and basement raft slab can bear on natural residual soil (clay) and highly weathered Phyllite respectively.

3.2.2. Lower Ground Floor

The slab on ground at basement has been designed as a raft slab in accordance with the geotechnical report and the site classification provided within the report.

3.2.3. Ground Floor

The slab on ground at ground floor level has been designed as a raft slab in accordance with the geotechnical report and the site classification provided within the report. Refer Appendix C.

3.2.4. Superstructure

The superstructure is to be a braced frame with columns placed on a 8.4m x 8.4m grid in accordance with the HI Design Guidelines. Lateral resistance is to be provided by in situ shear walls and the central lift shaft. Generally, column sizes are 400x400.

3.2.5. Floor Systems

A number of suspended floor systems have been considered and are shown in Table 3.3.5 below. As noted in the table, flat plate, flat slab and banded slab floor options have been developed to assist with preliminary costing. The thickness of these options vary based on the required vibration criteria set out in HI guidelines. Once clinical planning has been completed, the thicknesses can be rationalised.

FLOOR	USE	DESIGN PARAMETERS	STRUCTURAL SYSTEM	Reinforcement Rates (kg/m ³)	Post Tensioning Rates (kg/m ³)	Concrete
GROUND FLOOR	ED IPU Maternity Gym Community Health (over basement)	RF=2 (Future flexibility) 40mm sacrificial cover	Option 1 - Flat Plate 280mm thick slab 800W x 400D edge beams	50	26	S40
			Option 2 - Flat Slab 280mm thick slab 800W x 400D edge beams	50	26	S40
			Option 3 - Banded Slab 240mm thick slab (end bays) 240mm thick slab (int. bays) 2200W x 400D internal beams 1100W x 400D edge beams	60	24	S40
FIRST FLOOR	Admin	RF=2 (Future flexibility) 40mm sacrificial cover	Option 1 - Flat Plate 280mm thick slab 800W x 400D edge beams	50	26	S40
			Option 2 - Flat Slab 280mm thick slab 800W x 400D edge beams	50	26	S40
			Option 3 - Banded Slab 240mm thick slab (end bays) 240mm thick slab (int. bays) 2200W x 400D internal beams 1100W x 400D edge beams	60	24	S40
FIRST FLOOR	Theatres	RF=1 1-2.2Hz 75kg 100 Steps 40mm sacrificial cover	Option 1 - Flat Plate 350mm thick slab 800W x 450D edge beams	50	26	S40
			Option 2 - Flat Slab 280mm thick slab 2800sq. X 450D drop panels 800W x 450D edge beams	50	26	S40
			Option 3 - Banded Slab 260mm thick slab (end bays) 260mm thick slab (int. bays) 2200W x 450D internal beams 1100W x 450D edge beams	60	24	S40
ROOF	Roof over Theatres	RF=1 1-1.8Hz 75kg 100 Steps 40mm sacrificial cover	Option 1 - Flat Plate 300mm thick slab 800W x 450D edge beams Possible column capital required	50	28	S40
			Option 2 - Flat Slab 260mm thick slab 2800sq. X 450D drop panels 800W x 450D edge beams	60	26	S40
			Option 3 - Banded Slab 240mm thick slab (end bays) 240mm thick slab (int. bays) 2200W x 400D internal beams 1100W x 400D edge beams	60	24	S40
ROOF	General Roof zones		Lightweight steel structure Allow 30kg/sqm steelwork 250 deep purlins on top of steel Cantilever concrete columns if fire rating required	0	0	

Table 3.3.5 – Suspended floor system summary

3.2.6. Roof Structure

The roof structure is to be steel-framed metal deck roof supported on concrete columns. Extra allowance should be made for steel grillages to support pendants and equipment within the theatres. Steelwork will need to achieve the required fire rating.

3.2.7. Spandrel Panels

The building is to be sprinklered, therefore spandrel panels which comply with Clause C2.6 of the NCC will not be required in the façade.

3.2.8. Future Flexibility

The floor slabs are to be provided with a 40mm sacrificial cover zone as per the HI Design Guidelines. Structural details are shown below in Figure 3.3.9a-c. The reinforcement and post tensioning tendons are set down sufficiently so that they maintain the minimum cover when the 40mm sacrificial topping has been removed. This is in accordance with HI Design Guidelines.

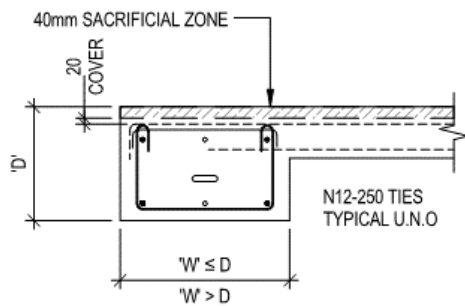


Figure 3.3.9a – Typical edge beam detail with sacrificial topping.

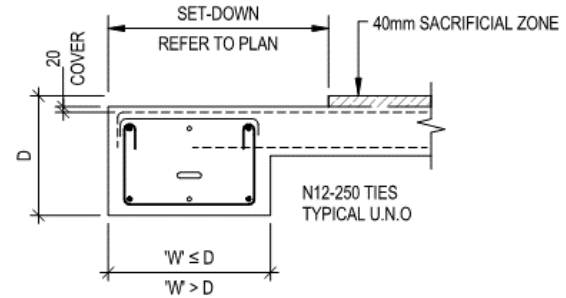


Figure 3.3.9b – Typical edge beam detail at set-down.

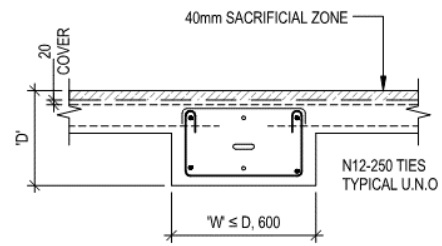
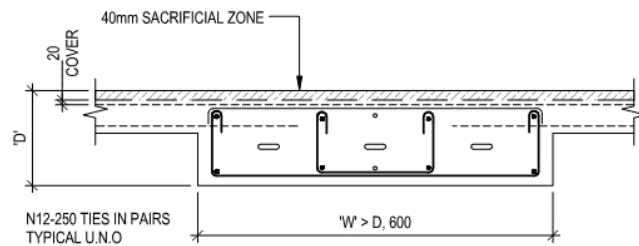


Figure 3.3.9c – Typical internal beam detail with sacrificial topping.

Allowance for additional service risers at each internal column is to be made in the design in accordance with HI Design Guidelines. This will require the reinforcement at the column lines to be displaced so that penetrations can be cut in the future and not require any associated strengthening works to the slab. Refer Figure 3.3.9d and Figure 3.3.9e.

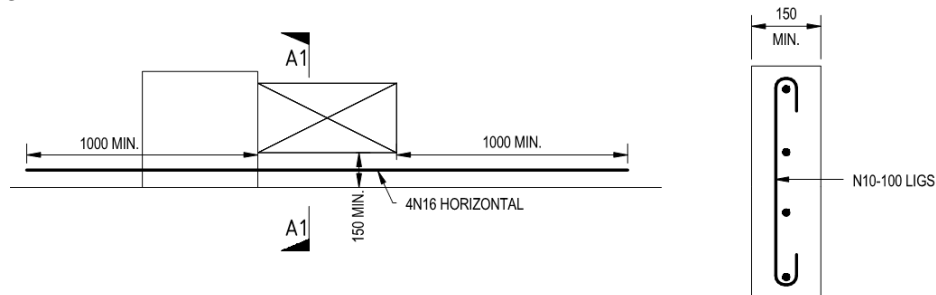


Figure 3.3.9d – Allowance for future service riser zone adjacent to column.

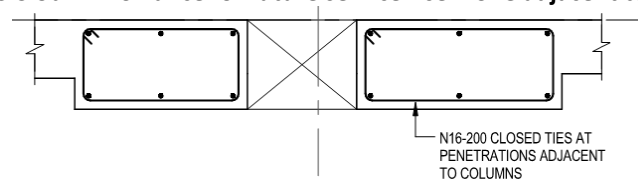


Figure 3.3.9e - Allowance for future service riser zone adjacent to column – Alternative detail.

4. PERFORMANCE PARAMETERS

4.1. Importance Factor

As the building is to accommodate medical emergency and surgical facilities, it has Importance Level 4 and will be designed to fulfil a post disaster function. This is in accordance with HI Design Guidance Note No. 024.

4.2. Design Loads

Table 4.2a: Floor & Roof Loads

Floor Type	Uniform Imposed Load (kPa)	Imposed Point Load (kN)	Superimposed Dead Load (kPa)	40mm Sacrificial Topping (kPa)
Stairs, ramps	4.0	4.5	0.0	0.0
Corridors, circulation areas and foyer spaces	5.0	4.5	1.3	1.0
Wards typically	2.0	1.8	1.8	1.0
Clinical areas	3.0	4.5	1.8	1.0
Plant rooms	7.5	4.5	2.4	0.0
Roof typically	0.25	1.4	0.75	0.0
Shell space future expansion	4.0	4.5	3.0	0.0

Table 4.2b: Wind Load Parameters

Item	Value
Location	Region A2
Importance Level	4
V_u	48m/s
V_s	37m/s
M_s	1.0
M_t	1.0
M_d	1.0
Terrain Category	2.5

Table 4.2c: Earthquake Load Parameters

Item	Value
Importance Level	4
Probability Factor, K_p	1.8
Hazard Factor, Z	0.05
Sub-Soil Class	C_e
Earthquake Design Category	II*
Structural Ductility Factor, μ	2**
Structural Performance Factor, S_p	0.67

*Structure height < 25m

**This assumes that limited ductile shear walls are to be utilised.

4.3. Floor Vibration

Footfall response will be calculated using the Concrete Centre Design Guide. The response will also be checked against the recommendations made within and Murray, Allen and Ungar in the AISC, 2003.

The footfall frequencies and corresponding response factors defined within the NSW Health Design Guidance Note No. 1 (refer Table 4.3) will be checked for compliance with the Concrete Centre Design Guide.

Once clinical planning has been completed, thicknesses of beams and slabs can be rationalised to meet the required vibration criteria. The current response factors are shown in Table 4.3 and Figure 4.3, both below.

Table 4.3: Footfall Response Factor Design Parameters – Concrete Centre Method

Facility/Equipment/Use	Design Response Factor	Footfall Frequency (Hz)
Generally procedure rooms, laboratories and general surgery	2	2.2
Corridors, circulation spaces, offices and other non-vibration sensitive areas	4	2.2
Imaging Suite and operating theatres	1	1.8
Plant areas	N/A	N/A
Roof areas	N/A	N/A

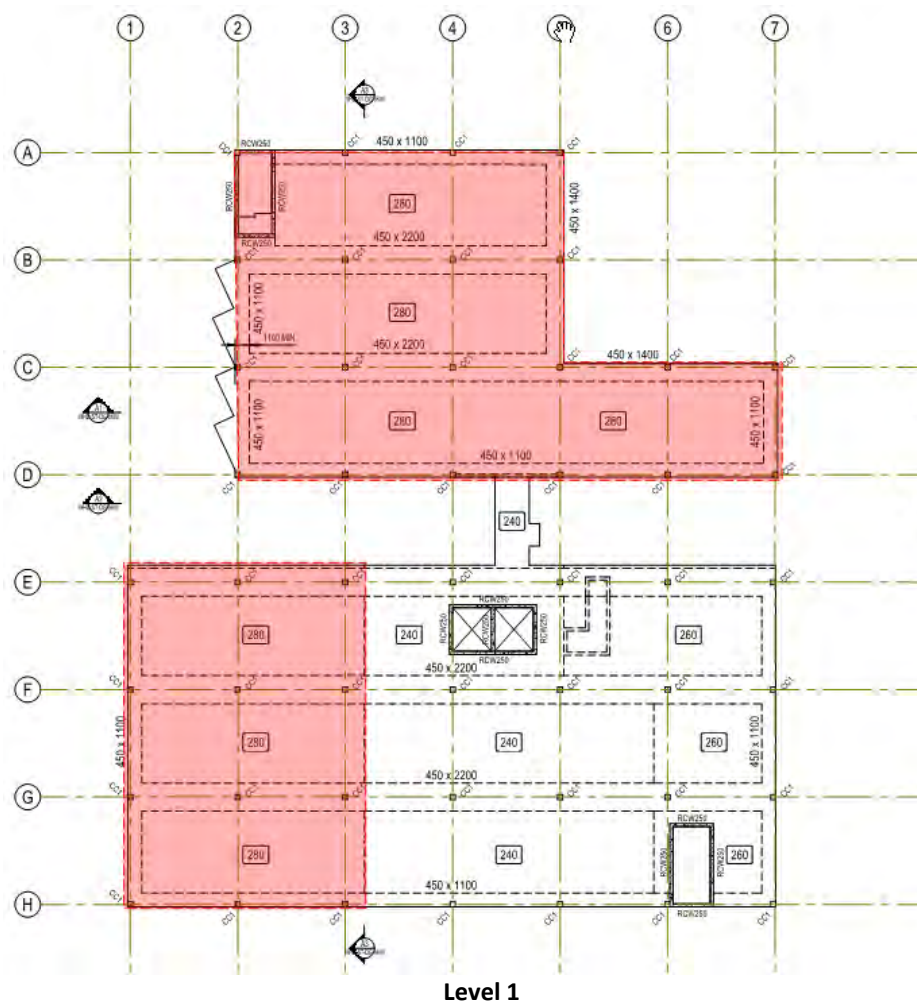


Figure 4.3 – Required response factors for each floor zone.

4.3.1. Robot Analysis

Autodesk Robot 2016 was used for the concept design stage vibration analysis. The parameters for both analyses carried out include:

- Dynamic Young's Modulus of Concrete = 38GPa
- Person mass = 75kg;
- Footfall frequency = 1-2.2 Hz;
- Footfall repetitions = 25 steps;
- Damping = 3.5%;
- Superimposed dead load = 1.5kPa; and
- Vertical support to slab is assumed to be provided by the perimeter curtain wall and riser shaft walls.

A flat plate, flat slab and banded slab system were all considered in the schematic design stage vibration analysis. As stipulated in the HI Design Guidelines, the response factor for a particular slab zone is required for the slab directly above and below. A summary of these analyses, design parameters and corresponding slab thicknesses can be seen in Table 3.3.5.

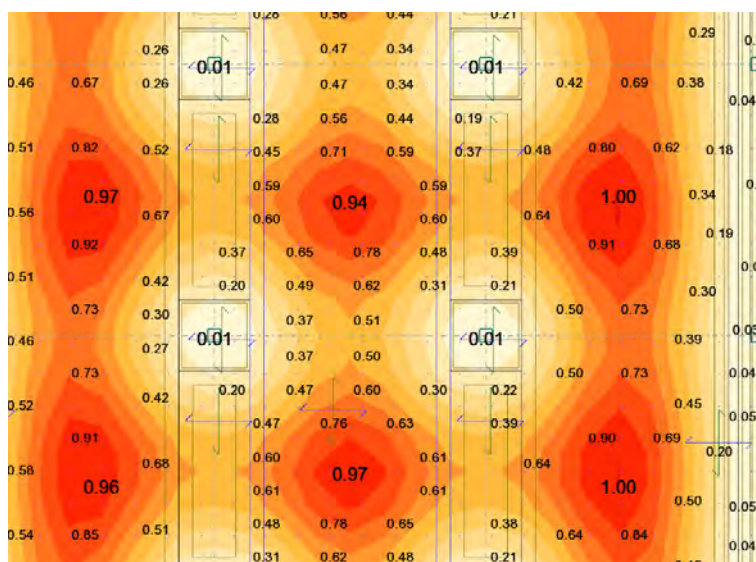


Figure 4.3.1 – Response factors for a banded floor slab system.

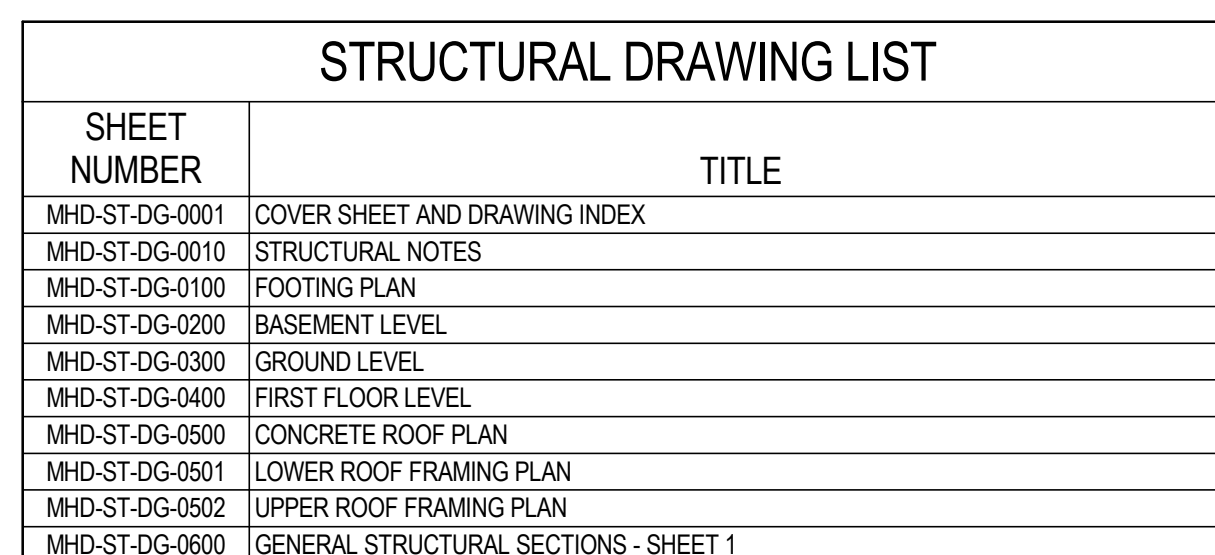
4.4. Fire Rating

Building Element	FRL (Type 9a)
External Walls (Load Bearing)	120/60/30
External Columns	120/-/-
Load Bearing Fire Walls	120/120/120
Shafts (Non-load Bearing)	-/-/-
Other Load Bearing Walls, Beams, Trusses, Columns	120/-/-
Floors	120/120/120
Steel Framed and Metal Sheeted Roofs Not Providing Fire Separating Function	No FRL*
Steel Columns Supporting Steel Framed and Metal Sheeted Roofs Not Providing Fire Separating Function	120/-/- (TBC)

*This concession is gained as the building is to be fully sprinklered

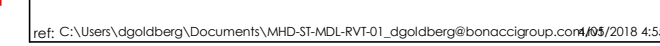
APPENDIX A. STRUCTURAL DRAWINGS

MACKSVILLE NSW 2447
STRUCTURAL DRAWINGS



LEGEND:

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SCHEMATIC DESIGN

STANDARD NOTES:

GENERAL

G1 THESE DRAWINGS SHALL BE READ IN CONJUNCTION WITH ARCHITECTURAL AND OTHER CONSULTANTS DRAWINGS AND SPECIFICATIONS AND WITH SUCH OTHER WRITTEN INSTRUCTIONS OR SKETCHES AS MAY BE ISSUED DURING THE COURSE OF THE WORK. ANY DISCREPANCY SHALL BE REFERRED TO THE SUPERINTENDENT BEFORE PROCEEDING WITH THE WORK.

G2 MATERIALS AND WORKMANSHIP SHALL BE IN ACCORDANCE WITH THE SPECIFICATION, CURRENT SAA CODES, BUILDING REGULATIONS AND THE REQUIREMENTS OF ANY OTHER RELEVANT STATUTORY AUTHORITIES.

G3 THESE DRAWINGS MUST NOT BE SCALED. DIMENSIONS ARE IN mm. ALL SET OUT DIMENSIONS AND LEVELS, INCLUDING THOSE SHOWN ON THESE DRAWINGS SHALL BE IN ACCORDANCE WITH THE ARCHITECT'S DRAWINGS AND VERIFIED ON SITE. THE CONSULTING ENGINEER HAS DESIGNED THE PERMANENT STRUCTURE. THE CONTRACTOR IS RESPONSIBLE FOR THE DESIGN, IMPLEMENTATION AND CERTIFICATION OF ALL TEMPORARY WORKS, PROPPING, NEEDLING, FALSE WORK, BRACING, BACK-PROPPING, AND SO FORTH, NECESSARY TO COMPLETE THE WORK. DURING CONSTRUCTION THE STRUCTURE SHALL BE MAINTAINED IN A STABLE CONDITION AND NO PART SHALL BE OVERSTRESSED. THE CONTRACTOR SHALL ALLOW TO ENGAGE A CHARTERED (INPE-3) ENGINEER TO DESIGN, INSPECT THE TEMPORARY WORKS AND VERIFY THE TEMPORARY STABILITY OF THE STRUCTURE. THE APPROVAL OF A SUBSTITUTION SHALL BE SOUGHT FROM THE SUPERINTENDENT BUT IS NOT AN AUTHORIZATION OF A COST VARIATION. THE SUPERINTENDENT MUST APPROVE ANY COST VARIATION INVOLVED BEFORE ANY WORK STARTS.

G4 THESE DRAWINGS SHALL NOT BE USED FOR CONSTRUCTION UNTIL ISSUED AS "FOR CONSTRUCTION" BY THIS OFFICE.

G5 THE CONTRACTOR IS TO ACCEPT RESPONSIBILITY OF THE WORKS EVEN IF THE ENGINEER HAS INSPECTED THE WORKS DURING CONSTRUCTION, WHERE ADDITIONAL CONSTRUCTION LOADS, SUCH AS TEMPORARY SHORING, MOBILE CRANES, ETC. ARE TO BE IMPOSED ON THE STRUCTURE. THE CONTRACTOR SHALL SUBMIT ALL DETAILS OF PROPOSED TEMPORARY SUPPORTS TO THE ENGINEER FOR REVIEW. SUCH INFORMATION MUST BE PROVIDED A MINIMUM OF 7 WORKING DAYS PRIOR TO THE PROPOSED WORKS COMMENCING.

G6 IF THE CONTRACTOR INTENDS TO VARY THE SCOPE OR METHOD OF WORKS OR MATERIALS USED, THE CONTRACTOR SHALL SUBMIT A PROPOSAL TO THE SUPERINTENDENT FOR APPROVAL.

G7 PROPOSAL TO THE DESIGN SUPERINTENDENT FOR DESIGN CHECK. ALL PROPRIETARY PRODUCTS SHALL BE INSTALLED STRICTLY IN ACCORDANCE WITH MANUFACTURERS' RECOMMENDATIONS.

G8 ALL REQUIRED TESTS TO COMPLETE THE WORKS SHALL BE AT THE CONTRACTOR'S EXPENSE.

HEALTH AND SAFETY

H1 THE OBLIGATION OF BONACCI GROUP PTY LTD (OR OTHER RELEVANT BONACCI ENTITY) (BONACCI) AS THE DESIGN ENGINEER IS LIMITED TO ENSURING THAT THOSE PARTS OF THE STRUCTURE THAT ARE TO BE USED AS A WORKPLACE ARE AS FAR AS REASONABLY PRACTICABLE, DESIGNED TO BE SAFE AND WITHOUT RISKS TO THE HEALTH OF THOSE PERSONS USING THE STRUCTURE AS A WORKPLACE FOR THE PURPOSE FOR WHICH IT WAS DESIGNED IN ACCORDANCE WITH SECT. 28 OF THE OCCUPATIONAL HEALTH AND SAFETY ACT 2004 (VIC).

H2 BONACCI IS NOT RESPONSIBLE FOR THE OCCUPATIONAL, HEALTH AND SAFETY OF PERSONS AT THE SITE AS THOSE OBLIGATIONS RESIDE WITH THE CONTRACTORS AND/OR SUBCONTRACTORS WHO OCCUPY OR HAVE CONTROL OF THE SITE IN ACCORDANCE WITH APPLICABLE OCCUPATIONAL HEALTH AND SAFETY LEGISLATION, CODES OF PRACTICE, GUIDANCE NOTES, AUSTRALIAN STANDARDS AND OTHER RELEVANT DOCUMENTATION.

H3 ANY ADVICE OR GUIDANCE CONCERNING OCCUPATIONAL HEALTH AND SAFETY ISSUES ARISING AT THE SITE SHOULD BE DIRECTED TO THE HEALTH AND SAFETY EXECUTIVE OR OFFICER NOMINATED FOR THE PROJECT.

FOUNDATIONS

F1 REFER TO THE GEOTECHNICAL REPORT FOR A DESCRIPTION OF THE ANTICIPATED SITE CONDITIONS. THE BUILDER IS TO STUDY THE REPORT AND MAKE HIS OWN EVALUATION OF THE SITE CONDITIONS. ANY ADDITIONAL COSTS INCURRED SHALL BE BORNE BY THE BUILDER.

F2 ALL FOOTINGS SHALL BE FOUNDED AT THE RECOMMENDED DEPTH AND INTO THE APPROPRIATE MATERIAL, AS SPECIFIED IN THE GEOTECHNICAL REPORT. THE ALLOWABLE BEARING CAPACITY SHALL BE AS SPECIFIED IN THE FOOTING SCHEDULE. THE TOPS OF FOOTINGS SHALL BE A MINIMUM OF 300mm BELOW THE LOWEST ADJACENT STRUCTURAL FLOOR LEVEL, UNLESS NOTED OTHERWISE.

F3 THE ALLOWABLE BEARING CAPACITY SHALL BE VERIFIED BY GEOTECHNICAL ENGINEER, WHO SHALL BE EMPLOYED BY THE BUILDER, BEFORE ANY CONCRETE IS PLACED. WHEREVER THE BEARING CAPACITY AT THE FOOTING BASE IS INADEQUATE, EXCAVATION SHALL CONTINUE UNTIL SUITABLE MATERIAL IS FOUND OR THE FOOTING IS ENLARGED TO THE ENGINEER DETAILS.

F4 BASES OF ALL FOOTINGS SHALL BE CLEARED OF ALL LOOSE MATERIAL PRIOR TO POURING OF CONCRETE. IN WET CONDITIONS, A 300 x 300 x 300 PIT SHALL BE DUG AT THE CORNER OF THE FOOTING FOR DETERMINING THE EXCAVATION BEFORE CONCRETING. A 50mm MINIMUM BLINDING LAYER OF N5 GRADE CONCRETE SHALL BE USED, UNLESS OTHERWISE APPROVED BY THE ENGINEER.

F5 WHENEVER A FOOTING IS LOCATED CLOSE TO A BATTER, AN EXISTING FOOTING, EXISTING OR NEW SERVICES, A LINE DRAWN AT THE BOTTOM OF THE FOOTING AT 40 DEGREES TO THE HORIZONTAL SHALL FALL BELOW THE BATTER, EXISTING FOOTING OR SERVICES. IF THIS DOES NOT HAPPEN THE FOOTING BASE SHALL BE DEEPENED AS REQUIRED TO ACHIEVE THE FORMER.

F6 THE OVER BREAK BETWEEN THE APPROVED FOUNDING LEVEL AND THE UNDERSIDE OF THE FOOTING SHALL BE FILLED WITH GRADE N15 CONCRETE. ANY OVER BREAK AT THE SIDES OF THE FOOTING SHALL BE FILLED WHEN CONCRETING THE FOOTING.

F7 THE BUILDER SHALL REMOVE ALL SPILL FROM THE SITE, AND DETERMINE THE EXCAVATION AS REQUIRED.

CONCRETE GRADE
PAD AND STRIP FOOTINGS: N40
FOUNDATION DESIGN CRITERIA
BEARING CAPACITY OF PADS ON CLASS IV SANDSTONE - 1000 kPa (WORKING)
BEARING CAPACITY OF PADS ON CLASS HEAVILY WEATHERED SANDSTONE - 400 kPa (WORKING)
BEARING CAPACITY OF STRIP AND PAD FOOTINGS ON NATURAL CLAY - 100 kPa (WORKING)
STRUCTURAL DESIGN BASED ON GEOTECHNICAL REPORT No: 7777

BORED PILES

BP1 REFER TO THE GEOTECHNICAL REPORT FOR A DESCRIPTION OF THE ANTICIPATED SITE CONDITIONS. THE PILING CONTRACTOR IS TO STUDY THE REPORT AND MAKE HIS OWN EVALUATION OF THE SITE CONDITIONS. ANY ADDITIONAL COSTS INCURRED SHALL BE BORNE BY THE PILING CONTRACTOR.

BP2 THE BORED PILES ARE PROPORTIONED FOR THE SCHEDULED LOADS WITH ALLOWABLE SOCKET SKIN FRICTION AND END BEARING CAPACITY AS INDICATED IN THE REPORT. THE DEPTHS AND LENGTHS NOMINATED IN THE SCHEDULE ARE INDICATIVE ONLY. THEY MAY NEED TO BE VARIED DEPENDING ON THE SITE CONDITIONS ENCOUNTERED. THE PILING CONTRACTOR NEEDS TO INCORPORATE ANY DESIGN CHANGES REQUIRED.

BP3 THE BORED PILES SHALL BE INSTALLED TO A MAXIMUM TOLERANCE OF ±75mm FROM THAT REQUIRED IN PLAN AND INCLINED AT NOT MORE THAN 1 IN 75 FROM THE VERTICAL OR SPECIFIED RAKE.

BP4 ALL WORKMANSHIP AND MATERIAL SHALL BE IN ACCORDANCE WITH AS 2159.

BP5 THE BORED PILES SHALL BE LOCATED CONCENTRIC WITH THE COLUMNS AND WALLS UNLESS NOTED OTHERWISE.

BP6 DRILL AND INSTALL THE BORED PILES IN THE LOCATIONS SHOWN ON THE DRAWINGS AND THE ABOVE REQUIREMENTS.

BP7 BEFORE ANY CONCRETE IS PLACED, ALL ROCK SOCKETS SHALL BE DEWATERED AND INSPECTED BY THE GEOTECHNICAL ENGINEER, WHO SHALL BE EMPLOYED BY THE BUILDER, TO VERIFY THE SOIL PARAMETERS. THE SOCKET BASE AND WALLS MUST BE CLEAN AND FREE FROM SLUR.

BP8 IF THE CONCRETE NEEDS TO BE TREMIED, SUPER PLASTICIZER MUST BE ADDED TO THE MIX AND THE CONCRETE GRADE INCREASED BY 30%. REFER TO THE SPECIFICATIONS FOR THE INSPECTION OF THE HOLE PRIOR TO CONCRETING.

BP9 THE PILING CONTRACTOR SHALL ALLOW FOR THE COST INTEREST TESTING OF ALL BORED PILES.

BP10 ANY ALTERNATIVE DESIGN SHALL MEET THE ABOVE REQUIREMENTS AND THE SCHEDULED LOADS. THE PILING CONTRACTOR SHALL OBTAIN CERTIFICATION FOR THE CALCULATIONS OF THE ALTERNATIVE SYSTEM. THE DETAILS AND CALCULATIONS SHALL BE SUBMITTED TO THE ENGINEER FOR REVIEW. THE CONTRACTOR SHALL BE FULLY RESPONSIBLE FOR THE PERFORMANCE OF THE ALTERNATIVE BORED PILES.

CONCRETE GRADE
BORED CAISSONS: N50 MINIMUM OR AS STATED IN THE SCHEDULE.
15mm COVER
FOUNDATION DESIGN CRITERIA
REFER TO REPORT No. 7777 DATED FOR RECOMMENDED FOUNDATION DESIGN CRITERIA

SLAB ON GROUND NOTES

SG01 ALL CONCRETE WORK TO COMPLY WITH AS 3600 CONCRETE CODE, AND BCA SECTIONS 3.1 AND 3.2

SG02 CONCRETE GRADE N20 MINIMUM (RESIDENTIAL)

SG03 CONCRETE GRADE N32 MINIMUM (ALL OTHER STRUCTURES)

SG04 ALL VEGETATION SHALL BE STRIPPED TO A MINIMUM DEPTH OF 150mm. ANY SOFT SPOTS OR DELETERIOUS MATERIAL SHALL BE REMOVED AND REPLACED WITH APPROVED GRANULAR FILLING COMPACTED TO 100% AS STANDARD.

SG05 COMPACTION, MINOR FILLING (800 MAXIMUM) SHALL BE PROVIDED WHERE REQUIRED TO BRING SLAB GRADE TO REQUIRED LEVEL. IN ACCORDANCE WITH LIMITS STATED IN AS 2870 AND BCA, FILLING SHALL BE APPROVED GRANULAR MATERIAL PLACED IN 150mm AND COMPACTED TO 100% AS STANDARD.

SG06 COMPACTION

SG07 A 0.2mm VAPOUR BARRIER SHALL BE USED, LAPPED A MINIMUM OF 200mm AT JOINTS AND TAPED AROUND SERVICES FITTINGS WITH ADHESIVE TAPE NOT INFERIOR TO DOUBLE SIDED BUTYL ADHESIVE TAPE. THE VAPOUR BARRIER SHALL BE PLACED ON A 50mm MINIMUM SAND BED OR SIMILAR APPROVED MATERIAL TO PROTECT MEMBRANE FROM DAMAGE.

SG08 TRENDON MESH IN BEAMS SHALL BE OVERLAPPED BY THE WIDTH OF FABRIC AT 'T' AND 'L' INTERSECTIONS AND SPLICED WITH A LAP OF 500mm. RANDOM LAP N12 BARS BY 500mm STAGGERED. THE OUTER BAR AT 'L' INTERSECTION MUST BE BENT AND CONTINUED FOR 500mm AROUND THE CORNER.

SG09 SLAB FABRIC TO BE LAPPED SUCH THAT THE TWO OUTERMOST TRANSVERSE WIRE OF ONE SHEET OF MESH OVERLAP THE TWO OUTERMOST TRANSVERSE WIRES OF THE SHEET BEING LAPPED BY A MINIMUM OF 25mm AND BE SUPPORTED ON BAR CHAIRS AT 800mm MAXIMUM CENTRES.

SG10 THIS DRAWING IS TO BE READ IN CONJUNCTION WITH THE SITE INVESTIGATION REPORT TO DETERMINE FOUNDING DEPTHS.

SG11 SITE CLASSIFICATION TO AS 2870 CLASS 3 ENGINEERING PRINCIPLES TO SECTIONS 4 OF AS 2870.

SG12 LOAD BEARING EXTERNAL AND INTERNAL BEAMS AND LOAD SUPPORT THICKENINGS ARE TO BE FOUNDED ON NATURAL SOIL WITH AN ALLOWABLE BEARING PRESSURE OF NOT LESS THAN 100 kPa.

SG13 SLAB PANELS ARE TO BE FOUNDED ON NATURAL SOIL WITH AN ALLOWABLE BEARING PRESSURE OF NOT LESS THAN 100 kPa.

SG14 DRAINAGE AND GRADING AWAY FROM SLAB SHALL BE PROVIDED TO PREVENT WATER COLLECTING ADJACENT TO SLAB. TREATMENT OF AREAS SURROUNDING SLAB SHALL ALSO BE IN ACCORDANCE WITH RECOMMENDATIONS BY THE HOUSING GUARANTEE FUND AND THE OWNER/OCCUPIER SHALL BE PROVIDED WITH A COPY OF CSIRO INFORMATION SHEET No. 10-19.

SG15 BROCKWICK CONTROL JOINTS ARE TO BE PROVIDED ON SIDES EXCEEDING 8000mm IN LENGTH OR THROUGH LARGE OPENINGS FROM EAVES TO SLAB OR THROUGH FULL HEIGHT WINDOWS AND DOORS.

SG16 WHERE REQUIRED BY COUNCIL, PROTECT THE STRUCTURE FROM SUBTERRANEAN TERMITES IN ACCORDANCE WITH AS 3660 AND BCA

STRUCTURAL DESIGN BASED ON GEOTECHNICAL REPORT No: 7777

SUSPENDED SLAB ON GROUND NOTES

SSG1 ALL CONCRETE WORK TO COMPLY WITH AS 3600 CONCRETE CODE, AND BCA VOLUME 1, SECTIONS 3.1 AND 3.2

SSG2 CONCRETE GRADE N32 MINIMUM

SSG3 ALL VEGETATION SHALL BE STRIPPED TO A MINIMUM DEPTH OF 150mm.

SSG4 ALLOW FOR COMPACTION OF EXISTING GROUND SURFACE OR FILL SUFFICIENT TO SUPPORT WET WEIGHT OF SUSPENDED SLAB ON GROUND PLUS FORMWORK AND PROPPED STRUCTURE ABOVE, AS ADVISED BY GEOTECHNICAL CONSULTANT.

SSG5 ANY SOFT SPOTS OR DELETERIOUS MATERIAL SHALL BE REMOVED AND REPLACED WITH SELECTED FILL COMPACTED IN ACCORDANCE WITH NOTE SSG4.

SSG6 PROPOSED SELECTED FILL TO ACHIEVE REQUIRED SUB-GRADE R.L. COMPACTED IN ACCORDANCE WITH NOTE SSG4.

SSG7 A 0.2mm VAPOUR BARRIER SHALL BE USED, LAPPED A MINIMUM OF 200mm AT JOINTS AND TAPED AROUND SERVICES FITTINGS WITH ADHESIVE TAPE NOT INFERIOR TO DOUBLE SIDED BUTYL ADHESIVE TAPE. THE VAPOUR BARRIER SHALL BE PLACED ON A 50mm MINIMUM SAND BED OR SIMILAR APPROVED MATERIAL TO PROTECT MEMBRANE FROM DAMAGE.

SSG8 TOP OF SLAB SHALL BE 150mm MINIMUM ABOVE THE FINAL GROUND LEVEL.

SSG9 DRAINAGE AND GRADING AWAY FROM SLAB SHALL BE PROVIDED TO PREVENT WATER COLLECTING ADJACENT TO SLAB.

SSG10 WHERE REQUIRED BY COUNCIL, PROTECT THE STRUCTURE FROM SUBTERRANEAN TERMITES IN ACCORDANCE WITH AS 3660 AND BCA.

SSG11 BAR CHAIR BASES ARE TO BE PROVIDED BENEATH ALL REINFORCING BAR CHAIRS TO ENSURE NO SETTLEMENT TO REINFORCEMENT OR DAMAGE TO VAPOUR BARRIER.

SSG12 SUB-GRADE AND SAND LAYER TO BE PREPARED SUCH THAT A STABLE AND LEVEL PLATFORM IS CONSTRUCTED ENSURING UNIFORM COVER TO REINFORCEMENT IS ACHIEVED ACROSS THE ENTIRE EXTENT OF THE SLAB.

POST TENSIONED CONCRETE

PT1 FULL COMPUTATIONS AND DETAILS OF PROPOSED SYSTEM SHALL BE SUBMITTED TO THE ENGINEERS FOR APPROVAL, INCLUDING DEAD, LIVE ANCHORAGE DETAILS AND LOSSES OCCURRING THROUGHOUT THE ANCHOR AND ATTACHMENTS.

PT2 ANY POST TENSIONING MATERIALS AND OPERATIONS SHALL COMPLY WITH THE REQUIREMENTS OF THE SPECIFICATION AND WITH AS 3600.

PT3 CONCRETE: f_c = 32 MPa
SLUMP = 60mm ± 15mm
BASIC SHRINKAGE STRAIN = 700 x 10⁻⁶ AT 56 DAYS.

PT4 TENDONS SHALL COMPRISE OF A NUMBER OF STRANDS AS NOTED ON THE DRAWINGS. STRANDS SHALL BE 7 WIRE STRESS RELIEVED LOW RELAXATION 127mm DIAMETER SUPERGRADE STRAND OF 184kN MINIMUM BREAKING LOAD, WHERE 15.2mm DIAMETER STRANDS ARE SPECIFIED THEY SHALL BE SUPERGRADE STRANDS OF 250kN MINIMUM BREAKING LOAD.

PT5 STEEL PRESTRESSING MATERIALS FOR CONCRETE SHALL COMPLY WITH AS/NZS 4672.

PT6 WHERE APPLICABLE, MATERIALS SHALL BE CUT AND BENT IN ACCORDANCE WITH AS 3600, AS 5100 OR AS 2870.

PT7 ACCEPTABLE MANUFACTURERS AND PROCESSORS OF STEEL REINFORCING AND PRESTRESSING MATERIALS MUST ALSO HOLD A VALID CERTIFICATE OF APPROVAL, ISSUED BY THE AUSTRALIAN CERTIFICATION AUTHORITY FOR REINFORCING STEELS LTD (ACRS). MATERIALS CERTIFIED TO AN ALTERNATIVE SYSTEM SHALL NOT BE USED WITHOUT DEMONSTRATED EQUIVALENCE AND SUBSEQUENT WRITTEN APPROVAL FROM THE SPECIFIER.

PT8 EVIDENCE OF COMPLIANCE WITH THIS CLAUSE MUST BE OBTAINED WHEN CONTRACT BIDS ARE RECEIVED.

PT9 THE CONTRACTOR MUST SUBMIT FOR APPROVAL SHOP DRAWINGS OF THE TENDON LAYOUT SHOWING TENDON PROFILES, ANCHOR DETAILS AND PROPOSED STRESSING SEQUENCE.

PT10 THE CONTRACTOR SHALL SUBMIT FOR APPROVAL CALIBRATION DATA FOR EVERY JACK TO BE USED ON THE JOB.

PT11 THE POST TENSIONED STRUCTURE SHALL BE CAST AS INDICATED ON THE PLAN WITH 25% PARTIAL TENSIONING APPLIED AT NOT MORE THAN 24 HOURS AFTER CASTING.

PT12 AND WHEN f_{cp} = 7 MPa (FOR 12.7mm DIA. STRANDS), OR WHEN f_{cp} = 9 MPa (FOR 15.2mm DIA. STRANDS).

PT13 FINAL TENSIONING SHALL BE APPLIED NOT LESS THAN 4 DAYS AFTER FINAL CASTING AND WHEN f_{cp} = 20 MPa (BY TEST). THE NEW FLOOR OVER SHALL NOT BE POURED UNTIL FINAL TENSIONING HAS BEEN APPLIED TO THE FLOOR BELOW.

PT14 TENDONS SHALL BE STRESSED TO A MAXIMUM OF 85 % OF THE TENSILE STRENGTH OF THE STRAND. PRESTRESSING OF TENDONS AFTER INITIAL STRESSING SHALL BE CARRIED OUT WHERE NECESSARY TO MAINTAIN 'DESIGN' PRESTRESSING FORCES AT ANCHORAGES AT THE LEVELS SPECIFIED.

PT15 THE FLOOR DESIGN ASSUMES A 75mm WIDE x 19mm DEEP DUCT OF ZINC COATED STEEL HAVING A CURVATURE COEFFICIENT (u) = 0.20 AND AN ANGULAR COEFFICIENT (θ) = 0.02.

PT16 DRAPED DIMENSIONS ARE MEASURED FROM THE CONCRETE SOFFIT TO UNDERSIDE OF DUCT. ANCHORAGE DIMENSIONS ARE FROM CONCRETE SOFFIT TO CENTRE LINE OF DUCT. TENDON DRAPE BETWEEN POINTS NOMINATED ARE PARABOLIC WITH SHALLOW CURVATURE AT CHANGE OF GRADE AS REQUIRED. THE SLAB TENDON PROFILES SHALL BE KEPT HORIZONTAL ACROSS THE WIDTH OF THE BEAMS UNLESS OTHERWISE NOTED. THE TOLERANCE ON THE TENDON PROFILE IS TO BE ± 3mm.

PT17 TENDON SPLICING SHALL TAKE PRECEDENCE OVER NON-TENSIONED REINFORCEMENT.

PT18 ENSURE MINIMUM 50mm SPACING BETWEEN BARS AND TENDONS FOR CONCRETE PLACING. PROVIDE SPECIAL CARE TO ENSURE PLACEMENT AND PROPER COMPACTION OF CONCRETE AROUND TENDONS AND ANCHORAGES.

PT19 ALL STRESSING EXTENSION RESULTS ARE TO BE SUBMITTED FOR APPROVAL BEFORE ANY STRANDS ARE CUT. TENDONS SHALL BE FULLY GROUTED AFTER APPROVAL OF STRAND EXTENSION RESULTS AND WITHIN 4 WEEKS OF POURING IN A MANNER APPROVED BY THE ENGINEER.

CONCRETE

SHALL COMPLY TO AS3600 AND AS 3610

C1 CONCRETE SIZES DO NOT INCLUDE FINISHES.

C2 NO HOLES, CHASES OR EMBEDMENTS OTHER THAN THOSE SHOWN ON THE DRAWINGS SHALL BE GIVEN IN CONCRETE ELEMENTS WITHOUT ENGINEER'S APPROVAL.

C3 ALL VEGETATION SHALL BE STRIPPED TO A MINIMUM DEPTH OF 150mm. ANY SOFT SPOTS OR DELETERIOUS MATERIAL SHALL BE REMOVED AND REPLACED WITH APPROVED GRANULAR FILLING COMPACTED TO 100% AS STANDARD.

C4 COMPACTION, MINOR FILLING (800 MAXIMUM) SHALL BE PROVIDED WHERE REQUIRED TO BRING SLAB GRADE TO REQUIRED LEVEL. IN ACCORDANCE WITH LIMITS STATED IN AS 2870 AND BCA, FILLING SHALL BE APPROVED GRANULAR MATERIAL PLACED IN 150mm AND COMPACTED TO 100% AS STANDARD.

C5 COMPACTION

C6 SATISFACTION OF THE ENGINEER, BUILDER SHALL ALLOW FOR ALL NECESSARY CONSTRUCTION JOINTS.

C7 WHERE NOTED ON DRAWINGS CAMBER TO SUSPENDED SLABS AND BEAMS SHALL BE 5 FOR EVERY 2500 OF SPAN UNLESS OTHERWISE NOTED. WHERE THE CONCRETE SOFFITS ARE CAMBERED, ALL UPPER SURFACES SHALL BE CAMBERED. DEPTH GAUGES SHALL BE USED TO VERIFY THE SLAB THICKNESS.

C8 REINFORCEMENT IS SHOWN DIAGRAMMATICALLY AND IS NOT NECESSARILY IN TRUE PROJECTION. SPLICES TO REINFORCEMENT SHALL BE MADE ONLY AT THE LOCATION SHOWN OR AS OTHERWISE APPROVED BY THE ENGINEER. WELDING OF REINFORCEMENT SHALL BE CARRIED OUT BY A QUALIFIED WELDER IN ACCORDANCE WITH AS/NZS 1554 PART 3.

C9 THE REINFORCEMENT SYMBOLS ARE:
N: NORMAL DUCTILITY CLASS HOT ROLLED 500N DEFORMED BARS WITH f_y = 500 MPa.
R: NORMAL DUCTILITY CLASS 250N PLAIN ROUND BARS WITH f_y = 250 MPa.
L: LOW DUCTILITY CLASS HARD DRAWN 500L WIRE REINFORCING MESH WITH f_y = 500 MPa.
DO NOT USE LOW DUCTILITY CLASS L REINFORCEMENT UNLESS SHOWN ON THE DRAWINGS.

C10 THE NUMBER FOLLOWING THE REINFORCEMENT SYMBOL IS THE NOMINAL BAR SIZE IN MILLIMETRES. ALL REINFORCING MATERIAL SHALL COMPLY WITH AS/NZS 4671. WHERE APPLICABLE, MATERIALS SHALL BE CUT AND BENT IN ACCORDANCE WITH AS 3600, AS 5100 OR AS 2870.

C11 ACCEPTABLE MANUFACTURERS AND PROCESSORS OF STEEL REINFORCING AND PRESTRESSING MATERIALS MUST ALSO HOLD A VALID CERTIFICATE OF APPROVAL, ISSUED BY THE AUSTRALIAN CERTIFICATION AUTHORITY FOR REINFORCING STEELS LTD (ACRS). MATERIALS CERTIFIED TO AN ALTERNATIVE SYSTEM SHALL NOT BE USED WITHOUT DEMONSTRATED EQUIVALENCE AND SUBSEQUENT WRITTEN APPROVAL FROM THE SPECIFIER.

C12 EVIDENCE OF COMPLIANCE WITH THIS CLAUSE MUST BE OBTAINED WHEN CONTRACT BIDS ARE RECEIVED.

C13 HOOKS AND COGS SHALL COMPLY WITH AS3600 UNLESS NOTED OTHERWISE. ALL PULL OUT BARS SHALL BE TEMPORARY BARS OR APPROVED EQUIVALENT.

C14 BENDING AND REBENDING OF BARS SHALL BE CARRIED OUT IN ACCORDANCE WITH AS3600, AS/NZS 4671, THE SPECIFICATIONS AND THE REINFORCEMENT SUPPLIER RECOMMENDATIONS. BARS SHALL NOT BE HEATED ABOVE 400 DEGREES WITHOUT THE ENGINEER'S WRITTEN APPROVAL. THERMAL CRACKS SHALL BE USED TO ENSURE COMPLIANCE WITH THIS TEMPERATURE LIMIT.

C15 COVER TO REINFORCEMENT (IN mm) AND CONCRETE GRADES SHALL BE AS FOLLOWS UNLESS NOTED OTHERWISE: THE COVER SHALL NOT BE LESS THAN THE BAR DIAMETER AND:

ELEMENT	FORMED AND INTERNAL	FORMED AND EXPOSED TO WEATHER (1)	NOT FORMED CAST AGAINST GROUND (2)
FOOTINGS, PILE CAPS	-	60	75
COLUMNS, PEDESTALS	40	50	75
SLABS, BAND BEAMS	20(3)	40	60
BEAMS	30	40	60
WALLS	-	-	-
HORIZONTAL BARS	30	40	60
VERTICAL BARS	40	50	60
MINIMUM CONCRETE GRADE	N25	N32	N25 (4)

- (1) FOR EXPOSURE CLASSIFICATION B2 AND D5mm TO THE COVER AND THE CONCRETE GRADE SHALL BE M40 MINIMUM.
- (2) IF THE ELEMENT IS CAST ON A DAMP PROOF MEMBRANE, DECREASE THE COVER BY 20mm.
- (3) FOR PRESTRESSING TENDONS THE MINIMUM COVER SHALL BE 25mm.
- (4) IN CORROSIVE SOILS AND WATER: N50
- NOTES:
- (i) COVER IS THE CLEAR DISTANCE BETWEEN ANY REINFORCING (INCLUDING FITMENTS) AND THE FACE OF THE STRUCTURAL ELEMENT.
- (ii) FOR ALL EXTERNAL SURFACES, PROVIDE FULLY PLASTIC BAR CHAIRS. TIE WIRE SHALL NOT BE WEALED TO THE FORMS. REINFORCING BARS SHALL NOT BE USED TO KEEP FORMS APART AND A THROUGH TIE SYSTEM SHALL BE USED TO THE FORMS.
- (iii) PROVIDE AN APPROVED VAPOUR BARRIER FOR SLABS, BEAMS AND THICKENING CAST AGAINST THE GROUND.
- (iv) THE COVERS SHALL BE MAINTAINED USING APPROVED BAR CHAIRS. BAR CHAIRS SUPPORTING MESH SHALL BE AT 600 x 800mm MAXIMUM CENTRES. BAR CHAIRS SUPPORTING BARS SHALL BE AT 60 BAR DIAMETERS OR 1500 MAXIMUM CENTRES WHICHEVER IS THE LESSER. BAR CHAIRS SHALL BE PROVIDED ALONG THE EDGES OF ALL CONSTRUCTION JOINTS. STOP ENDS SHALL NOT BE USED TO MAINTAIN THE COVERS.
- (v) EXTERNAL ELEMENTS ARE THOSE EXPOSED TO WEATHER, RAIN AND WATER PENETRATION AND ARE CLASSIFIED B1 UNLESS NOTED OTHERWISE.

C11 EXTERNAL CONCRETE ELEMENTS ABOVE GROUND SHALL MEET THE FOLLOWING REQUIREMENTS: MINIMUM PORTLAND CEMENT CONTENT 330 kg/m³; MAXIMUM WATER/CEMENT RATIO 0.5, AND THE CHLORIDE CONTENT RESTRICTED AS PER CLAUSE 4.9 OF AS3600.

C12 ALL CONCRETE SUPPLIED SHALL HAVE A SLUMP OF 80mm AND A MAXIMUM NOMINAL AGGREGATE SIZE OF 20mm. VARIATIONS FROM THESE SHALL BE APPROVED BY THE ENGINEER.

C13 THE MIX DESIGN WITH THE 7 AND 28 DAYS TARGET STRENGTHS AND THE BASIC SHRINKAGE STRAIN AT 56 DAYS SHALL BE SUBMITTED FOR REVIEW PRIOR TO POURING ANY CONCRETE.

C14 ALL CONCRETE IN CONTACT WITH AGGRESSIVE SOIL SHALL HAVE SULPHATE RESISTING CEMENT. THE C3A CONTENT OF THE CEMENT SHALL BE LESS THAN 5%.

C15 CONDUITS AND PIPES WHEN CAST IN SLABS OR WALLS ARE TO BE PLACED BETWEEN THE TWO REINFORCEMENT LAYERS, WHERE THERE IS ONLY ONE LAYER OF REINFORCEMENT, PROVIDE 20mm COVER TO CONDUIT. THE CONDUIT LOCATIONS ARE TO BE APPROVED BY THE ENGINEER.

C16 WHERE DISTRIBUTION BARS TO MAIN REINFORCEMENT ARE NOT SHOWN ON DRAWINGS PROVIDE MINIMUM N16 AT 400 CENTRES, LAPPED 500mm AT SPLICES.

C17 FORMWORK SHALL BE DESIGNED, CONSTRUCTED AND SUPPLIED IN ACCORDANCE WITH AS 3610. REFER TO ARCHITECTURAL DRAWINGS AND SPECIFICATIONS FOR CLASSES OF SURFACE FINISHES.

C18 STRIPPING AND BACKPROPPING OF SOFFITS SHALL NOT OCCUR UNTIL CONCRETE HAS REACHED 75% OF SPECIFIED STRENGTH. BACKPROPPING (OR A SECOND SET OF TABLE LAYOUT) SHALL BE EXTENDED DOWN TO THE EXISTING FLOOR IS SUPPORTED BY AT LEAST 3 FINISHED FLOORS OR AS CALICATED. DO NOT STRIP BAYS ADJACENT CONSTRUCTION JOINTS UNTIL THE ADJACENT BAYS ARE AT LEAST 3 DAYS OLD. CALCULATIONS ON THE BACKPROPPING REQUIREMENTS SHALL BE SUBMITTED FOR APPROVAL.

C19 CURING OF THE CONCRETE ELEMENTS SHALL BE STARTED AS SOON AS THE CONCRETE HAS HARDENED AND SHALL COMPLY WITH THE SPECIFICATIONS.

C20 PROVIDE A 25mm x 25mm CHAMFER TO ALL CORBELLS, UNLESS OTHERWISE INDICATED ON THE DRAWING. ENSURE THAT POLYSTYRENE IS PLACED AROUND THE BEARING, SO THAT THE CONCRETE SURFACES ARE NOT IN CONTACT. SUBMIT CONFIRMATION OF THE SPECIFICATIONS AND ALL BEARING MATERIALS TO THE ENGINEER.

STRUCTURAL MASONRY

M1 ALL BLOCKWORK WALLS SHALL BE CONSTRUCTED IN UNITS WITH A MINIMUM CHARACTERISTIC UNCONFINED COMPRESSIVE STRENGTH f_{cu} = 15 MPa.

M2 ALL BRICKS SHALL HAVE A MINIMUM CHARACTERISTIC UNCONFINED COMPRESSIVE STRENGTH f_{cu} = 25 MPa.

M3 THE MAXIMUM UNRESTRAINED FIVE YEAR EXPANSION OF BRICKS SHALL BE 0.7mm/m IN ACCORDANCE WITH NATA REGISTERED TEST B01.

M4 UNLESS NOTED OTHERWISE THE NOMINAL PROPORTIONS BY VOLUME OF MORTAR SHALL BE CLASS M3 AND HAVE NOMINAL PROPERTIES OF 1 : 1 : 6 OF CEMENT, LIME SAND, NO PLASTISERS SHALL BE USED IN THE MIX.

M5 GROUT USED TO FILL CAVITIES AND CORES IN REINFORCED MASONRY SHALL HAVE A MINIMUM 28 COMPRESSIVE STRENGTH f_{cu} OF 20 MPa AND A SLUMP OF 225 ±25mm. MAXIMUM AGGREGATE SHALL BE OF 10mm ROUNDED GRAVEL. NOMINAL PORTLAND CEMENT SHALL BE 1: 3: 3: 2 OF CEMENT, LIME, SAND, AGGREGATE AND 3 WITH A MINIMUM CEMENT CONTENT OF 300 kg/m³. PROVIDE CLEAN OUT HOLES AT BASE OF PILASTERS AND EVERY CORE OF REINFORCED WALLS. CLEAN OUT AND WET DOWN CORES BEFORE GROUTING. ALL CORES CONTAINING VERTICAL AND HORIZONTAL REINFORCEMENT ARE TO BE GROUTED.

M6 HORIZONTAL JOINT REINFORCEMENT CONSISTING OF GALVANIZED WOVEN WIRE MESH OR WELDED WIRE SHALL BE PROVIDED. THE WIDTH SHALL BE SUCH THAT 15mm COVER FROM THE MORTAR FACE IS PROVIDED. THE MESH SHALL BE PLACED IN THE FIRST THREE COURSES AT THE TOP AND BOTTOM OF THE WALL AND AT A MAXIMUM 600 mm VERTICAL SPACING IN BETWEEN. FOR ALL CONCRETE BLOCKWORK, CONCRETE BRICKWORK AND CALCULI SILICATE BRICKWORK, THE MESH SHALL BE LAPPED 450mm AT SPLICES AND FOLDED AND BENDED AT THE CORNERS SO THAT THE LONGITUDINAL WIRES ARE CONTINUED. THE MESH IS STOPPED 100mm SHORT OF CONTROL JOINTS OR ENDS OF WALLS.

M7 FULLY BED FACE SHELLS AND CROSS WEBS IN HOLLOW BLOCK WALLS. SOLID OR CORED UNITS SHALL BE LAID ON A FULL BED OF MORTAR.

M8 HOLLOW BLOCKWORK OPENINGS GREATER THAN 600mm VERTICALLY OR HORIZONTALLY SHALL BE TRIMMED AT THE SIDES AND BOTTOM BY FILLING ONE CORE AND REINFORCED WITH N12 EXTENDING 600mm PAST OPENING. THE TOP OF THE OPENING SHALL HAVE A REINFORCED LINTEL BEAM, ARCH BAR OR STEEL ANGLE SUPPORT AS DETAILED.

M9 HOLLOW BLOCKWORK SHALL HAVE MINIMUM CLEAR COVER OF 50mm TO EXTERNAL FACE OF MASONRY. TIES SHALL CONFORM TO AS 2699. ALL TIES SHALL BE BY 'CERRA MATERIALS' OR APPROVED EQUIVALENT. THE TIES SHALL BE FIXED TO THE MANUFACTURER'S RECOMMENDATIONS BUT WITH A MINIMUM OF 2 NO. 8mm DIAMETER DRIPNIPS. ALL TIES SHALL BE AT 400mm MAXIMUM CENTRES UNLESS NOTED OTHERWISE.

M10 NO CAVITY OR CORE SHALL BE FILLED TO A HEIGHT GREATER THAN 1200mm WITHOUT SUITABLE SHORING.

M11 NO CHASES OR HOLES SHALL BE MADE WITHOUT PRIOR APPROVAL OF THE ENGINEER. CONDUITS AND THE LIKE SHALL NOT BE PLACED INSIDE CORES CONTAINING REINFORCEMENT.

M12 VERTICAL JOINTS SHALL BE AT THE LESSER OF 6000mm OR TWICE THE HEIGHT OF THE WALL AND AT THE FOLLOWING LOCATIONS:
- AT MAJOR CHANGES IN WALL HEIGHT
- AT CHANGES IN WALL THICKNESSES OTHER THAN PIERS OR BUTTRESSES
- AT CONTROL JOINTS IN THE ADJACENT STRUCTURAL ELEMENTS
- AT CHASES AND RECESSES FOR PIPING, COLUMNS FIXTURES ETC.
- AT ONE OR BOTH SIDES OF WALL OPENINGS
- NEAR WALL INTERSECTIONS
- NEAR RETURN ANGLES IN L, T AND U SHAPED STRUCTURES

M13 WHERE SHOWN IN THE ARCHITECTURAL DRAWINGS THE CONTRACTOR IS TO OBTAIN APPROVED DRAWINGS SHOWING THE CONTROL JOINTS PRIOR TO BUILDING ANY WALL.

M14 ALL INTERSECTIONS THAT DON'T HAVE A CONTROL JOINT SHALL BE OF BONDED CONSTRUCTION OR TIED WITH HEAVY DUTY TIES AT 400mm MAXIMUM VERTICAL CENTRES.

M15 ALL CAVITY WALLS ARE TO BE CONSTRUCTED USING MEDIUM DUTY MASONRY TIES AT 800mm MAXIMUM CENTRES BOTH WAYS AND 300mm AVERAGE CENTRES EACH SIDE OF OPENINGS. THE TIES SHALL BE EMBEDDED 50mm MINIMUM INTO EACH LEAF, WITH A 30mm COVER TO THE EXPOSED FACES.

M16 WHERE A CONCRETE SLAB IS SUPPORTED ON MASONRY WALLS, THE TOP COURSE OF BLOCKS SHALL BE SOLID OR HOLLOW BLOCKS WITH CAVITIES FILLED TO A SMOOTH SURFACE OR A REINFORCED CONCRETE BEAM. IN THE CASE OF BRICKS THE UPPER COURSE SHALL BE PROGS DOWN, OR HOLES FILLED WITH MORTAR TO A SMOOTH SURFACE. FOR NON-LOAD BEARING WALLS, LEAVE A 20mm GAP TO THE UNDERSIDE OF THE STRUCTURE.

M17 BONDING SHALL BE STRETCHER BOND UNLESS NOTED OTHERWISE.

M18 WHEN CONSTRUCTING MASONRY WALLS ON SUSPENDED SLABS, ALL MASONRY UNITS SHALL BE STACKED NEAR THE FINAL LOCATION BEFORE BUILDING THE WALL. THE SUPPORTING ELEMENT MUST NOT BE PROPPED AND MUST HAVE ACHIEVED ITS DESIGN STRENGTH.

M19 FOR AREAS OF THE STRUCTURAL FLOOR SYSTEM WHICH SUPPORT MASONRY WALLS PARTITIONS OR OTHER SENSITIVE ATTACHMENTS AT THE TIME OF THE INITIAL DESIGN, THE FLOOR SYSTEM HAS BEEN DESIGNED FOR NOT LESS THAN THE REQUIREMENTS OF AS 3600 TABLE 2.4.2.2 WHERE PROVISION IS MADE TO MINIMISE THE EFFECT OF MOVEMENT.

M20 GENERIC JOINT DETAILS ARE INDICATED ON THESE DRAWINGS FOR INFORMATION, BUT IT IS THE ARCHITECT'S RESPONSIBILITY TO IDENTIFY JOINT LOCATIONS AND TYPES WHERE APPROPRIATE ON ARCHITECTURAL DRAWINGS, AND TO PROVIDE DETAILS OF NON-STANDARD ELEMENTS TO ACCOMMODATE ANTICIPATED MOVEMENTS.

M21 WALLPARTITIONS AND OTHER NON-LOAD BEARING MASONRY ARE NOT INCLUDED IN THE STRUCTURAL ENGINEER'S SCOPE OF WORKS.

M22 STACKING OF BLOCKWORK:
- GENERALLY, SUSPENDED SLABS AND SLABS ON GROUND, BLOCKS SHALL BE STOCKED ONE Pallet HIGH (MAXIMUM PALLET MASS 1300kg) WITH 1200mm CLEARANCE BETWEEN ADJACENT PALLET ON ALL SIDES. THE WEIGHT OF STACKED BLOCKS SHALL NOT EXCEED THE DESIGN LIVE LOAD FOR THE FLOOR. REFER PLANS FOR DESIGN LOADS.

STEELWORK

SHALL COMPLY TO AS 4100, AS/NZS 4600 AND AS/NZS 3628

S1 THE FABRICATOR SHALL BE RESPONSIBLE FOR SUBMITTING SHOP DRAWINGS, WHICH SHALL COMPLY WITH THE CONTRACT DRAWINGS AND SPECIFICATIONS, FOR REVIEW BEFORE FABRICATION IS STARTED. REVIEW DOES NOT INCLUDE CHECKING OF DIMENSIONS, NOR TAKE RESPONSIBILITY FOR CONTRACTORS OBLIGATIONS. ALLOW 3 WORKING DAYS MINIMUM FOR REVIEW.

S2 WHERE CONNECTION FORCES (IN KILONEUTONS) ARE SHOWN ON THE DRAWINGS, CONNECTIONS SHALL BE PROVIDED TO TRANSMIT THESE FORCES. CONNECTIONS SHALL PROVIDE FOR A MINIMUM FORCE OF 40kN.

S3 ALL DETAILS GAUGE LINES, ETC. WHERE NOT SPECIFICALLY SHOWN SHALL BE IN ACCORDANCE WITH AISC DESIGN CAPACITY TABLES FOR STRUCTURAL STEEL AND ALSO STANDARDIZED STRUCTURAL CONNECTIONS.

S4 UNLESS OTHERWISE NOTED, WELDS TO BE 6mm CONTINUOUS FILLETS LAID DOWN WITH APPROVED COVERED ELECTRODES. ALL WELDS SHALL BE CATEGORY S3 UNLESS OTHERWISE NOTED. WELDS SHALL CONFORM TO AS/NZS 1554 AND ELECTRODES TO AS/NZS 1553. GUSSET PLATES TO BE 10mm THICK. BOLTS TO BE M20-8.8S IN 22mm DIAMETER HOLES. PROVIDE A MINIMUM OF TWO BOLTS PER CONNECTION.

S5 FABRICATOR SHALL PROVIDE ALL FIXINGS FOR ARCHITECTURAL ELEMENTS ETC. WITHOUT WEAKENING STRUCTURAL MEMBER IN ANY WAY.

S6 CAMBER SHALL BE PROVIDED TO ALL ROOF BEAMS, TRUSSES, AND PORTALS ETC. AT 5 PER 2000 OF SPAN UNLESS OTHERWISE NOTED. FOR ALL MEMBERS SPANNING IN EXCESS OF 6m, NO MEMBER SHALL BE ERRECTED WITH NEGATIVE CAMBER, UNLESS SPECIFICALLY NOTED. FOR CONCRETE SLABS ON TOP OF STEELWORK DEPTH GAUGES SHALL BE USED TO VERIFY THE SLAB THICKNESS.

S7 ALL STEELWORK BELOW GROUND SHALL BE ENCASED BY CONCRETE WITH MIN. COVER OF 150mm. CONCRETE SHALL BE PLACED AND FINISHED IN ACCORDANCE WITH PRE-GALVANIZED 644MSH GHEM PLACED 25mm CLEAR OF STEEL. PROVIDE 50mm MINIMUM COVER.

S8 ALL STEELWORK NOT TO BE ENCASED IN CONCRETE OR GALVANIZED SHALL BE PROTECTED AGAINST CORROSION BY USING AN INHIBITOR. UNLESS OTHERWISE NOTED, FACES OF FRICTION GRIP CONNECTIONS SHALL NOT BE PAINTED.

S9 THE FOLLOWING PROCEDURE IS DESIGNATED AS FOLLOWS:
- 4.6/5 REFERS TO COMMERCIAL BOLTS OF STRENGTH GRADE 4.6 TO AS/NZS 1111
- 8.8/8 REFERS TO HIGH STRENGTH BOLTS OF STRENGTH GRADE 8.8 TO AS/NZS 1252 TIGHTENED USING A STANDARD WRENCH TO A SNUG-TIGHT CONDITION.
- 8.8/7 REFERS TO HIGH STRENGTH BOLTS OF STRENGTH GRADE 8.8 TO AS/NZS 1252 FULLY TENSIONED TO AS 1511, DESIGNED AS A BEARING TYPE JOINT.
- 10/10 REFERS TO HIGH STRENGTH BOLTS OF STRENGTH GRADE 10.9 TO AS/NZS 1252 FULLY TENSIONED TO AS 1511, DESIGNED AS A BEARING TYPE JOINT.
- 10/10 REFERS TO HIGH STRENGTH BOLTS OF STRENGTH GRADE 10.9 TO AS/NZS 1252 FULLY TENSIONED TO AS 1511, DESIGNED AS A BEARING TYPE JOINT.

S10 LOAD INDICATING WASHERS SHALL BE USED TO VERIFY TIGHTENING OF BOLTS IN T AND TB CONNECTIONS. A HARDENED WASHER SHALL BE USED UNDER THE BOLT HEAD OR NUT, WHICHEVER IS ROTATED. FULLY TENSIONED BOLTS SHALL NOT BE RE-USED. WELDING OF CAPTIVE NUTS TO STEELWORK SHALL BE GRADE 4.6S, CLASS 5 NUTS. THE ELECTRODES USED SHALL BE COMPATIBLE WITH THE CHEMISTRY OF THE STEEL. INVOLVED MEMBER OR CONNECTION COMPONENT AND THE BOLT DIAMETER SHALL HAVE 100% VISUAL INSPECTION. GRADE 4.6S BOLTS TO BE USED.

S11 ALL BOLTS SHALL BE OF SUCH LENGTH THAT AT LEAST ONE FULL THREAD IS EXPOSED BEYOND THE NUT AFTER THE NUT HAS BEEN TIGHTENED.

S12 MINIMUM STRENGTH OF GROUT TO BE f_{cu} = 25 MPa AT TIME OF LOAD TRANSFER. THE GROUT MIX SHALL BE OF DRY CONSISTENCY, RAM PACKED OVER THE FULL WIDTH AND DEPTH OF THE UNDERPINNING AND SHALL BE A MINIMUM OF 2 DAYS OLD BEFORE EXCAVATING THE NEXT PIN IN SEQUENCE.

S13 UNLESS NOTED OTHERWISE, ALL MATERIAL TO BE:
- GRADE 250 HOT ROLLED PLATES, FLATS
- GRADE 300PLS UB, UC, PFC, TFB AND ANGLES
- GRADE 300 WB, WC
- GRADE 350 RHS, CHS.

S14 STRUCTURAL STEEL SHALL COMPLY WITH AS/NZS 1163, AS/NZS 3678, AS/NZS 3679/1 OR AS/NZS 3679/2. TEST CERTIFICATES RELATING TO THE STRUCTURAL STEEL SUPPLIED, SHOL BE MADE AVAILABLE TO THE BUILDER.

S15 ACCEPTABLE MANUFACTURERS OF STRUCTURAL STEEL MUST ALSO HOLD A VALID CERTIFICATE OF APPROVAL, ISSUED BY THE AUSTRALIAN CERTIFICATION AUTHORITY FOR REINFORCING STEELS LTD (ACRS). MATERIALS CERTIFIED TO AN ALTERNATIVE SYSTEM SHALL NOT BE USED WITHOUT DEMONSTRATED EQUIVALENCE AND SUBSEQUENT WRITTEN APPROVAL FROM THE SPECIFIER.

S16 EVIDENCE OF COMPLIANCE WITH THIS CLAUSE MUST BE OBTAINED WHEN CONTRACT BIDS ARE RECEIVED.

S17 HOT DIPPED GALVANIZING SHALL BE IN ACCORDANCE WITH AS 4690 MINIMUM COATING THICKNESS OF 85 MICRONS. PROVIDE MEMBERS TO BE GALVANIZED WITH VENT AND DRAINAGE HOLES IN ACCORDANCE TO THE GALVANISER'S RECOMMENDATIONS AND THE ACCEPTANCE OF THE ENGINEER.

S18 THE ENDS OF TUBULAR MEMBERS SHALL BE SEALED WITH NOMINAL THICKNESS PLATES AND CONTINUOUS FILLET WELDED UNLESS NOTED OTHERWISE.

S19 WHERE MEMBERS SHOWN ON THE STRUCTURAL OR ARCHITECTURAL DRAWINGS ARE REQUIRED TO BE CURVED, BENT OR ROLLED, THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE METHODS REQUIRED TO ACHIEVE THE REQUIRED SHAPES WITHOUT LOCALIZED DISTORTION TO THE STRUCTURE.

S20 THE CONTRACTOR SHALL PROVIDE AND LEAVE IN PLACE, UNTIL PERMANENT BRACING ELEMENTS ARE CONSTRUCTED, SUCH TEMPORARY BRACING AS IS NECESSARY TO STABILIZE THE STRUCTURE DURING ERECTION. REFER TO NOTES G4 AND G5.

S21 THE DESIGN, SUPPLY AND INSTALLATION OF SECONDARY STEELWORK REQUIRED TO SUPPORT/CONNECT THE FACADE TO BASE STRUCTURE IS THE RESPONSIBILITY OF THE CONTRACTOR.

S22 CERTIFICATION OF ARCHITECTURAL FIXINGS/BRACING OF CEILINGS AND NON-STRUCTURAL WALLS TO THE BASE STRUCTURE SHALL BE OBTAINED FROM THE CONTRACTOR, FORWARD TO THE ENGINEER A CERTIFICATE OF SUFFICIENCY BY THE SUPPLIER FOR THE ARCHITECTURAL FIXTURES/PANELS/DORY-WALL TO RESIST THE PRESSURES DESIGNATED IN THE DESIGN DOCUMENTS.

UNDERPINNING NOTES

GENERAL

U1 THESE NOTES MUST BE READ IN CONJUNCTION WITH RELATIVE SECTIONS OF THE SPECIFICATIONS.

U2 CONCRETE STRENGTH FOR THE UNDERPINS SHALL BE f_{cu} = 25MPa. CONCRETE SHALL BE SAMPLED AND TESTED IN ACCORDANCE WITH AS 1460 - CONCRETE STRUCTURES CODE.

U3 THE BUILDERS SHALL PROVIDE ANY PROPPING, SHORING ETC. NECESSARY TO SAFELY SUPPORT SITES OF EXCAVATION SO AS TO PREVENT MOVEMENT AND ENSURE THE SAFETY OF THE EXISTING BUILDING.

U4 ANY VARIATION IN FOOTINGS OF ADJACENT BUILDING TO THOSE ON THIS DRAWING IS TO BE IMMEDIATELY BROUGHT TO THE ATTENTION OF THE ENGINEER.

CONSTRUCTION PROCEDURE

U5 UNDERPINNING SHALL BE CARRIED OUT IN SECTIONS NOT EXCEEDING 1200mm IN LENGTH AND TO THE FULL THICKNESS OF THE FOOTING BEING UNDERPINNED AS INDICATED ON THE DRAWING.

U6 UNDERPINS SHALL BE CONSTRUCTED IN THE NUMBERED SEQUENCE, STARTING WITH SECTIONS NOTED 1, THEN 2 & 3 PROGRESSIVELY.

U7 THE FOOTING TO BE UNDERPINNED SHALL



- FOOTINGS TO BEAR ON HIGHLY WEATHERED PHYLLITE.
- MASS CONCRETE FILL BELOW FOOTING TO PHYLLITE LEVEL AS REQUIRED.
- FOR PILES, ULTIMATE PILE END BEARING = 3000kPa AS NOTED IN GEOTECHNICAL REPORT. ULTIMATE SHAFT FRICTION OF 75kPa HAS BEEN ASSUMED. SOCKET LENGTH DENOTES PILE EMBEDMENT INTO HIGHLY WEATHERED PHYLLITE.

CONCRETE COLUMN SCHEDULE		
MARK	SIZE	REMARKS
CC1	400 x 400	R.C. COLUMN

STRIP FOOTING SCHEDULE			
MARK	DIMENSIONS		REMARKS
	WIDTH	DEPTH	
SF1	1000	400	CONCRETE STRIP FOOTING

- REFER TO DRAWING MHD-ST-DG-0001 FOR DRAWING LIST
- REFER TO DRAWING MHD-ST-DG-0010 FOR ALL GENERAL AND STRUCTURAL NOTES
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CLIENT



14/77 PACIFIC HIGHWAY
NORTH SYDNEY NSW 2060

PROJECT:

MACKSVILLE HOSPITAL REDEVELOPMENT

MACKSVILLE NSW 2447

DRAWING TITLE:

FOOTING PLAN

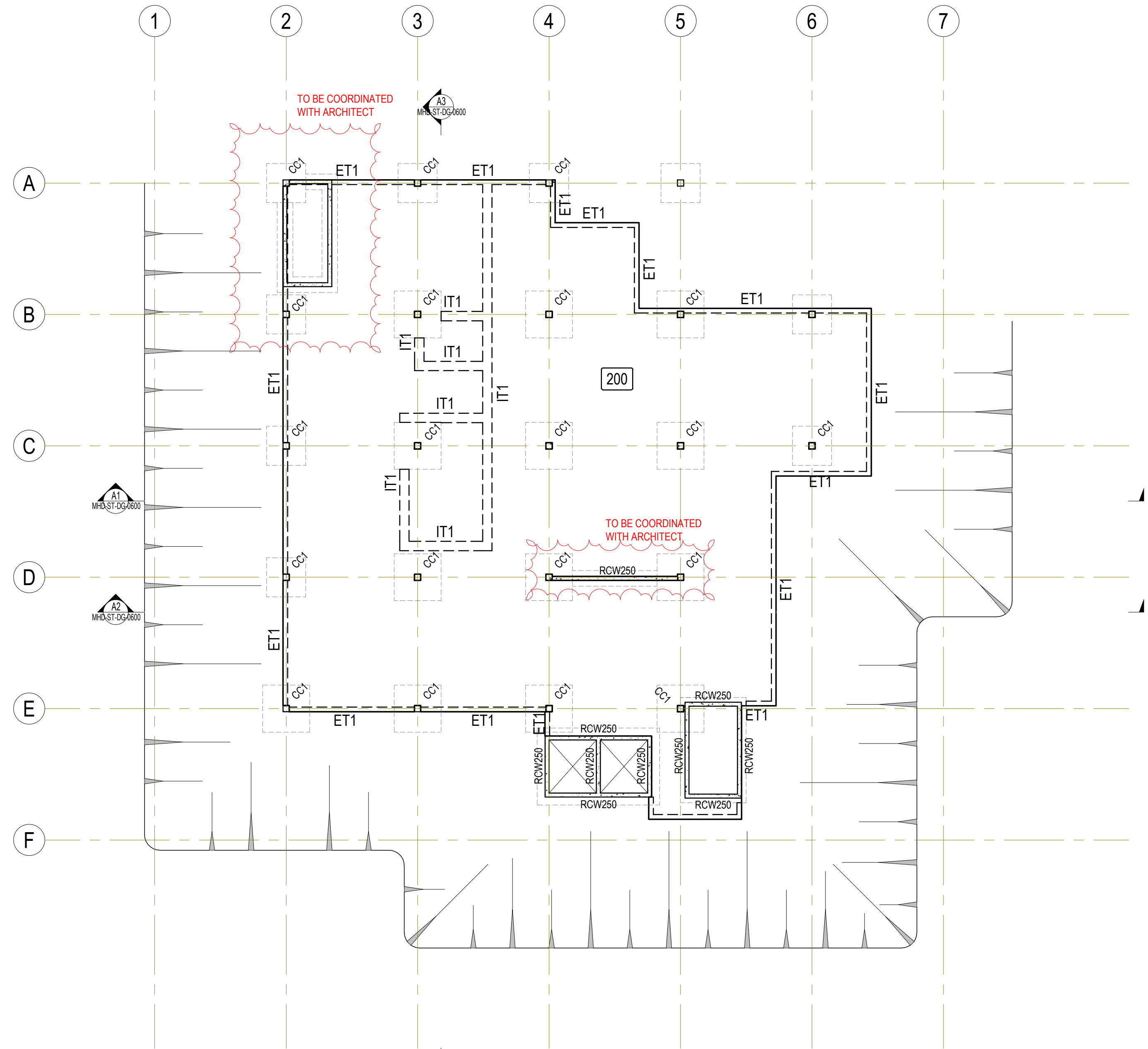
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SCHEMATIC DESIGN



BASEMENT PLAN
SCALE: 1 : 200

STRUCTURAL WALL SCHEDULE					
MARK	TYPE	THICKNESS	REINFORCEMENT		REMARKS
			VERT.	HORIZ.	
RCW250	INSITU	250			R.C. WALL

CONCRETE COLUMN SCHEDULE		
MARK	SIZE	REMARKS
CC1	400 x 400	R.C. COLUMN

CONCRETE FOOTING SCHEDULE			
MARK	DIMENSIONS		REMARKS
	WIDTH	DEPTH	
ET1	300	300	CONCRETE EDGE THICKENING
IT1	600	300	CONCRETE INTERNAL THICKENING
IT2	300	300	CONCRETE INTERNAL THICKENING

NOTE:

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LEGEND

(UNLESS OTHERWISE NOTED)

	DENOTES THICKNESS OF SLAB
	DENOTES CONSTRUCTION JOINT
	DENOTES KEYED CONSTRUCTION JOINT
	DENOTES SAW CUT JOINT
	DENOTES SLAB STEP REFER TO ARCHITECTUAL DRAWINGS FOR SETOUT AND DIMENSIONS
	DENOTES CONCRETE ELEMENT OVER
	DENOTES PRECAST ELEMENT OVER
	DENOTES LOAD-BEARING ELEMENT UNDER
	DENOTES LOAD-BEARING ELEMENT UNDER AND CONCRETE ELEMENT OVER
	DENOTES BLOCKWORK WALL OVER
	DENOTES COMPACTUS LOADING ZONE

FLOOR DESIGN LOADS

(UNLESS OTHERWISE NOTED)

GENERAL WARD	SDL - 1.8 kPa
	LL - 3.0 kPa
STAIRS	SDL - 0.5 kPa
	LL - 4.0 kPa
TERRACE	SDL - 5.0 kPa
	LL - 5.0 kPa
STEEL ROOF	SDL - 0.5 kPa (OVER WARDS, 1.0 kPa OVER PLANT ROOMS)
	LL - 0.25 kPa
LOBBY/CORRIDOR	SDL - 5.0 kPa
	LL - 3.0 kPa
PLANT	SDL - 2.0 kPa
	LL - 7.5 kPa
STORAGE	SDL - 1.8 kPa
	LL - 5.0 kPa

STRUCTURAL SIZES

(UNLESS OTHERWISE NOTED)

SLAB	GENERALLY 200mm THICK SLAB ON GROUND SL82 MESH TOP & BOTTOM
	POURED ON VAPOUR BARRIER OVER 50mm THICK SAND BLINDING LAYER OF 20mm SINGLE SIZED FREE DRAINING MATERIAL OVER ENGINEERED COMPACTED FILL, OR FIRM NATURAL GROUND.
	ALLOW FOR JOINTS AT 6m CTS BOTH WAYS

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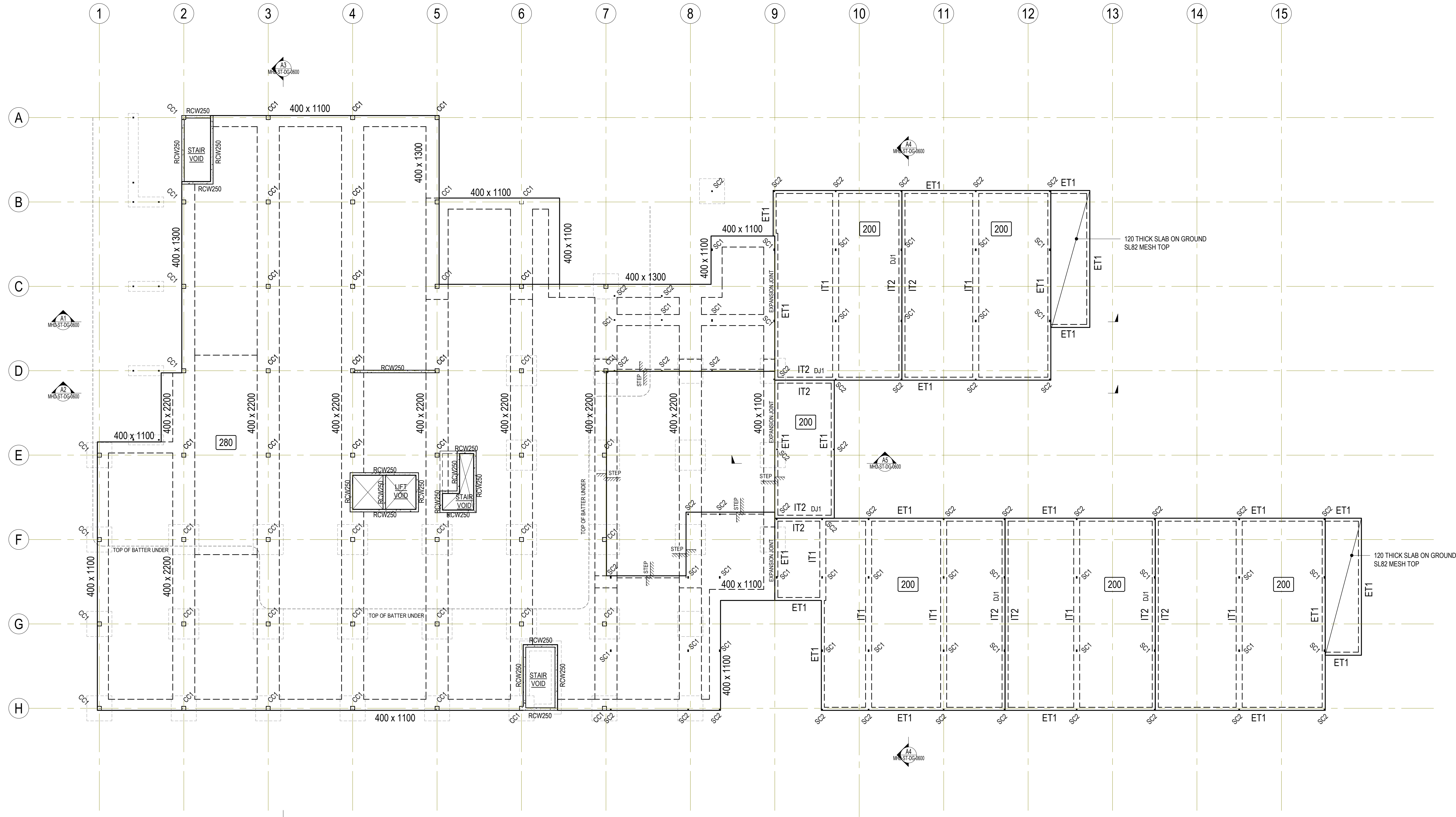
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PROJECT:
MACKSVILLE HOSPITAL REDEVELOPMENT
MACKSVILLE NSW 2447
DRAWING TITLE:
BASEMENT LEVEL

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PROJECT NUMBER: DRAWING NUMBER: ISSUE:
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SCHEMATIC DESIGN



GROUND FLOOR PLAN

SCALE: 1 : 200

STRUCTURAL WALL SCHEDULE					
MARK	TYPE	THICKNESS	REINFORCEMENT		REMARKS
			VERT.	HORIZ.	
RCW250	INSITU	250			R.C. WALL

CONCRETE COLUMN SCHEDULE		
MARK	SIZE	REMARKS
CC1	400 x 400	R.C. COLUMN

STRUCTURAL SIZES

(UNLESS OTHERWISE NOTED)

SLAB
GENERALLY 240mm THICK POST TENSIONED SLAB TO BE DESIGNED AND CERTIFIED BY D&C CONTRACTOR

STAIRS
REFER TO PART PLANS & DETAILS ON DRAWINGS S-----

CONCRETE GRADE

PT SLABS
40 MPa

LEGEND

(UNLESS OTHERWISE NOTED)

- DENOTES SPAN DIRECTION OF METAL TRAY
- DENOTES THICKNESS OF SLAB
- DENOTES DOWEL JOINT (DANLEY PLATE DOWEL ?)
- DENOTES CONSTRUCTION JOINT
- DENOTES EXPANSION JOINT
- DENOTES SLAB STEP
REFER TO ARCHITECTURAL DRAWINGS FOR SETOUT AND DIMENSIONS
- DENOTES CONCRETE ELEMENT OVER
- DENOTES LOAD-BEARING ELEMENT UNDER
- DENOTES LOAD-BEARING ELEMENT UNDER AND CONCRETE ELEMENT OVER
- DENOTES BLOCKWORK WALL OVER

FLOOR DESIGN LOADS

(UNLESS OTHERWISE NOTED)

GENERAL WARD	SDL - 1.8 kPa
	LL - 3.0 kPa
STAIRS	SDL - 0.5 kPa
	LL - 4.0 kPa
TERRACE	SDL - 5.0 kPa
	LL - 5.0 kPa
STEEL ROOF	SDL - 0.5 kPa (OVER WARDS, 1.0 kPa OVER PLANT ROOMS)
	LL - 0.25 kPa
LOBBY/CORRIDOR	SDL - 5.0 kPa
	LL - 3.0 kPa
PLANT	SDL - 2.0 kPa
	LL - 7.5 kPa
STORAGE	SDL - 1.8 kPa
	LL - 5.0 kPa

NOTE:

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PROJECT:

MACKSVILLE HOSPITAL REDEVELOPMENT

MACKSVILLE NSW 2447

DRAWING TITLE:

GROUND LEVEL

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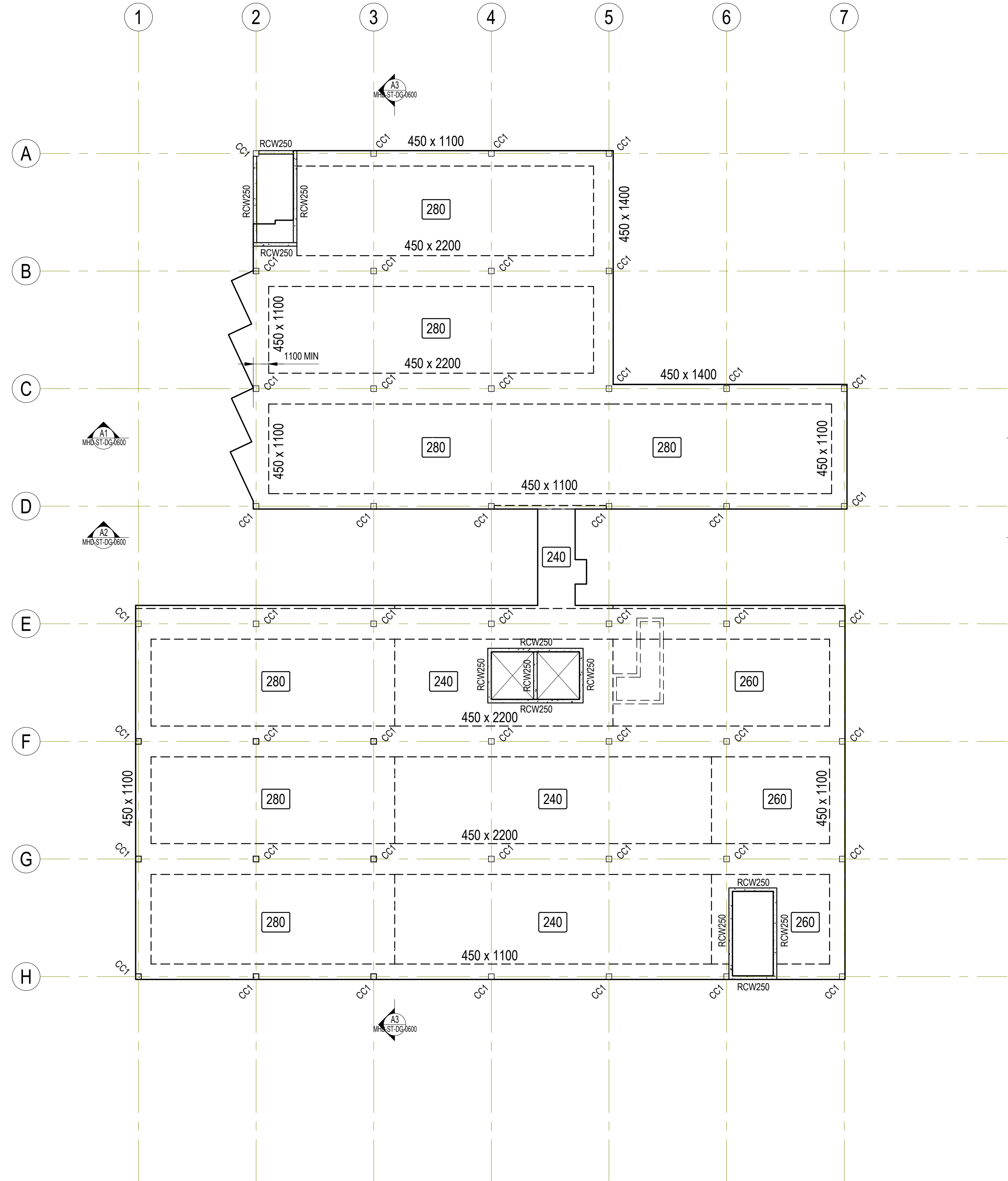
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SCHEMATIC DESIGN



FIRST FLOOR PLAN

SCALE: 1 : 200

STRUCTURAL WALL SCHEDULE					
MARK	TYPE	THICKNESS	REINFORCEMENT		REMARKS
			VERT.	HORIZ.	
RCW250	INSITU	250			R.C. WALL

CONCRETE COLUMN SCHEDULE		
MARK	SIZE	REMARKS
CC1	400 x 400	R.C. COLUMN

NOTE:

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	DENOTES SPAN DIRECTION OF METAL TRAY
	DENOTES THICKNESS OF SLAB
	DENOTES DOWEL JOINT (DANLEY PLATE DOWEL ?)
	DENOTES CONSTRUCTION JOINT
	DENOTES EXPANSION JOINT
	DENOTES SLAB STEP REFER TO ARCHITECTUAL DRAWINGS FOR SETOUT AND DIMENSIONS
	DENOTES CONCRETE ELEMENT OVER
	DENOTES LOAD-BEARING ELEMENT UNDER
	DENOTES LOAD-BEARING ELEMENT UNDER AND CONCRETE ELEMENT OVER
	DENOTES BLOCKWORK WALL OVER

FLOOR DESIGN LOADS

(UNLESS OTHERWISE NOTED)

GENERAL WARD	SDL - 1.8 kPa LL - 3.0 kPa
STAIRS	SDL - 0.5 kPa LL - 4.0 kPa
TERRACE	SDL - 5.0 kPa LL - 5.0 kPa
STEEL ROOF	SDL - 0.5 kPa (OVER WARDS, 1.0 kPa OVER PLANT ROOMS) LL - 0.25 kPa
LOBBY/CORRIDOR	SDL - 5.0 kPa LL - 3.0 kPa
PLANT	SDL - 2.0 kPa LL - 7.5 kPa
STORAGE	SDL - 1.8 kPa LL - 5.0 kPa

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DRAWING TITLE:

FIRST FLOOR LEVEL

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SCHEMATIC DESIGN

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STEEL FRAMING SCHEDULE		
MARK	SIZE	REMARKS
AB1	360 UB 45	STEEL AWNING BEAM
AB2	250 PFC	STEEL AWNING BEAM
AB3	410 UB 54	STEEL
B1	360 UB 45	STEEL BEAM
BR1	M20 DIA. ROD	ROOF BRACING (GRADE 4.6/s)
OR1	250 UB 31	STEEL OUTRIGGER
P1	Z25019	PURLIN - AT 1200 MAX. CRS. LAP 900 (2 ROWS BRIDGING EACH BAY)
P2	C25019	PURLIN - AT 1200 MAX. CRS. (2 ROWS BRIDGING EACH BAY)
R1	360 UB 45	STEEL RAFTER
R2	310 UB 40	STEEL RAFTER
R3	250 PFC	STEEL RAFTER
S1	100 x 100 x 6 SHS	STEEL STRUT
SC1	89 x 89 x 6 SHS (2-off)	STEEL COLUMN
SC2	89 x 89 x 6 SHS	STEEL COLUMN
WBR1	M20 DIA. ROD	WALL BRACING

P1			
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PROJECT:

MACKSVILLE HOSPITAL REDEVELOPMENT

MACKSVILLE NSW 2447

DRAWING TITLE:

UPPER ROOF FRAMING PLAN

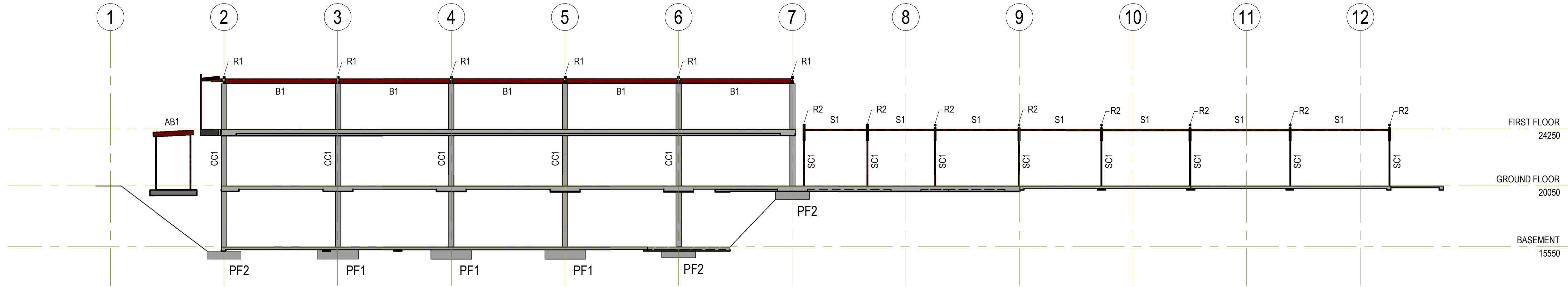
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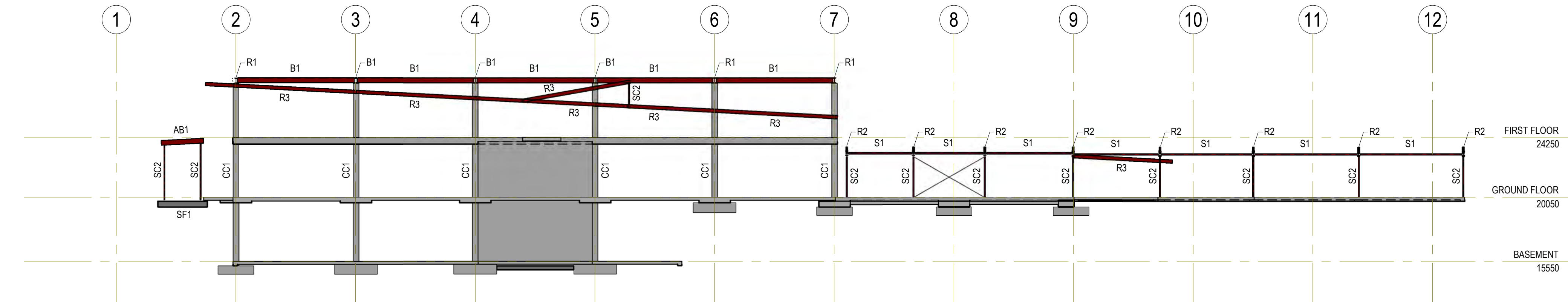
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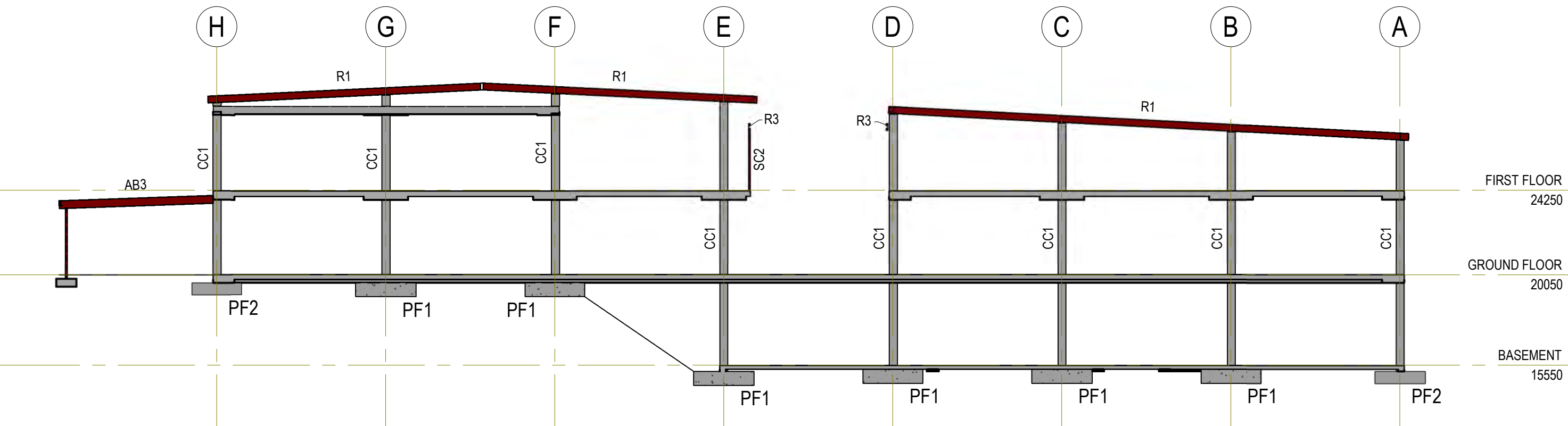
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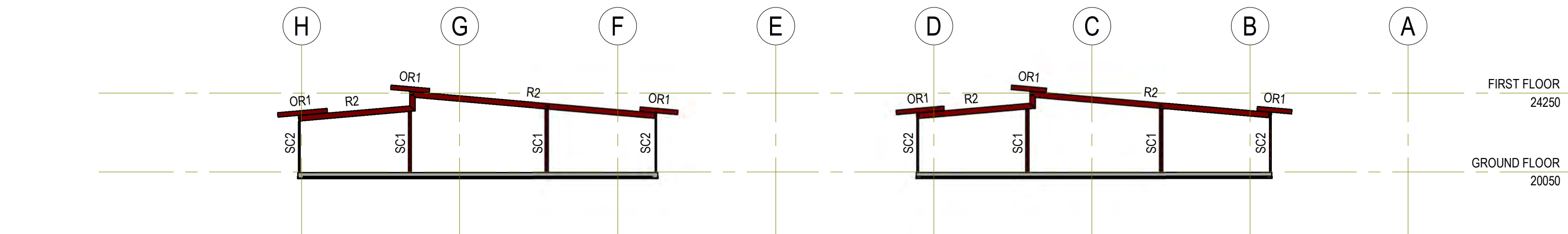
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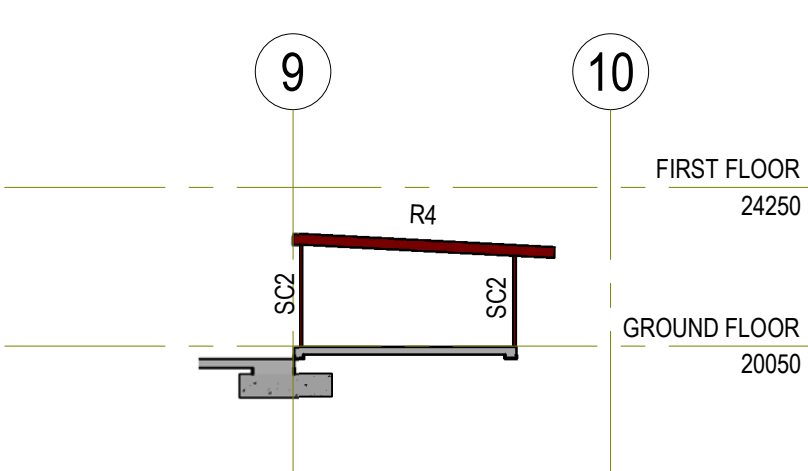
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SECTION A3
SCALE 1:200 MHD-ST-DG-0100



SECTION A4
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SECTION A5
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PROJECT:
MACKSVILLE HOSPITAL REDEVELOPMENT
MACKSVILLE NSW 2447

DRAWING TITLE:
GENERAL STRUCTURAL SECTIONS - SHEET 1

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SCHEMATIC DESIGN

APPENDIX B. GEOTECHNICAL REPORT

Health Infrastructure

Detailed Geotechnical Assessment

Proposed Macksville Hospital

Report No. RGS31237.1-AH (Rev 1)

2 May 2018

REGIONAL
GEOTECHNICAL SOLUTIONS





Manning-Great Lakes

Port Macquarie

Coffs Harbour

RGS31237.1 – AH (Rev 1)

2 May 2018

Health Infrastructure
C/O – PricewaterhouseCoopers Australia
One International Towers
Watermans Quay Barangaroo SYDNEY NSW 2000

Attention: Mr Alexander Wilson

Dear Alex

**RE: Detailed Geotechnical Assessment
Proposed Macksville Hospital**

Regional Geotechnical Solutions are pleased to provide this report providing a Geotechnical Assessment for the proposed Macksville Hospital Development at North Macksville.

If you require any further information regarding the report, please do not hesitate to contact the undersigned.

For and on behalf of

Regional Geotechnical Solutions Pty Ltd

Matt Rowbotham

Associate Engineering Geologist



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- Appendix A Engineering Logs (Previous Investigations)
- Appendix B Engineering Logs
- Appendix C Laboratory Test Results
- Appendix D Pavement Design Sheet
- Appendix D Acid Sulfate Soil Management Plan



1 INTRODUCTION

Regional Geotechnical Solutions (RGS) has conducted a geotechnical assessment of the proposed site of the new Macksville Hospital to be constructed off Letitia Close in North Macksville.

Based on the plans provided, the new hospital will involve the construction of new building structures and car parking facilities in the northern part of the site (which comprises a low rise hill). For the design to be achieved cuts up to approximately 5m to 6m and filling up to 3m are proposed for the building and car parking areas respectively. To access the new hospital a road approximately 800m in length is to be constructed south of the hillslope from Letitia Close across the alluvial floodplain. It is proposed to undertake cut and fill earthworks using the materials available on site to form the building pads and construct the car park and access road.

The aims of the study, which was commissioned by Pricewaterhouse Coopers on behalf of Health Infrastructure, were to address the following:

- General site conditions and geology including an assessment of the depth of existing filling and manner of fill placement including compaction;
- Preliminary assessment of site classification to AS2870 – 2011 for foundation design of buildings;
- Site earthworks requirements for the hillslope area including:
 - o Site preparation;
 - o Assessment of unsuitable materials;
 - o Stripping and foundation preparation;
 - o Fill material requirements, including suitability of site won materials for reuse;
 - o Fill placement and compaction control; and
 - o Site drainage requirements.
- Site earthworks requirements for the access road including:
 - o Site preparation;
 - o Assessment of foundation treatments, (i.e. bridging layers and removal and replacement of unsuitable materials);
 - o Assessment of potential settlements beneath embankments associated with soft soils;
 - o Fill placement and compaction control; and
 - o Site drainage requirements.
- Recommendations on excavation and fill retention including retaining wall and permanent and temporary batter slopes;
- Assessment of excavatability for areas of cut in the hillslope area;
- Suitable footing types and founding materials, including foundation design parameters for buildings and culverts;
- Assessment of soil aggressivity;
- Assessment for the Presence of Acid Sulfate Soils (ASS); and



- Pavement design parameters (CBR values) and flexible pavement thickness design for the access road and car parking areas.

RGS conducted the work in general accordance with proposal nos. RGS31237.1-AF and RGS31237.1-AG. This report presents the results of the site investigation.

2 EXISTING DATA AND INFORMATION

In producing this report the following available geotechnical data was reviewed:

- Coffey Geotechnics Letter GEOTLCOV24043AL-AP dated 29 January 2015 - Investigation logs undertaken for the precast yard and batch plant areas. Six CPT logs CPY-CPT01 to CPY-CPT06 and four test pit logs WC2NH-TP402 to WCNH-TP04 and WC2NH-TP09 and lab test results.
- Regional Geotechnical Solutions Report Ref RGS31237.-AE dated 27 November 2017. The investigation comprised eight test pits (TP1 to TP8) and three shrink swell tests over the hillslope area of the proposed hospital and car park area. Two boreholes were also drilled in the low lying floodplain area through the laydown working platform to assess the depth of soft soils.

3 SITE DESCRIPTION

The site is located on the eastern side of the recently completed Pacific Highway and north of Letitia Close, North Macksville.

Regionally the site is situated within gently undulating topography. Locally the site can be separated into two zones being:

- **The Hospital and Car Park Area** - located on the hillslope in the northern part of the site; and
- **The Access Road Area** - located in the area of the low lying alluvial floodplain (southern area of the site) between the hillslope and Letitia Close.

The hospital and car park area is located over a small low rise hill, the ground surface is generally gently to moderately sloping, with surface slopes falling towards the north, east and south away from the crest of the hill. A large proportion of the hill area has been modified by cut and fill earthworks associated with the former use of the site as a storage compound and precast yard for the highway works. Existing development on the site comprises gravel and earthfill laydown areas along the crest of the hill along the southern portion of the site, a earthfill borrow and stockpile area located on the north northern area of the site and an existing farm house, sheds and stockyards located along the eastern portion of the site. Vegetation has been stripped over most of the site apart from the grassed and treed areas around the old farmers residence. A water bore is located near the centre of the site on the northern side of the hill. Photos of the area are presented below.



Photo 1: Looking Towards North West From Hillslope Over Proposed Car Park Area



Photo 2: Looking Towards South East From Hillslope Across the Former Precast and Batch Plant Area



The ground surface around the access road is generally flat. Existing developments to the northern area of the access road comprise the construction of an all weather laydown area which was used for the precast concrete yard, the batch plant and earthfill stockpile area. A significant proportion of the laydown area was constructed over the alluvial floodplain comprising soft to firm clay soils. The foundation for the laydown area was constructed using rockfill as the ground improvement technique. Some sedimentation ponds also exist around the laydown area which were used to manage surface runoff.

In the southern area of the access road alignment, the majority of the alignment is greenfield with vegetation on the site consisting mainly of grasses. During periods of heavy rainfall, water stands in this area. Some minor earthworks have occurred in this area associated with the highway. At the time of the investigation a permanent sedimentation pond had been constructed adjacent to and on the eastern side of the proposed access road alignment.

4 PROPOSED DEVELOPMENT

The new hospital complex will involve the construction of new building structures and car parking facilities in the northern part of the site (which comprises a low rise hill). For the design to be achieved cuts up to approximately 5m to 6m and filling up to 3m are proposed for the building and car parking areas respectively. Materials from the hillside cuttings are proposed to be used for filling of the car park and building areas.

To access the new hospital, a road approximately 800m in length is to be constructed south of the hillslope from Letitia Close across the alluvial floodplain. The alluvial floodplain area is underlain by soft to firm alluvial clays and a shallow groundwater table. For construction of the access, a bridging layer will be required for construction purposes. For construction of the bridging layer, it is proposed to reuse the rockfill material which exists beneath the precast yard and batch plant areas.

5 SCOPE OF WORK

5.1 Fieldwork

Fieldwork in this scope of work comprised:

- A walk over assessment of the site which involved mapping surface features, surface slope angles, drainage lines, wet and low lying ground conditions and other site features considered of relevance;
- Drilling of nine boreholes (BH4 to BH12), four of the boreholes were drilled to depths of 5.88m in the area of the hillslope and five boreholes drilled to depths of up to 13.45m in the area of the floodplain. Boreholes were initially progressed through soil strength materials by auger/rotary drilling methods. Standard penetration tests were conducted at about 1.5m intervals; and
- Excavation of sixteen test pits (TP1 to TP16) which were excavated to depths of up to 3.3m.



Fieldwork was conducted by a Geotechnical Engineer from RGS who, logged the materials observed, took samples and recorded results of in-situ testing. Figures 4a to 4c show the investigation locations. Engineering Logs are presented in Appendix A, with explanation sheets defining the terms and symbols used in their preparation.

5.2 Laboratory Testing

Laboratory testing as follows was conducted on samples recovered during fieldwork:

- 3 shrink swell tests to assess clay reactivity for footing design;
- 4 Atterberg limits and linear shrinkage tests to confirm the soil plasticity classification;
- 6 standard compaction and soaked CBR tests on samples of materials expected to be encountered at subgrade level of the proposed pavements;
- 4 aggressivity tests for the assessment of corrosivity protection to buried structural elements.
- 18 ASS field screening tests and
- 6 Chromium Reducible Sulfur (CRS) tests to assess for the presence of Potential Acid Sulfate Soils (PASS) or Actual Acid Sulfate Soils (AASS).

Laboratory test result sheets are presented in Appendix B. Results of the lab testing for this scope of works and lab testing provided by previous investigations are summarised in the tables below.

Table 1: Results from Shrink Swell Testing

Location	Investigation Phase	Material Description	Sample Depth (m)	Field Moisture Content (%)	Shrink / Swell (%)
TP1	RGS31237.1-AE	Clay	1.2-1.5	24.9	2.1
TP5	RGS31237.1-AE	Clay	0.4-0.85	26.9	3.1
TP10	RGS31237.1-AE	Clay	0.3-0.75	29.4	2.8
TP13	RGS31237.1-AH	Clay	0.3 to 0.5	26.9	3.5
TP13	RGS31237.1-AH	EW Phyllite	1.0 to 1.2	15.6	1.3
TP14	RGS31237.1-AH	EW Phyllite	2.0 to 2.2	27.0	1.9



Table 2: Results from Atterberg Limits Testing

Location	Investigation Phase	Material Description	Sample Depth (m)	Liquid Limit (%)	Plastic Limit (%)	Plasticity Index (%)
TP402	GEOTLCOV24043AL-AP	Alluvial Silty Clay	1.4 to 1.6	46	22	24
TP403	GEOTLCOV24043AL-AP	Alluvial Silty Clay	1.4-1.6	44	24	20
TP404	GEOTLCOV24043AL-AP	Alluvial Silty Clay	1.4-1.6	27	21	6
TP409	GEOTLCOV24043AL-AP	Alluvial Silty Clay	1.4-1.6	46	22	24
TP14	RGS31237.1-AH	EW Phyllite	2.0 to 2.2	43	28	15
BH8	RGS31237.1-AH	Alluvial Clayey Silt	5.0 to 5.45	32	23	9
BH10	RGS31237.1-AH	Alluvial Clayey Silt	1.5 to 1.6	54	31	23
BH10	RGS31237.1-AH	Alluvial Silty Clay	2.4 to 2.5	44	25	19

Table 3: Results of Aggressivity Testing

Location	Investigation Phase	Material Description	Sample Depth (m)	Soluble Sulphate (mg/Kg)	Chloride (mg/Kg)	Ph	Conductivity (Ohm.cm)
BH4	RGS31237.1-AH	Extremely Weathered Phyllite	2.5 to 2.95	26	38	5.1	6900
BH8	RGS31237.1-AH	Alluvial Clayey Silt	6.5 to 6.9	377	70	3.8	920
BH10	RGS31237.1-AH	Alluvial Clayey Silt	1.0 to 1.45	88	175	4.9	1700



Location	Investigation Phase	Material Description	Sample Depth (m)	Soluble Sulphate (mg/Kg)	Chloride (mg/Kg)	Ph	Conductivity (Ohm.cm)
BH12	RGS31237.1-AH	Alluvial Clayey Silt	1.3-1.45	116	215	5.2	2100

Table 4: Summary of Compaction and CBR Test Results

Location	Investigation Phase	Material Description	Sample Depth (m)	Field Moisture Content (%)	Optimum Moisture Content (%)	CBR (%)
TP4	RGS31237.1-AH	Fill - Clayey Gravel	0 to 0.4	11.6	12.5	2.5
TP6	RGS31237.1-AH	Fill - Clayey Gravel	0 to 0.4	9.9	10.9	4.5
TP8	RGS31237.1-AH	Fill - Silty Clay	0.1 to 0.4	15.4	13.8	5.5
TP13	RGS31237.1-AH	Residual Silty Clay	0.3 to 0.5	22.9	19.8	3.5
TP13	RGS31237.1-AH	Extremely Weathered Phyllite	1.0 to 1.2	15.6	14.1	3.5
TP14	RGS31237.1-AH	Extremely Weathered Phyllite	2.0 to 2.2	17.5	16.0	6.5

6 SUB-SURFACE CONDITIONS

6.1 Stratigraphy

The Dorrigo Coffs Harbour 1:250,000 geological map sheet shows that the site is underlain by undifferentiated schist and phyllite.

Hillslope Areas (Northern Area of Site)

The stratigraphy interpreted from the boreholes and test pits undertaken in the hillslope area is summarised as follows:

Filled Areas



- **Fill (Encountered in Localised Test Pits):** Mainly soil materials comprising gravelly silty clay, medium plasticity, between 0.4m and 1.4m thick; overlying
- **Residual Soil:** Silty clay, medium plasticity, orange brown, very stiff; grading into
- **Extremely Weathered Phyllite:** Clayey silty gravel, friable, to beyond the depth of investigation (5.88m).

Non Filled Areas (Greenfield Areas)

- **Topsoil:** Silt, low plasticity, dark brown to depths of 0.2m, overlying;
- **Residual Soil:** Silty clay, medium plasticity, orange/brown, very stiff; grading into
- **Extremely Weathered Phyllite:** Clayey silty gravel, friable, to beyond the depth of investigation (5.88m).

No groundwater was observed in any of the test pits or boreholes. Ground water levels may fluctuate after rain or as a consequence of other climatic effects.

Alluvial Floodplain Areas (Southern Area of Site)

The stratigraphy interpreted from the boreholes and test pits undertaken in the hillslope area is summarised as follows:

Filled Laydown and Batch Plant Areas

- **Fill:** comprising clayey gravel, medium grained, between 0.3m and 1m depth; overlying
- **Fill (Rockfill):** gravel and cobbles, dense, to 1.6m depth; overlying
- **Alluvial Soil (Upper Crust):** generally comprising stiff silty clay to 3m depth, underlain by;
- **Alluvial Soil (Soft to Firm):** comprising silty clay to 6m depth, underlain by;
- **Alluvial Soil (Stiff):** comprising stiff silty clay to 13m depth, underlain by;
- **Extremely Weathered Argillite:** comprising silty clay, hard and friable, to beyond the depth of investigation.

Non Filled Areas

- **Alluvial Soil (Upper Crust):** generally comprising stiff silty clay to 1m depth, underlain by;
- **Alluvial Soil (Soft to Firm):** comprising silty clay to 4m depth, underlain by;
- **Alluvial Soil (Stiff):** comprising stiff silty clay to 9m depth, underlain by;
- **Extremely Weathered Argillite:** comprising silty clay, hard and friable, to beyond the depth of investigation.

Note the depths of soft clay soils decrease in the direction south away from the laydown and batch plant areas.

The groundwater levels were measured at natural ground surface level on completion of test pitting and drilling. Ground water levels are expected to fluctuate after rain, during flooding or as a consequence of other climatic effects.



7 CONSIDERATIONS FOR DESIGN & CONSTRUCTION (NORTHERN AREA OF SITE – HOSPITAL BUILDINGS AND CAR PARK AREA)

7.1 Preliminary Site Classification

The preliminary site classification presented herein is provided on the basis that the performance expectations of AS2870 - 2011 are acceptable.

Based on the presence of fill materials over the area of the hospital buildings to depths in excess of 0.4m, the site is classified as Class 'P' in accordance with Australian Standard AS2870 - 2011. Should the fill materials be removed and replaced with level 1 fill. Then the footings for the structures could be founded in the fill or the natural clay soils, with a Class 'M' site conditions with a shrink swell related characteristic free surface movement (γ_s) in the order of 20 to 40mm estimated for the site in its existing condition. This assessment is based on the soil and weathered rock materials profile encountered and should be reviewed following earthworks and laboratory shrink swell testing.

This classification is based on site conditions at the time of the assessment. Changes to the existing profile, in particular filling can have significant impacts on shrink swell related ground surface movements and subsequently the site classification. Any fill should therefore comprise non-reactive materials such as sands and gravel. The use of clay soils will result in higher shrink swell related surface movements.

Shrink swell related surface movements can be affected by alterations to the soil profile by cutting and filling, and by the suction related effects of trees close to the building area. The effects of any such cutting, filling, tree planting, or tree removal should be taken into account when selecting design values for differential movement across the building.

The classification presented above assumes that:

- All footings are founded in controlled fill (if applicable or in the residual clay soils or rock below all uncontrolled fill, topsoil material and root zones and fill under slab panels meets the requirements of AS2870-2011, in particular the root zone must be removed prior to placement of fill materials beneath slabs;
- Footings are to be founded outside of or below all zones of influence resulting from existing or future services trenches;

7.2 Founding Conditions & Parameters

Based on the cut and fill works proposed at the site of the hospital complex the foundation for the hospital building is expected to comprise residual clay soils and extremely weathered phyllite, we consider that there are several suitable options for support of the proposed structures depending on the magnitude of loads and the required founding levels. These options include:

- Shallow footings; and
- End-bearing piles founded within residual clays or the weathered phyllite bedrock.

Discussion of the options and design parameters for the relevant materials is provided in the following sections.



7.3 Shallow Footings

High level footings may comprise pad or strip footings supporting column loads or a raft slab. For pad or strip footings an allowable bearing pressure of 100kPa may be adopted for the residual clay soils and 300kPa adopted for the extremely weathered phyllite. The assessment of serviceability beneath shallow footings founded in clay and extremely weathered phyllite may be undertaken assuming an elastic modulus of $E = 15\text{MPa}$ and $E = 70\text{MPa}$ respectively.

High level footings are to be founded outside or below all zones of existing or future services trenches.

7.4 Piles

End bearing piles may be adopted to support the structures forming the development. Open bored piles are considered a suitable pile type.

Design parameters for end bearing piles founded at least 4 pile diameters below the excavation level are shown in Table 5

Table 5: Geotechnical Strength Parameters for Pile Design

Material Description	Elastic Modulus Vertical Response (MPa)	Elastic Modulus Horizontal Response (MPa)	Ultimate Skin Friction (MPa)	Ultimate End Bearing (MPa)
Level 1 Engineered Fill or Residual Soil: Silty Clay, medium plasticity, orange brown, very stiff.	20	15	50	1000
Extremely Weathered Phyllite: pale grey with orange / brown iron oxide staining, estimated low to medium strength.	70	2200	70	3000

For pile design in accordance with AS2159-2009, '*Piling-Design and installation*', the ultimate geotechnical strength ($R_{d,ug}$) can be calculated using the shaft capacity and ultimate end bearing capacity values provided in Table 5. Calculation of the design geotechnical strength ($R_{d,g}$) requires an assessment of the geotechnical strength reduction factor (Φ_g), which is based on a series of project specific variables. When assessing the geotechnical reduction factor (Φ_g) an assignment of an Average Risk Rating (ARR) is required which takes into account the redundancy of the pile system and the quantity and type of pile testing. In assessing the ARR and a suitable geotechnical strength reduction factor for this project, the following assumptions have been made:

- Design of piles and pile groups will be undertaken in accordance with the recommendations presented in this report;
- Limited geotechnical involvement will occur during pile installation;



- No performance monitoring of the supported structure will occur during or after construction; and
- The foundations will be designed by a designer of at least moderate experience in similar geotechnical profiles and pile design;
- Well established pile design methods will be adopted.

Based on the above and in accordance with AS2159-2009, a risk rating of 1.76 is estimated. Therefore, assuming the pile configuration will have low redundancy a Geotechnical Strength Reduction Factor of $\Phi_g=0.61$ would be appropriate for the site if no static load testing is undertaken. This could be increased to 0.75 if a reasonable proportion of the piles are statically or dynamically tested.

In the event that any of the assumptions outlined above are not correct, the Geotechnical Strength Reduction Factor may change and further advice should be sought.

7.5 Aggressivity to Buried Structural Elements – Residual Soil and Weathered Phyllite

Based on the recommendations provided in the Australian Standard "AS2159-2009, *Piling Design and Installation*", the following exposure classifications should be adopted for buried structural elements founded in the residual clay soils and weathered phyllite:

- Concrete Elements Soil Conditions – Mildly Aggressive exposure classification.
- Steel Elements in Soil Conditions – Non Aggressive exposure classification.

Based on the above exposures, the below design criteria should be adopted for structures with a 50 year design life:

- Cast in-situ concrete - Minimum concrete strength of 32MPa and steel cover of 60mm;
- Precast concrete - Minimum concrete strength of 50MPa and steel cover of 20mm;

Steel elements in the above environment should be designed with a uniform corrosion allowance of <0.01mm/year.

7.6 Excavation Conditions

The cut/fill sections indicate that excavations of up to 5.7m depth are proposed across the crest of the hillslope area. At this depth, excavations will extend through the residual clay soils and into the extremely to highly weathered phyllite.

Based on experience with similar conditions, excavation could be conducted using tracked, hydraulic excavators of 20 tonne capacity or larger or with the use of scrapers or bulldozers of D6 Capacity or larger. It is possible excavations may encounter localised zones of rock that is stronger, than that intersected in the boreholes and test pits. Such zones may require heavier ripping prior to general bulk excavation.

Groundwater was not encountered above 5.88m depth at the time of the investigation.



7.7 Site and Excavation Retention

7.7.1 Retaining Wall Options

On the basis of the available subsurface information, excavation will be within the residual clay and extremely to highly weathered phyllite which will require support if cut vertically to the levels proposed.

Suitable retaining walls for the site are likely to comprise relatively simple gravity or cantilever walls. These may be designed using the parameters given below. Design should include assessment of the global stability of the wall.

7.7.2 Retaining Wall Drainage

The wall backfill should be free draining, granular material. Drainage behind the wall should comprise a geocomposite drain or geotextile wrapped gravel drain at the back of the wall that drains to a geotextile wrapped subsoil drain along the wall toe. The toe drain should discharge to the site stormwater system to provide long term drainage behind excavation walls. Flushing points should be incorporated into the design of the perimeter drain to allow periodic maintenance.

7.7.3 Retaining Wall Design Parameters

Cantilevered or gravity walls may be designed based on a triangular stress distribution using the following parameters in Table 6.

Table 6: Retaining Wall Design Parameters

Unit	Effective Cohesion (c')	Friction Angle (Degrees)	Saturated Bulk Unit Weight (kN/m ³)
Topsoil / Uncontrolled Fill	4	25	18
Residual Clay and Extremely Weathered Phyllite	7	29	20
Highly Weathered Phyllite	12	30	22

Design of the walls must take into account any surcharge from sloping ground or other loadings behind the wall. Drainage measures as described above, if properly maintained, should reduce pore pressures at the back of the wall to zero, however pore pressures may still be generated at other points behind the wall. The design should incorporate an allowance for such pressures. A typical allowance of potential water pressure build-up equivalent to one-third the wall height is considered to be reasonable with such drainage measures installed.



7.8 Temporary & Permanent Batter Slopes

Where space permits, temporary batter slopes may be constructed to simplify retaining wall construction and conventional concrete panel or similar walls adopted. Temporary batter slopes may be cut in soil strength materials and weathered phyllite down to about 4m depth at 1H:1V. Permanent batter slopes in the same materials to 6m depth should be no steeper than 2H:1V and should be protected against erosion. Adequate drainage should be provided for all batter slopes. As a minimum during rainfall, temporary slopes should have surface water on the high side should be diverted away from the slope face.

7.9 Reuse of Site Won Materials

The following comments are made regarding the suitability of the site materials for reuse in filled areas:

For site regard works, topsoil or other potentially deleterious material should be removed to spoil or stockpiled for reuse as landscaping materials only. Topsoil depths are presented on the engineering logs in Appendix B. Stripping of topsoil is expected to be required to depths of up to 0.20m.

The uncontrolled fill materials placed across the crest of the hillslope area (former site compound area) and the underlying residual clays and weathered rock are suitable for re-use as general engineered fill subject to appropriate moisture conditioning.

7.10 Compaction Control Beneath Structures

Site preparation and earthworks suitable for structure support should be undertaken as follows:

- Prior to construction of pavements and placement of any fill, the proposed areas should be stripped to remove all vegetation, topsoil, root affected or other potentially deleterious material;
- Following stripping, the exposed subgrade materials should be proof rolled in the presence of a suitably qualified and experienced geotechnical practitioner to identify any wet or excessively deflecting material. Any such areas should be over excavated and backfilled with an approved material;
- Approved fill beneath structures should be placed in layers not exceeding 300mm loose thickness and compacted to a minimum density ratio of 98% Standard Compaction in accordance with AS1289 5.1.1 or equivalent. Clay fill should be placed and maintained at $\pm 2\%$ of Optimum Moisture Content.



8 CONSIDERATIONS FOR DESIGN & CONSTRUCTION (SOUTHERN AREA OF SITE – ACCESS ROAD AND REUSE OF FILL FROM PRECAST AND BATCH PLANT AREA)

8.1 Shallow Footings Beneath Culvert Structures

Based on the concept plans provided for the development three flood culvert locations have been nominated along the access road alignment. The culvert locations are located at the following chainages:

- 290m
- 460m
- 600m

Due to the presence of soft to firm clay soils at the site, the culverts and access road alignment are expected to experience some long term settlements over the lifetime of the road associated with primary and secondary “creep” settlements. For design of the culverts and embankments, consideration needs to be given to designing the foundations for the culverts which manage the potential for differential settlements over the design life. Due to the thin nature of the soft soils in this area (less than 2.5m in thickness) the ground conditions are not expected to require the use of construction methods which result in ground improvement (such as preloading etc) or piling the culvert structures. Therefore to manage the potential for different settlements, high level footings comprising preformed box culverts founded on reinforced concrete base slabs could be used for the site. For the preliminary assessment of footings and assuming an allowable bearing pressure of 50kPa will required for the reinforced concrete slab. A 0.6m thick rockfill platform will be required over the soft to firm clay foundation

An assessment of the estimated settlements to the structures associated with the above footing loads is discussed below.

8.2 Estimated Settlements Beneath Culvert Structures and Access Road Embankment

The design parameters for the assessment of settlements beneath culverts and the access road embankment are provided in Table 7 below.



Table 7: Summary of Geotechnical Parameters

Unit	Bulk Unit Weight (kN/m ³)	Elastic Modulus (MPa)	Undrained Shear Strength (kPa)	Cc/1+e ⁰	C _{αε}	C _v (m ² /yr)
Embankment Fill	20	15	100	-	-	-
Stiff Alluvial Clay (Upper Crust)	18	10	50	-	-	-
Soft to Firm Alluvial Clay	16.5		20 to 45	0.2	0.015	6 to 20
Stiff Alluvial Clay (Lower)	18	12	75	-	-	-

Presented in Table 8 and Table 9 are summaries of the estimated settlements likely to occur to embankments and culverts over a 50 year design period.

Table 8: Summary of Estimated Embankment Settlements

Chainage	Fill / Cut Level From Existing	Thickness of Soft to Firm Clay Soil	Primary Settlement Estimated	Secondary Settlement Expected for 50 Year Design Period	Elastic Settlement Expected (Internal Embankment Settlement)	Total Settlement Expected for 50 Year Design Period
100m	2.2 Fill	1.5m	<90mm	<60mm	<10mm	<160mm
200m	2.0 Fill	2.0m	<100mm	<50mm	<10mm	<160mm
300m	1.5 Fill	2.5m	<80mm	<50mm	<10mm	<140mm
400m	0.6 Fill	2.5m	<20mm	<50mm	<5mm	<75mm
500m	5m Cut Through Fill Stockpile	Not Encountered	0mm	0mm	0mm	0mm
600m	1.5m Fill	None	0mm	50mm	<10mm	<60mm
700m	2.5m Fill	None	0mm	0mm	25mm	<25mm
800m	6m Fill	None	0mm	0mm	40mm	<40mm



Table 9: Summary of Estimated Culvert Settlements

Chainage	Design Bearing Pressure (kPa)	Thickness of Soft Soil	Primary Settlement Estimated	Secondary Settlement Expected for 50 Year Design Period	Elastic Settlement Expected (Internal Embankment Settlement)	Total Settlement Expected for 50 Year Design Period
290m	50	2.5 (20kPa)	100mm	50mm	<10mm	<180mm
460m	50	2.0m (40kPa)	60mm	50mm	<10mm	<120mm
600m	50	2.0m (40kPa)	70mm	50mm	<10mm	<130mm

It should be noted that the parameters used to assess the settlements have been adopted based on experience with soils of similar properties on nearby projects and are not based on lab testing undertaken during this scope of work. Primary settlements are expected to occur within the first 8 months of construction. It is recommended that an allowance be made to undertake settlement monitoring during construction of the fill embankments.

8.3 Batter Design Recommendations for Access Road Embankments Placed Over Soft Soils

For construction of fill batters for the access road and to maintain stability of the embankment, design batters should not exceed grades of 2H to 1V.

8.4 Aggressivity to Buried Structural Elements – Alluvial Soil Areas

Based on the recommendations provided in the Australian Standard "AS2159-2009, *Piling Design and Installation*", the following exposure classifications should be adopted for buried structural elements in the alluvial soils:

- Concrete Elements Soil Conditions –Severe exposure classification.
- Steel Elements in Soil Conditions – Moderate exposure classification.

Based on the above exposures, the below design criteria should be adopted for structures with a 50 year design life:

- Cast in-situ concrete - Minimum concrete strength of 50MPa and steel cover of 70mm;
- Precast concrete - Minimum concrete strength of 50MPa and steel cover of 40mm;

Steel elements in the above environment should be designed with a uniform corrosion allowance of 0.02 to 0.04mm/year.



8.5 Excavation Conditions

Based on the available concept design information, excavations within the alluvial clay soils are only expected to occur for the provision of buried services and to construct rockfill bridging layers for the foundations of flood culvert structures.

For these types of construction works, excavations to depths of between 0.5m and 1.5m may be expected.

Temporary excavations such as utility trenches up to about 1m deep could be cut vertically through the clay soils encountered and should be self-supporting for short periods (i.e. several hours while the service is laid and backfilled). Lengths of open excavation should be limited to no greater than 10m. Large lengths of open unsupported trenching should be supported by trenching shields/ shoring boxes.

Larger temporary excavations in the firm to soft clay soils which will remain open for extended periods should be benched at 2H:1V or flatter if they are to remain open for extended periods of time and protected against erosion or supported by trenching shields/ shoring boxes.

Groundwater was encountered at the natural surface level at the time of the investigation. Based on our experience at the site water levels experienced are well above natural groundwater level during periods of increased rainfall.

8.6 Site and Excavation Retention

8.6.1 Retaining Wall Options

Suitable retaining walls for the retention of embankment fill behind culverts are likely to comprise relatively simple gravity or cantilever walls. These may be designed using the parameters given below. Design should include assessment of the global stability of the wall.

8.6.2 Retaining Wall Drainage

The wall backfill should be free draining, granular material. Drainage behind the wall should comprise a geocomposite drain or geotextile wrapped gravel drain at the back of the wall that drains to a geotextile wrapped subsoil drain along the wall toe. The toe drain should discharge to the site stormwater system to provide long term drainage behind excavation walls. Flushing points should be incorporated into the design of the perimeter drain to allow periodic maintenance.

8.6.3 Retaining Wall Design Parameters

Cantilevered or gravity walls may be designed on the basis of a triangular stress distribution using the following parameters in Table 10.



Table 10: Retaining Wall Design Parameters

Unit	Effective Cohesion (c')	Friction Angle (Degrees)	Saturated Bulk Unit Weight (kN/m ³)
Topsoil / Uncontrolled Fill	4	25	18
Rockfill Bridging	0	43	23
Engineered Embankment Fill	7	29	20

Design of the walls must take into account any surcharge from sloping ground or other loadings behind the wall. Drainage measures as described above, if properly maintained, should reduce pore pressures at the back of the wall to zero, however pore pressures may still be generated at other points behind the wall. The design should incorporate an allowance for such pressures. A typical allowance of potential water pressure build-up equivalent to one-third the wall height is considered to be reasonable with such drainage measures installed.

8.7 Reuse of Site Won Materials from Precast and Batch Plant Borrow Area

The following comments are made regarding the suitability of the site materials for reuse in the site access road area:

The general fill materials placed across the bridging layer in the precast and batch plant areas will be suitable for re-use as general engineered fill subject to appropriate moisture conditioning. Based on the test pits undertaken in the area, the layer of general fill ranges between 0.4m and 1.8m in thickness with depths typically in the range of 0.5 to 0.8m

The rockfill bridging layer materials generally comprised a mixture of gravel and cobbles of high strength rock. Therefore from a geotechnical viewpoint the materials will be suitable for reuse as a bridging layer material for the new road alignment. It should be noted that a number of the test pits encountered high silt and clay contents which may affect the performance of the bridging layer materials. Should it be proposed to use all of the rockfill materials in construction of the road then an allowance should be made to process (screen) some of the gravel materials with high silt/clay content.

The presence of the geofabric layers above and below the bridging layer, means that some of the general fill and rockfill bridging materials will be affected by geofabric inclusions. Allowance should be made for a proportion of wastage of the borrow material where the geofabric material cannot be practically removed.

From a construction viewpoint the contractor should assess the viability of reusing the materials in construction of the access road.



9 PAVEMENT DESIGN

9.1 Design Subgrade

Based on the CBR testing results and our experience with these materials on the Pacific Highway Upgrade projects a design CBR of 3.5% should be adopted for design of flexible pavements.

9.2 Design Traffic

Based on information provided for the project we understand that an indicative design traffic figure of 8×10^5 ESA's is to be used to design of the access road. A summary of the pavement design is provided in Table 11 below.

Table 11: Pavement Design Summary for Design CBR 3%

Pavement Location	Spray Seal type	Base Layer	Subbase Layer	Total Pavement Thickness
Access Road	2 Coat Seal 14/7	140mm	320mm	460mm

9.3 General Pavement Design Parameters and Compaction Control Beneath Pavement and Car Parks

The following scope of work is required as a minimum to enable the design CBR of 3.5% to be achieved.

Site preparation and earthworks suitable for pavement and structure support should comprise:

- Prior to construction of pavements and placement of any fill, the proposed areas should be stripped to remove all vegetation, topsoil, root affected or other potentially deleterious material;
- Following stripping, the exposed subgrade materials should be proof rolled in the presence of a suitably qualified and experienced geotechnical practitioner to identify any wet or excessively deflecting material. Any such areas should be over excavated and backfilled with an approved select material;
- Approved fill beneath pavements should be placed in layers not exceeding 300mm loose thickness and compacted to a minimum density ratio of 95% Standard Compaction in accordance with AS1289 5.1.1 or equivalent. Clay subgrade fill should be placed and maintained at 60% to 90% of Optimum Moisture Content;
- The top 300mm of natural subgrade below pavements or the final 300mm of road subgrade replaced should be compacted to a minimum density ratio of 100% Standard Compaction or equivalent within the above stated moisture range.

The following construction methodology is recommended for the pavements:



- Place new pavement over prepared subgrade as per design requirements as specific in pavement thickness design sheet presented in Appendix D.
- Where final sealing cannot be undertaken within a few days of completion of the base course, a primer seal should be used to protect the pavement and maintain equilibrium moisture content;
- Traffic should be prevented from travelling on partially completed pavement sections.
- Where a two coat seal is adopted, sealing should be avoided during winter months or at times when pavement temperatures of less than 15 degrees are likely, due to the potential for microcracking of the pavement surface, which can lead to water ingress, pumping of fines, and flushing or embedment of aggregate within wheel paths within a very short time frame. If sealing during winter or cold weather is required, consideration should be given to placing a 7mm primer seal that can remain in place for several weeks, with placement of the two-coat seal then able to be undertaken at a time when the pavement can be dried to remove excess moisture from the upper part of the base course and the microcracking in the primer can be sealed over.

Pavement construction, including sealing, should extend well beyond the outer wheel path of the pavement to provide lateral restraint to the outer wheel path and to assist in preventing ingress of moisture through the road shoulder.

9.4 Bridging Layer Construction Over the Alluvial Floodplain

For construction of the access road across the alluvial floodplain the following is recommended. It should be noted that the thickness of the bridging layer required will be dependent on the prevailing weather and site conditions at the time of construction. For costing purposes, the following is recommended:

- Placement of A39 Geofabric or equivalent across the footprint area of the embankment. A minimum overlap of 600mm between rolls of geofabric should be allowed for during construction; followed by
- Placement of a rockfill bridging layer over the geofabric. The rockfill bridging layer should be placed and pushed out over the geofabric layer. The rockfill bridging layer should comprise high strength angular rock free of fines which once compacted forms a strong mechanical interlock. The rockfill layer should have a minimum compacted layer thickness of 600mm. Rockfill should be sized so that no individual particles are greater than two thirds the compacted layer thickness. Once placed the bridging layer should be proof rolled to assess for any excessive deflections. Areas of excessive deflection noted should be treated at the time of construction.
- Following acceptance of the proof roll assessment, allowance should be made to cover the bridging layer with a layer of A39 geofabric or equivalent with a minimum 300mm overlap between rolls.



9.5 Assessment of Acid Sulfate Soils

A review of the 1: 25,000 Acid Sulfate Soil Risk Map of Macksville indicates the access road is located in an area of potentially high risk of acid sulfate soils within 1m of the ground surface.

Acid Sulfate Soils (ASS) produce sulphuric acid when exposed to oxygen due to the presence of iron sulphides in the form of pyrite within the soil matrix. These soils form when iron-rich sediments are deposited in saltwater or brackish water environments. Prior to oxidation, these pyritic soils are referred to as Potential ASS. ASS that have produced acid because of oxidation are referred to as Actual ASS. They typically occur in natural, low-lying coastal depositional environments below approximately 5m AHD. In the field ASS are generally identified as saline sediments such as alluvial or estuarine soils or bottom sediments in creeks and estuaries.

It is understood that excavations for the development will typically be associated with the construction of culvert structures and service lines, therefore it has been assumed that less than 1000 tonnes of material will be disturbed during the development.

Eighteen samples were submitted to a contract laboratory for ASS screening. The results are summarised below:

- The samples revealed pH_f values between 4.3 and 5.6 in distilled water. In this test, pH less than 4 is an indicator of Actual ASS;
- The samples revealed pH_{Fox} values between 1.9 and 4.1 in hydrogen peroxide. Values less than 3 in this test can be an indicator of Potential ASS.

To provide a more comprehensive assessment, seven samples were submitted for Chromium Reducible Sulphur (CRS) analysis. A summary of the test results is presented in Table 12.



Table 12: Summary of ASS CRS Test Results

Test location	Depth (m)	Texture	Sulfur Trail (% S Oxidisable)	
			S _{cr}	Action Criteria ⁽¹⁾
BH8	6.5 to 6.9	Fine	0.12	0.1
BH9	5.5 to 5.95	Fine	0.82	0.1
BH10	1.0 to 1.45	Fine	0.15	0.1
BH11	1.0 to 1.45	Fine	0.29	0.1
BH12	0.4 to 0.5	Fine	0.08	0.1
TP15	1.0 to 1.1	Fine	0.02	0.1
TP16	0.9 to 1.0	Fine	0.15	0.1

Notes: 1. Action criteria is based on less than 1000 tonnes of soil being disturbed

Based on Chromium Reducible Sulphur (CRS) analysis, the clay soils are assessed to be potential acid sulfate soils and therefore an Acid Sulfate Soil Management Plan will be required for the site. For excavations undertaken in the alluvial soils, a liming rate of 90kg per cubic meter of disturbed soil will be required.

10 LIMITATIONS

The findings presented in the report and used as the basis for recommendations presented herein were obtained using normal, industry accepted geotechnical design practises and standards. To our knowledge, they represent a reasonable interpretation of the general condition of the site. Under no circumstances, however, can it be considered that these findings represent the actual state of the site at all points. If site conditions encountered during construction vary significantly from those discussed in this report, Regional Geotechnical Solutions Pty Ltd should be contacted for further advice.



This report alone should not be used by contractors as the basis for preparation of tender documents or project estimates. Contractors using this report as a basis for preparation of tender documents should avail themselves of all relevant background information regarding the site before deciding on selection of construction materials and equipment.

If you have any questions regarding this project, or require any additional consultations, please contact the undersigned.

For and on behalf of

Regional Geotechnical Solutions Pty Ltd

Matt Rowbotham

Associate Engineering Geologist



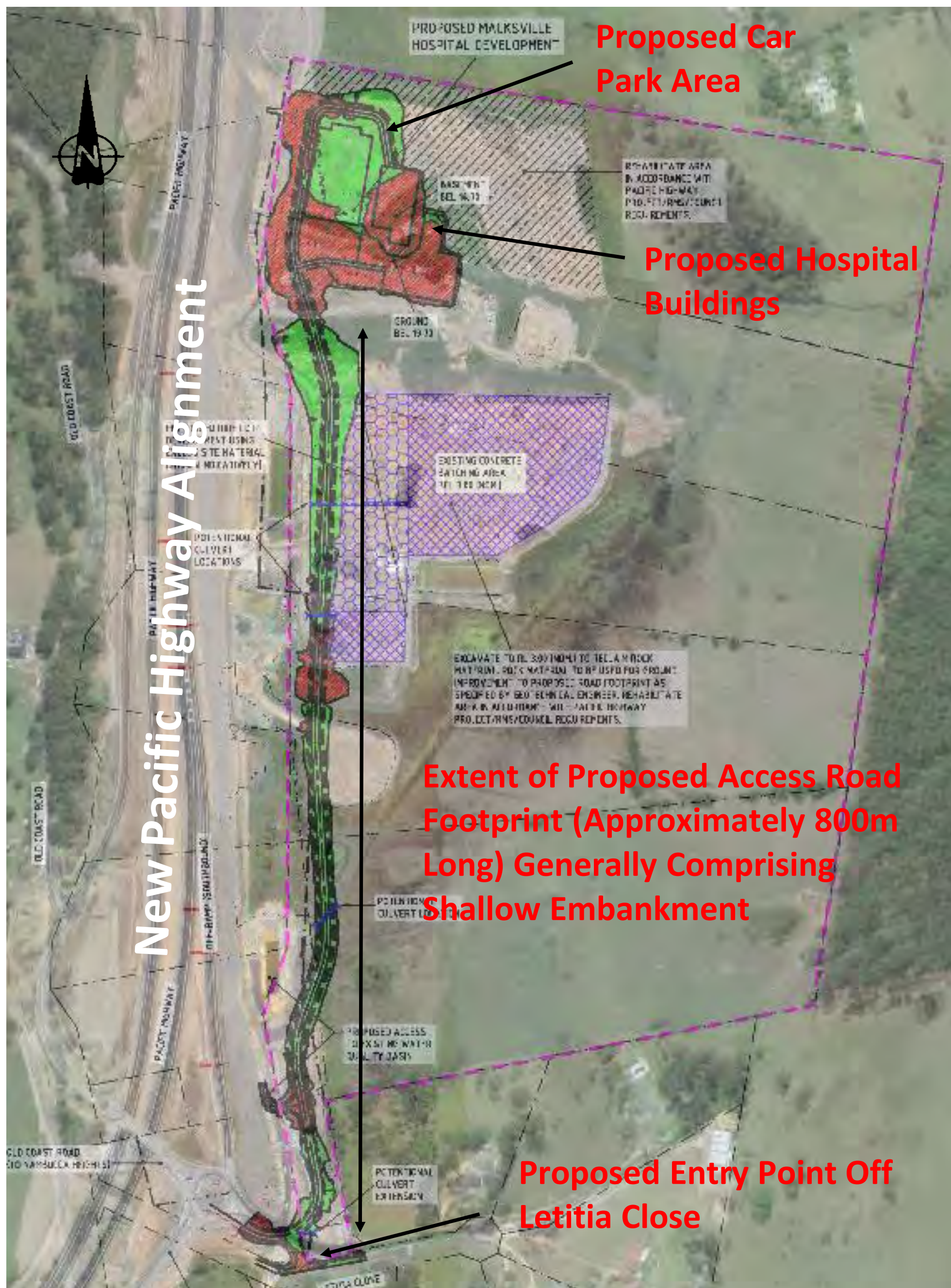
Figures



Client:	Health Infrastructure	Job No.	RGS31237.1
Project:	Proposed Macksville Hospital	Drawn By:	MR
		Date:	12-Apr-18
Title:	Site Location Plan Indicating Geology	Drawing No.	Figure 1



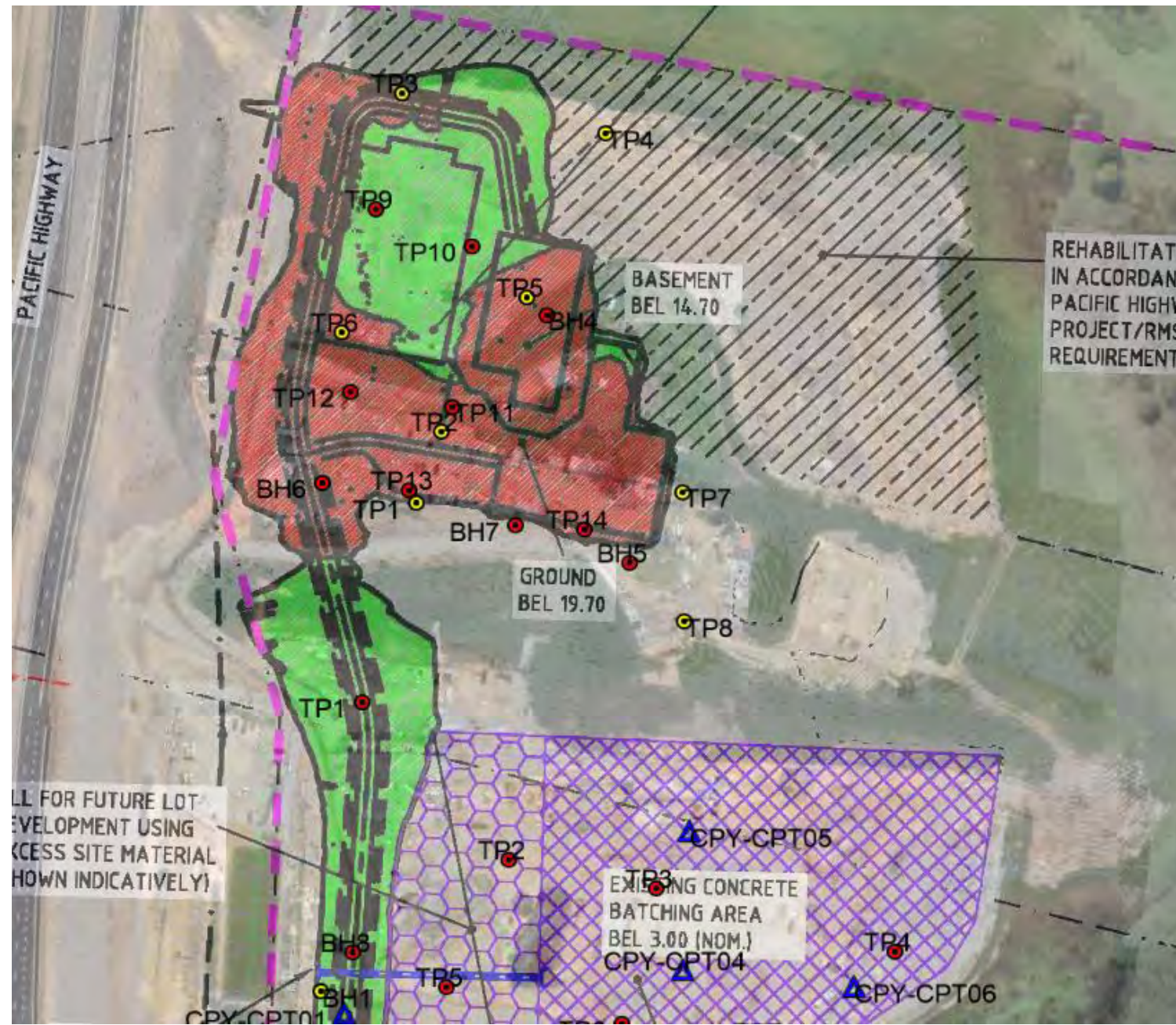
Client:	Health Infrastructure	Job No.	RGS31237.1
Project:	Proposed Macksville Hospital	Drawn By:	MR
		Date:	12-Apr-18
Title:	Site Plan Indicating Areas Affected by Filling	Drawing No.	Figure 2



Extent of Proposed Access Road Footprint (Approximately 800m Long) Generally Comprising Shallow Embankment

Proposed Entry Point Off Letitia Close

	Client:	Health Infrastructure	Job No.	RGS31237.1
	Project:	Proposed Macksville Hospital	Drawn By:	MR
			Date:	12-Apr-18
	Title:	Site Plan With Hospital Plan Layout	Drawing No.	Figure 3



Legend	
	Investigation Locations RGS31237.1-AE Report
	Investigation Locations GEOTLCOV24043AL-AP
	Investigation Locations RGS31237.1-AH

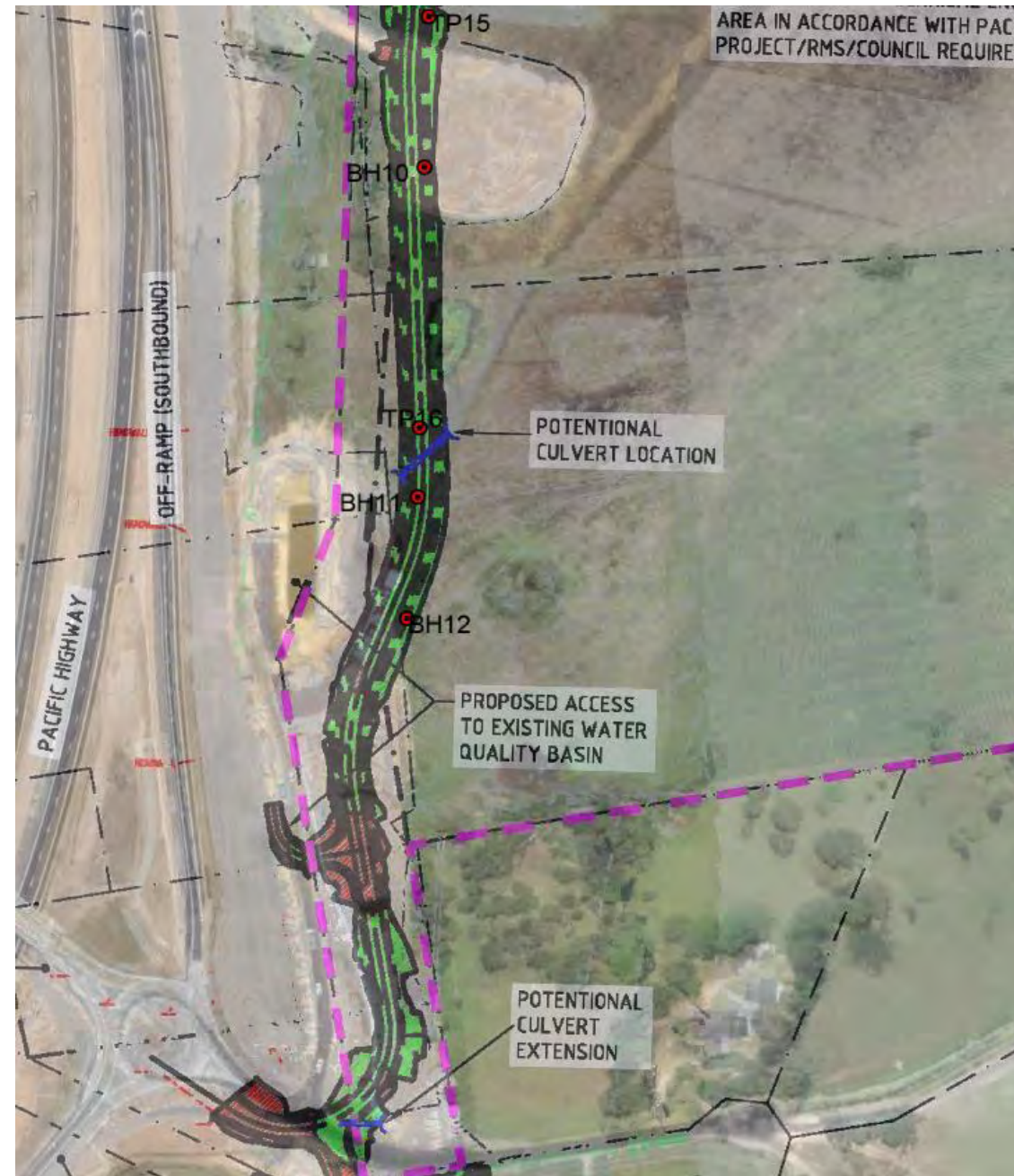


Client:	Health Infrastructure	Job No.	RGS31237.1
Project:	Proposed Macksville Hospital	Drawn By:	MR
		Date:	12-Apr-18
Title:	Test Pit and Borehole Location Plan	Drawing No.	Figure 3a



Legend	
	Investigation Locations RGS31237.1-AE Report
	Investigation Locations GEOTLCOV24043AL-AP
	Investigation Locations RGS31237.1-AH

	Client:	Health Infrastructure	Job No.	RGS31237.1
	Project:	Proposed Macksville Hospital	Drawn By:	MR
			Date:	12-Apr-18
	Title:	Test Pit and Borehole Location Plan	Drawing No.	Figure 4b



Legend	
	Investigation Locations RGS31237.1-AE Report
	Investigation Locations GEOTLCOV24043AL-AP
	Investigation Locations RGS31237.1-AH

	Client:	Health Infrastructure	Job No.	RGS31237.1
	Project:	Proposed Macksville Hospital	Drawn By:	MR
	Title:	Test Pit and Borehole Location Plan	Date:	12-Apr-18
			Drawing No.	Figure 4c



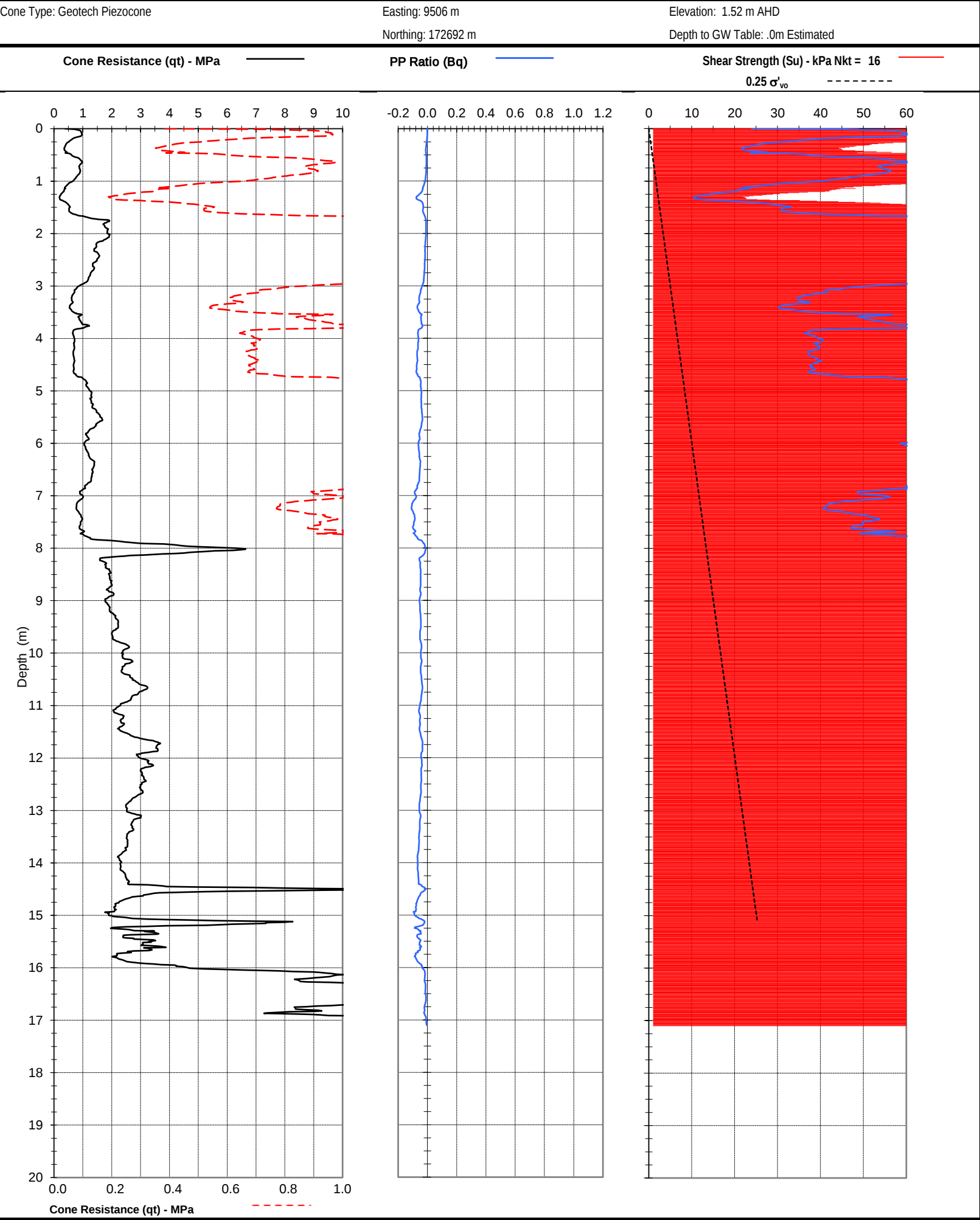
Appendix A

Investigation Logs (Previous Investigations)

Coffey Geotechnics Pty Ltd
Piezocone Penetrometer Test

Client:
Principal:
Project: *Macksville Hospital*
Location:

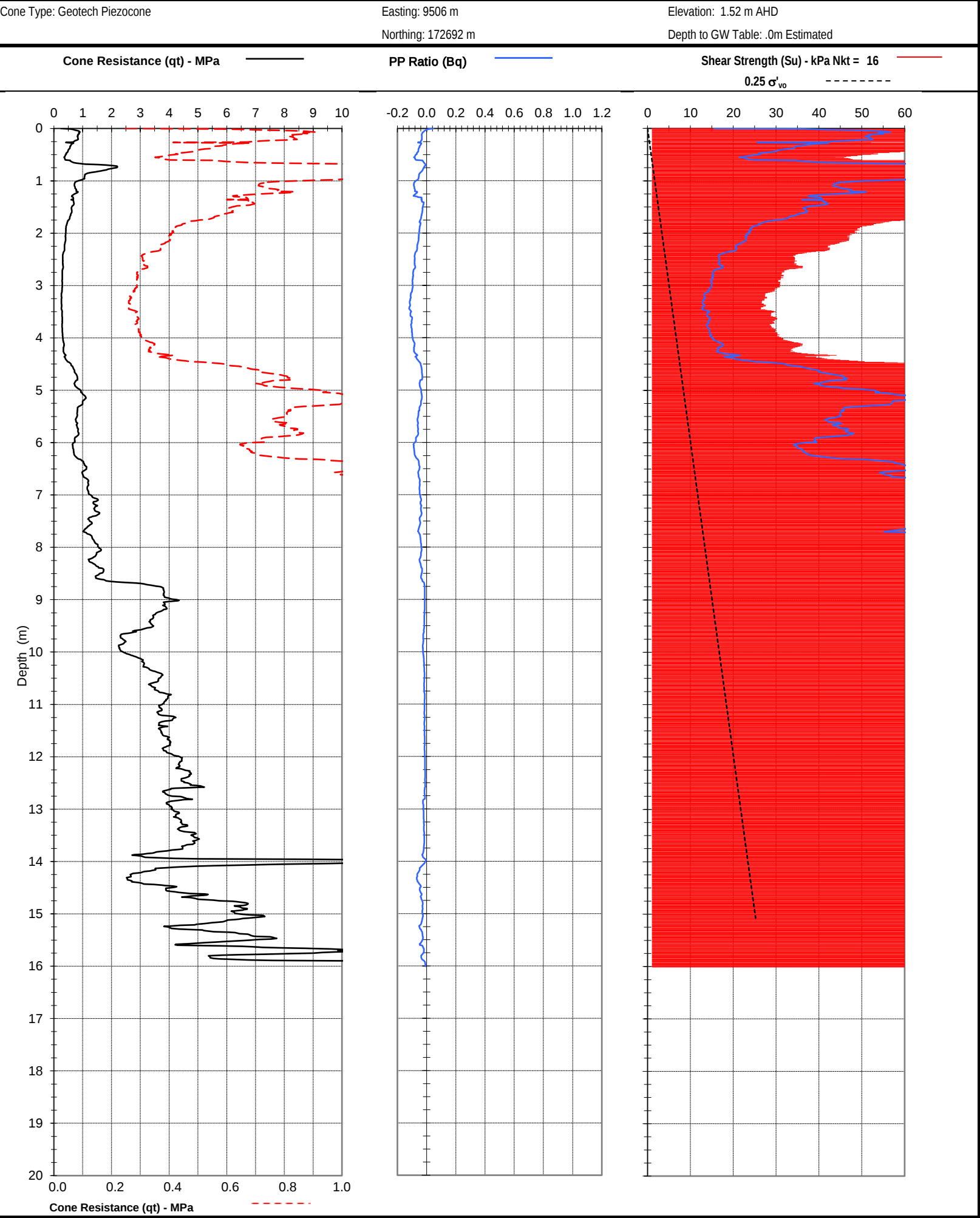
Test No.: **PCY-CPT01**
Sheet: 1 of 1
Project No. *RGS31237.1*
Date tested : *10-Feb-15*
Tested by: *IGS*



Coffey Geotechnics Pty Ltd
Piezocone Penetrometer Test

Client:
Principal:
Project: **Macksville Hospital**
Location:

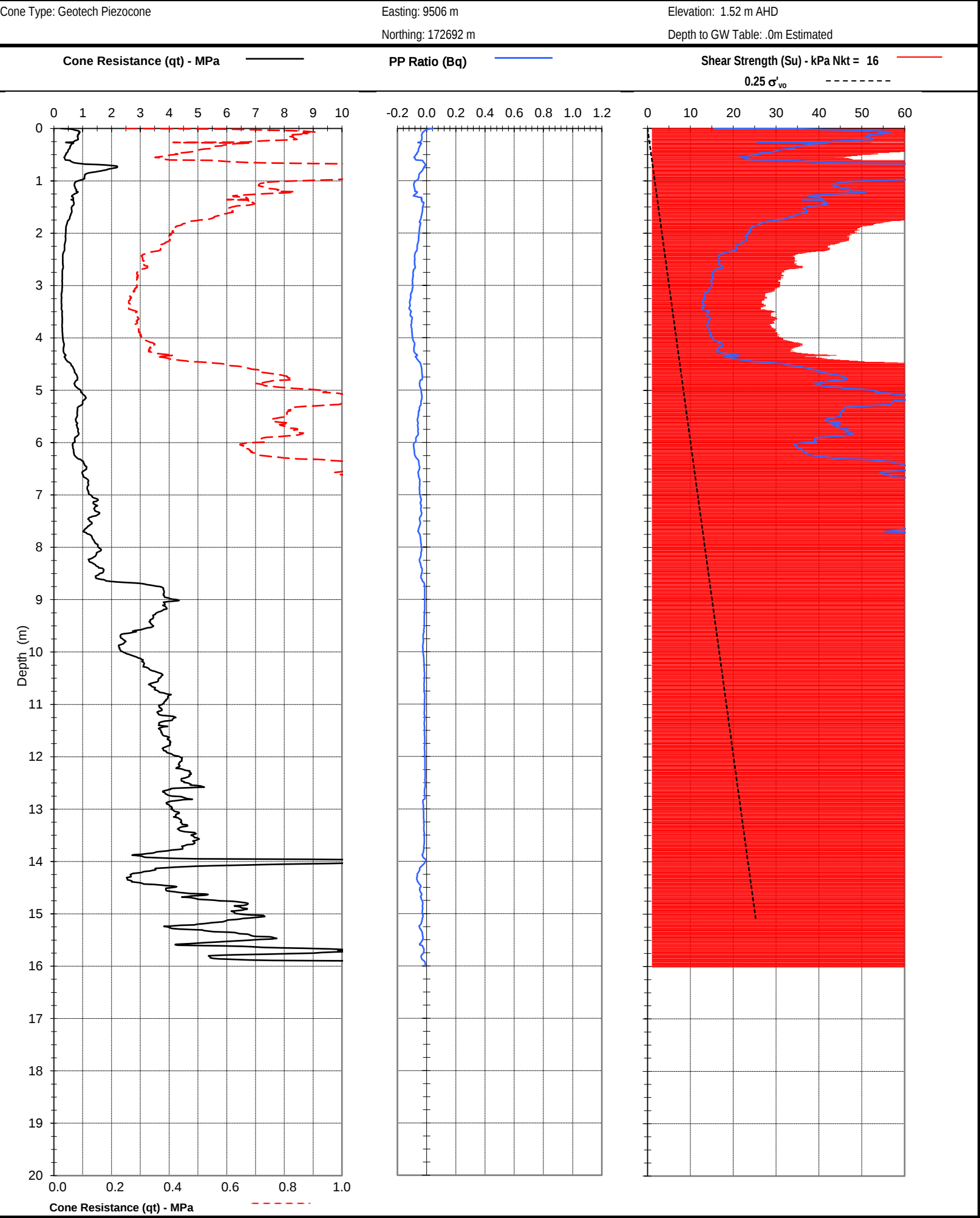
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Sheet: 1 of 1
Project No. **RGS31237.1**
Date tested : **10-Feb-15**
Tested by: **IGS**



Coffey Geotechnics Pty Ltd
Piezocone Penetrometer Test

Client:
Principal:
Project: **Macksville Hospital**
Location:

Test No.: **PCY-CPT03**
Sheet: 1 of 1
Project No. **RGS31237.1**
Date tested : **10-Feb-15**
Tested by: **IGS**





ENGINEERING LOG - BOREHOLE

CLIENT: NSW Health
PROJECT NAME: Proposed New Hospital
SITE LOCATION: Precast Yard
TEST LOCATION: As per GPS

BOREHOLE NO: BH1
PAGE: 1 of 2
JOB NO: RGS31237.1
LOGGED BY: DR
DATE: 20/9/17

DRILL TYPE: P160 **EASTING:** 494536 m **SURFACE RL:**
BOREHOLE DIAMETER: 125 mm **INCLINATION:** 90° **NORTHING:** 6604089 m **DATUM:** WG584

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
AD						GW	FILL: Sandy GRAVEL, dark grey, brown, 40mm or similar	D				FILL
RR		1.00m SPT 3,4,30/50 N=R 1.35m		1.0		GP	FILL: GRAVEL, fine to coarse grained, brown			HP	350	FILL - Building layer Rockfill
		2.50m SPT 2,9,3 N=12 2.95m		2.0		OH	Clayey SILT: Low plasticity, dark brown, trace of fine Sand	M > w _p	F	HP	120	ALLUVIUM
		4.00m SPT 4,4,7 N=11 4.45m		3.0		CH	Silty CLAY: Low plasticity, pale grey	M ~ w _p	St / VSt	HP	350	
		5.50m SPT 2,3,3 N=6 5.95m		4.0					VSt	HP	350	
		7.00m SPT 1,0,2 N=2 7.45m		5.0		ML	Clayey SILT: Low to medium plasticity, pale grey	W	S			SPT falling with rod weight and hammer. Minium return
		8.50m SPT 6,8,11 N=19 8.95m		6.0								
				7.0						HP	35	
				8.0						HP	30	
				8.0		CL	Silty CLAY: Low to medium plasticity, pale grey and brown mottle		St			RESIDUAL SOIL
				9.0								HP = 250-300 kPa
				10.00m								

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25	D	Dry
Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50	M	Moist
Water Inflow		E Environmental sample		F	Firm	50 - 100	W	Wet
Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200	W _p	Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400	W _L	Liquid Limit
Gradational or transitional strata		Field Tests		H	Hard	>400		
Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable			
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density	V	Very Loose	Density Index <15%	
		HP Hand Penetrometer test (UCS kPa)			L	Loose	Density Index 15 - 35%	
					MD	Medium Dense	Density Index 35 - 65%	
					D	Dense	Density Index 65 - 85%	
					VD	Very Dense	Density Index 85 - 100%	



ENGINEERING LOG - BOREHOLE

CLIENT: NSW Health
PROJECT NAME: Proposed New Hospital
SITE LOCATION: Precast Yard
TEST LOCATION: As per GPS

BOREHOLE NO: **BH1**
PAGE: 2 of 2
JOB NO: RGS31237.1
LOGGED BY: DR
DATE: 20/9/17

DRILL TYPE: P160 EASTING: 494536 m SURFACE RL:
BOREHOLE DIAMETER: 125 mm INCLINATION: 90° NORTHING: 6604089 m DATUM: WG584

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
RR		SPT 8,10,11 N=21 10.45m		11.0		CL	Silty CLAY: Low to medium plasticity, pale grey and brown mottle (<i>continued</i>)	W	St			RESIDUAL SOIL HP = 200-280 kPa
		11.50m		12.0			Trace of relic rock structure		St / VSt			HP = 300-350 kPa
		SPT 6,11,14 N=25 11.95m		13.0			Grey					
		13.00m		14.0					VSt			Drilling reported increase in resistance
		SPT 2,3,4 N=7 13.45m		15.0			Trace of relic rock structure			HP	300	HP = 450-550 kPa
		14.50m		16.0					VSt / H			HP = 300-500 kPa
		SPT 8,10,12 N=22 14.95m		17.0			Trace quartz Gravel (fine) and relic rock structure					
		16.00m		17.50m								
		SPT 11,20,26 N=46 17.95m		18.0			META SILTSTONE: Green, grey, foliated, some parts weathered to Clay		Fb			EXTREMELY WEATHERED PHYLLITE Increase in resistance
		19.00m		19.26m								
		SPT 20,30/100 N=R 19.25m					Hole Terminated at 19.25 m			HP	300	

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water				VS	Very Soft	<25	D	Dry
▼	Water Level	U ₅₀	50mm Diameter tube sample	S	Soft	25 - 50	M	Moist
	(Date and time shown)	CBR	Bulk sample for CBR testing	F	Firm	50 - 100	W	Wet
►	Water Inflow	E	Environmental sample	St	Stiff	100 - 200	W _p	Plastic Limit
◄	Water Outflow	ASS	Acid Sulfate Soil Sample	VSt	Very Stiff	200 - 400	W _L	Liquid Limit
		B	Bulk Sample	H	Hard	>400		
				Fb	Friable			
Strata Changes		Field Tests		Density		V	Very Loose	Density Index <15%
— — —	Gradational or transitional strata	PID	Photoionisation detector reading (ppm)	L	Loose			Density Index 15 - 35%
————	Definitive or distinct strata change	DCP(x-y)	Dynamic penetrometer test (test depth interval shown)	MD	Medium Dense			Density Index 35 - 65%
		HP	Hand Penetrometer test (UCS kPa)	D	Dense			Density Index 65 - 85%
				VD	Very Dense			Density Index 85 - 100%



ENGINEERING LOG - BOREHOLE

CLIENT: NSW Health
PROJECT NAME: Proposed New Hospital
SITE LOCATION: Precast Yard
TEST LOCATION: As per GPS

BOREHOLE NO: **BH2**
PAGE: 1 of 2
JOB NO: RGS31237.1
LOGGED BY: DR
DATE: 21/9/17

DRILL TYPE: P160 EASTING: SURFACE RL:
BOREHOLE DIAMETER: 125 mm INCLINATION: 90° NORTHING: DATUM: WG584

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations										
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result											
AD	Not Encountered	1.00m SPT 1,0,1 N=1 1.45m		1.0		CL	0.30m FILL: Sandy GRAVE, dark grey, brown, 40mm material or similar FILL: Sandy Silty CLAY, low plasticity, pale grey and brown, some Gravel	D M				FILL										
RR						2.0	2.00m FILL: GRAVEL, medium to coarse grained, brown	D					FILL Building layer Rockfill									
Not Encountered		4.00m SPT 3,3,4 N=7 4.45m		2.0		GP	3.50m FILL: GRAVEL, medium to coarse grained, brown	D				FILL Building layer Rockfill										
						ML	Clayey SILT: Low plasticity, dark brown	M					St	ALLUVIUM								
															CL	CLAY: Medium plasticity, dark grey	M > w _p	S	SPT falling on rod weight only			
																				CL	CLAY: Medium plasticity, pale grey	M < w _p
Not Encountered		5.50m SPT 0,0,0 N=0 5.95m		3.0		ML	5.30m CLAY: Medium plasticity, dark grey	M > w _p	S	HP	35	SPT falling on rod weight only										
													CL	CLAY: Medium plasticity, pale grey	M < w _p	St / VSt	SPT falling with rod and hammer weight only					
																		CL	CLAY: Medium plasticity, pale grey	M < w _p	St / VSt	SPT falling with rod and hammer weight only
Not Encountered		7.00m SPT 0,0,0 N=0 7.45m		4.0		CL	8.00m CLAY: Medium plasticity, pale grey	M < w _p	St / VSt	HP	30	SPT falling with rod and hammer weight only										
													CL	CLAY: Medium plasticity, pale grey	M < w _p	St / VSt	SPT falling with rod and hammer weight only					
																		CL	CLAY: Medium plasticity, pale grey	M < w _p	St / VSt	SPT falling with rod and hammer weight only
Not Encountered		8.50m SPT 0,3,3 N=6 8.95m		5.0		CL	8.00m CLAY: Medium plasticity, pale grey	M < w _p	St / VSt	HP	30	SPT falling with rod and hammer weight only										
													CL	CLAY: Medium plasticity, pale grey	M < w _p	St / VSt	SPT falling with rod and hammer weight only					
																		CL	CLAY: Medium plasticity, pale grey	M < w _p	St / VSt	SPT falling with rod and hammer weight only
Not Encountered		10.00m		6.0		CL	8.00m CLAY: Medium plasticity, pale grey	M < w _p	St / VSt	HP	30	SPT falling with rod and hammer weight only										
													CL	CLAY: Medium plasticity, pale grey	M < w _p	St / VSt	SPT falling with rod and hammer weight only					
																		CL	CLAY: Medium plasticity, pale grey	M < w _p	St / VSt	SPT falling with rod and hammer weight only

LEGEND: Water Water Level (Date and time shown) Water Inflow Water Outflow Strata Changes --- Gradational or transitional strata — Definitive or distinct strata change	Notes, Samples and Tests U ₅₀ 50mm Diameter tube sample CBR Bulk sample for CBR testing E Environmental sample ASS Acid Sulfate Soil Sample B Bulk Sample Field Tests PID Photoionisation detector reading (ppm) DCP(x-y) Dynamic penetrometer test (test depth interval shown) HP Hand Penetrometer test (UCS kPa)	Consistency VS Very Soft S Soft F Firm St Stiff VSt Very Stiff H Hard Fb Friable Density V Very Loose L Loose MD Medium Dense D Dense VD Very Dense	UCS (kPa) <25 25 - 50 50 - 100 100 - 200 200 - 400 >400	Moisture Condition D Dry M Moist W Wet W _p Plastic Limit W _L Liquid Limit



ENGINEERING LOG - BOREHOLE

CLIENT: NSW Health
PROJECT NAME: Proposed New Hospital
SITE LOCATION: Precast Yard
TEST LOCATION: As per GPS

BOREHOLE NO: BH2
PAGE: 2 of 2
JOB NO: RGS31237.1
LOGGED BY: DR
DATE: 21/9/17

DRILL TYPE: P160
BOREHOLE DIAMETER: 125 mm
INCLINATION: 90°
EASTING:
NORTHING:
SURFACE RL: WG584
DATUM:

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
RR		SPT 2,4,4 N=8 10.45m		11.0		CL	CLAY: Medium plasticity, pale grey (<i>continued</i>)	M < w _p	St / VSt	HP	200	ALLUVIUM
				11.50m			Becoming green/grey					RESIDUAL SOIL
		SPT 2,2,4 N=6 11.95m		12.0								HP = 100-120 kPa
				13.00m			Some relic rock structure, fine angular, fine to medium quartz Gravel					HP = 120-200 kPa
		SPT 14,7,10 N=17 13.45m		14.0								
				14.50m			Quartz and relic rock structure present, Clay has shell in some parts			HP	200	
		SPT 6,10,11 N=21 14.95m		15.0								
				16.00m			META SILTSTONE: Extremely weathered, trace foliations relic rock structure throughout, pale grey to brown	Fb				EXTREMELY WEATHERED META SILTSTONE HP = 100-200 kPa
		SPT 7,9,11 N=20 16.45m		17.0								
				17.50m								
		SPT 16,25,30/100 N=R 17.90m		18.0						HP	300	
				18.50m								
		SPT 19,30/130 N=R 19.00m		19.0								
				19.13m			Hole Terminated at 19.13 m					HP = 300-600 kPa

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)		Moisture Condition	
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25		D	Dry
Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50		M	Moist
Water Inflow		E Environmental sample		F	Firm	50 - 100		W	Wet
Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200		W _p	Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400		W _L	Liquid Limit
Gradational or transitional strata		Field Tests		H	Hard	>400			
Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable				
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density	V	Very Loose	Density Index <15%		
		HP Hand Penetrometer test (UCS kPa)			L	Loose	Density Index 15 - 35%		
					MD	Medium Dense	Density Index 35 - 65%		
					D	Dense	Density Index 65 - 85%		
					VD	Very Dense	Density Index 85 - 100%		



ENGINEERING LOG - TEST PIT

CLIENT: NSW Health
PROJECT NAME: Proposed Hospital
SITE LOCATION:
TEST LOCATION: UTM56J

TEST PIT NO: **TP01**
PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: MR
DATE: 18/10/17

EQUIPMENT TYPE: 5T Excavator
TEST PIT LENGTH: 2.5 m WIDTH: 0.5 m
EASTING: 494568 m SURFACE RL:
NORTHING: 6604287 m DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
0.45m TOOTH BUCKET	Not Encountered	B		0.5		CL	FILL: Gravelly Silty CLAY, medium to low plasticity, pale grey and pale yellow/pale brown	M				FILL (Ripped and recompacted Phyllite)
				0.90m		CL						
		1.20m			CL	CLAY: Medium plasticity, pale brown			RESIDUAL SOIL			
		1.50m										
		1.80m		Hole Terminated at 1.80 m								
				2.0								
				2.5								

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25	D	Dry
Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50	M	Moist
Water Inflow		E Environmental sample		F	Firm	50 - 100	W	Wet
Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200	W _p	Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400	W _L	Liquid Limit
Gradational or transitional strata		Field Tests		H	Hard	>400		
Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable			
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density	V	Very Loose	Density Index <15%	
		HP Hand Penetrometer test (UCS kPa)			L	Loose	Density Index 15 - 35%	
					MD	Medium Dense	Density Index 35 - 65%	
					D	Dense	Density Index 65 - 85%	
					VD	Very Dense	Density Index 85 - 100%	



ENGINEERING LOG - TEST PIT

CLIENT: NSW Health
PROJECT NAME: Proposed Hospital
SITE LOCATION:
TEST LOCATION: UTM56J

TEST PIT NO: **TP02**
PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: MR
DATE: 18/10/17

EQUIPMENT TYPE: 5T Excavator
TEST PIT LENGTH: 2.5 m WIDTH: 0.5 m
EASTING: 494577 m SURFACE RL:
NORTHING: 6604316 m DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
0.45m TOOTH BUCKET	Not Encountered					GW	FILL: Sandy GRAVEL, fine to medium grained, brown	M	VD			FILL: Existing unsealed pavement
				0.20m		CL	FILL: CLAY, medium plasticity, brown, orange/brown and pale grey	M < w _p	VSt			FILL
				0.5								HP=200-240kPa
				0.80m		CL	FILL: CLAY, medium plasticity, brown and dark brown	M < w _p	VSt			FILL
		1.40m		1.0								HP=210-240kPa
		BS		1.40m		CL	CLAY: Medium plasticity, orange/brown	M < w _p	VSt			RESIDUAL SOIL
		1.75m		1.5						HP	260	
				2.0			Hole Terminated at 2.00 m					
				2.5								

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25	D	Dry
Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50	M	Moist
Water Inflow		E Environmental sample		F	Firm	50 - 100	W	Wet
Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200	w _p	Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400	w _L	Liquid Limit
Gradational or transitional strata		Field Tests		H	Hard	>400		
Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable			
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density	V	Very Loose	Density Index <15%	
		HP Hand Penetrometer test (UCS kPa)			L	Loose	Density Index 15 - 35%	
					MD	Medium Dense	Density Index 35 - 65%	
					D	Dense	Density Index 65 - 85%	
					VD	Very Dense	Density Index 85 - 100%	



ENGINEERING LOG - TEST PIT

CLIENT: NSW Health
PROJECT NAME: Proposed Hospital
SITE LOCATION:
TEST LOCATION: UTM56J

TEST PIT NO: **TP03**
PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: MR
DATE: 18/10/17

EQUIPMENT TYPE: 5T Excavator
TEST PIT LENGTH: 2.0 m WIDTH: 0.5 m
EASTING: 494558 m SURFACE RL:
NORTHING: 6604452 m DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
0.45m TOOTH BUCKET	Not Encountered					CL	CLAY: Medium plasticity, brown	M < w _p	H	HP	500	RESIDUAL SOIL
				0.5								
				0.80m		CL	CLAY: Medium plasticity, pale grey and orange/brown mottle	M < w _p	H	HP	550	EXTREMELY WEATHERED PHYLLITE
				1.0								
		1.40m		1.20m			Extremely Weathered PHYLLITE: Pale grey with orange/brown and yellow iron oxide staining, estimated very low strength		Fb			
		BS		1.5								
		1.70m		1.75m								
				2.0			Hole Terminated at 1.75 m					
				2.5								

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25	D	Dry
Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50	M	Moist
Water Inflow		E Environmental sample		F	Firm	50 - 100	W	Wet
Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200	W _p	Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400	W _L	Liquid Limit
Gradational or transitional strata		Field Tests		H	Hard	>400		
Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable			
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density	V	Very Loose	Density Index <15%	
		HP Hand Penetrometer test (UCS kPa)			L	Loose	Density Index 15 - 35%	
					MD	Medium Dense	Density Index 35 - 65%	
					D	Dense	Density Index 65 - 85%	
					VD	Very Dense	Density Index 85 - 100%	

CLIENT: NSW Health
PROJECT NAME: Proposed Hospital
SITE LOCATION:
TEST LOCATION: UTM56J

PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: MR
DATE: 18/10/17

EQUIPMENT TYPE:	5T Excavator	EASTING:	494638 m	SURFACE RL:	
TEST PIT LENGTH:	3.0 m	WIDTH:	0.5 m	NORTHING:	6604438 m
				DATUM:	AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics,colour,minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
0.45m TOOTH BUCKET	Not Encountered			0.5		CL	FILL: Silty CLAY, medium plasticity, brown to dark brown, (organic roots throughout)	M	H	HP	550	FILL
					1.0		CL	Silty CLAY: Medium plasticity, orange/brown, trace of Gravel	M < w _p			H
				2.0			Hole Terminated at 2.00 m					
				2.5								

LEGEND:

Water

-  Water Level
 (Date and time shown)
 Water Inflow
 Water Outflow

Strata Changes

- — Gradational or transitional strata
— Definitive or distinct strata change

Notes, Samples and Tests

- | | |
|-----------------|-----------------------------|
| U ₅₀ | 50mm Diameter tube sample |
| CBR | Bulk sample for CBR testing |
| E | Environmental sample |
| ASS | Acid Sulfate Soil Sample |
| B | Bulk Sample |

Field Tests

- | | |
|----------|---|
| PID | Photoionisation detector reading (ppm) |
| DCP(x-y) | Dynamic penetrometer test (test depth interval shown) |
| HP | Hand Penetrometer test (UCS kPa) |

Consistency

- | | |
|-----|------------|
| VS | Very Soft |
| S | Soft |
| F | Firm |
| St | Stiff |
| VSt | Very Stiff |
| H | Hard |
| Fb | Friable |

UCS (kPa)

- <25
25 - 50
50 - 100
100 - 200
200 - 400
>400

Moisture Condition

- | | |
|-------|---------------|
| D | Dry |
| M | Moist |
| W | Wet |
| W_p | Plastic Limit |
| W_l | Liquid Limit |

Density

- | <u>Density</u> | | | |
|----------------|--------------|---------------|-----------|
| V | Very Loose | Density Index | <15% |
| L | Loose | Density Index | 15 - 35% |
| MD | Medium Dense | Density Index | 35 - 65% |
| D | Dense | Density Index | 65 - 85% |
| VD | Very Dense | Density Index | 85 - 100% |



ENGINEERING LOG - TEST PIT

CLIENT: NSW Health
PROJECT NAME: Proposed Hospital
SITE LOCATION:
TEST LOCATION: UTM56J

TEST PIT NO: **TP05**
PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: MR
DATE: 18/10/17

EQUIPMENT TYPE: 5T Excavator EASTING: 494609 m SURFACE RL:
TEST PIT LENGTH: 3.0 m WIDTH: 0.5 m NORTHING: 6604371 m DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
0.45m TOOTH BUCKET	Not Encountered	0.40m				GW	FILL: Sandy GRAVEL, fine to medium grained, brown/grey	M	VD			FILL
		BS		0.5		CL	Silty CLAY: Medium plasticity, orange/brown	M < w _p	VSt	HP	250	RESIDUAL SOIL
		0.85m		1.0				M < w _p	H	HP	450	
				1.5			Hole Terminated at 1.50 m					
				2.0								
				2.5								

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25	D	Dry
Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50	M	Moist
Water Inflow		E Environmental sample		F	Firm	50 - 100	W	Wet
Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200	W _p	Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400	W _L	Liquid Limit
Gradational or transitional strata		Field Tests		H	Hard	>400		
Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable			
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density		V	Very Loose	Density Index <15%
		HP Hand Penetrometer test (UCS kPa)		L		Loose		Density Index 15 - 35%
				MD		Medium Dense		Density Index 35 - 65%
				D		Dense		Density Index 65 - 85%
				VD		Very Dense		Density Index 85 - 100%



ENGINEERING LOG - TEST PIT

CLIENT: NSW Health
PROJECT NAME: Proposed Hospital
SITE LOCATION:
TEST LOCATION: UTM56J

TEST PIT NO: **TP07**
PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: MR
DATE: 18/10/17

EQUIPMENT TYPE: 5T Excavator
TEST PIT LENGTH: 3.0 m WIDTH: 0.5 m
EASTING: 494672 m SURFACE RL:
NORTHING: 6604294 m DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
0.45m TOOTH BUCKET	Not Encountered			0.5		GW	FILL: Sandy GRAVEL, fine to medium grained, brown	M	VD	HP	20	FILL: Existing unsealed pavement
					0.20m	CL	FILL: Silty CLAY, Medium plasticity, pale yellow/pale brown	M < w _p	VSt			FILL
					0.70m	GC	Clayey GRAVEL: Fine to medium grained, pale brown	M	VD			FILL
					0.90m	CL	CLAY: Medium plasticity, orange/brown	M < w _p	VSt			RESIDUAL SOIL
					1.0		Becoming pale grey and orange/brown mottle	M < w _p	H			HP
1.80m		Fb										
2.0												
		BS					Extremely Weathered PHYLLITE: Pale grey and orange/brown, estimated very low strength					
		2.00m		2.0			Hole Terminated at 2.00 m					
				2.5								

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25	D	Dry
Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50	M	Moist
Water Inflow		E Environmental sample		F	Firm	50 - 100	W	Wet
Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200	w _p	Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400	w _L	Liquid Limit
Gradational or transitional strata		Field Tests		H	Hard	>400		
Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable			
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density	V	Very Loose	Density Index <15%	
		HP Hand Penetrometer test (UCS kPa)			L	Loose	Density Index 15 - 35%	
					MD	Medium Dense	Density Index 35 - 65%	
					D	Dense	Density Index 65 - 85%	
					VD	Very Dense	Density Index 85 - 100%	



ENGINEERING LOG - TEST PIT

CLIENT: NSW Health
PROJECT NAME: Proposed Hospital
SITE LOCATION:
TEST LOCATION: UTM56J

TEST PIT NO: **TP08**
PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: MR
DATE: 18/10/17

EQUIPMENT TYPE: 5T Excavator
TEST PIT LENGTH: 3.0 m WIDTH: 0.5 m
EASTING: 494674 m SURFACE RL:
NORTHING: 6604242 m DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
0.45m TOOTH BUCKET	Not Encountered					GW	FILL: Sandy GRAVEL, fine to medium grained, brown	M	VD	HP	250	FILL
		0.20m	CL	FILL: Gravelly CLAY, medium plasticity, pale grey and brown/orange		M < w _p	VSt	FILL (Reworked Extremely Weathered PHYLLITE)				
		0.90m		0.90m	CL	Silty CLAY: Medium plasticity, orange/brown	M < w _p	VSt / H	RESIDUAL SOIL HP=250-450kPa			
		BS										
		1.50m		1.5								
				2.0		2.00m	Hole Terminated at 2.00 m					
				2.5								

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25	D	Dry
Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50	M	Moist
Water Inflow		E Environmental sample		F	Firm	50 - 100	W	Wet
Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200	w _p	Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400	w _L	Liquid Limit
Gradational or transitional strata		Field Tests		H	Hard	>400		
Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable			
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density	V	Very Loose	Density Index <15%	
		HP Hand Penetrometer test (UCS kPa)			L	Loose	Density Index 15 - 35%	
					MD	Medium Dense	Density Index 35 - 65%	
					D	Dense	Density Index 65 - 85%	
					VD	Very Dense	Density Index 85 - 100%	



ENGINEERING LOG - TEST PIT

CLIENT: NSW Health
PROJECT NAME: Proposed Hospital
SITE LOCATION:
TEST LOCATION: UTM56J

TEST PIT NO: **TP10**
PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: MR
DATE: 18/10/17

EQUIPMENT TYPE: 5T Excavator EASTING: 494750 m SURFACE RL:
TEST PIT LENGTH: 2.5 m WIDTH: 0.5 m NORTHING: 6603718 m DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
0.45m TOOTH BUCKET	Not Encountered	0.30m			ML	0.30m	TOPSOIL: SILT, low plasticity, dark brown, some organics	M	St	HP	160	TOPSOIL
		BS			CL		Silty CLAY: Medium plasticity, orange/brown	M > w _p	VSt	HP	250	RESIDUAL SOIL
		0.75m										
				2.0			Hole Terminated at 1.80 m					
				2.5								

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25	D	Dry
Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50	M	Moist
Water Inflow		E Environmental sample		F	Firm	50 - 100	W	Wet
Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200	W _p	Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400	W _L	Liquid Limit
Gradational or transitional strata		Field Tests		H	Hard	>400		
Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable			
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density		V	Very Loose	Density Index <15%
		HP Hand Penetrometer test (UCS kPa)		L		Loose		Density Index 15 - 35%
				MD		Medium Dense		Density Index 35 - 65%
				D		Dense		Density Index 65 - 85%
				VD		Very Dense		Density Index 85 - 100%

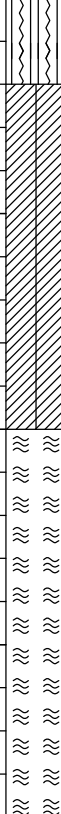


ENGINEERING LOG - TEST PIT

CLIENT: NSW Health
PROJECT NAME: Proposed Hospital
SITE LOCATION:
TEST LOCATION: UTM56J

TEST PIT NO: **TP11**
PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: MR
DATE: 18/10/17

EQUIPMENT TYPE: 5T Excavator
TEST PIT LENGTH: 2.9 m WIDTH: 0.5 m
EASTING: 494788 m SURFACE RL:
NORTHING: 6603749 m DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics,colour,minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
0.45m TOOTH BUCKET	Not Encountered				ML		TOPSOIL: SILT, low plasticity, dark brown, some roots, some quartz Gravel	M	St	HP	160	TOPSOIL
					CL		Silty CLAY: Medium plasticity, orange, brown, some quartz Gravel	M > W _p	VSt			RESIDUAL SOIL
							Extremely Weathered PHYLLITE: Pale grey with yellow/brown, iron oxide staining, estimated very low strength, some quartz lenses throughout	M	Fb			EXTREMELY WEATHERED PHYLLITE Excavates as Sandy GRAVEL
				2.0			Hole Terminated at 1.90 m					
				2.5								

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25	D	Dry
Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50	M	Moist
Water Inflow		E Environmental sample		F	Firm	50 - 100	W	Wet
Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200	W _p	Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400	W _L	Liquid Limit
Gradational or transitional strata		Field Tests		H	Hard	>400		
Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable			
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density	V	Very Loose	Density Index <15%	
		HP Hand Penetrometer test (UCS kPa)			L	Loose	Density Index 15 - 35%	
					MD	Medium Dense	Density Index 35 - 65%	
					D	Dense	Density Index 65 - 85%	
					VD	Very Dense	Density Index 85 - 100%	



ENGINEERING LOG - TEST PIT

CLIENT: NSW Health
PROJECT NAME: Proposed Hospital
SITE LOCATION:
TEST LOCATION: UTM56J

TEST PIT NO: **TP13**
PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: MR
DATE: 18/10/17

EQUIPMENT TYPE: 5T Excavator
TEST PIT LENGTH: 3.0 m WIDTH: 0.5 m
EASTING: 494841 m SURFACE RL:
NORTHING: 6603691 m DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
0.45m TOOTH BUCKET	Not Encountered					ML	TOPSOIL: SILT, low plasticity, dark brown, some organics and Gravel	M	St	HP	120	TOPSOIL
		0.50m	0.5		CL	0.25m Silty CLAY: Medium plasticity, orange/brown, some quartz Gravel throughout	M > w _p	RESIDUAL SOIL				
		BS										
		0.80m										
				1.0								
				1.5			Extremely to Highly Weathered PHYLLITE: Yellow with orange/brown and pale grey, estimated very low strength, some quartz		Fb			EXTREMELY TO HIGHLY WEATHERED PHYLLITE
				1.80m								
				2.0			Hole Terminated at 1.80 m					
				2.5								

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25	D	Dry
Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50	M	Moist
Water Inflow		E Environmental sample		F	Firm	50 - 100	W	Wet
Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200	w _p	Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400	w _L	Liquid Limit
Gradational or transitional strata		Field Tests		H	Hard	>400		
Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable			
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density	V	Very Loose	Density Index <15%	
		HP Hand Penetrometer test (UCS kPa)			L	Loose	Density Index 15 - 35%	
					MD	Medium Dense	Density Index 35 - 65%	
					D	Dense	Density Index 65 - 85%	
					VD	Very Dense	Density Index 85 - 100%	



ENGINEERING LOG - TEST PIT

CLIENT: NSW Health
PROJECT NAME: Proposed Hospital
SITE LOCATION:
TEST LOCATION: UTM56J

TEST PIT NO: **TP14**
PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: MR
DATE: 18/10/17

EQUIPMENT TYPE: 5T Excavator EASTING: 494813 m SURFACE RL:
TEST PIT LENGTH: 2.8 m WIDTH: 0.5 m NORTHING: 6603652 m DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
0.45m TOOTH BUCKET	Not Encountered					ML	TOPSOIL: SILT, low plasticity, dark brown, (trace of roots), trace Gravel	M	St	HP	140	TOPSOIL
						CL	Silty CLAY: Medium plasticity, orange/brown, some quartz Gravel throughout	M > W _p	St			RESIDUAL SOIL HP=180-200kPa
							Extremely to Highly Weathered PHYLLITE: Pale red and yellow/orange, iron oxide stain, estimated very low strength					EXTREMELY TO HIGHLY WEATHERED PHYLLITE
							Hole Terminated at 1.80 m					

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25	D	Dry
Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50	M	Moist
Water Inflow		E Environmental sample		F	Firm	50 - 100	W	Wet
Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200	W _p	Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400	W _L	Liquid Limit
Gradational or transitional strata		Field Tests		H	Hard	>400		
Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable			
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density		V	Very Loose	Density Index <15%
		HP Hand Penetrometer test (UCS kPa)		L		Loose		Density Index 15 - 35%
				MD		Medium Dense		Density Index 35 - 65%
				D		Dense		Density Index 65 - 85%
				VD		Very Dense		Density Index 85 - 100%



Appendix B

Investigation Logs



ENGINEERING LOG - BOREHOLE

BOREHOLE NO: **BH4**

CLIENT: Health Infrastructure

PAGE: 1 of 1

PROJECT NAME: Macksville Hospital Redevelopment

JOB NO: RGS31237.1

SITE LOCATION: Macksville

LOGGED BY: LD

TEST LOCATION: Refer to figure 1

DATE: 3/4/18

DRILL TYPE: Truck Mounted (NCR Rig 7)

EASTING: 494619 m

SURFACE RL:

BOREHOLE DIAMETER: 100 mm

INCLINATION: 90°

NORTHING: 6604358 m

DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
AD/TC	Not Encountered					ML	TOPSOIL: Clayey SILT, low plasticity, dark grey		St			TOPSOIL
		1.00m	1.0	CL	Silty CLAY: Medium plasticity, red-brown	M < w _p			HP	100	RESIDUAL SOIL	
		SPT 2,3,5 N=8					St	HP	150			
		1.45m					HP	160				
		2.50m	2.0	CL	Silty CLAY: Medium plasticity, pale brown, pale grey, red	M < w _p	VSt		HP	200	EXTREMELY WEATHERED PHYLLITE	
		SPT 3,6,8 N=14										
		2.95m	3.0	CL	Silty CLAY: Medium plasticity, pale brown, pale grey, with some fine angular quartz Gravel							
		4.00m	4.0	CL	Silty CLAY: Medium plasticity, pale grey, pale brown			HP	280			
		4.45m	5.0									
		5.50m					M	Fb				
SPT 14,25/130 N=R												
5.80m												
		5.80m					Hole Terminated at 5.78 m					

LEGEND:

Water

- Water Level (Date and time shown)
- Water Inflow
- Water Outflow

Strata Changes

- Gradational or transitional strata
- Definitive or distinct strata change

Notes, Samples and Tests

- U₅₀ 50mm Diameter tube sample
- CBR Bulk sample for CBR testing
- E Environmental sample
- ASS Acid Sulfate Soil Sample
- B Bulk Sample

Field Tests

- PID Photoionisation detector reading (ppm)
- DCP(x-y) Dynamic penetrometer test (test depth interval shown)
- HP Hand Penetrometer test (UCS kPa)

Consistency

- VS Very Soft
- S Soft
- F Firm
- St Stiff
- VSt Very Stiff
- H Hard
- Fb Friable

UCS (kPa)

- <25
- 25 - 50
- 50 - 100
- 100 - 200
- 200 - 400
- >400

Moisture Condition

- D Dry
- M Moist
- W Wet
- W_p Plastic Limit
- W_L Liquid Limit

Density

- V Very Loose
- L Loose
- MD Medium Dense
- D Dense
- VD Very Dense

- Density Index <15%
- Density Index 15 - 35%
- Density Index 35 - 65%
- Density Index 65 - 85%
- Density Index 85 - 100%



ENGINEERING LOG - BOREHOLE

BOREHOLE NO: **BH5**

CLIENT: Health Infrastructure

PAGE: 1 of 1

PROJECT NAME: Macksville Hospital Redevelopment

JOB NO: RGS31237.1

SITE LOCATION: Macksville

LOGGED BY: LD

TEST LOCATION: Refer to figure 1

DATE: 3/4/18

DRILL TYPE: Truck Mounted (NCR Rig 7)

EASTING: 494652 m

SURFACE RL:

BOREHOLE DIAMETER: 100 mm

INCLINATION: 90°

NORTHING: 6604265 m

DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations	
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result		
AD/TC	Not Encountered					GC	FILL: Clayey GRAVEL, fine to medium grained, brown, angular Gravel	D	MD	HP	180	FILL	
		1.00m	1.0		ML CL	0.80m 0.90m TOPSOIL: Clayey SILT, medium plasticity, dark brown Silty CLAY: Medium plasticity, mottled red, brown, grey	M < w _p M < w _p	F St	OLD TOPSOIL RESIDUAL SOIL				
		SPT 2,3,4 N=7											
		1.50m 1.45m											
		B											
		2.00m	2.0										
		2.50m											
		SPT 2,5,14 N=19											
		2.95m	3.0										
		4.00m	4.0										
SPT 13,22/50 N=R													
4.30m													
SPT 25/100 N=R													
5.59m	5.0												
							5.60m Hole Terminated at 5.60 m						

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25	D	Dry
Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50	M	Moist
Water Inflow		E Environmental sample		F	Firm	50 - 100	W	Wet
Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200	w _p	Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400	w _L	Liquid Limit
Gradational or transitional strata		Field Tests		H	Hard	>400		
Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable			
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density	V	Very Loose	Density Index <15%	
		HP Hand Penetrometer test (UCS kPa)			L	Loose	Density Index 15 - 35%	
					MD	Medium Dense	Density Index 35 - 65%	
					D	Dense	Density Index 65 - 85%	
					VD	Very Dense	Density Index 85 - 100%	



ENGINEERING LOG - BOREHOLE

CLIENT: Health Infrastructure
PROJECT NAME: Macksville Hospital Redevelopment
SITE LOCATION: Macksville
TEST LOCATION: Refer to figure 1

BOREHOLE NO: BH6
PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: LD
DATE: 3/4/18

DRILL TYPE: Truck Mounted (NCR Rig 7) **EASTING:** 494531 m **SURFACE RL:**
BOREHOLE DIAMETER: 100 mm **INCLINATION:** 90° **NORTHING:** 6604294 m **DATUM:** AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations	
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result		
AD/TC	Not Encountered					GP	0.10m FILL: GRAVEL, fine to medium grained, grey	D				FILL	
			GW	FILL: Clayey Sandy GRAVEL, fine grained, dark grey, angular Gravel									
		1.00m		1.0		CL	0.70m Silty CLAY: Medium plasticity, brown, with some fine angular Gravel	M < w _p	St / VSt				RESIDUAL SOIL
		SPT 7,14,15 N=29											
		1.45m		2.0		CL	2.00m Silty CLAY: Medium plasticity, pale brown, pale grey	M < w _p	H / Fb				EXTREMELY WEATHERED PHYLLITE
		2.50m		3.0									
		SPT 16,27/90 N=R		4.0		CL	4.00m Silty CLAY: Medium plasticity, pale brown, pale grey, with some fine to medium angular quartz Gravel						
		2.65m		5.0									
		4.00m											
		SPT 7,16,21 N=37											
4.45m													
5.50m													
SPT 12,30/110 N=R													
5.65m							5.76m Hole Terminated at 5.76 m						

LEGEND: Water Water Level (Date and time shown) Water Inflow Water Outflow Strata Changes Gradational or transitional strata Definitive or distinct strata change	Notes, Samples and Tests U ₅₀ 50mm Diameter tube sample CBR Bulk sample for CBR testing E Environmental sample ASS Acid Sulfate Soil Sample B Bulk Sample Field Tests PID Photoionisation detector reading (ppm) DCP(x-y) Dynamic penetrometer test (test depth interval shown) HP Hand Penetrometer test (UCS kPa)	Consistency VS Very Soft S Soft F Firm St Stiff VSt Very Stiff H Hard Fb Friable UCS (kPa) <25 25 - 50 50 - 100 100 - 200 200 - 400 >400 Density V Very Loose L Loose MD Medium Dense D Dense VD Very Dense	Moisture Condition D Dry M Moist W Wet W _p Plastic Limit W _L Liquid Limit Density Index <15% Density Index 15 - 35% Density Index 35 - 65% Density Index 65 - 85% Density Index 85 - 100%
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BOREHOLE NO: **BH7**

PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: LD
DATE: 3/4/18

SURFACE RL:

DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
AD/TC	Not Encountered					CL	0.03m FILL: Clayey GRAVEL, fine to medium grained, pale brown, grey, angular Gravel Silty CLAY: Medium plasticity, pale brown	D $M < w_p$	H	HP	200	FILL FILL
						CL	0.70m FILL: Gravelly CLAY, medium plasticity, pale brown, fine to medium angular Gravel	$M < w_p$				
		1.06m SPT 30/70 N=R	1.0	GC	1.00m FILL: Clayey GRAVEL, fine to coarse grained, dark grey, angular Gravel							
		1.50m		CL	1.30m Silty CLAY: Medium plasticity, brown	$M < w_p$	St / VSt					
		B	2.0									
		2.50m		CL	2.30m Silty CLAY: Medium plasticity, pale grey, pale brown	$M < w_p$	H / Fb					
		SPT 4,10,21 N=31	2.95m									
		3.50m										
		N=25/150mm	3.80m 4.00m									
		SPT 8,25,25/80 N=R	4.45m					HP	270			
							5.88m Hole Terminated at 5.88 m					

LEGEND:

Water

-  Water Level
 (Date and time shown)
-  Water Inflow
-  Water Outflow

Strata Changes

- — Gradational or transitional strata
—— Definitive or distinct strata change

Notes, Samples and Tests

- | | |
|-----------------|-----------------------------|
| U ₅₀ | 50mm Diameter tube sample |
| CBR | Bulk sample for CBR testing |
| E | Environmental sample |
| ASS | Acid Sulfate Soil Sample |
| B | Bulk Sample |

Field Tests

- | | |
|----------|---|
| PID | Photoionisation detector reading (ppm) |
| DCP(x-y) | Dynamic penetrometer test (test depth interval shown) |
| HP | Hand Penetrometer test (UCS kPa) |

Consistency

- | | | |
|-----|------------|-----------|
| VS | Very Soft | <25 |
| S | Soft | 25 - 50 |
| F | Firm | 50 - 100 |
| St | Stiff | 100 - 200 |
| VSt | Very Stiff | 200 - 400 |
| H | Hard | >400 |
| Fb | Friable | |

UCS (kPa)

- | | | |
|-----|------------|-----------|
| VS | Very Soft | <25 |
| S | Soft | 25 - 50 |
| F | Firm | 50 - 100 |
| St | Stiff | 100 - 200 |
| VSt | Very Stiff | 200 - 400 |
| H | Hard | >400 |
| Fb | Friable | |

Moisture Condition

- | | |
|-------|---------------|
| D | Dry |
| M | Moist |
| W | Wet |
| W_p | Plastic Limit |
| W_l | Liquid Limit |

Density

- | <u>Density</u> | | | |
|----------------|--------------|---------------|-----------|
| V | Very Loose | Density Index | <15% |
| L | Loose | Density Index | 15 - 35% |
| MD | Medium Dense | Density Index | 35 - 65% |
| D | Dense | Density Index | 65 - 85% |
| VD | Very Dense | Density Index | 85 - 100% |



ENGINEERING LOG - BOREHOLE

CLIENT: Health Infrastructure
PROJECT NAME: Macksville Hospital Redevelopment
SITE LOCATION: Macksville
TEST LOCATION: Refer to figure 1

BOREHOLE NO: BH8
PAGE: 1 of 2
JOB NO: RGS31237.1
LOGGED BY: LD
DATE: 4/4/18

DRILL TYPE: Truck Mounted (NCR Rig 7) **EASTING:** 494548 m **SURFACE RL:**
BOREHOLE DIAMETER: 100 mm **INCLINATION:** 90° **NORTHING:** 6604105 m **DATUM:** AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
AD/TC	Not Encountered	0.50m				GW	FILL: Sandy GRAVEL, fine to medium grained, brown, angular Gravel	D				FILL
		SPT 3,6,5 N=11	0.50m	CL		FILL: Silty CLAY, medium plasticity, pale brown, pale grey, with some fine to medium angular Gravel	M < w _p	F / St				
WB-RR		1.00m 0.95m		1.0		GP	FILL: GRAVEL, fine to coarse grained, dark grey					GEOFAB - DRAINAGE LAYER ROCK FILL
	SPT 3,13,18 N=31	1.20m										
		1.45m				CH	Silty CLAY: High plasticity, dark grey, with rootlets	M > w _p	F	HP	100	GEOFAB - ALLUVIAL
		2.00m		2.0					HP		90	
		SPT 2,1,3 N=4										
		2.45m		3.0								
		3.50m				CH	Silty CLAY: Medium to high plasticity, pale grey, pale brown	M > w _p	F			
		SPT 3,5,6 N=11		4.0								
		3.95m				ML	Clayey SILT: Low plasticity, grey, pale brown, with some medium grained Gravel		F			
		5.00m		5.0					S			
		SPT 1,0,1 N=1							VS	HP	0	
		5.45m				ML	Clayey SILT: Low plasticity, dark grey				HP	10

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25	D	Dry
Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50	M	Moist
Water Inflow		E Environmental sample		F	Firm	50 - 100	W	Wet
Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200	w _p	Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400	w _L	Liquid Limit
Gradational or transitional strata		Field Tests		H	Hard	>400		
Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable			
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density	V	Very Loose	Density Index <15%	
		HP Hand Penetrometer test (UCS kPa)			L	Loose	Density Index 15 - 35%	
					MD	Medium Dense	Density Index 35 - 65%	
					D	Dense	Density Index 65 - 85%	
					VD	Very Dense	Density Index 85 - 100%	



ENGINEERING LOG - BOREHOLE

CLIENT: Health Infrastructure
PROJECT NAME: Macksville Hospital Redevelopment
SITE LOCATION: Macksville
TEST LOCATION: Refer to figure 1

BOREHOLE NO: BH8
PAGE: 2 of 2
JOB NO: RGS31237.1
LOGGED BY: LD
DATE: 4/4/18

DRILL TYPE: Truck Mounted (NCR Rig 7) **EASTING:** 494548 m **SURFACE RL:**
BOREHOLE DIAMETER: 100 mm **INCLINATION:** 90° **NORTHING:** 6604105 m **DATUM:** AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
WB-RR		6.50m				ML	Clayey SILT: Low plasticity, dark grey (<i>continued</i>)	M > w _p	VS			GEOFAB - ALLUVIAL HP = 70-100kPa
		SPT 0,0,2 N=2				ML	Clayey SILT: Low plasticity, pale grey, grey					
		6.95m		7.0						HP	50	
						ML	Clayey SILT: Low plasticity, grey, pale brown, with some fine grained Sand	M < w _p	VSt			RESIDUAL SOIL
		8.00m		8.0						HP	60	
		SPT 1,3,4 N=7								HP	70	
		8.45m										
				9.0		ML	Clayey SILT: Low plasticity, grey					
		9.50m								HP	270	
		SPT 5,8,10 N=18								HP	300	
		9.95m		10.0						HP	300	
		11.00m		11.0						HP	140	
		SPT 8,7,10 N=17								HP	160	
										HP	220	
		11.45m					Hole Terminated at 11.45 m					

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water Water Level (Date and time shown) Water Inflow Water Outflow		U ₅₀ 50mm Diameter tube sample CBR Bulk sample for CBR testing E Environmental sample ASS Acid Sulfate Soil Sample B Bulk Sample		VS	Very Soft	<25	D	Dry
Strata Changes Gradational or transitional strata Definitive or distinct strata change		Field Tests PID Photoionisation detector reading (ppm) DCP(x-y) Dynamic penetrometer test (test depth interval shown) HP Hand Penetrometer test (UCS kPa)		S	Soft	25 - 50	M	Moist
				F	Firm	50 - 100	W	Wet
				St	Stiff	100 - 200	W _p	Plastic Limit
				VSt	Very Stiff	200 - 400	W _L	Liquid Limit
				H	Hard	>400		
				Fb	Friable			
				Density	V	Very Loose	Density Index <15%	
					L	Loose	Density Index 15 - 35%	
					MD	Medium Dense	Density Index 35 - 65%	
					D	Dense	Density Index 65 - 85%	
					VD	Very Dense	Density Index 85 - 100%	



ENGINEERING LOG - BOREHOLE

CLIENT: Health Infrastructure
PROJECT NAME: Macksville Hospital Redevelopment
SITE LOCATION: Macksville
TEST LOCATION: Refer to figure 1

BOREHOLE NO: BH9
PAGE: 1 of 3
JOB NO: RGS31237.1
LOGGED BY: LD
DATE: 4/4/18

DRILL TYPE: Truck Mounted (NCR Rig 7)

EASTING: 494544 m

SURFACE RL:

BOREHOLE DIAMETER: 100 mm

INCLINATION: 90°

NORTHING: 6603988 m

DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
AD/TC	Not Encountered					GP	0.10m FILL: GRAVEL, fine to medium grained, dark grey, angular FILL: Silty CLAY, medium plasticity, brown	D	L			FILL
		1.00m		1.0								
		SPT 2,3,7 N=10										
		1.45m										
						GP	1.70m FILL: GRAVEL, fine to coarse grained, dark grey	D	D			GEOFAB - DRAINAGE LAYER ROCK FILL
		2.50m				CL	2.40m FILL: Silty CLAY, medium plasticity, pale brown, pale grey, with some fine to medium angular Gravel		St			FILL
		SPT 3,4,3 N=7										
		3.00m		3.0								
		2.95m										
Not Encountered	Not Encountered	SPT 2,5,7 N=12										
		3.45m										
		4.00m		4.0								
		SPT 2,1,2 N=3										
		4.45m										
		5.40m		5.0		ML	5.00m Clayey SILT: Low plasticity, dark grey, with some fine grained Sand	M > w _p	St			ALLUVIAL
		5.50m										
		DS SPT 1,2,2 N=4								HP	120	

LEGEND:

Water

- Water Level (Date and time shown)
- Water Inflow
- Water Outflow

Strata Changes

- Gradational or transitional strata
- Definitive or distinct strata change

Notes, Samples and Tests

- U₅₀ 50mm Diameter tube sample
- CBR Bulk sample for CBR testing
- E Environmental sample
- ASS Acid Sulfate Soil Sample
- B Bulk Sample

Field Tests

- PID Photoionisation detector reading (ppm)
- DCP(x-y) Dynamic penetrometer test (test depth interval shown)
- HP Hand Penetrometer test (UCS kPa)

Consistency

- VS Very Soft
- S Soft
- F Firm
- St Stiff
- VSt Very Stiff
- H Hard
- Fb Friable

UCS (kPa)

- <25
- 25 - 50
- 50 - 100
- 100 - 200
- 200 - 400
- >400

Moisture Condition

- D Dry
- M Moist
- W Wet
- w_p Plastic Limit
- w_L Liquid Limit

Density

- V Very Loose
- L Loose
- MD Medium Dense
- D Dense
- VD Very Dense

- Density Index <15%
- Density Index 15 - 35%
- Density Index 35 - 65%
- Density Index 65 - 85%
- Density Index 85 - 100%



ENGINEERING LOG - BOREHOLE

CLIENT: Health Infrastructure
PROJECT NAME: Macksville Hospital Redevelopment
SITE LOCATION: Macksville
TEST LOCATION: Refer to figure 1

BOREHOLE NO: **BH9**
PAGE: 2 of 3
JOB NO: RGS31237.1
LOGGED BY: LD
DATE: 4/4/18

DRILL TYPE: Truck Mounted (NCR Rig 7)

EASTING: 494544 m

SURFACE RL:

BOREHOLE DIAMETER: 100 mm

INCLINATION: 90°

NORTHING: 6603988 m

DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations	
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result		
AD/TC	Not encountered	5.95m					ML	Clayey SILT: Low plasticity, dark grey, with some fine grained Sand (<i>continued</i>)	M > w _p	St			ALLUVIAL
		7.00m		7.0		CH	Silty CLAY: Medium to high plasticity, grey						
		SPT 2,5,6 N=11											
		7.45m											
		8.50m							M < w _p	St			RESIDUAL SOIL
		SPT 2,3,5 N=8											
		8.95m						HP			120		
		10.00m		10.0				HP			60		
		SPT 2,4,6 N=10						HP			80		
		10.45m											
		11.50m											
		SPT 3,5,10 N=15											

LEGEND:

Water

- Water Level (Date and time shown)
- Water Inflow
- Water Outflow

Strata Changes

- Gradational or transitional strata
- Definitive or distinct strata change

Notes, Samples and Tests

- U₅₀ 50mm Diameter tube sample
- CBR Bulk sample for CBR testing
- E Environmental sample
- ASS Acid Sulfate Soil Sample
- B Bulk Sample

Field Tests

- PID Photoionisation detector reading (ppm)
- DCP(x-y) Dynamic penetrometer test (test depth interval shown)
- HP Hand Penetrometer test (UCS kPa)

Consistency

- VS Very Soft
- S Soft
- F Firm
- St Stiff
- VSt Very Stiff
- H Hard
- Fb Friable

UCS (kPa)

- <25
- 25 - 50
- 50 - 100
- 100 - 200
- 200 - 400
- >400

Moisture Condition

- D Dry
- M Moist
- W Wet
- w_p Plastic Limit
- w_L Liquid Limit

Density

- V Very Loose
- L Loose
- MD Medium Dense
- D Dense
- VD Very Dense

- Density Index <15%
- Density Index 15 - 35%
- Density Index 35 - 65%
- Density Index 65 - 85%
- Density Index 85 - 100%



ENGINEERING LOG - BOREHOLE

BOREHOLE NO: **BH9**

CLIENT: Health Infrastructure

PAGE: 3 of 3

PROJECT NAME: Macksville Hospital Redevelopment

JOB NO: RGS31237.1

SITE LOCATION: Macksville

LOGGED BY: LD

TEST LOCATION: Refer to figure 1

DATE: 4/4/18

DRILL TYPE: Truck Mounted (NCR Rig 7)

EASTING: 494544 m

SURFACE RL:

BOREHOLE DIAMETER: 100 mm

INCLINATION: 90°

NORTHING: 6603988 m

DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
AD/TC		11.95m				CH	Silty CLAY: Medium to high plasticity, pale grey, pale brown, with some fine grained Sand to some fine angular Gravel (<i>continued</i>)	M < w _p	St			RESIDUAL SOIL
		13.00m		13.0								
		SPT 5,8,9 N=17								HP 100 HP 110		
		13.45m					Hole Terminated at 13.45 m					
				14.0								
				15.0								
				16.0								
				17.0								

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25	D	Dry
Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50	M	Moist
Water Inflow		E Environmental sample		F	Firm	50 - 100	W	Wet
Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200	W _p	Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400	W _L	Liquid Limit
Gradational or transitional strata		Field Tests		H	Hard	>400		
Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable			
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density	V	Very Loose	Density Index <15%	
		HP Hand Penetrometer test (UCS kPa)			L	Loose	Density Index 15 - 35%	
					MD	Medium Dense	Density Index 35 - 65%	
					D	Dense	Density Index 65 - 85%	
					VD	Very Dense	Density Index 85 - 100%	



ENGINEERING LOG - BOREHOLE

BOREHOLE NO: **BH10**

CLIENT: Health Infrastructure

PAGE: 1 of 2

PROJECT NAME: Macksville Hospital Redevelopment

JOB NO: RGS31237.1

SITE LOCATION: Macksville

LOGGED BY: LD

TEST LOCATION: Refer to figure 1

DATE: 5/4/18

DRILL TYPE: Truck Mounted (NCR Rig 7)

EASTING: 494546 m

SURFACE RL:

BOREHOLE DIAMETER: 100 mm

INCLINATION: 90°

NORTHING: 6603852 m

DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
AD/TC						CL	FILL: Silty CLAY, medium plasticity, brown, with some fine angular Gravel	M < w _p	St			FILL
		0.60m										
WB-RR		0.70m DS				ML	Clayey SILT: Low plasticity, dark brown	M > w _p	F			ALLUVIAL
		0.90m										
		1.00m DS			1.0							
		SPT 1,0,0 N=0								HP	70	
		1.50m										
		1.45m										
		1.60m DS			2.0							
		2.50m										
		SPT 1,4,5 N=9								HP	100	
		2.95m			3.0					HP	120	
		4.00m			4.0							
		SPT 1,1,2 N=3								HP	30	
		4.45m								HP	60	
										HP	60	
		5.50m			5.0							
	SPT 3,3,7 N=10								St			
										HP	200	
										HP	200	
										HP	100	

LEGEND:

Water

- Water Level (Date and time shown)
- Water Inflow
- Water Outflow

Strata Changes

- Gradational or transitional strata
- Definitive or distinct strata change

Notes, Samples and Tests

- U₅₀ 50mm Diameter tube sample
- CBR Bulk sample for CBR testing
- E Environmental sample
- ASS Acid Sulfate Soil Sample
- B Bulk Sample

Field Tests

- PID Photoionisation detector reading (ppm)
- DCP(x-y) Dynamic penetrometer test (test depth interval shown)
- HP Hand Penetrometer test (UCS kPa)

Consistency

- VS Very Soft
- S Soft
- F Firm
- St Stiff
- VSt Very Stiff
- H Hard
- Fb Friable

UCS (kPa)

- <25
- 25 - 50
- 50 - 100
- 100 - 200
- 200 - 400
- >400

Moisture Condition

- D Dry
- M Moist
- W Wet
- W_p Plastic Limit
- W_L Liquid Limit

Density

- V Very Loose
- L Loose
- MD Medium Dense
- D Dense
- VD Very Dense

- Density Index <15%
- Density Index 15 - 35%
- Density Index 35 - 65%
- Density Index 65 - 85%
- Density Index 85 - 100%



ENGINEERING LOG - BOREHOLE

BOREHOLE NO: **BH10**

CLIENT: Health Infrastructure
PROJECT NAME: Macksville Hospital Redevelopment
SITE LOCATION: Macksville
TEST LOCATION: Refer to figure 1

PAGE: 2 of 2
JOB NO: RGS31237.1
LOGGED BY: LD
DATE: 5/4/18

DRILL TYPE: Truck Mounted (NCR Rig 7)

EASTING: 494546 m

SURFACE RL:

BOREHOLE DIAMETER: 100 mm

INCLINATION: 90°

NORTHING: 6603852 m

DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations	
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result		
WB-RR		5.95m				CH	Silty CLAY: Medium plasticity, grey with trace fine grained Sand (<i>continued</i>) Colour becoming green	M > w _p	St	HP	100	ALLUVIAL	
		7.00m		7.0									
		SPT 2,4,6 N=10											
		7.45m											
				8.0		8.00m	CH	Silty CLAY: High plasticity, grey, with trace fine angular Gravel	M < w _p			St	
		8.50m											
		SPT 1,2,5 N=7		9.0									
	8.95m												
		10.00m		10.0		10.00m	CL	Silty CLAY: Medium plasticity, pale grey and orange/brown, mottle		St			RESIDUAL SOIL
						10.45m							
		10.45m		11.0			Hole Terminated at 10.45 m						

LEGEND:

Water

- Water Level (Date and time shown)
- Water Inflow
- Water Outflow

Strata Changes

- Gradational or transitional strata
- Definitive or distinct strata change

Notes, Samples and Tests

- U₅₀ 50mm Diameter tube sample
- CBR Bulk sample for CBR testing
- E Environmental sample
- ASS Acid Sulfate Soil Sample
- B Bulk Sample

Field Tests

- PID Photoionisation detector reading (ppm)
- DCP(x-y) Dynamic penetrometer test (test depth interval shown)
- HP Hand Penetrometer test (UCS kPa)

Consistency

- VS Very Soft
- S Soft
- F Firm
- St Stiff
- VSt Very Stiff
- H Hard
- Fb Friable

UCS (kPa)

- <25
- 25 - 50
- 50 - 100
- 100 - 200
- 200 - 400
- >400

Moisture Condition

- D Dry
- M Moist
- W Wet
- W_p Plastic Limit
- W_L Liquid Limit

Density

- V Very Loose
- L Loose
- MD Medium Dense
- D Dense
- VD Very Dense

- Density Index <15%
- Density Index 15 - 35%
- Density Index 35 - 65%
- Density Index 65 - 85%
- Density Index 85 - 100%



ENGINEERING LOG - BOREHOLE

BOREHOLE NO: **BH11**

CLIENT: Health Infrastructure
PROJECT NAME: Macksville Hospital Redevelopment
SITE LOCATION: Macksville
TEST LOCATION: Refer to figure 1

PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: LD
DATE: 5/4/18

DRILL TYPE: Truck Mounted (NCR Rig 7)

EASTING: 494548 m

SURFACE RL:

BOREHOLE DIAMETER: 100 mm

INCLINATION: 90°

NORTHING: 6603692 m

DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
AD/TC		0.90m 1.00m DS SPT 0,1,2 N=3		1.0		CL	FILL: Silty CLAY, low plasticity, brown with some fine grained Gravel					FILL
						ML	0.50m Clayey SILT: Low plasticity, dark brown	M > w _p	VS		ALLUVIAL	
WB-RR		1.45m		2.0		CL	1.90m Silty CLAY: Medium to high plasticity, grey, pale grey	M > w _p	St			
		2.50m		3.0								
		SPT		4.0								
		2.95m		4.45m								
		4.00m		5.0								
		SPT										
		3,6,7										
		N=13										
		4.45m					Hole Terminated at 4.45 m					

LEGEND:

Water

- Water Level (Date and time shown)
- Water Inflow
- Water Outflow

Strata Changes

- Gradational or transitional strata
- Definitive or distinct strata change

Notes, Samples and Tests

- U₅₀ 50mm Diameter tube sample
- CBR Bulk sample for CBR testing
- E Environmental sample
- ASS Acid Sulfate Soil Sample
- B Bulk Sample

Field Tests

- PID Photoionisation detector reading (ppm)
- DCP(x-y) Dynamic penetrometer test (test depth interval shown)
- HP Hand Penetrometer test (UCS kPa)

Consistency

- VS Very Soft
- S Soft
- F Firm
- St Stiff
- VSt Very Stiff
- H Hard
- Fb Friable

UCS (kPa)

- <25
- 25 - 50
- 50 - 100
- 100 - 200
- 200 - 400
- >400

Moisture Condition

- D Dry
- M Moist
- W Wet
- w_p Plastic Limit
- w_L Liquid Limit

Density

- V Very Loose
- L Loose
- MD Medium Dense
- D Dense
- VD Very Dense

- Density Index <15%
- Density Index 15 - 35%
- Density Index 35 - 65%
- Density Index 65 - 85%
- Density Index 85 - 100%



ENGINEERING LOG - TEST PIT

CLIENT: Health Infrastructure
PROJECT NAME: Proposed Macksville Hospital
SITE LOCATION:
TEST LOCATION: Refer to Figure 1

TEST PIT NO: TP1
PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: DR
DATE: 5/4/18

EQUIPMENT TYPE: 12T Excavator
TEST PIT LENGTH: 3.0 m
WIDTH: 0.5 m
EASTING:
NORTHING:
SURFACE RL:
DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
EXCAVATOR	Not Encountered			0.5		GP	Clayey GRAVEL: Medium grained, grey, angular Gravel, some Sand	M	D	HP	450	PAVEMENT/FILL
				0.50m		GP	Clayey GRAVEL: Medium grained, red-orange, trace Sand					FILL
				0.70m		CL	Silty CLAY: Medium plasticity, mottled red and pale brown, trace quartz Gravel	M < w _p	H	HP	600	RESIDUAL SOIL
				1.0								
				1.30m			Hole Terminated at 1.30 m					
				1.5								
				2.0								
				2.5								
				3.0								
				3.5								

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25	D	Dry
Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50	M	Moist
Water Inflow		E Environmental sample		F	Firm	50 - 100	W	Wet
Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200	W _p	Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400	W _L	Liquid Limit
Gradational or transitional strata		Field Tests		H	Hard	>400		
Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable			
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density		V	Very Loose	Density Index <15%
		HP Hand Penetrometer test (UCS kPa)				L	Loose	Density Index 15 - 35%
						MD	Medium Dense	Density Index 35 - 65%
						D	Dense	Density Index 65 - 85%
						VD	Very Dense	Density Index 85 - 100%



ENGINEERING LOG - TEST PIT

CLIENT: Health Infrastructure
PROJECT NAME: Proposed Macksville Hospital
SITE LOCATION:
TEST LOCATION: Refer to Figure 1

TEST PIT NO: TP2
PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: DR
DATE: 5/4/18

EQUIPMENT TYPE: 12T Excavator
TEST PIT LENGTH: 3.0 m
WIDTH: 0.5 m
EASTING:
NORTHING:
SURFACE RL:
DATUM: AHD

Drilling and Sampling					Material description and profile information						Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result		
EXCAVATOR	Not Encountered	CBR 0.50m		0.5 1.0 1.30m		GP	Clayey GRAVEL: Medium grained, grey, brown	M	D	HP	600	FILL/PAVEMENT	
						CL	Silty CLAY: Medium plasticity, orange, some fine to coarse grained Gravel	M < w _p	VSt			FILL	
						GP	Clayey GRAVEL/COBBLES: Medium to coarse grained, some cobble sized	M	D			GEOFAB ROCK FILL	
						CL	Silty CLAY: Medium plasticity, dark brown	M > w _p	St			GEOFAB - ALLUVIAL	
				1.5 2.0 2.5 3.0 3.5			Hole Terminated at 1.30 m						

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water Water Level (Date and time shown) Water Inflow Water Outflow		U ₅₀ 50mm Diameter tube sample CBR Bulk sample for CBR testing E Environmental sample ASS Acid Sulfate Soil Sample B Bulk Sample		VS Very Soft	<25		D Dry	
Strata Changes Gradational or transitional strata Definitive or distinct strata change		Field Tests PID Photoionisation detector reading (ppm) DCP(x-y) Dynamic penetrometer test (test depth interval shown) HP Hand Penetrometer test (UCS kPa)		S Soft	25 - 50		M Moist	
				F Firm	50 - 100		W Wet	
				St Stiff	100 - 200		W _p Plastic Limit	
				VSt Very Stiff	200 - 400		W _L Liquid Limit	
				H Hard	>400			
				Fb Friable				
				Density	V Very Loose	Density Index <15%		
					L Loose	Density Index 15 - 35%		
					MD Medium Dense	Density Index 35 - 65%		
					D Dense	Density Index 65 - 85%		
					VD Very Dense	Density Index 85 - 100%		



ENGINEERING LOG - TEST PIT

CLIENT: Health Infrastructure
PROJECT NAME: Proposed Macksville Hospital
SITE LOCATION:
TEST LOCATION: Refer to Figure 1

TEST PIT NO: TP3
PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: DR
DATE: 5/4/18

EQUIPMENT TYPE: 12T Excavator
TEST PIT LENGTH: 3.0 m
WIDTH: 0.5 m
EASTING:
NORTHING:
SURFACE RL:
DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
EXCAVATOR						GP	Clayey GRAVEL: Medium grained, grey, trace Sand	M	D	HP	600	PAVEMENT / COARSE MATERIAL
						CL	Silty CLAY: Medium plasticity, orange, some fine to medium grained Gravel	M < w _p	H			GENERAL FILL
						GP	GRAVEL/COBBLES: Coarse to cobble size up to 300mm in size, some fines	M	MD			GEOFAB - DRAINAGE LAYER ROCK FILL
						CL	Silty CLAY: Medium plasticity, dark brown	M > w _p	St	HP	120	GEOFAB - ALLUVIAL
							Hole Terminated at 1.50 m					

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25	D	Dry
Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50	M	Moist
Water Inflow		E Environmental sample		F	Firm	50 - 100	W	Wet
Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200	W _p	Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400	W _L	Liquid Limit
--- Gradational or transitional strata		Field Tests		H	Hard	>400		
— Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable			
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density	V	Very Loose	Density Index <15%	
		HP Hand Penetrometer test (UCS kPa)			L	Loose	Density Index 15 - 35%	
					MD	Medium Dense	Density Index 35 - 65%	
					D	Dense	Density Index 65 - 85%	
					VD	Very Dense	Density Index 85 - 100%	



ENGINEERING LOG - TEST PIT

CLIENT: Health Infrastructure
PROJECT NAME: Proposed Macksville Hospital
SITE LOCATION:
TEST LOCATION: Refer to Figure 1

TEST PIT NO: TP4
PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: DR
DATE: 5/4/18

EQUIPMENT TYPE: 12T Excavator
TEST PIT LENGTH: 3.0 m
WIDTH: 0.5 m
EASTING: 494731 m
NORTHING: 6604133 m
SURFACE RL:
DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
EXCAVATOR		CBR 0.40m				GW	Clayey GRAVEL: Fine to medium grained, grey/brown, some fine Sand	M	D			PAVEMENT / WEARING COARSE
				0.5		CL	Silty CLAY: Medium plasticity, orange, some fine to medium Gravel	M < w _p	VSt / H	HP	600	FILL
				1.0		GP	GRAVEL/COBBLES: Coarse to cobble size up to 100mm, some fines	M	L			GEOFAB - DRAINAGE LAYER ROCK FILL
				1.5		CL	Silty CLAY: Medium plasticity, dark brown	M > w _p	St	HP	120	GEOFAB - ALLUVIAL
							Hole Terminated at 1.50 m					
				2.0								
				2.5								
				3.0								
				3.5								

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25	D	Dry
Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50	M	Moist
Water Inflow		E Environmental sample		F	Firm	50 - 100	W	Wet
Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200	W _p	Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400	W _L	Liquid Limit
Gradational or transitional strata		Field Tests		H	Hard	>400		
Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable			
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density	V	Very Loose	Density Index <15%	
		HP Hand Penetrometer test (UCS kPa)			L	Loose	Density Index 15 - 35%	
					MD	Medium Dense	Density Index 35 - 65%	
					D	Dense	Density Index 65 - 85%	
					VD	Very Dense	Density Index 85 - 100%	



ENGINEERING LOG - TEST PIT

CLIENT: Health Infrastructure
PROJECT NAME: Proposed Macksville Hospital
SITE LOCATION:
TEST LOCATION: Refer to Figure 1

TEST PIT NO: **TP5**
PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: DR
DATE: 5/4/18

EQUIPMENT TYPE: 12T Excavator
TEST PIT LENGTH: 3.0 m WIDTH: 0.5 m EASTING:
NORTHING: SURFACE RL: AHD
DATUM:

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
EXCAVATOR				0.5		CL	Clayey GRAVEL: Fine to medium grained, orange/brown, Phyllite Gravel	M	MD			GENERAL FILL
				0.50m		GP	GRAVEL/COBBLES: Coarse grained, some cobbles and fines		D			GEOFAB - DRAINAGE LAYER ROCK FILL
				1.0		CL	Silty CLAY: Medium plasticity, dark brown	M > w _p	F / St	HP	100	GEOFAB - ALLUVIAL
				1.40m			Hole Terminated at 1.40 m					
				1.5								
				2.0								
				2.5								
				3.0								
				3.5								

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25	D	Dry
Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50	M	Moist
Water Inflow		E Environmental sample		F	Firm	50 - 100	W	Wet
Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200	W _p	Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400	W _L	Liquid Limit
Gradational or transitional strata		Field Tests		H	Hard	>400		
Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable			
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density	V	Very Loose	Density Index <15%	
		HP Hand Penetrometer test (UCS kPa)			L	Loose	Density Index 15 - 35%	
					MD	Medium Dense	Density Index 35 - 65%	
					D	Dense	Density Index 65 - 85%	
					VD	Very Dense	Density Index 85 - 100%	



ENGINEERING LOG - TEST PIT

CLIENT: Health Infrastructure
PROJECT NAME: Proposed Macksville Hospital
SITE LOCATION:
TEST LOCATION: Refer to Figure 1

TEST PIT NO: TP6
PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: DR
DATE: 5/4/18

EQUIPMENT TYPE: 12T Excavator
TEST PIT LENGTH: 3.0 m
WIDTH: 0.5 m
EASTING:
NORTHING:
SURFACE RL:
DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
EXCAVATOR		CBR 0.40m		0.5		GP	Clayey GRAVEL: Medium grained, grey, trace fines	M	D			PAVEMENT / WEARING COARSE
						CL	Silty CLAY: Medium plasticity, orange, some medium Gravel	M < w _p	VSt			GENERAL GILL
						GP	GRAVEL/COBBLES: Some fines	M	L			GEOFAB - DRAINAGE LAYER ROCK FILL
						CL	Silty CLAY: Medium plasticity, dark brown	M > w _p	F			GEOFAB - ALLUVIAL
				1.0								
				1.5			Hole Terminated at 1.30 m					
				2.0								
				2.5								
				3.0								
				3.5								

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25	D	Dry
Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50	M	Moist
Water Inflow		E Environmental sample		F	Firm	50 - 100	W	Wet
Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200	w _p	Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400	w _L	Liquid Limit
Gradational or transitional strata		Field Tests		H	Hard	>400		
Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable			
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density	V	Very Loose	Density Index <15%	
		HP Hand Penetrometer test (UCS kPa)			L	Loose	Density Index 15 - 35%	
					MD	Medium Dense	Density Index 35 - 65%	
					D	Dense	Density Index 65 - 85%	
					VD	Very Dense	Density Index 85 - 100%	



ENGINEERING LOG - TEST PIT

CLIENT: Health Infrastructure
PROJECT NAME: Proposed Macksville Hospital
SITE LOCATION:
TEST LOCATION: Refer to Figure 1

TEST PIT NO: TP7
PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: DR
DATE: 5/4/18

EQUIPMENT TYPE: 12T Excavator
TEST PIT LENGTH: 3.0 m
WIDTH: 0.5 m
EASTING:
NORTHING:
SURFACE RL:
DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
EXCAVATOR				0.5		GM	Silty GRAVEL: Fine to medium grained, orange, trace fine Sand	M	VSt / H	HP	100	GENERAL FILL HP = 500-550kPa
				1.0		GP	GRAVEL/COBBLES: Trace fines		L			GEOFAB - DRAINAGE LAYER ROCK FILL
				1.40m		CL	Silty CLAY: Medium plasticity, dark brown, some organics	M > w _p	St			GEOFAB - ALLUVIAL
				1.5			Hole Terminated at 1.40 m					
				2.0								
				2.5								
				3.0								
				3.5								

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25	D	Dry
Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50	M	Moist
Water Inflow		E Environmental sample		F	Firm	50 - 100	W	Wet
Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200	W _p	Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400	W _L	Liquid Limit
Gradational or transitional strata		Field Tests		H	Hard	>400		
Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable			
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density	V	Very Loose	Density Index <15%	
		HP Hand Penetrometer test (UCS kPa)			L	Loose	Density Index 15 - 35%	
					MD	Medium Dense	Density Index 35 - 65%	
					D	Dense	Density Index 65 - 85%	
					VD	Very Dense	Density Index 85 - 100%	



ENGINEERING LOG - TEST PIT

CLIENT: Health Infrastructure
PROJECT NAME: Proposed Macksville Hospital
SITE LOCATION:
TEST LOCATION: Refer to Figure 1

TEST PIT NO: TP8
PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: DR
DATE: 5/4/18

EQUIPMENT TYPE: 12T Excavator
TEST PIT LENGTH: 3.0 m
WIDTH: 0.5 m
EASTING:
NORTHING:
SURFACE RL:
DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
EXCAVATOR	Not Encountered	0.10m		0.5		GM	0.10m Silty GRAVEL: Medium grained, grey, trace Sand	M	D			PAVEMENT - WEARING COARSE GENERAL FILL
		CL				Silty CLAY: Medium plasticity, orange/pale grey, some medium sized Gravel	M < w _p	VSt				
		0.50m										
				1.0								
				1.5								
				1.80m		GP	1.80m BOULDERS/COBBLES	M	L			GEOFAB - DRAINAGE LAYER ROCK FILL
				1.90m								
				2.0			Hole Terminated at 1.90 m					
				2.5								
				3.0								
				3.5								

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25	D	Dry
Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50	M	Moist
Water Inflow		E Environmental sample		F	Firm	50 - 100	W	Wet
Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200	W _p	Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400	W _L	Liquid Limit
Gradational or transitional strata		Field Tests		H	Hard	>400		
Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable			
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density	V	Very Loose	Density Index <15%	
		HP Hand Penetrometer test (UCS kPa)			L	Loose	Density Index 15 - 35%	
					MD	Medium Dense	Density Index 35 - 65%	
					D	Dense	Density Index 65 - 85%	
					VD	Very Dense	Density Index 85 - 100%	

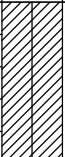
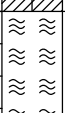


ENGINEERING LOG - TEST PIT

CLIENT: Health Infrastructure
PROJECT NAME: Proposed Macksville Hospital
SITE LOCATION:
TEST LOCATION: Refer to Figure 1

TEST PIT NO: TP9
PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: DR
DATE: 5/4/18

EQUIPMENT TYPE: 12T Excavator
TEST PIT LENGTH: 3.0 m
WIDTH: 0.5 m
EASTING:
NORTHING:
SURFACE RL:
DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
EXCAVATOR	Not Encountered			0.5		CL	Silty CLAY: Medium plasticity, brown, trace Gravel and organics	M < w _p	St	HP	200	RESIDUAL SOIL
				0.50m		CL	Silty CLAY: Medium plasticity, orange/pale grey, trace Phyllite Gravel					HP = 250-350kPa
				1.0			Extremely to Highly Weathered PHYLLITE: Foliated, brown, grey, low strength	H / Fb				EXTREMELY TO HIGHLY WEATHERED PHYLLITE
				1.40m			Hole Terminated at 1.40 m					
				1.5								
				2.0								
				2.5								
				3.0								
				3.5								

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25	D	Dry
 Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50	M	Moist
 Water Inflow		E Environmental sample		F	Firm	50 - 100	W	Wet
 Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200	W _p	Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400	W _L	Liquid Limit
 Gradational or transitional strata		Field Tests		H	Hard	>400		
 Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable			
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density	V	Very Loose	Density Index <15%	
		HP Hand Penetrometer test (UCS kPa)			L	Loose	Density Index 15 - 35%	
					MD	Medium Dense	Density Index 35 - 65%	
					D	Dense	Density Index 65 - 85%	
					VD	Very Dense	Density Index 85 - 100%	



ENGINEERING LOG - TEST PIT

CLIENT: Health Infrastructure
PROJECT NAME: Proposed Macksville Hospital
SITE LOCATION:
TEST LOCATION: Refer to Figure 1

TEST PIT NO: TP11
PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: DR
DATE: 5/4/18

EQUIPMENT TYPE: 12T Excavator
TEST PIT LENGTH: 3.0 m
WIDTH: 0.5 m
EASTING: 494581 m
NORTHING: 6604352 m
SURFACE RL:
DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
EXCAVATOR	Not Encountered			0.5		GM	Silty GRAVEL: Fine to coarse grained, trace Sand	M	D			FILL
						ML	Clayey SILT: Low plasticity, dark brown, some organics	M	S			TOPSOIL
						CL	Silty CLAY: Medium plasticity, brown, trace Gravel and relic Rock structure	M < w _p	VSt / H			RESIDUAL SOIL
							Hole Terminated at 1.20 m	M < w _p		HP	600	HP = 600kPa
				1.5								
				2.0								
				2.5								
				3.0								
				3.5								

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25	D	Dry
Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50	M	Moist
Water Inflow		E Environmental sample		F	Firm	50 - 100	W	Wet
Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200	w _p	Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400	w _L	Liquid Limit
Gradational or transitional strata		Field Tests		H	Hard	>400		
Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable			
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density	V	Very Loose	Density Index <15%	
		HP Hand Penetrometer test (UCS kPa)			L	Loose	Density Index 15 - 35%	
					MD	Medium Dense	Density Index 35 - 65%	
					D	Dense	Density Index 65 - 85%	
					VD	Very Dense	Density Index 85 - 100%	



ENGINEERING LOG - TEST PIT

CLIENT: Health Infrastructure
PROJECT NAME: Proposed Macksville Hospital
SITE LOCATION:
TEST LOCATION: Refer to Figure 1

TEST PIT NO: TP12
PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: DR
DATE: 5/4/18

EQUIPMENT TYPE: 12T Excavator
TEST PIT LENGTH: 3.0 m
WIDTH: 0.5 m
EASTING: 494543 m
NORTHING: 6604362 m
SURFACE RL:
DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
EXCAVATOR	Not Encountered			0.15m		GM	Silty GRAVEL: Fine to coarse grained, trace Sand	M	MD			FILL
						CL	Silty CLAY: Medium plasticity, red/brown, some quartz Gravel	M < w _p	VSt			RESIDUAL SOIL
				0.5								
				1.0								HP = 500-550kPa
				1.10m								
							Hole Terminated at 1.10 m					
				1.5								
				2.0								
				2.5								
				3.0								
				3.5								

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25	D	Dry
Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50	M	Moist
Water Inflow		E Environmental sample		F	Firm	50 - 100	W	Wet
Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200	W _p	Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400	W _L	Liquid Limit
Gradational or transitional strata		Field Tests		H	Hard	>400		
Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable			
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density	V	Very Loose	Density Index <15%	
		HP Hand Penetrometer test (UCS kPa)			L	Loose	Density Index 15 - 35%	
					MD	Medium Dense	Density Index 35 - 65%	
					D	Dense	Density Index 65 - 85%	
					VD	Very Dense	Density Index 85 - 100%	



ENGINEERING LOG - TEST PIT

CLIENT: Health Infrastructure
PROJECT NAME: Proposed Macksville Hospital
SITE LOCATION:
TEST LOCATION: Refer to Figure 1

TEST PIT NO: TP13
PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: DR
DATE: 5/4/18

EQUIPMENT TYPE: 12T Excavator
TEST PIT LENGTH: 3.0 m
WIDTH: 0.5 m
EASTING:
NORTHING:
SURFACE RL:
DATUM: AHD

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
EXCAVATOR	Not Encountered	0.30m				CL	Silty CLAY: Medium plasticity, orange/brown/grey, trace Gravel	M	H	HP	550	RESIDUAL SOIL
		B 0.50m		0.5								
		1.00m		1.0			Some Gravel			HP	600	EXTREMELY TO HIGHLY WEATHERED PHYLLITE
		B 1.20m		1.30m			Extremely to Highly Weathered PHYLLITE: Foliated, pale grey, low strength		Fb	HP	600	
				1.5			Hole Terminated at 1.30 m					
				2.0								
				2.5								
				3.0								
				3.5								

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water				VS	Very Soft	<25	D	Dry
Water Level		U ₅₀	50mm Diameter tube sample	S	Soft	25 - 50	M	Moist
(Date and time shown)		CBR	Bulk sample for CBR testing	F	Firm	50 - 100	W	Wet
Water Inflow		E	Environmental sample	St	Stiff	100 - 200	W _p	Plastic Limit
Water Outflow		ASS	Acid Sulfate Soil Sample	VSt	Very Stiff	200 - 400	W _L	Liquid Limit
		B	Bulk Sample	H	Hard	>400		
				Fb	Friable			
Strata Changes		Field Tests		Density			Density Index <15%	
Gradational or transitional strata		PID	Photoionisation detector reading (ppm)	L	Loose		Density Index 15 - 35%	
Definitive or distinct strata change		DCP(x-y)	Dynamic penetrometer test (test depth interval shown)	MD	Medium Dense		Density Index 35 - 65%	
		HP	Hand Penetrometer test (UCS kPa)	D	Dense		Density Index 65 - 85%	
				VD	Very Dense		Density Index 85 - 100%	

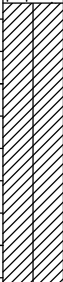


ENGINEERING LOG - TEST PIT

CLIENT: Health Infrastructure
PROJECT NAME: Proposed Macksville Hospital
SITE LOCATION:
TEST LOCATION: Refer to Figure 1

TEST PIT NO: TP14
PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: DR
DATE: 5/4/18

EQUIPMENT TYPE: 12T Excavator
TEST PIT LENGTH: 4.0 m **WIDTH:** 0.5 m
EASTING: **NORTHING:** **SURFACE RL:** AHD
DATUM:

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations	
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result		
EXCAVATOR	Not Encountered					GP	Sandy GRAVEL: Medium grained, grey, trace fines	M	D	HP	200	PAVEMENT / WEAR COARSE	
				0.25m		CL	Silty CLAY: Medium plasticity, orange/grey mottled, some medium grained size Gravel	M < w _p	VSt			GENERAL FILL	
				0.5									HP = 300-350kPa
				1.0									TOPSOIL
				1.15m		ML	Clayey SILT: Low plasticity, dark brown, some organics	M ~ w _p					
		1.50m		1.40m		CL	Silty CLAY: Medium plasticity, orange, grey, brown, trace Gravel	M < w _p	VSt			RESIDUAL SOIL	
		B 1.70m										HP = 500-600kPa	
		2.00m		2.00m			Extremely to Highly Weathered PHYLLITE: Foliated, grey/brown	M	Fb			EXTREMELY TO HIGHLY WEATHERED PHYLLITE	
		B 2.20m										HP = 550-600kPa	
							Hole Terminated at 2.30 m						
				2.5									
				3.0									
				3.5									

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25	D Dry
Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50	M Moist
Water Inflow		E Environmental sample		F	Firm	50 - 100	W Wet
Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200	W _p Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400	W _L Liquid Limit
Gradational or transitional strata		Field Tests		H	Hard	>400	
Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable		
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density	V Very Loose		Density Index <15%
		HP Hand Penetrometer test (UCS kPa)			L Loose		Density Index 15 - 35%
					MD Medium Dense		Density Index 35 - 65%
					D Dense		Density Index 65 - 85%
					VD Very Dense		Density Index 85 - 100%



ENGINEERING LOG - TEST PIT

CLIENT: Health Infrastructure
PROJECT NAME: Proposed Macksville Hospital
SITE LOCATION:
TEST LOCATION: Refer to Figure 1

TEST PIT NO: **TP15**
PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: DR
DATE: 5/4/18

EQUIPMENT TYPE: 12T Excavator
TEST PIT LENGTH: 4.0 m WIDTH: 0.5 m EASTING:
NORTHING: SURFACE RL: AHD
DATUM:

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
EXCAVATOR	Not Encountered					CL	Silty CLAY: Low plasticity, dark brown, some organics Becoming more Clayey	M	St	HP	120	ALLUVIAL
		0.50m	0.5									
		ASS	1.0									
		1.00m	1.5									
		ASS	2.0									
1.50m	2.5											
						CL	Silty CLAY: Medium plasticity, mottled brown/pale grey	M < w _p	St / VSt	HP	200	RESIDUAL SOIL

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)		Moisture Condition	
Water Water Level (Date and time shown) Water Inflow Water Outflow		U ₅₀ 50mm Diameter tube sample CBR Bulk sample for CBR testing E Environmental sample ASS Acid Sulfate Soil Sample B Bulk Sample		VS Very Soft S Soft F Firm St Stiff VSt Very Stiff H Hard Fb Friable		<25 25 - 50 50 - 100 100 - 200 200 - 400 >400		D Dry M Moist W Wet W _p Plastic Limit W _L Liquid Limit	
Strata Changes Gradational or transitional strata Definitive or distinct strata change		Field Tests PID Photoionisation detector reading (ppm) DCP(x-y) Dynamic penetrometer test (test depth interval shown) HP Hand Penetrometer test (UCS kPa)		Density V Very Loose L Loose MD Medium Dense D Dense VD Very Dense		Density Index <15% Density Index 15 - 35% Density Index 35 - 65% Density Index 65 - 85% Density Index 85 - 100%			

RG LIB 1.043.GLB Log RG NON-CORED BOREHOLE - TEST PIT RGS31237.1 PROPOSED MACKSVILLE HOSPITAL TP LOGS GPJ <<DrawingFile>> 16/04/2018 16:36 8.30.004 Datagel Lab and In Situ Tool



ENGINEERING LOG - TEST PIT

CLIENT: Health Infrastructure
PROJECT NAME: Proposed Macksville Hospital
SITE LOCATION:
TEST LOCATION: Refer to Figure 1

TEST PIT NO: TP16
PAGE: 1 of 1
JOB NO: RGS31237.1
LOGGED BY: DR
DATE: 5/4/18

EQUIPMENT TYPE: 12T Excavator
TEST PIT LENGTH: 4.0 m **WIDTH:** 0.5 m
EASTING: **NORTHING:** **SURFACE RL:** AHD
DATUM:

Drilling and Sampling					Material description and profile information					Field Test		Structure and additional observations
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity/particle characteristics, colour, minor components	MOISTURE CONDITION	CONSISTENCY DENSITY	Test Type	Result	
EXCAVATOR						ML	Clayey SILT: Low plasticity, dark brown, organics throughout	W	S			ALLUVIAL
		0.50m		0.5								
		ASS		1.0								
		1.00m		1.0								
		ASS		1.50m		CL	Silty CLAY: Medium plasticity, grey	M < w _p	VSt	HP	250	RESIDUAL SOIL
				1.5			Hole Terminated at 1.50 m					
				2.0								
				2.5								
				3.0								
				3.5								

LEGEND:		Notes, Samples and Tests		Consistency		UCS (kPa)	Moisture Condition	
Water		U ₅₀ 50mm Diameter tube sample		VS	Very Soft	<25	D	Dry
Water Level (Date and time shown)		CBR Bulk sample for CBR testing		S	Soft	25 - 50	M	Moist
Water Inflow		E Environmental sample		F	Firm	50 - 100	W	Wet
Water Outflow		ASS Acid Sulfate Soil Sample		St	Stiff	100 - 200	W _p	Plastic Limit
Strata Changes		B Bulk Sample		VSt	Very Stiff	200 - 400	W _L	Liquid Limit
--- Gradational or transitional strata		Field Tests		H	Hard	>400		
— Definitive or distinct strata change		PID Photoionisation detector reading (ppm)		Fb	Friable			
		DCP(x-y) Dynamic penetrometer test (test depth interval shown)		Density	V	Very Loose	Density Index <15%	
		HP Hand Penetrometer test (UCS kPa)			L	Loose	Density Index 15 - 35%	
					MD	Medium Dense	Density Index 35 - 65%	
					D	Dense	Density Index 65 - 85%	
					VD	Very Dense	Density Index 85 - 100%	



Appendix C

Laboratory Test Results

Client:	Regional Geotechnical Solutions	Report No. ACTS-1739
Address:	14,25-27 Hurley Drive, Coffs Harbour, NSW, 2450	Issue No. 1
Project:	RGS31237.1-Health Infrastructure	Date Sampled 11.04.18 By: Client
Location:	Proposed Macksville Hospital	Date Tested: 26.04.18 Page: 1 of 1
	Macksville	Sample No ACTS18-04-031

CALIFORNIA BEARING RATIO REPORT

Sample No.	ACTS18-04-031				
Location	TP 4 0.0 - 0.4m				

LABORATORY COMPACTION		LABORATORY REPORT			
Maximum Dry Density	t/m3	1.93			
Optimum Moisture Content	%	12.5			
Material Retained 19.0 mm sieve	%	15.8			
Compaction Specified	%	100.0			
Compaction Achieved	%	99.9			

SPECIMEN DRY DENSITY					
i At Compaction	t/m3	1.92			
ii After Soaking	t/m3	1.91			

SPECIMEN MOISTURE CONTENT					
Field / Initial	%	11.6			
i At Compaction	%	12.8			
ii After Soaking	%	17.8			
iii Top 30mm layer	%	20.1			
iv Rest of Sample	%	17.8			

CBR TEST DETAILS					
Soaking Period	days	4			
Swell	%	5.2			
Surcharge mass	kg	4.5			
CALIFORNIA BEARING RATIO	%	2.5			
Test Methods Used	F,H,I,J				

Test Methods

- A. RMS T111 Dry Density/Moisture Relations of Road Materials (Standard Compaction).
- C. RMS T120 Determination of Moisture Content of Road Materials (Standard Method).
- D. RTA T117 Determination of the California Bearing Ratio of Remoulded Specimens of Road Materials (Standard Method).
- F. AS 1289 5.1.1 Dry Density/Moisture Relationship (Standard Compaction).
- H. AS 1289 2.1.1 Determination of Moisture Content (Standard Method).
- I. AS 1289 6.1.1 Determination of the California Bearing Ratio of A Soil -Standard Method For a Remoulded Specimens .
- J. 5.0 mm result reported, NO repeat test performed.
- K. Sampled according to AS 1141.3.1



Approved Signatory: Adam Crawford

Date: 02.05.18

Client:	Regional Geotechnical Solutions	Report No. ACTS-1740
Address:	14,25-27 Hurley Drive, Coffs Harbour, NSW, 2450	Issue No. 1
Project:	RGS31237.1-Health Infrastructure	Date Sampled 11.04.18 By: Client
Location:	Proposed Macksville Hospital	Date Tested: 26.04.18 Page: 1 of 1
	Macksville	Sample No ACTS18-04-032

CALIFORNIA BEARING RATIO REPORT

Sample No.	ACTS18-04-032				
Location	TP 6 0.0 - 0.4m				

LABORATORY COMPACTION		LABORATORY REPORT			
Maximum Dry Density	t/m3	1.92			
Optimum Moisture Content	%	10.9			
Material Retained 19.0 mm sieve	%	0.0			
Compaction Specified	%	1.9			
Compaction Achieved	%	100.3			

SPECIMEN DRY DENSITY					
i At Compaction	t/m3	1.93			
ii After Soaking	t/m3	1.91			

SPECIMEN MOISTURE CONTENT					
Field / Initial	%	9.9			
i At Compaction	%	10.9			
ii After Soaking	%	16.4			
iii Top 30mm layer	%	17.0			
iv Rest of Sample	%	16.4			

CBR TEST DETAILS					
Soaking Period	days	4			
Swell	%	3.5			
Surcharge mass	kg	4.5			
CALIFORNIA BEARING RATIO	%	4.5			
Test Methods Used	F,H,I,J				

Test Methods

- A. RMS T111 Dry Density/Moisture Relations of Road Materials (Standard Compaction).
- C. RMS T120 Determination of Moisture Content of Road Materials (Standard Method).
- D. RTA T117 Determination of the California Bearing Ratio of Remoulded Specimens of Road Materials (Standard Method).
- F. AS 1289 5.1.1 Dry Density/Moisture Relationship (Standard Compaction).
- H. AS 1289 2.1.1 Determination of Moisture Content (Standard Method).
- I. AS 1289 6.1.1 Determination of the California Bearing Ratio of A Soil -Standard Method For a Remoulded Specimens .
- J. 5.0 mm result reported, NO repeat test performed.
- K. Sampled according to AS 1141.3.1



Approved Signatory: Adam Crawford

Date: 02.05.18



AC TESTING SERVICES

AC Testing Services:Accreditation No.19604

2/1 Monro St, Nambucca Heads, NSW 2448

ABN: 38578525858

Ph:0438857377

Client:	Regional Geotechnical Solutions	Report No. ACTS-1741
Address:	14,25-27 Hurley Drive, Coffs Harbour, NSW, 2450	Issue No. 1
Project:	RGS31237.1-Health Infrastructure	Date Sampled 11.04.18 By: Client
Location:	Proposed Macksville Hospital	Date Tested: 26.04.18 Page: 1 of 1
	Macksville	Sample No ACTS18-04-033

CALIFORNIA BEARING RATIO REPORT

Sample No.	ACTS18-04-033				
Location	TP 8 0.1 - 0.4m				

LABORATORY COMPACTION

LABORATORY REPORT

Maximum Dry Density	t/m3	1.89			
Optimum Moisture Content	%	13.8			
Material Retained 19.0 mm sieve	%	0.7			
Compaction Specified	%	100.0			
Compaction Achieved	%	99.2			

SPECIMEN DRY DENSITY

i At Compaction	t/m3	1.88			
ii After Soaking	t/m3	1.88			

SPECIMEN MOISTURE CONTENT

Field / Initial	%	15.4			
i At Compaction	%	13.2			
ii After Soaking	%	19.2			
iii Top 30mm layer	%	16.5			
iv Rest of Sample	%	19.2			

CBR TEST DETAILS

Soaking Period	days	4			
Swell	%	3.2			
Surcharge mass	kg	4.5			

CALIFORNIA BEARING RATIO	%	5.5			
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Test Methods Used	F,H,I,J				
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Test Methods

- A. RMS T111 Dry Density/Moisture Relations of Road Materials (Standard Compaction).
 C. RMS T120 Determination of Moisture Content of Road Materials (Standard Method).
 D. RTA T117 Determination of the California Bearing Ratio of Remoulded Specimens of Road Materials (Standard Method).
 F. AS 1289 5.1.1 Dry Density/Moisture Relationship (Standard Compaction).
 H. AS 1289 2.1.1 Determination of Moisture Content (Standard Method).
 I. AS 1289 6.1.1 Determination of the California Bearing Ratio of A Soil -Standard Method For a Remoulded Specimens .
 J. 5.0 mm result reported, NO repeat test performed.
 K. Sampled according to AS 1141.3.1



Approved Signatory: Adam Crawford

Date: 02.05.18

Accredited for compliance with ISO/IEC 17025-Testing.

Report Form No.3

**AC TESTING SERVICES**

AC Testing Services:Accreditation No.19604

2/1 Monro St, Nambucca Heads, NSW 2448

ABN: 38578525858

Ph:0438857377

Client:	Regional Geotechnical Solutions	Report No. ACTS-1742
Address:	14,25-27 Hurley Drive, Coffs Harbour, NSW, 2450	Issue No. 1
Project:	RGS31237.1-Health Infrastructure	Date Sampled 11.04.18 By: Client
Location:	Proposed Macksville Hospital	Date Tested: 26.04.18 Page: 1 of 2
	Macksville	Sample No ACTS18-04-034

CALIFORNIA BEARING RATIO REPORT

Sample No.	ACTS18-04-034				
Location	TP 13 0.3 - 0.5m				

LABORATORY COMPACTION**LABORATORY REPORT**

Maximum Dry Density	t/m3	1.65			
Optimum Moisture Content	%	19.8			
Material Retained 19.0 mm sieve	%	0.0			
Compaction Specified	%	100.0			
Compaction Achieved	%	101.0			

SPECIMEN DRY DENSITY

i At Compaction	t/m3	1.66			
ii After Soaking	t/m3	1.67			

SPECIMEN MOISTURE CONTENT

Field / Initial	%	22.9			
i At Compaction	%	19.5			
ii After Soaking	%	26.1			
iii Top 30mm layer	%	28.5			
iv Rest of Sample	%	26.1			

CBR TEST DETAILS

Soaking Period	days	4			
Swell	%	3.9			
Surcharge mass	kg	4.5			

CALIFORNIA BEARING RATIO	%	3.5			
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Test Methods Used	F,H,I,J				
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Test Methods

- A. RMS T111 Dry Density/Moisture Relations of Road Materials (Standard Compaction).
C. RMS T120 Determination of Moisture Content of Road Materials (Standard Method).
D. RTA T117 Determination of the California Bearing Ratio of Remoulded Specimens of Road Materials (Standard Method).
F. AS 1289 5.1.1 Dry Density/Moisture Relationship (Standard Compaction).
H. AS 1289 2.1.1 Determination of Moisture Content (Standard Method).
I. AS 1289 6.1.1 Determination of the California Bearing Ratio of A Soil -Standard Method For a Remoulded Specimens .
J. 5.0 mm result reported, NO repeat test performed.
K. Sampled according to AS 1141.3.1

**Approved Signatory: Adam Crawford**

Date: 02.05.18

Accredited for compliance with ISO/IEC 17025-Testing.

Report Form No.3



Client:	Regional Geotechnical Solutions	Report No.	ACTS-1742		
Address:	14/25-27 Hurley Drive	Issue No.	1		
	Coffs Harbour, NSW, 2450	Date Sampled:	11.04.18	By:	Client
Project:	RGS31237.1-RGS31237.1 - Health Infrastructure	Date Tested:	27.04.18	Page: 2	of 2
	Proposed Macksville Hospital	Sample No:	ACTS18-04-034		
Location:	Macksville				

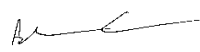
**SOIL REACTIVITY REPORT
SHRINK-SWELL INDEX
AS 1289 7.1.1**

Sample No.		ACTS18-04-034			
Location		Macksville			
Test Pit No.		TP 13			
Test Depth (m)		0.3 - 0.5			
U50 Recovery (m)		0.3 - 0.5			
Shrink-Swell Index I _{ss} (%)		1.3			
Moisture Content of Shrink Specimen (%)		26.9			
Moisture Content of Swell Specimen Field (%)		21.6			
After test (%)		28.6			
Extent of Crumbling during Shrink test		0			
Extent of Cracking of the Shrink specimen		Minor			
Significant Inert Inclusions in the Soil Sample (Estimated %)		0			



Accredited for compliance with ISO/IEC 17025 - Testing.

Approved Signatory:


Adam Crawford

Date:

02.05.18

Client:	Regional Geotechnical Solutions	Report No. ACTS-1743
Address:	14,25-27 Hurley Drive, Coffs Harbour, NSW, 2450	Issue No. 1
Project:	RGS31237.1-Health Infrastructure	Date Sampled 11.04.18 By: Client
Location:	Proposed Macksville Hospital	Date Tested: 26.04.18 Page: 1 of 2
	Macksville	Sample No ACTS18-04-035

CALIFORNIA BEARING RATIO REPORT

Sample No.	ACTS18-04-035				
Location	TP 13 1.0 - 1.2m				

LABORATORY COMPACTION		LABORATORY REPORT			
Maximum Dry Density	t/m3	1.81			
Optimum Moisture Content	%	14.1			
Material Retained 19.0 mm sieve	%	0.0			
Compaction Specified	%	100.0			
Compaction Achieved	%	99.2			

SPECIMEN DRY DENSITY					
i At Compaction	t/m3	1.81			
ii After Soaking	t/m3	1.78			

SPECIMEN MOISTURE CONTENT					
Field / Initial	%	15.6			
i At Compaction	%	13.7			
ii After Soaking	%	19.7			
iii Top 30mm layer	%	22.6			
iv Rest of Sample	%	19.7			

CBR TEST DETAILS					
Soaking Period	days	4			
Swell	%	2.7			
Surcharge mass	kg	4.5			
CALIFORNIA BEARING RATIO	%	3.5			
Test Methods Used		F,H,I,J			

Test Methods

- A. RMS T111 Dry Density/Moisture Relations of Road Materials (Standard Compaction).
- C. RMS T120 Determination of Moisture Content of Road Materials (Standard Method).
- D. RTA T117 Determination of the California Bearing Ratio of Remoulded Specimens of Road Materials (Standard Method).
- F. AS 1289 5.1.1 Dry Density/Moisture Relationship (Standard Compaction).
- H. AS 1289 2.1.1 Determination of Moisture Content (Standard Method).
- I. AS 1289 6.1.1 Determination of the California Bearing Ratio of A Soil -Standard Method For a Remoulded Specimens .
- J. 5.0 mm result reported, NO repeat test performed.
- K. Sampled according to AS 1141.3.1



Approved Signatory: Adam Crawford

Date: 02.05.18



Client:	Regional Geotechnical Solutions	Report No.	ACTS-1743
Address:	14/25-27 Hurley Drive	Issue No.	1
	Coffs Harbour, NSW, 2450	Date Sampled:	11.04.18 By: Client
Project:	RGS31237.1-RGS31237.1 - Health Infrastructure	Date Tested:	27.04.18 Page: 2 of 2
	Proposed Macksville Hospital	Sample No:	ACTS18-04-035
Location:	Macksville		

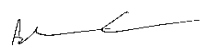
**SOIL REACTIVITY REPORT
SHRINK-SWELL INDEX
AS 1289 7.1.1**

Sample No.	ACTS18-04-035			
Location	Macksville			
Test Pit No.	TP 13			
Test Depth (m)	1.0 - 1.2			
U50 Recovery (m)	1.0 - 1.2			
Shrink-Swell Index I _{ss} (%)	1.4			
Moisture Content of Shrink Specimen (%)	15.7			
Moisture Content of Swell Specimen Field (%)	16.5			
After test (%)	20.8			
Extent of Crumbling during Shrink test	0			
Extent of Cracking of the Shrink specimen	Nil			
Significant Inert Inclusions in the Soil Sample (Estimated %)	0			



Accredited for compliance with ISO/IEC 17025 - Testing.

Approved Signatory:


Adam Crawford

Date:

02.05.18



AC TESTING SERVICES

AC Testing Services:Accreditation No.19604

2/1 Monro St, Nambucca Heads, NSW 2448

ABN: 38578525858

Ph:0438857377

Client:	Regional Geotechnical Solutions	Report No. ACTS-1744
Address:	14,25-27 Hurley Drive, Coffs Harbour, NSW, 2450	Issue No. 1
Project:	RGS31237.1-Health Infrastructure	Date Sampled 11.04.18 By: Client
Location:	Proposed Macksville Hospital	Date Tested: 26.04.18 Page: 1 of 3
	Macksville	Sample No ACTS18-04-036

CALIFORNIA BEARING RATIO REPORT

Sample No.	ACTS18-04-036				
Location	TP 14 2.0 - 2.2m				

LABORATORY COMPACTION

LABORATORY REPORT

Maximum Dry Density	t/m3	1.77			
Optimum Moisture Content	%	16.0			
Material Retained 19.0 mm sieve	%	0.0			
Compaction Specified	%	100.0			
Compaction Achieved	%	98.5			

SPECIMEN DRY DENSITY

i At Compaction	t/m3	1.74			
ii After Soaking	t/m3	1.74			

SPECIMEN MOISTURE CONTENT

Field / Initial	%	17.5			
i At Compaction	%	17.0			
ii After Soaking	%	20.7			
iii Top 30mm layer	%	21.9			
iv Rest of Sample	%	20.7			

CBR TEST DETAILS

Soaking Period	days	4			
Swell	%	2.3			
Surcharge mass	kg	4.5			

CALIFORNIA BEARING RATIO	%	6.5			
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Test Methods Used	F,H,I,J				
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Test Methods

- A. RMS T111 Dry Density/Moisture Relations of Road Materials (Standard Compaction).
 C. RMS T120 Determination of Moisture Content of Road Materials (Standard Method).
 D. RTA T117 Determination of the California Bearing Ratio of Remoulded Specimens of Road Materials (Standard Method).
 F. AS 1289 5.1.1 Dry Density/Moisture Relationship (Standard Compaction).
 H. AS 1289 2.1.1 Determination of Moisture Content (Standard Method).
 I. AS 1289 6.1.1 Determination of the California Bearing Ratio of A Soil -Standard Method For a Remoulded Specimens .
 J. 5.0 mm result reported, NO repeat test performed.
 K. Sampled according to AS 1141.3.1



Approved Signatory: Adam Crawford

Date: 02.05.18

Accredited for compliance with ISO/IEC 17025-Testing.

Report Form No.3



Client:	Regional Geotechnical Solutions	Report No.	ACTS-1744
Address:	14/25-27 Hurley Drive	Issue No.	1
	Coffs Harbour, NSW, 2450	Date Sampled:	11.04.18 By: Client
Project:	RGS31237.1-RGS31237.1 - Health Infrastructure	Date Tested:	27.04.18 Page: 2 of 3
	Proposed Macksville Hospital	Sample No:	ACTS18-04-036
Location:	Macksville		

SOIL REACTIVITY REPORT
SHRINK-SWELL INDEX
AS 1289 7.1.1

Sample No.	ACTS18-04-036			
Location	Macksville			
Test Pit No.	TP 14			
Test Depth (m)	2.0 - 2.2			
U50 Recovery (m)	2.0 - 2.2			
Shrink-Swell Index I _{ss} (%)	1.9			
Moisture Content of Shrink Specimen (%)	27.0			
Moisture Content of Swell Specimen Field (%)	28.0			
After test (%)	29.7			
Extent of Crumbling during Shrink test	0			
Extent of Cracking of the Shrink specimen	Minor			
Significant Inert Inclusions in the Soil Sample (Estimated %)	0			



Accredited for compliance with ISO/IEC 17025 - Testing.

Approved Signatory:

Adam Crawford

Date:

02.05.18



Client: Regional Geotechnical Solutions Report No. ACTS-1744
Address: 14/25-27 Hurley Drive. Issue No. 1
Coffs Harbour, NSW,2450 Date Sampled: 11.04.18 By: Client
RGS31237.1-Health Infrastructure Sample No: ACTS18-04-036 Page: 3 of 3
Proposed Macksville Hospital
Location: Macksville

ATTERBERG LIMITS REPORT

Test Methods: AS1289.3.1.1, 3.2.1, 3.3.1

Location: TP 14, 2.0 - 2.2m

Date Tested: 24.04.18

Sample No.	ACTS18-04-036
I.D.	TP 14, 2.0 - 2.2m
Liquid Limit(AS1289.3.1.1) - %	43
Plastic Limit(AS1289.3.2.1) -%	28
Plasitcity Index(AS1289.3.3.1) - %	15
Linear Shrinkage(AS1289.3.4.1) -%	-
Crumbling &/or Curling	-
Sample History	Oven Dried
Sample Preparation	Dry Sieved

Approved Signatory:

Name: Adam Crawford

Date of Issue

02.05.18



Accredited for compliance with ISO/IEC
17025-Testing.

Report Form No. 14



Client: Regional Geotechnical Solutions Report No. ACTS-1745
Address: 14/25-27 Hurley Drive. Issue No. 1
Coffs Harbour, NSW,2450 Date Sampled: 11.04.18 By: Client
RGS31237.1-Health Infrastructure Sample No: ACTS18-04-037 Page: 1 of 1
Proposed Macksville Hospital
Location: Macksville

ATTERBERG LIMITS REPORT

Test Methods: AS1289.3.1.1, 3.2.1, 3.3.1

Location: BH 8, 5.0 - 5.45m

Date Tested: 24.04.18

Sample No.	ACTS18-04-037
I.D.	BH 8, 5.0 - 5.45m
Liquid Limit(AS1289.3.1.1) - %	32
Plastic Limit(AS1289.3.2.1) -%	23
Plasticity Index(AS1289.3.3.1) - %	9
Linear Shrinkage(AS1289.3.4.1) -%	-
Crumbling &/or Curling	-
Sample History	Oven Dried
Sample Preparation	Dry Sieved

Approved Signatory:

Name: Adam Crawford

Date of Issue

02.05.18



Accredited for compliance with ISO/IEC
17025-Testing.

Report Form No. 14



Client: Regional Geotechnical Solutions Report No. ACTS-1746
Address: 14/25-27 Hurley Drive. Issue No. 1
Coffs Harbour, NSW,2450 Date Sampled: 11.04.18 By: Client
RGS31237.1-Health Infrastructure Sample No: ACTS18-04-038 Page: 1 of 1
Proposed Macksville Hospital
Location: Macksville

ATTERBERG LIMITS REPORT

Test Methods: AS1289.3.1.1, 3.2.1, 3.3.1

Location: BH 10, 1.5 - 1.6m

Date Tested: 24.04.18

Sample No.	ACTS18-04-038
I.D.	BH 10, 1.5 - 1.6m
Liquid Limit(AS1289.3.1.1) - %	54
Plastic Limit(AS1289.3.2.1) -%	31
Plasticity Index(AS1289.3.3.1) - %	23
Linear Shrinkage(AS1289.3.4.1) -%	-
Crumbling &/or Curling	-
Sample History	Oven Dried
Sample Preparation	Dry Sieved

Approved Signatory:

Name: Adam Crawford

Date of Issue

02.05.18





Client: Regional Geotechnical Solutions Report No. ACTS-1747
Address: 14/25-27 Hurley Drive. Issue No. 1
Coffs Harbour, NSW,2450 Date Sampled: 11.04.18 By: Client
RGS31237.1-Health Infrastructure Sample No: ACTS18-04-039 Page: 1 of 1
Proposed Macksville Hospital
Location: Macksville

ATTERBERG LIMITS REPORT

Test Methods: AS1289.3.1.1, 3.2.1, 3.3.1

Location: BH 10, 2.4 - 2.5m

Date Tested: 24.04.18

Sample No.	ACTS18-04-039
I.D.	BH 10, 2.4 - 2.5m
Liquid Limit(AS1289.3.1.1) - %	44
Plastic Limit(AS1289.3.2.1) -%	25
Plasitcity Index(AS1289.3.3.1) - %	19
Linear Shrinkage(AS1289.3.4.1) -%	-
Crumbling &/or Curling	-
Sample History	Oven Dried
Sample Preparation	Dry Sieved

Approved Signatory:

Name: Adam Crawford

Date of Issue

02.05.18



Biotrack Certificate of Analysis

Signatory:



Ph: +617 3289 7179 ABN 91 056 237 275

Test Code/Name	[1] FIELD SCREEN SUITE		
Lab Reference (LR)	170418.711	Client Name	Regional Geotechnical Solutions Pty Ltd (Wingham)
SampleID	All Samples	Client Contact	Matt Rowbotham
		Project Name	Proposed Machsville Hospital
Report Date	20/04/2018	Job Number	RGS31237.1
Sample Received Date	17/04/2018	Order Number	
Sample Disposal Date	16/06/2018	Chain of Custody	
Sample Packaging	Plastic Bag	Client Email	matt.r@regionalgeotech.com.au
Temperature	Ambient	Client Address	44 Bent Street Wingham New South Wales 2429

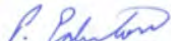
Analytical Method: Test Methodology for pH_f and pH_{fox} as per QASSIT 2004 Laboratory Methods. Indications based on pH data only.

RATE: 0 = No Reaction 2=Moderate 3=High 4=Very High (steam evolved).

TEMP: Surface temperature rise (°C) oxidised sample at 5 minutes - cooling may occur for fast reaction.

S#	SampleID	pH _f	pH _{Fox}	Change	RATE	TEMP	Indication
1	BH8 5-5.45	4.5	3.3	-1.2	0	3	low TAA & moderate TPA
2	BH8 6.5-6.9	4.8	3.0	-1.8	2	7	low TAA & moderate TPA
3	BH9 5.5-5.95	4.3	1.9	-2.4	4	7	high TPA & sulphide possible
4	BH10 0.6-0.7	5.6	3.5	-2.1	4	0	low TAA & sulphide possible
5	BH10 0.9-1	5.4	3.6	-1.8	4	3	low TAA
6	BH10 1-1.45	5.3	3.5	-1.8	1	2	low TAA
7	BH10 2.5-2.95	4.8	2.7	-2.1	1	4	low TAA & moderate TPA & sulphide possible
8	BH10 4-4.45	4.8	2.9	-1.9	4	8	low TAA & moderate TPA
9	BH11 1-1.45	5.3	3.3	-2.0	1	3	low TAA & moderate TPA
10	BH12 0.4-0.5	5.0	3.0	-2.0	3	7	low TAA & moderate TPA
11	BH12 0.9-1	5.1	3.1	-2.0	3	5	low TAA & moderate TPA
12	TP15 0.4-0.5	5.5	4.0	-1.5	4	6	low TAA
13	TP15 1-1.1	5.4	4.1	-1.3	4	1	low TAA
14	TP15 1.4-1.5	4.9	3.6	-1.3	1	2	low TAA
15	TP16 0.4-0.5	4.9	3.2	-1.7	1	4	low TAA & moderate TPA
16	TP16 0.9-1	4.8	3.6	-1.2	1	0	low TAA
17	TP16 1.4-1.5	4.8	3.5	-1.3	1	4	low TAA

Biotrack Certificate of Analysis

Signatory:  Ph: +617 3289 7179 ABN 91 056 237 275

Test Code/Name	[1] FIELD SCREEN SUITE		
Lab Reference (LR)	170418.711	Client Name	Regional Geotechnical Solutions Pty Ltd (Wingham)
SampleID	All Samples	Client Contact	Matt Rowbotham
		Project Name	Proposed Machsville Hospital
Report Date	20/04/2018	Job Number	RG531237.1
Sample Received Date	17/04/2018	Order Number	
Sample Disposal Date	16/06/2018	Chain of Custody	
Sample Packaging	Plastic Bag	Client Email	matt.r@regionalgeotech.com.au
Temperature	Ambient	Client Address	44 Bent Street Wingham New South Wales 2429

Analytical Method: Test Methodology for pH_f and pH_{fox} as per QASSIT 2004 Laboratory Methods. Indications based on pH data only.

RATE: 0 = No Reaction 2=Moderate 3=High 4=Very High (steam evolved).

TEMP: Surface temperature rise (°C) oxidised sample at 5 minutes - cooling may occur for fast reaction.

S#	SampleID	pH _f	pH _{Fox}	Change	Rate	Indication
1	BH8 5-5.45	4.5	3.3	-1.2	0	low TAA & moderate TPA
2	BH8 6.5-6.9	4.8	3.0	-1.8	2	low TAA & moderate TPA
3	BH9 5.5-5.95	4.3	1.9	-2.4	4	high TPA & sulphide possible
4	BH10 0.6-0.7	5.6	3.5	-2.1	4	low TAA & sulphide possible
5	BH10 0.9-1	5.4	3.6	-1.8	4	low TAA
6	BH10 1-1.45	5.3	3.5	-1.8	1	low TAA
7	BH10 2.5-2.95	4.8	2.7	-2.1	1	low TAA & moderate TPA & sulphide possible
8	BH10 4-4.45	4.8	2.9	-1.9	4	low TAA & moderate TPA
9	BH11 1-1.45	5.3	3.3	-2.0	1	low TAA & moderate TPA
10	BH12 0.4-0.5	5.0	3.0	-2.0	3	low TAA & moderate TPA
11	BH12 0.9-1	5.1	3.1	-2.0	3	low TAA & moderate TPA
12	TP15 0.4-0.5	5.5	4.0	-1.5	4	low TAA
13	TP15 1-1.1	5.4	4.1	-1.3	4	low TAA
14	TP15 1.4-1.5	4.9	3.6	-1.3	1	low TAA
15	TP16 0.4-0.5	4.9	3.2	-1.7	1	low TAA & moderate TPA
16	TP16 0.9-1	4.8	3.6	-1.2	1	low TAA
17	TP16 1.4-1.5	4.8	3.5	-1.3	1	low TAA

DETERMINATION OF ACID SULFATE SOIL PROPERTIES

CERTIFICATE OF ANALYSIS



Analysis By: **Bio-Track Pty Ltd** ABN 91 056 237 275

781 Mt. Glorious Road Highvale, Brisbane, Australia, 4520 Ph. 07 3289 7179

LAB REFERENCE LR170418.712 DATE OF REPORT 20 APRIL 2018 @08:36:16 Page 1 of 1 Report Pages.
 CLIENT NAME Matt Rowbotham c/o Regional Geotechnical Solutions Pty Ltd (Wingham) 44 Bent Street Wingham 2429
 PROJECT NAME Proposed Machsville Hospital YOUR PROJECT/JOB REFERENCE RGS31237.1
 SAMPLING DATE NUMBER OF SAMPLES 7 Samples supplied by client SAMPLE TYPE: Soil/Solid
 DATE RECEIVED 17/04/2018 4:47:07 PM PACKAGING Plastic Bag Ground Oven Dry Samples DISPOSED ON 16/06/2018

Sample ID as received. METHODOLOGY: As per (DNR QASSIT May 2004), oven dried (85°C), >1000 um shell removed, fine grind. All reported values gravimetric, dry mass.
 %sEQ (equivalent sulphur) calculated as moles TAA/624 + %S Cr + %sNAS - sANC BT (sNAS included irrespective of pH).

LIME1 rates calculated to neutralise TPA (or TAA if >TPA) + aS_RAS -ANC_BT/1.5 LIME2 rates calculated to neutralise TAA + aS_POS or S_Cr + aS_RAS -ANC_BT/ 1.5

NB. Lime rates assume 97% lime neutralisation but DO NOT include any safety factors. Suggested factor=1.5-2. Rates are kg/ton. Multiply by bulk density to convert to kg/m³.

Fineness Factor (FF)=1.5 CBN POS= moles carbonate alkalinity released by oxidation assuming (Ca POS - Ca KCl) + (Mg POS - Mg KCl) is due to carbonate solution.

Blanks represent unmeasured values, zeros & <0.x represent measured values. If pH KCl>4.5 then s-RAS (calculated from acid extract) may be zero for undisturbed soil. Ca NAS is the acid reactive calcium calculated as the difference between 1 M KCl and 4 M HCl soluble Ca.

ID.	DEPTH	pH	pH	TAA	TPA	TSA	S KCl	S P	S POS	S Cr	s-NAS	s EQ	Ca KCl	Ca P	Mg KCl	Mg P	CBN POS	LIME1	LIME2	sANC_BT	Ca NAS
	None	KCL	ox	m/t	m/t	m/t	%	%	%	%	%	%	mg/kg	mg/kg	mg/kg	mg/kg	m/t	kg/t	kg/t	%	mg/kg
Analytical	Method Codes	23A	23B	23F	23G	23H	23Ce	23De	23Ee	22B	s20Je	s	23Vh	23Wh	23Sm	23Tm	a23U&X			s19A2	20E
BH8	6.5-6.9	3.88		56			0.04			0.12	<0.01	0.215	442		285				7		<10
BH9	5.5-5.95	4.26		38			0.04			0.82	0.01	0.892	332		256				28		348
BH10	1-1.45	4.25		79			<0.01			0.15	<0.01	0.281	280		719				9		<10
BH11	1-1.45	4.38		94			<0.01			0.29	<0.01	0.445	264		599				14		<10
BH12	0.4-0.5	4.36		80			<0.01			0.08	<0.01	0.217	440		372				7		<10
TP15	1-1.1	4.61		58			<0.01			0.02	<0.01	0.124	220		204				4		24
TP16	0.9-1	4.77		97			0.02			0.15	0.04	0.340	179		227				11		<10

Signatory

For and on behalf of Bio-Track Pty Ltd

CERTIFICATE OF ANALYSIS



Analysis By: Bio-Track Pty Ltd
ABN 91 056 237 275
Mt. Glorious Road
Highvale, Brisbane, Australia, 4520
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DATE OF REPORT 26 APRIL 2018 Page 1 of 1 Report Pages.
CLIENT NAME Matt Rowbotham c/o Regional Geotechnical Solutions Pty Ltd (Wingham)
CLIENT ADDRESS 44 Bent Street Wingham 2429
PROJECT NAME Proposed Machsville Hospital YOUR PROJECT/JOB REFERENCE RGS31237.1
SAMPLING DATE NUMBER OF SAMPLES 3 SAMPLE TYPE: Soil/Solid
PACKAGING Plastic Bag ** SAMPLES DISPOSED ON 16/06/2018
DATE RECEIVED 17/04/2018 4:47:07 PM LAB REF. LR170418.713

METHODOLOGY: EC Cl as 1:5, pH 1:2.5; air dried soil in water, 30 minute rolling shake, Cl by ion selective electrode. S as 1:40 IN KCl extract measured by ICP OES.
RESIS: soil resistivity per AS1289.4.4.1 SO4 calculated as S x 3 SO3 calculated as S x 2.5

SAMPLE ID	EC	pH	Cl	S	SO4	SO3	RESIS
None depth	dS/m		mg/kg	mg/kg	%	%	ohm-cm
BH4 2.5-2.95	0.04	5.1	38	26	<0.1	<0.1	6900
BH8 6.5-6.9	0.42	3.8	70	377	0.1	<0.1	920
BH10 1-1.45	0.19	4.9	175	88	<0.1	<0.1	1700

Signatory

For and behalf of Bio-Track Pty Ltd

CERTIFICATE OF ANALYSIS



Analysis By: Bio-Track Pty Ltd
ABN 91 056 237 275
Mt. Glorious Road
Highvale, Brisbane, Australia, 4520
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DATE OF REPORT 26 APRIL 2018 Page 1 of 1 Report Pages.
CLIENT NAME Matt Rowbotham c/o Regional Geotechnical Solutions Pty Ltd (Wingham)
CLIENT ADDRESS 44 Bent Street Wingham 2429
PROJECT NAME Proposed Machsville Hospital YOUR PROJECT/JOB REFERENCE RGS31237.1
SAMPLING DATE NUMBER OF SAMPLES 1 SAMPLE TYPE: Soil/Solid
PACKAGING Plastic Bag ** SAMPLES DISPOSED ON 19/06/2018
DATE RECEIVED 20/04/2018 12:41:07 PM LAB REF. LR200418.529

METHODOLOGY: EC Cl as 1:5, pH 1:2.5; air dried soil in water, 30 minute rolling shake, Cl by ion selective electrode. S as 1:40 IN KCl extract measured by ICP OES.
RESIS: soil resistivity per AS1289.4.4.1 SO4 calculated as S x 3 SO3 calculated as S x 2.5

SAMPLE ID	EC	pH	Cl	S	SO4	SO3	RESIS
None depth	dS/m		mg/kg	mg/kg	%	%	ohm-cm
BH12 1.3-1.45	0.21	5.2	215	116	<0.1	<0.1	2100

Signatory

A handwritten signature in blue ink, appearing to read 'P. Edwards'.

For and behalf of Bio-Track Pty Ltd



Appendix D

Pavement Design Sheet

FLEXIBLE PAVEMENT THICKNESS DESIGN

CLIENT: NSW Health
PROJECT: Proposed New Macksville Hospital
LOCATION: North Macksville

Job No.: RGS31237.1

Date: 16-Apr-18



ROAD NAME:	Access Road off Letitia Close		Refer to drawing:	
Chainage Interval (m):	0m to 800m		Road classification ref:	N/A
Road Classification:	N/A		Design Traffic:	8.0x 10 ⁵ ESAs
Subgrade Conditions				
Expected subgrade:	Gravelly Silty Clay			
Adopted Subgrade CBR value:	3.5	Required subgrade compaction:	100% Standard Compaction	
Potential construction or performance issues:	Proof roll to identify any areas showing evidence of deflection. Where identified, remove and replace with approved granular fill.			
Pavement Design				
Recommended Pavement Layer Thickness:		Recommended Material requirements	Required Compaction	
Wearing course thickness (mm):		14/7 two coat seal or to Council requirements. 30mm AC recommended in areas of high screwing loads.		
Base thickness (mm):	140	DGB20 or equivalent	98% Modified Compaction	
Sub-base thickness (mm):	320	Existing pavement gravel or imported DGS40.	97% Modified Compaction	
Select thickness (mm):	0	Existing pavement gravel CBR>13, PI<15, or DGS40	100% Standard Compaction	
Total thickness (mm):	460			
Definitions:				
Design traffic loading:	The anticipated number of equivalent standard axles (ESA), as defined by AUSTROADS, in the design lane during the design life of the pavement.			
Modified Compaction:	Minimum required dry density ratio (AS1289 5.4.1-2007) defined as the ratio of the calculated field dry density (AS1289 5.3.1-2004 or equivalent) to the maximum dry density obtained using AS1289 5.2.1-2003 or equivalent.			
Standard Compaction:	Minimum required dry density ratio (AS1289 5.4.1-2007) defined as the ratio of the calculated field dry density (AS1289 5.3.1-2004 or equivalent) to the maximum dry density obtained using AS1289 5.1.1-2003 or equivalent.			
Density Index:	Minimum required Density Index AS1289 5.6.1-1998, defined as the ratio of field dry density determined by AS1289 5.3.1-2004 or equivalent to the laboratory values of maximum and minimum density obtained by AS1289 5.5.1-1998 or equivalent			
Note:	Pavement designs assume appropriate drainage is installed and maintained. Refer to Regional Geotechnical Solutions Report No. RGS31237.1-AH for recommendations regarding pavement construction and drainage.			



Appendix E

Acid Sulfate Soil Management Plan



INTRODUCTION

This Acid Sulfate Soil Management Plan (ASSMP) has been prepared for the proposed Macksville Hospital Development and should be read in conjunction with the Geotechnical Report prepared for the project by Regional Geotechnical Solutions (Pty Ltd) (RGS) (Ref: RGS31237.1 – AH dated 2 May 2018).

In summary, the report indicates the soils encountered along the alluvial floodplain are potential acid sulfate soils (PASS). Therefore, where these soils will be disturbed as part of the development they should be treated and this ASSMP implemented.

This ASSMP has been prepared for the development and outlines the measures that must be implemented on site during excavation works to control, treat and manage ASS.

It is noted that validation testing of the treated ASS will be required and testing generally takes about 10 working days, therefore this should be allowed in the earthworks management plan to reduce the potential for delays during construction.

RESPONSIBILITIES

The project superintendent is responsible for implementing the ASS management protocols detailed within this ASSMP. Only a suitably experienced ASS consultant may vary the procedures detailed herein.

The superintendent shall:

- Record a daily log showing the volume of material that has been excavated, and treated;
- Ensure that validation testing is undertaken by an independent monitoring consultant on a regular basis.

The requirements of the ASSMP are in addition to, but do not override any other standard procedures such as safety considerations. Where conflict results, or may result from, the implementation of the ASS management as against other performance criteria, the project superintendent shall obtain directives from the project manager or the ASS consultant as appropriate.



NEUTRALISING MATERIALS

Fine Agricultural Lime (aglime) must be used for liming of excavated materials. Hydrated lime, Dolomatic aglime, or magnesium blend aglime, should not be used. The aglime grind shall have:

- At least 85% by weight passing 1mm, and 100% passing 2.5mm. In general a finer grind is better; and
- Aglime shall have a Neutralising Value (NV) of 90% or better (i.e. $NV > 90$).

MANAGEMENT AND PROCESSING OF ASS

Treatment Area

ASS shall be placed in a prepared treatment area, be it onsite or at an approved offsite location. Preferably the treatment area should be located close to the area where the materials will be excavated. The treatment area shall be fully enclosed by a bund wall to prevent runoff to other areas of the site. The bund must have a height of at least 0.5m that comprises of soils that are not ASS or are treated ASS. The size of the treatment area should be of sufficient size to treat the excavated materials at the proposed excavation rate and to store material for the period required to undertake the verification testing. The treatment area should be lined with several layers of heavy duty plastic (HDPE). The lining should be replaced periodically as required, where it is damaged during the treatment process.

Alternatively, for small volumes of materials, treatment could be undertaken in a large skip.

The treatment area / skip should be covered with heavy duty plastic at all times to prevent runoff, particularly when inclement weather is forecast.

Treatment

The ASS shall be placed in the treatment area and spread in a layer of not more than 300mm thick with lime being applied across the treatment area at the rate specific in the geotechnical report (90kg / cubic meter for the materials tested). The lime shall be evenly mixed and be applied within 8 hours of excavation.

Validation Testing

Validation testing shall be undertaken by an independent ASS consultant at the initial rate of two samples per 500m³ or part thereof. The sample shall be submitted to a NATA accredited laboratory for testing by the Chromium Reducible Sulfur suite.

If testing indicates reducible sulphur values that exceed ASSMAC Action Criteria in the processed soil the material will require reprocessing (potentially requiring variation in the



processing methodology). Further validation testing should then be undertaken to assess that acceptable values have been obtained.

All records applicable to acid sulfate testing and treatment shall be collated to substantiate treatment.

Post Treatment

Once the ASS materials have been treated in accordance with this ASSMP, the materials may be reused onsite or disposed of in accordance with the relevant regulatory requirements. It is noted that additional testing may be required to appropriately classify the materials for offsite disposal or reuse on another approved site.