



STORMWATER MANAGEMENT PLAN

FOR

MACQUARIE UNIVERSITY ARTS PRECINCT

PROPOSED NEW ARTS PRECINCT BUILDING

REPORT NO. R01790-SWMP
REVISION B

AUGUST 2017

PROJECT DETAILS

Property Address: Macquarie University

Development Proposal: Proposed New Arts Precinct Building

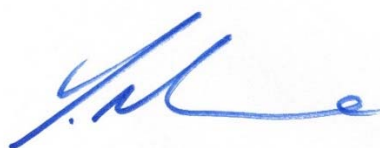
REPORT CERTIFICATION

Report prepared by:



XAN PHILP
Civil Engineer
B.E.(Civil), DipEngPrac, GradCertEM MIEAust

Report reviewed by:



ANTHONY MANCONE
Civil Engineer
B.E.(Civil)Hons., MIEAust, CPEng,
NER(Civil), NER (Building Services)

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DOCUMENT CONTROL

REVISION	ISSUE DATE	ISSUED TO	ISSUED FOR
A	JULY 17	Capital Insight	INFORMATION
		Council	APPROVAL
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		Council	APPROVAL

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1. INTRODUCTION

This Stormwater Management Plan & Report has been prepared in accordance with City of Ryde Development Control Plan to support the Development Application for the proposed development at Macquarie University.

Due to the nature of this development, this report addresses the requirements of Condition C04 & Commitments SOC5, SOC9 & SOC12 of the State Significant Development (SSD) Application. It also addresses requirements KI-01, KI-06, KI-09 & KI-11 of the Secretary's Environmental Assessment Requirements (SEARs).

The scope of this report includes a comprehensive assessment of the stormwater management requirements for the proposed development. Accordingly, this report includes findings of the assessment and proposes a best practice stormwater management strategy.

The report describes the principles and operation of the proposed stormwater systems as well as the primary components of the drainage system. As further assessment is required under the conditions of consent, the final stormwater system layout may need to be revised in the future during the application for a Construction Certificate.

The following information and documents were used for this investigation:

- Concept Civil Engineering Drawings for the Development Application submission prepared by C&M Consulting Engineers;
- Architectural Drawings by Budden Nangle Michael & Hudson Architects
- Ryde Local Environment Plan (LEP) 2014
- City of Ryde Development Control Plan (DCP) 2014
- The City of Ryde Water Sensitive Urban Design – MUSIC Modelling Guidelines (2009)
- City of Ryde – Macquarie Park Floodplain Risk Management Study and Plan (2010)
- “Australian Runoff Quality – A Guide to Water Sensitive Urban Design”, Engineers Australia (2006)
- “Australian Rainfall and Runoff – A Guide to Flood Estimation”, Institute of Engineers, Australia (1987)
- Australian Standard AS3500.3 – Plumbing and drainage – Part 3: Stormwater drainage

1.1 The Site

The site is located within the Macquarie University campus at North Ryde (Refer to **Figure 1**).



Figure 1 - Aerial Photo of Existing Site
(Source: maps.six.nsw.gov.au)

The proposed development involves the refurbishment of existing buildings and the construction of a new building with associated civil works.

1.2 Key Issues

The key issues to be addressed in this report include:

- **Water Quantity** – Increases in impervious areas as a result of development (such as roofs, driveways, etc) has the potential to increase stormwater flows from the site during storm events. To avoid impacting on the site and downstream properties, the site stormwater system must be designed to safely convey flows through the site and within the capacity of the downstream drainage system.
- **Water Quality** – Urban developments have the potential to increase gross pollutants, sediments and nutrient concentrations in storm water runoff. To limit the impact on the downstream water quality, pollution control measures will be provided within the sites stormwater management system prior to discharging into the drainage network.

2. RELEVANT GUIDELINES

2.1 Design Guidelines

The site based stormwater management and planning elements are to be designed and constructed in accordance with the following:

Water Quantity

Guidelines: City of Ryde DCP (2014) – Part: 8.2 – Stormwater and Floodplain Management

City of Ryde DCP – Part: 8.2 – Stormwater Management Technical Manual (2015)

The proposed development increases the total impervious area of the existing area and therefore may increase the flow and discharge rate of flow to the downstream waterway. Therefore, on-site detention (OSD) is required to maintain the existing discharge flows.

Water Quality

Guidelines: City of Ryde DCP (2014) – Part: 8.2 – Stormwater and Floodplain Management

The main objective for stormwater quality is to minimise the impacts on downstream water bodies.

City of Ryde has adopted a stormwater management policy that incorporates “best practice” principles of Water Sensitive Urban. The site specific council water quality targets are outlined in Table 1 below:

Table 1 - Water Quality Reduction Targets

PARAMETERS	CRITERIA
Gross Pollutants	90% reduction of the average annual load
Suspended Solids	85% reduction of the average annual load
Total Phosphorus	65% reduction of the average annual load
Total Nitrogen	45% reduction of the average annual load

2.2 Objectives and Targets

The objective is to provide stormwater controls that ensure the proposed development does not adversely impact on the quantity or quality of stormwater flows within, adjacent to and downstream of the site.

Compatible with the legislation, policy and requirements, the objectives and targets for stormwater management are as provided in Table 2.

Table 2 - Stormwater Management Objectives

STORMWATER MANAGEMENT	OBJECTIVES	TARGET
Quantity	▪ The existing runoff flow regimes for the full storm events should be maintained, and provide safe conveyance system for the major storm events.	▪ Limit post development flow from the proposed development site to less than or equal to the pre-development flows.
Quality	▪ The full range of typical urban stormwater pollutants shall meet Council requirements	▪ Runoff from site to achieve minimum reductions in total pollutant loads in accordance with Council's requirements

2.3 Overall Strategies

The proposed stormwater management strategies to manage runoff and ensure no detriment to the receiving environments have been divided into short and long term strategies in Table 3 below:

Table 3 - Stormwater Management Strategies

STRATEGY	DESCRIPTION
Short Term Strategies	Short term strategies generally refer to the control of soil and water erosion during the construction phase. The primary risk occurs while soils are exposed during construction works when suspended sediments and associated pollutants can be washed into downstream waterways. Strategies to prevent this potential degradation include the adequate provision of sediment and erosion control measures which should be documented prior to commencement of works in a Soil and Water Management Plan (SWMP). These controls will limit the movement of sediment in disturbed areas, and will be designed to remove sediment from runoff prior to discharge from the site.
Long Term Strategies	Long term strategies to maintain stormwater quality discharged from the site include utilisation of a number of permanent treatment measures to remove pollutants effectively. The water quality requirements will be addressed through a rainwater reuse tank and downstream filter cartridges to further polish the phosphorus and nitrogen removal rates.

This report addresses the long term impacts of the development. For short term effects (i.e. during the construction phase) water quality control is achieved by implementing the measures in the Sedimentation & Erosion Control Plans to be included with the Construction Certificate Application.

3. STORMWATER QUANTITY CONTROL

3.1 Introduction

The main criterion for the stormwater quantity control is to ensure that the post-development design flows do not exceed the capacity of the downstream drainage network or cause erosion/detriment to natural waterways.

3.2 Proposed Drainage System

The drainage system for the proposed development will be designed to collect the majority of concentrated flows from impermeable surfaces such as access ways, parking areas and buildings. Where possible (and practical), runoff from pervious areas will also be collected.

The drainage system proposed for the development includes:

- A pipe network system to collect minor storm runoff from areas;
- A rainwater tank with overflow into the OSD
- An on-site detention (OSD) storage tank with orifice control;

A reduced set of concept civil engineering drawings is included in Appendix A.

3.2.1 Rainwater Tank Requirements

It is proposed that a rainwater tank with a minimum volume of 30kL be provided and connected for non-potable water usage. The overflows from this proposed rainwater tank will be directed into the on-site stormwater detention (OSD)

3.2.2 On-Site Stormwater Detention Requirements

On-site detention is required for the development of the site as per Council's DCP and technical specification. The requirements for the OSD design is that the post-development flows not exceed the pre-development flows from the site.

DRAINS modelling has been undertaken for the proposed site restricting the post-development flows to the pre-development flows for all storms up to and including the 1% AEP peak flow. This modelling showed that a minimum OSD volume of 38.8m³ would be required.

The DRAINS layout and results for the minor (20% AEP) and major (1% AEP) storms are attached as Appendix B.

4. WATER QUALITY CONTROL

4.1 Introduction

The quality of runoff from a catchment depends upon many factors such as land use, degree of urbanisation, population density, sanitation, waste disposal practices, landform, soil types, and climate. Pollutants typically transported by runoff include litter, sediment, nutrients, oil, grease, and heavy metals. Whilst these pollutants have a negative impact on the receiving water quality, suspended solids and nutrients cause the highest detrimental impact to the environment. Litter, oils, and other surfactants have an aesthetic impact.

Activity within a catchment during urbanisation includes the disturbance of vegetation, removal of topsoil, land shaping, road construction, installation of services, and building works. It is during this phase that the sediment movement is greatest and is estimated that the sediment production levels may be up to 6 times higher than under the existing conditions. However, once development is completed, the sediment loading may return to the existing level depending on land management practices.

As with all development projects, soil erosion during the construction phase presents a potential risk to water quality. The primary risk occurs while soils are exposed during earthworks when suspended sediment and associated pollutants can be washed into downstream watercourses.

This section of the report addresses the long term impacts of the development on water quality. For short term effects (i.e. during the construction phase) water quality control is achieved by implementing the measures in the Sedimentation & Erosion Control Plans to be included with future Construction Certificate submissions.

4.2 Water Quality Control Measures

There are number of measures that can reduce pollutant loadings, however, each different type has its own effectiveness in reducing pollutant loadings that depends on land use type, topography and the target control.

The adopted Treatment Train will provide the most efficient and manageable measures, suited to the subject development setting, surrounded by residential environmentally sensitive areas.

The measures proposed for the redevelopment are summarised in Table 4.

Table 4 - Water Quality Control Measures

MEASURES	DESCRIPTIONS
Gross Pollutant Traps	- An EnviroPod is a catch basin insert installed inside inlet pits. It is effective in removing trash, debris and other pollutants from runoff. - EnviroPods proposed for the project utilise a 200 micron filter system. - These filter baskets will be installed in indicated pits for the proposed development.
Rainwater Tank	- Rainwater tanks are effective in the removal of pollutant loads at source. The pollutant removal process occurs by harvesting runoff for reuse, thereby limiting the nutrients that are discharged into the waterways. - It is proposed to provide a rainwater reuse tank for with a minimum effective volume of 30m³ plumbed for non-potable water use.
Filter Cartridges	<i>StormFilter</i> is a proprietary device containing multiple cartridge units in a single system thereby suitable for larger catchments - One of the advantages of using <i>StormFilter</i> is that the cartridges come with various filtration media available to target site-specific pollutants - Each cartridge consists of Perlite/Zeolite media - There will be total of 8 x 690mm standard cartridges within the OSD tanks respectively as detailed in the engineering drawings.

In addition to the above measures for pollutant control, natural vegetated buffers will be maintained along the edges of roads, accesses, and areas of activity, which will further reduce pollutants to meet reduction targets. This added benefit has not been included in the modelling hence contributing to the conservative nature of the modelling and assessment.

4.3 Strategy Effectiveness

The effectiveness of the proposed water quality measures have been assessed using numerical modelling. The results were assessed against the established WSUD requirements to determine the effectiveness of the proposed strategy.

4.4 Water Quality Modelling

4.4.1 MUSIC Program

The water quality model adopted for this project is the MUSIC (Model for Urban Stormwater Improvement Conceptualisation Version 6) water quality numerical model developed by the MUSIC Development Team of the Cooperative Research Centre for Catchment Hydrology (CRCCH). MUSIC is an event basis model, and will simulate the performance of a group of stormwater management measures, configured in series or in parallel to form a “treatment train”.

The MUSIC User Manual suggests that the time-step should not be greater than the time of concentration of the smallest sub-catchment, but consideration should also be given to the smallest detention time of treatment nodes in the system. To accurately model the performance of the treatment nodes, a 6-minute time step was chosen.

The MUSIC model was generated using the historical 6-minute rainfall and monthly evapotranspiration data for Sydney Airport (BOM Station No. 66037) for a period of 10 years from 1988 to 1998.

Catchment characteristics were defined by the roof areas, communal open space and balconies with generally impervious characteristics to replicate the catchment for the development condition.

The MUSIC model layout (01790_Mac Uni_RevC.sqz) is shown in Appendix D of this report.

4.4.2 Event Mean Concentration

MUSIC uses different event mean concentrations (EMC) to determine the pollutant loads generated by different land uses. The standard EMCs adopted within MUSIC were based on research undertaken by Duncan (1999) through the CRCCH and the results are reproduced in Australian Runoff Quality – A Guide to Water Sensitive Urban Design (ARQ).

The EMC values used in the MUSIC models for this project were obtained from ARQ. Table 5 summarises the parameters used for the site.

Table 5 - EMC Parameters

LAND USE	MEAN BASE FLOW CONCENTRATION PARAMETERS Log ₁₀ (mg/l)			MEAN STORM FLOW CONCENTRATION PARAMETERS Log ₁₀ (mg/l)		
	TSS	TP	TN	TSS	TP	TN
Roof Areas	Not Applicable ^{*Note 1}			1.300	-0.890	0.300
Impervious Areas	Not Applicable ^{*Note 1}			2.150	-0.600	0.300
Driveways	Not Applicable ^{*Note 1}			2.430	-0.300	0.340
Landscaping	1.200	-0.850	0.110	2.150	-0.600	0.300

*Note 1 – Roof/Impervious areas consists of 100% impervious area so there is no base flow generated from this area

4.4.3 Configuration

Table 6 and 7 provide the treatment configurations used in the MUSIC model.

Table 6 - Catchment Areas

LAND USE	DEVELOPED CONDITIONS	
	AREA (m ²)	IMPERVIOUSNESS (%)
Roof	2,882	100
Impervious	415	100
Pervious	43	0
Total	3340m²	99%

Table 7 - Stormwater Quality Improvement Devices (SQID)

STORMWATER QUALITY IMPROVEMENT DEVICE (SQID)	QUANTITY OF SQID
StormFilters	8 x 690mm Cartridges
Rainwater Tank	1 x 30kL Rainwater Tank
Gross Pollutant Traps	2 X Enviropods in nominated pits

4.4.4 Results

The results of the MUSIC modelling are summarised in Table 8. The total pollutant loads from the development are expressed in kilograms per year. The reduction rate is expressed as a percentage and compares the pollution from the post developed site to that of the existing developed state of the site.

Table 8 - Summary of MUSIC Model Results

PARA-METER	EXISTING SITE LOADS (KG/YR)	POST DEVELOPMENT WITH TREATMENT (KG/YR)	REDUCTION %	TARGET ACHIEVED
GP	79.4	0	100	Yes
TSS	143	17.8	87.6	Yes
TP	0.527	0.174	67	Yes
TN	6.8	3.52	48.2	Yes

GP = Gross Pollutants TSS = Total Suspended Solids
TP = Total Phosphorus TN = Total Nitrogen

In all instances, the proposed water quality control measures enabled the reduction targets to be achieved for all key stormwater pollutants. Therefore, by implementing the proposed treatment train measures within the proposed development there will be no detrimental effect on the quality of stormwater running off from the site.

5. FLOOD IMPACT ASSESSMENT

As per the City of Ryde – Macquarie Park Floodplain Risk Management Study and Plan (2010), the area adjacent to the site is subject to overland flow during a 1% AEP storm event (Refer to **Figure 2** below).



Figure 2 – Extract from 100 Year ARI Flood Model
(Source: Macquarie Park Floodplain Risk Management Study and Plan)

This area, however, is not considered to be mainstream flooding. Rather it is localised flooding due to trapped low point adjacent to the site and issues with the local drainage network.

Since the 2010 study was published, Macquarie University has undertaken drainage amplification works to address the localised flooding issues associated with undersized pipes adjacent to the proposed development. A copy of the drainage amplification plans have been attached to this report as Appendix D.

Due to the aforementioned drainage amplification works, the overland flow issue has been resolved and the proposed development site is no longer affected by overland flow or localised flooding.

The proposed development therefore is not affected by flooding nor impacts the existing flooding regime at the University.

It should also be noted that in accordance with the Ryde LEP, the site is not within a Flood Planning Area (Refer to **Figure 3** below).

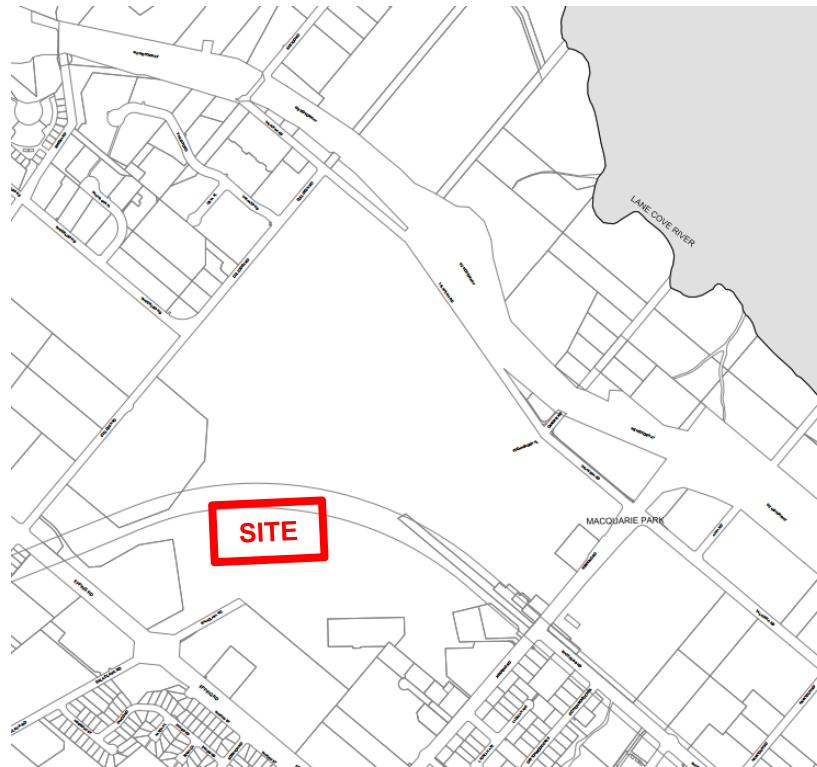


Figure 3 – Extract from Flood Planning Map
(Source: Ryde LEP)

6. RECOMMENDATIONS

The proposed development of the subject site could potentially lead to significant changes in water quantity as well as quality if a water sensitive urban design approach is not adopted as part of the development strategy. The traditional stormwater management and investigation that only considers impacts of flooding and flood mitigation is a thing of the past. Stormwater management practices must now also consider water quality, aquatic habitats, riparian vegetation, recreation, aesthetic and economic issues.

The key strategies to be adopted for this development include the following:

1. A pipe network system to collect minor storm runoff from surface areas which will minimise nuisance flooding;
2. A 30kL effective volume rainwater tank will be provided to allow rainwater reuse whilst providing an improvement of the quality of stormwater runoff and also providing a level of stormwater detention. The harvested rainwater will be plumbed for non-potable water use;
3. On-Site Detention will be provided for the development in the form of a detention tank with orifice and weir control and a minimum effective volume of 38.8m³;
4. EnviroPods in the external surface inlet pits to form part of the water quality treatment train system that removes gross pollutants that are detrimental to the down stream waterways
5. 8 x standard 690mm StormFilter cartridges to polish stormwater prior to discharge to the downstream drainage network.

The results from the investigations and modelling for this project that have been summarised in this report indicate that the development with the proposed WSUD strategy and management can provide a safe and ecologically sustainable environment.

7. REFERENCES

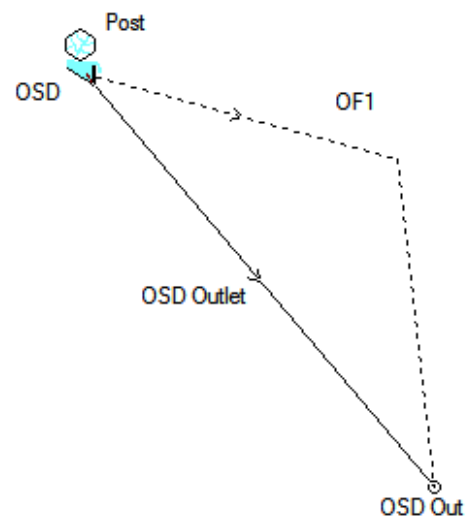
- Concept Civil Engineering Drawings for the Development Application submission prepared by C&M Consulting Engineers;
- Ryde Local Environment Plan (LEP) 2014
- City of Ryde Development Control Plan (DCP) 2014
- The City of Ryde Water Sensitive Urban Design – MUSIC Modelling Guidelines (2009)
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- “Australian Runoff Quality – A Guide to Water Sensitive Urban Design”, Engineers Australia (2006)
- “Australian Rainfall and Runoff – A Guide to Flood Estimation”, Institute of Engineers, Australia (1987)
- Australian Standard AS3500.3 – Plumbing and drainage – Part 3: Stormwater drainage
- Watercom – DRAINS Version 2017.09
- eWater – *MUSIC Version 6.2 (Build 1.0)*

APPENDIX A

CONCEPT CIVIL ENGINEERING DRAWINGS

DRAINS MODEL SETUP

Pre
Pre-out



PIT / NODE DETAILS

Name	Type	Family	Size	Ponding Volume (cu.m)	Pressure Change Coeff. Ku	Surface Elev (m)	Max Pond Depth (m)	Base Inflow (cu.m/s)	Blocking Factor	x y	Bolt-down lid	Part Full Shock Loss	Inflow Hydrograph	Pit is
Pre-out	Node					100		0	255.266	-43.6		3	No	
OSD Out	Node					62		0	462	-151		11	No	

DETENTION BASIN DETAILS

Name	Elev	Surf. Area	Not Used	Outlet Type	K	Dia(mm)	Centre RL	Pit Family	Pit Type	x y	HED	Crest RL	Crest Length	id
OSD	61.7	0.81		Orifice		260	61.9			375	-48 No			7
	61.9	0.81												
	61.99	36												
	63.5	36												
	64	36												

SUB-CATCHMENT DETAILS

Name	Pit or Node	Total Area (ha)	Paved Area %	Grass Area %	Supp Area %	Paved Time (min)	Grass Time (min)	Supp Time (min)	Paved Length (m)	Grass Length (m)	Supp Length (m)	Paved Slope(%)	Grass Slope %	Supp Slope %	Paved Rough	Grass Rough	Supp Rough	Lag Time or Factor	Gutter Length (m)	Gutter Slope %	Gutter Flow	Rainfall Factor	Multiplier
Pre-out	Pre-out	0.334	30	70	0	5	0	0	0	50	0	1	1	0	0.01	0.06	0	1.24E-294					
Post	OSD	0.334	99	1	0	5	0	0	0	10	0	1	1	0	0.01	0.06	0	1.38E-294					

PIPE DETAILS

Name	From	To	Length (m)	U/S IL (m)	D/S IL (m)	Slope (%)	Type	Dia (mm)	I.D. (mm)	Rough	Pipe Is	No. Pipes	Chg From	At Chg	Chg (m)	RI (m)	Chg (m)	RL (m)	etc (m)
OSD Outlet	OSD	OSD Out	3	61.7	61.67		1 Concrete, t	375	375	0.013	NewFi	1	OSD		0				

DETAILS of SERVICES CROSSING PIPES

Pipe	Chg (m)	Bottom Elev (m)	Height of S (m)	Chg (m)	Bottom Elev (m)	Height of S (m)	Chg (m)	Bottom Elev (m)	Height of S (m)	etc
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CHANNEL DETAILS

Name	From	To	Type	Length (m)	U/S IL (m)	D/S IL (m)	Slope (%)	Base Wid (m)	L.B. Slope (1:?)	R.B. Slope (1:?)	Mannin n	Depth (m)	Roofed
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OVERFLOW ROUTE DETAILS

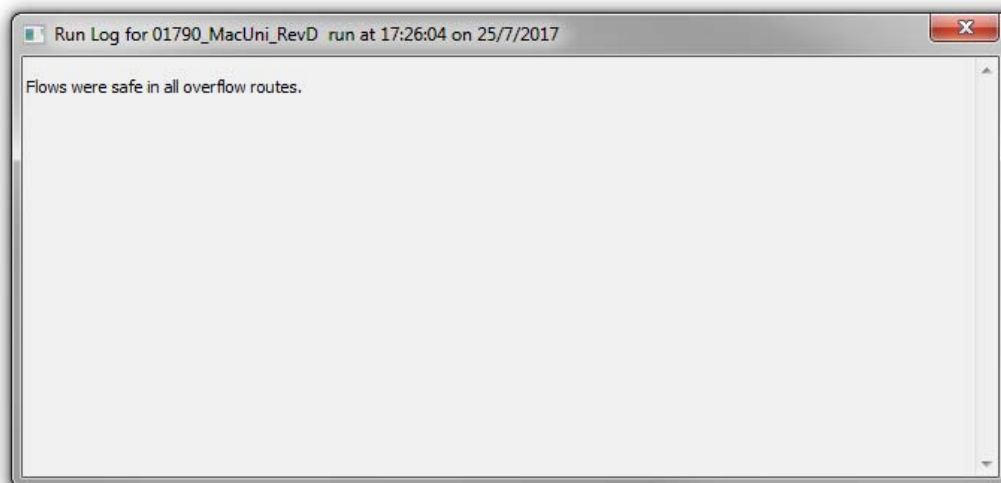
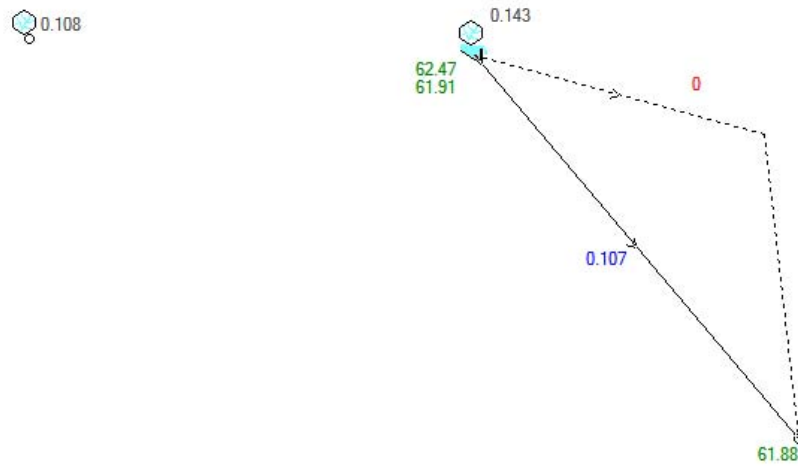
Name	From	To	Travel Time (min)	Spill Level (m)	Crest Length (m)	Weir Coeff. C	Cross Section	Safe Dep Major (m)	Safe Dep Minor (m)	Safe Dep St D (sq.m/sec)	Bed Slope (%)	D/S Area Contributing %	id
OF1	OSD	OSD Out	0.1	63.15	1.8	1.7	4 m wide p	0.3	0.15	0.4	0.01	0	361

PIPE COVER DETAILS

Name	Type	Dia (mm)	Safe Cover (m)	Cover (m)
OSD Outlet	Concrete, t	375	0.6	-0.08 Unsafe

This model has no pipes with non-return valves

DRAINS RESULTS – MINOR STORM (20% AEP)



DRAINS results prepared from Version 2017.09

PIT / NODE DETAILS

Name	Max HGL	Max Pond HGL	Max Surface Flow Arriving (cu.m/s)	Version 8 Max Pond Volume (cu.m)	Min Freeboard (m)	Overflow (cu.m/s)	Constraint
OSD Out	61.88			0			

SUB-CATCHMENT DETAILS

Name	Max Flow Q (cu.m/s)	Paved Max Q (cu.m/s)	Grassed Max Q (cu.m/s)	Paved Tc (min)	Grassed Tc (min)	Supp. Tc (min)	Due to Storm
Pre	0.108	0.043	0.066	5	9.3		0 AR&R 5 year, 25 minutes storm, average 79.0 mm/h, Zone 1
Post	0.143	0.141	0.001	5	3.54		0 AR&R 5 year, 25 minutes storm, average 79.0 mm/h, Zone 1

Outflow Volumes for Total Catchment (0.43 impervious + 0.24 pervious = 0.67 total ha)

Storm	Total Rainfall cu.m	Total Runoff cu.m (Runoff %)	Impervious Runoff cu.m (Runoff %)	Pervious Runoff cu.m (Runoff %)
AR&R 5 year, 5 minutes storm	85.73	60.10 (70.1%)	50.99 (92.2%)	9.12 (30.0%)
AR&R 5 year, 10 minutes storm	132.49	101.75 (76.8%)	81.15 (95.0%)	20.60 (43.8%)
AR&R 5 year, 15 minutes storm	167	132.21 (79.2%)	103.41 (96.0%)	28.81 (48.6%)
AR&R 5 year, 20 minutes storm	195.95	158.01 (80.6%)	122.08 (96.6%)	35.93 (51.7%)
AR&R 5 year, 25 minutes storm	219.88	178.10 (81.0%)	137.52 (97.0%)	40.58 (52.0%)
AR&R 5 year, 30 minutes storm	240.48	195.29 (81.2%)	150.80 (97.2%)	44.49 (52.1%)
AR&R 5 year, 45 minutes storm	290.58	237.95 (81.9%)	183.12 (97.7%)	54.83 (53.2%)
AR&R 5 year, 1 hour storm	329.99	271.37 (82.2%)	208.54 (98.0%)	62.84 (53.6%)
AR&R 5 year, 1.5 hours storm	391.78	323.10 (82.5%)	248.39 (98.3%)	74.71 (53.7%)
AR&R 5 year, 2 hours storm	440.88	363.98 (82.6%)	280.06 (98.5%)	83.93 (53.6%)
AR&R 5 year, 3 hours storm	519.02	429.66 (82.8%)	330.46 (98.7%)	99.20 (53.8%)

PIPE DETAILS

Name	Max Q (cu.m/s)	Max V (m/s)	Max U/S HGL (m)	Max D/S HGL (m)	Due to Storm
OSD Outlet	0.107	1.67	61.912	61.882	AR&R 5 year, 25 minutes storm, average 79.0 mm/h, Zone 1

CHANNEL DETAILS

Name	Max Q (cu.m/s)	Max V (m/s)	Due to Storm
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OVERFLOW ROUTE DETAILS

Name	Max Q U/S	Max Q D/S	Safe Q	Max D	Max DxV	Max Width	Max V	Due to Storm
OF1	0	0	0.091	0	0	0	0	0

DETENTION BASIN DETAILS

Name	Max WL	MaxVol	Max Q Total	Max Q Low Level	Max Q High Level
OSD	62.47	18.8	0.107	0.107	0

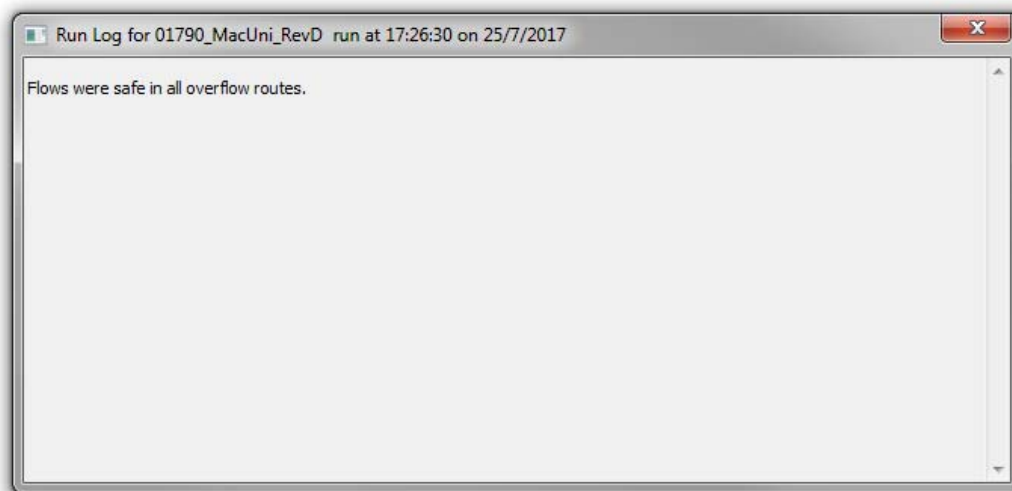
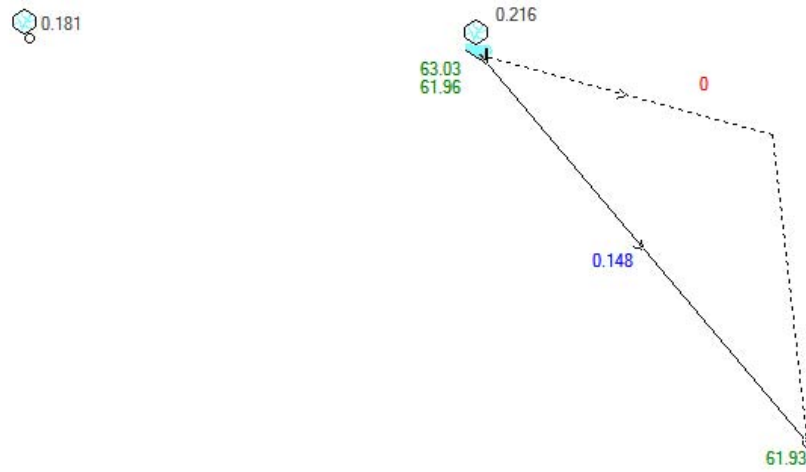
CONTINUITY CHECK for AR&R 5 year, 25 minutes storm, average 79.0 mm/h, Zone 1

Node	Inflow (cu.m)	Outflow (cu.m)	Storage Change (cu.m)	Difference %
Pre-out	71.98	71.98	0	0
OSD	106.12	106.06	0.06	0
OSD Out	106.06	106.06	0	0

Run Log for 01790_MacUni_RevD run at 17:21:16 on 25/7/2017

Flows were safe in all overflow routes.

DRAINS RESULTS – MAJOR STORM (1% AEP)



DRAINS results prepared from Version 2017.09

PIT / NODE DETAILS

Name	Max HGL	Max Pond HGL	Max Surface Flow Arriving (cu.m/s)	Version 8 Max Pond Volume (cu.m)	Min Freeboard (m)	Overflow (cu.m/s)	Constraint
OSD Out	61.93			0			

SUB-CATCHMENT DETAILS

Name	Max Flow Q (cu.m/s)	Paved Max Q (cu.m/s)	Grassed Max Q (cu.m/s)	Paved Tc (min)	Grassed Tc (min)	Supp. Tc (min)	Due to Storm
Pre	0.181	0.064	0.117	5	6.98		0 AR&R 100 year, 15 minutes storm, average 1
Post	0.216	0.214	0.002	5	2.25		0 AR&R 100 year, 5 minutes storm, average 24

Outflow Volumes for Total Catchment (0.43 impervious + 0.24 pervious = 0.67 total ha)

Storm	Total Rainfall cu.m	Total Runoff cu.m (Runoff %)	Impervious Runoff cu.m (Runoff %)	Pervious Runoff cu.m (Runoff %)
AR&R 100 year, 5 minutes storm	136.38	111.06 (81.4%)	83.66 (95.1%)	27.40 (56.6%)
AR&R 100 year, 10 minutes storm	213.76	183.16 (85.7%)	133.57 (96.9%)	49.59 (65.4%)
AR&R 100 year, 15 minutes storm	270.54	235.56 (87.1%)	170.19 (97.5%)	65.37 (68.1%)
AR&R 100 year, 20 minutes storm	318.41	279.66 (87.8%)	201.07 (97.9%)	78.59 (69.5%)
AR&R 100 year, 25 minutes storm	356.27	313.68 (88.0%)	225.48 (98.1%)	88.20 (69.7%)
AR&R 100 year, 30 minutes storm	394.12	348.29 (88.4%)	249.90 (98.3%)	98.39 (70.3%)
AR&R 100 year, 45 minutes storm	480.97	427.28 (88.8%)	305.91 (98.6%)	121.37 (71.1%)
AR&R 100 year, 1 hour storm	547.75	487.94 (89.1%)	348.99 (98.8%)	138.95 (71.5%)
AR&R 100 year, 1.5 hours storm	661.32	591.72 (89.5%)	422.24 (99.0%)	169.48 (72.2%)
AR&R 100 year, 2 hours storm	748.18	670.39 (89.6%)	478.26 (99.1%)	192.12 (72.3%)
AR&R 100 year, 3 hours storm	903.79	811.60 (89.8%)	578.64 (99.3%)	232.96 (72.6%)

PIPE DETAILS

Name	Max Q (cu.m/s)	Max V (m/s)	Max U/S HGL (m)	Max D/S HGL (m)	Due to Storm
OSD Outlet	0.148	1.78	61.964	61.936	AR&R 100 year, 25 minutes storm, average 128 mm/h, Zone 1

CHANNEL DETAILS

Name	Max Q (cu.m/s)	Max V (m/s)	Due to Storm
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OVERFLOW ROUTE DETAILS

Name	Max Q U/S	Max Q D/S	Safe Q	Max D	Max DxV	Max Width	Max V	Due to Storm
OF1	0	0	0.302	0	0	0	0	0

DETENTION BASIN DETAILS

Name	Max WL	Max Vol	Max Q Total	Max Q Low Level	Max Q High Level
OSD	63.03	38.8	0.148	0.148	0

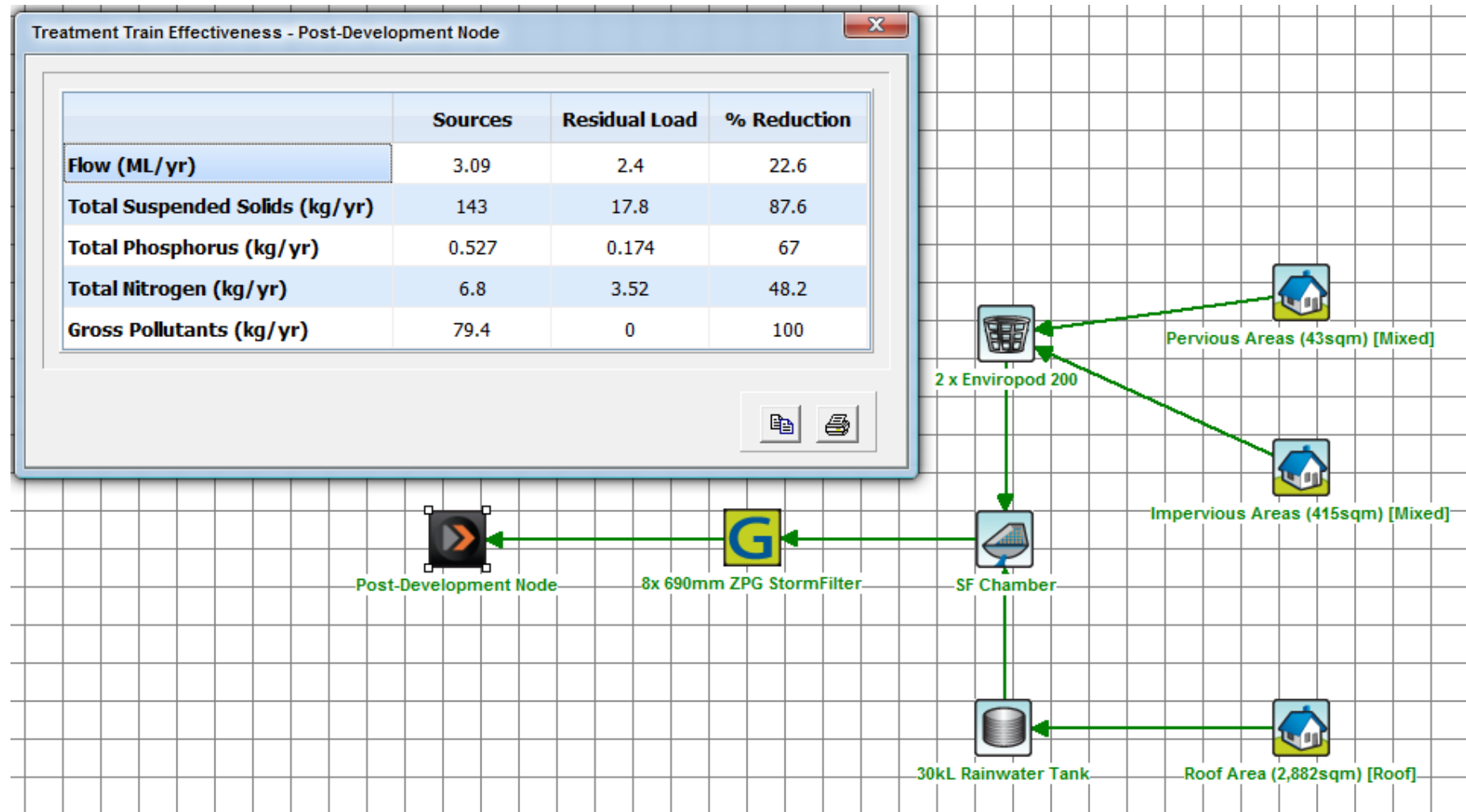
CONTINUITY CHECK for AR&R 100 year, 15 minutes storm, average 162 mm/h, Zone 1

Node	Inflow (cu.m)	Outflow (cu.m)	Storage Change (cu.m)	Difference %
Pre-out	104.01	104.01	0	0
OSD	131.55	131.49	0.06	0
OSD Out	131.49	131.49	0	0

Run Log for 01790_MacUni_RevD run at 17:20:45 on 25/7/2017

Flows were safe in all overflow routes.

MUSIC MODEL LAYOUT & RESULTS



APPENDIX D

DRAINAGE AMPLIFICATION WORKS

ISSUE FOR TENDER ONLY
NOT TO BE USED FOR CONSTRUCTION

C	ISSUE FOR CONSTRUCTION	NB	MS	15.11.10
B	RE ISSUE FOR TENDER	SB	MS	09.09.10
A	ISSUE FOR TENDER	SB	MS	27.07.10
Rev	Description	Eng	Draft	Date

Project

MACQUARIE UNIVERSITY
ARCHIVE ROOM FLOOD
INVESTIGATION

Sheet Subject

NOTES AND LEGENDS SHEET



48 Chandos Street St.Leonards NSW 2065
T: +61 2 9439 7288 F: +61 2 9439 3146 ttwsyd@ttw.com.au

Taylor Thomson Whitting (NSW) Pty Ltd A.C.N. 113 578 377

Scale : A1	Drawn	Authorised
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MS

Job No	Drawing No	Revision
101100	001	0

101138 C01 C

Plot File Created: Nov 15, 2010 - 3:19pm

File Name: C:\dwn - USER: marlos - Plot File Created: Nov 15 2010 - 3:20pm



- ### Sequence Of Works

-

Diagram 1 (Left): Siltation Fence Detail. This diagram shows a cross-section of a siltation fence. The fence is 450mm high and 500mm wide at the base. It is constructed from 3 x 2.5 wires at 150mm centres, secured to a star picket. The geotextile fabric is securely fixed to the fence and is embedded 200mm into the ground. The fence is positioned 200mm from the proposed bulk earthworks line. The flow direction is indicated by an arrow pointing right.

Diagram 2 (Right): Siltation Fence Detail. This diagram shows a cross-section of a siltation fence. The fence is 453mm high and 179mm wide at the base. It is constructed from geotextile fabric secured to a safety fence. The geotextile fabric is embedded 200mm into the ground. The fence is positioned 200mm from the proposed bulk earthworks line. The flow direction is indicated by an arrow pointing right.

NOTE: ENDS OF SILTATION FENCE TO RETURNED UP SLOPE TO PREVENT RUNOFF

SCALE 1: 20

Diagram 1 (Left): Siltation Fence Detail. This diagram shows a cross-section of a siltation fence. The fence is 450mm high and 500mm wide at the base. It is constructed from 3 x 2.5 wires at 150mm centres, secured to a star picket. The geotextile fabric is securely fixed to the fence and is embedded 200mm into the ground. The fence is positioned 200mm from the proposed bulk earthworks line. The flow direction is indicated by an arrow pointing right.

Diagram 2 (Right): Siltation Fence Detail. This diagram shows a cross-section of a siltation fence. The fence is 453mm high and 179mm wide at the base. It is constructed from geotextile fabric secured to a safety fence. The geotextile fabric is embedded 200mm into the ground. The fence is positioned 200mm from the proposed bulk earthworks line. The flow direction is indicated by an arrow pointing right.

NOTE: ENDS OF SILTATION FENCE TO RETURNED UP SLOPE TO PREVENT RUNOFF

SCALE 1: 20

Diagram illustrating a Geotextile Pit Filter. The diagram shows a cross-section of a pit where runoff water with sediment enters from the left. The water passes through a geotextile filter fabric wrapped over a grate, which is placed over an existing pit or grate. The filtered water is shown flowing out from the bottom of the pit. Labels include: 'RUNOFF WATER WITH SEDIMENT', 'FILTERED WATER', 'GEOTEXTILE FILTER FABRIC WRAPPED OVER GRATE.', and 'EXISTING PIT OR GRATE AS SPECIFIED'.

GEOTEXTILE PIT FILTER
NTS

EXISTING SURFACE LEVEL

100 MIN

500 MIN

500 MIN

TYPICAL SECTION THROUGH CATCH DRAIN

SCALE 1: 20

Diagram illustrating the construction of a Temporary Construction Exit. The exit is a raised structure with a 300 mm high berm on the right side, adjacent to an existing roadway. The exit is constructed using 50-75 mm gravel over a geotextile fabric. The length of the exit is 15000 mm, and the width is 3000 mm. The exit is designed to provide wash water for trucks exiting the site. Runoff from the pad is directed to a sediment trap. The diagram also shows a construction site and a runoff path from the pad directed to a sediment trap.

Project

Sheet Subject

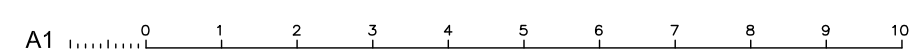
TTW

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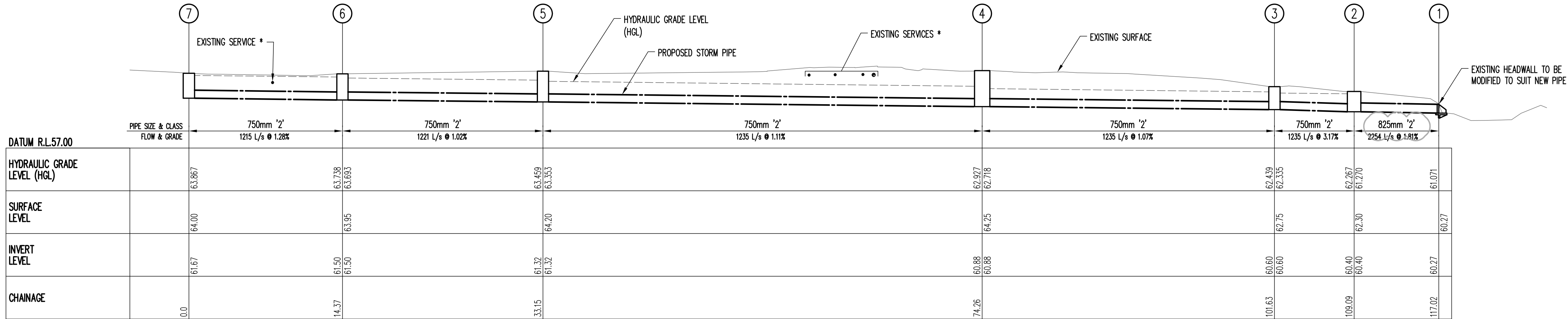
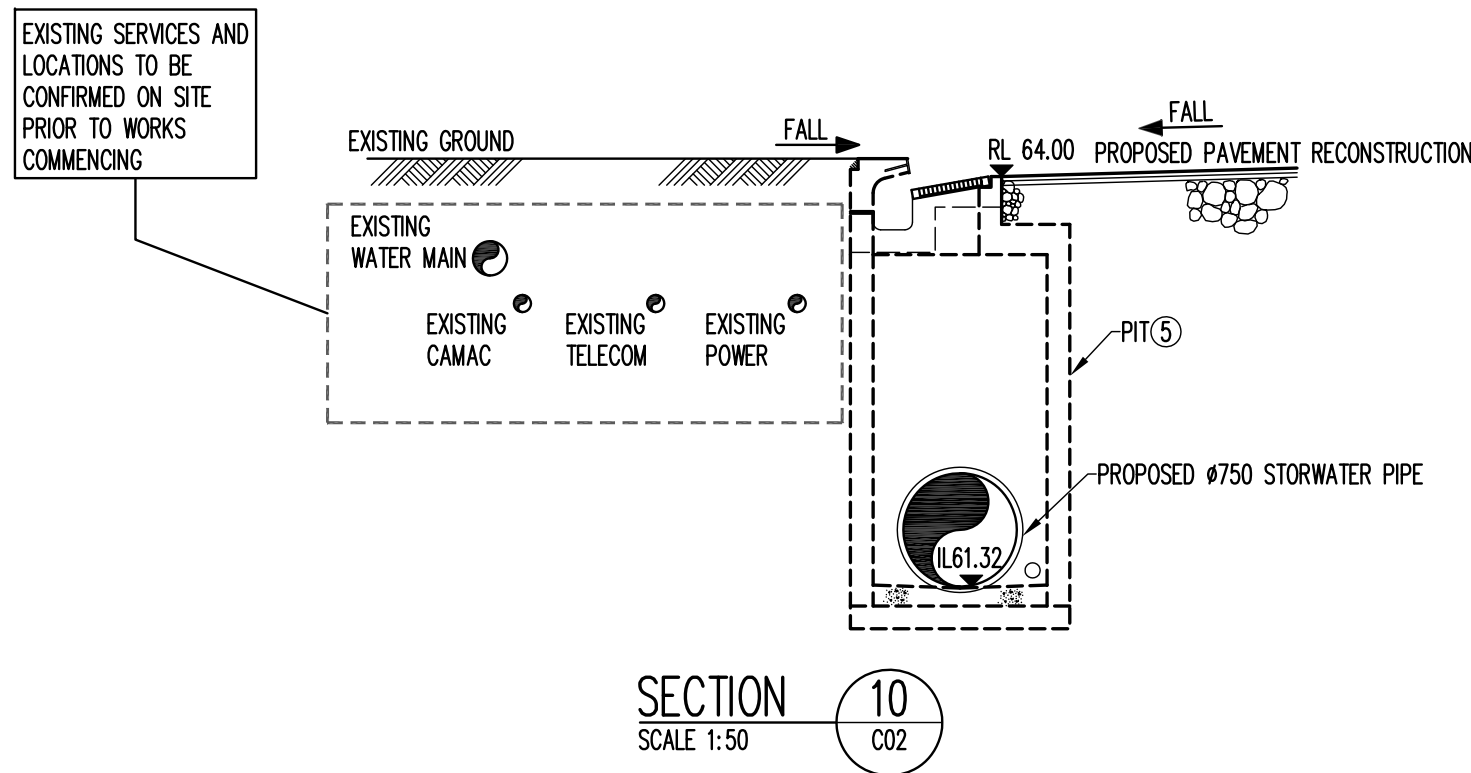
Consulting Engineers

48 Chandos Street St Leonards NSW 2065
T: +61 2 9439 7288 F: +61 2 9439 3146 ttwsyd@ttw.com.au

Taylor Thomson Whitting (NSW) Pty Ltd A.C.N. 113 578 377



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STORMWATER LONG SECTION
SCALE 1: 250

FOR NOTES AND LEGENDS
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D	ISSUE FOR CONSTRUCTION	NB	MS	15.11.10
C	RE-ISSUE FOR TENDER	SB	MS	09.09.10
B	RE-ISSUE FOR TENDER	SB	MS	10.08.10
A	ISSUE FOR TENDER	SB	MS	27.07.10
Rev	Description	Eng	Draft	Date

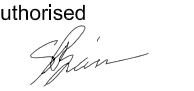
Project
**MACQUARIE UNIVERSITY
ARCHIVE ROOM FLOOD
INVESTIGATION**

Sheet Subject

SECTION SHEET



TaylorThomsonWhitting
Consulting Engineers
48 Chandos Street St.Leonards NSW 2065
T: +61 2 9439 7288 F: +61 2 9439 3146 tlwsysd@tlw.com.au
Taylor Thomson Whitting (NSW) Pty Ltd A.C.N. 113 578 377

Scale : A1 AS SHOWN	Drawn MS	Authorised 
Job No 101138	Drawing No C05	Revision D
Plot File Created: Nov 15, 2010 - 3:20pm		

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