

Report on Dewatering Management Plan

> Fiveways Falcon Street, Crows Nest

> > Prepared for Deicorp Pty Ltd

Project 86645.03 10 January 2025



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The undersigned, on behalf of Douglas Partners Pty Ltd, confirm that this document and all attached drawings, logs and test results have been checked and reviewed for errors, omissions and inaccuracies.

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Douglas Partners acknowledges Australia's First Peoples as the Traditional Owners of the Land and Sea on which we operate. We pay our respects to Elders past and present and to all Aboriginal and Torres Strait Islander peoples across the many communities in which we live, visit and work. We recognise and respect their ongoing cultural and spiritual connection to Country.



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Report on Dewatering Management Plan Fiveways Falcon Street, Crows Nest

1. Introduction

This report presents the results of a dewatering management plan (DMP) and hydrogeological assessment undertaken for the proposed Fiveways at Falcon Street, Crows Nest. The DMP was commissioned in an email dated 10 May 2023 by Greg Colbran of Deicorp Pty Ltd and was undertaken in accordance with Douglas Partners' proposal 86645.03.P.003.Rev0 dated 05/05/2023.

It is understood that the proposed development will include the demolition of the existing buildings and construction of a mixed-use structure (residential with retail uses) with a 7-level basement, with a finish floor level at RL 74.8 m.

This DMP is based on the recent geotechnical investigation undertaken by Douglas Partners Pty Ltd (DP) at the site, complemented by additional measurements of groundwater levels, in-situ permeability tests and numerical modelling to estimate seepage inflow rates and drawdown of groundwater levels associated with dewatering of the proposed basement.

Details of the field work and numerical modelling are given in this report. This DMP may be used to accompany an application for a "Water Supply Works Approval" from Water NSW and an application for a permit to discharge groundwater to stormwater system from the Council.

2. Previous Work

Information used to develop the conceptual groundwater model was obtained from the previous investigations undertaken by DP.

- Douglas Partners Pty Ltd: "Report on Geotechnical Investigation: Fiveways, Falcon Street, Pacific Highway and Alexander Street, Crows Nest", dated September 2023 (DP, 2023a);
- Douglas Partners Pty Ltd: "Report on Pre-demolition Detailed Site Investigation (Contamination): Fiveways, Cnr Falcon Street, Pacific Highway and Alexander Street, Crows Nest", dated August 2023 (DP, 2023b); and
- Douglas Partners Pty Ltd: "Report on Due Diligence Geotechnical Desktop Study: Fiveways, Cnr Falcon Street, Pacific Highway and Alexander Street, Crows Nest", dated December 2018 (DP, 2018).

The locations of groundwater monitoring wells (BH103, BH104, BH105) installed as part of the aforementioned works are shown on Drawing 1 in Appendix C.



3. Site Description

The site is a triangular city block and covers approximately 3,300 m², located in the suburb of Crows Nest. The site is bounded by Falcon Street, Pacific Highway and Alexander Street. The existing surface slopes gradually from west to east along Falcon Street (from RL 99.1 m to RL 96.7 m) and north to south along Pacific Highway (from RL 99.1 m to RL 96.0 m). Along Alexander Street the existing surface slopes towards the south (from RL 96.7 m to RL 96.0 m).

The site is currently occupied by a number of commercial properties, between 2 and 4 levels high, with some properties having an existing 1 level basement.

4. Geotechnical and Hydrogeological Model

4.1 Subsurface Profile

Reference to the Sydney 1:100 000 Geological Series Sheet indicates that the site in underlain by rock of the lower Ashfield Shale formation, overlying the Mittagong formation, which is a transitional unit between the Ashfield Shale and underlying Hawkesbury Sandstone. The results of the investigation confirmed the regional mapping with Ashfield Shale being underlain with Mittagong formation and underlain with Hawkesbury Sandstone noted at depth.

The previous investigation identified semi-shallow depths of fill and residual soils over shale bedrock. The shale was generally noted to be extremely to highly weathered to depths of between 3.0 m to 10.0 m before grading to slightly weathered to fresh shale, then fresh sandstone at depth.

The general strata encountered in the boreholes is summarised as follows:

Pavement / Fill:	Generally, clay, gravelly clay and sandy gravel, with building rubble, plastic and sandstone cobbles to depths of 0.9 m to 2.5 m.
Residual Soil:	Mostly apparently firm silty clay, trace ironstone gravel, increasing to apparently very stiff clay to depths of between 2.0 m and 4.9 m.
Shale (Ashfield Shale):	Generally, very low and low strength, extremely weathered to fresh, fragmented to slightly fractured shale to depths of approximately 13.0 m to 17.4 m.
Siltstone / Sandstone (Mittagong Formation):	Generally, very low, low and medium strength, slightly weathered to fresh, slightly fractured to unbroken siltstone and sandstone to depths of approximately 13.8 m to 19.0 m.
Sandstone (Hawkesbury Sandstone):	Medium to high and high strength, fresh, slightly fractured to unbroken sandstone.



4.2 Groundwater

Three groundwater monitoring wells were installed during the previous geotechnical investigation. Free groundwater during auguring was only observed in BH103, at 2.0 m depth. The use of water as a drilling fluid during coring of the boreholes precluded any further groundwater observations.

Groundwater monitoring wells were installed in Boreholes BH103, BH104 and BH105. After installation, the groundwater monitoring wells were purged of drilling fluid using a submersible pump and In situ permeability testing was carried out in each of the wells. Digital data loggers were then installed to monitor recharge of the groundwater and for long term groundwater level monitoring. The filter zone depths and groundwater measurements taken following installation of the groundwater wells are presented in Table 1, Table 2 and Table 3 below.

Table 1: Well Construction Details

BH Ref	Ground Surface Level (m AHD)	Filter Zone Depth (m)	Filter Zone Material
BH103	96.0	11.6 - 30.57	Rock
BH104	93.6	5.8 - 18.8	Rock
BH105	98.1	10.3 - 23.31	Rock

BH Ref	Water Level (m) [RL m AHD)	Date of Reading	Comments
	(7.5) [88.5]	16/05/2023	Day of well installation and after purging.
	(7.5) [88.5] 06/06/2023 [88.5] 11/07/2023 [88.8]	06/06/2023	21 days after purging.
BH103		1 st monthly reading	
[88.7]	11/08/2023	2 nd monthly reading	
		12/09/2023	3 rd and last monthly reading

Table 2: Summary of Manual Groundwater Measurements



BH Ref	Water Level (m) [RL m AHD)	Date of Reading	Comments
	(4.5) [89.1]	26/09/22	Day of well installation and after purging.
	(5.0) [88.6]	29/09/22	21 days after purging.
BH104	(4.7) [88.9]	11/07/2023	1 st monthly reading
-	(4.7) [88.9]	11/08/2023	2 nd monthly reading
	(4.6) [89.0]	12/09/2023	3 rd and last monthly reading
	(5.0) [93.1]	26/09/22	Day of well installation and after purging.
	(5.1) [93.0]	29/09/22	3 days after purging.
BH105	(5.4) [92.7]	11/07/2023	1 st monthly reading
	(5.1) [93.0]	11/08/2023	2 nd monthly reading
	(10.0) [51.6]	12/09/2023	3 rd and last monthly reading

Table 3: Continued: Summary of Manual Groundwater Measurements

The continuous ground water level readings captured by the data loggers between 16/05/2023 and 12/09/2023 are presented within Appendix C of this report. The daily rainfall is also included. These readings are summarised in Table 4 below.



Derehole	Groundwater Readings (m) [RL m AHD]			
Borehole	Shallowest	Deepest	Mean	Range (m)
DU 14.0.2	(10.7)	(6.2)	(6.6)	4 5
BH103	[85.3]	[89.8]	[89.4)	4.5
BL104	(5.3)	(4.5)	(4.7)	0.9
BH104	[88.3]	[89.1]	[88.9]	0.8
DUMOS	(6.4)	(6.0)	(6.2)	0.4
BH105	[91.7]	[92.1]	[91.9]	0.4

Table 4: Summary of Continuous Groundwater Readings (Data-loggers)

Note: Data excluded if interpreted to be influenced by the removal of water as part of the hydraulic conductivity testings

Permeability Testing 4.3

To estimate the rock mass hydraulic conductivity (or "permeability"), rising head permeability tests were carried out in BH103 and BH105 and a water pressure (packer) test was carried out in BH104. The tests were carried out between 18 May 2023 and 8 June 2023.

The rising head permeability test involves removing water and measuring the changes in water level within the well at regular time intervals. The packer test involves pumping water into the rock formation below a packer at various pressure. The results of the permeability tests using Hvorslev's (1951) method (rising head test) and packer tests are summarised in Table 5 below, with the full reports provided in Appendix F.

Table 5: Hydraulic Conductivity Test Results			
Borobolo	Test Zone Donth (m)	Estimated Hy	

Borehole	Test Zone Depth (m)	Estimated Hydraulic Conductivity (k) (m/s)	Estimated Hydraulic Conductivity (k) (m/day)
BH103	11.6 - 30.57	1.7 x 10 ⁻⁷	0.015
BH104*	5.8 - 18.8	3.3 x 10 ⁻⁷	0.029
BH105	10.3 - 23.31	3.0 x 10 ⁻⁷	0.026

* upper bound value recorder for packer test in Hawkesbury Sandstone

4.4 Surface Waters, Groundwater Dependent Ecosystems & Groundwater Extraction **Bores**

The surface water sources in the vicinity of the site include Berry's Creek which is located about 900 m west of the site and Flat Rock Creek with is about 1 km to the north-east. Berry's creek is a tributary to the Lane Cove River which is situated approximately 1400 m southwest of the site. Berry's Creek, which runs into Willoughby Bay, situated approximately 1800 m northeast of the site. No other surface water sources are mapped within 1 km of the site to the north or east.





Reference to the Australian Bureau of Meteorology GDE Atlas indicates that there are no mapped groundwater dependant ecosystems (GDEs) in close proximity to the site.

One groundwater extraction bore was located within 1 km of the site. Details of the bore extracted from the available WaterNSW records are presented within Table 6 below.

Bore Reference	Approximate Location relative to site (m)	Water Bearing Stratum	Approximate Ground surface RL (m AHD) ¹	Standing Water Level	Approximate Water Level RL (m AHD)
GW108224	960 m NW	Sandstone	72	35	37

Table 6:	WaterNSW	Groundwater	Extraction Bores
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Note: ¹ Ground surface RL inferred from NSW Department of Land 2m contour mapping.

5. Proposed Development

It is understood that the proposed development will include demolition of the existing buildings on site and construction of a mixed-use structure (residential with retail uses) with a 7 level basement, with a finish floor level at RL 74.8 m (refer architectural drawings prepared by Turner attached in Appendix B).

The development is understood to be located partly in the Sydney Metro tunnel second reserve, with the dual tunnels (RT01 and RT02) running beneath the northeastern corner of the site (refer TfNSW "for construction" drawing SMCSWTSE-JAB-TPW-AL-DRG-505123-02 attached in Appendix B). The tunnels are shown to plunge towards the east with the tunnel crown increasing in depth from approximately RL 65 m to RL 63 m. A cross passage is shown between the two tunnels, located just to the north of the site. Both tunnels are shown to be circular with a diameter of approximately 7.05 m (refer sheet 2 to 4 of drawing 3050-01019-001-002-02, prepared by Stantec, attached in Appendix B). It is understood that the tunnel is fully tanked.

6. Groundwater Modelling

6.1 Methodology

A 3-dimensional (3D) numerical groundwater model was developed for the site. The modelling was carried out using the 3D finite element software PLAXIS 3D (V22).

Information from the investigations on the site and surrounding area were used to construct a conceptual hydrogeological model for the site, which was represented in the multi-layered numerical model, prepared for the site.



6.2 Boundary Conditions and Hydraulic Parameters

To limit boundary interference, the model boundaries were set approximately 150 m from the site. The ground surface was modelled to simulate the slope to the southeast.

The proposed development is located within an urban setting, mostly covered by pavements and commercial buildings, with only minor gardens. As such, a net infiltration rate of 2% of the 2 m annual rainfall was assigned.

The constant head far-field boundary conditions (upslope to the west and downslope to the east) were calibrated to generate a hydraulic head matching the measured head of approximate RL 93 m at the upstream end of the basement, and approximately RL 89 m at the downstream end. The pore pressures along the north and south boundary were not fixed (allowed to change – no flow through boundary).

The geological units were subdivided into layers corresponding to the soil and rock units described in the geological model. The permeability for each model unit adopted is summarised in Table 7. The horizontal permeabilities (k_h) of the Hawkesbury Sandstone and shale/siltstone adopted was based on the highest value from the in-situ permeability testing results (consistent with parameters proposed by Bertuzzi and Pells (2002)¹). Soils permeability was based on published literature.

Considering the nature of horizontally bedded massive sandstone, the ratio of vertical to horizontal permeability (k_v/k_h) of the Hawkesbury Sandstone was assigned to be 0.2. For the more fractured shale and siltstone, however, a ratio of 0.5 was used.

Model Layer	Geological Unit	Base of Layer (RL m)	Porosity	Typical Horizontal Hydraulic Conductivity k _h (m/sec)	kv∕kh
1	Fill/Residual Soil	95-88*	0.5	1.0 x 10 ⁻⁶	1.0
2	Shale/Siltstone	81	0.2	3 x 10 ⁻⁷	0.5
3	Hawkesbury Sandstone	50**	0.05	3.3 x 10 ⁻⁷	0.2

 Table 7: Model Layer Summary

Note: * range provided – base of the layer follows topography

** base of model

6.3 Basement Shoring Wall and Dewatering

No detailed on the shoring design were available at the time of preparing this report. It is assumed that the basement shoring wall will comprise 'non-watertight' soldier piles with shotcrete infill panels. The strip drains to be installed behind the shotcrete will essentially direct all groundwater, through the basement subfloor drainage system, to the sump (i.e., the basement is assumed to be drained in the long term).

¹ Bertuzzi, R. and Pells, P.J.N (2002), Geotechnical Parameters of Sydney Sandstone and Shale. Australian Geomechanics, Vol 37, No 5, December 2002.

To allow the construction works, a proposed bulk excavation level at RL 74 m was assumed. This level corresponds to a depth of approximately 0.8 m below the lowest finished floor level, taking into account slab thickness, locally deepened excavations for a sump and pump system, footings, etc.



The subsurface strata intersected by the basement excavation is shown in Figure 1 below.

Figure 1: View of Model Ground Conditions

It has been assumed in the model that any seepage into the basement will be collected and pumped out of the basement.

6.4 Groundwater Modelling Simulations

To simulate temporary dewatering required during construction, the transient flows over time were modelled. For the purpose of the analysis, excavation was undertaken in a single stage (i.e., "whished into place"). The subsequent temporary dewatering period was assumed to be one year, subdivided into multiple time intervals. The analysis was also run under 'steady state' conditions for the long term (i.e., fully drained basement).

Sensitivity analyses were undertaken to assess the impact of higher permeabilities for the shale and siltstone (refer Table 9 for values of k_h used). The sensitivity analysis also included the effect of the basement excavation intersecting a high permeability seam.



6.5 Groundwater Modelling Results

The inflow rates provided in this report represent the estimated total rate of groundwater flowing into the excavation and the volume (per unit time) requiring extraction via the dewatering system in order to dewater the basement excavation during construction and in the long term.

The estimated inflows from the analysis for the first year (i.e., during construction) and in the long term are summarised in:

- Table 8, for the baseline case as detailed in previous sections; and
- Table 9, for the sensitivity cases considering higher permeability for the shale and siltstone.

	Baseline Case			
Elapsed Time	L/min	m ³ /day	Cumulative Inflow (ML)	
1 day	91	131	0.1	
3 days	89	128	0.4	
7 days	88	126	0.9	
14 days	86	124	1.8	
30 days	83	120	3.7	
60 days	79	113	7.2	
120 days	70	101	13.7	
240 days	61	87	25.0	
365 days	55	79	35.4	
Long to me	L/min	m3/day	Annual Inflow (ML)	
Long term	37	53	19.2	

 Table 8: Simulated Inflow Results for Baseline Case

Table 9: Simulated Inflow Results for Sensitivity Cases

	k _h (m/sec)	Maximum Inflow		Annual
Case	Shale and Siltstone	(L/min) *	Long Term Inflow (L/min)	Annual Inflow (ML)
Baseline	3 x 10 ⁻⁷	91	37	19.2
Higher Permeability for Shale and Siltstone	1 x 10 ⁻⁶	162	58	30.3

Note: * simulation results at the 1^{st} day.

The results of the baseline groundwater inflow analysis indicate that inflow of about 35 ML in the first year of construction is predicted, which reduces to about 19 ML/year in the long term.



The inflow rate presented above is a prediction only and may vary significantly depending on the assumptions presented. The actual flow rate will only be known once the excavation has been completed and the inflow measured. Appropriate planning should be in place to monitor and compensate for inflows different to than that predicted by the assessment.

It should be noted that the predictions obtained from the PLAXIS 3D analysis is based on permeability estimates obtained from testing in the boreholes. The permeability test results can vary significantly between the boreholes. Also, the results are only indicative of the rock mass around the borehole. For inflow analysis conservative permeability values are used (highest permeability). Therefore, actual inflows can be substantially less than those predicted in the analysis, especially if the underlying Hawkesbury sandstone is of lower permeability than used in the model.

6.6 Drawdown Estimates

The simulated lowered groundwater levels, or impact to the water table, outside the excavation are shown in Figure 2 and Figure 3.

The model results indicate a maximum drawdown of about 14 m adjacent to the excavation, which reduces and extends to the model boundary (i.e., 150 m from the excavation).



Figure 2: Groundwater Head Contour through Excavation in Northwest-Southeast Direction





Figure 3: Simulated Groundwater Drawdown Levels

Based on the investigation results, groundwater drawdown occurs within the rock units around the perimeter of the site. Accordingly, the drawdown is not expected to impact any surrounding sites.

7. Groundwater Quality

DP (2023b) identified potential sources of contamination that may impact on groundwater quality beneath the site, including contaminated filling, on-site and nearby commercial activities including motor garages, associate car service centres and dry cleaners; and underground features including grease traps.

In order to assess the current groundwater contamination status at the site and evaluate whether historical / current / off-site land uses have impacted on groundwater, groundwater sampling was conducted from three groundwater monitoring wells (BH103, BH104 and BH105) installed as part of DP (2023b).

Groundwater wells BH103 and BH105 were sampled on 20 June 2023, whilst groundwater well BH104 was sampled on 22 June 2023. Groundwater samples including a replicated sample were collected using a low flow peristatic pump via the micro-purge (minimal drawdown) method.

Groundwater samples were tested for a range of potential contaminants including: heavy metals (arsenic, cadmium, chromium, copper, lead, mercury, nickel, zinc), total recoverable hydrocarbon (TRH), polycyclic aromatic hydrocarbons (PAH), benzene, toluene, ethyl benzene (BTEX), organochlorine pesticides (OCP), organophosphorus pesticides (OPP), polychlorinated biphenyls (PCB), phenols and per-and polyfluoroalkyl substances (PFAS). In addition, groundwater samples were



also tested for total dissolved solids (TDS), total suspended solids (TSS), oil and grease and iron to assist in establishing groundwater characterisation needed as part of this DMP.

The following key guidelines and reference documents were consulted for deriving the assessment criteria for groundwater quality at the site:

- NEPC National Environment Protection (Assessment of Site Contamination) Measure 1999 (as amended 2013) [NEPM] (NEPC, 2013);
- ANZG Australian and New Zealand Guidelines for Fresh and Marine Water Quality (ANZG, 2018);
- CRC CARE Health screening levels for petroleum hydrocarbons in soil and groundwater (CRC CARE, 2011); and
- HEPA PFAS National Environmental Management Plan (NEMP) (HEPA, 2020).

The results of the laboratory testing on groundwater samples are summarised in Table J3 (extracted from DP, 2023b) in Appendix F. The relevant assessment criteria are slow shown on Table J3. The laboratory test results certificates are also included in Appendix F.

DP (2023b) concluded the following:

- All analytical results for groundwater samples were below the site adopted assessment criteria for freshwater and health screening level adopted for the site for TRH, BTEX, PAH, OCP/OPP, PCB, phenols and PFAS;
- Metals concentrations (dissolved and total) exceeded the assessment criteria in all samples for zinc;
- Metals concentrations (dissolved and total) exceeded the assessment criteria in sample BH104 for cadmium, chromium, copper and lead; and
- Metals concentration (dissolved and total) exceeded the assessment criteria in sample BH105 for copper.

However, these detected concentrations are likely to be representative of regional conditions and are often found in urban environments where there are impacts associated with water supply and waste water infrastructure.

The inorganics concentrations for TSS, TDS and iron were elevated. Given the metals concentrations discussed above, and the elevated inorganics concentrations, it was considered likely that any form of dewatering would require treatment of the groundwater prior to stormwater or sewer disposal to meet the relevant criteria.

DP (2023b) also provided comment that, according to 1:25,000 Acid Sulfate Soil Risk map, the site is not located at or near an area associated with a risk of acid sulphate soils.



8. Groundwater Disposal and Council Requirements

All collected groundwater requiring disposal will need to be tested against the requirements of the receiving authority. For example, disposal to stormwater will require Council approval and be subject to their water quality requirements for discharge to stormwater.

Ongoing monitoring of groundwater quality will be required to check that the groundwater quality complies with the nominated criteria for disposal. Suggested monitoring and reporting requirements are given in Section 10.

Where groundwater does not comply with the nominated requirements some form of groundwater treatment will be required prior to disposal. The treatment system should be determined and adjusted based on the groundwater test results prior to disposal and may include a combination of the following:

- Use of settlement tanks with addition of a flocculation agent to control heavy metals and suspended solids;
- Use of carbon filters to control hydrocarbons; and
- Use of specialist treatment systems to control heavy metals and hydrocarbons.

DP consider that, where there is an absence of Council-provided water quality criteria, water quality data should be compared to the following criteria (including the criteria reference in Table 10) for the purpose of discharging to stormwater:

- Physical parameters (pH, conductivity, turbidity, TSS) based on requirements of (NHRMC, 2008), ANZECC (2000) and (Landcom, 2004);
- Aesthetics: the water should be free from floating debris; oil, scum and other matter; and substances producing objectionable colour, odour or turbidity; and
- Chemical contaminants: default guideline values (DGV) for the protection of freshwater ecosystems from ANZG (2018) and HEPA (2020). DGV should be for a 95% level of protection or, for bioacculmulative contaminants or to protect against species with risk of chronic toxicity, a 99% level of protection.

Analyte / Parameter	Screening value (µg/L unless otherwise stated)
I	Metals / Metalloids
Arsenic (III) / (V)	24 / 13
Cadmium	0.2
Chromium (III) / (VI)	3.3 / 1
Copper	1.4
Lead	3.4
Mercury (inorganic)	0.06
Nickel	11
Zinc	8

Table 10: Nominated groundwater quality criteria



Analyte / Parameter	Screening value
Analyte / Farameter	(μg/L unless otherwise stated)
	BTEX
Benzene	950
Toluene	180
Ethylbenzene	80
m-Xylene	75
o-Xylene*	350
p-Xylene*	200
	РАН
Naphthalene	2.5
B(a)P	0.1
Anthracene	0.4
Phenanthrene	2.0
Fluoranthene	1
TRH and VOC	Laboratory practical quantification limit as initial screen.
	Phenols
Phenol	320
	OCP
Aldrin	1
DDT	0.006
Endrin	0.01
Heptachlor	0.01
Hexachlorobenzene	0.05
Lindane	0.07
Methoxychlor	0.005
	OPP
Azinphos methyl (Guthion)	0.02
Chlorpyrifos	0.01
Diazinon	0.01
Dimethoate	0.01
Fenitrothion	0.1
Malathion	0.05
Parathion	0.0007



Analyte / Parameter	Screening value (µg/L unless otherwise stated)
	РСВ
Arochlor 1242	0.3
Aroclor 1254	0.01
PFAS	
PFOS	0.00023
PFOA	19
Physic	ochemical Parameters
Conductivity	200 - 300 μs/cm
рН	6.5 – 8.5 pH units
Dissolved Oxygen	60 - 120 % saturation
Turbidity	50 NTU
Total Suspended Solids	< 50 mg/L

Any drained basement design may require periodic inspections to prevent build up / blockages in the drain systems, e.g. ferrous iron sludge.

In addition, a long-term treatment system is recommended to form part of a contingency plan in the design of drained basement should it be required to facilitate stormwater discharge.

9. Impact Assessment

9.1 Aquifer Interference Policy Considerations

The NSW Aquifer Interference Policy (AIP) indicates that the term "aquifer" is commonly understood to mean a groundwater system that is sufficiently permeable to allow water to move within it, and which can yield productive volumes of groundwater. A groundwater system is defined as any type of saturated geological formation that can yield low or high volumes of water. The site is underlain by shallow fill / soils, then shale and sandstone that is of relatively low permeability with potentially low yield. The groundwater system is therefore considered to be a 'less productive groundwater source' as outlined in the AIP.

Table 1 in Section 3.2.1 of the AIP outlines minimal impact considerations. The AIP indicates that "if predicted impacts are less than the Level 1 minimal impact considerations, then these impacts will be considered as acceptable". The following minimal impact considerations are outlined for less productive porous and fractured rock groundwater sources:

- Less than or equal to 10% cumulative variation in water table 40 m from any high priority GDE or high priority culturally significant site;
- A cumulative pressure head decline of no more than a 2 m at any water supply work; and



Any change in groundwater quality should not lower the beneficial use category of the groundwater source beyond 40 m from the activity.

9.2 **Risk Assessment**

An assessment of the potential effects of dewatering on neighbouring properties and groundwater dependent ecosystems has been summarised in Table 11.

	Table 11: Assessment of Potential Effects of Dewatering.			
	ltem	Comment		
	Proximity of Groundwater Dependent Ecosystems (GDEs)	The closest water course is Berrys Creek, located 900 m west of the site. Drawdown impacts to GDEs are unlikely.		
	Water Supply Losses by neighbouring groundwater users	A review of registered bores within a 500 m radius of the surrounding site was undertaken. The search identified no extraction bores within the search area.		
	Potential Subsidence of neighbouring structures	The groundwater drawdown is expected to occur within bedrock. Settlements on adjacent structures due to the drawdown in rock would be expected to be negligible.		
	Mounding of water upgradient of structure	The basement is designed to be drained. Due to the drained basement induced mounding due to drained basement is expected to be unlikely.		

10. Monitoring and Reporting Requirements

10.1 Monitoring and reporting requirements

The following monitoring programme and associated reporting outlined in Table 12 below is suggested during excavation and construction works on-site, assuming a continuous dewatering process.

ltem	Monitoring Required	Monitoring Frequency, Reporting and Notes	Reporting
Assess effect of works on groundwater levels	Installation of 3 groundwater wells outside the excavation perimeter (including at least one upgradient) and subsequent measurement of groundwater levels would be required.	Base reading two weeks after installation. Once excavation reaches water table carry out weekly monitoring. Continue weekly monitoring two weeks after completion of bulk excavation level. Then monitor monthly or as advised by the geotechnical engineer until the water level differences reduce to acceptable levels. Preferably dataloggers should be installed.	Weekly then monthly

Table 12: Monitoring and Reporting Requirements



ltem	Monitoring Required	Monitoring Frequency, Reporting and Notes	Reporting
Quantity of water disposed off-site	Calibrated Flowmeter connected to any pump-out system.	Continuous monitoring of pump-out volumes. Inclusion of results in a final water quality monitoring report (i.e., as outlined in a DMP)	Weekly
Visual Inspection	No visible oil and grease, 'sheen' and / or no significant discolouration or odours If any of the above signs are noted, then any discharge will be suspended until further analytical testing is completed.	Inspections daily where accessible (e.g. holding tanks, wells, discharge points).	
Routine Water Quality Sampling and Testing (Assuming Continuous treatment)	Sample collection will be based on the dewatering method to be used. In general, samples are to be collected from both water entering the system and water following treatment. Contaminant and physical properties tested to be nominated by the authority accepting water but to include: Metals (total and dissolved); TRH; BTEX; PAH; Conductivity; pH; Dissolved Oxygen; Turbidity; Total dissolved solids; Major cation / anions / sodium absorption ratio / hardness;	Samples collected initially daily (first week) and then weekly. Results to be compared against criteria in Section 8. Physical parameters (pH, dissolved oxygen, turbidity and conductivity) may be monitored using suitable on-site probes / testing kits once correlations are established with analytical results. Based on ongoing review of results the scope (and/or need) of inlet water testing, and the scope of outlet testing may be reduced, i.e., once the treatment system has been assessed as adequate for the range of contaminants detected. Inclusion of results in a final water quality monitoring report (i.e., the dewatering completion report).	Weekly



ltem	Monitoring Required	Monitoring Frequency, Reporting and Notes	Reporting				
	 Major nutrients (ammonia, nitrate, N and P); and 						
	Faecal coliforms and e.coli						
Construction Dewatering Completion Report		qualified consultant upon completion of con- ubmitted to Council. The summary report w tion and:					
Кероп	• Any on-site records kept by the contractor (e.g., visual observations, any unexpected finds records etc.);						
	• All analytical results (i.e., each batch of water disposed) compared against the adopted screening criteria;						
	Quality control testing;						
	Record of water disposed (i.e., for each disposal event); and						
		ected finds or non-conformances, and / or or ve complied with this DMP.	therwise if				

Note: Testing frequency and analysis requirements may be reviewed in consultation with the environmental consultant dependent upon ongoing results.

10.2 Long-term monitoring

Monitoring for potential long-term impacts from the drained basement design is recommended to include the following:

- Monthly in-situ field water quality measurements using a calibrated portable water quality meter for both groundwater and discharge water (ie, from any pump out point / drains) for the following:
 - o Electrical conductivity, temperature, pH and redox potential;
- If identified during the construction dewatering phase as a potential contaminant issue, additional analytical testing for specific contaminants of concern;
- Monthly meter readings of discharge volumes / flowrates. In this regard automated readings are recommended; and
- Preparation of an annual report to the approval authority.

Groundwater quality monitoring frequency during long-term monitoring may be considered to be reduced based on both the results of the construction dewatering monitoring and / or initial long-term monitoring results, eg, reduction to quarterly or bi-annual.

Requirements for long-term monitoring are recommended to be incorporated into a building management plan for the property.



10.3 Contingency plan

As per Section 10.1, at any hold point if any non-conformance is encountered then dewatering will be suspended. The following general contingency plan will be enacted:

- Notify the Site Manager / Contractor and the Geotechnical / Environmental Consultant (as relevant);
- Environmental Consultant to inspect the site / unexpected finds and collect additional water quality samples as advised;
 - o If required, notification to the approval authority / NSW EPA in the event of a potential contaminant release to groundwater;
- Should water quality be deemed unsuitable for disposal, suspend dewatering and treat water prior to discharge. If on-site treatment cannot meet the required discharge criteria then a contingency strategy of off-site disposal as liquid waste may need to be adopted until the on-site treatment system can be modified / adjusted;
- Should dewatering volumes be higher than predicted or higher than discharge limits provided by relevant authorities, suspend construction and reduce pumping rates. Options may include lowering to 0.5 m below BEL, reduced pumping rates, or staged basement construction; and
- Written confirmation by the Consultant that disposal may resume (e.g., upon receipt of laboratory results).

11. Comments

Based on the results of the analysis, the groundwater inflow is sensitive to permeability of the shale and siltstone. Increased inflows may therefore occur if permeable shale and siltstone layers are intersected.

If required, further testing can be carried out to obtain additional information on the permeability of the shale and siltstone. This could include further testing in the existing wells over an extended period to establish if the bores will continue to yield over time, or if they are likely to dry up. Additional wells outside the excavation footprint may be required for longer term monitoring. This may be required as the existing wells could be damaged during demolition / excavation works. These wells may also be used for further testing.

The predicted lowered groundwater levels extend to the model boundaries. This indicates that the extent of the drawdown may be slightly underestimated in the far field. The predicted inflow, on the other hand, may be overestimated.

Based on the inflow estimate of over 3 ML/year, the proposed drained basement requires a Water Access License and a Water Supply Works Approval from WaterNSW, assuming that the groundwater take is approved.

The selection of an appropriate strategy for basement design should include consideration of the regulatory risks (i.e., whether or not the necessary approvals and licenses can be obtained, or conditions of consent become too onerous), construction stage risks (e.g. excessive costs or delays due to



grouting, groundwater management, dewatering or design changes), long-term risks (e.g. cost of ongoing groundwater management/licenses), as well as the known costs of design and construction.

12. References

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NEPC. (2013). National Environment Protection (Assessment of Site Contamination) Measure 1999 (as amended 2013) [NEPM]. Australian Government Publishing Services Canberra: National Environment Protection Council.

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NHMRC, NRMMC. (2022). Australian Drinking Water Guidelines 6 2011, Version 3.8 updated Sept 2022. Canberra: National Health and Medical Research Council, National Resource Management Ministerial Council.

NHRMC. (2019). *Guidance on Per and Polyfluoroalkyl substances (PFAS) in Recreational Water.* Canberra: National Health and Medical Research Council.

13. Limitations

Douglas Partners (DP) has prepared this report (or services) for this project at Falcon Street, Crows Nest in accordance with DP's proposal 86645.03.P.002.Rev0 dated 5 May 2023 and acceptance received from Greg Colbran dated 10 May 2023. The work was carried out under DP's Conditions of Engagement. This report is provided for the exclusive use of Deicorp Pty Ltd for this project only and for the purposes as described in the report. It should not be used by or relied upon for other projects or purposes on the same or other site or by a third party. Any party so relying upon this report beyond its exclusive use and purpose as stated above, and without the express written consent of DP, does so entirely at its own risk and without recourse to DP for any loss or damage. In preparing this report DP has necessarily relied upon information provided by the client and/or their agents.



The results provided in the report are indicative of the sub-surface conditions on the site only at the specific sampling and / or testing locations, and then only to the depths investigated and at the time the work was carried out. Sub-surface conditions can change abruptly due to variable geological processes and also as a result of human influences. Such changes may occur after DP's field testing has been completed.

DP's advice is based upon the conditions encountered during this investigation. The accuracy of the advice provided by DP in this report may be affected by undetected variations in ground conditions across the site between and beyond the sampling and / or testing locations. The advice may also be limited by budget constraints imposed by others or by site accessibility.

The assessment of atypical safety hazards arising from this advice is restricted to the (geotechnical / environmental / groundwater) components set out in this report and based on known project conditions and stated design advice and assumptions. While some recommendations for safe controls may be provided, detailed 'safety in design' assessment is outside the current scope of this report and requires additional project data and assessment.

This report must be read in conjunction with all of the attached and should be kept in its entirety without separation of individual pages or sections. DP cannot be held responsible for interpretations or conclusions made by others unless they are supported by an expressed statement, interpretation, outcome or conclusion stated in this report.

This report, or sections from this report, should not be used as part of a specification for a project, without review and agreement by DP. This is because this report has been written as advice and opinion rather than instructions for construction.

Douglas Partners Pty Ltd

Appendix A

About This Report



Introduction

These notes have been provided to amplify DP's report in regard to classification methods, field procedures and the comments section. Not all are necessarily relevant to all reports.

DP's reports are based on information gained from limited subsurface excavations and sampling, supplemented by knowledge of local geology and experience. For this reason, they must be regarded as interpretive rather than factual documents, limited to some extent by the scope of information on which they rely.

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This report is the property of Douglas Partners Pty Ltd. The report may only be used for the purpose for which it was commissioned and in accordance with the Conditions of Engagement for the commission supplied at the time of proposal. Unauthorised use of this report in any form whatsoever is prohibited.

Borehole and Test Pit Logs

The borehole and test pit logs presented in this report are an engineering and/or geological interpretation of the subsurface conditions, and their reliability will depend to some extent on frequency of sampling and the method of drilling or excavation. Ideally, continuous undisturbed sampling or core drilling will provide the most reliable assessment, but this is not always practicable or possible to justify on economic grounds. In any case the boreholes and test pits represent only a very small sample of the total subsurface profile.

Interpretation of the information and its application to design and construction should therefore take into account the spacing of boreholes or pits, the frequency of sampling, and the possibility of other than 'straight line' variations between the test locations.

Groundwater

Where groundwater levels are measured in boreholes there are several potential problems, namely:

 In low permeability soils groundwater may enter the hole very slowly or perhaps not at all during the time the hole is left open;

- A localised, perched water table may lead to an erroneous indication of the true water table;
- Water table levels will vary from time to time with seasons or recent weather changes. They may not be the same at the time of construction as are indicated in the report; and
- The use of water or mud as a drilling fluid will mask any groundwater inflow. Water has to be blown out of the hole and drilling mud must first be washed out of the hole if water measurements are to be made.

More reliable measurements can be made by installing standpipes which are read at intervals over several days, or perhaps weeks for low permeability soils. Piezometers, sealed in a particular stratum, may be advisable in low permeability soils or where there may be interference from a perched water table.

Reports

The report has been prepared by qualified personnel, is based on the information obtained from field and laboratory testing, and has been undertaken to current engineering standards of interpretation and analysis. Where the report has been prepared for a specific design proposal, the information and interpretation may not be relevant if the design proposal is changed. If this happens, DP will be pleased to review the report and the sufficiency of the investigation work.

Every care is taken with the report as it relates to interpretation of subsurface conditions, discussion of geotechnical and environmental aspects, and recommendations or suggestions for design and construction. However, DP cannot always anticipate or assume responsibility for:

- Unexpected variations in ground conditions. The potential for this will depend partly on borehole or pit spacing and sampling frequency;
- Changes in policy or interpretations of policy by statutory authorities; or
- The actions of contractors responding to commercial pressures.

If these occur, DP will be pleased to assist with investigations or advice to resolve the matter.

About this Report

Site Anomalies

In the event that conditions encountered on site during construction appear to vary from those which were expected from the information contained in the report, DP requests that it be immediately notified. Most problems are much more readily resolved when conditions are exposed rather than at some later stage, well after the event.

Information for Contractual Purposes

Where information obtained from this report is provided for tendering purposes, it is recommended that all information, including the written report and discussion, be made available. In circumstances where the discussion or comments section is not relevant to the contractual situation, it may be appropriate to prepare a specially edited document. DP would be pleased to assist in this regard and/or to make additional report copies available for contract purposes at a nominal charge.

Site Inspection

The company will always be pleased to provide engineering inspection services for geotechnical and environmental aspects of work to which this report is related. This could range from a site visit to confirm that conditions exposed are as expected, to full time engineering presence on site.

Appendix B

Provided Drawings



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Ground Level

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Rev. B _	14.0	5.20		







Basement 07

PP-110-008 1:500, 1:200 @ A3 ______5 ____10 ____15m Rev. B _ 14.05.20



BULK EXCAVATION LEVELS FOR SLAB ON GROUND ALLOWS FOR SLAB THICKNESS AS NOTED ON BASEMENT PLANS AND A 50mm BLINDING LAYER. REFER WATER PROOFING CONTRACTORS DETAILS IF ADDITIONAL BLINDING LAYER IS REQUIRED. REFER BASEMENT PLANS FOR PILE CAPS & FOOTINGS. HYDRAULIC ENGINEER TO ADVISE ANY ADDITIONAL SUBSOIL DRAINAGE REQUIREMENTS.

NOTE: GROUND LEVEL SHOWN ON ELEVATIONS ARE APPROXIMATE ONLY AND NEED TO BE CONFIRMED ON SITE BY THE SURVEYOR

NOTE: ROCK LEVEL SHOWN ON ELEVATIONS ARE APPROXIMATE ONLY AND NEED TO BE CONFIRMED ON SITE BY THE GEOTECHNICAL ENGINEER

BULK EARTHWORK NOTES:

GEOTECHNICAL REPORT: REFER TO GEOTECHNICAL REPORT PREPARED BY EI AUSTRALIA, CONTRACTOR IS TO ENSURE GEOTECHNICAL REPORT RECOMMENDATIONS ARE ADHERED TO.

<u>SITE SURVEY:</u> THE SITE HAS BEEN SURVEYED BY DAW & WALTON PTY LTD. REFER DRAWINGS FOR DETAILS. THIS IS A COMPILATION OF ENGINEERING AND SITE SURVEY DRAWING, DEPICTING SITE EARTHWORKS OVER THE SURVEY DRAWING.

<u>SPECIFICATION:</u> THESE NOTES ARE TO BE READ IN CONJUNCTION WITH THE HEAD SPECIFICATION.

EROSION AND SEDIMENT CONTROL: ALLOW TO SUBMIT AND EROSION AND SEDIMENT CONTROL (ESC) PROGRAM TO GOLD COAST CITY COUNCIL FOR ENDORSEMENT PRIOR TO SITE WORKS COMMENCING. THE ESC PROGRAM IS TO COMPLY WITH THE COUNCILS EROSION AND SEDIMENT CONTROL STANDARD (VERSION 9 OR LATER) AND IS TO BE CERTIFIED BY A REGISTERED PROFESSIONAL ENGINEER OR QUEENSLAND - CIVIL OR CERTIFIED PROFESSIONAL IN EROSION AND SEDIMENT CONTROL.

DUST CONTROL: THE CONTRACTOR IS TO ENSURE THAT THE DUST PREVENTION METHODS HE ADOPTS ARE SUFFICIENT TO MEET THE REQUIREMENTS OF THE ENVIRONMENTAL PROTECTION REGULATION 1998 PART 2A, ENVIRONMENTAL NUISANCE. IT IS THE CONTRACTORS RESPONSIBILITY TO ACQUAINT HIMSELF WITH THE REQUIREMENTS.

SITE SETOUT: REFER TO ARCHITECTS DRAWINGS FOR THE ACCURATE SETOUT OF ALL BUILDINGS, DRIVEWAYS, PARKING AREAS ETC. NOTE BULK EARTHWORKS PLAN IS INDICATIVE ONLY. CALCULATE AND CUT BATTERS FROM ARCHITECTS PLANS AND SURVEY. CROSSOVER PROFILES TO COUNCIL REQUIREMENTS.

GENERALLY: PROCEED WITH BULK EARTHWORKS AND SHORING TO PROVIDE A STABLE SUBGRADE AND WORK SPACE FOR THE CONSTRUCTION OF THE PROPOSED DEVELOPMENT. STRIP AND DISPOSE OF TOPSOIL, REDUCE SITE TO LEVELS INDICATED AND DISPOSE OF ALL UNWANTED MATERIAL LEGALLY. SUPERVISION:

A GEOTECHNICAL ENGINEER IS TO PROVIDE LEVEL 1 SUPERVISION (AS3798) FOR ALL EARTHWORKS DURING THE COURSE OF CONSTRUCTION. AT THE COMPLETION OF THE BULK EXCAVATION CONTRACT, THE GEOTECHNICAL ENGINEER IS TO PROVIDE CERTIFICATION THAT THE WORKS HAVE BEEN CARRIED OUT IN ACCORDANCE WITH BULK EARTHWORKS SPECIFICATIONS.

BULK EARTHWORKS PROCEDURE AND SPECIFICATION: THE SITE IS TO BE STRIPPED OF TOPSOIL AND UNCONSOLIDATED EXISTING FILL. AT THE COMPLETION OF THE BULK EARTHWORKS, THE CONTRACTOR SHALL PROVIDE TEMPORARY OR PERMANENT DRAINAGE TO ENSURE NO SURFACE WATER IS RETAINED ON THE SITE, OR THAT SURFACE WATER FLOW DETRIMENTALLY SCOURS THE PREPARED BASE.

GEOTECHNICAL ENGINEER NOTES: EXCAVATION TO BE CARRIED OUT UNDER GEOTECHNICAL ENGINEERS SUPERVISION. GEOTECHNICAL ENGINEER (GE) TO COMMENT ON SUITABILITY OF THE SUBCONTRACTORS METHOD OF EXCAVATION AS REMOVAL PROCEEDS.

HYDRAULICS ENGINEER: DURING EXCAVATION COORDINATE WITH ALL HYDRAULIC ENGINEERS REQUIREMENTS FOR SEWER, GAS AND STORMWATER LINES.

AS-BUILT DRAWING: PROVIDE AND AS-BUILT DRAWING PREPARED BY A REGISTERED SURVEYOR TO CONFIRM BULK EARTHWORKS IS COMPLETED TO REQUIRED DIMENSIONS AND LEVELS.

<u>DILAPIDATION REPORT:</u> THE APPROVED SHORING WALL CONTRACTOR SHALL PREPARE A DILAPIDATION REPORT OF STREET, FOOTPATH AND ROAD FEATURES PRIOR TO INSTALLATION OF SHORING WALL.

COMPACTION NOTES: COMPACTION BEHIND INTERNAL FORMED RETAINING WALL BY EXCAVATION CONTRACTOR USING HAND HELD RAMMERS TO ACHIEVE 98% MODIFIED DENSITY. COMPACT IN MAXIMUM 300mm THICK LAYERS AT OPTIMUM MOISTURE CONTENT OF ± 3%.

LEGEND: B.E.L. - DENOTES BULK EXCAVATION LEVEL E.L. - DENOTES DETAILED EXCAVATION LEVEL

PROJECT: FIVEWAYS CROWS NEST 391/423 PACIFIC HIGHWAY	JOB NUMBER: 23012	DRG NUMBER:		
CROWS NEST NSW 2065	DESIGNED BY:	DATE:		
SITE RETENTION PLAN	DRAWN BY: RCL	SCALE: 1:100 @ A0	SIZE: A0	REV: P2

THEWALLSWA

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PRELIMINARY ISSUE	-			
		P2	09.06.23	ISSUED FOR PRELIMINARY INFO
NOTE: DO NOT SCALE OFF DRAWINGS. REFER TO		P1	22.05.23	ISSUED FOR PRELIMINARY INFO
ARCHITECTURAL PLANS. VERIFY DIMENSIONS ON SITE.		REV	DATE	REVISION DESCRIPTION

SHORING SURCHARGE LOADING PLAN SCALE 1:200

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SHORING WALL SW2



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without the written permission of ABC Consul



CLIENT:





20kPa SURCHARGE AFTER INSTALLATION OF FIRST ANCHOR

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'LO' DENOTES LOCK OFF LOAD 'LO' DENOTES LOCK OFF LOAD <u>SHORING ANCHOR NOTES:</u> BOND LENGTH NOMINATED IN SHORING ANCHOP PURPOSES ONLY. SHORING CONTRACTOR IS F BOND LENGTHS MAY NEED TO BE VARIED DEP ENCOUNTERED. BOND LENGTH BASED ON A 130mm HOLE WITH	RESPONSIBLE FO ENDING ON SITE	R FINAL ANCHOR DE CONDITIONS	ESIGN.	20	ATCH DENOTES 00 THICK SHOT ETWEEN SHOR	ICRETE		TO BE RE	ENOTES EXPOSE TAINED WITH SH KBOLTS TO GEO R'S DETAILS	OTCRETE																						
NOTE: GROUND LEVEL SHOWN ON ELEVATIONS AR AND NEED TO BE CONFIRMED ON SITE BY TH NOTE: ROCK LEVEL SHOWN ON ELEVATIONS ARE A AND NEED TO BE CONFIRMED ON SITE BY TH ENGINEER MOTE: MAXIMUM 500mm EXCAVATION BELOW ANCH PRIOR TO INSTALLING ANCHOR	IE SURVEYOR PPROXIMATE ON IE GEOTECHNIC	LY		TECHNICAL E IRING EXCAV SHOTCRETE THIS DRAWING -001 - SITE RE	ATION ANE AS REQUI G SHOULD	D NOMINATE IRED TO ENS	APPROPRIA SURE STABIL	TE ROCK BO ITY AT ALL T ON WITH DR	OLTS AND TIMES. AWING								PRELI NOTE: DO NOT S RCHITECTURAL P		VINGS. REFER	TO SITE	P1 22.05.23	ISSUED FOR PRELIN ISSUED FOR PRELIN REVISION DESCRIP	MINARY INFORMATIC		All I The	PYRIGHT rights reserved. ese drawings, plans yright are the prope be used, reproduce hout the written perr	and specifications orty of ABC Consu of or copied wholly nission of ABC Co	s and the Itants and must y or in part onsultants.	CLIENT:	DEICO		Contact Phone: (02) 9746 9201 Email: info@abc-consultants.com.au Web: www.abc-consultants.com.au

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SH4 S01-012	







SHORING KEY PLAN

PROJECT: FIVEWAYS CROWS NEST 391/423 PACIFIC HIGHWAY	JOB NUMBER: 23012	drg number: \$01-005		
CROWS NEST NSW 2065	DESIGNED BY: RC	DATE:		
SHORING WALL ELEVATIONS - SHEET 1	DRAWN BY: RCL	SCALE: 1:100, 1:600 @ A0	size: A0	REV: P2

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SH8 S01-014			S01-014	S01-015 SSL 98.474
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T2	990kN	675kN	30°	11m										
Т3	600kN	400kN	30°	5m										
		LOAD		I3 600kin 400kin 30° 5m 'SWL' DENOTES SAFE WORKING LOAD 'LO' DENOTES LOCK OFF LOAD										

SHORING ANCHOR NOTES: BOND LENGTH NOMINATED IN SHORING ANCHOR SCHEDULE FOR COORDINATION PURPOSES ONLY. SHORING CONTRACTOR IS RESPONSIBLE FOR FINAL ANCHOR DESIGN. BOND LENGTHS MAY NEED TO BE VARIED DEPENDING ON SITE CONDITIONS ENCOUNTERED. BOND LENGTH BASED ON A 130mm HOLE WITH ALLOWABLE BOND STRESS OF 300 kPa.

NOTE: GROUND LEVEL SHOWN ON ELEVATIONS ARE APPROXIMATE ONLY AND NEED TO BE CONFIRMED ON SITE BY THE SURVEYOR

NOTE: ROCK LEVEL SHOWN ON ELEVATIONS ARE APPROXIMATE ONLY AND NEED TO BE CONFIRMED ON SITE BY THE GEOTECHNICAL ENGINEER

NOTE: MAXIMUM 500mm EXCAVATION BELOW ANCHOR HEIGHT PERMITTED PRIOR TO INSTALLING ANCHOR

HATCH DENOTES EXTENT OF 200 THICK SHOTCRETE BETWEEN SHORING PILES

ENGINEER'S DETAILS

GEOTECHNICAL ENGINEER TO INSPECT EXPOSED SHALE FACE REGULARLY DURING EXCAVATION AND NOMINATE APPROPRIATE ROCK BOLTS AND SHOTCRETE AS REQUIRED TO ENSURE STABILITY AT ALL TIMES.

THIS DRAWING SHOULD BE READ IN CONJUNCTION WITH DRAWING S01-001 - SITE RETENTION PLAN FOR SHORING PILE SETOUT DIMENSIONS.

SHORING WALL SW5

HATCH DENOTES EXPOSED ROCK FACE TO BE RETAINED WITH SHOTCRETE AND ROCKBOLTS TO GEOTECHNICAL

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SHORING KEY PLAN SCALE 1 : 600

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Scale 1:50 S01-001



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 SECTION
 SH2

 Scale
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 S01-001



Basement 1 RL 92800

- <u>Basement 3</u> RL 86000

- <u>Basement 4</u> RL 83200

- Basement 5 RL 80400

- Basement 6 RL 77600

- Basement 7 RL 74800

REV: **P2**

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PROJECT: FIVEWAYS CROWS NEST 391/423 PACIFIC HIGHWAY	JOB NUMBER: 23012	drg number:	
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 SECTION
 SH5

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RL 88800 - Basement 3 RL 86000 - Basement 4 RL 83200 - Basement 5 RL 80400 - Basement 6 RL 77600

Ground RL 98100

- Basement 1 RL 92800

- Basement 7 RL 74800

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Basement 1 RL 92800

RL 88800

Basement 3 RL 86000

Basement 4 RL 83200

Basement 5 RL 80400

Basement 6 RL 77600

Basement 7 RL 74800

FIVEWAYS CROWS NEST

391/423 PACIFIC HIGHWAY

CROWS NEST NSW 2065

PROJECT:

Postal Address PO Box 77 NORTH RYDE BC NSW 1670 SHORING WALL SECTIONS - SHEET 3

DRG NUMBER: S01-013

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CROWS NEST NSW 2065	DESIGNED BY:	DATE:		
SHORING WALL SECTIONS - SHEET 4	DRAWN BY: RCL	scale: 1:50 @ A0	size: A0	rev: P2

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PROJECT: FIVEWAYS CROWS NEST 391/423 PACIFIC HIGHWAY	JOB NUMBER: 23012	drg number: S01-015		
CROWS NEST NSW 2065	DESIGNED BY:	DATE:		:13:21 PM
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REFERENCED DRAWINGS

SURVEY - JOB NUMBER 4950-20 REVISION 02 DATE 23-04-20 BY DAW & WALTON CONSULTING SURVEYORS

DESIGN APPROACH BASEMENT DRAWINGS BY TURNER DESIGN APPROACH METRO SECTION DRAWING BY TURNER

SWCSWTSE-JAB-TPW-AL-DRG-505123 REVISION 02 DATE 17-05-19, CLIENT TRANSPORT FOR NSW SYDNEY METRO UNDERGROUND CORRIDOR PROTECTION TECHNICAL GUIDELINES, REFERENCE iCentral SM-20-00081444 VERSION 2 DATE APRIL 2021 BY WSP

PROJECT: FIVEWAYS CROWS NEST 391/423 PACIFIC HIGHWAY	JOB NUMBER: 23012	drg number:		
CROWS NEST NSW 2065	DESIGNED BY:	DATE:		
SITE RETENTION PLAN WITH METRO RAIL TU	NNEL DRAWN BY: RCL	SCALE: 1:200 @ A0	SIZE:	REV: P2

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 <u>Basement 1</u> RL 92800
 <u>Basement 2</u>
<u>Basement 3</u>
 <u>Basement 4</u> RL 83200
 <u>Basement 5</u> RL 80400
 <u>Basement 6</u> RL 77600
 <u>Basement 7</u>

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	<u>Basement 2</u> RL 88800
	<u>Basement 3</u> RL 86000

PROJECT: FIVEWAYS CROWS NEST 391/423 PACIFIC HIGHWAY	JOB NUMBER: 23012	drg number:		
CROWS NEST NSW 2065	DESIGNED BY:	DATE:		
SITE SECTIONS WITH METRO RAIL TUNNEL	DRAWN BY: RCL	scale: 1:200 @ A0	size: A0	REV: P2

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Appendix C

DP Groundwater Well Location Plan and Borehole/Well Logs



NOTE:

- Base image from Metromap (Dated (01.03.2023)
 Base Plan from Stantec, Drawing No.3050-01019-001-002, Revision 02 (Dated 05.05.2023)

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Test Location Plan	
Fiveways, Crows Nest	
391-423 Pacific Hwy, 3-15 Falcon St and 8 Alexander S	3t



Locality Plan

LEGEND

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DP Borehole Location

- EI Australia Borehole Location
- MW Temporary Observation Well

---- Site Boundary



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St, Crows Nest

REVISION:

1

Soil Descriptions

Description and Classification Methods

The methods of description and classification of soils and rocks used in this report are generally based on Australian Standard AS1726:2017, Geotechnical Site Investigations. In general, the descriptions include strength or density, colour, structure, soil or rock type and inclusions.

Soil Types

Soil types are described according to the predominant particle size, qualified by the grading of other particles present:

Туре	Particle size (mm)
Boulder	>200
Cobble	63 - 200
Gravel	2.36 - 63
Sand	0.075 - 2.36
Silt	0.002 - 0.075
Clay	<0.002

The sand and gravel sizes can be further subdivided as follows:

Туре	Particle size (mm)
Coarse gravel	19 - 63
Medium gravel	6.7 - 19
Fine gravel	2.36 - 6.7
Coarse sand	0.6 - 2.36
Medium sand	0.21 - 0.6
Fine sand	0.075 - 0.21

Definitions of grading terms used are:

- Well graded a good representation of all particle sizes
- Poorly graded an excess or deficiency of particular sizes within the specified range
- Uniformly graded an excess of a particular particle size
- Gap graded a deficiency of a particular particle size with the range

The proportions of secondary constituents of soils are described as follows:

In fine grained soils (>	>35% fines)
--------------------------	-------------

Term	Proportion	Example		
	of sand or			
	gravel			
And	Specify	Clay (60%) and		
		Sand (40%)		
Adjective	>30%	Sandy Clay		
With	15 – 30%	Clay with sand		
Trace	0 - 15%	Clay with trace		
		sand		

In coarse grained soils (>65% coarse)

 with clays or silts 	6	
Term	Proportion of fines	Example
And	Specify	Sand (70%) and Clay (30%)
Adjective	>12%	Clayey Sand
With	5 - 12%	Sand with clay
Trace	0 - 5%	Sand with trace

clay

In coarse grained soils (>65% coarse) - with coarser fraction

Term	Proportion	Example		
	of coarser			
	fraction			
And	Specify	Sand (60%) and		
		Gravel (40%)		
Adjective	>30%	Gravelly Sand		
With	15 - 30%	Sand with gravel		
Trace	0 - 15%	Sand with trace		
		gravel		

The presence of cobbles and boulders shall be specifically noted by beginning the description with 'Mix of Soil and Cobbles/Boulders' with the word order indicating the dominant first and the proportion of cobbles and boulders described together.

Soil Descriptions

Cohesive Soils

Cohesive soils, such as clays, are classified on the basis of undrained shear strength. The strength may be measured by laboratory testing, or estimated by field tests or engineering examination. The strength terms are defined as follows:

Description	Abbreviation	Undrained shear strength (kPa)
Very soft	VS	<12
Soft	S	12 - 25
Firm	F	25 - 50
Stiff	St	50 - 100
Very stiff	VSt	100 - 200
Hard	Н	>200
Friable	Fr	-

Cohesionless Soils

Cohesionless soils, such as clean sands, are classified on the basis of relative density, generally from the results of standard penetration tests (SPT), cone penetration tests (CPT) or dynamic penetrometers (PSP). The relative density terms are given below:

Relative Density	Abbreviation	Density Index (%)
Very loose	VL	<15
Loose	L	15-35
Medium dense	MD	35-65
Dense	D	65-85
Very dense	VD	>85

Soil Origin

It is often difficult to accurately determine the origin of a soil. Soils can generally be classified as:

- Residual soil derived from in-situ weathering of the underlying rock;
- Extremely weathered material formed from in-situ weathering of geological formations. Has soil strength but retains the structure or fabric of the parent rock;
- Alluvial soil deposited by streams and rivers;

- Estuarine soil deposited in coastal estuaries;
- Marine soil deposited in a marine environment;
- Lacustrine soil deposited in freshwater lakes;
- Aeolian soil carried and deposited by wind;
- Colluvial soil soil and rock debris transported down slopes by gravity;
- Topsoil mantle of surface soil, often with high levels of organic material.
- Fill any material which has been moved by man.

Moisture Condition – Coarse Grained Soils For coarse grained soils the moisture condition

should be described by appearance and feel using the following terms:

- Dry (D) Non-cohesive and free-running.
- Moist (M) Soil feels cool, darkened in colour.

Soil tends to stick together. Sand forms weak ball but breaks easily.

Wet (W) Soil feels cool, darkened in colour.

Soil tends to stick together, free water forms when handling.

Moisture Condition – Fine Grained Soils

For fine grained soils the assessment of moisture content is relative to their plastic limit or liquid limit, as follows:

- 'Moist, dry of plastic limit' or 'w <PL' (i.e. hard and friable or powdery).
- 'Moist, near plastic limit' or 'w ≈ PL (i.e. soil can be moulded at moisture content approximately equal to the plastic limit).
- 'Moist, wet of plastic limit' or 'w >PL' (i.e. soils usually weakened and free water forms on the hands when handling).
- 'Wet' or 'w ≈LL' (i.e. near the liquid limit).
- 'Wet' or 'w >LL' (i.e. wet of the liquid limit).

Rock Descriptions

Rock Strength

Rock strength is defined by the Unconfined Compressive Strength and it refers to the strength of the rock substance and not the strength of the overall rock mass, which may be considerably weaker due to defects.

The Point Load Strength Index $Is_{(50)}$ is commonly used to provide an estimate of the rock strength and site specific correlations should be developed to allow UCS values to be determined. The point load strength test procedure is described by Australian Standard AS4133.4.1-2007. The terms used to describe rock strength are as follows:

Strength Term	Abbreviation	Unconfined Compressive Strength MPa	Point Load Index * Is ₍₅₀₎ MPa
Very low	VL	0.6 - 2	0.03 - 0.1
Low	L	2 - 6	0.1 - 0.3
Medium	М	6 - 20	0.3 - 1.0
High	Н	20 - 60	1 - 3
Very high	VH	60 - 200	3 - 10
Extremely high	EH	>200	>10

* Assumes a ratio of 20:1 for UCS to $Is_{(50)}$. It should be noted that the UCS to $Is_{(50)}$ ratio varies significantly for different rock types and specific ratios should be determined for each site.

Degree of Weathering

The degree of weathering of rock is classified as follows:

Term	Abbreviation	Description
Residual Soil	RS	Material is weathered to such an extent that it has soil properties. Mass structure and material texture and fabric of original rock are no longer visible, but the soil has not been significantly transported.
Extremely weathered	XW	Material is weathered to such an extent that it has soil properties. Mass structure and material texture and fabric of original rock are still visible
Highly weathered	HW	The whole of the rock material is discoloured, usually by iron staining or bleaching to the extent that the colour of the original rock is not recognisable. Rock strength is significantly changed by weathering. Some primary minerals have weathered to clay minerals. Porosity may be increased by leaching, or may be decreased due to deposition of weathering products in pores.
Moderately weathered	MW	The whole of the rock material is discoloured, usually by iron staining or bleaching to the extent that the colour of the original rock is not recognisable, but shows little or no change of strength from fresh rock.
Slightly weathered	SW	Rock is partially discoloured with staining or bleaching along joints but shows little or no change of strength from fresh rock.
Fresh	FR	No signs of decomposition or staining.
Note: If HW and MW cannot be differentiated use DW (see below)		
Distinctly weathered	DW	Rock strength usually changed by weathering. The rock may be highly discoloured, usually by iron staining. Porosity may be increased by leaching or may be decreased due to deposition of weathered products in pores.

Rock Descriptions

Degree of Fracturing

The following classification applies to the spacing of natural fractures in diamond drill cores. It includes bedding plane partings, joints and other defects, but excludes drilling breaks.

Term	Description
Fragmented	Fragments of <20 mm
Highly Fractured	Core lengths of 20-40 mm with occasional fragments
Fractured	Core lengths of 30-100 mm with occasional shorter and longer sections
Slightly Fractured	Core lengths of 300 mm or longer with occasional sections of 100-300 mm
Unbroken	Core contains very few fractures

Rock Quality Designation

The quality of the cored rock can be measured using the Rock Quality Designation (RQD) index, defined as:

RQD % = <u>cumulative length of 'sound' core sections ≥ 100 mm long</u> total drilled length of section being assessed

where 'sound' rock is assessed to be rock of low strength or stronger. The RQD applies only to natural fractures. If the core is broken by drilling or handling (i.e. drilling breaks) then the broken pieces are fitted back together and are not included in the calculation of RQD.

Stratification Spacing

For sedimentary rocks the following terms may be used to describe the spacing of bedding partings:

Term	Separation of Stratification Planes
Thinly laminated	< 6 mm
Laminated	6 mm to 20 mm
Very thinly bedded	20 mm to 60 mm
Thinly bedded	60 mm to 0.2 m
Medium bedded	0.2 m to 0.6 m
Thickly bedded	0.6 m to 2 m
Very thickly bedded	> 2 m

Symbols & Abbreviations

Introduction

These notes summarise abbreviations commonly used on borehole logs and test pit reports.

Drilling or Excavation Methods

С	Core drilling
R	Rotary drilling
SFA	Spiral flight augers
NMLC	Diamond core - 52 mm dia
NQ	Diamond core - 47 mm dia
HQ	Diamond core - 63 mm dia
PQ	Diamond core - 81 mm dia

Water

\triangleright	Water seep
\bigtriangledown	Water level

Sampling and Testing

- A Auger sample
- B Bulk sample
- D Disturbed sample
- E Environmental sample
- U₅₀ Undisturbed tube sample (50mm)
- W Water sample
- pp Pocket penetrometer (kPa)
- PID Photo ionisation detector
- PL Point load strength Is(50) MPa
- S Standard Penetration Test
- V Shear vane (kPa)

Description of Defects in Rock

The abbreviated descriptions of the defects should be in the following order: Depth, Type, Orientation, Coating, Shape, Roughness and Other. Drilling and handling breaks are not usually included on the logs.

Defect Type

В	Bedding plane
Cs	Clay seam
Cv	Cleavage
Cz	Crushed zone
Ds	Decomposed seam
F	Fault
J	Joint
Lam	Lamination
Pt	Parting
Sz	Sheared Zone
V	Vein

Orientation

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The inclination of defects is always measured from the perpendicular to the core axis.

- h horizontal
- v vertical
- sh sub-horizontal
- sv sub-vertical

Coating or Infilling Term

cln	clean
со	coating
he	healed
inf	infilled
stn	stained
ti	tight
vn	veneer

Coating Descriptor

ca	calcite
cbs	carbonaceous
cly	clay
fe	iron oxide
mn	manganese
slt	silty

Shape

cu	curved
ir	irregular
pl	planar
st	stepped
un	undulating

Roughness

ро	polished
ro	rough
sl	slickensided
sm	smooth
vr	verv rouah

Other

fg	fragmented
bnd	band
qtz	quartz

Symbols & Abbreviations

Graphic Symbols for Soil and Rock

General

0. 	
A. A. A. A A. A. A. A	

Asphalt Road base

Concrete

Filling

Soils



Topsoil

Peat Clay

Silty clay

Sandy clay

Gravelly clay

Shaly clay

Silt

Clayey silt

Sandy silt

Sand

Clayey sand

Silty sand

Gravel

Sandy gravel



Talus

Sedimentary Rocks



Limestone

Metamorphic Rocks

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Slate, phyllite, schist

Quartzite

Gneiss

Igneous Rocks

Granite

Dolerite, basalt, andesite

Dacite, epidote

Tuff, breccia

Porphyry

May 2017

SURFACE LEVEL: 97.1 m AHD BORE No: BH101 EASTING: 333557 **NORTHING:** 6255475 **NORTHING:** 6255475 **DIP/AZIMUTH:** 90°/--

PROJECT No: 86645.03 DATE: 1/6/2023 SHEET 1 OF 1

		Description	Degree of Weathering BARE S S C E	Rock		Fracture	Discontinuities	Sa	amplir	ng & I	n Situ Testing
RL	Depth	of		Suengui	ater	Spacing					Test Results
Ľ	(m)	Strata	Gran Carl		°,≥_	(m) ۵۰۰۰۰۰	B - Bedding J - Joint S - Shear F - Fault	Type	e G	RQD %	&
	0.05		M H M S S C H		0.01	0.05	e enear i raan		۳ ۳	<u> </u>	Comments
6	0.05				l li						
ţ.		BEDDING SAND - 50mm thick			1						
È		FILL/Gravelly CLAY: low to medium plasticity, grey and mottled									
È I		orange-brown, sub-angular brick,			l li						
Ē	-1	concrete and bluemetal gravel, trace fine to medium sand, w = PL,			1						
-8		apparently firm									
ţ.											
ţ.				i i i i i i	İ	ii ii					
È I	1.8	Gravelly CLAY CI: medium									
Ē	-2 ^{1.9}	plasticity, grey and pale orange,			1 1						
- 95		sub-angular shale gravel, w = PL,	iiiii	İİİİİİ	l li	ii ii					
Ē		extremeley weathered shale Bore discontinued at 1.9m									
F		- discontinued due to sewer position			l li						
F		unconfirmed.									
94	-3										
6											
			iiiii	İİİİİİ	i	ii ii					
- 6	-4										
					l li						
È					1						
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Ē	-5				li	ii ii					
-8											
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	-6				l li						
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RIG: Vac-Truck

CLIENT:

PROJECT:

LOCATION:

Deicorp Pty Ltd

Crows Nest

Fiveways Crows Nest

Pacific Highway, Alexander St, Falcon St,

DRILLER: AUM TYPE OF BORING: Non Destructive Digging

LOGGED: JCP

CASING: None

WATER OBSERVATIONS: No free groundwater observed

REMARKS: Borehole discontinued to due to unknown location of sewer pipe.

	SAN	/IPLING	G & IN SITU TESTING	LEG	END	1				
A	Auger sample	G	Gas sample	PID	Photo ionisation detector (ppm)		_		-	— –
В	Bulk sample	Р	Piston sample	PL(A	A) Point load axial test Is(50) (MPa)					Partners
BL	K Block sample	U,	Tube sample (x mm dia.)	PL(E	D) Point load diametral test ls(50) (MPa)					Parlners
C	Core drilling	Ŵ	Water sample	pp	Pocket penetrometer (kPa)					
D	Disturbed sample	⊳	Water seep	S	Standard penetration test			O		
E	Environmental sample	Ŧ	Water level	V	Shear vane (kPa)			Geotechnics	s I Envir	onment Groundwater
						•				

SURFACE LEVEL: 96.5 m AHD BORE No: BH102 **EASTING:** 333552 NORTHING: 6255441.3 DIP/AZIMUTH: 90°/--

PROJECT No: 86645.03 DATE: 15 - 17/5/2023 SHEET 1 OF 3

			Degree of	Rock	Energia de la composición de		-			- City Taratia
	Depth	Description			Fracture Spacing	Discontinuities			-	n Situ Testing Test Results
RL	(m)	of Strata	Grat	[응]의 [밤] [반응]	(m)	B - Bedding J - Joint S - Shear F - Fault	Type	Core Rec. %	ROD %	&
\vdash		FILL/Sandy SILT: low plasticity, pale	N N N N N N N N N N N N N N N N N N N	High Me	0.01			° æ	<u> </u>	Comments
		brown and brown, fine sand, with					E			
-8		gravel, brick and gyprock cobbles, trace fabric, wood, plastic fines, w <					E			
		PL, apparently loose								
	- 0.9 -1	Silty CLAY CI: low plasticity, pale			i ii ii		E			
		orange-brown and grey mottled orange, w < PL, ironstone gravel,								
-36		apparently dense, residual Below 1.48m: ironstone gravel								
		lenses								
Ē	2 2.0	SHALE: pale grey, grey and				Unless otherwise stated,				
}		orange-brown, thinly laminated, very low strength, extremely weathered,				discontinuities are bedding, 0-5°, pl, sm, cly	С	100	0	
2		fractured, Ashfield Shale				vn or fe stn				
ļ	.				┍╾╾┿┛ ┝╴╸╇┿┓╎╎╎					
Ē	-3				╎╎╏	א 3.02m: J40°, pl, sm, cln	<u> </u>			
		Below 3.0m: highly weathered				3.06m: Fg 40mm 3.1m: J60°, pl, he, cly vn				
8					┝╍╡┼┓╎╎	¹ 3.19m: J30°, pl, sm, cln, roots				
					╞═╅┼┛╎╎	^L 3.21m: J60°, pl-ir, sm,	С	93	9	
	-4				i 🗍 ii	cln - 3.26-3.35m: J60-80°,				PL(A) = 0.4
ÈÈ	4.34	Below 4.34m: very low to low				pl-ir, sm, cln 3.36m: J85-90°, pl-un,				
-8		strength			╎╎┙	sm, cln, 50mm - 3.45m: J30°, un, sm, cln				
ŧ						-3.48m: J60°, pl, he, fe stn				PL(A) = <0.1
	-5					-3.53m: B0°, pl-un, sm, cly vn and roots		100	0	
Ē					╎╎┛╎╎	⁻ 3.54m: J40°, pl, he, cly vn	С	100	0	PL(A) = <0.1
-2					i ibgii	 -3.66-3.81m: J70-90°, ir, sm, cln				
Ē						-3.82-3.92m: 2x J50°, pl,				PL(A) = 0.2
	-6				┝━━┛	he -4.06-4.14m: J60°, pl,				PL(A) = 0.1
					i i r ii	sm, cly vn -4.19m: Ds 50mm				
-8					 	-4.24m: CORE LOSS: 100mm				
	6.8	SHALE: dark grey, thinly laminated,				-4.35m: J75°, pl, sm, cly vn	С	100	52	
ŧ	-7	very low to low strength, slightly weathered to fresh, slightly			┊╺┫┊┊┊	-4.59m: J30°, pl, sm, cln -4.7m: J75°, pl, sm, cly				
		fractured, Ashfield Shale			i Li II	vn ⁻ 4.78m: J40°, pl, sm, cln				
-68						4.82m: J40°, pl, sm, cln 4.84m: J60°, pl-un, sm,				
<u> </u>						cln, 60mm -4.94m: J40° pl, sm, cln				PL(A) = 0.1
Ē	-8	Below 8.0m: low strength			┊╶┽┚╵╵	5.02m: B10°, pl, he, cly	_			(//) - 0.1
F	.					5.1m: J10°, pl, he, cly vn	С	92	21	PL(A) = 0.2
-8						5.17m: Ds 60mm 5.33m: Ds 30mm				
ŧ						5.37m: B10°, pl, cly ctg				
	-9				╎╺┿┽┶┛╎╎	-5.48m: J55°, pl, sm, cln -5.76-5.96m: 3x B10°, pl,				
						sm, cly vn and fe stn 6.02m: J20°, pl, sm, cln				PL(A) = 0.1
-8-						6.06m: J80°, pl, sm, cln, 30mm	С	91	12	
ŧ	- - 10.0					⁻ 6.28m: J15°, pl, he, fe				
PI			ED: Tightsite			CASING: HO				

DRILLER: Tightsite

LOGGED: ECB

CASING: HQ to 1.5m

TYPE OF BORING: Hand auger to 1.5m, NMLC Coring to 23.25m WATER OBSERVATIONS: No free groundwater observed **REMARKS:**

RIG: Proline

Deicorp Pty Ltd

Crows Nest

Fiveways Crows Nest

Pacific Highway, Alexander St, Falcon St,

CLIENT:

PROJECT:

LOCATION:

SAMPLING & IN SITU TESTING LEGEND

 LEGEND

 PID
 Photo ionisation detector (ppm)

 PL(A) Point load axial test Is(50) (MPa)

 PL(D) Point load diametral test Is(50) (MPa)

 pp
 Pocket penetrometer (kPa)

 S
 Standard penetration test

 V
 Shear vane (kPa)

 A Auger sample B Bulk sample BLK Block sample C Core drilling D Disturbed sample E Environmental sample G & IN SHID TESTING Gas sample Piston sample Tube sample (x mm dia.) Water sample Water seep Water level G P U, W ₽



SURFACE LEVEL: 96.5 m AHD BORE No: BH102 **EASTING:** 333552 NORTHING: 6255441.3 DIP/AZIMUTH: 90°/--

PROJECT No: 86645.03 DATE: 15 - 17/5/2023 SHEET 2 OF 3

Γ		Description	Degree of Weathering ·∈	Rock Strength	Fracture	Discontinuities	Sa	amplii	ng & I	n Situ Testing
님	Depth (m)	of	Weathering		Spacing (m)	B - Bedding J - Joint	be	re .%	Q.	Test Results
	(,	Strata	G FR S S M F E		0.05 0.05 0.05 0.01 0.01 0.01 0.01 0.01	S - Shear F - Fault	Type	ပြီးမို	RQD %	& Comments
	-	SHALE: dark grey, thinly laminated, low strength, fresh, slightly fractured, Ashfield Shale				stn 16.44m: J10°, pl, he, fe stn 16.72m: J20°, pl, sm, cln	с	91	12	PL(A) = 0.3
85	10.76	Below 10.15m: fractured, steeply dipping joints At 11.76m: tuff layer, 10mm thick				6.82-6.91m: J90°, pl-ir, sm, cln 6.91m: J30°, pl, sm, cln, 70mm 6.97m: J20°, pl, sm, cln 7.06m: J70°, pl-un, sm, cln, 70mm 7.14-7.41m: 5x J40°, pl, sm, cln 7.5-8.0m: 2x J85°, pl, sm, cln 8.19-8.67m: 8x J20-30°, pl, sm, cln 8.60-9.04m: J85°, pl, sm, cln 9.18m: J85°, pl, sm, cln	С	97	90	PL(A) = 0.2
83	- 13					9.20-10.09m: 12x J15-30°, pl, sm, cln -10.1-10.2m: J70° pl, sm, cln, 100mm -10.46m: Fg 40mm -10.51-10.73m: J60°, pl, sm, cln -10.73m: CORE LOSS: - 30mm	С	100	90	PL(A) = 0.2
	- 14					-11.07-11.65m: J85°, pl, sm, cln -11.88m: Fg 300mm -11.66-12.23m: J85-90°, pl, sm, cln -12.29-12.83m: 2x J85-90°, pl, sm, cl -12.9m: J70°, pl, sm, cln -12.96m: J30°, pl, sm, cln -12.05m: J50°, pl, sm,	С	100	94	PL(A) = 0.3
	- 15.34 - 16 - 16.1	SILTSTONE: dark grey and pale grey, thickly laminated, low strength, fresh, slightly fractured, Mittagong Formation SANDSTONE: fine grained, pale grey and grey, distinct and indistinctly cross-bedded medium strength, fresh, slightly fractured, Mittagong Formation				-13.09m: J50°, pl, sm, cln 13.14m: J20°, pl, sm, cln 13.14-13.38m: 3x J20-30°, pl, sm, cln -13.49-13.66m: 2x J50-60°, pl, cm, cln -13.86m: J30°, pl, sm, cln 13.86-14.01m: 2x J25-30°, pl sm, cln	с			PL(A) = 0.2 PL(A) = 0.7 PL(A) = 0.2
	-17 17.0	SANDSTONE: fine to medium grained, pale grey and grey, thinly cross-bedded, with siltstone laminations, high strength, fresh, unbroken, Hawkesbury Sandstone				14.22-14.54m: J15-40°, pl, sm, cln 14.22-14.54m: J15-40°, pl, sm, cln 14.94-15.04m: J60° pl, sm, cln, 100mm 15.35m: J25°, pl, sm, cln 15.49m: J40°, pl, sm, cln 15.59-16.09m: 4x J15-30°, pl, sm, cln	С	100	68	PL(A) = 0.9 PL(A) = 1.2
82	- 19 - 19 					16.21m: J70°, pl, sm, cln 16.27-16.59m: 4x J25-40°, pl, ro, cln 17.28-17.71m: 5x J15-30°, pl, ro, cln 19.17m: B20°, pl, ro, cln 19.37m: B0-5°, un, ro, cln	С	100	93	PL(A) = 1

RIG: Proline

DRILLER: Tightsite

LOGGED: ECB

CASING: HQ to 1.5m

TYPE OF BORING: Hand auger to 1.5m, NMLC Coring to 23.25m WATER OBSERVATIONS: No free groundwater observed **REMARKS:**

Deicorp Pty Ltd

Crows Nest

Fiveways Crows Nest

Pacific Highway, Alexander St, Falcon St,

CLIENT:

PROJECT:

LOCATION:

SAMPLING & IN SITU TESTING LEGEND

 LEGEND

 PID
 Photo ionisation detector (ppm)

 PL(A) Point load axial test Is(50) (MPa)

 PL(D) Point load diametral test Is(50) (MPa)

 pp
 Pocket penetrometer (kPa)

 S
 Standard penetration test

 V
 Shear vane (kPa)

 A Auger sample B Bulk sample BLK Block sample C Core drilling D Disturbed sample E Environmental sample G & IN SHID TESTING Gas sample Piston sample Tube sample (x mm dia.) Water sample Water seep Water level G P U, W ₽



SURFACE LEVEL: 96.5 m AHD BORE No: BH102 **EASTING:** 333552 NORTHING: 6255441.3 DIP/AZIMUTH: 90°/--

PROJECT No: 86645.03 DATE: 15 - 17/5/2023 SHEET 3 OF 3

$\left[\right]$		Description	Degree of Weathering A A A A A A A A A A A A A A A A A A A	Rock Strength ត្រ	Fracture	Discontinuities	Sa	amplii	ng & l	n Situ Testing
님	Depth (m)	of			Spacing (m)	B - Bedding J - Joint	e	e %.	Q.,	Test Results
	(''')	Strata	G_G_	Strength Medium Net High Kex High Very Low Very Low Very Low Very Low Very Low		S - Shear F - Fault	Type	ပိမ္မိ	RQD %	& Comments
75 76	-21	SANDSTONE: fine to medium grained, pale grey and grey, thinly cross-bedded, with siltstone laminations, high strength, fresh, unbroken, Hawkesbury Sandstone				20.57m: B20°, pl, ro, cln	С	100		PL(A) = 1.3
74	-22 -23 -23 -23.25						С	100	100	PL(A) = 0.9 PL(A) = 1.1 PL(A) = 0.7
73		Bore discontinued at 23.25m - target depth reached								
	- 24									
22										
	- 25									
12										
	-26									
92	-									
ŧ	-27									
69	-									
	-28									
	-29			iiiiii						

RIG: Proline

A Auger sample B Bulk sample BLK Block sample C Core drilling D Disturbed sample E Environmental sample

DRILLER: Tightsite

LOGGED: ECB

CASING: HQ to 1.5m

TYPE OF BORING: Hand auger to 1.5m, NMLC Coring to 23.25m WATER OBSERVATIONS: No free groundwater observed **REMARKS:**

Deicorp Pty Ltd

Crows Nest

Fiveways Crows Nest

Pacific Highway, Alexander St, Falcon St,

CLIENT:

PROJECT:

LOCATION:



BORE: BH102	PROJECT: 86645.03	MAY 2023					
Douglas Pa Geolechnics Environment	Project No: 86645.03 BH ID: 6462 Depth: 148-6.0m Core Box No.: 1						
86645-03 BH102 CR9WI NEST 15-5-23	STRACT 1-48m	autor a the					
3		MB2-AL-					
4	CORE LOSS LOOMM						

BORE: BH102	PROJECT: 86645.03	MAY 2023
Geotechnics Environment Groundwat	er Depth: 0.0-11.0M Core Box No.: 2	Latinha
hadanhada	0.1.0.1.0.1.0.1	
6- 7 7		
8 CORE LOSS		
130mm		
	6.0 – 11.0m	



	ouglas Pa	Project No: - 86645-0 BH ID: ' 84/02 Depth: - 160-21-0 Core Box No: - 4	1.1.0.
16	<u>SALL</u>		
18			
19			
20	6		

BORE: BH102	PROJECT: 86645.03	MAY 2023
Douglas Part Geotechnics Environment G	Core Box No.: - 5	
hadaadaa	ատարարարություն	հահան
2		
31 - 11 1	EOH @ 2325	m

SURFACE LEVEL: 96.0 m AHD BORE No: BH103 **EASTING:** 333581 **NORTHING:** 6255420.4 DIP/AZIMUTH: 90°/--

PROJECT No: 86645.03 DATE: 11 - 15/5/2023 SHEET 1 OF 4

$\left[\right]$		Description	Degree of Weathering	. <u>0</u>	Rock Strength	Fracture	Discontinuities	Sa	amplii	ng & I	n Situ Testing
님	Depth (m)	of	Weathering	Log	Very Low Very Low Very High Very High Kater 001	Spacing (m)	B - Bedding J - Joint	Type	ore : %	RQD %	Test Results &
9	, í	Strata	HW HW EW	U U		0.10	S - Shear F - Fault	Ţ	ပိမ္ရွိ	Я,	Comments
	0.1 - 1	CONCRETE: 100mm thick FILL/Sandy GRAVEL: sub-angular to sub-rounded gravel, grey, fine to medium sand, plastic fines, trace cobbles, moist, apparently loose						E E S			1,1,2 N = 3
	2.3	FILL/CLAY: low to medium plasticity, grey, trace fine to medium sand, w = PL, firm Below 2.0m: w > PL CLAY CI: medium plasticity, grey and pale grey, w = PL, firm, residual					Unless otherwise stated, all discontinuities are bedding, 0-5°, pl, sm, cln, cly vn or fe stn	E	-		2,4,25/140mm refusal
	-3	LAMINITE: pale grey, thinly laminated, grey and brown, medium strength then very low strength, highly weathered, highly fractured, Ashfield Shale					3.07-3.19m: J55°, pl, ∖sm, cln, 120mm 3.26m: J20°, he, pl, cly ∖vn 3.56m: J20°, pl, sm, cln	с	100	0	PL(A) = 0.8
	- 5					·····································	3.91m: B0°, pl, sm, cly ctg 20mm 3.95m: Ds 50mm 4.26m: J0-5°, ir, sm, fe stn 4.31m: Fg 40mm 4.35-4.77m: 4x Ds 20-60mm 4.85m: J20°, pl, sm, fe stn 5.56m: J70°, pl, sm, cln 5.15-6.12m: 4x B0°, pl, sm, cly ctg 2-30mm 6.16m: J30°, pl, he 6.27-6.32m: 3x J70-80°, pl, sm, fe stn 6.47m: Fg 80mm 6.49m: J20°, pl, sm, cln 6.65m: J10°, pl, sm, cln	С	100	25	PL(A) = <0.1 PL(A) = <0.1 PL(A) = <0.1
87					16-05-23		 6.75-6.9m: J85-90°, pl, sm, fe stn 6.89m: Ds 40mm 6.96m: J15°, pl, sm, cln 7.16m: B0, pl, sm, cly ctg 20mm 7.05-7.36m: 3x J30°, pl, sm, cln or fe stn 7.39m: Ds 40mm 7.43-7.53m: 2x J70°, pl, sm, cly vn 8.37-8.44m: 2x J60°, pl, he, fe stn 8.62m: J60°, pl, sm, fe stn 	С	69	5	PL(A) = 0.1 PL(A) = <0.1 PL(A) = 0.1
	9 9.0						\ ¹ 8.64-8.79m: Fg 150mm 9m: CORE LOSS: 910mm				

RIG: Bobcat

CLIENT:

PROJECT:

LOCATION:

Deicorp Pty Ltd

Crows Nest

Fiveways Crows Nest

Pacific Highway, Alexander St, Falcon St,

LOGGED: ECB

CASING: HWT to 2.5m

TYPE OF BORING: Diatube to 0.1m, Solid flight augering to 2.5m, NMLC Coring to 30.57m WATER OBSERVATIONS: Free groundwater observed at 2.0m.

DRILLER: Ground Test

	SAN	IPLINC	3 & IN SITU TESTING	LEG	END						
A	Auger sample	G	Gas sample	PID	Photo ionisation detector (ppm)	_		-	_	_	
B	Bulk sample	Р	Piston sample) Point load axial test Is(50) (MPa)					Partner	
BL	K Block sample	U,	Tube sample (x mm dia.)	PL(C) Point load diametral test ls(50) (MPa)	1.			5 8		5
C	Core drilling	Ŵ	Water sample	pp	Pocket penetrometer (kPa)						
D	Disturbed sample	⊳	Water seep	S	Standard penetration test	1.					
E	Environmental sample	Ŧ	Water level	V	Shear vane (kPa)		Geotechnics	S I Envi	ironr	ment Groundwat	er

SURFACE LEVEL: 96.0 m AHD BORE No: BH103 **EASTING:** 333581 **NORTHING:** 6255420.4 DIP/AZIMUTH: 90°/--

PROJECT No: 86645.03 DATE: 11 - 15/5/2023 SHEET 2 OF 4

	_	Description	Degree of Weathering	Rock Strength	Fracture	Discontinuities	Sa	amplii	ng & I	n Situ Testing
R I	Depth (m)	of Strata	Graph	Vate Vate	Spacing (m)	B - Bedding J - Joint S - Shear F - Fault	Type	Core ec. %	RQD %	Test Results &
	10.0 [,]	Strata SHALE: dark grey, thinly laminated, very low to low strength, slightly weathered, highly fractured, Ashfield Shale				Y9.92m: J90°, pl, sm, cln 9.93m: J40°, pl, sm, cln 9.96m: J65°, pl, sm, cln 10.12-10.3m: 4x J20-45°, pl, sm, cln 10.45m: J35°, pl, sm, 10.45m: J35°, pl, sm, 10.45m: J35°, pl, sm, 10.38-10.58m: J85°, pl,	c	91 91	22	Comments PL(A) = <0.1
8	12					sm, cly vn 10.7m: J60°, pl, he 10.86m: Fg 20mm 11m: CORE LOSS: 50mm 11.15m: J60°, pl, sm, cln 11.25m: J30°, pl, sm, cln 11.37-11.48m: J60°, pl,	с	98	36	PL(A) = 0.1
	12.44 13 13.28	SILTSTONE: pale grey and grey, very low strength, sandstone laminations, slightly weathered, webselsen. Mittheware Formation				sm, cln 11.64m: J35°, pl, sm, 11.64m: J35°, pl, sm, cln 11.8-11.95m: 2x J60°, pl, sm, cln 12.05-12.13m: 3x J50°, pl, sm, cln 12.25-12.35m: J75°, pl, sm, cln 12.41m: CORE LOSS:	с	100	0	PL(A) = <0.1 PL(A) = <0.1
	14	unbroken, Mittagong Formation				30mm 12.73m: J20°, pl, sm, cln 12.74-12.84m: 2x J40°, he, pl 13.25m: J20°, pl, sm, cln	с	100	0	PL(A) = <0.1 PL(A) = <0.1
	15 15.0	SANDSTONE: fine grained, pale grey and grey, low strength, thinly cross-bedded, siltstone laminations, slightly weathered then fresh, slightly fractured, Mittagong Formation Below 15.75m: low to medium							0	PL(A) = <0.1 PL(A) = 0.4
	10	strength				16.05m: Fg 60mm 16.27-16.55m: 2x Ds 20mm				PL(A) = 0.4
62 - 1 	17					17.13m: J45°, st, ro, cln 17.34m: Fg 40mm	с	100	85	PL(A) = 0.2 PL(A) = 0.4
	17.8 · 18	SANDSTONE: medium grained, pale grey, high strength, thinly cross-bedded, siltstone laminations, fresh, slightly fractured, Hawkesbury Sandstone				17.62m: J30°, pl-ir, ro, cln				PL(A) = 0.7
	19									PL(A) = 1.3 PL(A) = 1.2
	20.0						С	100	100	PL(A) = 1.2

RIG: Bobcat **TYPE OF BORING:** Diatube to 0.1m, Solid flight augering to 2.5m, NMLC Coring to 30.57m

CLIENT:

PROJECT:

LOCATION:

Deicorp Pty Ltd

Crows Nest

Fiveways Crows Nest

Pacific Highway, Alexander St, Falcon St,

DRILLER: Ground Test

LOGGED: ECB

CASING: HWT to 2.5m

WATER OBSERVATIONS: Free groundwater observed at 2.0m.

	SAN	IPLIN	3 & IN SITU TESTING	LEGEND						
A	Auger sample	G	Gas sample	PID Photo ionisation detector (ppm)		_		_		— –
B	Bulk sample	Р	Piston sample	PL(A) Point load axial test Is(50) (MPa)						Partners
BLI	< Block sample	U,	Tube sample (x mm dia.)	PL(D) Point load diametral test ls(50) (MPa	i)	11.				Partners
C	Core drilling	Ŵ	Water sample	pp Pocket penetrometer (kPa)	<u> </u>					
D	Disturbed sample	⊳	Water seep	S Standard penetration test			O to . to . !			
E	Environmental sample	Ŧ	Water level	V Shear vane (kPa)			Geotechnic:	SIE	nvirc	onment Groundwater
<u> </u>	Entrioninonianoampio		Trator lotor							

SURFACE LEVEL: 96.0 m AHD BORE No: BH103 **EASTING:** 333581 **NORTHING:** 6255420.4 DIP/AZIMUTH: 90°/--

PROJECT No: 86645.03 DATE: 11 - 15/5/2023 SHEET 3 OF 4

	_	Description	Degree of Weathering	jc	Rock Strength _o	Fracture	Discontinuities			-	n Situ Testing
R	Depth (m)	of		iraph Log	Ex Low Very Low Medium High Kery High Ex High	Spacing (m)	B - Bedding J - Joint	Type	Core Rec. %	0 %	Test Results &
0 0	. ,		F S S W H W	U	Ex Lo Very Very Very Ex H	0.05 0.10 1.00	S - Shear F - Fault	Ţ	ŭ ğ	Ж,	Comments
75	-21	SANDSTONE: medium grained, pale grey, high strength, thinly cross-bedded, siltstone laminations, fresh, unbroken, Hawkesbury Sandstone					20.52m: B5°, pl-ir, ro, cly ctg 2mm 20.71m: J20°, pl, ro, cly vn	С	100	100	PL(A) = 1
74	-22										PL(A) = 1.2
73	-23	Between 23.1 and 27.0m: medium to coarse grained					23.21m: B0°, pl-un, ro, cly ctg 2mm	С	100	97	PL(A) = 1.1
72	- 24						24.21m: J40°, pl, ro, cln				PL(A) = 1.5
71	- 25										PL(A) = 1.6
70	- 26							С	100	100	PL(A) = 1.2
69	-27						27.23m: B5°, pl, ro, cly vn				PL(A) = 0.7
68	- 28										PL(A) = 0.8
67	-29						28.63-29.57m: 3x B15-20°, pl, ro, cbs vn and cly vn	с	100	96	PL(A) = 1.1
	- - - 30.0						29.64m: J30°, pl, ro, cln 29.67m: B5°, pl, ro, cly				PL(A) = 1.1

RIG: Bobcat **TYPE OF BORING:** Diatube to 0.1m, Solid flight augering to 2.5m, NMLC Coring to 30.57m

CLIENT:

PROJECT:

LOCATION:

Deicorp Pty Ltd

Crows Nest

Fiveways Crows Nest

Pacific Highway, Alexander St, Falcon St,

DRILLER: Ground Test

LOGGED: ECB

CASING: HWT to 2.5m

WATER OBSERVATIONS: Free groundwater observed at 2.0m.

A Auger sample G Gas sample PID Photo ionisation detector (ppm) B Bulk sample P Piston sample PL(A) Point load axial test ls(50) (MPa) BLK Block sample U, Tube sample (x mm dia.) PL(D) Point load axial test ls(50) (MPa) C Core drilling W Water sample P Pocket penetrometer (kPa)		SAM	PLIN	3 & IN SITU TESTING	LEG	END			
B Bulk sample P Piston sample PL(A) Point load axial test Is(50) (MPa) BLK Block sample U Tube sample (x mm dia.) C Core drilling W Water sample	A	Auger sample	G	Gas sample	PID	Photo ionisation detector (ppm)	 	-	
BLK Block sample U Tube sample (x mm dia.) PL(D) Point load diametral test 15(50) (MPa) DOUGIAS PARTINERS			Р					100	Douteono
C. Core drilling W Water sample np Pocket penetrometer (kPa)	BLK	Block sample	U,	Tube sample (x mm dia.)	PL(E	0) Point load diametral test Is(50) (MPa)			Pariners
	С	Core drilling	Ŵ	Water sample	pp	Pocket penetrometer (kPa)		140	
D Disturbed cample N Water seen S Standard population fact	D	Disturbed sample	⊳	Water seep	S	Standard penetration test			
E Environmental sample V Water level V Shear vane (kPa)	E	Environmental sample	Ŧ	Water level	V	Shear vane (kPa)	Geotechnics	I Envir	onment Groundwater

SURFACE LEVEL: 96.0 m AHD BORE No: BH103 **EASTING:** 333581 **NORTHING:** 6255420.4 DIP/AZIMUTH: 90°/--

PROJECT No: 86645.03 DATE: 11 - 15/5/2023 SHEET 4 OF 4

	Description	Degree of Weathering ﷺ ≩ ≩ ਨ ∞ ੯੯	.c	Rock Strength	_	Fracture	Discontinuities				n Situ Testing
니 Depth	of	weathering	aphi og	Strength Very Low High High Very High	ate	Spacing	B - Bedding J - Joint	e	Core Rec. %	D	Test Results
<u>م</u> (m)	Strata	H H W M M W F S W	5 J	ery Low ery Low igh ery H		0.100 (m)	S - Shear F - Fault	Type	Š Č	RQ %	& Comments
8	SANDSTONE: As above	шт≥юйц	::::	ייצי≖יציניציש 	<u>и</u> с		vn				Comments
								с	100	96	PL(A) = 1.2
								-			1 L(A) = 1.2
30.57	Bore discontinued at 30.57m				1						
	- target depth reached										
-ස – 31											
		i i i i i				i ii ii					
- 5 - 32											
-8 - 33											
EE											
-&-34											
 36											
		liiiii				i ii ii					
[[
-ස – 37											
-ଞ - 38											
F [
[[
-15-39											

RIG: Bobcat

CLIENT:

PROJECT:

LOCATION:

Deicorp Pty Ltd **Fiveways Crows Nest**

Crows Nest

Pacific Highway, Alexander St, Falcon St,

DRILLER: Ground Test

LOGGED: ECB

CASING: HWT to 2.5m

TYPE OF BORING: Diatube to 0.1m, Solid flight augering to 2.5m, NMLC Coring to 30.57m WATER OBSERVATIONS: Free groundwater observed at 2.0m. REMARKS: Groundwater well installed to 30.1m. Screen 18.1m - 30.1m. Solid PVC 0.1m-18.1m. Sand to 17.3m. Bentonite to 3.3m. Backfill to 0.1m.

A Auger sample B Bulk sample BLK Block sample C Core drilling D Disturt SAMPLING & IN SITU TESTING LEGEND LEGEND PID Photo ionisation detector (ppm) PL(A) Point load axial test Is(50) (MPa) PL(D) Point load diametral test Is(50) (MPa) pp Pocket penetrometer (kPa) S Standard penetration test V Shear vane (kPa) Gas sample Piston sample Tube sample (x mm dia.) Water sample Water seep Water level G P U, W **Douglas Partners** 1 Core drilling Disturbed sample Environmental sample ₽ Geotechnics | Environment | Groundwater

SURFACE LEVEL: 96.0 m AHD 333581 EASTING: NORTHING: 6255420.4 DIP/AZIMUTH: 90°/--

BORE No: BH103 **PROJECT No: 86645.03** DATE: 11 - 15/5/2023 SHEET 1 OF 4

Sampling & In Situ Testing Graphic Log Well Description Water Depth 宧 of Sample Construction Depth Type Results & Comments (m) Details Strata Gatic cove CONCRETE: 100mm thick 0.1 0.2 0.1 FILL/Sandy GRAVEL: sub-angular to sub-rounded gravel, grey, fine to medium sand, plastic fines, trace cobbles, 0.5 moist, apparently loose 0.6 Blank pipe 0.9 0.1-12.1m E 95 1.0 1,1,2 s N = 31.45 1.8 FILL/CLAY: low to medium plasticity, grey, trace fine to 1.9 2.0 Backfill 0.0-3.8m E 94 -2 - 2 medium sand, w = PL, firm Below 2.0m: w > PL 2.3 CLAY CI: medium plasticity, grey and pale grey, w = PL, 2.5 firm, residual 2,4,25/140mm s refusal Nor South on South of South 2.9 2.94 LAMINITE: pale grey, thinly laminated, grey and brown, medium strength then very low strength, highly weathered, highly fractured, Ashfield Shale -8-3 - 3 3.0 3.1 PL(A) = 0.8С 3.89 -8-4 - 4 4.66 PL(A) = <0.1 - 5 -5 -6 С 5.65 PL(A) = <0.1 -8 6 6 6.49 PL(A) = <0.1 6.96 7.05 -8-7 7 PL(A) = 0.1▼ 16-05-23 Bentonite 3.8-11.6m 7.95 PL(A) = <0.1 -8-8 - 8 8.16 PL(A) = 0.1 С 9 9.0 - q 9.91 9.91

RIG: Bobcat

TYPE OF BORING:

DRILLER: Ground Test

LOGGED: ECB Diatube to 0.1m, Solid flight augering to 2.5m, NMLC Coring to 30.57m

CASING: HWT to 2.5m

WATER OBSERVATIONS: Free groundwater observed at 2.0m.

Deicorp Pty Ltd

Crows Nest

Fiveways Crows Nest

Pacific Highway, Alexander St, Falcon St,

CLIENT:

PROJECT:

LOCATION:

	SAN	IPLIN	3 & IN SITU TESTING	LEG	END]					
A	Auger sample	G	Gas sample	PID	Photo ionisation detector (ppm)		_		-		
В	Bulk sample	P	Piston sample	PL(A) Point load axial test Is(50) (MPa)						Doutrooko
BL	K Block sample	U,	Tube sample (x mm dia.)	PL(C) Point load diametral test ls(50) (MPa)		11.			15	Partners
C	Core drilling	Ŵ	Water sample	pp	Pocket penetrometer (kPa)						
D	Disturbed sample	⊳	Water seep	S	Standard penetration test		1.				
E	Environmental sample	Ŧ	Water level	V	Shear vane (kPa)			Geotechnics	IE	nviro	onment Groundwater

SURFACE LEVEL: 96.0 m AHD BORE No: BH103 **EASTING:** 333581 **NORTHING:** 6255420.4 DIP/AZIMUTH: 90°/--

PROJECT No: 86645.03 DATE: 11 - 15/5/2023 SHEET 2 OF 4

_		Clows Nest					1. 90 /		SHEET 2 OF 4
	Depth	Description	hic				In Situ Testing	er	Well
ßL	(m)	of Strata	Graphic Log	Type	Depth	Sample	Results & Comments	Water	Construction Details
	10.0	SHALE: dark grey, thinly laminated, very low to low strength, slightly weathered, highly fractured, Ashfield Shale		с с	10.07		PL(A) = <0.1		
85 · ·	¹¹ 11.05				11.05 11.1		PL(A) = 0.1		-11
				С					
84	12				- 12.45 12.62		PL(A) = <0.1		
83	13				12.62		PL(A) = <0.1 PL(A) = <0.1		
	13.28 -	SILTSTONE: pale grey and grey, very low strength, sandstone laminations, slightly weathered, unbroken, Mittagong Formation		С					
82	14		· · ·		13.9 13.97		PL(A) = <0.1		
31	15 15.0-		· · · · · ·	С	14.56		PL(A) = <0.1		
	- 10.0	SANDSTONE: fine grained, pale grey and grey, low strength, thinly cross-bedded, siltstone laminations, slightly weathered then fresh, slightly fractured, Mittagong Formation			15.45		PL(A) = <0.1		
	16	Below 15.75m: low to medium strength			15.95 16.0		PL(A) = 0.4		
					16.5		PL(A) = 0.2		
	17			С	16.96 17.0		PL(A) = 0.2 PL(A) = 0.4		
	17.8 - 18	SANDSTONE: medium grained, pale grey, high strength, thinly cross-bedded, siltstone laminations, fresh, slightly fractured, Hawkesbury Sandstone			17.97		PL(A) = 0.7		
	19				18.89 18.96		PL(A) = 1.3		
				С	19.34		PL(A) = 1.2		
ŀ	20.0				19.92		PL(A) = 1.2		

RIG: Bobcat

CLIENT:

PROJECT:

LOCATION:

Deicorp Pty Ltd

Crows Nest

Fiveways Crows Nest

Pacific Highway, Alexander St, Falcon St,

DRILLER: Ground Test

LOGGED: ECB

CASING: HWT to 2.5m

TYPE OF BORING: Diatube to 0.1m, Solid flight augering to 2.5m, NMLC Coring to 30.57m WATER OBSERVATIONS: Free groundwater observed at 2.0m.

	SAN	IPLIN	3 & IN SITU TESTING	LEG	END				
A	Auger sample	G	Gas sample	PID	Photo ionisation detector (ppm)	_		_	
B	Bulk sample	P	Piston sample		A) Point load axial test Is(50) (MPa)				Doutroovo
BL	K Block sample	U,	Tube sample (x mm dia.)	PL(I	D) Point load diametral test Is(50) (MPa)				Pariners
C	Core drilling	Ŵ	Water sample	pp	Pocket penetrometer (kPa)			140	Partners
D	Disturbed sample	⊳	Water seep	S	Standard penetration test				
E	Environmental sample	Ŧ	Water level	V	Shear vane (kPa)		Geotechnics	S Envir	onment Groundwater

SURFACE LEVEL: 96.0 m AHD BORE No: BH103 **EASTING:** 333581 **NORTHING:** 6255420.4 DIP/AZIMUTH: 90°/--

PROJECT No: 86645.03 DATE: 11 - 15/5/2023 SHEET 3 OF 4

		Clows Nest	,				n. 90 /		
	Dent	Description	- Lic		Sam		& In Situ Testing	~	Well
6 RL	Depth (m)	of Strata	Graphic Log	Type	Depth	Sample	Results & Comments	Water	Construction Details
75	-21	SANDSTONE: medium grained, pale grey, high strength, thinly cross-bedded, siltstone laminations, fresh, unbroken, Hawkesbury Sandstone		С	20.96		PL(A) = 1		Gravel -21 11.6-30.57m PVC screen 12.1-30.1m -21 -20.1m -20.
74	-22				21.87 21.96		PL(A) = 1.2		
73	-23	Between 23.1 and 27.0m: medium to coarse grained		С	22.96		PL(A) = 1.1		
72	-24				23.95		PL(A) = 1.5		
71	-25				24.91 24.96		PL(A) = 1.6		
02	-26			С	25.96		PL(A) = 1.2		
69	-27				26.96		PL(A) = 0.7		
68	-28				27.83 27.95		PL(A) = 0.8		
	-29			С	28.95		PL(A) = 1.1		
	30.0		· · · · · · · · · · · · · · · · · · ·		29.95		PL(A) = 1.1		

RIG: Bobcat

CLIENT:

PROJECT:

LOCATION:

Deicorp Pty Ltd

Crows Nest

Fiveways Crows Nest

Pacific Highway, Alexander St, Falcon St,

DRILLER: Ground Test

LOGGED: ECB **TYPE OF BORING:** Diatube to 0.1m, Solid flight augering to 2.5m, NMLC Coring to 30.57m

CASING: HWT to 2.5m

WATER OBSERVATIONS: Free groundwater observed at 2.0m.

	SAN	IPLIN	3 & IN SITU TESTING	LEG	END					
A	Auger sample	G	Gas sample	PID	Photo ionisation detector (ppm)	_		-	_	_
B	Bulk sample	P	Piston sample) Point load axial test Is(50) (MPa)					
BL	K Block sample	U,	Tube sample (x mm dia.)	PL(C) Point load diametral test Is(50) (MPa)					
C	Core drilling	Ŵ	Water sample	pp	Pocket penetrometer (kPa)		Doug			
D	Disturbed sample	⊳	Water seep	s	Standard penetration test		_			
E	Environmental sample	Ŧ	Water level	V	Shear vane (kPa)		Geotechnics	I Envi	ronment G	Froundwater

SURFACE LEVEL: 96.0 m AHD BORE No: BH103 **EASTING:** 333581 **NORTHING:** 6255420.4 DIP/AZIMUTH: 90°/--

PROJECT No: 86645.03 DATE: 11 - 15/5/2023 SHEET 4 OF 4

	Crows nest					H: 90 /		SHEET 4 OF 4
	Description	lic		Sam		& In Situ Testing	-	Well
Depth (m)	of Strata	Graphic Log	Type	Depth	Sample	Results & Comments	Water	Construction Details
20.57	NDSTONE: As above		С	30.31 -30.57-		PL(A) = 1.2		End cap
F Bor	re discontinued at 30.57m arget depth reached			50.57				-31
-32								-32
								-33
								- 34
								-35
								-36
ස - 37 - ය 								-37
								-38
								- 39

DRILLER: Ground Test LOGGED: ECB CASING: HWT to 2.5m RIG: Bobcat **TYPE OF BORING:** Diatube to 0.1m, Solid flight augering to 2.5m, NMLC Coring to 30.57m WATER OBSERVATIONS: Free groundwater observed at 2.0m. REMARKS: Groundwater well installed to 30.1m. Screen 18.1m - 30.1m. Solid PVC 0.1m-18.1m. Sand to 17.3m. Bentonite to 3.3m. Backfill to 0.1m.

	SAMPLING & IN SITU TESTING LEGEND						
A	Auger sample	G	Gas sample	PID	Photo ionisation detector (ppm)	_	
B	Bulk sample K Block sample	Р	Piston sample Tube sample (x mm dia.)		a) Point load axial test Is(50) (MPa) D) Point load diametral test Is(50) (MPa)		Douglas Partners
C	Core drilling	Ŵ	Water sample		Pocket penetrometer (kPa)		Duy ias Pai liicis
Ď	Disturbed sample	⊵	Water seep	S	Standard penetration test		
E	Environmental sample	Ŧ	Water level	V	Shear vane (kPa)		Geotechnics Environment Groundwater



Crows Nest

LOCATION:

BORE: BH103	PROJECT: 86645.03	MAY 2023	
Douglas Part	Core Box No.: - 1		
86645.03 CROWS NEST	BH103 11-5-23 START CORING A	T 3.0M	
3			
1		A MARIA D	
5		The best monthly	
6			
APOTTO MARCAN			
	3.0 - 7.0m		

Project No: 86645 03 BH ID: 8H103 Depth: 7 0 - 12 0m Core Box No.: 2	Douglas Partner Geolechnics Environment Groundwa
	7 (<u>(</u>))
910 mm	9 CORE LOSS
7.0 – 12.0m	

BORE: BH103	PROJECT: 86645.03	MAY 2023
	Project No: - 86645: 03 BH ID: 041103 Depth: 12.0 - 17.0 M Core Box No.: 3	di cada cada ca
12		
14		
16 21	13.0 – 17.0m	

	ouglas Pa technics Environmen		Project N BH ID: ² Depth: Core Box	o: - 86645 0 BH103 D 13 0-22.0 No.: - 4	3 -	
7	7	Fit				
18		1				
19						
20						
21					Mar Anna	
Geotechnics Environment Groundwate	Core Box No.: 95					
--	------------------	----------				
հասիական	ահարթարություն	adradiai				
2						
3 (
24						
50000						
6						

Douglas Partners Geotechnics Environment Groundwater	Project No: - 86645.03 BH ID: 6H103 Depth: 21.0 - 30.57 m Core Box No.: - 6	
հայտորային	ulundandun	hadradaan
27		
28	C. C. C. C. C. C. C. C. C. C. C. C. C. C	11111 Million Colorante St
29		
30	EOH	@ 30 57 m
	27.0 – 30.57m	

SURFACE LEVEL: 93.6 m AHD BORE No: BH104 **EASTING:** 333577 NORTHING: 6255452.5 DIP/AZIMUTH: 90°/--

PROJECT No: 86645.03 DATE: 17 - 19/5/2023 SHEET 1 OF 2

		Description	Degree of Weathering	. <u>c</u>	Rock Strength	Fracture	Discontinuities				n Situ Testing
Ч	Depth (m)	of	Weathering	Log	Very Low Very Low Medium Medium Very High Ex High	Spacing (m)	B - Bedding J - Joint	Type	Core Rec. %	ac %	Test Results &
	. ,	Strata	E N N N N N N N N N N N N N N N N N N N	U U	Ex Low Very Very Very Ex H	0.05	S - Shear F - Fault	Τ	ŭ ğ	ж.	Comments
93	0.1 · 0.25 ·	CONCRETE: 100mm thick FILL/GRAVEL: sub-angular bluemetal gravel, grey, with plastic lines, moist						E			
	1	Silty CLAY CI: medium plasticity, pale grey, grey and red, trace non-plastic fines, w-PL, apparently hard, extremely weathered shale					Unless otherwise stated, all disconformities are bedding, 0-5°, pl, sm or ro, cln or cly vn or fe stn				
	2	SHALE: brown, thinly laminated, very low strength, highly weathered then slightly weathered, fractured, Ashfield Shale					1.45m: B0°, pl, sm, cly ctg 10mm 1.72m: B0°, pl, sm, cly ctg 10mm 1.92m: Cs 80mm 2.05-2.16m: 5x B0°, pl, he, fe stn				PL(A) = <0.1
	3						2.19m: Cs 20mm 2.33m: B0°, pl, sm, cly ctg 3mm 2.43m: J50°, pl, sm, cln 2.51m: J45°, pl, sm, fg 2.61m: Fg 50mm 2.81m: J30°, pl, sm, fg 2.00m	с	100		PL(A) = <0.1
-6	4						3.22m: Cs 50mm 3.29m: B0°, pl, sm, cly ctg 10mm				PL(A) = <0.1
	5				17-06-23 ▲		 3.32m: J50°, pl, sm, cln 3.41m: Cs 70mm 3.43m: J70-80°, pl, sm, cly ctg 10mm 3.5-3.56m: 2x J30°, pl, sm, ctg 10mm 3.58m: B0°, pl, sm, cly ctg 10mm 3.70-4.16m: 3x J70-80°, 	С	76		PL(A) = <0.1 PL(A) = <0.1
88	5.12 - 5.61	SHALE: brown, thinly laminated, very low strength, highly weathered then slightly weathered, fractured, Ashfield Shale					pl, sm, cln 4.23m: Cs 40mm 4.88-5.06m: J70-80°, pl, sm, cln 5.08m: J70°, pl, sm, cln 5.12m: CORE LOSS:				Γ <u>μ</u> (η) = <0.1
87	6	Below 6.42m: very low to low					490mm 5.61-5.83m: Cz 220mm 5.93-6.83m: 5x J30-55°, pl, sm, cln				PL(A) = <0.1
	7						6.89m: J80-90°, ir, sm, ch 6.96m: B0°, pl, sm, cly ctg 10mm 7.17m: J90°, pl, sm, cln 7.37-7.41m: 2x Ds 20-30mm 77.19-7.82m: 3x J30-50°,	с			PL(A) = 0.1
85	8 8.27 8.41 9	Below 8.41m: fresh					P pl, sm, cln 7.89m: Cs 20mm 8m: B0°, pl, sm, cly ctg 10mm 8.04m: Ds 20mm 8.27m: CORE LOSS: 140mm 8.44-8.57m: 3x 45-60°,		-		PL(A) = <0.1
	10.0						pl, sm, cln 18.71m: J60°, pl ,sm, cln 8.78-9.11m: J70-80°, pl, sm, cln 9.09-9.15m: 2xJ25-40°, pl, sm, cln 9.33m: B0°, pl, sm, cly	С			

RIG: Bobcat

CLIENT:

PROJECT:

LOCATION:

Deicorp Pty Ltd

Crows Nest

Fiveways Crows Nest

Pacific Highway, Alexander St, Falcon St,

DRILLER: Ground Test

LOGGED: ECB **TYPE OF BORING:** Diatube to 0.1m, Solid flight augering to 1.3m, NMLC Coring to 18.85m

CASING: HWT to 1.3m

WATER OBSERVATIONS: No free groundwater observed

	SAM	IPLIN	G & IN SITU TESTING	LEG	END]
A	Auger sample	G	Gas sample	PID	Photo ionisation detector (ppm)	
B	Bulk sample	Р	Piston sample) Point load axial test Is(50) (MPa)	Douglas Partners
BLI	K Block sample	U,	Tube sample (x mm dia.)	PL(E) Point load diametral test ls(50) (MPa)	A Douglas Partners
C	Core drilling	Ŵ	Water sample	pp	Pocket penetrometer (kPa)	
D	Disturbed sample	⊳	Water seep	S	Standard penetration test	Ocatastarias I Frankrauset I Orace durates
E	Environmental sample	Ŧ	Water level	V	Shear vane (kPa)	Geotechnics Environment Groundwater
						-

SURFACE LEVEL: 93.6 m AHD BORE No: BH104 **EASTING:** 333577 NORTHING: 6255452.5 DIP/AZIMUTH: 90°/--

PROJECT No: 86645.03 DATE: 17 - 19/5/2023 SHEET 2 OF 2

		Description	Degree of Weathering	Rock Strength	L	Fracture	Discontinuities	Sa	amplii	ng & l	n Situ Testing
님	Depth (m)	of	Weathering	Ex Low Very Low Medium Kery High Ex High	Water	Spacing (m)	B - Bedding J - Joint	Type	ore . %	RQD %	Test Results
	(,	Strata	D FR S S M F S S S M F S S S S S S S S S S S S S S S S S S S	Ex Lo Very I Very Ex High	>	0.01 0.10 0.50	S - Shear F - Fault	Ţ	ပိမ္ရွိ	R0%	& Comments
83	10.48 10.59-	SHALE: dark grey, thinly laminated, very low to low strength, fresh, fragmented to fractured, Ashfield Shale At 10.03m: tuff layer, 10mm			<<		ctg 5mm '9.40-9.49m: 4x J20-30°, pl, sm, cln '9.47-9.74m: Clay band 270mm '9.77m: J40°, pl, sm, cln	с			
	⁻¹¹ 11.05						9.8-10.47m: Clay band 670mm 10.48m: CORE LOSS: 110mm 10.58m: J30°, pl, sm, cly ctg 20mm				PL(A) = <0.1
82	- 12	Below 11.6m: medium strength					-10.69-11.18m: 7x 20-40°, pl, sm, cln -11m: CORE LOSS: 50mm				PL(A) = 0.3
81					<<		¹ 11.2-11.64m: 6x : J60-70°, pl, sm, cln, 2x he ¹ 11.36-11.59m: J30-40°, pl, sm, cln		-		
	-13 13.0-	SILTSTONE: pale grey, thickly laminated, medium strength, fresh,					^{-11.72} m: Cs 60mm -11.89-12.16m: 3x J25-35°, pl, sm, cln	С	-		PL(A) = 0.4 PL(A) = 0.4
- 8	13.75	SANDSTONE: fine grained, grey			<<		12.25m: Fg 40mm 12.35m: Fg 40mm 12.4m: J30°, pl ,sm, cln 12.45-12.56m: Ds 110mm	с			
	- 14	and pale grey, very thinly cross-bedded, medium to high strength, fresh, fractured, Hawkesbury Sandstone					12.58-12.7m: 2x J70-80°, pl, sm, cln 13.25-13.35m: Clay band 100mm 13.74m: Fg 20mm		-		PL(A) = 2.4
	- 15						14.52-14.79m: Cz 270mm 14.74m: B15°, pl, sm, cbs vn				PL(A) = 0.7
	- 16	SANDSTONE: fine to medium grained, grey and pale grey,					15.59-15.64m: Cz ∖150mm 15.77m: CORE LOSS:	С			PL(A) = 1.2
	16.22	cross-bedded, high strength, fresh, unbroken, Hawkesbury Sandstone					450mm			-	
	- 17						17.16-17.19m: 3x B15°, pl, he	с	100		PL(A) = 1.1
9/	- 18	Below 18.2m: coarse grained									PL(A) = 1.3
121	18.85										PL(A) = 1.1
	- 19	Bore discontinued at 18.85m - target depth reached									
74											

RIG: Bobcat

CLIENT:

PROJECT:

LOCATION:

Deicorp Pty Ltd

Crows Nest

Fiveways Crows Nest

Pacific Highway, Alexander St, Falcon St,

DRILLER: Ground Test

LOGGED: ECB

CASING: HWT to 1.3m

TYPE OF BORING: Diatube to 0.1m, Solid flight augering to 1.3m, NMLC Coring to 18.85m WATER OBSERVATIONS: No free groundwater observed

	SAMPLIN	IG & IN SITU TESTING	LEGEND		
A Auger sar	nple G	Gas sample	PID Photo ionisation detector	(ppm)	
B Bulk samp	e P	Piston sample	PL(A) Point load axial test Is(50)) (MPa)	Douglas Partners
BLK Block san	ple U	, Tube sample (x mm dia.)	PL(D) Point load diametral test ls	ś(50) (MPa)	
C Core drilli	ig W	Water sample	pp Pocket penetrometer (kPa	a)	
D Disturbed	šample ⊳	Water seep	S Standard penetration test	, i	
E Environme	ntal sample 🛛 📱	Water level	V Shear vane (kPa)		Geotechnics Environment Groundwater

CLIENT:

PROJECT:

LOCATION:

Deicorp Pty Ltd **Fiveways Crows Nest**

Crows Nest

Pacific Highway, Alexander St, Falcon St,

SURFACE LEVEL: 93.6 m AHD BORE No: BH104 **EASTING:** 333577 **NORTHING:** 6255452.5 DIP/AZIMUTH: 90°/--

PROJECT No: 86645.03 DATE: 17 - 19/5/2023 SHEET 1 OF 2

_			Crows nest					. 90 /		SHEET I UF 2	
	_		Description	ic		Sam		In Situ Testing	-	Well	
R	De (r	epth m)	of	Graphic Log	e	oth	ple	Results &	Water	Construction	
	(.	,	Strata	Ū	Type	Depth	Sample	Results & Comments	>	Details	
	-	0.1	CONCRETE: 100mm thick	6.		0.2				Gatic cover	
		0.25	FILL/GRAVEL: sub-angular bluemetal gravel, grey, with	$\overline{7}$	E E	0.3				-	
93-	-		plastic fines, moist	$\langle / /$	<u>E</u>	0.4 0.5					
Ē	-		Silty CLAY CI: medium plasticity, pale grey, grey and red, trace non-plastic fines, w~PL, apparently hard, extremely							Blank pipe	
	-1		weathered shale	$\langle / / \rangle$						-1 -1	
Ē	-	1.3	SHALE: brown, thinly laminated, very low strength, highly	$\underline{//}$		1.3					
5	-		weathered then slightly weathered, fractured, Ashfield								
	-		Shale	====		1.67		PL(A) = <0.1		-	
Ē	-2			===						-2	
	-			<u> </u>							
	-				с	2.48		PL(A) = <0.1			
5				<u>E</u>							
	- 3			E						Bentonite 3.7-5.8m	
F	-										
				E							
-6	-			<u> </u>		3.58		PL(A) = <0.1		-	
Ē	- - - 4			F===		3.87					
										-	
Ē	-					4.47		PL(A) = <0.1	Ţ	-	
-8								1200	-23		
				<u> </u>	с				17-05-23		
Ē	-5	5.12	SHALE: brown, thinly laminated, very low strength, highly	<u> </u>		5.04		PL(A) = <0.1		-5	
	-		weathered then slightly weathered, fractured, Ashfield	$ \times $						-	
-88	-	5.61	Shale	\vdash							
						5.87				-	
Ē	-6			E						-6	
	-			====		6.42		PL(A) = <0.1			200
87	-		Below 6.42m: very low to low	F====		0.42		1 L(A) = 30.1		-	2001
Ē	-			F===							
	-7				с						
Ē	-					7.39		PL(A) = 0.1		-	
-98				E		1.59		FL(A) = 0.1		-	0
Ĩ										-	
F	-8			E						-8	
	-	8.27				8.26		PL(A) = <0.1		-	
E.	-	8.41	Below 8.41m: fresh			8.41				-	
85	-			EE							11111
ţ	-9			<u> </u>						- 9	0.0
Ē	-			<u> </u>	с					E	
E	-			[===							
-8-	-			EEE							00-00
E	-	10.0								-	200

RIG: Bobcat DRILLER: Ground Test LOGGED: ECB CASING: HWT to 1.3m TYPE OF BORING: Diatube to 0.1m, Solid flight augering to 1.3m, NMLC Coring to 18.85m WATER OBSERVATIONS: No free groundwater observed



Deicorp Pty Ltd

Crows Nest

Fiveways Crows Nest

Pacific Highway, Alexander St, Falcon St,

CLIENT:

PROJECT:

LOCATION:

 SURFACE LEVEL:
 93.6 m AHD

 EASTING:
 333577

 NORTHING:
 6255452.5

 DIP/AZIMUTH:
 90°/-

BORE No: BH104 PROJECT No: 86645.03 DATE: 17 - 19/5/2023 SHEET 2 OF 2

Sampling & In Situ Testing Well Description Graphic Log Water Depth Construction 宧 of Sample Depth Type Results & Comments (m) Strata Details SHALE: dark grey, thinly laminated, very low to low strength, fresh, fragmented to fractured, Ashfield Shale С At 10.03m: tuff layer, 10mm 10.48 -8 10.59 10.6 11 ¹¹ 11.05 11 52 PL(A) = <0.1 8 Below 11.6m: medium strength 12 12 12.1 PL(A) = 0.3Gravel 5.8-18.8m 12.67 Machine slotted С PVC screen 13 6.8-18.8, 12.96 PL(A) = 0.4 PL(A) = 0.4 13 13.0 SILTSTONE: pale grey, thickly laminated, medium strength, fresh, fractured, Mittagong Formation 13.0 _ . _ -8 13.75 С SANDSTONE: fine grained, grey and pale grey, very 13.97 PL(A) = 2.4 thinly cross-bedded, medium to high strength, fresh, 14 14 fractured, Hawkesbury Sandstone 14.58 14.96 PL(A) = 0.7 15 15 ° С 15.48 PL(A) = 1.2 . . . 15.77 SANDSTONE: fine to medium grained, grey and pale grey, cross-bedded, high strength, fresh, unbroken, Hawkesbury Sandstone 16 16 16.22 16.22 16.95 PL(A) = 1.1 17 - 17 С 17.96 PL(A) = 1.3 18 - 18 Below 18.2m: coarse grained -¹⁰ End cap .18.81 .PL(A) = 1.1 18 85 Bore discontinued at 18.85m 18.85 10 19 - target depth reached

 RIG:
 Bobcat
 DRILLER:
 Ground Test
 LOGGED:
 ECB
 CASING:
 HWT to 1.3m

 TYPE OF BORING:
 Diatube to 0.1m, Solid flight augering to 1.3m, NMLC Coring to 18.85m
 Diatube to 0.1m, Solid flight augering to 1.3m, NMLC Coring to 18.85m
 WATER OBSERVATIONS:
 No free groundwater observed

 PEMABLES:
 Craundwater well installed to 18 gm
 Served 6 gm
 18 gm
 Selid DVC 0.1m
 6 gm
 Send to 5 gm
 Bentanite to 0.5m

	SAN	IPLING	3 & IN SITU TESTING	LEGEND	7
A	Auger sample	G	Gas sample	PID Photo ionisation detector (ppm)	
B	Bulk sample	P	Piston sample	PL(A) Point load axial test Is(50) (MPa)	Douglas Partners
BL	Block sample	U,	Tube sample (x mm dia.)	PL(D) Point load diametral test ls(50) (MPa)	
C	Core drilling	Ŵ	Water sample	pp Pocket penetrometer (kPa)	
D	Disturbed sample	⊳	Water seep	S Standard penetration test	
E	Environmental sample	Ŧ	Water level	V Shear vane (kPa)	Geotechnics Environment Groundwater

BORE: BH104	PROJECT: 86645.03	MAY 2023
Contraction Contra	Core Box No.: - Box 1/L	
86645.03 BM104 3		Charles Charles
3		LI WINE
4 CORE LO	ss 490 mm	





	Douglas Pa Geotechnics Environment	Groundwater	Project No: 8464 BH ID: 8H1o4 Depth: 16.00 - Core Box No.: 8	and the second se	0.1.0
6	RE LOSS 220mm				
7		and have seen of			
8					EOH @ 18-85m

SURFACE LEVEL: 98.1 m AHD BORE No: BH105 **EASTING:** 333534.6 **NORTHING:** 6255480 **DIP/AZIMUTH:** 90°/--

PROJECT No: 86645.03 DATE: 31/5 - 6/6/2023 SHEET 1 OF 3

197 - 197 - 197 - 198 - RL			Description of Strata \FLOORBOARDS: wooden flooring, [herin	Graphic			ngth		22	0				-		
	0	.02⁄-	Strata					1	: :c		اعل	ate		icing n)	B - Bedding J - Joint	ø	e %	ا ۵	Test Results
			\FLOORBOARDS: wooden flooring, [≥ ≥	SW FS	_ ق _	x Low	§ 9 ediu	ngth	L Hig	≥ ^{0.0}	•		S - Shear F - Fault	Type	Core Rec. %	RQ %	& Comments
		0.5			⊑ ≥ 	<u>о ш</u>	ш. 	<u> ></u>	<u> </u>		>'ш 								Comments
		0 E	20mm																
	1	0.5	VOID: 480mm	l¦	i						;	- li					-		
L L		0.9	FILL/Gravelly Silty SAND: fine, pale grey, angular concrete and brick gravel, non-plastic fines, with concrete cobbles, wood fragments, metal sheeting, plastic, fluorescent lights, brick and wire, dry, apparently loose													A A			
	-2		Silty CLAY (CL): low plasticity, orange-brown, non-plastic fines, trace gravel, w < PL, apparently stiff, residual Below 1.2m: red and pale grey, with ironstone gravel																
			Below 2.5m: extremely weathered shale																
	•3																		
94	•4	3.6-	SHALE: dark grey and mottled orange, thinly laminated, very low to low strength, highly weathered then moderately weathered, highy										ן וו וו		3.68m: B0°, pl, sm, fe stn 3.75m: B0°, pl, sm, fe	с	100	62	PL(A) = 0.1
	4	.37	fractured, Ashfield Shale		\geq					\leq					stn, cly ctg 10mm 4.1m: CORE LOSS: 270mm				PL(A) = 0.1
	- 5		Below 5.0m: pale to dark grey, slightly weathered									06-06-23 ∲▲ 		 	4.86m: J60°, pl, sm, cln 4.89m: J40°, pl, sm, cln 4.91m: B0, pl, sm, cly vn 5.03m: Fg 60mm 5.13m: J85°, pl, sm, cln	с	82	80	PL(A) = <0.1
	- 6		Below 6.0m: fresh												5.29m: Fg 20mm 5.46m: B, pl, sm, cly ctg 5mm 5.49m: Ds 30mm 5.53m: J55°, pl, sm, cln 6.11m: J40°, pl, sm, cln 6.20-6.30m: J60°, pl, sm, cln 6.29m: J40°, pl, sm, cln	с	100	61	PL(A) = 0.1
	7												╡	ן	6.35m: Fg 30mm 6.42m: Fg 40mm 6.52-6.77m: 2x J40°, pl, sm, cln				PL(A) = <0.1
	· 8														16.83m: Cs 30mm 16.89m: J40°, pl, sm, cln 17.1m: J30°, pl, sm, cln 17.12m: Cs 30mm 17.22m: J40°, pl, sm, cln 17.33-7.52m: Fg 190mm 17.90-7.97m: 2x J45°, pl, sm, cln 18m: J30°, pl, sm, cly vn	с	100	63	PL(A) = 0.1 PL(A) = 0.1
	· 9							 		 	 		 	┛╎ ┨╎╎	18.09m: Cs 20mm 8.21m: B0°, pl, sm, cly vn 8.66m: Fg 30mm				
		0.0											لر اللے الا		 *8.86m: BÕ°, pl, sm, cly ctg 20mm *8.89m: J60°, pl, sm, cln *8.95-9.14m: J60-70°, pl, sm, cln *9.23m: J75°, pl, sm, cln *9.3m: B0°, pl, sm, cly 	с	100	52	PL(A) = <0.1

RIG: Geo 205

CLIENT:

PROJECT:

LOCATION:

Deicorp Pty Ltd **Fiveways Crows Nest**

Crows Nest

Pacific Highway, Alexander St, Falcon St,

DRILLER: Ground Test

LOGGED: ECB

CASING: PVC to 3.4m

TYPE OF BORING: Diatube to 0.02m, Solid flight augering to 1.5m, Wash boring to 3.6m, NMLC coring to 23.31m

WATER OBSERVATIONS: No free groundwater observed



SURFACE LEVEL: 98.1 m AHD BORE No: BH105 **EASTING:** 333534.6 **NORTHING:** 6255480 **DIP/AZIMUTH:** 90°/--

PROJECT No: 86645.03 DATE: 31/5 - 6/6/2023 SHEET 2 OF 3

Π		Description	Degree of	Rock	Fracture	Discontinuities	S	amolir	na & I	n Situ Testing
RL	Depth	of	Veathering ≥ ≥ ≥ ≤ ∞ ∞	Strength High High High	Spacing				-	Test Results
Ľ.	(m)	Strata	Gra	Ex Low Very Low Medium Very High Ex High	0.01 0.050 0.050 0.050 0.050 0.050	B - Bedding J - Joint S - Shear F - Fault	Type	Core Rec. %	RQI %	&
-88		SHALE: pale to dark grey, thinly	ш́±≥́о́ш́́⊞—–			ctg 10mm	С	100	52	Comments
	10.24	laminated, very low to low strength,fresh, highy fractured, Ashfield Shale				9.38m: J55°, pl, sm, cln 9.41m: B0°, pl, sm, cly cn 9.57m: J50°, pl, sm, cln 9.82m: J90°, pl, sm, cln		100	02	PL(A) = <0.1
87	-11	Below 11.5m: low strength, slightly				10.06m: J60°, pl, sm, cln 10.11m: Ds 50mm 10.19m: CORE LOSS: 50mm 10.28m: Cs 30mm	С	97	55	PL(A) = 0.2
	- 12	fractured			L	10.86m: Fg 20mm 10.98m: B0°, pl, sm, cly ctg 5mm 11.06-11.12m: 2x J30°, pl, sm, cln 11.25m: J50°, pl, sm, cln	с	100	91	PL(A) = 0.1
85	- 13	Below 12.5m: medium and high strength			 	11.41m: J30°, pl, sm, fg 11.48m: B0°, pl, sm, cly ctg 5mm 11.50-11.60m: 4x J30°, ir, sm, cln				PL(A) = 0.7 PL(A) = 1
84	- 14					11.76m: J50°, pl, sm, cln 11.84-11.94m: J70°, pl, sm, cln 12.52m: J30°, pl, he 13.35-13.74m: 3x J35-55°, pl, sm, cln 14.04m: J45°, pl, sm,	с	100	57	PL(A) = 1.7
		Between 14.67 and 14.77m: pyrite inclusions				14.23m: J30°, pl, he 14.23-14.28m: 2x J30°, pl, he 14.31m: J85°, pl, p he	C	100,		PL(A) = 1.5
83	- 15					-14.33m: J50°, pl, sm, cln -14.45-14.49m: 2x J20-30°, pl, sm, cln, fg	с	100	27	
82	- 16					*14.68m: J40°, pl, sm, cln *14.74m: F40°, pl, sm, slickenside, *14.84m: J25°, pl, sm, cln	с	100	86	PL(A) = 0.6 PL(A) = 0.5
81	- 17					14.94-15.08m: J75°, pl, sm, cln 15.08m: B0°, pl, sm, cly ctg 2mm 15.11m: J10°, pl, sm, cln 15.36m: J25°, pl, sm,	с	100	65	
	17.41	SILTSTONE: grey, thickly laminated, medium strength, fresh, fractured, Mittagong Formation				cln -15.55m: J20°, pl, sm, cln -15.98m: J30°, pl, sm, cln				PL(A) = 0.4
	- 18	SANDSTONE: fine to medium grained, pale grey and grey, thinly cross-bedded, with siltstone laminations (40%), medium to high and high strength, fresh, slightly fractured then unbroken, Hawkesbury Sandstone				17.06m: B0°, pl, sm, cly vn 17.27m: J60°, pl, sm, cly vn 17.36m: J30°, pl, sm, cln 17.45-17.52m: slickensides	с	100	75	PL(A) = 1 PL(A) = 0.4
62	20.0					17.57m: Fg 40mm 17.64m: B0°, pl, sm, cly vn 17.7m: Fg 50mm 17.76-17.88m: J85°, pl, sm, cln, p he 18.18m: J20°, pl, sm,	с	100	76	PL(A) = 1.3

RIG: Geo 205

CLIENT:

PROJECT:

LOCATION:

Deicorp Pty Ltd **Fiveways Crows Nest**

Crows Nest

Pacific Highway, Alexander St, Falcon St,

DRILLER: Ground Test

LOGGED: ECB

CASING: PVC to 3.4m

TYPE OF BORING: Diatube to 0.02m, Solid flight augering to 1.5m, Wash boring to 3.6m, NMLC coring to 23.31m WATER OBSERVATIONS: No free groundwater observed



SURFACE LEVEL: 98.1 m AHD BORE No: BH105 EASTING: 333534.6 **NORTHING:** 6255480 **DIP/AZIMUTH:** 90°/--

PROJECT No: 86645.03 DATE: 31/5 - 6/6/2023 SHEET 3 OF 3

		Description	Degree of Weathering ≞ ≩ ≩ ≶ ፼ ፼	<u>.</u>	Rock Strength _ত	Fracture	Discontinuities	Sa	ampli	ng &	In Situ Testing
님	Depth (m)	of		Log		Spacing (m)	B - Bedding J - Joint	be	e.	RQD %	Test Results
	()	Strata	E S W W W	Ū	Very Low Very Low Medium Very High Ex High		S - Shear F - Fault	Type	ပြီ မို	R0%	& Comments
78	20.6	SANDSTONE: medium grained,					l cln 18.19m: J55°, pl, sm, cln 18.39m: Fg 50mm 18.62m: J40°, pl, ro, cln 18.76m: B0°, pl, ro, cly	С	100		PL(A) = 0.7
76	-21	pale grey, cross-bedded, trace siltstone laminations, high strength, fresh, unbroken, Hawkesbury Sandstone Below 20.61m: minor siltstone laminations					vn 18.77m: B0°, pl, ro, cly ctg 10mm 18.81m: J30°, pl, ro, cln 19.03m: B0°, pl, ro, cly vn 19.52m: J20°, pl, sm, cln 19.92m: J60°, pl-ir, ro, cly and fg 20.13m: J60°, pl-ir, ro,	С	100	100	PL(A) = 1.5 PL(A) = 1.3
75	-23 -23 -23.31						20.54m: Fg and Cly 80mm	с	100	100	PL(A) = 1.1 PL(A) = 1.4
		Bore discontinued at 23.31m - target depth reached									
74	- 24										
73	- 25										
72	- 26										
	-27										
20	- 28										
69	- 29										

RIG: Geo 205

CLIENT:

PROJECT:

LOCATION:

Deicorp Pty Ltd **Fiveways Crows Nest**

Crows Nest

Pacific Highway, Alexander St, Falcon St,

DRILLER: Ground Test

LOGGED: ECB

CASING: PVC to 3.4m TYPE OF BORING: Diatube to 0.02m, Solid flight augering to 1.5m, Wash boring to 3.6m, NMLC coring to 23.31m

WATER OBSERVATIONS: No free groundwater observed



SURFACE LEVEL: 98.1 m AHD 333534.6 EASTING: NORTHING: 6255480 DIP/AZIMUTH: 90°/--

BORE No: BH105 **PROJECT No: 86645.03** DATE: 31/5 - 6/6/2023 SHEET 1 OF 3

Sampling & In Situ Testing Graphic Log Well Description Water Depth Sample 宧 of Depth Construction Type Results & Comments (m) Details Strata 0.02 FLOORBOARDS: wooden flooring, 20mm -8 VOID: 480mm 0.5 0.5 Stopcock FILL/Gravelly Silty SAND: fine, pale grey, angular E 0.6 concrete and brick gravel, non-plastic fines, with concrete cobbles, wood fragments, metal sheeting, plastic, Blank pipe 0.9 0.9 0.0-11.31m A fluorescent lights, brick and wire, dry, apparently loose 1.0 Silty CLAY (CL): low plasticity, orange-brown, non-plastic 1.3 fines, trace gravel, w < PL, apparently stiff, residual А 1.5 Below 1.2m: red and pale grey, with ironstone gravel 2 -2 -8 Below 2.5m: extremely weathered shale - 3 -3 -ജ 36 3.6 SHALE: dark grey and mottled orange, thinly laminated, very low to low strength, highly weathered then moderately weathered, highly fractured, Ashfield Shale С 3.88 PL(A) = 0.1Δ - 4 -2 4.1 4.37 4.43 PL(A) = 0.1С 4 94 PL(A) = <0.1 5 -5 T -8 Below 5.0m: pale to dark grey, slightly weathered 06-06-23 Bentonite 0.5-10.6m 5.6 PL(A) = 0.15.77 6 6 Below 6.0m: fresh -8 С 6.94 PL(A) = <0.1 - 7 7 -7 7.15 7.77 PL(A) = 0.1 С 8 - 8 -8 8.42 PL(A) = 0.1 8.62 q - q -ഇ С 9.49 PL(A) = <0.1 10.0

RIG: Geo 205

TYPE OF BORING:

CLIENT:

PROJECT:

LOCATION:

Deicorp Pty Ltd

Crows Nest

Fiveways Crows Nest

Pacific Highway, Alexander St, Falcon St,

DRILLER: Ground Test

LOGGED: ECB

CASING: PVC to 3.4m Diatube to 0.02m, Solid flight augering to 1.5m, Wash boring to 3.6m, NMLC coring to 23.31m

WATER OBSERVATIONS: No free groundwater observed



SURFACE LEVEL: 98.1 m AHD BORE No: BH105 **EASTING:** 333534.6 **NORTHING:** 6255480 DIP/AZIMUTH: 90°/--

PROJECT No: 86645.03 **DATE:** 31/5 - 6/6/2023 SHEET 2 OF 3

Π		Description	υ		Sam	pling a	& In Situ Testing		Well	
R	Depth	of	og					Water	Construction	n
	(m)	Strata	Graphic Log	Type	Depth	Sample	Results & Comments	Ň	Details	1
-8		SHALE: pale to dark grey, thinly laminated, very low to low		С	10.19					
	10.24	strength, fresh, highy fractured, Ashfield Shale	F===		10.15				-	
<u>}</u>			<u> </u>		10.51		PL(A) = <0.1		-	
<u> </u>			E						-	
Ę	-11			С					-11	
6	-		F====							20000000000000000000000000000000000000
ŀ	-		<u> </u>		11.42		PL(A) = 0.2		-	
ļ	-	Below 11.5m: low strength, slightly fractured			11.67				-	
ŀ	10		<u> </u>		11.81		PL(A) = 0.1		- 12	001 001
-8	-12								- 12	
			F====	с					-	
		Below 12.5m: medium and high strength							-	000
E			E		12.78		PL(A) = 0.7		[
-8	-13				13.0		PL(A) = 1		- 13	
[]	:		E		13.22					
E										
<u>}</u>	-		<u> </u>						-	00000 00000
Ŀ	- 14		<u> </u>	с	13.92		PL(A) = 1.7		- 14	
-2	-									
	-		<u> </u>		14.53		PL(A) = 1.5		-	600
<u> </u>		Between 14.67 and 14.77m: pyrite inclusions					1 L(A) = 1.5		-	
Ē	- 15	Detween 14.07 and 14.77m. pyrite inclusions	====	_C_	14.79 14.84				- 15	
-8	-		<u></u>	с					- 15	00000 00000
					15.44				-	
Ē	-		E						-	
	-			с	15.88		PL(A) = 0.6		-	
8-	- 16				16.13		PL(A) = 0.5		- 16	
Ē					16.31					
									-	
	-								- - Gravel	
-20	-17		<u> </u>	с					10.3-23.31m	
Ĩ	.		E						- Machine slotted —	
	17.41	SILTSTONE: grey, thickly laminated, medium strength,	F=		17.42		PL(A) = 0.4		PVC screen 11.31-23.31m	00-00
E		fresh, fractured, Mittagong Formation								000
<u> </u>	- 17.9 - 18	SANDSTONE: fine to medium grained, pale grey and	<u> </u>		17.91				- 18	0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,
-8	:	grey, thinly cross-bedded, with siltstone laminations (40%), medium to high and high strength, fresh, slightly								
EĒ		fractured then unbroken, Hawkesbury Sandstone			10 50				[00000
t i	:			с	18.53		PL(A) = 1		-	
 					10.0					61=61
6	- 19				19.0		PL(A) = 0.4		- 19	
	:				19.43				-	
 	.				19.40		PL(A) = 1.3			0000
E				С						
	20.0				1		1	1		101-101

RIG: Geo 205

CLIENT:

PROJECT:

LOCATION:

Deicorp Pty Ltd

Crows Nest

Fiveways Crows Nest

Pacific Highway, Alexander St, Falcon St,

DRILLER: Ground Test

LOGGED: ECB

CASING: PVC to 3.4m TYPE OF BORING: Diatube to 0.02m, Solid flight augering to 1.5m, Wash boring to 3.6m, NMLC coring to 23.31m

WATER OBSERVATIONS: No free groundwater observed

	SAM	PLINC	3 & IN SITU TESTING	LEG	END]			
A	Auger sample	G	Gas sample	PID	Photo ionisation detector (ppm)			_	— –
В	Bulk sample	Р	Piston sample) Point load axial test Is(50) (MPa)				Doutrooko
BLK	Block sample	U,	Tube sample (x mm dia.)	PL(C) Point load diametral test ls(50) (MPa)				Pariners
C	Core drilling	Ŵ	Water sample	pp	Pocket penetrometer (kPa)			140	Partners
D	Disturbed sample	⊳	Water seep	S	Standard penetration test		_		
E	Environmental sample	Ŧ	Water level	V	Shear vane (kPa)		Geotechnics	Envir	onment Groundwater
	· · · · ·					-			

CLIENT:

PROJECT:

LOCATION:

Deicorp Pty Ltd **Fiveways Crows Nest**

Crows Nest

Pacific Highway, Alexander St, Falcon St,

SURFACE LEVEL: 98.1 m AHD BORE No: BH105 EASTING: 333534.6 **NORTHING:** 6255480 **DIP/AZIMUTH:** 90°/--

PROJECT No: 86645.03 DATE: 31/5 - 6/6/2023 SHEET 3 OF 3

		Crows Nest					n: 90 /		SHEET 3 OF 3
		Description	jc		Sam		& In Situ Testing	L.	Well
RL	Depth (m)	of Strata	Graphic Log	Type	Depth	Sample	Results & Comments	Water	Construction Details
82	- 20.6	SANDSTONE: refer above		С	20.43		PL(A) = 0.7		
	-21	SANDSTONE: medium grained, pale grey, cross-bedded, trace siltstone laminations, high strength, fresh, unbroken, Hawkesbury Sandstone Below 20.61m: minor siltstone laminations			20.87 20.95		PL(A) = 1.5		
	- 22			с	21.95		PL(A) = 1.3		
92	-				22.3				
75	-23			С	22.95		PL(A) = 1.1		
-	23.31	Bore discontinued at 23.31m			23.26 23.31		PL(A) = 1.4		- 23
-	- - - - - 24	- target depth reached							-24
74	- - - -								
13	- 25								-25
72	-26								-26
	- 27								-27
	-28								-28
	-29								-29
	- - - -								

RIG: Geo 205 DRILLER: Ground Test LOGGED: ECB CASING: PVC to 3.4m TYPE OF BORING: Diatube to 0.02m, Solid flight augering to 1.5m, Wash boring to 3.6m, NMLC coring to 23.31m WATER OBSERVATIONS: No free groundwater observed



BORE: BH105	PROJECT: 86645.03	JUNE 2023
Douglas Part Geotechnics Environment Gro	Oundwater Project No: - 86645.03 BH ID: Core Box No.: - 1 or 5 Core Box No.: - 1 or 5	
86645.03 CROWS NEST	3 21	
5		
	3.6 – 8.0m	

Project No: 86645.03 BH ID: BHIOS Depth: Sto-13.0 mr Core Box No.: 2 or 5	BORE: BH105	PROJECT: 86645.03	JUNE 2023
		ater Depth: 8.0-13.0 m Core Box No.: 2 or 5	di cultura di cu
	Alter Alter Alter		



BORE: BH105	PROJECT: 86645.03	JUNE 2023
Douglas Partner Geotechnics Environment Groundwa	Project No: - 86645.03 BH ID: 9 64105 Depth: 18:0 - 25.0m Core Box No: - 1 of 5	
18		
20 21 (
	18.0 – 23.0m	



SURFACE LEVEL: 96.8 m AHD BORE No: BH106 **EASTING:** 333580 **NORTHING:** 62255395 DIP/AZIMUTH: 90°/--

PROJECT No: 86645.03 **DATE:** 7 - 15/6/2023 SHEET 1 OF 3

Γ			Description	Τ	De	egr	ee o	f		Т	Roc			Fr	acture	Discontinuities	Sa	ampli	na & I	n Situ Testing
RL	Dep		Description of	V	Ve	ath	nerin	g	Graphic	<u>_</u>	Streng	gth	Water		pacing				. <u> </u>	Test Results
R	(n	n)	Strata		>	>	>		Gra	5	Very Low Medium	, E H E H E H E H	Š,	- u	(m)	B - Bedding J - Joint S - Shear F - Fault	Type	ec	RQD %	&
\vdash		0.02	TILE: 20mm thick /	٦ -	È	₹	SW FS	Æ		ٽ ب	:ا <u>چ</u> ارداردان	<u></u> <u></u> 1812			0.10			~ 22	-	Comments
EE			FILL/CONCRETE: 230mm thick		į.	İ	İ		4	4	İİİİ	İİ		į	i ii					
k			with steel reinforcement																	
ŧ,			VOID: 750mm		ļ.	İ	Ì				İİİİ	ÌÌ		ĺ	İİİ					
-96	_ 1	1.0			 															
		1.0	FILL/Silty SAND: fine to medium, brown-grey, with sub-angular to		ļ	İ	Ì		\bigotimes	5	İİİİ	İİ		ĺ	İİİ		Е			
 			sub-rounded brick, ceramic and		 				\bigotimes	Z										
ĒĒ		Ē	igneous gravel, dry, apparently loose		Ì.				\bigotimes	\$							E			
-95		1.9	At 1.5m: asbestos fragment						\bigotimes	4										
	-2	1.0	observed // FILL/GRAVEL: dark grey,		ļ.				\bigotimes	8							с			
F F			sub-angular igneous gravel, dry,		 				\otimes	Ž										
ĒĒ		2.5	apparently medium dense		į.	İ	İ		\sum		İİİİ	i i		ĺ	i ii					
- 49			Silty CLAY CL: medium plasticity, brown, with rootlet, w > PL,		 				\mathbb{X}	1										
F F	- 3		apparently firm, residual		ļ.		Ì		//	1										
ĒĒ			Below 3.2m: brown and red mottled						$\langle \rangle$								С			
			grey, with ironstone gravel,						//	1										
È.		3.7	apparently very stiff Silty CLAY CL: medium to high						<u>//</u>	4						Unless otherwise stated,				
-8-	-4		plasticity, pale grey and red, with													discontinuities comprise (B0-10°, pl/un, sm/ro/he,				
[4		ironstone gravel, w~PL, apparently hard, residual						//	1						cln or fe stn, cly vn) and				
 			hard, roolddal													(J20-60°, pl, sm/he, cln or fe stn or cly vn)				
FF					ľ		ł		//	1										
-8		4.9							//	1					 •					PL(A) = <0.1
	- 5		SHALE: pale grey, grey and pale brown, thinly laminated, very low to		i		i	i		-	itti	Ϊİ			L _i	4.98m: J75°, pl, sm, cln				
ĒĒ			low strength, highly weathered with							-						5.11-5.34m: J65°, pl,	С	100	43	P(A) = 0.4
EE			extremely weathered bands, highly fractured, Ashfield Shale		i	İİ	i			-	i iriji	ii		İ	ŋ ii	sm, fe stn and fg 5.38m: J70°, pl, sm, cln				PL(A) = 0.4
-5-										-	╎╷┙				╏╎	5.51-5.69m: J70-75°, pl, √ sm, fe stn, cly vn				
ĒĒ	-6				Ì	İ	İ			-	j Ti i	ij		۲		5.73m: J90°, ir, sm, fe				
EE										-				đ		stn 5.83m: Cs 70mm				
					įL	Ļ	i			-	أألزا	ij			Ţ į	5.92m: J70°, pl, sm, fe				PL(A) = 0.1
-6			Below 6.5m: pale grey and dark grey, moderately weathered							-						6.02-6.13m: J80-85°, pl, sm, fe stn	С	100	85	
Ē	-7				ļ	İ	Ì			-	i i i i	ÌÌ		ĺ	i [i	6.33m: Cs 30mm				
ŧ ŧ										-					┟┛╎╎	^c 6.77-6.87m: J80°, pl, sm, cln				
ĘF										-				Ì						PL(A) = 0.1
$\begin{bmatrix} \\ \\ \\ \end{bmatrix}$				ſ	1	ľ				-					╡╎╎					
-8		7.8 7.93	SHALE: dark grey and pale grey,	Ľ	Þ	Þ	\triangleleft		\geq	t		#	1 4			7.63-7.80m: Fg 170mm 7.8m: CORE LOSS:				
ŧŧ	-8		thinly laminated, very low strength, slightly weathered with an extremely							-				-		130mm 8.02m: Cs 20mm	С	89	49	
EE			weathered band, highly fractured,							-						8.28-8.38m: J60-80°, pl,				PL(A) = 0.1
<u></u>			Ashfield Shale							-				-	╅┛╎╎	sm, cln				
-88										-				-4		8.57m: Cs 20mm 8.71m: J80°, pl, sm, cln 8.75m: Cs 20mm				
EE	-9			ſ		H]¦			-					۲, h	¹ 8.8m: J60°, pl, sm, cln				
<u></u>										-						⁸ .96m: B5°, pl, he, cly ctg 5mm		100		
ţţ				l		H	ן רו			-						0	С	100	57	
		9.8								-					┨╎╎	9.04-10.00m: J80°(x2), \ pl, sm, cly				
ŀ		9.0 10.0	SHALE: refer next page		Ĺ	Ĺ				-	iiii			j	ilii	9.67m: Cs 10mm				PL(A) = 0.1

RIG: Geo 205

CLIENT:

PROJECT:

LOCATION:

Deicorp Pty Ltd

Crows Nest

Fiveways Crows Nest

Pacific Highway, Alexander St, Falcon St,

DRILLER: Ground Test

LOGGED: ECB/YB

CASING: PVC to 1.9m

TYPE OF BORING: Diatube to 0.25m, Hand auger to 1.9m, NMLC to 3.6m, Wash boring to 4.5m, NMLC to 22.30m WATER OBSERVATIONS: No free groundwater observed

REMARKS: 100% water loss after 13.45m

SA	MPLIN	G & IN SITU TESTING	LEGEND	
A Auger sample	G	Gas sample	PID Photo ionisation detector (ppm)	
B Bulk sample BLK Block sample	P	Piston sample Tube sample (x mm dia.)	PL(A) Point load axial test Is(50) (MPa) PL(D) Point load diametral test Is(50) (MPa)	Douglas Partners
C Core drilling	Ŵ	Water sample	pp Pocket penetrometer (kPa)	Douglas Partners
D Disturbed sample	⊵	Water seep	S Standard penetration test (
E Environmental sample	e ž	Water level	V Shear vane (kPa)	Geotechnics Environment Groundwater

SURFACE LEVEL: 96.8 m AHD BORE No: BH106 **EASTING:** 333580 NORTHING: 62255395 DIP/AZIMUTH: 90°/--

PROJECT No: 86645.03 **DATE:** 7 - 15/6/2023 SHEET 2 OF 3

$\left[\right]$		Description	Degree of Weathering .⊖	Rock Strength	Fracture	Discontinuities	Sa	amplir	ng & l	n Situ Testing
R	Depth (m)	of	Weathering	Strendth Medium Keny High Ex High Mater	Spacing (m)	B - Bedding J - Joint	Type	ore : %	RQD %	Test Results
	(,	Strata	C R R R R R R R R R R R R R R R R R R R		0.01 0.10 0.50	S - Shear F - Fault	Ę	ပိမ္မိ	RS⊗	& Comments
	- - - -	SHALE: dark grey and pale grey, thinly laminated, very low to low strength, fresh with extremely weathered bands, fractured, Ashfield				10.21-10.34m: J70-80°, pl, sm, cly vn	С	100	57	
85	- 11	Shale At 10.03m: tuff layer, 5mm				10.34m: Cs 20mm 10.53m: B0°, pl, sm, cly ctg 5mm 10.49-10.63m: J70-80°, cu, sm, cly vn 10.56m: Ds 70mm 11.06m: Cs 20mm 11.10-11-30: J45-80°(x4), pl, sm, cln 11.46m: Cs 20mm 11.8m: J70-80°, pl, sm,	С	100	74	PL(A) = 0.1 PL(A) = 0.1
84	- 12 - 13					Cln 11.77-12.00m: J70-80°, pl, sm, cln 12.18m: J50°, pl, he, cln 12.25m: Cs 50mm 12.25-12.66m: J70-80°(x2), pl, sm, cln 12.76m: B0°, pl, he, cly ctg 5mm 12.78m: Cs 80mm	С	100	76	PL(A) = 0.2
83	- 14 - 14.3 -	SILTSTONE: dark grey and pale grey, thickly laminated, low strength,				13.66m: Cs 20mm 13.73m: J70-80°, pl, sm, cln 13.70-14.22m: J70-80°(x2), pl, sm, cln 14.22-14.34m: Ds 120mm	с	100	78	PL(A) = 0.2
	- 15	fresh, slightly fractured, Mittagong Formation				[└] 14.57m: B0°, pl, he, cly inf 5mm				PL(A) = 0.1
81	15.62	SANDSTONE: fine to medium grained, pale grey, distinctly and indistinctly bedded, with siltstone laminations, very low and low strength, fresh with extremely weathered bands, slightly fractured,				15.62-15.88m: Ds 260mm 16.16m: J45°, pl, ro, cly inf 5mm	С	100	84	PL(A) = <0.1
79	- 17	Mittagong Formation				17.25m: B10°, pl, ro, cbs vn 17.36m: Ds 80mm 17.38-17.40m: B5°(x2),	С	100	81	PL(A) = 0.1
78 7	- 18					pl, he, cbs vn 17.55m: B5°, pl, he, cly inf 5mm 17.62m: Ds 40mm 17.66-17.92m: J70-80°, pl, ro, cln 17.84m: Ds 40mm 18.22m: Ds 50mm	с	100	91	PL(A) = 0.2
	-19 19.0	SANDSTONE: fine to medium grained, pale grey, distinctly and indistinctly bedded, with siltstone laminations, high then medium to high strength, fresh, unbroken, Hawkesbury Sandstone				L18.46m: J45°, pl, ro, cly inf 5mm 18.91m: B5°, pl, ro, cbs vn 19.18m: B5°, pl, he, cbs vn 19.5m: Cs 20mm	с	100	99	PL(A) = 0.2 PL(A) = 1

RIG: Geo 205

CLIENT:

PROJECT:

LOCATION:

Deicorp Pty Ltd

Crows Nest

Fiveways Crows Nest

Pacific Highway, Alexander St, Falcon St,

DRILLER: Ground Test

LOGGED: ECB/YB

CASING: PVC to 1.9m

TYPE OF BORING: Diatube to 0.25m, Hand auger to 1.9m, NMLC to 3.6m, Wash boring to 4.5m, NMLC to 22.30m WATER OBSERVATIONS: No free groundwater observed

REMARKS: 100% water loss after 13.45m

	SAN	IPLIN	3 & IN SITU TESTING	LEG	END				
A	Auger sample	G	Gas sample	PID	Photo ionisation detector (ppm)	_		_	
B	Bulk sample	Р	Piston sample	PL(/	A) Point load axial test Is(50) (MPa)				Partners
BL	K Block sample	U,	Tube sample (x mm dia.)	PL(I	D) Point load diametral test ls(50) (MPa)	41.			Partners
C	Core drilling	Ŵ	Water sample	pp	Pocket penetrometer (kPa)			140	
D	Disturbed sample	⊳	Water seep	S	Standard penetration test	<u>.</u>			
E	Environmental sample	ž	Water level	V	Shear vane (kPa)		Geotechnics	Envir	onment Groundwater
	· · · ·								

SURFACE LEVEL: 96.8 m AHD BORE No: BH106 **EASTING:** 333580 **NORTHING:** 62255395 DIP/AZIMUTH: 90°/--

PROJECT No: 86645.03 **DATE:** 7 - 15/6/2023 SHEET 3 OF 3

		Description	Degree of Weathering ∴ £ ≹ § ⊗ ∞ ₭	Rock Strength	Fracture	Discontinuities	Sa	amplii	In Situ Testing	
⊾	Depth (m)	of		Strength Low Low Very High Weddum Address Strength Very High Vater Very High Address Strength Address Stre	Spacing (m)	B - Bedding J - Joint	Type	ore 3. %	RQD %	Test Results &
	()		A M M M M M M M M M M M M M M M M M M M	Ex Low Very Very Very	0.05	S - Shear F - Fault	Ţ	с я	RC %	Comments
76	-21	SANDSTONE: fine to medium grained, pale grey, distinctly and indistinctly bedded, with siltstone laminations, high then medium to high strength, fresh, unbroken, Hawkesbury Sandstone <i>(continued)</i>					с	100	99	PL(A) = 0.9
75	-22					21.13m: Ds 40mm	с	100	97	PL(A) = 0.9
	22.3	Bore discontinued at 22.3m								PL(A) = 0.4
74	-23	- target depth reached								
73	-24									
72	- 25									
71	-26									
20	-27									
	-28									
67	-29									

RIG: Geo 205

CLIENT:

PROJECT:

LOCATION:

Deicorp Pty Ltd

Crows Nest

Fiveways Crows Nest

Pacific Highway, Alexander St, Falcon St,

DRILLER: Ground Test

LOGGED: ECB/YB

CASING: PVC to 1.9m

TYPE OF BORING: Diatube to 0.25m, Hand auger to 1.9m, NMLC to 3.6m, Wash boring to 4.5m, NMLC to 22.30m WATER OBSERVATIONS: No free groundwater observed

REMARKS: 100% water loss after 13.45m

SAM	PLING & IN SITU TESTING	G LEGEND	
A Auger sample	G Gas sample	PID Photo ionisation detector (ppm)	
B Bulk sample	P Piston sample	PL(A) Point load axial test Is(50) (MPa)	Douglas Partners
BLK Block sample	U, Tube sample (x mm dia.)	PL(D) Point load diametral test ls(50) (MPa)	
C Core drilling	W Water sample	pp Pocket penetrometer (kPa)	
D Disturbed sample	Water seep	S Standard penetration test	
E Environmental sample	Water level	V Shear vane (kPa)	Geotechnics Environment Groundwater
· · · ·		. /	

BORE: BH106	PROJECT: 86645.03	JUNE 2023
Douglas Partners Geotechnics Environment Groundwate	Core Box No.: Box 1/4	
86645.03 BHIDE (ROWS NEST 9.6.23 5 6	Trans	S CORE LOSS 150mm
8	4.5 – 9.0m	





BORE: BH106	PROJECT: 86645.03	JUNE 2023
Douglas Partr Geotechnics Environment Grou	Project No: - 86645.03 BH ID: 684106 Depth: 019.00 - 22 Core Box No.: - Box 47	3om
2	End of Hole at	22.30 m
	19.0 – 22.3m	

Appendix D

Groundwater Level Readings







Appendix E

Permeability Test Results



Permeability Testing - Rising or Falling Head Test Report

Client: Project: Location:	Propose	Properties d Residential Pacific Hwy,			Project No: 86645.03 Test date: 09.06.2023 Tested by: YB
Test Locatio Description: Material type:	Standpip	e in borehole r Siltstone over	Sandston	е	Test No.BH103Easting:333582mNorthing6255420mSurface Level:96m AHD
Details of We Well casing d Well screen d Length of wel	iameter (2r) liameter (2R))	50 96 18	mm mm m	Depth to water before test7.8mDepth to water at start of test16.4m
Test Results					
Time (min)	Depth (m)	Change in Head: δH (m)	δH/Ho	_	
0.00	16.40 13.1	8.60 5.30	1.000 0.616	_	
10.00	11.15	3.35	0.390		
15.00	10.13	2.33	0.271	1.00	
20.00	9.6	1.80	0.209	1.00	
25.00	9.35	1.55	0.180		
30.00	9.19	1.39	0.162		
35.00	9.09	1.29	0.150		
45.00	8.97	1.17	0.136	o	
55.00	8.87	1.07	0.124	Head Ratio	
75.00	8.76	0.96	0.112	io d	
105.00	8.66	0.86	0.100	0.10	
				ead	
				Ť	
				0.01	1 1.00 10.00 100.00 1000.00
					Time (minutes)
					To = 10 mins 600 secs
Theory:	•	ead Permeability (Le/R)]/2Le To	calculated	where r = ra R = radius Le = length	by Hvorslev adius of casing of well screen of well screen aken to rise or fall to 37% of initial change
Hydra	ulic Condu	ctivity	k = =		



Permeability Testing - Rising or Falling Head Test Report

Client:Deicorp PropertieProject:Proposed ResideLocation:391-423 Pacific H						Project No: Test date: Tested by:	86645.03 09.06.20 YB	
Test Location Description: Material type:	Standpip	e in borehole / over Siltstone				Test No. Easting: Northing Surface Level:	BH105 333534 6255480 98.1	m m m AHD
Details of We	ell Installatio	on						
Well casing di	iameter (2r)		50	mm	Depth to	o water before test	5.11	m
Well screen d)	96	mm	Depth to	o water at start of t	est 10.66	m
Length of well	screen (Le)		12	m	•			
Test Results								
Time (min)	Depth (m)	Change in Head: δH (m)	δH/Ho					
0.00	10.66	5.55	1.000	-				
5.00	8.46	3.35	0.604	_				
10.00	6.76	1.65	0.297	_				
15.00	6.46	1.35	0.243					
20.00	6.32	1.21	0.218	1.00				
25.00	6.2	1.09	0.196					
30.00	6.11	1.00	0.180					
35.00	6.06	0.95	0.171					
40.00	5.99	0.88	0.159					
45.00	5.93	0.82	0.148	Head Ratio				
50.00	5.9	0.79	0.142	o dl			ر 	
55.00	5.85	0.74	0.133	0.10				
60.00	5.83	0.72	0.130	ad				<u> </u>
65.00	5.69	0.58	0.105	Р Н				
70.00	5.61	0.5	0.090					
75.00	5.56	0.45	0.081					
				0.01				
				0	10	1.00	10.00	100.00
				_		Time (min	utes)	
							mins	
Theory:	-	ad Permeability o	calculated u		-		secs	
	k = [r ² ln((Le/R)]/2Le To		where r = ra R = radius Le = length To = time ta	of well scre of well scr	een	tial change	
Hydra	ulic Condu	ictivity	k = =			m/sec cm/hour		

WATER PRESSURE TEST RESULTS

Client :	Deicorp P					Pro	ject No. :	86645.03								
Project :	Fiveways.	Crows Nest					Field inpu	t sheet only	,		Bore :		BH104			
-		er St, Crows								Test	section :			- 18.85 m		
Test Details		, -														
Date:		18-May-23		Bottom of p	acker (m):	14.50		Height of n	ressure gaug	ne (m):		1.0		Drum Area (m ²		
Bore diameter	(mm):	56		Bore depth		18.85		•	pth to ground			6.0	0.264			
Bore inclination (deg):		90		Section leng	. ,	4.35			base of pac	. ,		0.0		0.204		
		90 head loss in n	ods and nas		,		tor dopth) x									
		11680 1033 111	Test	(g	auge neight	· grounawa		RATES	- 11g •1110-111			Water	Lugeons	Approx		
Hg	н	Total	Total	Duration		Flowmeter		D	rum readin		Leakage	Assigned		-	Permeability	
(kPa)	(kPa)	(kPa)	(min)	Initial (litres)	Final (litres)	Total (litres)	Initial (mm)	Final (mm)	Equivalent litres	(litres)	Flow (litres)	(l/m/min)	(I/m/min at 1000 kPa)	(m/sec)		
()	(=)	(2)	()	(((()	()		(((********		(
50	0	119	5	250882.2	250883.6	1.4	780.0	775.0	1		1.4	0.1	0.5	5.4E-08		
50	0	119	5	250883.6	250884.1	0.5	775.0	775.0	0		0.0	0.0	0.0	0.0E+00		
50	0	119	5	250884.1	250884.2	0.1	775.0	775.0	0		0.0	0.0	0.0	0.0E+00		
	0	119	6			0.1			0		0.0	0.0	0.0			
50	0	119	0	250884.2	250884.2	0.0	775.0	775.0	0		0.0	0.0	0.0	0.0E+00		
100	0	169	5	250887.0	250893.2	6.2	765.0	740.0	7		6.2	0.3	1.7	1 75 07		
														1.7E-07		
100	0	169	5	250893.2	250898.5	5.3	740.0	720.0	5		5.3	0.2	1.4	1.4E-07		
100	0	169	5	250898.5	250904.2	5.7	720.0	700.0	5		5.7	0.3	1.6	1.6E-07		
100	0	169	5	250904.2	250910.3	6.1	700.0	690.0	3		6.1	0.3	1.7	1.7E-07		
100	0	169	5	250910.3	250915.8	5.5	690.0	670.0	5		5.5	0.3	1.5	1.5E-07		
140	0	209	5	250932.6	250946.9	14.3	605.0	550.0	15		14.3	0.7	3.2	3.2E-07		
140	0	209	5	250946.9	250961.1	14.2	550.0	500.0	13		14.2	0.7	3.1	3.1E-07		
140	0	209	5	250961.1	250974.4	13.3	500.0	460.0	11		13.3	0.6	2.9	2.9E-07		
140	0	209	5	250974.4	250987.8	13.4	460.0	410.0	13		13.4	0.6	3.0	3.0E-07		
100	0	169	5	250992.1	251004.1	12.0	390.0	340.0	13		12.0	0.6	3.3	3.3E-07		
100	0	169	5	251004.1	251015.6	11.5	340.0	300.0	11		11.5	0.5	3.1	3.1E-07		
100	0	169	5	251015.6	251027.1	11.5	300.0	260.0	11		11.5	0.5	3.1	3.1E-07		
50	0	119	5	251046.5	251050.4	3.9	500.0	480.0	3		3.9	0.2	1.5	1.5E-07		
50	0	119	5		251054.2	3.8	480.0	460.0	3		3.8	0.2	1.5	1.5E-07		
50	0	119	5		251058.1	3.9	460.0	460.0	3		3.9	0.2	1.5	1.5E-07		
	Ŭ		-			2.0			Ű		2.0					
Notes		1														







86645.03 BH104 14.50-18.85 Packer Results.xlsx

Appendix F

Groundwater Quality Results



CHAIN OF CUSTODY DESPATCH SHEET

Projec	t No:	86645.0	4		Subur):	Crows I	Vest						To:	Lab nar	ne		
	t Manager:	Paul Go				Number:				Samp	er:	TG			Lab add	dress		
Email		paul.gon	man@do	uglaspartne	rs.com.a	m.au F								Attn:	Name			
Turna	round time:	Standa	ard	72 hour	48 hour	24 ho		Same da	-						Lab pho	one		Lab email
Prior	Storage: 🗹 F	ridge 🔲	Freezer	Esky		Do sam	oles co	ntain '	potent	ial' HBI	Ŵ? ⊡	No	Yes	(If YE	S, then h	andle, tr	ansport a	and store in accordance with FPM HAZID)
	Sai	nple ID		oled	Sample Type	Container Type					/	Analyte	s					
Lab ID	Location / Other ID	Depth From	Depth To	Date Sampled	S - soil W - water M - Material	G - glass P - plastic	Combo 8 (dissolved and total)	PFAS- Short Suite	TDS/TSS	Oil &Grease	Ferrous Iron	Ferric Iron	Combo 3	BTEX				Notes/ Preservation/ Additional Requirements
·(BH103			20.6.23	w	G+P	х	Х	х		х	x						
2	BH104			22.6.23	w	G+P	×	х	x	x	х	x						
3	BH105			20.6.23	w	G+P	x	х	х		x	x					-	
4	BD1/20230620			20.6.23	w	G+P							x					
2	Trip Spike				· w	G								x			65.V.3	12 Ashley St
6	Trip Blank				w	G							L	x			4100	Ph: (02) 9910 6200
										<u> </u> !							<u>Job N</u> Date f	23/06/2023
										<u> </u>							Time I	ecolyed is 30
										<u> </u>							Temp	
					_												Secur	ty: Intact/Broken/None
	-			<u> </u>														8.5
					L					<u> </u>							 	
	 			ļ								<u> </u>					 	
		L															<u> </u>	<u>_</u>
·	s to analyse:															RECEI	<u>PT</u>	
	per of sample					Transpo	orted to	labora	atory b	<u>y:</u>	Courie	r				ef. No:		<u>p-0000</u>
	results to:	Douglas	Partners	Pty Ltd		Dhanas										ved by: k Time:		Leher Loury
Addre		<u> </u>	TO			Phone: Date:	22,6.23	1		Signe	d.	VG	\sim		Signe		<u>`1</u>	5/6/1013-15-10
Renu	quished by:		TG					,		Joighe	<u>u.</u>	<u>[</u>]]]	<u>`</u> `			M.		<u> </u>

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Envirolab Services Pty Ltd ABN 37 112 535 645 12 Ashley St Chatswood NSW 2067 ph 02 9910 6200 fax 02 9910 6201 customerservice@envirolab.com.au www.envirolab.com.au

SAMPLE RECEIPT ADVICE

Client Details	
Client	Douglas Partners Pty Ltd
Attention	Paul Gorman

Sample Login Details	
Your reference	86645.04 Crows Nest
Envirolab Reference	326366
Date Sample Received	23/06/2023
Date Instructions Received	23/06/2023
Date Results Expected to be Reported	30/06/2023

Sample Condition	
Samples received in appropriate condition for analysis	Yes
No. of Samples Provided	6 Water
Turnaround Time Requested	Standard
Temperature on Receipt (°C)	8
Cooling Method	Ice Pack
Sampling Date Provided	YES

Comments Nil

Please direct any queries to:

Aileen Hie	Jacinta Hurst							
Phone: 02 9910 6200	Phone: 02 9910 6200							
Fax: 02 9910 6201	Fax: 02 9910 6201							
Email: ahie@envirolab.com.au	Email: jhurst@envirolab.com.au							

Analysis Underway, details on the following page:



Envirolab Services Pty Ltd ABN 37 112 535 645 12 Ashley St Chatswood NSW 2067 ph 02 9910 6200 fax 02 9910 6201

customerservice@envirolab.com.au www.envirolab.com.au

Sample ID	vTRH(C6-C10)/BTEXN in Water	svTRH (C10-C40) in Water	PAHs in Water	Organochlorine Pesticides in Water	OP Pesticides in Water	PCBs in Water	Total Phenolicsin Water	HM in water - dissolved	HM in water - total	Total Suspended Solids	Total Dissolved Solids(grav)	Oil & Grease (LLE)	Ferrous Iron	Ferric Iron (by calculation)	PFAS in Waters Short
BH103	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	✓	✓		✓	✓	\checkmark
BH104	\checkmark	✓	✓	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	✓	✓	✓	✓	✓	\checkmark
BH105	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark	✓	✓		✓	✓	\checkmark
BD1/20230620	\checkmark	\checkmark	\checkmark					\checkmark	\checkmark						
Trip Spike	\checkmark														
Trip Blank	\checkmark														

The ' \checkmark ' indicates the testing you have requested. THIS IS NOT A REPORT OF THE RESULTS.

Additional Info

Sample storage - Waters are routinely disposed of approximately 1 month and soils approximately 2 months from receipt.

Requests for longer term sample storage must be received in writing.

Please contact the laboratory immediately if observed settled sediment present in water samples is to be included in the extraction and/or analysis (exceptions include certain Physical Tests (pH/EC/BOD/COD/Apparent Colour etc.), Solids testing, Total Recoverable metals and PFAS analysis where solids are included by default.

TAT for Micro is dependent on incubation. This varies from 3 to 6 days.



CERTIFICATE OF ANALYSIS 326366

Client Details	
Client	Douglas Partners Pty Ltd
Attention	Paul Gorman
Address	96 Hermitage Rd, West Ryde, NSW, 2114

Sample Details	
Your Reference	86645.04 Crows Nest
Number of Samples	6 Water
Date samples received	23/06/2023
Date completed instructions received	23/06/2023

Analysis Details

Please refer to the following pages for results, methodology summary and quality control data.

Samples were analysed as received from the client. Results relate specifically to the samples as received.

Results are reported on a dry weight basis for solids and on an as received basis for other matrices.

Please refer to the last page of this report for any comments relating to the results.

Report Details			
Date results requested by	30/06/2023		
Date of Issue	03/07/2023		
NATA Accreditation Number 2901. This document shall not be reproduced except in full.			
Accredited for compliance with ISO/IEC 17025 - Testing. Tests not covered by NATA are denoted with *			

Results Approved By Diego Bigolin, Inorganics Supervisor Jenny He, Senior Chemist Kyle Gavrily, Senior Chemist Loren Bardwell, Development Chemist Phalak Inthakesone, Organics Development Manager, Sydney <u>Authorised By</u> Nancy Zhang, Laboratory Manager



Client Reference: 86645.04 Crows Nest

vTRH(C6-C10)/BTEXN in Water						
Our Reference		326366-1	326366-2	326366-3	326366-4	326366-5
Your Reference	UNITS	BH103	BH104	BH105	BD1/20230620	Trip Spike
Date Sampled		20/06/2023	22/06/2023	20/06/2023	20/06/2023	20/06/2023
Type of sample		Water	Water	Water	Water	Water
Date extracted	-	26/06/2023	26/06/2023	26/06/2023	26/06/2023	26/06/2023
Date analysed	-	27/06/2023	27/06/2023	27/06/2023	27/06/2023	27/06/2023
TRH C ₆ - C ₉	µg/L	<10	<10	<10	<10	[NA]
TRH C ₆ - C ₁₀	µg/L	<10	<10	<10	<10	[NA]
TRH C ₆ - C ₁₀ less BTEX (F1)	µg/L	<10	<10	<10	<10	[NA]
Benzene	µg/L	<1	<1	<1	<1	104%
Toluene	µg/L	<1	<1	<1	<1	105%
Ethylbenzene	µg/L	<1	<1	<1	<1	119%
m+p-xylene	µg/L	<2	<2	<2	<2	100%
o-xylene	µg/L	<1	<1	<1	<1	110%
Naphthalene	µg/L	<1	<1	<1	<1	[NA]
Surrogate Dibromofluoromethane	%	112	111	121	118	101
Surrogate toluene-d8	%	110	108	118	116	107
Surrogate 4-BFB	%	104	106	107	108	109

vTRH(C6-C10)/BTEXN in Water		
Our Reference		326366-6
Your Reference	UNITS	Trip Blank
Date Sampled		20/06/2023
Type of sample		Water
Date extracted	-	26/06/2023
Date analysed	-	27/06/2023
TRH C ₆ - C ₉	µg/L	<10
TRH C6 - C10	µg/L	<10
TRH C ₆ - C ₁₀ less BTEX (F1)	μg/L	<10
Benzene	µg/L	<1
Toluene	µg/L	<1
Ethylbenzene	µg/L	<1
m+p-xylene	µg/L	<2
o-xylene	µg/L	<1
Naphthalene	µg/L	<1
Surrogate Dibromofluoromethane	%	119
Surrogate toluene-d8	%	120
Surrogate 4-BFB	%	104

Client Reference: 86645.04 Crows Nest

svTRH (C10-C40) in Water					
Our Reference		326366-1	326366-2	326366-3	326366-4
Your Reference	UNITS	BH103	BH104	BH105	BD1/20230620
Date Sampled		20/06/2023	22/06/2023	20/06/2023	20/06/2023
Type of sample		Water	Water	Water	Water
Date extracted	-	26/06/2023	26/06/2023	26/06/2023	26/06/2023
Date analysed	-	27/06/2023	27/06/2023	27/06/2023	27/06/2023
TRH C ₁₀ - C ₁₄	µg/L	<50	<50	<50	<50
TRH C ₁₅ - C ₂₈	µg/L	<100	<100	<100	<100
TRH C ₂₉ - C ₃₆	µg/L	<100	<100	<100	<100
Total +ve TRH (C10-C36)	µg/L	<50	<50	<50	<50
TRH >C10 - C16	µg/L	<50	<50	<50	<50
TRH >C ₁₀ - C ₁₆ less Naphthalene (F2)	µg/L	<50	<50	<50	<50
TRH >C ₁₆ - C ₃₄	µg/L	<100	<100	<100	<100
TRH >C ₃₄ - C ₄₀	µg/L	<100	<100	<100	<100
Total +ve TRH (>C10-C40)	µg/L	<50	<50	<50	<50
Surrogate o-Terphenyl	%	93	93	82	86
PAHs in Water					
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Our Reference		326366-1	326366-2	326366-3	326366-4
Your Reference	UNITS	BH103	BH104	BH105	BD1/20230620
Date Sampled		20/06/2023	22/06/2023	20/06/2023	20/06/2023
Type of sample		Water	Water	Water	Water
Date extracted	-	26/06/2023	26/06/2023	26/06/2023	26/06/2023
Date analysed	-	27/06/2023	27/06/2023	27/06/2023	26/06/2023
Naphthalene	µg/L	<0.2	<0.2	<0.2	<0.2
Acenaphthylene	µg/L	<0.1	<0.1	<0.1	<0.1
Acenaphthene	µg/L	<0.1	<0.1	<0.1	<0.1
Fluorene	µg/L	<0.1	<0.1	<0.1	<0.1
Phenanthrene	µg/L	<0.1	<0.1	<0.1	<0.1
Anthracene	µg/L	<0.1	<0.1	<0.1	<0.1
Fluoranthene	µg/L	<0.1	<0.1	<0.1	<0.1
Pyrene	µg/L	<0.1	<0.1	<0.1	<0.1
Benzo(a)anthracene	µg/L	<0.1	<0.1	<0.1	<0.1
Chrysene	µg/L	<0.1	<0.1	<0.1	<0.1
Benzo(b,j+k)fluoranthene	µg/L	<0.2	<0.2	<0.2	<0.2
Benzo(a)pyrene	µg/L	<0.1	<0.1	<0.1	<0.1
Indeno(1,2,3-c,d)pyrene	µg/L	<0.1	<0.1	<0.1	<0.1
Dibenzo(a,h)anthracene	µg/L	<0.1	<0.1	<0.1	<0.1
Benzo(g,h,i)perylene	µg/L	<0.1	<0.1	<0.1	<0.1
Benzo(a)pyrene TEQ	µg/L	<0.5	<0.5	<0.5	<0.5
Total +ve PAH's	µg/L	<0.1	<0.1	<0.1	<0.1
Surrogate p-Terphenyl-d14	%	112	114	98	99

Organochlorine Pesticides in Water				
Our Reference		326366-1	326366-2	326366-3
Your Reference	UNITS	BH103	BH104	BH105
Date Sampled		20/06/2023	22/06/2023	20/06/2023
Type of sample		Water	Water	Water
Date extracted	-	26/06/2023	26/06/2023	26/06/2023
Date analysed	-	27/06/2023	27/06/2023	27/06/2023
alpha-BHC	µg/L	<0.2	<0.2	<0.2
НСВ	µg/L	<0.2	<0.2	<0.2
beta-BHC	μg/L	<0.2	<0.2	<0.2
gamma-BHC	µg/L	<0.2	<0.2	<0.2
Heptachlor	μg/L	<0.2	<0.2	<0.2
delta-BHC	µg/L	<0.2	<0.2	<0.2
Aldrin	μg/L	<0.2	<0.2	<0.2
Heptachlor Epoxide	µg/L	<0.2	<0.2	<0.2
gamma-Chlordane	μg/L	<0.2	<0.2	<0.2
alpha-Chlordane	μg/L	<0.2	<0.2	<0.2
Endosulfan I	μg/L	<0.2	<0.2	<0.2
pp-DDE	µg/L	<0.2	<0.2	<0.2
Dieldrin	μg/L	<0.2	<0.2	<0.2
Endrin	µg/L	<0.2	<0.2	<0.2
Endosulfan II	μg/L	<0.2	<0.2	<0.2
pp-DDD	µg/L	<0.2	<0.2	<0.2
Endrin Aldehyde	µg/L	<0.2	<0.2	<0.2
pp-DDT	µg/L	<0.2	<0.2	<0.2
Endosulfan Sulphate	µg/L	<0.2	<0.2	<0.2
Methoxychlor	µg/L	<0.2	<0.2	<0.2
Surrogate TCMX	%	106	106	93

OP Pesticides in Water				
Our Reference		326366-1	326366-2	326366-3
Your Reference	UNITS	BH103	BH104	BH105
Date Sampled		20/06/2023	22/06/2023	20/06/2023
Type of sample		Water	Water	Water
Date extracted	-	26/06/2023	26/06/2023	26/06/2023
Date analysed	-	27/06/2023	27/06/2023	27/06/2023
Dichlorvos	µg/L	<0.2	<0.2	<0.2
Dimethoate	µg/L	<0.2	<0.2	<0.2
Diazinon	μg/L	<0.2	<0.2	<0.2
Chlorpyriphos-methyl	µg/L	<0.2	<0.2	<0.2
Ronnel	μg/L	<0.2	<0.2	<0.2
Fenitrothion	µg/L	<0.2	<0.2	<0.2
Malathion	μg/L	<0.2	<0.2	<0.2
Chlorpyriphos	µg/L	<0.2	<0.2	<0.2
Parathion	μg/L	<0.2	<0.2	<0.2
Bromophos ethyl	µg/L	<0.2	<0.2	<0.2
Ethion	µg/L	<0.2	<0.2	<0.2
Azinphos-methyl (Guthion)	µg/L	<0.2	<0.2	<0.2
Surrogate TCMX	%	106	106	93

PCBs in Water				
Our Reference		326366-1	326366-2	326366-3
Your Reference	UNITS	BH103	BH104	BH105
Date Sampled		20/06/2023	22/06/2023	20/06/2023
Type of sample		Water	Water	Water
Date extracted	-	26/06/2023	26/06/2023	26/06/2023
Date analysed	-	27/06/2023	27/06/2023	27/06/2023
Aroclor 1016	µg/L	<2	<2	<2
Aroclor 1221	µg/L	<2	<2	<2
Aroclor 1232	µg/L	<2	<2	<2
Aroclor 1242	µg/L	<2	<2	<2
Aroclor 1248	μg/L	<2	<2	<2
Aroclor 1254	µg/L	<2	<2	<2
Aroclor 1260	µg/L	<2	<2	<2
Surrogate TCMX	%	106	106	93

Total Phenolics in Water				
Our Reference		326366-1	326366-2	326366-3
Your Reference	UNITS	BH103	BH104	BH105
Date Sampled		20/06/2023	22/06/2023	20/06/2023
Type of sample		Water	Water	Water
Date extracted	-	26/06/2023	26/06/2023	26/06/2023
Date analysed	-	26/06/2023	26/06/2023	26/06/2023
Total Phenolics (as Phenol)	mg/L	<0.05	<0.05	<0.05

HM in water - dissolved					
Our Reference		326366-1	326366-2	326366-3	326366-4
Your Reference	UNITS	BH103	BH104	BH105	BD1/20230620
Date Sampled		20/06/2023	22/06/2023	20/06/2023	20/06/2023
Type of sample		Water	Water	Water	Water
Date prepared	-	26/06/2023	26/06/2023	26/06/2023	26/06/2023
Date analysed	-	26/06/2023	26/06/2023	26/06/2023	26/06/2023
Arsenic-Dissolved	µg/L	5	13	31	6
Cadmium-Dissolved	µg/L	<0.1	0.1	1.6	0.1
Chromium-Dissolved	µg/L	<1	<1	<1	<1
Copper-Dissolved	µg/L	<1	1	6	<1
Lead-Dissolved	µg/L	<1	<1	<1	<1
Mercury-Dissolved	µg/L	<0.05	<0.05	<0.05	<0.05
Nickel-Dissolved	µg/L	22	41	73	23
Zinc-Dissolved	µg/L	300	65	460	300

HM in water - total					
Our Reference		326366-1	326366-2	326366-3	326366-4
Your Reference	UNITS	BH103	BH104	BH105	BD1/20230620
Date Sampled		20/06/2023	22/06/2023	20/06/2023	20/06/2023
Type of sample		Water	Water	Water	Water
Date prepared	-	26/06/2023	26/06/2023	26/06/2023	26/06/2023
Date analysed	-	26/06/2023	26/06/2023	26/06/2023	26/06/2023
Arsenic-Total	µg/L	5	16	50	5
Cadmium-Total	µg/L	<0.1	0.3	2.0	<0.1
Chromium-Total	µg/L	<1	4	<1	<1
Copper-Total	µg/L	<1	17	10	<1
Lead-Total	µg/L	2	6	1	3
Mercury-Total	µg/L	<0.05	<0.05	<0.05	<0.05
Nickel-Total	µg/L	21	56	82	22
Zinc-Total	µg/L	300	180	530	320

Miscellaneous Inorganics				
Our Reference		326366-1	326366-2	326366-3
Your Reference	UNITS	BH103	BH104	BH105
Date Sampled		20/06/2023	22/06/2023	20/06/2023
Type of sample		Water	Water	Water
Date prepared	-	23/06/2023	23/06/2023	23/06/2023
Date analysed	-	23/06/2023	23/06/2023	23/06/2023
Total Suspended Solids	mg/L	40	540	50
Total Dissolved Solids (grav)	mg/L	1,200	1,500	1,300
Oil & Grease (LLE)	mg/L		<5	[NA]
Ferrous Iron	mg/L	19	64	33
Ferric Iron (by calculation)	mg/L	<1	<1	<1

PFAS in Waters Short				
Our Reference		326366-1	326366-2	326366-3
Your Reference	UNITS	BH103	BH104	BH105
Date Sampled		20/06/2023	22/06/2023	20/06/2023
Type of sample		Water	Water	Water
Date prepared	-	26/06/2023	26/06/2023	26/06/2023
Date analysed	-	26/06/2023	26/06/2023	26/06/2023
Perfluorohexanesulfonic acid - PFHxS	μg/L	<0.01	<0.01	<0.01
Perfluorooctanesulfonic acid PFOS	µg/L	<0.01	<0.01	<0.01
Perfluorooctanoic acid PFOA	μg/L	<0.01	<0.01	<0.01
6:2 FTS	μg/L	<0.01	<0.01	<0.01
8:2 FTS	μg/L	<0.02	<0.02	<0.02
Surrogate ¹³ C ₈ PFOS	%	100	98	105
Surrogate ¹³ C ₂ PFOA	%	106	104	108
Extracted ISTD ¹⁸ O ₂ PFHxS	%	109	107	106
Extracted ISTD ¹³ C ₄ PFOS	%	115	112	104
Extracted ISTD ¹³ C ₄ PFOA	%	128	118	112
Extracted ISTD ¹³ C ₂ 6:2FTS	%	139	114	108
Extracted ISTD ¹³ C ₂ 8:2FTS	%	100	111	121
Total Positive PFHxS & PFOS	μg/L	<0.01	<0.01	<0.01
Total Positive PFOA & PFOS	μg/L	<0.01	<0.01	<0.01
Total Positive PFAS	µg/L	<0.01	<0.01	<0.01

Method ID	Methodology Summary
Inorg-003	Oil & Grease - determine gravimetrically following extraction with Hexane, in accordance with APHA latest edition, 5520-B.
Inorg-018	Total Dissolved Solids - determined gravimetrically. The solids are dried at 180+/-10°C.
	NOTE: Where the EC of the sample is <100µS/cm, the TDS will typically be below 70mg/L (as the sample is very likely to be at least drinking water quality). Therefore to ensure data quality for TDS, the TDS is typically calculated as per the equation below:-
	TDS = EC * 0.6
Inorg-019	Suspended Solids - determined gravimetricially by filtration of the sample. The samples are dried at 104+/-5°C.
Inorg-031	Total Phenolics by segmented flow analyser (in line distillation with colourimetric finish). Solids are extracted in a caustic media prior to analysis.
Inorg-076	Ferrous Iron is determined colourimetrically by discrete analyser. Waters samples are filtered on receipt prior to analysis.
Metals-021	Determination of Mercury by Cold Vapour AAS.
Metals-022	Determination of various metals by ICP-MS.
	Please note for Bromine and lodine, any forms of these elements that are present are included together in the one result reported for each of these two elements.
Org-020	Soil samples are extracted with Dichloromethane/Acetone and waters with Dichloromethane and analysed by GC-FID. F2 = (>C10-C16)-Naphthalene as per NEPM B1 Guideline on Investigation Levels for Soil and Groundwater (HSLs Tables 1A (3, 4)). Note Naphthalene is determined from the VOC analysis.
Org-021	Soil samples are extracted with dichloromethane/acetone and waters with dichloromethane and analysed by GC-ECD.
Org-022/025	Soil samples are extracted with Dichloromethane/Acetone and waters with Dichloromethane and analysed by GC-MS/GC-MSMS.
Org-022/025	Soil samples are extracted with Dichloromethane/Acetone and waters with Dichloromethane and analysed by GC-MS/GC-MSMS. Benzo(a)pyrene TEQ as per NEPM B1 Guideline on Investigation Levels for Soil and Groundwater - 2013.
Org-023	Water samples are analysed directly by purge and trap GC-MS.
Org-023	Soil samples are extracted with methanol and spiked into water prior to analysing by purge and trap GC-MS. Water samples are analysed directly by purge and trap GC-MS. F1 = (C6-C10)-BTEX as per NEPM B1 Guideline on Investigation Levels for Soil and Groundwater.

Method ID	Methodology Summary
Org-029	Soil samples are extracted with basified Methanol. Waters and soil extracts are directly injected and/or concentrated/extracted using SPE. TCLPs/ASLP leachates are centrifuged, the supernatant is then analysed (including amendment with solvent) - as per the option in AS4439.3.
	Analysis is undertaken with LC-MS/MS.
	PFAS results include the sum of branched and linear isomers where applicable.
	Please note that PFAS results are corrected for Extracted Internal Standards (QSM 5.4 Table B-15 terminology), which are mass labelled analytes added prior to sample preparation to assess matrix effects and verify processing of the sample. PFAS analytes without a commercially available mass labelled analogue are corrected vs a closely eluting mass labelled PFAS compound. Surrogates are also reported, in this context they are mass labelled PFAS compounds added prior to extraction but are used as monitoring compounds only (not used for result correction). Envicarb (or similar) is used discretionally to remove interfering matrix components.
	Please contact the laboratory if estimates of Measurement Uncertainty are required as per WA DER.

QUALITY CONTI	ROL: vTRH((C6-C10)/E	BTEXN in Water			Du	plicate		Spike Re	covery %
Test Description	Units	PQL	Method	Blank	#	Base	Dup.	RPD	LCS-W2	[NT]
Date extracted	-			26/06/2023	1	26/06/2023	26/06/2023		26/06/2023	
Date analysed	-			27/06/2023	1	27/06/2023	27/06/2023		27/06/2023	
TRH C ₆ - C ₉	µg/L	10	Org-023	<10	1	<10	<10	0	109	
TRH C ₆ - C ₁₀	μg/L	10	Org-023	<10	1	<10	<10	0	109	
Benzene	μg/L	1	Org-023	<1	1	<1	<1	0	98	
Toluene	μg/L	1	Org-023	<1	1	<1	<1	0	111	
Ethylbenzene	μg/L	1	Org-023	<1	1	<1	<1	0	109	
m+p-xylene	μg/L	2	Org-023	<2	1	<2	<2	0	113	
o-xylene	μg/L	1	Org-023	<1	1	<1	<1	0	111	
Naphthalene	μg/L	1	Org-023	<1	1	<1	<1	0	[NT]	
Surrogate Dibromofluoromethane	%		Org-023	105	1	112	110	2	103	
Surrogate toluene-d8	%		Org-023	99	1	110	95	15	104	
Surrogate 4-BFB	%		Org-023	104	1	104	104	0	106	

QUALITY CON	QUALITY CONTROL: svTRH (C10-C40) in Water								Spike Recovery %	
Test Description	Units	PQL	Method	Blank	#	Base	Dup.	RPD	LCS-W1	[NT]
Date extracted	-			26/06/2023	1	26/06/2023	26/06/2023		26/06/2023	
Date analysed	-			26/06/2023	1	27/06/2023	27/06/2023		26/06/2023	
TRH C ₁₀ - C ₁₄	µg/L	50	Org-020	<50	1	<50	<50	0	112	
TRH C ₁₅ - C ₂₈	µg/L	100	Org-020	<100	1	<100	<100	0	116	
TRH C ₂₉ - C ₃₆	µg/L	100	Org-020	<100	1	<100	<100	0	86	
TRH >C ₁₀ - C ₁₆	µg/L	50	Org-020	<50	1	<50	<50	0	112	
TRH >C ₁₆ - C ₃₄	µg/L	100	Org-020	<100	1	<100	<100	0	116	
TRH >C ₃₄ - C ₄₀	µg/L	100	Org-020	<100	1	<100	<100	0	86	
Surrogate o-Terphenyl	%		Org-020	77	1	93	85	9	77	

QUALI	TY CONTROI	.: PAHs ir	n Water		Duplicate				Spike Recovery %			
Test Description	Units	PQL	Method	Blank	#	Base	Dup.	RPD	LCS-W3	326366-2		
Date extracted	-			26/06/2023	1	26/06/2023	26/06/2023		26/06/2023	26/06/2023		
Date analysed	-			27/06/2023	1	27/06/2023	27/06/2023		27/06/2023	27/06/2023		
Naphthalene	μg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	87	90		
Acenaphthylene	μg/L	0.1	Org-022/025	<0.1	1	<0.1	<0.1	0	[NT]	[NT]		
Acenaphthene	μg/L	0.1	Org-022/025	<0.1	1	<0.1	<0.1	0	90	93		
Fluorene	μg/L	0.1	Org-022/025	<0.1	1	<0.1	<0.1	0	85	87		
Phenanthrene	μg/L	0.1	Org-022/025	<0.1	1	<0.1	<0.1	0	86	88		
Anthracene	μg/L	0.1	Org-022/025	<0.1	1	<0.1	<0.1	0	[NT]	[NT]		
Fluoranthene	μg/L	0.1	Org-022/025	<0.1	1	<0.1	<0.1	0	91	95		
Pyrene	μg/L	0.1	Org-022/025	<0.1	1	<0.1	<0.1	0	93	97		
Benzo(a)anthracene	μg/L	0.1	Org-022/025	<0.1	1	<0.1	<0.1	0	[NT]	[NT]		
Chrysene	μg/L	0.1	Org-022/025	<0.1	1	<0.1	<0.1	0	94	96		
Benzo(b,j+k)fluoranthene	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	[NT]	[NT]		
Benzo(a)pyrene	µg/L	0.1	Org-022/025	<0.1	1	<0.1	<0.1	0	107	111		
Indeno(1,2,3-c,d)pyrene	μg/L	0.1	Org-022/025	<0.1	1	<0.1	<0.1	0	[NT]	[NT]		
Dibenzo(a,h)anthracene	µg/L	0.1	Org-022/025	<0.1	1	<0.1	<0.1	0	[NT]	[NT]		
Benzo(g,h,i)perylene	µg/L	0.1	Org-022/025	<0.1	1	<0.1	<0.1	0	[NT]	[NT]		
Surrogate p-Terphenyl-d14	%		Org-022/025	99	1	112	102	9	104	107		

QUALITY CONTR	OL: Organoo	hlorine P	esticides in Water			Du		Spike Recovery %		
Test Description	Units	PQL	Method	Blank	#	Base	Dup.	RPD	LCS-W3	326366-2
Date extracted	-			26/06/2023	1	26/06/2023	26/06/2023		26/06/2023	26/06/2023
Date analysed	-			27/06/2023	1	27/06/2023	27/06/2023		27/06/2023	27/06/2023
alpha-BHC	μg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	87	88
НСВ	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	[NT]	[NT]
beta-BHC	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	89	93
gamma-BHC	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	[NT]	[NT]
Heptachlor	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	77	93
delta-BHC	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	[NT]	[NT]
Aldrin	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	90	92
Heptachlor Epoxide	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	91	93
gamma-Chlordane	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	[NT]	[NT]
alpha-Chlordane	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	[NT]	[NT]
Endosulfan I	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	[NT]	[NT]
pp-DDE	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	99	103
Dieldrin	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	102	107
Endrin	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	94	104
Endosulfan II	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	[NT]	[NT]
pp-DDD	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	97	105
Endrin Aldehyde	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	[NT]	[NT]
pp-DDT	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	[NT]	[NT]
Endosulfan Sulphate	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	93	107
Methoxychlor	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	[NT]	[NT]
Surrogate TCMX	%		Org-022/025	85	1	106	95	11	107	101

QUALITY CC	ONTROL: OF	P Pesticid	es in Water			Du		Spike Recovery %		
Test Description	Units	PQL	Method	Blank	#	Base	Dup.	RPD	LCS-W3	326366-2
Date extracted	-			26/06/2023	1	26/06/2023	26/06/2023		26/06/2023	26/06/2023
Date analysed	-			27/06/2023	1	27/06/2023	27/06/2023		27/06/2023	27/06/2023
Dichlorvos	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	111	114
Dimethoate	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	[NT]	[NT]
Diazinon	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	[NT]	[NT]
Chlorpyriphos-methyl	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	[NT]	[NT]
Ronnel	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	93	95
Fenitrothion	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	130	139
Malathion	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	110	130
Chlorpyriphos	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	105	110
Parathion	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	125	128
Bromophos ethyl	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	[NT]	[NT]
Ethion	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	107	132
Azinphos-methyl (Guthion)	µg/L	0.2	Org-022/025	<0.2	1	<0.2	<0.2	0	[NT]	[NT]
Surrogate TCMX	%		Org-022/025	85	1	106	95	11	107	101

QUALITY	Y CONTROL	: PCBs ir	n Water		Duplicate				Spike Recovery %	
Test Description	Units	PQL	Method	Blank	#	Base	Dup.	RPD	LCS-W3	326366-2
Date extracted	-			26/06/2023	1	26/06/2023	26/06/2023		26/06/2023	26/06/2023
Date analysed	-			27/06/2023	1	27/06/2023	27/06/2023		27/06/2023	27/06/2023
Aroclor 1016	μg/L	2	Org-021	<2	1	<2	<2	0	[NT]	[NT]
Aroclor 1221	µg/L	2	Org-021	<2	1	<2	<2	0	[NT]	[NT]
Aroclor 1232	µg/L	2	Org-021	<2	1	<2	<2	0	[NT]	[NT]
Aroclor 1242	µg/L	2	Org-021	<2	1	<2	<2	0	[NT]	[NT]
Aroclor 1248	µg/L	2	Org-021	<2	1	<2	<2	0	[NT]	[NT]
Aroclor 1254	µg/L	2	Org-021	<2	1	<2	<2	0	114	101
Aroclor 1260	µg/L	2	Org-021	<2	1	<2	<2	0	[NT]	[NT]
Surrogate TCMX	%		Org-021	85	1	106	95	11	107	101

QUALITY CO	QUALITY CONTROL: Total Phenolics in Water							Duplicate			
Test Description	Units	PQL	Method	Blank	#	Base	Dup.	RPD	LCS-W1	[NT]	
Date extracted	-			26/06/2023	[NT]		[NT]	[NT]	26/06/2023	[NT]	
Date analysed	-			26/06/2023	[NT]		[NT]	[NT]	26/06/2023	[NT]	
Total Phenolics (as Phenol)	mg/L	0.05	Inorg-031	<0.05	[NT]	[NT]	[NT]	[NT]	102	[NT]	

QUALITY CC	NTROL: HN	1 in water	- dissolved			Du		Spike Recovery %		
Test Description	Units	PQL	Method	Blank	#	Base	Dup.	RPD	LCS-W1	[NT]
Date prepared	-			26/06/2023	1	26/06/2023	26/06/2023		26/06/2023	
Date analysed	-			26/06/2023	1	26/06/2023	26/06/2023		26/06/2023	
Arsenic-Dissolved	µg/L	1	Metals-022	<1	1	5	[NT]		92	
Cadmium-Dissolved	µg/L	0.1	Metals-022	<0.1	1	<0.1	[NT]		94	
Chromium-Dissolved	µg/L	1	Metals-022	<1	1	<1	[NT]		88	
Copper-Dissolved	µg/L	1	Metals-022	<1	1	<1	[NT]		89	
Lead-Dissolved	µg/L	1	Metals-022	<1	1	<1	[NT]		94	
Mercury-Dissolved	µg/L	0.05	Metals-021	<0.05	1	<0.05	<0.05	0	114	
Nickel-Dissolved	µg/L	1	Metals-022	<1	1	22	[NT]		89	
Zinc-Dissolved	µg/L	1	Metals-022	<1	1	300	[NT]		92	

QUALITY	CONTROL:	HM in wa	ter - total			Du		Spike Recovery %		
Test Description	Units	PQL	Method	Blank	#	Base	Dup.	RPD	LCS-W2	326366-2
Date prepared	-			26/06/2023	1	26/06/2023	26/06/2023		26/06/2023	26/06/2023
Date analysed	-			26/06/2023	1	26/06/2023	26/06/2023		26/06/2023	26/06/2023
Arsenic-Total	µg/L	1	Metals-022	<1	1	5	5	0	90	89
Cadmium-Total	µg/L	0.1	Metals-022	<0.1	1	<0.1	<0.1	0	91	96
Chromium-Total	µg/L	1	Metals-022	<1	1	<1	<1	0	88	94
Copper-Total	µg/L	1	Metals-022	<1	1	<1	<1	0	89	92
Lead-Total	µg/L	1	Metals-022	<1	1	2	2	0	89	91
Mercury-Total	µg/L	0.05	Metals-021	<0.05	1	<0.05	<0.05	0	100	78
Nickel-Total	µg/L	1	Metals-022	<1	1	21	22	5	88	91
Zinc-Total	µg/L	1	Metals-022	<1	1	300	320	6	91	#

QUALITY COI	NTROL: Mis	cellaneou	s Inorganics			Duj		Spike Recovery %		
Test Description	Units	PQL	Method	Blank	#	Base	Dup.	RPD	LCS-W1	326366-2
Date prepared	-			23/06/2023	1	23/06/2023	23/06/2023		23/06/2023	23/06/2023
Date analysed	-			23/06/2023	1	23/06/2023	23/06/2023		23/06/2023	23/06/2023
Total Suspended Solids	mg/L	5	Inorg-019	<5	1	40	[NT]		108	[NT]
Total Dissolved Solids (grav)	mg/L	5	Inorg-018	<5	1	1200	[NT]		110	[NT]
Oil & Grease (LLE)	mg/L	5	Inorg-003	<5	[NT]		[NT]	[NT]	99	[NT]
Ferrous Iron	mg/L	0.05	Inorg-076	<0.05	1	19	19	0	101	[NT]
Ferric Iron (by calculation)	mg/L	0.05		<0.05	1	<1	<1	0	[NT]	[NT]

QUALITY C	ONTROL: P	FAS in W	aters Short			Du	plicate		Spike Recovery %		
Test Description	Units	PQL	Method	Blank	#	Base	Dup.	RPD	LCS-W1	326366-2	
Date prepared	-			26/06/2023	1	26/06/2023	26/06/2023		26/06/2023	26/06/2023	
Date analysed	-			26/06/2023	1	26/06/2023	26/06/2023		26/06/2023	26/06/2023	
Perfluorohexanesulfonic acid - PFHxS	µg/L	0.01	Org-029	<0.01	1	<0.01	<0.01	0	105	101	
Perfluorooctanesulfonic acid PFOS	µg/L	0.01	Org-029	<0.01	1	<0.01	<0.01	0	103	99	
Perfluorooctanoic acid PFOA	µg/L	0.01	Org-029	<0.01	1	<0.01	<0.01	0	106	102	
6:2 FTS	µg/L	0.01	Org-029	<0.01	1	<0.01	<0.01	0	105	97	
8:2 FTS	μg/L	0.02	Org-029	<0.02	1	<0.02	<0.02	0	97	100	
Surrogate ¹³ C ₈ PFOS	%		Org-029	102	1	100	96	4	102	98	
Surrogate ¹³ C ₂ PFOA	%		Org-029	103	1	106	108	2	106	105	
Extracted ISTD ¹⁸ O ₂ PFHxS	%		Org-029	107	1	109	105	4	103	109	
Extracted ISTD ¹³ C ₄ PFOS	%		Org-029	109	1	115	116	1	108	116	
Extracted ISTD ¹³ C ₄ PFOA	%		Org-029	117	1	128	128	0	112	118	
Extracted ISTD ¹³ C ₂ 6:2FTS	%		Org-029	124	1	139	145	4	113	113	
Extracted ISTD ¹³ C ₂ 8:2FTS	%		Org-029	82	1	100	117	16	100	116	

Result Definiti	ons
NT	Not tested
NA	Test not required
INS	Insufficient sample for this test
PQL	Practical Quantitation Limit
<	Less than
>	Greater than
RPD	Relative Percent Difference
LCS	Laboratory Control Sample
NS	Not specified
NEPM	National Environmental Protection Measure
NR	Not Reported

Quality Contro	ol Definitions
Blank	This is the component of the analytical signal which is not derived from the sample but from reagents, glassware etc, can be determined by processing solvents and reagents in exactly the same manner as for samples.
Duplicate	This is the complete duplicate analysis of a sample from the process batch. If possible, the sample selected should be one where the analyte concentration is easily measurable.
Matrix Spike	A portion of the sample is spiked with a known concentration of target analyte. The purpose of the matrix spike is to monitor the performance of the analytical method used and to determine whether matrix interferences exist.
LCS (Laboratory Control Sample)	This comprises either a standard reference material or a control matrix (such as a blank sand or water) fortified with analytes representative of the analyte class. It is simply a check sample.
Surrogate Spike	Surrogates are known additions to each sample, blank, matrix spike and LCS in a batch, of compounds which are similar to the analyte of interest, however are not expected to be found in real samples.

Australian Drinking Water Guidelines recommend that Thermotolerant Coliform, Faecal Enterococci, & E.Coli levels are less than 1cfu/100mL. The recommended maximums are taken from "Australian Drinking Water Guidelines", published by NHMRC & ARMC 2011.

The recommended maximums for analytes in urine are taken from "2018 TLVs and BEIs", as published by ACGIH (where available). Limit provided for Nickel is a precautionary guideline as per Position Paper prepared by AIOH Exposure Standards Committee, 2016.

Guideline limits for Rinse Water Quality reported as per analytical requirements and specifications of AS 4187, Amdt 2 2019, Table 7.2

Laboratory Acceptance Criteria

Duplicate sample and matrix spike recoveries may not be reported on smaller jobs, however, were analysed at a frequency to meet or exceed NEPM requirements. All samples are tested in batches of 20. The duplicate sample RPD and matrix spike recoveries for the batch were within the laboratory acceptance criteria.

Filters, swabs, wipes, tubes and badges will not have duplicate data as the whole sample is generally extracted during sample extraction.

Spikes for Physical and Aggregate Tests are not applicable.

For VOCs in water samples, three vials are required for duplicate or spike analysis.

Duplicates: >10xPQL - RPD acceptance criteria will vary depending on the analytes and the analytical techniques but is typically in the range 20%-50% – see ELN-P05 QA/QC tables for details; <10xPQL - RPD are higher as the results approach PQL and the estimated measurement uncertainty will statistically increase.

Matrix Spikes, LCS and Surrogate recoveries: Generally 70-130% for inorganics/metals (not SPOCAS); 60-140% for organics/SPOCAS (+/-50% surrogates) and 10-140% for labile SVOCs (including labile surrogates), ultra trace organics and speciated phenols is acceptable.

In circumstances where no duplicate and/or sample spike has been reported at 1 in 10 and/or 1 in 20 samples respectively, the sample volume submitted was insufficient in order to satisfy laboratory QA/QC protocols.

When samples are received where certain analytes are outside of recommended technical holding times (THTs), the analysis has proceeded. Where analytes are on the verge of breaching THTs, every effort will be made to analyse within the THT or as soon as practicable.

Where sampling dates are not provided, Envirolab are not in a position to comment on the validity of the analysis where recommended technical holding times may have been breached.

Where matrix spike recoveries fall below the lower limit of the acceptance criteria (e.g. for non-labile or standard Organics <60%), positive result(s) in the parent sample will subsequently have a higher than typical estimated uncertainty (MU estimates supplied on request) and in these circumstances the sample result is likely biased significantly low.

Measurement Uncertainty estimates are available for most tests upon request.

Analysis of aqueous samples typically involves the extraction/digestion and/or analysis of the liquid phase only (i.e. NOT any settled sediment phase but inclusive of suspended particles if present), unless stipulated on the Envirolab COC and/or by correspondence. Notable exceptions include certain Physical Tests (pH/EC/BOD/COD/Apparent Colour etc.), Solids testing, total recoverable metals and PFAS where solids are included by default.

Samples for Microbiological analysis (not Amoeba forms) received outside of the 2-8°C temperature range do not meet the ideal cooling conditions as stated in AS2031-2012.

Report Comments

8 HM in water - total - # Percent recovery is not applicable due to the high concentration of the element/s in the sample/s. However an acceptable recovery was obtained for the LCS.

MISC_INORG Ferric Iron (by calculation): PQLs for samples have been raised due to sample matrix interference.



Table J3 : Summary of Groundwater Laboratory Results

					METALS (DISSOLVED)					METALS (TOTAL)								т	RH				BT	TEX							
		Arsenic	Cadmium	Total Chromium	Copper	Lead	Mercury (Inorganic)	Nickel	Zinc	Arsenic	Cadmium	Total Chromium	Copper	Lead	Mercury (inorganic)	Nickel	Zinc	F1 ((C6-C10)-BTEX)	F2 (>C10-C16 less Naphthalene)	F3 (>C16-C34)	F4 (>C34-C40)	Benzene	Toluene	Ethylbenzene	o-Xylene	m+p-Xylene	Total Xylenes	Acenaphthene	Acenaphthylene	Anthracono	Benzo(a) anthracen e	Naphthalene
	PQL	1	0.1	1	1	1	0.05	1	1	1	0.1	1	1	1	0.05	1	1	10	50	100	100	1	1	1	1	2	1	0.1	0.1	0.1	0.1	0.2
NZG (2018) 95% LOP Fresh		24	0.2	1	1.4	3.4	0.06	11	8	24	0.2	1	1.4	3.4	0.06	11	8					950	180	80	350	75				0.01		16
EPA (2018) 99% LOP Fresh																																
IEPC (2013) HSL 4-8m																		1000	1000			800					NL					NL
Sample ID	Sample Date	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L
BH103	20/06/23	5	<0.1	<1	<1	<1	<0.05	22	300	5	<0.1	<1	<1	2	<0.05	21	300	<10	<50	<100	<100	<1	<1	<1	<1	<2	<1	<0.1	<0.1	<0.1	<0.1	<0.2
BD1/20230620	20/06/23	6	0.1	<1	<1	<1	<0.05	23	300	5	<0.1	<1	<1	3	<0.05	22	320	<10	<50	<100	<100	<1	<1	<1	<1	<2	<1	<0.1	<0.1	<0.1	<0.1	<0.2
BH104	22/06/23	13	0.1	<1	1	<1	<0.05	41	65	16	0.3	4	17	6	<0.05	56	180	<10	<50	<100	<100	<1	<1	<1	<1	<2	<1	<0.1	<0.1	<0.1	<0.1	<0.2
BH105	20/06/23	31	1.6	<1	6	<1	< 0.05	73	460	50	2	<1	10	1	<0.05	82	530	<10	<50	<100	<100	<1	<1	<1	<1	<2	<1	<0.1	<0.1	<0.1	<0.1	<0.2

Notes:

QA/QC replicate of sample listed directly below the primary sample

• PQL

QACC replicate of sample listed directly below the primary sample
Practical quantitation limit
No criterion innt defined / not tested / not applicable
Shaded cell is exceedance of guideline value
Where one or more guideline value is exceeded, the cell is shaded to the colour of the highest guideline value exceeded
ANCS (2018) Australian on Mex Zaland Guidelines for Fresh and Marine Water Quality, orange text is 'unknown' level of protection
NHMRC (2018) Australian Drinking Water Guidelines 6 2011, drinking water assthetic-based oriteria
HEPA PFAS National Environmental Management Plan (NEMP) (HEPA, 2020)



Table J3 : Summary of Groundwater Laboratory Results

		РАН												OCP																							
		Benzo(a)pyrene (BaP)	Berzo(b,j+k)f luora nthere	Benzo(g,h,i)perylen e	Chrysene	Dibenzo(a,h)anthra cene	Fluoranthene	Fluorene	Indeno(1,2,3- c,d)pyrene	Phenanthrene	Pyrene	Aldrin	alpha-BHC	alpha-chlordane	beta-BHC	DDE	DO	delta-BHC	Dieldrin	Endosulfan I	Endosulfan II	Endosulfan Sulphate	Endrin	gamma-Chlordane	Heptachlor	Heptachlor Epoxide	He xa chlor obenze n e	Lindane	Methoxychlor	QQQ	ORGANOCHLORIN E PESTICIDES	Aldrin + Dieldrin (calculated)	Azinphos methyl (Guthion)	Bromophos-ethy!	C hlorpy riphos	Chlorpyriphos- methyl	Diazinon
	PQL	0.1	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2
ANZG (2018) 95% LOP Fresh		0.1					1			0.6		0.001					0.006		0.01				0.01		0.01				0.005	0.006					0.01		0.01
HEPA (2018) 99% LOP Fresh																				1824	31																
NEPC (2013) HSL 4-8m																																					
Sample ID	Sample Date	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	μg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L
BH103	20/06/23	<0.1	<0.2	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2
BD1/20230620	20/06/23	<0.1	<0.2	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	-	-	-				-	-		-			-	-		-		-	-	-	-	-	-	-	-	-
BH104	22/06/23	<0.1	<0.2	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2
BH105	20/06/23	<0.1	<0.2	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2



Table J3 : Summary of Groundwater Laboratory Results

		OPP								PCB										PF	AS			Inoganics				
	Dichlorvos	Dimethoate	Ethion	Ronnel (fenchlorphos)	Fenitrothion	Malathion	Parathion	ORGANOPHOSPH ORUS PESTICIDES	Arochlor 1016	Arochlor 1221	Arochlor 1232	Arochlor 1242	Arochlor 1248	Arochlor 1254	Aroclor 1260	POLYCHLORINATE D BIPHENYLS	VOLATILE ORGANIC COMPOUNDS	PFOS	PFOA	PFHXS	Sum of PFHxS and PFOS	8:2 FTS	PFAS	Total Suspended Solids (TSS)	Total Dissolved Solids (TDS)	Oll & Grease	Ferrous Iron	Ferric fron
PQL	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	2	2	2	2	2	2	2	2	1	0.01	0.01	0.01	0.01	0.02	0.01	0.01	0.01	0.01	0.01	0.02
ANZG (2018) 95% LOP Fresh		0.15			0.2	0.05	0.04					0.3		0.01				0.00023	19									
HEPA (2018) 99% LOP Fresh																												\square
NEPC (2013) HSL 4-8m																												
Sample ID Sample D	ate µg/L	µg/L	µg/L	μg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	μg/L	µg/L	µg/L	μg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	μg/L	µg/L	µg/L	µg/L	µg/L
BH103 20/06/2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<2	<2	<2	<2	<2	<2	<2	<2	<1	<0.01	<0.01	<0.01	<0.01	<0.02	<0.01	40000	1200000		19000	<1000
BD1/20230620 20/06/2	-	-	-	-			-	-	-	-	-	-		-	-		<1			-	-	-	-	-	-			· · ·
BH104 22/06/2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<2	<2	<2	<2	<2	<2	<2	<2	<1	<0.01	<0.01	<0.01	<0.01	<0.02	<0.01	540000	1500000	<5000	64000	<1000
BH105 20/06/2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<2	<2	<2	<2	<2	<2	<2	<2	<1	<0.01	<0.01	<0.01	<0.01	<0.02	<0.01	50000	1300000	,	33000	<1000