

# Structural Report External Development Adjacent Metro Corridor

For Proposed Development:

At Fiveways,
Cnr Falcon St, Pacific Highway and
Alexander St, Crows Nest

Prepared For:

Deicorp Pty Ltd Level 3, 161 Redfern Street REDFERN NSW 2016

Report Number: 23012-Structural Metro Report

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#### **Document Control**

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#### 1. Introduction

ABC Consultants has been engaged by Deicorp Pty Ltd to complete the structural engineering design for the proposed residential and commercial development at Fiveways, located at the corner of Falcon Street, Pacific Highway and Alexander Street in Crows Nest.

The purpose of this report is to provide an assessment of the impact of the proposed structure on the proposed Sydney Metro infrastructure and demonstrate compliance with structural design requirements outlined in TfNSW Technical Guidelines – NWRLSRT-PBA-SRT-TU-REP-000008 – Sydney Metro Underground Corridor Protection – Revision 1.





## 2. Project Description

The proposed development site is located at Fiveways, Crows Nest. The site is bound by Falcon St to the North West, Alexander St to the North East and Pacific Highway to the South.

The metro infrastructure adjacent to the development consists of a Metro tunnel that runs partially under the site on its Northern end with their location and depths having been confirmed by site surveys works undertaken by Stantec.

The total site area is approximately 3,280 m2. The site is currently occupied by a number of commercial brick/timber framed buildings with a maximum of 1 level of existing below ground basements. Refer to the existing site survey for survey details.

The proposed development is a mixed retail and residential development consisting of a single residential building above a retail/open space podium with associated basement parking. The residential tower is proposed to extend up to 21 stories in height with the proposed basement extending five levels below ground. Refer to architectural plans prepared by Turner architects for full development details.

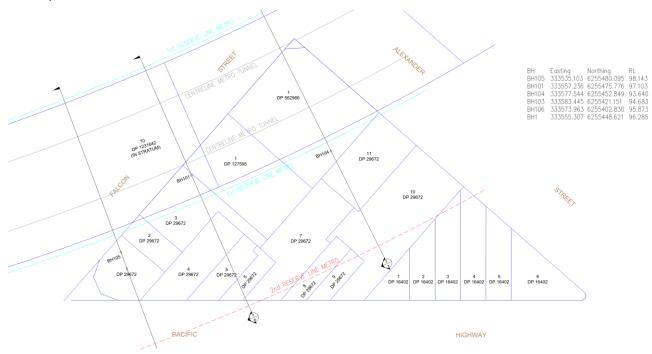


Figure 1 - Locality Map



#### 3. Sydney Metro

The Sydney Metro is a rail infrastructure project which was completed in mid-2019. The project consists of twin metro tunnels serving stations from Tallawong through to Chatswood and extending through the Sydney CBD.

#### 3.1. Protection Reserves

Protection reserves define the extent of zones that have been established to protect existing metro infrastructure and protect the feasibility of planned metro infrastructure from future adjacent developments.

The technical guideline defines two reserves for the protection of the Sydney Metro tunnels and station boxes. A first reserve is defined for a distance nearer to the tunnel where all works are heavily restricted and stringently reviewed. A second reserve is defined beyond the first reserve where any proposed works are still required to be assessed however less may proceed provided they meet the requirements set out by TfNSW. Table 4.5 of the technical guidelines provides a list of construction restrictions that apply to each reserve.

For the metro tunnels the reserves are defined as follows:

- First reserve extends from the tunnel edge inscribed with a square to a distance the greater of 5m or the extent of the Sydney Metro Substratum.
- Second reserve extends to a greater of 25m or the width of the tunnel from the first reserve.

For the metro station boxes the reserves are defined similarly as follows:

- First reserve extends up to the Sydney Metro Substratum or property boundary.
- Second reserve extends from the first reserve up to 25m.

The first reserve has been identified by the project survey and included in the structural drawings as can be seen in extracts below.

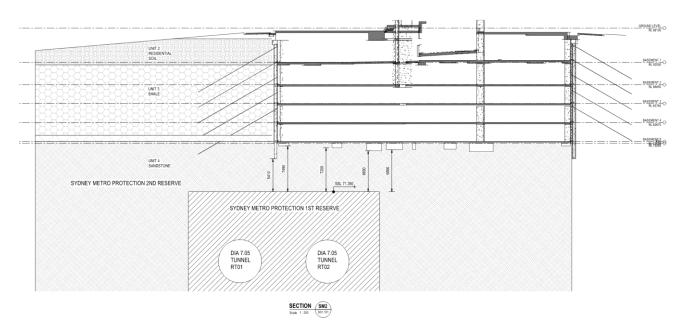


Figure 2 - Extract from structural plan S01.102 showing Metro tunnels beneath the site



#### 3.2. Infrastructure location

The proposed development is located above the two Metro tunnels and as such the location of the infrastructure and protection reserves are based on the property boundary of the tunnel and train lines as defined in the survey.

Based on the survey drawings the distance between the Sydney Metro infrastructure and development site property boundaries ranges.

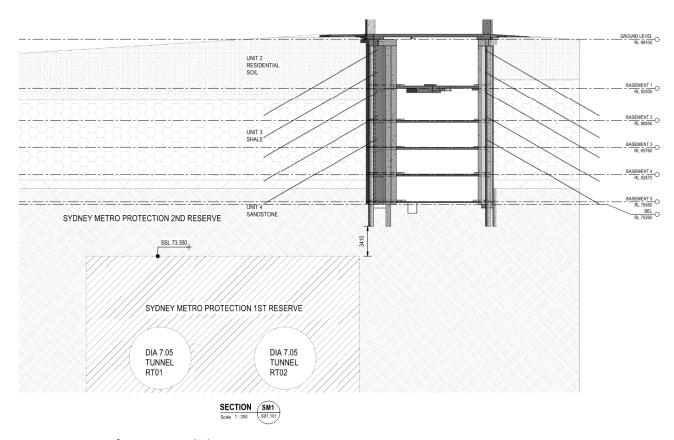


Figure 2 - Extract from structural plan S01.102

Given the second reserve is defined as extending 25m past the metro property boundary it can be seen that the development site exists inside the second reserve but completely outside the first reserve.



## 4. Geotechnical Investigation

A geotechnical engineering report has been completed for the subject project by Douglas Partners, Report No. 86645.03 dated March 2025. The report details a geotechnical investigation of the site which includes existing site condition, soil stratigraphy, ground water measurements and recommendations for foundation design and basement retention.

Below is a summary of the geotechnical report with relevance to the structural engineering design.

#### 4.1. Stratigraphy

The sub-surface material below the existing basement is described in the geotechnical engineering report generally consists of fill, residual soil, Class V/IV sandstone and Class I/II sandstone.

Table 5: Summary of Geotechnical Model

Geotechnical Unit	Description	Detailed Description		
Unit A Fill / Residual Soils  Unit B Class IV and III Shale and Laminite		Fill comprising sandy gravel, sandy and clayey soils / Residual, low to high plasticity, stiff to hard clay soils and dense sands.		
		Shale and laminite bedrock of very low and low strength with some medium strength bands. Mainly highly weathered then fresh, with extremely weathered bands, highly fractured to slightly fractured.		
Unit C	Class IV and III Sandstone and Siltstone	Sandstone and siltstone bedrock of generally very low and low strength with medium strength bands, mainly fresh, fractured to slightly fractured.		
Unit D	Class II Sandstone	Sandstone of medium to high and high strength. Mainly fresh, slightly fractured to unbroken.		

Notes: Rock Class in accordance with Bertuzzi & Pells (2002) Application of Classification To A General Rock Profile

Six boreholes were completed for the site. The depth to each sub-surface material at each borehole is shown in Table 4 below.

Table 4: Results of UCS and Deformation Testing

	Uniaxial		Tan	gent	Secant		
Bore	Depth (m)	Compressive Strength (MPa)	Elastic Modulus (GPa)	Poisson's Ratio	Elastic Modulus (GPa)	Poisson's Ratio	
BH102	17.0-17.3	12.7	2.9	0.22	2.6	0.12	
BH103	19.1–19.3	29.5	6.4	0.39*	5.1	0.21	
BH104	16.2-16.5	29.6	6.3	0.40*	4.6	0.24	
BH105	12.5-12.8	10.8	1.6	0.12	1.2	0.07	
BH105	16.0-16.3	18.1	1.1	0.42*	2.3	0.31*	
BH106	21.6-21.9	20.5	4.4	0.31*	3.7	0.25	

<sup>\*</sup> Poisson's ratio values should not be relied upon.

Table 1 - Approximate Depth to Sub-surface Material (m).



The geotechnical design parameters, including the earth pressure coefficients, cohesion, friction angle and unit weight adopted in the shoring wall design are shown below.

Table 7: Recommended Design Parameters for Shoring Systems

Material	Unit Weight	Earth Pressure Coefficient		
Material	(kN/m³)	Active (K <sub>a</sub> )	At Rest (K <sub>o</sub> )	
Filling, and residual sand	20	0.30 (0.40)	(0.50)	
Very low to low strength Shale / laminate / siltstone	22	0.25 (0.30)	(0.40)	
Low to medium strength sandstone / siltstone	22	0.20 (0.25)	(0.35)	
Medium strength or stronger sandstone	24	0	0	

Table 2 – Geotechnical design parameters for site materials.

The geotechnical design parameters adopted in the foundation design are shown below.

Table 9: Recommended Design Parameters for Foundation Design

Foundation Stratum	Ultimate End Bearing Pressure (kPa)	Allowable End Bearing Pressure (kPa)	Field Elastic Modulus* (MPa)	Allowable Defects	Testing Requirements
Medium strength sandstone (Class III)	20,000	3,500	350 - 1200	< 5%	Minimum 4 cored bores with spoon testing in at least 1/3 of footings.
Medium to high strength sandstone (Class II)	60,000	6,000	900 - 2000	< 3% No seams >10mm in first 250mm or >20mm in first 500mm	Cored bores at max 10 m grid spacing or cored bores for 50% of footings, and spoon testing remainder.

#### Notes:

- Values for sandstone are in accordance with Pells et al AGS Dec 1998.
- Bearing pressure values assume a minimum embedment of one footing width into the relevant bearing stratum.
- Ultimate parameters are mobilized at large settlements (i.e., >5% foundation width).
- Additional analysis is required to calculate the modulus of subgrade reaction for individual footings.
- Allowable end bearing pressures to cause settlement of less than 1% of minimum footing dimension.

#### 4.2. Ground Water

Geotechnical report has identified ground water at depths of 5m below current BEL which is above the future BEL during or immediately after boring the holes, based on the initial investigation. No long-term monitoring of water table levels has occurred and geotechnical engineer is of the opinion that a further borehole with piezometer added would confirm that only small volumes of seepage is present.



Due to the low permeability of the rock, the geotechnical engineer advises that ground water inflows should not have an adverse impact on the proposed development or neighbouring sites. The geotechnical engineer recommends that the drainage should be provided behind the shoring wall and below the basement floor slab to capture any seepage water.

It is recommended that adequate drainage is provided behind the proposed shoring walls to collect and drain any inflow water.

#### 4.3. Excavation Support

The five-level basement excavation proposed for the site is not feasible to excavate using a batter slope. To ensure the stability of existing structures and infrastructure during construction the geotechnical engineer recommends an anchored soldier pile wall to support the fill, residual soil, shale and Class IV/III sandstone.

The Class II sandstone is considered suitable to be able to be vertically cut without support with some stabilisation measures such as rock bolts and shotcrete or dental treatment to be provided to local defects. The excavation of the unsupported rock must be completed in the presence of a geotechnical engineer however the piles have been taken to below BEL so this situation is not present for this site.

For all the boundaries, it is proposed to use a concrete soldier pile wall supported with temporary ground anchors that will be destressed once the final basement and ground floor slabs are constructed which will provide the permanent support to the shoring wall system. The concrete soldier piles are 600mm in diameter at typically 2.4m cts with a shotcrete wall between the piles and temporary ground anchors.

#### 4.4. Foundation Design

The expected material to be encountered at the site following bulk excavation is expected to be Class II sandstone. In order to limit the potential for differential settlement, the footings will be founded in a uniform material.

Basement strip and pad footings will be proportioned to suit a maximum allowable bearing capacity of 6,000 kPa for the bedrock.



## 5. Structural Design

The building structure of the proposed development is a typical concrete framed building consisting of concrete footings, walls, columns and slabs. A copy of the structural engineering documentation for the shoring wall is provided in Appendix A.

The structural engineering design for the shoring wall has been completed in accordance with the following Australian Standards:

- AS1170.0:2002 Structural Design Actions: General Design Principals
- AS1170.1:2002 Structural Design Actions: Permanent Imposed and Other Actions
- AS1170.2:2021 Structural Design Actions: Wind Actions
- AS1170.4:2007 Structural Design Actions: Earthquake Actions in Australia
- AS2159:2009 Piling Design and Installation
- AS3600:2018 Concrete Structures
- AS4100:2020 Steel Structures
- AS4678:2002 Earth Retaining Structures

#### 5.1. Shoring Wall

The proposed development includes five levels of basement excavation with a proposed bulk earth level of 79.26. Detailed excavations for footings, pits and services will be below this level.

The shoring wall on the boundaries is generally designed as a concrete pile spaced at typically 2.4m centres with an infill shotcrete wall and restrained with at least four rows of rock anchors with the base of the pile typically founded 2.5m below BEL into the Class II/I sandstone.

#### **5.1.1.** Loading

The shoring wall along the boundary is designed to withstand the dead load applied by the site soil conditions as well as live load surcharges as shown on the structural engineering documentation.

The design live load surcharge is as nominated below;

- General construction zone 20kPa
- Road Traffic zone 20 kPa

Nil surcharge is imposed on the shoring wall from the Sydney Metro tunnels as these tunnels are founded in the Class I/II sandstone below the depth of the proposed basement.



#### 5.1.2. Basement Excavation Sequence

The proposed basement excavation will proceed in the following sequence:

- 1. Setout the location of the piles and capping beams as noted on plans, elevation and sections.
- Hold point the geotechnical engineer (who shall be employed by the builder) is required to
  certify that the soil conditions comply with the design assumptions detailed in the geotechnical
  investigation report. The geotechnical engineer is to determine the level of supervision required
  to be able to provide this certificate. Supervision of the material removed as piles are drilled may
  be required.
- 3. Drill required bore holes to the diameter specified and depth shown on plans, elevations and sections. Ensure the socket is fully cleaned and all loose material is removed.
- 4. <u>Hold point</u> the structural engineer is to witness the reinforcement cages prior to placement in the bored piles. Placement of the cages within the piles for piles greater than 6m deep is to be witnessed on site
- 5. Place reinforcement cages in holes ensuring that cages are orientated so drilling through soldier piles for anchors / rock bolts will clear any vertical reinforcement in piles. End caps are to be placed at the base of the reinforcement cage and roller chairs placed at 2m intervals along the length of the pile (a minimum of 3 per section) to ensure minimum cover to the cage is maintained.
- 6. Using a tremie pipe or similar from the base of the bored hole to ensure no separation of concrete aggregate, place concrete from the base of the pile to underside of capping beam. Vibrate concrete progressively from the base of the pile as the pile is filled.
- 7. Install capping beam reinforcement in accordance with details on these drawings.
- 8. Hold point the structural engineer is to witness the reinforcement of the capping beam.
- 9. Place capping beam concrete and allow to cure for a minimum of 7 days.
- 10. <u>Hold point</u> project surveyor is to establish a datum of the capping beam location prior to any excavation past the capping beam. Refer to monitoring notes. Monitoring of the wall is to continue on a regular basis as detailed in the monitoring notes.
- 11. Excavate against the piles to maximum 500mm below the top level of rock anchors / bolts or to a maximum of 2.0m whichever is the lesser.
- 12. Drill and epoxy shotcrete dowels into shoring piles as nominated on drawings. Place reinforcement to the shotcrete wall.
- 13. <u>Hold point</u> the structural engineer is to witness the reinforcement of the shotcrete panels and ensure minimum depth is achieved to the panel.
- 14. Place concrete to shotcrete wall. Shotcrete panels are to be formed and poured or sprayed. If shotcrete walls are sprayed, the panels are to be over sprayed and then screeded back to the design thickness. Shotcrete is to be self-compacting in accordance with AS3600
- 15. If the excavation is at the level of the shoring anchor; scan pile for reinforcement prior to coring anchor hole, a maximum horizontal deviation of 5° to clear any reinforcement is permitted, otherwise contact the structural engineer for further advice. Drill anchor bore holes, install rock anchors / bolts with associated centralisers and grout tubes, place grout within the bore hole. (refer Rock Anchors Post Tensioned Strand notes).
- 16. <u>Hold point</u> the geotechnical engineer is to witness the wedge lift off and anchor lift off tests as required
- 17. Once the grout has achieved design strength and after a minimum 3 days, the rock anchors / bolts may be stressed.
- 18. Provided the shotcrete panels have reached 25mpa strength and the shoring anchors are fully stressed excavation may continue to the next stage. Repeat steps 10 to 17 until the final anchor is installed at the toe of the pile and then excavation continues to the nominated level.



19. Minimum 3 months after ground floor / level 1 slab has been cast, rebates at each slab / pile interface shall be cleaned out and grouted up with an approved non-shrink grout (monolith or equal). When f'c grout is at least 40 MPa. Typical anchors / rock bolts shall be destressed, anchor heads removed and piles made good.

#### 5.1.3. Displacement

A major issue associated with deep excavation is the lateral displacement of the soil mass behind the shoring wall due to the shoring wall deflection. The shoring wall has been designed to limit soil movements around the proposed excavation and provide the temporary and long-term support to enable the excavation of the proposed basement.

The geotechnical engineer has undertaken FEM analysis to investigate the stress relief in the rock during the excavation works and hence the predicted movement of the rock around the Sydney Metro tunnel lines. Please refer to their report for more details on their assumptions, modelling and predicted results, Ref Douglas Partners Report "Report on Numerical Analysis – Sydney Metro", Report No: 86645.03 dated 13 May 2025.



#### 5.1.4. Monitoring

To ensure the maximum design displacement of the shoring wall discussed above is not exceeded, the shoring wall will be monitored by means of survey points installed along the wall at regular intervals prior to excavation.

A registered surveyor will monitor the points throughout excavation and construction for any lateral movement. A project specific monitoring report has been undertaken by the project geotechnical engineers Douglas Partners, refer "Sydney Metro Preliminary Tunnel Geotechnical Monitoring Plan, Fiveways Project", Report No: 86645.03 R.003.Rev 0 dated 1st September 2023

#### 5.2. Foundations

The building foundations consist of a combination of strip and pad footings to support the concrete walls and columns above founded below the bulk earth levels at RL 79.26.

Based on the bulk earth levels above and allowing for a pad footing depth ranging depth of 800mm to 1400mm; the building footings will be founded at a level of RL78.46 – 77.86.

The footings will be uniformly founded on strong rock material with an Allowable Bearing pressure of 6,000 kPa as described in the geotechnical engineer's report and will be constructed using min 40 MPa concrete and 50mm cover.

#### 5.3. Lateral Design

As part of the permanent design of the development, lateral loads due to wind and earthquake will be imposed on the structure throughout its lifetime.

In order to withstand these applied loads, the buildings will utilise concrete core walls to transfer the loads through the structure and down to foundation level. The bearing pressure at the foundation level will not exceed the design Allowable Bearing pressure of 6,000kPa.



## 6. Compliance with TfNSW Sydney Metro Technical Guidelines

The following sections aims to demonstrate compliance with TfNSW Sydney Metro Underground Corridor Protection Technical Guidelines NWRLSRT-PBA-SRT-TU-REP-000008 which outlines the specific design requirements for external developments near the Sydney Metro tunnel.

In accordance with the standard, the structural engineering design has been completed in accordance with relevant Australian Standards. Refer to the Section 5 of this report for a full list of standards which have been referenced in the design.

#### 6.1. Construction Restrictions Within Tunnel Reserves

Table 4.5 of Section 4.4 of the technical guidelines outline specific construction restrictions within the first and second reserves. The table below summaries compliance with these restrictions.

Type of construction	Designer comment
Excavation for basements and footings	No excavations are proposed within the first protection reserves.
Shallow footings or pile foundations	No footings or piles are proposed within the first protection reserve.
Tunnels and underground	No tunnels or underground excavations are proposed within the first reserve.
excavations	Bore holes are proposed within the second reserve to allow installation of temporary ground anchors to restrain the proposed shoring piles.
	Refer to structural elevations and sections for full details on the extent of the proposed anchors.
Demolition of	No demolition of existing structures is proposed within the first reserve.
existing sub-surface structures	Demolition of existing sub-surface structures within the second reserve are presented in the referenced documentation for approval.
Penetrative subsurface investigations	No additional sub-surface investigations are proposed.



#### 6.2. Imposed Loading

Section 9.1.1 of the technical guideline "Any temporary or permanent works adjacent to the metro could be subject to the influence of train loading and as such will need to be assessed in accordance with AS5100 for live load surcharge".

The level of the Sydney Metro tunnel is below the lowest level of the proposed excavation within the immediate vicinity of the site. As such, no loads are imposed from the Sydney Metro infrastructure on to the development site and no additional surcharge loading needs to be considered.

#### 6.3. Induced Movement

Section 9.1.2 of the technical guideline "Displacement of metro infrastructure as induced by the development must not affect the operational functionality and durability of the affected infrastructure. The developer must consider the possibility that future metro construction may induce movement on the development."

In both the temporary and permanent case, please refer to the geotechnical modelling report undertaken by Douglas Partners for a more detailed and in-depth analysis of the movements.

In the long term, the shoring wall will be restrained by the basement slabs with lateral pressure acting on the back face of the pile towards the inner face of the basement.

"Any development activity, whether beneath or adjacent to contained metro tracks, that has the potential to cause track displacement must comply with the requirements of SPC 207 Track Monitoring Requirements for Undertrack Excavation"

In accordance with the requirements of the technical guideline the track is to be monitored in accordance with the requirements of SPC 207 Track Monitoring Requirements for Undertrack Excavation.

The project geotechnical engineer Douglas Partners and the tunnel engineer Delve Underground have both undertaken finite element analysis using Plaxis to assess the movement of the adjoining tunnels and train lines as a result of the proposed excavation and reference should be made to their reports for further details.

#### 6.4. Induced Cracking

Section 9.1.3 outlines technical criteria regarding the monitoring and treatment of existing and new cracks to the tunnel lining.

A detailed assessment of the impact on the existing Metro tunnel structure has been undertaken by Delve which confirms the impact of the proposed development on the existing Metro tunnel satisfies the requirements of "Sydney Metro Underground Corridor Protection Technical Guidelines". Please refer to their report for more details, Ref: 6466-DLV-MEM-001 "Fiveways Crows Nest — Structural Impact Assessment".



#### 6.5. Temporary Components

Section 9.2 requires "Sections of temporary shoring installed to support excavations for the development must have a minimum service life of 3 years..."

Compliance with the above clause has been achieved by the proposed shoring wall. The concrete components of the wall have all been designed for the permanent structure case and as such have a minimum design life of 50 years.

Shoring anchors which will be de-commissioned following completion of the final structure and are designed for a minimum life of 3 years.

#### 6.6. Noise and vibration

Section 9.3 of T HR CI 12080 ST "The effects of noise and vibration from rail operations shall be considered in the design of the development. The noise from construction and rail operation shall be considered against statutory and project noise vibration limit requirements."

Refer to the geotechnical and acoustic engineers report for details regarding excavation and vibration considerations.

#### 6.7. Stray currents and electrolysis from rail operations

An independent stray current electrolysis report has been completed by Corrosion Control Engineering dated 20<sup>th</sup> March 2025.

The report recommends the following details be incorporated into the structural design:

#### 6 Recommendations

CCE recommends the following conservative protective measures, where possible/practical, to mitigate against long-term stray current corrosion at on-ground and in-ground metallic structures:

- The installation of heavy plastic membrane (e.g. Fortecon) under (or behind) all reinforced concrete slabs, permanent retaining walls, permanent anchors, piers/piles, and metallic posts/bollards, to electrically isolate from soil and stray currents. Note: that this may not be possible/practical at piers/piles or where friction is relied upon for structural purposes.
- The use of high strength (minimum 32 MPa), high cover (minimum 50 mm) concrete to effectively prevent/limit soil moisture penetrating through to the steel/metal.

These recommendations have been adopted in the structural engineering design.



#### 7. Conclusion

The structural assessment report demonstrates that the proposed development at Fiveways ,Crows Nest can be completed within the requirements set by Transport for New South Wales for building adjacent to the Sydney Metro infrastructure.

The structural engineering design has been completed to ensure existing rail infrastructure is maintained and unaffected by the proposed development. Nil reliance has been placed on the rail infrastructure or corridor for support of the development in both the temporary and permanent case.

This structural assessment report is to be read in conjunction with the ABC Consultants structural engineering documentation, project 23012 – Fiveways, Crows Nest.



## 8. Appendix A – Structural Engineering Drawings

	Regulated Design Record						
Proje	Project Address: 391/423 PACIFIC HIGHWAY CROWS NEST NSW 2065						
Proje	ct Title:	FIVEWAYS CROWS	NEST				
Cons	ent No:	ent No: SSD-66826207 Body Corporate Reg No: DEP0000250			00250		
Drawing Title: SITE RETENTION NOTES			Drawing No: S00-005				
Rev	Date dd.mm.yy	Description		DP Full Name	Reg No		
1	12.11.24	APPROVED FOR C	ONSTRUCTION	RYAN CAMPBELL	DEP0000027		

## BORED PILES

- REFER TO THE GEOTECHNICAL REPORT E24770.G03\_REV 1 BY EI AUSTRALIA (DATED 31 OCTOBER 2024) FOR A DESCRIPTION OF THE ANTICIPATED SITE CONDITIONS. THE PILING CONTRACTOR IS TO STUDY THE REPORT AND MAKE HIS OWN EVALUATION OF THE SITE CONDITIONS. ANY ADDITIONAL COSTS INCURRED SHALL BE BORNE BY THE PILING CONTRACTOR.
- THE BORED PILES ARE PROPORTIONED FOR THE SCHEDULED LOADS WITH ALLOWABLE SOCKET SKIN FRICTION AND END BEARING CAPACITY AS INDICATED IN THE REPORT. THE DEPTHS AND LENGTHS NOMINATED IN THE SCHEDULE ARE INDICATIVE ONLY. THEY MAY NEED TO BE VARIED DEPENDING ON THE SITE CONDITIONS ENCOUNTERED. THE PILING CONTRACTOR NEEDS TO INCORPORATE ANY DESIGN CHANGES REQUIRED AND ADVISE PROJECT ENGINEER WHO WILL ASSESS ANY DESIGN CHANGES RESULTING FROM THESE
- ALL WORKMANSHIP AND MATERIAL SHALL BE IN ACCORDANCE WITH AS 2159. THE BORED PILES SHALL BE LOCATED CONCENTRIC WITH THE COLUMNS AND

CHANGES THAT MAY BE REQUIRED BEFORE WORK RE-COMMENCE.

- WALLS UNLESS NOTED OTHERWISE. DRILL AND INSTALL THE BORED PILES IN THE LOCATIONS SHOWN ON THE
- DRAWINGS AND THE ABOVE REQUIREMENTS. THE PILING CONTRACTOR SHALL ALLOW FOR THE COST OF INTEGRITY TESTING OF 10% ALL BORED PILES IN ACCORDANCE WITH AS2159 CLAUSE 8.8. ALL PILE

INTEGRITY TESTING IS TO BE WITNESSED BY THE PROJECT GEOTECHNICAL

- BEFORE ANY CONCRETE IS POURED, ALL ROCK SOCKETS SHALL BE DEWATERED AND INSPECTED BY A GEOTECHNICAL ENGINEER, WHO SHALL BE EMPLOYED BY THE BUILDER, TO VERIFY THE SOIL PARAMETERS. THE SOCKET BASE AND WALLS MUST BE CLEAN AND FREE FROM CLAY.
- IF THE CONCRETE NEEDS TO BE TREMIED, SUPER PLASTICIZER MUST BE ADDED TO THE MIX AND THE CONCRETE GRADE INCREASED BY 30%. REFER TO THE SPECIFICATIONS FOR THE INSPECTION OF THE HOLE PRIOR TO
- ANY ALTERNATIVE DESIGN SHALL MEET THE ABOVE REQUIREMENTS AND THE SCHEDULED LOADS. THE PILING CONTRACTOR SHALL OBTAIN CERTIFICATION FOR THE CALCULATIONS OF THE ALTERNATIVE SYSTEM. THE DETAILS AND CALCULATIONS SHALL BE SUBMITTED TO THE ENGINEER FOR REVIEW. THE CONTRACTOR SHALL BE FULLY RESPONSIBLE FOR THE PERFORMANCE OF THE ALTERNATIVE BORED PILES.
- PILING CONTRACTOR TO ALLOW FOR CASING OF ALL PILES IN LOOSE MATERIAL
- 11. SPLICING TO LONGITUDINAL PILE REINFORCEMENT IS TO BE AVOIDED WHERE POSSIBLE I.E. FOR PILE CAGE LENGTHS LESS THAN 12m. SPLICES OF CAGE REINFORCEMENT ARE TO ENSURE MINIMUM SPACING BETWEEN TIES ARE MAINTAINED. LOCATION OF SPLICED CAGES ARE TO BE APPROVED BY THE STRUCTURAL ENGINEER.

## **BULK EARTHWORKS AND SHORING NOTES**

REFER TO GEOTECHNICAL REPORT E24770.G03 REV 1 BY EI AUSTRALIA (DATED 31 OCTOBER 2024) AND THE CONTRACTOR IS TO ENSURE GEOTECH REPORT RECOMMENDATIONS ARE ADHERED TO.

THESE NOTES ARE TO BE READ IN CONJUNCTION WITH THE HEAD SPECIFICATION.

PROVIDE GRAVEL SHAKEDOWN AREA FOR 10 METRES AT BOUNDARY OF SITE AND OTHER SEDIMENT CONTROL MEASURES GENERALLY CONSISTENT WITH THE REQUIREMENTS OF THE PUBLICATION SOIL AND WATER MANAGEMENT FOR URBAN DEVELOPMENT NSW DEPARTMENT OF HOUSING 1993, (ISDN 0 7305 9423 0), FOR THE DURATION OF THE WORKS. NOTE THAT ALL WORKS ON SITE ARE TO COMPLY WITH COUNCIL SOIL AND EROSION CONTROL REQUIREMENTS. ALLOW TO SUBMIT DETAILS TO COUNCIL FOR APPROVAL IF REQUIRED. ENSURE STREETS ARE KEPT CLEAN OF ALL DEBRIS.

THE CONTRACTOR IS TO ENSURE THAT THE DUST PREVENTION METHODS HE ADOPTS ARE SUFFICIENT TO MEET THE REQUIREMENTS OF THE COUNCIL. IT IS THE CONTRACTORS' RESPONSIBILITY TO ACQUAINT HIMSELF WITH THE REQUIREMENTS.

REFER TO THE ARCHITECTS DRAWINGS FOR THE ACCURATE SETOUT OF ALL BUILDINGS, DRIVEWAYS, PARKING AREAS ETC. NOTE BULK EARTHWORKS PLAN IS INDICATIVE ONLY. CALCULATE AND CUT BATTERS FROM ARCHITECT'S PLANS AND SURVEY. CROSSOVER PROFILES TO COUNCIL REQUIREMENTS.

PROCEED WITH BULK EARTHWORKS AND SHORING TO PROVIDE A STABLE SUBGRADE AND WORK SPACE FOR THE CONSTRUCTION OF THE PROPOSED DEVELOPMENT. STRIP AND DISPOSE OF TOPSOIL, REDUCE SITE TO LEVELS INDICATED AND DISPOSE OF ALL UNWANTED MATERIAL LEGALLY.

A GEOTECHNICAL ENGINEER IS TO PROVIDE SUPERVISION (AS3798) FOR ALL EARTHWORKS DURING THE COURSE OF CONSTRUCTION. AT THE COMPLETION OF THE BULK EXCAVATION CONTRACT, THE GEOTECHNICAL ENGINEER IS TO PROVIDE CERTIFICATION THAT THE WORKS HAVE BEEN CARRIED OUT IN ACCORDANCE WITH

BULK EARTHWORKS SPECIFICATION. DRAINAGE DURING CONSTRUCTION PROVIDE ADEQUATE DRAINAGE DURING CONSTRUCTION TO ENSURE MINIMUM

DISRUPTION FROM RAIN.

DURING EXCAVATION COORDINATE WITH ALL SERVICES INCLUDING SEWER, GAS AND POWER.

BULK EARTHWORKS PROCEDURE AND SPECIFICATION.

- THE SITE IS TO BE STRIPPED OF TOPSOIL AND UNCONSOLIDATED EXISTING FILL AT THE COMPLETION OF THE BULK EARTHWORKS, THE CONTRACTOR SHALL PROVIDE TEMPORARY OR PERMANENT DRAINAGE TO ENSURE NO SURFACE WATER IS RETAINED ON THE SITE, OR THAT SURFACE WATER FLOW DETRIMENTALLY SCOURS THE PREPARED BASE.
- GEOTECHNICAL ENGINEER NOTES EXCAVATION TO BE CARRIED OUT UNDER GEOTECHNICAL ENGINEER'S SUPERVISION
- GEOTECHNICAL ENGINEER (GE) TO COMMENT ON SUITABILITY OF THE SUBCONTRACTOR'S METHOD OF EXCAVATION AS REMOVAL PROCEEDS.
- DURING EXCAVATION COORDINATE WITH ALL HYDRAULIC ENGINEERS REQUIREMENTS FOR SEWER, GAS AND STORMWATER LINES. PROVIDE AN AS-BUILT DRAWING PREPARED BY A REGISTERED SURVEYOR
- DIMENSIONS AND LEVELS. DILAPIDATION REPORT THE APPROVED SHORING WALL CONTRACTOR SHALL PREPARE A DILAPIDATION REPORT OF STREET, FOOTPATH, ROAD FEATURES AND ALL REQUESTED RAILCORP ASSETS PRIOR TO INSTALLATION OF SHORING

TO CONFIRM BULK EARTHWORKS IS COMPLETED TO REQUIRED

COMPACTION NOTES COMPACTION BEHIND INTERNAL FORMED RETAINING WALL BY

EXCAVATION CONTRACTOR USING HAND HELD RAMMERS TO ACHIEVE 98% MODIFIED DENSITY. COMPACT IN MAXIMUM 300mm THICK LAYERS AT OPTIMUM MOISTURE CONTENT OF ±3%.

CONTRACTOR TO ALLOW FOR 15% INCREASE IN ANCHOR QUANTITIES OR SIZES TO ACCOMMODATE REQUIREMENTS BY GEOTECHNICAL CONSULTANT **DURING EXCAVATION WORKS** 

BOND LENGTH AND DIAMETER OF ANCHOR HOLE TO BE CONFIRMED BY SHORING WALL CONTRACTOR. THE ANCHOR LENGTHS SHOWN ON THE

STRUCTURAL DRAWINGS ARE INDICATIVE ONLY

# SHORING DESIGN CRITERIA

STRUCTURE IMPORTANCE LEVEL: DESIGN WORKING LIFE: 50 YEARS OR MORE WIND ANNUAL PROBABILITY OF EXCEEDANCE: EARTHQUAKE ANNUAL PROBABILITY OF EXCEEDANCE: EARTHQUAKE DESIGN CATEGORY: CONCRETE EXPOSURE CLASSIFICATION: REFER LOADING PLANS GEOTECHNICAL REDUCTION FACTOR:  $\phi_{q} = 0.56$ 

## **GEOTECHNICAL DESIGN PARAMETERS**

ALLOWABLE END BEARING CAPACITY CLASS II SANDSTONE ALLOWABLE SHAFT ADHESION CLASS II SANDSTONE

PERMANENT SHORING WALLS HAVE BEEN DESIGNED IN ACCORDANCE WITH AS3600, AS1170, AS2159 WITH A DURABILITY DESIGN LIFE OF 50 YEARS

## CONCRETE GRADE

_	LEMENT CONCRETE QUALITY	STRENGTH f'c	MAX SIZE AGG. mm	SLUMP mm	CEMENT TYPE	ADMIXTURE
S	HORING PILES	50	20	80	GP	-
S	HOTCRETE	32	10	150 - 200	GP	-
	ADDING DEAM	50	20	90	CD	

NOTE: ALL CEMENTITIOUS MATERIAL MUST CONFIRM TO TINSW SPECIFICATION 3211

COVERS			
ELEMENT	TOP	ВТМ	SIDES
PILES	60mm	60mm	60mm
CAPPING BEAM	50mm	50mm	50mm
SHOTCRETE	50mm	50mm	50mm

# **TOLERANCE**

- BORES SHALL BE CENTERED WITHIN 25mm OF THE 'DESIGN' CENTRE AS INDICATED ON THE PLANS.
- MAXIMUM "OUT OF PLUMB" OF BORES SHALL BE 75mm OR 1:500, WHICHEVER IS LESS
- GROUND ANCHORS

## **MONITORING**

- MONITORING OF THE ADJACENT BUILDINGS AND TOP AND MIDDLE OF THE SOLDIERS SHALL BE CARRIED OUT IN ACCORDANCE WITH GEOTECHNICAL AND VIBRATION MONITORING PLANS PREPARED BY GEOTECHNICAL ENGINEER.
- MONITORING OF SURVEY POINTS SHALL BE BY A LICENSED SURVEYOR AND BE INITIALLY AT MAXIMUM THREE WEEK INTERVALS & FOR EVERY BASEMENT LEVEL EXCAVATED.
- 3. IF ANY MOVEMENTS ABOVE THE LIMITS NOMINATED BY THE GEOTECHNICAL ENGINEER ARE DETECTED, ALL WORKS SHALL BE CEASED, THE ENGINEER SHALL BE IMMEDIATELY NOTIFIED. THE PROJECT MANAGER SHALL NOTIFY THE ADJOINING PROPERTY
- RECORDS SHALL BE KEPT OF ALL MONITORING AND BE AVAILABLE FOR INSPECTION AT ANY TIME.

GEOTECHNICAL ENGINEER TO APPROVE ALL PILE SPACINGS ON SITE AND TO CONFIRM RETAINED MATERIALS ABILITY TO ARCH BETWEEN PILES TEMPORARILY.

## CONSTRUCTION SEQUENCE FOR EXTERNALLY ANCHORED SOLDIER WALLS:

- THE PROPOSED BASEMENT EXCAVATION WILL PROCEED IN THE FOLLOWING SEQUENCE:
- 1. SETOUT THE LOCATION OF THE PILES AND CAPPING BEAMS AS NOTED ON PLANS, ELEVATION AND SECTIONS.
- HOLD POINT THE GEOTECHNICAL ENGINEER (WHO SHALL BE EMPLOYED BY THE BUILDER) IS REQUIRED TO CERTIFY THAT THE SOIL CONDITIONS COMPLY WITH THE DESIGN ASSUMPTIONS DETAILED IN THE GEOTECHNICAL INVESTIGATION REPORT. THE GEOTECHNICAL ENGINEER IS TO DETERMINE THE LEVEL OF SUPERVISION REQUIRED TO BE ABLE TO PROVIDE THIS
- CERTIFICATE. SUPERVISION OF THE MATERIAL REMOVED AS PILES ARE DRILLED MAY BE REQUIRED. DRILL REQUIRED BORE HOLES TO THE DIAMETER SPECIFIED AND DEPTH SHOWN ON PLANS, ELEVATIONS AND SECTIONS. ENSURE

THE SOCKET IS FULLY CLEANED AND ALL LOOSE MATERIAL IS

- **HOLD POINT** THE STRUCTURAL ENGINEER IS TO WITNESS THE REINFORCEMENT CAGES PRIOR TO PLACEMENT IN THE BORED
- PILES. PLACEMENT OF THE CAGES WITHIN THE PILES FOR PILES GREATER THAN 6M DEEP IS TO BE WITNESSED ON SITE PLACE REINFORCEMENT CAGES IN HOLES ENSURING THAT CAGES ARE ORIENTATED SO DRILLING THROUGH SOLDIER PILES FOR ANCHORS / ROCK BOLTS WILL CLEAR ANY VERTICAL REINFORCEMENT IN PILES. END CAPS ARE TO BE PLACED AT THE BASE OF THE REINFORCEMENT CAGE AND ROLLER CHAIRS PLACED AT 2M INTERVALS ALONG THE LENGTH OF THE PILE (A
- MINIMUM OF 3 PER SECTION) TO ENSURE MINIMUM COVER TO THE CAGE IS MAINTAINED. USING A TREMIE PIPE OR SIMILAR FROM THE BASE OF THE BORED HOLE TO ENSURE NO SEPARATION OF CONCRETE AGGREGATE, PLACE CONCRETE FROM THE BASE OF THE PILE TO UNDERSIDE OF CAPPING BEAM. VIBRATE CONCRETE PROGRESSIVELY FROM THE BASE OF THE PILE AS THE PILE IS
- INSTALL CAPPING BEAM REINFORCEMENT IN ACCORDANCE WITH DETAILS ON THESE DRAWINGS. **HOLD POINT** THE STRUCTURAL ENGINEER IS TO WITNESS THE
- REINFORCEMENT OF THE CAPPING BEAM. PLACE CAPPING BEAM CONCRETE AND ALLOW TO CURE FOR A MINIMUM OF 7 DAYS.
- HOLD POINT PROJECT SURVEYOR IS TO ESTABLISH A DATUM OF THE CAPPING BEAM LOCATION PRIOR TO ANY EXCAVATION PAST THE CAPPING BEAM. REFER TO MONITORING NOTES. MONITORING OF THE WALL IS TO CONTINUE ON A REGULAR
- BASIS AS DETAILED IN THE MONITORING NOTES. EXCAVATE AGAINST THE PILES TO MAXIMUM 500MM BELOW THE TOP LEVEL OF ROCK ANCHORS / BOLTS OR TO A MAXIMUM OF
- 2.0M WHICHEVER IS THE LESSER. 12. DRILL AND EPOXY SHOTCRETE DOWELS INTO SHORING PILES AS NOMINATED ON DRAWINGS. PLACE REINFORCEMENT TO THE SHOTCRETE WALL.
- HOLD POINT THE STRUCTURAL ENGINEER IS TO WITNESS THE REINFORCEMENT OF THE SHOTCRETE PANELS AND ENSURE MINIMUM DEPTH IS ACHIEVED TO THE PANEL. PLACE CONCRETE TO SHOTCRETE WALL. SHOTCRETE PANELS
- ARE TO BE FORMED AND POURED OR SPRAYED. IF SHOTCRETE WALLS ARE SPRAYED, THE PANELS ARE TO BE OVERSPRAYED AND THEN SCREEDED BACK TO THE DESIGN THICKNESS. SHOTCTRETE IS TO BE SELF-COMPACTING IN ACCORDANCE WITH
- IF THE EXCAVATION IS AT THE LEVEL OF THE SHORING ANCHOR; SCAN PILE FOR REINFORCEMENT PRIOR TO CORING ANCHOR HOLE, A MAXIMUM HORIZONTAL DEVIATION OF 5° TO CLEAR ANY REINFORCEMENT IS PERMITTED, OTHERWISE CONTACT THE STRUCTURAL ENGINEER FOR FURTHER ADVICE. DRILL ANCHOR BORE HOLES, INSTALL ROCK ANCHORS / BOLTS WITH ASSOCIATED CENTRALISERS AND GROUT TUBES, PLACE GROUT WITHIN THE BORE HOLE. (REFER ROCK ANCHORS – POST TENSIONED STRAND NOTES).
- HOLD POINT THE GEOTECHNICAL ENGINEER IS TO WITNESS THE WEDGE LIFT OFF AND ACHOR LIFT OFF TESTS AS REQURIED. ONCE THE GROUT HAS ACHIEVED DESIGN STRENGTH AND AFTER A MINIMUM 3 DAYS, THE ROCK ANCHORS / BOLTS MAY BE
- STRESSED. PROVIDED THE SHOTCRETE PANELS HAVE REACHED 25MPA STRENGTH AND THE SHORING ANCHORS ARE FULLY STRESSED EXCAVATION MAY CONTINUE TO THE NEXT STAGE. REPEAT STEPS 10 TO 17 THE FINAL ANCHOR IS INSTALLED AT THE TOE OF
- CONTINUE EXCAVATION INTO THE UNSUPPORTED CLASS II / III SANDSTONE IN ACCORDANCE WITH THE GEOTECHNICAL
- ENGINEERING REPORT AND ADVICE. MINIMUM 3 MONTHS AFTER GROUND FLOOR / LEVEL 1 SLAB HAS BEEN CAST, REBATES AT EACH SLAB / PILE INTERFACE SHALL BE CLEANED OUT AND GROUTED UP WITH AN APPROVED NON-SHRINK GROUT (MONOLITH OR EQUAL). WHEN F'C GROUT IS AT LEAST 40 MPA. TYPICAL ANCHORS / ROCK BOLTS SHALL BE DESTRESSED, ANCHOR HEADS REMOVED AND PILES MADE

## **ROCK ANCHORS - POST-TENSIONED STRAND**

- IN ADDITION TO ANY NOTES PROVIDED BELOW AND DETAILS SHOWN ON THESE DRAWINGS, ALL ROCK ANCHORS ARE TO BE INSTALLED IN ACCORDANCE WITH AS4678 AND TRANSPORT FOR NSW QA SPECIFICATION B114
- ANCHORS SHALL CONSIST OF LOW RELAXATION STRESS-RELIEVED SUPERGRADE STEEL STRAND TO AS4672.1 AND AS4672.2 AND ANCHORAGES AND WEDGES SHALL CONFORM TO AS1314.
- ALL STEEL ELEMENTS, INCLUDING BEARING PLATES AND WASHERS, MUST BE FABRICATED FROM GRADE 250 STEEL IN ACCORDANCE WITH AS3678. NUTS FOR THE ROCK BOLTS MUST BE GRADE C COMPLYING WITH AS1112.3 AND PROPERTY CLASS 5 COMPLYING WITH AS4291.2 OR EQUIVALENT TO SUIT THE END THREAD
- 4. THE USE OF COUPLERS TO THE ANCHOR STRANDS IS NOT PERMITTED.
- PRIOR TO ANY DRILLING OPERATIONS, THE BUILDER SHALL ACQUAINT THEMSELVES WITH ALL ADJACENT UNDERGROUND SERVICES AND ENSURE THAT NONE OF THESE ARE DISRUPTED BY ROCK ANCHORS. ALL APPROPRIATE APPROVALS, PERMITS AND AGREEMENTS SHALL BE OBTAINED BEFORE
- COMMENCEMENT OF THE WORK. BORE HOLES FOR THE ROCK BOLTS MUST BE DRILLED USING ROTARY OR ROTARY PERCUSSION DRILLING EQUIPMENT. DRILLING FLUIDS AND CORE DRILLING ARE NOT PERMITTED. BORE HOLES MUST BE INSTALLED WITH A MAXIMUM DEVIATION FROM THE DESIGN INCLINATION IN ANY DIRECTION OF 2° AND A MAXIMUM DEVIATION FROM THE ENTRY POINT OF +/- 25mm.
- CENTRALISERS MUST BE PROVIDED ALONG THE LENGTH OF THE STRAND AT 1000mm CENTRES WITHIN THE BOND LENGTH, 2000mm CENTRES WITHIN THE FREE LENGTH AND 300mm FROM EACH END TO ENSURE THE STRAND IS CENTRALISED TO THE CENTRE OF THE BOREHOLE. THE CENTRALISERS MUST BE; NON-CORRODIBLE, FIRMLY FIXED TO THE BOLT AND A SHAPE THAT PERMITS THE FREE FLOW OF GROUT TO FULLY ENCAPSULATE THE BOLT.
- GROUT TUBES MUST EXTEND TO THE BASE OF THE LOWEST PORTION OF THE BORE HOLE AND BE SECURELY FIXED TO THE STRANDS. TUBING MUST BE OF ADEQUATE STRENGTH TO RESIST ANY DAMAGE DURING INSTALLATION AND
- GROUTING AND BE OF SUFFICIENT SIZE TO ALLOW PUMPING OF GROUT. MATERIAL PROPERTIES OF THE GROUT MUST CONFORM TO TABLE B114.2 OF TFNSW QA SPECIFICATION R64. GROUTS MUST GENERALLY HAVE A HIGH BLEED RESISTANCE, LOW SHRINKAGE AND HIGH FLUIDITY. THE GROUT SHALL HAVE A MINIMUM COMPRESSIVE STRENGTH OF S20MPA AT THREE (3) DAYS. GROUT CYLINDERS SHALL BE TAKEN ON THE BASIS OF ONE SAMPLE (TWO CYLINDERS) FOR EVERY TEN ANCHORS AND TESTED ON THE DAY OF STRESSING. THE GROUT SHALL BE MIXED IN A HIGH SPEED IMPELLER TYPE MACHINE.
- THE STRANDS SHALL PULLED TAUT AND MARKED AT THE FACE OF THE WEDGE PRIOR TO UNDERTAKING THE TENSIONING PROCEDURE. MEASUREMENTS FROM THE FACE OF THE WEDGE TO THE MARKING SHALL BE TAKEN AT 25%, 50%, 75%, 100% AND 125% AS THE STRAND IS PROGRESSIVELY TENSIONED TO THE PROOF LOAD. RESULTS OF THE MEASUREMENTS SHALL BE PROVIDED TO THE ENGINEER FOR COMPARISON AGAINST THEORETICAL EXTENSIONS.
- EACH ANCHOR SHALL BE PROOF LOADED I.E. STRESSED TO 125% OF THE WORKING LOAD, HELD FOR FIVE MINUTES, AND SLOWLY EASED BACK. THE ANCHOR SHALL BE THEN STRESSED TO WORKING LOAD AND LOCKED OFF. ANY ANCHOR WHICH FAILS TO HOLD THE LOAD SHALL BE REMOVED AND REPLACED WITH ANOTHER ANCHOR. SUCH WORK SHALL BE CARRIED OUT IN THE PRESENCE
- STRANDS WHICH EXTEND EXCESSIVELY BEYOND THE FACE OF THE PILE MAY BE CUT TO A MINIMUM LENGTH OF 300mm + THE EXTENSION LENGTH FROM THE PILE
- ALL ANCHORS TO BE TESTED USING THE INDUSTRY STANDARD 'WEDGE LIFT-OFF' TEST METHODOLOGY AND IN ADDITION 10% OF ALL ANCHORS TO BE ADDITIONALLY TESTED USING THE 'ANCHOR LIFT-OFF' TESTING METHODOLOGY IMMEDIATELY FOLLOWING LOCK-OFF OF THE ANCHORS.
- ALL ROCK ANCHORS TO BE INSPECTED BY GEOTECHNICAL ENGINEER DURING INSTALLATION TO CONFIRM CORRECT INSTALLATION AND ANCHOR LOADS
- MINIMUM DESIGN LIFE OF ALL TEMPORARY ROCK ANCHORS TO BE 2 YEARS OR AS NOMINATED BY BUILDER.
- THE BUILDER SHALL KEEP ON SITE AN ADEQUATE SUPPLY OF ANCHOR CABLES, GROUT ETC. FOR EMERGENCY USE.
- THE BUILDER SHALL REGULARLY MONITOR THE STRESS IN THE ANCHORS REGULARLY BY MEANS OF A LIFT OFF TEST TO ENSURE NO MAJOR LOSSES ARE OCCURRING. IF STRESS LOSSES ARE DETECTED THEY SHALL BE IMMEDIATELY BROUGHT TO THE ATTENTION OF THE ENGINEER.

## **ROCK ANCHORS - SOLID BAR**

- IN ADDITION TO ANY NOTES PROVIDED BELOW AND DETAILS SHOWN ON THESE DRAWINGS, ALL ROCK BOLTS ARE TO BE INSTALLED IN ACCORDANCE WITH AS 4678 AND TRANSPORT FOR NSW QA SPECIFICATION R64.
- ROCKS BOLTS MUST BE STEEL REINFORCEMENT BARS GRADE 500N DEFORMED BAR TO AS4671. THE BOLTS MUST BE THREADED AT ONE END TO SUIT ISO COARSE PITCH THREAD TO AS1275.
- ALL STEEL COMPONENTS OF THE ROCK BOLT SYSTEM, INCLUDING THE BOLT, BEARING PLATES, WASHERS AND NUTS MUST BE HOT-DIP GALVANISED TO AS/NZS4680 WITH A MINIMUM AVERAGE COATING WEIGHT OF 600 G/M2/.
- ALL STEEL ELEMENTS, INCLUDING BEARING PLATES AND WASHERS, MUST BE FABRICATED FROM GRADE 250 STEEL IN ACCORDANCE WITH AS3678. NUTS FOR THE ROCK BOLTS MUST BE GRADE C COMPLYING WITH AS1112.3 AND PROPERTY CLASS 5 COMPLYING WITH AS 4291.2 OR EQUIVALENT TO SUIT THE END THREAD
- 5. THE USE OF COUPLERS TO THE ROCK BOLTS IS NOT PERMITTED.

COMMENCEMENT OF THE WORK.

- PRIOR TO ANY DRILLING OPERATIONS, THE BUILDER SHALL ACQUAINT THEMSELVES WITH ALL ADJACENT UNDERGROUND SERVICES AND ENSURE THAT NONE OF THESE ARE DISRUPTED BY ROCK ANCHORS. ALL APPROPRIATE APPROVALS, PERMITS AND AGREEMENTS SHALL BE OBTAINED BEFORE
- BORE HOLES FOR THE ROCK BOLTS MUST BE DRILLED USING ROTARY OR ROTARY PERCUSSION DRILLING EQUIPMENT. DRILLING FLUIDS AND CORE DRILLING ARE NOT PERMITTED. BORE HOLES MUST BE INSTALLED WITH A MAXIMUM DEVIATION FROM THE DESIGN INCLINATION IN ANY DIRECTION OF 2° AND A MAXIMUM DEVIATION FROM THE ENTRY POINT OF +/- 25mm.
- CENTRALISERS MUST BE PROVIDED ALONG THE LENGTH OF THE BOLT AT 2000mm CENTRES AND 300mm FROM EACH END TO ENSURE THE BOLT IS CENTRALISED TO THE CENTRE OF THE BOREHOLE. THE CENTRALISERS MUST BE; NON-CORRODIBLE, FIRMLY FIXED TO THE BOLT AND A SHAPE THAT PERMITS THE FREE
- GROUT TUBES MUST EXTEND TO THE BASE OF THE LOWEST PORTION OF THE BORE HOLE AND BE SECURELY FIXED TO THE ROCK BOLT. TUBING MUST BE OF GROUTING AND BE OF SUFFICIENT SIZE TO ALLOW PUMPING OF GROUT.

FLOW OF GROUT TO FULLY ENCAPSULATE THE BOLT.

- MATERIAL PROPERTIES OF THE GROUT MUST CONFORM TO TABLE R64.1 OF TFNSW QA SPECIFICATION R64. GROUTS MUST GENERALLY HAVE A HIGH BLEED RESISTANCE, LOW SHRINKAGE AND HIGH FLUIDITY. THE GROUT SHALL HAVE A MINIMUM COMPRESSIVE STRENGTH OF S20MPA AT THREE (3) DAYS. GROUT CYLINDERS SHALL BE TAKEN ON THE BASIS OF ONE SAMPLE (TWO CYLINDERS) FOR EVERY TEN ANCHORS AND TESTED ON THE DAY OF STRESSING. THE GROUT SHALL BE MIXED IN A HIGH SPEED IMPELLER TYPE MACHINE.
- A MINIMUM OF 1% OF THE ROCK BOLTS MUST BE TESTED IN ACCORDANCE WITH THE "SUITABILITY TEST" AND A MINIMUM OF 3% OF THE ROCK BOLTS MUST BE TESTED IN ACCORDANCE WITH THE "ACCEPTANCE TEST" AS DEFINED IN TRANSPORT FOR NSW QA SPECIFICATION R64.
- RE-BOLTING OF THE ROCK BOLTS AT THE DISCRETION OF THE GEOTECHNICAL AND STRUCTURAL ENGINEERS MAY BE REQUIRED WHERE THE BOLT BECOMES OVERSTRESSED DURING EXCAVATION OR EXCESSIVE DEFORMATION OF ANY INCLINED ROCK BEDS EXISTS.

**CONSTRUCTION DESIGN** 

NOTE: DO NOT SCALE OFF DRAWINGS. REFER TO ARCHITECTURAL PLANS. VERIFY DIMENSIONS ON SITE.

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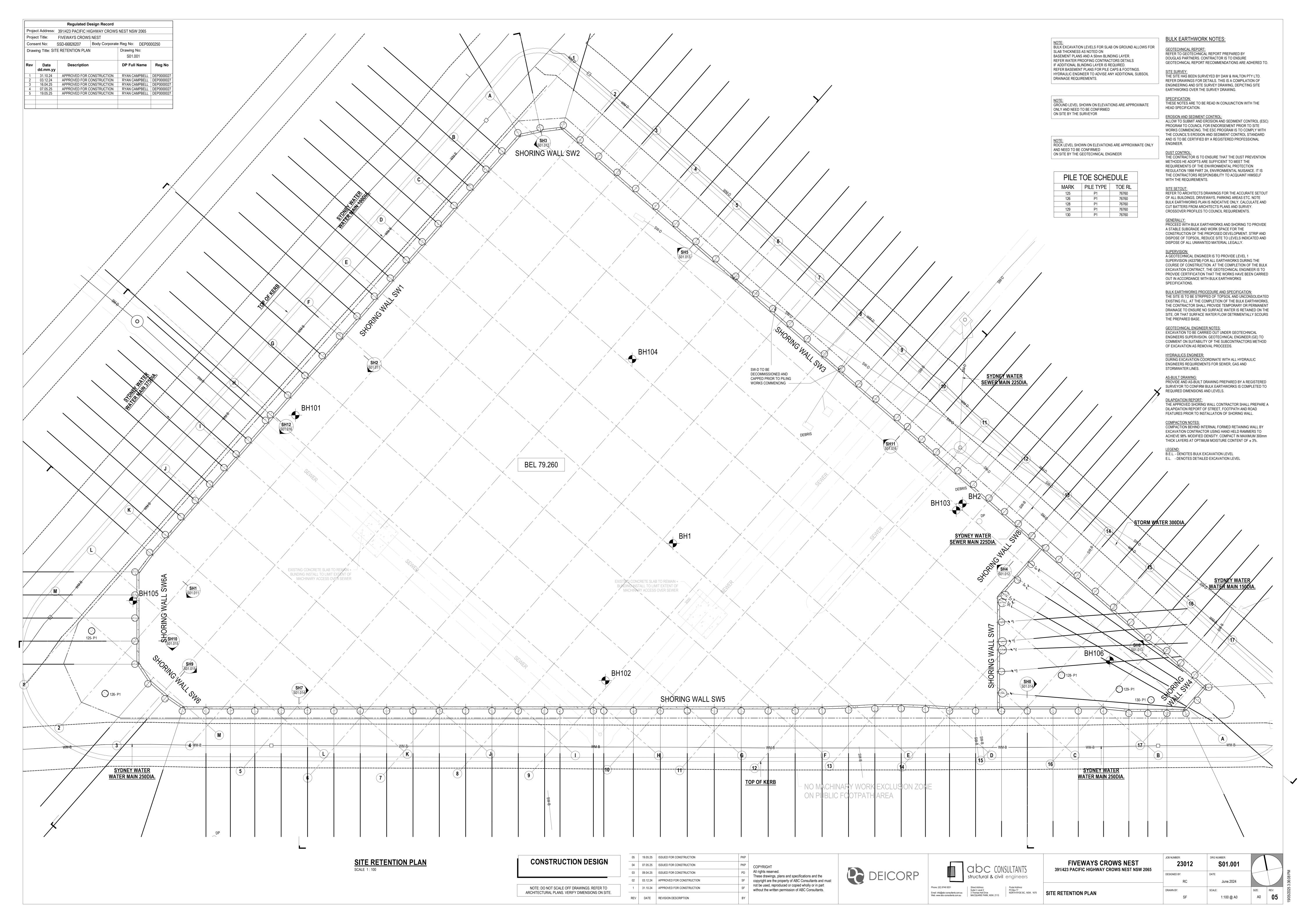
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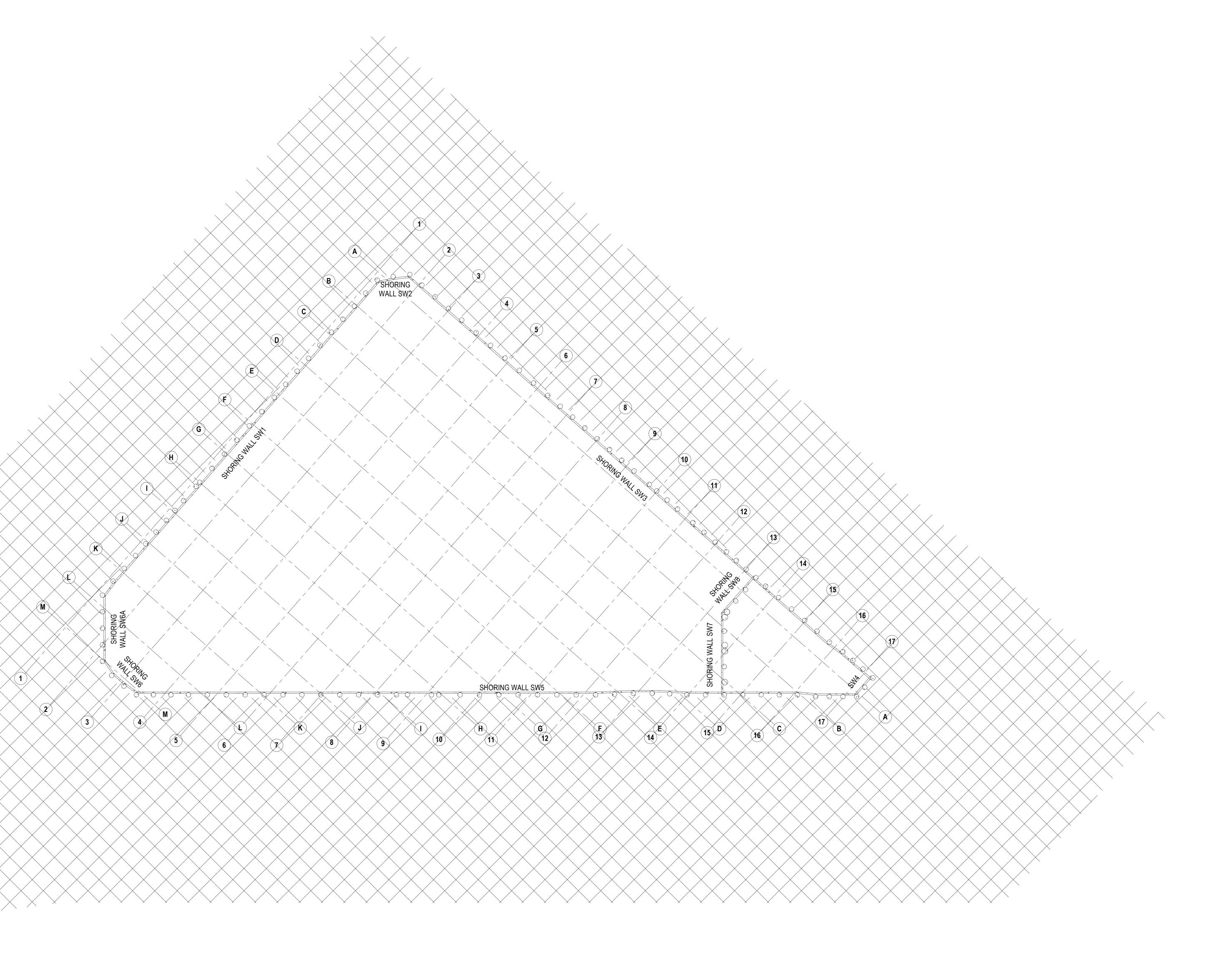




**FIVEWAYS CROWS NEST** DESIGNED BY:







# SHORING SURCHARGE LOADING PLAN

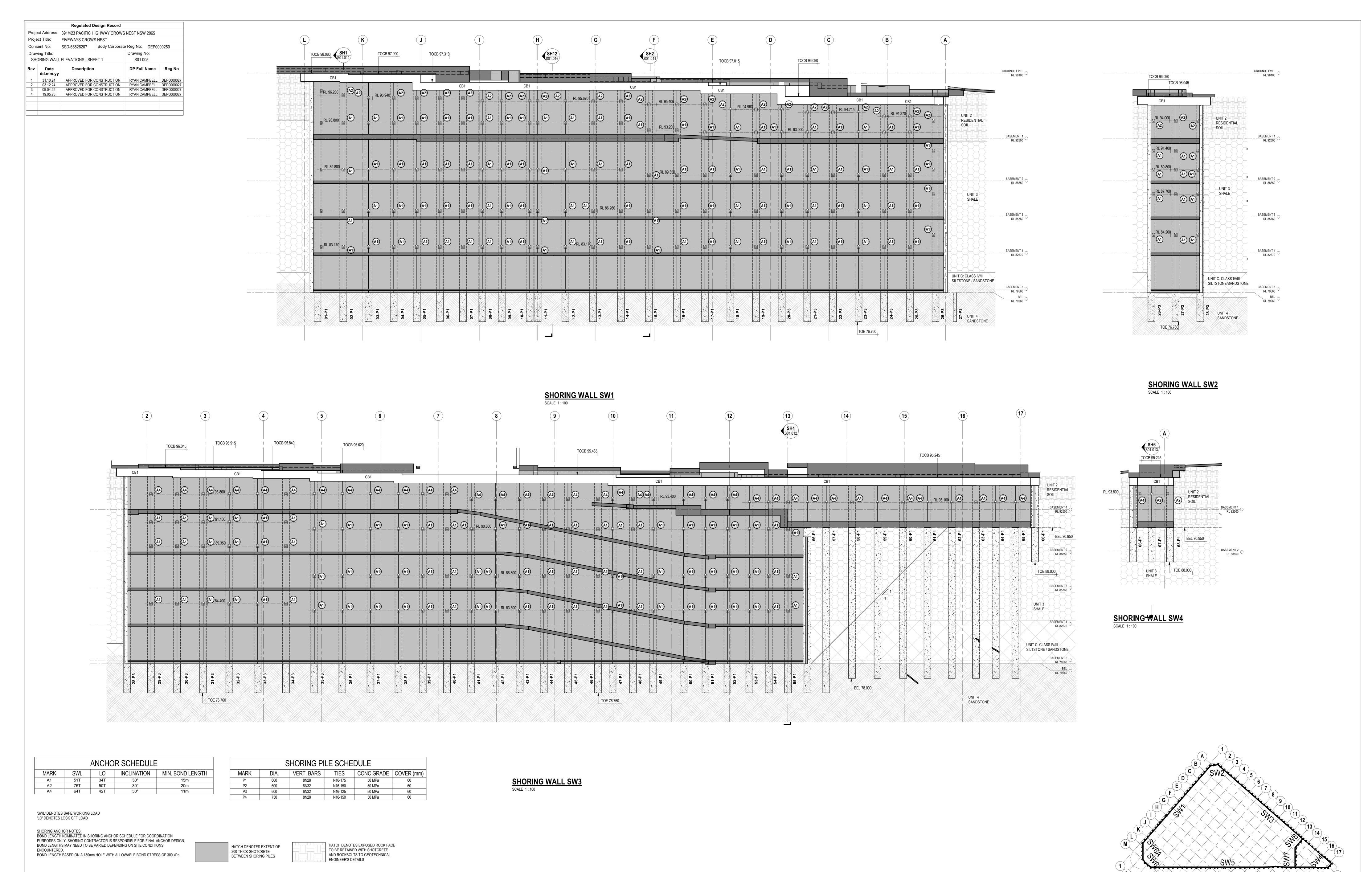
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FIVEWAYS CROWS NEST 391/423 PACIFIC HIGHWAY CROWS NEST NSW 2065	JOB NUMBER: 23012	DRG NUMBER: <b>\$01.002</b>			
E:	DESIGNED BY:	DATE: June.2024			
HORING SURCHARGE LOADING PLAN	DRAWN BY:	scale: 1:200 @ A0	SIZE:	REV: <b>03</b>	



NOTE:
MAXIMUM 500mm EXCAVATION BELOW ANCHOR HEIGHT PERMITTED PRIOR TO INSTALLING ANCHOR

ENGINEER

NOTE:
GROUND LEVEL SHOWN ON ELEVATIONS ARE APPROXIMATE ONLY

AND NEED TO BE CONFIRMED ON SITE BY THE SURVEYOR

ROCK LEVEL SHOWN ON ELEVATIONS ARE APPROXIMATE ONLY

AND NEED TO BE CONFIRMED ON SITE BY THE GEOTECHNICAL

GEOTECHNICAL ENGINEER TO INSPECT EXPOSED SHALE FACE REGULARLY DURING EXCAVATION AND NOMINATE APPROPRIATE ROCK BOLTS AND SHOTCRETE AS REQUIRED TO ENSURE STABILITY AT ALL TIMES.

THIS DRAWING SHOULD BE READ IN CONJUNCTION WITH DRAWING S01-001 - SITE RETENTION PLAN FOR SHORING PILE SETOUT DIMENSIONS.

**CONSTRUCTION DESIGN** NOTE: DO NOT SCALE OFF DRAWINGS. REFER TO ARCHITECTURAL PLANS. VERIFY DIMENSIONS ON SITE.

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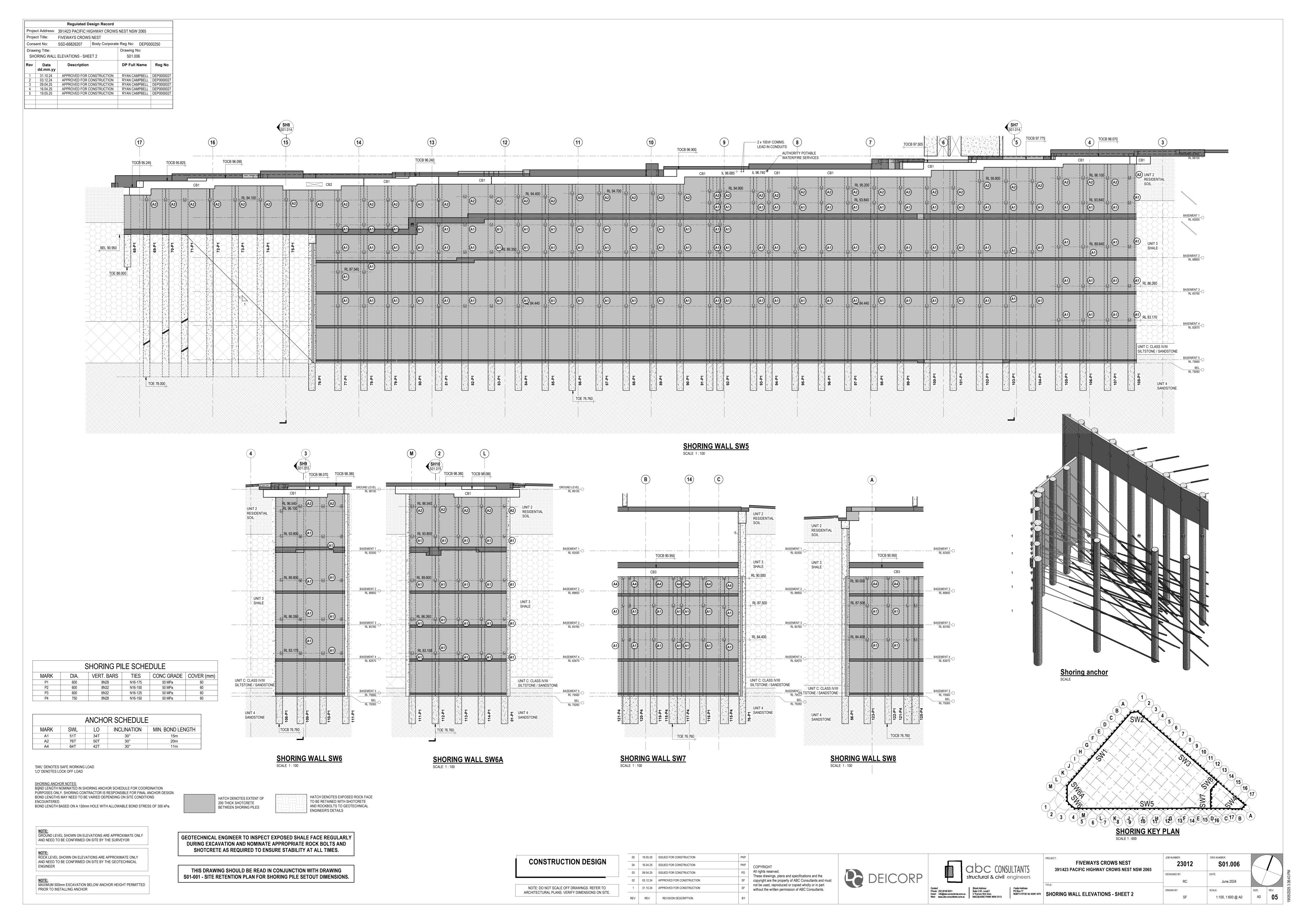
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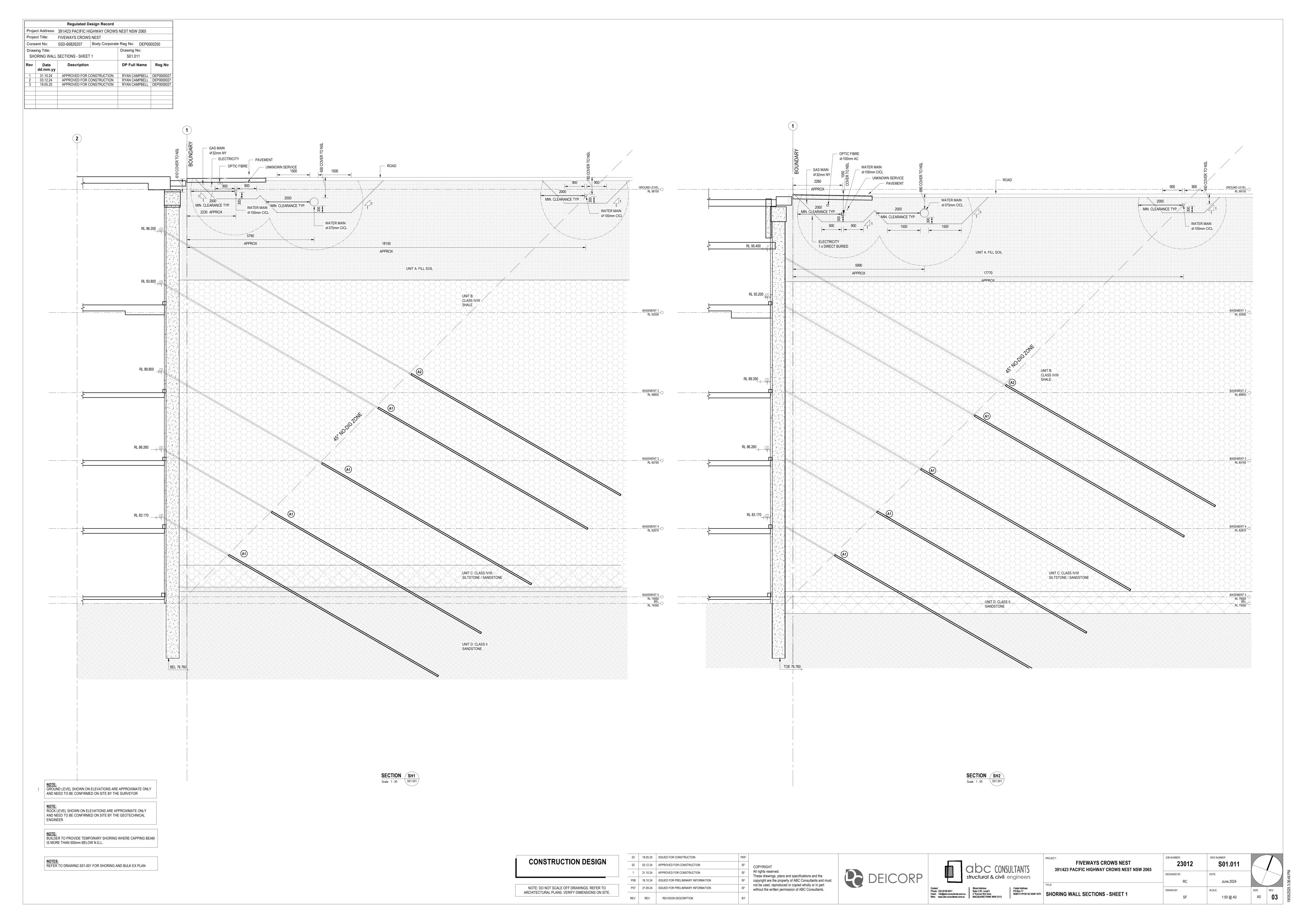


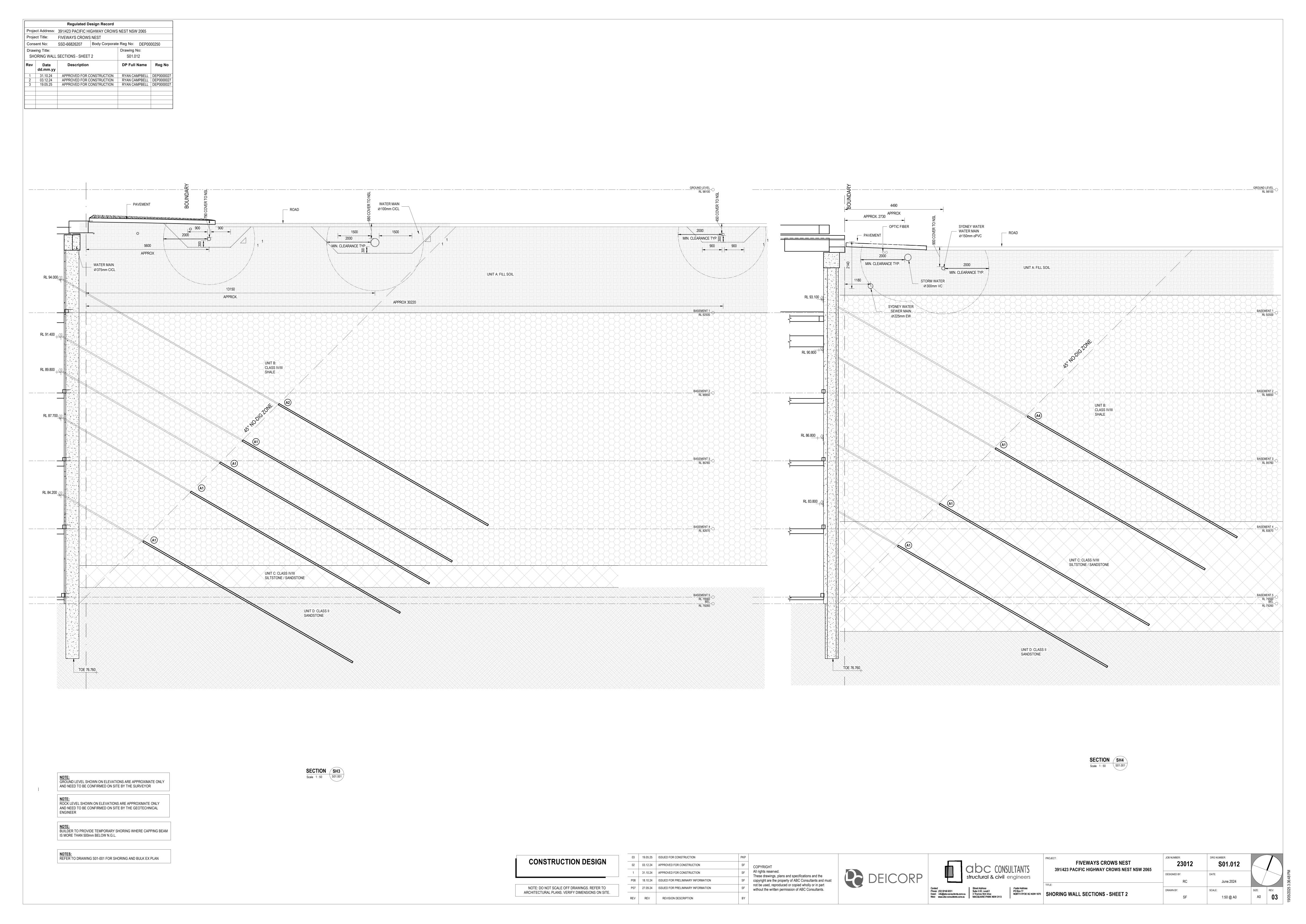


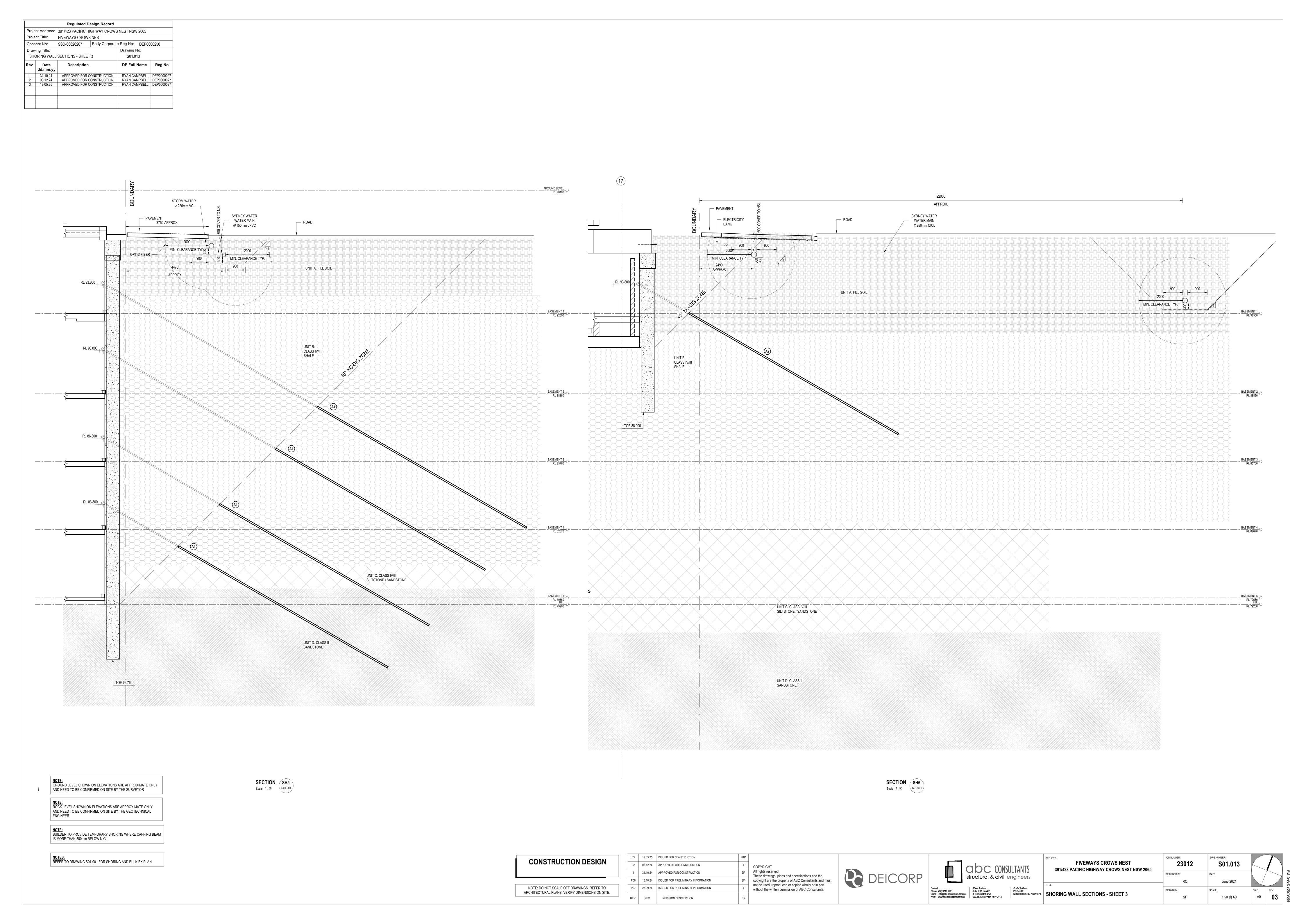
**FIVEWAYS CROWS NEST** 391/423 PACIFIC HIGHWAY CROWS NEST NSW 2065

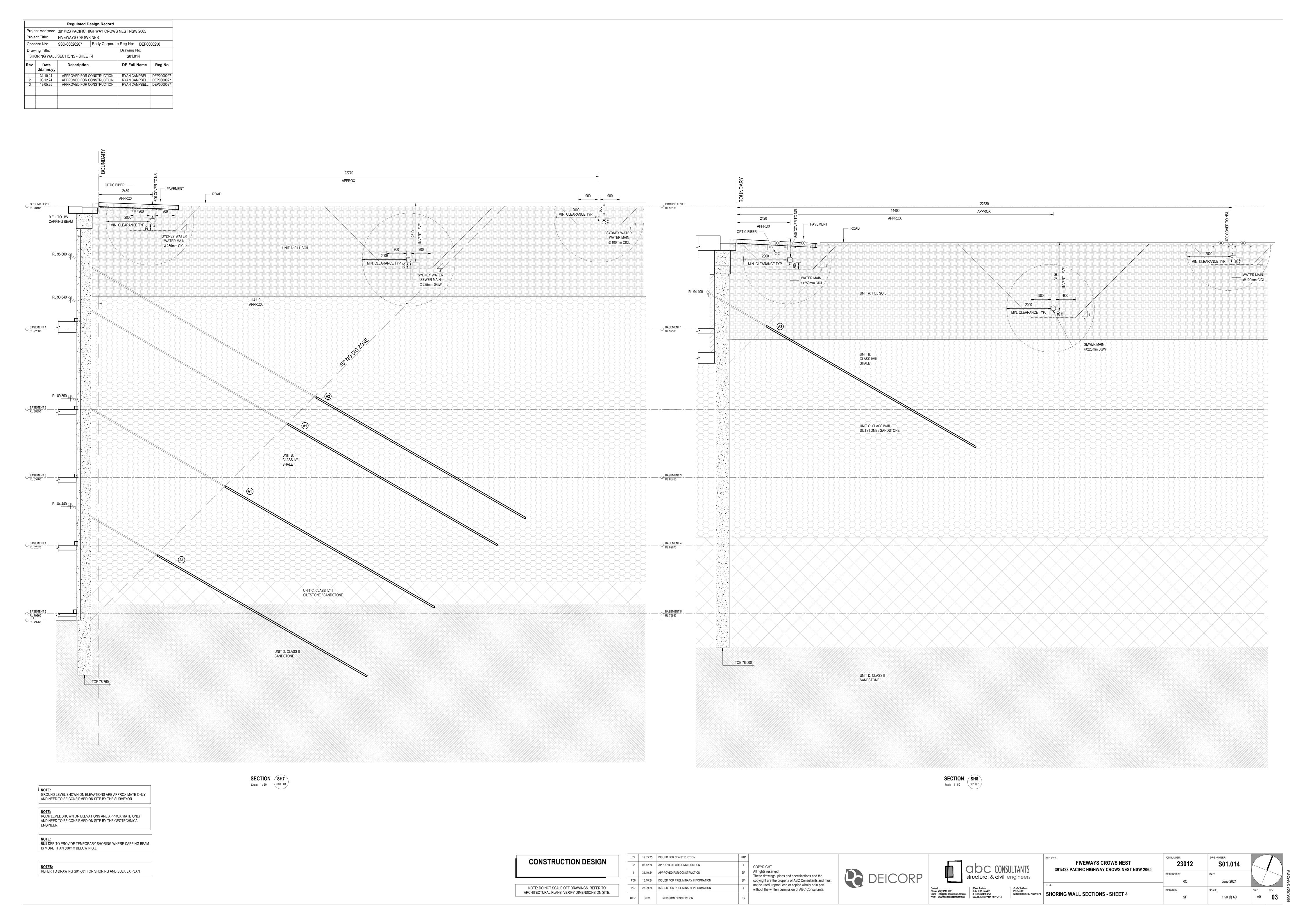
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NORTH RYDE BC NSW 1670
SHORING WALL ELEVATIONS - SHEET 1 1:100, 1:600 @ A0

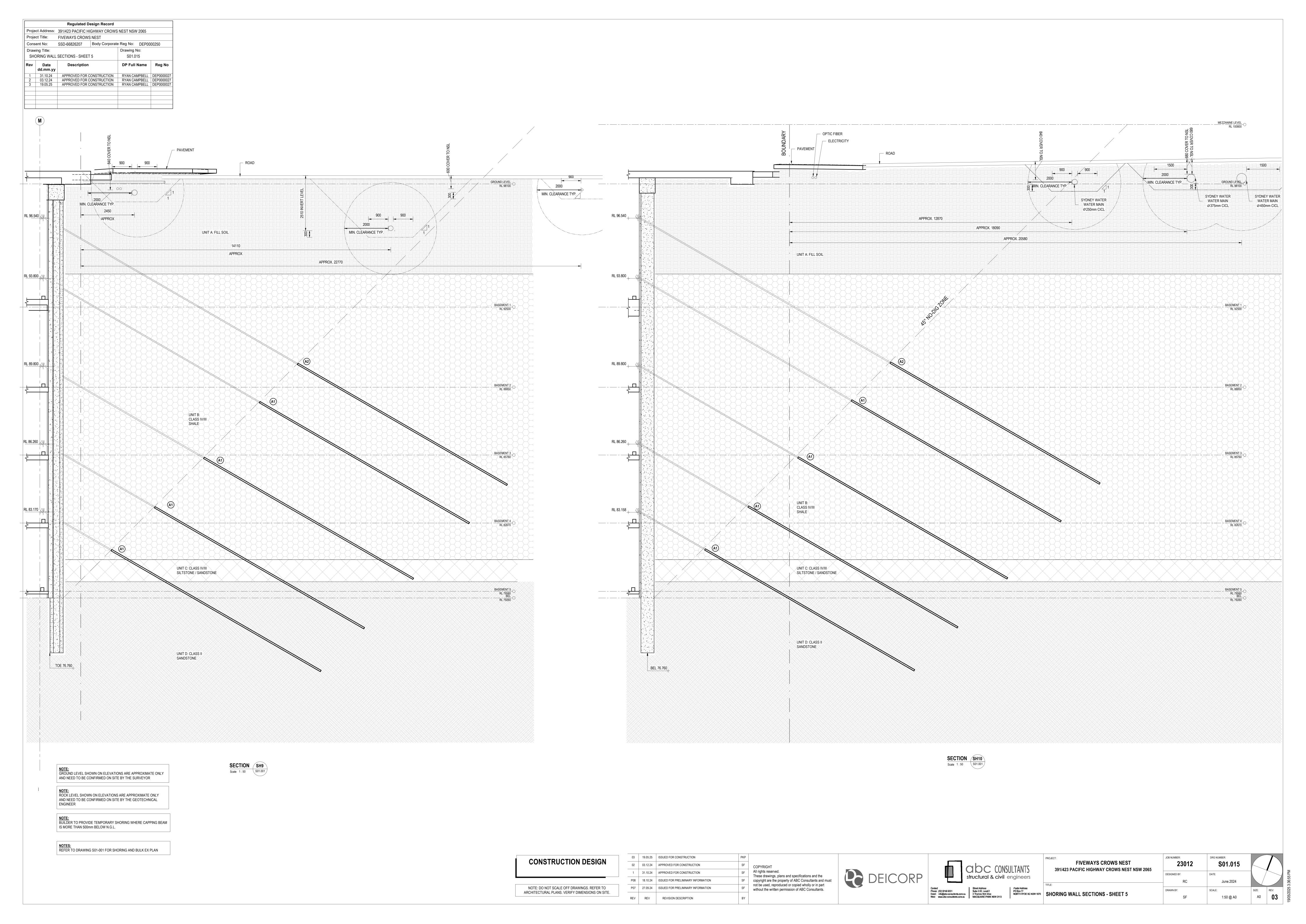


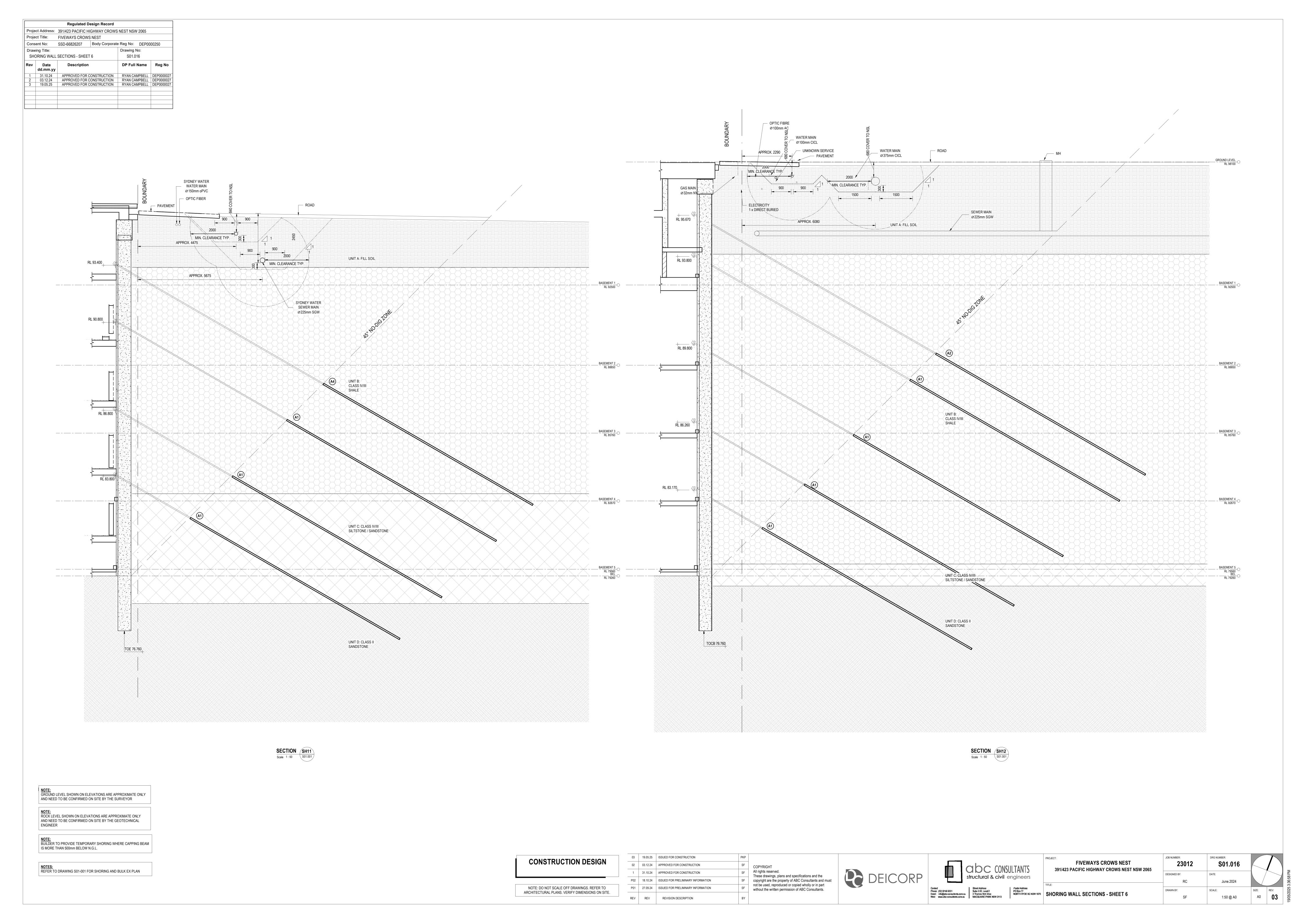


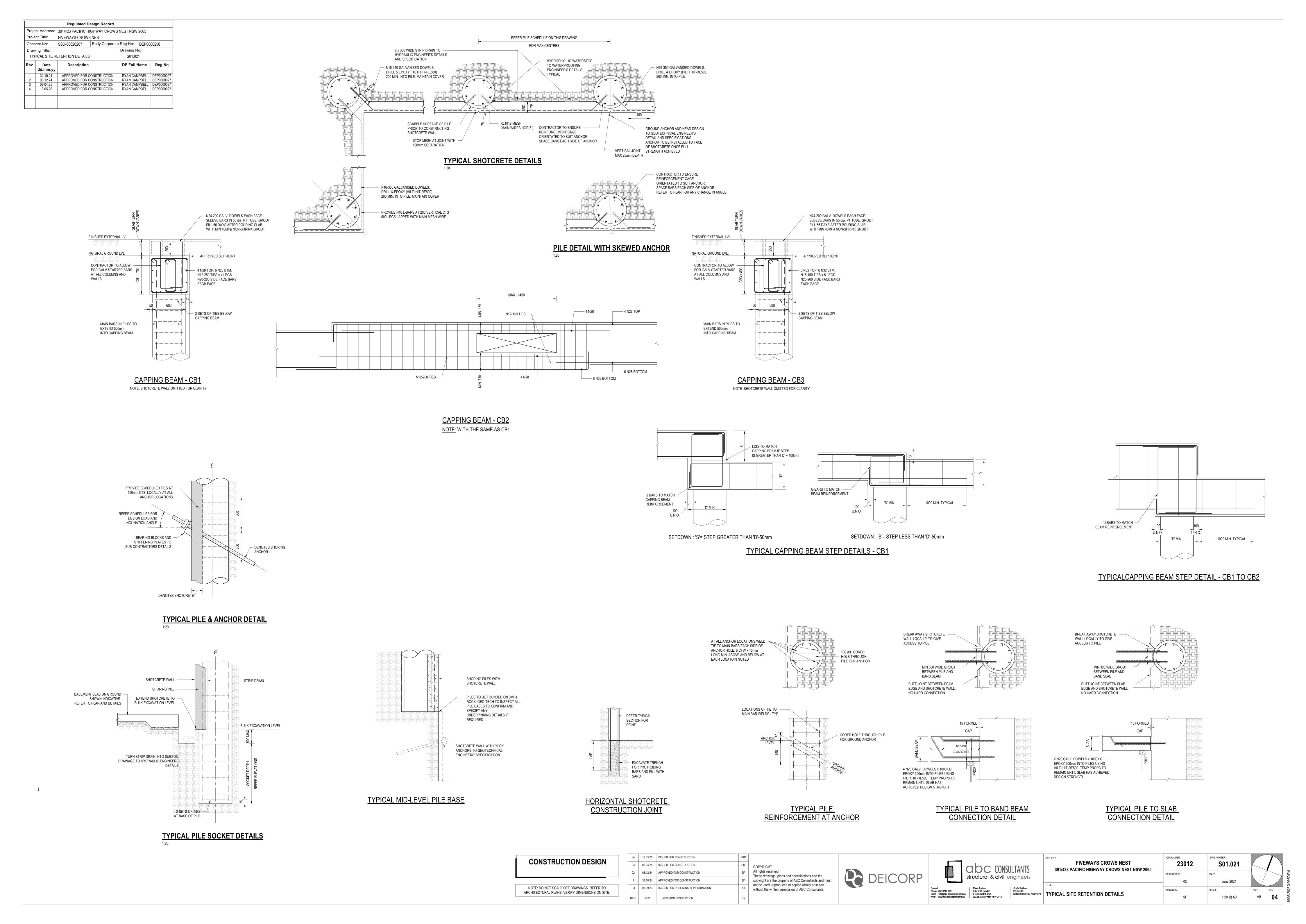


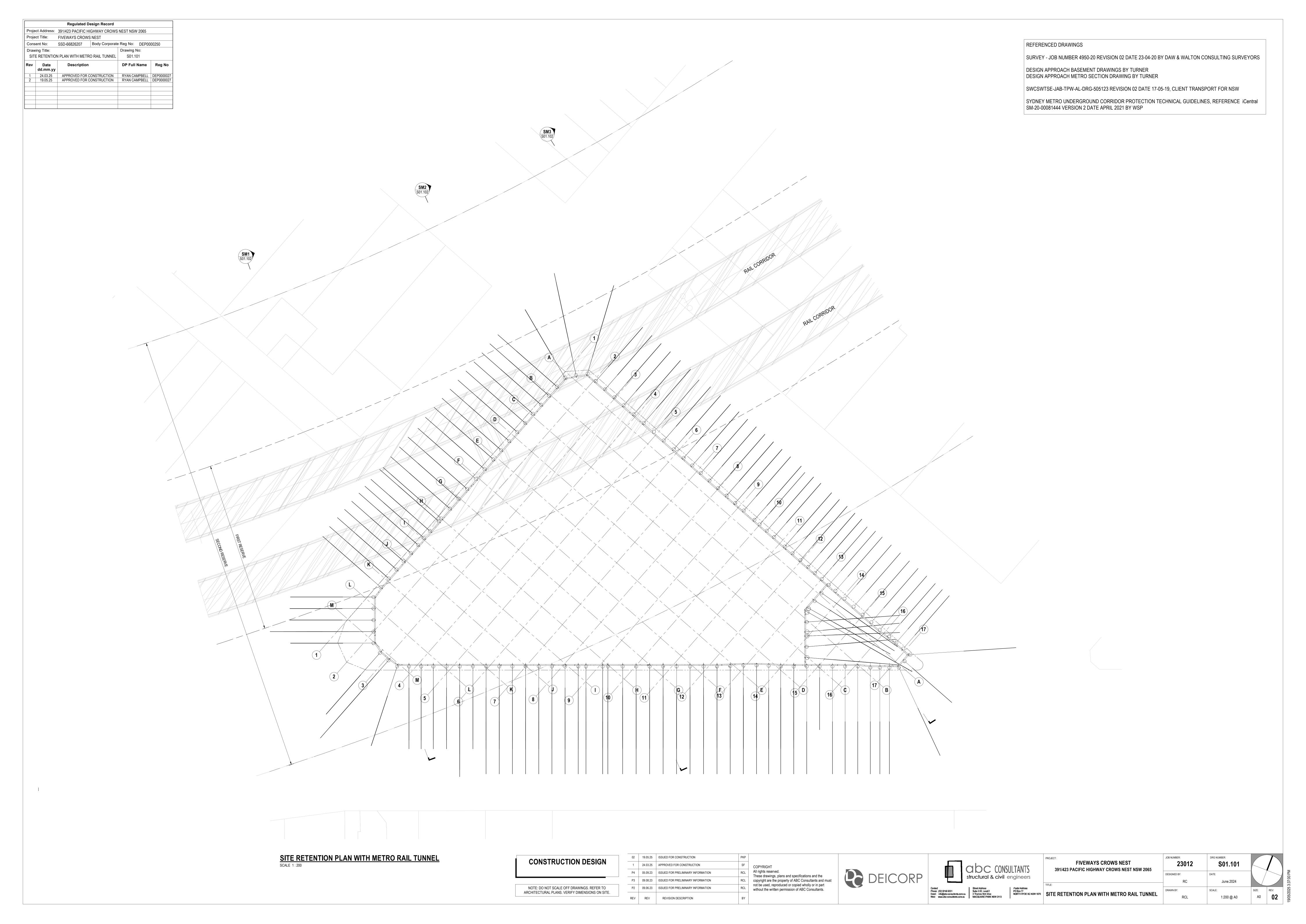




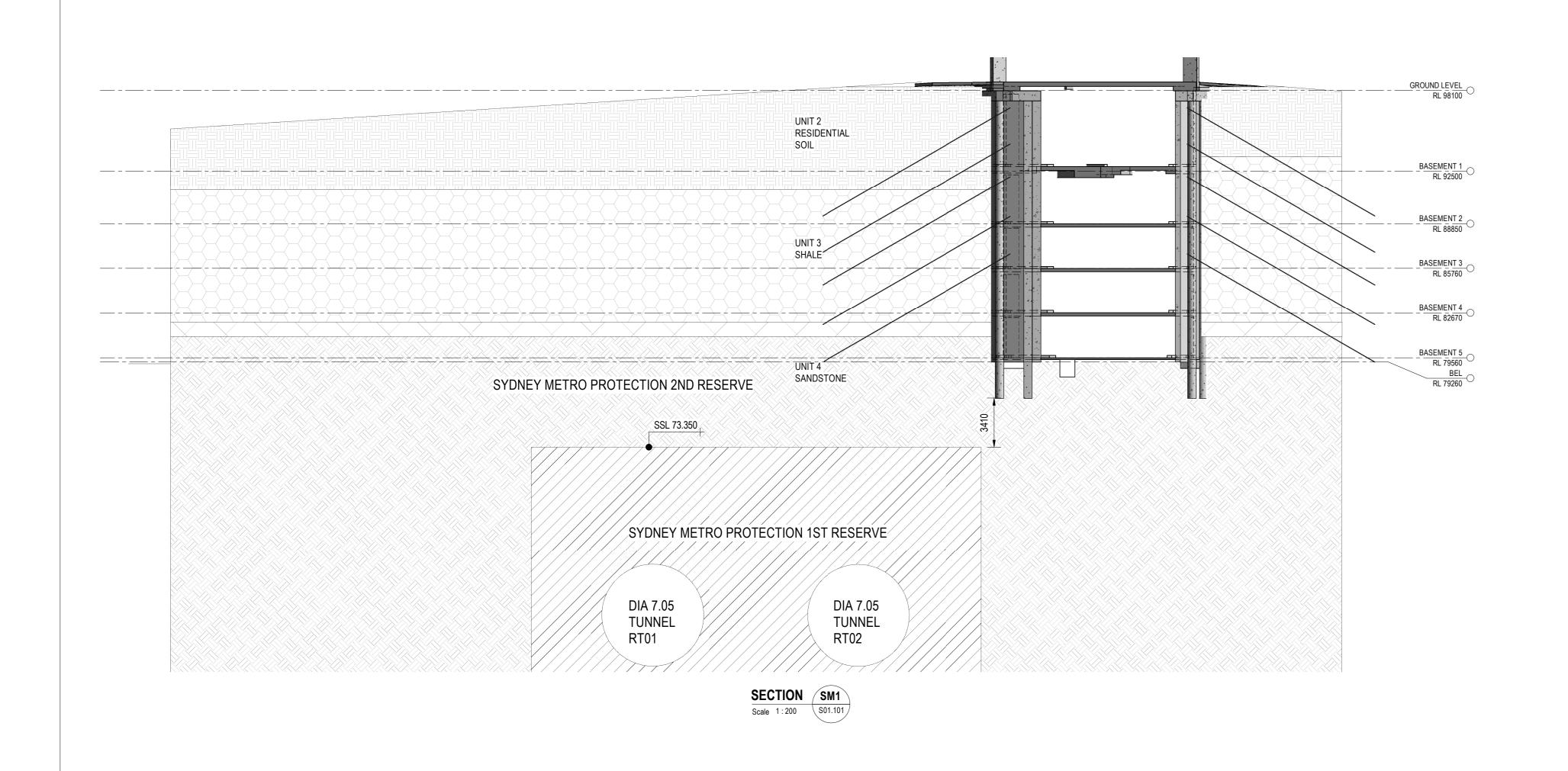


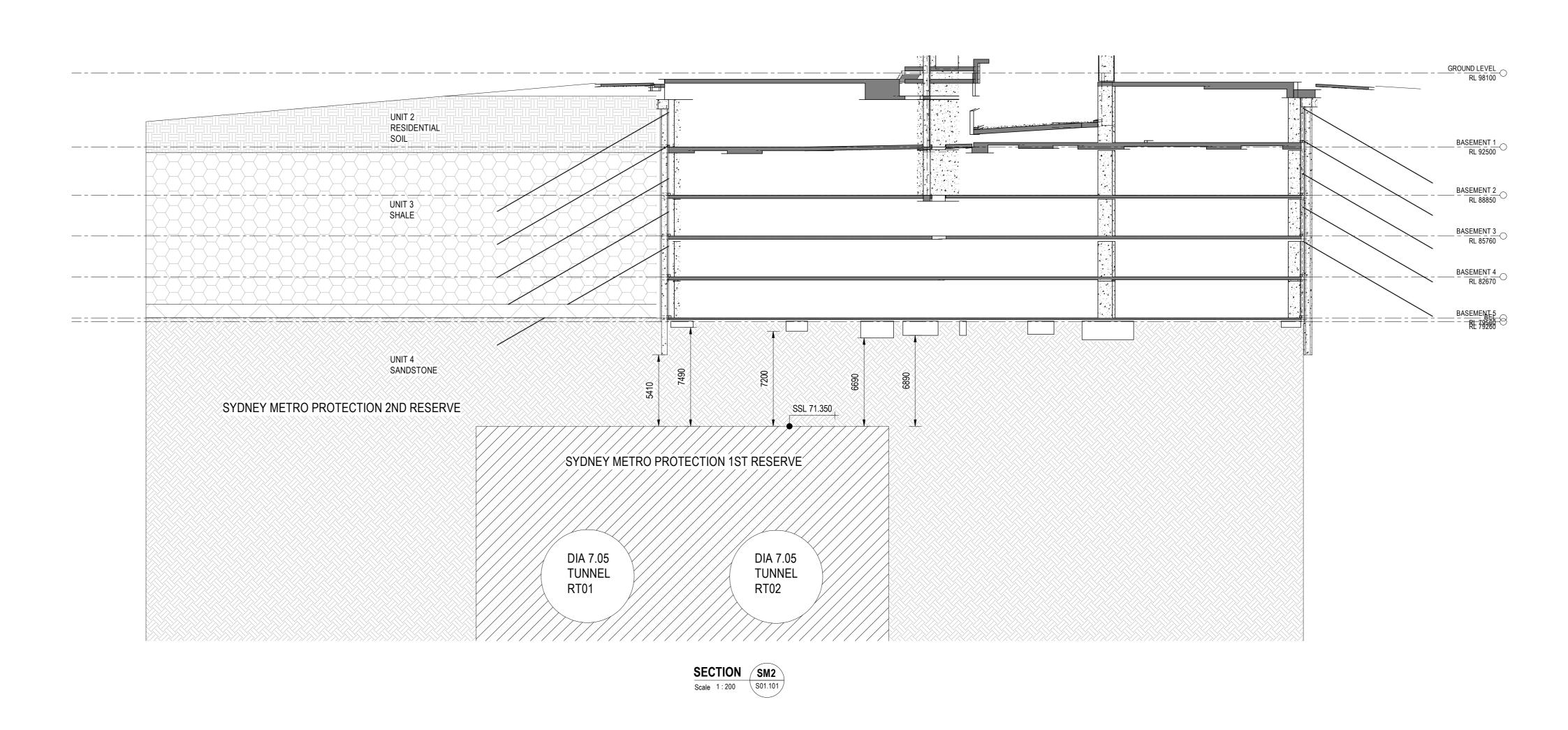


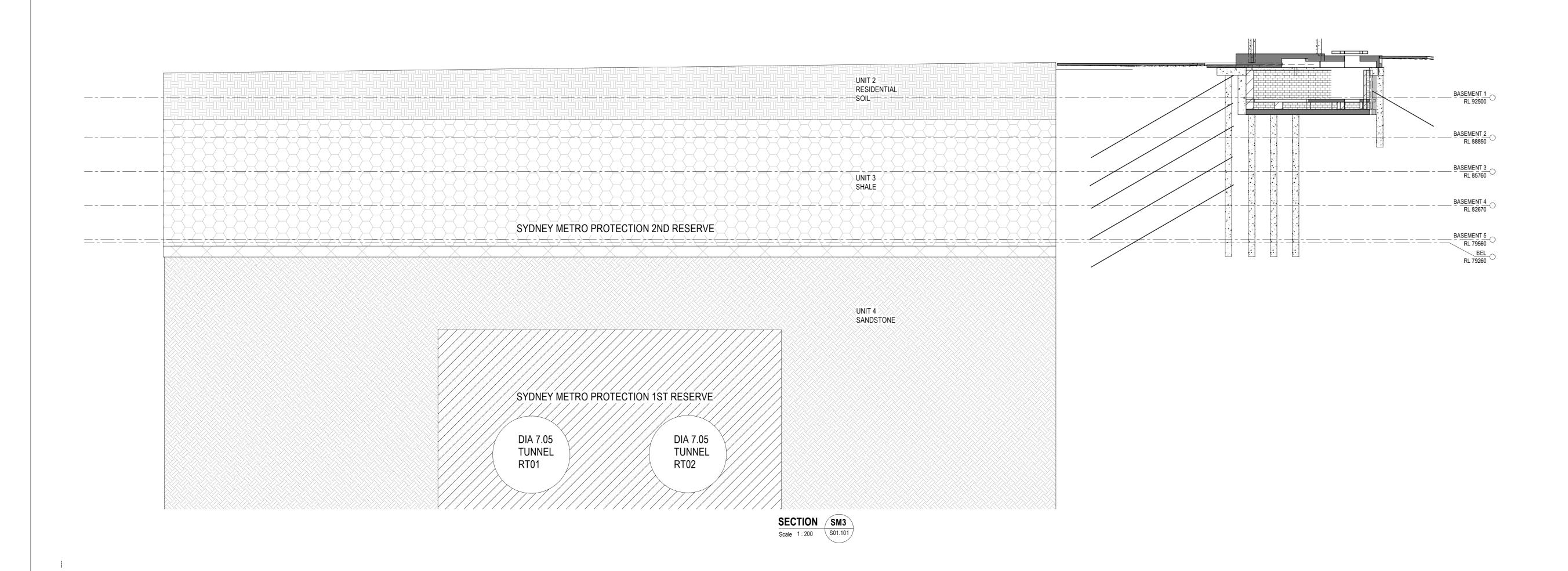




	Regulated Design Record								
Project Address:	391/423 PACIFIC HI	NEST NSW	/ 2065						
Project Title:	FIVEWAYS CROWS	VAYS CROWS NEST							
Consent No:	SSD-66826207	Body Corporate Reg No: DEP0000250							
Drawing Title:			Drawing No:						
SITE SECTIONS	WITH METRO RAIL	S01.102							
Rev Date Description dd.mm.yy			DP Full	Name	Reg No				
1 19.05.25	APPROVED FOR C	ONSTRUCTION	RYAN CAI	MPBELL	DEP0000027				







PRELIMINARY ISSUE
NOTE: DO NOT SCALE OFF DRAWINGS. REFER TO ARCHITECTURAL PLANS. VERIFY DIMENSIONS ON SITE.

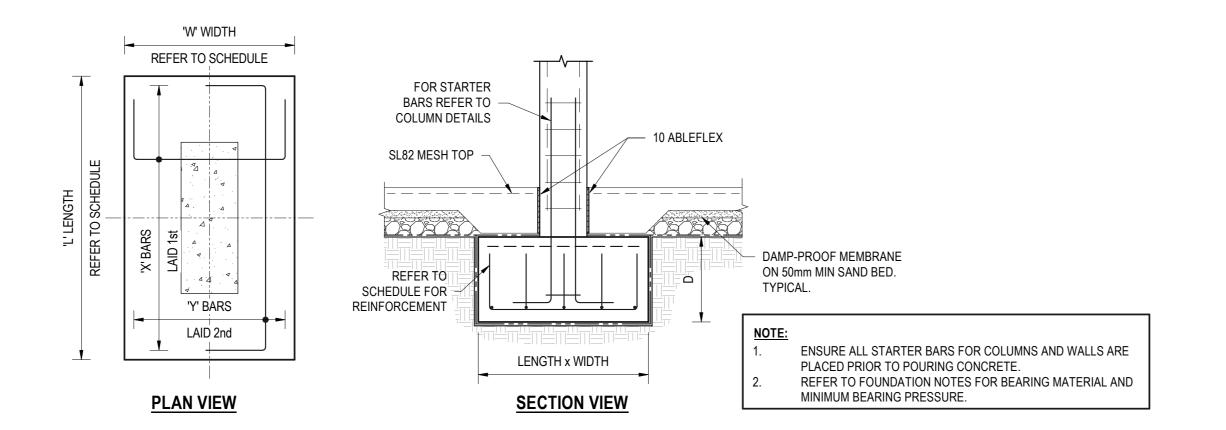
	1	19.05.25	ISSUED FOR CONSTRUCTION	PKP	
	P05	10.07.24	PRELIMINARY ISSUE	PKP	COF
	P4	05.09.23	ISSUED FOR PRELIMINARY INFORMATION	RCL	All ri Thes
	P3	09.08.23	ISSUED FOR PRELIMINARY INFORMATION	RCL	сору
-	P2	09.06.23	ISSUED FOR PRELIMINARY INFORMATION	RCL	not b with
E	REV	REV	REVISION DESCRIPTION	BY	



	abc constituctural & civil &	~ - · · · · · ·	
Contact Phone: (02) 9746 9201 Email: info@abc-consultants.com.au Web: www.abc-consultants.com.au	Street Address Suite 2.02, Level 2 3 Thomas Holt Drive MACQUARIE PARK NSW 2113	Postal Address PO Box 77 NORTH RYDE BC NSW 1670	

	PROJECT:  FIVEWAYS CROWS NEST  391/423 PACIFIC HIGHWAY CROWS NEST NSW 2065	JOB NUMBER: <b>23012</b>	DRG NUMBER: <b>\$01.102</b>			
		DESIGNED BY:	DATE:			
	TITLE:	RC	June.2024			
		DRAWN BY:	SCALE:	SIZE:	REV:	
70	SITE SECTIONS WITH METRO RAIL TUNNEL	RCL	1:200 @ A0	A0	1	

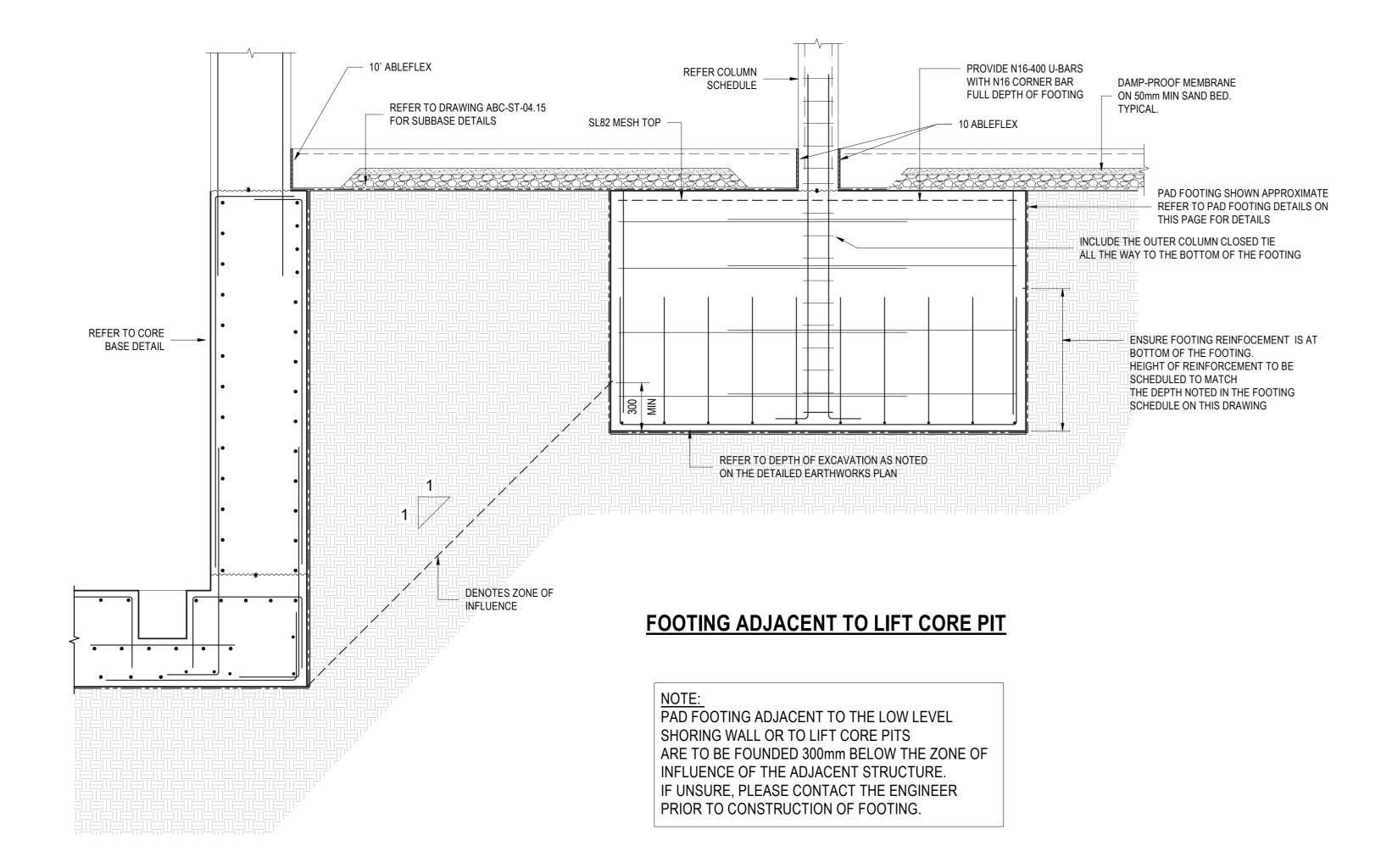


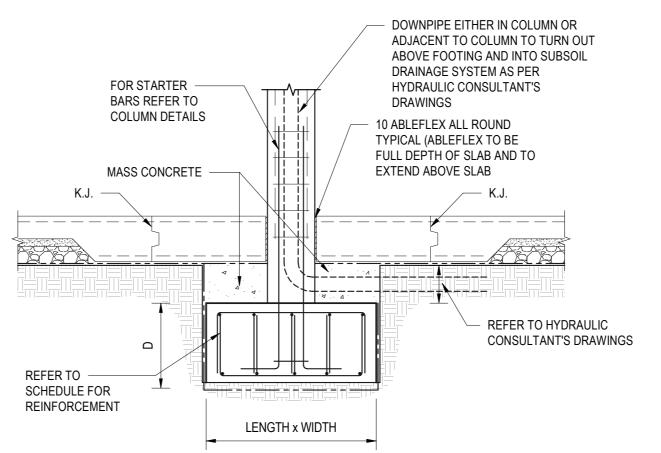


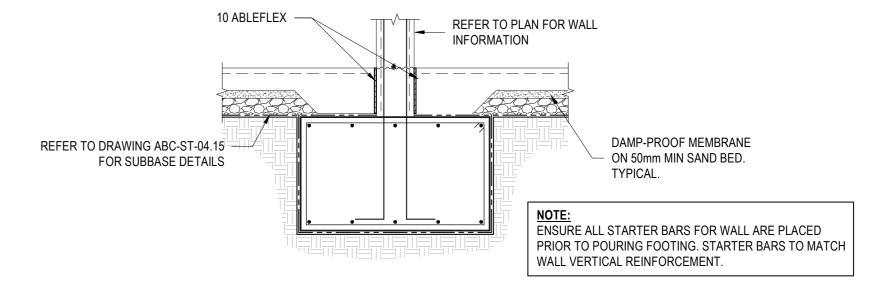
# TYPICAL COLUMN PAD FOOTING DETAIL

\* PROVIDED SPOON TESTING OF 50% OF FOOTINGS IS UNDERTAKEN AS PER GEOTECHNICAL ENGINEER'S REQUIREMENTS

PAD FOOTING SCHEDULE FOR 3000 kPa							PAD FOOTING SCHEDULE FOR 6000 kPa					
MARK	LENGTH	WIDTH	DEPTH	'X' BARS	'Y' BARS	CONCRETE STRENGTH f c	LENGTH	WIDTH	DEPTH	'X' BARS	'Y' BARS	CONCRETE STRENGTH f c
PF1	1400	800	500	N20-300	N20-300	40 MPa	1200	600	400	N20-300	N20-300	40 MPa
PF2	1800	1200	600	N20-300	N20-300	40 MPa	1500	900	600	N20-300	N20-300	40 MPa
PF3	2800	2200	1200	N24-200	N24-200	40 MPa	1800	1200	800	N24-250	N24-250	40 MPa
PF4	3000	2200	1000	N28-250	N28-250	40 MPa	2200	1600	800	N24-200	N24-200	40 MPa
PF5	2700	2500	1200	N28-250	N28-250	40 MPa	2000	1800	800	N28-200	N28-200	40 MPa
PF6	2800	2600	1400	N28-200	N28-200	40 MPa	2200	2000	1000	N28-200	N28-200	40 MPa
PF7	3200	3000	1400	N28-150	N28-150	40 MPa	2200	2000	1000	N28-150	N28-150	40 MPa
PF8	2800	2300	1000	N28-250	N28-250	40 MPa	2100	1600	800	N24-300	N24-300	40 MPa
PF9	3000	1900	1000	N28-250	N28-250	40 MPa	2400	1300	800	N28-300	N28-300	40 MPa
PF10	3500	2000	1200	N28-250	N28-250	40 MPa	2900	1400	800	N28-250	N28-250	40 MPa
PF11	3200	3200	1400	N28-150	N28-150	40 MPa	2300	2300	1000	N28-200	N28-200	40 MPa
PF12	3700	2600	1400	N28-200	N28-200	40 MPa	2900	1800	1000	N28-200	N28-200	40 MPa
PF13	3500	1800	1500	N28-150	N28-150	40 MPa	3000	1500	1500	N28-200	N28-200	40 MPa
PF14	2000	1200	1000	N28-250	N28-250	40 MPa	1800	1000	1000	N28-250	N28-250	40 MPa
PF15	5600	1000	900	N24-200	N24-200	40 MPa	5600	1000	900	N24-200	N24-200	40 MPa
PF16	5400	2500	1200	N28-250	N28-250	40 MPa	4600	1800	800	N28-200	N28-200	40 MPa







## TYPICAL PAD FOOTING SECTION VIEW WITH DOWNPIPE PRESENT

# TYPICAL STRIP FOOTING 'SF1' DETAIL SCALE 1: 20

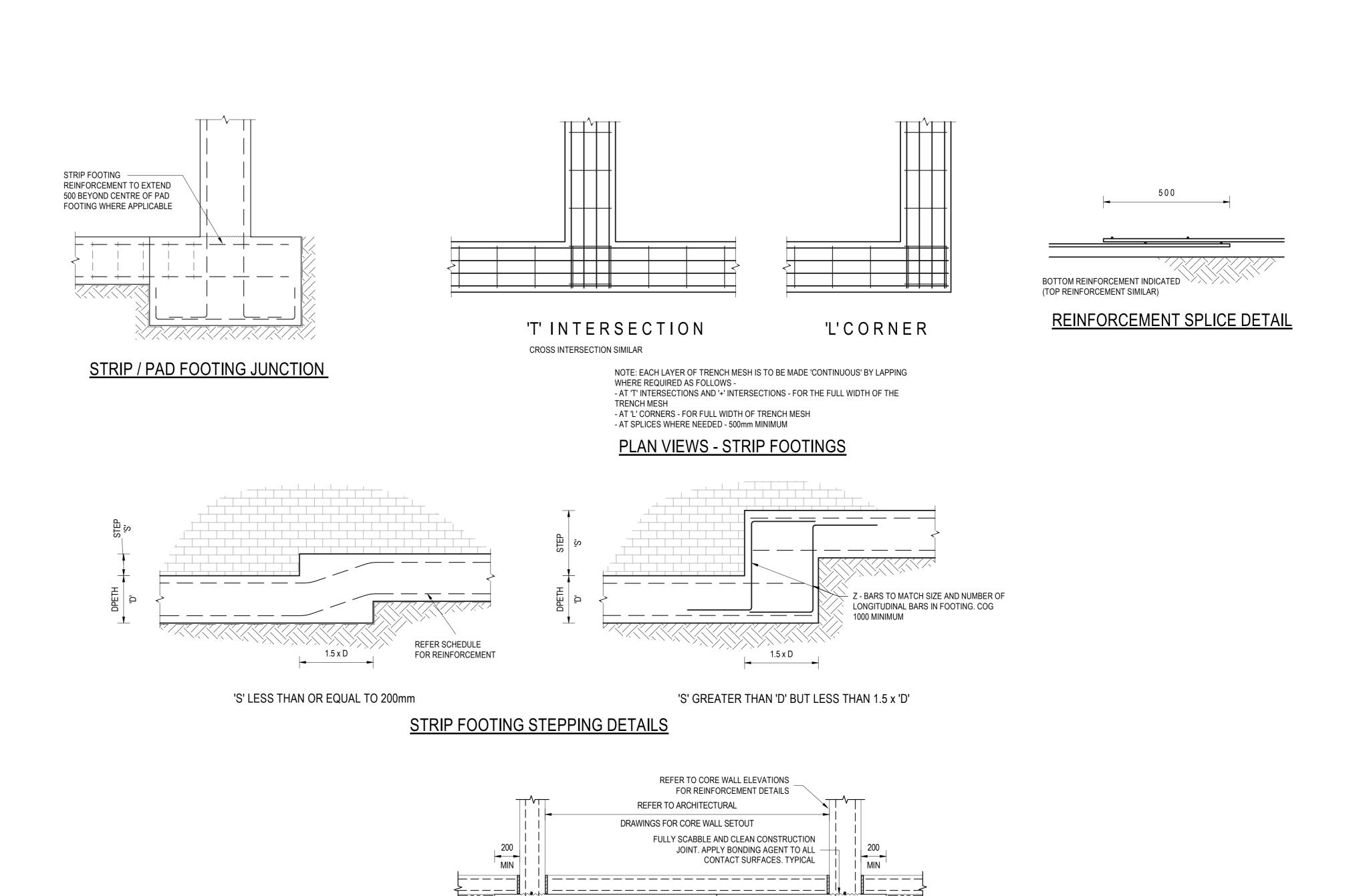
DAMP-PROOF MEMBRANE

ON 50mm MIN SAND BED.

FILL VOIDS WITH CEMENT STABILIZED SAND, USE NO FINES CONCRETE, ENSURE NO VOIDS fc' =

TYPICAL.

STRIP FOOTING SCHEDULEMARKWIDTHDEPTHTOP&BTM REOTIESSF1140012007N20 TOP & BTMN16-200 TIES



NOTE:

1. ENSURE ALL STARTER BARS FOR WALLS ARE PLACED PRIOR TO POURING CONCRETE.

2. REFER TO FOUNDATION NOTES FOR BEARING MATERIAL AND MINIMUM BEARING PRESSURE.

TYPICAL STAIR BASE DETAIL

PRELIMINARY ISSUE

NOTE: DO NOT SCALE OFF DRAWINGS. REFER TO

ARCHITECTURAL PLANS. VERIFY DIMENSIONS ON SITE.

 P5
 19.05.25
 ISSUED FOR PRELIMINARY INFORMATION

 P4
 07.03.25
 ISSUED FOR PRELIMINARY INFORMATION

 P3
 20.12.24
 ISSUED FOR PRELIMINARY INFORMATION

 P2
 05.09.23
 ISSUED FOR PRELIMINARY INFORMATION

 P1
 22.05.23
 ISSUED FOR PRELIMINARY INFORMATION

REV DATE REVISION DESCRIPTION

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REFER TO RELEVANT CORE BASE DRAWING

FOR REINFORCEMENT DETAILS



