

Investigation Summary Report

Client	Western Sydney University	Project No.	227191.00
Project	P1 Carpark Relocation	Date	15 November 2024
Address	Western Sydney University, 171 Victoria Road, Parramatta NSW	Reference	R.001.Rev0

1. Proposed development

The P1 Carpark is to be temporarily relocated to the south and south-west, requiring the construction of two temporary carparks identified as the Western and Eastern carparks, as shown on Drawing 1, attached. The Western and Eastern carparks will contain 142 and 178 parking spaces, respectively.

Based on the earthworks cut and fill volume plans provided (Ref: Sheet No.02011, Revision TI dated 8 October 2024 by Taylor Thomson Whitting), it is understood that the cut and fill contours on the drawing denote the cut and fill depth from the natural surface to the 'design finished surface', which we take to mean the top of the wearing surface. Hence, assuming a pavement thickness of 0.5 m:

- For the Western carpark, the maximum depth of cut proposed ranges from 0.4 m at the south-western end to 2.5 m at the north-eastern end of the footprint; and
- For the Eastern carpark, the maximum depth of cut proposed ranges from 0.5 m to 1.2 m.

2. Background

Douglas previously undertook bulk sampling and laboratory CBR testing of the subgrade for the re-alignment of the western end of Fifth Street, south-west of the proposed Western carpark footprint (ca. 2012). The subgrade samples comprised natural silty clay and the CBR test results ranged from 4% to 6%. It was understood at the time the new pavement was being designed for a subgrade CBR of 2.5%.

More recently, Douglas carried out geotechnical investigations for the proposed Indigenous Centre of Excellence, within the footprint of the existing P1 Carpark (Ref: 227190.00.R.001.Rev2 dated 26 June 2024) to the north-east of the site, which also included bulk sampling and CBR testing. The subgrade samples comprised natural alluvial clay and the CBR test results ranged from 4% to 6%.



3. Site description

The overall site is located on and near the floor of a shallow valley with a south-west to northeast alignment.

The Western carpark footprint is to be an irregular-shaped area that is bound by an existing sports oval to the north-west, and by existing internal roads to the east and south-east (being Bridge Street and Fifth Street, respectively). The ground surface within the proposed Western carpark footprint is mostly gently undulating with a gentle slope falling generally to the north-west but which rises more steeply to the north-east at an 11% grade at its north-eastern end, where the site appears to form part of the southern approach embankment of a bridge over Victoria Road, further to the north. The ground surface at the proposed Western carpark footprint is generally covered by lawn with some fringing trees along its south-eastern side.

The Eastern carpark will also be an irregular-shaped area that is bound by an internal road to the north and north-west (being Fifth Street), by a footpath and tennis courts to the east and by the Graduate Research School buildings (Block ED) to the south. Surface levels fall gently to the north across this part of the site at a 6% grade. The ground surface is generally covered by lawn with some fringing trees on all sides.

The tributary Vineyard Creek flows southward some 85 m east of the site to its confluence with the Parramatta River some 430 m south of the site.

4. Published data

4.1 Geology

The Geological Survey of NSW Seamless Geology Web Map indicates that the site is located at the inferred geological boundary between Ashfield Shale and Hawkesbury Sandstone of the Triassic Period. The Geological Survey of NSW 1:100 000 Geological Series Sheet 9130 (Sydney) further indicates that Hawkesbury Sandstone underlies Ashfield Shale in the geological sequence. Ashfield Shale typically comprises black to light grey shale and laminite, while Hawkesbury Sandstone typically comprises medium - to coarse-grained quartz sandstone displaying small - to large-scale, high-angle crossbedding, with minor shale and laminite lenses.

4.2 Soil landscape

The Soil Conservation Service of NSW 1:100 000 Soil Landscape Series Sheet 9130 (Sydney) indicates that most of the site is located within the 'Blacktown' residual soil landscape unit, with the northern and western ends of the proposed Western carpark footprint located within the 'Birrong' alluvial soil landscape unit.

The Blacktown residual soil landscape unit is characterised by a topography of gently undulating rises on Wianamatta Group shales and Hawkesbury Sandstone, having broad, rounded crests and ridges with gently inclined slopes. The map notes indicate that local



relief of up to 30 m is typical, with slope grade usually less than 5% and the typical soil profile comprises:

- Shallow to moderately deep (i.e., greater than 1.0 m deep) red and brown podzolic soils on crests, upper slopes and well drained areas; and
- Deep (i.e., 1.5-3.0 m deep) yellow podzolic soils and soloths on lower slopes and in areas of poor drainage.

The Birrong alluvial soil landscape unit is characterised by a topography of level to gently undulating alluvial floodplain with broad valley flats draining the Wianamatta Group shales. The map notes indicated that local relief of up to 5 m is typical with slope grade of less than 3% and the typical soil profile comprises:

- Deep (i.e., greater than 2.5 m deep) yellow podzolic soils and yellow solodic soils on older alluvial terraces; and
- Deep solodic soils and yellow solonetzic soils on current floodplain.

5. Field work

5.1 **Methods**

The geotechnical field work was carried out over two days (14 and 15 October 2024) as part of a larger programme of field work for contamination assessment, and comprised:

- Electromagnetic scanning and ground penetrating radar survey for buried services at proposed test pit locations;
- Excavation of four test pits (TP19, TP21, TP22 and TP23) by a six-tonne excavator using a 600 mm wide bucket through soils to depths ranging from 0.6 m to 3.2 m;
- Dynamic cone penetrometer (DCP) tests at three test pit locations (being TP21 TP23) to depths ranging from 0.7 m to 1.7 m within the soil profile; and
- Discrete disturbed and bulk sampling of soil.

All test pits were backfilled with site spoil upon completion and made safe, with the surface restored using turf. The locations of the test pits are shown on Drawing 1, attached. The test pit locations and levels were determined by survey using a differential GPS receiver, typically accurate to ±0.1 m (MGA2020 Zone 56 and Australian Height Datum, AHD).

We note that although TP24 was one of the four originally nominated test locations for the geotechnical investigation, due to an encounter with a redundant buried service at shallow depth, TP19 was used instead.

5.2 **Results**

The detailed test pit logs are attached. Notes defining classification methods and terms used to describe the soils and rocks are also attached.



Based on the results of the site investigation, the ground profile within the proposed Western and Eastern carpark footprints is summarised in the following sub-sections for clarity.

5.2.1 **Proposed western carpark**

The ground profile within the proposed Western carpark footprint is summarised as follows:

- FILL apparently variably compacted and of varying composition, including silty clay, silty sand, clayey silty sand, sandy clay, silty sandy clay and clayey sandy silt, with minor proportions of building rubble (brick, tile, terracotta, plastic, concrete and timber fragments, steel pipes and rods, and trace amounts of potential asbestos-containing material and geofabric), with minor proportions of gravel-, cobble- and boulder-sized sandstone fragments in the eastern part of the footprint, to depths ranging from 0.5 m to 3.0 m, thickening to the north-east; overlying;
- **ALLUVIUM** a discontinuous stratum that underlies the fill near the north-eastern end of the footprint only, of predominantly medium to high plasticity silty clay and silty sandy clay to terminations depths ranging from 1.3 m to 3.7 m, deepening to the northeast; or
- **RESIDUAL SOIL** a discontinuous stratum that underlies the fill over most of the site, of varying composition including silty clay, silty sandy clay and sandy clay of medium to high plasticity, to termination depths ranging from 1.1 m to 2.4 m.

Bedrock was not encountered in any test pit, nor was free groundwater observed in the test pits during excavation.

5.2.2 **Proposed eastern carpark**

The ground profile within the proposed Eastern carpark footprint is summarised as follows:

- **FILL / Silty SAND** apparently moderately to well compacted, fine to medium, with trace proportions of rootlets and gravel to depths ranging from 0.2 m to 0.6 m; overlying
- **Fill / Silty Sandy CLAY** apparently moderately compacted with minor proportions of cobble- and boulder-sized sandstone fragments, inclusions of boulder-sized concrete fragments and trace proportions of gravel, rootlets and ceramic pipe fragments to depths ranging from 0.4 m to 1.1 m; overlying
- **RESIDUAL SOIL** a generally continuous stratum (absent at TP13 only) of varying composition including silty clay, silty sandy clay and sandy clay of medium to high plasticity, with minor proportions of gravel-, cobble- and boulder-sized sandstone fragments to depths ranging from 0.6 m to 1.6 m; overlying
- **SANDSTONE** of inferred low strength, at depths ranging from 0.6 m to 1.6 m with an average depth of about 1.2 m.

Free groundwater was not observed in the test pits during excavation.



6. Laboratory test results

Laboratory testing of selected soil samples was carried out by a NATA accredited laboratory following completion of the field work. The laboratory test schedule comprised:

- Four tests for moisture content to assess the current state of the subsoil profile;
- Four Atterberg limits tests for soil classification; and
- Four California bearing ratio (CBR) tests (subjected to 4-days of soaking, compacted to a target density ratio of 100% relative to Standard compaction and surcharged with 4.5 kg) for assessment of pavement subgrade design CBR.

The details and results of the laboratory testing are provided on the test reports attached. The laboratory test results are briefly summarised in Tables 1 and 2.

Table 1: Summary of Laboratory Soil Moisture and Classification Test Results

Test Location	Depth (m)	Moisture Content (%)	Plastic Limit (%)	Liquid Limit (%)	Plasticity Index (%)
TP19	0.5 – 0.7	13.6	20	40	20
TP21	0.7 – 0.9	27.8	27	61	34
TP22	0.5 – 0.7	9.6	17	23	6
TP23	0.9 – 1.1	14.0	18	40	22

Table 2: Summary of Laboratory CBR Test Results

Test Location	Depth (m)	Soil Description	FMC¹ (%)	CBR (%)	Swell (%)	SMDD ² (t/m ³)	OMC ³ (%)
TP19	0.5 – 0.7	Sandy CLAY	13.6	10	-1.54	1.78	16.5
TP21	0.7 – 0.9	Silty CLAY	27.8	4.5	2.0	1.53	26.0
TP22	0.5 – 0.7	FILL/Silty SAND	9.6	15	-0.5	1.82	15.0
TP23	0.9 – 1.1	Sandy CLAY	14.0	8	1.0	1.87	15.0

- Notes: 1. Field moisture content
 - 2. Standard maximum dry density
 - 3. Optimum moisture content
 - 4. Result considered to be a laboratory error.

7. Comments

7.1 Site preparation and earthworks

Site preparation for the purposes of trafficking of the site by construction plant and pavement construction should be carried out in accordance with the guidelines contained in AS 3798 – 2007. This includes clearing, to the minimum extent necessary for the works,



of all materials unsuitable for incorporation into the works, as well as the removal of all debris (such as buried pipes and building rubble) to sufficient depth to prevent obstruction of subsequent excavation works.

The subgrade that will be exposed at the design subgrade levels for the proposed Western carpark will mainly comprise existing fill, although residual soil will likely be exposed at the south-eastern perimeter of the footprint (in the vicinity of TP4).

The subgrade that will be exposed at the design subgrade levels for the proposed Eastern carpark will also mainly comprise existing fill, although residual soil will likely be exposed at the western end (in the vicinity of TP11) and in the north-eastern (in the vicinity of TP16, TP19 and TP20).

Due to its variable composition, including the minor proportions of oversize material and timber fragments contained therein, the existing fill is considered to be 'uncontrolled'. Uncontrolled fill presents an elevated risk of non-uniform performance under traffic loading in the medium term, due to the possible presence of voids and the voids that will form in future as the timber fragments within the fill decay over time.

The following general procedure is suggested for site preparation and engineered filling for temporary on-grade pavements at this site:

- Strip any organic topsoil and 'uncontrolled' fill down to the design subgrade level (DSL);
- Manually and / or mechanically screen (i.e., 'hen-pick') the exposed fill subgrade to remove unsuitable material such as oversize, timber and asbestos fragments;
- Tyne the exposed subgrade and adjust the subgrade to optimum moisture content (OMC);
- Compact the moisture conditioned subgrade with at least six passes of a minimum 12tonne deadweight roller, with a final test roll pass ('proof roll') accompanied by a careful visual inspection by a geotechnical engineer or senior geotechnician to ensure that any deleterious materials such as loose, wet or highly compressible soil and organic materials are identified for removal;
- Strip and remove the weak material and replace with select approved fill if excessive movement is observed under passage of the roller;
- Place fill, if required, in near horizontal layers of maximum 200 mm loose thickness. Fill should be approved, homogeneous, free of organic or other deleterious material, and have a maximum particle size of 75 mm;
- Compact each fill layer to a least 98% Standard maximum dry density ratio;
- Maintain moisture contents for fill exhibiting clay-like properties in the range 2% dry to 2% wet of optimum moisture content for Standard compaction; and
- Seal or cover any natural or compacted clay foundation soil, at or close to formation level, as soon as practicable, to reduce the opportunity for desiccation and cracking, or swelling and softening.



From a geotechnical engineering perspective, the existing fill material and natural soils are considered capable of re-use in an engineered fill, provided it is first screened to remove any deleterious and / or oversize material that may be present, then thoroughly mixed and moisture-conditioned to within $\pm 2\%$ of its optimum moisture content. An experienced geotechnical engineer should inspect and approve any stripped and stockpiled spoil material proposed for re-use in an engineered fill prior to its incorporation. With respect to the suitability of the existing fill and residual soil for incorporation in a fill from an environmental standpoint, please refer to the associated contamination report prepared by Douglas.

Level 1 inspection and testing of earthworks, as defined in Section 8 of AS 3798 – 2007 is recommended.

Due to the medium to high plasticity of the clayey soils, it is expected that rubber-tyred vehicles will have trafficability problems during and after periods of rainfall or other increases in subgrade moisture content, and in some cases tracked plant may experience some difficulty. It will be essential to keep the site well drained during construction. A granular working platform is suggested to reduce potential lost time during or following wet weather.

7.2 **Pavements**

Following site preparation in accordance with Section 7.1, the prepared surface would be expected to provide adequate support to pavements. The results of laboratory testing indicate CBR values that range between 4.5% and 15%Based on the results of previous and current laboratory testing of samples collected both close to and at the site, and Douglas' experience with subgrade materials of these types, pavement thickness design should be based on a design subgrade CBR of 3%.

8. Limitations

Douglas Partners Pty Ltd (Douglas) has prepared this report for this project at Western Sydney University, 171 Victoria Road, Parramatta NSW, in line with Douglas' proposal dated 3 October 2024 and acceptance received from Stuart Pullens of Western Sydney University dated 4 October 2024. The work was carried out under Douglas' Engagement Terms. This report is provided for the exclusive use of Western Sydney University for this project only and for the purposes as described in the report. It should not be used by or be relied upon for other projects or purposes on the same or another site or by a third party. Any party so relying upon this report beyond its exclusive use and purpose as stated above, and without the express written consent of Douglas, does so entirely at its own risk and without recourse to Douglas for any loss or damage. In preparing this report Douglas has necessarily relied upon information provided by the client and / or their agents.

The results provided in the report are indicative of the sub-surface conditions on the site only at the specific sampling and/or testing locations, and then only to the depths investigated and at the time the work was carried out. Sub-surface conditions can change



abruptly due to variable geological processes and as a result of human influences. Such changes may occur after Douglas' field testing has been completed.

Douglas' advice is based upon the conditions encountered during this investigation. The accuracy of the advice provided by Douglas in this report may be affected by undetected variations in ground conditions across the site between and beyond the sampling and / or testing locations. The advice may also be limited by budget constraints imposed by others or by site accessibility.

The assessment of atypical safety hazards arising from this advice is restricted to the geotechnical components set out in this report and based on known project conditions and stated design advice and assumptions. While some recommendations for safe controls may be provided, detailed 'safety in design' assessment is outside the current scope of this report and requires additional project data and assessment.

This report must be read in conjunction with all the attached notes and should be kept in its entirety without separation of individual pages or sections. Douglas cannot be held responsible for interpretations or conclusions made by others unless they are supported by an expressed statement, interpretation, outcome or conclusion stated in this report.

This report, or sections from this report, should not be used as part of a specification for a project, without review and agreement by Douglas. This is because this report has been written as advice and opinion rather than instructions for construction.

Douglas Partners Pty Ltd

Atha Kapitanof

Associate / Geotechnical Engineer

Reviewed by

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Attachments: About this Report

Drawing 1 – Test Location Plan

Borehole Logs and Explanatory Notes

Laboratory Test Reports

About this Report



October 2024

Introduction

These notes have been provided to amplify Douglas' report in regard to classification methods, field procedures and the comments section. Not all are necessarily relevant to all reports.

Douglas' reports are based on information gained from limited subsurface excavations and sampling, supplemented by knowledge of local geology and experience. For this reason, they must be regarded as interpretive rather than factual documents, limited to some extent by the scope of information on which they rely.

Copyright

This report is the property of Douglas Partners Pty Ltd. The report may only be used for the purpose for which it was commissioned and in accordance with the Engagement Terms for the commission supplied at the time of proposal. Unauthorised use of this report in any form whatsoever is prohibited.

Borehole and Test Pit Logs

The borehole and test pit logs presented in this report are an engineering and/or geological interpretation of the subsurface conditions, and their reliability will depend to some extent on frequency of sampling and the method of drilling or excavation. Ideally, continuous undisturbed sampling or core drilling will provide the most reliable assessment, but this is not always practicable or possible to justify on economic grounds. In any case the boreholes and test pits represent only a very small sample of the total subsurface profile.

Interpretation of the information and its application to design and construction should therefore take into account the spacing of boreholes or pits, the frequency of sampling, and the possibility of other than 'straight line' variations between the test locations.

Groundwater

Where groundwater levels are measured in boreholes there are several potential problems, namely:

- In low permeability soils groundwater may enter the hole very slowly or perhaps not at all during the time the hole is left open:
- A localised, perched water table may lead to an erroneous indication of the true water table;
- Water table levels will vary from time to time with seasons or recent weather

- changes. They may not be the same at the time of construction as are indicated in the report; and
- The use of water or mud as a drilling fluid will mask any groundwater inflow. Water has to be blown out of the hole and drilling mud must first be washed out of the hole if water measurements are to be made.

More reliable measurements can be made by installing standpipes which are read at intervals over several days, or perhaps weeks for low permeability soils. Piezometers, sealed in a particular stratum, may be advisable in low permeability soils or where there may be interference from a perched water table.

Reports

The report has been prepared by qualified personnel, is based on the information obtained from field and laboratory testing, and has been undertaken to current engineering standards of interpretation and analysis. Where the report has been prepared for a specific design proposal, the information and interpretation may not be relevant if the design proposal is changed. If this happens, Douglas will be pleased to review the report and the sufficiency of the investigation work.

Every care is taken with the report as it relates to interpretation of subsurface conditions, discussion of geotechnical and environmental aspects, and recommendations or suggestions for design and construction. However, Douglas cannot always anticipate or assume responsibility for:

- Unexpected variations in ground conditions. The potential for this will depend partly on borehole or pit spacing and sampling frequency;
- Changes in policy or interpretations of policy by statutory authorities; or
- The actions of contractors responding to commercial pressures.

If these occur, Douglas will be pleased to assist with investigations or advice to resolve the matter.



About this Report

Site Anomalies

In the event that conditions encountered on site during construction appear to vary from those which were expected from the information contained in the report, Douglas requests that it be immediately notified. Most problems are much more readily resolved when conditions are exposed rather than at some later stage, well after the event.

Information for Contractual Purposes

Where information obtained from this report is provided for tendering purposes, it is recommended that all information, including the written report and discussion, be made available. In circumstances where the discussion or comments section is not relevant to the contractual situation, it may be appropriate to prepare a specially edited document. Douglas would be pleased to assist in this regard and/or to make additional report copies available for contract purposes at a nominal charge.

Site Inspection

The company will always be pleased to provide engineering inspection services for geotechnical and environmental aspects of work to which this report is related. This could range from a site visit to confirm that conditions exposed are as expected, to full time engineering presence on site.

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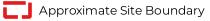


SITE LOCATION

NOTE:

- 1. Drawing projection in GDA2020 / MGA zone 56, adapted from aerial imagery from "Metromap" dated 23/07/2024,
- 2. Features shown are approximate only.

LEGEND



Environmental Test Pit

Geotechnical / Environmental



CLIENT: Western Sydney University

OFFICE: Sydney DRAWN BY: ZW

SCALE: 1:1000 @A3 DATE: 6/11/2024

TITLE: Site and Test Location Plan
Proposed Carpark P1 Relocation
Western Sydney University, Parramatta South Campus, NSW



PROJECT:	227191.00)
DRAWING No:		l
DEMICIONI:	(_

Terminology, Symbols and Abbreviations



Introduction to Terminology, Symbols and Abbreviations

Douglas Partners' reports, investigation logs, and other correspondence may use terminology which has quantitative or qualitative connotations. To remove ambiguity or uncertainty surrounding the use of such terms, the following sets of notes pages may be attached Douglas Partners' reports, depending on the work performed and conditions encountered:

- Soil Descriptions;
- Rock Descriptions; and
- Sampling, insitu testing, and drilling methodologies

In addition to these pages, the following notes generally apply to most documents.

Abbreviation Codes

Site conditions may also be presented in a number of different formats, such as investigation logs, field mapping, or as a written summary. In some of these formats textual or symbolic terminology may be presented using textual abbreviation codes or graphic symbols, and, where commonly used, these are listed alongside the terminology definition. For ease of identification in these note pages, textual codes are presented in these notes in the following style XW. Code usage conforms with the following guidelines:

- Textual codes are case insensitive, although herein they are generally presented in upper case; and
- Textual codes are contextual (i.e. the same or similar combinations of characters may be used in different contexts with different meanings (for example `PL` is used for plastic limit in the context of soil moisture condition, as well as in `PL(A)` for point load test result in the testing results column)).

Data Integrity Codes

Subsurface investigation data recorded by Douglas Partners is generally managed in a highly structured database environment, where records "span" between a top and bottom depth interval. Depth interval "gaps" between records are considered to introduce ambiguity, and, where appropriate, our practice guidelines may require contiguous data sets. Recording meaningful data is not always appropriate (for example assigning a "strength" to a concrete pavement) and the following codes may be used to maintain contiguity in such circumstances.

Term	Description	Abbreviation Code
Core loss	No core recovery	KL
Unknown	Information was not available to allow classification of the property. For example, when auguring in loose, saturated sand auger cuttings may not be returned.	UK
No data	Information required to allow classification of the property was not available. For example if drilling is commenced from the base of a hole predrilled by others	ND
Not Applicable	Derivation of the properties not appropriate or beyond the scope of the investigation. For example providing a description of the strength of a concrete pavement	NA

Graphic Symbols

Douglas Partners' logs contain a "graphic" column which provides a pictorial representation of the basic composition of the material. The symbols used are directly representing the material name stated in the adjacent "Description of Strata" column, and as such no specific graphic symbology legend has been provided in these notes.

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Introduction

All materials which are not considered to be "in-situ rock" are described in general accordance with the soil description model of AS 1726-2017 Part 6.1.3, and can be broken down into the following description structure:



The "classification" comprises a two character "group symbol" providing a general summary of dominant soil characteristics. The "name" summarises the particle sizes within the soil which most influence its behaviour. The detailed description presents more information about composition, condition, structure, and origin of the soil.

Classification, naming and description of soils require the relative proportion of particles of different sizes within the whole soil mixture to be considered.

Particle size designation and Behaviour Model

Solid particles within a soil are differentiated on the basis of size.

The engineering behaviour properties of a soil can subsequently be modelled to be either "fine grained" (also known as "cohesive" behaviour) or "coarse grained" ("non cohesive" behaviour), depending on the relative proportion of fine or coarse fractions in the soil mixture.

Particle Size	Particle	Behavi	our Model
Designation	Size	Behaviour	Approximate
	(mm)		Dry Mass
Boulder	>200	Excluded fro	om particle
Cobble	63 - 200	behaviour m	nodel as
		"oversize"	
Gravel ¹	2.36 - 63	Coarse	>65%
Sand ¹	0.075 - 2.36	Coarse	² 65%
Silt	0.002 - 0.075	Fine	>35%
Clay	<0.002	Title	× 5570

¹ – refer grain size subdivision descriptions below

The behaviour model boundaries defined above are not precise, and the material behaviour should be assumed from the name given to the material (which considers the particle fraction which dominates the behaviour, refer "component proportions" below), rather than strict observance of the proportions of particle sizes. For example, if a material is named a "Sandy CLAY", this is indicative that the material exhibits fine grained behaviour, even if the dry mass of coarse grained material may exceed 65%.

Component proportions

The relative proportion of the dry mass of each particle size fraction is assessed to be a "primary", "secondary", or "minor" component of the soil mixture, depending on its influence over the soil behaviour.

Component	Definition ¹	Relative P	Proportion
Proportion Designation		In Fine Grained Soil	In Coarse Grained Soil
Primary	The component (particle size designation, refer above) which dominates the engineering behaviour of the soil	The clay/silt component with the greater proportion	The sand/gravel component with the greater proportion
Secondary	Any component which is not the primary, but is significant to the engineering properties of the soil	Any component with greater than 30% proportion	Any granular component with greater than 30%; or Any fine component with greater than 12%
Minor ²	Present in the soil, but not significant to its engineering properties	All other components	All other components

¹ As defined in AS1726-2017 6.1.4.4

Composite Materials

In certain situations, a lithology description may describe more than one material, for example, collectively describing a layer of interbedded sand and clay. In such a scenario, the two materials would be described independently, with the names preceded or followed by a statement describing the arrangement by which the materials co-exist. For example, "INTERBEDDED Silty CLAY AND SAND".



² In the detailed material description, minor components are split into two further sub-categories. Refer "identification of minor components" below.

Classification

The soil classification comprises a two character group symbol. The first character identifies the primary component. The second character identifies either the grading or presence of fines in a coarse grained soil, or the plasticity in a fine grained soil. Refer AS1726-2017 6.1.6 for further clarification.

Soil Name

For most soils, the name is derived with the primary component included as the noun (in upper case), preceded by any secondary components stated in an adjective form. In this way, the soil name also describes the general composition and indicates the dominant behaviour of the material.

Component	Prominence in Soil Name
Primary	Noun (eg "CLAY")
Secondary	Adjective modifier (eg "Sandy")
Minor	No influence

¹ – for determination of component proportions, refer component proportions on previous page

For materials which cannot be disaggregated, or which are not comprised of rock or mineral fragments, the names "ORGANIC MATTER" or "ARTIFICIAL MATERIAL" may be used, in accordance with AS1726-2017 Table 14.

Commercial or colloquial names are not used for the soil name where a component derived name is possible (for example "Gravelly SAND" rather than "CRACKER DUST").

Materials of "fill" or "topsoil" origin are generally assigned a name derived from the primary/secondary component (where appropriate). In log descriptions this is preceded by uppercase "FILL" or "TOPSOIL". Origin uncertainty is indicated in the description by the characters (?), with the degree of uncertainty described (using the terms "probably" or "possibly" in the origin column, or at the end of the description).

Identification of minor components

Minor components are identified in the soil description immediately following the soil name. The minor component fraction is usually preceded with a term indicating the relative proportion of the component.

Minor Component	R	elative Proportion
Proportion Term	In Fine Grained Soil	In Coarse Grained Soil
With	All fractions: 15-30%	Clay/silt: 5-12%
		sand/gravel: 15-30%
Trace	All fractions: 0-15%	Clay/silt: 0-5%
		sand/gravel: 0-15%

The terms "with" and "trace" generally apply only to gravel or fine particle fractions. Where cobbles/boulders are encountered in minor proportions (generally less than about 12%) the term "occasional" may be used. This term describes the sporadic distribution of the material within the confines of the investigation excavation only, and there may be considerable variation in proportion over a wider area which is difficult to factually characterise due to the relative size of the particles and the investigation methods.

Soil Composition

Plasticity

Descriptive	Laboratory liq	uid limit range	
Term	Silt	Clay	
Non-plastic	Not applicable	Not applicable	
materials			
Low	≤50	≤35	
plasticity			
Medium	Not applicable	>35 and ≤50	
plasticity			
High	>50	>50	
plasticity			

Note, Plasticity descriptions generally describe the plasticity behaviour of the whole of the fine grained soil, not individual fine grained fractions.

<u>Grain Size</u>

Type		Particle size (mm)
Gravel	Coarse	19 - 63
	Medium	6.7 - 19
	Fine	2.36 – 6.7
Sand	Coarse	0.6 - 2.36
	Medium	0.21 - 0.6
	Fine	0.075 - 0.21

Grading

Grading Term	Particle size (mm)
Well	A good representation of all
	particle sizes
Poorly	An excess or deficiency of
	particular sizes within the
	specified range
Uniformly	Essentially of one size
Gap	A deficiency of a particular
	size or size range within the
	total range

Note, AS1726-2017 provides terminology for additional attributes not listed here.



Soil Condition

Moisture

The moisture condition of soils is assessed relative to the plastic limit for fine grained soils, while for coarse grained soils it is assessed based on the appearance and feel of the material. The moisture condition of a material is considered to be independent of stratigraphy (although commonly these are related), and this data is presented in its own column on logs.

Applicability	Term	Tactile Assessment	Abbreviation code
Fine	Dry of plastic limit	Hard and friable or powdery	w <pl< td=""></pl<>
	Near plastic limit	Can be moulded	w=PL
	Wet of plastic limit	Water residue remains on hands when handling	w>PL
	Near liquid limit	"oozes" when agitated	w=LL
	Wet of liquid limit	"oozes"	w>LL
Coarse	Dry	Non-cohesive and free running	D
	Moist	Feels cool, darkened in colour, particles may stick together	М
	Wet	Feels cool, darkened in colour, particles may stick together, free water forms when handling	W

The abbreviation code NDF , meaning "not-assessable due to drilling fluid use" may also be used.

Note, observations relating to free ground water or drilling fluids are provided independent of soil moisture condition.

Consistency/Density/Compaction/Cementation/Extremely Weathered Material

These concepts give an indication of how the material may respond to applied forces (when considered in conjunction with other attributes of the soil). This behaviour can vary independent of the composition of the material, and on logs these are described in an independent column and are generally mutually exclusive (i.e it is inappropriate to describe both consistency and compaction at the same time). The method by which the behaviour is described depends on the behaviour model and other characteristics of the soil as follows:

- In fine grained soils, the "consistency" describes the ease with which the soil can be remoulded, and is generally correlated against the materials undrained shear strength;
- In granular materials, the relative density describes how tightly packed the particles are, and is generally correlated against the density index;
- In anthropogenically modified materials, the compaction of the material is described qualitatively;
- In cemented soils (both natural and anthropogenic), the cemented "strength" is described qualitatively, relative to the difficulty with which the material is disaggregated; and
- In soils of extremely weathered material origin, the engineering behaviour may be governed by relic rock features, and expected behaviour needs to be assessed based the overall material description.

Quantitative engineering performance of these materials may be determined by laboratory testing or estimated by correlated field tests (for example penetration or shear vane testing). In some cases, performance may be assessed by tactile or other subjective methods, in which case investigation logs will show the estimated value enclosed in round brackets, for example (VS).

Consistency (fine grained soils)

Consistency Term	Tactile Assessment	Undrained Shear Strength (kPa)	Abbreviation Code
Very soft	Extrudes between fingers when squeezed	<12	VS
Soft	Mouldable with light finger pressure	>12 - ≤25	S
Firm	Mouldable with strong finger pressure	>25 - ≤50	F
Stiff	Cannot be moulded by fingers	>50 - ≤100	St
Very stiff	Indented by thumbnail	>100 - ≤200	VSt
Hard	Indented by thumbnail with difficulty	>200	Н
Friable	Easily crumbled or broken into small pieces by hand	-	Fr

Relative Density (coarse grained soils)

Relative Density Term	Density Index	Abbreviation Code
Very loose	<15	VL
Loose	>15 - ≤35	L
Medium dense	>35 - ≤65	MD
Dense	>65 - ≤85	D
Very dense	>85	VD

Note, tactile assessment of relative density is difficult, and generally requires penetration testing, hence a tactile assessment guide is not provided.



Compaction (anthropogenically modified soil)

Compaction Term	Abbreviation Code
Well compacted	WC
Poorly compacted	PC
Moderately compacted	MC
Variably compacted	VC

Cementation (natural and anthropogenic)

Cementation Term	Abbreviation Code
Moderately cemented	MOD
Weakly cemented	WEK

Extremely Weathered Material

AS1726-2017 considers weathered material to be soil if the unconfined compressive strength is less than 0.6 MPa (i.e. less than very low strength rock). These materials may be identified as "extremely weathered material" in reports and by the abbreviation code XWM on log sheets. This identification is not correlated to any specific qualitative or quantitative behaviour, and the engineering properties of this material must therefore be assessed according to engineering principles with reference to any relic rock structure, fabric, or texture described in the description.

Soil Origin

Term	Description	Abbreviation Code
Residual	Derived from in-situ weathering of the underlying rock	RS
Extremely weathered material	Formed from in-situ weathering of geological formations. Has strength of less than 'very low' as per as1726 but retains the structure or fabric of the parent rock.	XWM
Alluvial	Deposited by streams and rivers	ALV
Fluvial	Deposited by channel fill and overbank (natural levee, crevasse splay or flood basin)	FLV
Estuarine	Deposited in coastal estuaries	EST
Marine	Deposited in a marine environment	MAR
Lacustrine	Deposited in freshwater lakes	LAC
Aeolian	Carried and deposited by wind	AEO
Colluvial	Soil and rock debris transported down slopes by gravity	COL
Slopewash	Thin layers of soil and rock debris gradually and slowly deposited by gravity and possibly water	SW
Topsoil	Mantle of surface soil, often with high levels of organic material	TOP
Fill	Any material which has been moved by man	FILL
Littoral	Deposited on the lake or seashore	LIT
Unidentifiable	Not able to be identified	UID

Cobbles and Boulders

The presence of particles considered to be "oversize" may be described using one of the following strategies:

- Oversize encountered in a minor proportion (when considered relative to the wider area) are noted in the soil description; or
- Where a significant proportion of oversize is encountered, the cobbles/boulders are described independent of the soil description, in a similar manner to composite soils (described above) but qualified with "MIXTURE OF".

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Rock Descriptions



March 2024

Rock Strength

Rock strength is defined by the unconfined compressive strength, and it refers to the strength of the rock substance and not the strength of the overall rock mass, which may be considerably weaker due to defects.

The Point Load Strength Index $I_{s(50)}$ is commonly used to provide an estimate of the rock strength and site specific correlations should be developed to allow UCS values to be determined. The point load strength test procedure is described by Australian Standard AS4133.4.1-2007. The terms used to describe rock strength are as follows:

Strength Term	Unconfined Compressive Strength (MPa)	Point Load Index ¹ I _{s(50)} MPa	Abbreviation Code
Very low	0.6 - 2	0.03 - 0.1	VL
Low	2 - 6	0.1 - 0.3	L
Medium	6 - 20	0.3 - 1.0	М
High	20 - 60	1 - 3	Н
Very high	60 - 200	3 - 10	VH
Extremely high	>200	>10	EH

 $^{^{1}}$ Rock strength classification is based on UCS. The UCS to $I_{s(50)}$ ratio varies significantly for different rock types and specific ratios may be required for each site. The point load Index ranges shown above are as suggested in AS1726 and should not be relied upon without supporting evidence.

The following abbreviation codes are used for soil layers or seams of material "within rock" but for which the equivalent UCS strength is less than 0.6 MPa.

Scenario	Abbreviation
	Code
The material encountered has an equivalent UCS strength of less than 0.6 MPa, and	SOIL
therefore is considered to be soil (as per Note 1 of Table 20 of AS 1726-2017). The	
properties of the material encountered over this interval are described in the	
"Description of Strata" and soil properties columns.	
The material encountered has an equivalent UCS strength of less than 0.6 MPa, and therefore is considered to be soil (as per Note 1 of Table 20 of AS 1726-2017). The	SEAM
prominence of the material is such that it can be considered to be a seam (as defined	
in Table 22 of AS1726-2017) and the properties of the material are described in the defect	
column.	

Degree of Weathering

The degree of weathering of rock is classified as follows:

Weathering	Description	Abbreviation
Residual Soil ¹	Material is weathered to such an extent that it has soil properties. Mass structure and material texture and fabric of original rock are no longer visible, but the soil has not been significantly transported.	RS
Extremely weathered ¹	Material is weathered to such an extent that it has soil properties. Mass structure and material texture and fabric of original rock are still visible	XW
Highly weathered	The whole of the rock material is discoloured, usually by iron staining or bleaching to the extent that the colour of the original rock is not recognisable. Rock strength is significantly changed by weathering. Some primary minerals have weathered to clay minerals. Porosity may be increased by leaching or may be decreased due to deposition of weathering products in pores.	HW
Moderately weathered	The whole of the rock material is discoloured, usually by iron staining or bleaching to the extent that the colour of the original rock is not recognisable but shows little or no change of strength from fresh rock.	MW
Slightly weathered	Rock is partially discoloured with staining or bleaching along joints but shows little or no change of strength from fresh rock.	SW
Fresh	No signs of decomposition or staining.	FR
Note: If HW ar	ote: If HW and MW cannot be differentiated use DW (see below)	
Distinctly weathered	Rock strength usually changed by weathering. The rock may be highly discoloured, usually by iron staining. Porosity may be increased by leaching or may be decreased due to deposition of weathered products in pores.	DW

¹The parent rock type, of which the residual/extremely weathered material is a derivative, will be stated in the description (where discernible).



Rock Descriptions

Degree of Alteration

The degree of alteration of the rock material (physical or chemical changes caused by hot gasses or liquids at depth) is classified as follows:

Term	Description	Abbreviation Code
Extremely altered	Material is altered to such an extent that it has soil properties. Mass structure and material texture and fabric of original rock are still visible.	XA
Highly altered	The whole of the rock material is discoloured, usually by staining or bleaching to the extent that the colour of the original rock is not recognisable. Rock strength is changed by alteration. Some primary minerals are altered to clay minerals. Porosity may be increased by leaching or may be decreased due to precipitation of secondary materials in pores.	НА
Moderately altered	The whole of the rock material is discoloured, usually by staining or bleaching to the extent that the colour of the original rock is not recognisable but shows little or no change of strength from fresh rock.	MA
Slightly altered	Rock is slightly discoloured but shows little or no change of strength from fresh rock	SA
Note: If HA and	Note: If HA and MA cannot be differentiated use DA (see below)	
Distinctly altered	Rock strength usually changed by alteration. The rock may be highly discoloured, usually by staining or bleaching. Porosity may be increased by leaching or may be decreased due to precipitation of secondary minerals in pores.	DA

Degree of Fracturing

The following descriptive classification apply to the spacing of natural occurring fractures in the rock mass. It includes bedding plane partings, joints and other defects, but excludes drilling breaks. These terms are generally not required on investigation logs where fracture spacing is presented as a histogram, and where used are presented in an unabbreviated format.

Term	Description
Fragmented	Fragments of <20 mm
Highly Fractured	Core lengths of 20-40 mm with occasional fragments
Fractured	Core lengths of 30-100 mm with occasional shorter and longer sections
Slightly Fractured	Core lengths of 300 mm or longer with occasional sections of 100-300 mm
Unbroken	Core contains very few fractures

Rock Quality Designation

The quality of the cored rock can be measured using the Rock Quality Designation (RQD) index, defined as:

RQD %=
$$\frac{\text{cumulative length of 'sound' core sections > 100 mm long}}{\text{total drilled length of section being assessed}}$$

where 'sound' rock is assessed to be rock of low strength or stronger. The RQD applies only to natural fractures. If the core is broken by drilling or handling (i.e., drilling breaks) then the broken pieces are fitted back together and are not included in the calculation of RQD.

Stratification Spacing

These terms may be used to describe the spacing of bedding partings in sedimentary rocks. Where used, these terms are generally presented in an unabbreviated format

Term	Separation of Stratification Planes
Thinly laminated	< 6 mm
Laminated	6 mm to 20 mm
Very thinly bedded	20 mm to 60 mm
Thinly bedded	60 mm to 0.2 m
Medium bedded	0.2 m to 0.6 m
Thickly bedded	0.6 m to 2 m
Very thickly	> 2 m
bedded	



Rock Descriptions

Defect Descriptions

Defect Type

Term	Abbreviation Code	
Bedding plane	В	
Cleavage	CL	
Crushed seam	CS	
Crushed zone	CZ	
Drilling break	DB	
Decomposed seam	DS	
Drill lift	DL	
Extremely Weathered seam	EW	
Fault	F	
Fracture	FC	
Fragmented	FG	
Handling break	НВ	
Infilled seam	IS	
Joint	JT	
Lamination	LAM	
Shear seam	SS	
Shear zone	SZ	
Vein	VN	
Mechanical break	MB	
Parting	Р	
Sheared Surface	S	

Rock Defect Orientation

. Cook Boroot of Cornellation				
Term	Abbreviation Code			
Horizontal	Η			
Vertical	V			
Sub-horizontal	SH			
Sub-vertical	SV			

Rock Defect Coating

Term	Abbreviation Code	
Clean	CN	
Coating	CT	
Healed	HE	
Infilled	INF	
Stained	SN	
Tight	TI	
Veneer	VNR	

Rock Defect Infill

Term	Abbreviation Code
Calcite	CA
Carbonaceous	CBS
Clay	CLAY
Iron oxide	FE
Manganese	MN
Pyrite	Py
Secondary material	MS
Silt	М
Quartz	Qz
Unidentified material	MU

Rock Defect Shape/Planarity

Term	Abbreviation Code	
Curved	CU	
Discontinuous	DIS	
Irregular	IR	
Planar	PR	
Stepped	ST	
Undulating	UN	

Rock Defect Roughness

Term	Abbreviation Code	
Polished	PO	
Rough	RF	
Smooth	SM	
Slickensided	SL	
Very rough	VR	

Defect Orientation

The inclination of defects is always measured from the perpendicular to the core axis.

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Sampling, Testing and Excavation Methodology



October 2024

Sampling and Testing

A record of samples retained, and field testing performed is usually shown on a Douglas Partners' log with samples appearing to the left of a depth scale, and selected field and laboratory testing (including results, where relevant) appearing to the right of the scale, as illustrated below:

SA	MPLE	•		TESTING	
SAMPLE REMARKS	TYPE	INTERVAL	DEPTH (m)	TEST TYPE	RESULTS AND REMARKS
	SPT		- 1.0 - -1.45	SPT	4,9,11 N=20

<u>Sampling</u>

The type or intended purpose for which a sample was taken is indicated by the following abbreviation codes.

Sample Type	Code
Auger sample	Α
Acid Sulfate sample	ASS
Bulk sample	В
Core sample	C
Disturbed sample	D
Environmental sample	ES
Driven Tube sample	DT
Gas sample	G
Piston sample	Р
Sample from SPT test	SPT
Undisturbed tube sample	U ¹
Water sample	W
Material Sample	MT
Core sample for unconfined	UCS
compressive strength testing	

¹ – numeric suffixes indicate tube diameter/width in mm

The above codes only indicate that a sample was retained, and not that testing was scheduled or performed.

Field and Laboratory Testing

A record that field and laboratory testing was performed is indicated by the following abbreviation codes.

Test Type	Code
Pocket penetrometer (kPa)	PP
Photo ionisation detector (ppm)	PID
Standard Penetration Test	SPT
x/y =x blows for y mm	
penetration	
HB = hammer bouncing	
HW = fell under weight of	
hammer	
Shear vane (kPa)	V

Unconfined compressive	UCS
strength, (MPa)	

Field and laboratory testing (continued)

Test Type	Code
Point load test, (MPa),	PLT(_)
axial (A) , diametric (D) ,	
irregular (I)	
Dynamic cone penetrometer,	DCP9/150
followed by blow count	`
penetration increment in mm	
(cone tip, generally in	
accordance with AS1289.6.3.2)	
Perth sand penetrometer,	PSP/150
followed by blow count	
penetration increment in mm	
(flat tip, generally in accordance	
with AS1289.6.3.3)	

Groundwater Observations

1	>		seepage/inflow
` '	∇		standing or observed water level
	NFGV	VO	no free groundwater observed
	OBS		observations obscured by drilling
			fluids

Drilling or Excavation Methods/Tools

The drilling/excavation methods used to perform the investigation may be shown either in a dedicated column down the left-hand edge of the log, or stated in the log footer. In some circumstances abbreviation codes may be used.

Method	Abbreviation Code
Direct Push	DP
Solid flight auger. Suffixes:	AD ¹
/T = tungsten carbide tip,	
/V = v-shaped tip	
Air Track	AT
Diatube	DT
Hand auger	HA ¹
Hand tools (unspecified)	HAND
Existing exposure	X
Hollow flight auger	HSA ¹
HQ coring	HQ3
HMLC series coring	HMLC
NMLC series coring	NMLC
NQ coring	NQ3
PQ coring	PQ3
Predrilled	PD
Push tube	PT ¹
Ripping tyne/ripper	R
Rock roller	RR ¹
Rock breaker/hydraulic	EH
hammer	
Sonic drilling	SON1
Mud/blade bucket	MB ¹
Toothed bucket	TB ¹
Vibrocore	VC ¹
Vacuum excavation	VE
Wash bore (unspecified bit	WB ¹
type)	

^{1 –} numeric suffixes indicate tool diameter/width in mm



CLIENT: Western Sydney University **PROJECT:** P1 Carpark Relocation

LOCATION: Parramatta South Campus, Parramatta NSW

SURFACE LEVEL: 9.0 AHD

COORDINATE: E:317154.3, N:6257099.4 **PROJECT No:** 227191.00 **DATUM/GRID:** MGA2020 Zone 56 **DATE:** 14/10/24

DIP/AZIMUTH: 90°/---°

LOCATION ID: TP1

DATE: 14/10/24 **SHEET:** 1 of 1

		CONDITIONS ENCOUNTERED)				SAN	1PLE				TESTING AND REMARKS
RL (m)	DЕРТН (m)	DESCRIPTION OF STRATA	GRAPHIC	ORIGIN(#)	CONSIS.(*)	MOISTURE	REMARKS	TYPE	INTERVAL	DEРТН (m)	TEST TYPE	RESULTS AND REMARKS
		FILL / Silty CLAY: dark brown; low to medium plasticity; with roots, trace igneous gravel and building rubble (tile, plastic and concrete fragments).						ES		- 0.20 -		
	-	0.60m: metal pipe, possible redundant water main		FJLL		D		ES		- 0.50 - - 0.70 -		
_8	0.90	Silty CLAY: orange-brown mottled grey; medium to high plasticity; trace ironstone gravel.	X		ND			ES		- 1.00 - - 1.20 -		
	-		× × × × × × × × × × × × × × × × × × ×	RS possibly ALV		w=PL	,	* ES		- 1.50 -		
	2 _	Test Pit discontinued at 1.80m depth. Target depth reached.	X X X X X X X X X X X X X X X X X X X							- 1.70 -		
9	1											

PLANT: 6T excavator OPERATOR: A & A Hire Service LOGGED: NW

METHOD: TB (300mm wide)

REMARKS: *Field Replicate BD1/20241014 sample taken from 1.5-1.7m



Western Sydney University CLIENT: **PROJECT:** P1 Carpark Relocation

LOCATION: Parramatta South Campus, Parramatta NSW

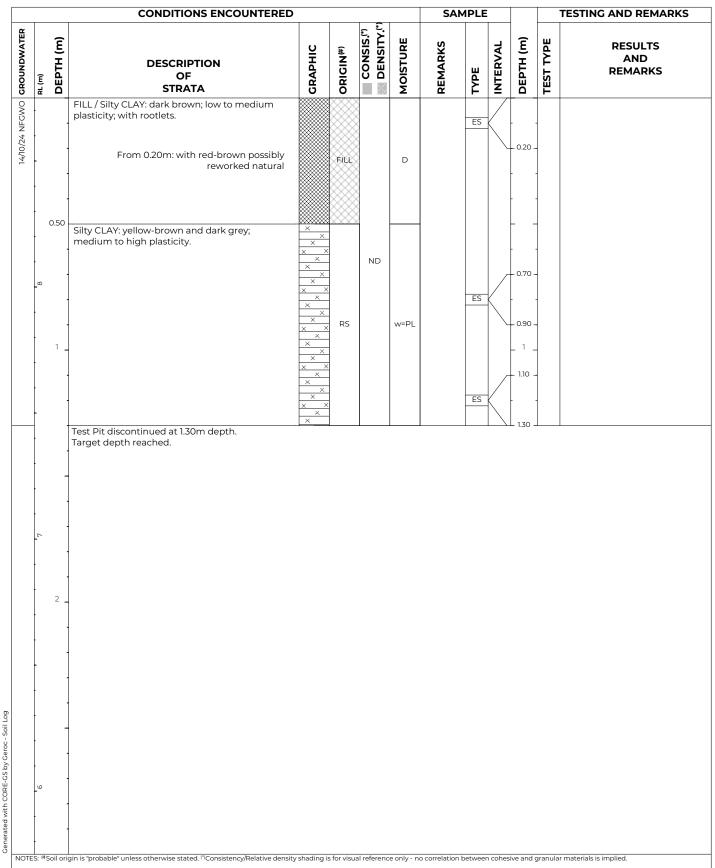
SURFACE LEVEL: 8.8 AHD

COORDINATE: E:317170.9, N:6257104.8 **PROJECT No:** 227191.00

DATUM/GRID: MGA2020 Zone 56 DIP/AZIMUTH: 90°/---°

LOCATION ID: TP2

DATE: 14/10/24 SHEET: 1 of 1



PLANT: 6T excavator

METHOD: TB (300mm wide) **REMARKS:**

OPERATOR: A & A Hire Service

LOGGED: NW



CLIENT: Western Sydney University **PROJECT:** P1 Carpark Relocation

LOCATION: Parramatta South Campus, Parramatta NSW

SURFACE LEVEL: 9.6 AHD

COORDINATE: E:317208.8, N:6257100.7 **PROJECT No:** 227191.00

DATUM/GRID: MGA2020 Zone 56 DIP/AZIMUTH: 90°/---°

LOCATION ID: TP3

DATE: 14/10/24 SHEET: 1 of 1

	F	DEPTH (m)	DESCRIPTION OF	GRAPHIC	ORIGIN(#)	CONSIS.(*) DENSITY.(*)	MOISTURE	REMARKS	TYPE	INTERVAL	DEРТН (m)	TEST TYPE	RESULTS AND REMARKS
	RL (m)		STRATA FILL / Silty CLAY: dark brown; low to medium plasticity; with rootlets.	G	Ж		Σ	2		Ż	DE	2	
	• •	-	0.30m: with igneous gravel and gravel-sized concrete fragments, trace terracotta		FILL		D		ES		- 0.20 - - - 0.40 -	-	
	_6	0.60	Silty CLAY: red-brown; medium to high plasticity; with angular to subangular	×	***	ND					- 0.60 -	_	
			plasticity; with angular to subangular ironstone gravel.	× × × × × × ×					ES		- 0.70 -		
				× × × ×	RS		w=PL				- 0.90 -	_	
		1_		X X X X							- 1.00 -	-	
_			Test Pit discontinued at 1.20m depth.	× × × ×					ES		- - 1.20 -		
			Target depth reached.										
		-											
		2 _											
	-												
		-											
	7												
ſ													

METHOD: TB (300mm wide)

REMARKS:



CLIENT: Western Sydney University **PROJECT:** P1 Carpark Relocation

LOCATION: Parramatta South Campus, Parramatta NSW

SURFACE LEVEL: 9.9 AHD

COORDINATE: E:317220.7, N:6257096.8 **PROJECT No:** 227191.00

DATUM/GRID: MGA2020 Zone 56 DIP/AZIMUTH: 90°/---°

LOCATION ID: TP4

DATE: 14/10/24 SHEET: 1 of 1

!						£ £.			MPLE				
	RL (m) DEPTH (m)		DESCRIPTION OF STRATA	GRAPHIC	ORIGIN(#)	CONSIS.(*)	MOISTURE	REMARKS	TYPE	INTERVAL	ОЕРТН (m)	TEST TYPE	RESULTS AND REMARKS
		FIL	LL / Silty SAND: brown to dark brown; fine to edium; trace rootlets, roots and gravel.		FILL		ND		ES		- 0.20 -	-	
	0.4	Silt gre me	ty CLAY: orange-brown, mottled red and ey; medium to high plasticity; with fine to edium sand, trace angular to subangular nstone gravel.	× × × × × × × × × × × × × × × × × × ×		ND			ES		- 0.50 - - 0.70 -		
	ກ]		1.00m-1.10m: boulder-sized sandstone fragments	X X X X X X X X X X X X X X X X X X X	RS		w=PL		ES		- 1.00 - - 1.10 -	-	
			st Pit discontinued at 1.10m depth. get depth reached.						•		- 1.10 -		
-													
	ω												
	ω 2												

METHOD: TB (300mm wide)

REMARKS:



CLIENT: Western Sydney University **PROJECT:** Pl Carpark Relocation

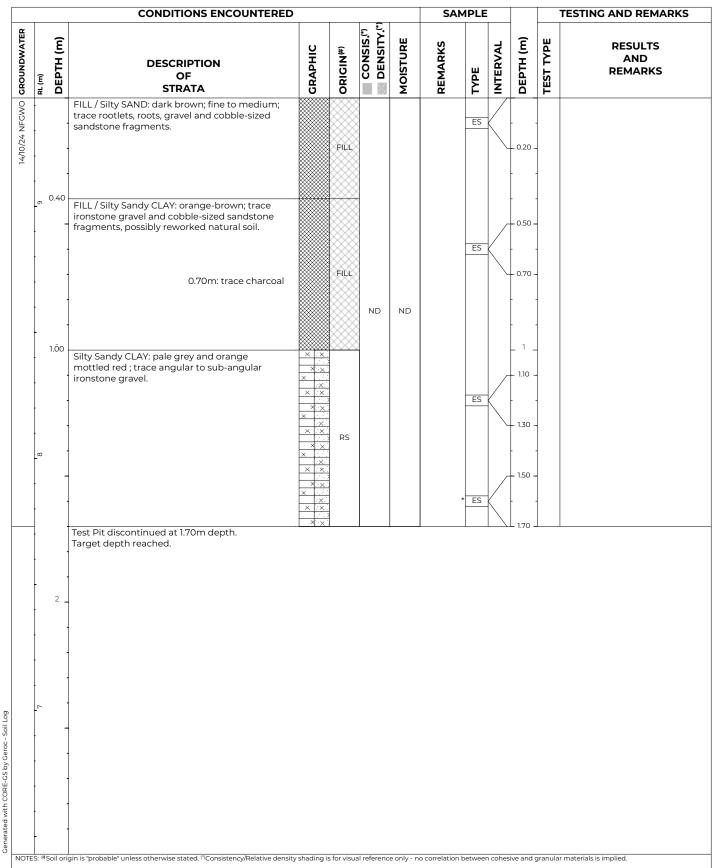
LOCATION: Parramatta South Campus, Parramatta NSW

SURFACE LEVEL: 9.4 AHD **COORDINATE:** E:317224.2, N:6257111.8

DATUM/GRID: MGA2020 Zone 56 **DIP/AZIMUTH:** 90°/---°

LOCATION ID: TP5
PROJECT No: 227191.00

DATE: 14/10/24 **SHEET:** 1 of 1



PLANT: 6T excavator OPERATOR: A & A Hire Service LOGGED: JC

METHOD: TB (300mm wide)

REMARKS: *Field Replicate BD3/20241014 sample taken from 1.5-1.7m



CLIENT: Western Sydney University **PROJECT:** P1 Carpark Relocation

LOCATION: Parramatta South Campus, Parramatta NSW

SURFACE LEVEL: 9.1 AHD

COORDINATE: E:317236.2, N:6257122.7 **PROJECT No:** 227191.00

DATUM/GRID: MGA2020 Zone 56 DIP/AZIMUTH: 90°/---°

LOCATION ID: TP6

DATE: 14/10/24 SHEET: 1 of 1

FILL / Clayey Sity SAND: brown and dark brown grading to yellow-brown with depth; fine to medium; trace gravel and rootlets. FILL / Sandy CLAY: red-orange; fine to medium sand; with cobble- and boulder-sized sandstone fragments and ironstone gravel. FILL / Sandy CLAY: red-orange; fine to medium sand; with cobble- and boulder-sized sandstone fragments and ironstone gravel. FILL / Sandy CLAY: pale grey mottled red; fine to well-with sand; with cobble- and boulder-sized sandstone fragments and ironstone gravel. FILL / ND FILL / Sandy CLAY: pale grey mottled red; fine to well-with sand; with cobble- and boulder-sized sandstone fragments and ironstone gravel. FILL / ND FILL / Sandy CLAY: pale grey mottled red; fine to well-with sand; with cobble-with sand; with sand	FILL / Clayey Silty SAND: brown and dark brown grading to yellow-brown with depth; fine to medium; trace gravel and rootlets. FILL / Sandy CLAY: red-orange; fine to medium sand; with cobble- and boulder-sized sandstone fragments and ironstone gravel. Silty Sandy CLAY: pale grey mottled red; fine to medium sand. Silty Sandy CLAY: pale grey mottled red; fine to medium sand. Silty Sandy CLAY: pale grey mottled red; fine to medium sand. Silty Sandy CLAY: pale grey mottled red; fine to medium sand. Silty Sandy CLAY: pale grey mottled red; fine to medium sand.	Т			CONDITIONS ENCOUNTERED	· 		٠	€.		SAN	/PLE				TESTING AND REMARKS
FILL / Clayey Silty SAND: brown and dark brown grading to yellow-brown with depth; fine to medium; trace gravel and rootlets. FILL / Sandy CLAY: red-orange; fine to medium sand; with cobble- and boulder-sized sandstone fragments and ironstone gravel. FILL Sandy CLAY: red-orange; fine to medium sand; with cobble- and boulder-sized sandstone fragments and ironstone gravel. FILL ND W=PL 1 1 1 1 1 1 1 1 1	FILL / Clayer, Silty SAND: brown and dark brown grading to yellow-brown with depth; fine to medium; trace gravel and rootlets. FILL / Sandy CLAY: red-orange: fine to medium sand; with cobble- and boulder-sized sandstone fragments and ironstone gravel. FILL / Sandy CLAY: red-orange: fine to medium sand; with cobble- and boulder-sized sandstone fragments and ironstone gravel. FILL / Sandy CLAY: pale grey mottled red; fine to well well well and boulder-sized sandstone fragments and ironstone gravel. FILL / Sandy CLAY: pale grey mottled red; fine to well well well well well well well wel	1	RL (m)	DEPTH (m)	OF	GRAPHIC	ORIGIN#)	CONSIS.(*)	DENSITY.(*)	MOISTURE	REMARKS	TYPE	INTERVAL	DЕРТН (m)	TEST TYPE	AND
FILL / Sandy CLAY: red-orange; fine to medium sand; with cobble- and boulder-sized sandstone fragments and ironstone gravel. ND FILL ND FILL ND Silty Sandy CLAY: pale grey mottled red; fine to medium sand. Silty Sandy CLAY: pale grey mottled red; fine to medium sand. Test Pit discontinued at 1.60m depth.	FILL / Sandy CLAY: red-orange; fine to medium sand, with cobbie- and boulder-sized sandstone fragments and ironstone gravel. 120 Silty Sandy CLAY: pale grey mottled red; fine to medium sand.		n		brown grading to yellow-brown with depth;		FILL			ND				-	-	
Silty Sandy CLAY: pale grey mottled red; fine to medium sand. X	Silty Sandy CLAY: pale grey mottled red; fine to medium sand. Silty Sandy CLAY: pale grey mottled red; fine to medium sand. Silty Sandy Clay: Silty Sandy Clay:		ω	- - - -	sand; with cobble- and boulder-sized		FILL	×	ND	w=PL		ES		- 0.70 - -		
				1.20	medium sand. Test Pit discontinued at 1.60m depth.	× × × × × × × × × × × × × × × × × ×	possibly RS	y				ES		-		
			(th C		gin is "probable" unless otherwise stated. (" Consistency/Relative densit	v shoulter	s for the	2-1-1-		a anh:	parrol-+:-	o o tu		h (a = = -1)	arar d	v gostarials is impalied

PLANT: 6T excavator METHOD: TB (300mm wide)

REMARKS:



CLIENT: Western Sydney University **PROJECT:** P1 Carpark Relocation

LOCATION: Parramatta South Campus, Parramatta NSW

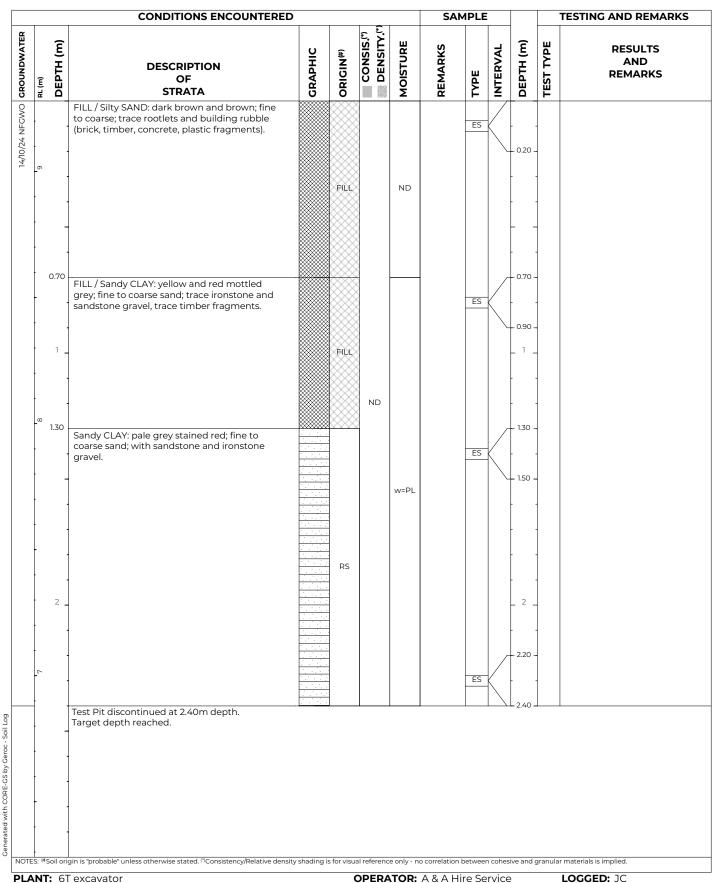
SURFACE LEVEL: 9.3 AHD

COORDINATE: E:317247.5, N:6257136.5

DATUM/GRID: MGA2020 Zone 56 DIP/AZIMUTH: 90°/---°

LOCATION ID: TP7 PROJECT No: 227191.00

DATE: 14/10/24 SHEET: 1 of 1



PLANT: 6T excavator

METHOD: TB (600mm wide)

REMARKS:



CLIENT: Western Sydney University **PROJECT:** P1 Carpark Relocation

LOCATION: Parramatta South Campus, Parramatta NSW

SURFACE LEVEL: 10.3 AHD

DATUM/GRID: MGA2020 Zone 56

DIP/AZIMUTH: 90°/---°

LOCATION ID: TP8 COORDINATE: E:317263.5, N:6257142.5 **PROJECT No:** 227191.00

> **DATE:** 15/10/24 SHEET: 1 of 1

	CONDITIONS ENCOUNTERED			٠		SAM	1PLE				TESTING AND REMARKS
RL (m) DEPTH (m)	DESCRIPTION OF STRATA	GRAPHIC	ORIGIN(#)	CONSIS.(*)	MOISTURE	REMARKS	TYPE	INTERVAL	DEРТН (m)	TEST TYPE	RESULTS AND REMARKS
0	FILL / Silty SAND: brown and dark brown; with gravel, trace building rubble (brick, plastic, concrete and potential asbestos-containing material fragments).						ES		- 0.20 -		
			PILL		М		ES		- 0.50 - - 0.70 -		
. 1.ÕO	FILL / Silty Sandy CLAY: grey brown and brown; with gravel, cobble and boulder-sized fragments of concrete, sandstone and igneous rock. 1.20m: geofabric with fine to coarse sand			ND			ES		- 1 - 1.10		
	1.60m: dark brown-grey		PILL		ND		ES		1.70 -		
1.90 2	FILL / Silty SAND: dark brown to dark grey; trace building rubble (brick, concrete and plastic fragments).		FILL		М		ES		- 1.90 - - 2.00 - 		
2.30	Silty Sandy CLAY: yellow-grey and grey-brown.	X X X X X X X X X X X X X X X X X X X	ALV		ND		ES		- 2.40 -		
_	Test Pit discontinued at 2.60m depth. Target depth reached.	.l·x. ··x	1			<u> </u>			- 2.60 -		

PLANT: 6T excavator METHOD: TB (600mm wide)

REMARKS:



CLIENT: Western Sydney University **PROJECT:** P1 Carpark Relocation

LOCATION: Parramatta South Campus, Parramatta NSW

SURFACE LEVEL: 10.3 AHD

COORDINATE: E:317247.8, N:6257164.7 **PROJECT No:** 227191.00

DATUM/GRID: MGA2020 Zone 56 **DIP/AZIMUTH:** 90°/---°

LOCATION ID: TP9

DATE: 14/10/24 **SHEET:** 1 of 2

							-	1. 30 /					SHEET: 1012
		CONDITIONS ENCOUNTERED			T_	£		SAN	/PLE				TESTING AND REMARKS
RL (m)	DEPTH (m)	DESCRIPTION OF STRATA	GRAPHIC	ORIGIN(#)	CONSIS.(*)	DENSITY.(*)	MOISTURE	REMARKS	TYPE	INTERVAL	DЕРТН (m)	TEST TYPE	RESULTS AND REMARKS
	0.20	FILL / Silty SAND: dark brown and brown; fine to medium; with clay and ironstone gravel, with cobble and boulder-sized fragments of sandstone, trace building rubble (brick and PVC pipe). FILL / Silty Sandy CLAY: brown; trace sandstone gravel and building rubble (brick and timber fragments).		FILL					ES		- 0.20 - - 0.50 - - 0.70 -		
	1 _			FILL					ES		- 0.90 - - 1 - - 1.10 -		
	1.60	FILL / Clayey Sandy SILT: dark brown; low plasticity; fine sand; trace sandstone gravel and building rubble (timber and brick fragments).							ES		- 1.50 - - 1.60 - - 1.80 - - 2.00 -		
	-			FILL									
OTES: (#S	Sail orig	gin is "probable" unless otherwise stated. ("Consistency/Relative density	shading in	s for vien	al ref	erenco	only - no	correlation	ES	coher	ve and	granula	ur materials is implied

PLANT: 6T excavator
METHOD: TB (300mm wide)

REMARKS:



CLIENT: Western Sydney University **PROJECT:** P1 Carpark Relocation

LOCATION: Parramatta South Campus, Parramatta NSW

SURFACE LEVEL: 10.3 AHD

DATUM/GRID: MGA2020 Zone 56

DIP/AZIMUTH: 90°/---°

LOCATION ID: TP9 COORDINATE: E:317247.8, N:6257164.7 **PROJECT No:** 227191.00

> **DATE:** 14/10/24 **SHEET:** 2 of 2

Y			CONDITIONS ENCOUNTERED			£ £,		5, 11	MPLE				TESTING AND REMARKS
GROONDWAIER		DEPTH (m)	DESCRIPTION OF STRATA	GRAPHIC	ORIGIN(#)	CONSIS.(*)	MOISTURE	REMARKS	TYPE	INTERVAL	DEPTH (m)	TEST TYPE	RESULTS AND REMARKS
	3	3.00	Silty Sandy CLAY: grey-brown and yellow- brown.	X X X X X X X X X X X X X X X X X X X						_			
				× × × × × × × × × × × × × × × × × × ×									
				XX						_	- 3.20 -		
	7	ł		×××					ES				
				X X X X X X	ALV						_ 3.40 -		
				XXX									
				× × ×									
		1		× × × ×								-	
		ł	Test Pit discontinued at 3.70m depth.	×××									
	-	ł	Target depth reached.										
		4											
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METHOD: TB (300mm wide)

REMARKS:



CLIENT: Western Sydney University **PROJECT:** P1 Carpark Relocation

LOCATION: Parramatta South Campus, Parramatta NSW

SURFACE LEVEL: 11.0 AHD **COORDINATE:** E:317264.0, N:6257166.4 **PROJECT No:** 227191.00

DATUM/GRID: MGA2020 Zone 56

DIP/AZIMUTH: 90°/---°

LOCATION ID: TP10

DATE: 15/10/24 SHEET: 1 of 1

			CONDITIONS ENGOUNTEDED					C 4 1	4D: -				TECTING AND DELLARIES
~			CONDITIONS ENCOUNTERED			_ €.		SAM	1PLE	: 			TESTING AND REMARKS
GROUNDWATER	RL (m)	DEPTH (m)	DESCRIPTION OF STRATA	GRAPHIC	ORIGIN ^(#)	CONSIS.(*)	MOISTURE	REMARKS	TYPE	INTERVAL	DEРТН (m)	TEST TYPE	RESULTS AND REMARKS
			FILL / Silty SAND: brown and dark brown; trace rootlets and igneous gravel.	_	FILL				ES		- 0.20 -		
	_	0.50	FILL / Clayey Silty SAND: brown; with sandstone gravel and building rubble (brick, concrete, plastic and timber fragments), trace rootlets .						ES		- 0.60 - - · ·		
	· <u>o</u> l ·	1 .	1.00m-1.20m: boulder-sized fragment of asphalt (possible buried pavement surface)		FILL	ND	D to M		ES		- 1 - · · · · · · · · · · · · · · · · ·		
		1.90 2 <u> </u>	FILL / Silty CLAY: dark grey and grey-brown; with boulder-sized sandstone fragments, trace rootlets, timber, gravel, and inclusions of orange-brown clay.		FILL		w=PL possibly		ES		- 1.50		
		-	2.30m: metal rod(large) Test Pit discontinued at 2.40m depth. Refusal on boulder-sized fragment .								- 2.20 -		
1OTE	S: (#)	Soil or	gin is "probable" unless otherwise stated. ("Consistency/Relative density	shading is	s for visua	al referenc	e only - n	o correlation b	oetweer	n cohes	ive and ç	granula	r materials is implied.

PLANT: 6T excavator METHOD: TB (300mm wide)

REMARKS:



CLIENT: Western Sydney University **PROJECT:** P1 Carpark Relocation

LOCATION: Parramatta South Campus, Parramatta NSW

SURFACE LEVEL: 10.5 AHD

COORDINATE: E:317276.6, N:6257108.0 **PROJECT No:** 227191.00 DATUM/GRID: MGA2020 Zone 56

DIP/AZIMUTH: 90°/---°

LOCATION ID: TP11

DATE: 15/10/24 SHEET: 1 of 1

	CONDITIONS ENCOUNTERED	D				SAN	IPLE				TESTING AND REMARKS
RL (m) DEPTH (m)	DESCRIPTION OF STRATA	GRAPHIC	ORIGIN(#)	CONSIS.(*)	MOISTURE	REMARKS	TYPE	INTERVAL	DЕРТН (m)	TEST TYPE	RESULTS AND REMARKS
0.40	FILL / Clayey Silty SAND: dark brown and brown; trace rootlets.		FILL				ES		- 0.20 -		
01	Silty Sandy CLAY: yellow-brown and orange- brown; trace gravel.	X X X X X X X X X X X X X X X X X X X	possibly ALV	ND	ND		ES		- 0.50 - - - 0.70 -		
1.00	Silty CLAY: pale grey mottled red and yellow; with ironstone and sandstone gravel, with cobble-sized sandstone fragments.	× × × × × × × × × × × × × × × × × × ×	RS				ES		_ 1.10 -		
_ _ _	Test Pit discontinued at 1.30m depth. Refusal on inferred bedrock.										
2.											
	gin is "probable" unless otherwise stated. (")Consistency/Relative dens	sity shading is				o correlation b					r materials is implied.

METHOD: TB (300mm wide)

REMARKS:



CLIENT: Western Sydney University **PROJECT:** P1 Carpark Relocation

LOCATION: Parramatta South Campus, Parramatta NSW

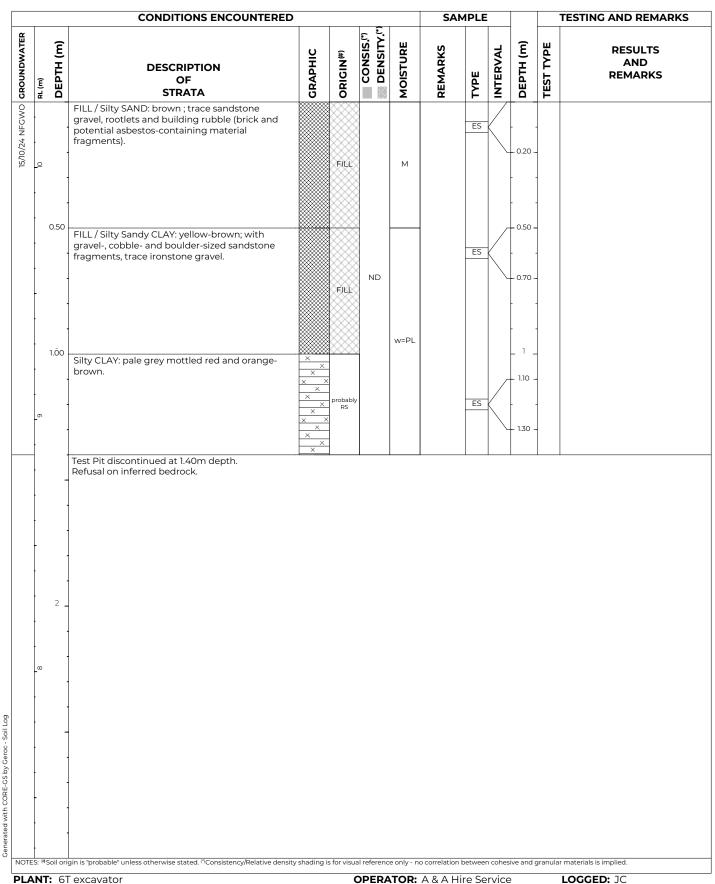
SURFACE LEVEL: 10.3 AHD

COORDINATE: E:317290.0, N:6257115.7

DATUM/GRID: MGA2020 Zone 56 DIP/AZIMUTH: 90°/---°

LOCATION ID: TP12 PROJECT No: 227191.00

DATE: 15/10/24 SHEET: 1 of 1



PLANT: 6T excavator

METHOD: TB (300mm wide)

REMARKS:



CLIENT: Western Sydney University **PROJECT:** P1 Carpark Relocation

LOCATION: Parramatta South Campus, Parramatta NSW

SURFACE LEVEL: 10.9 AHD **COORDINATE:** E:317298.7, N:6257101.0 **PROJECT No:** 227191.00

DATUM/GRID: MGA2020 Zone 56 DIP/AZIMUTH: 90°/---°

LOCATION ID: TP13

DATE: 15/10/24 SHEET: 1 of 1

GROONDWATER	RL (m)	DEPTH (m)	DESCRIPTION OF STRATA	GRAPHIC	ORIGIN(#)	CONSIS.(*) DENSITY.(*)	MOISTURE	REMARKS	TYPE	INTERVAL	DEРТН (m)	TEST TYPE	RESULTS AND REMARKS
NPCVVO		-	FILL / Silty SAND: brown and dark brown; fine to medium; trace rootlets, trace sandstone and ironstone gravel.		PILL		D to M		ES		- 0.20 -		
		0.40	FILL / Silty Sandy CLAY: yellow-brown and red- brown; fine to coarse sand; with cobble-sized sandstone fragments, trace ironstone and sandstone gravel, trace rootlets.		FILL	ND	w=PL		ES		- 0.50 - - 0.70 -		
-	ot Ot		0.80m: ceramic pipe										
\dashv			Test Pit discontinued at 1.00m depth. Refusal on inferred bedrock.		0000	1							
-		-											
	o	-											
	_	2 -											
	_ ნ	2 -											

METHOD: TB (300mm wide)

REMARKS:



CLIENT: Western Sydney University **PROJECT:** P1 Carpark Relocation

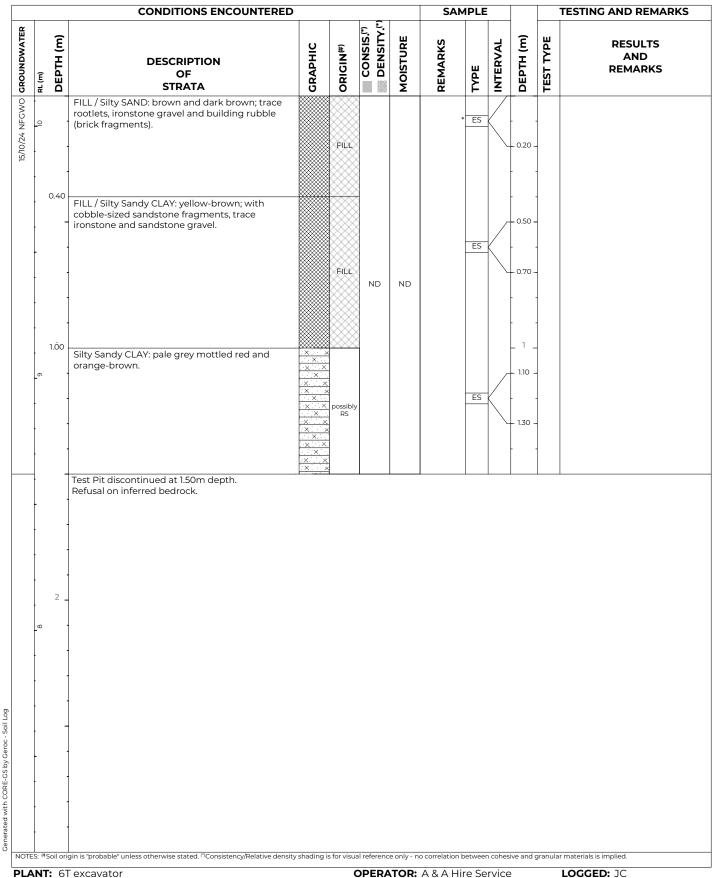
LOCATION: Parramatta South Campus, Parramatta NSW

SURFACE LEVEL: 10.1 AHD COORDINATE: E:317301.9, N:6257120.3

DATUM/GRID: MGA2020 Zone 56 DIP/AZIMUTH: 90°/---°

LOCATION ID: TP14 PROJECT No: 227191.00

DATE: 15/10/24 SHEET: 1 of 1



METHOD: TB (300mm wide)

REMARKS:



CLIENT: Western Sydney University **PROJECT:** P1 Carpark Relocation

LOCATION: Parramatta South Campus, Parramatta NSW

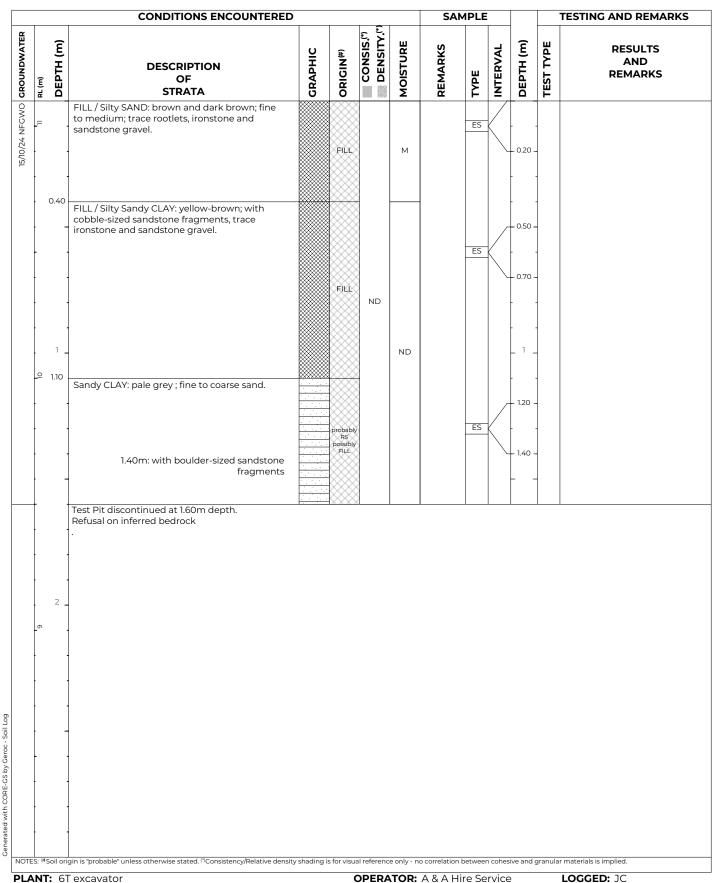
SURFACE LEVEL: 11.1 AHD

COORDINATE: E:317328.3, N:6257102.0 **PROJECT No:** 227191.00

DATUM/GRID: MGA2020 Zone 56 DIP/AZIMUTH: 90°/---°

LOCATION ID: TP15

DATE: 15/10/24 SHEET: 1 of 1



METHOD: TB (300mm wide)

REMARKS:



CLIENT: Western Sydney University **PROJECT:** P1 Carpark Relocation

LOCATION: Parramatta South Campus, Parramatta NSW

SURFACE LEVEL: 10.0 AHD COORDINATE: E:317330.5, N:6257123.6

DATUM/GRID: MGA2020 Zone 56

DATE: 15/10/24 DIP/AZIMUTH: 90°/---° SHEET: 1 of 1

LOCATION ID: TP16

PROJECT No: 227191.00

CONDITIONS ENCOUNTERED SAMPLE **TESTING AND REMARKS** CONSIS.(*) 15/10/24 NFGWO GROUNDWATER **DEPTH (m)** DEPTH (m) **TEST TYPE** MOISTURE **RESULTS** REMARKS INTERVAL GRAPHIC ORIGIN(#) AND **DESCRIPTION** TYPE **REMARKS** RL (m) OF **STRATA** FILL / Silty SAND: dark brown; trace ironstone and sandstone gravel. ES PILL 0.20 0.30m: clay band, fine to medium FILL / Silty Sandy CLAY: yellow-brown; fine to coarse sand. 0.50 ES ND М 0.70 Silty CLAY: pale grey and orange mottled red; with boulder-sized sandstone fragments and 1.00 ironstone gravel. ES Test Pit discontinued at 1.40m depth. Refusal on inferred bedrock. 2 NOTES: "Soil origin is "probable" unless otherwise stated. "Consistency/Relative density shading is for visual reference only - no correlation between cohesive and granular materials is implied.

OPERATOR: A & A Hire Service

PLANT: 6T excavator METHOD: TB (300mm wide)

REMARKS:

Generated with CORE-GS by Geroc - Soil Log

LOGGED: JC

CLIENT: Western Sydney University **PROJECT:** P1 Carpark Relocation

LOCATION: Parramatta South Campus, Parramatta NSW

SURFACE LEVEL: 11.3 AHD **COORDINATE:** E:317362.1, N:6257094.5 **PROJECT No:** 227191.00

DATUM/GRID: MGA2020 Zone 56

DATE: 15/10/24 DIP/AZIMUTH: 90°/---° SHEET: 1 of 1

LOCATION ID: TP17

CONDITIONS ENCOUNTERED SAMPLE **TESTING AND REMARKS** DENSITY.(*) CONSIS.(*) 15/10/24 NFGWO GROUNDWATER **DEPTH (m)** DEPTH (m) **TEST TYPE** MOISTURE **RESULTS** REMARKS INTERVAL GRAPHIC ORIGIN#) AND **DESCRIPTION** TYPE **REMARKS** OF RL (m) **STRATA** FILL / Silty SAND: brown and dark brown; fine to medium; trace rootlets, ironstone and ES sandstone gravel. PILL 0.20 0.30m-0.40m: asphalt layer FILL / Silty Sandy CLAY: yellow-brown; fine to coarse sand; with cobble-sized sandstone 0.50 fragments, trace ironstone and sandstone gravel. ES 0.70 FJLD ND М 1.10 Silty Sandy CLAY: pale orange-grey mottled red; fine to coarse sand. ES 1.40 Test Pit discontinued at 1.50m depth. Refusal on inferred bedrock. 2 NOTES: "Soil origin is "probable" unless otherwise stated. "Consistency/Relative density shading is for visual reference only - no correlation between cohesive and granular materials is implied.

PLANT: 6T excavator METHOD: TB (300mm wide)

REMARKS:

Generated with CORE-GS by Geroc - Soil Log

OPERATOR: A & A Hire Service LOGGED: JC



CLIENT: Western Sydney University **PROJECT:** P1 Carpark Relocation

LOCATION: Parramatta South Campus, Parramatta NSW

SURFACE LEVEL: 10.1 AHD **COORDINATE:** E:317351.5, N:6257122.2

DATUM/GRID: MGA2020 Zone 56 **DIP/AZIMUTH:** 90°/---°

DATE: 15/10/24 **SHEET:** 1 of 1

LOCATION ID: TP18

PROJECT No: 227191.00

CONDITIONS ENCOUNTERED SAMPLE **TESTING AND REMARKS** DENSITY.(*) CONSIS.(*) 15/10/24 NFGWO GROUNDWATER **DEPTH (m)** DEPTH (m) **TEST TYPE** MOISTURE **RESULTS** REMARKS INTERVAL GRAPHIC ORIGIN(#) AND **DESCRIPTION** TYPE **REMARKS** RL (m) OF **STRATA** FILL / Silty SAND; fine to medium; trace rootlets and gravel. ES 0.20 FILL М 0.60 FILL / Silty Sandy CLAY: yellow-brown and red; trace ironstone and sandstone gravel. ND 0.70 ES XXX 0.90 w=PL 1.10 Silty CLAY: pale grey mottled yellow and red; with cobble- and boulder-sized sandstone fragments and ironstone gravel. RS ES Test Pit discontinued at 1.40m depth. Refusal at inferred bedrock 2

NOTES: #Isoil origin is "probable" unless otherwise stated. "Consistency/Relative density shading is for visual reference only - no correlation between cohesive and granular materials is implied.

PLANT: 6T excavator

OPERATOR: A & A Hire Service

LOGGED: JC

METHOD: TB (300mm wide)

Generated with CORE-GS by Geroc - Soil Log

REMARKS: *Field Replicate BD6/20241015 sample taken from 0-0.2m



CLIENT: Western Sydney University **PROJECT:** P1 Carpark Relocation

LOCATION: Parramatta South Campus, Parramatta NSW

SURFACE LEVEL: 10.2 AHD **COORDINATE:** E:317368.2, N:6257111.0 **PROJECT No:** 227191.00

DATUM/GRID: MGA2020 Zone 56 DIP/AZIMUTH: 90°/---°

LOCATION ID: TP19

DATE: 15/10/24 SHEET: 1 of 1

			CONDITIONS ENCOUNTERED			£ £.		· · ·	MPLE				TESTING AND REMARKS
OROGINAL PROPERTY OF THE PROPE	RL (m)	DEPTH (m)	DESCRIPTION OF STRATA	GRAPHIC	ORIGIN(#)	CONSIS.(*)	MOISTURE	REMARKS	TYPE	INTERVAL	DEPTH (m)	TEST TYPE	RESULTS AND REMARKS
			FILL / Silty SAND: brown ; trace rootlets and ironstone gravel.										
	0	•	3			3			ES			-	
	•					}				\	- 0.20 -		
					FILL		М						
						ND							
		•										-	
		0.50	Sandy CLAY: brown; medium plasticity.							_	- 0.50 -		
			, , , , , , , , , , , , , , , , , , , ,		RS		w=PL		В				
		•	Test Pit discontinued at 0.70m depth. Terminated.								- 0.70 -		
			Terrimated.										
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METHOD: TB (300mm wide)

REMARKS:



CLIENT: Western Sydney University **PROJECT:** P1 Carpark Relocation

LOCATION: Parramatta South Campus, Parramatta NSW

SURFACE LEVEL: 10.1 AHD

COORDINATE: E:317372.4, N:6257120.3 **PROJECT No:** 227191.00

DATUM/GRID: MGA2020 Zone 56 DIP/AZIMUTH: 90°/---°

LOCATION ID: TP20

DATE: 15/10/24 SHEET: 1 of 1

	RL (m)	DEPTH (m)	DESCRIPTION OF STRATA	GRAPHIC	ORIGIN(#)	CONSIS.(*)	MOISTURE	REMARKS	TYPE	INTERVAL	DEPTH (m)	TEST TYPE	RESULTS AND REMARKS
100000000000000000000000000000000000000	00	0.30	FILL / Silty SAND: brown and dark brown; fine to medium; trace rootlets and ironstone gravel.		FILL		М		ES		- 0.20 -	-	
-		0.80	FILL / Silty Sandy CLAY: yellow-brown; fine to coarse sand; trace rootlets.		FILL	ND	w=PL		ES		- 0.50 - - 0.70 -		
	<u>о</u>	1 _	Silty Sandy CLAY: grey and orange; fine to coarse sand; with cobble- and boulder-sized sandstone fragments, trace sandstone and ironstone gravel.	X	RS		w=PL		ES		- 0.90 - _ 1 _	-	
-	œ		Refusal on inferred bedrock.										

METHOD: TB (300mm wide)

REMARKS:



CLIENT: Western Sydney University **PROJECT:** P1 Carpark Relocation

LOCATION: Parramatta South Campus, Parramatta NSW

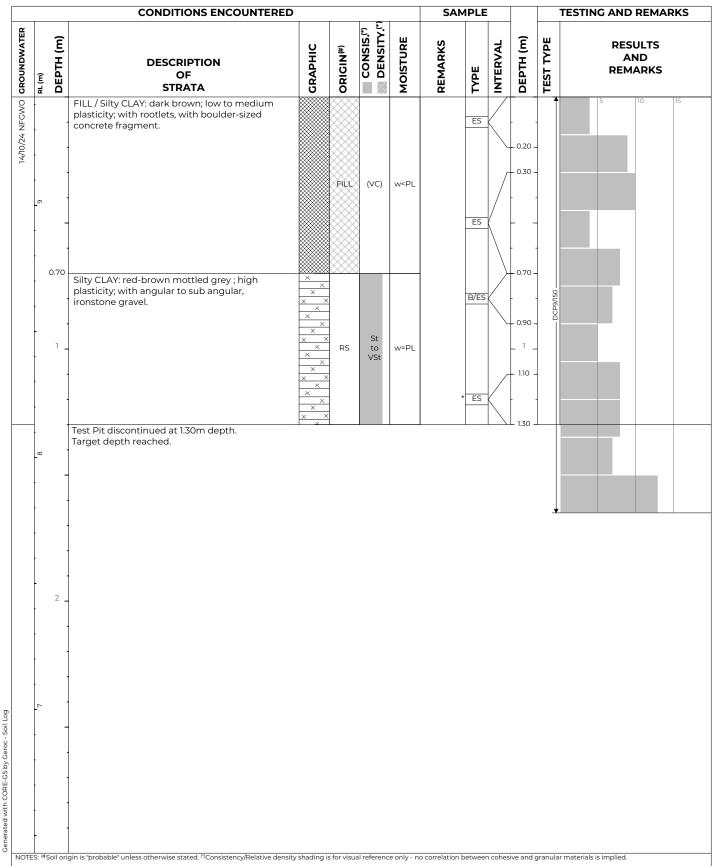
SURFACE LEVEL: 9.4 AHD

COORDINATE: E:317189.9, N:6257094.3 **PROJECT No:** 227191.00

DATUM/GRID: MGA2020 Zone 56 **DIP/AZIMUTH:** 90°/---°

LOCATION ID: TP21
PROJECT No: 227191.00

DATE: 14/10/24 **SHEET:** 1 of 1



PLANT: 6T excavator OPERATOR: A & A Hire Service LOGGED: NW

METHOD: TB (300mm wide)

REMARKS: *Field Replicate BD2/20241014 sample taken from 1.1-1.3m



CLIENT: Western Sydney University **PROJECT:** P1 Carpark Relocation

LOCATION: Parramatta South Campus, Parramatta NSW

SURFACE LEVEL: 10.3 AHD **COORDINATE:** E:317255.5, N:6257149.7 **PROJECT No:** 227191.00

DATUM/GRID: MGA2020 Zone 56 DIP/AZIMUTH: 90°/---°

LOCATION ID: TP22

DATE: 14/10/24 **SHEET:** 1 of 2

				··· // _		H: 90°/					SHEET: 1012
	CONDITIONS ENCOUNTERED)		£		SAM	IPLE				TESTING AND REMARKS
RL (m) DEPTH (m)	DESCRIPTION OF STRATA	GRAPHIC	ORIGIN(#)	CONSIS.(*)	MOISTURE	REMARKS	TYPE	INTERVAL	DEРТН (m)	TEST TYPE	RESULTS AND REMARKS
	FILL / Silty SAND: brown and dark brown; fine to medium; non-plastic silt; with boulder-sized sandstone fragment, trace building rubble (brick, PVC pipe, terracotta and concrete fragments), trace sandstone gravel, grass and rootlets.				_	_	ES B/ES		- 0.20 -		5 10 15
1 -			PILL	(MC)	М				- 0.70	DCP9/150	
. 1.60	FILL / Clayey Silty SAND: dark brown and brown; with cobble- and boulder-sized								· ·		
2 .	sandstone fragments, trace sandstone gravel, trace building rubble (concrete, geofabric, rubber, tile, and plastic fragments).		FILL		М		ES .		- 1.70 1.90 2 -		
	Silty Sandy CLAY: yellow brown mottled dark grey; fine to medium sand; trace rootlets.	X		ND			ES		- 2.30 - - 2.50 -		
TES: ^(A) Soil or	igin is "probable" unless otherwise stated. ("Consistency/Relative densi	X	ALV	ıl referenc	w=PL e only - n	o correlation b	ES	cohesi	- 2.70 - - 2.90 - ve and ç	granula	r materials is implied.

PLANT: 6T excavator METHOD: TB (600mm wide)

REMARKS:

OPERATOR: A & A Hire Service

LOGGED: NW



CLIENT: Western Sydney University **PROJECT:** P1 Carpark Relocation

LOCATION: Parramatta South Campus, Parramatta NSW

SURFACE LEVEL: 10.3 AHD **COORDINATE:** E:317255.5, N:6257149.7

DATUM/GRID: MGA2020 Zone 56 **DATE:** 14/10/24 **DIP/AZIMUTH:** 90°/---° **SHEET:** 2 of 2

LOCATION ID: TP22

PROJECT No: 227191.00

CONDITIONS ENCOUNTERED SAMPLE **TESTING AND REMARKS** CONSIS.(*) GROUNDWATER DEPTH (m) DEPTH (m) TEST TYPE MOISTURE **RESULTS** REMARKS INTERVAL GRAPHIC ORIGIN(#) AND **DESCRIPTION** TYPE **REMARKS** RL (m) OF **STRATA** [CONT] Silty Sandy CLAY: yellow brown mottled dark grey; fine to medium sand; trace ALV ND w=PL rootlets. Test Pit discontinued at 3.20m depth. Target depth reached.

PLANT: 6T excavator

5

METHOD: TB (600mm wide)

REMARKS:

Generated with CORE-GS by Geroc - Soil Log

OPERATOR: A & A Hire Service LOGGED: NW



NOTES: [#Soil origin is "probable" unless otherwise stated. ("Consistency/Relative density shading is for visual reference only - no correlation between cohesive and granular materials is implied.

CLIENT: Western Sydney University **PROJECT:** P1 Carpark Relocation

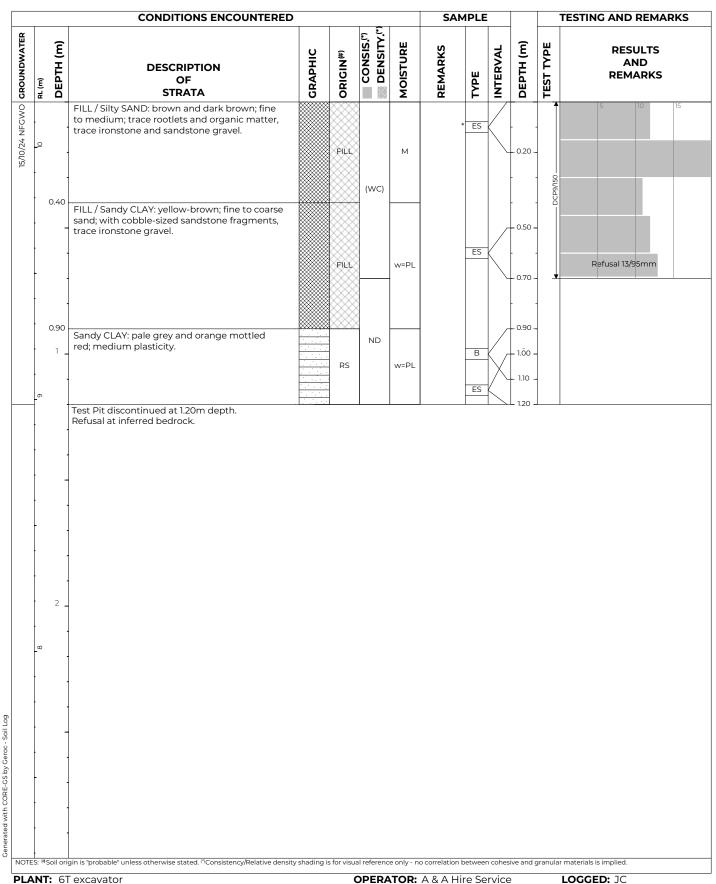
LOCATION: Parramatta South Campus, Parramatta NSW

SURFACE LEVEL: 10.2 AHD **COORDINATE:** E:317317.2, N:6257112.7

DATUM/GRID: MGA2020 Zone 56 DIP/AZIMUTH: 90°/---°

LOCATION ID: TP23 PROJECT No: 227191.00

DATE: 15/10/24 SHEET: 1 of 1



PLANT: 6T excavator

METHOD: TB (300mm wide)

REMARKS:



CLIENT: Western Sydney University **PROJECT:** P1 Carpark Relocation

LOCATION: Parramatta South Campus, Parramatta NSW

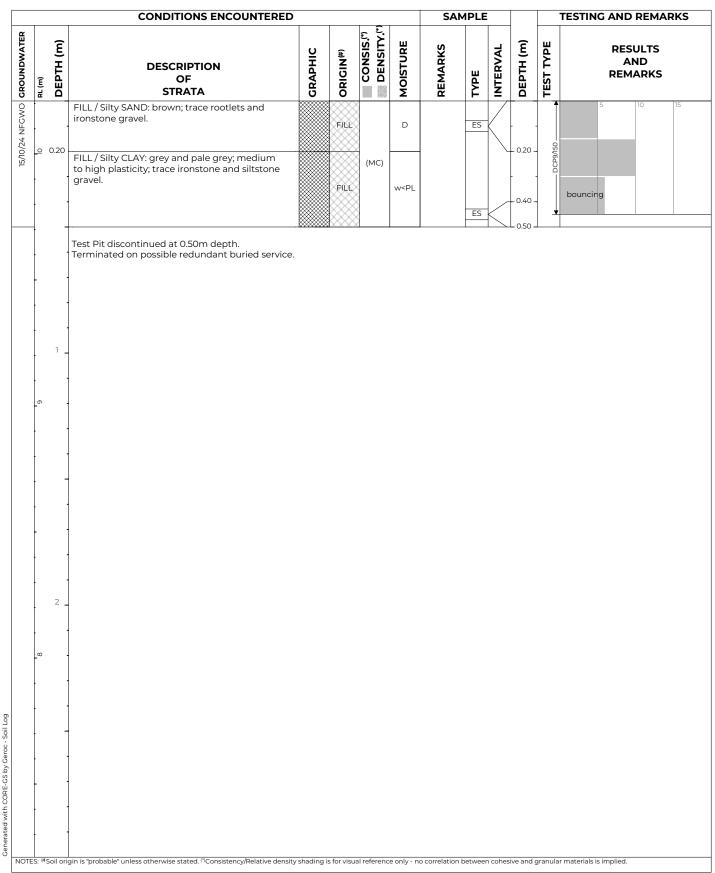
SURFACE LEVEL: 10.2 AHD

COORDINATE: E:317379.0, N:6257104.4 **PROJECT No:** 227191.00

DATUM/GRID: MGA2020 Zone 56 **DIP/AZIMUTH:** 90°/---°

LOCATION ID: TP24

DATE: 15/10/24 **SHEET:** 1 of 1



PLANT: Hand tools OPERATOR: JC LOGGED: JC

METHOD: HAND REMARKS:



Report Number: 227191.00-1

Issue Number:

Date Issued: 13/11/2024

Client: Western Sydney University

Victoria Road, Rydalmere NSW

Contact: Stuart Pullens **Project Number:** 227191.00

Project Name: P1 Carpark Relocation

Project Location: Western Sydney University, Rydalmere NSW

 Work Request:
 11895

 Sample Number:
 SY-11895A

 Date Sampled:
 14/10/2024

Dates Tested: 21/10/2024 - 12/11/2024

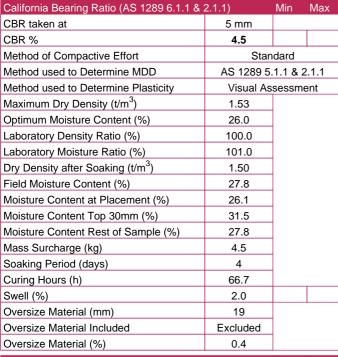
Sampling Method: Sampled by Engineering Department

The results apply to the sample as received

Sample Location: TP21 (0.7-0.9m)

Material: Silty CLAY: red-brown mottled grey, with angular to sub

angular, ironstone gravel.



Atterberg Limit (AS1289 3.1.2 & 3.2	Min	Max	
Sample History	Oven Dried		
Preparation Method	Dry Sieve		
Liquid Limit (%)	61		
Plastic Limit (%)	27		
Plasticity Index (%)	34		

Report Number: 227191.00-1



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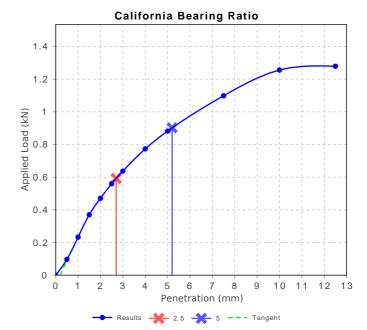
Phone: (02) 9809 0666 Email: mick.gref@douglaspartners.com.au





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Report Number: 227191.00-1

Issue Number:

Date Issued: 13/11/2024

Client: Western Sydney University

Victoria Road, Rydalmere NSW

Contact: Stuart Pullens **Project Number:** 227191.00

Project Name: P1 Carpark Relocation

Western Sydney University, Rydalmere NSW **Project Location:**

Work Request: 11895 Sample Number: SY-11895B **Date Sampled:** 14/10/2024

Dates Tested: 21/10/2024 - 12/11/2024

Sampling Method: Sampled by Engineering Department

The results apply to the sample as received

Sample Location: TP22 (0.5-0.7m)

Material:

FILL / Silty SAND: brown and dark brown, fine to medium, trace brick, pvc pipe, rootlets, gravel, sandstone boulder, terracotta, concrete and grass.

California Bearing Ratio (AS 1289 6.1.1 & 2	2.1.1)	Min	Max
CBR taken at	5 mm		
CBR %	15		
Method of Compactive Effort	Stan	dard	
Method used to Determine MDD	.1.1 & 2	.1.1	
Method used to Determine Plasticity	Visual As	sessme	ent
Maximum Dry Density (t/m ³)	1.82		
Optimum Moisture Content (%)	15.0		
Laboratory Density Ratio (%)	100.0		
Laboratory Moisture Ratio (%)	98.5		
Dry Density after Soaking (t/m³)	1.82		
Field Moisture Content (%)	9.6		
Moisture Content at Placement (%)	14.8		
Moisture Content Top 30mm (%)	16.2		
Moisture Content Rest of Sample (%)	14.9		
Mass Surcharge (kg)	4.5		
Soaking Period (days)	4		
Curing Hours (h)	67.0		
Swell (%)	-0.5		
Oversize Material (mm)	19		
Oversize Material Included	Excluded		
Oversize Material (%)	6.5		
C2			

Atterberg Limit (AS1289 3.1.2 & 3.2	Min	Max	
Sample History	Oven Dried		
Preparation Method	Dry Sieve		
Liquid Limit (%)	23		
Plastic Limit (%)	17		
Plasticity Index (%)	6		

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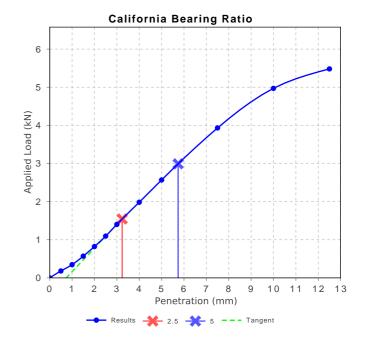
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Report Number: 227191.00-1

Issue Number:

Date Issued: 13/11/2024

Client: Western Sydney University

Victoria Road, Rydalmere NSW

Contact: Stuart Pullens **Project Number:** 227191.00

Project Name: P1 Carpark Relocation

Project Location: Western Sydney University, Rydalmere NSW

Work Request: 11895
Sample Number: SY-11895C
Date Sampled: 14/10/2024

Dates Tested: 21/10/2024 - 12/11/2024

Sampling Method: Sampled by Engineering Department

The results apply to the sample as received

Sample Location: TP23 (0.9-1.1m)

Material: Sandy CLAY: pale grey and orange mottled red

California Bearing Ratio (AS 1289 6.1.1 &	2.1.1)	Min	Max		
CBR taken at	5 mm				
CBR %	8				
Method of Compactive Effort	Stan	dard			
Method used to Determine MDD	AS 1289 5.	9 5.1.1 & 2.1.1			
Method used to Determine Plasticity	Visual As	sessme	ent		
Maximum Dry Density (t/m ³)	1.87				
Optimum Moisture Content (%)	15.0				
Laboratory Density Ratio (%)	100.5				
Laboratory Moisture Ratio (%)	97.5				
Dry Density after Soaking (t/m ³)	1.86				
Field Moisture Content (%)	14.0				
Moisture Content at Placement (%)	14.5				
Moisture Content Top 30mm (%)	17.1				
Moisture Content Rest of Sample (%)	15.9				
Mass Surcharge (kg)	4.5				
Soaking Period (days)	4				
Curing Hours (h)	67.0				
Swell (%)	1.0				
Oversize Material (mm)	19				
Oversize Material Included	Excluded				
Oversize Material (%)	2.7				

Atterberg Limit (AS1289 3.1.2 & 3.2	Min	Max	
Sample History	Oven Dried		
Preparation Method	Dry Sieve		
Liquid Limit (%)	40		
Plastic Limit (%)	18		
Plasticity Index (%)	22		



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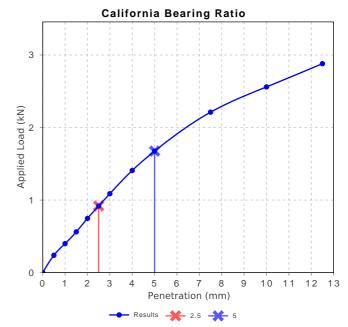
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Report Number: 227191.00-1

Issue Number:

Date Issued: 13/11/2024

Client: Western Sydney University

Victoria Road, Rydalmere NSW

Contact: Stuart Pullens **Project Number:** 227191.00

Project Name: P1 Carpark Relocation

Project Location: Western Sydney University, Rydalmere NSW

 Work Request:
 11895

 Sample Number:
 SY-11895D

 Date Sampled:
 14/10/2024

Dates Tested: 21/10/2024 - 12/11/2024

Sampling Method: Sampled by Engineering Department

The results apply to the sample as received

Preparation Method: AS 1289.1.1 - Sampling and Preparation of Soils

Sample Location: TP19 (0.5-0.7m)

Material: Sandy CLAY: brown, trace rootlets and ironstone gravel

California Bearing Ratio (AS 1289 6.1.1 &	2.1.1)	Min	Max
CBR taken at	5 mm		
CBR %	10		
Method of Compactive Effort	Stan	dard	
Method used to Determine MDD	AS 1289 5.	1.1 & 2	.1.1
Method used to Determine Plasticity	Visual As	sessme	ent
Maximum Dry Density (t/m ³)	1.78		
Optimum Moisture Content (%)	16.5		
Laboratory Density Ratio (%)	100.0		
Laboratory Moisture Ratio (%)	100.5		
Dry Density after Soaking (t/m ³)	1.80		
Field Moisture Content (%)	13.6		
Moisture Content at Placement (%)	16.7		
Moisture Content Top 30mm (%)	19.3		
Moisture Content Rest of Sample (%)	18.1		
Mass Surcharge (kg)	4.5		
Soaking Period (days)	4		
Curing Hours (h)	96.2		
Swell (%)	-1.5		
Oversize Material (mm)	19		
Oversize Material Included	Excluded		
Oversize Material (%)	8.2		

Atterberg Limit (AS1289 3.1.2 & 3.2	Min	Max	
Sample History	Oven Dried		
Preparation Method	Dry Sieve		
Liquid Limit (%)	40		
Plastic Limit (%)	20		
Plasticity Index (%)	20		



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