MGO MT OWEN/GLENDELL OPERATIONS GLENCORE

MT OWEN/GLENDELL OPERATIONS THE ANNUAL REVIEW APPENDICIES

1 January 2019 – 31 December 2019

Glencore Code of Conduct – Environment and Compliance

Environment

We are aware that our global operations can have direct and indirect impacts on the environment.

Our operations are geographically widespread and extremely diverse in nature, including prospecting, production, reclamation, processing, storage, transportation and marketing of natural resources. This means that our potential environmental impacts are complex and specific to different commodity groups or production sites.

We are aware of the increasing regulatory pressure and societal demand for a low emission economy to address the global climate change situation. We are working to integrate this into our existing resource efficiency programmes at our operations. We comply with applicable laws, regulations and other requirements for environmental management. Where these are less stringent than our own standards we seek to exceed the statutory requirements wherever possible.

We also participate in supply chains that are not under our direct control. Here we work in partnership with our customers, suppliers and service providers to limit the overall environmental impact along the entire supply chain, and promote environmental awareness.

Our managers are required to:

- Identify, assess and monitor environmental impacts
- Comply with applicable regulatory requirements and monitor relevant regulations for changes
- Implement appropriate environmental management programmes and controls, including appropriate measures for emergency preparedness
- Ensure competent staff and sufficient resources for environmental management
- Involve contractors and service providers where appropriate
- Implement programmes and targets for continuous improvement of our:
 - Efficient use of resources (eg energy, water and land)
 - Protection of biodiversity
 - · Climate change impact
 - Pollution prevention (by addressing management of fresh water and effluent, waste, air emissions, hazardous materials and rehabilitation of land)
- 7. Track actual environmental performance

Compliance

Everyone who works for Glencore Xstrata must comply with or exceed the laws, regulations and best practice guidelines applicable in the jurisdictions where we operate.

We will not assist any third party in breaching the law in any country, or participate in any other criminal, fraudulent or corrupt practice. We seek to prevent such misconduct through strong leadership, internal policies and procedures.

Anyone acting on behalf of Glencore Xstrata, along our entire supply chain, must comply with applicable laws and corporate policies. Our managers and supervisors must ensure this is the case, and take appropriate action to prevent, detect and report any failures to comply.

You must follow the guidance and instructions regarding the corporate policies applicable to your duties, including related training. Where appropriate, you must confirm that you have received and understood the compliance policies, manuals and guidance. Local compliance co-ordinators have been appointed to support you in day-to-day business considerations.

Individual operations may implement their own policies in addition to the Glencore Xstrata corporate policies. These should be designed to address their specific requirements, while consistent with Our Values and principles as set out by the Code and Glencore Xstrata corporate policies.

Conflict of interest

A conflict of interest is a situation in which an individual has a private interest sufficient to appear to influence the objective exercise of his or her professional duties.

You must avoid actual conflicts of interest and avoid, wherever possible, apparent or potential conflicts or otherwise carefully manage them accordingly. Everyone working for Glencore Xstrata must carefully perform their professional duties and safeguard Glencore Xstrata's legitimate interests.

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Appendix A: Correspondence



Mr Ned Stephenson Environment and Community Manager Mt Owen Complex PO Box 320 SINGLETON NSW 2330 Contact: Heidi Watters Phone: (02) 6575 3401

Email: heidi.watters@planning.nsw.gov.au compliance@planning.nsw.gov.au

Our Ref: SSD-5850 and DA 80/952

Email: ned.stephenson@glencore.com.au

Dear Mr Stephenson

Mt Owen Complex (SSD 5850 and DA 80/952) 2018 Annual Review

Reference is made to the revised Mt Owen Complex 2018 Annual Review for the period 1 January 2018 to 31 December 2018, prepared as required by Schedule 5 condition 5 of SSD-5850, as modified and DA 80/952, as modified (the approvals), and submitted to the Department of Planning, Industry and Environment (the Department) on 27 June 2019.

The Department has reviewed the revised 2018 Annual Review and considers that it satisfies the reporting requirements of the approvals and the Department's *Annual Review Guideline* (October 2015). As required by Schedule 6 condition 12 of the mining consent and Schedule 6 condition 8 of the rail consent, please make a copy of the 2018 Annual Review available on the project website by **31 July 2019**.

Please note that acceptance of the Annual Review is not an endorsement of the compliance status of the project. Non-compliances identified in the Annual Review may be investigated further by the Department.

Should you need to discuss the above, please contact Heidi Watters on the details above or email to compliance@planning.nsw.gov.au

Yours sincerely

Leah Cook

Team Leader Compliance As nominee of the Secretary

8/7/19

Appendix B: Daily Train Movements

Table 1: Daily Train Movements and Tonnes Loaded 2019

Date	Number of Trains Per Day	Total Tonnes Loaded
1/01/2019	5	46,412.65
2/01/2019	5	46,141.85
3/01/2019	3	27,746.70
4/01/2019	3	27,574.75
5/01/2019	4	36,503.15
6/01/2019	3	27,980.65
7/01/2019	2	18,605.80
8/01/2019	0	0.00
9/01/2019	2	18,579.30
10/01/2019	2	18,584.05
11/01/2019	4	27,202.10
12/01/2019	2	8,592.80
13/01/2019	4	27,233.00
14/01/2019	2	13,176.40
15/01/2019	3	17,618.85
16/01/2019	2	8,594.25
17/01/2019	1	4,291.35
18/01/2019	2	8,575.45
19/01/2019	2	8,609.15
20/01/2019	2	13,530.15
21/01/2019	3	22,908.25
22/01/2019	2	13,621.85
23/01/2019	7	58,465.35
24/01/2019	2	18,594.90
25/01/2019	1	9,354.35
26/01/2019	4	36,673.15
27/01/2019	6	55,132.75
28/01/2019	6	55,113.70
29/01/2019	5	45,702.00
30/01/2019	7	64,261.35
31/01/2019	6	54,509.60
1/02/2019	4	36,846.70
2/02/2019	4	37,237.10
3/02/2019	3	27,732.15
4/02/2019	4	36,629.70
5/02/2019	3	27,497.35
6/02/2019	4	36,918.15
7/02/2019	3	27,781.80

Date	Number of Trains Per Day	Total Tonnes Loaded
8/02/2019	5	46,229.30
9/02/2019	3	27,772.70
10/02/2019	2	18,363.30
11/02/2019	2	18,511.95
12/02/2019	2	18,181.45
13/02/2019	2	18,626.70
14/02/2019	2	17,817.05
15/02/2019	2	18,566.20
17/02/2019	4	36,639.85
18/02/2019	1	9,270.30
19/02/2019	0	0.00
20/02/2019	0	0.00
21/02/2019	0	0.00
22/02/2019	4	36,892.65
23/02/2019	4	36,061.70
24/02/2019	4	36,608.55
25/02/2019	1	8,927.05
27/02/2019	1	9,155.10
28/02/2019	3	27,113.90
1/03/2019	4	36,747.25
2/03/2019	3	27,973.90
3/03/2019	6	54,827.20
4/03/2019	2	18,495.75
5/03/2019	2	18,037.15
6/03/2019	2	18,586.15
7/03/2019	2	18,630.00
8/03/2019	0	0.00
9/03/2019	2	18,111.90
10/03/2019	4	36,594.25
11/03/2019	4	36,618.45
12/03/2019	3	27,779.55
13/03/2019	2	18,434.75
14/03/2019	2	18,328.10
15/03/2019	3	22,640.55
16/03/2019	5	35,893.35
17/03/2019	7	49,272.65
18/03/2019	5	41,143.25
19/03/2019	3	17,660.75
20/03/2019	5	40,692.75
21/03/2019	4	27,153.55
22/03/2019	2	13,423.25
23/03/2019	2	8,552.30

Date	Number of Trains Per Day	Total Tonnes Loaded
24/03/2019	3	17,771.75
25/03/2019	2	8,574.25
26/03/2019	1	9,253.40
27/03/2019	2	18,073.65
28/03/2019	1	9,240.95
29/03/2019	3	27,572.10
30/03/2019	2	18,556.70
31/03/2019	6	55,213.15
1/04/2019	5	45,687.00
2/04/2019	2	17,770.75
3/04/2019	4	36,477.60
4/04/2019	2	18,383.25
5/04/2019	3	27,698.75
6/04/2019	2	17,826.85
7/04/2019	3	27,386.85
8/04/2019	5	44,752.60
9/04/2019	0	0.00
10/04/2019	0	0.00
11/04/2019	0	0.00
12/04/2019	2	18,598.30
13/04/2019	5	45,849.00
14/04/2019	0	0.00
15/04/2019	3	26,818.95
16/04/2019	1	9,299.45
17/04/2019	2	18,153.00
18/04/2019	1	9,061.55
19/04/2019	2	13,264.95
20/04/2019	3	17,667.40
21/04/2019	4	26,507.05
22/04/2019	2	8,538.20
23/04/2019	1	4,283.65
24/04/2019	0	0.00
25/04/2019	1	8,990.50
26/04/2019	0	0.00
27/04/2019	1	4,275.00
28/04/2019	2	13,512.10
29/04/2019	3	22,407.50
30/04/2019	1	9,223.60
1/05/2019	3	26,832.00
2/05/2019	4	35,356.15
3/05/2019	4	36,081.20
4/05/2019	3	27,592.90

Date	Number of Trains Per Day	Total Tonnes Loaded
5/05/2019	3	26,879.05
6/05/2019	2	17,659.25
7/05/2019	0	0.00
8/05/2019	3	26,646.25
9/05/2019	3	26,998.55
10/05/2019	4	35,728.05
11/05/2019	3	26,726.05
12/05/2019	4	35,674.55
13/05/2019	2	18,572.80
14/05/2019	2	18,312.35
15/05/2019	6	54,581.55
16/05/2019	1	9,148.60
17/05/2019	4	26,474.90
18/05/2019	2	13,073.50
19/05/2019	2	8,552.75
20/05/2019	3	22,535.40
21/05/2019	0	0.00
22/05/2019	0	0.00
23/05/2019	0	0.00
24/05/2019	4	31,722.95
25/05/2019	4	26,254.10
26/05/2019	2	8,563.75
27/05/2019	4	31,091.65
28/05/2019	3	17,785.15
29/05/2019	4	31,201.20
30/05/2019	4	31,441.15
31/05/2019	1	9,176.50
1/06/2019	1	9,294.05
2/06/2019	5	44,915.75
3/06/2019	2	18,155.75
4/06/2019	2	17,673.20
5/06/2019	3	26,668.85
6/06/2019	3	26,988.10
7/06/2019	0	0.00
8/06/2019	1	9,256.95
9/06/2019	2	18,660.65
10/06/2019	2	18,168.60
11/06/2019	2 13,498.45	
12/06/2019	6	45,298.55
13/06/2019	1	9,256.95
14/06/2019	1	8,829.30
15/06/2019	1	9,108.50

Date	Number of Trains Per Day	Total Tonnes Loaded
16/06/2019	1	8,713.90
17/06/2019	2	17,894.85
18/06/2019	5	44,768.05
19/06/2019	3	27,361.05
20/06/2019	4	36,944.90
21/06/2019	2	18,146.85
22/06/2019	3	27,840.40
23/06/2019	1	9,144.20
24/06/2019	1	8,750.55
25/06/2019	0	0.00
26/06/2019	1	8,774.65
27/06/2019	1	8,746.80
28/06/2019	0	0.00
29/06/2019	3	26,322.05
30/06/2019	4	36,334.55
1/07/2019	0	0.00
2/07/2019	0	0.00
3/07/2019	2	17,914.05
4/07/2019	2	17,378.95
5/07/2019	3	27,631.60
6/07/2019	3	27,729.20
7/07/2019	3	27,476.55
8/07/2019	2	18,147.45
9/07/2019	0	0.00
10/07/2019	2	18,580.15
11/07/2019	3	27,195.75
12/07/2019	2	18,414.60
13/07/2019	5	46,097.30
14/07/2019	4	37,146.35
15/07/2019	4	36,997.65
16/07/2019	5	36,067.75
17/07/2019	2	13,251.00
18/07/2019	4	24,886.15
19/07/2019	4	31,527.40
20/07/2019	5	36,068.75
21/07/2019	5	46,308.65
22/07/2019	1	9,292.10
23/07/2019	2	18,345.30
24/07/2019	2	18,619.45
25/07/2019	3	27,474.45
26/07/2019	2	17,985.85
27/07/2019	6	55,348.10

Date	Number of Trains Per Day	Total Tonnes Loaded
28/07/2019	3	27,161.60
29/07/2019	1	9,036.15
30/07/2019	2	17,907.50
31/07/2019	2	18,438.55
1/08/2019	5	36,208.40
2/08/2019	4	31,879.40
3/08/2019	6	50,084.85
4/08/2019	4	27,164.80
5/08/2019	2	18,122.80
6/08/2019	0	0.00
7/08/2019	0	0.00
8/08/2019	0	0.00
9/08/2019	3	22,744.90
10/08/2019	4	31,553.20
11/08/2019	6	44,951.75
12/08/2019	4	26,811.20
13/08/2019	3	27,359.85
14/08/2019	4	26,900.05
15/08/2019	4	32,053.25
16/08/2019	2	18,413.20
17/08/2019	4	27,040.65
18/08/2019	3	17,608.80
19/08/2019	2	18,554.35
20/08/2019	1	9,327.70
21/08/2019	2	17,974.00
22/08/2019	4	36,820.05
23/08/2019	2	18,159.20
24/08/2019	3	27,522.00
25/08/2019	1	9,285.75
26/08/2019	1	9,318.90
27/08/2019	3	27,214.30
28/08/2019	3	24,104.70
29/08/2019	4	37,016.45
30/08/2019	1	8,978.95
31/08/2019	4	36,561.35
1/09/2019	3	27,558.05
2/09/2019	3	27,596.25
3/09/2019	5	45,872.70
4/09/2019	2	18,382.45
5/09/2019	1	9,230.10
6/09/2019	1	9,307.90
7/09/2019	6	45,108.35

Date	Number of Trains Per Day	Total Tonnes Loaded	
8/09/2019	2	13,343.80	
9/09/2019	3	17,672.65	
10/09/2019	4	27,145.45	
11/09/2019	1	4,292.15	
12/09/2019	4	31,557.75	
13/09/2019	5	35,715.35	
14/09/2019	4	31,829.35	
15/09/2019	3	22,745.70	
16/09/2019	2	18,189.10	
17/09/2019	2	18,291.25	
18/09/2019	3	27,719.00	
19/09/2019	0	0.00	
20/09/2019	0	0.00	
21/09/2019	1	9,349.30	
22/09/2019	3	17,287.75	
23/09/2019	3	17,735.05	
24/09/2019	0	0.00	
25/09/2019	0	0.00	
26/09/2019	0	0.00	
27/09/2019	3	22,656.70	
28/09/2019	5	35,608.35	
29/09/2019	4	26,346.40	
30/09/2019	4	26,898.05	
1/10/2019	1	9,344.60	
2/10/2019	4	30,623.95	
3/10/2019	5	35,371.84	
4/10/2019	4	26,921.10	
5/10/2019	5	35,732.35	
6/10/2019	4	36,700.75	
7/10/2019	3	27,007.65	
8/10/2019	5	36,173.25	
9/10/2019	4	36,575.25	
10/10/2019	6	39,712.40	
11/10/2019	5	41,077.75	
12/10/2019	7	54,031.05	
13/10/2019	7	54,677.00	
14/10/2019	3	27,669.20	
15/10/2019	3 22,783.00		
16/10/2019	3 27,842.80		
17/10/2019	3 26,991.50		
18/10/2019	3	26,570.85	
19/10/2019	2	18,147.40	

Date	Number of Trains Per Day	Total Tonnes Loaded
20/10/2019	1	4,269.80
21/10/2019	2	8,529.75
22/10/2019	1	9,170.75
23/10/2019	3	27,153.85
24/10/2019	2	18,038.45
25/10/2019	3	27,132.40
26/10/2019	2	18,159.85
27/10/2019	2	18,645.70
28/10/2019	6	55,148.40
29/10/2019	3	27,671.30
30/10/2019	3	27,566.20
31/10/2019	5	45,437.60
1/11/2019	3	27,400.50
2/11/2019	0	0.00
3/11/2019	1	4,272.90
4/11/2019	2	8,576.90
5/11/2019	1	4,275.65
6/11/2019	1	4,278.20
7/11/2019	2	8,549.60
8/11/2019	2	13,622.30
9/11/2019	4	26,900.15
10/11/2019	3	27,611.95
11/11/2019	8	63,500.90
12/11/2019	3	22,671.70
13/11/2019	4	26,755.30
14/11/2019	3	17,506.40
15/11/2019	4	26,343.05
16/11/2019	1	4,175.35
17/11/2019	3	12,597.30
18/11/2019	2	13,243.95
19/11/2019	0	0.00
20/11/2019	0	0.00
21/11/2019	0	0.00
22/11/2019	4	36,306.40
23/11/2019	4	36,404.15
24/11/2019	4	36,496.75
25/11/2019	4	36,632.15
26/11/2019	2 18,008.30	
27/11/2019	4 35,615.75	
28/11/2019	5	35,579.30
29/11/2019	6	34,875.30
30/11/2019	8	62,769.05

Date	Number of Trains Per Day	Total Tonnes Loaded
1/12/2019	7	44,411.00
2/12/2019	5	30,796.10
3/12/2019	7	49,176.15
4/12/2019	4	21,832.60
5/12/2019	5	35,541.30
6/12/2019	5	35,748.60
7/12/2019	4	26,952.35
8/12/2019	3	22,483.10
9/12/2019	3	17,674.75
10/12/2019	3	17,712.90
11/12/2019	3	22,164.50
12/12/2019	4	26,549.95
13/12/2019	4	26,826.60
14/12/2019	5	36,431.60
15/12/2019	3	22,675.85
16/12/2019	7	54,492.35
17/12/2019	5	35,154.90
18/12/2019	1	4,274.55
19/12/2019	4	26,696.95
20/12/2019	7	53,924.10
21/12/2019	3	22,777.65
22/12/2019	4	36,606.05
23/12/2019	6	44,974.65
24/12/2019	0	0.00
25/12/2019	0	0.00
26/12/2019	1	9,011.85
27/12/2019	5	44,534.35
28/12/2019	5	34,911.55
29/12/2019	3	17,062.65
30/12/2019	1	4,036.05
31/12/2019	4	26,022.85
Total	1039	8.39 MT

Appendix C: Environmental Incidents

Environmental incidents at the MGO are classified into six categories (based on Glencore's Internal Incident Reporting):

- Nil Category: below category 1;
- Category 1: Negligible An incident that causes negligible, reversible environmental impact, requiring very minor or no remediation;
- Category 2: Minor An incident that causes minor, reversible environmental impacts, require minor remediation;
- Category 3: Significant An incident that has caused moderate, reversible environmental impact with short-term effect, requiring moderate remediation;
- Category 4: Serious An incident that has caused significant environmental impact, with medium-term effect, requiring significant remediation; and
- Category 5: Disastrous An incident that has caused disastrous environmental impact, with long-term effect, requiring major remediation.

Table 2: Environmental Incidents 2019

No.	Incident Date	Incident Category	Incident Type	Response	
Glende	Glendell and Ravensworth East				
1	07-Jan-19	1	Oil Spill O-ring Failure	Shut down machine. High Pressure O-ring had failed.	
2	20-Feb-19	1	Waste	New lock installed on entry gate	
3	26-Jan-19	Nil	Oil Spill Crack diff housing	Dozer diff housing condition monitored, planned maintenance and implemented.	
4	26-Feb-19	1	Coolant Spill	Machine parked fundamentally stable, repairs carried out.	
5	28-Feb-19	Nil	Oil Spill	Contaminated dirt removed and transported to bioremediation area.	
6	14-Mar-19	1	Oil Spill Failed ram pin	Operator notified the OCE. A bund was set up to contain the oil leak.	
7	18-Mar-19	Nil	Oil Spill	Leaks repaired and contaminated dirt removed from under ST35 and transported to bioremediation area.	
8	25-Mar-19	1	Oil Spill	OCE isolated the truck and surrounding area Hard barricading installed. Product transported bioremediation area	
9	26-Mar-19	1	Oil Leak	Machine isolated spill contained and cleaned up	
10	27-Mar-19	1	Oil Spill Brake Hose Fail	Digger hut down, spill controlled and cleaned up.	
11	29-Apr-19	1	Oil Spill	Leak repaired in digger spill mitigated	
12	12-May-19	1	Oil Spill Hydraulic Hose Fail	Turned off hydraulic tank taps to prevent further spill. Replaced blown hose, fill hydraulics and tested.	
13	20-Jun-19	1	Oil Leak	Machine stopped, area barricaded and oil contained. Oil was cleaned up using a front end loader and taken to bioremediation area	
14	05-Jul-19	1	Oil Leak	Operator stopped excavator and called the OCE to inspect the damage.	
15	06-Jul-19	1	Oil Spill Hydraulic Hose Fail	Westrac attended truck to inspect the leak, mitigated spill by using spill sorb.	
16	24-Jul-19	1	Oil Spill Main driveshaft failure	Crusher dust used to contain the scene. Contaminated product taken to bioremediation area	
17	04-Aug-19	1	Oil Spill Failed engine oil pump O-ring	Spill trailer was used to contain and collect the oil. Contaminated product taken to bioremediation area.	
18	14-Aug-19	1	Oil Spill	Oil was contained, machine was moved from area. Skid steer loader was utilised to remove contaminated soil and placed in the remediation area.	
19	20-Aug-19	1	Oil Leak Engine	Spill sorb used to clean up.	
20	28-Aug-19	1	Oil Spill Failed boom hose	While parked up the hose was removed and replaced with a new one.	

No.	Incident Date	Incident Category	Incident Type	Response
21	09-Sep-19	Nil	Air Quality Total Suspended Solid (TSP 2) Dust Sample destroyed	Reported to MGO task coordinator and CBE Projects Manager. Refer to App C_2019 Cbased Incident Investigation.
22	02-Oct-19	1	Oil Spill Failed boom hose	Shut down, contained spill where possible, changed hose and topped up oils
23	02-Nov-19	1	Fuel Spill Service tail damage	Fuel tap was turned off, the area was bunded, a 1000ltr pod used to contain fuel. Machine repaired and contaminated material sent to bioremediation area
24	03-Nov-19	1	Oil Spill 30w bulk oil tank overfilled	Oil spill cleaned up with dry sorb
25	11-Nov-19	1	Oil Spill Hydraulic	Machine shut down. Failed contamination sensor. A new contamination sensor was fitted to the pump.
26	21-Nov-19	1	Oil Leak Fan hose failure	Oil spill controlled until repairs and clean-up take place. Minimal remediation required.
27	03-Dec-19	1	Oil Leak Slew motor	Operator called supervisor to assist, machine walked into position for repair and clean up
28	06-Dec-19	1	Oil Leak Fan pipe	Minimal mitigation required. Fan pipe repaired
29	06-Dec-19	1	Oil Spill Joint hose O-ring	Machine shutdown. New O-ring found and fitted.
30	18-Dec-19	1	Oil Spill Lock-up hose failure	Machine isolated and oil spill controlled and contained to ensure minimal oil loss after failure.
31	19-Dec-19	1	Oil Spill Bunded fuel farm	The spill has been absorbed by the use of spill sorb
33	20-Dec-19	1	Oil Spill Park brake filter tube	Machine isolated and oil spill controlled and contained to ensure minimal oil loss after failure. Spill sorb used to mitigate
		I		Owen
1	13-Feb-19	Nil	Oil Leak	Supervisor requested a subcontractor to clean-up the hydraulic oil stain and realign the hydraulic oil tray into place to capture all potential oil leaked.
2	23-Mar-19	1	Oil Leak Hydraulic - minor	The Operator of truck RD2743 immediately shut down the truck. Contaminated material was taken to the Bioremediation area.
3	28-Mar-19	1	Oil Spill	The Operator immediately lowered his bucket to the ground, shut the machine down and released the pressure valve: Contaminated material was recovered and taken to the bioremediation area
4	22-Apr-19	1	Diesel Spill	The fuel cart Operator immediately shut the refuelling truck off. The diesel spill was contained, the contaminated material was recovered and taken to the bioremediation pad
5	12-May-19	1	Oil Spill Hydraulic	Immediately shutdown the loader The hydraulic oil spill was contained and the contaminated material was taken to the bioremediation area
6	04-Jun-19	1	Spill Coolant Oil Spill	The Operator immediately shut down the grader The spills were contained within the reject material and removed to the bio remedial area and recorded.
7	20-Jun-19	1	Oil Spill Hydraulic	Immediately shutdown the drill The hydraulic oil spill was contained and the contaminated material was taken to the bioremediation area.
8	12-Aug-19	1	Oil Spill Hydraulic Oil	The spill was contained, contaminated material was relocated to the bioremediation area and recorded. The blown hose was replaced and hydraulic oil topped up.
9	26-Aug-19	Nil	Noise Attended noise monitoring loss of recording data.	In order to ensure adequate storage capacity is available for the buffer data, Umwelt's monitoring procedures have been updated, to include a step to download and clear all buffer data prior to the commencement of the each noise monitoring session, with noise data also downloaded daily from noise logger to ensure data is collected and the storage capacity within the noise logger is maximised.
10	21-Oct-19	Nil	Oil Leak Hydraulic - minor	The tank was inspected no signs of an active leakage were observed. Clean up of the hydraulic oil stain, implemented strategic options to prevent reoccurrence.
11	10-Nov-19	1	Oil Leak Hydraulic Oil	The operator immediately shut down the excavator The spill was contained contaminated material taken to the bioremediation area.

Appendix D: Noise

Table 3: MGO Noise Monitoring Locations

Monitoring Location	Description of Monitoring Location	Property Location Reference
Sx1	Continuous noise unit located on Property 86	Mt Owen EIS
Sx4	Continuous noise unit located on Property 109	Mt Owen EIS
Sx5	Mt Owen reference continuous noise unit located south east of Mt Owen Mine on Property 66.	Mt Owen EIS
Sx6	Mobile Continuous Noise unit – used for targeted monitoring	-
Sx7	Continuous noise unit located to the south of the Glendell Pit	-
SX11	Refurbsed Mobile Continuous Noise unit – used for targeted monitoring	-
Sx12	Continuous noise unit located near Property 31	Glendell EA
Sx122	Mobile Continuous Noise unit – used for targeted monitoring	-
Sx13 M8	Meteorological station located to the west of Mt Owen Mine	-
Sx13 M1	Meteorological station located to the west of Glendell Mine	-
Sx13 M2	Meteorological station located to the east of Glendell Mine	-
N1	Greenlands, to the west of Property 54	Mt Owen EIS
N2	Falbrook Road, adjacent to Property 71	Mt Owen EIS
N3	Corner of Falbrook and Middle Falbrook Road	-
N4	Glennies Creek Road adjacent to Property 109	Mt Owen EIS
N8	South of Camberwell Village at Property 7a	Glendell EA
N9	Camberwell Village (central section) adjacent to Property R47	Glendell EA
N10	Camberwell Village (western section) adjacent to Property R27	Glendell EA
N11	Glennies Creek Road adjacent to Property R37a	Glendell EA
N17*	Representative of the rural residence on Scrumlo Road, Hebden near property R134	Mt Owen EIS

^{*}Monioring point added to EPL 4460 on 19th of September 2019. MGO have included N17 on its recelty submitted (not yet approved) Noise Management Plan and results will be provided in the next annual report. Alternatively, EPL noise report has been made publically available on the MGO website

(https://www.mtowencomplex.com.au/en/environment/environmental-monitoring/Pages/mtowen-complex-noise-monitoring-report.aspx)

Table 4: Summary of Attended Noise Monitoring - Summer (January) 2019, dB(A)

Location	Start Time	Mea	sured Noise L	evels		Estimated ¹ Mt Owen Contribution		l¹ Glendell bution	Local Meteorological Conditions ²			
Locution	(15 min period)	LA90, 15min	LAeq, 15min	LA1, 1 min	LAeq, 15min	LA1, 1 min	LAeq, 15min	LA1, 1 min	Local motoriological conditions			
Night-time Period – 22, 23, 28-29 January 2019												
N1	23:19:00	37.8	42.1	47.4	< 25.0	< 25.0	Not Audible	Not Audible	Wind NW at 4.9 m/s, 0/8 octa cloud cover, 32 °C, 46% RH			
N2	23:54:00	28.1	29.5	39.0	< 30.0	33.0	Not Audible	Not Audible	Wind NW at 5.5 m/s, 0/8 octa cloud cover, 33 °C, 42% RH			
N3	0:27:00	31.4	50.7	74.7	31.0	35.0	< 30.0	< 30.0	Wind NW at 4.6 m/s, 0/8 octa Cloud cover, 34 °C, 41% RH			
N4	1:02:00	36.3	45.8	69.1	Not Audible	Not Audible	< 30.0	34.0	Wind W at 2.9 m/s, 0/8 octa Cloud cover, 35 °C, 38% RH			
N8	23:34:00	38.6	43.7	53.7	Not Audible	Not Audible	< 30.0	33.0	Wind SSE at 4.1 m/s, 0/8 octa Cloud cover, 26 °C, 76% RH			
N9	22:17:00	35.6	46.1	67.0	Not Audible	Not Audible	Not Audible	Not Audible	Wind SSE at 4.9 m/s, 0/8 octa Cloud cover, 26 °C , 75% RH			
N10	22:49:00	32.3	38.3	48.4	Not Audible	Not Audible	Not Audible	Not Audible	Wind SSE at 4 m/s, 0/8 octa Cloud cover, 26 °C, 76% RH			
N11	0:13:00	34.5	39.0	52.3	Not Audible	Not Audible	Not Audible	Not Audible	Wind SSE at 3.4 m/s; 0/8 octa Cloud cover, 25 °C, 77% RH			

¹ Assessed by the operator during the monitoring session.

Meteorological conditions are a summary of meteorological data from the attended monitoring period from a Kestrel 4500 weather monitor, Serial Number 658027, positioned within 5 metres and at a corresponding height of the noise monitoring microphone.

Table 5: Summary of Attended Noise Monitoring - Summer (February) 2019, dB(A)

Location	Start Time	Meas	sured Noise L	evels		l¹ Mt Owen bution		d¹ Glendell ibution	Local Meteorological Conditions ²				
Location	(15 min period)	LA90, 15min	LAeq, 15min	LA1, 1 min	LAeq, 15min	LA1, 1 min	LAeq, 15min	LA1, 1 min	Local Meteorological Conditions-				
					Day Pe	riod – 26 February	y 2019						
N1	17:45	31.2	36.7	47.3	< 25.0	Not audible	Not audible	Not audible	Wind SE at 3.6 m/s, 5/8 octa cloud cover, 29 °C, 37% RH				
N2	17:22	35.6	33.7	46.0	< 25.0	Not audible	Not audible	Not audible	Wind S at 2.5 m/s, 6/8 octa cloud cover, 29 °C, 36% RH				
N3	16:58	25.8	58.2	77.6	Not audible	Not audible	Not audible	Not audible	Wind S at 3.6 m/s 6/8 octa cloud cover, 29 °C, RH 34% RH				
	Evening Period – 26 February 2019												
N1	21:14	37.3	38.5	44.2	< 25.0	Not audible	Not audible	Not audible	Wind S at 2.3 m/s; 2/8 octa cloud cover, 24 °C, 64% RH				
N2	20:39	24.3	26.3	36.2	< 25.0	Not audible	Not audible	Not audible	Wind SSE at 2.9 m/s; 5/8 octa cloud cover, 25 °C, 59% RH				
N3	20:09	31.4	46.3	65.2	Not audible	Not audible	Not audible	Not audible	Wind SE at 4.5 m/s; 5/8 octa cloud cover, 25 °C, 57% RH				
					Night-time F	Period – 25-27 Feb	ruary 2019						
N1	00:04	29.2	30.2	32.3	< 20.0	< 25.0	Not audible	Not audible	Wind S at 1.3 m/s; 2/8 octa cloud cover, 20 °C, 77% RH				
N2	23:35	24.4	25.1	28.7	< 25.0	27.0	Not audible	Not audible	Wind S at 1.9 m/s; 1/8 octa cloud cover, 21 °C, 76% RH				
N3	23:02	27.2	32.1	38.9	30.0	39.0	Not audible	Not audible	Wind S at 2.4 m/s; 1/8 octa cloud cover, 21 °C, 74% RH				
N4	22:34	35.1	37.1	44.3	36.0	42.0	Not audible	Not audible	Wind S at 2.2 m/s; 1/8 octa cloud cover, 22 °C, 72% RH				
N8	00:41	35.1	39.4	55.7	Not audible	Not audible	< 25.0	Not audible	Wind S at 2.4 m/s; 0/8 octa cloud cover, 18 °C, 80% RH				
N9	23:35	33.0	42.3	51.0	Not audible	Not audible	< 25.0	Not audible	Wind SE at 3.3 m/s; 0/8 octa cloud cover, 19 °C, 76% RH				
N10	22:26	36.7	42.9	54.4	Not audible	Not audible	Not audible	Not audible	Wind SE at 4.0 m/s; 0/8 octa cloud cover, 20 °C, 72% RH				
N11	22:00	36.8	39.9	45.8	Not audible	Not audible	Not audible	41.7	Wind SE at 3.9 m/s; 0/8 octa cloud cover, 20 °C, 70% RH				

¹ Assessed by the operator during the monitoring session.

Meteorological conditions are a summary of meteorological data from the attended monitoring period from a Kestrel 4500 weather monitor, Serial Number 655400, positioned within 5 metres and at a corresponding height of the noise monitoring microphone.

Table 6: Summary of Attended Noise Monitoring - Autumn (March) 2019 dB(A)

Location	Start Time	Mea	sured Noise L	evels		Estimated ¹ Mt Owen Contribution		¹ Glendell bution	Local Meteorological Conditions ²				
Location	(15 min period)	LA90, 15min	LAeq, 15min	LA1, 1 min	LAeq, 15min	LA1, 1 min	LAeq, 15min	LA1, 1 min	Local Meteorological conditions				
	Night-time Period – 26 – 28 March 2019												
N1	0:20:00	25.0	28.0	41.0	< 25.0	45.0	Not audible	Not audible	Wind SE at 2.5 m/s; 1/8 octa cloud cover, 18 °C, 70% RH				
N2	23:47:00	27.0	30.0	35.0	< 30.0	Not audible	Not audible	Not audible	Wind SE at 2.6 m/s; 0/8 octa cloud cover, 19 °C, 70% RH				
N3	23:16:00	26.0	28.0	37.0	<25.0	45.0	Not audible	Not audible	Wind SE at 2.4 m/s; 0/8 octa cloud cover, 19 °C, 70% RH				
N4	22:46:00	34.0	37.0	43.0	Not audible	50.0	Not audible	Not audible	Wind SE at 2.4 m/s; 2/8 octa cloud cover, 19 °C, 70% RH				
N8	22:23:00	33.0	37.0	44.0	Not audible	Not audible	Not audible	Not audible	Wind E at 1.4 m/s; 1/8 octa cloud cover, 19 °C, 70% RH				
N9	0:24:00	37.0	41.0	55.0	Not audible	45.0	Not audible	Not audible	Wind SE at 1.6 m/s; 0/8 octa cloud cover, 19 °C, 70% RH				
N10	22:09:00	37.0	42.0	52.0	Not audible	45.0	Not audible	Not audible	Wind E at 1.3 m/s; 0/8 octa cloud cover, 18 °C, 70% RH				
N11	0:20:00	25.0	28.0	41.0	< 25.0	45.0	Not audible	Not audible	Wind SEE at 2.7 m/s; 2/8 octa cloud cover, 20 °C, 70% RH				

¹ Assessed by the operator during the monitoring session.

Meteorological conditions are a summary of meteorological data from the attended monitoring period from a Kestrel 4500 weather monitor, Serial Number 645400, positioned within 5 metres and at a corresponding height of the noise monitoring microphone.

Table 7: Summary of Attended Noise Monitoring - Autumn (April) 2019, dB(A)

Location	Start Time	Meas	ured Noise L	evels	Estimated ¹ Mt Owen Contribution		Estimated ¹ Glendell Contribution		Local Meteorological Conditions ²				
Location	(15 min period)	LA90, 15min	LAeq, 15min	LA1, 1 min	LAeq, 15min	LA1, 1 min	LAeq, 15min	LA1, 1 min	Local Meteorological Conditions				
	Night-time Period – 16-17 April 2019												
N1	21:07:00	23.0	26.0	36.0	Not audible	Not audible	Not audible	Not audible	Wind S at 0.6 m/s; 0/8 octa cloud cover, 18 °C, 88% RH				
N2	21:41:00	28.0	32.0	43.0	Not audible	Not audible	Not audible	Not audible	Wind S at 0. 0 m/s; 0/8 octa cloud cover, 17 °C, 89% RH				
N3	22:08:00	26.0	42.0	65.0	Not audible	Not audible	Not audible	Not audible	Wind W at 0. 0 m/s; 0/8 octa cloud cover, 16 °C, 89% RH				
N4	22:37:00	36.0	39.0	50.0	Not audible	Not audible	Not audible	Not audible	Wind SW at 1.3 m/s; 1/8 octa cloud cover, 16 °C, 90% RH				
N8	22:56:00	35.0	40.0	52.0	Not audible	Not audible	<30.0	<30.0	Wind S at 0.4 m/s; 0/8 octa cloud cover, 17 °C, 88% RH				
N9	21:56:00	39.0	45.0	54.0	Not audible	Not audible	<30.0	32.0	Wind S at 0.0 m/s; 0/8 octa cloud cover, 17 °C, 86% RH				
N10	21:06:00	37.0	40.0	49.0	Not audible	Not audible	<30.0	<30.0	Wind S at 0.0 m/s; 0/8 octa cloud cover, 18 °C, 83% RH				
N11	23:26:00	38.0	41.0	51.0	Not audible	Not audible	Not audible	Not audible	Wind SSW at 0.0 m/s; 1/8 octa cloud cover, 16 °C, 91% RH				

¹ Assessed by the operator during the monitoring session.

Meteorological conditions are a summary of meteorological data from the attended monitoring period from a Kestrel 4500 weather monitor, Serial Number 658027, positioned within 5 metres and at a corresponding height of the noise monitoring microphone.

Table 8: Summary of Attended Noise Monitoring -Autumn (May) 2019, dB(A)

	Start Time	Mea	sured Noise Le	evels		I ¹ Mt Owen ibution	Estimated ¹ Glen	dell Contribution	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
Location	(15 min period)	LA90, 15min	LAeq, 15min	LA1, 1 min	LAeq, 15min	LA1, 1 min	LAeq, 15min	LA1, 1 min	Local Meteorological Conditions ²
					Day	Period – 30 May 20	019		
N1	17:40	36.3	51.2	75.7	< 25.0	Not applicable	Not applicable	Not applicable	Wind NW at 5.6 m/s; 8/8 octa cloud cover, 12.8 °C, 50% RH
N2	1710	38.2	40.6	47.1	40.0	Not applicable	Not applicable	Not applicable	Wind NW at 5.3 m/s; $8/8$ octa cloud cover, 13.2 °C, 48% RH
N3	16:43	41.8	55.6	75.2	< 32.0	Not applicable	Not applicable	Not applicable	Wind NW at 4.6 m/s ; $8/8 \text{ octa cloud cover}$, $13.8 ^{\circ}\text{C}$, $45\% \text{ RH}$
					Eveni	ng Period 30 May	2019		
N1	18:54	39.2	52.9	78.0	< 30	Not applicable	Not applicable	Not applicable	Wind NW at 4.9 m/s; 8/8 octa cloud cover, 11.4 °C, 54% RH
N2	18:20	40.4	42.1	48.2	41	Not applicable	Not applicable	Not applicable	Wind NW at 4.8 m/s ; $8/8 \text{ octa cloud cover}$, $11.9 ^{\circ}\text{C}$, $52\% \text{ RH}$
N3	19:26	42.3	56.6	75.7	< 32.0	Not applicable	Not applicable	Not applicable	Wind NW at 4.9 m/s ; $8/8 \text{ octa cloud cover}$, $11.0 ^{\circ}\text{C}$, $54\% \text{ RH}$
					Night-tim	e Period – 30-31 M	lay 2018		
N1	23:23:00	40.0	44.0	51.0	< 30.0	39.0	Not applicable	Not applicable	Wind NW at 7.2 m/s; 8/8 octa cloud cover, 8.1 °C, 67% RH
N2	23:58:00	39.0	42.0	51.0	39.0	51.0	Not applicable	Not applicable	Wind NW at 6.4 m/s; $8/8$ octa cloud cover, 7.9 °C, 67% RH
N3	0:28:00	43.0	55.0	78.0	< 32.0	43.0	Not applicable	Not applicable	Wind NW at 6 m/s; 8/8 octa cloud cover, 7.2 °C, 68% RH
N4	0:59:00	40.0	44.0	53.0	< 30.0	46.0	< 30.0	< 45.0	Wind NW at 6.1 m/s; 8/8 octa cloud cover, 7.5 °C, 68% RH
N8	2:27:00	38.0	41.0	48.0	Not applicable	Not applicable	< 35.0	43.0	Wind NW at 4.4 m/s; 8/8 octa cloud cover, 7.0 °C, 70% RH
N9	21:00:00	42.0	50.0	70.0	Not applicable	Not applicable	< 42.0	45.0	Wind NW at 4.9 m/s; 8/8 octa cloud cover, 9.8 °C, 58% RH
N10	21:31:00	39.0	43.0	49.0	< 20.0	33.0	39.0	45.0	Wind NW at 4.2 m/s; $8/8$ octa cloud cover, 9.4 °C, 60% RH
N11	23:23:00	40.0	44.0	51.0	< 30.0	39.0	Not applicable	Not applicable	Wind NW at 5.2 m/s; $8/8$ octa cloud cover, 7.3 °C, 69% RH

¹ Assessed by the operator during the monitoring session.

Meteorological conditions are a summary of meteorological data from the attended monitoring period from a Kestrel 4500 weather monitor, Serial Number 645400, positioned within 5 metres and at a corresponding height of the noise monitoring microphone

Table 9: Summary of Attended Noise Monitoring - Winter (June) 2019, dB(A)

Location	Start Time (15	Meas	ured Noise L	evels	Estimated ¹ Mt Owen Contribution		Estimated ¹ Glendell Contribution		Local Matagraph grical Conditions?			
Location	min period)	LA90, 15min	LAeq, 15min	LA1, 1 min	LAeq, 15min	LA1, 1 min	LAeq, 15min	LA1, 1 min	Local Meteorological Conditions ²			
Night-time Period – 19-20 and 26-27 June 2019												
N1	23:33:00	23.0	26.0	41.0	Not audible	Not audible	Not audible	Not audible	Wind NNW at 0.6 m/s; 8/8 octa cloud cover, 7.3 °C, 88% RH			
N2	22:47:00	31.0	33.0	37.0	33.0	40.0	Not audible	Not audible	Wind N at 1.2 m/s; 8/8 octa cloud cover, 7.3 °C, 85% RH			
N3	0:13:00	31.0	33.0	41.0	< 21.0	33.0	Not audible	Not audible	Wind NNE at 0.7 m/s; 8/8 octa cloud cover, 7.3 °C, 89% RH			
N4	1:31:00	37.0	42.0	52.0	Not audible	Not audible	Not audible	Not audible	Wind SE at 1.3 m/s; 2/8 octa cloud cover, 7.3 °C, 99% RH			
N8	0:15:00	35.0	38.0	45.0	Not audible	Not audible	Not audible	Not audible	Wind S at 1.8 m/s; 3/8 octa cloud cover, 7.3 °C, 97% RH			
N9	22:41:00	35.0	45.0	54.0	Not audible	Not audible	Not audible	Not audible	Wind E at 0.5 m/s; 5/8 octa cloud cover, 7.3 °C, 93% RH			
N10	23:40:00	38.0	41.0	50.0	Not audible	Not audible	Not audible	Not audible	Wind SE at 1.8 m/s; 5/8 octa cloud cover, 7.3 °C, 96% RH			
N11	1:31:00	37.0	42.0	52.0	Not audible	Not audible	Not audible	Not audible	Wind E at 0.8 m/s; 2/8 octa cloud cover, 7.3 °C, 97% RH			

¹ Assessed by the operator during the monitoring session.

Meteorological conditions are a summary of meteorological data from the attended monitoring period from a Kestrel 4500 weather monitor, Serial Number 658027, positioned within 5 metres and at a corresponding height of the noise monitoring microphone

Table 10: Summary of Attended Noise Monitoring - Winter (July) 2019, dB(A)

Location	Start Time	Meas	ured Noise Lo	evels		¹ Mt Owen bution	Estimated ¹ Glendell Contribution		Local Meteorological Conditions ²				
Location	(15 min period)	LA90, 15min	LAeq, 15min	LA1, 1 min	LAeq, 15min	LA1, 1 min	LAeq, 15min	LA1, 1 min	Local incleorological conditions				
	Night-time Period – 17, 19, and 24 July 2019												
N1	0:00:00	31.0	32.0	36.0	32.0	36.0	Not audible	Not audible	Wind NW at 4.1 m/s; 8/8 octa cloud cover, 11.8 °C, 53% RH				
N2	0:34:00	38.0	42.0	48.0	42.0	55.0	Not audible	Not audible	Wind NW at 04.2 m/s; 8/8 octa cloud cover, 11.4 °C, 53% RH				
N3	2:32:00	34.0	36.0	40.0	< 38.0	< 45.0	< 30	< 40.0	Wind NW at 2.4 m/s; 8/8 octa cloud cover, 10.5 °C, 64% RH				
N4	1:06:00	40.0	48.0	54.0	Not audible	Not audible	Not audible	Not Audible0.0	Wind NW at 4.7 m/s; 8/8 octa cloud cover, 11.1 °C,55% RH				
N8	21:56:00	32.0	33.0	38.0	Not audible	Not audible	Not audible	Not audible	Wind N at 1.4 m/s; 8/8 octa cloud cover, 12.0 °C, 56% RH				
N9	21:24:00	32.0	48.0	56.0	Not audible	Not audible	< 30	31	Wind NNE at 0.6 m/s; 8/8 octa cloud cover, 12.4 °C, 55% RH				
N10	23:57:00	34.0	44.0	51.0	Not audible	Not audible	< 25	< 30	Wind SE at 0.7 m/s; 8/8 octa cloud cover, 14.4 °C, 47% RH				
N11	0:00:00	38.0	41.0	45.0	Not audible	Not audible	Not audible	Not audible	Wind NNW at 1.5 m/s; 8/8 octa cloud cover, 11.6 °C, 58% RH				

¹ Assessed by the operator during the monitoring session.

Meteorological conditions are a summary of meteorological data from the attended monitoring period from a Kestrel 4500 weather monitor, Serial Number 658027, positioned within 5 metres and at a corresponding height of the noise monitoring microphone.

Table 11: Summary of Attended Noise Monitoring - Winter (August) 2019, dB(A)

Location	Start Time	Meas	sured Noise L	evels		1 Mt Owen bution		d¹ Glendell ibution	Local Meteorological Conditions ²
LUCALIUII	(15 min period)	LA90, 15min	LAeq, 15min	LA1, 1 min	LAeq, 15min	LA1, 1 min	LAeq, 15min	LA1, 1 min	Local Meteorological Conditions
					Day P	eriod – 31 August	2019		
N1	10:51	44	51	60	< 30.0	Not audible	Not audible	Not audible	Wind S at 4.9 m/s; 8/8 octa cloud cover, 13.2 °C, 91% RH
N2	11:26	44	51	63	32.0	Not audible	Not audible	Not audible	Wind S at 2.2 m/s; 8/8 octa cloud cover, 13.9 °C, 90% RH
N3	12:00	44	60	75	Not audible	Not audible	Not audible	Not audible	Wind S at 1.7 m/s; 8/8 octa cloud cover, 14.8 °C, 88.4% RH
					Evening	Period – 26 Augu	ıst 2019		
N1	21:44	26	29	45	< 20	Not audible	Not audible	Not audible	Wind SSE at 2.7 m/s; 6/8 octa cloud cover, 14.5 °C, 77% RH
N2	21:21	29	31	39	< 30	Not audible	Not audible	Not audible	Wind SSE at 2.3 m/s; 6/8 octa cloud cover, 14.6 °C, 77% RH
N3	20:58	28	30	36	Not audible	Not audible	Not audible	Not audible	Wind SSE at 3.1 m/s; 8/8 octa cloud cover, 14.4 °C, 78% RH
					Night-time Pe	riod – 20,21,23,24	August 2019		
N1	22:05:00	26.0	27.0	38.0	< 20	25	Not audible	Not audible	Wind SSE at 2.5 m/s; 2/8 octa cloud cover, 14.5 °C, 77% RH
N2	22:35:00	25.0	29.0	36.0	< 25	< 25	< 25	32	Wind S at 3 m/s; 6/8 octa cloud cover, 14.4 °C, 78% RH
N3	23:04:00	27.0	31.0	43.0	Not audible	Not audible	Not audible	Not audible	Wind SSE at 2 m/s; 8/8 octa cloud cover, 14.4 °C, 78% RH
N4	23:34:00	31.0	38.0	58.0	Not audible	Not audible	Not audible	Not audible	Wind SSE at 1.6 m/s; 8/8 octa cloud cover, 14.3 °C, 78% RH
N8	23:02:00	30.0	35.0	53.0	Not audible	Not audible	Not audible	Not audible	Wind SSE at 0.4 m/s; 8/8 octa cloud cover, 10.6 °C, 69% RH
N9	21:39:00	37.0	50.0	62.0	Not audible	Not audible	Not audible	Not audible	Wind S at 0.2 m/s; 8/8 octa cloud cover, 11.5 °C, 64% RH
N10	21:12:00	33.0	39.0	51.0	Not audible	Not audible	Not audible	Not audible	Wind SSE at 0.6 m/s; 4/8 octa cloud cover, 12.5 °C, 762% RH
N11	0:06:00	33.0	39.0	57.0	Not audible	Not audible	Not audible	Not audible	Wind SSE at 2.1 m/s; 4/8 octa cloud cover, 14.3 °C, 79% RH

Assessed by the operator during the monitoring session.

Meteorological conditions are a summary of meteorological data from the attended monitoring period from a Kestrel 4500 weather monitor, Serial Number 658027, positioned within 5 metres and at a corresponding height of the noise monitoring microphone

Table 12: Summary of Attended Noise Monitoring - Spring (September) 2019, dB(A)

Location	Start Time	Meas	sured Noise Lo	evels		¹ Mt Owen bution		d¹ Glendell ibution	Local Meteorological Conditions ²
Location	(15 min period)	LA90, 15min	LAeq, 15min	LA1, 1 min	LAeq, 15min	LA1, 1 min	LAeq, 15min	LA1, 1 min	Local Meteorological Conditions
					Day Per	iod – 20 Septemb	er 2019		
N1	11:32	34	56	74	Not audible	Not audible	Not audible	Not audible	Wind S at 1.8 m/s; 1/8 octa cloud cover, 23.2 °C, 91% RH
N2	12:06	33	42	60	< 30	Not audible	Not audible	Not audible	Wind E at 2.5 m/s; 1/8 octa cloud cover, 22.6 °C, 90% RH
N3	12:38	33	56	81	< 30	Not audible	Not audible	Not audible	Wind E at 2.4 m/s; 1/8 octa cloud cover, 23.2 °C, 88.4% RH
					Evening P	eriod – 19 Septen	nber 2019		
N1	19:02	38	42	50	Not audible	Not audible	Not audible	Not audible	Wind SSE at 5 m/s; 8/8 octa cloud cover, 18.2 °C, 77% RH
N2	19:33	34	37	50	< 30	Not audible	Not audible	Not audible	Wind SSE at 4.9 m/s; 6/8 octa cloud cover, 18 °C, 78% RH
N3	20:04	33	55	78	< 30	Not audible	Not audible	Not audible	Wind SSE at 4.3 m/s; 4/8 octa cloud cover, 17.8 °C, 79% RH
					Night-time Per	iod – 19, 24-25 Se	ptember 2019		
N1	21:00:00	35.0	42.0	63.0	Not audible	Not audible	Not audible	Not audible	Wind S at 3.9 m/s; 4/8 octa cloud cover, 17.5 °C, 81% RH
N2	21:29:00	33.0	35.0	45.0	< 25.0	< 25.0	Not audible	Not audible	Wind S at 4.2 m/s; 6/8 octa cloud cover, 17.5 °C, 81% RH
N3	22:00:00	32.0	33.0	39.0	< 25.0	< 25.0	Not audible	Not audible	Wind S at 3.5 m/s; 2/8 octa cloud cover, 17.34 °C, 81% RH
N4	23:16:00	36.0	38.0	45.0	Not audible	Not audible	< 30.0	< 35.0	Wind N at 1.1 m/s; 8/8 octa cloud cover, 10.9 °C,778% RH
N8	0:32:00	35.0	39.0	51.0	Not audible	Not audible	Not audible	Not audible	Wind N at 2.8 m/s; 8/8 octa cloud cover, 9.7 °C, 80% RH
N9	21:44:00	39.0	47.0	55.0	Not audible	Not audible	< 35.0	< 40.0	Wind S at 1.5 m/s; 8/8 octa cloud cover, 12.9 °C, 69% RH
N10	21:09:00	39.0	42.0	53.0	Not audible	Not audible	< 36.0	< 40.0	Wind S at 2.4 m/s; 8/8 octa cloud cover, 12.9 °C, 64% RH
N11	23:53:00	39.0	42.0	55.0	Not audible	Not audible	Not audible	Not audible	Wind NW at 2.3 m/s; 8/8 octa cloud cover, 10.3 °C, 78% RH

¹ Assessed by the operator during the monitoring session.

Meteorological conditions are a summary of meteorological data from the attended monitoring period from a Kestrel 4500 weather monitor, Serial Number 658027, positioned within 5 metres and at a corresponding height of the noise monitoring microphone.

Table 13: Summary of Attended Noise Monitoring - Spring (October) 2019, dB(A)

Location	Start Time (15	Meas	ured Noise Le	evels	Estimated ¹ Mt Owen Contribution		Estimated ¹ Glendell Contribution		Local Meteorological Conditions ²			
Location	min period)	LA90, 15min	LAeq, 15min	LA1, 1 min	LAeq, 15min	LA1, 1 min	LAeq, 15min	LA1, 1 min	Local meteorological contactorio			
Night Period – 9-11 October 2019												
N1	22:51:00	23.0	34.0	56.0	Not Audible	Not Audible	Not Audible	Not Audible	Wind SE at 1.8 m/s, 2/8 octa cloud cover, 13.54 ℃, 78% RH			
N2	22:06:00	23.0	29.0	44.0	Not Audible	Not Audible	Not Audible	Not Audible	Wind SE at 3.1 m/s, 1/8 octa cloud cover,14.0 °C, 76% RH			
N3	0:10:00	26.0	47.0	73.0	< 30.0	38.0	Not Audible	Not Audible	Wind S at 2.3 m/s, 1/8 octa cloud cover, 12.3 °C, 83% RH			
N4	1:09:00	35.0	40.0	50.0	< 30.0	< 30.0	Not Audible	Not Audible	Wind S at 2.1m/s, 1/8 octa cloud cover, 12.2 °C, 86% RH			
N8	23:23:00	30.0	37.0	50.0	Not Audible	Not Audible	Not Audible	Not Audible	Wind E at 1.5 m/s; 1/8 octa cloud cover, 13.3 °C, 72% RH			
N9	21:44:00	33.0	44.0	59.0	Not Audible	Not Audible	Not Audible	Not Audible	Wind SE at 3 m/s, 1/8 octa cloud cover, 14.0 °C, 68% RH			
N10	21:14:00	37.0	42.0	53.0	Not Audible	Not Audible	Not Audible	Not Audible	Wind SE at 6.2 m/s, 1/8 octa cloud cover, 15.0 °C, 63% RH			
N11	2:24:00	32.0	38.0	52.0	< 30.0	34.0	Not Audible	Not Audible	Wind S at 2.4 m/s, 2/8 octa cloud cover, 11.7 °C, 87% RH			

¹ Assessed by the operator during the monitoring session.

² Meteorological conditions are a summary of meteorological data from the attended monitoring period from a Kestrel 4500 weather monitor, Serial Number 658027, positioned within 5 metres and at a corresponding height of the noise monitoring microphone

Table 14: Summary of Attended Noise Monitoring - Spring (November) 2019, dB(A)

Location	Start Time	Measured Noise Levels		Estimated¹ Mt Owen Contribution		Estimated¹ Glendell Contribution		Local Meteorological Conditions ²	
Location	(15 min period)	LA90, 15min	LAeq, 15min	LA1, 1 min	LAeq, 15min	LA1, 1 min	LAeq, 15min	LA1, 1 min	
	Night Period – 11, 12, 14, 15 November 2019								
N1	0:19:00	31.0	41.0	57.0	< 25	< 30	Not audible	Not audible	Wind NW at 0.5 m/s, 1/8 octa cloud cover, 18.0 °C, 48% RH
N2	1:14:00	34.0	36.0	45.0	32	42	Not audible	Not audible	Wind NW at 1.2 m/s, 1/8 octa cloud cover, 18.0 °C, 50% RH
N3	1:47:00	35.0	38.0	44.0	37	44	Not Audible	Not Audible	Wind NW at 1.5 m/s, 1/8 octa cloud cover, 17.0 °C, 51% RH
N4	23:16:00	38.0	49.0	75.0	39	48	Not Audible	Not Audible	Wind NW at 0.5 m/s, 1/8 octa cloud cover, 20.0 ∘C,427% RH
N8	0:00:00	32.0	35.0	45.0	Not Audible	Not Audible	Not Audible	Not Audible	Wind NW at 2.4 m/s, 1/8 octa cloud cover, 22.0 °C, 39% RH
N9	21:45:00	42.0	49.0	59.0	Not Audible	Not Audible	<40.0	44.0	Wind NW at 5.1 m/s, 1/8 octa cloud cover, 25.0 °C, 31% RH
N10	2:10:00	36.0	39.0	50.0	Not Audible	Not Audible	<35.0	35.0	Wind NW at 4.3 m/s, 1/8 octa cloud cover, 26.0 °C, 31% RH
N11	23:22:00	34.0	39.0	51.0	Not Audible	Not Audible	Not audible	Not audible	Wind NW at 4.5 m/s, 1/8 octa cloud cover, 23.0 °C, 25% RH

Note 1: Assessed by the operator during the monitoring session.

Note 2: Meteorological conditions are a summary of meteorological data from the attended monitoring period from a Kestrel 4500 weather monitor, Serial Number 658027, positioned within 5 metres and at a corresponding height of the noise monitoring microphone.

Table 15: Summary of Attended Noise Monitoring - Summer (December) 2019, dB(A)

Location	Start Time	Measured Noise Levels		Estimated¹ Mt Owen Contribution		Estimated ¹ Glendell Contribution		Local Meteorological Conditions ²	
Location	(15 min period)	LA90, 15min	LAeq, 15min	LA1, 1 min	LAeq, 15min	LA1, 1 min	LAeq, 15min	LA1, 1 min	Local meteorological containers
Night Period – 3-4 December 2019									
N1	1:03:00	35.0	57.0	62.0	<30.0	40.0	Not Audible	Not Audible	Wind NW at 3.3 m/s, 1/8 octa cloud cover, 21.0 °C, 37% RH
N2	1:55:00	38.0	40.0	46.0	39.0	49.0	Not Audible	Not Audible	Wind NW at 2.8 m/s, 1/8 octa cloud cover, 20.0 °C, 41% RH
N3	0:06:00	41.0	44.0	52.0	<30.0	35.0	<35.0	<35.0	Wind NW at 5.1 m/s, 1/8 octa cloud cover, 22.0 °C, 35% RH
N4	23:16:00	35.0	41.0	55.0	<35.0	<35.0	<35.0	<35.0	Wind NW at 5.5 m/s, 1/8 octa cloud cover, 23.0 °C, 32% RH
N8	23:41:00	32.0	34.0	43.0	Not Audible	Not Audible	<30.0	<30.0	Wind NW at 4 m/s, 1/8 octa cloud cover, 24.0 °C, 25% RH
N9	21:30:00	41.0	52.0	77.0	Not Audible	Not Audible	<40.0	<45.0	Wind NW at 5.9 m/s, 1/8 octa cloud cover, 26.0 °C, 20% RH
N10	21:01:00	39.0	44.0	54.0	Not Audible	Not Audible	<35.0	<35.0	Wind NW at 5.4 m/s, 1/8 octa cloud cover, 27.0 °C, 19% RH
N11	23:04:00	37.0	40.0	50.0	Not Audible	Not Audible	Not Audible	Not Audible	Wind W at 2.7 m/s, 1/8 octa cloud cover, 25.0 °C, 24% RH

Note 1: Assessed by the operator during the monitoring session.

Note 2: Meteorological conditions are a summary of meteorological data from the attended monitoring period from a Kestrel 4500 (and Kestrel 5500) weather monitor, Serial Number 658027 (and SN 2420169), positioned within 5 metres and at a corresponding height of the noise monitoring microphone.

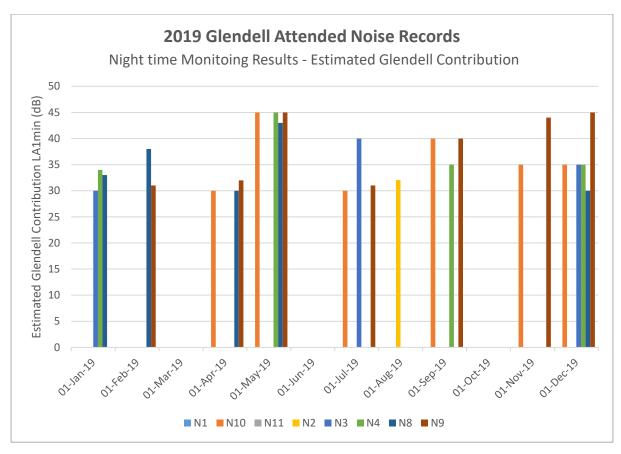


Figure 1: 2019 Attended Noise Records - Night time noise contribution - Glendell

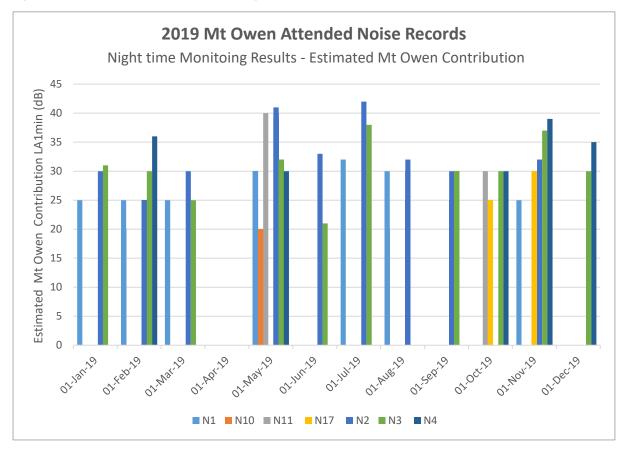


Figure 2: 2019 Attended Noise Records - Night time noise contribution - Mt Owen





GLENCORE

MACHINE SOUND POWER LEVEL TESTING

2019

Glendell Mine

FINAL

Prepared by
Umwelt (Australia) Pty Limited
on behalf of
Glencore

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Report No. 4545/R01
Date: July 2019

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Document Status

Rev No.	Reviewer		Approved for Issue		
	Name	Date	Name	Date	
Final	Tim Procter	04/07/2019	Luke Bettridge	05/07/2019	



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Machine Sound Power Level Testing 4545_R01_V2



1.0 Introduction

As per Glendell Mine's DPE approved Noise Management Plan, Glendell Mine is required to conduct periodic review of the noise performance of its equipment fleet. It is recommended that all fleet should be tested within a five year period.

Umwelt Australia Pty Ltd was engaged by Glencore to undertake sound power level (SWL) testing of a selection of mobile machines, listed in **Table 1.1**. testing was conducted on 21 March and 13 May 2019 at Glendell Mine.

Table 1.1 Tested Machines

Plant Type	Unit Number	Model	
Dozers	DZ 403	Cat D10T	
	DZ 401		
	DZ 492	Cat 854K	
Haul Truck	TR 205	Cat 793DXQ	
Water Carts	WT 642	Cat 777F WC	
	WT 643	Cat 777F WC	

Dynamic SWL testing was undertaken generally in accordance with the methodology presented in ISO 6395 and ISO 6393 for stationary (static) testing. In accordance with these standards, sound power is determined in one-third octave bands from 25 Hz to 10 kHz. However, Glendell Mine requires assessment in one-third octave bands from 12.5 Hz to 10 kHz. The SWL testing methodology used at Glendell mine is summarised in **Appendix A**. The calibration certificates for the sound measurement equipment can be found in **Appendix B**. The results for each machine tested is presented in detail in **Appendix C**.



2.0 Results

2.1 Measured Sound Power Levels

Dynamic SWL testing of equipment included the measurement of the following machines in representative operating conditions:

- dozers in 1st and 2nd gear forward and reverse motion on flat surfaces
- haul truck laden up-ramp and unladen down-ramp
- water carts laden up-ramp and laden down-ramp
- static SWL testing of the equipment included stationary testing of machines at the same test site surface used from the dynamic test.

Table 2.1 summarises the sound power level test results for each item of equipment tested. The detailed sound power level results are presented as one-third octave graphs in **Appendix C**. Results are presented as Linear (Z – weighted) and A-weighted¹ sound power levels.

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Results

¹ A-weighting is an adjustment made to sound level measurement, by means of an electronic filter, to approximate the response of the human ear.



Table 2.1 Sound Power Level Monitoring Results

Equipment Description		Mode of Operation	Dynamic				Static			
				Up or f	Up or Forward		Down or Reverse			
				dB(Z)	dB(A)	dB(Z)	dB(A)	dB(Z)	dB(A)	
Dozers	DZ 403	Cat D10T	1 st gear	116	108	120	112	117	107	
			2 nd gear	123	117	123	118			
	DZ 401	Cat D10T	1 st gear	122	110	123	110	121	109	
			2 nd gear	123	116	126	119			
	DZ 492	Cat 854K	1 st gear	115	108	114	109	115	107	
			2 nd gear	114	107	115	110			
Haul Truck	TR 205	Cat 793 DXQ	1 st up / 4 th down	124	116	121	113	120	113	
Water Carts	WT 642	Cat 777F WC	1 st up / 4 th down	127	116	120	114	127	116	
	WT 643	Cat 777F WC	1 st up / 4 th down	124	115	119	112	128	114	

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Results



2.2 Meteorological Conditions

The meteorological conditions at the time of the monitoring program are presented in Table 2.2.

Table 2.2 Local Meteorological Conditions (Sentinex13)

Date Wind Speed (m/s)		Temperature (°C)	Relative Humidity (%)		
21/03/2019	2.6 (0.0 – 8.6)	22.7 (18.5 – 28.3)	78.0 (50.7 - 93.9)		
13/05/2019	1.0 (0.0 – 2.5)	15.2 (8.4 – 21.9)	78.7 (54.3 – 91.3)		



3.0 Discussion

The Z and A-weighted sound power levels for machines in different modes of operation are presented in **Table 2.1**. The one-third octave bands of the sound power spectrum for each machine are included in **Appendix C. Table 3.1** compares the measured Z and A-weighted sound power levels to the target inservice Z-weighted sound power levels nominated in Glencore Noise Management Protocol GCAA-625378177-10238 (GCAA NMP) and the A-weighted sound power level targets for the Year 9 targets nominated in the Glendell Environmental Assessment 2007 (GEA, 2007).

Table 3.1 Comparison of Sound Power Levels Results to In-service Targets Nominated in the GCAA NMP and the Year 9 Proposed Fleet Specification Targets in (GEA, 2007)

Equipment Description			Mode of	Dynamic			GCAA	GEA,	
		Operation	Operation Up or Forward		Down or Reverse		NMP	2007 For/Rev ^a	
				dB(Z)	dB(A)	dB(Z)	dB(A)	dB(Z)	dB(A)
Dozers	DZ 403	Cat D10T	1 st gear	116	108	120	112	123	110/118
	DZ 401	Cat D10T	1 st gear	122	110	123	110	123	110/118
	DZ 492	Cat 854K	1 st gear	115	108	114	109	123	110/118
Haul Truck	TR 205	Cat 793 DXQ	1 st up/4 th down	124	116	121	113	123	115
Water Carts	WT 642	Cat 777F WC	1 st up/4 th down	127	116	120	114	125	114
	WT 643	Cat 777F WC	1 st up/4 th down	124	115	119	112	125	114

NOTE a – GEA, 2007 gives specific SWL targets for dozers in forward and reverse modes of operation. For other machines, only one SWL target is given for all modes of operation

DZ403 in 1st gear forward and 1st gear reverse is either at, or below both the GCAA NMP target for Z-weighted results and the GEA, 2007 targets for A-weighted results shown in **Table 3.1**. DZ403 results are also within a one-standard-deviation-envelope calculated from equivalent machines in Umwelt's sound power level database.

DZ401 in 1st gear forward and 1st gear reverse is either at, or below both the GCAA NMP target for Z-weighted results and the GEA, 2007 targets for A-weighted results shown in **Table 3.1.** DZ401 results are also within the one-standard-deviation-envelope for equivalent machines.

DZ492 in 1st gear forward and 1st gear reverse is either at, or below both the GCAA NMP target for Z-weighted results and the GEA, 2007 targets for A-weighted results shown in **Table 3.1.** DZ492 results are also within the one-standard-deviation-envelope for equivalent machines.

TR205 up-ramp laden Z-weighted and A-weighted results are both 1 dB above the GCAA NMP target and the GEA, 2007 target, respectively, but within the one-standard-deviation-envelope for equivalent machines. To reduce the Z and A-weighted level by 1 dB the sound power level of the exhaust side of the truck would have to be reduced by 3 dB in the 80 to 125 Hz frequency range. TR205 down-ramp unladen Z-weighted and A-weighted results are both below the GCAA NMP target and the GEA, 2007 target,

Machine Sound Power Level Testing 4545_R01_V2

Discussion

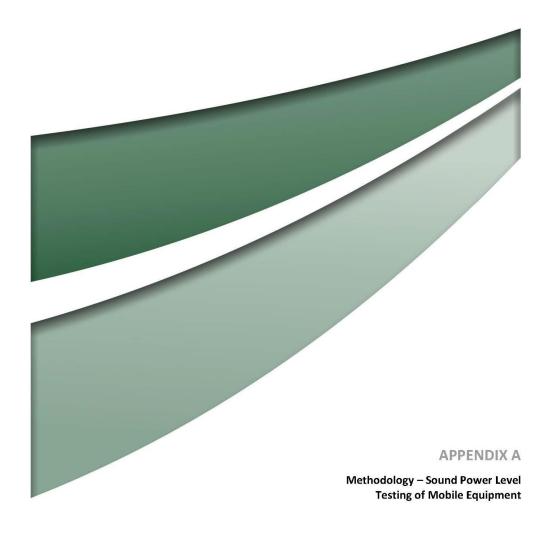


respectively. TR205 down-ramp unladen is quieter than the one-standard-deviation-envelope of equivalent machines in the Z and A-weighting.

WT642 up-ramp laden Z-weighted and A-weighted results are both 2 dB above the GCAA NMP target and the GEA, 2007 target, respectively. The A-weighted results is largely within the one-standard-deviation-envelope for equivalent machines except for the 80 Hz one-third octave band. To reduce the Z and A-weighted level by 2 dB the sound power level of the front and exhaust side of the truck would have to be reduced by 4 dB in the 80 Hz range. The dominance of the 80 Hz one-third octave level is clearly shown in the laden up-ramp chart for WT642 in **Appendix C**.

WT642 down-ramp laden Z-weighted and A-weighted results are either at, or below both the GCAA NMP target and the GEA, 2007 target shown in **Table 3.1**.

WT643 up-ramp laden Z-weighted result is below the GCAA NMP target and the A-weighted result is 1 dB above the GEA 2007 target but within the one-standard-deviation-envelope for equivalent machines. WT643 down-ramp laden is either at, or below both the GCAA NMP target for Z-weighted results and the GEA 2007 targets for A-weighted results shown in **Table 3.1**





A.1 Testing Standards

The monitoring program was conducted in accordance with:

MGD15 - Mobile and transportable plant for use on mines and petroleum sites (Amd. 2018)

ISO 6395:2008 – Earth-moving machinery - Determination of sound power level - Dynamic test conditions

 ${\sf ISO~6393:2008-Earth-moving~machinery-Determination~of~sound~power~level-Stationary~test~conditions}$

ISO 3744:2010 - Acoustics – Determination of sound power levels and sound energy levels of noise sources using sound pressure – Engineering methods for an essentially free field over a reflecting plane

ISO 4872 – Measurement of airborne noise emitted by construction equipment intended for outdoor use -- Method for determining compliance with noise limits

The monitoring program also took into consideration the requirements of:

AS 2012.2-1990 – Acoustics - Measurement of airborne noise emitted by earth-moving machinery and agricultural tractors - Stationary test condition, Operator's position

AS/NZS 1269.1-2005 - Occupational noise management - Measurement and assessment of noise emission and exposure

A.2 Equipment Used

The monitoring program was conducted using the following equipment

SVAN958A (59838) - four (4) channel sound and vibration analyser

SVAN958A (59839) - four (4) channel sound and vibration analyser

SVAN SV36 (90131) - 94/114 dB calibrator

Kestrel 4500 - weather meter

Calibration certificates are included in Appendix B.

A.3 Sound Power Level Testing

The monitoring program methodology is outlines as follows:

- Sound power levels have been determined in one-third octave bands.
- Glencore Noise Management Protocol GCAA-625378177-10238 (GCAA NMP) requires the
 measurements to be from 25 Hz to 10 kHz to enable reporting of Linear (Z-weighted) and A-weighting
 sound power levels. Data capture data from 12.5 Hz to 20 Hz has been included in the reporting of the
 monitoring data but not the determination of sound power levels. The 12.5 Hz to 20 Hz data can be
 used to assess low frequency noise and/or are often identifiable within the background acoustic
 environment.

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Appendix A

1



- Measurements made from six ISO microphones. Figure A.1 shows the horizontal (left image) and vertical (right image) positions of each microphone.
- The size of the measurement surface is determined as per ISO 6395:2008(E). This generally constitutes a radius of 16 20m to accommodate the tested haul trucks.

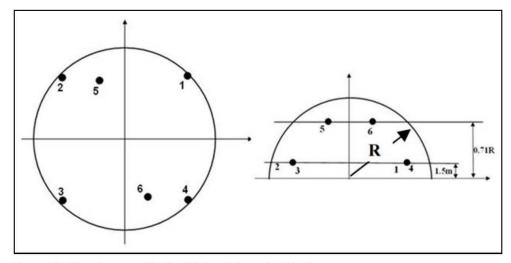


Figure A.1 - Microphone position for ISO Sound Power Level testing

A.4 Test Area Environment

The test areas included a haul road and flat dump area with sufficient length to allow machines to safely accelerate, pass through the test area and decelerate.

In accordance with ISO 6395 and GCAA NMP, the location of the test area was chosen to minimise the impacts of reflective surfaces such as highwalls and windrows.

Care was also taken to ensure that background noise levels were at least 6 dB less than measured equipment being tested. A correction is also applied for background levels between 6 dB - 15 dB less than measured dynamic levels to ensure that background noise has limited effect on measured levels. In addition to this, Mt Owen requires the background noise levels to be reported in one-third octave bands from 12.5 Hz to 10 kHz

The haul road test area had a nominal slope of approximately 10%. Testing consisted of uphill loaded test and a downhill unloaded test on the haul road. The dump area had a slope of approximately 0% to facilitate the forward and reverse testing of the bulldozers and rubber tyres dozer.

Machine Sound Power Level Testing 4545_R01_V2

Appendix A

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A.5 Mobile Equipment

Haul truck uphill loaded test

As per GCAA NMP, haul trucks are loaded with the nominal rated load and driven up hill through the test area while maintaining the manufacturers rated engine speed. Trucks progress at a consistent speed through the test area.

Haul truck downhill unloaded test

As per GCAA NMP, the unloaded haul truck moved downhill through the test area while maintaining the maximum descent speed considered safe (approximately 20-23 km/hr). Trucks progress at a consistent speed through the test area.

Water truck

As per GCAA NMP, uphill and downhill tests are conducted with the water truck operating with the maximum rated load

Bulldozer and loader 1st gear test forward and reverse

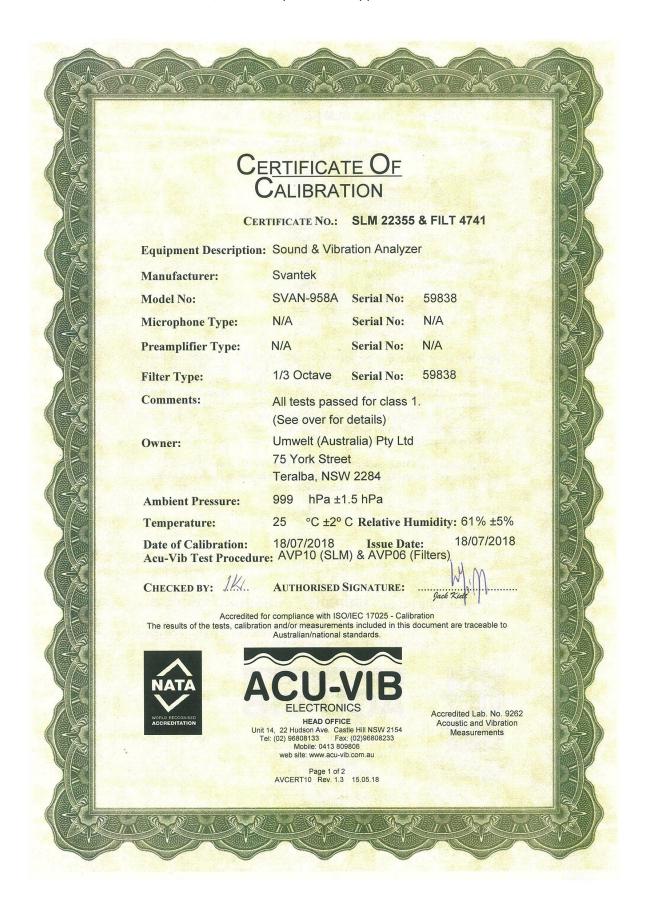
As per GCAA NMP, earthmoving machine moved through the test area unloaded in 1^{st} gear/ 2^{nd} gear at a constant speed with auxiliary equipment attached and raised to approximately 0.3 m above the test surface.

Bulldozer and loader 2nd gear test forward and reverse

To provided reference material for assessing machine performance and data for noise modelling purposes the earthmoving machine moved through the test area unloaded in 2nd gear at a constant speed with auxiliary equipment attached and raised to approximately 0.3 m above the test surface.

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CERTIFICATE No.: SLM 22355 & FILT 4741

The performance characteristics listed below were tested. The tests are based on the relevant clauses of IEC 61672-3:2013

Tests Performed:	Clause	Result
Absolute Calibration	10	N/A
Acoustical Frequency Weighting	12	N/A
Self Generated Noise	11.1	N/A
Electrical Noise	11.2	Entered
Long Term Stability	15	Pass
Electrical Frequency Weightings	13	Pass
Frequency and Time Weightings	14	Pass
Reference Level Linearity	16	Pass
Range Level Linearity	17	Pass
Toneburst	18	Pass
Peak C Sound Level	19	Pass
Overload Indicator	20	Pass
High Level Stability	21	Pass

Statement of Compliance: The sound level meter submitted for testing has successfully completed the class 1 periodic tests of IEC 61672-3:2013, for the environmental conditions under which the tests were performed. As public evidence was available, from an independent organization responsible for approving the results of pattern evaluation tests performed in accordance with IEC 61672-2:2013, to demonstrate that the model of sound level meter fully conformed to the requirements in IEC 61672-1:2013, the sound level meter submitted for testing conforms to the class 1 requirements of IEC61672-1:2013.

A full technical report is available if required.

This Sound Level Meter included an Octave Filter Set. Tests were based on IEC 1260: 1995 and AS/NZS 4476 - 1997 and were conducted to test the following performance characteristics:

1. Relative attenuation

clause 5.3

Date of Calibration: 18/07/2018 Issue Date: 18/07/2018

Checked by: Accredited for compliance with ISO/IEC 17025 - Calibration
The results of the tests, calibration and/or measurements included in this document are traceable to Australian/national standards.

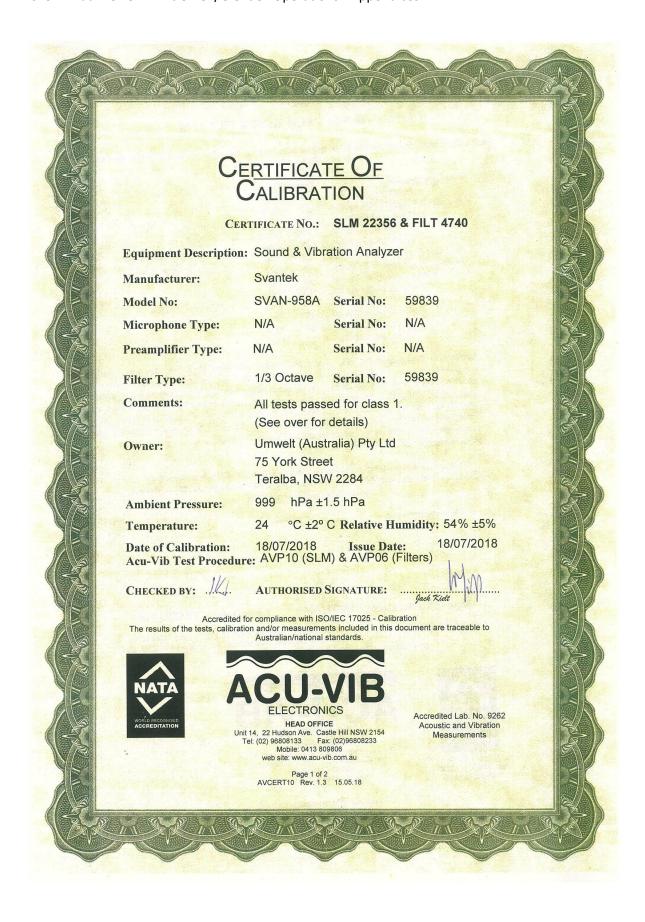


Accredited Lab. No. 9262 Acoustic and Vibration Measurements



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Page 2 of 2 End of Calibration Certificate
AVCERT10



CERTIFICATE NO.: SLM 22356 & FILT 4740

The performance characteristics listed below were tested. The tests are based on the relevant clauses of IEC 61672-3:2013

	Tests Performed:	Clause	Result
	Absolute Calibration	10	N/A
	Acoustical Frequency Weighting	12	N/A
	Self Generated Noise	11.1	N/A
	Electrical Noise	11.2	Entere
	Long Term Stability	15	Pass
	Electrical Frequency Weightings	13	Pass
	Frequency and Time Weightings	14	Pass
	Reference Level Linearity	16	Pass
	Range Level Linearity	17	Pass
	Toneburst	18	Pass
	Peak C Sound Level	19	Pass
	Overload Indicator	20	Pass
	High Level Stability	21	Pass

Statement of Compliance: The sound level meter submitted for testing has successfully completed the class 1 periodic tests of IEC 61672-3:2013, for the environmental conditions under which the tests were performed. As public evidence was available, from an independent organization responsible for approving the results of pattern evaluation tests performed in accordance with IEC 61672-2:2013, to demonstrate that the model of sound level meter fully conformed to the requirements in IEC 61672-1:2013, the sound level meter submitted for testing conforms to the class 1 requirements of IEC61672-1:2013. A full technical report is available if required.

This Sound Level Meter included an Octave Filter Set. Tests were based on IEC 1260: 1995 and AS/NZS 4476 - 1997 and were conducted to test the following performance characteristics:

1. Relative attenuation

clause 5.3

Date of Calibration: 18/07/2018

Issue Date: 18/07/2018

Checked by: /K/

by: Accredited for compliance with ISO/IEC 17025 - Calibration
The results of the tests, calibration and/or measurements included in
this document are traceable to Australian/national standards.

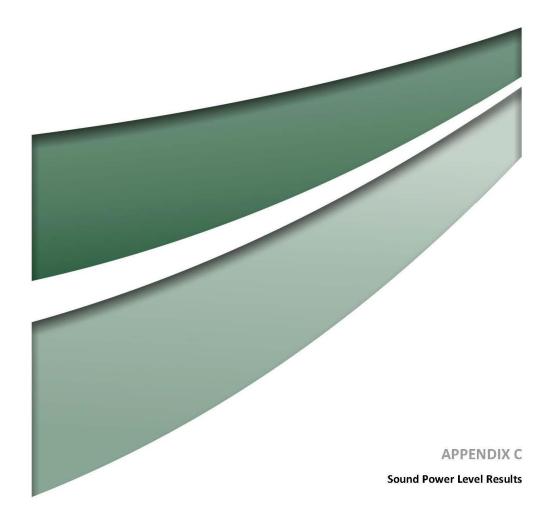


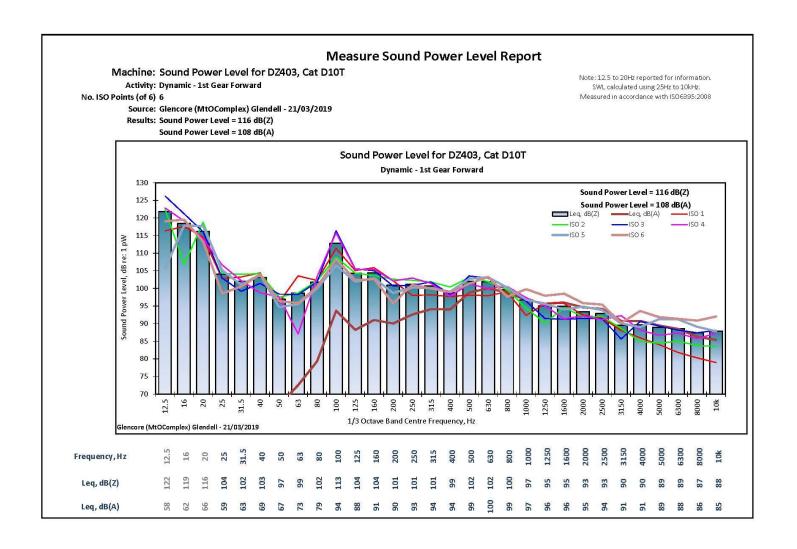
Accredited Lab. No. 9262 Acoustic and Vibration Measurements



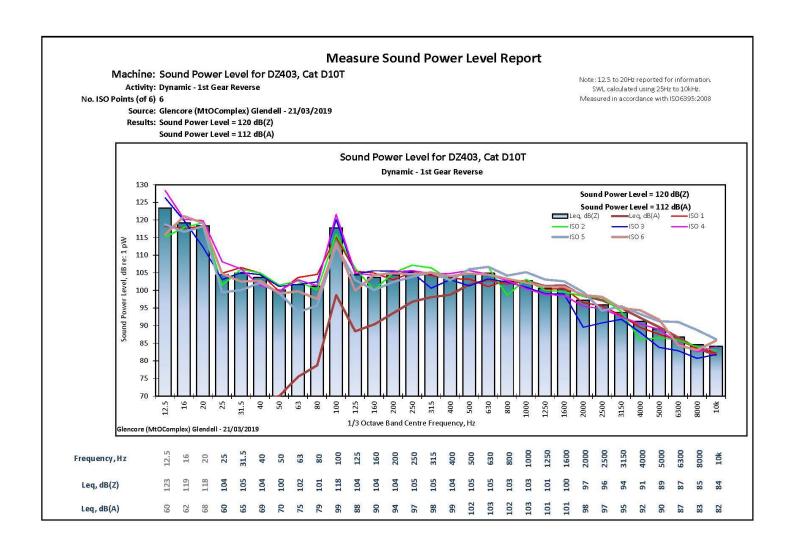
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Page 2 of 2 End of Calibration Certificate AVCERT10

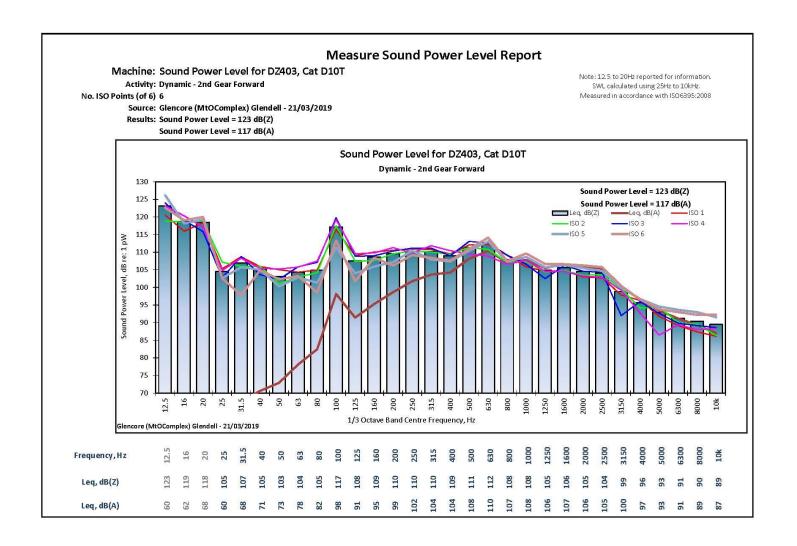




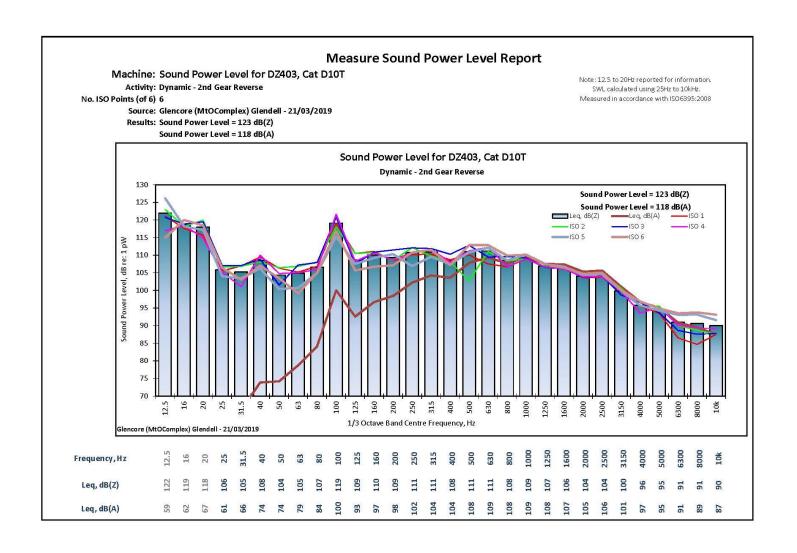
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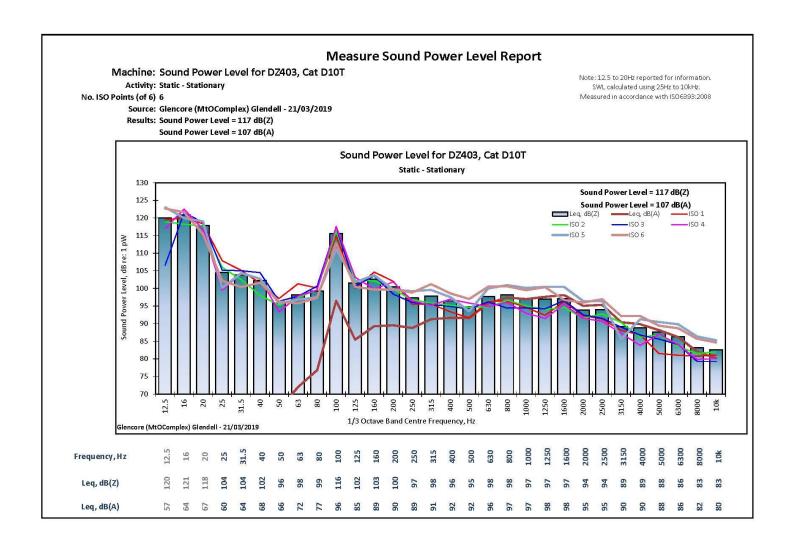
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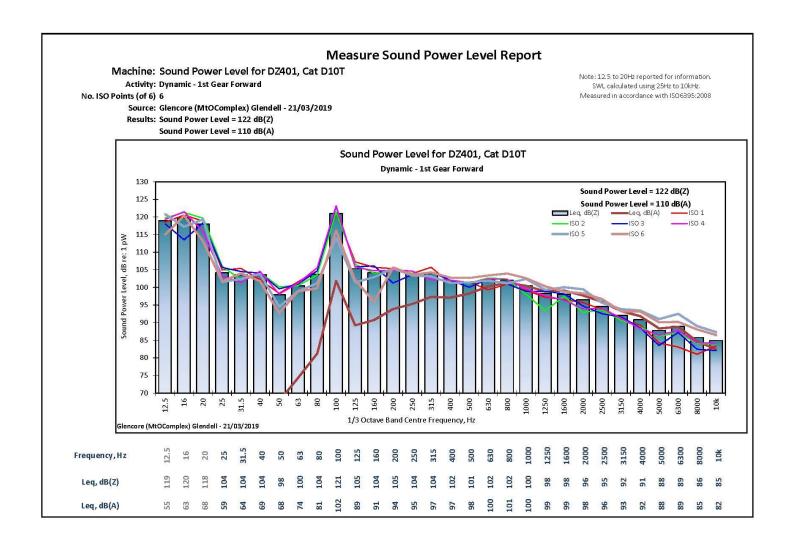
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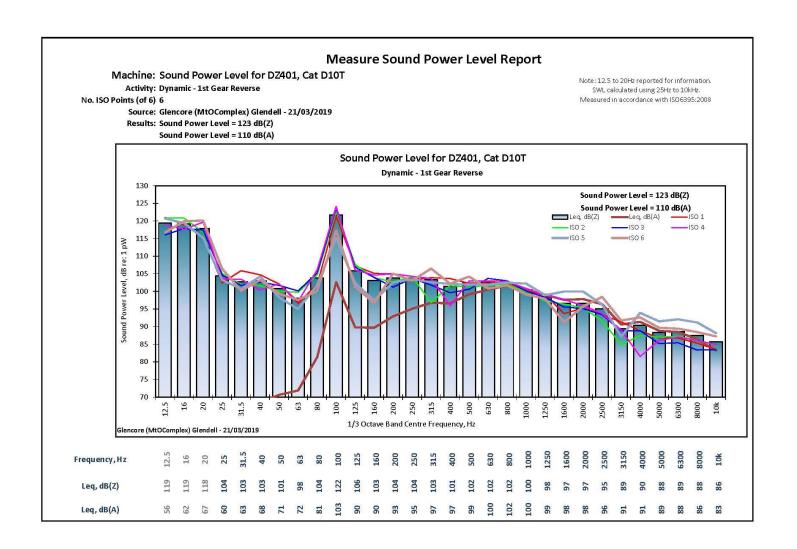
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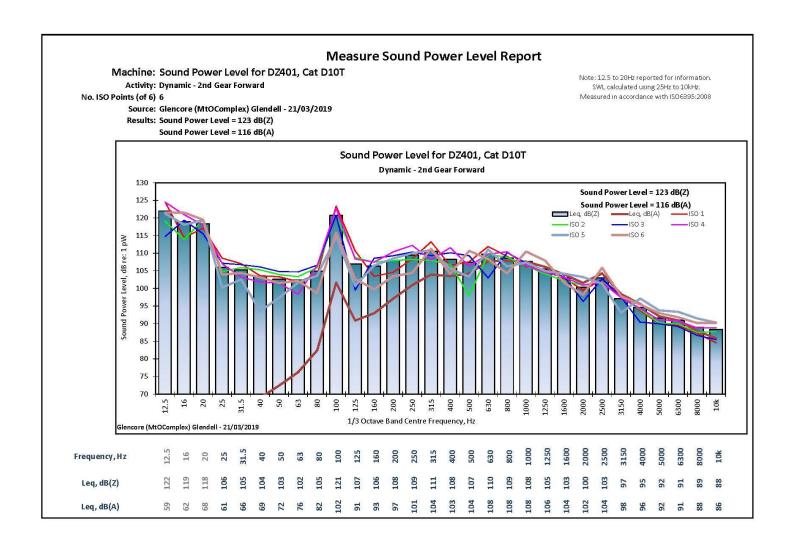
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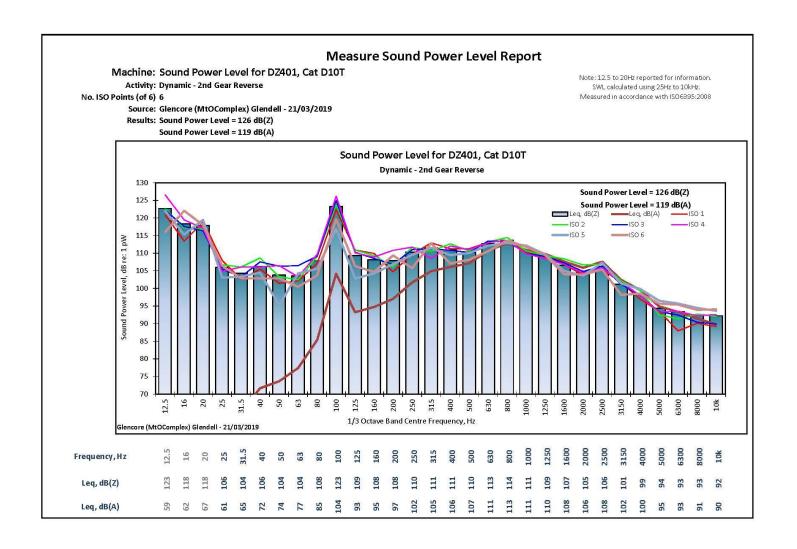
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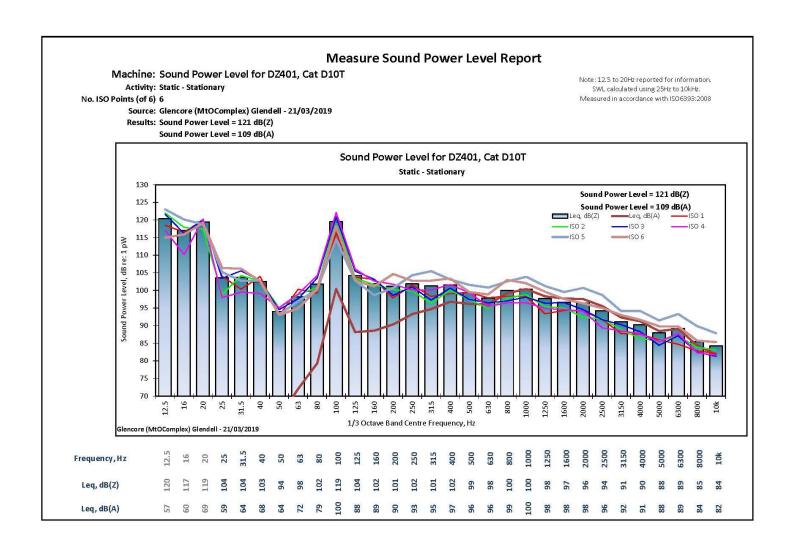
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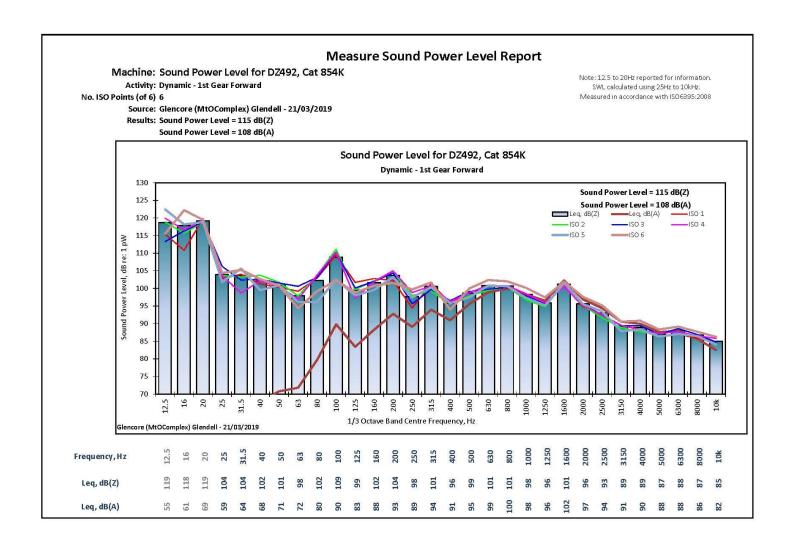
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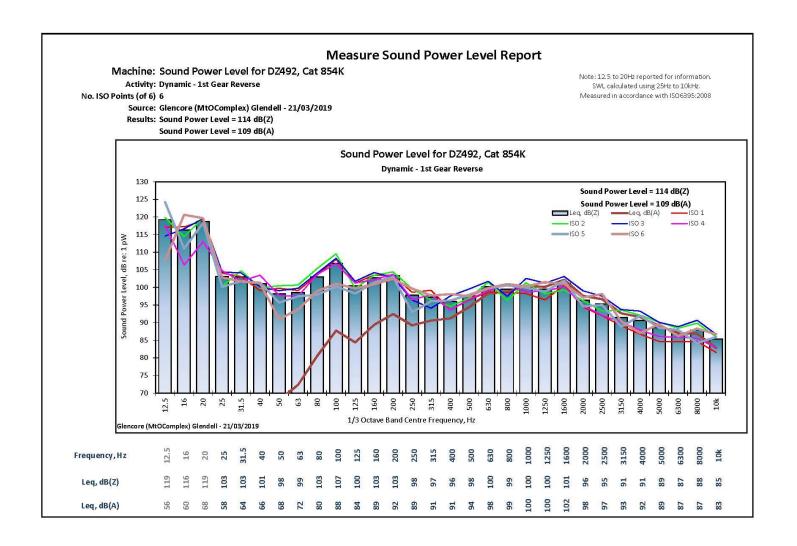
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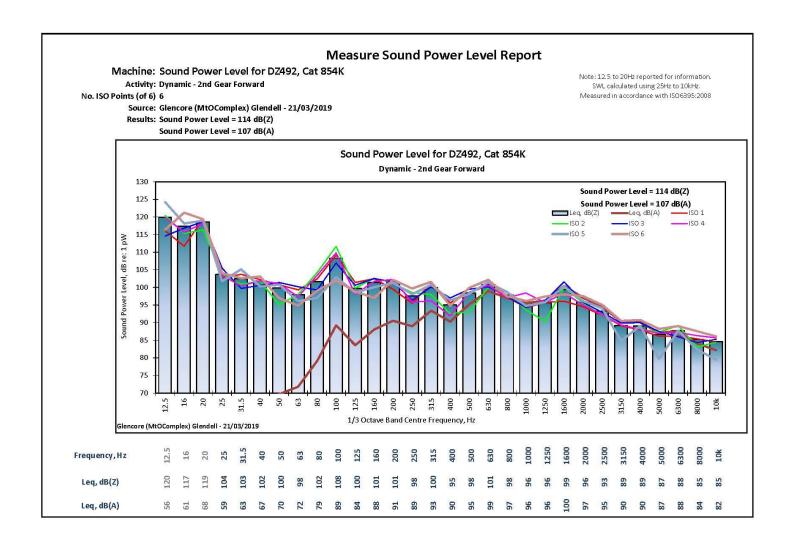
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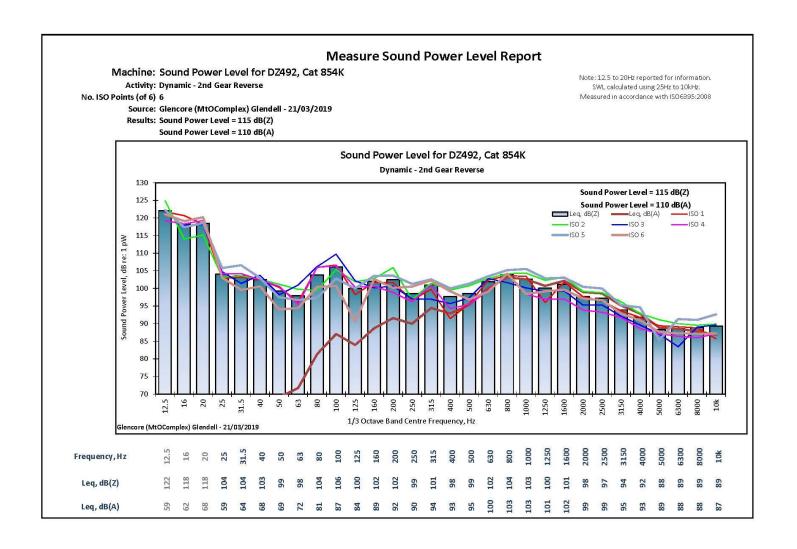
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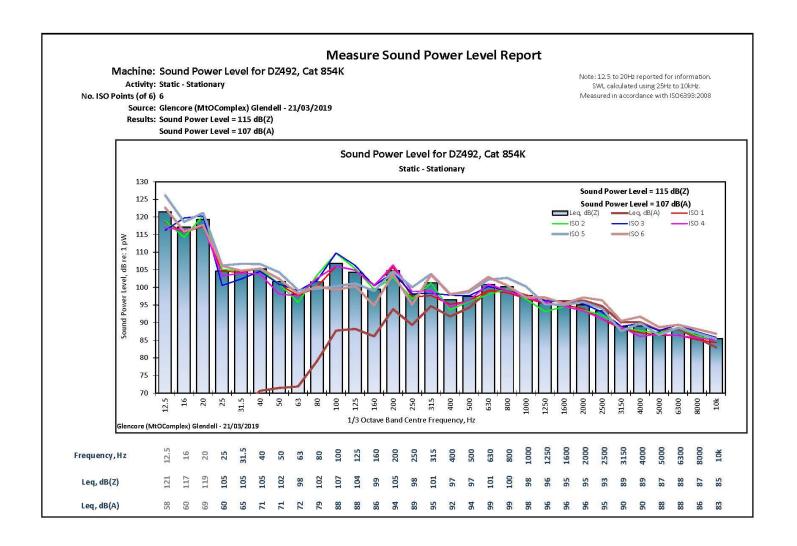
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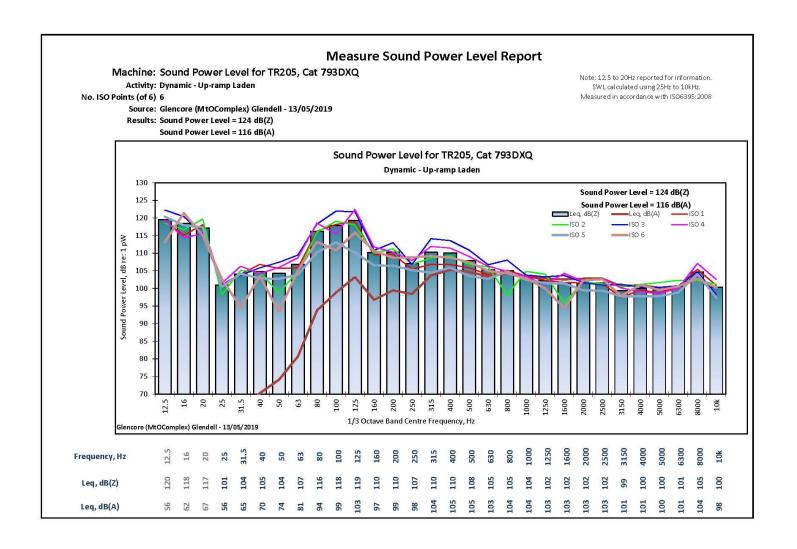
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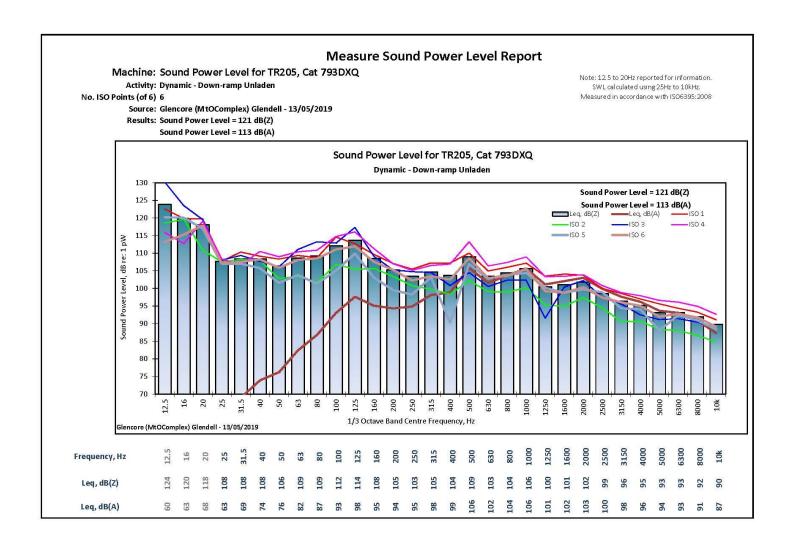
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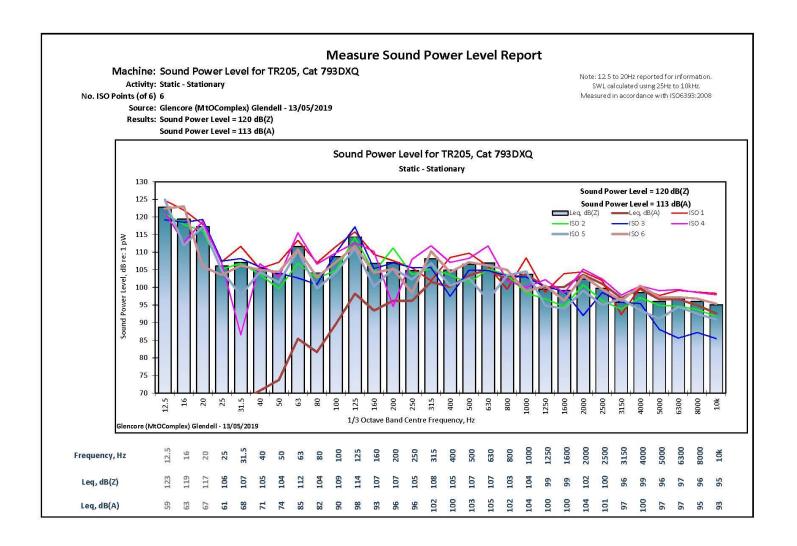
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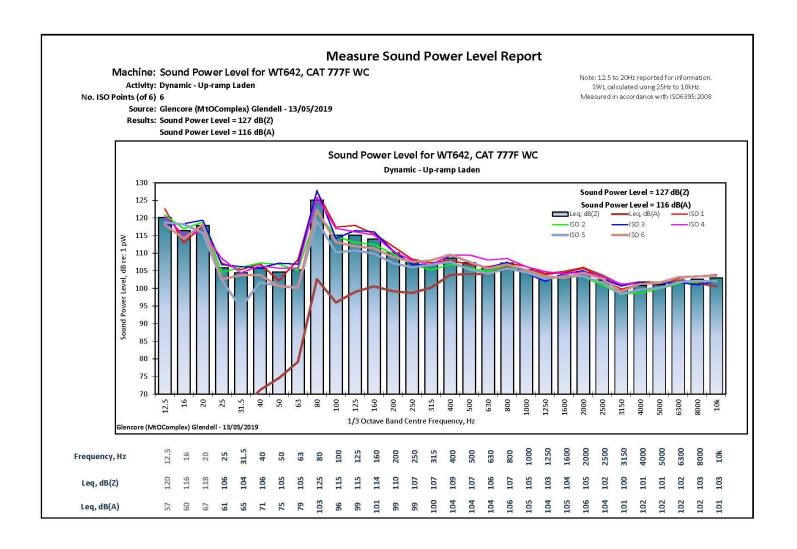
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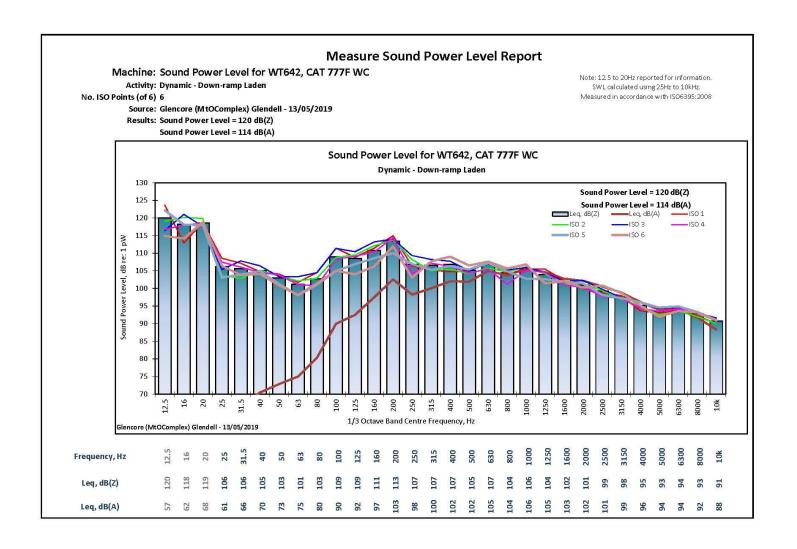
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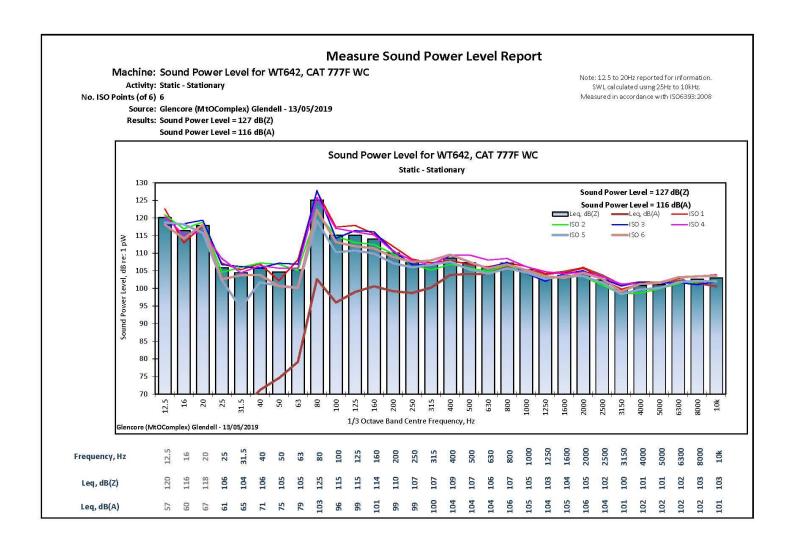
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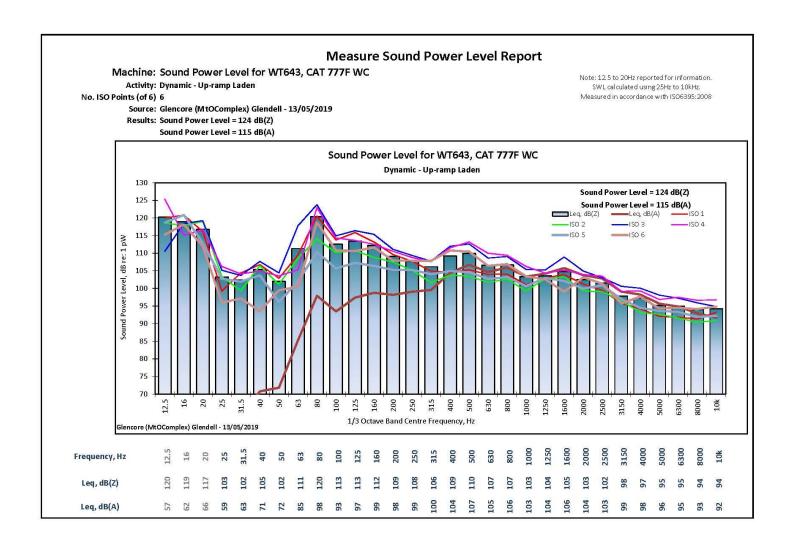
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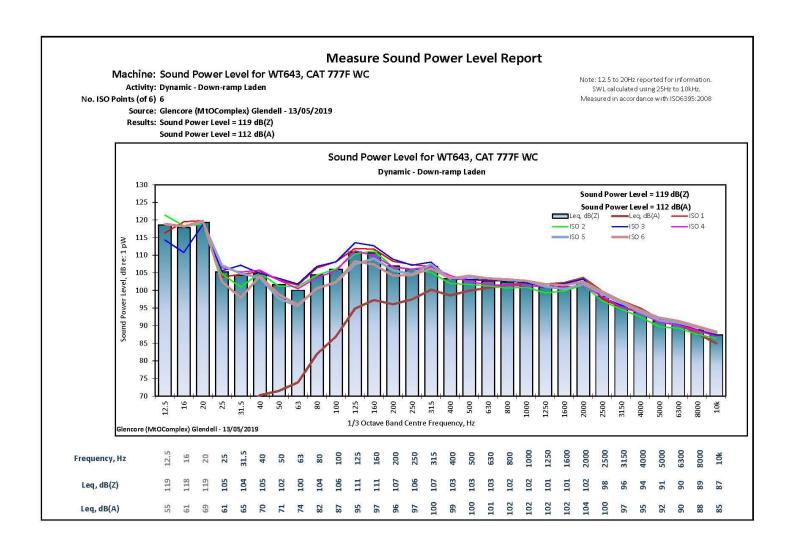
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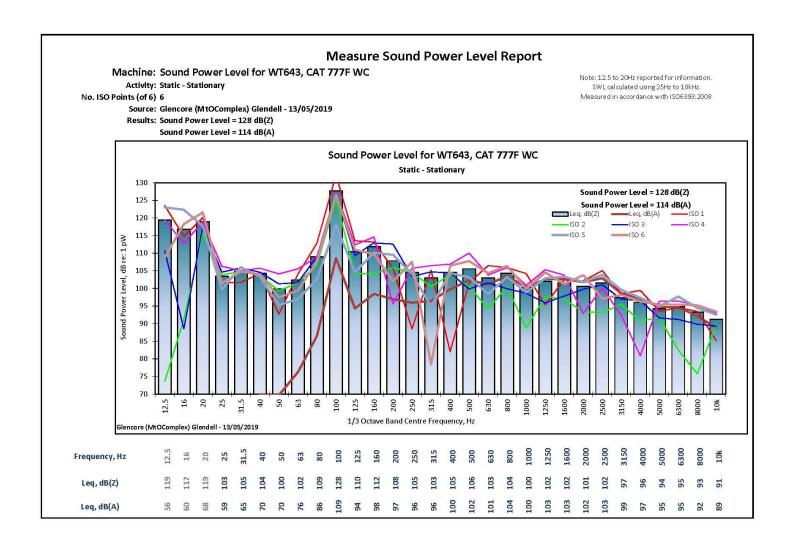
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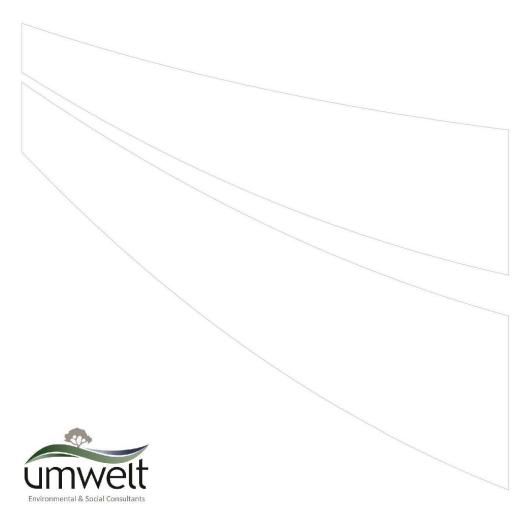
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Umwelt (Australia) Pty Limited WT643 Downhill Laden.xlsb



Umwelt (Australia) Pty Limited WT643 Uphill Static.xlsb



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GLENCORE

MACHINE SOUND POWER LEVEL TESTING

2019

Glendell Mine

FINAL

Prepared by
Umwelt (Australia) Pty Limited
on behalf of
Glencore

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Report No. 4748/R01
Date: December 2019

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Document Status

Rev No.	Reviewer		Approved for Issue			
	Name	Date	Name	Date		
1	T Procter	6 December 2019	T Procter	6 December 2019		
2	E Moore	16 December 2019	R Williams	16 December 2019		

		umw	elt
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Machine Sound Power Level Testing 4748_R01_Machine SPL Testing_FINAL V2



2.0 Results

2.1 Measured Sound Power Levels

Dynamic SWL testing of equipment included the measurement of the following machines in representative operating conditions:

- dozers and grader in 1st and 2nd gear forward and reverse motion on flat surfaces
- excavator performing 90° swing

Static SWL testing of the equipment included stationary testing of machines at the same test site surface used from the dynamic test.

Table 2.1 summarises the sound power level test results for each item of equipment tested. The detailed sound power level results are presented as one-third octave graphs in **Appendix C**. Results are presented as Linear (Z – weighted) and A-weighted¹ sound power levels.

Machine Sound Power Level Testing 4748_R01_Machine SPL Testing_FINAL V2

Results

 $^{^1\}text{A-weighting is an adjustment made to sound level measurement, by means of an electronic filter, to approximate the response of the human ear.}$



1.0 Introduction

As per Glendell Mine's DPIE approved Noise Management Plan, Glendell Mine is required to conduct periodic review of the noise performance of its equipment fleet. It is recommended that all fleet should be tested within a five-year period.

In 2019, Umwelt conducted noise performance tests on twelve of Glendell's equipment fleet (refer to Report No 4545/R01 for further details regarding these test results).

Umwelt Australia Pty Ltd was engaged by Glencore to undertake sound power level (SWL) testing of a selection of mobile machines, listed in **Table 1.1**. Testing was conducted on 16, 22 and 29 October 2019 at various locations at Glendell Mine.

Table 1.1 Tested Machines

Plant Type	Unit Number	Model	
	DZ 406	Cat D10T	
Dozers	DZ 453	CAT D11T	
Dozers	DZ 472	CAT D11R (CHPP)	
	DZ 473	CAT D11R (CHPP)	
Grader	GR 611	CAT 24M	
Excavator	EX 103	Hitachi 5500	

Dynamic SWL testing was undertaken generally in accordance with the methodology presented in ISO 6395 and ISO 6393 for stationary (static) testing. In accordance with these standards, sound power is determined in one-third octave bands from 25 Hz to 10 kHz. However, Glendell Mine requires assessment in one-third octave bands from 12.5 Hz to 10 kHz. The SWL testing methodology used at Glendell mine is summarised in **Appendix A**. The calibration certificates for the sound measurement equipment can be found in **Appendix B**. The results for each machine tested is presented in detail in **Appendix C**.

Machine Sound Power Level Testing 4748_R01_Machine SPL Testing_FINAL V2 Introduction



Table 2.1 Sound Power Level Monitoring Results

Machine ID	Make / Model	Transmission/	Dynamic - Up or Forward		Dynamic - Down or Reverse		Static		Testing Date
		Mode of operation	dB(Z)	dB(A)	dB(Z)	dB(A)	dB(Z)	dB(A)	
Dozers									
		1 st gear	121	116	122	118	119	109	16/10/2019
DZ 406	Cat D10T	2 nd gear	124	121	127	124	= :	=	16/10/2019
DZ 453	CAT D11T	1 st gear	123	118	124	120	119	109	16/10/2019
		2 nd gear	127	124	129	127	-	-	16/10/2019
DZ 472	CAT D11R (CHPP)	1 st gear	123	116	123	114	119	108	29/10/2019
		2 nd gear	126	120	126	121	-	=	29/10/2019
D7 473	CAT D11R (CHPP)	1 st gear	120	115	122	117	119	112	29/10/2019
		2 nd gear	125	121	126	123	-	-	29/10/2019
Grader									
	CAT 24M	1 st gear	122	117	122	117	122	114	16/10/2019
GR 611		2 nd gear	122	117	122	117			16/10/2019
Excavator									
EX 103	Hitachi 5500	90° Swing	120	113	NA	NA	120	113	22/10/2019

Machine Sound Power Level Testing 4748_R01_Machine SPL Testing_FINAL V2 Resul



2.2 Meteorological Conditions

The meteorological conditions at the time of the monitoring program are presented in Table 2.2.

Table 2.2 Local Meteorological Conditions (Sentinex13)

Date Wind Speed (m/s)		Temperature (°C)	Relative Humidity (%)		
16/10/2019	1.7 (0.5 - 3.8)	31.4 (26.3 - 34.8)	32.3 (23.0 - 47.0)		
22/10/2019	2.1 (0.7 - 4.1)	25.0 (20.9 - 28.9)	39.3 (29 - 55.0)		
29/10/2019	1.3 (0.2 - 3.0)	24.6 (20.5 - 28.3)	51.7 (36.0 - 68.0)		

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3.0 Discussion

The Z and A-weighted sound power levels for machines in different modes of operation are presented in **Table 2.1**. The one-third octave bands of the sound power spectrum for each machine are included in **Appendix C. Table 3.1** compares the measured Z and A-weighted sound power levels to the target inservice Z-weighted sound power levels nominated in Glencore Noise Management Protocol GCAA-625378177-10238 (GCAA NMP) and the A-weighted sound power level targets for the Year 9 targets nominated in the Glendell Environmental Assessment 2007 (GEA, 2007).

Table 3.1 Comparison of Sound Power Levels Results to In-service Targets Nominated in the GCAA NMP and the Year 9 Proposed Fleet Specification Targets in (GEA, 2007)

Equipment Description			Dynamic				GCAA	GEA, 2007	
		Mode of Operation	Up or Forward		Down or Reverse		NMP	For/Rev ^a	
			dB(Z)	dB(A)	dB(Z)	dB(A)	dB(Z)	dB(A)	
	DZ 406	Cat D10T	1 st gear	121	116	122	118	123	110/118
	DZ 453	CAT D11T	1 st gear	123	118	124	120	123	110/118
Dozers	DZ 472	CAT D11R (CHPP)	1 st gear	123	116	123	114	123	110/118
	DZ 473	CAT D11R (CHPP)	1 st gear	120	115	122	117	123	110/118
Grader	GR 611	CAT 24M	1 st gear	120	114	122	117	117	104
Excavator	EX 103	Hitachi 5500	Dynamic	120	113	N/A	N/A	125	117

NOTE a GEA, 2007 gives specific SWL targets for dozers in forward and reverse modes of operation. For other machines, only one SWL target is given for all modes of operation

The results in **Table 3.1** indicate DZ406 in 1^{st} gear forward is below the GCAA NMP Z-weighted target but 6 dB above the GEA 2007 A-weighted target. The high A-weighted result was due to a cyclic rattle in the 630 Hz to > 2000 Hz range in the rear left hand side of the machine. Elimination of this rattle would reduce the 1^{st} gear forward sound power level to $120 \, dB(Z)/111 \, dB(A)$. This difference is shown in **Figure 3.1**.

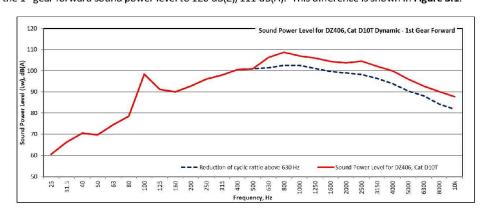


Figure 3.1 Comparison of DZ406 SWL results with reduction in cyclic rattle

Machine Sound Power Level Testing 4748_R01_Machine SPL Testing_FINAL V2 Discussion



The results in **Table 3.1** indicate DZ406 in 1st gear reverse is at or below the GCAA NMP Z-weighted and the GEA 2007 A-weighted targets. During the monitoring of 1st gear reverse the reversing beeper could not be isolated. Isolation of the reversing beeper would reduce the 1st gear reverse sound power level to 121 dB(Z)/114 dB(A).

The results in **Table 3.1** indicate DZ453 in 1st gear forward was at the GCAA NMP Z-weighted target but 8 dB above the GEA 2007 A-weighted target. Overall the measured sound power level of DZ453 in 1st gear forward was within the standard deviation of the sound power envelope of similar machines except in the 100 Hz and 630 Hz 1/3 octave bands. The 100 Hz is associated with the exhaust and the 630 Hz is apparent at all measurement locations while the machine was in motion (refer to difference between static results and dynamic results). The results in **Table 3.1** indicate DZ453 in 1st gear reverse was 1 dB above the GCAA NMP Z-weighted target and 2 dB above the GEA 2007 A-weighted target. Similar to the 1st gear forward results, the machine was within the standard deviation of the sound power envelope of similar machines except in the 100 Hz and 630 Hz 1/3 octave bands.

The results in **Table 3.1** indicate DZ472 in 1st gear forward was below the GCAA NMP Z-weighted target but 4 dB above the GEA 2007 A-weighted target. The results in **Table 3.1** indicate DZ406 in 1st gear reverse was at the GCAA NMP Z-weighted target and below the GEA 2007 A-weighted target. Overall the measured sound power level of DZ472 was within the standard deviation of the sound power envelope of similar machines.

The results in **Table 3.1** indicate DZ473 in 1st gear forward was below the GCAA NMP Z-weighted target but 5 dB above the GEA 2007 A-weighted target. The results in **Table 3.1** indicate DZ406 in 1st gear reverse was below the GCAA NMP Z-weighted and GEA 2007 A-weighted targets. Overall the measured sound power level of DZ472 was within the standard deviation of the sound power envelope of similar machines.

The results in **Table 3.1** indicate GR611 in 1st gear forward was 3 dB above the GCAA NMP Z-weighted target and 10 dB above the GEA 2007 A-weighted target. The results in **Table 3.1** also indicate GR611 in 1st gear reverse was 5 dB above the GCAA NMP Z-weighted target and 13 dB above the GEA 2007 A-weighted target. Comparison of the measured sound power level of GR611 with the standard deviation of the sound power envelope of similar machines indicates GR611 exceeded the upper +1 standard deviation by up to 1 to 2 dB. This is shown in **Figure 3.2**. It is also noted that the 2015 results for GR611 report a sound power level in 1st gear forward of 114 dB(Z) and 106 dB(A). It is recommended that Glendell review the maintenance records for GR611 for the period from 2015 to present, as this may indicate the cause of the difference between the 2015 and 2019 test results.

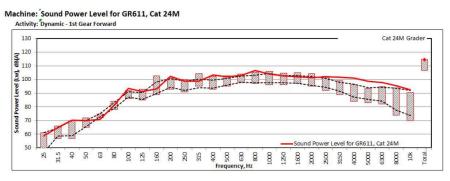
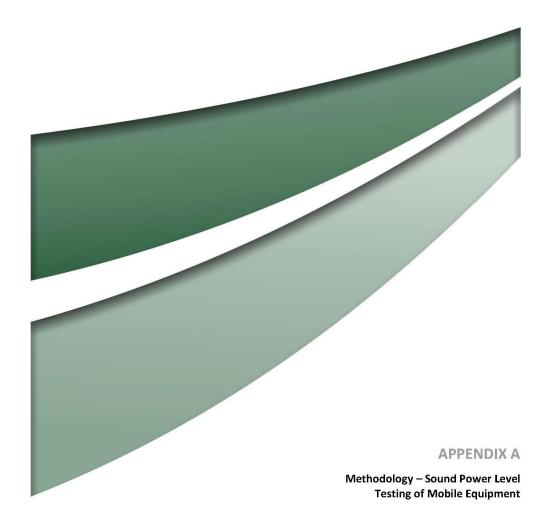


Figure 3.2 Comparison of GR611 SWL results with equivalent machines

The results in **Table 3.1** indicate EX103 in dynamic mode of operation is below the GCAA NMP Z-weighted and GEA 2007 A-weighted targets.

Machine Sound Power Level Testing 4748_R01_Machine SPL Testing_FINAL V2

Discussion





A.1 Testing Standards

The monitoring program was conducted in accordance with:

MGD15 - Mobile and transportable plant for use on mines and petroleum sites (Amd. 2018)

 ${\sf ISO~6395:2008-Earth-moving~machinery-Determination~of~sound~power~level-Dynamic~test~conditions}$

 ${\sf ISO~6393:2008-Earth-moving~machinery-Determination~of~sound~power~level-Stationary~test~conditions}$

ISO 3744:2010 - Acoustics – Determination of sound power levels and sound energy levels of noise sources using sound pressure – Engineering methods for an essentially free field over a reflecting plane

ISO 4872 – Measurement of airborne noise emitted by construction equipment intended for outdoor use -- Method for determining compliance with noise limits

The monitoring program also took into consideration the requirements of:

AS 2012.2-1990 – Acoustics - Measurement of airborne noise emitted by earth-moving machinery and agricultural tractors - Stationary test condition, Operator's position

AS/NZS 1269.1-2005 - Occupational noise management - Measurement and assessment of noise emission and exposure

A.2 Equipment Used

The monitoring program was conducted using the following equipment

SVAN958A (59838) - four (4) channel sound and vibration analyser

SVAN958A (59839) - four (4) channel sound and vibration analyser

SVAN SV36 (90131) - 94/114 dB calibrator

SVAN SV36 (90124) – 94/114 dB calibrator

Kestrel 4500 – weather meter

Calibration certificates are included in Appendix B.

Machine Sound Power Level Testing 4748_R01_Machine SPL Testing_FINAL V2 Appendix A



A.3 Sound Power Level Testing

The monitoring program methodology is outlines as follows:

- · Sound power levels have been determined in one-third octave bands.
- Glencore Noise Management Protocol GCAA-625378177-10238 (GCAA NMP) requires the
 measurements to be from 25 Hz to 10 kHz to enable reporting of Linear (Z-weighted) and A-weighting
 sound power levels. Data capture data from 12.5 Hz to 20 Hz has been included in the reporting of the
 monitoring data but not the determination of sound power levels The 12.5 Hz to 20 Hz data can be
 used to assess low frequency noise and/or are often identifiable within the background acoustic
 environment.
- Measurements made from six ISO microphones. Figure A.1 shows the horizontal (left image) and vertical (right image) positions of each microphone.
- The size of the measurement surface is determined as per ISO 6395:2008(E). This generally constitutes a radius of 16 20 m to accommodate the tested machines.

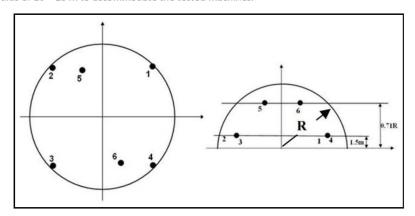


Figure A.1 - Microphone position for ISO Sound Power Level testing

A.4 Test Area Environment

The test areas included a haul road and flat dump area with sufficient length to allow machines to safely accelerate, pass through the test area and decelerate.

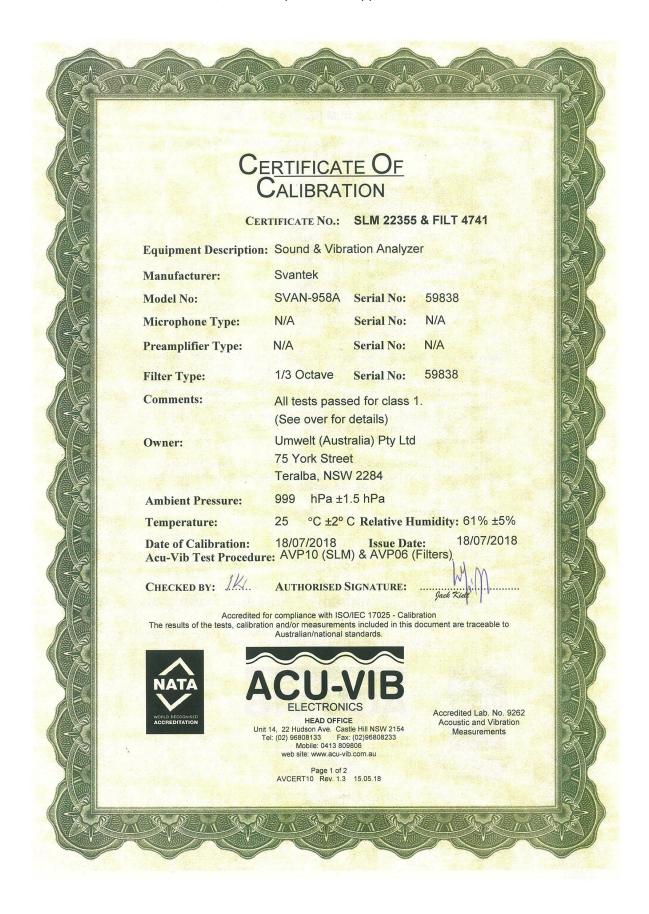
In accordance with ISO 6395 and GCAA NMP, the location of the test area was chosen to minimise the impacts of reflective surfaces such as highwalls and windrows.

Care was also taken to ensure that background noise levels were at least 6 dB less than measured equipment being tested. A correction is also applied for background levels between 6 dB - 15 dB less than measured dynamic levels to ensure that background noise has limited effect on measured levels. In addition to this, Mount Owen requires the background noise levels to be reported in one-third octave bands from 12.5 Hz to 10 kHz

All machines were tested on slope of approximately 0% to facilitate the forward and reverse testing of the bulldozers, grader and excavator.

Machine Sound Power Level Testing 4748_R01_Machine SPL Testing_FINAL V2 Appendix A





CERTIFICATE No.: SLM 22355 & FILT 4741

The performance characteristics listed below were tested. The tests are based on the relevant clauses of IEC 61672-3:2013

Tests Performed:	Clause	Result
Absolute Calibration	10	N/A
Acoustical Frequency Weighting	12	N/A
Self Generated Noise	11.1	N/A
Electrical Noise	11.2	Entered
Long Term Stability	15	Pass
Electrical Frequency Weightings	13	Pass
Frequency and Time Weightings	14	Pass
Reference Level Linearity	16	Pass
Range Level Linearity	17	Pass
Toneburst	18	Pass
Peak C Sound Level	19	Pass
Overload Indicator	20	Pass
High Level Stability	21	Pass

Statement of Compliance: The sound level meter submitted for testing has successfully completed the class 1 periodic tests of IEC 61672-3:2013, for the environmental conditions under which the tests were performed. As public evidence was available, from an independent organization responsible for approving the results of pattern evaluation tests performed in accordance with IEC 61672-2:2013, to demonstrate that the model of sound level meter fully conformed to the requirements in IEC 61672-1:2013, the sound level meter submitted for testing conforms to the class 1 requirements of IEC61672-1:2013.

A full technical report is available if required.

This Sound Level Meter included an Octave Filter Set. Tests were based on IEC 1260: 1995 and AS/NZS 4476 - 1997 and were conducted to test the following performance characteristics:

1. Relative attenuation

clause 5.3

Checked by: Accredited for compliance with ISO/IEC 17025 - Calibration
The results of the tests, calibration and/or measurements included in this document are traceable to Australian/national standards.

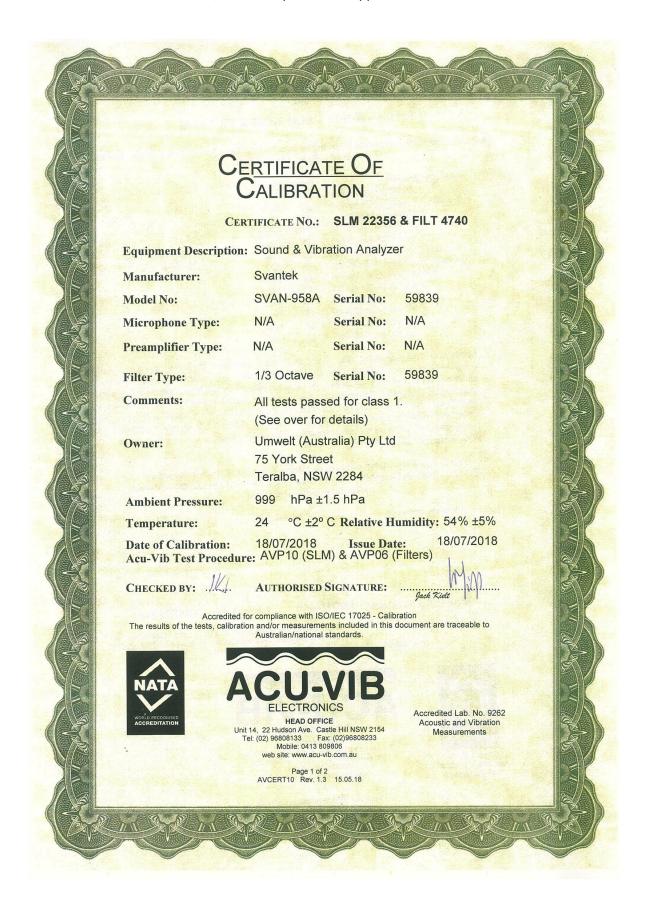


Accredited Lab. No. 9262
Acoustic and Vibration
Measurements



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Tel: (02) 96808133 Fax: (02)96808233
Mobile: 0413 809806
web site: www.acu-vib.com.au

Page 2 of 2 End of Calibration Certificate
AVCERT10



CERTIFICATE No.: SLM 22356 & FILT 4740

The performance characteristics listed below were tested. The tests are based on the relevant clauses of IEC 61672-3:2013

Tests Performed:	Clause	Result
Absolute Calibration	10	N/A
Acoustical Frequency Weighting	12	N/A
Self Generated Noise	11.1	N/A
Electrical Noise		Entere
Long Term Stability	15	Pass
Electrical Frequency Weightings	13	Pass
Frequency and Time Weightings	14	Pass
Reference Level Linearity	16	Pass
Range Level Linearity	17	Pass
Toneburst	18	Pass
Peak C Sound Level	19	Pass
Overload Indicator	20	Pass
High Level Stability	21	Pass

Statement of Compliance: The sound level meter submitted for testing has successfully completed the class 1 periodic tests of IEC 61672-3:2013, for the environmental conditions under which the tests were performed. As public evidence was available, from an independent organization responsible for approving the results of pattern evaluation tests performed in accordance with IEC 61672-2:2013, to demonstrate that the model of sound level meter fully conformed to the requirements in IEC 61672-1:2013, the sound level meter submitted for testing conforms to the class 1 requirements of IEC61672-1:2013. A full technical report is available if required.

This Sound Level Meter included an Octave Filter Set. Tests were based on IEC 1260: 1995 and AS/NZS 4476 - 1997 and were conducted to test the following performance characteristics:

1. Relative attenuation

Date of Calibration: 18/07/2018

Issue Date: 18/07/2018

Checked by: /K/

by: Accredited for compliance with ISO/IEC 17025 - Calibration
The results of the tests, calibration and/or measurements included in
this document are traceable to Australian/national standards.

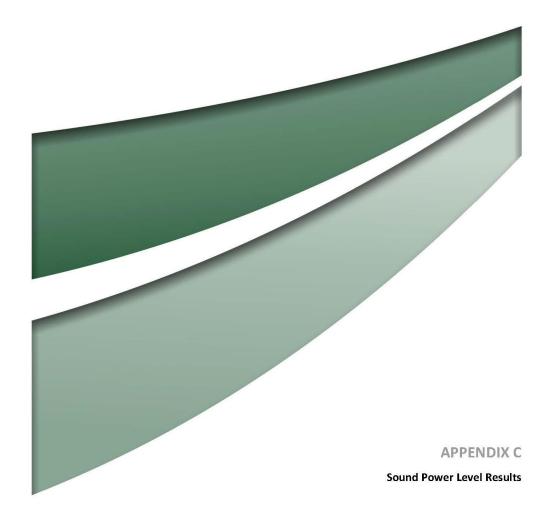


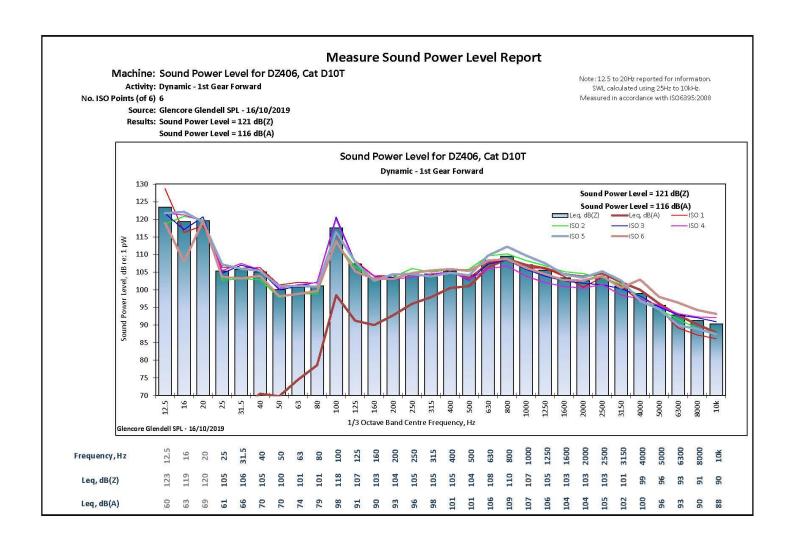
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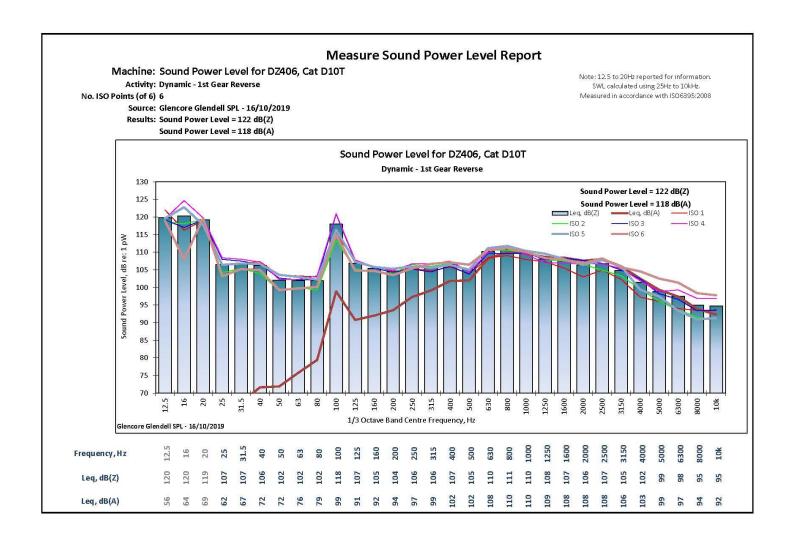
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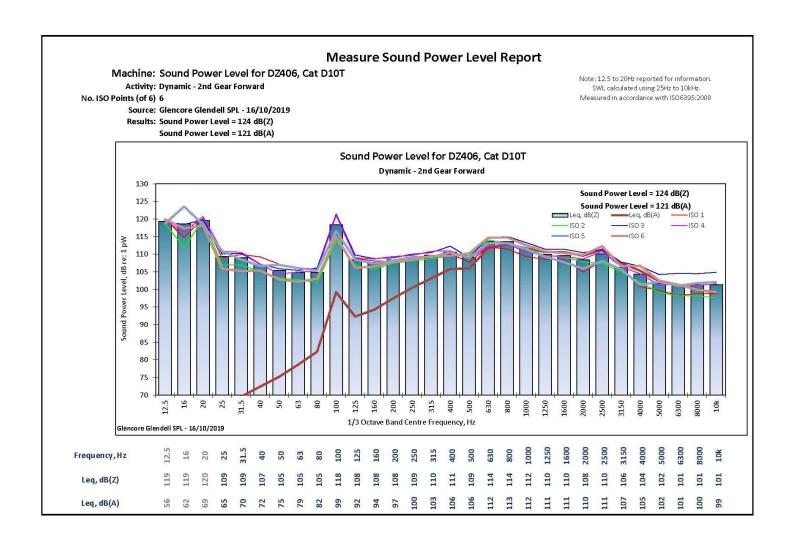




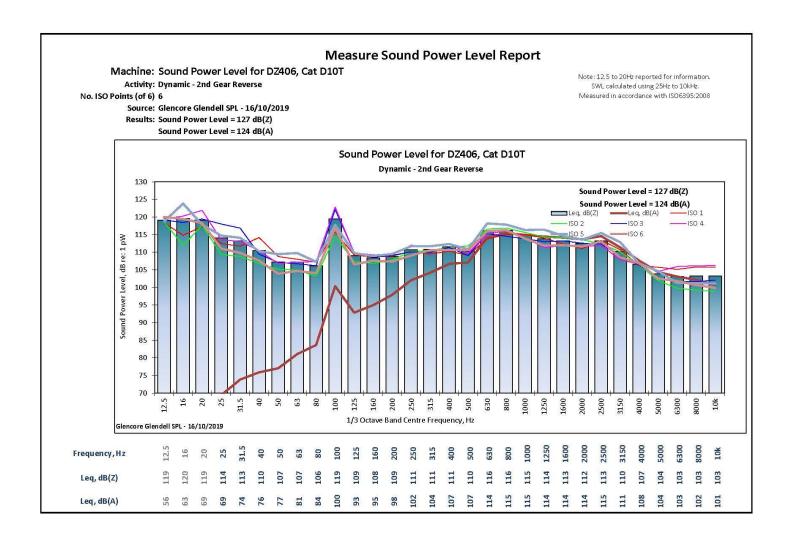
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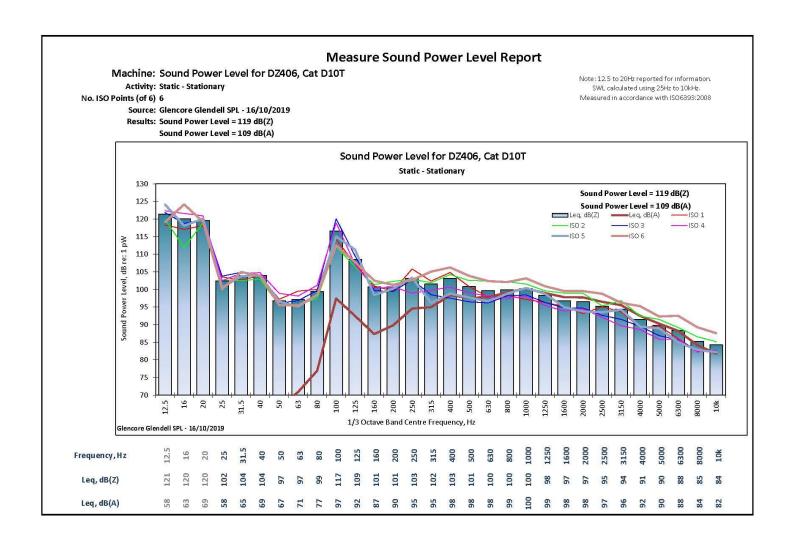
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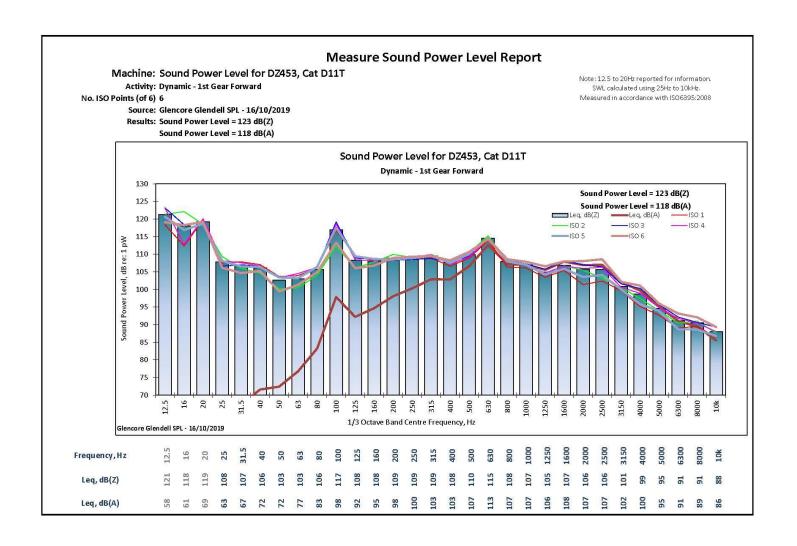
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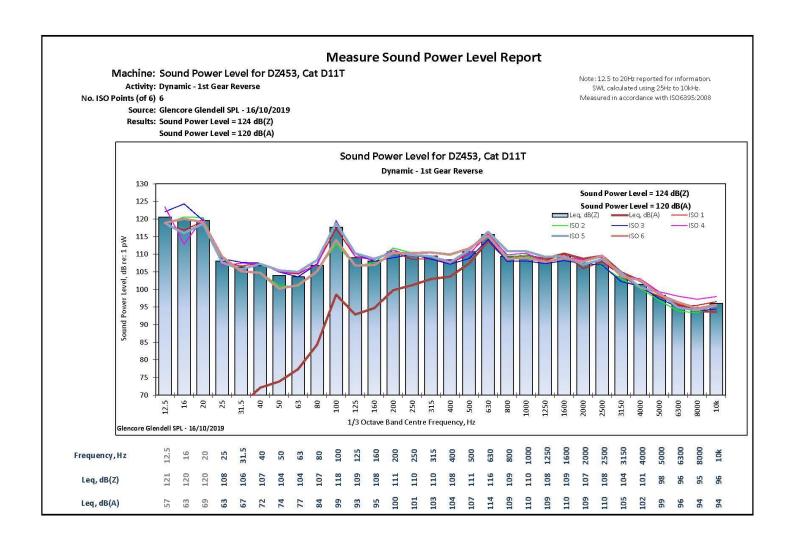
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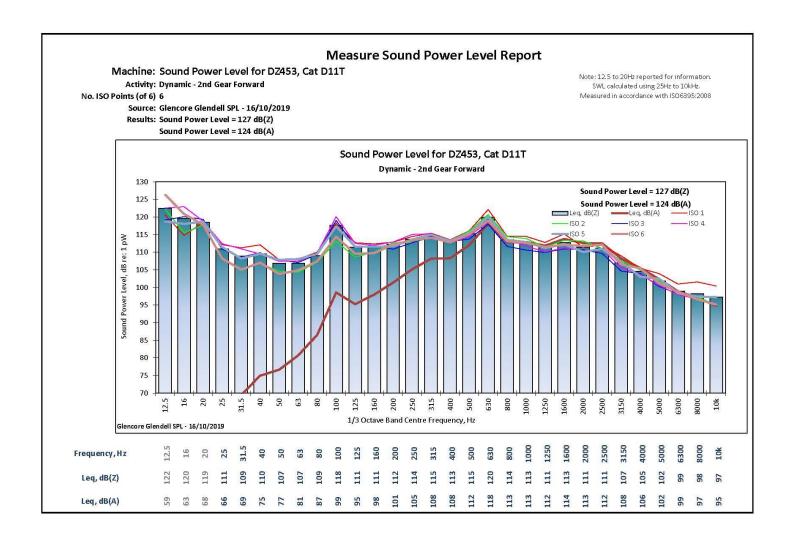
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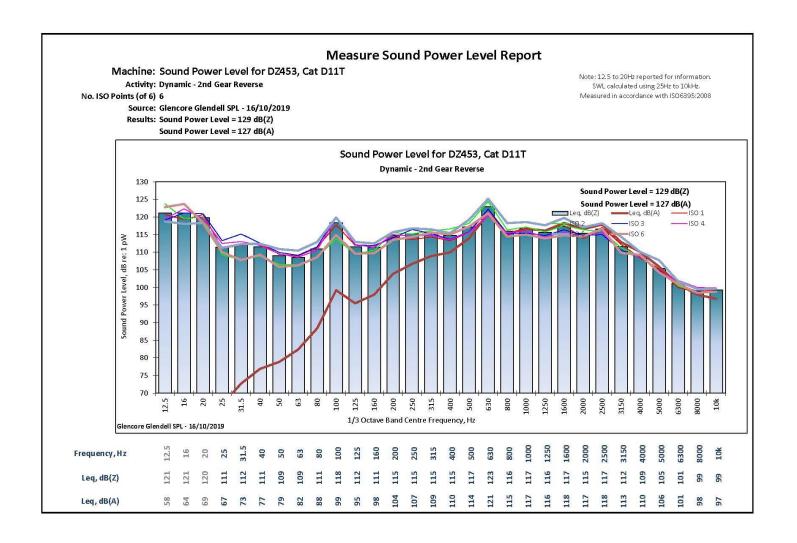
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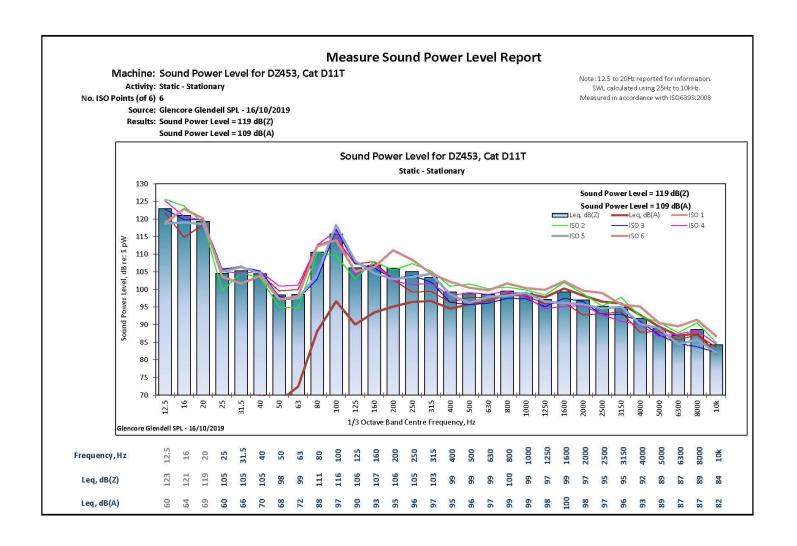
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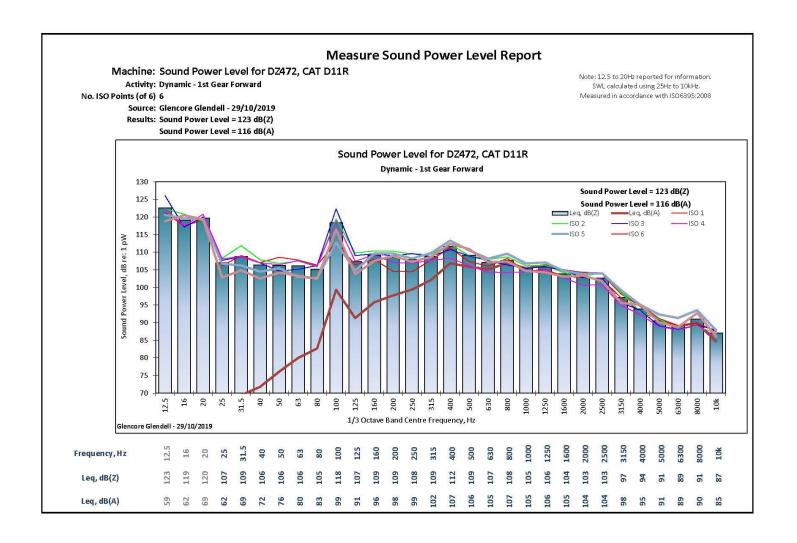
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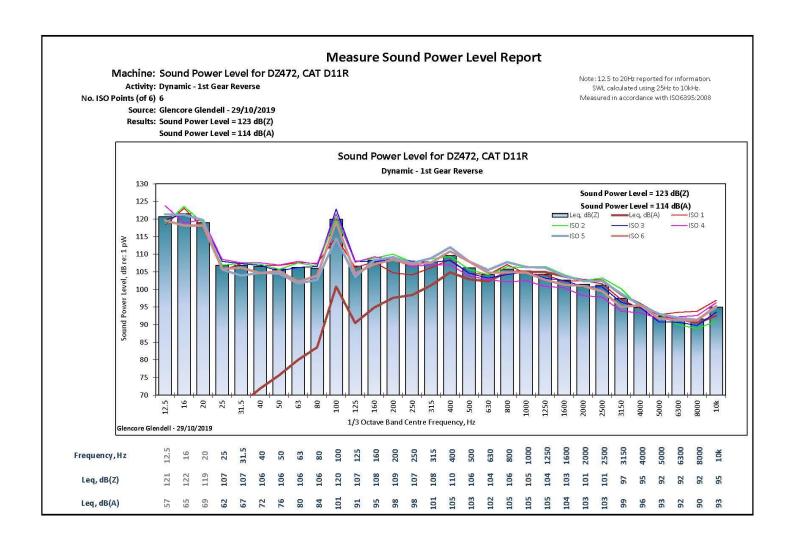
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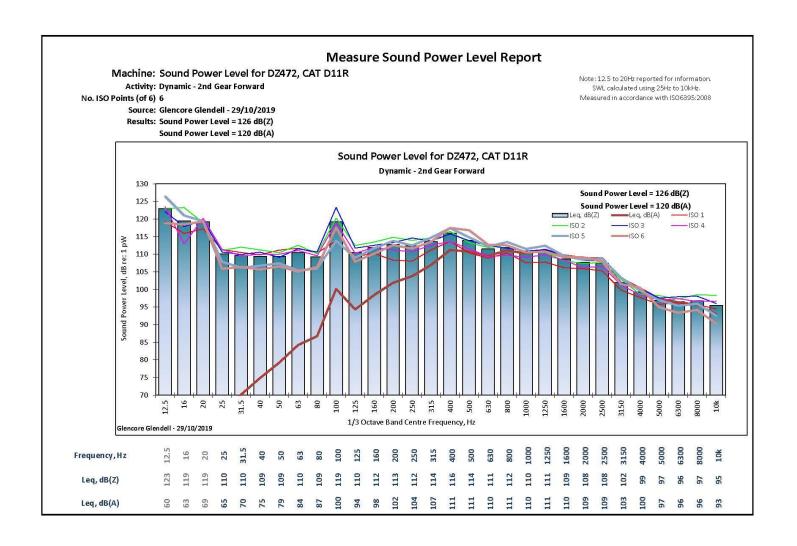
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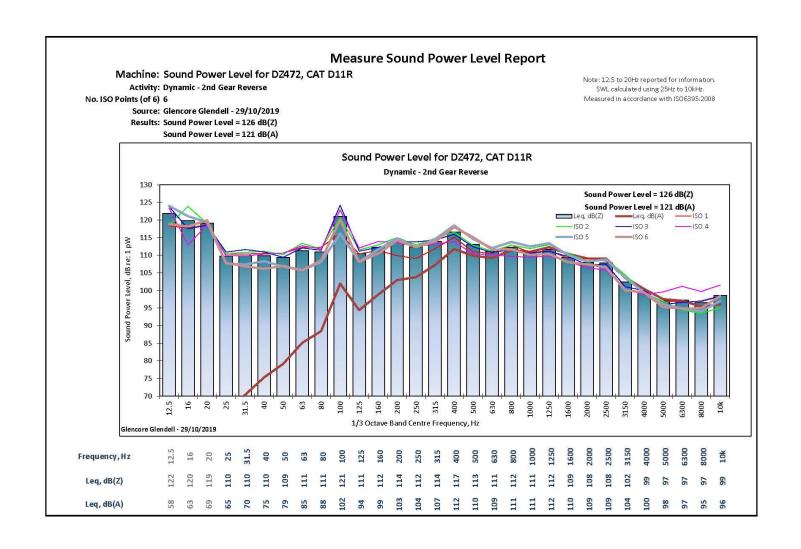
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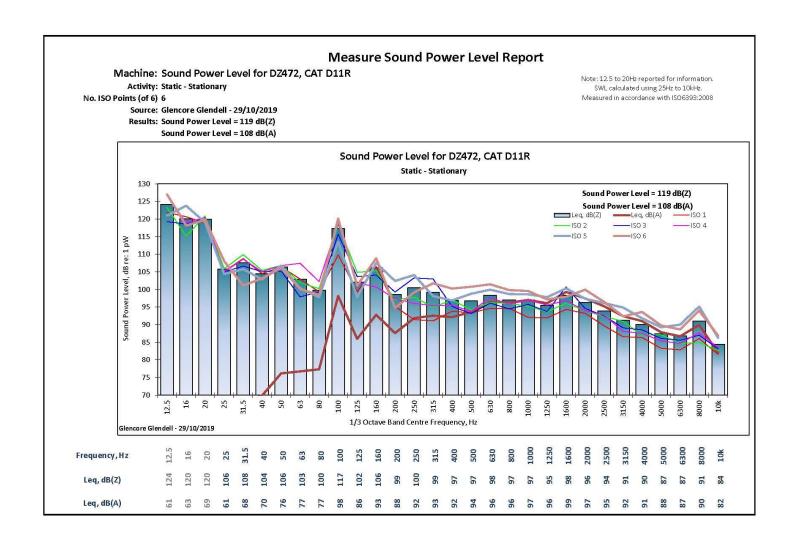
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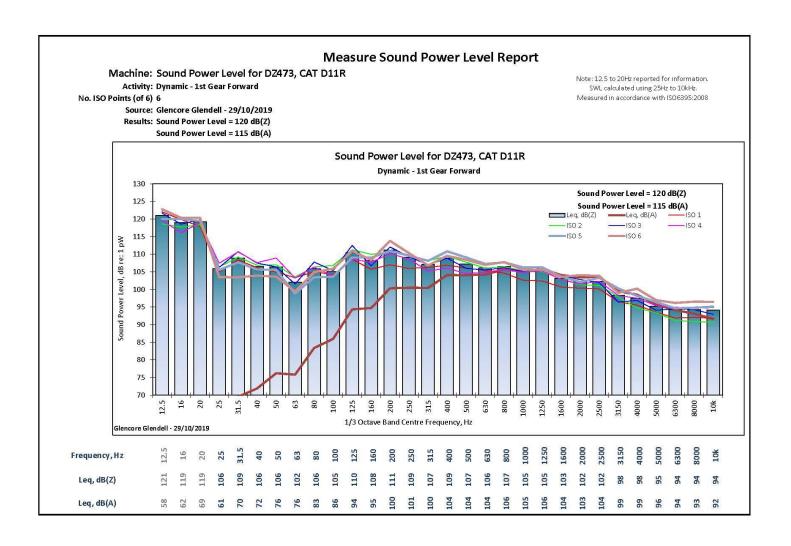
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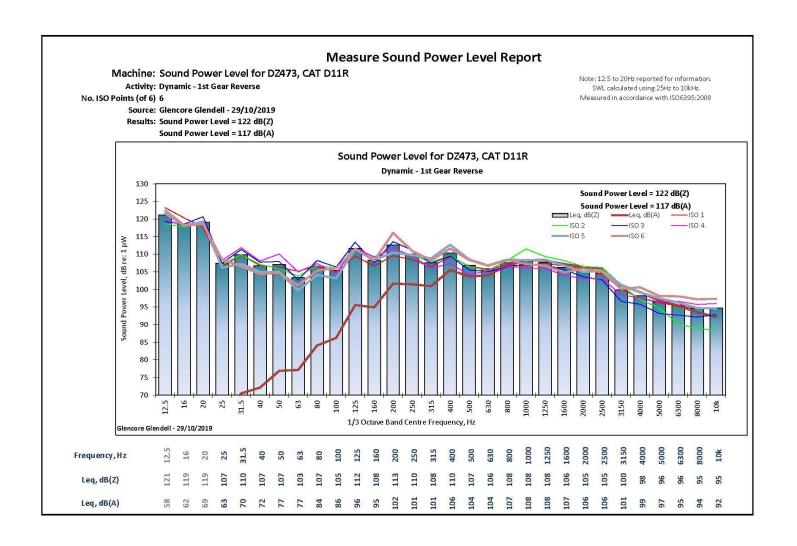
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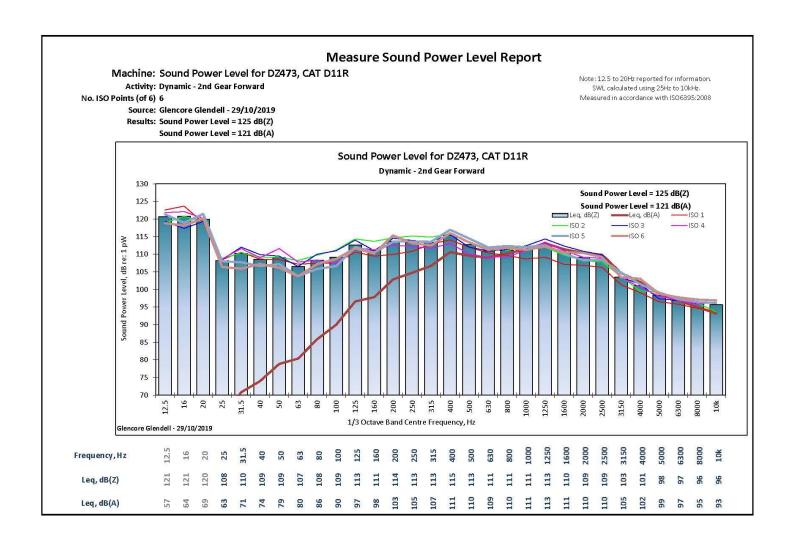
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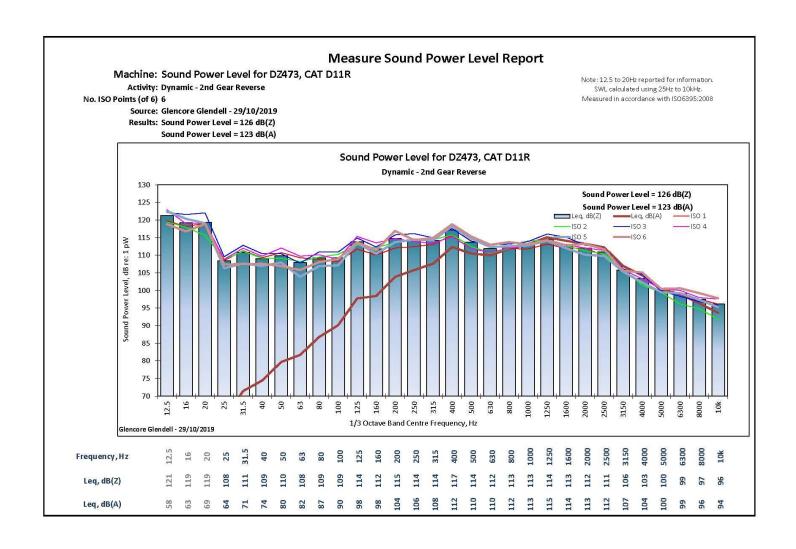
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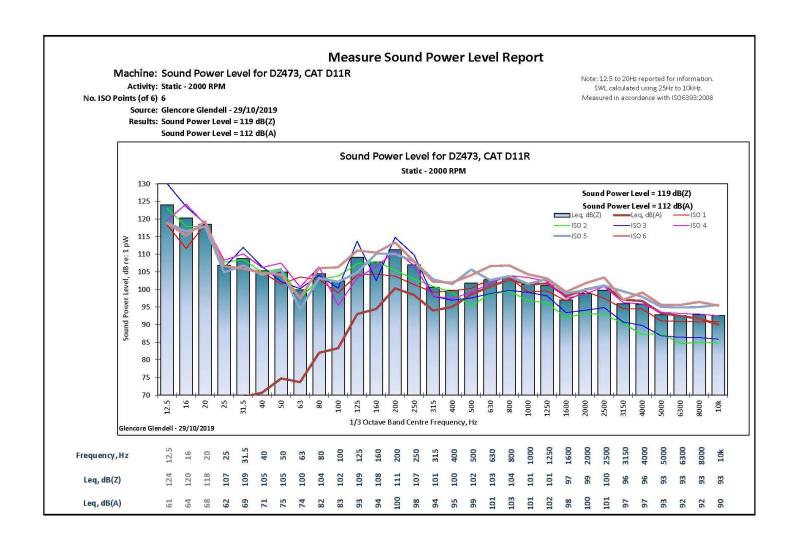
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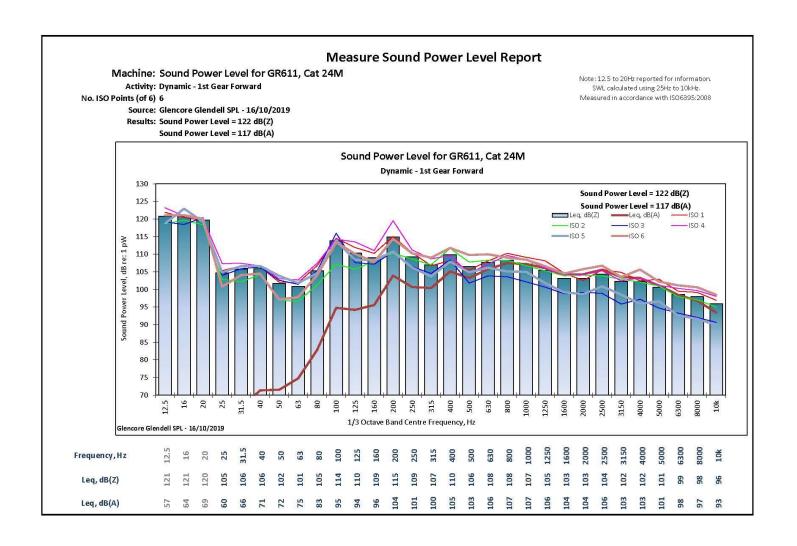
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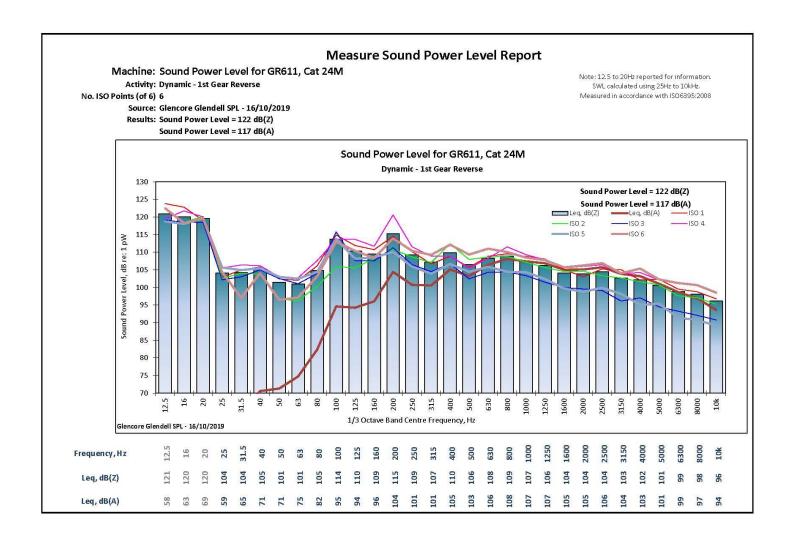
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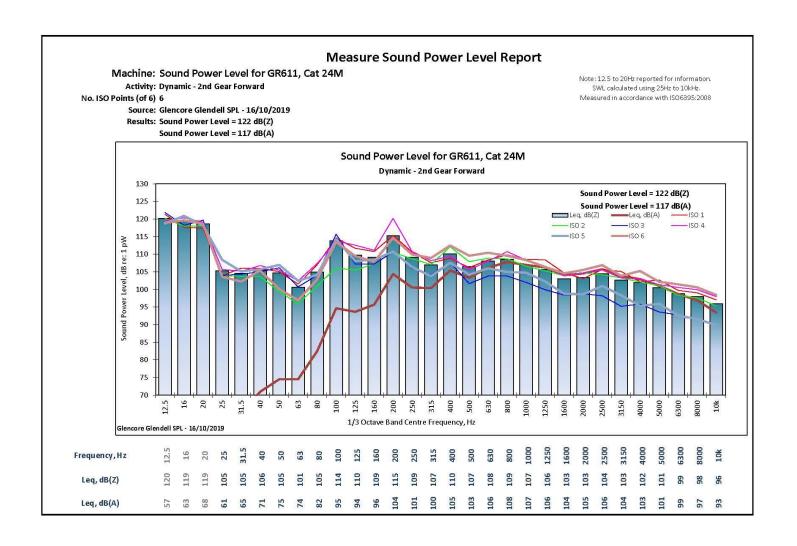
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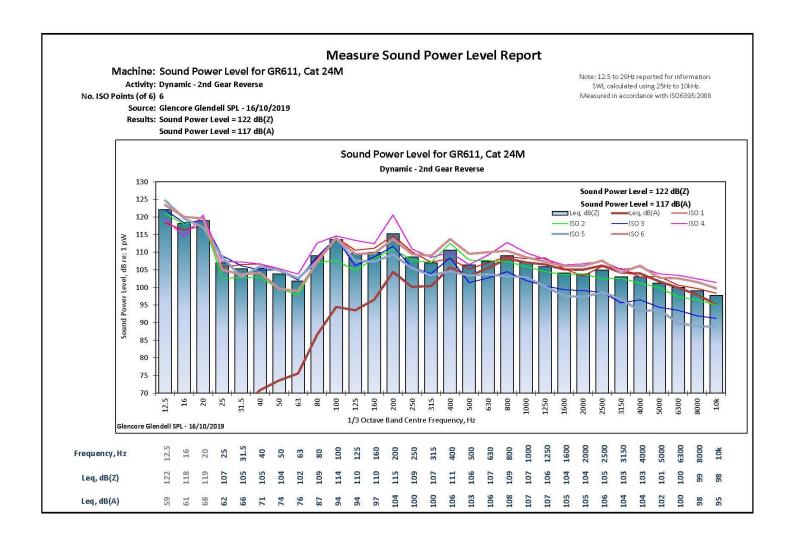
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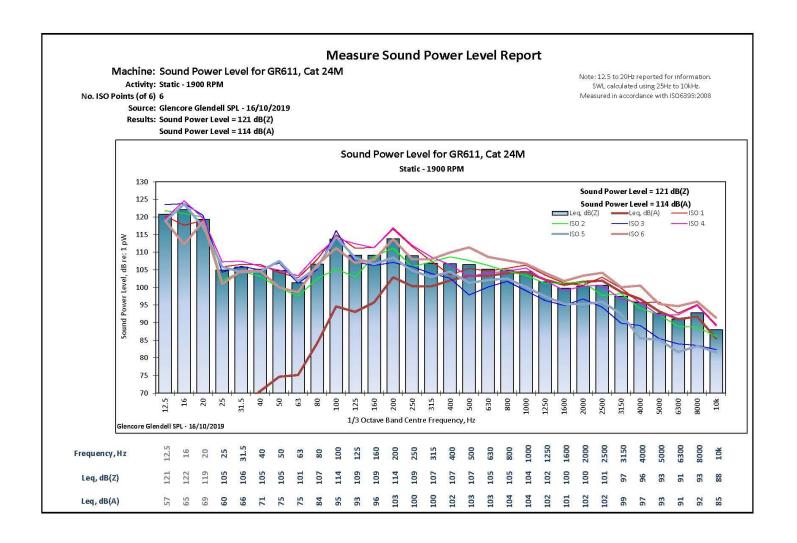
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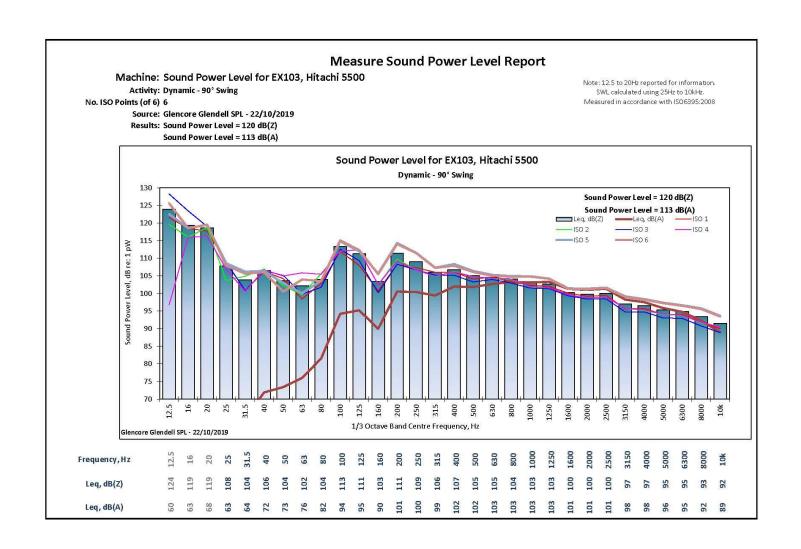
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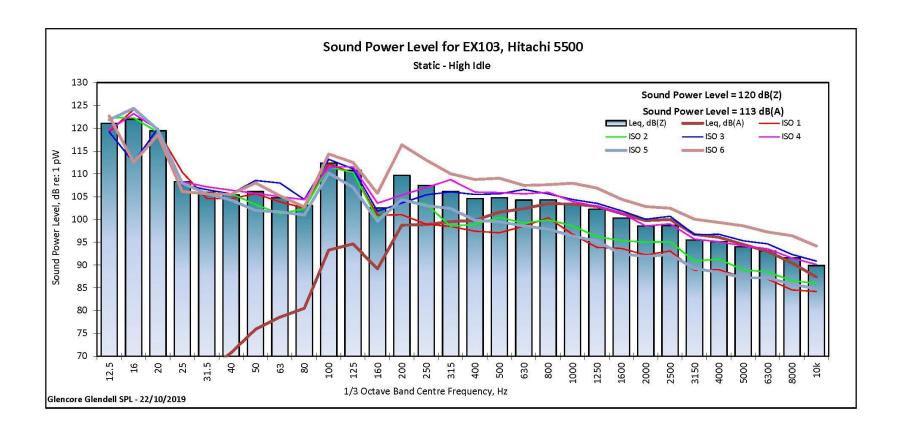


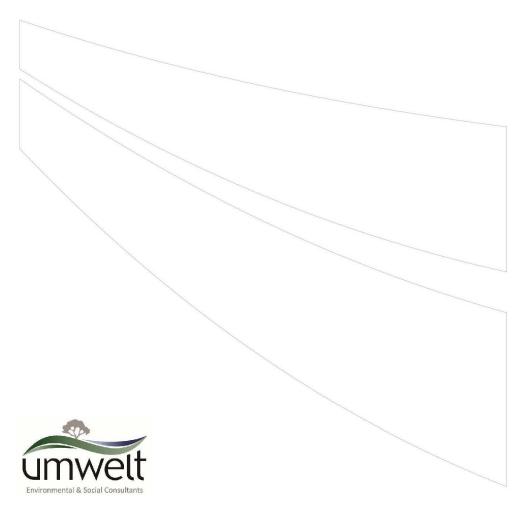
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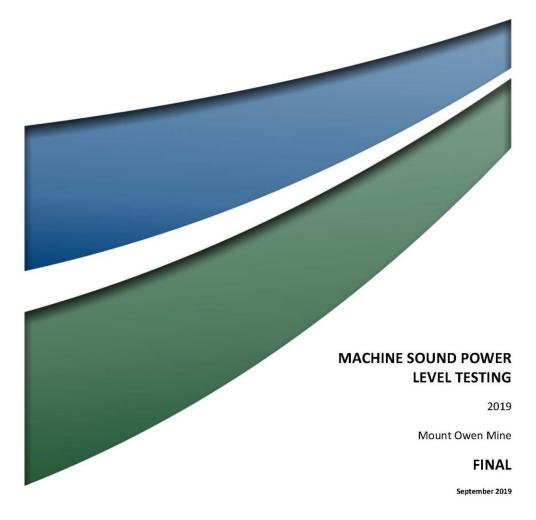
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MACHINE SOUND POWER LEVEL TESTING

2019

Mount Owen Mine

FINAL

Prepared by
Umwelt (Australia) Pty Limited
on behalf of
Thiess Mount Owen

Project Director: Tim Procter
Project Manager: Rod Williams
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Report No. 4609/R01
Date: September 2019



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Document Status

Rev No.	Reviewer		Approved for Issue		
	Name	Date	Name	Date	
1 Draft	Tim Procter	14 August 2019	Rod Williams	15 August 20189	
1 Final	Rod Williams	25 September 2019	Rod Williams	25 September 2019	



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Figure 1 Comparison of measured A-weight EX1850 sound power level with the one standard deviation envelop of equivalent equipment 8

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Appendices

Appendix A Methodology - Sound Power Level Testing of Mobile Equipment
Appendix B Calibration Certificates
Appendix C Sound Power Level Results

Machine Sound Power Level Testing 4609_R01_V1_Final



1.0 Introduction

As per the DPE approved Mount Owen/Glendell Noise Management Plan (MGOOC-1779562647-10975), ongoing monitoring requires periodic review of the equipment fleet, at a minimum review rate of 20% of the mobile fleet per year. Umwelt (Australia) Pty Limited (Umwelt) was engaged by Thiess to undertake sound power level (SWL) testing of a selection of mobile machines. **Table 1.1** lists the machines that were tested.

Table 1.1 Tested Machines

Machine Type	Machine ID	Make/Model
Dozers	DZ 1678	Caterpillar D10T
	DZ 1679	Caterpillar D10T
Graders	GR 1220	Caterpillar 24M
Loader	LO 1150	Caterpillar 992G
Haul Truck	RD 1757	Hitachi EH4500
	RD 1758	Hitachi EH4500
	RD 2744	Caterpillar 785C XQ
	RD 2728	Caterpillar 793F XQ
	RD 2741	Caterpillar 793F XQ
	RD 2738	Caterpillar 793F XQ
Water Carts	RD 2059	Caterpillar 777F
Drills	DR 0820	Drilltech D55SP
Excavators	EX 1850	Liebherr 996
	EX 8114	Liebherr 9100

Dynamic SWL was undertaken generally in accordance with the methodology presented in international standards ISO 6395 for dynamic testing and ISO 6393 for stationary (static) testing. In accordance with these standards, sound power is determined in one-third octave bands from 25 Hz to 10 kHz. However, Thiess requested assessment in one-third octave bands from 12.5 Hz to 10 kHz. The SWL testing methodology used is summarised in **Appendix A**. The calibration certificates for the sound measurement equipment can be found in **Appendix B**. The one-third octave results for each machine tested are presented in **Appendix C**.

Dynamic SWL testing of the equipment included their measurement in representative operating conditions, being:

- Dozers, graders and loaders in 1st and 2nd gear forward / reverse motion on relatively flat surfaces
- Haul truck laden up-ramp and unladen down-ramp directions
- Water carts laden up-ramp and laden down-ramp directions
- Drills while drilling
- Excavators through 90° swings.

Machine Sound Power Level Testing 4609_R01_V1_Final

Introduction



Static SWL testing of the equipment included stationary testing of machines at the same test site surface used for the dynamic test.

2.0 Results

2.1 Meteorological Conditions

Meteorological conditions at the time of the monitoring program are presented in Table 2.1.

Table 2.1 Local Meteorological Conditions (Sentinex13)

Date	Wind Speed (m/s)	Temperature (°C)	Relative Humidity (%)		
	Average (range)	Average (range)	Average (range)		
16/05/2019	2.0 (0.0 - 5.2)	15.0 (8.3 – 22.1)	79.4 (51.4 – 94.0)		
17/05/2019	1.2 (0.0 – 2.7)	15.6 (10.7 – 22.5)	79.2 (52.1 – 93.7)		
23/05/2019	0.0 (1.4 – 3.0)	16.8 (12.4 – 23.4)	76.4 (52.0 – 90.1)		

2.2 Measured Sound Power Levels

The Z and A-weighted sound power level results for machines in each operating condition are presented in **Table 2.2.** Detailed results for one-third octave bands of the sound power spectrum are included in **Appendix C**.

Table 2.3 lists the sound power level targets, including nominated A-weighted sound power targets from Mount Owen Continued Operations 2015 Environmental Impact Statement (MOCO EIS) and Z-weighted target in Glencore Noise Management Protocol GCAA-625378177-10238 (GCAA NMP). Delivered and inservice targets from GCAA NMP are regardless of mode or operation (i.e. both static and dynamic).

Table 2.4 compares the measured A and Z-weighted sound power levels against the relevant targets presented in



Table 2.2 2019 Sound Power Level Testing Results

Machine ID	Make / Model	Transmission/Mode of	Dynamic -	Up/Forward	Dynamic - Down/Reverse		Static		Testing Date
		operation	dB(Z)	dB(A)	dB(Z)	dB(A)	dB(Z)	dB(A)	
Dozers									
DZ 1678	Cat D10T	1 st gear	121	110	122	116	120	110	17/05/2019
		2 nd gear	124	120	128	125			
DZ 1679	Cat D10T	1 st gear	121	113	123	117	120	109	17/05/2019
		2 nd gear	125	122	128	126			
Graders									
GR 1220	Cat 24M	1 st gear	118	111	117	111	118	112	17/05/2019
		2 nd gear	119	112	118	112			
Loader									
LO 1150	Cat 992G	1 st gear	119	113	116	110	118	113	16/05/2019
		2 nd gear	116	111	116	111			
Haul Trucks									
RD 1757	Hitachi EH4500	1 st up / -	126	115	122	110	129	112	17/05/2019
RD 1758	Hitachi EH4500	1 st up / -	128	116	128	114	128	116	17/05/2019
RD 2744	Cat 785C XQ	1 st up / 4 th down	120	113	118	109	125	116	16/05/2019
RD 2728	Cat 793F XQ	1 st up / 4 th down	126	118	123	114	127	117	23/05/2019
RD 2741	Cat 793F XQ	1 st up / 3 rd down	127	119	127	118	126	119	17/05/2019
RD 2738	Cat 793F XQ	1 st up / 4 th down	126	117	123	114	129	119	23/05/2019
Water Carts									
RD 2059	Cat 777F	3 rd up / 4 th down	125	115	114	108	125	114	16/05/2019
Drills									
DR 0820	Drilltech D55SP	Drilling	116	112	-	-	115	112	23/05/2019
Excavators									
EX 1850	Liebherr 996	90° Swing	125	121	1.	-	128	125	23/05/2019
EX 8114	Liebherr 9100	90° Swing	116	106	-	-	113	104	23/05/2019



Table 2.3 Sound Power Level Target Values for Mount Owen Machines

Equipment	Operation Mode	MOCO EIS ¹	GCAA NMF	² Delivered	GCAA NMP ² In Service		
Description		dB(A)	Full Attenuated, dB(Z)	No Attenuation, dB(Z)	Full Attenuated, dB(Z)	No Attenuation, dB(Z)	
Dozer	Forward	112 - 113	121	127	123	129	
	Reverse (1 st /2 nd gear)	118-120 / 120-122					
Grader Cat 16M	Static/Dynamic	108	115	121	117	123	
Grader Cat 24M	Static/Dynamic	112	115	121	117	123	
Loader	Static/Dynamic	113	121	127	123	129	
Haul Truck	Up/Forward	116	121	130	123	132	
Cat 793 equiv.	Down/Reverse	114					
	Static	113					
Haul Truck	Up/Forward	114	121	130	123	132	
Cat 785 equiv.	Down/Reverse	111					
	Static	112					
Water Cart	Static/Dynamic	115	123	130	125	132	
Drill	Static/Dynamic	114	117	125	119	127	
Excavator Liebherr 996 equiv.	Static/Dynamic	117	123	130	125	132	
Excavator Liebherr 9400 equiv.	Static/Dynamic	116	123	130	125	132	

Note 1: nominated A-weighted sound power targets from Mount Owen Continued Operations 2015 Environmental Impact Statement (MOCO EIS)

Note 2: Z-weighted target in Glencore Noise Management Protocol GCAA-625378177-10238 (GCAA NMP). Delivered and in-service targets are regardless of mode or operation (i.e. both static and dynamic)



Table 2.4 Comparison of 2019 Sound Power Level Results Against Target Values

			Comparison Machine (see Table 2.3)	Dynamic					GCAA NMP	GCAA NMP
Machine ID	Make/Model	Transmission/Mode of operation		Up or	Forward	Down o	r Reverse	MOCO EIS	Delivered	In-Service
		or operation		dB(Z)	dB(A)	dB(Z)	dB(A)	dB(A)	dB(Z)	dB(Z)
Dozers										
DZ 1678	Cat D10T	1 st gear forward 1 st gear reverse	Dozer	121	110	122	116	Below Below	At +1 above	Below Below
DZ 1679	Cat D10T	1 st gear forward 1 st gear reverse	Dozer	121	113	123	117	At Below	At +2 above	Below At
Graders										
GR 1220	Cat 24M	1 st gear forward 1 st gear reverse	Grader Cat 24M	118	111	- 117	111	Below Below	+3 above +2 above	+1 above At
Loader										
LO 1150	Cat 992G	1 st gear forward 1 st gear reverse	Loader	119 -	113	116	- 110	At Below	Below Below	Below Below
Haul Trucks										
RD 1757	Hitachi EH4500	1 st up ramp 4 th down	Cat 793 equiv.	126	115	- 122	- 110	Below Below	+5 above +1 above	+3 above Below
RD 1758	Hitachi EH4500	1 st up ramp down ramp	Cat 793 equiv.	128	116	128	- 114	At At	+7 above +7 above	+5 above +5 above
RD 2744	Cat 785C XQ	1 st up ramp 4 th down	Cat 785 equiv.	120	113	118	109	Below Below	Below Below	Below Below
RD 2728	Cat 793F XQ	1 st up ramp 4 th down	Cat 793 equiv.	126	118	123	114	+2 above At	+5 above +2 above	+3 above At
RD 2741	Cat 793F XQ	1 st up ramp 4 th down	Cat 793 equiv.	127	119	127	118	+3 above +4 above	+6 above +6 above	+4 above +4 above
RD 2738	Cat 793F XQ	1 st up ramp 4 th down	Cat 793 equiv.	126	117	123	114	+1 above At	+5 above +2 above	+3 above At
Water Carts										
RD 2059	Cat 777F	3 rd up ramp 4 th down	Water Cart	125 -	115	114	108	At Below	+2 above Below	At Below
Drills										
DR 0820	Drilltech D55SP	Drilling	Drill	116	112	-	15	Below	Below	Below
Excavators										
EX 1850	Liebherr 996	90° Swing	Liebherr 996 equiv.	125	121	-		+4 above	+2 above	At
EX 8114	Liebherr 9100	90° Swing	NO REF DATA	116	106 ¹	:=:	100	NA	NA	NA

Note 1: 10 dB below Liebherr 996 equivalent A-weighted



3.0 Discussion

A discussion of the results relative to the corresponding target values (refer to **Table 2.3**) is included below. Tested machines are considered as 'in-service' and are compared against the GCAA NMP 'in-service' target values. Reference is made to GCAA NMP 'delivered' targets where measured results were both at, or below the 'in-service' targets and the 'delivered' targets. Results for dozer, loaders and graders in second gear forward and second gear reverse are not compared against target values.

Dozers

DZ1678

DZ1678 1^{st} gear forward and 1^{st} gear reverse results were below the MOCO EIS target for A-weighted sound power levels and below both the GCAA 'in-service' Z-weighted sound power level targets for machines with full attenuation. The test data, including static results, show a dominant 100 Hz frequency associated with engine exhaust.

DZ1697

DZ1697 1^{st} gear forward and 1^{st} gear reverse results were either at, or below the MOCO EIS target for A-weighted sound power levels and were either at, or below the Z-weighted GCAA 'in-service' sound power level targets for machines with full attenuation. The test data, including static results, show a dominant 100 Hz frequency associated with engine exhaust. 1^{st} gear reverse also reports a dominant frequency at 1250 Hz

Grader

GR1220 1^{st} gear forward and 1^{st} gear reverse results were below the MOCO EIS target for A-weighted sound power levels. 1^{st} gear forward Z-weighted results was 1 dB above the GCAA 'in-service' target for machines with full attenuation but below the Z-weighted target for machines with no attenuation. 1^{st} gear reverse Z-weighted was at the GCAA 'in-service' target for machines with full attenuation. The test data, including static results, show a dominant 200 Hz 1/3 octave level associated with engine noise.

Loader

LO1150 1^{st} gear forward and 1^{st} gear reverse results were either at, or below the MOCO EIS target for A-weighted sound power levels, and below the GCAA 'in-service' and 'delivered' Z-weighted sound power levels for machines with full attenuation.

Haul Trucks

RD1757

RD1757 1st gear up-ramp laden and 4th gear down-ramp unladen results were below the MOCO EIS target for A-weighted sound power levels. 1st gear up-ramp laden was 3 dB above the GCAA 'in-service' target for full-attenuation but below the Z-weighted target for no attenuation. 4th gear down-ramp unladen was below the GCAA 'in-service' target for machines with full attenuation. To reduce the Z-weighted by 3 dB, the sound power level from the rear of the truck would have to be reduce by 6 dB in the 50 and 80 Hz range. The dominance of the 50 to 80 Hz 1/3 octave level is clearly shown in the Laden Up-ramp chart for RD1757 in **Appendix C**.

RD1758

RD1758 1st gear up-ramp laden and 4th gear down-ramp unladen results were equal to the MOCO EIS target for A-weighted sound power levels. 1st gear up-ramp laden and 4th gear down-ramp unladen results were

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Discussion



both 5 dB above the GCAA 'in-service' Z-weighted target for full-attenuation but below the Z-weighted target for no attenuation. To reduce the Z-weighted by 4 to 5 dB, the sound power level from the rear of the truck would have to be reduce by 8 dB in the 50 and 125 Hz range. The dominance of the 50 to 125 Hz 1/3 octave level from the rear of the truck is clearly shown in the up-ramp laden chart and the Static chart for RD1758 in **Appendix C**. Treatment of the truck to reduce the sound power emanating from the rear of the truck when traveling up-ramp laden would reduce the down-ramp unladen sound power by 4 dB.

RD2744

RD2744 1st gear up-ramp laden and 4th gear down-ramp unladen results were both below the MOCO EIS target values for A-weighted sound power levels and below both the GCAA 'delivered' and 'in-service' Z-weighted sound power targets for machines with full attenuation.

RD 2728

RD 2728 1st gear up-ramp laden is 2 dB above the MOCO EIS target A-weighted sound power levels while 4th gear down-ramp unladen is equal to the MOCO EIS target A-weighted sound power levels. 1st gear up-ramp laden is 3 dB above the GCAA 'in-service' Z-weighted sound power target for full-attenuation, while 4th gear down-ramp unladen is equal to the target. Both 1st gear laden up-ramp and 4th gear down-ramp unladen are below Z-weighted target for 'in-service' no attenuation. Reducing the dominant 2000 Hz 1/3 octave level from the rear of the truck, clearly shown in the up-ramp laden chart for RD2728 in **Appendix C**, by 6 dB would reduce the overall A-weighted sound power level by 2 dB. To reduce the Z-weighted by 3 dB the sound power level from the engine exhaust presenting at the rear and right-hand side of the truck would need to be reduce by 6 dB in the 50 and 100 Hz range. The dominance of the 50 and 100 Hz 1/3 octave level from the rear of the truck is clearly shown in the up-ramp laden chart for RD2728 in **Appendix C**.

RD2714

RD2714 1st gear up-ramp laden and 4th gear down-ramp unladen are 3 dB and 4 dB above the MOCO EIS target values for A-weighted sound power levels, respectively. 1st gear up-ramp laden and 4th gear down-ramp unladen are 4 dB above the GCAA 'in-service' Z-weighted sound power target for full-attenuation. Both 1st gear laden up-ramp and 4th gear down-ramp unladen are below Z-weighted target for 'in-service' no attenuation. Reducing the 800 to 2000 Hz 1/3 octave level from the rear and right-hand side of the truck, apparent in the up-ramp laden chart for RD2741 in **Appendix C**, by 6 dB and reducing the 160 Hz from the front of the tuck by at least 6 dB would reduce the overall A-weighted sound power level by 3 dB. Treatment of the truck to reduce the sound power emanating from the rear and right-hand side of the truck and the 160 Hz from the front would reduce the down-ramp unladen sound power by 4 dB. To reduce the Z-weighted by 4 dB the sound power level from the engine enclosure needs to be reduce by 6 dB in the 50 and 125 Hz range. The dominance of the 50 and 125 Hz 1/3 octave level from the rear of the truck is shown in the up-ramp laden chart for RD2741 in **Appendix C**. Treatment of the truck to reduce the sound power emanating from the engine enclosure would reduce the down-ramp unladen sound power by 4 dB

RD2738

RD2738 1st gear up-ramp laden is 1 dB above the MOCO EIS target A-weighted sound power level, while 4th gear down-ramp was equal to the target A-weighted sound power level. 1st gear up-ramp laden is 3 dB above GCAA 'in-service' Z-weighted sound power target for full-attenuation, while 4th gear down-ramp unladen is equal to the target. Both results are below the Z-weighted sound power levels for no attenuation. Reducing the 2000 Hz 1/3 octave level from the rear of the truck, shown in the up-ramp laden chart for RD2738 in **Appendix C**, by up to 6 dB would reduce the overall A-weighted sound power level by 1 dB. To reduce the Z-weighted by 3 dB the sound power level from the engine exhaust presenting at the in the 50 and 100 Hz range would need to be reduced by 6 dB. The presence of the 50 and 100 Hz 1/3 octave level are shown in the up-ramp laden chart for RD2738 in **Appendix C**.

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Water Cart

RD2059 3rd gear up-ramp laden and 4th gear down-ramp laden were either at, or below the MOCO EIS target for A-weighted sound power levels and at, or below the GCAA NMP 'in-service' Z-weighted sound power levels for machines with full attenuation. The test data, including static results, show a dominant 80 Hz 1/3 octave level associated with the engine exhaust.

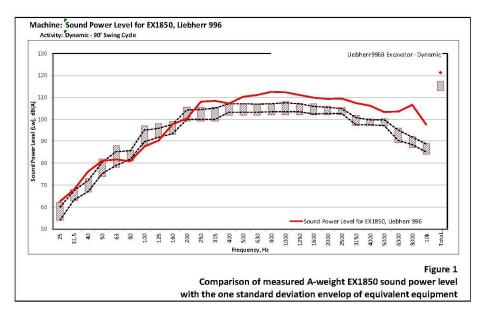
Drill

The dynamic results for DR0820 were below the MOCO EIS target for A-weighted sound power levels and below the GCAA 'in-service' Z-weighted sound power levels for machines with full attenuation.

Excavators

EX1850

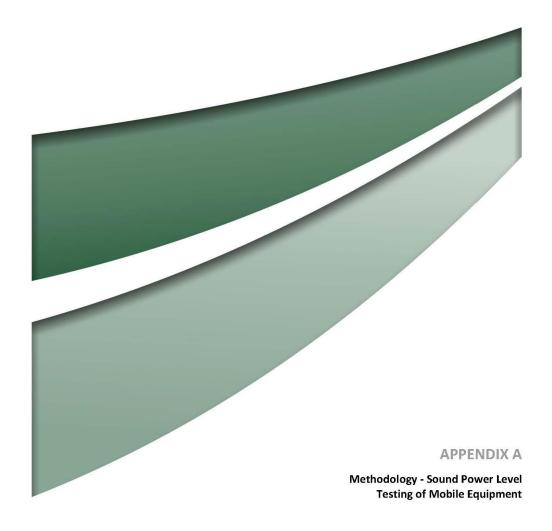
The dynamic result was for EX1850 were 4 dB above the MOCO EIS target for A-weighted sound power level and equal to the GCAA NMP 'in-service' Z-weighted sound power levels for machines with full attenuation. The test data shows the presence of dominant frequencies in the 250 to 8000 Hz 1/3 octave level range. The test data, presented in **Figure 1** compared with the one standard deviation envelop of equivalent equipment, indicates the higher than anticipated sound power level is likely associated with the excavator fans. As the fan sound attenuation equipment was in place, it is likely the fan speeds were controlled to 75% of the maximum speed. Below 250 Hz the measured 1/3 octave sound power levels are within the one standard deviation envelop of equivalent equipment.



EX8114

The dynamic results for EX8114 were 10 dB below the MOCO EIS target for A-weighted sound power level of the larger waste excavators.

Machine Sound Power Level Testing 4609_R01_V1_Final Discussion





A.1 Testing Standards

The monitoring program was conducted in accordance with:

MGD15 - Mobile and transportable plant for use on mines and petroleum sites (Amd. 2018)

ISO 6395:2008 – Earth-moving machinery - Determination of sound power level - Dynamic test conditions

ISO 6393:2008 – Earth-moving machinery - Determination of sound power level - Stationary test conditions

ISO 3744:2010 - Acoustics – Determination of sound power levels and sound energy levels of noise sources using sound pressure – Engineering methods for an essentially free field over a reflecting plane

ISO 4872 – Measurement of airborne noise emitted by construction equipment intended for outdoor use -- Method for determining compliance with noise limits

The monitoring program also took into consideration the requirements of:

AS 2012.2-1990 – Acoustics - Measurement of airborne noise emitted by earth-moving machinery and agricultural tractors - Stationary test condition, Operator's position

AS/NZS 1269.1-2005 - Occupational noise management - Measurement and assessment of noise immission and exposure

A.2 Equipment Used

The monitoring program was conducted using the following equipment

SVAN958A (59838) - four (4) channel sound and vibration analyser

SVAN958A (59839) - four (4) channel sound and vibration analyser

SVAN SV36 (90131) - 94/114 dB calibrator

Kestrel 4500 – weather meter

Calibration certificates are included in Appendix B.

A.3 Sound Power Level Testing

The monitoring program methodology is outlines as follows:

- Sound power levels have been determined in one-third octave bands.
- Glencore Coal Assets Australia (GCAA) protocol GCAA 11.11 Noise Management requires the
 measurements to be from 25 Hz to 10 kHz to enable reporting of Linear (Z-weighted) and A-weighting
 sound power levels. Data capture data from 12.5 Hz to 20 Hz has been included in the reporting of the
 monitoring data but not the determination of sound power levels. The 12.5 Hz to 20 Hz data can be
 used to assess low frequency noise and/or are often identifiable within the background acoustic
 environment.

Machine Sound Power Level Testing 4609_R01_V1_Final Appendix A

1



- Measurements made from six ISO microphones. Figure A.1 shows the horizontal (left image) and vertical (right image) positions of each microphone.
- The size of the measurement surface is determined as per ISO 6395:2008(E). This generally constitutes a radius of 16 20m to accommodate the tested haul trucks.

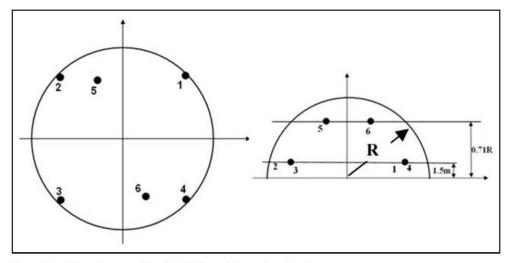


Figure A.1 - Microphone position for ISO Sound Power Level testing

A.4 Test Area Environment

The test areas included a haul road and flat dump area with sufficient length to allow machines to safely accelerate, pass through the test area and decelerate.

In accordance with ISO 6395 and GCAA 11.11 Noise Management Protocol, the location of the test area was chosen to minimise the impacts of reflective surfaces such as highwalls and windrows.

Care was also taken to ensure that background noise levels were at least 6 dB less than measured equipment being tested. A correction is also applied for background levels between 6 dB - 15 dB less than measured dynamic levels to ensure that background noise has limited effect on measured levels. In addition to this, Mount Owen requires the background noise levels to be reported in one-third octave bands from 12.5 Hz to 10 kHz

The haul road test area had a nominal slope of approximately 10%. Testing consisted of up-ramp loaded test and a down-ramp unloaded test on the haul road. The dump area had a slope of approximately 0% to facilitate the forward and reverse testing of the bulldozers and rubber tyres dozer.

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Appendix A



A.5 Mobile Equipment

Haul truck up-ramp laden test

As per GCAA 11.11 Noise Management Protocol, haul trucks are loaded with the nominal rated load and driven up hill through the test area while maintaining the manufacturers rated engine speed. Trucks progress at a consistent speed through the test area.

Haul truck down-ramp unladen test

As per GCAA 11.11 Noise Management Protocol, the unloaded haul truck moved down-ramp through the test area while maintaining the maximum descent speed considered safe (approximately 20-23 km/hr). Trucks progress at a consistent speed through the test area.

Water truck

As per GCAA 11.11 Noise Management Protocol, up-ramp and down-ramp tests are conducted with the water truck operating with the maximum rated load

Bulldozer and loader 1st gear test forward and reverse

As per GCAA 11.11 Noise Management Protocol, earthmoving machine moved through the test area unloaded in 1^{st} gear/ 2^{nd} gear at a constant speed with auxiliary equipment attached and raised to approximately 0.3 m above the test surface.

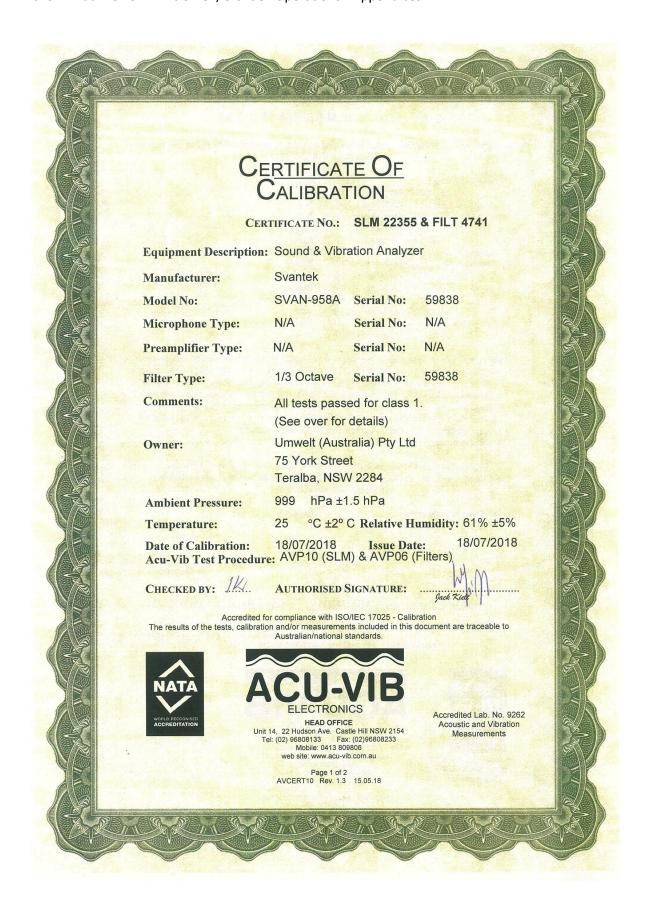
Bulldozer and loader 2nd gear test forward and reverse

To provided reference material for assessing machine performance and data for noise modelling purposes the earthmoving machine moved through the test area unloaded in 2nd gear at a constant speed with auxiliary equipment attached and raised to approximately 0.3 m above the test surface.

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Appendix A





CERTIFICATE No.: SLM 22355 & FILT 4741

The performance characteristics listed below were tested. The tests are based on the relevant clauses of IEC 61672-3:2013

Tests Performed:	Clause	Result
Absolute Calibration	10	N/A
Acoustical Frequency Weighting	12	N/A
Self Generated Noise	11.1	N/A
Electrical Noise	11.2	Entered
Long Term Stability	15	Pass
Electrical Frequency Weightings	13	Pass
Frequency and Time Weightings	14	Pass
Reference Level Linearity	16	Pass
Range Level Linearity	17	Pass
Toneburst	18	Pass
Peak C Sound Level	19	Pass
Overload Indicator	20	Pass
High Level Stability	21	Pass

Statement of Compliance: The sound level meter submitted for testing has successfully completed the class 1 periodic tests of IEC 61672-3:2013, for the environmental conditions under which the tests were performed. As public evidence was available, from an independent organization responsible for approving the results of pattern evaluation tests performed in accordance with IEC 61672-2:2013, to demonstrate that the model of sound level meter fully conformed to the requirements in IEC 61672-1:2013, the sound level meter submitted for testing conforms to the class 1 requirements of IEC61672-1:2013.

A full technical report is available if required.

This Sound Level Meter included an Octave Filter Set. Tests were based on IEC 1260: 1995 and AS/NZS 4476 - 1997 and were conducted to test the following performance characteristics:

1. Relative attenuation

clause 5.3

Checked by: Accredited for compliance with ISO/IEC 17025 - Calibration
The results of the tests, calibration and/or measurements included in
this document are traceable to Australian/national standards.

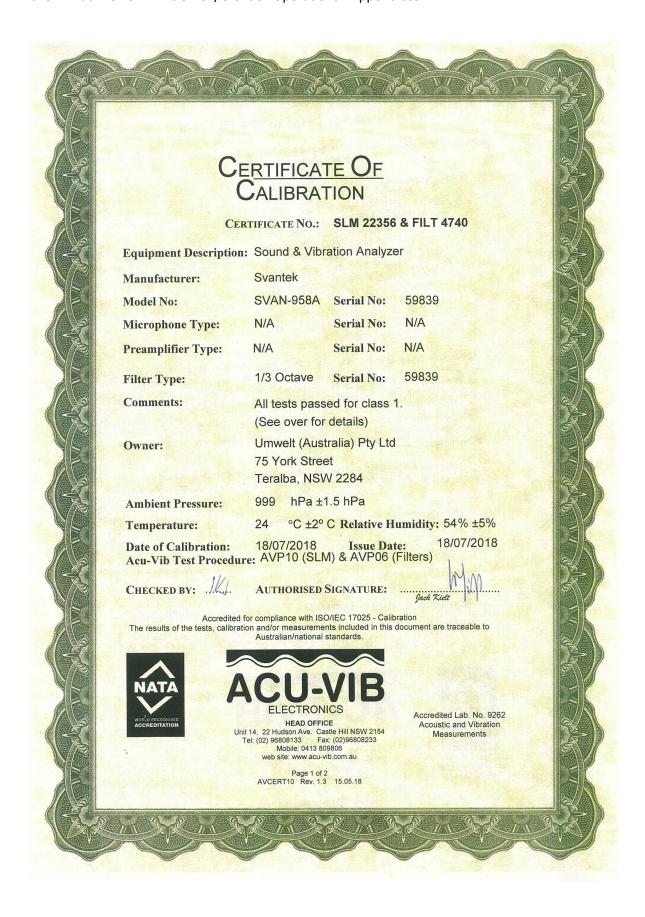


Accredited Lab. No. 9262
Acoustic and Vibration
Measurements



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web site: www.acu-vib.com.au

Page 2 of 2 End of Calibration Certificate
AVCERT10



CERTIFICATE No.: SLM 22356 & FILT 4740

The performance characteristics listed below were tested. The tests are based on the relevant clauses of IEC 61672-3:2013

Tests Performed:	Clause	Result
Absolute Calibration	10	N/A
Acoustical Frequency Weighting	12	N/A
Self Generated Noise	11.1	N/A
Electrical Noise		Entere
Long Term Stability	15	Pass
Electrical Frequency Weightings	13	Pass
Frequency and Time Weightings	14	Pass
Reference Level Linearity	16	Pass
Range Level Linearity	17	Pass
Toneburst	18	Pass
Peak C Sound Level	19	Pass
Overload Indicator	20	Pass
High Level Stability	21	Pass

Statement of Compliance: The sound level meter submitted for testing has successfully completed the class 1 periodic tests of IEC 61672-3:2013, for the environmental conditions under which the tests were performed. As public evidence was available, from an independent organization responsible for approving the results of pattern evaluation tests performed in accordance with IEC 61672-2:2013, to demonstrate that the model of sound level meter fully conformed to the requirements in IEC 61672-1:2013, the sound level meter submitted for testing conforms to the class 1 requirements of IEC61672-1:2013. A full technical report is available if required.

This Sound Level Meter included an Octave Filter Set. Tests were based on IEC 1260: 1995 and AS/NZS 4476 - 1997 and were conducted to test the following performance characteristics:

1. Relative attenuation

Date of Calibration: 18/07/2018

Issue Date: 18/07/2018

Checked by: /K/

by: Accredited for compliance with ISO/IEC 17025 - Calibration
The results of the tests, calibration and/or measurements included in
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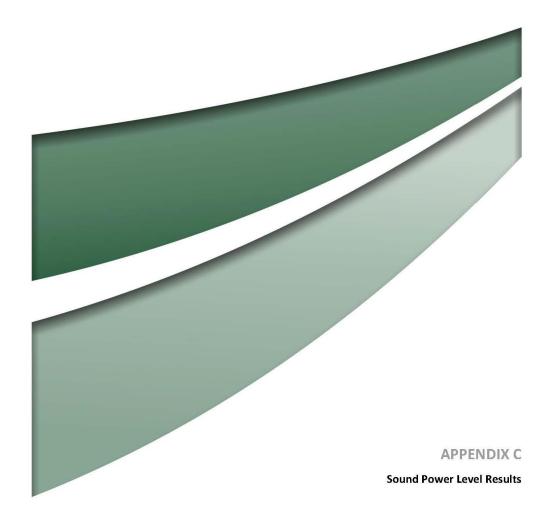


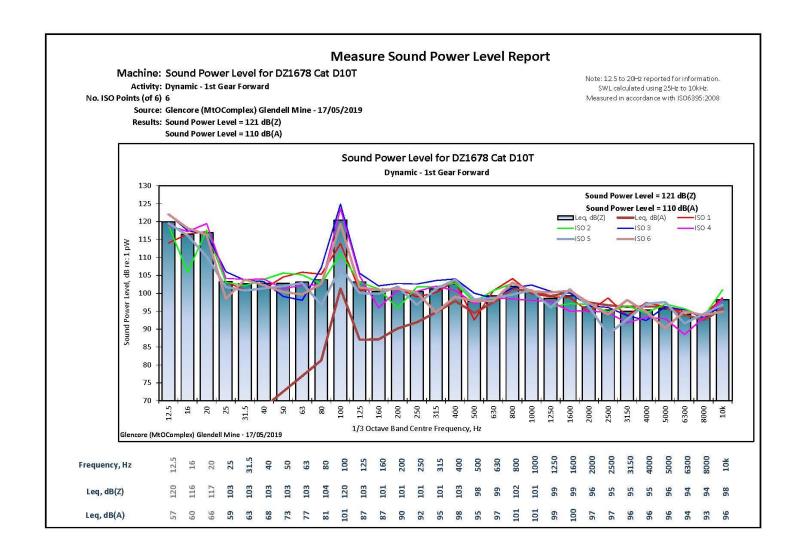
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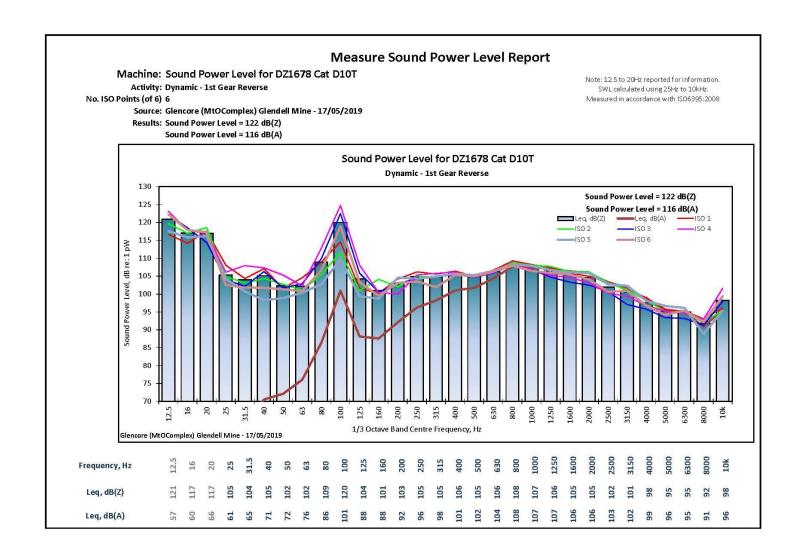
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Page 2 of 2 End of Calibration Certificate AVCERT10

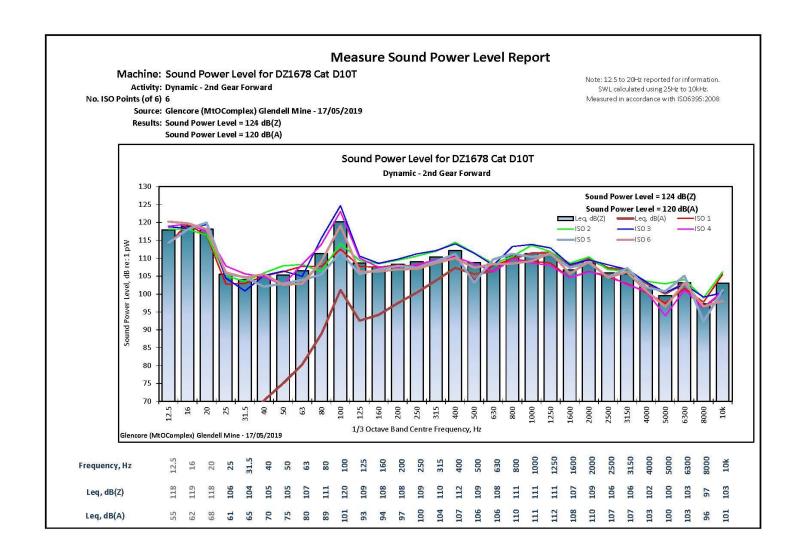




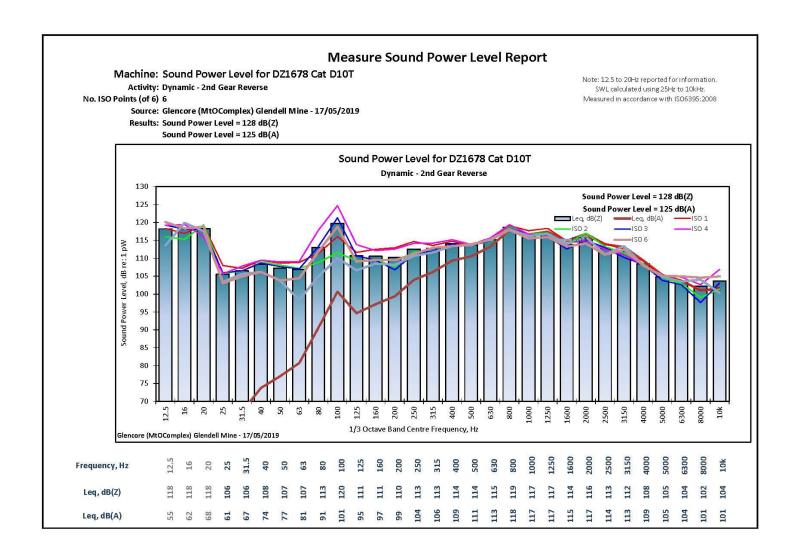
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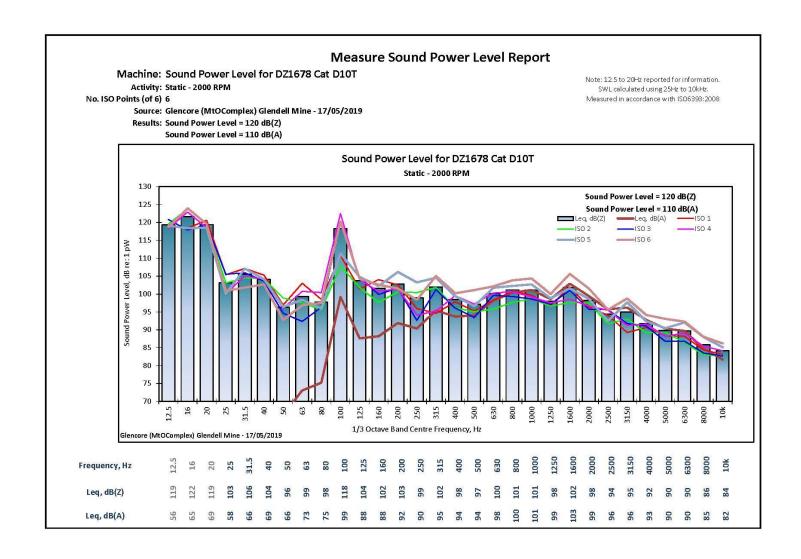
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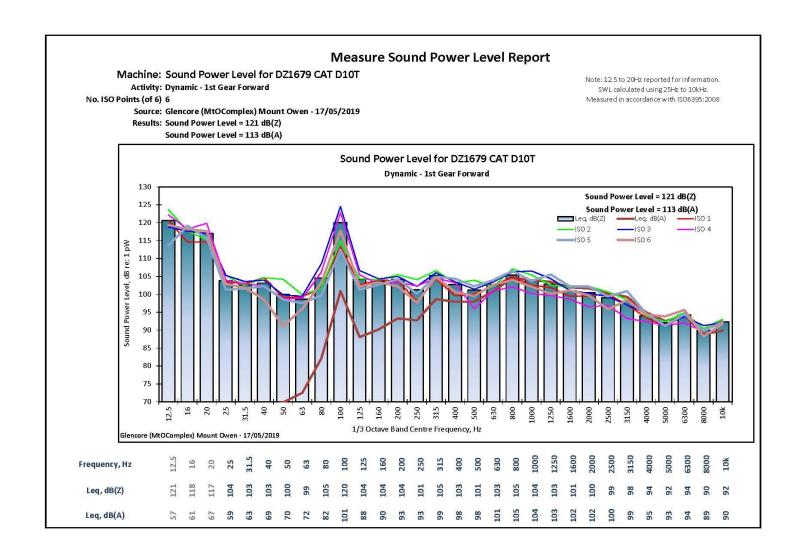
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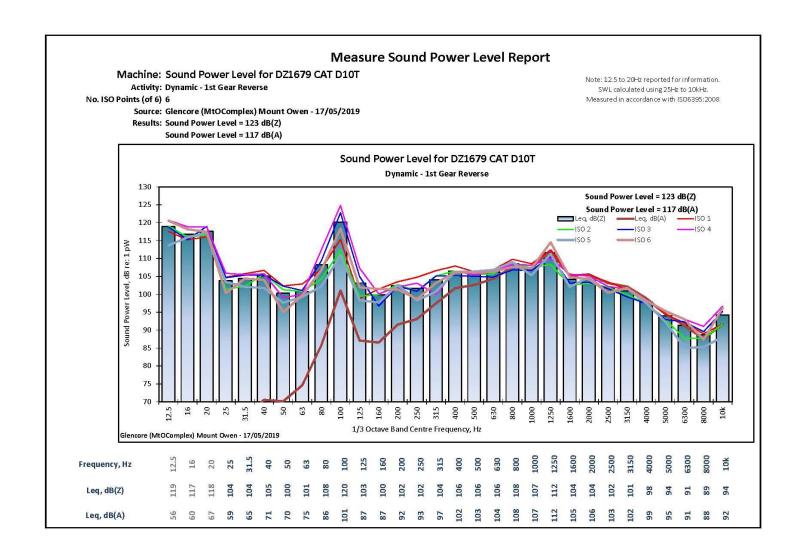
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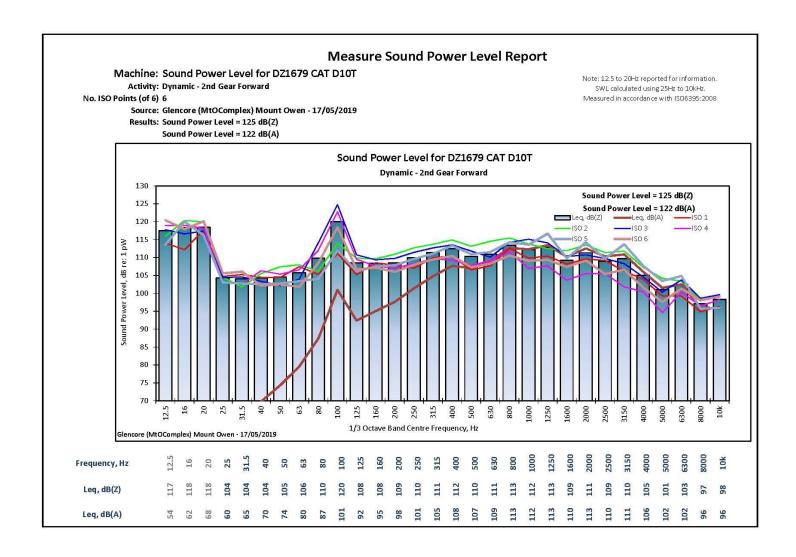
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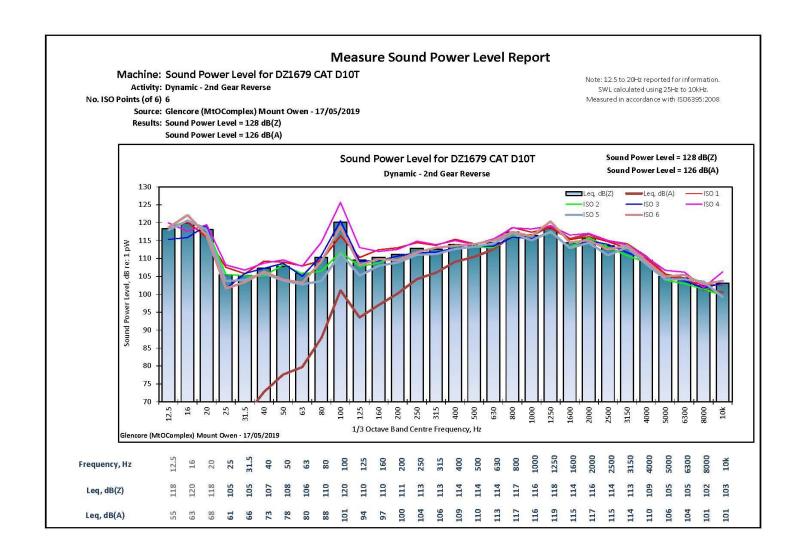
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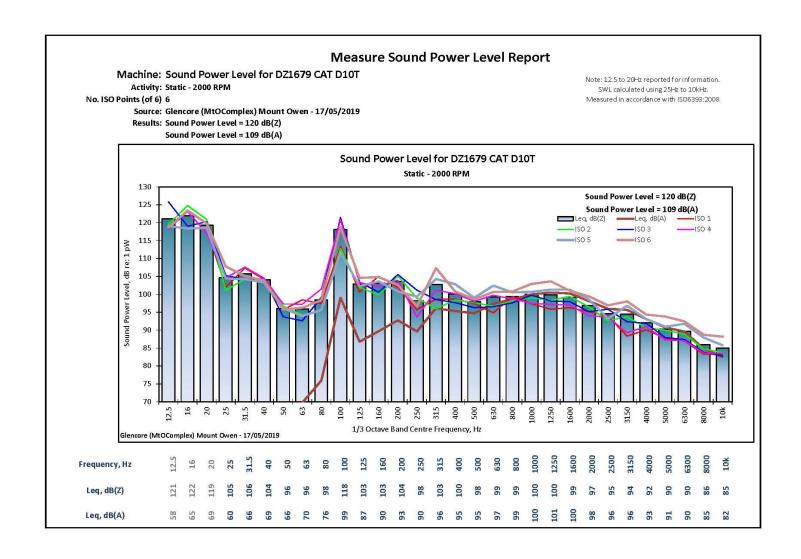
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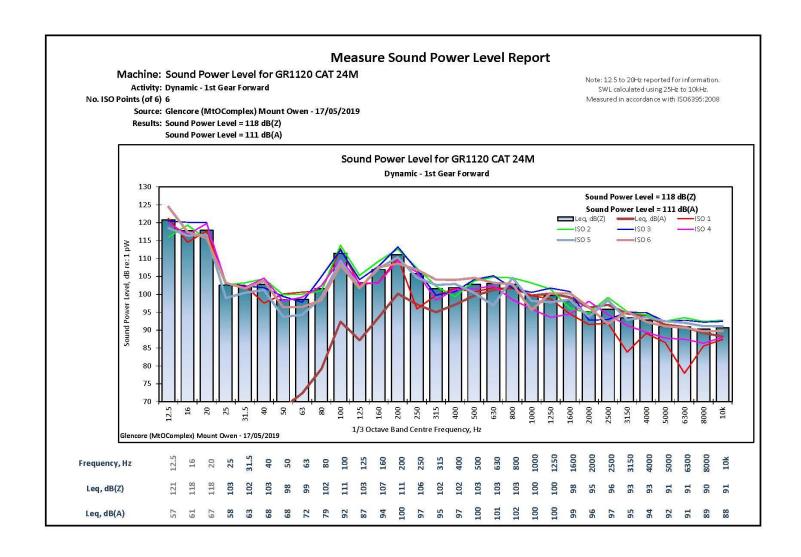
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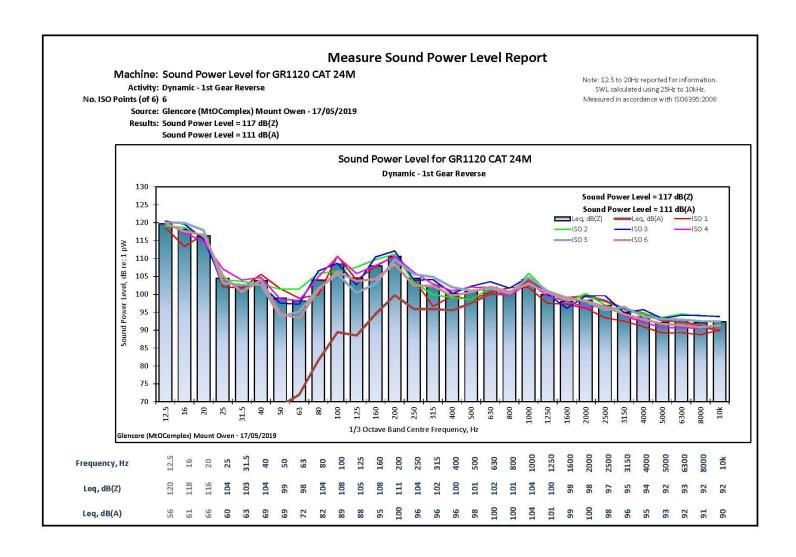
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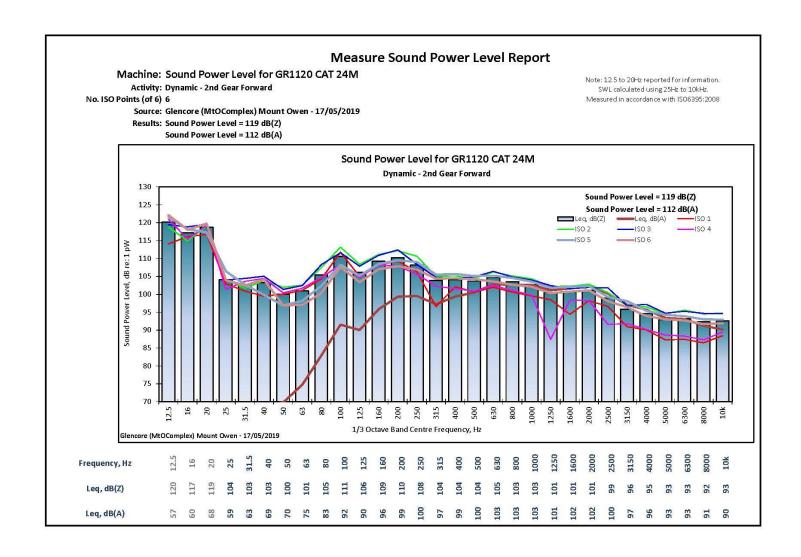
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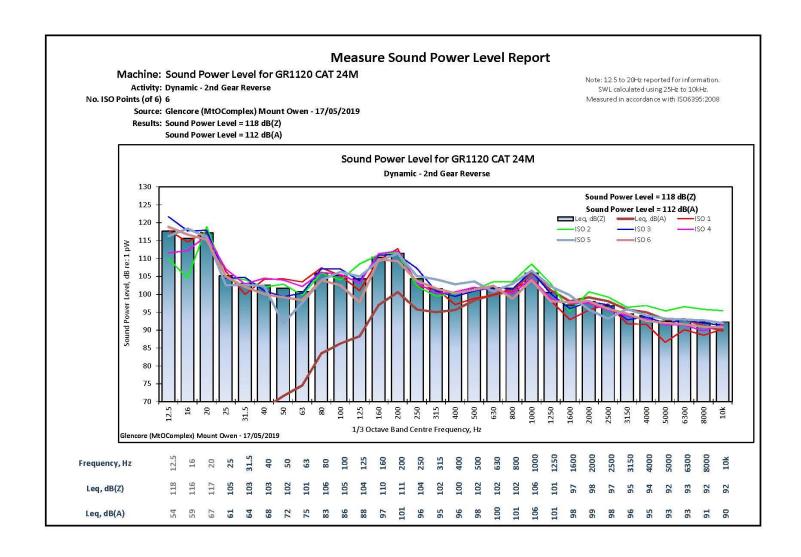
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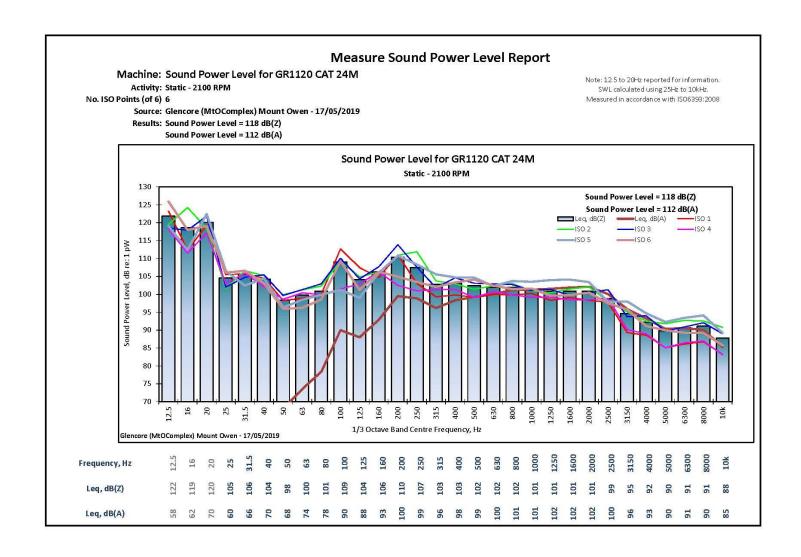
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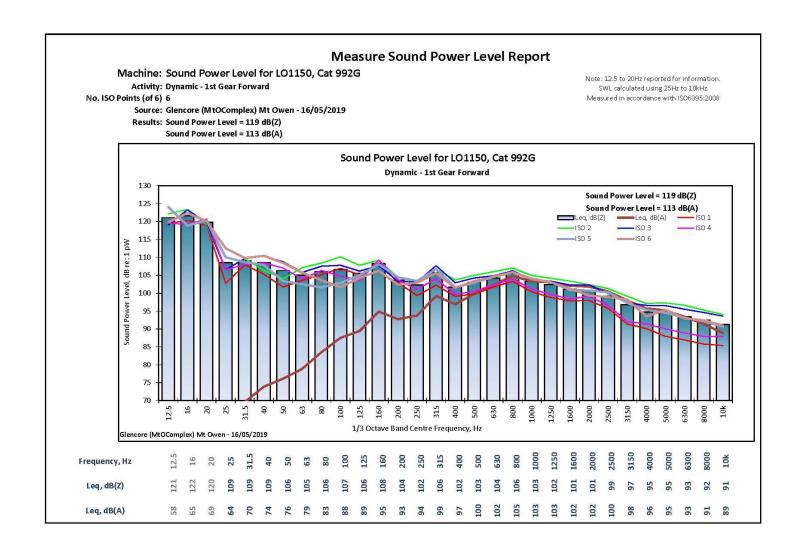
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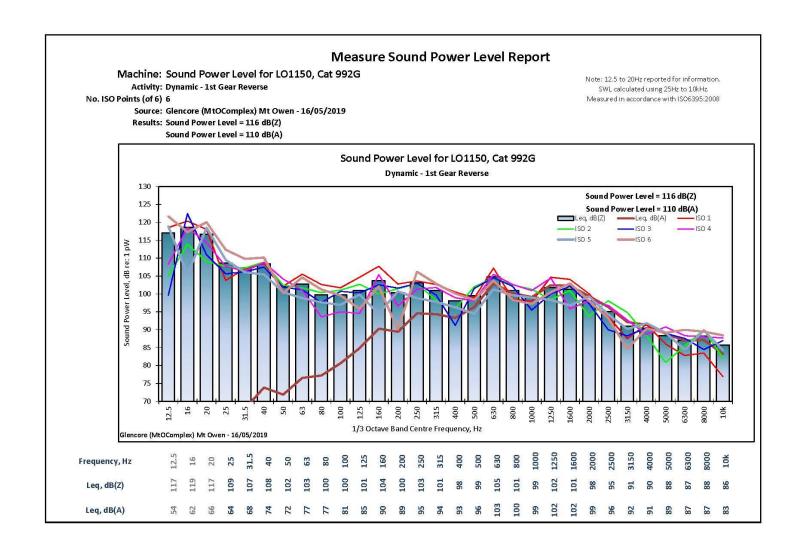


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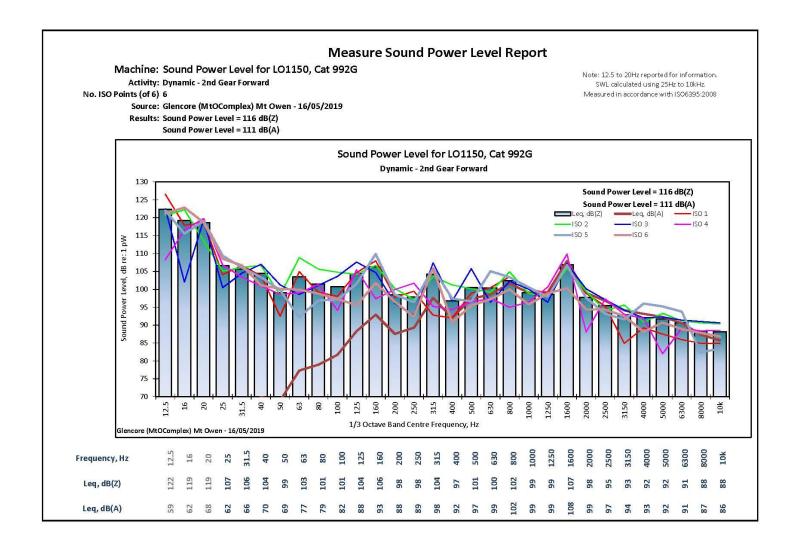


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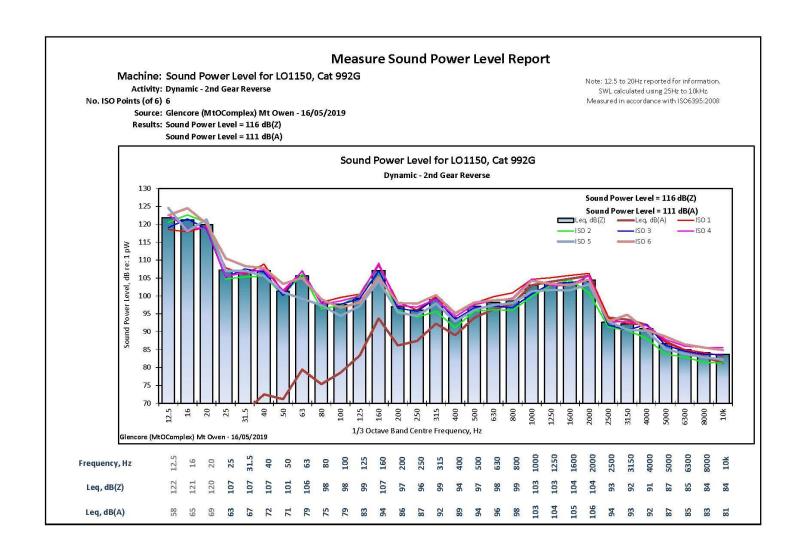
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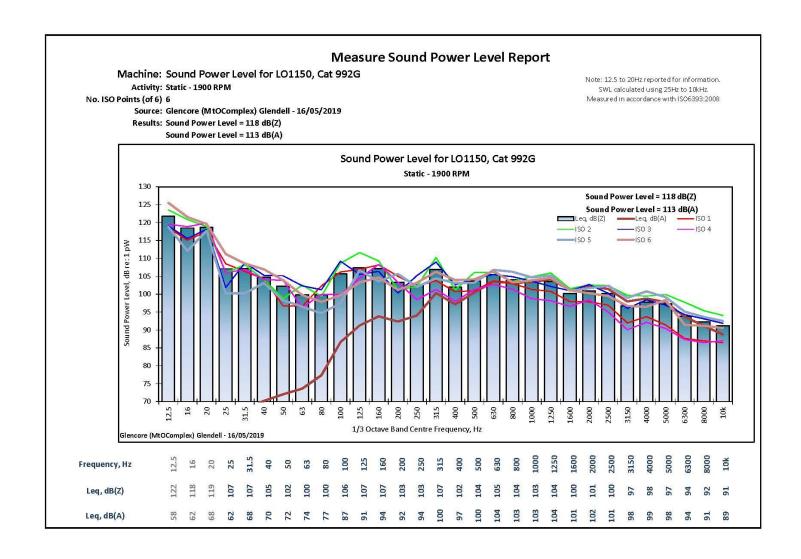
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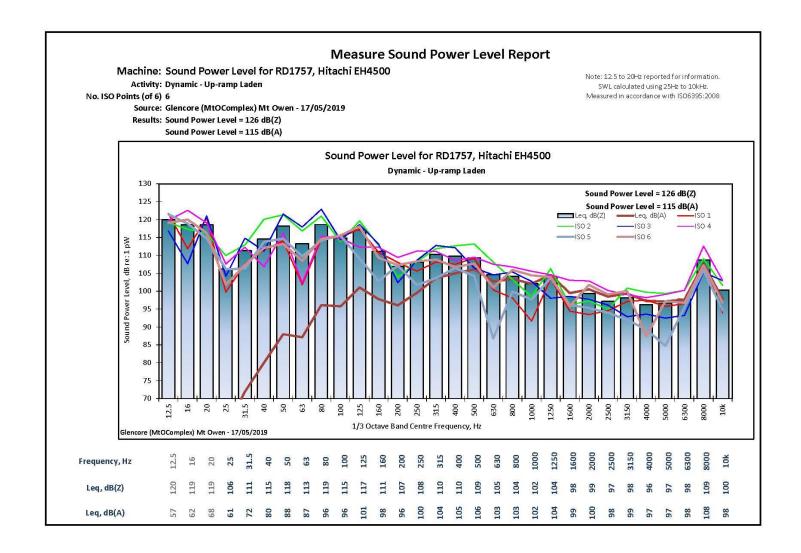
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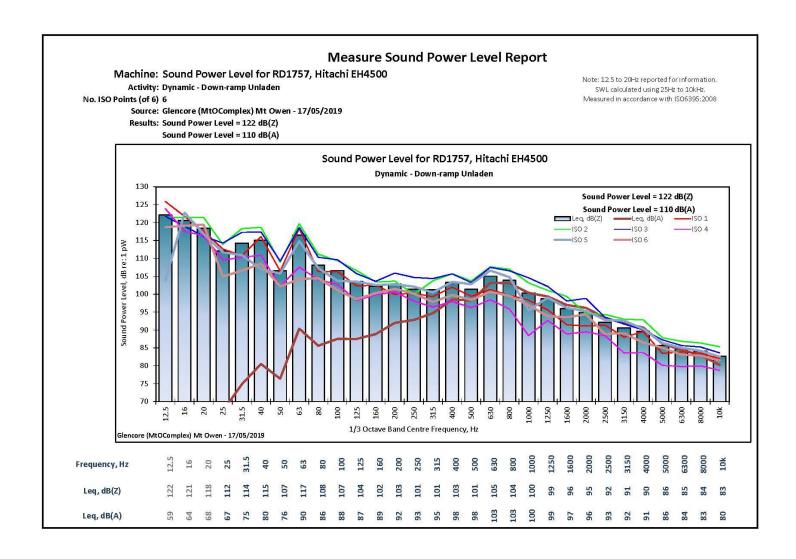
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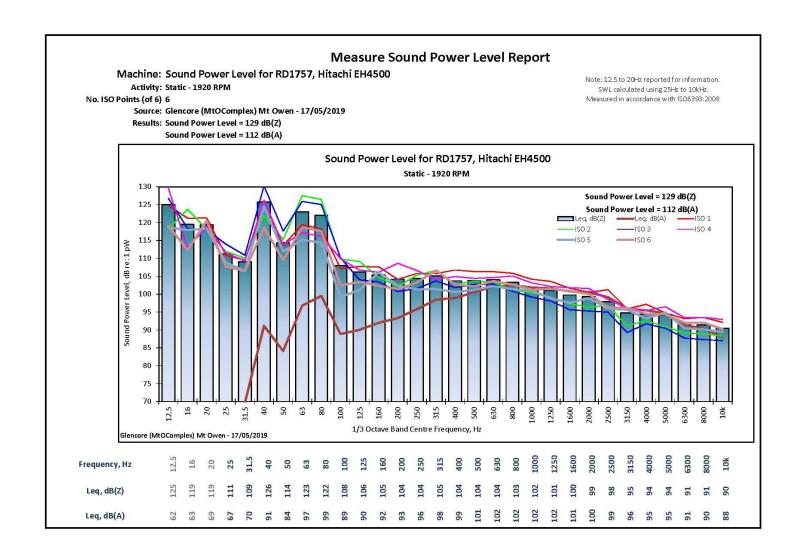
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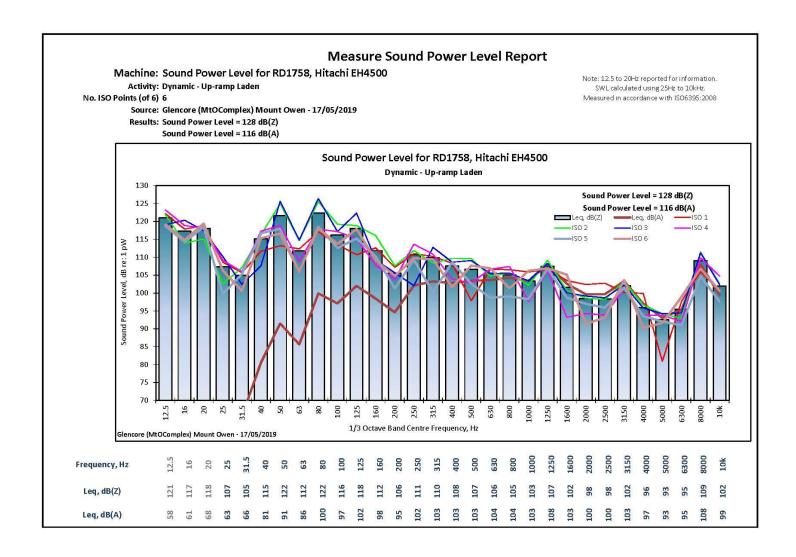
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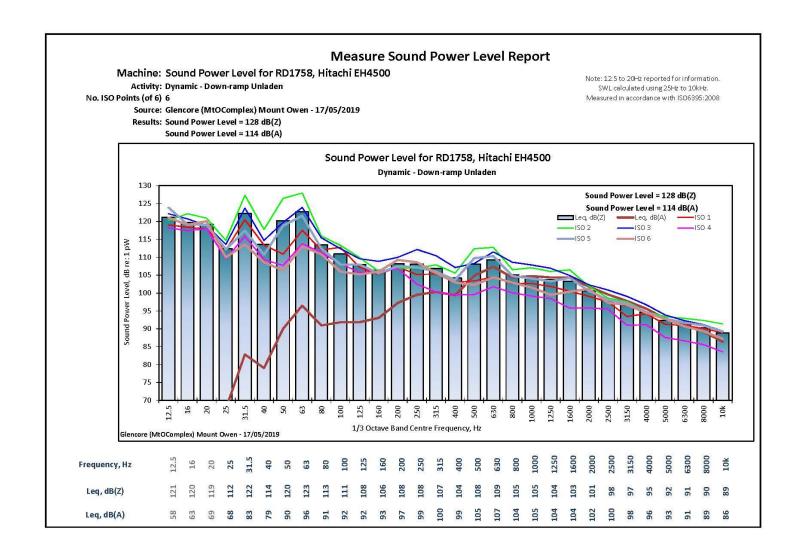
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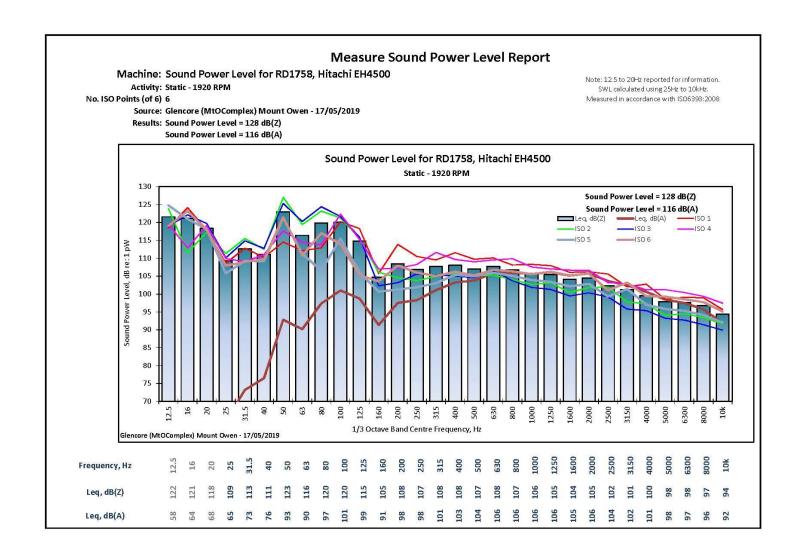
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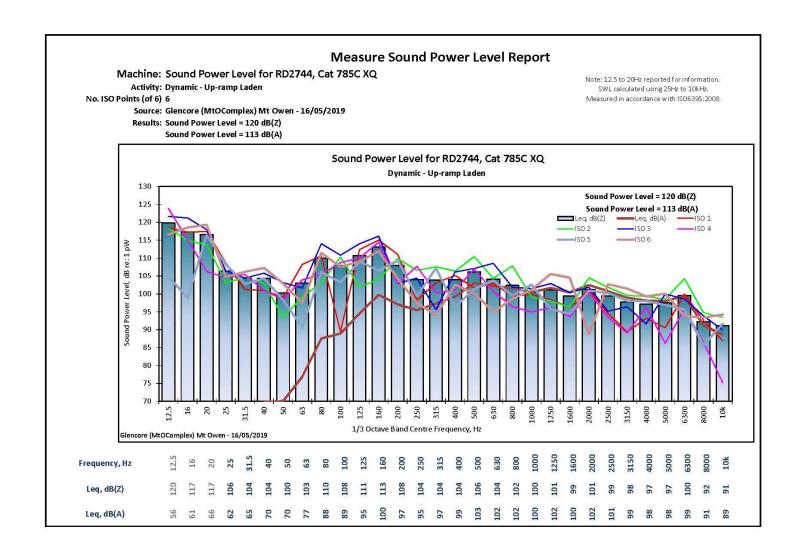
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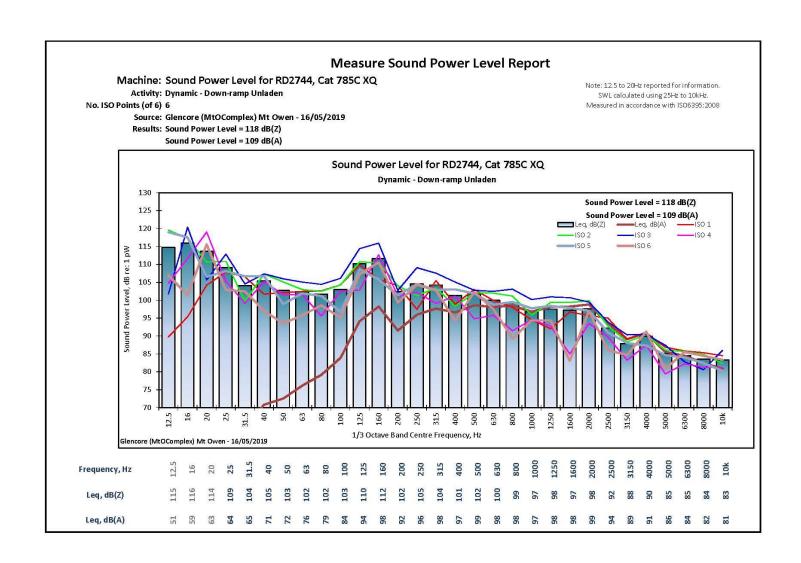
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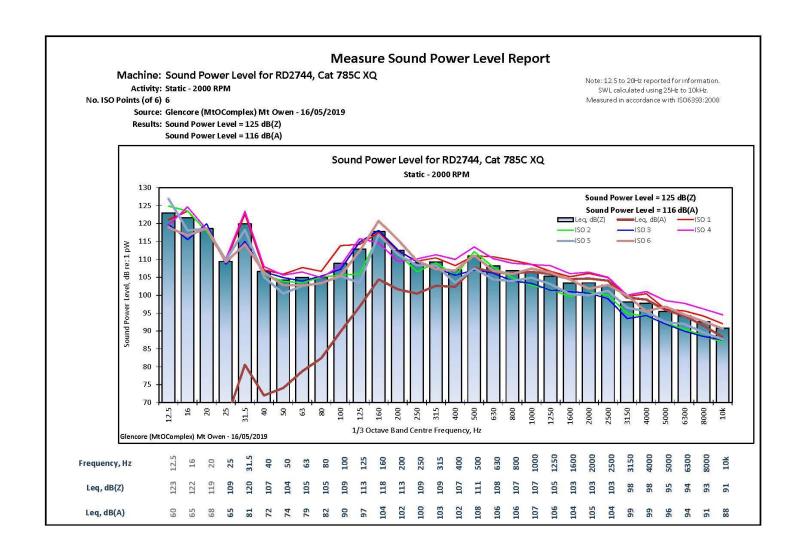


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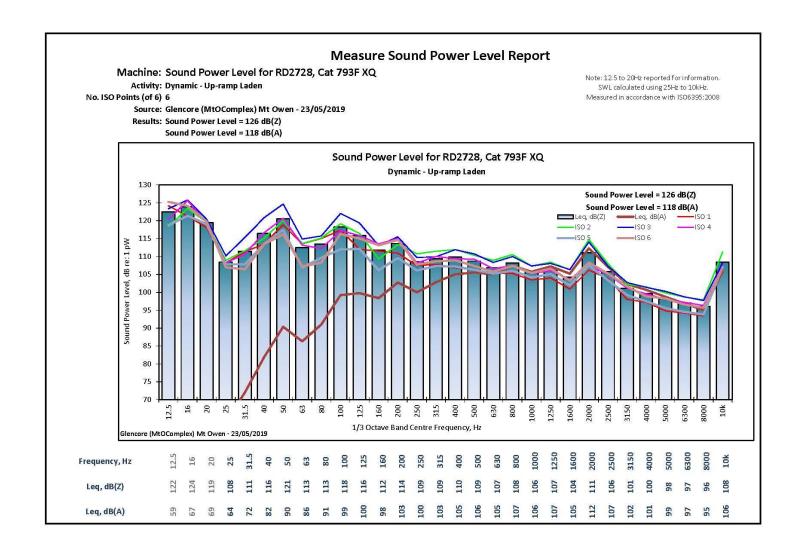


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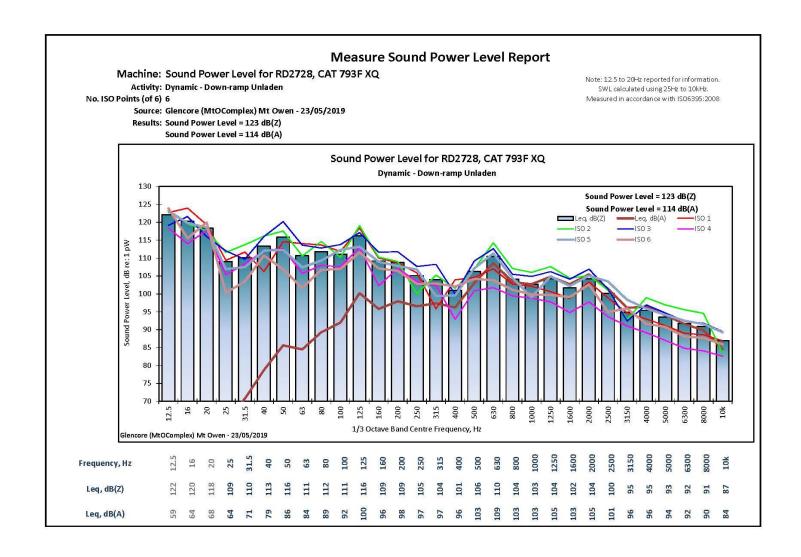




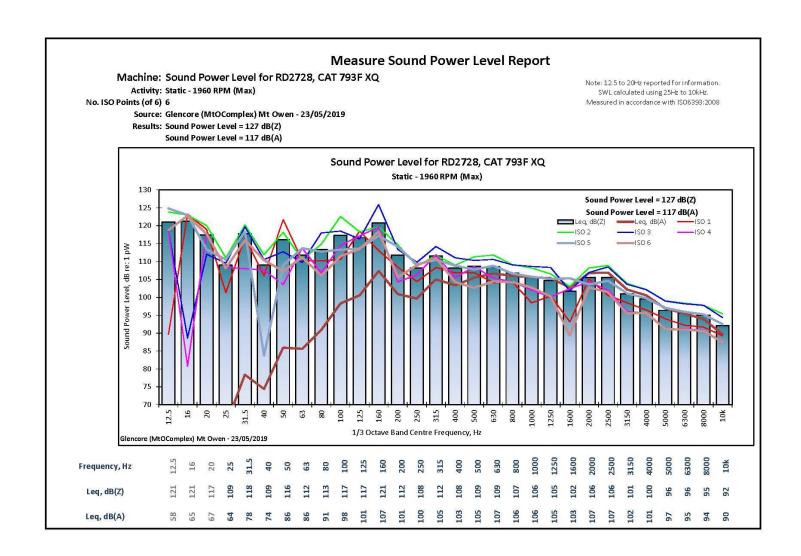
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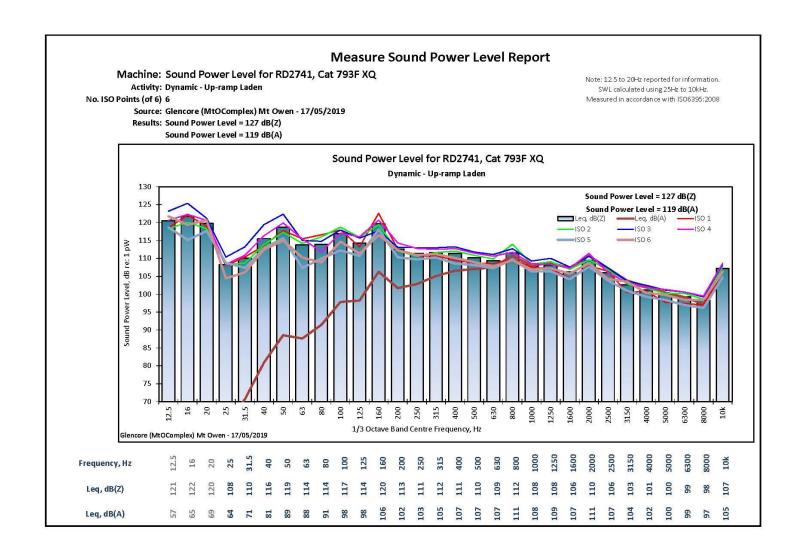
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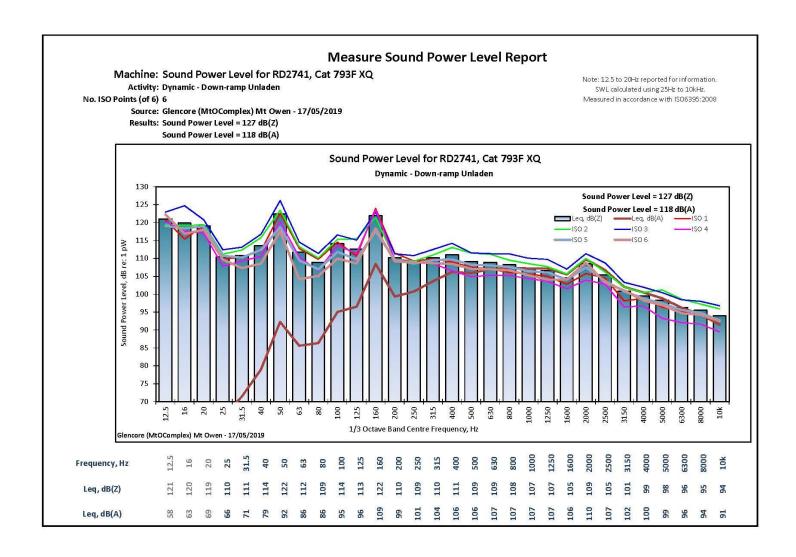
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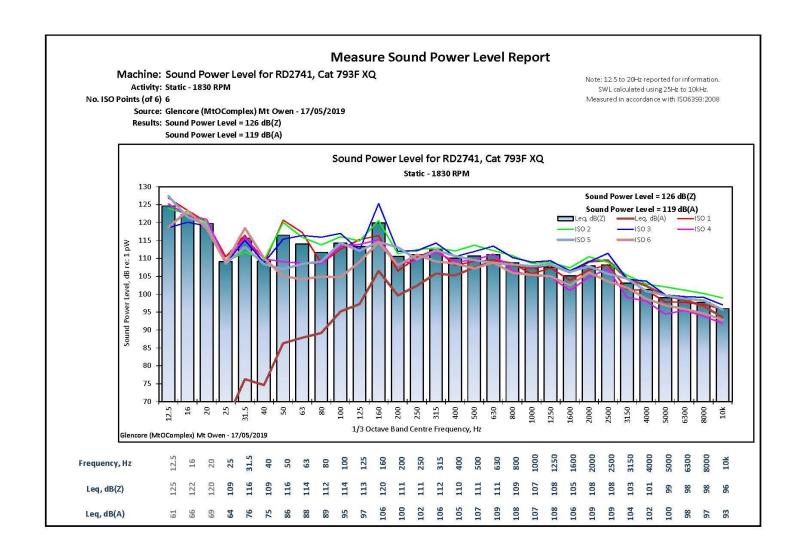
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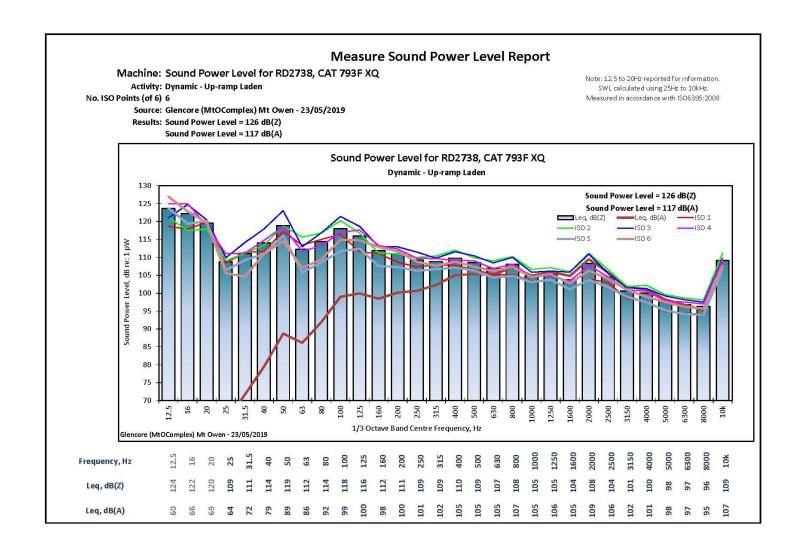
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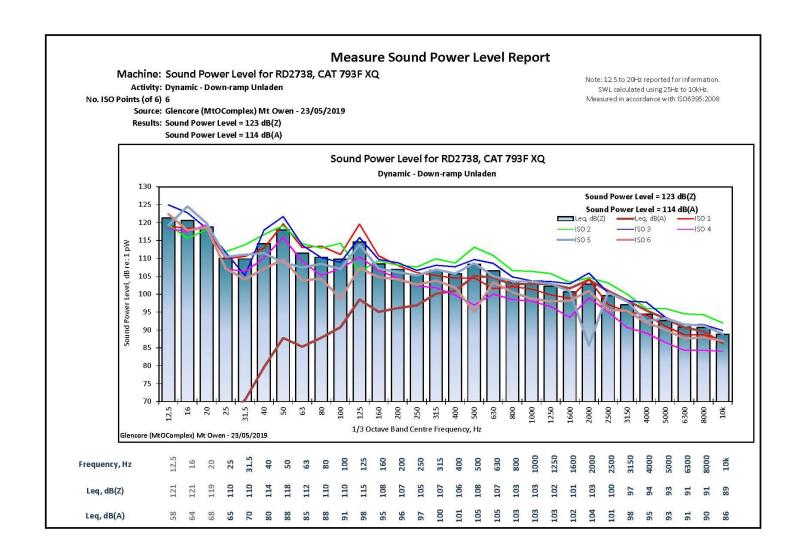
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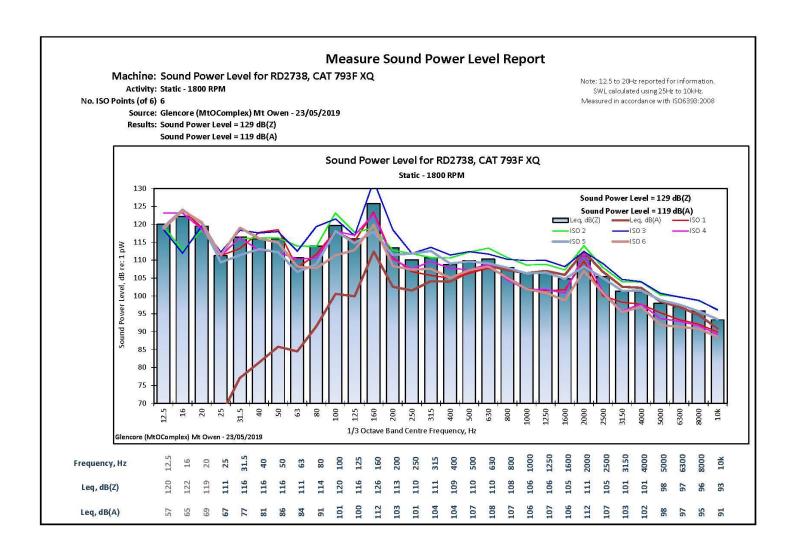
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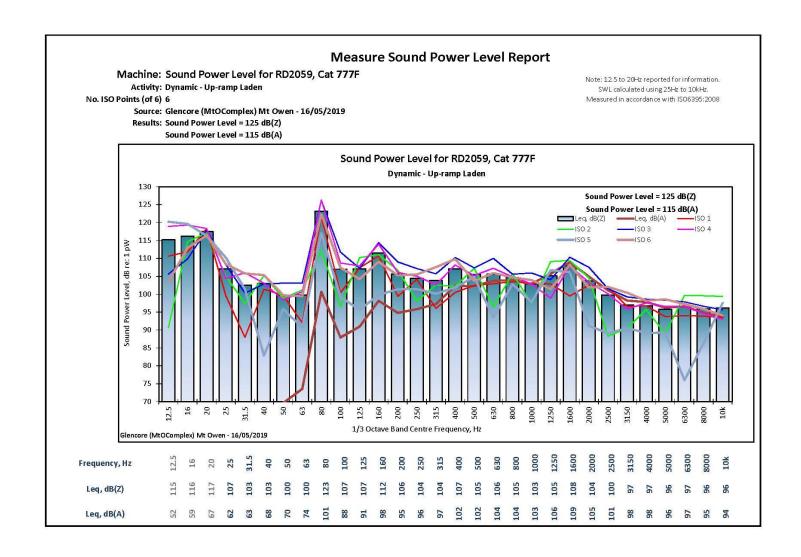
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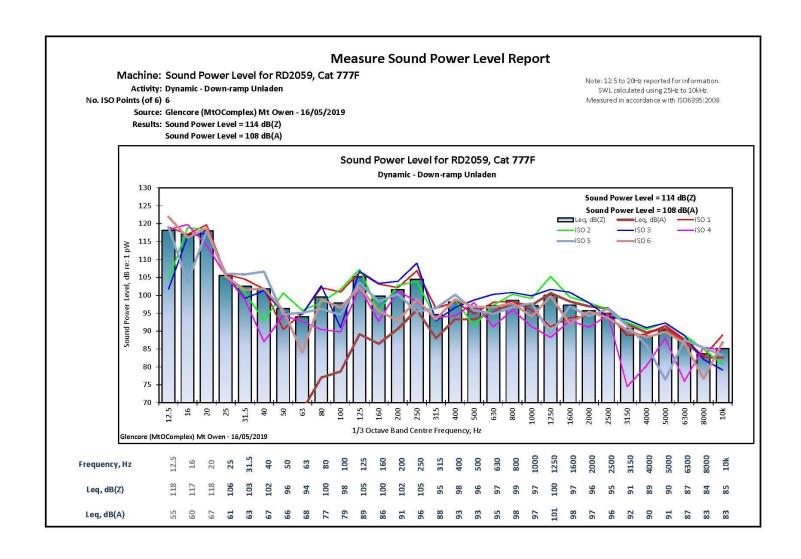
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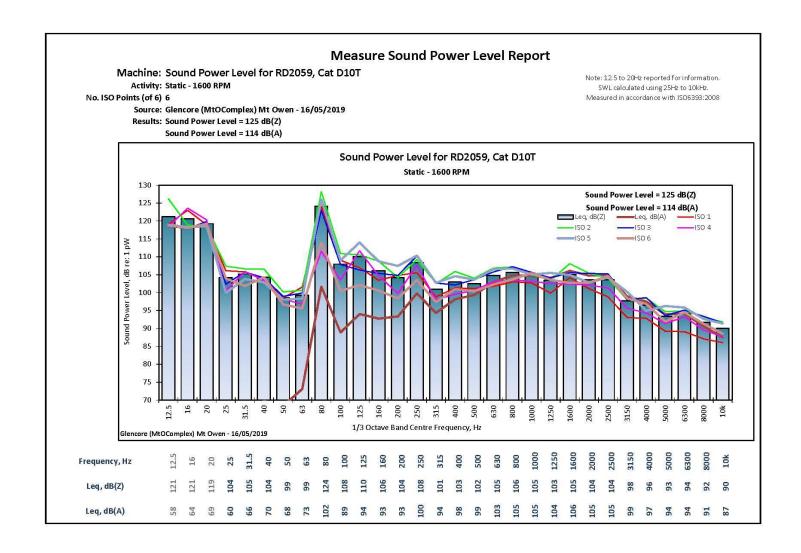
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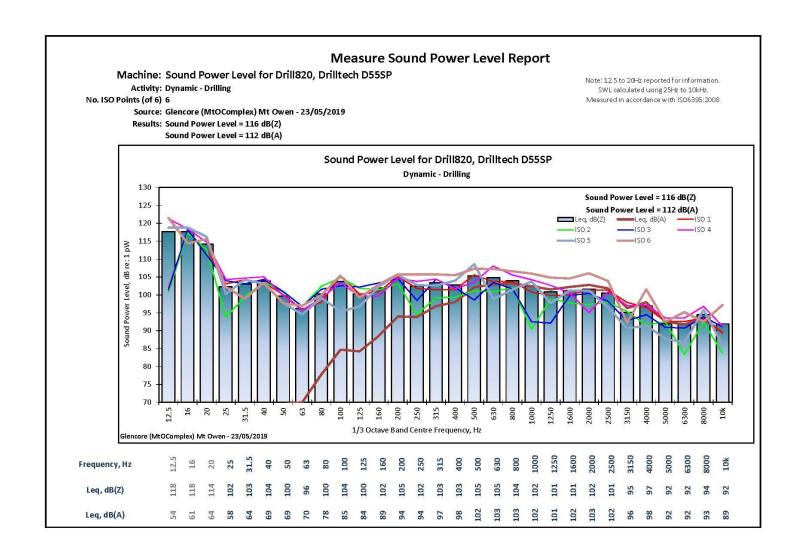
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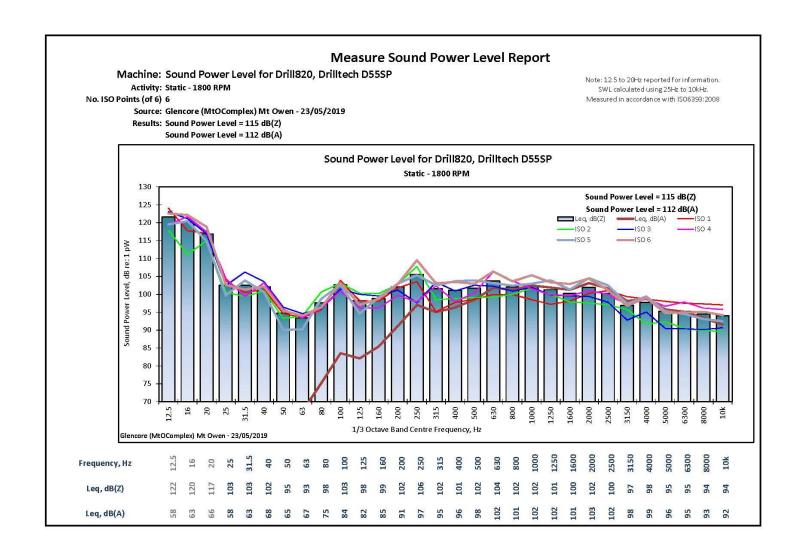
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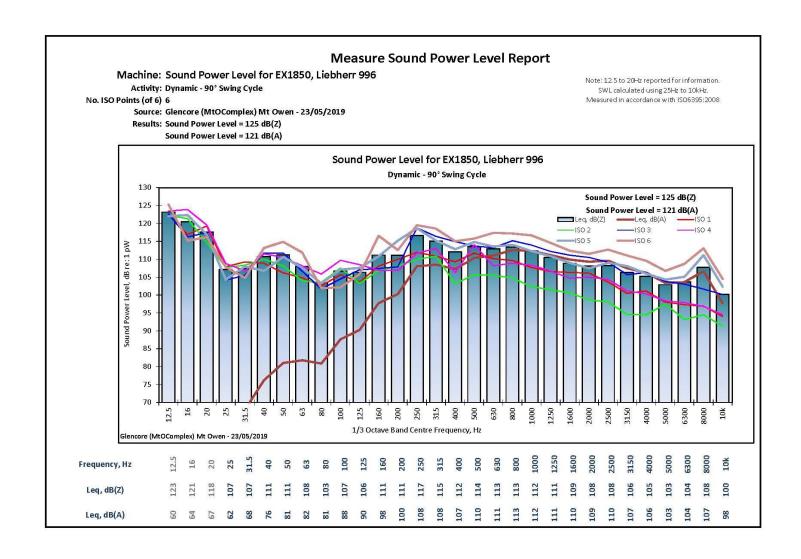
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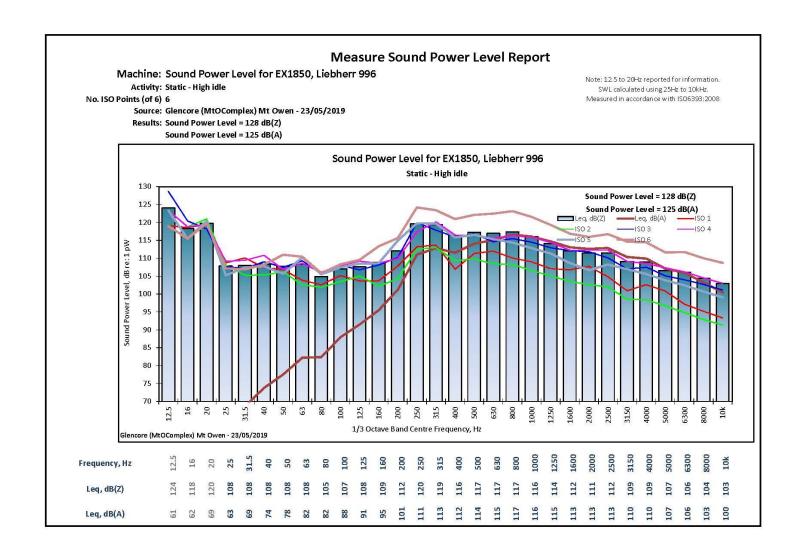
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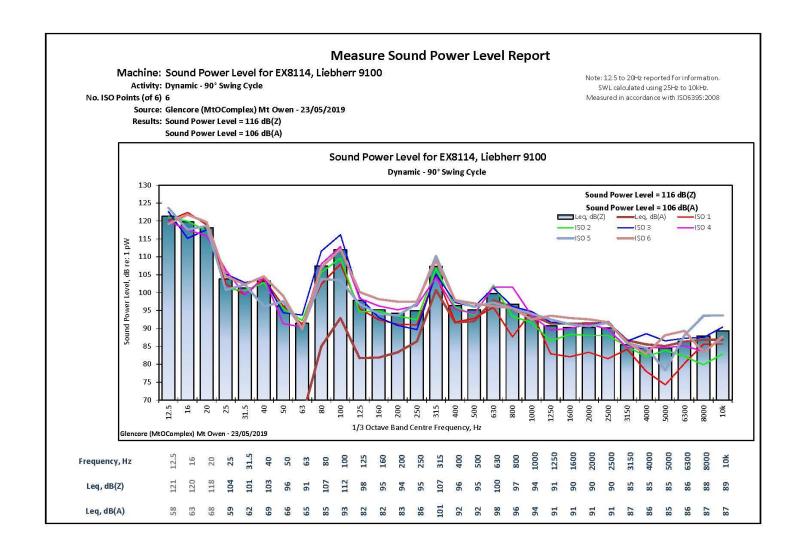
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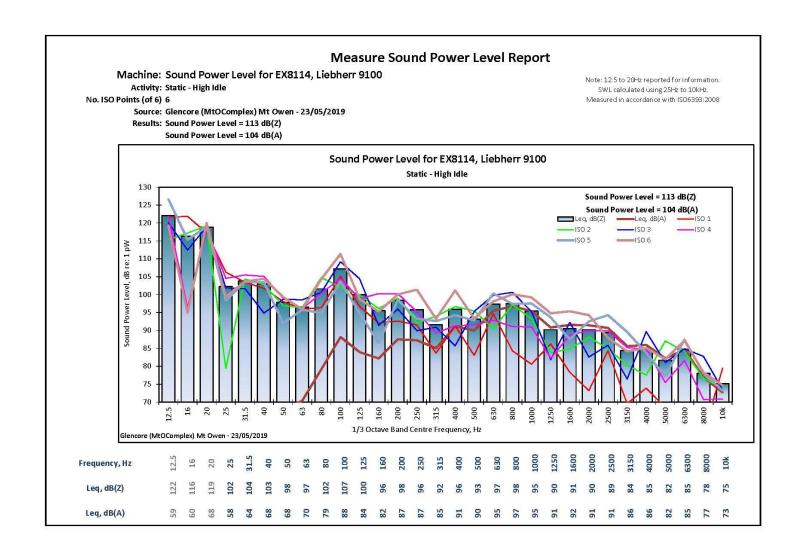
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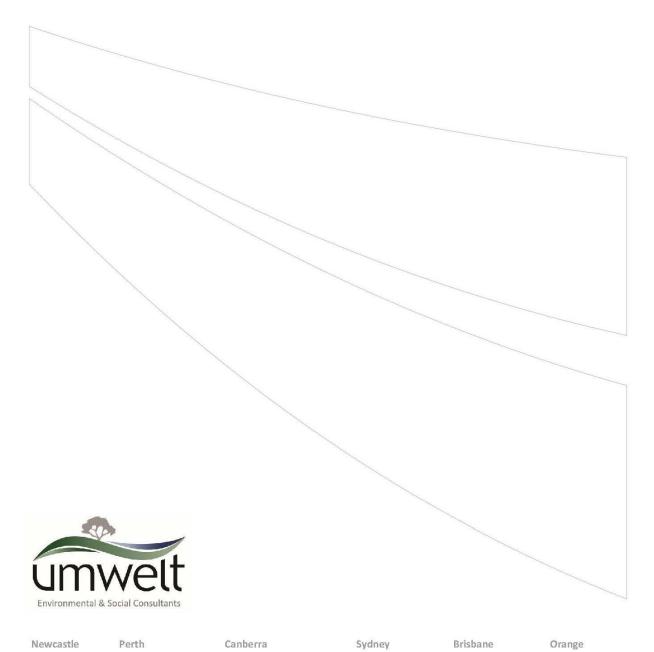
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Umwelt (Australia) Pty Limited EX8114_Dynamic.xlsb



Umwelt (Australia) Pty Limited EX8114_Static.xlsb



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Appendix E: Blasting

Table 16: MGO Overpressure Blasting Compliance Summary

Blast Monitor	Location	Maximum Airblast (dB(L))	Average Airblast (dB(L))
Mt Owen			
MOC1	Glennies Ck Road	113.6	99.2
MOC2	Glennies Ck Road	114.1	97.6
MOC3	Glennie St Camberwell Village	115.0	92.4
MOC4	Middle Falbrook Area	111.8	94.7
MOC5	Goorangoola Area	114.8	97.9
Ravensworth Homestead	Ravensworth Homestead	115.5	95.7
Chain of Ponds Inn	Chain of Ponds Inn	110.5	93.1
Former Hebden Public School	Former Hebden Public School	112.9	94.4
Church	Camberwell Church	111.4	94.4
Integra Surface	Integra Surface	114.7	99.7
Integra Underground Workings	Integra Underground Workings	120.8	104.1
Glendell			
Ravensworth Homestead	Ravensworth Homestead	111.6	96.5
MOC3	Glennie St Camberwell Village	110.7	95.2
Church	Camberwell Church	117.7	89.0
Powerlines	Powerlines	115.1	105.6
ARTC 1	Main Northern Railway	114	104.8
ARTC 2	Main Northern Railway	120.7	106.3
ARTC 3	Main Northern Railway	111.3	102.7
ARTC 4	Main Northern Railway	114.5	100.0

MOC2	Glennies Creek Road	109.5	94.7						
Integra Surface	Integra Surface	110.4	100.6						
Ravensworth East	Ravensworth East								
MOC1	Glennies Ck Road	114.7	93.3						
MOC2	Glennies Ck Road	111.6	95.8						
MOC3	Glennie St Camberwell Village	107.7	88.0						
MOC4	Middle Falbrook Area	106.0	86.7						
MOC5	Goorangoola Area	108.3	92.4						
Ravensworth Homestead	Ravensworth Homestead	113.7	99.2						
Chain of Ponds Inn	Chain of Ponds Inn	114.4	94.1						
Former Hebden Public School	Former Hebden Public School	111.9	102.1						
Church	Camberwell Church	111.3	91.6						

Table 17: MGO Vibration Blasting Compliance Summary

Blast Monitor	Location	Maximum Vibration (mm/s)	Average Vibration (mm/s)
Mt Owen			
MOC1	Glennies Ck Road	1.76	0.3
MOC2	Glennies Ck Road	0.76	0.3
MOC3	Glennie St Camberwell Village	0.33	0.1
MOC4	Middle Falbrook Area	0.77	0.3
MOC5	Goorangoola Area	0.59	0.2
Ravensworth Homestead	Ravensworth Homestead	0.57	0.2
Chain of Ponds Inn	Chain of Ponds Inn	0.46	0.1
Former Hebden Public School	Former Hebden Public School	0.61	0.2
Church	Camberwell Church	0.22	0.1

Integra Surface	Integra Surface	1.05	0.3					
Integra Underground Workings	Integra Underground Workings	9.97	2.1					
Glendell								
Ravensworth Homestead	Ravensworth Homestead	1.68	0.38					
MOC3	Glennie St Camberwell Village	0.82	0.38					
Church	Camberwell Church	0.61	2.21					
MOC2	Glennies Creek Road	1.09	0.23					
Powerlines	Powerlines	13.61	2.43					
ARTC 1	Main Northern Railway	9.62	1.84					
ARTC 2	Main Northern Railway	13.8	0.77					
ARTC 3	Main Northern Railway	1.47	0.5					
ARTC 4	Main Northern Railway	2.43	0.59					
Integra Surface	Integra Surface	1.46	0.36					
Ravensworth East								
MOC1	Glennies Ck Road	0.1	0.05					
MOC2	Glennies Ck Road	0.24	0.11					
MOC3	Glennie St Camberwell Village	1.08	0.07					
MOC4	Middle Falbrook Area	0.13	0.05					
MOC5	Goorangoola Area	0.14	0.05					
Ravensworth Homestead	Ravensworth Homestead	1.09	0.53					
Chain of Ponds Inn	Chain of Ponds Inn	0.27	1.15					
Former Hebden Public School	Former Hebden Public School	1.12	0.56					
Church	Camberwell Church	0.06	0.03					
Integra Surface	Integra Surface	0.26	0.29					
Integra Underground Workings	Integra Underground Workings	0.29	0.14					

Table 18: Mt Owen Blast Monitoring Results – MOC 1 and MOC 2

		M	OC1	MOC2		
Date Fired	Time Fired	Peak Vibration (mm/s)	Peak Overpressure (dBL)	Peak Vibration (mm/s)	Peak Overpressure (dBL)	
2/01/2019	12:39	0.32	91.7	0.38	92.3	
4/01/2019	10:58	0.17	99	0.22	95.4	
7/01/2019	14:22	0.2	98.2	0.35	102.8	
10/01/2019	9:41	0.17	96.3	0.17	92.3	
11/01/2019	12:03	0.25	99	0.25	96.8	
16/01/2019	14:09	0.37	100	0.49	97.5	
18/01/2019	10:43	0.18	96.8	0.17	94.4	
23/01/2019	13:20	0.19	97.8	0.38	94.5	
25/01/2019	12:18	0.23	98	0.49	94.1	
30/01/2019	16:00	0.15	91.8	0.14	92.1	
01/02/2019	12:25	0.27	96.3	0.42	96.2	
01/02/2019	12:27	0.18	107.2	0.3	93.7	
05/02/2019	12:32	0.12	101.5	0.27	105	
07/02/2019	13:06	0.17	98.3	0.13	91.3	
07/02/2019	13:10	0.04	102.4	0.1	89.5	
13/02/2019	12:44	0.27	96.9	0.29	95.4	
15/02/2019	12:11	0.34	99.2	0.31	97.5	
20/02/2019	15:57	0.36	107.1	0.39	109.2	
22/02/2019	11:58	0.18	107.1	0.15	106.7	
28/02/2019	13:13	0.26	104.5	0.4	102.1	
5/03/2019	12:34	1.76	97	0.24	105.8	
7/03/2019	12:37	0.24	97.9	0.23	97	
12/03/2019	13:18	0.38	101.4	0.23	96	
15/03/2019	12:03	0.51	99.1	0.36	94.6	
21/03/2019	16:17	0.34	107.9	0.31	107.5	
27/03/2019	12:46	0.26	112.8	0.25	97.5	
29/03/2019	12:19	0.17	100.4	0.34	98.2	
4/04/2019	13:15	0.2	103	0.15	103	
5/04/2019	12:20	0.17	94.7	0.11	88.2	
11/04/2019	13:01	0.47	99.8	0.36	99.4	
17/04/2019	12:11	0.22	96.4	0.3	92.9	
18/04/2019	13:05	0.11	90.9	0.14	91.8	
23/04/2019	16:02	0.3	112.9	0.28	92.5	
24/04/2019	14:05	0.17	88.7	0.25	88.5	
26/04/2019	12:44	0.21	99.5	0.25	106.8	
1/05/2019	12:14	0.37	96.6	0.23	93.3	
3/05/2019	10:44	0.26	101.7	0.44	100.1	
8/05/2019	11:53	0.53	111	0.75	103.9	
10/05/2019	9:58	0.46	103.3	0.32	104.1	
15/05/2019	12:06	0.24	92.7	0.26	88.9	
16/05/2019	13:03	0.29	92.9	0.17	99.1	

	MOC1		OC1	MOC2		
Date Fired	Time Fired	Peak Vibration (mm/s)	Peak Overpressure (dBL)	Peak Vibration (mm/s)	Peak Overpressure (dBL)	
04/05/0040	40.47					
21/05/2019	13:17	0.28	97.9	0.35	94.3	
24/05/2019 30/05/2019	12:15 16:17	0.23	93.1	0.33	97.5 98.1	
31/05/2019	7:09	0.14	108.1	0.18	109.7	
4/06/2019	12:52	0.14	104.8	0.22	101.6	
7/06/2019	12:17	0.54	103	0.44	99.9	
11/06/2019	16:02	0.2	95.6	0.23	96.9	
12/06/2019	9:30	0.28	104.8	0.21	100.2	
14/06/2019	12:22	0.38	97.1	0.31	91.2	
19/06/2019	13:18	0.45	92.5	0.27	91.8	
21/06/2019	12:18	0.22	98.1	0.25	98.3	
28/06/2019	15:23	0.38	95.3	0.35	92.9	
3/07/2019	12:47	0.24	102.6	0.19	95.5	
5/07/2019	11:16	0.39	95.1	0.34	90.1	
5/07/2019	11:18	0.11	110.7	0.12	83.5	
11/07/2019	13:18	0.31	112.5	0.25	107.5	
13/07/2019	8:57:53	0.16	104.5	0.22	97.4	
19/07/2019	12:30	0.72	100.4	0.76	98.7	
19/07/2019	12:58	0.27	98.9	0.26	101.6	
24/07/2019	12:52	0.21	105.1	0.25	99.4	
25/07/2019	13:24	0.17	92.7	0.16	89.1	
30/07/2019	12:17	0.17	99.8	0.24	96.6	
1/08/2019	12:36	0.25	91.1	0.36	87.3	
6/08/2019	9:27	0.21	102.9	0.2	98.6	
12/08/2019	12:24	0.16	103.4	0.25	105.3	
13/08/2019	13:13	0.21	100.4	0.23	102.5	
15/08/2019	12:48	0.26	97.6	0.38	92.9	
20/08/2019	12:50	0.24	102	0.33	110	
22/08/2019	14:37	0.79	96.4	0.63	100.9	
27/08/2019	13:18	0.16	89.6	0.23	91.7	
29/08/2019	13:10	0.61	101.9	0.15	107.5	
30/08/2019	10:45	0.14	104	0.18	108.7	
3/09/2019	12:02	0.34	95.1	0.24	92.9	
5/09/2019	12:04	0.29	89.2	0.37	84.2	
9/09/2019	12:21	0.26	113.6	0.39	112.2	
11/09/2019	12:12	0.24	91 94.7	0.23	96.2	
13/09/2019 13/09/2019	12:01 12:02	0.36	93.9	0.43	86 96.4	
19/09/2019 24/09/2019	13:06 13:00	0.19	97.1 103.3	0.35	98.6 100.2	
26/09/2019	13:26	0.37	93.7	0.37	94.4	
1/10/2019	12:17	0.16	96.5	0.16	96.6	
1/10/2019	12:17	0.20	95.8	0.09	94.8	
1/10/2019	12:17	0.07	90.0	0.09	94.0	

			MOC1)C2
Date Fired	Time Fired	Peak Vibration	Peak Overpressure	Peak Vibration	Peak Overpressure
		(mm/s)	(dBL)	(mm/s)	(dBL)
3/10/2019	12:03	0.19	94.4	0.24	89.6
9/10/2019	12:18	0.56	97.6	0.26	96.5
11/10/2019	12:20	0.34	95.2	0.3	101.1
21/10/2019	13:23	0.49	92.5	0.37	96.9
29/10/2019	12:16	0.34	91.8	0.24	91.6
31/10/2019	12:17	0.28	87.6	0.32	97.3
5/11/2019	12:23	0.34	100.4	0.33	98.8
11/11/2019	12:22	0.32	95.2	0.32	108
13/11/2019	12:22	0.34	99.7	0.42	90.9
18/11/2019	12:21	0.54	99.6	0.51	101.2
20/11/2019	11:14	0.25	99.9	0.45	103.6
21/11/2019	13:29	0.28	100.5	0.39	90.7
29/11/2019	11:54	0.15	92.5	0.32	88.8
29/11/2019	11:57	0.16	98.2	0.25	96
4/12/2019	11:22	0.23	106.9	0.33	109.7
5/12/2019	12:32	0.19	102.4	0.34	101.9
5/12/2019	12:34	0.05	105.3	0.18	114.1
12/12/2019	12:13	0.39	103.7	0.37	102
18/12/2019	13:06	0.54	97.9	0.56	102.6

Table 19: Mt Owen Blast Monitoring Results – MOC 3 and MOC 4

		M	OC3	MOC4		
Date Fired	Time Fired	Peak Vibration (mm/s)	Peak Overpressure (dBL)	Peak Vibration (mm/s)	Peak Overpressur (dBL)	
2/01/2019	12:39	0.06	88.5	0.44	92.1	
4/01/2019	10:58	0.07	91.3	0.17	96.4	
7/01/2019	14:22	0.05	85	0.16	84.5	
10/01/2019	9:41	0.08	91	0.28	89.1	
11/01/2019	12:03	0.06	86.4	0.32	92.9	
16/01/2019	14:09	0.33	95.3	0.37	95	
18/01/2019	10:43	0.06	95.6	0.24	91	
23/01/2019	13:20	0.1	89.7	0.17	97.6	
25/01/2019	12:18	0.07	96.4	0.24	96.3	
30/01/2019	16:00	0.04	87.9	0.17	95.8	
01/02/2019	12:25	0.08	87.7	0.27	89.7	
01/02/2019	12:27	0.08	92.4	0.11	87.4	
05/02/2019	12:32	0.06	96.4	0.12	95	
07/02/2019	13:06	0.04	89.2	0.16	95.3	
07/02/2019	13:10	0.02	78.1	0.06	89.8	
13/02/2019	12:44	0.08	95.1	0.37	94.4	
15/02/2019	12:11	0.15	93.9	0.34	93.3	
20/02/2019	15:57	0.13	102.6	0.4	95.1	
22/02/2019	11:58	0.05	95.5	0.27	98.3	
28/02/2019	13:13	0.09	96.3	0.29	101.2	
5/03/2019	12:34	0.07	89.4	0.14	96.8	
7/03/2019	12:37	0.07	90.5	0.33	87.7	
12/03/2019	13:18	0.08	96	0.31	100.1	
15/03/2019	12:03	0.15	91.5	0.77	92.2	
21/03/2019	16:17	0.1	91.2	0.33	88.8	
27/03/2019	12:46	0.07	87.9	0.36	91.1	
29/03/2019	12:19	0.13	94.6	0.18	96.3	
4/04/2019	13:15	0.05	86	0.27	84.7	
5/04/2019	12:20	0.04	86.6	0.16	100.2	
11/04/2019	13:01	0.08	96.1	0.3	92.2	
17/04/2019	12:11	0.1	90.5	0.23	90.9	
18/04/2019	13:05	0.05	87.5	0.12	89.9	
23/04/2019	16:02	0.09	96.2	0.31	85.8	
24/04/2019	14:05	0.08	82.5	0.15	87.9	
26/04/2019	12:44	0.08	95.3	0.32	101.6	
1/05/2019	12:14	0.08	93.5	0.3	102	
3/05/2019	10:44	0.11	96.1	0.27	105.2	
8/05/2019	11:53	0.19	96.4	0.51	96.2	
10/05/2019	9:58	0.14	104.3	0.48	104.1	
15/05/2019	12:06	0.07	89.9	0.39	89.1	

			OC3	MOC4	
Date Fired	Time Fired	Peak Vibration (mm/s)	Peak Overpressure (dBL)	Peak Vibration (mm/s)	Peak Overpressure (dBL)
16/05/2019	13:03	0.1	88.6	0.27	89.4
21/05/2019	13:17	0.09	91.5	0.3	97.4
24/05/2019	12:15	0.06	93	0.35	90.3
30/05/2019	16:17	0.1	90.3	0.26	97.6
31/05/2019	7:09	0.06	100	0.13	108.2
4/06/2019	12:52	0.05	89.9	0.19	90.4
7/06/2019	12:17	0.12	100.2	0.65	99.5
11/06/2019	16:02	0.08	91.1	0.24	99.7
12/06/2019	9:30	0.09	97.7	0.35	103.7
14/06/2019	12:22	0.1	89.6	0.47	93.2
19/06/2019	13:18	0.09	86.7	0.54	88.4
21/06/2019	12:18	0.06	93.5	0.25	99.8
28/06/2019	15:23	0.11	91	0.26	95.8
3/07/2019	12:47	0.07	87.8	0.24	94.3
5/07/2019	11:16	0.1	94.4	0.7	88.8
5/07/2019	11:18	0.04	88.7	0.09	84.5
11/07/2019	13:18	0.07	115	0.44	104.4
13/07/2019	8:57	0.07	93.2	0.44	104.6
19/07/2019	12:30	0.29	90.9	0.62	95.3
19/07/2019	12:58	0.07	90.5	0.37	94.8
24/07/2019	12:52	0.07	89.8	0.27	105.9
25/07/2019	13:24	0.05	86.7	0.27	86.8
30/07/2019	12:17 12:36	0.07	95.7 88.1	0.22	96.9
1/08/2019 6/08/2019	9:27	0.12	89.8	0.27	87.4 111.8
12/08/2019			92.8		98.2
13/08/2019	12:24 13:13	0.07	89.2	0.18	98.2
15/08/2019	12:48	0.08	100.2	0.33	101.8
20/08/2019	12:50	0.12	100.2	0.16	103
22/08/2019	14:37	0.31	109.6	0.66	95
27/08/2019	13:18	0.09	84.5	0.12	88.3
29/08/2019	13:10	0.04	96.7	0.24	97.4
30/08/2019	10:45	0.07	88.5	0.14	96.7
3/09/2019	12:02	0.09	90.6	0.57	89.1
5/09/2019	12:04	0.09	83.7	0.33	83.8
9/09/2019	12:21	0.15	105.9	0.35	97.8
11/09/2019	12:12	0.07	93.7	0.26	87.9
13/09/2019	12:01	0.12	91.3	0.32	90.6
13/09/2019	12:02	0.1	86.4	0.33	98.7
19/09/2019	13:06	0.08	94.7	0.34	93
24/09/2019	13:00	0.13	91	0.26	101.4
26/09/2019	13:26	0.06	84.5	0.24	90.9
1/10/2019	12:17	0.08	91.4	0.24	94.7

		MC	DC3	MC)C4
Date Fired	Time Fired	Peak Vibration (mm/s)	Peak Overpressure (dBL)	Peak Vibration (mm/s)	Peak Overpressure (dBL)
1/10/2019	12:17	. ,	` ′		
	.=	0.05	91.4	0.09	90.3
3/10/2019	12:03	0.06	84.3	0.29	93.7
9/10/2019	12:18	0.11	90.1	0.32	90.8
11/10/2019	12:20	0.08	87.7	0.57	94.3
21/10/2019	13:23	0.1	88	0.6	97.3
29/10/2019	12:16	0.07	89.6	0.43	97.3
31/10/2019	12:17	0.08	86.6	0.43	89.8
5/11/2019	12:23	0.13	86.6	0.41	95.1
11/11/2019	12:22	0.06	87.8	0.31	91.9
13/11/2019	12:22	0.11	100.7	0.23	103.4
18/11/2019	12:21	0.1	91.6	0.64	94.9
20/11/2019	11:14	0.1	96.5	0.2	95.2
21/11/2019	13:29	0.14	87.1	0.51	100.8
29/11/2019	11:54	0.06	90.4	0.21	88.7
29/11/2019	11:57	0.08	96.8	0.31	94.2
4/12/2019	11:22	0.07	90.8	0.34	102.6
5/12/2019	12:32	0.08	105.9	0.29	92.7
5/12/2019	12:34	0.07	113	0.06	94.9
12/12/2019	12:13	0.13	97.3	0.37	95.8
18/12/2019	13:06	0.14	92.9	0.54	91

Table 20 Mt Owen Blast Monitoring Results – MOC 5 and Homestead

		MOC5		Homes	Homestead	
Date Fired	Time Fired	Peak Overpressure (dBL)	Peak Vibration (mm/s)	Peak Overpressure (dBL)	Peak Vibration (mm/s)	
2/01/2019	12:39	93.1	0.21	90.4	0.14	
4/01/2019	10:58	100.9	0.12	84.1	0.2	
7/01/2019	14:22	95.8	0.23	96.6	0.18	
10/01/2019	9:41	99.6	0.15	94.3	0.08	
11/01/2019	12:03	95.8	0.14	88.7	0.1	
16/01/2019	14:09	103.9	0.13	96.6	0.27	
18/01/2019	10:43	97.7	0.15	93.8	0.2	
23/01/2019	13:20	94.4	0.11	86.8	0.24	
25/01/2019	12:18	100.6	0.17	90	0.29	
30/01/2019	16:00	94.8	0.09	88.2	0.08	
01/02/2019	12:25	100.6	0.2	93.9	0.25	
01/02/2019	12:27	92.5	0.07	92.1	0.14	
05/02/2019	12:32	97.8	0.06	94	0.15	
07/02/2019	13:06	97.1	0.1	88.3	0.07	
07/02/2019	13:10	95	0.01	83.2	0.04	
13/02/2019	12:44	96	0.26	96.2	0.26	
15/02/2019	12:11	109.6	0.15	103.7	0.23	
20/02/2019	15:57	92.7	0.29	109.2	0.21	
22/02/2019	11:58	106	0.12	109.4	0.09	
28/02/2019	13:13	112.9	0.26	94.4	0.32	
5/03/2019	12:34	99.5	0.12	94.5	0.18	
7/03/2019	12:37	95.7	0.24	87.6	0.12	
12/03/2019	13:18	100.8	0.14	98.5	0.14	
15/03/2019	12:03	95.7	0.33	93.9	0.26	
21/03/2019	16:17	105.9	0.21	107	0.14	
27/03/2019	12:46	107.4	0.28	96.3	0.16	
29/03/2019	12:19	99	0.13	92.3	0.17	
4/04/2019	13:15	89.5	0.15	90.8	0.11	
5/04/2019	12:20	95.4	0.09	88.2	0.06	
11/04/2019	13:01	100.1	0.28	100	0.17	
17/04/2019	12:11	99.4	0.11	93.2	0.16	
18/04/2019	13:05	96.2	0.04	87	0.07	
23/04/2019	16:02	100.1	0.32	98.6	0.2	
24/04/2019	14:05	89.6	0.07	83.2	0.15	
26/04/2019	12:44	97.4	0.14	102.2	0.21	
1/05/2019	12:14	95.8	0.17	85.5	0.08	
3/05/2019	10:44	99.7	0.17	95.9	0.29	
8/05/2019	11:53	114.8	0.53	108.1	0.25	
10/05/2019	9:58	94.7	0.22	92.5	0.08	
15/05/2019	12:06	96.2	0.17	91.1	0.2	
16/05/2019	13:03	94.6	0.21	89.6	0.1	

21/05/2019	13:17	94.6	0.25	100.1	0.22
24/05/2019	12:15	97.6	0.24	96	0.15
30/05/2019	16:17	96.1	0.16	93.9	0.2
31/05/2019	7:09	107.5	0.06	88	0.08
4/06/2019	12:52	101.4	0.08	113.5	0.11
7/06/2019	12:17	94.9	0.31	91.6	0.23
11/06/2019	16:02	98	0.11	90	0.17
12/06/2019	9:30	93.9	0.12	93	0.09
14/06/2019	12:22	100.5	0.2	88.5	0.17
19/06/2019	13:18	90.5	0.33	86.9	0.18
21/06/2019	12:18	99.6	0.13	92.3	0.08
28/06/2019	15:23	97.1	0.17	92.3	0.31
3/07/2019	12:47	100.3	0.15	90.8	0.07
5/07/2019	11:16	92.8	0.27	95.3	0.35
5/07/2019	11:18	96	0.03	88.9	0.09
11/07/2019	13:18	102.9	0.24	108.8	0.12
13/07/2019	8:57	110.1	0.14	109.7	0.12
19/07/2019	12:30	97.7	0.59	94.4	0.57
19/07/2019	12:58	94.2	0.14	96.3	0.1
24/07/2019	12:52	98.4	0.14	97.1	0.2
25/07/2019	13:24	91.2	0.12	87.4	0.1
30/07/2019	12:17	105.3	0.12	97.6	0.24
1/08/2019	12:17	92.5	0.13	89	0.24
6/08/2019	9:27	96.2	0.13	88.9	0.06
	12:24	100.3	0.09	105.1	0.06
12/08/2019	13:13	97.3	0.09	103.3	0.17
13/08/2019		101	0.17		0.13
15/08/2019	12:48	104.5		105.1	0.14
20/08/2019	12:50		0.09	102.1	
22/08/2019	14:37	99.6	0.38	107.9	0.38
27/08/2019	13:18	89.3	0.09	90.9	0.3
29/08/2019	13:10	104.4	0.08	101	0.04
30/08/2019	10:45	101.8	0.05	97	0.11
3/09/2019	12:02	89.9	0.24	93.9	0.21
5/09/2019	12:04	92.5	0.24	89.3	0.23
9/09/2019	12:21	97.3	0.19	111.3	0.45
11/09/2019	12:12	88.5	0.13	93.2	0.18
13/09/2019	12:01	94.9	0.23	97.3	0.19
13/09/2019	12:02	94.9	0.23	90.8	0.46
19/09/2019	13:06	98.2	0.18	99.5	0.25
24/09/2019	13:00	96.3	0.12	92.1	0.18
26/09/2019	13:26	93.2	0.12	90	0.18
1/10/2019	12:17	100.4	0.09	98.6	0.08
1/10/2019	12:17	100.4	0.02	96.9	0.05
3/10/2019	12:03	95.8	0.17	85.7	0.11
9/10/2019	12:18	96.8	0.11	115.5	0.11
11/10/2019	12:20	102.8	0.16	105	0.13
21/10/2019	13:23	95.1	0.34	103.5	0.16

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00/40/0040	40.40	05.4	0.04	00.5	0.44
29/10/2019	12:16	95.1	0.31	98.5	0.11
31/10/2019	12:17	96.1	0.23	91.2	0.19
5/11/2019	12:23	98.9	0.1	88.5	0.15
11/11/2019	12:22	96.6	0.21	99.8	0.15
13/11/2019	12:22	97.3	0.2	105.6	0.28
18/11/2019	12:21	95.9	0.24	92	0.35
20/11/2019	11:14	100.9	0.13	97.4	0.24
21/11/2019	13:29	97.3	0.1	98.4	0.16
29/11/2019	11:57	94.3	0.15	89.2	0.2
4/12/2019	11:22	94.8	0.16	93.8	0.21
5/12/2019	12:32	104.6	0.23	107.1	0.17
5/12/2019	12:34	99.2	0.16	110	0.17
12/12/2019	12:13	96.8	0.06	99.8	0.05
18/12/2019	13:06	96.6	0.21	97.8	0.21

Table 21 Mt Owen Blast Monitoring Results – Chain of Ponds, Hebden School and Church

		Chain	of Ponds	Hebde	n School	Church		
Date Fired	Time Fired	Peak Vibration	Peak Overpressure	Peak Vibration	Peak Overpressure	Peak Vibration	Peak Overpressure	
		(mm/s)	(dBL)	(mm/s)	(dBL)	(mm/s)	(dBL)	
2/01/2019	12:39	0.09	88.4	0.18	89.5	0.08	93.8	
4/01/2019	10:58	0.08	91.2	0.17	83.7	0.04	91.8	
7/01/2019	14:22	0.09	90.6	0.12	104	0.04	95.2	
10/01/2019	9:41	0.07	96.3	0.1	101	0.06	91.1	
11/01/2019	12:03	0.08	88.8	0.1	93.3	0.06	87.3	
16/01/2019	14:09	0.14	89.9	0.26	97.4	0.14	96.6	
18/01/2019	10:43	0.11	91.5	0.18	98.9	0.06	95	
23/01/2019	13:20	0.11	94.4	0.14	92	0.06	89.1	
25/01/2019	12:18	0.13	89.9	0.21	93.4	0.05	94.1	
30/01/2019	16:00	0.08	89.9	0.05	102.3	0.03	84.6	
01/02/2019	12:25	0.19	90.9	0.17	95.6	0.06	107.4	
01/02/2019	12:27	0.08	91.8	0.13	101.1	0.04	96.2	
05/02/2019	12:32	0.1	92.6	0.11	97.3	0.04	104.1	
07/02/2019	13:06	0.06	87.5	0.05	103.8	0.04	88.9	
07/02/2019	13:10	0.05	87.1	0.05	97.5	0.01	85.7	
13/02/2019	12:44	0.09	94	0.15	101.3	0.09	94.9	
15/02/2019	12:11	0.12	95.2	0.16	106.9	0.08	94	
20/02/2019	15:57	0.15	107.5	0.16	96.8	0.09	108.5	
22/02/2019	11:58	0.06	91.2	0.04	112.9	0.05	108.2	
28/02/2019	13:13	0.17	93.3	0.28	78.1	0.06	95.3	
5/03/2019	12:34	0.11	96.3	0.13	78.1	0.06	99.4	
7/03/2019	12:37	0.09	98	0.11	94.8	0.06	98.6	
12/03/2019	13:18	0.12	103.4	0.11	103.2	0.08	99.3	
15/03/2019	12:03	0.12	98.7	0.12	95.6	0.11	92.3	
21/03/2019	16:17	0.11	102.6	0.17	99	0.08	101.9	
27/03/2019	12:46	0.1	100.3	0.15	90.9	0.08	98.4	
29/03/2019	12:19	0.11	88.8	0.17	95.3	0.05	94.4	
4/04/2019	13:15	0.07	92.6	0.1	95.3	0.07	86.9	
5/04/2019	12:20	0.06	86.6	0.05	95.1	0.03	86.2	
11/04/2019	13:01	0.11	91.8	0.12	104.3	0.09	95.7	
17/04/2019	12:11	0.13	91.8	0.18	97.1	0.06	90.1	
18/04/2019	13:05	0.06	82	0.04	88.3	0.03	85.2	
23/04/2019	16:02	0.13	92.1	0.09	94.2	0.06	102.2	
24/04/2019	14:05	0.09	91.8	0.22	88.3	0.05	82.5	
26/04/2019	12:44	0.1	95.6	0.22	98.2	0.05	104.6	
1/05/2019	12:14	0.08	89.6	0.07	90.8	0.04	95	
3/05/2019	10:44	0.14	95.2	0.27	101.7	0.09	94.7	
8/05/2019	11:53	0.13	99.1	0.28	90.8	0.1	106.5	
10/05/2019	9:58	0.1	88.4	0.09	94.2	0.1	111.4	
15/05/2019	12:06	0.07	86.1	0.12	90.1	0.07	88.9	
16/05/2019	13:03	0.09	88	0.1	95.4	0.06	87.3	

						1	
21/05/2019	13:17	0.13	99.5	0.16	90.2	0.09	90.8
24/05/2019	12:15	0.13	95.8	0.14	103.5	0.05	93.9
30/05/2019	16:17	0.12	90.9	0.23	97.2	0.06	96.8
31/05/2019	7:09	0.07	91.8	0.06	98.3	0.06	100.5
4/06/2019	12:52	0.1	108.9	0.07	103.2	0.09	100.8*
7/06/2019	12:17	0.15	89.6	0.17	93.2	0.09	100.1
11/06/2019	16:02	0.11	86.6	0.18	95	0.04	91.3
12/06/2019	9:30	0.08	88	0.1	88.8	0.07	97.2
14/06/2019	12:22	0.09	92.3	0.16	98.2	0.09	94.6
19/06/2019	13:18	0.1	84.9	0.14	92.6	0.09	87.6
21/06/2019	12:18	0.07	90.6	0.09	98.7	0.08	92.2
28/06/2019	15:23	0.12	92.3	0.23	100.3	0.08	91.2
3/07/2019	12:47	0.07	89.6	0.07	96.2	0.04	88.3
5/07/2019	11:16	0.14	96.1	0.25	99.2	0.16	91.2
5/07/2019	11:18	0.06	85.5	0.07	87.5	0.03	104.1
11/07/2019	13:18	0.09	105.4	0.11	92.8	0.09	102.8
13/07/2019	8:57	0.07	103	0.13	80.4	0.05	97.4
19/07/2019	12:30	0.46	91.2	0.61	97	0.13	89
19/07/2019	12:58	0.40	93.8	0.09	88.3	0.06	84.8
24/07/2019	12:52	0.07	88.4	0.03	82.7	0.06	95.4
25/07/2019	13:24	0.12	84.9	0.12	88.6	0.06	83.6
30/07/2019	12:17	0.07	96.5	0.03	100.9	0.05	96.6
1/08/2019	12:17	0.1	88.4	0.12	97.1	0.03	87.1
6/08/2019	9:27	0.07	92.6	0.08	93.6	0.00	88.2
12/08/2019	12:24	0.11	103.7	0.12	92.2	0.06	97.6
13/08/2019	13:13	0.08	94.8	0.1	90.7	0.06	93.6
15/08/2019	12:48	0.11	107.3	0.13	87.8	0.05	106.5
20/08/2019	12:50	0.09	104.4	0.17	86.4	0.06	90.4
22/08/2019	14:37	0.26	104.2	0.31	103	0.22	101
27/08/2019	13:18	0.08	92.6	0.19	95.5	0.05	84.2
29/08/2019	13:10	0.06	95.2	0.06	97.3	0.04	107.8
30/08/2019	10:45	0.07	90.3	0.08	97.2	0.05	92.8
3/09/2019	12:02	0.19	89.9	0.18	89.9	0.07	91.8
5/09/2019	12:04	0.15	88.8	0.3	96.8	0.05	86.4
9/09/2019	12:21	0.11	88	0.39	92.4	0.1	98.8
11/09/2019	12:12	0.11	90.6	0.12	94.6	0.04	92.1
13/09/2019	12:01	0.1	94	0.18	90.6	0.05	87.4
13/09/2019	12:02	0.07	85.5	0.14	93	0.07	86.4
19/09/2019	13:06	0.11	90.9	0.19	96	0.05	95.4
24/09/2019	13:00	0.13	91.8	0.17	91.9	0.11	91.7
26/09/2019	13:26	0.09	84.9	0.11	94.7	0.06	90.9
1/10/2019	12:17	0.1	92.3	0.08	99.5	0.05	91.5
1/10/2019	12:17	0.06	92.3	0.04	99.5	0.03	91.5
3/10/2019	12:03	0.08	95	0.11	88.7	0.07	84.9
9/10/2019	12:18	0.11	93.8	0.09	93.1	0.07	91.3
11/10/2019	12:20	0.08	98	0.11	91.3	0.06	92.3
21/10/2019	13:23	0.11	84.9	0.1	94.3	0.08	88.4

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29/10/2019	12:16	0.11	84.2	0.08	100.3	0.07	92.3
31/10/2019	12:17	0.13	88.4	0.14	91.2	0.05	88.1
5/11/2019	12:23	0.14	94.4	0.14	93.7	0.09	104.9
11/11/2019	12:22	0.13	103	0.19	90.2	0.04	93.9
13/11/2019	12:22	0.15	98.7	0.26	87.3	0.09	98.9
18/11/2019	12:21	0.15	89.9	0.27	100.4	0.09	87.8
20/11/2019	11:14	0.21	91.8	0.28	97	0.06	96.1
21/11/2019	13:29	0.13	86.6	0.09	93.9	0.08	94.5
29/11/2019	11:57	0.11	88.4	0.12	91.2	0.03	89.8
4/12/2019	11:22	0.14	88	0.17	95.2	0.05	95.2
5/12/2019	12:32	0.13	105.1	0.11	93.7	0.04	99.9
5/12/2019	12:34	0.12	99.6	0.16	84.7	0.05	100.5
12/12/2019	12:13	0.09	110.5	0.11	99.6	0.02	108.2
18/12/2019	13:06	0.18	91.5	0.19	98.5	0.08	98.4

^{*}Calculated result – refer to App_E Enviro Strata – Review of Air Vibration Result

Table 22 Mt Owen Blast Monitoring Results – Integra Underground and Integra Surface*

		Integra Uı	nderground*	Integra	Surface*
Date Fired	Time Fired	Peak Vibration (mm/s)	Peak Overpressure dB(L)	Peak Vibration (mm/s)	Peak Overpressure dB(L)
2/01/2019	12:39	0.74	105.2	0.22	102.2
4/01/2019	10:58	1.98	109.2	0.18	102.3
7/01/2019	14:22	1.1	105.3	0.25	101.9
10/01/2019	9:41	0.47	110.1	0.15	97.1
11/01/2019	12:03	0.62	103.5	0.18	96.6
16/01/2019	14:09	8.39	120.8	0.68	101.5
18/01/2019	10:43	1.75	113.2	0.19	100.1
23/01/2019	13:20	6	112.6	0.27	99.7
25/01/2019	12:18	0.99	115.3	0.28	99.9
30/01/2019	16:00	0.92	106.6	0.15	95
01/02/2019	12:25	0.64	107	0.34	97.9
01/02/2019	12:27	6.13	112	0.2	96.6
05/02/2019	12:32	2.69	117.1	0.2	101.6
07/02/2019	13:06	0.31	104.7	0.12	96.8
07/02/2019	13:10	1.73	103	0.05	95.3
13/02/2019	12:44	0.71	114.1	0.25	99.6
15/02/2019	12:11	3.74	115.5	0.39	100.5
20/02/2019	15:57	1.83	107	0.35	105.6
22/02/2019	11:58	0.94	108.6	0.19	106.7
28/02/2019	13:13	2.11	116.7	0.33	102.4
5/03/2019	12:34	1.76	111	0.28	100.5
7/03/2019	12:37	0.42	107.7	0.19	95.8
12/03/2019	13:18	0.96	115.9	0.25	102.5
15/03/2019	12:03	0.84	108.9	0.32	97.8
21/03/2019	16:17	0.93	106.5	0.39	102
27/03/2019	12:46	0.82	108.2	0.31	98.8
29/03/2019	12:19	5.06	114	0.26	106.1
4/04/2019	13:15	0.87	106	0.17	102.6
5/04/2019	12:20	1.01	111.1	0.17	99.4
11/04/2019	13:01	0.79	112.7	0.27	101.6
17/04/2019	12:11	6.5	115.1	0.29	106
18/04/2019	13:05	2.03	115.7	0.18	101.6
23/04/2019	16:02	0.57	105.7	0.3	9.2
24/04/2019	14:05	6.99	106.3	0.2	98.8
26/04/2019	12:44	2.45	109.5	0.22	109
1/05/2019	12:14	0.68	107.5	0.16	105.2
3/05/2019	10:44	1.89	114.2	0.36	105
8/05/2019	11:53	1.46	108.4	0.61	106.7
10/05/2019	9:58	3.26	116.8	0.4	114.7
15/05/2019	12:06	1.83	108.3	0.17	100.7
16/05/2019	13:03	1.44	109.2	0.26	104.4
21/05/2019	13:17	0.8	107.3	0.28	99.9

24/05/2019	12:15	1.31	112.9	0.24	102.8
30/05/2019	16:17	0.98	111.7	0.3	103.7
31/05/2019	7:09	3.09	117.7	0.21	109.6
4/06/2019	12:52	0.91	109.3	0.17	107.2
7/06/2019	12:17	0.83	113.8	0.04	98.2
11/06/2019	16:02	4.37	112.9	0.28	101.8
12/06/2019	9:30	0.99	105.1	0.21	101.3
14/06/2019	12:22	1.55	105.9	0.35	99.4
19/06/2019	13:18	0.88	106.4	0.3	99.1
21/06/2019	12:18	0.98	113.7	0.22	102.9
28/06/2019	15:23	5.98	114.5	0.4	104
3/07/2019	12:47	1.07	109	0.3	104.1
5/07/2019	11:16	1.52	107.5	0.34	104.6
5/07/2019	11:18	2.25	104.4	0.14	104
11/07/2019	13:18	0.52	111	0.22	110.1
13/07/2019	8:57	2.6	110.8	0.15	105.9
19/07/2019	12:30	2.68	109.8	1.05	104.7
19/07/2019	12:58	4.36	111.7	0.3	103.4
24/07/2019	12:52	1.48	110.4	0.21	103.2
25/07/2019	13:24	1.57	106.1	0.23	99.8
30/07/2019	12:17	1.08	116.8	0.28	102.7
1/08/2019	12:36	0.73	105.9	0.38	99.8
6/08/2019	9:27	0.81	105.4	0.12	100.8
12/08/2019	12:24	1.46	114.3	0.24	101.7
13/08/2019	13:13	1.44	109.4	0.28	98.7
15/08/2019	12:48	0.7	109.8	0.27	98.2
20/08/2019	12:50	7.81	119.3	0.32	103.4
22/08/2019	14:37	1.29	111.6	0.67	96.1
27/08/2019	13:18	4.62	107.1	0.18	93.9
29/08/2019	13:10	0.66	111.3	0.16	98.8
30/08/2019	10:45	4.12	113.4	0.19	96.9
3/09/2019	12:02	0.45	108.1	0.21	96.5
5/09/2019	12:04	0.81	103.8	0.33	93.3
9/09/2019	12:21	3.95	110.1	0.35	97.1
11/09/2019	12:12	1.15	110.8	0.21	98
13/09/2019	12:01	0.81	106.9	0.38	0.96
13/09/2019	12:02	2.43	108.8	0.22	93.8
19/09/2019	13:06	0.54	110	0.26	99.1
24/09/2019	13:00	7.52	82.3	0.43	100.5
26/09/2019	13:26	1.79	73	0.16	92
1/10/2019	12:17	2.97	81.8	0.24	102.9
1/10/2019	12:17	0.95	68.8	0.1	102.9
3/10/2019	12:03	1.5	70.7	0.19	104.4
9/10/2019	12:18	0.71	77.9	0.28	103.8
11/10/2019	12:20	1.48	74.8	0.26	103.9
21/10/2019	13:23	1.29	75.8	0.35	97.8
29/10/2019	12:16	0.7	74.8	0.18	98.9
20, 10,2010	12.10	V.1	1 1.0	0.10	00.0

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31/10/2019	12:17	0.81	71.5	0.23	100.2
5/11/2019	12:23	9.97	76.7	0.48	101.6
11/11/2019	12:22	0.52	70.7	0.26	103.8
13/11/2019	12:22	2.92	75.3	0.32	106.2
18/11/2019	12:21	1.31	73	0.36	103.3
20/11/2019	11:14	2.91	84.9	0.32	107.2
21/11/2019	13:29	4.97	78.7	0.49	100.4
29/11/2019	11:57	1.36	70.7	0.16	99.6
4/12/2019	11:22	1.53	79.3	0.2	100.3
5/12/2019	12:32	0.79	109.8	0.29	105.2
5/12/2019	12:34	0.47	109.2	0.27	109.5
12/12/2019	12:13	0.44	99.7	0.08	104
18/12/2019	13:06	1.78	112.9	0.41	108.5

^{*}No Monitoring required at these sites under SSD-5850. Internal Purposes Only.

Table 23: Glendell Blast Monitoring Results – MOC 3, Church, MOC2, Ravensworth Homestead

		MOCO		Oh		МОС	2	Davisans	th Hamastand
		MOC3		Chu	rcn	MOC	2	Ravenswor	th Homestead
Date Fired	Time Fired	Peak Overpressure (dBL)	Peak Vibration	Peak Overpressure (dBL)	Peak Vibration (mm/s)	Peak Overpressure (dBL)	Peak Vibration (mm/s)	Peak Overpressure (dBL)	Peak Vibration (mm/s)
2/01/2019	13:47	97.8	0.18	101.3	0.1	87.6	0.11	101.8	0.18
2/02/2019	13:43	96.4	0.2	93.4	0.1	97.7	0.29	91.8	0.2
3/01/2019	13:36	95.5	0.36	94.4	0.24	99.8	0.23	107.6	0.42
3/01/2019	13:33	93.3	0.18	94.5	0.09	103.3	0.05	96.9	0.22
8/01/2019	13:41	92.9	0.21	93.4	0.09	88.3	0.05	92.6	0.07
9/01/2019	13:29	104.8	0.3	103.4	0.12	92.2	0.15	93.9	0.41
11/01/2019	13:27	95.1	0.31	90.4	0.24	90.5	0.19	90.2	0.26
14/01/2019	13:31	94.6	0.44	93.6	0.21	87.3	0.17	100.8	0.33
15/01/2019	13:34	99.5	0.17	94.4	0.13	91.6	0.13	93	0.39
15/01/2019	13:35	105.5	0.47	105.4	0.3	98.4	0.24	99.3	0.66
21/01/2019	13:30	94.4	0.48	90.6	0.3	94.1	0.41	93.5	0.49
24/01/2019	13:35	93.6	0.45	93.9	0.22	92.9	0.21	105.2	0.3
31/01/2019	14:00	97.5	0.52	93.7	0.16	94.3	0.2	98.5	0.25
6/02/2019	13:43	97.5	0.41	110.7	0.24	109.5	0.26	105.1	0.35
11/02/2019	13:32	94.2	0.4	96.3	0.24	102.5	0.08	97.2	0.04
14/02/2019	9:25	96.5	0.57	96.0	0.34	106.7	0.31	98.4	0.63
14/02/2019	9:27	89.6	0.4	88.6	0.2	108.5	0.1	107.7	0.25
15/02/2019	13:37	94.3	0.48	94.3	0.16	105.4	0.22	98.8	0.23
21/02/2019	13:30	82.9	0.21	88.2	0.13	93.4	0.07	97.8	0.31
21/02/2019	13:32	88.1	0.28	97.1	0.13	95.9	0.08	100	0.31
25/02/2019	13:40	102.8	0.39	97.7	0.35	89.2	0.18	101.8	0.49
1/03/2019	10:31	94.0	0.2	93.4	0.1	92.2	0.1	95.2	0.2
4/03/2019	13:36	95	0.67	94.4	0.38	93.8	0.45	96.6	0.75
7/03/2019	10:22	90.2	0.35	90.4	0.16	89.7	0.09	103	0.1
8/03/2019	13:30	97	0.17	95.1	0.09	91.5	0.1	90.2	0.22
14/03/2019	13:45	92.2	0.27	92.6	0.12	90.8	0.27	96.4	0.4
19/03/2019	9:22	100.6	0.59	99	0.2	97.3	0.4	89.2	0.21
21/03/2019	13:32	86.1	0.37	87	0.21	82.2	0.11	97.5	0.14
21/03/2019	13:42	89.9	0.23	91.9	0.08	85.8	0.16	93.1	0.11
26/03/2019	13:28	99.9	0.16	97.9	0.11	101.2	0.08	93.6	0.21
29/03/2019	11:22	90.5	0.29	90.4	0.14	88.5	0.08	86.2	0.23
29/03/2019	11:25	95.2	0.23	93.4	0.17	89.2	0.17	89.9	0.34
10/04/2019	13:53	93.4	0.34	90.7	0.18	107	0.24	107.1	0.47
11/04/2019	13:27	96.1	0.46	91.7	0.21	108.1	0.15	89.5	0.23
18/04/2019	14:30	94.1	0.54	92.6	0.42	95.1	0.26	95.6	0.3
24/04/2019	12:27	92.5	0.06	92.6	0.03	96.5	0.06	88.2	0.04
29/04/2019	11:26	93.9	0.2	97.2	0.15	96.5	0.1	96.7	0.27
1/05/2019	12:12	97.7	0.33	98	0.22	90.9	0.25	88.4	0.32
4/05/2019	10:39	89.6	0.28	88.6	0.2	90.9	0.23	97.5	0.15

0/05/2040	12.20	07.4	0.43	98	0.0	00.4	0.40	02.6	0.40
9/05/2019	13:30	97.1			0.2	92.1	0.19	93.6	0.48
13/05/2019	13:29	93.3	0.33	92.7	0.21	92.5	0.22	91	0.69
16/05/2019	13:24	96.7	0.4	93.1	0.2	89.8	0.44	92.5	0.26
21/05/2019	13:33	96.5	0.41	102.6	0.26	99.6	0.34	90.8	0.53
29/05/2019	16:13	103.8	0.4	97.9	0.22	95.2	0.15	111.6	0.17
30/05/2019	13:24	96.7	0.58	99.5	0.25	105.6	0.3	101.2	0.38
1/06/2019	13:02	99.5	0.77	96.9	0.25	91.2	1.09	86.8	0.5
3/06/2019	13:41	97.4	0.21	103.4	0.13	100.8	0.12	92.5	0.23
7/06/2019	13:38	93	0.2	96.8	0.15	87.8	0.11	98.1	0.17
7/06/2019	13:41	96.1	0.36	97.8	0.24	91.5	0.16	96.7	0.37
14/06/2019	13:44	97.6	0.53	92.4	0.47	94.5	0.44	92.6	0.61
14/06/2019	13:47	97.4	0.57	96.7	0.24	91	0.33	86.6	0.51
19/06/2019	13:41	96	0.3	93.6	0.2	92.7	0.31	98.1	0.29
20/06/2019	13:34	93.6	0.43	92.8	0.29	93.9	0.21	88.4	0.25
27/06/2019	13:41	93.4	0.4	92.1	0.23	99.9	0.18	96.2	0.24
27/06/2019	13:44	101.9	0.21	95.7	0.09	93.7	0.06	91.2	0.22
2/07/2019	13:51	102.6	0.33	99.7	0.14	96.3	0.2	101.2	0.25
4/07/2019	11:19	98.4	0.34	96.2	0.16	89.6	0.24	102.8	0.35
15/07/2019	15:39	96.7	0.29	95.6	0.18	98.5	0.19	99	0.51
15/07/2019	15:41	100.4	0.58	99.2	0.27	94.3	0.78	94.9	0.5
18/07/2019	16:39	110.7	0.82	111.7	0.5	97.9	0.26	100.1	0.42
22/07/2019	11:54	99.3	0.25	99	0.19	91.6	0.25	93.4	0.49
25/07/2019	13:25	93.5	0.62	93.5	0.35	89.1	0.16	91.6	0.26
31/07/2019	13:25	88	0.46	88.2	0.34	85.9	0.28	90	0.31
1/08/2019	13:37	94.2	0.79	96.5	0.37	93	0.16	92.7	0.75
2/08/2019	10:53	94.7	0.33	93	0.15	90.1	0.23	88.6	0.29
7/08/2019	14:39	97.5	0.4	98.2	0.22	94.2	0.73	89.5	0.52
12/08/2019	13:23	97.3	0.24	96.2	0.1	93.7	0.14	106.4	0.28
23/08/2019	11:58	92.3	0.4	93.1	0.2	91.9	0.24	103.8	0.82
28/08/2019	13:30	96.2	0.32	96.3	0.22	93.5	0.24	94.9	0.24
28/08/2019	13:32	97.3	0.63	97.1	0.3	95.2	0.2	94.5	0.41
9/09/2019	13:28	93.9	0.37	101.6	0.2	97.8	0.18	105	0.44
11/09/2019	11:07	91.7	0.28	89.5	0.2	87.5	0.18	92.3	0.17
5/09/2019	13:33	86.7	0.01	74.0	0.0	83.3	0.01	77.3	0
19/09/2019	13:43	94.3	0.47	97.0	0.2	94.2	0.16	96.7	0.39
24/09/2019	10:33	93.9	0.33	91.8	0.2	87.9	0.18	90.3	0.25
30/09/2019	13:34	95.3	0.18	107.9	0.2	104.1	0.11	108.6	0.48
26/09/2019	13:28	94.7	0.58	95.5	0.36	103.5	0.91	89.7	1.68
1/10/2019	13:40	97.7	0.25	98.1	0.29	99.7	0.13	105.2	0.37
3/10/2019	13:29	92.5	0.35	92.3	0.29	85.5	0.12	95	0.4
3/10/2019	13:32	91.9	0.46	93.2	0.21	91.9	0.26	93.2	0.35
9/10/2019	10:51	97.9	0.22	95.6	0.21	90	0.21	100.9	1.61
10/10/2019	13:34	90	0.27	89.8	0.24	94.1	0.32	88.5	0.24
12/10/2019	9:25	92.8	0.29	91.8	0.17	97.7	0.19	109.6	0.72
18/10/2019	11:35	103	0.8	102.5	0.39	108.2	0.36	103.3	0.53
22/10/2019	13:25	92.3	0.33	94.7	0.15	101.9	0.12	90.2	0.27

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00/40/0040	40.00	00.0	0.4	05.0	0.04	00.7	0.00	00.4	0.54
23/10/2019	13:39	96.2	0.4	95.8	0.21	90.7	0.29	93.1	0.54
28/10/2019	15:24	93.6	0.37	105.8	0.18	93.2	0.12	107.1	0.45
31/10/2019	13:58	92.7	0.28	94.8	0.16	99.6	0.11	104.5	0.33
31/10/2019	14:01	97.6	0.44	96.7	0.25	85.8	0.18	101.1	0.22
5/11/2019	13:31	88.6	0.38	96.8	0.17	93.2	0.18	102.4	0.25
9/11/2019	9:06	97.6	0.45	100.1	0.31	95.6	0.2	103.6	0.64
18/11/2019	12:29	86.4	0.21	89.7	0.17	92.2	0.07	87.9	0.25
18/11/2019	12:31	99.3	0.46	94.9	0.35	102.3	0.31	92.9	0.42
20/11/2019	12:32	94.1	0.21	95.7	0.15	93	0.2	96.3	0.7
21/11/2019	13:32	95.8	0.52	94.5	0.31	92.1	0.55	94.5	0.45
28/11/2019	15:48	99.9	0.59	97.8	0.61	98.6	0.23	94.4	0.75
9/12/2019	11:16	94.3	0.27	91.5	0.19	90.9	0.14	104	0.36
9/12/2019	11:19	90.5	0.22	91.7	0.1	87.8	0.24	96.5	0.24
11/12/2019	10:58	92.1	0.57	92.5	0.2	93.7	0.25	90.5	0.43
13/12/2019	13:34	94.9	0.22	93.8	0.19	95.7	0.17	105.8	0.48
13/12/2019	13:37	92.3	0.51	101.8	0.19	103.7	0.41	105.3	0.38
18/12/2019	14:18	91	0.3	90.9	0.23	97.5	0.15	96.5	0.63
20/12/2019	13:46	95.9	0.49	93.9	0.23	100	0.14	93.8	0.59
20/12/2019	13:48	95.9	0.48	97.2	0.17	96.5	0.29	100	0.41

Table 24 Glendell Blast Monitoring Results – Powerlines

Table 24 Glendell Blas		Power	lines
Date Fired	Time Fired	Peak Overpressure (dBL)	Peak Vibration (mm/s)
2/01/2019	13:47	108.2	1.34
2/02/2019	13:43	107	1.16
3/01/2019	13:36	105.6	1.43
3/01/2019	13:33	102.9	1.42
8/01/2019	13:41	102.9	0.3
9/01/2019	13:29	104.1	1.51
11/01/2019	13:27	105.8	4.01
14/01/2019	13:31	105.2	1.89
15/01/2019	13:34	110.8	1.12
15/01/2019	13:35	115.1	4.71
21/01/2019	13:30	108.3	4.93
24/01/2019	13:35	107.8	1.6
31/01/2019	14:00	102.4	1.04
6/02/2019	13:43	114.9	3.23
11/02/2019	13:32	105.8	1.7
14/02/2019	9:25	108.5	3.53
14/02/2019	9:27	100.8	0.89
15/02/2019	13:37	113.4	1.4
21/02/2019	13:30	94.5	1.82
21/02/2019	13:32	98.6	0.71
25/02/2019	13:40	112.6	2.15
1/03/2019	10:31	104.3	0.9
4/03/2019	13:36	109.1	5.21
7/03/2019	10:22	103.1	1.04
8/03/2019	13:30	104.4	0.62
14/03/2019	13:45	105.9	1.59
19/03/2019	9:22	104.7	1.31
21/03/2019	13:32	106.7	2.46
21/03/2019	13:42	103.3	1.18
26/03/2019	13:28	105	0.66
29/03/2019	11:22	97.8	0.7
29/03/2019	11:25	106.1	1.17
10/04/2019	13:53	108.9	1.74
11/04/2019	13:27	106.7	2.73
18/04/2019	14:30	110.2	10.35
24/04/2019	12:27	101.9	0.46
29/04/2019	11:26	103.3	0.84
1/05/2019	12:12	104.5	3.27
4/05/2019	10:39	104.2	3.21
9/05/2019	13:30	103.4	1.72
13/05/2019	13:29	101.8	1.68
16/05/2019	13:24	107.3	4.56
21/05/2019	13:33	101.9	1.98

20/05/2040	16,12	111 0	2 54
29/05/2019	16:13	111.3	3.54
30/05/2019	13:24	106.1	1.47
1/06/2019	13:02	105.8	6.46
3/06/2019	13:41	105.3	0.94
7/06/2019	13:38	108.1	1.2
7/06/2019	13:41	106.6	3.12
14/06/2019	13:44	109.7	5.11
14/06/2019	13:47	105	1.28
19/06/2019	13:41	106.6	1.34
20/06/2019	13:34	108.6	3
27/06/2019	13:41	108.2	2.18
27/06/2019	13:44	100.8	0.35
2/07/2019	13:51	107.4	1.5
4/07/2019	11:19	109.4	1.85
15/07/2019	15:39	107.5	2.56
15/07/2019	15:41	108.1	3.42
18/07/2019	16:39	113.1	7.38
22/07/2019	11:54	108.8	1.42
25/07/2019	13:25	107.5	13.61
31/07/2019	13:25	107	10.54
1/08/2019	13:37	105.6	1.23
2/08/2019	10:53	103.7	2.6
7/08/2019	14:39	106.9	2.17
12/08/2019	13:23	106.5	1.03
23/08/2019	11:58	104.8	1.68
28/08/2019	13:30	105.8	1.88
28/08/2019	13:32	108.1	0.77
9/09/2019	13:28	105.1	2.97
11/09/2019	11:07	104.3	1.75
5/09/2019	13:33	89.6	0.11
19/09/2019	13:43	107.8	4.94
24/09/2019	10:33	103.7	1.86
30/09/2019	13:34	111.7	0.68
26/09/2019	13:28	105.5	2.73
1/10/2019	13:40	108.7	1.92
3/10/2019	13:40	114.2	3.78
3/10/2019	13:32	107.6	1.48
		111.7	1.48
9/10/2019	10:51		
10/10/2019	13:34	102.4	3.73
12/10/2019	9:25	102.5	0.82
18/10/2019	11:35	107.8	6.5
22/10/2019	13:25	101.3	0.67
23/10/2019	13:39	105.7	3.03
28/10/2019	15:24	107.1	0.8
31/10/2019	13:58	100	0.73
31/10/2019	14:01	103.5	2.8
5/11/2019	13:31	104.1	0.53

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9/11/2019	9:06	104.1	3.21
18/11/2019	12:29	95.4	1.22
18/11/2019	12:31	104.8	5.32
20/11/2019	12:32	102.4	0.91
21/11/2019	13:32	104	7.1
28/11/2019	15:48	108.9	5.29
9/12/2019	11:16	100	0.82
9/12/2019	11:19	104.5	0.7
11/12/2019	10:58	103.2	1.23
13/12/2019	13:34	102.5	1.59
13/12/2019	13:37	104.5	1.43
18/12/2019	14:18	101.5	2.7
20/12/2019	13:46	99.9	0.93

Table 25: Glendell Main North Railway Blast Monitoring Results

			Peak Vib	ration (mm/s)			Peak Overp	ressure (dBL)	
Date Fired	Time Fired	ARTC 1	ARTC 2	ARTC 3	ARTC 4	ARTC 1	ARTC 2	ARTC 3	ARTC 4
2/01/2019	13:47	0.97	0.51	0.27	0.25	107.5	110.2	104.8	99.4
2/02/2019	13:43	1.04	0.39	0.54	0.54	109.2	109.9	102	98.1
3/01/2019	13:36	1.28	0.51	0.6	0.67	103.9	107.4	104.9	102
3/01/2019	13:33	1.03	0.24	0.18	0.16	102.9	102.7	99.3	93.1
8/01/2019	13:41	0.24	0.3	0.19	0.18	104.3	105.5	100.7	96.6
9/01/2019	13:29	1.02	0.45	0.52	0.73	103.1	113.4	109.9	103.8
11/01/2019	13:27	3.83	0.88	0.37	0.83	104.3	108.2	104.4	101.2
14/01/2019	13:31	0.99	0.65	0.62	0.73	108.7	108.2	102.4	99.6
15/01/2019	13:34	1.15	0.45	0.22	0.22	106.2	107.1	103.5	100.7
15/01/2019	13:35	2.85	0.68	0.42	0.62	111.5	111.1	111.3	107.1
21/01/2019	13:30	3.08	0.91	0.54	0.54	107.7	110	103.5	99.5
24/01/2019	13:35	1.35	0.73	0.58	0.47	106.1	109	101.6	97
31/01/2019	14:00	0.81	0.59	0.99	0.54	100.2	107.5	107.3	102.5
6/02/2019	13:43	2.17	0.76	0.47	0.71	113.2	110.9	107.8	109.5
11/02/2019	13:32	3.19	13.8	0.77	0.25	106.5	120.7	105.1	99.3
14/02/2019	9:25	3.45	0.97	0.69	1	111.4	108.8	107.2	103.8
14/02/2019	9:27	0.82	0.46	0.40	0.67	102.6	98	99.8	101.3
15/02/2019	13:37	1.43	0.48	0.84	0.71	110.4	107.3	101.6	101.6
21/02/2019	13:30	1.76	0.42	0.32	0.18	92.6	102.4	90.6	85.5
21/02/2019	13:32	0.66	0.36	0.3	0.23	96.9	99.6	95.1	95.3
25/02/2019	13:40	1.93	0.43	0.46	0.4	108.5	111	106.9	105.4
1/03/2019	10:31	0.59	0.4	0.22	0.19	102.6	99.3	97.7	94.6
4/03/2019	13:36	5.44	0.8	0.54	0.64	106.5	109.6	103.1	99.8
7/03/2019	10:22	1.31	0.57	0.29	0.37	101.5	109.4	99.5	95.8
8/03/2019	13:30	0.5	0.32	0.19	0.18	104.8	107.3	105.4	101.3
14/03/2019	13:45	1.62	0.45	0.38	0.34	103.6	106.6	101.4	97.6
19/03/2019	9:22	1.23	0.8	0.54	0.77	104.5	109.4	109.3	107.1
21/03/2019	13:32	2.4	0.56	0.4	0.23	106.4	104.5	101.4	95.5
21/03/2019	13:42	0.87	0.56	0.32	0.4	100.3	103.9	102.3	95.3
26/03/2019	13:28	0.45	0.25	0.25	0.27	105.3	104.3	106.4	104.9
29/03/2019	11:22	0.45	0.34	0.7	0.2	97.8	101	103.1	93
29/03/2019	11:25	1.1	0.33	0.41	0.86	103.1	104.5	103.6	99.7
10/04/2019	13:53	1.59	0.51	0.45	0.49	108.9	102.7	102.9	97.4
11/04/2019	13:27	2.95	1.28	0.38	0.57	106.5	106.1	105.2	100.5
18/04/2019	14:30	9.62	1.64	0.78	0.84	107.8	108.4	104.9	103.9
24/04/2019	12:27	0.27	0.22	0.12	0.11	101.8	100.7	98.7	93.9
29/04/2019	11:26	0.85	0.29	0.17	0.18	102.7	101	95.4	96.9
1/05/2019	12:12	2.65	0.88	0.42	0.63	105.3	109.2	108.3	104
4/05/2019	10:39	1.48	0.95	0.42	0.6	103.3	107.3	101.4	95.8
9/05/2019	13:30	0.99	0.55	0.63	0.69	104.2	104.5	104.3	99.6
13/05/2019	13:29	1.12	0.54	0.74	0.79	100.2	102	103	98.8
16/05/2019	13:24	3.56	1.07	0.47	1.27	107.5	110.1	104.6	97.9
21/05/2019	13:33	1.03	0.51	0.89	0.91	100.6	107.2	103.8	99.6

29/05/2019	16:13	2.69	1.42	0.48	0.63	103.2	109.6	107.3	114.5
30/05/2019	13:24	1	0.46	0.68	0.98	105.1	105.7	107.7	109.1
1/06/2019	13:02	3.57	1.04	1.02	2.43	106.1	111	106.3	101.1
3/06/2019	13:41	0.66	0.35	0.29	0.3	107.7	104.8	106.3	106.2
7/06/2019	13:38	0.78	0.32	0.23	0.19	107.8	103.9	100.2	97.9
7/06/2019	13:41	2.75	0.57	0.39	0.55	106.7	105.5	104.9	98.8
14/06/2019	13:44	4.67	2.43	0.96	1.21	108.8	108.9	104.9	101.8
14/06/2019	13:47	1.15	0.67	0.72	0.67	103	110.5	106.6	103.4
19/06/2019	13:41	0.65	0.33	0.3	0.36	106.6	104.2	104.5	100.3
20/06/2019	13:34	2.35	1.16	0.53	0.9	108.3	105.7	101.8	99.2
27/06/2019	13:41	1.8	0.72	0.42	0.41	102.8	103.9	100.2	92
27/06/2019	13:44	0.24	0.3	0.22	0.33	102.1	101.5	97.1	93.2
2/07/2019	13:51	1.14	0.47	0.49	0.52	106.5	110.3	110.7	107.8
4/07/2019	11:19	1.55	0.53	0.45	0.7	108.9	109.3	107.6	101
15/07/2019	15:39	1.67	0.36	0.32	0.34	105.2	108.9	103.2	100.4
15/07/2019	15:41	1.58	0.79	1.22	1.28	110.1	112.4	106.7	109.9
18/07/2019	16:39	5.91	1.68	0.63	1.11	114	118.4	111.2	107
22/07/2019	11:54	0.74	0.32	0.43	0.36	107.3	108.1	107.5	103
25/07/2019	13:25	7.03	2.67	0.79	0.69	110	108.2	105.2	100.3
31/07/2019	13:25	7.22	1.17	0.54	0.96	105.4	105.4	101.3	99.9
1/08/2019	13:37	1.14	0.93	0.64	0.53	104.9	104.8	105.1	105
2/08/2019	10:53	1.63	0.59	1.47	0.56	105	107.1	110.1	98.9
7/08/2019	14:39	1.08	0.57	0.54	0.48	105.9	105.8	101.9	99.7
12/08/2019	13:23	0.71	0.3	0.18	0.2	105	103.9	98.8	99.1
23/08/2019	11:58	1.51	0.59	0.49	0.57	104.7	103.8	99.7	97
28/08/2019	13:30	2.11	0.54	0.34	0.38	103.2	104.2	100.4	94.5
28/08/2019	13:32	0.95	0.53	0.48	0.47	106.1	107.9	108.1	101.8
9/09/2019	13:28	1.97	0.51	0.36	0.41	100.8	103.8	102.6	106.6
11/09/2019	11:07	1.48	0.67	0.40	0.51	104.6	109.2	101.8	97.5
5/09/2019	13:33	0.22	0.15	0.05	0.01	91.3	86.8	78.3	87.8
19/09/2019	13:43	2.81	0.71	0.36	0.31	110.1	113.0	104.5	99.7
24/09/2019	10:33	1.51	0.63	0.42	0.50	102.8	107.9	104.5	98.2
30/09/2019	13:34	0.49	0.39	0.37	0.27	108.4	106.9	102.2	109.9
26/09/2019	13:28	2.56	0.84	1.04	2.09	104.4	106.1	104.2	99.3
1/10/2019	13:40	1.6	0.89	0.46	0.5	107.6	104.7	102.7	98
3/10/2019	13:29	2.46	0.45	0.26	0.33	111.4	103.5	94.8	96.3
3/10/2019	13:32	1.17	0.57	0.95	1.01	108.1	105.6	101.6	95
9/10/2019	10:51	1.15	0.6	0.32	0.42	111.5	110.2	104.1	104.6
10/10/2019	13:34	2.64	1.02	0.41	0.69	103.2	103.2	99.9	94.9
12/10/2019	9:25	0.89	0.35	0.47	0.35	101.3	100.5	97	94.4
18/10/2019	11:35	3.79	1.2	0.74	1.1	107.7	112.6	106.3	107.8
22/10/2019	13:25	0.39	0.38	0.37	0.38	101.4	104.4	101.5	98.5
23/10/2019	13:39	2.15	0.83	0.5	0.56	103.9	108.1	104.2	97.2
28/10/2019	15:24	1.02	0.44	0.35	0.44	103.7	108.4	102.7	101.4
31/10/2019	13:58	0.54	0.49	0.32	0.36	99.4	98.8	99.7	104.4
31/10/2019	14:01	1.69	0.61	0.4	0.68	102.7	104.5	102.7	104.7
5/11/2019	13:31	0.51	0.46	0.56	0.96	100.4	107.4	104.5	99.8

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9/11/2019	9:06	2.44	0.82	0.4	0.82	103.9	111.5	104.4	104.1
18/11/2019	12:29	1.06	0.33	0.41	0.23	97.5	95.7	92.6	93.1
18/11/2019	12:31	2.42	0.71	0.6	1.12	103.7	107.7	103.3	99.8
20/11/2019	12:32	0.87	0.41	0.33	0.42	103.1	107.9	102.6	97.6
21/11/2019	13:32	2.9	0.72	0.77	0.9	107.3	107	101.4	100.2
28/11/2019	15:48	6.31	0.82	0.52	0.55	106.8	112	105.1	101.3
9/12/2019	11:16	0.59	0.73	0.38	0.3	100	104.7	101.1	98.2
9/12/2019	11:19	0.44	0.29	0.36	0.3	102.5	103.8	97.1	95.3
11/12/2019	10:58	1.74	0.62	0.94	0.97	101.3	107	100.1	97.1
13/12/2019	13:34	1.01	0.33	0.57	0.43	104.2	103	100.8	98.1
13/12/2019	13:37	1.02	0.44	0.53	0.92	104.9	105.3	97.1	106.5
18/12/2019	14:18	2.26	0.38	0.28	0.47	100.8	101.7	100.4	94.2
20/12/2019	13:46	0.8	0.55	0.61	0.75	100	102.7	98.5	93.8

Table 26 Glendell Blast Monitoring Results – Integra Surface*

Data Fired	Time Fired	Integra S	Surface
Date Fired	rime rirea	Peak Overpressure dB(L)	Peak Vibration (mm/s)
2/01/2019	13:47	102.5	0.16
2/02/2019	13:43	102.2	0.21
3/01/2019	13:36	101.5	0.32
3/01/2019	13:33	103.4	0.09
8/01/2019	13:41	95	0.1
9/01/2019	13:29	97.1	0.32
11/01/2019	13:27	96.4	0.4
14/01/2019	13:31	96.9	0.36
15/01/2019	13:34	95.8	0.25
15/01/2019	13:35	102	0.46
21/01/2019	13:30	99.3	0.47
24/01/2019	13:35	96.6	0.37
31/01/2019	14:00	96.7	0.31
6/02/2019	13:43	99.7	0.57
11/02/2019	13:32	104.3	0.11
14/02/2019	9:25	98.6	0.71
14/02/2019	9:27	92.5	0.25
15/02/2019	13:37	95.5	0.37
21/02/2019	13:30	92	0.19
21/02/2019	13:32	93.4	0.13
25/02/2019	13:40	91.9	0.24
1/03/2019	10:31	94	0.12
4/03/2019	13:36	95.9	0.52
7/03/2019	10:22	99.6	0.24
8/03/2019	13:30	99.9	0.16
14/03/2019	13:45	98	0.29
19/03/2019	9:22	101.4	0.55
21/03/2019	13:32	100.5	0.14
21/03/2019	13:42	100.4	0.2
26/03/2019	13:28	100.2	0.13
29/03/2019	11:22	103.5	0.16
29/03/2019	11:25	105.7	0.23
10/04/2019	13:53	109	0.3
11/04/2019	13:27	100.4	0.44
18/04/2019	14:30	104.5	0.42
24/04/2019	12:27	97.8	0.05
29/04/2019	11:26	106.5	0.15
1/05/2019	12:12	103	0.4
4/05/2019	10:39	105.2	0.41
9/05/2019	13:30	103.8	0.35
13/05/2019	13:29	98.2	0.35
16/05/2019	13:24	105.9	0.62
21/05/2019	13:33	100.7	0.39

29/05/2019	16:13	106	0.34
30/05/2019	13:24	110.4	0.37
1/06/2019	13:02	107.4	1.46
3/06/2019	13:41	109.7	0.16
7/06/2019	13:38	101.9	0.15
7/06/2019	13:41	100.6	0.26
14/06/2019	13:44	100.4	0.77
14/06/2019	13:47	97.9	0.48
19/06/2019	13:41	98.7	0.25
20/06/2019	13:34	97.7	0.44
27/06/2019	13:41	103.6	0.25
27/06/2019	13:44	105.2	0.15
2/07/2019	13:51	106.5	0.4
4/07/2019	11:19	105.5	0.43
15/07/2019	15:39	105.9	0.26
15/07/2019	15:41	102.6	0.53
18/07/2019	16:39	105.1	0.51
22/07/2019	11:54	102.7	0.23
25/07/2019	13:25	100	0.3
31/07/2019	13:25	99.6	0.44
1/08/2019	13:37	99.9	0.42
2/08/2019	10:53	100.8	0.45
7/08/2019	14:39	100.7	0.45
12/08/2019	13:23	98.2	0.23
23/08/2019	11:58	94.7	0.34
28/08/2019	13:30	95.7	0.37
28/08/2019	13:32	100.5	0.38
9/09/2019	13:28	98.6	0.38
11/09/2019	11:07	94.0	0.33
5/09/2019	13:33	92.2	0.02
19/09/2019	13:43	94.0	0.34
24/09/2019	10:33	93.6	0.44
30/09/2019	13:34	101.7	0.18
26/09/2019	13:28	92.2	1.25
1/10/2019	13:40	100.5	0.19
3/10/2019	13:29	87.6	0.22
3/10/2019	13:32	91.7	0.55
9/10/2019	10:51	102.1	0.55
10/10/2019	13:34	105.8	0.4
12/10/2019	9:25	102.9	0.29
18/10/2019	11:35	104.8	1.11
22/10/2019	13:25	99.6	0.27
23/10/2019	13:39	96.6	0.82
28/10/2019	15:24	101.2	0.17
31/10/2019	13:58	100.4	0.19
31/10/2019	14:01	101.5	0.33
5/11/2019	13:31	99	0.38

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9:06	104.3	0.7
12:29	103.6	0.15
12:31	103.5	0.44
12:32	102.7	0.38
13:32	102.7	0.55
15:48	102.3	0.42
11:16	102	0.28
11:19	101.2	0.22
10:58	107.3	0.44
13:34	105.7	0.21
13:37	104.8	0.56
14:18	107.3	0.25
13:46	105.2	0.29
	12:29 12:31 12:32 13:32 15:48 11:16 11:19 10:58 13:34 13:37 14:18	12:29 103.6 12:31 103.5 12:32 102.7 13:32 102.7 15:48 102.3 11:16 102 11:19 101.2 10:58 107.3 13:34 105.7 13:37 104.8 14:18 107.3

^{*}No Monitoring required at these sites under SSD-5850. Internal Purposes Only

Table 27: Ravensworth East Blast Monitoring Results – MOC 1 and MOC 2

		M	OC1	M	DC2
Date Fired	Time Fired	Peak Vibration (mm/s)	Peak Overpressure (dBL)	Peak Vibration (mm/s)	Peak Overpressure (dBL)
7/01/2019	9:14	0.04	77	0.07	84.4
16/01/2019	13:35	0.03	85.1	0.06	86.6
22/01/2019	13:27	0.07	97.9	0.13	89.7
25/01/2019	13:32	0.05	84.5	0.11	94.6
20/02/2019	13:41	0.08	105.8	0.18	104.9
7/03/2019	9:14	0.03	102.1	0.06	93.1
12/03/2019	13:28	0.08	100.4	0.14	105.1
26/03/2019	14:16	0.03	91.3	0.08	110.8
16/04/2019	12:22	0.06	98.5	0.16	81.8
24/04/2019	13:24	0.06	82.9	0.1	85
2/05/2019	13:34	0.05	82.2	0.08	85
7/05/2019	11:38	0.04	114.7	0.11	108.4
9/05/2019	14:28	0.04	84.8	0.06	90.3
15/05/2019	13:36	0.03	74.8	0.08	85
24/05/2019	13:38	0.09	99.6	0.24	89.4
14/06/2019	12:53	0.01	90.1	0.03	82.7
25/06/2019	13:33	0.03	82.2	0.08	83.8
1/07/2019	13:32	0.07	85.1	0.14	85.9
15/07/2019	13:25	0.06	101.4	0.15	102.7
17/07/2019	13:37	0.04	97.3	0.07	96.7
22/07/2019	13:36	0.05	77	0.1	82.2
30/07/2019	13:32	0.08	88.5	0.14	87.3
5/08/2019	13:30	0.08	83.6	0.12	103.1
12/08/2019	12:20	0.06	82.6	0.2	107.4
15/08/2019	13:33	0.07	109.2	0.11	104.8
21/08/2019	10:12	0.04	110.5	0.11	111
23/08/2019	13:49	0.04	79.1	0.09	91.3
23/08/2019	13:52	0.06	85.7	0.14	87.6
4/09/2019	13:36	0.04	94.2	0.08	94.4
16/09/2019	15:54	0.06	94.7	0.11	102.5
16/10/2019	13:25	0.01	107.5	0.02	106.8
18/10/2019	13:37	0.1	94.9	0.17	104.2
5/11/2019	12:36	0.03	96.9	0.04	101.1
13/11/2019	13:35	0.07	105.9	0.2	93.9
15/11/2019	12:32	0.08	112.5	0.11	104.7
20/11/2019	13:35	0.04	110.8	0.05	102.8
27/11/2019	13:47	0.05	75.3	0.13	94.2
29/11/2019	12:39	0.05	86.4	0.08	92.3
5/12/2019	13:26	0.08	102	0.19	111.6
11/12/2019	13:33	0.07	93.6	0.13	105.7
23/12/2019	13:20	0.06	95.2	0.11	93.6

Table 28 Ravensworth East Blast Monitoring Results – MOC 3 and MOC 4

		M	ОСЗ	MOC4			
Date Fired	Time Fired	Peak Vibration	Peak Overpressure	Peak Vibration	Peak Overpressure		
		(mm/s)	(dBL)	(mm/s)	(dBL)		
7/01/2019	9:14	0.03	80.7	0.08	76.8		
16/01/2019	13:35	0.02	83.9	0.03	80.2		
22/01/2019	13:27	0.04	77.7	0.06	82		
25/01/2019	13:32	0.03	83.3	0.08	89.2		
20/02/2019	13:41	0.11	91	0.13	87.1		
7/03/2019	9:14	0.03	85.2	0.04	79.3		
12/03/2019	13:28	0.04	87	0.06	91		
26/03/2019	14:16	0.02	93.2	0.04	86.5		
16/04/2019	12:22	0.04	82.7	0.08	94.2		
24/04/2019	13:24	0.04	83.9	0.05	80.5		
2/05/2019	13:34	0.04	85.5	0.05	83		
7/05/2019	11:38	0.04	90.5	0.04	94.4		
9/05/2019	14:28	0.04	86	0.03	82		
15/05/2019	13:36	0.03	80.4	0.03	78.7		
24/05/2019	13:38	0.06	97.8	0.09	88.2		
14/06/2019	12:53	0.02	84.3	0.02	82.6		
25/06/2019	13:33	0.06	79.8	0.04	78		
1/07/2019	13:32	0.04	85.2	0.09	79		
15/07/2019	13:25	0.18	107.7	0.08	87.7		
17/07/2019	13:37	0.04	104.2	0.04	98.5		
22/07/2019	13:36	0.04	80.7	0.05	79.9		
30/07/2019	13:32	0.05	76.9	0.05	85.5		
5/08/2019	13:30	0.05	90.5	0.06	83.6		
12/08/2019	12:20	0.04	85.00	0.06	84.3		
15/08/2019	13:33	0.03	88	0.04	106		
21/08/2019	10:12	0.05	94.7	0.07	92.7		
23/08/2019	13:49	0.04	82	0.04	76.4		
23/08/2019	13:52	0.06	85.8	0.07	83.4		
4/09/2019	13:36	0.03	93.4	0.04	86.1		
16/09/2019	15:54	0.05	87.9	0.04	89.1		
16/10/2019	13:25	0.04	86.6	0.02	90.4		
18/10/2019	13:37	0.05	91.1	0.06	94.2		
5/11/2019	12:36	0.03	94.3	0.03	77.2		
13/11/2019	13:35	0.06	81.2	0.09	95.5		
15/11/2019	12:32	0.07	99.8	0.04	96.8		
20/11/2019	13:35	0.06	83.3	0.03	87.4		
27/11/2019	13:47	0.05	84.5	0.05	87.5		
29/11/2019	12:39	1.08	93.2	0.03	91		
5/12/2019	13:26	0.06	107.4	0.08	89.4		
11/12/2019	13:33	0.04	86.6	0.05	92.7		
23/12/2019	13:20	0.04	87.7	0.07	87.9		

Table 29 Ravensworth East Blast Monitoring Results – MOC 5 and Homestead

		M	OC5	Homestead		
Date Fired	Time Fired	Peak Vibration (mm/s)	Peak Overpressure (dBL)	Peak Vibration (mm/s)	Peak Overpressure (dBL)	
7/01/2019	9:14	0.04	79.3	0.21	90.7	
16/01/2019	13:35	0.02	86.7	0.18	105.1	
22/01/2019	13:27	0.06	89.8	0.55	91.1	
25/01/2019	13:32	0.04	89.7	0.37	95.8	
20/02/2019	13:41	0.09	96.2	1.09	101.2	
7/03/2019	9:14	0.03	102.4	0.25	96.4	
12/03/2019	13:28	0.07	98.5	0.46	98.7	
26/03/2019	14:16	0.04	95.9	0.33	103.3	
16/04/2019	12:22	0.06	104.1	0.64	99.5	
24/04/2019	13:24	0.05	81.7	0.46	94.2	
2/05/2019	13:34	0.05	83.6	0.83	95.4	
7/05/2019	11:38	0.06	102.1	0.5	108.7	
9/05/2019	14:28	0.03	81.7	0.41	93.5	
15/05/2019	13:36	0.04	97.7	0.14	105.6	
24/05/2019	13:38	0.11	87.2	0.89	98.6	
14/06/2019	12:53	0.02	90.9	0.14	94.1	
25/06/2019	13:33	0.04	79	0.73	97.9	
1/07/2019	13:32	0.07	84.2	0.46	99.6	
15/07/2019	13:25	0.09	94	0.74	103.4	
17/07/2019	13:37	0.05	101.2	0.19	102.2	
22/07/2019	13:36	0.05	80.6	0.43	98	
30/07/2019	13:32	0.07	79.8	0.46	94.6	
5/08/2019	13:30	0.07	82.1	0.99	97.9	
12/08/2019	12:20	0.06	100	0.34	91.3	
15/08/2019	13:33	0.04	101.1	0.82	103.8	
21/08/2019	10:12	0.06	108.9	0.45	104.9	
23/08/2019	13:49	0.05	84.2	0.62	93.5	
23/08/2019	13:52	0.08	85.3	0.53	96.1	
4/09/2019	13:36	0.03	95.9	0.49	109.1	
16/09/2019	15:54	0.06	95.8	0.63	102	
16/10/2019	13:25	0.01	92.8	0.13	94.6	
18/10/2019	13:37	0.07	98.8	1.08	100.9	
5/11/2019	12:36	0.02	82.9	0.2	91	
13/11/2019	13:35	0.14	97.8	1	98.4	
15/11/2019	12:32	0.03	100.8	0.36	113.7	
20/11/2019	13:35	0.02	90.6	0.33	111.2	
27/11/2019	13:47	0.06	108.1	0.79	96.8	
29/11/2019	12:39	0.02	84.6	0.23	85.8	
5/12/2019	13:26	0.08	105.6	0.87	101.9	
11/12/2019	13:33	0.06	89.2	0.59	104.7	
23/12/2019	13:20	0.06	98.2	0.79	101.8	

Table 30 Ravensworth East Blast Monitoring Results – Chain of Ponds, Hebden School and Church

		Chain o	f Ponds	Hebden	School	Chu	ırch
Date Fired	Time Fired	Peak Vibration (mm/s)	Peak Overpressure (dBL)	Peak Vibration (mm/s)	Peak Overpressure (dBL)	Peak Vibration (mm/s)	Peak Overpressure (dBL)
7/01/2019	9:14	0.1	86.6	0.32	104.1	0.01	94.6
16/01/2019	13:35	0.1	95	0.29	105.9	0.01	83.6
22/01/2019	13:27	0.14	87.1	0.4	105.7	0.03	82.5
25/01/2019	13:32	0.13	88.8	0.21	100.4	0.02	81.6
20/02/2019	13:41	0.18	93.6	0.76	106.5	0.04	110.6
7/03/2019	9:14	0.11	91.2	0.48	106.1	0.02	91.5
12/03/2019	13:28	0.12	94.4	0.33	93.6	0.03	95.9
26/03/2019	14:16	0.08	92.6	0.44	94.4	0.02	95.3
16/04/2019	12:22	0.13	88.4	0.41	105.8	0.03	79.8
24/04/2019	13:24	0.16	87.5	0.5	102.5	0.03	81.2
2/05/2019	13:34	0.16	87.1	0.54	109	0.03	83.4
7/05/2019	11:38	0.15	103.5	0.47	95.1	0.02	99.2
9/05/2019	14:28	0.19	90.9	0.36	103.1	0.02	90.2
15/05/2019	13:36	0.1	91.8	0.81	107.8	0.03	86.8
24/05/2019	13:38	0.15	88.8	1	102.2	0.03	93.7
14/06/2019	12:53	0.07	86.1	0.18	101.8	0.01	80.3
25/06/2019	13:33	0.12	88.4	0.38	104.3	0.04	82.4
1/07/2019	13:32	0.14	90.9	0.65	107.1	0.03	83.4
15/07/2019	13:25	0.19	101	0.55	100.8	0.02	95.7
17/07/2019	13:37	0.11	110.1	0.43	95.7	0.02	102.3
22/07/2019	13:36	0.13	86.6	0.5	103.7	0.02	78.5
30/07/2019	13:32	0.2	92.8	1.11	111.9	0.04	95.9
5/08/2019	13:30	0.16	90.6	0.54	101.4	0.03	84.2
12/08/2019	12:20	0.11	99.4	0.38	94.3	0.03	95.4
15/08/2019	13:33	0.2	104.6	0.83	93.8	0.02	100.6
21/08/2019	10:12	0.18	114.4	0.96	100.7	0.03	110.1
23/08/2019	13:49	0.14	87.1	0.51	103.1	0.02	79.8
23/08/2019	13:52	0.18	90.3	0.65	109.5	0.04	85
4/09/2019	13:36	0.15	105.8	0.43	96.5	0.02	93.6
16/09/2019	15:54	0.2	101.7	0.91	103.2	0.03	92.8
16/10/2019	13:25	0.06	92.1	0.09	95	0.01	92.3
18/10/2019	13:37	0.21	92.8	0.81	96.1	0.03	84.5
5/11/2019	12:36	0.16	96.3	0.31	107	0.02	81.8
13/11/2019	13:35	0.18	96.8	0.93	97.9	0.04	95.9
15/11/2019	12:32	0.26	104.6	0.76	96.9	0.06	111.3
20/11/2019	13:35	0.22	93.6	0.37	106.1	0.02	99.3
27/11/2019	13:47	0.21	89.2	0.56	104.6	0.03	85.6
29/11/2019	12:39	0.12	87.1	0.28	96.4	0.03	91.9
5/12/2019	13:26	0.27	94.6	1.12	106.6	0.04	109.7
11/12/2019	13:33	0.2	95	0.68	103.5	0.04	108.3
23/12/2019	13:20	0.14	102.1	0.56	106.2	0.03	87.4

Table 31 Ravensworth East Blast Monitoring Results – Integra Underground and Integra Surface

		Integra U	nderground*	Integra Surface*		
Date Fired	Time Fired	Peak Vibration (mm/s)	Peak Overpressure (dBL)	Peak Vibration (mm/s)	Peak Overpressure	
7/01/2019	9:14	0.21	96.3	0.11	0.11	
16/01/2019	13:35	0.1	101.2	0.06	0.06	
22/01/2019	13:27	0.4	96.1	0.11	0.11	
25/01/2019	13:32	0.29	99.5	0.09	0.09	
20/02/2019	13:41	0.53	105.1	0.21	0.21	
7/03/2019	9:14	0.16	93.9	0.09	0.09	
12/03/2019	13:28	0.42	107.2	0.14	0.14	
26/03/2019	14:16	0.21	100.4	0.11	0.11	
16/04/2019	12:22	0.36	98.6	0.17	0.17	
24/04/2019	13:24	0.45	95.9	0.16	0.16	
2/05/2019	13:34	0.38	94.6	0.1	0.1	
7/05/2019	11:38	0.32	109.4	0.16	0.16	
9/05/2019	14:28	0.22	97.4	0.08	0.08	
15/05/2019	13:36	0.1	99.6	0.1	0.1	
24/05/2019	13:38	0.3	98.2	0.18	0.18	
14/06/2019	12:53	0.11	93	0.05	0.05	
25/06/2019	13:33	0.26	92.7	0.14	0.14	
1/07/2019	13:32	0.41	96.2	0.16	0.16	
15/07/2019	13:25	0.45	103.7	0.18	0.18	
17/07/2019	13:37	0.24	106	0.09	0.09	
22/07/2019	13:36	0.38	89.4	0.1	0.1	
30/07/2019	13:32	0.46	101.3	0.14	0.14	
5/08/2019	13:30	0.37	96.1	0.2	0.2	
12/08/2019	12:20	0.44	96.1	0.14	0.14	
15/08/2019	13:33	0.28	109.9	0.12	0.12	
21/08/2019	10:12	0.3	116.9	0.13	0.13	
23/08/2019	13:49	0.22	91.8	0.13	0.13	
23/08/2019	13:52	0.42	98.5	0.14	0.14	
4/09/2019	13:36	0.1	90	0.27	0.27	
16/09/2019	15:54	0.11	92.2	0.29	0.29	
16/10/2019	13:25	0.05	62.7	0.03	0.03	
18/10/2019	13:37	0.5	69.8	0.17	0.17	
5/11/2019	12:36	0.1	66.3	0.08	0.08	
13/11/2019	13:35	0.49	66.3	0.18	0.18	
15/11/2019	12:32	0.19	73.6	0.17	0.17	
20/11/2019	13:35	0.14	76.7	0.09	0.09	
27/11/2019	13:47	0.34	69.8	0.16	0.16	
29/11/2019	12:39	0.16	62.7	0.11	0.11	
5/12/2019	13:26	0.43	101.1	0.24	0.24	
11/12/2019	13:33	0.27	93.4	0.15	0.15	
23/12/2019	13:20	0.33	98.3	0.15	0.15	

^{*}No Monitoring required at these sites under SSD-5850. Internal Purposes Only.

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MOUNT OWEN COMPLEX

AIR VIBRATION DATA ANALYSIS FOR A BLAST FIRED ON THE 04thOF JUNE2019

REPORT NO. MO-1901-250619

Thomas Lewandowski 25th June2019 ENVIRO STRATA
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REPORT NO. MO-1901-250619

1. INTRODUCTION

Enviro Strata Consulting Pty Ltd (ESC) was engaged to undertake an independent environmental assessment of blast vibration resulting from through-seam blast C9W_3474 fired by Mount Owen mine on the 04th of June 2019. The request was instigated by an elevated level of air vibration measured by the permanent monitoring system located at Camberwell Church. The Church monitoring station recorded 118.5 dBL which is in excess of the 115 dBL vibration limit (allowed for 5 % of blasts) specified in the environmental licence conditions.

The report presents detailed analyses of the air vibration data generated by through-seam blast C9W 3474 fired on the 04th of June 2019 at 12:53 in the North Pit of the Mount Owen mine.

2. VIBRATION MONITORING RESULTS AND WEATHER CONDITIONS

The location of the blast and vibration monitoring results recorded by monitoring stations are presented in **Figure 1**. The vibration measurements and data files recorded during the blast are summarised in **Table 1**.

The environmental record corresponding to the blast period revealed windy conditions persisting on 04.06.19. The record at 12:50 pm measured as a 10 minute average, around the blast time; indicated a south-westerly wind direction (200 degrees) with a wind speed of approximately 4.2 m/s (average) and up to 8.3 m/s gust conditions, see **Figure 2A**. For completeness the review of the EnvMet results did not reveal any other weather impacts for the Church monitoring station, see **Figure 2B**.

Table 1: Vibration Monitoring Results – 04.06.19 Blast.

Monitoring Station	Distance (m)	Peak Air Vibration (dBL)	PPV (mm/s)	Wavetrace	File
Integra Surface	4,206	107.2	0.17	V	MTN1MOINS
MOC 4	4,046	90.4	0.19	V	MTN1MOMO4
Camberwell	6,868	89.9	0.05	V	MTN1MOCAM
Chain of Ponds	8,470	108.9	0.10	V	MTN1MOCOP
MOC 2Green Acres	4,244	101.6	0.22	V	MTN1MOMO2
Homestead	4,829	113.5	0.11	V	MTN1MOHOM
Church	7,177	118.5*	0.09	V	MTN1MOCHU
MOC 1	4,279	104.8	0.14	V	MTN1MOMO1
Integra U/G	1,266	109.3	0.91	V	MTN1MOINU
MOC 5	4,704	101.4	0.08	V	MTN1MOMO5
Hebden School	5,488	103.2	0.07	V	MTN1MOHES

^{*} In excess of the normal limit of 115 dBL (allowed for 5% of blasts) specified in the environmental licence conditions.

3. BLAST DESIGN DETAILS

The blasting sequence included firing of the through-seam blast with an MIC of $1,132~\mathrm{kg}$ and a maximum hole depth of $16~\mathrm{metres}$. The blast design details are summarised in Table 2.

Table 2: Blast Design Details – 04.06.19 12:53 Blast

Parameters	Details	
Blast type:	Through-seam blast	
Blast ID:	C9W_3474	
Initiation Type:	Electronics	
Blast Coordinates:	(322752; 6412223) R.L. 40	
Hole diameter (mm):	229	
Burden (m):	7.35	
Spacing (m):	8.45	
Hole depth (m):	16	
Stemming height (m)	4.2	
Stemming type:	14/20 mm gravel/aggregate	
MIC (kg):	1,132	
Blast duration (ms):	18,296	

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4. MONITORING DATAANALYSIS

Airblast Arrival Analysis

To assess the validity of the Ecotech system's results, wavetrace records from the Church and Integra U/G monitoring stations were analysed applying the airblast arrival technique. This technique utilises the fact that there are four different types of waves generated during a blast. Each wave travels at a different speed. The following velocities were used for ground vibration waves: 2,200 m/s for P wave, 1,200 m/s for S wave, and 700 m/s for Rayleigh – surface wave. The airblast wave travels at a speed of 340 m/s. The analysis of the data is shown in **Figures 3** - **4**. The time corresponding to the airblast arrival period is marked on each analysed wavetrace.

The Church monitoring station was 7,177 m from the blast. Analysis of the air vibration record from the Church monitoring station indicates gusty wind conditions characterised by the presence of positive and negative peaks; refer to **Figure 3**. The investigated air vibration peak of 118.5 dBL occurred during the airblast arrival period and was caused by a strong wind gust. As the whole air vibration record is affected by continuous wind activity the other type of assessment such as sonic decay law analysis needs to be undertaken, see section below.

To validate the above conclusion regarding wind influence on the recorded data, a supporting analysis from the closest monitoring station (Integra U/G) to the blast was undertaken, see **Figure 4.**

The Integra U/G station was approximately 1,266 m from the blast and recorded a maximum peak of 109.3 dBL. The wavetrace record confirmed lack of any blast abnormalities and relatively low airblast overpressure level for the considered distance (i.e. 1,266 m). Also, an inspection of the wavetrace indicates mild wind conditions, most likely due to localised wind shielding for this particular station.

Sonic Decay Law Analysis

To estimate air vibration level for the Church monitoring station, a sonic decay law analysis was undertaken. For that purpose, monitoring data from other stations and blast design parameters were used.

The results were plotted and used to generate a sonic decay law for the blast, see **Figure 5**. As indicated in the Australian Standard AS2187.2-2006 the sonic decay law analysis is based on the assumption that there is an 8.6 dBL decrease with the doubling of the distance.

The estimated sonic decay parameters were as follows:

```
site exponent = -1.45site constant = 25
```

Therefore, based on the obtained sonic decay parameters, the estimated maximum airblast overpressure level was as follows:

• ChurchStation – 100.8 dBL for 7,177 metres distance

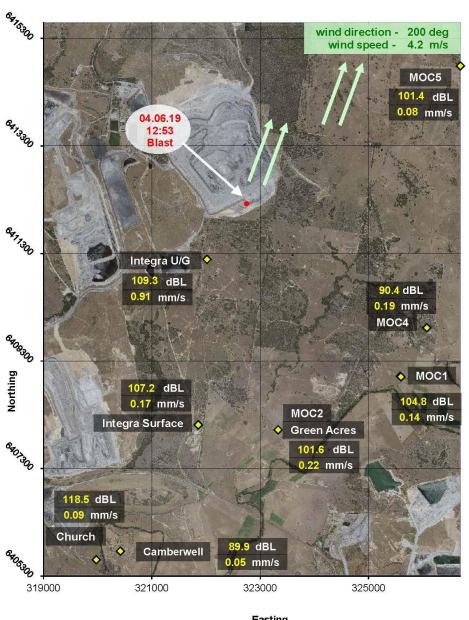
5. CONCLUSIONS

At the request of Mount Owen mine, detailed analyses of the air vibration monitoring data from through-seam blast C9W_3474 fired on the 04th of June 2019 at 12:53 were performed. The analyses revealed the following:

- The peak air vibration of 118.5 dBL recorded by the Church monitoring station (located at 7,177 m) was due to a wind gust. The maximum estimated airblast overpressure level for the Church monitoring station was 100.8dBL. This is based on sonic decay law and wavetrace analyses.
- An additional analysis of the monitoring data from the closest monitoring station (i.e. Integra U/G located at 1,266 m) confirmed a low airblast overpressure level (i.e. 109.3 dBL) generated by the blast and the lack of any blast abnormalities. The record confirmed some mild wind influence on the monitoring results.
- The environmental record confirmed windy conditions; which impacted on the measured air vibration levels (i.e. av. wind speed of 4.2 m/s and wind gust in the order of 8.3 m/s).

On the basis of the above it can be concluded that the airblast overpressure generated during the blast was adequate and there was no exceedance of the air vibration limit.

Thomas Lewandowski 25th June2019



 $FIGURE\ 1-Blast\ Location\ and\ Vibration\ Monitoring\ Results-04.06.19 Blast$

Easting

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MO-1901-250619 Final

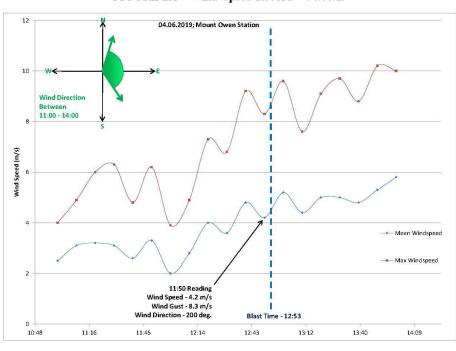
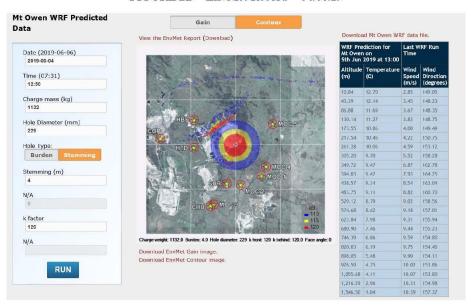


FIGURE 2A - Wind Speed Record - 04.06.19

FIGURE 2B - EnvMet Record - 04.06.19



MO-1901-250619 Final

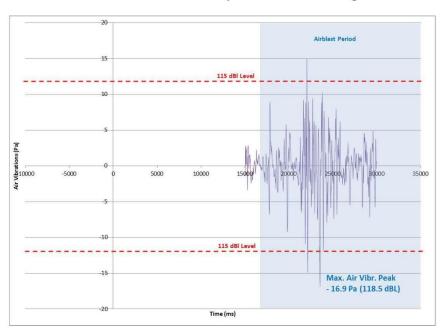
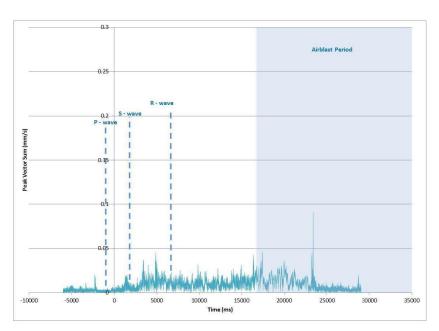


FIGURE 3 – Wavetrace Data Analysis – Church Monitoring Station



8

MO-1901-250619 Final

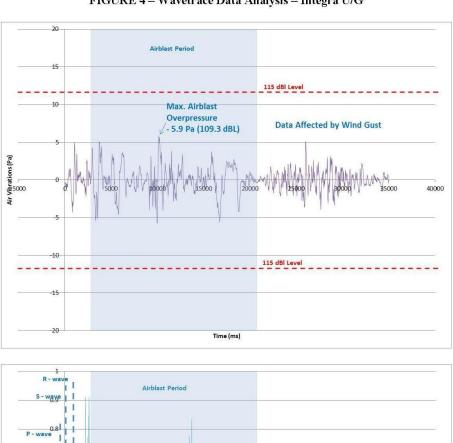
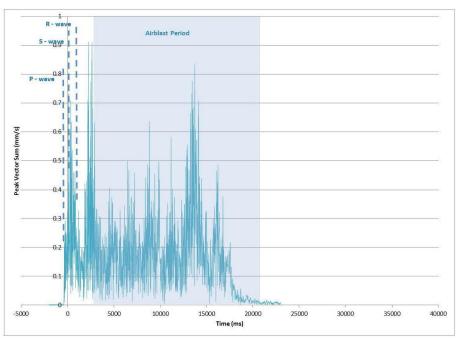


FIGURE 4 – Wavetrace Data Analysis – Integra U/G



9

MO-1901-250619 Final

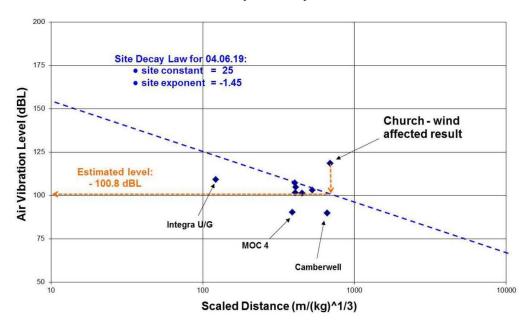


FIGURE 5 – Sonic Decay Law Analysis – 04.06.19 Blast

Appendix F: Air Quality

Table 32: MGO Depositional Dust Gauge Results 2019 (g/m2/month)

Gauge AQMP Ref.	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec		
	Mt Owen													
DD6	2.7	1.6	1.8	1.1	1	1.2	1	0.9	2	0.6	2.2	1.5		
DD7 (DG2)	2.9	2.9	2.5	2.8	2.5	3.1	3.1	2.9	2.30	2.6	3.7	3.3		
DD12	2.8	С	1.1	2.3	2.3	3.9	3.9	4.8	5.1	2.8	С	4.4		
DD14	С	С	С	1.6	1.8	1.8	1.6	1.7	2	1.4	1.6	С		
DD16	1.8	3.2	0.9	2.4	3.2	5.3	С	5.1	6.1	С	3.5	3.8		
					G	lendell								
DG3	1.2	4.5	0.9	1.8	0.3	1.8	С	1.6	2.00	1.8	2.4	2.3		
DG4 (DD15)	2	2.6	4.3	С	2.2	С	3	2.2	5.1	3.3	2.5	3		
DG5	3.8	3.9	С	3.1	3.2	2.9	3.4	3.6	2.60	2.1	4	1.4		
DG6	3.2	С	2.4	2.3	1.5	2.3	2.4	2.3	2.00	С	2	2		
DG7	3.9	D	2.4	2.4	С	3.7	3.8	2.1	2.30	1.6	2.8	2.4		
DG8	2.3	6.2	С	9	3.2	7.9	5.3	2.9	3.20	2.4	3.7	5.6		

C – Dust gauge deemed contaminated after analysis of influencing factors. These factors include an ash residue result of <50%, the presence of bird droppings or other contaminants such as insects in the dust gauge and analysis of historical results from the dust gauge.

D-DG7 sample was knocked off in February 2019, due to strong winds impacting on gauge condition, a new gauge pole was installed in the same month.

Table 33: MGO Total Suspended Particulate Monitoring Results 2019 (µg/m³ 24hr period/wk)

Sampling Date	TSP 1 (Pictons In)	TSP 2 (Middle Falbrook)	TSP 3 (Camberwell)
Sampling Date	(µg/m³)	(µg/m³)	(µg/m³)
2/01/2019	90	44	183
8/01/2019	79	59	93
14/01/2019	86	30	49
20/01/2019	75	34	35
26/01/2019	83	137	86
1/02/2019	61	31	43
7/02/2019	83	23	30
13/02/2019	186	203	180
19/02/2019	137	127	120
25/02/2019	90	23	44
03/03/2019	66	16	31
9/03/2019	63	81	94
15/03/2019	76	27	45
21/03/2019	41	15	16
27/03/2019	68	32	46
2/04/2019	28	19	26
8/04/2019	63	139	171
14/04/2019	52	32	37
20/04/2019	51	18	20
26/04/2019	90	175	190
2/05/2019	78	58	26
8/05/2019	43	105	123
14/05/2019	41	91	111
20/05/2019	39	101	106
26/05/2019	39	165	103
1/06/2019	43	193	127
7/06/2019	36	116	115
13/06/2019	61	178	179
19/06/2019	54	105	67
25/06/2019	40	17	20
1/07/2019	55	83	79
7/07/2019	28	18	21
13/07/2019	22	112	88
19/07/2019	29	160	115
25/07/2019	57	79	108
31/07/2019	49	24	28
6/08/2019	43	112	195
12/08/2019	22	118	159

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18/08/2019	54	80	84
24/08/2019	50	250	177
30/08/2019	53	23	31
5/09/2019	63	73	89
11/09/2019	57	99	13
17/09/2019	24	19	33
23/09/2019	41	54	81
29/09/2019	63	59	77
5/10/2019	60	37	48
11/10/2019	60	11	33
17/10/2019	116	148	150
23/10/2019	87	91	110
29/10/2019	138	87	106
4/11/2019	83	32	59
10/11/2019	92	139	61
16/11/2019	125	138	137
22/11/2019	180	259	215
28/11/2019	150	110	120
4/12/2019	108	224	101
10/12/2019	176	197	206
16/12/2019	144	215	78
22/12/2019	113	91	101
28/12/2019	95	65	99

Note: Days highlighted blue have been denoted as 'extraordinary events' as advised by DPIE. As advised by DPIE, days which were identified as 'extraordinary events' were not included in Long term impact assessment criteria.

Table 34: Continuous PM10 (µg/m3) Monitoring Results 2019

		DPIE PM10	Monitoring 24 H	r Avg		EPA PM10 Monitoring 24 Hr Avg*				
Date	Sx13D1 - Project Office	Sx13D4 - McInerney	Sx13D8 - Pictons In	Sx13D9 - Nobles In	Sx13D11 - Middle Falbrook	Sx13D10 - Cramps	Sx13D6 - EBAM 1	Sx13D5 - EBAM 2		
1/01/2019	18.3	26.2	20.4	21.2	29.5	20.6	24.0	22.5		
2/01/2019	23.0	23.1	35.8	23.4	23.4	24.0	18.3	25.9		
3/01/2019	29.9	30.1	33.5	24.7	22.2	19.7	20.6	24.0		
4/01/2019	29.9	31.0	35.2	27.8	22.9	25.9	32.8	27.8		
5/01/2019	36.8	44.0	28.4	28.2	43.9	44.0	26.1	37.4		
6/01/2019	6.7	7.4	10.9	8.2	44.7	7.3	20.2	8.6		
7/01/2019	10.4	12.4	10.7	9.2	Maintenance	7.2	32.3	8.5		
8/01/2019	19.9	25.9	27.0	25.3	performed	21.3	21.1	22.5		
9/01/2019	38.1	35.1	33.0	33.0	30.5	33.5	25.5	32.7		
10/01/2019	23.7	27.1	28.7	24.8	22.2	21.2	29.2	23.0		
11/01/2019	18.9	21.4	23.7	21.3	18.9	17.2	30.7	18.9		
12/01/2019	20.3	25.8	22.8	24.4	23.5	22.3	25.7	93.0		
13/01/2019	21.9	25.2	32.1	24.2	22.0	19.5	21.9	21.7		
14/01/2019	17.2	19.4	28.4	18.3	18.3	14.7	18.9	17.0		
15/01/2019	28.6	33.0	38.2	31.5	23.7	30.4	49.1	28.8		
16/01/2019	44.3	37.2	56.6	38.5	46.3	37.9	35.0	42.3		
17/01/2019	29.4	32.1	41.1	29.3	40.6	23.6	31.2	28.9		
18/01/2019	34.1	47.9	38.2	37.8	24.6	31.3	26.3	35.2		
19/01/2019	54.3	57.9	40.3	57.9	45.6	45.1	34.5	46.8		
20/01/2019	13.0	17.2	18.6	14.0	13.6	12.2	29.9	13.7		
21/01/2019	7.7	9.5	12.3	9.5	7.3	8.1	23.9	11.1		
22/01/2019	25.1	21.8	25.8	21.3	18.8	23.1	17.3	26.8		
23/01/2019	28.9	35.0	28.9	31.5	37.1	38.0	26.6	34.1		
24/01/2019	27.0	25.4	34.6	28.1	24.6	25.3	25.5	29.5		
25/01/2019	31.6	32.5	34.3	32.5	34.3	33.6	30.2	32.4		
26/01/2019	32.2	33.1	35.1	39.4	47.2	47.6	29.2	33.4		
27/01/2019	41.7	36.3	50.3	38.7	30.5	37.3	37.5	36.1		
28/01/2019	27.0	27.0	37.0	29.3	27.8	26.3	26.1	47.2		
29/01/2019	25.6	32.4	37.2	32.3	30.2	30.2	26.1	28.3		
30/01/2019	24.2	31.0	43.4	29.8	Technical Issue - Circuit	28.2	33.6	26.1		
31/01/2019	47.6	48.5	41.5	37.6	Breaker Malfunction	44.9	37.6	40.6		
1/02/2019	13.9	13.7	16.6	14.2	13.7	13.4	18.0	13.1		
2/02/2019	7.8	9.6	11.6	9.1	7.2	8.1	45.0	10.8		
3/02/2019	12.3	13.8	19.9	12.4	8.3	10.5	11.3	13.8		
4/02/2019	30.5	28.5	31.2	25.7	25.6	25.3	21.1	36.8		
5/02/2019	17.3	22.1	20.1	18.1	19.8	14.7	14.4	15.8		
6/02/2019	9.2	13.5	18.3	9.3	9.8	8.5	13.7	10.4		
7/02/2019	11.8	12.3	25.1	9.7	9.9	10.8	9.6	11.6		
8/02/2019	26.2	29.0	29.8	24.9	23.5	25.8	23.5	22.3		

9/02/2019	20.2	21.2	17.4	17.4	18.0	23.5	38.4	21.5
10/02/2019	61.7	53.0	60.2	56.6	55.4	55.3	33.0	50.5
11/02/2019	31.2	34.8	32.0	37.1	35.0	34.3	38.3	46.3
12/02/2019	43.2	57.1	42.0	53.1	64.0	83.2	49.9	45.5
13/02/2019	66.1	59.4	76.1	62.5	53.3	58.4	42.0	62.9
14/02/2019	19.8	25.9	22.4	21.6	24.0	21.0	13.7	15.9
15/02/2019	20.2	23.2	20.8	15.3	15.4	14.1	11.3	16.0
16/02/2019	10.1	10.6	17.7	12.3	12.4	11.0	12.9	10.8
17/02/2019	14.9	19.3	19.1	17.1	16.6	18.8	13.1	15.0
18/02/2019	36.0	34.4	34.5	33.2	25.5	29.8	29.9	31.3
19/02/2019	55.5	64.3	63.4	59.4	51.2	61.3	47.7	43.9
20/02/2019	17.6	18.3	22.4	19.6	14.5	16.0	21.9	17.0
21/02/2019	9.9	13.2	12.3	11.4	10.5	9.3	15.3	7.8
22/02/2019	16.8	17.1	17.0	12.5	12.1	11.0	25.4	15.8
23/02/2019	9.2	9.1	13.4	9.4	8.9	8.4	10.7	8.7
24/02/2019	18.0	17.9	21.5	16.2	16.6	14.5	20.7	17.0
25/02/2019	20.6	23.0	24.6	15.9	15.5	14.3	13.2	15.9
26/02/2019	16.7	22.2	21.6	17.7	18.2	16.7	12.5	14.0
27/02/2019	16.3	20.8	16.3	10.7	10.4	9.7	8.6	12.6
28/02/2019	11.4	11.5	13.7	8.9	8.4	7.8	9.8	8.7
1/03/2019	12.9	17.7	21.2	10.5	10.0	9.3	23.1	9.6
2/03/2019	15.6	18.8	22.4	11.1	10.3	9.5	11.5	11.5
3/03/2019	10.7	12.7	16.1	10.1	9.2	10.0	7.8	33.7
4/03/2019	20.8	23.2	24.2	16.0	14.1	14.9	20.3	16.0
5/03/2019	30.1	33.6	31.6	25.7	22.9	25.4	21.6	24.3
6/03/2019	69.6	87.1	55.7	65.4	72.0	80.7	61.2	54.3
7/03/2019	23.5	27.1	24.6	23.1	23.4	20.7	69.2	18.9
8/03/2019	21.0	21.3	24.6	20.7	18.5	20.2	14.0	16.0
9/03/2019	28.4	37.6	21.8	27.3	27.7	40.8	30.2	21.8
10/03/2019	18.4	24.7	15.4	16.0	Negative Results Excluded	15.8	32.0	18.4
11/03/2019	52.9	56.1	55.2	52.7	60.9	60.7	43.5	37.7
12/03/2019	33.0	41.6	36.4	33.7	34.2	45.1	34.5	29.5
13/03/2019	27.2	32.3	34.8	27.2	33.6	25.2	34.1	23.0
14/03/2019	25.1	27.5	31.5	24.5	23.0	22.5	39.0	18.5
15/03/2019	16.6	18.4	20.4	13.4	14.9	12.3	14.1	13.8
16/03/2019	11.5	11.8	15.9	11.8	10.6	10.3	33.0	
17/03/2019	4.6	11.2	7.0	7.9	7.9	10.5	25.5	Inconsistent flow – flow
18/03/2019	8.4	12.3	9.3	8.7	10.5	10.9	31.5	calibration performed
19/03/2019	12.0	11.7	13.6	13.0	12.5	11.9	26.0	pononnou
20/03/2019	14.2	16.0	16.3	14.1	13.6	12.2	20.2	13.5
21/03/2019	10.9	11.6	14.4	11.0	9.2	9.0	9.1	10.8
22/03/2019	11.5	11.2	11.8	8.4	10.3	6.8	24.8	12.0
23/03/2019	15.6	18.8	17.3	20.7	17.2	18.7	32.2	15.1
24/03/2019	19.0	26.5	19.3	23.9	22.4	23.1	36.0	17.4

25/03/2019	18.5	25.5	15.5	18.0	19.7	17.0	23.0	18.3
26/03/2019	35.2	38.4	43.4	36.4	42.8	43.2	58.0	31.3
27/03/2019	24.8	24.1	27.9	21.8	20.6	19.3	20.0	23.7
28/03/2019	16.4	18.6	17.7	15.0	13.6	12.6	51.4	23.2
29/03/2019	23.0	25.7	27.1	21.4	25.8	22.4	37.8	19.2
30/03/2019	16.3	21.9	17.4	13.6	21.6	20.7	24.5	17.7
31/03/2019	63.1	69.5	68.9	72.5	71.3	76.1	45.0	44.9
1/04/2019	11.3	18.0	18.8	15.6	13.6	16.6	20.1	7.0
2/04/2019	7.1	8.3	10.6	9.0	6.8	8.8	63.3	5.2
3/04/2019	7.3	10.8	7.7	4.0	8.1	5.7	10.3	18.8
4/04/2019	13.5	12.0	13.5	9.6	10.1	8.7	10.3	14.5
5/04/2019	11.2	12.3	14.5	10.8	10.5	7.9	17.3	8.9
6/04/2019	10.9	18.3	11.2	13.6	12.1	18.4	20.6	12.1
7/04/2019	24.8	35.3	16.1	24.1	29.8	39.1	26.3	22.2
8/04/2019	30.7	43.7	29.0	45.2	53.2	54.6	26.3	23.1
9/04/2019	48.5	52.2	37.2	51.3	49.4	46.4	39.1	30.9
10/04/2019	16.8	19.7	21.8	19.4	16.7	16.3	18.9	17.2
11/04/2019	12.9	15.8	18.7	11.7	10.4	10.2	15.7	11.3
12/04/2019	11.8	14.4	18.2	10.0	9.0	8.5	13.8	15.0
13/04/2019	21.4	28.6	17.0	19.9	19.3	21.9	24.8	17.9
14/04/2019	24.4	22.8	24.7	20.3	19.5	19.7	26.3	23.0
15/04/2019	16.2	16.9	19.0	14.6	16.1	16.1	38.2	14.4
16/04/2019	14.6	15.9	14.2	13.4	11.4	11.3	43.5	19.8
17/04/2019	9.3	9.9	11.5	7.5	8.2	11.2	31.7	8.0
18/04/2019	11.6	13.8	16.5	13.8	16.3	14.2	15.6	10.0
19/04/2019	12.5	17.7	17.0	12.8	12.0	11.0	48.7	12.7
20/04/2019	9.6	12.7	12.2	9.6	8.9	8.1	Unit stopped –	9.5
21/04/2019	9.4	11.1	10.5	10.1	11.7	10.7	technician completed checks	10.0
22/04/2019	12.0	13.8	15.2	13.9	15.2	14.3	Planned	9.3
23/04/2019	8.6	10.2	15.4	8.4	10.6	10.6	Maintenance	14.6
24/04/2019	10.5	11.1	16.8	10.5	13.2	13.2	18.6	9.7
25/04/2019	25.3	31.3	17.0	28.3	38.0	35.9	22.3	19.8
26/04/2019	28.4	55.5	38.2	43.0	55.2	90.3	33.6	25.5
27/04/2019	Low flow	33.1	33.9	34.7	37.1	34.2	23.2	23.5
28/04/2019	alarms received.	40.5	24.4	33.4	32.3	37.2	40.1	23.0
29/04/2019	Maintenance undertaken to	28.4	32.9	23.0	29.6	31.9	21.3	19.0
30/04/2019	address malfunction	29.8	29.6	23.8	24.6	25.8	20.0	17.0
1/05/2019	59.6	28.2	33.2	30.9	43.4	40.9	33.7	19.7
2/05/2019	59.9	29.5	35.1	26.2	30.4	39.9	22.1	26.6
3/05/2019	Low flow	34.0	23.0	29.7	41.2	45.4	31.2	Insufficient
4/05/2019	alarms received.	8.7	7.9	9.0	9.3	9.5	31.6	data – Telstra outage
5/05/2019	Additional maintenance	10.6	9.2	11.6	11.9	10.2	18.5	10.3
6/05/2019	undertaken to address malfunction	21.1	11.0	13.9	14.0	15.1	39.8	9.8

7/05/2019	15.4	33.4	12.6	22.0	24.3	26.2	33.0	13.7
8/05/2019	32.7	40.6	21.8	30.7	32.9	44.4	58.1	25.2
9/05/2019	31.3	26.8	16.2	29.4	30.1	26.8	27.2	29.0
10/05/2019	31.7	28.5	27.2	32.8	34.2	46.6	37.1	20.1
11/05/2019	21.5	22.0	12.8	17.6	24.2	44.8	25.1	15.9
12/05/2019	12.1	15.3	10.7	14.5	16.7	16.4	39.2	10.9
13/05/2019	19.5	26.4	20.2	24.7	35.5	32.6	22.3	17.7
14/05/2019	17.9	26.5	16.6	25.3	33.1	32.0	23.5	15.8
15/05/2019	18.7	21.8	16.2	16.6	16.6	16.8	38.7	15.8
16/05/2019	12.4	16.5	14.5	13.4	22.0	20.1	17.0	10.7
17/05/2019	27.1	25.6	22.7	22.5	20.1	26.9	36.4	20.1
18/05/2019	19.5	20.8	19.7	19.2	27.4	23.7	24.1	15.0
19/05/2019	15.0	19.2	12.3	13.4	13.8	13.2	27.3	21.4
20/05/2019	16.8	21.2	17.2	18.3	25.6	29.8	27.5	12.0
21/05/2019	22.8	29.3	15.6	33.5	41.2	36.3	29.4	15.9
22/05/2019	26.6	32.5	21.1	27.4	37.3	35.5	32.3	18.0
23/05/2019	27.2	32.1	26.9	25.8	31.9	27.6	24.6	20.0
24/05/2019	24.0	35.2	22.8	34.6	41.8	44.7	32.2	19.2
25/05/2019	22.5	33.2	13.9	33.9	47.7	54.8	31.4	18.2
26/05/2019	38.4	38.4	19.0	40.0	55.0	56.6	36.3	24.3
27/05/2019	62.5	66.1	21.0	36.4	67.4	110.6	103.4	51.6
28/05/2019	34.2	31.5	14.8	21.1	33.4	29.5	33.4	25.0
29/05/2019	12 Month	54.4	16.8	24.4	35.3	37.9	55.7	25.4
30/05/2019	Planned Maintenance	22.0	12.0	20.1	27.8	50.0	35.0	19.4
31/05/2019	16.8	23.0	12.5	15.7	30.0	25.2	29.7	12.5
1/06/2019	26.7	32.9	22.5	29.4	35.8	37.9	34.4	19.7
2/06/2019	19.6	25.2	29.6	24.8	26.6	24.6	25.9	30.2
3/06/2019	20.1	23.2	6.9	17.2	21.6	24.4	19.1	21.5
4/06/2019	13.5	12.1	9.7	11.7	15.4	19.9	16.5	Battery not recharged -
5/06/2019	9.5	10.9	11.8	12.6	11.0	7.7	44.1	Solar Panels cleaned
6/06/2019	19.2	22.8	12.3	21.2	28.2	24.8	49.7	14.9
7/06/2019	23.6	35.5	16.5	43.2	64.6	44.5	30.0	17.0
8/06/2019	35.3	36.4	18.2	30.5	33.8	30.8	30.8	23.0
9/06/2019	17.0	23.6	9.9	20.0	21.6	24.9	34.6	12.6
10/06/2019	18.6	26.2	8.2	22.7	31.4	29.9	35.1	13.1
11/06/2019	23.6	25.6	20.5	25.2	31.7	28.4	29.8	14.4
12/06/2019	29.1	28.1	16.2	25.0	45.5	34.2	30.6	21.9
13/06/2019	44.1	51.1	34.6	37.4	41.6	39.5	49.5	27.2
14/06/2019	21.3	28.1	33.4	20.8	24.6	20.8	36.7	13.8
15/06/2019	16.2	22.7	14.4	26.5	54.7	42.8	42.3	13.0
16/06/2019	24.0	25.6	19.2	23.4	Filter Load alarm received. Data removed	40.7	45.7	16.1
17/06/2019	15.9	25.1	23.6	30.6	21.8	24.3	18.5	13.3
18/06/2019	11.2	21.9	7.4	13.2	Maintenance Performed	16.4	24.0	Solar Battery replaced

19/06/2019	13.5	17.5	16.7	12.3	19.5	25.1	38.2	
20/06/2019	15.4	19.2	15.4	16.4	46.4	29.4	51.4	11.8
21/06/2019	21.1	22.2	18.6	19.2	25.8	28.2	25.6	15.3
22/06/2019	24.2	26.1	10.3	19.2	45.9	33.0	27.1	17.0
23/06/2019	9.6	13.8	11.0	11.0	14.8	12.2	22.0	7.3
24/06/2019	8.1	7.6	7.8	5.2	5.2	5.5	42.4	4.3
25/06/2019	7.2	7.0	9.7	6.1	6.2	5.8	22.2	5.2
26/06/2019	7.8	9.7	9.2	6.5	6.2	6.4	11.5	Additional solar panel installed
27/06/2019	7.2	10.8	11.3	7.1	6.6	5.8	9.5	6.4
28/06/2019	10.1	12.7	9.3	8.1	11.5	13.5	14.3	17.0
29/06/2019	14.0	13.7	7.5	11.0	16.5	14.1	17.7	11.0
30/06/2019	26.3	26.1	18.5	22.5	33.7	39.0	21.0	17.1
1/07/2019	22.7	23.3	21.7	21.0	27.6	22.5	17.5	14.7
2/07/2019	26.1	35.3	30.0	33.6	49.8	39.8	21.2	16.9
3/07/2019	22.5	23.3	32.0	18.9	31.9	24.5	18.1	13.9
4/07/2019	9.5	9.7	12.2	10.2	7.7	8.1	13.5	7.7
5/07/2019	9.0	9.1	9.7	7.5	6.4	5.8	12.5	9.1
6/07/2019	5.1	6.4	8.9	6.0	5.5	4.8	10.8	7.1
7/07/2019	8.5	10.0	9.3	8.9	7.3	6.5	14.1	9.8
8/07/2019	9.7	15.4	7.5	11.2	14.9	15.6	15.1	7.5
9/07/2019	13.2	19.7	6.6	10.9	18.4	18.3	19.7	8.8
10/07/2019	15.4	21.2	13.2	14.6	27.7	18.9	17.1	10.6
11/07/2019	29.0	48.5	14.9	24.9	33.3	Invalid results - filter	34.2	23.0
12/07/2019	26.7	43.8	13.4	20.7	29.7	contaminated with insects	23.9	20.2
13/07/2019	28.3	34.5	13.5	20.3	32.1	52.4	24.8	23.6
14/07/2019	28.7	45.7	9.7	17.6	34.5	33.6	18.8	22.5
15/07/2019	14.1	38.8	13.5	14.8	29.1	26.2	12.1	10.5
16/07/2019	17.3	39.4	10.8	16.3	25.4	23.9	14.9	13.2
17/07/2019	20.9	32.4	10.2	16.8	22.9	16.3	16.1	14.0
18/07/2019	24.2	44.4	9.4	17.0	28.6	24.1	14.9	16.4
19/07/2019	19.1	27.5	14.3	18.1	29.1	33.4	21.5	13.9
20/07/2019	20.1	32.6	13.6	32.0	61.6	55.6	19.7	15.4
21/07/2019	33.9	40.9	14.6	32.5	52.0	52.2	23.8	25.4
22/07/2019	37.2	36.8	46.5	35.8	32.5	32.2	20.0	25.4
23/07/2019	44.8	46.4	12 Month	32.4	61.0	51.8	44.1	32.1
24/07/2019	44.0	32.1	Planned	29.6	39.4	65.0	51.0	30.9
25/07/2019	21.6	26.6	Maintenance	21.7	26.6	25.3	17.1	14.2
26/07/2019	29.4	49.3	17.0	23.5	33.0	36.1	25.0	21.6
27/07/2019	32.7	33.9	19.5	30.1	36.6	34.8	23.6	22.6
28/07/2019	18.8	20.1	16.6	17.7	29.9	34.6	19.2	14.7
29/07/2019	28.4	33.1	30.8	29.6	38.0	39.6	23.3	19.9
30/07/2019	13.2	12.8	12.7	12.9	11.5	10.1	14.1	9.4
31/07/2019	13.1	11.9	12.4	10.0	10.3	8.3	10.6	10.5
1/08/2019	17.2	17.7	17.6	11.7			12.2	13.3

2/08/2019	18.2	16.4	16.8	12.4	12 Month Planned Maintenance	12 Month Planned Maintenance	Low flow – Vacuum pump	15.4
3/08/2019	30.0	53.4	14.1	23.3	47.9	46.1	cleaned	29.4
4/08/2019	27.9	41.0	20.5	28.0	29.4	35.4	Inconsistent flow – DC converted replaced	22.4
5/08/2019	28.2	35.6	23.2	23.2	27.4	33.0		23.2
6/08/2019	35.0	47.6	Temporary Power Outage due to external electrical (Ausgrid) works	38.5	45.8	64.5	Low flow – Vacuum pump replaced	28.8
7/08/2019	33.7	46.4	25.6	53.9	53.1	62.9	38.6	25.9
8/08/2019	65.7	100.3	49.6	66.3	69.9	101.1	60.3	47.6
9/08/2019	64.8	111.4	50.8	70.1	70.1	79.5	76.7	54.3
10/08/2019	32.7	45.9	17.5	22.8	36.6	44.0	45.5	27.2
11/08/2019	33.0	35.5	11.2	17.8	26.6	31.9	25.0	21.9
12/08/2019	12.4	27.4	7.7	14.7	17.8	18.7	10.7	10.6
13/08/2019	16.0	31.2	20.4	17.9	23.7	32.7	21.2	22.9
14/08/2019	22.8	33.2	24.7	27.1	35.9	39.8	23.1	18.8
15/08/2019	26.4	36.0	17.8	37.4	57.2	73.3	38.9	26.8
16/08/2019	35.0	46.7	17.5	51.8	69.7	96.4	41.8	27.9
17/08/2019	35.3	51.6	23.7	51.9	44.4	44.8	29.2	24.9
18/08/2019	29.1	27.4	21.8	18.8	21.4	21.0	18.7	24.6
19/08/2019	52.9	57.8	50.8	61.0	64.4	90.4	66.5	42.5
20/08/2019	34.7	56.4	14.7	29.3	49.7	46.4	33.8	27.2
21/08/2019	40.6	57.9	16.3	31.8	44.6	53.4	38.3	32.2
22/08/2019	31.8	35.7	20.2	25.2	39.0	42.8	45.1	22.6
23/08/2019	32.0	24.7	35.1	22.7	21.1	21.9	21.8	21.9
24/08/2019	46.9	60.9	24.2	54.8	77.1	74.0	33.2	36.8
25/08/2019	37.6	44.2	40.5	43.8	47.2	62.1	43.2	23.9
26/08/2019	26.6	12 Month	32.3	23.2	22.8	21.5	19.0	10.3
27/08/2019	16.1	Planned Maintenance	20.9	14.6	13.8	13.5	13.5	15.5
28/08/2019	24.7	32.9	31.8	25.5	21.4	39.8	28.6	22.0
29/08/2019	30.6	29.5	30.1	25.8	29.4	27.9	16.9	20.8
30/08/2019	2.2	7.6	10.0	9.1	7.2	8.8	7.9	2.0
31/08/2019	3.5	6.3	6.9	6.0	5.7	5.6	8.1	4.1
1/09/2019	10.4	14.9	9.7	12.6	13.7	13.2	8.4	8.4
2/09/2019	15.9	19.9	18.3	22.4	27.0	29.8	14.1	14.1
3/09/2019	20.2	23.4	23.3	21.4	25.3	26.3	18.5	18.5
4/09/2019	36.4	31.5	34.3	28.8	37.6	47.3	28.2	28.2
5/09/2019	25.6	33.9	30.4	27.7	30.9	31.9	20.1	20.1
6/09/2019	56.1	84.1	73.9	51.2	65.8	64.0	70.2	70.2
7/09/2019	39.4	50.6	24.8	36.4	44.0	100.0	37.1	37.1
8/09/2019	17.3	27.3	13.8	19.3	26.5	55.9	14.4	14.4
9/09/2019	16.0	23.6	22.3	16.2	19.7	41.7	16.9	16.9
10/09/2019	18.3	16.5	22.1	16.2	14.4	15.8	13.3	13.3

11/09/2019	23.9	25.2	34.8	21.7	24.0	21.9	16.9	16.9
12/09/2019	46.8	53.9	29.5	45.1	48.4	65.4	37.5	37.5
13/09/2019	53.3	64.1	39.5	53.8	46.8	57.6	39.5	39.5
14/09/2019	27.4	32.3	22.1	30.1	28.0	31.3	20.5	20.5
15/09/2019	19.7	31.7	12.3	21.7	23.0	25.4	18.1	18.1
16/09/2019	53.9	56.5	30.1	50.2	54.6	63.4	43.1	43.1
17/09/2019	9.5	11.5	9.1	10.5	9.6	10.2	6.3	6.3
18/09/2019	4.0	7.2	9.0	7.3	7.5	7.3	3.5	3.5
19/09/2019	11.5	12.7	13.6	12.9	11.3	10.9	37.2	37.2
20/09/2019	6.7	11.3	12.0	10.0	10.8	10.1	7.1	7.1
21/09/2019	18.4	24.4	19.8	23.0	25.6	26.7	17.9	17.9
22/09/2019	31.0	37.5	29.5	33.3	44.2	47.1	24.4	24.4
23/09/2019	18.3	22.6	20.2	16.3	19.5	35.4	16.4	16.4
24/09/2019	23.0	28.9	21.6	25.3	28.6	29.7	17.1	17.1
25/09/2019	25.4	22.2	23.2	20.6	21.1	20.8	16.7	16.7
26/09/2019	Temporary Power Outage due to external electrical (Ausgrid) works	25.7	Temporary Power Outage due to external electrical (Ausgrid) works	23.2	20.8	23.0	20.8	20.8
27/09/2019	37.9	54.9	21.2	32.6	33.5	53.1	33.7	33.7
28/09/2019	33.8	60.6	24.1	45.7	45.5	54.2	25.4	25.4
29/09/2019	26.2	26.4	21.4	23.1	22.1	22.4	18.9	18.9
30/09/2019	24.3	22.8	23.7	17.6	17.2	16.4	17.5	17.5
1/10/2019	18.6	18.8	19.1	15.5	14.3	14.4	17.3	15.7
2/10/2019	26.5	29.3	19.5	22.3	27.7	28.6	18.7	22.5
3/10/2019	38.9	45.7	28.5	45.5	49.9	44.7	25.6	29.7
4/10/2019	47.9	63.6	43.6	63.9	71.7	90.4	50.9	34.5
5/10/2019	14.7	19.4	19.2	17.5	17.7	17.2	17.9	12.3
6/10/2019	20.8	26.7	21.8	21.8	26.2	27.6	16.1	16.7
7/10/2019	69.2	59.6	62.6	60.8	68.4	82.9	46.2	Inconsistent
8/10/2019	38.2	48.8	43.9	47.4	34.9	72.4	54.1	flow – Vacuum pump replaced
9/10/2019	19.3	28.8	19.0	23.0	15.4	24.8	22.0	14.7
10/10/2019	17.2	19.3	20.4	15.5	11.8	12.2	12.4	12.4
11/10/2019	12.6	15.8	17.4	9.5	6.2	6.4	12.8	8.6
12/10/2019	3.9	7.4	11.4	6.5	4.9	4.8	7.1	2.6
13/10/2019	9.5	11.1	12.9	9.1	7.3	8.3	8.5	7.2
14/10/2019	15.1	19.4	23.1	18.5	21.0	26.7	15.7	11.7
15/10/2019	30.0	25.0	38.9	21.3	18.1	20.0	18.3	21.1
16/10/2019	38.5	Replacement of monitoring unit	51.2	44.2	45.7	40.7	32.0	30.3
17/10/2019	38.1	65.1	53.5	43.5	55.3	94.1	88.4	37.2
18/10/2019	56.3	71.7	31.1	46.9	52.7	55.8	36.9	41.5
19/10/2019	62.3	60.4	43.5	56.6	58.8	78.2	43.3	46.9
20/10/2019	20.7	21.8	30.6	24.1	18.5	17.6	16.5	16.3
	19.2	21.4	29.2	17.7	15.7	18.9	15.5	15.3

22/10/2019	17.4	17.5	31.1	16.9	13.6	13.3	13.1	13.1
23/10/2019	33.2	36.1	Technical Issue - Circuit Breaker Malfunction	28.2	28.2	30.1	26.1	28.2
24/10/2019	54.3	59.7	Temporary Power Outage due to external electrical (Ausgrid) works	56.3	64.2	73.5	46.9	47.1
25/10/2019	61.6	59.0	36.5	55.6	79.4	65.8	64.2	49.3
26/10/2019	88.9	150.3	105.5	131.7	85.6	127.7	127.9	79.0
27/10/2019	58.1	50.4	57.6	64.6	59.1	71.5	34.0	45.2
28/10/2019	47.2	53.2	51.7	48.2	46.1	46.9	34.6	37.2
29/10/2019	44.9	46.1	48.4	Maintenance Performed	42.0	41.9	40.4	43.0
30/10/2019	87.7	100.6	85.2	46.1	97.8	103.1	78.8	69.7
31/10/2019	70.9	96.2	61.3	83.0	88.6	96.8	75.5	59.8
1/11/2019	63.7	72.5	94.1	67.8	73.9	71.7	65.0	61.7
2/11/2019	39.3	41.7	39.5	39.4	43.0	53.3	34.2	33.8
3/11/2019	52.0	68.5	37.2	43.6	58.0	98.8	71.2	42.3
4/11/2019	11.9	18.4	7.5	10.0	18.3	19.5	24.5	11.8
5/11/2019	9.4	12.5	10.8	11.4	10.9	14.0	13.6	9.0
6/11/2019	29.2	35.6	15.0	25.1	29.4	37.6	63.0	27.9
7/11/2019	85.5	125.4	88.6	89.7	106.5	154.2	214.0	78.5
8/11/2019	94.2	116.4	78.0	98.9	96.8	143.9	139.0	80.8
9/11/2019	26.0	32.5	35.1	42.4	28.8	62.4	38.6	23.1
10/11/2019	33.5	50.2	32.6	28.8	40.4	60.4	28.1	25.8
11/11/2019	21.2	34.9	25.5	24.2	22.3	31.1	24.8	17.9
12/11/2019	93.6	133.6	94.5	96.5	128.6	159.6	141.9	83.0
13/11/2019	38.3	55.3	53.4	48.0	54.4	65.1	51.3	34.0
14/11/2019	42.7	52.9	39.5	43.5	48.6	56.0	44.0	37.2
15/11/2019	69.9	69.3	33.9	56.8	63.9	111.8	100.2	56.0
16/11/2019	74.9	67.8	51.9	67.2	62.9	75.4	43.3	56.0
17/11/2019	55.2	67.6	54.0	58.8	57.7	56.3	55.3	53.0
18/11/2019	42.2	64.6	46.5	45.2	45.1	49.4	46.0	41.6
19/11/2019	53.6	62.3	45.2	49.0	47.3	66.2	61.2	44.7
20/11/2019	45.0	49.9	53.5	44.5		40.8	33.3	37.9
21/11/2019	91.4	107.9	98.3	102.3	I In: 4 a COlina Air	101.1	93.4	85.8
22/11/2019	107.1	135.8	106.3	128.5	Unit offline. Air Conditioner/	124.6	101.5	92.9
23/11/2019	48.1	52.5	67.4	49.0	Cooling fault in unit.	46.8	50.4	43.5
24/11/2019	17.7	20.4	22.5	19.4		19.3	22.4	17.4
25/11/2019	36.8	44.8	45.1	36.6		48.9	35.5	32.9
26/11/2019	201.1	242.9	220.6	190.6	175.4	211.4	158.5	156.3
27/11/2019	82.5	71.9	109.4	88.7	43.0	84.9	44.4	59.3
28/11/2019	67.4	66.1	Temporary Power Outage due to external electrical (Ausgrid) works	61.9	46.4	56.6	58.6	59.2

2019 Annual Review - Mt Owen/Glendell Operations - Appendices

29/11/2019	120.9	120.6	112.4	115.5	109.4	120.2	122.5	118.4
30/11/2019	93.3	119.7	71.3	88.7	52.9	86.7	70.6	67.9
1/12/2019	50.8	81.4	61.4	64.7	46.3	85.5	87.8	59.3
2/12/2019	91.7	186.4	108.0	111.3	77.9	158.6	151.5	83.8
3/12/2019	73.0	88.4	64.7	71.9	68.0	107.1	85.9	57.3
4/12/2019	53.6	86.8	54.3	45.5	54.3	105.3	77.1	45.2
5/12/2019	73.8	102.6	60.4	92.8	75.8	136.4	78.8	58.3
6/12/2019	84.5	128.9	98.7	120.9	83.7	178.1	129.9	66.2
7/12/2019	94.8	109.4	101.6	101.3	71.0	97.7	88.8	89.2
8/12/2019	51.9	47.2	48.4	39.1	18.5	36.1	36.4	47.4
9/12/2019	77.3	79.2	95.3	70.9	50.3	65.9	66.7	71.9
10/12/2019	102.6	114.1	Maintenance Performed	Maintenance Performed	82.2	105.9	98.8	94.4
11/12/2019	80.8	92.6	74.5	71.6	57.0	65.0	87.9	90.3
12/12/2019	39.2	42.2	49.2	38.0	23.4	36.0	35.6	39.8
13/12/2019	19.4	19.2	23.0	18.4	6.7	18.2	16.8	18.3
14/12/2019	56.1	71.5	52.9	57.6	44.2	57.3	52.0	56.3
15/12/2019	49.3	63.9	48.5	44.2	33.2	69.0	60.4	48.4
16/12/2019	66.7	78.9	74.2	67.8	67.2	101.4	51.6	56.9
17/12/2019	20.1	28.2	28.6	18.0	9.2	18.7	15.8	15.9
18/12/2019	30.5	30.0	36.0	20.2	9.2	19.7	16.6	22.6
19/12/2019	116.1	122.9	106.6	98.9	90.2	106.2	82.0	94.0
20/12/2019	40.0	51.3	44.9	35.7	26.1	36.5	33.1	35.2
21/12/2019	59.5	107.2	85.3	87.9	59.6	78.6	74.9	74.9
22/12/2019	40.2	45.8	42.6	43.5	24.1	52.4	33.8	35.8
23/12/2019	29.6	34.5	25.0	25.7	10.2	24.5	25.0	24.2
24/12/2019	25.3	40.7	20.6	18.5	Maintenance performed following receipt of Temperature and Humidity Alarms	17.8	17.2	19.3
25/12/2019	14.4	28.1	19.2	19.4	3.8	18.7	18.4	15.0
26/12/2019	16.7	25.9	22.6	24.3	7.3	21.1	19.1	18.1
27/12/2019	25.0	28.3	21.0	18.5	Negative Results Excluded	17.7	14.2	18.7
28/12/2019	38.5	52.7	44.4	37.1	Negative Results Excluded	36.8	41.6	35.0
29/12/2019	39.3	50.5	44.2	38.9	33.4	39.7	29.7	31.8
30/12/2019	57.5	72.2	72.0	62.8	60.4	68.3	47.6	46.8
31/12/2019	102.0	99.9	70.3	79.4	63.8	77.0	55.7	69.1
Note: Days	hiahliahted in hlue h	nave heen denoted	as 'extraordinary e	vents' as advised h	v DPIF As advised	hy DPIF days white	h are identified as	

Note: Days highlighted in blue have been denoted as 'extraordinary events' as advised by DPIE. As advised by DPIE, days which are identified as 'extraordinary events' are not included in Long term impact assessment criteria.

^{*} Units used for management purposes as located on Mine Owned land and not representative of nearby neighbours.

Table 34: 2015 to 2019 Depositional Dust Air Quality Monitoring Results (g/m2/month)

Dust Gauge Code	2015 Annual Average (g/m2/month)	2016 Annual Average (g/m2/month)	2017 Annual Average (g/m2/month)	2018 Annual Average (g/ m2/month)	2019 Annual Average (g/m2/month)
DD6	0.9	1.0	0.9	0.9	1.5
DD7	2.0	2.3	2.5	2.6	2.9
DD12	2.4	4.3	2.7	1.0	3.3
DD14	1.4	2.6	1.8	2.5	1.7
DD16	2.3	1.8	4.0	2.8	3.5
DG3	1.3	3.3	1.7	1.4	1.9
DG4	1.9	1.6	2.4	2.5	3
DG5	1.5	1.8	2.5	2.3	3.1
DG6	2.8	1.6	2.0	1.9	2.4
DG7	2.1	2.0	2.2	2.6	2.7
DG8	2.6	4.0	2.7	3.6	4.7*

*Refer to Jacobs - Review of 2019 Dust Deposition Data (IA005400) at the end of this appendix.

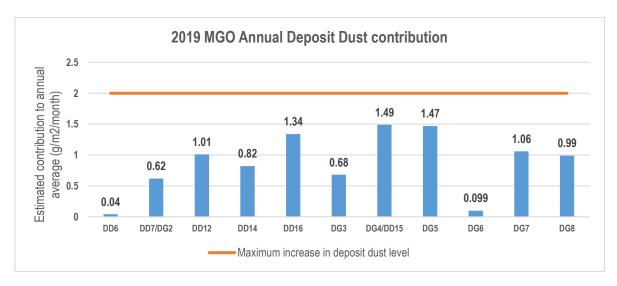


Figure 3 MGO Estimated Deposit Dust contribution to annual average

Table 35: 2015 to 2019 Continuous PM10 Monitoring Comparison

Year	Sx13D8 (Pictons In)	Sx13D1 (Project Office	Sx13D11 (Middle Falbrook)	Sx13D9 (Nobles In)	Sx13D4 (McInerney)	Criterion
		Maximu	m 24-hour average i	n μg/m³		
2015	70	71	61	74	64	
2016	51	56	61	76	54	
2017	111	63	86	66	79	
2018	168	144	163	166	210	50
2019	220.6	201	175	191	243	
2019 (exlcuding extraordinary events)	60	70	77	64	69	
		Number of da	ys above 24-hour av	erage criteria		
2015	7	6	2	4	3	
2016	1	2	1	2	5	
2017	28	6	17	4	20	
2018	15	13	27	11	34	N/A
2019	49	58	62	55	81	
2019 (exlcuding extraoridnary events)	7	11	22	14	28	
		An	nual average in µg/n	n ^{3b}		
2015	20	18	14	18	20	
2016	19	20	14	18	23	
2017	24	20	23	19	24	
2018	23	23	25	22	29	30**
2019*	22	23	27	23	28	
2019 (1 January 2019 – 3 September 2019 (SSD-5850)*	21	22	26	22	26	
4 September 2019 - 31 December 2019 (SSD-5850)*	26	27	28	27	33	25**

Note: Days have been denoted as 'extraordinary events' as advised by DPIE. As advised by DPIE, days which are identified as 'extraordinary events' are not included in Long term impact assessment criteria.

^{**} MOCO Mod 2 (SSD-5850) approved during September 2019. Long Term average criterion revised from 30 μg/m³ to 25 μg/m³ as part of modification. Long term average calculations for this report are based upon advice received from DPIE. Averages for the two periods (i.e. 1 January 2019 – 3 September 2019 and 4 September 2019 – 31 December 2019) do not represent an 'annual' average for comparison to assessment criteria. Therefore statistics provided for these periods have been presented for information purposes only and not for detrmining compliance.

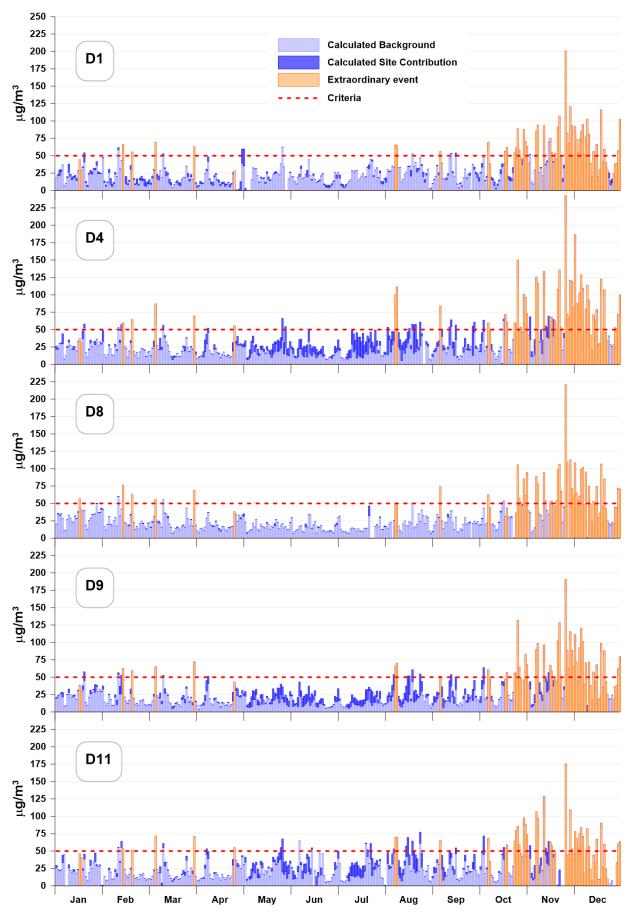


Figure 4 Measured 24-hour average PM₁₀ summary 2019.

2019 Annual Review – Mt Owen/Glendell Operations - Appendices

Table 36: 2015 to 2019 HVAS TSP Comparison

HVAS Site	Location	2015 Annual Average (µg/m³)	2016 Annual Average (µg/m³)	2017 Annual Average (µg/m³)	2018 Annual Average (µg/m³)	2019 Annual Average (µg/m³)
TSP 1	Picton	54.8	52.5	60	59.0	60
TSP 2	Falbrook Road	60.8	76.4	73	78.0	76
TSP 3	Camberwell Church	56.7	62.4	68	80.4	79

	*
-	C
	-
	1

Incident and Investigation Report

1,				Committee of the second second					
SECTION 1: INCIDEN	T REPOR	T		Incident Number: IF	R-084				
	rs on clie	plete this sect nt's site, comp submit a copy	olete client's s	ite specific report/in	vestigations				
Date & Time of Incident:	Date: 9/9/	/19		Time: Approx. 3pm					
Site/Location of Incident:	Mt Owen/	Glendell TSP2 (f	Mid Falbrook)						
Name of Employee/s involved:	Alex Smit	lex Smith, Michael Tracey							
Type of Incident:	□Injury	□Near Miss	□Equipment	Damage ☑ Quality	□Other				
Describe the Incident: Include location of incident, sequence of events, contributing factors, witnesses, description of injury etc.	On lookin within a 5 the filter b	paper was still in g around he not 00m radius of the pag) (see Photo 2	the cassette. ticed multiple pie sampler (which 2).	oler on 9/9/19, Alex notic eces of the filter paper in he subsequently collect and the result for the TSF	on the ground ted and put in				
For Injuries Only:	Part of B	Injury / Illness type: N/A Part of Body: N/A First Aid Treatment Provided: N/A □ Return to Normal Duties □ Referred to doctor/hospital/medical treatment							
	Reported	to MGO task cod		Pereira) and CBE Project					
What immediate	(Renae Mikka).								
action was taken?									
Is there any Change of Management or Corrective Action required?				agement (Corrective Act o WHS Manager with thi					
Has the Incident been reported to the client?	☑Yes	□No □N/A	If NO, please	inform client immediately	/ !				
What was the actual or potential incident severity?	Investiga	forward to WHS		v (16-25) npletion of SECTION 2 : the Risk Assessment Wo					
Name of employee filing report:	Renae Mi	kka							
Signature of Employee:	RA	Am		Date: 9/9/19					

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Investigation Form
Inh 2016

Authorized By:_____

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Incident and Inves	tigation	Report	
SECTION 2: INCIDENT INVESTIGATION			
Investigator/Position: Renae Mikka (Projects Manager)	Date Incid	ent Report Re	ceived: 9/9/19
DRE Notification Report completed and sent? (confirm	m with mine s	ite owner): N/	A
Detailed Description of incident: (attach photos, drawing etc)			
On unlocking and opening the TSP2 sampler on 9/9/19, the casette.	Alex noticed or	nly part of the t	filter paper was still in
On looking around he noticed multiple pieces of the fil subsequently collected and put in the filter bag) (see Photos		he ground wit	hin a 50m radius he
This damage to the filter paper invalidated the result for the	ne TSP on 5/9/	19.	
Identify witnesses and obtain their version of events			
Name/s of Witness	Contact	ed?	Date
Ryan Foggett (installed filter paper on 4/9/19)	✓Yes	□No	11/9/19
Alex Smith (collected filter paper on 9/9/19)	✓Yes	□No	11/9/19
Michael Tracey (collected filter paper on 9/9/19)	✓Yes	□No	11/9/19
	□Yes	□No	
	□Yes	□No	
How exactly did the injury, accident or incident happe	en?		
Two theories have been suggested by field staff involv cassette and escaping through the inlet, the other is interference.			
Ryan confirmed that the cassette was in place and the Michael confirmed that the door was locked on arrival at filter paper was missing) and didn't notice any obvious door and inlet). Accordingly, it is not considered likely that this instance. However, we have seen numerous instance (from switching the power off to physical removal of the model.	nd cassette in signs of tampe t the monitor w ces of interfere	place on 9/9/1 ring to the sa ras interfered v	9 (though majority of mpler (including lock, vith by a third party in
Regarding the first option of the paper coming loose fro evidence of filter papers moving in the cassette, and completely flat, but never coming loose from the cass although it was not significantly worn, it has been replace	sometimes li ette altogether	fting in the m	iddle if not installed e was inspected and
It was also identified that the muffler was missing its of 13/9/19 (see Photo 4). Although we don't have any evided plausible that this, paired with the strong gusty W-NW wirthrough the sampler which pushed the filter paper free from	nce of this hap	pening elsewh September all	ere, we consider it owed air flow back

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able to break apart into smaller pieces (the filter material is quite fragile), which were then able to escape from the inlet. The other factor that leads us to believe the damage occurred between the 6/9/19 and 9/9/19 is that on the run day, the volume of air running through the filter paper would act to hold the filter in place, as evident on Photo 2, the filter paper looks like a typical filter that has successfully completed a run. Reconstruct the sequence of events that lead to the undesired event. As above. 1. 7. 2. 5. 8. 3. 6. 9. List any contributing factors: Wear and tear of the cassette and rubber over time leading to insufficient grip of filter paper. Strong W-NW winds on 6th & 7th September (gusts recorded up to 80km/h). Broken muffler flap allowing air flow back through sampler. Additional actions 1. Replace cassette - completed 13/9/19 from investigation: 2. Replace muffler - completed 20/9/19 3. Conduct make up run for sample run on 5/9/19 - completed 13/9/19 Note: Complete a 4. Inspect TSP1 (Picton) to ensure cassette & muffler are compliant - to be Change Management completed 24/9/19 (Corrective Action 5. Request - CAR) Form (F413) for additional 6. actions. 8. 9. Estimated cost of incident: \$ N/A Estimated cost of actions: \$ N/A WHS or Operations Manager Comments: Feedback given to N/A Employee: Signature of Employee: N/A Date: N/A Signature of Investigator: Completion Date: 20/9/19 RAMO

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Photo 1: Location of TSP2 (on left).



Photo 2: Recovered pieces of filter paper.



Photo 3: Filter paper casette.

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Photo 4: TSP2 (note missing flap on muffler on left of side of sampler).



Photo 5: TSP2 with inlet open showing placement of filter cassette and inside of inlet.

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Change Management Form (Corrective Action Request – CAR)

SECTION 1 - C	larify Ch	ange Required							
Source of Prob	lem or S	uggested Change/In	nproveme	ent					
☐ Hazard ☐	☐ Incident	: 🔲 Injury	□Envi	ronment 🗆 Custome	r complaint				
☐ Supplier issi	ue 🗆	Potential issue 🔲	Improvem	ent Process r	eview Q Quality				
Completed by: F	≀enae Mikk	а	Signed	RAME	Date: 20/9/19				
2006	HVAS filt	er paper appears to ha	ve come lo	ose from cassette, invalida	ting sampling result				
Brief Description of	(see IR-0	184).							
Problem									
	Mara III.a				:h111h1				
Cause of			r and/or mis	ssing muffler flap (and conti	ibuted to by strong and				
Problem	gusty wir	nd conditions).							
		26							
		ed - To prevent the problem ation and date required.	recurring or e	ensure change is permanent —Inc	ude each action/control,				
Action				By Who	By When				
Replace filter pap	er cassette			Coordinated by R.Mikka	Completed 13 <i>/</i> 9/19				
Replace muffler				Coordinated by R.Mikka	Completed 20 <i>/</i> 9/19				
Contract the contract of the c	with the state of	ΓSP2 run on 5 <i>1</i> 9/19		Coordinated by R.Mikka	Completed 13/9/19				
Inspect TSP1 (Pid compliant	cton) to en	sure cassette & muffler	are	Coordinated by R.Mikka	24/9/19				
Changes commi	unicated to	relevant persons:		economic con anti-adequate a	()				
	560-540 Accordance	· · · · · · · · · · · · · · · · · · ·	Øγ	YES N/A					
CAR Number As	signed: C	AR-124	Non	Nominated Follow Up Date: 18/10/19					
SECTION 2 - F	ollow up	and Close Out							
Comments on Fo	-	ally Diose Out							
Up / Close Out confirm corrective active effective	То								
	ļ								
CAR Register Up	dated:	☐ Yes – CAR Regist	er must be	e updated					
Completed by:	8		Signed		Date:				

F413 – Change Management (CAR) Form Version 5 Revised: 16 April 2019





Level 4, 12 Stewart Avenue Newcastle West NSW 2302 Australia PO Box 2147 Dangar NSW 2309 Australia T +61 2 4979 2600 F +61 2 4979 2666 www.jacobs.com

28 January 2020

Attention: Mike Pereira Environment and Community Officer Mt Owen / Glendell Operations, Glencore

Project Name: 2019 Mt Owen Complex Annual Review

Project Number: IA005400

Dear Mike,

Review of 2019 Dust Deposition Data

I have completed a review of Mt Owen's dust deposition data for 2019. Please see attached for the outcomes of the analyses.

In summary, it has been concluded that Mt Owen was in compliance with its development consents in terms of total and incremental dust deposition impacts at all monitoring sites for data collected in 2019.

Yours sincerely

Shane Lakmaker Principal (Air Quality) (02) 4979 2663 shane.lakmaker@jacobs.com

Jacobs Group (Australia) Pty Limited ABN 37 001 024 095 Final



28 January 2020

1. Background

Mt Owen Pt Ltd (Mt Owen) has a network of air quality and meteorological monitoring equipment around the Mt Owen Complex which is designed to meet relevant conditions under the development consents for Glendell Mine (DA 80/952) and Mt Owen Mine (SSD-5850).

Figure 1 shows the meteorological and air quality monitoring network. This network includes:

- Three (3) meteorological stations
- Three (3) high volume air samplers (HVAS) measuring TSP
- Six (6) tapered element oscillating microbalances (TEOM) measuring PM₁₀
- Two (2) EBAM units measuring PM₁₀
- Eleven (11) dust deposition gauges

A review of the dust deposition data that were collected in 2019 has been carried out. The main purpose of the review was to identify the likely factors for any elevated results, including estimating contributions from the Mt Owen Complex, and to determine whether Mt Owen had complied with the criteria specified in the development consents (DA 80/952 and SSD-5850). Table 1 shows the relevant development consent criteria.

Table 1 Development consent criteria

Substance	Averaging time	^d Impact assessment criteria from Glendell Consent (DA 80/952)	^d Impact assessment criteria from Mount Owen Consent (SSD-5850)
(D : 11 -	Annual (maximum increase)	^b 2 g/m ² /month	^b 2 g/m ² /month
^c Deposited dust	Annual (maximum total)	^a 4 g/m ² /month	^a 4 g/m ² /month

^aTotal impact (i.e. incremental increase in concentrations due to the development plus background concentrations due to all other sources).

b Incremental impact (i.e. incremental increase in concentrations due to the development on its own).

^c Deposited dust is to be assessed as insoluble solids as defined by Standards Australia, AS/NZS 3580.10.1:2003: Methods for Sampling and Analysis of Ambient Air - Determination of Particulate Matter - Deposited Matter - Gravimetric Method.

^d Excludes extraordinary events such as bushfires, prescribed burning, dust storms, fire incidents or any other activity agreed to by the Secretary.



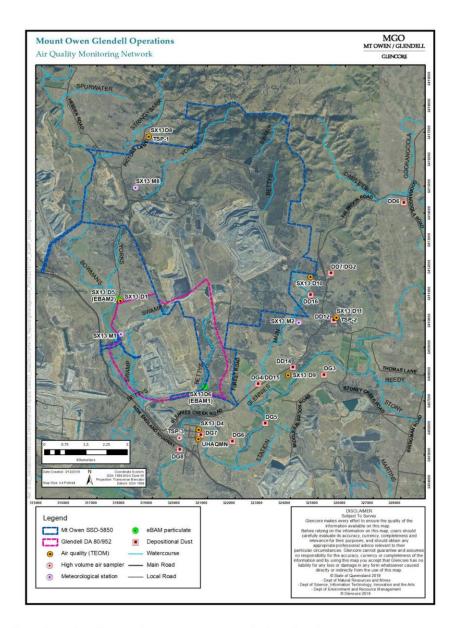


Figure 1 Location of monitoring stations around the Mt Owen Complex



2. Approach to Review

The monitoring data review involved:

- Obtaining monthly dust deposition data from all monitoring sites for 2019 and calculating annual averages.
- Obtaining hourly meteorological data from the Mt Owen Complex weather stations for 2019 and calculating the frequency of winds towards each dust monitor to determine potential maximum contributions from the Mt Owen Complex to each dust deposition result.
- Summarising of all monitored dust deposition data, likely factors for elevated results and estimated contributions from the Mt Owen Complex.

In accordance with AS 5380.10-1, there is only one measurement of dust deposition each month, from each monitor. Consequently, it is not possible to determine whether a monthly measurement was being influenced by a single source over a few days, multiple sources over the entire month, or some other combination. This complicates the process for isolating and determining contributions from a source of interest, such as the Mt Owen Complex. In addition, there is no standard prescribed methodology for determining site contributions to air quality for mining operations, so an estimation technique had to be adopted.

The contribution of the Mount Owen Complex mining activities to each measured result was calculated by first determining the wind direction ranges which represent a wind direction from the operation towards each monitor. Table 2 shows the wind direction ranges that represented the direction to the Mt Owen Complex from each monitor.

Table 2 Wind directions to Mt Owen Complex mining activities

Monitoring site	Directions to Mt Owen Complex
DD6	Between 230 and 280 degrees from true north
DD7/DG2	Between 230 and 320 degrees from true north
DD12	Between 240 and 330 degrees from true north
DD14	Between 250 and 360 degrees from true north
DD16	Between 230 and 340 degrees from true north
DG3	Between 260 and 340 degrees from true north
DD15/DG4	Between 260 and 10 degrees from true north
DG5	Between 280 and 10 degrees from true north
DG6	Between 300 and 30 degrees from true north
DG7	Between 310 and 40 degrees from true north
DG8	Between 330 and 40 degrees from true north

The potential site contribution to each monitor was then calculated by multiplying the annual average dust deposition by the percentage of time that winds were in the direction of that monitor. This calculation assumes that the Mt Owen Complex was contributing to the measurements at all times when the wind was in the direction of the monitor, which may not necessarily be the case.



3. Monitored Results

Table 3 shows the measured monthly dust deposition results from each monitor for data collected in 2019. Annual averages have been calculated for comparison with the development consent criteria. The annual average data presented in Table 3 excluded monthly results marked as contaminated ('C') by the monitoring contractor but did not exclude periods of extraordinary events such as bushfires, prescribed burning, dust storms, fire incidents or any other activity agreed to by the Secretary, as per the provisions of the development consents.

Table 3 Measured dust deposition from Mt Owen Complex monitors in 2019

						g/m²/	month					
Month	DDe	DD7/DG2	DD12	DD14	DD16	DG3	DD15/DG4	DG5	950	DG7	DG8	Criterion
Jan	2.7	2.9	2.8	С	1.8	1.2	2.0	3.8	3.2	3.9	2.3	-
Feb	1.6	2.9	С	С	3.2	4.5	2.6	3.9	С	С	6.2	-
Mar	1.8	2.5	1.1	С	0.9	0.9	4.3	С	2.4	2.4	С	-
Apr	1.1	2.8	2.3	1.6	2.4	1.8	С	3.1	2.3	2.4	9.0	-
May	1.0	2.5	2.3	1.8	3.2	0.3	2.2	3.2	1.5	С	3.2	-
Jun	1.2	3.1	3.9	1.8	5.3	1.8	С	2.9	2.3	3.7	7.9	-
Jul	1.0	3.1	3.9	1.6	С	С	3.0	3.4	2.4	3.8	5.3	
Aug	0.9	2.9	4.8	1.7	5.1	1.6	2.2	3.6	2.3	2.1	2.9	-
Sep	2.0	2.3	5.1	2.0	6.1	2.0	5.1	2.6	2.0	2.3	3.2	-
Oct	0.6	2.6	2.8	1.4	С	1.8	3.3	2.1	С	1.6	2.4	
Nov	2.2	3.7	С	1.6	3.5	2.4	2.5	4.0	2.0	2.8	3.7	
Dec	1.5	3.3	4.4	С	3.8	2.3	3.0	1.4	2.0	2.4	5.6	
Annual average	1.5	2.9	3.3	1.7	3.5	1.9	3.0	3.1	2.2	2.7	4.7	4

The annual average dust deposition results from Table 3 were below 4 g/m²/month at all monitoring sites except at DG8 where the annual average result was 4.7 g/m²/month. DG8 is located southwest of Camberwell Village, on the south side of the New England Highway. Further investigation of this result has therefore been carried out.

Table 4 shows the calculated site contributions to each monitor, including DG8, as per the methodology described in Section 2. The calculations show that the Mt Owen Complex was estimated to have contributed up to $1.0~{\rm g/m^2/month}$ to the measured 4.7 ${\rm g/m^2/month}$ at DG8. This result demonstrates compliance with the "incremental impact" criteria from the development consent (that is, $2~{\rm g/m^2/month}$).

In addition, the data do not indicate that the Mt Owen Complex was the cause of an exceedance of the "total impact" criteria (4 $g/m^2/month$) at DG8. This is because the calculated contribution to DG8 (1.0 $g/m^2/month$) was within the range of contributions calculated for other monitoring sites, so the result is not unique. It is also useful to make comparisons to the results at other



locations to assist with determining possible causes of elevated results. For example, DG7 is located closer to the Glendell Mine than DG8 and experienced a higher proportion of winds from Glendell Mine towards the monitor, however the dust deposition at DG7 was lower than at DG8. This suggests that there were local sources of dust near DG8 that contributed to the measured result.

Table 4 Estimated contributions of Mt Owen Complex to measured dust deposition

Parameter	9DQ	DD7/DG2	DD12	DD14	DD16	DG3	DD15/DG4	DG5	DG6	DG7	DG8	Criterion
Lower bound of wind from MOC to monitor (degrees)	230	230	240	250	230	260	260	280	300	310	330	-
Upper bound of wind from MOC to monitor (degrees)	280	320	330	360	340	340	10	10	30	40	40	(*)
Percentage of time that wind was from MOC towards monitor (%)	3	21	30	48	38	36	49	48	44	39	21	S=
Annual average dust deposition (g/m²/month)	1.5	2.9	3.3	1.7	3.5	1.9	3.0	3.1	2.2	2.7	4.7	4
Estimated MOC contribution to annual average (g/m²/month)	0.04	0.62	1.01	0.82	1.34	0.68	1.49	1.47	0.99	1.06	0.99	2

Finally, late 2019 coincided with a period of unprecedented bushfires in Australia, predominantly across southeast Australia, but also affecting a reported 5.2 million hectares of land in NSW since early November 2019. Additional detail can be found at:

https://en.m.wikipedia.org/wiki/2019%E2%80%9320 Australian bushfire season

These bushfire events adversely affected air quality across large parts of NSW including the Upper and Lower Hunter Valley. The adverse air quality conditions were evident from monitoring data collected by the Department of Planning, Industry and Environment (DPIE). Figure 2 shows the measured PM_{10} concentrations at the Singleton, Muswellbrook and Newcastle monitoring stations in 2019. These data clearly show the increased PM_{10} concentrations in November and December and, based on the documented bushfire activity and bushfire locations, it would not be unreasonable to classify most days in these two months as related to extraordinary events in the Hunter Valley.

Jacobs. 28 January 2020

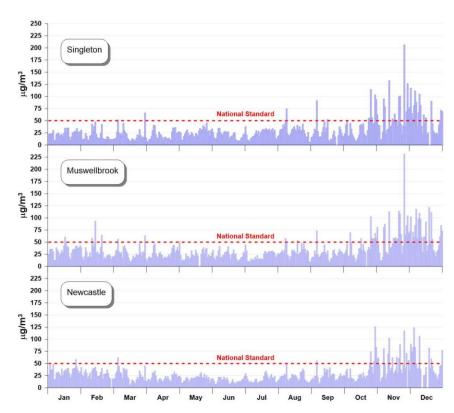


Figure 2 Measured 24-hour average PM_{10} concentrations in the Hunter Valley in 2019

4. Conclusion

Based on the analysis and estimated site contributions it has been concluded that Mt Owen was in compliance with its development consents in terms of total and incremental dust deposition impacts at all monitoring sites for data collected in 2019.



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3 March 2020

Attention: Mike Pereira **Environment and Community Officer** Mt Owen / Glendell Operations, Glencore

Project Name: 2019 Mt Owen Glendell Operations Annual Review

Project Number: IA005400

Dear Mike,

Review of 2019 Annual Average PM10 and TSP Data

I have completed a review of Mt Owen's annual average PM₁₀ and TSP data for 2019. Please see attached for the outcomes of the analyses.

In summary, it has been concluded that Mt Owen Glendell Operations was in compliance with its development consents in terms of total PM₁₀ and TSP impacts at all monitoring sites for data collected in 2019.

Yours sincerely

Shane Lakmaker Principal (Air Quality) (02) 4979 2663

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Jacobs Group (Australia) Pty Limited ABN 37 001 024 095



Background

Mt Owen Pt Ltd (Mt Owen) has a network of air quality and meteorological monitoring equipment around the Mt Owen Glendell Operations (MGO) which is designed to meet relevant conditions under the development consents for Glendell Mine (DA 80/952) and Mt Owen Mine (SSD-5850).

Figure 1 shows the meteorological and air quality monitoring network. This network includes:

- Three (3) meteorological stations.
- Six (6) tapered element oscillating microbalances (TEOM) measuring PM₁₀. Compliance is determined at SX13 D1, SX13 D4, SX13 D8, SX13 D9 and SX13 D11.
- Two (2) EBAM units measuring PM₁₀. Data from these units are used for operations management.
- Three (3) high volume air samplers (HVAS) measuring TSP. Compliance is determined at TSP 1 and TSP 2.
- Eleven (11) dust deposition gauges.

A review of the annual average PM_{10} and TSP data that were collected in 2019 has been carried out. The main purpose of the review was to estimate contributions from MGO, and to determine whether Mt Owen had complied with the criteria specified in the development consents (DA 80/952 and SSD-5850). Table 1 shows the relevant development consent criteria. The annual average PM_{10} criterion was revised from 30 $\mu g/m^3$ to 25 $\mu g/m^3$ on 4 September 2019 as part of SSD-5850 Modification 2.

Table 1 Development consent criteria

Substance	Averaging time	^d Impact assessment criteria from Glendell Consent (DA 80/952)	^d Impact assessment criteria from Mount Owen Consent (SSD- 5850) up to 4 Sep 2019	dImpact assessment criteria from Mount Owen Consent (SSD- 5850 Mod 2) from 4 Sep 2019
Particulate matter (PM ₁₀)	Annual	³30 μg/m³	^a 30 μg/m ³	^a 25 μg/m ³
Particulate matter (TSP)	Annual	⁴90 μg/m³	^a 90 μg/m ³	^a 90 μg/m ³

^a Total impact (i.e. incremental increase in concentrations due to the development plus background concentrations due to all other sources).

It is understood that Mt Owen reports compliance against their 24-hour average PM_{10} criteria via a separate process established with the Department of Planning, Industry and Environment (DPIE).

^b Incremental impact (i.e. incremental increase in concentrations due to the development on its own).

Deposited dust is to be assessed as insoluble solids as defined by Standards Australia, AS/NZS 3580.10.1:2003: Methods for Sampling and Analysis of Ambient Air - Determination of Particulate Matter - Deposited Matter - Gravimetric Method.

^dExcludes extraordinary events such as bushfires, prescribed burning, dust storms, fire incidents or any other activity agreed to by the Secretary.



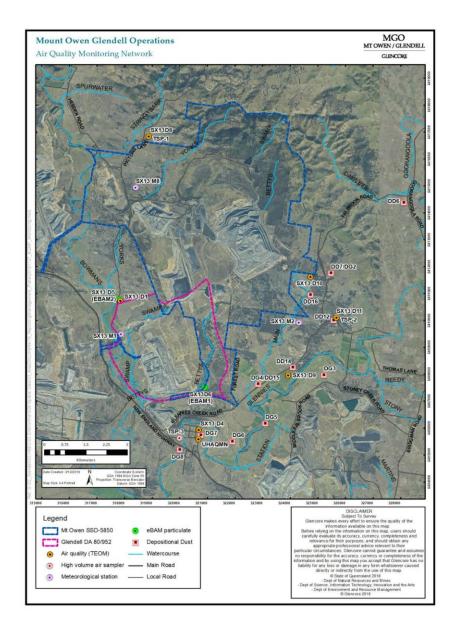


Figure 1 Location of monitoring stations around the MGO



2. Approach to Review

2.1 Extraordinary Events

Late 2019 coincided with a period of unprecedented bushfires in Australia, predominantly across southeast Australia, but also affecting a reported 4 million hectares of land in NSW since early November 2019. Additional detail can be found at:

https://www.environment.nsw.gov.au/topics/air/air-quality-statement

The bushfires adversely affected air quality across many parts of NSW and a total of 66 days in 2019 were subsequently declared as extraordinary events, based on advice from Mt Owen who had been in consultation with the DPIE. Table 2 identifies the days that have been declared as extraordinary events.

Table 2 Days declared as extraordinary events in 2019

Month	Day(s)
Jan	16, 17
Feb	13, 19
Mar	6, 31
Apr	26
May	-
Jun	-
Jul	e .
Aug	8, 9
Sep	6
Oct	7, 8, 18, 19, 24, 25, 26, 27, 28, 30, 31
Nov	1, 2, 7, 8, 12, 16, 17, 19, 20, 21, 22, 23, 26, 27, 28, 29, 30
Dec	1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15, 16, 17, 18, 19, 20, 21, 22, 23, 27, 28, 29, 30, 31

The reporting of Mt Owen's PM_{10} and TSP air quality monitoring data has excluded records from the days listed as extraordinary in Table 2 above, as per the provisions of the development consents.

2.2 Annual average PM₁₀

The analysis of PM_{10} data involved:

- Obtaining hourly average PM₁₀ concentration data from all monitoring sites for 2019 and calculating annual averages.
- Obtaining hourly meteorological data from MGO weather stations for 2019 and calculating the contributions from MGO to each hourly PM₁₀ concentration result.
- Summarising of all monitored PM₁₀ concentration data and estimated annual contributions from MGO.



There is no standard prescribed methodology for determining site contributions to air quality for mining operations. The methodology described below is based on the use of concurrent hourly meteorological and air quality monitoring data from suitably located monitoring stations around the mine site to estimate site contributions. This method is referred to as an upwind / downwind calculation approach.

The contribution of MGO mining activities to the measured results was calculated by first determining the wind direction ranges which represent a wind direction from the operation towards each monitor. Table 5 shows the wind direction ranges that represented the direction to MGO from each monitor. Calculations of contributions from both Glendell mine and Mt Owen mine had been considered however it was determined that there are some wind directions for which the individual contributions could not be calculated due to overlap in the wind direction ranges to some monitors.

Table 3 Wind directions to MGO mining activities

Monitoring site	Directions to MGO					
SX13 D1	Between 10 and 170 degrees from true north					
SX13 D4	Between 310 and 40 degrees from true north					
SX13 D8	Between 30 and 110 degrees from true north					
SX13 D9	Between 250 and 360 degrees from true north					
SX13 D11	Between 240 and 330 degrees from true north					

The site contribution to each monitor was calculated for every 1-hour average record for every day based on the concurrent wind direction and from a downwind concentration minus upwind concentration calculation. Table 4 shows the data representing upwind and downwind conditions for each monitoring site. The downwind minus upwind result was only calculated downwind for hours with wind speeds greater than 0 m/s.

Table 4 Data for upwind and downwind calculations

Monitoring site	Data representing conditions upwind	Data representing conditions downwind		
SX13 D1	SX13 D11	SX13 D1		
SX13 D4	SX13 D8	SX13 D4		
SX13 D8	SX13 D9	SX13 D8		
SX13 D9	SX13 D8	SX13 D9		
SX13 D11	SX13 D8	SX13 D11		

The site contribution to each monitor was then calculated as an annual average (not including negative values) from the 8,760 hourly records.

2.3 Annual average TSP

The analysis of TSP data involved:

 Obtaining six day records of TSP concentration data from all monitoring sites for 2019 and calculating annual averages.



- Obtaining hourly meteorological data from MGO weather stations for 2019 and calculating the frequency of winds towards each monitor to determine potential maximum contributions from MGO to each TSP concentration result.
- Summarising of all monitored TSP concentration data and estimated contributions from MGO

In accordance with AS 3580.9.10, there is only one measurement of TSP concentration every six days, from each monitor. Consequently, it is not possible to determine whether a daily average was being influenced by a single source over a few hours, multiple sources over the entire day, or some other combination. This complicates the process for isolating and determining contributions from a source of interest, such as MGO. In addition, there is no standard prescribed methodology for determining site contributions to air quality for mining operations, so an estimation technique had to be adopted.

The contribution of MGO mining activities to each measured result was calculated by first determining the wind direction ranges which represent a wind direction from the operation towards each monitor. Table 5 shows the wind direction ranges that represented the direction to MGO from each monitor.

Table 5 Wind directions to MGO mining activities

Monitoring site	Directions to MGO
TSP 1	Between 30 and 110 degrees from true north
TSP 2	Between 240 and 330 degrees from true north
TSP 3	Between 330 and 40 degrees from true north

The potential site contribution to each monitor was then calculated by multiplying the annual average TSP concentration by the percentage of time that winds were in the direction of that monitor. This calculation assumes that MGO was contributing to the measurements at all times when the wind was in the direction of the monitor, which may not necessarily be the case.



3. Monitored Results

3.1 Extraordinary Events

The bushfire events in late 2019 adversely affected air quality across large parts of NSW including the Upper and Lower Hunter Valley. The adverse air quality conditions were evident from monitoring data collected by the DPIE. Figure 2 shows the measured PM_{10} concentrations at the Singleton, Muswellbrook and Newcastle monitoring stations in 2019. These data clearly showed the increased PM_{10} concentrations in November and December and, as noted in Section 2.1, there were a total of 66 days declared as extraordinary events in the Hunter Valley.

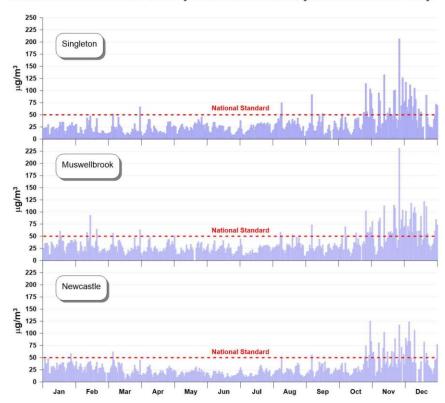


Figure 2 Measured 24-hour average PM₁₀ concentrations in the Hunter Valley in 2019



3.2 Annual average PM₁₀

Table 8 shows the measured annual average PM_{10} concentrations from each monitor for data collected in 2019. As noted in the development consents (DA 80/952 and SSD-5850), and reproduced in Table 1, determination of compliance against the impact assessment criteria is to exclude "extraordinary events such as bushfires, prescribed burning, dust storms, fire incidents or any other activity agreed to by the Secretary". Therefore the annual averages have been calculated without extraordinary events. This means that the annual averages have been based on one year of records but only represents 82% of one year; that is, below the minimum 90% data capture rate that is required for applications of air quality data analysis (see for example EPA 2016 and US EPA 2000). However this data capture outcome could not have been avoided. The data in Table 8 show that, without extraordinary events, the PM_{10} concentrations at all five monitors (bold text) were below 30 μ g/m³. Consequently the monitoring demonstrates compliance with DA 80/952 and SSD-5850 in terms of annual average particulate matter as PM_{10} .

As noted in Section 1 the annual average PM_{10} criterion in SSD-5850 was revised from 30 $\mu g/m^3$ to 25 $\mu g/m^3$ on 4 September 2019 as part of SSD-5850 Modification 2. The PM_{10} data have therefore been presented as averages for the 1 January to 3 September and 4 September to 31 December periods, excluding extraordinary events. The statistics represent even lower data capture rates (65% and 17% of one year respectively) so have been presented for information only, and not for determining compliance. Determination of compliance against the revised criterion (25 $\mu g/m^3$) will need to be carried out once a full year of data is available.

Table 6 Measured PM₁₀ concentrations from MGO monitors in 2019

Year	SX13 D1	SX13 D4	SX13 D8	SX13 D9	SX13 D11	Criterion
Annual average in µg/m³						
2019 (all data)	31	37	30	31	32	NA
2019 (without extraordinary events)	23	28	22	23	26	30
2019 (1 Jan to 3 Sep) (without extraordinary events) 237 days, 65% of one year	22	26	21	22	26	30
2019 (4 Sep to 31 Dec) (without extraordinary events) 62 days, 17% of one year	27	33	26	27	28	25

Table 7 shows the calculated site contributions to each monitor as per the methodology described in Section 2.

Table 7 Estimated contributions of MGO to measured PM_{10} concentrations

Parameter	SX13 D1	SX13 D4	SX13 D8	SX13 D9	SX13 D11	Criterion
Annual average PM ₁₀ concentration (μg/m³)	23	28	22	23	26	30
Estimated MOC contribution to annual average PM ₁₀ (µg/m³)	1	5	0	3	4	NA



3 March 2020

The calculations from Table 7 show that, of all sites, the MGO was estimated to have contributed up to 5 μ g/m³; at SX13 D4. The basis for the calculated site contributions can be seen from Figure 3. This figure shows the measured 24-hour average PM₁₀ concentration from each monitoring site, broken down into calculated background and calculated site contributions for each day of the year. The calculated higher site contributions at SX13 D4 can be seen to occur in the winter months when winds from the northwest are more common. As noted in Section 1 Mt Owen reports compliance against their 24-hour average PM₁₀ criteria via a separate process established with the DPIE so these results are not discussed further.

Jacobs. 3 March 2020

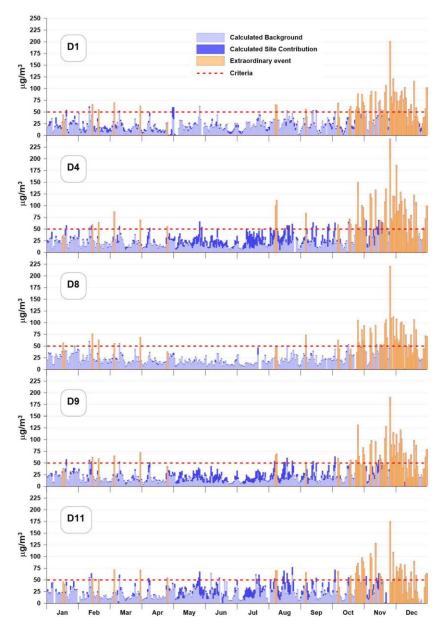


Figure 3 Measured 24-hour average PM_{10} concentrations at MGO monitoring sites in 2019 $\,$



3.3 Annual average TSP

Table 8 shows the measured annual average TSP concentrations from each monitor for data collected in 2019. Annual averages have been calculated without extraordinary events for comparison with the development consent criteria. These data show that, without extraordinary events, the TSP concentrations at TSP 1 and TSP 2 were below 90 $\mu g/m^3$. Consequently the monitoring demonstrates compliance with the development consent in terms of particulate matter as TSP.

Table 8 Measured TSP concentrations from MGO monitors in 2019

Year	TSP 1	TSP 2	TSP 3	Criterion
Annual average in μg/m³				
2019 (all data)	73	92	90	NA
2019 (without extraordinary events)	60	76	79	90

Table 9 shows the calculated site contributions to each monitor as per the methodology described in Section 2.

Table 9 Estimated contributions of MGO to measured TSP concentrations

Parameter	TSP 1	TSP 2	TSP 3	Criterion
Lower bound of wind from MOC to monitor (degrees)	30	240	330	-
Upper bound of wind from MOC to monitor (degrees)	110	330	40	-
Percentage of time that wind was from MOC towards monitor (%)	4	30	21	-
Annual average TSP concentration (μg/m³)	60	76	79	90
Estimated MOC contribution to annual average TSP (µg/m³)	3	23	17	-

The calculations from Table 9 show that the MGO was estimated to have contributed up to 3 $\mu g/m^3$ to the measured 60 $\mu g/m^3$ at TSP 1, up to 23 $\mu g/m^3$ to the measured 76 $\mu g/m^3$ at TSP 2, and up to 17 $\mu g/m^3$ to the measured 79 $\mu g/m^3$ at TSP 3. The higher potential contribution at TSP 2 would be expected since this monitor was located downwind of the MGO for a higher proportion of the year. There are no specific criteria for which to assess a calculated site contribution.

4. Conclusion

Based on the analysis and it has been concluded that Mt Owen was in compliance with its Glendell (DA 80/952) and Mount Owen (SSD-5850) development consents in terms of total PM_{10} and TSP impacts at all reportable monitoring sites for data collected in 2019.



5. References

EPA (2016) "Approved Methods for the Modelling and Assessment of Air Pollutants in NSW". Environment Protection Authority.

US EPA (2000) "Meteorological Monitoring Guidance for Regulatory Modeling Applications". United States Environmental Protection Agency. Office of Air Quality, Planning and Standards, Research Triangle Park NC 27711. EPA-454/R-99-005, February 2000.

Appendix G: Water

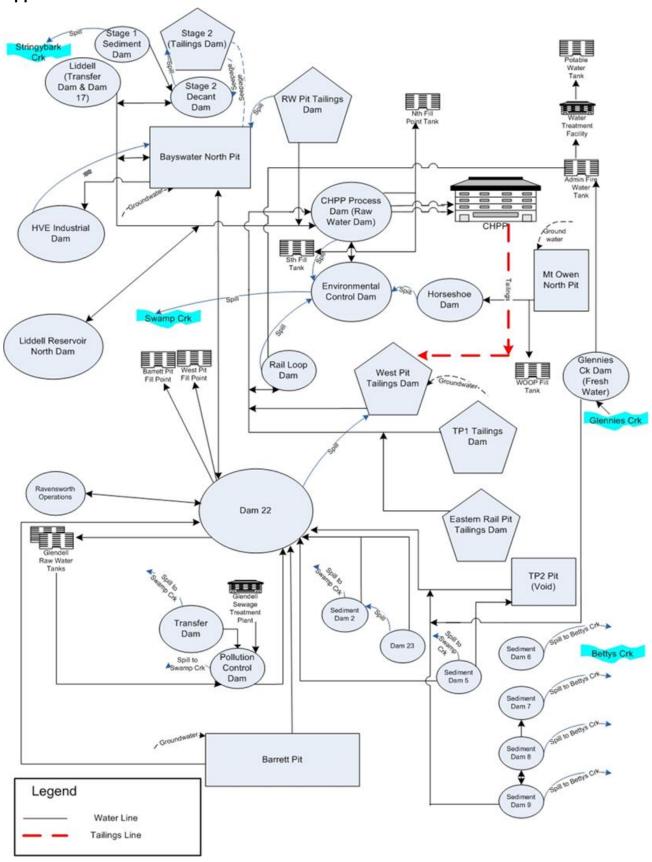


Figure 5: MGO Water Schematic

Surface Water

Table 35: Surface Monitoring Results Bowmans Creek

Sampling	BMC1 – Bowman's Creek Upstream				BMC2 – Bowman's Creek Midstream			
Date	рН	EC (µS/cm)	TSS (mg/L)	TDS (mg/L)	рН	EC (µS/cm)	TSS (mg/L)	TDS (mg/L)
18/01/2019	7.70	1,559	3	894	7.80	1,691	44	950
21/02/2019	8.10	1,636	2	1,190	8.30	1,652	82	1,050
26/03/2019	8.00	1,790	23	1,110	8.80	1,536	42	976
30/04/2019	7.60	2,170	11	1,400	7.20	1,728	27	1,150
20/05/2019	7.70	2,190	22	1,500	7.40	2,060	58	1,490
24/06/2019	7.10	1,699	1	1,280	7.20	1,982	36	1,460
23/07/2019	7.90	1,645	2	1,200	7.60	1,951	68	1,410
26/08/2019	8.00	1,743	3	1,510	8.00	2,320	60	1,480
23/09/2019	7.90	1,766	3	1,170	7.90	1,741	103	1,230
15/10/2019	7.90	1,901	1	1,200	7.50	2,820	642	1,780
19/11/2019	7.90	2,690	2	1,720				
20/12/2019	8.00	3,880	8	2,590				

Samulina Data	В	MC3 – Bowman'	s Creek Downs	tream	BMC4 – Bowman's Creek (Hebden Road)			
Sampling Date	рН	EC (µS/cm)	TSS (mg/L)	TDS (mg/L)	рН	EC (µS/cm)	TSS (mg/L)	TDS (mg/L)
18/01/2019	8.40	2,410	134	1,380	7.80	1,316	5	773
21/02/2019					7.30	1,292	10	1,050
26/03/2019			Dry		7.40	1,391	14	919
30/04/2019		'	ыу		7.70	1,449	9	972
20/05/2019					7.20	1,382	16	922
24/06/2019	7.40	2,600	4	1,870	7.00	1,290	10	839
23/07/2019					7.20	1,318	18	845
26/08/2019					7.40	1,327	30	845
23/09/2019			D.m.		7.70	1,386	20	900
15/10/2019		Dry				1,354	36	776
19/11/2019					7.50	1,429	41	886
20/12/2019					7.50	1,850	201	1,170

Sampling Date	BMC5 – Bowman's Creek NEH Bridge						
Sampling Date	рН	EC (µS/cm)	TSS (mg/L)	TDS (mg/L)			
7/01/2019	8.00	5,620	28	3,650			
12/02/2019		-)m/				
6/03/2019		L	Ory				
9/04/2019	7.60	3,930	5	2,380			
6/05/2019	7.90	4,020	20	2,490			
4/06/2019	8.00	4,090	18	2,800			
9/07/2019	8.30	4,070	17	2,680			
7/08/2019							
11/09/2019							
10/10/2019	Dry						
13/11/2019							
10/12/2019							

Table 36: Surface Water Monitoring Results Yorks Creek

Sampling Data	YC1 – Yorks Creek Upstream				YC2 – Yorks Creek Midstream			m	
Sampling Date	рН	EC (µS/cm)	TSS (mg/L)	TDS (mg/L)	рН	EC (µS/cm)	TSS (mg/L)	TDS (mg/L)	
18/01/2019									
21/02/2019									
26/03/2019									
30/04/2019									
20/05/2019									
24/06/2019		D	ry		Dry				
23/07/2019			.,						
26/08/2019									
23/09/2019									
15/10/2019									
19/11/2019									
20/12/2019									

Sampling Date	YC3 – Yorks Creek Downstream							
oumpining zatio	рН	EC (µS/cm)	TSS (mg/L)	TDS (mg/L)				
18/01/2019								
21/02/2019								
26/03/2019								
30/04/2019								
20/05/2019								
24/06/2019		D	rv					
23/07/2019		D	ıy					
26/08/2019								
23/09/2019								
15/10/2019								
19/11/2019								
20/12/2019								

Table 37: Surface Water Monitoring Swamp Creek

Samulina Data	SC1 -	- Swamp Cree	k Upstream (D	am 5)	SC2 – Swamp Creek Midstream (Dam 1)				
Sampling Date	рН	EC (µS/cm)	TSS (mg/L)	TDS (mg/L)	рН	EC (µS/cm)	TSS (mg/L)	TDS (mg/L)	
18/01/2019	8.90	503	6	254	8.30	675	57	389	
21/02/2019	9.10	524	6	344	8.30	938	31	591	
26/03/2019	9.10	524	5	350	8.50	930	33	561	
30/04/2019	8.10	524	47	362	7.40	409	19	321	
20/05/2019	7.30	421	39	331	8.10	522	3	329	
24/06/2019	7.30	533	7	378	7.10	436	17	291	
23/07/2019	8.70	536	1	338	7.80	445	16	275	
26/08/2019	8.80	552	2	340	8.10	496	15	316	
23/09/2019	9.20	539	3	355	7.30	462	39	340	
15/10/2019	9.10	548	9	339	8.50	483	15	288	
19/11/2019	9.40	572	2	345	9.50	596	17	417	
20/12/2019	9.30	590	8	366	7.60	823	29	543	

Sampling		SC3 – Swamp	Creek Downst	tream	SC4 – Prior to Ashton					
Date	рН	EC (µS/cm)	TSS (mg/L)	TDS (mg/L)	рН	EC (µS/cm)	TSS (mg/L)	TDS (mg/L)		
18/01/2019										
21/02/2019										
26/03/2019					Dry					
30/04/2019										
20/05/2019										
24/06/2019			Dry							
23/07/2019			Diy							
26/08/2019										
23/09/2019										
15/10/2019										
19/11/2019										
20/12/2019										

Table 38: Surface Water Monitoring Betty's Creek

Sampling	I	BC1 – Bettys Cro	eek Upstream		BC2 – Bettys Creek Downstream					
Date	рН	EC (µS/cm)	TSS (mg/L)	TDS (mg/L)	рН	TDS (mg/L)				
18/01/2019					(mg/L) (mg/L)					
21/02/2019					Dry					
26/03/2019										
30/04/2019										
20/05/2019										
24/06/2019		Dry								
23/07/2019		,								
26/08/2019										
23/09/2019										
15/10/2019										
19/11/2019										
20/12/2019										

Sampling	ВС	3 – Bettys Cre	ek Prior to As	hton	BC4 – Bettys Creek 4				
Date	рН	EC (µS/cm)	TSS (mg/L)	TDS (mg/L)	рН	EC (µS/cm)	TSS (mg/L)	TDS (mg/L)	
18/01/2019						Ь	ry		
21/02/2019						D	ТУ		
26/03/2019					6.60	288	66	254	
30/04/2019						354	35	320	
20/05/2019					7.10	390	9	338	
24/06/2019		D	ry		6.90	408	23	356	
23/07/2019		D	'i y		7.10	423	10	358	
26/08/2019					7.30	465	9	399	
23/09/2019					7.00	493	17	465	
15/10/2019							ry		
19/11/2019						U	'i y		
20/12/2019					6.70	276	54	291	

Table 39: Surface Water Monitoring Main Creek

Sampling Date		MC1 – Mai	n Creek Upstre	am	MC2 – Main Creek Downstream					
	рН	EC (µS/cm)	TSS (mg/L)	(mg/L) TDS (mg/L)		EC (µS/cm)	TSS (mg/L)	TDS (mg/L)		
18/01/2019										
21/02/2019										
26/03/2019										
30/04/2019			Dry	v						
20/05/2019			,							
24/06/2019					Dry					
23/07/2019										
26/08/2019		ı								
23/09/2019	6.80	207	39	228						
15/10/2019										
19/11/2019			Dry							
20/12/2019										

Sampling Date	MC3 – Main Creek Upstream								
Camping Date	рН	EC (µS/cm)	TSS (mg/L)	TDS (mg/L)					
18/01/2019									
21/02/2019									
26/03/2019									
30/04/2019									
20/05/2019									
24/06/2019			Dry						
23/07/2019			Diy						
26/08/2019									
23/09/2019									
15/10/2019									
19/11/2019									
20/12/2019									

Table 40: Historical Surface Water Data Comparison – pH

O'ta Nama	Trigge	r Level				Annual Avera	ge						
Site Name	Lower	Upper	2013	2014	2015	2016	2017	2018	2019				
	Bowmans Creek												
BMC1	6.5	8.0	8	7.9	7.8	8.01	7.88	7.69	7.82				
BMC2	6.5	8.0	8.1	8	7.9	7.99	7.96	7.78	7.77				
ВМС3	6.5	8.0	8	7.9	8	8.05	8.05	7.87	7.90				
BMC4	6.5	8.0	7.9	7.7	7.7	7.87	7.63	7.40	7.47				
BMC 5	6.5	8.0	N/A	N/A	7.9	7.76	7.78	8.11	7.96				
	Yorks Creek												
YC1	6.5	8.6	7.6	7.5	7.5	7.6	7.25	6.7	N/A				
YC2	6.5	8.6	7.5	7.5	7.6	7.77	7.28	N/A	N/A				
YC3	6.5	8.6	7.7	7.3	7.5	7.79	7.4	N/A	N/A				
				Swa	mp Creek								
SC1	6.5	8.6	N/A	8.1	8	8.16	8.18	9.13	8.69				
SC2	6.5	8.6	N/A	7.5	7.7	7.88	7.42	7.64	8.04				
SC3	6.5	8.6	8.1	8.1	8.1	8.03	7.3	N/A	N/A				
SC4	6.5	8.6	7.3	N/A	7.2	7.27	6.75	N/A	N/A				
				Bett	ys Creek								
BC1	7.7	6.9	7.5	7.69	7.5	7.7	6.9	N/A	N/A				
BC2	7.5	8.2	7.4	7.7	7.4	7.5	8.2	N/A	N/A				
BC3	8	8.1	7.4	7.3	6.97	8	8.1	N/A	N/A				
BC4	7.9	7.6	7.4	7.55	7.27	7.9	7.6	6.65	6.97				
				Ма	in Creek								
MC1	N/A	N/A	7.4	7.49	7.24	N/A	N/A	7.10	6.8				
MC2	N/A	N/A	7.5	7.49	7.55	N/A	N/A	7.00	N/A				
МС3	N/A	N/A	N/A	N/A	7.46	N/A	N/A	N/A	N/A				

Table 41: Historical Surface Water Data Comparison – Electrical Conductivity (μ S/cm)

0'' N	Trigger	Annual Average									
Site Name	Level	2013	2014	2015	2016	2017	2018	2019			
			Е	Sowmans Creek							
BMC1	2,200	1,018	1,201	1,026	940	767	1,447	2,056			
BMC2	2,200	1,204	1,353	1,114	964	860	1,293	1,948			
BMC3	2,200	1,449	1,942	1,337	1,344	1,354	1,656	2,505			
BMC4	2,200	1,044	1,356	1,065	1,124	1,115	1,274	1,399			
BMC 5	2,200	N/A	N/A	1,415	1,179	1,461	3,888	4,306			
	Yorks Creek										
YC1	6,668	3,476	4,344	3,012	3,818	3,422	4,990	N/A			
YC2	6,668	2,266	13,074	7,194	5,241	9,002	N/A	N/A			
YC3	6,668	5,009	4,532	4,971	2,903	6,739	N/A	N/A			
				Swamp Creek							
SC1	6,668	N/A	396	392	351	393	524	531			
SC2	6,668	N/A	241	265	315	227	469	601			
SC3	6,668	4,997	6,608	4,184	5,075	7,180	N/A	N/A			
SC4	6,668	688	N/A	898	720	281	N/A	N/A			
				Bettys Creek							
BC1	6,668	1,193	21	926	1,096	776	N/A	N/A			
BC2	6,668	189	6,093	529	696	188	N/A	N/A			
ВС3	6,668	4,209	4,447	763	529	288	N/A	N/A			
BC4	6,668	2,473	2,755	559	1,227	427	300	403			
				Main Creek							
MC1	6,668	N/A	N/A	1,253	1,207	872	1,321	207			
MC2	6,668	N/A	N/A	1,634	1,311	1,968	1,720	N/A			
MC3	6,668	N/A	N/A	N/A	N/A	1,103	N/A	N/A			

Table 42: Historical Surface Water Data Comparison – TSS (mg/L)

0'' N	Trigger	ger Annual Average									
Site Name	Level	2013	2014	2015	2016	2017	2018	2019			
Bowmans Creek											
BMC1	21	12.3	6.3	10.3	9	26	5	7			
BMC2	21	11.4	14.4	47.5	14.1	12	19	116			
ВМС3	21	28.2	23.9	13.4	17.3	13	33	69			
BMC4	21	11.5	8.3	13.5	15.2	6	10	34			
BMC 5	21	N/A	N/A	9.4	9.9	14	20	18			
Yorks Creek											
YC1	68	22	7	48.6	32.7	12	14	N/A			
YC2	68	21	11.3	58.5	17.4	9	N/A	N/A			
YC3	68	54	12.5	38	35.3	33	N/A	N/A			
			S	wamp Creek							
SC1	68	N/A	15	9.3	8.2	8	7.3	11			
SC2	68	N/A	13.2	13.5	8	19	25.6	24			
SC3	68	15.2	29	46.9	53.6	7	N/A	N/A			
SC4	68	35.7	N/A	27.3	31	37	N/A	N/A			
			В	ettys Creek							
BC1	68	7.3	21	9.5	64.5	6	N/A	N/A			
BC2	68	9	2.6	41.1	11.5	7	N/A	N/A			
ВС3	68	13	51.7	106	37.7	14	N/A	N/A			
BC4	68	168	61.7	38	21.6	46	56	24			
			ı	Main Creek							
MC1	68	N/A	N/A	144.8	187.5	252	100	39			
MC2	68	N/A	N/A	239.6	56.9	153	56	N/A			
MC3	68	N/A	N/A	N/A	N/A	6.8	N/A	N/A			

Table 43: Historical Surface Water Data Comparison – TDS (mg/L)

Olfa Nama	Trigger			A	Annual Averag	е		
Site Name	Level	2013	2014	2015	2016	2017	2018	2019
			Bowmans	Creek				
ВМС1	890	567	690.3	586.6	529.5	615	964	1,397
ВМС2	890	682	782.5	649.3	557.7	636	827	1,298
ВМС3	890	829	1,136	766.8	779.3	710	1,052	1,625
ВМС4	890	591	746	575.7	651.4	687	781	908
BMC 5	890	N/A	N/A	902.9	714.6	721	2,463	2,800
			•	Yorks Creek				
YC1	4,384	2,077	2,641	1822	2,278.2	2,013	3,240	N/A
YC2	4,384	1,233	8,500	4,797.3	3,375.4	6,476	N/A	N/A
YC3	4,384	3,035	2,814	3,051.3	1914	4,210	N/A	N/A
			S	wamp Creek				
SC1	4,384	N/A	297.9	236.8	218.4	295	344.2	342
SC2	4,384	N/A	253.9	179	211.1	199	331	388
SC3	4,384	3,378.9	3,954	2,204.3.	3,072.9	4,890	N/A	N/A
SC4	4,384	524	N/A	618.2	501.33	295	N/A	N/A
			E	Bettys Creek				
BC1	4,384	685.8	568	513	644.8	515	N/A	N/A
BC2	4,384	194	3,932	338.6	473.3	187	N/A	N/A
ВС3	4,384	2,861	2,726	530.4	277.7	293	N/A	N/A
BC4	4,384	1,543	1,743	342.3	797.7	322	265	338
				Main Creek				
MC1	4,384	N/A	N/A	837.9	918.6	739	812	228
MC2	4,384	N/A	N/A	986.8	875.1	1,258	1,080	N/A
МС3	4,384	N/A	N/A	N/A	N/A	678	N/A	N/A

Ground Water

Table 44: MGO Ground Water Monitoring Results

	I	BC-SP02	2		BC-SP	03		BC-SP	04	i	BC-SP05	
Samplin g Date	Depth to Water (m)	рН	EC (µS/c m)	Depth to Water (m)	рН	EC (µS/cm)	Dept h to Wat er (m)	рН	EC (μS/cm)	Depth to Water (m)	рН	EC (µS/c m)
Jan-19	7.70	6.8	5,000	7.71	7.3	8,100	7.59	7.2	8,930	7.63	7.21	9,720
Mar-19	7.80	6.8	6,060	7.83	7.2	11,440	7.68	7.1	9,950	7.72	7.16	9,900
Jun-19	7.84	6.9	6,030				7.73	7.1	11,9200	7.77	7.20	12,43 0
Sep-19	7.94	6.8	6,640	7.94			7.81	7.1	11,780	7.85	7.03	12,24 0

		BC-SP0)6		BC-SP0	7		BC-SP)8		BC-SP)9
Sampling Date	Depth to Water (m)	рН	EC (μS/cm)	Depth to Water (m)	рН	EC (µS/cm)	Depth to Water (m)	рН	EC (μS/cm)	Depth to Water (m)	рН	EC (µS/cm)
Jan-19	8.39	7.20	7,950				7.29	7.12	11,270	7.47	7.26	8,850
Mar-19	8.37	7.14	10,800				7.48	7.06	14,340	7.69		
Jun-19	8.44	7.18	10,440				7.61	7.10	14,120	7.79	7.23	11,360
Sep-19	8.51	7.11	9,970	10.09	7.02	11,030	7.78	7.05	14,370	7.87	7.26	11,070

		BC-SP	10		BC-SP1	11		BC-SP	12		BC-SP	14
Sampling Date	Depth to Water (m)	рН	EC (μS/cm)	Depth to Water (m)	рН	EC (µS/cm)	Depth to Water (m)	рН	EC (µS/cm)	Depth to Water (m)	рН	EC (μS/cm)
Mar-19	5.97	7.55	7,540.00	5.45	6.36	6,560	5.81	6.74	5,250.00	5.26	7.31	8,670.00
Jun-19	6.02	7.40	8,220.00	5.39	6.53	8,230	5.92	6.84	5,590.00	5.34	7.36	6,210.00
Sep-19	6.23			5.64	6.58	6,210	6.21			5.44		
Dec-19	6.23			5.87	6.50	8,920						

	ı	BC-SP	15	i	BC-SP	16		BC-SP17		В	C-SP1	8
Sampling Date	Depth to Water (m)	рН	EC (µS/cm)	Depth to Water (m)	рН	EC (µS/cm)	Depth to Water (m)	рН	EC (µS/cm)	Depth to Water (m)	рН	EC (µS/cm)
Mar-19		(iii)										
Jun-19		Dny			Dn			Dny			Dny	
Sep-19		Dry			Dry			Dry			Dry	
Dec-19		Dry										

		BC-SP2	0		BC-SP2	1		BC-SP2	2		GA1	
Sampling Date	Depth to Water (m)	рН	EC (μS/cm)	Depth to Water (m)	рН	EC (µS/cm)	Depth to Water (m)	рН	EC (μS/cm)	Depth to Water (m)	рН	EC (µS/cm)
Mar-19	4.82	6.73	831	5.98	7.43	1,213	5.78	7.33	22,430			
Jun-19					6.47	7.65	1,760	5.71	7.64		Dmi	
Sep-19	4.35			6.61	7.53	2,453	5.89	7.55	8,590			
Dec-19				6.75	7.52	5,530	5.94	7.43	15,380			

		GA2			GNPS-0)2		GNPS-0)6		NPZ1	01
Sampling Date	Depth to Water (m)	рН	EC (µS/cm)	Depth to Water (m)	рН	EC (µS/cm)	Depth to Water (m)	рН	EC (µS/cm)	Depth to Water (m)	рН	EC (µS/cm)
Jan-19	N/A	N/A	N/A	6.01	6.76	1,223	7.15	6.28	3,010	5.37	7.35	11,220
Mar-19	7.38	6.78	3,860	6.07	6.52	1,035	7.33	6.53	3,890	5.49	7.10	16,060
Jun-19	7.45	6.92	2,481	6.00	6.55	1,325	7.37	6.37	4,420	5.58	7.05	13,660
Sep-19	7.54	6.79	3,410	6.16	6.38	1,105	7.59	6.35	4,770	5.72	7.10	15,720
Dec-19	7.70	6.77	3,550	6.23	6.45	1,176	7.88	6.60	5,390	5.87	7.06	12,740

		NPZ102	2		NPZ103	3		NPZ104	4		NPZ10	ô
Sampling Date	Depth to Water (m)	рН	EC (µS/cm)	Depth to Water (m)	рН	EC (µS/cm)	Depth to Water (m)	рН	EC (µS/cm)	Depth to Water (m)	рН	EC (µS/cm)
Jan-19	2.43	7.20	5,310	4.50	7.35	6,200						
Mar-19	2.70	7.08	7,740							7.50		
Jun-19	2.80	6.97	6,730	6.09	7.30	7,640			7.59			14,210
Sep-19	2.92	7.14	7,450	6.07	7.48	8,810			7.39			
Dec-19	3.22	7.07	6,000						7.45			

	N	IPZ1-Laı	rge	N	IPZ1-Sm	all	N	IPZ3-Laı	rge	ı	NPZ3-S	mall
Sampling Date	Depth to Water (m)	рН	EC (µS/cm)	Depth to Water (m)	рН	EC (µS/cm)	Depth to Water (m)	рН	EC (µS/cm)	Depth to Water (m)	рН	EC (µS/cm)
Jan-19	15.93	7.20	12,320	42.05	7.15	8,790	13.56	7.57	7,290	9.20	6.64	20,870
Mar-19	15.57	7.16	17,110	41.75	7.05	11,520	14.39	7.31	10,660	9.85	6.58	18,340
Jun-19	15.66	7.07	14,830	42.27	6.88	9,960	13.04	7.32	9,190	9.55	6.79	15,480
Sep-19	15.60	7.07	18,590	41.62	7.59	11,660	14.23	7.58	10,300	10.17	7.04	17,000
Dec-19	16.22	7.01	15,330	44.19	8.31	10,410	15.12	7.59	10,490	10.73	6.80	16,520

		NPZ4- La	arge	I	NPZ4- Sr	nall	N	PZ6-La	rge	NP	Z6-Sn	nall
Sampling Date	Depth to Water (m)	рН	EC (μS/cm)	Depth to Water (m)	рН	EC (µS/cm)	Depth to Water (m)	рН	EC (μS/cm)	Depth to Water (m)	рН	EC (µS/cm)
Jan-19	6.81	6.99	26,100	6.84	7.08	23,910						
Mar-19	6.02	7.00	27,810	6.48	7.07	24,940						
Jun-19	6.35	6.88	23,220	6.60	6.92	20,990						
Sep-19	6.60	7.26	27,630	6.67	7.24	24,900						
Dec-19	6.94	7.09	21,970	6.89	7.12	19,830						

	N	IPZ7 – La	rge	N	PZ7 - Sn	nall	NI	PZ8 – La	rge	N	PZ8 – Sr	mall
Sampling Date	Depth to Water (m)	рН	EC (µS/cm)	Depth to Water (m)	рН	EC (µS/cm)	Depth to Water (m)	рН	EC (µS/cm)	Depth to Water (m)	рН	EC (µS/cm)
Jan-19	14.95	7.57	6,870	35.84	7.36	7,170	10.02	7.82	13,950	35.40	7.41	2,640
Mar-19	15.27	7.42	9,980	35.33	7.42	8,610	10.20	7.63	20,730	35.50	7.37	3,180
Jun-19	15.49	7.39	8,740	36.76	7.38	7,330	10.11	7.51	17,620	35.94	7.26	2,701
Sep-19	15.69	7.46	9,550	37.08	7.46	7,960	10.08	7.66	19,840	35.91	7.43	2,757
Dec-19	16.33	7.37	7,900	38.13	7.42	6,800	10.38	7.70	15,950	36.06	7.44	2,448

	ı	NPZ9- La	rge	N	PZ9- S	Small	N	PZ10-La	rge	NI	PZ10-Sr	nall
Sampling Date	Depth to Water (m)	рН	EC (µS/cm)	Depth to Water (m)	to pH EC (µS/cm)		Depth to Water (m)	рН	EC (μS/cm)	Depth to Water (m)	рН	EC (µS/cm)
Jan-19	4.29	7.11	7,230				26.65	7.72	4,140			
Mar-19	4.47	6.81	10,010				25.88	7.57	6,770			
Jun-19	4.60	6.73	9,940		Block	ed	26.42	7.41	7,260	37.31	6.97	14,930
Sep-19	4.74	6.91	7,390	_		26.46	7.17	6,280	37.61	7.09	11,170	
Dec-19	4.90	6.89	7,880	_			27.03	7.06	6,500	37.64	7.02	11,100

	N	PZ11- La	rge	N	PZ11- Small		NPZ12-Large			NPZ12-Small		
Sampling Date	Depth to Water (m)	рН	EC (µS/cm)	Depth to Water (ml)	рН	EC (µS/cm)	Depth to Water (m)	рН	EC (µS/cm)	Depth to Water (m)	рН	EC (µS/cm)
Jan-19	24.07	7.23	9,830	57.02								
Mar-19	24.97	7.20	11,420									
Jun-19	24.76	7.42	11,690	57.20	8	3.51						
Sep-19	25.95	7.23	12,130	59.50	8	3.33						
Dec-19	26.21	7.13	11,240	59.91	8	3.25						

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	NI	PZ13- Large		NPZ13- Small			NPZ16- Large			NPZ16- Small		
Sampling Date	Depth to Water (m)	рН	EC (µS/cm)	Depth to Water (m)	рН	EC (μS/cm)	Depth to Water (m)	рН	EC (µS/cm)	Depth to Water (m)	рН	EC (µS/cm)
Mar-19	17.41	7.16	12,270	51.96	7.31	13,280	11.48	7.28	14,230			
Jun-19	17.82	7.11	11,770	51.99	7.13	13,270	10.91	7.28	13,980			
Sep-19	18.53	7.11	11,860	52.50	7.18	13,100	12.47	7.27	13,940			
Dec-19	19.11	7.08	12,310	52.96	7.20	13,590	13.74	7.32	13,940			

0 "	North								
Sampling Date	Depth to Water (m)	рН	EC (µS/cm)						
Jan-19	10.53	7.48	3,770						
Mar-19	10.80	7.32	6,080						
Jun-19	11.00	7.22	4,470						
Sep-19	11.34	7.28	5,220						
Dec-19	11.69	7.41	4,710						

Table 45: MGO Summary Ground Water Monitoring Results 2019

Min	Disc		EC (μS/cm)			рН			Depth to Wa	ater (m)
BC-SP02 5000 6640 6022.00 6.8 6.9 6.83 7.7 8.05 7.87 BC-SP03 8100 11440 9770.00 7.24 7.31 7.28 7.71 8.8 7.87 BC-SP04 8930 11920 10766.00 7.04 7.22 7.12 7.59 7.91 7.74 BC-SP05 9720 12430 111620 7.03 7.21 7.13 7.63 7.96 7.79 BC-SP06 7950 10800 9704.00 7.07 7.2 7.14 8.37 8.6 8.46 BC-SP07 11030 11030 11030 11030.00 7.02 7.02 7.02 10.09 10.09 10.09 BC-SP08 11270 14370 13414.00 7 7.12 7.07 7.29 7.93 7.62 BC-SP08 8850 11360 10460.00 7.14 7.26 7.22 7.47 7.96 7.76 BC-SP09 8850 11360 10460.00 7.4 7.55 7.48 5.97 6.33 6.11 BC-SP11 6210 8920 7480.00 6.36 6.58 6.49 5.39 5.87 5.59 BC-SP12 5250 5590 5420.00 6.74 6.84 6.79 5.81 6.21 5.98 BC-SP13 ND	Piezometer	Min	Max	Ave	Min	Max	Ave	Min	Max	Ave
BGS-P03 8100 11440 977000 7.24 7.31 7.28 7.71 8 7.87 BGS-SP04 8930 11920 10766.00 7.04 7.22 7.12 7.59 7.91 7.74 BGS-SP04 8930 11920 10766.00 7.03 7.21 7.13 7.63 7.96 7.79 BGS-SP06 9720 12430 11162.00 7.03 7.21 7.13 7.63 7.96 7.79 BGS-SP06 7950 10800 9704.00 7.07 7.2 7.14 8.37 8.6 8.46 8.46 BGS-SP07 11030 11030 11030.00 7.02 7.02 7.02 10.09 10.09 10.09 10.09 BGS-SP08 11270 14370 13414.00 7 7.12 7.07 7.29 7.93 7.62 BGS-SP08 11270 14370 13414.00 7 7.12 7.07 7.29 7.93 7.62 BGS-SP09 8850 11360 10460.00 7.14 7.26 7.22 7.47 7.96 7.76 BGS-SP10 7540 8220 7880.00 7.4 7.55 7.48 5.97 6.23 6.11 BGS-SP11 6210 8920 7480.00 6.36 6.58 6.49 5.39 5.87 5.59 BGS-SP12 5250 5590 5420.00 6.74 6.84 6.79 5.81 6.21 5.98 BGS-SP13 ND BGS-SP14 6210 8670 7440.00 7.31 7.36 7.34 5.26 5.44 5.35 BGS-SP15 ND	BC-SP01	ND	ND	ND	ND	ND	ND	ND	ND	ND
BC-SP04 8830 11920 10766.00 7.04 7.22 7.12 7.59 7.91 7.74 BC-SP05 9720 12430 11162.00 7.03 7.21 7.13 7.63 7.96 7.79 BC-SP06 7950 10800 9704.00 7.07 7.2 7.14 8.37 8.6 8.46 BC-SP07 11030 11030 11030.00 7.02 7.02 7.02 10.09 10.09 10.09 BC-SP08 11270 14370 13414.00 7 7.12 7.07 7.29 7.93 7.62 BC-SP09 8850 11360 10460.00 7.4 7.55 7.48 5.97 6.23 6.11 BC-SP10 7540 8220 7880.00 7.4 7.55 7.48 5.97 6.23 6.11 BC-SP11 6210 8920 7480.00 6.36 6.58 6.49 5.39 5.87 5.59 BC-SP12 850 5420.00<	BC-SP02	5000	6640	6022.00	6.8	6.9	6.83	7.7	8.05	7.87
BC-SP05 9720 12430 11162.00 7.03 7.21 7.13 7.63 7.96 7.79 BC-SP06 7950 10800 9704.00 7.07 7.2 7.14 8.37 8.6 8.46 BC-SP07 11030 11030 11030.00 7.02 7.02 10.09 10.09 10.09 BC-SP08 11270 14370 13414.00 7 7.12 7.07 7.29 7.93 7.62 BC-SP09 8850 11360 10460.00 7.4 7.55 7.48 5.97 6.23 6.11 BC-SP10 7540 8220 7880.00 7.4 7.55 7.48 5.97 6.23 6.11 BC-SP11 6210 8920 7480.00 6.36 6.58 6.49 5.39 5.87 5.59 BC-SP12 5250 5590 5420.00 6.74 6.84 6.79 5.81 6.21 5.98 BC-SP13 ND ND ND	BC-SP03	8100	11440	9770.00	7.24	7.31	7.28	7.71	8	7.87
BC-SP06 7950 10800 9704.00 7.07 7.2 7.14 8.37 8.6 8.46 BC-SP07 11030 11030 11030 7.02 7.02 7.02 10.09 10.09 10.09 BC-SP08 11270 14370 13414.00 7 7.12 7.07 7.29 7.93 7.62 BC-SP09 8850 11360 10460.00 7.4 7.55 7.48 5.97 6.23 6.11 BC-SP10 7540 8220 7880.00 7.4 7.55 7.48 5.97 6.23 6.11 BC-SP11 6210 8920 7480.00 6.36 6.58 6.49 5.39 5.87 5.59 BC-SP12 5250 5590 5420.00 6.74 6.84 6.79 5.81 6.21 5.98 BC-SP13 ND N	BC-SP04	8930	11920	10766.00	7.04	7.22	7.12	7.59	7.91	7.74
BC-SP07 11030 11030 1103000 7.02 7.02 7.02 10.09 10.09 10.09 BC-SP08 11270 14370 13414.00 7 7.12 7.07 7.29 7.93 7.62 BC-SP09 8850 11360 10460.00 7.14 7.26 7.22 7.47 7.96 7.76 BC-SP10 7540 8220 7880.00 7.4 7.55 7.48 5.97 6.23 6.11 BC-SP11 6210 8920 7480.00 6.36 6.58 6.49 5.39 5.87 5.59 BC-SP13 ND	BC-SP05	9720	12430	11162.00	7.03	7.21	7.13	7.63	7.96	7.79
BC-SP08 11270 14370 13414.00 7 7.12 7.07 7.29 7.93 7.62 BC-SP09 8860 11360 10460.00 7.14 7.26 7.22 7.47 7.96 7.76 BC-SP10 7540 8220 7880.00 7.4 7.55 7.48 5.97 6.23 6.11 BC-SP11 6210 8920 7480.00 6.36 6.58 6.49 5.39 5.87 5.59 BC-SP12 5250 5590 5420.00 6.74 6.84 6.79 5.81 6.21 5.98 BC-SP13 ND	BC-SP06	7950	10800	9704.00	7.07	7.2	7.14	8.37	8.6	8.46
BC-SP09 8850 11360 10460.00 7.14 7.26 7.22 7.47 7.96 7.76 BC-SP10 7540 8220 7880.00 7.4 7.55 7.48 5.97 6.23 6.11 BC-SP11 6210 8920 7480.00 6.36 6.58 6.49 5.39 5.87 5.59 BC-SP12 5250 5590 5420.00 6.74 6.84 6.79 5.81 6.21 5.98 BC-SP13 ND <	BC-SP07	11030	11030	11030.00	7.02	7.02	7.02	10.09	10.09	10.09
BC-SP10 7540 8220 7880.00 7.4 7.55 7.48 5.97 6.23 6.11 BC-SP11 6210 8920 7480.00 6.36 6.58 6.49 5.39 5.87 5.59 BC-SP12 5250 5590 5420.00 6.74 6.84 6.79 5.81 6.21 5.98 BC-SP13 ND ND </td <td>BC-SP08</td> <td>11270</td> <td>14370</td> <td>13414.00</td> <td>7</td> <td>7.12</td> <td>7.07</td> <td>7.29</td> <td>7.93</td> <td>7.62</td>	BC-SP08	11270	14370	13414.00	7	7.12	7.07	7.29	7.93	7.62
BC-SP11 6210 8920 7480.00 6.36 6.58 6.49 5.39 5.87 5.59 BC-SP12 5250 5590 5420.00 6.74 6.84 6.79 5.81 6.21 5.98 BC-SP13 ND	BC-SP09	8850	11360	10460.00	7.14	7.26	7.22	7.47	7.96	7.76
BC-SP12 5250 5590 5420.00 6.74 6.84 6.79 5.81 6.21 5.98 BC-SP13 ND ND ND ND ND ND ND ND ND BC-SP14 6210 8670 7440.00 7.31 7.36 7.34 5.26 5.44 5.35 BC-SP15 ND ND </td <td>BC-SP10</td> <td>7540</td> <td>8220</td> <td>7880.00</td> <td>7.4</td> <td>7.55</td> <td>7.48</td> <td>5.97</td> <td>6.23</td> <td>6.11</td>	BC-SP10	7540	8220	7880.00	7.4	7.55	7.48	5.97	6.23	6.11
BC-SP13 ND ND <t< td=""><td>BC-SP11</td><td>6210</td><td>8920</td><td>7480.00</td><td>6.36</td><td>6.58</td><td>6.49</td><td>5.39</td><td>5.87</td><td>5.59</td></t<>	BC-SP11	6210	8920	7480.00	6.36	6.58	6.49	5.39	5.87	5.59
BC-SP14 6210 8670 7440.00 7.31 7.36 7.34 5.26 5.44 5.35 BC-SP15 ND	BC-SP12	5250	5590	5420.00	6.74	6.84	6.79	5.81	6.21	5.98
BC-SP15 ND ND <t< td=""><td>BC-SP13</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td></t<>	BC-SP13	ND	ND	ND	ND	ND	ND	ND	ND	ND
BC-SP16 ND ND <t< td=""><td>BC-SP14</td><td>6210</td><td>8670</td><td>7440.00</td><td>7.31</td><td>7.36</td><td>7.34</td><td>5.26</td><td>5.44</td><td>5.35</td></t<>	BC-SP14	6210	8670	7440.00	7.31	7.36	7.34	5.26	5.44	5.35
BC-SP17 ND ND <t< td=""><td>BC-SP15</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td></t<>	BC-SP15	ND	ND	ND	ND	ND	ND	ND	ND	ND
BC-SP18 ND ND <t< td=""><td>BC-SP16</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td></t<>	BC-SP16	ND	ND	ND	ND	ND	ND	ND	ND	ND
BC-SP19 ND ND <t< td=""><td>BC-SP17</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td></t<>	BC-SP17	ND	ND	ND	ND	ND	ND	ND	ND	ND
BC-SP20 831 831 831.00 6.73 6.73 6.73 4.35 4.82 4.59 BC-SP21 1213 5530 2739.00 7.43 7.65 7.53 5.98 6.75 6.45 BC-SP22 5590 22430 12997.50 7.33 7.64 7.49 5.71 5.94 5.83 BNO002 11170 18500 16170.00 6.72 6.92 6.82 15.04 15.66 15.30 BNO003 9490 14140 12181.00 6.82 7.22 6.98 15.12 16.96 15.94 BNO004 723 2539 1989.44 6.81 7.06 6.92 43.7 46.17 44.77 BNO006 ND N	BC-SP18	ND	ND	ND	ND	ND	ND	ND	ND	ND
BC-SP21 1213 5530 2739.00 7.43 7.65 7.53 5.98 6.75 6.45 BC-SP22 5590 22430 12997.50 7.33 7.64 7.49 5.71 5.94 5.83 BNO002 11170 18500 16170.00 6.72 6.92 6.82 15.04 15.66 15.30 BNO003 9490 14140 12181.00 6.82 7.22 6.98 15.12 16.96 15.94 BNO004 723 2539 1989.44 6.81 7.06 6.92 43.7 46.17 44.77 BNO006 ND 104.12 104.12 104.12	BC-SP19	ND	ND	ND	ND	ND	ND	ND	ND	ND
BC-SP22 5590 22430 12997.50 7.33 7.64 7.49 5.71 5.94 5.83 BNO002 11170 18500 16170.00 6.72 6.92 6.82 15.04 15.66 15.30 BNO003 9490 14140 12181.00 6.82 7.22 6.98 15.12 16.96 15.94 BNO004 723 2539 1989.44 6.81 7.06 6.92 43.7 46.17 44.77 BNO006 ND	BC-SP20	831	831	831.00	6.73	6.73	6.73	4.35	4.82	4.59
BNO002 11170 18500 16170.00 6.72 6.92 6.82 15.04 15.66 15.30 BNO003 9490 14140 12181.00 6.82 7.22 6.98 15.12 16.96 15.94 BNO004 723 2539 1989.44 6.81 7.06 6.92 43.7 46.17 44.77 BNO006 ND	BC-SP21	1213	5530	2739.00	7.43	7.65	7.53	5.98	6.75	6.45
BNO003 9490 14140 12181.00 6.82 7.22 6.98 15.12 16.96 15.94 BNO004 723 2539 1989.44 6.81 7.06 6.92 43.7 46.17 44.77 BNO006 ND ND <td>BC-SP22</td> <td>5590</td> <td>22430</td> <td>12997.50</td> <td>7.33</td> <td>7.64</td> <td>7.49</td> <td>5.71</td> <td>5.94</td> <td>5.83</td>	BC-SP22	5590	22430	12997.50	7.33	7.64	7.49	5.71	5.94	5.83
BNO004 723 2539 1989.44 6.81 7.06 6.92 43.7 46.17 44.77 BNO006 ND	BNO002	11170	18500	16170.00	6.72	6.92	6.82	15.04	15.66	15.30
BNO006 ND ND <th< td=""><td>BNO003</td><td>9490</td><td>14140</td><td>12181.00</td><td>6.82</td><td>7.22</td><td>6.98</td><td>15.12</td><td>16.96</td><td>15.94</td></th<>	BNO003	9490	14140	12181.00	6.82	7.22	6.98	15.12	16.96	15.94
BNO007 ND ND <th< td=""><td>BNO004</td><td>723</td><td>2539</td><td>1989.44</td><td>6.81</td><td>7.06</td><td>6.92</td><td>43.7</td><td>46.17</td><td>44.77</td></th<>	BNO004	723	2539	1989.44	6.81	7.06	6.92	43.7	46.17	44.77
BNO008 ND ND <th< td=""><td>BNO006</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td><td>ND</td></th<>	BNO006	ND	ND	ND	ND	ND	ND	ND	ND	ND
BNO009 10270 14730 12803.33 6.6 6.99 6.76 100.69 107.39 104.12 BNO011 ND ND ND ND ND 106.59 112.6 109.85 GA1 ND	BNO007	ND	ND	ND	ND	ND	ND	ND	ND	ND
BNO011 ND ND ND ND 106.59 112.6 109.85 GA1 ND	BNO008	ND	ND	ND	ND	ND	ND	ND	ND	ND
GA1 ND	BNO009	10270	14730	12803.33	6.6	6.99	6.76	100.69	107.39	104.12
GA2 2481 3860 3325.25 6.77 6.92 6.82 7.38 7.7 7.52 GNP10D 990 1084 1042.00 7.31 7.66 7.52 5.62 6.08 5.82	BNO011	ND	ND	ND	ND	ND	ND	106.59	112.6	109.85
GNP10D 990 1084 1042.00 7.31 7.66 7.52 5.62 6.08 5.82	GA1	ND	ND	ND	ND	ND	ND	ND	ND	ND
	GA2	2481	3860	3325.25	6.77	6.92	6.82	7.38	7.7	7.52
	GNP10D	990	1084	1042.00	7.31	7.66	7.52	5.62	6.08	5.82

		EC (µS/c	m)		рН			Depth to Wa	ater (m)
Piezometer	Min	Max	Ave	Min	Max	Ave	Min	Max	Ave
GNP11D	1164	1619	1406.25	6.93	7.67	7.30	5.83	6	5.90
GNP11S	ND	ND	ND	ND	ND	ND	5.75	5.98	5.83
GNP9D	1190	1539	1367.00	6.92	7	6.97	9.48	10.3	9.99
GNP9S	ND	ND	ND	ND	ND	ND	ND	ND	ND
GNPS-01	ND	ND	ND	ND	ND	ND	ND	ND	ND
GNPS-02	1035	1325	1172.80	6.38	6.76	6.53	6	6.23	6.09
GNPS-03	ND	ND	ND	ND	ND	ND	ND	ND	ND
GNPS-05	ND	ND	ND	ND	ND	ND	ND	ND	ND
GNPS-06	3010	5390	4296.00	6.28	6.6	6.43	7.15	7.88	7.46
GNPS-07	ND	ND	ND	ND	ND	ND	ND	ND	ND
North	3770	6080	4850.00	7.22	7.48	7.34	10.53	11.69	11.07
NPZ1	12320	18590	15636.00	7.01	7.2	7.10	15.57	16.22	15.80
NPZ10	4140	7260	6190.00	7.06	7.72	7.39	25.88	27.03	26.49
NPZ101	11220	16060	13880.00	7.05	7.35	7.13	5.37	5.87	5.61
NPZ102	5310	7740	6646.00	6.97	7.2	7.09	2.43	3.22	2.81
NPZ103	6200	8810	7550.00	7.3	7.48	7.38	4.5	6.09	5.55
NPZ104	ND	ND	ND	ND	ND	ND	ND	ND	ND
NPZ105	ND	ND	ND	ND	ND	ND	ND	ND	ND
NPZ106	ND	ND	ND	ND	ND	ND	7.39	7.59	7.48
NPZ107D	8070	10310	9178.00	11.85	13.4	12.31	18.66	19.73	19.04
NPZ107S	12620	16410	14368.00	6.79	7.89	7.06	6.92	7.67	7.28
NPZ108D	7860	9290	8710.00	11.09	11.35	11.24	7.76	8.14	7.91
NPZ108S	13480	16880	15442.50	7.04	7.16	7.10	7.51	7.8	7.64
NPZ109D	ND	ND	ND	ND	ND	ND	56.36	59.51	58.47
NPZ109S	ND	ND	ND	ND	ND	ND	5.96	5.96	5.96
NPZ10a	11100	14930	12400.00	6.97	7.09	7.03	37.31	37.64	37.52
NPZ11	9830	12130	11262.00	7.13	7.42	7.24	24.07	26.21	25.19
NPZ11a	10090	10860	10480.00	8.25	8.51	8.36	57.02	59.91	58.41
NPZ12	ND	ND	ND	ND	ND	ND	ND	ND	ND
NPZ12a	ND	ND	ND	ND	ND	ND	ND	ND	ND
NPZ13	11770	12310	12052.50	7.08	7.16	7.12	17.41	19.11	18.22
NPZ13a	13100	13590	13310.00	7.13	7.31	7.21	51.96	52.96	52.35
NPZ15	ND	ND	ND	ND	ND	ND	ND	ND	ND
NPZ15a	6420	13240	8780.00	6.99	7.27	7.12	126.78	127.01	126.90
NPZ16	13940	14230	14022.50	7.27	7.32	7.29	10.91	13.74	12.15
NPZ16a	ND	ND	ND	ND	ND	ND	ND	ND	ND

		EC (µS/cı	m)		рН			Depth to Wa	ater (m)
Piezometer	Min	Max	Ave	Min	Max	Ave	Min	Max	Ave
NPZ1a	8790	11660	10468.00	6.88	8.31	7.40	41.62	44.19	42.38
NPZ3	7290	10660	9586.00	7.31	7.59	7.47	13.04	15.12	14.07
NPZ3a	15480	20870	17642.00	6.58	7.04	6.77	9.2	10.73	9.90
NPZ4	21970	27810	25346.00	6.88	7.26	7.04	6.02	6.94	6.54
NPZ4a	19830	24940	22914.00	6.92	7.24	7.09	6.48	6.89	6.70
NPZ6	ND	ND	ND	ND	ND	ND	ND	ND	ND
NPZ6a	ND	ND	ND	ND	ND	ND	ND	ND	ND
NPZ7	6870	9980	8608.00	7.37	7.57	7.44	14.95	16.33	15.55
NPZ7a	6800	8610	7574.00	7.36	7.46	7.41	35.33	38.13	36.63
NPZ8	13950	20730	17618.00	7.51	7.82	7.66	10.02	10.38	10.16
NPZ8a	2448	3180	2745.20	7.26	7.44	7.38	35.4	36.06	35.76
NPZ9	7230	10010	8490.00	6.73	7.11	6.89	4.29	4.9	4.60
NPZ9a	ND	ND	ND	ND	ND	ND	ND	ND	ND
NV10A	6230	6990	6510.00	6.84	6.89	6.86	16.5	16.95	16.72
NV10B	ND	ND	ND	ND	ND	ND	ND	ND	ND
NV10C	ND	ND	ND	ND	ND	ND	ND	ND	ND
NV11A	11090	11600	11415.00	6.56	6.68	6.63	23.01	23.37	23.16
NV11B	10950	15530	13227.00	6.79	6.98	6.89	23	23.35	23.14
NV11C	ND	ND	ND	ND	ND	ND	ND	ND	ND
NV12A	7440	9960	8388.00	6.78	6.92	6.86	19.56	19.99	19.79
NV12B	8350	11030	9311.00	7	7.14	7.07	21.01	21.41	21.18
NV12C	ND	ND	ND	ND	ND	ND	1.38	1.38	1.38
NV13A	5270	11850	8975.00	6.81	6.92	6.88	19.56	19.96	19.762
NV13B	9510	13160	11004.00	6.8	6.99	6.94	20.94	21.35	21.104
NV13C	ND	ND	ND	ND	ND	ND	ND	ND	ND
NV14A	ND	ND	ND	ND	ND	ND	ND	ND	ND
NV14B	11090	15920	12670.00	6.69	7	6.85	21.37	21.75	21.521
NV14C	ND	ND	ND	ND	ND	ND	ND	ND	ND
NV15A	4010	5810	4660.00	6.65	6.93	6.75	26.45	26.83	26.585
NV15B	ND	ND	ND	ND	ND	ND	ND	ND	ND
NV16A	7440	9230	8086.67	6.88	6.89	6.88	21.17	21.58	21.38
NV16B	6990	9960	8476.00	6.87	7.09	6.98	21.25	21.66	21.463
NV16C	ND	ND	ND	ND	ND	ND	ND	ND	ND
NV17A	6060	7970	6799.00	6.73	6.91	6.83	22.07	22.4	22.246
NV17B	7260	9580	8088.00	6.8	7.01	6.87	22.09	22.42	22.264
NV17C	ND	ND	ND	ND	ND	ND	ND	ND	ND

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		EC (μS/cı	m)		рН		Depth to Water (m)			
Piezometer	Min	Max	Ave	Min	Max	Ave	Min	Max	Ave	
NV18A	ND	ND	ND	ND	ND	ND	ND	ND	ND	
NV18B	5570	8920	6873.00	6.68	6.98	6.88	26.73	27.63	26.981	
NV19A	ND	ND	ND	ND	ND	ND	ND	ND	ND	
NV19B	6510	8910	7468.00	6.53	6.75	6.65	27.03	28.46	27.893	
RW1	7390	12450	9723.00	6.49	6.61	6.56	7.23	8.11	7.662	
RW2	7970	10710	9118.00	6.39	6.56	6.46	7.56	8.41	7.986	
RW3	1518	1518	1518.00	5.61	5.61	5.61	7.55	8.5	8.17	
RW4	5870	7520	6694.00	5.56	5.9	5.76	8.82	10.09	9.462	
RW5	4530	8520	6523.00	6.39	6.85	6.60	10.17	11.06	10.57	
TPZ 01	6810	10450	9147.00	7.36	8	7.68	2.08	2.47	2.241	
TPZ 02	8080	11740	10386.00	7.17	7.66	7.42	2.48	2.9	2.625	
TPZ 03	5470	8650	7510.00	7.2	7.98	7.52	2.18	2.68	2.366	
TPZ 04	7990	11820	10622.00	6.51	7.48	6.76	10.23	10.39	10.336	
TPZ 05	5940	8780	7876.00	6.75	7.41	6.92	9.11	9.32	9.216	
TPZ 06	10120	19560	16439.00	6.08	6.52	6.26	5.19	5.72	5.491	
TPZ 07	12090	17630	15688.00	5.87	6.33	6.11	6.18	6.76	6.496	
TPZ 08	11370	16340	14491.00	6.24	6.62	6.33	6.7	7.12	6.912	
TPZ 09	11390	16140	14377.00	6.34	6.74	6.54	6.87	7.24	7.07	
TPZ 10	ND	ND	ND	ND	ND	ND	ND	ND	ND	
TPZ 11	ND	ND	ND	ND	ND	ND	ND	ND	ND	

Appendix H: Community

Table 46: MGO Summary of Community Complaints (Glendell)

Date	Time	Site	Nature of Complaint	Company Response
				January
23/1/19	10:41am	Glendell	Noise and Dust	A complaint was received by the Department of Planning and Environment via email by a Camberwell community member regarding operational noise and dust between 12:00AM and 5:30AM on 23 Jan 2019. Mt Owen Complex Environment & Community personnel provided the requested information to DP&E. For the complaint period, no noise or dust related alarms were received from Sx12 or Sx13D4. The complainant did not wish to be contacted.
				February
18/2/19	7:39am	Glendell	Dust	A complaint was received via the Mt Owen Complex Complaints Hotline by a Camberwell community member regarding dust. The complainant stated that 'there was a lot of dust that you could taste in your mouth'. Mt Owen Complex Environment & Community personnel investigated the complaint to find no dust alarms were received during/prior to the complaint because the levels were below the compliance limits (50ug/m3). The complainant did not wish to be contacted.
19/2/19	7:47am	Glendell	Noise	A complaint was received via the Mt Owen Complex Complaints Hotline by a Camberwell community member regarding operational noise. The complainant described the noise as 'dozer/machinery noise started at 06:30am this morning, and is still going'. Mt Owen Complex Environment & Community personnel investigated the complaint to find no noise alarms were received during/prior to the complaint because the levels were below the compliance limits (40dB) being 38.2dB (LF) at 6:30AM and noise coming from the operation was 35dB in the area of influence. The complainant did not wish to be contacted.
				March
18/3/19	6:36pm	Glendell	Noise	A complaint was received via the Mt Owen Complex Complaints Hotline by a Camberwell community member regarding operational noise. The complainant described the noise as 'all she can hear is mining noise'. The Glendell Mining Supervisor reviewed the Noise Analysis Tool confirming the mining contribution was 5dB under the 40dB with valid meteorological conditions of 2.3m/s with NW winds. No Sx12 alarms located at Camberwell were received during/prior to the complaint. The complainant did not wish to be contacted.

Camberwell community described the noise Owen Complex I complaint to find no The Glendell Minimining contribution with conditions (high variations of the conditions of the co	ceived via the Mt Owen Complex Complaints Hotline by a nity member regarding operational noise. The complainant se as 'large amount of noise coming from the mine'. Mt Environment & Community personnel investigated the noise alarms were received during/prior to the complaint ing Supervisor reviewed the Noise Analysis Tool noting vas 4dB over the 40dB criteria, however due to unlicensed wind (3.8m/s)), no alarms were triggered. Even though ons were experienced, Mining Supervisor inspected the the mine, replaced tracked with rubber dozer, instructed a gear and changed dumping to the lowest RL available. Viewed the Noise Analysis Tool noting mining contribution 40dB criteria however due to unlicensed condition, high alarms were trigged. The complainant did not wish to be contacted.
April	
07/04/2019 6.45am Glendell Noise Camberwell commundescribed the noise suddenly noise'. complaint. The Glendell licensable condition down and dozer to unwas received becate Mining Supervisor response below the criteria at licensable. Even with all trucks, excavators monitor via the NAT the NAT showed	ceived via the Mt Owen Complex Complaints Hotline by a nity member regarding operational noise. The complainant se as 'it has been quiet but excessive noise has started No Noise alarms had been received at the time of the indell Mining Supervisor reviewed the Noise Analysis Tooling contribution was 1dB under the 40dB criteria with nonons, high wind (3.3m/s) and still instructed trucks to slow use first gear only. After the complaint a single noise alarm use the wind had momentarily dropped below 3m/s. The eviewed the NAT, noting the mining contribution was 1dB and the wind had picked up again (3.5m/s), so was non-in non-licensable conditions, the Mining Supervisor parked is and dozers, listened to the live stream and continuing to one tool. Equipment was gradually brought back online, and the mine contribution was compliant, and the wind had le (2.7m/s). The complainant did not wish to be contacted.
A complaint was rec Camberwell commun described the noise received prior to, 28/4/2019 7.13pm Glendell Noise Mining supervisor rev was an F-class temp under the 40dB crit supervisor continue alarms received. En monitor and identifi	ceived via the Mt Owen Complex Complaints Hotline by a nity member regarding operational noise. The complainant as 'a very loud bang and machine noise'. No alarms were or after the complaint, and the noise levels were within licences conditions. viewed the Noise Analysis Tool (NAT) and noted the there perature inversion in place but the mining contribution was eria, even with the non-licensable conditions. The mining ed to monitor conditions and levels continued steady, no extraordinated officer listened to audio from the Camberwell fied background noise amplified by the F class inversion.

Date	Time	Site	Nature of Complaint	Company Response
7/5/2019	5:30am, 7:00am & 7:51am	Glendell	Noise	Three complaints were received via the Mt Owen Complex Complaints Hotline by a Camberwell Community member regarding operational noise. The complainant generally noted "noise coming from both mines. Complainant said that the noise is coming from both directions and is very loud." In response to the first complaint, the Mining Supervisor reviewed the Noise Analysis Tool and noted that noise levels were non-licensable due to high wind conditions during this period. The Mining Supervisor further inspected operations and continued to monitor conditions. No alarms were received during this period. In response to the second complaint, the Mining Supervisor continue to consult the Noise Analysis Tool and noted that noise levels continued to be non-licensable due to high wind conditions. The Mining Supervisor further instructed operators to limit dozer and vehicle speeds. One alarm was received during this period at approximately 7:40am, the Mining Supervisor inspected the mine area and ensure all previously implemented controls were being implemented. In response to the third complaint, the Environmental Officer reviewed the Noise Analysis Tool and audio from the live stream noting high wind condition and general mine noise. A response was provided to the complainant via email.
20/5/2019		Glendell	Noise & Dust	A complaint was received via the Mt Owen Complex Complaints Hotline by a Camberwell Community member regarding operational noise and dust. The complainant noted "loud machinery noise inside the house and outside all I can taste is dust". Noise levels were below compliance limits at the time and an F-Class temperature inversion was present prior to and at the time of the complaint. The Mining Supervisor reviewed operations and continued to monitor conditions. The Camberwell dust level at the time of the complaint was approximately 23.4µg/m³. A response was provided to the complainant via email.
				June
10/6/19	20:50	Glendell	Noise	A complaint was received via the Mt Owen Complex Complaints Hotline and email via the EPA by a Camberwell Community member regarding operational noise. The complainant noted "loud banging noises coming from the mine site". The mining supervisor reviewed operations at the time of the complaint and amended operations accordingly. Mt Owen Complex Environment and Community staff provided details of
				operations conducted during this period in a response to the EPA. A complaint was received via the Mt Owen Complex Community Complaints
12/6/19	20:03	Glendell	Noise	Hotline by an anonymous community member regarding operational noise. The complainant noted "large bangs, drone noise and very loud, numerous large bangs, machinery noise".
				The mining supervisor reviewed operations at the time of the complaint and amended operations accordingly.
12/6/19	21:50	Glendell	Noise	A complaint was received via the Mt Owen Complex Community Complaints Hotline by an anonymous community member regarding operational noise. The complainant noted "mine machinery noise and a lot of banging coming from Glendell Mine. Mine are making large volumes of noise from heavy machinery that has not stopped all night. It has been going on for the last 3 hours". The mining supervisor reviewed operations at the time of the complaint and amended operations accordingly.
				Mt Owen Complex Environment and Community staff provided details of operations conducted during this period in a response to the EPA.

Date	Time	Site	Nature of Complaint	Company Response
12/6/19	11:09	Glendell	Dust	A complaint was received via the EPA from a Camberwell Community member regarding a blast event at Glendell Mine on 7 June 2019. The blast event was undertaken in accordance with the Mount Owen Complex Blast Management Plan.
				Mount Owen Complex Environment and Community staff provided details of the blast event in a response to the EPA.
29/6/19	12:00 & 6:00	Glendell	Noise	A complaint was received via the Mt Owen Complex Community Complaints Hotline by an anonymous community member regarding operational noise. The complainant noted "noise at both sites".
				The mining supervisor reviewed operations at the time of the complaint and amended operations accordingly.
				July
			No Commi	unity Complaints Received
				August
7/8/19	20:43	Glendell	Noise	A complaint was received via the Mt Owen Complex Community Complaints line by an anonymous community member regarding operational noise. The complainant noted "Loud Banging Noise in the Glendell Mine".
				The mining supervisor reviewed operations at the time of the complaint and amended operations accordingly.
8/8/19	7:40	Glendell	Noise & Dust	A complaint was received via the Mt Owen Complex Community Complaints line by an anonymous community member regarding operational noise.
				The mining supervisor reviewed operations at the time of the complaint and amended operations accordingly.
13/8/19	21:39	Glendell	Noise	A complaint was received via the Mt Owen Complex Community Complaints line by an anonymous community member regarding operational noise. The complainant noted 'Heavy Machinery'.
				The mining supervisor reviewed operations at the time of the complaint and amended operations accordingly.
22/8/19	4:40	Glendell	Lighting &	A complaint was received via the Mt Owen Complex Community Complaints line by a community member located in Middle Falbrook, NSW regarding operational Lighting and Dust.
2210/13	7.70	Cicindon	Dust	The mining supervisor reviewed operations at the time of the complaint and amended operations accordingly. A response was also provided to the EPA regarding operational dust controls during this period.
24/8/19	20:00	Glendell	Noise	A complaint was received via the Mt Owen Complex Community Complaints line by an anonymous community member regarding operational noise. The complainant noted 'Industrial Noise'.
				The mining supervisor reviewed operations at the time of the complaint and amended operations accordingly.
04/0/40	7.05	Clardall	Naiss 9 Dust	A complaint was received via the Mt Owen Complex Community Complaints line by a community member located in Camberwell, NSW regarding operational noise and dust.
24/8/19	7:25	Glendell	Noise & Dust	The mining supervisor reviewed operations at the time of the complaint and amended operations accordingly. The complainant did not wish to be contacted.
05/0/40	7.00	Olar-dall	Naisa 9 Duri	A complaint was received via the Mt Owen Complex Community Complaints line by a community member located in Camberwell, NSW regarding operational noise and dust.
25/8/19	7:22	Glendell	Noise & Dust	The mining supervisor reviewed operations at the time of the complaint and amended operations accordingly. The complainant did not wish to be contacted.
				September

				October				
7/10/19	8:25	Glendell	Noise	A complaint was received via the Mt Owen Complex Community Complaints line by a Camberwell Community member regarding operational noise. Specifically, the complainant noted 'it is ridiculous that you can't listen to a noise monitor in a village'.				
			The mining supervisor reviewed operations at the time of the complaint, and amended operations accordingly.					
				November				
	No Community Complaints Received							
	December							
			No Comm	nunity Complaints Received				
Date	Time	Site	Nature of Complaint	Company Response				
2/9/19	7:17	Glendell	Noise	A complaint was received via the Mt Owen Complex Community Complaints line by an anonymous community member regarding operational noise. The complainant noted 'Industrial Noise'.				
				The mining supervisor reviewed operations at the time of the complaint, and amended operations accordingly.				
3/9/19	7:20	Glendell	Noise	A complaint was received via the Mt Owen Complex Community Complaints line by a community member located in Camberwell, NSW regarding operational noise.				
				No noise alarms had been received the mining supervisor reviewed operations at the time of the complaint, and amended operations accordingly.				

Table 47: MGO Summary of Community Complaints (Mt Owen/Ravensworth East)

Time	Site	Nature of Complaint	Company Response			
January						
No Community Complaints Received						
February						
No Community Complaints Received						
March						
No Community Complaints Received						
April						
No Community Complaints Received						
May						
No Community Complaints Received						
	Time	Time Site	No Community No Community No Community No Community			

June No Community Complaints Received July											
										No Communi	ty Complaints Received
											August
16 Aug 2019	12:08	Mt Owen	Air Quality	The MGO Environment and Community Manager received a complaint via a Department of Planning Industry and Environment (DPIE) Compliance Officer on Friday 16 August 2019 regarding dust emissions at Mt Owen. A response was provided to the DPIE Compliance Officer on 22 September 2019. A subsequent response was provided to DPIE on 6 September 2019.							
			5	September							
			No Communi	ty Complaints Received							
				October							
			No Communi	ty Complaints Received							
				November							
			No Communi	ty Complaints Received							
				December							
			No Communi	ty Complaints Received							