## F. 1 Traffic impact assessment

## Gunlake Quarry Continuation Project (SSD-12469087)

Traffic impact assessment

Prepared for Gunlake Quarries Pty Ltd September 2021

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# Gunlake Quarry Continuation Project 

Traffic Impact Assessment

## Report Number

J190263 RP

## Client

## Gunlake Quarries Pry Ltd

## Date

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## Executive Summary

## ES1 Introduction

Gunlake Quarries Pty Ltd (Gunlake) operates a hard rock quarry (the 'Quarry') located at 715 Brayton Road, Marulan NSW. The Quarry is approximately 7 kilometres (km) north-west of the centre of Marulan in the Goulburn Mulwaree local government area. The land surrounding the Quarry is rural land with a low population density. Gunlake commenced operations in 2009 under project approval 07-0074 granted in September 2008.

Since the Quarry received approval for the Extension Project in 2017 (SSD 7090, NSW Land and Environmental Court Approval 20017/108663), the tonnage of saleable product dispatched by the Quarry has steadily increased and, with an infrastructure boom across the State, Gunlake forecast that demand for products from the Quarry will continue to increase. In response to the increased demand for products from the Quarry, it is proposed to transport more saleable product along the Primary Transport Route. This will require an increase in truck movements than what is currently approved. The additional truck movements will all occur on the recently upgraded Primary Transport Route that has been designed to accommodate comfortably the additional truck movements. The Project is known as the Gunlake Quarry Continuation Project (the 'Continuation Project'). The ignimbrite hard-rock resource will continue to be extracted and processed using the methods currently employed at the Quarry.

The Continuation Project is classified as a State Significant Development (SSD) under Schedule 1, Clause 7 of the State Environmental Planning Policy (State and Regional Development) 2011 (SRD SEPP). This report accompanies a new SSD application and environmental impact statement (EIS) for the Continuation Project.

## ES2 Gunlake Quarry Continuation Project

Gunlake seeks a new development approval for the Continuation Project that allows:

- ongoing Quarry operations;
- a maximum of 375 inbound and 375 outbound daily truck movements with up to 4.2 million tonnes per annum (Mtpa) of Quarry products transported from the site in any calendar year;
- 24-hours Quarry operations Monday to Saturday, except 6 pm Saturday to 2 am Monday;
- an extraction depth of 546 metres Australian Hight Datum (mAHD); and
- a 30-year Quarry life (from the date of Continuation Project approval).


## ES3 Evaluation of the project

The associated traffic impacts for the proposed continuation project traffic and potential cumulative traffic have been assessed as follows:

- the future cumulative traffic volumes (ie Gunlake Quarry traffic plus the approved/proposed traffic from approved local quarries and residential subdivision) at the end of the proposed Quarry life (2051) was calculated by adding: combined non-Gunlake project development traffic; future background traffic; and Continuation Project traffic;
- based on SIDRA analysis of the existing background traffic volumes, the five key intersections currently operate with a Level of Service (LOS) A;
- based on SIDRA analysis of future (2051) cumulative traffic volumes, the five key intersections will continue to operate with a LOS A; and
- the sight distance at the site access complies with Austroads guidelines.

Road safety is addressed in in the Road Safety Assessment Report (ARRB 2021, EIS Appendix F.2).

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## Abbreviations

AM
AS
CBD
CTMP
TCP
DA
DEL
DOS
DP
DPIE
EIS
ha
HV
km
LEC
LGA
LOS
m
NHVR
PM
Q95
TfNSW
RMS
SEARs
SRD SEPP
SSD
TIA
morning
Australian Standard
central business district
construction traffic and management plan
traffic control plan
development application
average delay
Degree of Saturation
Deposited Plan
NSW Department of Planning, Industry and Environment
environmental impact statement
hectares
heavy vehicles
kilometre
Land \& Environment Court
local government area
Level of Service
light vehicles
metres
National Heavy Vehicle Regulator
Afternoon
95\% queue lengths
Transport for New South Wales
NSW Roads and Maritime Services, now TfNSW
Secretary's environmental assessment requirements
State Environmental Planning Policy (State and Regional Development) 2011
State significant development
traffic impact assessment

## 1 Introduction

### 1.1 Overview

Gunlake Quarries Pty Ltd (Gunlake) operates a hard rock quarry (the 'Quarry') located at 715 Brayton Road, Marulan NSW. The Quarry is approximately 7 kilometres (km) north-west of the centre of Marulan in the Goulburn Mulwaree local government area (Figure 1.1). The land surrounding the Quarry is rural land with a low population density. Gunlake commenced operations in 2009 under project approval 07-0074 granted in September 2008.

Since the Quarry received approval for the Extension Project in 2017 (SSD 7090, NSW Land and Environmental Court Approval 20017/108663), the tonnage of saleable product dispatched by the Quarry has steadily increased and, with an infrastructure boom across the State, Gunlake forecast that demand for products from the Quarry will continue to increase. In response to the increased demand for products from the Quarry, it is proposed to transport more saleable product along the Primary Transport Route. This will require an increase in truck movements than what is currently approved. The additional truck movements will all occur on the recently upgraded Primary Transport Route that has been designed to accommodate comfortably the additional truck movements. The Project is known as the Gunlake Quarry Continuation Project (the 'Continuation Project'). The ignimbrite hard-rock resource will continue to be extracted and processed using the methods currently employed at the Quarry.

The Continuation Project is classified as a State Significant Development (SSD) under Schedule 1, Clause 7 of the State Environmental Planning Policy (State and Regional Development) 2011 (SRD SEPP). This report accompanies a new SSD application and environmental impact statement (EIS) for the Continuation Project.

### 1.2 Assessment approach and requirements

This Traffic Impact Assessment (TIA) has been prepared generally in accordance with the requirements of the NSW Government's Guide to Traffic Generating Developments (RTA 2002) and incorporated the following investigations and analysis:

- background traffic data review;
- $\quad$ site inspection and current traffic surveys;
- SIDRA intersection analysis;
- mid-block analysis;
- future road upgrade requirements and maintenance impacts; and
- reporting.

A visual inspection of the primary affected roads, including Hume Highway, Marulan South Road, Brayton Road, Ambrose Road and Red Hills Road, was undertaken on 23 September 2020 to confirm the current general road widths and traffic conditions for these routes and photographs have been taken at the key project access intersections.

The TIA was prepared in accordance with the requirements of the Planning Secretary's Environmental Assessment Requirements (SEARs) for the proposed development, issued on 6 May 2021. The SEARs identify matters which must be addressed in the EIS. The individual requirements relevant to this TIA and where they are addressed in this report are provided in Table 1.1.

Table 1.1 SEARs relating to traffic and transport

## Item no. Assessment requirement from SEARs

EMM responses/information location

1. accurate predictions of the road traffic generated by the development, including a description of the types of vehicles likely to be used for transportation of quarry products;
2. a detailed assessment of potential traffic impacts on the capacity, condition, safety and efficiency of the local and State Road network (as identified above), including undertaking a road safety audit; and

Sections 6.1, 6.3 and 6.4
Separate Road Safety Impact Report (including a road safety audit) provided in EIS Appendix F. 2 (ARRB 2021)
3. a description of the measures that would be implemented to mitigate any impacts.

Section 6.4
Separate Road Safety Impact Report provided in EIS Appendix F. 2 (ARRB 2021)


## 2 Project description and setting

### 2.1 The site

The Quarry is located wholly on Lot 13 DP 1123374 (the 'Quarry site'). There are biodiversity management areas in Lot 13 DP1123374, Lot 12 DP1123374, Lot 271 DP750053 and Lot 1 DP841147. These lots are owned by Gunlake Quarries Pty Ltd.

The land surrounding the Quarry is rural with low population density, predominately used for agriculture, generally grazing. Built features immediately surrounding the Quarry include dams, access tracks and fences. There are a small number of residences around the Quarry (Figure 2.1). The nearest town is Marulan, about 7 km south-east of the site boundary.

There are four local operational quarries within approximately 15 km of the Quarry site: Lynwood Quarry; Peppertree Quarry; Marulan South Limestone Mine; and Johnniefelds Quarry.


### 2.2 Continuation Project description

Gunlake seeks a new development approval for the Continuation Project that allows:

- ongoing Quarry operations;
- a maximum of 375 inbound and 375 outbound daily truck movements with up to 4.2 million tonnes per annum (Mtpa) of Quarry products transported from the site in any calendar year;
- 24-hours Quarry operations Monday to Saturday, except 6 pm Saturday to 2 am Monday;
- an extraction depth of 546 metres Australian Hight Datum (mAHD); and
- a 30-year Quarry life (from the date of Continuation Project approval).

A summary of the key elements of the approved Extension Project compared to the Continuation Project is provided in Table 2.1.

Table 2.1 Extension Project compared to the Continuation Project

| Project element | Approved Extension Project | Proposed Continuation Project |
| :---: | :---: | :---: |
| Extraction method | Blasting and excavation. | Blasting and excavation. |
| Resource | Ignimbrite hard-rock. | Ignimbrite hard-rock. |
| Extraction | Quarry pit - pit depth of 572 mAHD. | Quarry pit - pit depth of 546 mAHD (ie 26 m deeper than the Extension Project). <br> No change to pit disturbance area. |
| Operations | Onsite rock processing, including crushing and screening. | Onsite rock processing, including crushing and screening. |
| Product transport | Transport of up to 2.6 million tonnes per annum (Mtpa) of Quarry products. <br> Truck movements limited to: <br> - a maximum of 295 inbound movements and 295 outbound movements, including no more than 38 outbound truck movements on the Secondary Transport Route, per working day; and <br> - an average of 220 inbound movements and 220 outbound movements, including no more than 25 outbound movements on the Secondary Transport Route, per working day (averaged over the working days in each quarter). | Transport of up to 4.2 Mtpa of quarry products. <br> Total truck movements limited to: <br> - a maximum of 375 inbound movements and 375 outbound movements, including no more than 38 outbound laden movements on the Secondary Transport Route, per working day; <br> - an average of no more than 25 outbound movements on the Secondary Transport Route, per working day (averaged over the working days in each quarter). |

General infrastructure Offices, amenity buildings, processing plant and other Offices, amenity buildings, processing plant and other minor infrastructure. minor infrastructure.

| Project element | Approved Extension Project | Proposed Continuation Project |
| :---: | :---: | :---: |
| Management of wastes | Overburden ${ }^{1}$ is emplaced in designated emplacement areas. | Overburden is emplaced in designated emplacement areas. |
|  | Receipt of up to 30,000 tonnes of cured concrete per calendar year for beneficial reuse/recycling. | Receipt of up to 50,000 tonnes of cured concrete per calendar year for beneficial reuse/recycling. |
|  | No other classified waste materials to be received on site. | No other classified waste materials to be received on site. |
| Hours of operation | 24-hours Quarry operations Monday to Saturday, except 6 pm Saturday to 2 am Monday. | 24-hours Quarry operations Monday to Saturday, except 6 pm Saturday to 2 am Monday. |
| Blasting | Up to twice weekly, 9 am to 5 pm Monday to Friday. | Up to twice weekly, 9 am to 5 pm Monday to Friday. |
| Quarry life | To 30 June 2042. | Extension of the Quarry life to 30 years from the date of approval. |

Further information on the project is available in the Continuation Project EIS.

### 2.3 Product transport

### 2.3.1 Transport routes

All saleable products are transported from the Quarry to markets by truck. The Continuation Project will continue to use the currently approved Primary and Secondary Transport Routes.

Trucks delivering Quarry products to markets to the north and returning from these destinations use the Primary Transport Route (Figure 2.2). The Primary Transport Route consists of the following roads:

- Brayton Road (classified as a collector road) between Ambrose Road and the Gunlake Quarry access road;
- Ambrose Road between Brayton Road and Red Hills Road; and
- Red Hills Road between Ambrose Road and the Hume Highway.

The eastern end of Red Hills Road can only be accessed from the northbound side of the Hume Highway. Inbound Quarry trucks, returning from the north, are required to pass the Red Hills Road intersection and use the South Marulan Road interchange, approximately 3.5 km south-west of Marulan, to leave the southbound highway, cross the interchange bridge and join the northbound highway before travelling north to exit the highway at Red Hills Road (Figure 2.2).

The Primary Transport Route between the Quarry and the Hume Highway is about 7.8-km long.
The Secondary Transport Route is only used by outbound trucks travelling to markets south of the Quarry. The Secondary Transport Route consists of Brayton Road between the Quarry access road and the Hume Highway's southbound access ramp at Marulan.

[^0]
### 2.3.2 Vehicle movements

The Continuation Project will transport no more than 4.2 Mtpa of Quarry products transported from the site in any calendar year.

Under the Continuation Project it is proposed to limit daily Quarry product truck movements to a maximum of 375 inbound and 375 outbound movements.

Gunlake currently has approval for a daily average of 25 outbound Quarry product truck movements, and a daily maximum of 38 outbound Quarry product trucks movements on the Secondary Transport Route. It is not proposed to change the number of trucks that are allowed to use the Secondary Transport Route.

There are also a small number of transport movements associated with employee travel, fuel deliveries and service vehicles.


## 3 Existing conditions

### 3.1 Site location and access

Gunlake Quarry is located at 715 Brayton Road in Marulan, NSW, legally described as Lot 13 of DP1123374 within the Goulburn Mulwaree local government area (LGA). The Marulan township is located to the south-east of the Quarry with residential land uses generally to the west of the town centre and industrial land uses further west. The Quarry is accessed via Brayton Road.

### 3.2 Road network

The NSW administrative road hierarchy comprises the following road classifications, which align with the generic road hierarchy as follows:

- state roads - freeways and primary arterials (managed by Transport for NSW (TfNSW));
- regional roads - secondary or sub arterials (council managed and part funded by the NSW Government); and
- local roads - collector and local access roads (council managed).

Each of the key roads along the Primary Transport Route are shown in Figure 2.1 and Figure 2.2 above.
A summary of each road on the Primary and Secondary Transport Routes and the Hume Highway in the region is provided in Table 3.1 to Table 3.5.

Table 3.1 Brayton Road (between Gunlake site access and Ambrose Road intersection)

| Aspect | Description |
| :--- | :--- |
| Transport Route | Primary and Secondary (inbound and outbound) |
| Road classification and connectivity | Local road (collector road) |
| Alignment | North-west/south-east |
| Number of lanes | One lane each way |
| Carriageway type | Sealed road |
| Carriageway width | Typically 11 m with 3.25 travel lane each way, plus 1.25 m sealed shoulder and 0.5 m <br> unsealed shoulder on either side as well as a 1-m wide centreline |
| Default speed limit | $100 \mathrm{~km} / \mathrm{h}$ |
| Heavy vehicle access | $26 \mathrm{~m} \mathrm{B-double}$ approved |
| Traffic function | Carries local traffic, including Quarry trucks |



Plate 3.1 Brayton Road (looking north-east on Brayton Road)

Table 3.2 Brayton Road (between Ambrose Road intersection and the Georges Road/Hume Highway interchange)

| Aspect | Description |
| :--- | :--- |
| Transport Route | Secondary (outbound only) |
| Road classification and connectivity | Local road |
| Alignment | East-west |
| Number of lanes | One lane each way |
| Carriageway type | Sealed road |
| Carriageway width | Approximately 11 m wide carriageway with 0.5 m centreline |
| Default speed limit | $50 \mathrm{~km} / \mathrm{h}$ |
| Heavy vehicle access | 26 m B -double approved |
| Traffic function | Carries local traffic, including limited Gunlake Quarry trucks |



Plate 3.2 Brayton Road (looking east from near Station Street)

Table 3.3 Ambrose Road

| Aspect | Description |
| :--- | :--- |
| Transport Route | Primary (inbound and outbound) |
| Road classification and connectivity | Local road |
| Alignment | East/west |
| Number of lanes | One lane each way |
| Carriageway type | Sealed road |
| Carriageway width | Typically 11 m with 3.25 m travel lane each way, plus 1.25 m sealed shoulder and <br> 0.5 m unsealed shoulder on either side as well as a 1 m wide centreline <br> Default speed limit <br> Heavy vehicle access <br> Traffic function $100 \mathrm{~km} / \mathrm{h}$ |



Plate 3.3 Ambrose Road (looking west on Ambrose Road)

Table 3.4 Red Hills Road

| Aspect | Description |
| :--- | :--- |
| Transport Route | Primary (inbound and outbound) |
| Road classification and connectivity | Local road |
| Alignment | East/west |
| Number of lanes | One lane each way |
| Carriageway type | Sealed road |
| Carriageway width | Typically 11 m with 3.25 m travel lane each way, plus 1.25 m sealed shoulder and 0.5 m <br> unsealed shoulder on either side as well as a 1 m wide centreline <br> Default speed limit <br> Heavy vehicle access <br> Traffic function |



Plate 3.4 Red Hills Road (looking west from close to the Hume Highway)

Table 3.5 Hume Highway

| Aspect | Description |
| :--- | :--- |
| Road classification and connectivity | State road |
| Alignment | North-east/south-west |
| Number of lanes | Two lanes each way at the vicinity of the site |
| Carriageway type | Dual carriageway with central median island |
| Carriageway width | Approximately 32 m with 3.5 m travel lanes each way and 18 m wide median island |
| Posted speed limit | $110 \mathrm{~km} / \mathrm{h}$ in the vicinity of the site |
| Heavy vehicle access | 26 m B-double approved |
| Traffic function | Provides arterial connection between townships |



Plate 3.5 Hume Highway (looking north-east towards Red Hills Road)

### 3.3 Key intersections

The key intersections along the Primary and Secondary Transport Routes for which Quarry-related traffic impacts have been assessed are shown in Figure 3.1 and are described in Table 3.6 to Table 3.10.


Source: Google Maps
Figure 3.1 Key intersections

Table 3.6

| Aspect | Description |
| :--- | :--- |
| Location | 4.3 km south-east of the site |
| Intersection control | Give Way controlled |
| Major road | Brayton Road |
| North-western approach | One lane on approach and departure |
| South-eastern approach | One lane on approach and departure |
| North-eastern approach | One lane on approach and departure |
| Traffic function | Predominantly carries local traffic, including Quarry trucks |



Plate 3.6 Brayton Road/Ambrose Road intersection

Table 3.7 Hume Highway/Red Hills Road

| Aspect | Description |
| :--- | :--- |
| Location | 7.8 km south-east of the site |
| Intersection control | Priority |
| Major road | Hume Highway |
| North approach | One lane on approach and departure |
| East approach | Two eastbound travel lanes, plus approximately 580 m long eastbound acceleration |
|  | lane |
| West approach | Two eastbound travel lanes, plus approximately 130 m long eastbound deceleration |
|  | lane |
| Traffic function | Predominantly carries arterial traffic, including Quarry trucks |



Plate 3.7 Hume Highway/Red Hills Road intersection

Table 3.8 George Street/Brayton Road

| Aspect | Description |
| :--- | :--- |
| Location | 7 km south-east of the site |
| Intersection control | Priority |
| Major road | George Street |
| North-east approach | One lane on approach and departure |
| North-west approach | One lane on approach and departure |
| South-east approach | One lane on approach and departure |
| South-west approach | One lane on approach and departure |
| Traffic function | Predominantly carries local traffic, including secondary route Quarry trucks |



Plate 3.8
George Street/Brayton Road intersection

Table 3.9

| Aspect | Description |
| :--- | :--- |
| Location | Approx. 3.3km south-west from Marulan |
| Intersection control | Roundabout |
| North-western approach | One lane on approach and departure |
| South-eastern approach | One lane on approach and departure |
| North-eastern approach | One lane on approach |
| South-western approach | One lane on approach and departure |
| Traffic function | Predominantly carries local traffic, including Quarry trucks |



Plate 3.9 Hume Highway Off Ramp/Jerrara Road/Marulan South Road intersection

| Aspect | Description |
| :--- | :--- |
| Location | Approx. 3.3km south-west from Marulan |
| Intersection control | Priority controlled |
| North-western approach | One lane on approach and departure |
| South-eastern approach | One lane on approach and departure |
| North-eastern approach | One lane on departure |
| South-western approach | One lane on approach |
| Traffic function | Predominantly carries local traffic, including Quarry trucks |



Plate 3.10
Hume Highway On Ramp/Hume Highway Off Ramp/Jerrara Road intersection

### 3.4 Baseline traffic volumes

### 3.4.1 Existing traffic volumes

i Intersection counts
The intersections were surveyed for 24 -hour periods on Thursday, 10 September 2020 and Wednesday, 16 September 2020. Therefore, the traffic volumes from traffic surveys are less than a year old.

The traffic count data is provided inAnnexure A.
The peak hour traffic varied between intersections. The survey results indicate the following peak hours:

- Brayton Road/Ambrose Road:
- AM peak hour: 8.15 am-9.15 am
- PM peak hour: $3.30 \mathrm{pm}-4.30 \mathrm{pm}$
- Hume Highway/Red Hills Road:
- AM peak hour: $11.00 \mathrm{am}-12.00 \mathrm{pm}$
- PM peak hour: $3.45 \mathrm{pm}-4.45 \mathrm{pm}$
- George Street/Brayton Road
- AM peak hour: 8.30 am-9.30 am
- PM peak hour: $3.00 \mathrm{pm}-4.00 \mathrm{pm}$
- Hume Highway Off Ramp/ Jerrara Road/ Marulan South Road:
- AM peak hour: 6.45 am-7.45 am
- PM peak hour: $3.15 \mathrm{pm}-4.15 \mathrm{pm}$
- Hume Highway On Ramp/ Hume Highway Off Ramp/ Jerrara Road:
- AM peak hour: 5.15 am-6.15 am
- PM peak hour: $3.30 \mathrm{pm}-4.30 \mathrm{pm}$

Due to the proximity of the Hume Highway Off Ramp/Jerrara Road/Marulan South Road and Hume Highway On Ramp/Hume Highway Off Ramp/Jerrara Road intersections, the network peak hours ${ }^{2}$ are adopted for these two intersections for the purpose of intersection analysis, as follows:

- AM peak hour: $6.45 \mathrm{am}-7.45 \mathrm{am}$; and
- PM peak hour: $3.15 \mathrm{pm}-4.15 \mathrm{pm}$.

The surveyed traffic volumes during the AM and PM peak hours are summarised in Figure 3.2 for light vehicles (LV) and heavy vehicles (HV).

The traffic volume data show that with the exception of the Hume Highway, the other intersections are generally not heavily trafficked.

The Brayton Road/George Street intersection has relatively higher traffic volumes along the north-west and southwest approaches. This is mainly because there is residential development along these sections of the road, hence contributing to higher traffic volumes.

[^1]

Figure 3.2
Existing AM and PM peak surveyed baseline intersection traffic volume

Tube counts were undertaken at three locations over a seven-day period from 10 June 2020. The tube count data are presented in Figure 3.3. While the traffic volumes from the tube are approximately 14 months old, the baseline traffic volumes are not anticipated to have changed over this period. The impact assessment in Chapter 6 allows for long-term annual background traffic growth.


Figure 3.3 Tube count data
The traffic data shows that Ambrose Road carried just below 400 vehicles per day with $60 \%$ heavy vehicles.
Brayton Road, west of Ambrose Road, carried close to 800 vehicles per day with an average $42 \%$ heavy vehicles. Both the volumes and heavy vehicle proportion is lower for the count undertaken east of Ambrose Road, with below 600 vehicles per day with an average $15 \%$ heavy vehicles. This is expected given that the Primary Transport Route bypasses Marulan township.

Intersection and tube count data are attached in Annexure A.

### 3.4.2 Existing site related traffic volumes

The Gunlake Quarry weighbridge data for outgoing heavy vehicle movements on 10 September and 16 September 2020 (traffic survey dates) are provided in Table 3.11.

Table 3.11 Peak hour outgoing heavy vehicle movements from Gunlake Quarry

| Survey date | Relevant road network peak hours* | Outgoing heavy vehicle movements |
| :--- | :---: | :---: |
| 10 September 2020 | $8.15 \mathrm{am}-9.15 \mathrm{am}$ | 7 |
|  | $8.30 \mathrm{am}-9.30 \mathrm{am}$ | 7 |
|  | $11.00 \mathrm{am}-12.00 \mathrm{pm}$ | 6 |
|  | $3.00 \mathrm{pm}-4.00 \mathrm{pm}$ | 9 |
| 16 September 2020 | $3.30 \mathrm{pm}-4.30 \mathrm{pm}$ | 10 |
|  | $3.45 \mathrm{pm}-4.45 \mathrm{pm}$ | 10 |

[^2]Trucks use the approved routes and it has been assumed that the inbound and outbound trips are equal within each hour. Based on this assumption, the site related heavy vehicles at each of the key intersections are presented in Figure 3.4.


Figure 3.4
Existing AM and PM peak site related traffic volume

### 3.4.3 Existing background traffic volumes

The intersection and tube surveys include existing traffic from Gunlake Quarry. The 'background traffic volume' (ie the traffic volume if Gunlake Quarry was not operating) has been calculated by subtracting Quarry traffic from the surveyed baseline traffic volume.

### 3.5 Crash analysis

Crash data from the TfNSW Centre for Road Safety is presented in the Road Safety Impact Assessment report (ARRB 2021, EIS Appendix F.2).

### 3.6 Public transport

Due to the remote location of the site, there are no public bus services near the Quarry which could be used by Quarry staff or visitors.

School buses travel along Brayton Road in the vicinity of the site in both directions each school day. The school buses drop off and collect school children along this route. As part of the recent road upgrades of Brayton Road financed by Gunlake, safe school bus collection/drop off points have been built along Brayton Road.

## 4 Proposal

### 4.1 Description

The proposal will result in an increase in Quarry product truck movements via the Primary Transport Route from a maximum of 295 outbound and 295 inbound truck movements per day to a maximum of 375 outbound and 375 inbound truck movements per day. A comparison of the currently approved and proposed vehicular activity is provided in Table 4.1.

Table 4.1 A comparison of currently approved and proposed vehicular activity

| Description | Currently approved | Proposed |
| :---: | :---: | :---: |
| Maximum daily Quarry product truck movements | 295 outbound and 295 inbound movements | 375 outbound and 375 inbound movements |
| Maximum daily Quarry product truck movements on Primary Transport Route | As above | As above |
| Maximum daily Quarry product truck movements on Secondary Transport Route | No more than 25 outbound trucks movements with a maximum of 38 per day | No change |
| Quarry life | 25 years to 30 June 2042 | 30 years (nominally to 2051) |
| Hours of operation | Truck loading and dispatching, and transportation on the Primary Transport Route is approved to occur 24 hours a day, except from 6 pm Saturday evenings to 2 am Monday morning or on public holidays. <br> Transportation on the Secondary Transport Route is approved to occur 6 am to 7 pm Monday to Saturday but not on Sundays or public holidays | No change |

### 4.2 Hours of operation

As stated in Table 4.1, it is not proposed to alter the currently approved hours of operation, which permits truck loading and dispatching, and transportation as follows:

- Primary Transport Route: 24 hours a day, except from 6 pm Saturday evenings to 2 am Monday morning or on public holidays; and
- Secondary Transport Route: 6 am to 7 pm Monday to Saturday but not on Sundays or public holidays.


### 4.3 Workforce

The Quarry currently employs about 52 staff. In addition, about 20 contractors work on the Quarry site. The workforce may increase to 70 full-time positions for the Continuation Project and with ongoing opportunities for the contractors.

In addition, around 200 contract truck drivers deliver products from the Quarry. The proposed project will provide further work for these drivers and opportunities for more drivers.

### 4.4 Operational traffic

### 4.4.1 Vehicle types

The transport routes are currently permitted for all vehicles up to 26 m in length (including rigid vehicles, truck and dogs, B-doubles and A-doubles). The types of vehicles used currently and in the future are as dictated by TfNSW road restrictions.

### 4.4.2 Peak hour traffic generation

A maximum of 40 trucks will be loaded per hour at the Quarry as part of the Continuation Project, which translates to a maximum of 40 outbound trucks dispatched during a peak hour.

The employee, fuel deliveries and service vehicles generally arrive and depart outside the commuter peak hours. Therefore, these limited trips are not included in the traffic assessment.

### 4.4.3 Traffic generation and distribution

As stated in Table 4.1, it is proposed that there will be a daily maximum of 375 outbound and 375 inbound Quarry product truck movements.

There will be no change in the number of approved Quarry product truck movements along the Secondary Transport Route (an average of 25 outbound movements per day). As such, the traffic surveys completed for this assessment would include these movements.

For a conservative assessment of peak hour traffic impacts, this TIA assumes that all peak hour Quarry product truck movements (a maximum 40 trucks) would be dispatched along the Primary Transport Route.

The Continuation Project traffic volumes are presented in Figure 4.1.


Figure 4.1 AM and PM peak Continuation Project traffic volume

### 4.5 Construction traffic

Construction of a new weighbridge and road resurfacing activities will occur within the next few years as part of ongoing quarry operations. These activities will be relatively short-term duration and will generate negligible construction traffic. Given the preceding, a detailed assessment of construction traffic impacts has not been included within this report.

### 4.6 Road upgrade work

The Primary Transport Route has been substantially upgraded in accordance with the Austroads Guidelines (Geometric Design Table 4.5) for rural roads with 1,000 to 3,000 average vehicle movements per day (Austroads 2020) since the Land and Environment Court Approval was granted in 2017. Gunlake and Goulburn Mulwaree Council have implemented a road maintenance work plan and budget to ensure that the Transport Routes are properly maintained by Council using Gunlake Section 94 Contributions. Gunlake and Council will continue to work together on road maintenance Section 7.11 contributions and any road upgrades that may be required as part of the Continuation Project

The Primary Transport Route road design has been independently reviewed by the Australian Road Research Board, the findings of which are provided in Appendix F. 2 of the EIS.

## 5 Future traffic volumes

### 5.1 Future traffic volumes components

The traffic impacts of the Continuation Project are assessed in Chapter 6 based on the following future traffic volumes components:

- combined non-Gunlake project development traffic;
- the linear growth in background traffic; and
- Continuation Project traffic (see Chapter 4).

Future traffic volumes, excluding Gunlake Quarry traffic, are described below.


## $\square$ Site boundary

( Quarry

- Future residential subdivision


### 5.2 Non-Gunlake project development traffic

### 5.2.1 Local quarries

There are five local operational quarries:

- Lynwood Quarry;
- Peppertree Quarry;
- Marulan South Limestone Mine (limestone quarries are officially defined as a mine in NSW);
- Ardmore Park Quarry; and
- Johnniefelds Quarry.

These quarries currently use the following intersections as part of their transport routes:

- Hume Highway Off Ramp/Jerrara Road/ Marulan South Road; and
- Hume Highway On Ramp/Hume Highway Off Ramp/Jerrara Road.

Johnniefelds Quarry is the only operation, other than Gunlake Quarry, that uses the Brayton Road/Ambrose Road/Red Hills Road section of the Primary Transport Route.

The approved traffic generation for these quarries have been extracted from publicly traffic reports and approvals. It has been assumed that any current development applications, such as for the Marulan South Limestone Mine Continuation Project, will be approved.

The traffic generation for each of the five quarries at full capacity is presented in Table 5.1 and shown in Figure 5.2 to Figure 5.6.

Table 5.1 Traffic generation from the nearby quarries (including proposals)
\(\left.$$
\begin{array}{lcccc}\text { Quarry } & \begin{array}{c}\text { Annual truck } \\
\text { movements }\end{array} & \begin{array}{c}\text { Daily truck } \\
\text { movements }\end{array} & \begin{array}{c}\text { Peak hourly truck Source } \\
\text { movements }\end{array} \\
\hline \begin{array}{l}\text { Marulan South } \\
\text { Limestone Mine }\end{array} & 16,718 & 218 & 18 & \begin{array}{l}\text { Proposed Marulan South Limestone Mine Continued } \\
\text { Operations Project }\end{array}
$$ <br>
Traffic Impact Assessment (Transport \& Urban Planning <br>

2019)\end{array}\right]\)| Modification 6 |
| :--- |
| Peppertree <br> Quarry |
| 1,460 |
| Ardmore Park <br> Quarry |
| 36,608 |

[^3]

Figure 5.2
Marulan South Limestone Mine peak hour traffic


Figure 5.3 Peppertree peak hour traffic


Figure 5.4 Ardmore Park Quarry peak hour traffic


Figure 5.5 Lynwood Quarry peak hour traffic


Figure 5.6 Johnniefelds peak hour traffic

### 5.2.2 Recent residential subdivision

There is a residential subdivision currently under construction, located off Corriedale Drive west of Brayton Road and near the Merino Road/Brayton Road intersection (Figure 5.1). The subdivision can only be accessed from Merino Road south of the Brayton Road/Ambrose Road intersection, with no access from Brayton Road north of this intersection (ie there is no access to the subdivision from the Primary Transport Route and no change to quarry truck movements is proposed on the Secondary Transport Route).

The RMS Guide to Traffic Generating Developments Updated traffic surveys (RMS 2013) provides trip generation rates for low-density residential dwellings. The trip generation rates are provided in Table 5.2.

Table 5.2 Trip generation rate low density residential dwellings

|  | Sydney |  | Regional areas |  |
| :--- | :---: | :---: | :---: | :---: |
|  | Regular rate | Maximum rate | Regular rate | Maximum rate |
| Daily vehicle trips | 10.7 | - | 7.4 | - |
| Weekday average evening peak hour <br> vehicle trips | 0.99 | 1.39 | 0.78 | 0.90 |
| Weekday average morning peak hour <br> vehicle trips | 0.95 | 1.32 | 0.71 | 0.85 |

A conservative trip generation rate of one trip per lot for morning and evening peak hours has been adopted for this study, which is up to 53 trips during the morning and evening peak hours. The following trip assumptions have been made:

- $20 \%$ and $80 \%$ split has been used for morning in and out movements respectively;
- $70 \%$ and $30 \%$ split has been used for evening in and out movements respectively;
- $90 \%$ of the trips would be to travel south (towards Goulburn) and $10 \%$ north (towards Sydney) from the Brayton Road/Merino Road intersection; and
- the traffic distribution at Brayton Road/George Street intersection is as per ratios of existing traffic distribution from the traffic surveys.

The traffic generation for the residential subdivision off Corriedale Drive is shown in Figure 5.7.


Figure 5.7 Residential subdivision of Corriedale Drive peak hour traffic

The total combined potential traffic generation from the surrounding projects - five local quarries (at full capacity) and residential subdivision (when fully developed) - is presented in Figure 5.8.


Figure 5.8 Combined traffic of the five nearby quarries (at full capacity) and residential subdivision (when fully developed)

### 5.3 Future background traffic

The Quarry life is proposed to be extended by 30 years to 2051 . Future background traffic volumes have been calculated for 2051 future scenario by applying the following growth rates to the existing background traffic volume (ie, excluding Gunlake Quarry traffic) (see Section 3.4.3):

- $0.5 \%$ per annum (pa) linear growth on arterial roads; and
- $\quad 1 \%$ pa linear growth on local roads.

This growth allows for potential residential developments in the local area over the next 30 years, such as development of the Marulan North and Marulan West areas as included in the Urban and Fringe Housing Strategy, Goulburn and Marulan (Elton 2020).

These growth projections are consistent with the Department of Planning, Industry and Environment population projections (DPIE 2019) that estimate the population of the regional area will increase from 79,259 in 2016 to 84,971 in 2041 - a total increase of $7.2 \%$ and an average annual increase of $0.3 \%$.

### 5.4 Future cumulative traffic

The future (2051) cumulative traffic volumes (ie Gunlake Quarry traffic plus all non-Gunlake Quarry traffic) at the end of the proposed Quarry life (2051) was calculated by adding:

- combined non-Gunlake project development traffic (Section 5.2.3);
- future background traffic (Section 5.3); and
- $\quad$ Continuation Project traffic (Section 4.4.3).

The future cumulative traffic volumes are presented in Figure 5.9. These volumes have been used for SIDRA modelling of the potential impact of the Continuation Project on intersection performance.


Figure 5.9
Future (2051) cumulative traffic volumes (ie Gunlake Quarry traffic plus all non-Gunlake Quarry traffic)

## 6 Impact assessment

### 6.1 Intersection performance

The key intersections have been modelled with the SIDRA Intersection 9.0 software; a micro-analytical tool for individual intersections and linked intersection-network modelling. The modelling is based on the traffic survey data detailed in Section 3.4.1 and the continuation project traffic with net cumulative traffic, as detailed in Section 5.4. SIDRA provides the following performance indicators:

- Degree of saturation (DOS) - the total usage of the intersection expressed as a factor of 1 with 1 representing $100 \%$ use/saturation (eg $0.8=80 \%$ saturation);
- Average delay (DEL) - the average delay in seconds encountered by all vehicles passing through the intersection. It is often important to review the average delay of each approach as a side road could have a long delay time, while the large free flowing major traffic will provide an overall low average delay;
- Level of service (LOS) - this is a categorisation of average delay, intended for simple reference; and
- $\quad 95 \%$ queue lengths (Q95) - is defined to be the queue length in metres that has only a $5 \%$ probability of being exceeded during the analysed time period. It transforms the average delay into measurable distance units.

The LOS is a good indicator of overall performance for individual intersections, with each level summarised in Table 6.1.

Table 6.1 Intersection LOS standards

| Level of <br> service | Average delay <br> (seconds per vehicle) | Traffic signals, roundabout | Priority intersection ('Stop' and 'Give Way') |
| :--- | :---: | :--- | :--- |
| A | $<14$ | Good operation | Good operations |
| B | 15 to 28 | Good with acceptable delays and spare <br> capacity | Acceptable delays and spare capacity |
| C | 29 to 42 | Satisfactory | Satisfactory, but accident study required |
| D | 43 to 56 | Operating near capacity | Near capacity and accident study required |
| E | 57 to 70 | At capacity. At traffic signals, incidents will <br> cause extensive delays. <br> Roundabouts require other control mode. | At capacity; required other control mode |
| F | $>71$ | Unsatisfactory with excessive queuing | Unsatisfactory with excessive queuing; required <br> other control mode |

Source: RTA Guide to Traffic Generating Development (RTA 2002).
Two scenarios have been modelled in SIDRA and they are as follows:

1. Existing: this scenario assesses the surveyed baseline traffic volumes.
2. Future 2051: this scenario assesses cumulative traffic volumes for 2051 (ie all non- Gunlake Quarry traffic with Gunlake Quarry traffic).

The SIDRA results for the key intersections are presented in the following tables. The details of the SIDRA results are attached in Annexure B.

Table 6.2 SIDRA modelling result for Brayton Road/Ambrose Road intersection

| Control/scenarios | AM Peak |  |  |  |  | PM Peak |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Priority controlled (Give Way) | Intersection volume | DEL(s) | LOS | DOS | Max $\mathbf{Q}$ in m (approach) | Intersection volume | DEL(s) | LOS | DOS | Max $\mathbf{Q}$ in m (approach) |
| 1. Existing | 61 | 9.1 | A | 0.021 | 0.8 (north-east) | 71 | 10.0 | A | 0.022 | $\begin{aligned} & 0.3 \text { (north- } \\ & \text { east) } \end{aligned}$ |
| 2. Future 2051 | 156 | 10.6 | A | 00.14 | 5.3 (north-east) | 180 | 11.5 | A | 0.105 | $\begin{aligned} & 5.4 \text { (north- } \\ & \text { east) } \end{aligned}$ |

The key findings for the Brayton Road/Ambrose Road intersection are:

- with the existing scenario, the intersection currently operates LOS A on all approaches; and
- with the future 2051 scenario, the intersection will continue to operate LOS A.

Table 6.3 SIDRA modelling result for Hume Highway/Red Hills Road intersection

| Control/scenarios | AM Peak |  |  |  |  | PM Peak |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Priority controlled (Give Way) | Intersection volume | DEL(s) | LOS | DOS | Max Q in m (approach) | Intersection volume | DEL(s) | LOS | DOS | Max $Q$ in $m$ (approach) |
| 1. Existing | 639 | 9.8 | A | 0.199 | 0.0 | 780 | 9.0 | A | 0.228 | 0.0 |
| 2. Future 2051 | 836 | 10.3 | A | 0.232 | 0.0 | 1014 | 10.2 | A | 0.272 | 0.0 |

The key findings for the Hume Highway/Red Hills Road intersection are:

- with the existing scenario, the intersection currently operates LOS A on all approaches; and
- with the future 2051 scenario, the intersection will continue to operate LOS A.

Table 6.4 SIDRA modelling result for George Street/Brayton Road intersection

| Control/Scenarios | AM Peak |  |  |  |  | PM Peak |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Roundabout | Intersection volume | DEL(s) | LOS | DOS | Max Q in m (approach) | Intersection volume | DEL(s) | LOS | DOS | Max Q in m (approach) |
| 1. Existing | 280 | 6.1 | A | 0.106 | 3.2 (northwest) | 328 | 6.9 | A | 0.128 | 4.0 (southwest) |
| 2. Future 2051 | 414 | 7.8 | A | 0.230 | $\begin{aligned} & 9.0 \text { (north- } \\ & \text { west) } \end{aligned}$ | 473 | 8.5 | A | 0.187 | 6.1 (north- <br> west) |

The key findings for the George Street/Brayton Road intersection are:

- with the existing scenario, the intersection currently operates LOS A on all approaches;
- with the future 2051 scenario, the intersection will continue to operate LOS A; and
- the intersection is currently operating around $10 \%$ capacity which will marginally increase with the development and cumulative traffic.

Table 6.5 SIDRA modelling result for Hume Highway Off Ramp/Jerrara Road/Marulan South Road intersection

| Control/Scenarios | AM Peak Peak |  |  |  |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Roundabout | Intersection <br> volume | DEL(s) | LOS | DOS | Max $\mathbf{Q}$ in $m$ <br> (approach) | Intersection <br> volume | DEL(s) | LOS | DOS | Max $\mathbf{Q}$ in $m$ <br> (approach) |  |
| 1. Existing | 204 | 5.2 | A | 0.100 | 4.5 (north-east) | 187 | 5.6 | A | 0.055 | 2.4 (north- <br> east) |  |
| 2. Future 2051 | 304 | 5.9 | A | 0.164 | 8.5 (north-east) | 299 | 6.6 | A | 0.124 | 6.7 (north- <br> east) |  |

The key findings for the Hume Highway Off Ramp/ Jerrara Road/ Marulan South Road intersection are:

- with the existing scenario, the intersection currently operates LOS A on all approaches; and
- with the future 2051 scenario, the intersection will continue to operate LOS A.

Table 6.6 SIDRA modelling result for Hume Highway On Ramp/Hume Highway Off Ramp/Jerrara Road

| Control/Scenarios | AM Peak |  |  |  |  | PM Peak |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Priority controlled (Give Way) | Intersection volume | DEL(s) | LOS | DOS | Max $Q$ in $m$ (approach) | Intersection volume | DEL(s) | LOS | DOS | Max $\mathbf{Q}$ in m (approach) |
| 1. Existing | 106 | 6.7 | A | 0.047 | 1.8 (south-east) | 133 | 8.1 | A | 0.057 | 2.1 (southeast) |
| 2. Future 2051 | 182 | 7.6 | A | 0.108 | 5.4 (south-east) | 236 | 10.3 | A | 0.135 | $\begin{aligned} & 6.2 \text { (south- } \\ & \text { east) } \end{aligned}$ |

The key findings for the Hume Highway On Ramp/ Hume Highway Off Ramp/Jerrara Road intersection are:

- with the existing scenario, the intersection currently operates LOS A on all approaches;
- with the future 2051 scenario, the intersection will continue to operate LOS A; and
- with the future 2051 scenario, the intersection will operate under $15 \%$ capacity.

The continuation project with net cumulative traffic would not reduce the LOS of any key intersections.

### 6.2 Sight distances

The Quarry access on Brayton Road has good sight distance to the left and right (Plate 6.1). The sight distance is estimated to be 456 m to the left and 296 m to the right. In accordance with Austroads Guide to Road Design Part 4A: Unsignalised and Signalised Intersections (Austroads 2017), for a road with a design speed of $110 \mathrm{~km} / \mathrm{h}$ (generally $10 \mathrm{~km} / \mathrm{h}$ higher than the speed limit), the minimum safe intersection sight distance (SISD) required for a general minimum 2 second driver reaction time is 285 m , therefore the existing site access has adequate sight distance.


Plate 6.1 Sight distance from the Quarry access

### 6.3 Road safety

Potential impacts of the Continuation Project are addressed in the Road Safety Impact Assessment report (ARRB 2021, EIS Appendix F.2).

### 6.4 Mitigation measures

Quarry traffic will continue to be managed in accordance with the Gunlake Quarry Traffic Management Plan (Gunlake 2020), including the Driver Code of Conduct, as updated in accordance with the development approval.

As all intersections are predicted to continue to operate with a LOS A to 2051, including with the operation of the Continuation Project, and sightlines are adequate at the site access intersection, no additional mitigation measures are proposed as a result of the findings of this TIA.

## 7 Conclusion

The associated traffic impacts for the proposed continuation project traffic and potential cumulative traffic have been assessed as follows:

- the future (2051) cumulative traffic volumes (ie Gunlake Quarry traffic plus the approved/proposed traffic from the five other local quarries and the future residential subdivision off Corriedale Drive) at the end of the proposed Quarry life (2051) was calculated by adding: combined non-Gunlake project development traffic (Section 5.2.3); future background traffic (Section 5.3); and Continuation Project traffic (Section 4.4.3);
- based on SIDRA analysis of the existing background traffic volumes, the five key intersections currently operate with a LOS A;
- based on SIDRA analysis of future (2051) cumulative traffic volumes, the five key intersections will continue to operate with a LOS A; and
- the sight distance at the site access complies with Austroads guidelines.

Road safety is addressed in in the Road Safety Impact Assessment report (ARRB 2021, EIS Appendix F.2).

## References

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Annexure A

## Traffic survey data (intersection and tube counts)

|  |  |
| :--- | :--- |
| Job No. | : N5936 |
| Client | $:$ EMM Consulting |
| Suburb | $:$ Marulan |
| Location | $: 1$. Brayton Rd / Ambrose Rd |
|  |  |
| Day/Date | : Thu, 10th Sept 2020 |
| Weather | : Fine |
| Description | : Classified Intersection Count |
|  | : Hourly Summary |




| 15:30 to $16: 30$ | 25 | 2 | ${ }^{27}$ | 2 | 2 | 4 | 0 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15:45 to $16: 45$ | 14 | 0 | 14 | 3 | 2 | 5 | 0 | 0 | 0 |
| 16:00 to 17 1700 | ${ }^{12}$ | 0 | 12 | ${ }^{3}$ | 2 | 5 | 0 | 0 | 0 |
| 16:15 to 17:15 | 16 | 0 | 16 | 1 | 1 | 2 | 0 | 0 | 0 |
| 16:30 to 17 1730 | 14 | 0 | ${ }^{14}$ | 1 | 0 | 1 | 0 | 0 | 0 |
| 16:45 to 17 17:45 | 17 | 0 | 17 | 1 | 0 | 1 | 0 | 0 | 0 |
| 17:00 to $18: 00$ | ${ }^{21}$ | 0 | ${ }^{21}$ | 1 | 1 | 2 | 0 | 0 | 0 |
| 177:15 to $18: 15$ | 16 | 0 | 16 | 2 | 1 | 3 | 0 | 0 | 0 |
| 17730 to $18: 30$ | 16 | 0 | 16 | 2 | 1 | 3 | 0 | 0 | 0 |
| 17:45 to $18: 45$ | ${ }^{14}$ | 0 | 14 | 3 | 1 | 4 | 0 | 0 | 0 |
| 18:00 to $19: 00$ | 10 | 0 | 10 | 4 | 0 | 4 | 0 | 0 | 0 |
| $18: 15$ to $19: 15$ | ${ }^{8}$ | 0 | 8 | ${ }^{3}$ | 0 | 3 | 0 | 0 | 0 |
| 18:30 to $19: 30$ | 5 | 0 | 5 | ${ }^{3}$ | 0 | 3 | 0 | 0 | 0 |
| 18:45 to $19: 45$ | 3 | 0 | 3 | 1 | 0 | 1 | 0 | 0 | 0 |
| 19:00 to $20: 00$ | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| 19:15 to 20:15 | 6 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 |
| 19330 to $20: 30$ | 7 | 0 | 7 | 1 | 0 | 1 | 0 | 0 | 0 |
| 19:45 to $20: 45$ | 6 | 0 | 6 | 1 | 0 | 1 | 0 | 0 | 0 |
| 20:00 to $21: 00$ | 7 | 0 | 7 | 1 | 0 | 1 | 0 | 0 | 0 |
| 20.15 to $21: 15$ | 3 | 0 | 3 | 2 | 0 | 2 | 0 | 0 | 0 |
| 20:30 to $21: 30$ | 2 | 0 | 2 | 2 | 0 | 2 | 0 | 0 | 0 |
| 20:45 to $21: 45$ | 3 | 0 | 3 | 3 | 0 | 3 | 0 | 0 | 0 |
| 21:00 to 22:00 | 1 | 0 | 1 | 3 | 0 | 3 | 0 | 0 | 0 |
| 22.15 to $22: 15$ | 3 | 0 | 3 | 2 | 0 | 2 | 0 | 0 | 0 |
| 21:30 to $22: 30$ | 4 | 0 | 4 | 1 | 0 | 1 | 0 | 0 | 0 |
| 21:45 to $22: 45$ | 4 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| 22:00 to $23: 00$ | 6 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 |
| $22: 15$ to $23: 15$ | 4 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| 22:30 to $23: 30$ | 3 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 |
| 22:45 to $23: 45$ | 3 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 |
| 23:00 to 0.000 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 24hr Totals | 205 | 15 | 220 | 29 | 8 | 37 | 0 | 0 | 0 |




|  |  |
| :--- | :--- |
| Job No. | : N5936 |
| Client | $:$ EMM Consulting |
| Suburb | : Marulan |
| Location | $:$ 2. Hume Hwy / Red Hills Rd |
|  |  |
| Day/Date | : Thu, 10th Sept 2020 |
| Weather | : Fine |
| Description | : Classified Intersection Count |
|  | : Hourly Summary |



Apprach

| Approach |
| :---: |
| Direction |
|  |
| Time Period |


| Time Period |  |
| :---: | :---: |
| $0: 00$ | to $\quad 1: 00$ |


| $0: 15$ | to | $1: 15$ |
| :---: | :---: | :---: |
| $0: 30$ | to | $1: 30$ |
| 0.5 |  | $1: 30$ |


| $0: 45$ | to |
| :--- | :--- |
| $1: 00$ | to |
| $1: 20$ |  |

$\begin{array}{lll}1: 00 & \text { to } \\ 1: 150 & \text { to } & 2 \\ 1: 3 & \text { to } & 2: 3 \\ 10 & \text { to } & 2: 45\end{array}$

| 1:30 | to |
| :--- | :--- |
| 1:45 | to |
| 2:00 | to |

$\begin{array}{lll}\text { 2:15 } & \text { to } & 3: 1 \\ 2: 30 & \text { to } & 3: 3 \\ 2: 5 & & 3\end{array}$

| 2:45 | to |
| :--- | :--- |
| $3: 00$ | to |
| $3: 15$ |  |


| 3:15 | to |
| :--- | :--- |
| 3:30 | to |
| 3:45 | to |
|  |  |

$\begin{array}{ll}\text { 3:45 } & \text { to } \\ \text { to }\end{array}$

| 4:15 | to |
| :--- | :--- |
| 4:30 | to |
| $4: 45$ | to |


| 4:45 | to |
| :--- | :--- |
| $5: 00$ | to |


| $5: 15$ | to |
| :--- | :--- |
| $5: 30$ | to |
| 5 | to |


| 5:30 | to |
| :---: | :---: |
| 5:45 | to |
| $6: 00$ | to |


| $6: 15$ | to |
| :--- | :--- |
| $6: 30$ | to |


| $6: 45$ | to |
| :--- | :--- |
| $7: 00$ | to |
| $7: 125$ | to |


| 7:15 | to |
| :--- | :--- |
| 7:30 | to |
| $7: 45$ | to |

$8: 00$ to

| $8: 15$ | to |
| :--- | :--- |
| $8: 30$ | to |


| $8: 45$ | to |
| :--- | :--- |
| $9: 00$ | to |


| 9:15 | to |
| :--- | :--- |
| $9: 30$ | to |

$\begin{array}{ll}\text { 9:45 } & \text { to } \\ 10: 00 & \text { to }\end{array}$
10:15 to $11:$

| $10: 30$ | to |
| :--- | :--- |
| $10: 45$ | to |


| $11: 00$ | to |
| :--- | :--- |
| $11: 15$ | to |
| 1120 | to |

11:30 to $12: 30$
$\begin{array}{lll}\text { 11:45 } & \text { to } 12: 45 \\ \text { 12:00 } & \text { to } 13: 0\end{array}$
12:15 to 13:15

| $12: 30$ | to | $13:$ |
| :--- | :--- | :--- |
| $12: 45$ | to | $13:$ |

13:00 to

| $13: 15$ | to | $14:$ |
| :--- | :--- | :--- |
| $13: 30$ | to | $14: 3$ |

$\begin{array}{lll}13: 30 & \text { to } 143 \\ 13: 45 & \text { to } & 1: 4 \\ 14 & & \end{array}$
14:00 to 15:00

| $14: 15$ |  |
| :--- | :--- |
| $14: 30$ | to |
| 14:45 | to |
| $15: 00$ |  |


| $15: 00$ | to | $16: 00$ |
| :--- | :--- | :--- |
| 15:15 | to | $16: 15$ |

5:15 to $16: 15$





| Job No. | : N5936 |
| :--- | :--- |
| Client | $:$ EMM Consulting |
| Suburb | $:$ Marulan |
| Location | $: 3$. Brayton Rd / George St |
|  |  |
| Day/Date | : Thu, 10th Sept 2020 |
| Weather | : Fine |
| Description | $:$ Classified Intersection Count |
|  | : Hourly Summary |



George St


| 15：30 to 16.30 | 71 | 4 | 75 | ${ }^{8}$ | 2 | 10 | 81 | 4 | ${ }^{85}$ | 0 | 0 | 0 | ${ }^{39}$ | 2 | ${ }^{41}$ | 32 | 2 | 34 | 2 | 2 | 4 | 0 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15．45 to 16：45 | 50 | 4 | 54 | 5 | 2 | 7 | 84 | 4 | ${ }^{88}$ | 0 | 0 | 0 | 38 | 3 | ${ }^{41}$ | 23 | 1 | 24 | 2 | 2 | 4 | 1 | 0 | 1 |
| 16：00 to 17：00 | 49 | 2 | 51 | 5 | 2 | 7 | ${ }^{77}$ | 3 | ${ }^{80}$ | 0 | 0 | 0 | 35 | 4 | 39 | 22 | 1 | 23 | 2 | 0 | 2 | 1 | 0 | 1 |
| $16: 15$ to 17：15 | 52 | 2 | 54 | 6 | ${ }^{3}$ | 9 | 81 | 4 | ${ }^{85}$ | 0 | 0 | 0 | 34 | 5 | ${ }^{39}$ | 23 | 1 | 24 | 2 | 0 | 2 | 1 | 0 | 1 |
| 16.30 to 17.30 | 54 | 1 | 55 | 5 | 1 | ${ }^{6}$ | 71 | 4 | 75 | 0 | 0 | 0 | 26 | 4 | ${ }^{30}$ | 27 | 1 | 28 | 1 | 0 | 1 | 1 | 0 | 1 |
|  | ${ }_{58}$ | 2 | 60 | 4 | 1 | 5 | 55 | 4 | 59 | 0 | 0 | 0 | 24 | 2 | 26 | 27 | 0 | 27 | 2 | 0 | 2 | 0 | 0 | 0 |
| 17：00 to 18：00 | 53 | 4 | 57 | 5 | 1 | ${ }^{5}$ | ${ }^{44}$ | 5 | 49 | 0 | 0 | 0 | 24 | 2 | 26 | 26 | 1 | 27 | 1 | 0 | 1 | 0 | 0 | 0 |
| 17：15 to 18：15 | 48 | 3 | 51 | 5 | 0 | 5 | 40 | 7 | 47 | 0 | 0 | 0 | 25 | 2 | 27 | 24 | 2 | 26 | 1 | 2 | 3 | 0 | 0 | 0 |
| 17：30 to 18.30 | 45 | 3 | 48 | 7 | 1 | 8 | ${ }^{44}$ | 7 | 51 | 0 | 0 | 0 | ${ }^{28}$ | 2 | ${ }^{30}$ | 20 | 2 | 22 | 1 | 2 | 3 | 0 | 0 | 0 |
| 17：45 to 18，45 | 51 | 2 | 53 | 7 | 1 | 8 | ${ }^{48}$ | 6 | 54 | 0 | 0 | 0 | ${ }^{21}$ | ${ }^{3}$ | 24 | 19 | 2 | 21 | 0 | 2 | 2 | 0 | 0 | 0 |
| 18.00 to 19.00 | 51 | 0 | 51 | 6 | 2 | 8 | 49 | 5 | 54 | 0 | 0 | 0 | 20 | 2 | 22 | 18 | 2 | 20 | 0 | 3 | 3 | 0 | 0 | 0 |
| 18.15 to $19: 15$ | 47 | 0 | 47 | 4 | 2 | 6 | ${ }^{44}$ | 3 | 47 | 0 | 0 | － | ${ }^{14}$ | 2 | ${ }^{16}$ | 15 | 1 | 16 | 2 | 2 | 4 | 0 | 0 | 0 |
|  | 38 | 0 | 38 | 2 | 1 | 3 | 29 | 3 | 32 | 0 | 0 | 0 | ${ }^{11}$ | 3 | ${ }^{14}$ | ${ }^{13}$ | 1 | 14 | 2 | 2 | 4 | 0 | 0 | 0 |
| 18.45 to 19：45 | 24 | 0 | 24 | 2 | 1 | 3 | 23 | 4 | 27 | 0 | 0 | 0 | ${ }^{11}$ | 2 | ${ }^{13}$ | ${ }^{12}$ | 1 | 13 | 2 | 2 | 4 | 0 | 0 | 0 |
| 19.00 to 20.00 | 19 | 0 | 19 | 1 | 0 | 1 | ${ }^{21}$ | ${ }^{3}$ | 24 | 0 | 0 | 0 | ${ }^{8}$ | 2 | 10 | 8 | 0 | 8 | 2 | 1 | 3 | 0 | 0 | 0 |
| 19：15 to $20: 15$ | 16 | 0 | 16 | 1 | 0 | 1 | 22 | 3 | 25 | 0 | 0 | 0 | 10 | 1 | ${ }^{11}$ | 10 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 |
| 19：30 to 20.30 | 22 | 0 | 22 | 1 | 0 | 1 | 24 | 3 | 27 | 0 | 0 | 0 | 8 | 0 | 8 | 8 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 |
| 19：45 to 20.45 | 24 | 0 | 24 | 1 | 0 | 1 | 24 | 2 | 26 | 0 | 0 | 0 | 7 | 0 | 7 | 5 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 |
| 20：00 to 21：00 | 24 | 0 | 24 | 1 | 0 | 1 | ${ }^{23}$ | 2 | 25 | 0 | 0 | 0 | ${ }^{8}$ | 0 | ${ }^{8}$ | 7 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 |
| 20：15 to $21: 15$ | 18 | 0 | 18 | 1 | 1 | 2 | ${ }^{18}$ | 1 | 19 | 0 | 0 | 0 | 5 | 0 | 5 | 7 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 |
| 20：30 to $^{21: 30}$ | 12 | 0 | 12 | 1 | 1 | 2 | 19 | 0 | 19 | 0 | 0 | 0 | 4 | 1 | 5 | ${ }^{11}$ | 0 | ${ }^{11}$ | 0 | 0 | 0 | 0 | 0 | 0 |
| 20．45 to 21：45 | 9 | 0 | 9 | 0 | 1 | 1 | ${ }^{13}$ | 0 | ${ }^{13}$ | 0 | 0 | 0 | 3 | 1 | 4 | ${ }^{13}$ | 0 | ${ }^{13}$ | 0 | 0 | 0 | 0 | 0 | 0 |
| 21：00 to 22：00 | 6 | 0 | 6 | 0 | 1 | 1 | 11 | 0 | ${ }^{11}$ | 0 | 0 | 0 | 4 | 1 | 5 | 12 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 0 |
| 21：15 to 22：15 | 5 | 0 | 5 | 0 | 0 | 0 | 9 | 0 | 9 | 0 | 0 | 0 | 6 | 1 | 7 | ${ }^{10}$ | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 |
| 21：30 to 22：30 | 9 | 0 | 9 | 0 | 0 | 0 | ${ }^{3}$ | 1 | 4 | 0 | 0 | 0 | ${ }^{6}$ | 1 | 7 | ${ }^{6}$ | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 |
| 21：45 to 22：45 | 9 | 0 | 9 | 0 | 1 | 1 | 5 | 1 | 6 | 0 | 0 | 0 | 6 | 2 | 8 | 4 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| 22：00 to 23：00 | ${ }^{11}$ | 0 | ${ }^{11}$ | 0 | 1 | 1 | 7 | 2 | 9 | 0 | 0 | 0 | 5 | 2 | 7 | 3 | 0 | 3 | 0 | 0 | $\bigcirc$ | 0 | 0 | 0 |
| 22：15 to $23: 15$ | ${ }^{10}$ | 0 | 10 | 0 | 1 | 1 | ${ }^{8}$ | 2 | 10 | 0 | 0 | 0 | ${ }^{3}$ | 2 | 5 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| 22,30 to <br> $23: 30$  | 6 | 0 | 6 | 0 | 1 | 1 | 7 | 2 | 9 | 0 | 0 | 0 | 2 | 1 | 3 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| 22：45 to 23，45 | 4 | 0 | 4 | 1 | 0 | 1 | 5 | 2 | 7 | 0 | 0 | 0 | 2 | 0 | 2 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 23．00 to 0.00 | 2 | 0 | 2 | 1 | 0 | 1 | 2 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 24hr Totals | 579 | 35 | 614 | ${ }_{53}$ | 15 | 68 | 877 | 100 | 97 | 1 | 1 | 2 | 427 | 56 | 483 | 197 | 13 | 210 | 16 | 20 | ${ }^{36}$ | 3 | － | 3 |


| Approach <br> Direction | George St |  |  |  |  |  |  |  |  |  |  |  | Brayton Rd |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Direction 7 （Left Turn） |  |  | Direction 8 （Through） |  |  | Direction 9 （Right Turn） |  |  | Direction 90 （U Turn） |  |  | Direction 10 （Left Turn） |  |  | Direction 11 （Through） |  |  | Direction 12 （Right Turn） |  |  | Direction 12 U （U Turn） |  |  |
| Time Period |  | $\begin{aligned} & \text { y } \\ & \stackrel{y}{2} \\ & \text { ax } \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \text { n } \\ & \substack{\text { an } \\ \hline} \\ & \hline \end{aligned}$ | $\stackrel{0}{0}$ <br> $\stackrel{y}{0}$ <br> dun <br> in |  | $\begin{aligned} & \frac{n}{2} \\ & \text { 曾 } \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { ! } \\ & \stackrel{0}{6} \\ & \text { on } \\ & \hline \end{aligned}$ | $\stackrel{\stackrel{5}{\mathrm{O}}}{\stackrel{y}{2}}$ | $\begin{aligned} & \text { n } \\ & \text { 臺 } \\ & \hline \end{aligned}$ |  | $\stackrel{\bar{\circ}}{\stackrel{\rightharpoonup}{\circ}}$ | $\begin{aligned} & \text { n } \\ & \stackrel{y}{\text { an }} \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \bar{\circ} \mathrm{b} \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { n } \\ & \text { 喜 } \\ & \hline \end{aligned}$ |  | $\stackrel{\bar{\circ}}{\stackrel{\circ}{\circ}}$ | $\begin{aligned} & \text { n } \\ & \text { 亭 } \\ & \hline \end{aligned}$ |  |  |  |  | $\stackrel{\text { 든 }}{ }$ |
| 0：00 ${ }^{\text {to }}$ to 1：00 | 1 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 0：15 to 1：15 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 0：30 to 1：30 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 0：45 to 1：45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1：00 $\begin{aligned} & \text { to } \\ & 2: 00\end{aligned}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1：15 to 2：15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 1 | 0 | 1 | 0 | 0 | 0 |
| 1：30 to $^{1: 3} 830$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 1 | 0 | 1 | 0 | 0 | 0 |
| 1：45 to 2：45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 0 |
| 2：00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 0 |
| 2：15 to 3：15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 |
| 2：30 ${ }^{\text {to }}$ to $3: 30$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 |
| 2：45to $3: 45$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 |
| 3：00 $\quad$ to $4: 00$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 0 |
| 3：15to $4: 15$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 6 | 1 | 1 | 2 | 0 | 0 | 0 |
| 3：30 to $^{3} 4: 30$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 10 | 0 | 10 | 2 | 1 | 3 | 0 | 0 | 0 |
| 3：45to $4: 45$ <br> 108  | 0 | 0 | 0 | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 16 | 0 | 16 | 2 | 1 | 3 | 0 | 0 | 0 |
| 4：00 ${ }^{\text {to }}$ 5：00 | 0 | 0 | 0 | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 20 | 0 | 20 | 3 | 1 | 4 | 0 | 0 | 0 |
| 4：15 $\mathrm{to}^{\text {to }}$ 5：15 | 0 | 0 | 0 | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 17 | 0 | 17 | 2 | 0 | 2 | 0 | 0 | 0 |
| 4：30 to $^{5} 5: 30$ | 0 | 0 | 0 | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 18 | 0 | 18 | 1 | 0 | 1 | 0 | 0 | 0 |
| 4：45 ${ }^{\text {to }}$ 5：45 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 24 | 1 | 25 | 4 | 0 | 4 | 0 | 0 | 0 |
| 5：00 $\quad$ to 6：00 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | ${ }^{31}$ | 2 | 33 | 5 | 0 | 5 | 0 | 0 | 0 |
| 5：15 to 6：15 | 2 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | ${ }^{36}$ | 6 | 42 | 7 | 0 | 7 | 0 | 0 | 0 |
| 5：30to | 2 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 37 | 7 | 44 | 8 | 0 | 8 | 0 | 0 | 0 |
| 5：45 ${ }^{\text {to }}$（t）6：45 | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 37 | 7 | 44 | 9 | 0 | 9 | 0 | 0 | 0 |
| 6：00 to 7：00 | 0 | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 31 | 6 | 37 | 14 | 0 | 14 | 0 | 0 | 0 |
| 6：15 to 7：15 | 2 | 0 | 2 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 38 | 3 | 41 | 17 | 2 | 19 | 0 | 0 | 0 |
| 6：30 to 7：30 | 2 | 0 | 2 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 42 | 2 | 44 | 19 | 2 | 21 | 0 | 0 | 0 |
| 6：45 to 7：45 | 2 | 0 | 2 | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 39 | 1 | 40 | 19 | 2 | 21 | 0 | 0 | 0 |
| 7：00to $8: 00$ <br> 7  | 2 | 0 | 2 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 41 | 1 | 42 | 17 | 2 | 19 | 0 | 0 | 0 |
| 7：15to $8: 15$ | 2 | 1 | 3 | 1 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 2 | 0 | 2 | 42 | 1 | ${ }^{43}$ | 15 | 2 | 17 | 0 | 0 | 0 |
| 7：30 $\mathrm{to}^{\text {to }} 8: 30$ | 2 | 1 | 3 | 1 | 1 | 2 | 0 | 1 | 1 | 0 | 0 | 0 | 2 | 0 | 2 | 41 | 1 | 42 | 22 | 2 | 24 | 0 | 0 | 0 |
| 7：45to $8: 45$ | 3 | 1 | 4 | 0 | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 47 | 2 | 49 | 36 | 3 | 39 | 0 | 0 | 0 |
| 8：00 ${ }^{\text {to }}$ 9：00 | 3 | 1 | 4 | 1 | 1 | 2 | 0 | 1 | 1 | 0 | 0 | 0 | 2 | 0 | 2 | 50 | 3 | 53 | 50 | 4 | 54 | 0 | 0 | 0 |
| 8：15 to 9：15 | 2 | 1 | 3 | 2 | 1 | 3 | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 39 | 3 | 42 | 60 | 2 | 62 | 1 | 0 | 1 |
| 8：30 ${ }^{\text {to }}$ 9：30 | 2 | 2 | 4 | 4 | 0 | 4 | 1 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 2 | 32 | 3 | 35 | 52 | 2 | 54 | 1 | 0 | 1 |
| 8：45 to 9：45 | 3 | 2 | 5 | 5 | 0 | 5 | 2 | 0 | 2 | 0 | 0 | 0 | 4 | 0 | 4 | 25 | ${ }^{3}$ | 28 | 36 | 1 | 37 | 1 | 0 | 1 |
| 9：00 to 10：00 | 4 | 2 | 6 | 5 | 1 | 6 | 2 | 0 | 2 | 0 | 0 | 0 | 3 | 0 | 3 | 18 | ${ }^{3}$ | 21 | 23 | 0 | ${ }^{23}$ | 1 | 0 | 1 |
| 9：15 to 10：15 | 3 | 2 | 5 | 5 | 1 | 6 | 1 | 0 | 1 | 0 | 0 | 0 | 4 | 0 | 4 | 20 | 3 | 23 | 11 | 0 | 11 | 0 | 0 | 0 |
| 9：30 to 10：30 | 4 | 1 | 5 | 4 | 2 | 6 | 1 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 3 | 21 | 4 | 25 | 11 | 1 | 12 | 0 | 0 | 0 |
| 9：45 to 10：45 | 5 | 2 | 7 | 5 | 2 | 7 | 2 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 2 | 20 | 4 | 24 | 15 | 1 | 16 | 0 | 0 | 0 |
| 10：00 to 11：00 | 4 | 2 | 6 | 4 | 1 | 5 | 2 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 2 | 22 | 3 | 25 | 13 | 1 | 14 | 0 | 0 | 0 |


| 10:15 to 11:15 | 5 | 1 | 6 | 3 | 1 | 4 | 2 | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 1 | 20 | 2 | 22 | 17 | 1 | 18 | 0 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10:30 to 11:30 | 5 | 2 | 7 | 2 | 0 | 2 | 2 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 2 | 24 | 1 | 25 | 18 | 0 | 18 | 0 | 0 | 0 |
| 10:45 to 11:45 | 3 | 1 | 4 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 22 | 1 | 23 | 14 | 0 | 14 | 0 | 0 | 0 |
| 11:00 to 12:00 | 4 | 2 | 6 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 20 | 1 | 21 | 14 | 0 | 14 | 0 | 0 | 0 |
| 11:15 to 12:15 | 4 | 2 | 6 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 23 | 2 | 25 | 13 | 1 | 14 | 0 | 0 | 0 |
| 11:30 to $^{12} 12: 30$ | 4 | 4 | 8 | 5 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 19 | 3 | 22 | 18 | 1 | 19 | 0 | 0 | 0 |
| 11:45 to 12:45 | 3 | 5 | 8 | 5 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 17 | 2 | 19 | 20 | 2 | 22 | 0 | 0 | 0 |
| 12:00 to 13:00 | 3 | 5 | 8 | 4 | 1 | 5 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 20 | 4 | 24 | 22 | 2 | 24 | 0 | 0 | 0 |
| 12:15 to 13:15 | 3 | 5 | 8 | 4 | 1 | 5 | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 15 | 3 | 18 | 23 | 2 | 25 | 0 | 0 | 0 |
| 12:30 to $13: 30$ | 4 | 2 | 6 | 2 | 1 | 3 | 1 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 2 | 15 | 2 | 17 | 22 | ${ }^{2}$ | 24 | 0 | 0 | 0 |
| 12:45 to 13:45 | 5 | 1 | 6 | 2 | 1 | 3 | 2 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 2 | 15 | 3 | 18 | 23 | 1 | 24 | 0 | 0 | 0 |
| 13:00 to 14:00 | 5 | 1 | 6 | 3 | 1 | 4 | 1 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 3 | 12 | 2 | 14 | 21 | 1 | 22 | 0 | 0 | 0 |
| 13:15 to 14:15 | 7 | 1 | 8 | 3 | 1 | 4 | 1 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 2 | 18 | 2 | 20 | 19 | 0 | 19 | 0 | 0 | 0 |
| 13:30 to 14:30 | 7 | 2 | 9 | 2 | 1 | 3 | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 17 | 4 | 21 | 14 | 0 | 14 | 0 | 0 | 0 |
| 13:45 to 14:45 | 8 | 3 | 11 | 2 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 20 | 6 | 26 | 15 | 0 | 15 | 0 | 0 | 0 |
| 14:00 to 15:00 | 8 | ${ }^{3}$ | 11 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 20 | 6 | 26 | 21 | 0 | 21 | 0 | 0 | 0 |
| 14:15 to 15:15 | 6 | 4 | 10 | 3 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 7 | 21 | 26 | 0 | 26 | 0 | 0 | 0 |
| 14:30 to 15:30 | 5 | 3 | 8 | 5 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 19 | 5 | 24 | 29 | 0 | 29 | 0 | 0 | 0 |
| 14:45 to 15:45 | 5 | 3 | 8 | 5 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 19 | 2 | 21 | 28 | 0 | 28 | 0 | 0 | 0 |
| 15:00 to $16: 00$ | 6 | 2 | 8 | 5 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 17 | 2 | 19 | 23 | 1 | 24 | 0 | 0 | 0 |
| 15:15 to 16:15 | 6 | 2 | 8 | 6 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 28 | 1 | 29 | 20 | 1 | 21 | 0 | 0 | 0 |
| 15:30 to $16: 30$ | 5 | 2 | 7 | 4 | 0 | 4 | 1 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 2 | 27 | 1 | 28 | 25 | 3 | 28 | 0 | 0 | 0 |
| 15:45 to 16:45 | 4 | 1 | 5 | 4 | 2 | 6 | 1 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 2 | 24 | 1 | 25 | 27 | 4 | 31 | 0 | 0 | 0 |
| 16:00to $17: 00$ <br> 1  | 2 | 1 | 3 | 4 | 2 | 6 | 1 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 2 | 28 | 0 | 28 | 30 | 3 | 33 | 0 | 0 | 0 |
| 16:15 to 17:15 | 2 | 0 | 2 | 2 | 3 | 5 | 3 | 0 | 3 | 0 | 0 | 0 | 2 | 0 | 2 | 22 | 0 | 22 | 28 | ${ }^{3}$ | 31 | 0 | 0 | 0 |
| 16:30 to 17:30 | 2 | 0 | 2 | 2 | 3 | 5 | 2 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 2 | 25 | 1 | 26 | 21 | 1 | 22 | 0 | 0 | 0 |
| 16:45 to 17:45 | 1 | 0 | 1 | 2 | 2 | 4 | 4 | 0 | 4 | 0 | 0 | 0 | 3 | 0 | 3 | 25 | 1 | 26 | 15 | 0 | 15 | 0 | 0 | 0 |
| 17:00 to 18:00 | 1 | 0 | 1 | 2 | 2 | 4 | 5 | 0 | 5 | 0 | 0 | 0 | 4 | 0 | 4 | 27 | 1 | 28 | 21 | 0 | 21 | 0 | 0 | 0 |
| 17:15 to 18:15 | 1 | 0 | 1 | 2 | 1 | 3 | 3 | 0 | 3 | 0 | 0 | 0 | 2 | 0 | 2 | 23 | 1 | 24 | 22 | 2 | 24 | 0 | 0 | 0 |
| 17:30to $18: 30$ <br> $17: 5$  | 3 | 0 | 3 | ${ }^{3}$ | 1 | 4 | ${ }^{3}$ | 0 | 3 | 1 | 0 | 1 | 3 | 0 | ${ }^{3}$ | 19 | 0 | 19 | 28 | 2 | 30 | 0 | 0 | 0 |
| 17:45 to $18: 45$ | 5 | 1 | 6 | 2 | 1 | 3 | 1 | 0 | 1 | 1 | 0 | 1 | 2 | 0 | 2 | 18 | 0 | 18 | 34 | 2 | 36 | 0 | 0 | 0 |
| 18:00 to 19:00 | 6 | 1 | 7 | 4 | 1 | 5 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 1 | 12 | 0 | 12 | 22 | 2 | 24 | 0 | 0 | 0 |
| 18:15 to 19:15 | 5 | ${ }^{3}$ | 8 | 6 | 1 | 7 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 1 | 9 | 0 | 9 | 18 | 0 | 18 | 0 | 0 | 0 |
| 18:30 to 19:30 | 4 | 4 | 8 | 5 | 1 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 7 | 9 | 0 | 9 | 0 | 0 | 0 |
| 18:45 to 19:45 | 2 | 3 | 5 | 6 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 5 | 3 | 0 | ${ }^{3}$ | 0 | 0 | 0 |
| 19:00 to 20:00 | 1 | 3 | 4 | 3 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 4 | 0 | 4 | 0 | 0 | 0 |
| 19:15 to 20:15 | 1 | 1 | 2 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 4 | 0 | 4 | 0 | 0 | 0 |
| 19:30 to $20: 30$ | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 7 | 0 | 7 | 0 | 0 | 0 |
| 19:45 to 20:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 5 | 9 | 0 | 9 | 0 | 0 | 0 |
| 20:00 to 21:00 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 7 | 8 | 0 | 8 | 0 | 0 | 0 |
| 20:15 to 21:15 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 7 | 9 | 0 | 9 | 0 | 0 | 0 |
| 20:30to $21: 30$ | 1 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 8 | 7 | 0 | 7 | 0 | 0 | 0 |
| 20:45 to 21:45 | 1 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 5 | 5 | 0 | 5 | 0 | 0 | 0 |
| 21:00to $22: 00$ <br> 20  | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 5 | 3 | 0 | 3 | 0 | 0 | 0 |
| 21:15 $\quad$ to 22:15 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 6 | 2 | 0 | 2 | 0 | 0 | 0 |
| 21:30to $22: 30$ <br> 10  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 1 | 0 | 1 | 0 | 0 | 0 |
| 21:45 to 22:45 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 5 | 0 | 5 | 1 | 0 | 1 | 0 | 0 | 0 |
| 22:00 to 23:00 | 1 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 5 | 0 | 5 | 1 | 0 | 1 | 0 | 0 | 0 |
| 22:15 $\quad$ to 23:15 | 1 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 4 | 0 | 4 | 1 | 0 | 1 | 0 | 0 | 0 |
| 22:30 $\quad$ to 23:30 | 1 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 3 | 0 | 3 | 1 | 0 | 1 | 0 | 0 | 0 |
| 22:45 to 23:45 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 |
| 23:00 to 0:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 0 |
| 24hr Totals | 54 | 24 | 78 | 42 | 14 | 56 | 12 | 1 | 13 | 1 | 0 | 1 | 25 | 1 | 26 | 395 | 34 | 429 | 318 | 17 | 335 | 1 | 0 | 1 |


| Job No． | $:$ N5936 |
| :--- | :--- |
| Client | $:$ EMM Consulting |
| Suburb | $:$ Marulan |
| Location | $: 4$ A．Hume Hwy Westbound／Jerrara Rd |
|  |  |
| Day／Date | ：Wed，16th Sept 2020 |
| Weather | $:$ Fine |
| Description | $:$ Classified Intersection Count |
|  | $:$ Hourly Summary |



Marulan SRd

|  | $\begin{aligned} & \hline \text { 麔 } \\ & \text { of } \\ & \text { ". } \\ & \hline \end{aligned}$ | 罴 | 勫 | 蓠 | 产 |  | 葆 | 沱 |  | 荷 | 范 | ｜rür | 苞 | 㴦 | 䓪 | ｜r | 苞 | （H） | 苓 | 葡 |  | 而 |  |  | 洝 | 范 | \％ |  | \％ | 閨 | \％ | 仿 | （ | 岩 | \％ |  | \％ |  |  | 资 |  | 萢 | ¢ ¢ t \％ \％ | 苓 | 荌 | 薷 | 合 <br> t <br> U <br> ¢ | 苓 | ｜c｜ | 苞 | \％ | 答 | 華 | 范 | 筞 | 苓 | ｜r | 苞 | H \％ \％ \％ | 会 | ｜l｜ | 品 |  |  | 읓 | 吝 |
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| N | ～ | $\sim$ | $\sim$ | $\bullet$ | $\bullet$ | ¢ |  | $\bullet$ | の | $\checkmark$ | － | $\infty$ | $\infty$ | $\stackrel{\square}{\circ}$ | $\infty$ | $\checkmark$ | － | ～ | $\omega$ | － |  | － |  | $\omega$ | N | $\omega$ | ～ | ～ | $\stackrel{ }{\sim}$ | ～ | － | － | $\sim$ | 号 | 号 | ت | $\stackrel{\text { }}{ }$ | $\checkmark$ | $\checkmark$ | $\stackrel{ }{*}$ | － | － | － | $\stackrel{ }{+}$ | ～ | ～ | ～ | $\sim$ | － | － | － | － | － | － | － | $\stackrel{ }{+}$ | $\stackrel{ }{+}$ | － | － | － | － | $\stackrel{\rightharpoonup}{+}$ | ${ }^{+}$ | Lights |  |  |
| $\checkmark$ | の | $u$ | $u$ | w | $\checkmark$ | － |  | u | － | ～ | － | － | $\checkmark$ | $\checkmark$ | － | ～ | N | N | N | N | － | － |  | $\stackrel{+}{+}$ | ${ }^{\omega}$ | u | 9 | u | $\because$ | ${ }^{\omega}$ | ～ | w | ～ | ～ | ～ | － | － | ～ | ～ | w | N | ＋ | ～ | ${ }^{+}$ | ＋ | ${ }^{+}$ | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | Heavies | $\stackrel{7}{\square}$ |  |
| $\stackrel{\sim}{\sim}$ | \％ | \％ | え | ～ | 5 | $\square$ |  | $\stackrel{+}{4}$ | \％ | $\checkmark$ | $\infty$ | ～ | む | 4 | ～ | $\checkmark$ | の | － | $\checkmark$ | $\sigma$ |  | ＂ |  | － | $\checkmark$ | $\infty$ | $\infty$ | $\checkmark$ | の | $\checkmark$ | の | $\checkmark$ | $\bullet$ | ～ | ～ | ～ |  | $\bullet$ | $\checkmark$ | $\checkmark$ | ～ | － | ～ | ～ | ${ }^{\omega}$ | ${ }^{\omega}$ | ～ | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | Total |  |  |
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| ※ | m | $\sim$ | む | $\sim$ | $\simeq$ | ニ |  | \％ | $\stackrel{\square}{6}$ | $\forall$ | N | む | ～ | $\checkmark$ | $\checkmark$ | $\checkmark$ | 4 | ～ | ～ | L |  | $\stackrel{\rightharpoonup}{\text { a }}$ |  | $\stackrel{\square}{4}$ | \％ | u | \％ | H | $\infty$ | $\checkmark$ | の | $\sim$ | $v$ | $\bullet$ | $\bullet$ | $v$ | $\infty$ | $\checkmark$ | － | $\checkmark$ | の | $\checkmark$ | $\sim$ | の | － | $\omega$ | ～ | N | ${ }^{\omega}$ | $\omega$ | $\omega$ | ～ | － | － | － | － | － | ～ | ～ | $\omega$ | ～ | － | $\square$ | rotal |  | $\stackrel{3}{2}$ |
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| － | ${ }^{\omega}$ | $\omega$ | $\checkmark$ | u | の | $\sim$ |  | の | － | $\checkmark$ | $\checkmark$ | の | $\infty$ | $\bullet$ | $\checkmark$ | $\infty$ | $\infty$ | $\checkmark$ | $\checkmark$ | $\cdots$ |  | $\infty$ |  | $\stackrel{\square}{5}$ | 岁 | $\stackrel{\square}{\omega}$ | ～ | $\infty$ | $\infty$ | $\sim$ | $\omega$ | $\omega$ | u | u | In | $\because$ | $\stackrel{\square}{\sim}$ | w | \％ | ～ | $\sim$ | $\sim$ | $\stackrel{\square}{\infty}$ | $\bullet$ | $\sim$ | u | － | － | － | ＋ | － | － | － | － | － | － | － | － | － | － | － | ～ | N | Lights |  |  |
| － | ～ | $\omega$ | $u$ | － | － | － |  |  | － | $\checkmark$ | $\infty$ | $\infty$ | $\sim$ | $\checkmark$ | ～ | $\checkmark$ | $u$ | $u$ |  | n N |  | ～ |  | $\omega$ | － |  | － | $u$ |  |  |  | の | の | の | $u$ | ～ | $\omega$ | ＋ | － | ～ | ～ | $\omega$ | $\checkmark$ | $\checkmark$ | の | $u$ | － | $\omega$ | ～ | ～ | － | － | － | － | － | － | － | － | － | ～ | N | ～ |  | Heavies |  |  |
| $\cdots$ | $\sim$ | の | ธ | $\bullet$ | $\stackrel{\square}{\square}$ | H |  |  | $\infty$ | $\stackrel{5}{5}$ | $\checkmark$ | $\stackrel{\square}{5}$ | $\stackrel{4}{4}$ | $\stackrel{\square}{5}$ | $\bullet$ | む | ぁ | ¢ | \％ | $\infty$ |  | $\stackrel{\square}{5}$ |  | $\stackrel{\square}{6}$ | \％ | $\because$ | \％ | $\stackrel{\rightharpoonup}{\omega}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{\sim}{\sim}$ | $\infty$ | $\bullet$ | $\square$ | － | $\because$ | ¢ | $\because$ | ～ | $\sim$ | \％ | $\simeq$ | $\approx$ | ะ | $\stackrel{\square}{\square}$ | む | ธ | $\infty$ | $\checkmark$ | $\omega$ | $\omega$ | ～ | － | － | － | － | － | － | － | － | ～ | ～ | － | －${ }^{\text {T }}$ | Total |  |  |
| ～ | n | $\sim$ | ～ | ～ | $\sim$ | ¢ |  | $\stackrel{\square}{6}$ | 岇 | $\stackrel{\square}{\infty}$ | 号 | 4 | \％ | $\stackrel{\square}{\square}$ | ～ | \％ | « | $v$ | む | $\approx \sim$ | $\simeq$ | \％ |  | ～ | \％ | 4 | ～ | $\stackrel{\square}{\omega}$ | － | \％ | － | の | $\bigcirc$ | 号 | $\sim$ | $\infty$ | $\infty$ | $\sigma$ | 号 | ت | $\infty$ | $\sim$ | $\omega$ | ～ | ～ | ～ | N | － | 。 | 。 | － | － | － | － | 。 | 。 | － | － | － | $\stackrel{ }{+}$ | ～ | ～ | $u$ | Lights |  |  |
| $\infty$ | $\infty$ | $\infty$ | $\infty$ | $u$ | － | － |  | $\checkmark$ | $\checkmark$ | $\sim$ | $\checkmark$ | － | ${ }^{\omega}$ | の | $\checkmark$ | $\sim$ | $\checkmark$ | － | N | $\sim$ w | $\omega$ | $\omega$ |  | － | － | $\omega$ | － | ～ | ～ | ～ | $\omega$ | $\omega$ | ${ }^{\omega}$ | の | の | $\stackrel{\square}{5}$ | 岇 | ¢ | $\stackrel{\text { i }}{ }$ | $u$ | $\omega$ | $\omega$ | ${ }^{\omega}$ | $\omega$ | ～ | N | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | Heavies | $\stackrel{\circ}{2}$ |  |
| w | w | w | ${ }^{\circ}$ | $\sim$ | n | ๙ |  | \％ | ๙ | $\sim$ | « | $\checkmark$ | $\approx$ | $\sim$ | ะ | ${ }_{\sim}^{*}$ | ¢ | ะ | $\sim$ | $\sim \sim$ | ～ | $\sim$ |  | ะ | ～ | ¢ | ¢ | $\square$ | \％ | ～ | \％ | $\bullet$ | ～ | ¢ | い | ～ | ～ | $\stackrel{\square}{0}$ | ～ | 祘 | $\pm$ | ¢ | $\sigma$ | $\cdots$ | － | － | $\omega$ | － | 。 | － | － | － | － | － | － | － | － | － | 。 | － | ～ | ～ | u | Total |  | $\begin{aligned} & 0 \\ & \frac{1}{\xi} \\ & \hline \end{aligned}$ |
| ～ | $\stackrel{ }{+}$ | － | ${ }^{\omega}$ | $\bigcirc$ | $\sigma$ | $\sigma$ |  | $\bigcirc$ | 9 | $\square$ | $\infty$ | $\checkmark$ | $\omega$ | － | ${ }^{\omega}$ | $\omega$ | $\omega$ | $\omega$ | ${ }^{\omega}$ | w w | w | － |  | の | $u$ | － | ＋ | ～ | ～ | $\omega$ | $\omega$ | $\stackrel{\square}{+}$ | ${ }^{\omega}$ | ～ | ～ | w | ${ }^{\omega}$ | － | a | 9 | $\bullet$ | ¢ | $\bullet$ | $\bullet$ | $u$ | $\checkmark$ | $\checkmark$ | － | w | $\sim$ | － | － | － | － | － | － | － | － | － | － | － | － | － | Lights |  | 읒 |
| $\stackrel{\square}{5}$ | $u$ | ¢ | ¢ | $\stackrel{5}{5}$ | « | 觡 |  | む | $\bullet$ | $\infty$ | ～ | む | \％ | $\stackrel{4}{4}$ | $\stackrel{\square}{\infty}$ | $\stackrel{\square}{\infty}$ | $\simeq$ | $\pm$ | ～ | ज | \％ | $\checkmark$ |  | $\exists$ | $u$ | ${ }_{\infty}$ | $\underset{\sim}{\sim}$ | ～ | $\stackrel{\square}{\infty}$ | ${ }_{\infty}$ | $\square_{\infty}$ | 动 | ～ | \％ | $\sim$ | $\sim$ | \％ | $\checkmark$ | 4 | 号 | H | \％ | $\sim$ | w | w | ～ | \％ | $\stackrel{u}{4}$ | H | $\checkmark$ | の | $\sim$ | － | $\omega$ | N | － | － | － | － | － | － | － | $\checkmark$ | Heav | 沯 |  |
| ち | ¢ | ： | む | ～ | $\square$ | n |  | $\square$ | 4 | $\stackrel{\square}{2}$ | \％ | \％ | $\square$ | $\stackrel{\square}{\square}$ | $\simeq$ | $\simeq$ | ニ | $\stackrel{\sim}{\sim}$ | $\square$ | $\stackrel{\square}{0}$ | $\sim$ | $\cong$ |  | ๙ | \％ | ～ | N | ～ | \％ | ～ | ～ | $\because$ | n | ～ | $\sim$ | \％ | $\sim$ | ～ | ～ | \％ | \％ | \％ | $\pm$ | w | ～ | $\sim$ | $\sim$ | $\square$ | S | $\infty$ | $\sigma$ | $\checkmark$ | － | $\omega$ | N | － | － | － | － | － | － | － | $\square$ | Total |  |  |
| － | － | － | － | － | － | － |  | － | － | － | － | － | － | － | － | － | － | － | － | － 0 | － | － |  | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | Lights |  |  |
| － | － | － | － | － | － | － |  |  | － | － | － | － | － | － | － | － | － |  |  | － 0 | － | － |  |  | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | Heavies | 隹 |  |
| － | － | － | － | － | － |  |  | － | － | － | － | － | － | － | － | － | － | － |  | － | － | － |  | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | Total |  |  |


| $\begin{aligned} & \circ \\ & 0 \\ & 0 \\ & 4 \\ & \hline \end{aligned}$ | 号 | ｜ $\mid$ | 范 | \％ | \％ | \％ | （ex | \％ |  | \％ | 范 | \％ | \％ |  | 尔 | \％ |  | 皆 |  | 洔 |  | （\％ | 荌 | 咅 | 炭 | 碳 |  | 淙 |  |  |  | 管 | \％ |  | \％ | 号 | 砣 |  |  | － | 亳 |  | ｜r | \％ |  | （1） | 潆 | 管 | ｜r | 管 | 䓪 | ｜ | 答管 |  | ｜rier | 荷 | ｜ |  | ｜ |  | 麇 |  | 4 | 器 | 蒤 | ｜r | 館 | 管 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| － | － | － | － | － | － | － | － | － | － | － | － | － |  | － 0 | － |  | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － 0 | － | － | － | － 0 | Lights |  |  | E | － | － 0 | － | － | － | － | － | － | － | － | $\checkmark$ A | － | E | ヶ | $\sim$ | $\sim$ | － | － | $\omega$ | $\cdots \infty$ | ¢ | $\infty$ | こ | $\bigcirc$ | $\bigcirc$ | u | \％ | $\sim$ |
| － | － | － | － | － | － | － | － | － | － | － | － | － |  | － 0 | － |  | － | － | － | － | － | $\bigcirc$ | － | － | － | － | － | － | － | － | － | － | － | － 0 | － | － | － | － 0 | Heavies |  |  | \％ | － | － 0 | －－ | － | － | － | － | － | － | $\sim$ | $\square$ | － | － | － | － | $\square$ | $\square$ | $\square$ | ${ }^{-}$ | － |  | ${ }^{-}$ | $\square$ | $\square$ | － | $\square$ | w |  |
| － | － | － | － | － | － |  |  | － |  |  | － |  |  | － |  |  |  |  |  |  | － | $\bigcirc$ 。 | － | － |  | － | － | － | － | － | － | － | － | － | － | － | － | － | Tot |  |  | 5 | － | － 0 | － 0 | － | － | － | － | － | － | － | $\sim$ | $\cdots$ | E | ¢ | $\sim$ | $\infty$ | － | $\sim$ | － | $\cdots \infty$ |  | $\bullet$ | ¢ | ¢ | $\bullet$ | 5 | $\square$ | \％ |
| ${ }^{\sim}$ | ～ | w | ${ }^{\omega}$ | $\square$ | － |  | －～ | $\omega$ |  | の | $\square$ | $u$ |  | ～ | $\sigma$ |  | \％ | 5 | あ | $\stackrel{5}{5}$ | $\infty$ | $\infty$ の | $\omega$ | $\omega$ | $\omega$ | － | － | － | － | － | － | － | － | － | － | － | $\square$ | $\square$ | ight |  |  | 5 | － | － 0 | － 0 | － | $\square$ | $\square$ | $\sim$ | － | $\square$ | $\square$ | $\checkmark$ | $\checkmark$ | の | $\infty$ | の | － | － | ＂ | $\bullet$ | \％ | \％ | ～ | ゅ | ¢ | $\checkmark$ | 5 | $\approx \sim$ | ะ |
| ${ }^{\omega}$ | ～ | － | － | － | ～ |  | $\sim$ | － |  | $\omega$ | － | － |  | $\cdots$ | $\sim$ |  | ～～ | ${ }^{\sim}$ | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － 0 | － | － | － | － | Heavie |  |  | $\stackrel{\square}{8}$ | － | － 0 | － 0 | － | － | $\square$ | $\square$ | － | － | － | － 0 | － | － | － | － | － | － | $\square$ | $\square$ | $\cdots$－ | － | － | ～ | $\omega$ | ${ }^{\omega}$ | － | $\omega{ }^{\sim}$ | ${ }^{\omega}$ |
| の | － | w | $\cdots$ | ～ | $\omega$ |  |  | $\checkmark$ |  |  | ぁ | \％ |  | \％ |  |  | $\approx$ | ¢ | 5 | $\stackrel{5}{5}$ | － | －の | $\omega$ | $\omega$ | $\omega$ | － | － | － | － | － | － | － | － | － 0 | － | 。 | $\square$ | － | Total |  |  | ก | － | － 0 | － 0 | ～ | $\sim$ | ～ | ～ | － | － | － | － | $\cdots$ | － | $\infty$ | $\sigma$ | － | － | の | 5 | $=$ | む | ๖ | ะ | $\square$ | ¢ | ぁ | $\square \mathrm{a}$ | \％ |
| $\sim$ | の | $\cdots$ | $\omega$ | $\omega$ | － |  | －w | $\omega$ |  | ${ }^{\omega}$ | ＂ | u |  | 4 |  |  | $\bullet \infty$ | $\bigcirc$ | － 0 | $\sim$ | ～ | $\sim$ | $\square$ | ～ | w | － | $\omega$ | $\sim$ | － | － | － | － | $\square$ | ～ | $\sim$ w | － | w | 0 | Light |  |  | － | － | － 0 | － 0 | － | － | － | － | － | － | － | － 0 | － | － | － | － | － | － | － | － | － 0 | 。 | － | － | － | － | － | － 0 | － |
| ～ | ＂ | ${ }^{\circ}$ | － | u | － |  | － | u | － | ${ }^{\omega}$ | － | ～ |  | ～ |  |  | u | $\sigma$ | 04 | －w | － | － | － | － | － | － | － | － | － | － | － | － | － | － 0 | － | － | － | － | Heavie |  |  | － | － | － 0 | －－ | － | － | － | － | － | － | － | － 0 | － | － | － | － | － | － | － | － | － 0 | 。 | － | － | － | － | － | － 0 | － |
| － | E | ～ | $\sim$ |  | $\infty$ |  |  | $\infty$ |  |  | $\cdots$ |  |  |  | － |  |  |  |  |  |  | $\cdots$ | － |  | $\sim$ | － |  | ～ | － | － | － | － | － |  |  |  | $\omega$ |  | $\sim$ Total |  |  | － | － | － | －－ | － | － | － | － | － | － | － | － 0 |  | － | － | － | － | － | － | － |  |  | － | － | － | － | － | － 0 |  |
| $\sim$ | ～ | $\sim$ | － | － | － |  | 。 | － |  | － | － | － |  | － |  |  | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － 0 | － | － | － | － | Light |  |  | － | － | － 0 | － 0 | － | － | － | － | － | － | － | － 0 | － | － | － | － | － | － | － | － | － 0 | － | － | － | － | － | － | － 0 |  |
| － | － | － | － | － | － |  | － | － | $\sim$ | $\sim$ | － | － |  |  | － |  | － 0 | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － 0 | － | － | － | － 0 | Heavies |  |  | － | － | － 0 | －－ | － | － | － | － | － | － | － | － 0 | － | － | － | － | － | － | － | － | － 0 | 。 | － | － | － | － | － | － 0 |  |
| $\sim$ | ～ | － | － | － | － |  | － | － |  | － | － |  |  |  |  |  |  | － |  |  | － | － | － | － | － | － | － | － | － | － | － | － | － |  | － 0 | － | － | －${ }^{\circ}$ | Total |  |  | － | － | － | － 0 | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － 0 |  | － | － | － | － | － | － 0 |  |
| $\stackrel{\square}{\infty}$ | $\checkmark$ | ゅ | 5 | $\square$ | $\simeq$ |  | ～ | $\approx$ |  | $\approx$ | ะ | ～ |  | あ |  | $\bigcirc$ | $=$ | $\square$ |  | い | $\checkmark$ | $\sim$ w | $\square$ | － | ～ | ～ | ～ | ～ | － | － | － | － | － | $\square$ | $\cdots$ | － | $\omega$ | w～ | Light |  |  | 2 | － | － | $\square$ | $\stackrel{+}{ }$ | $\square$ | $\stackrel{ }{+}$ | ～ | ～ | $\omega$ | ～ | $\square$ | $\checkmark$ | w | － | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\sigma$ | $\checkmark \sim$ | － | の | $\checkmark$ | u | $\omega$ | ～ | ～ |  |
| ＊ | $\sigma$ | $\checkmark$ | ${ }^{\circ}$ | － | $\bigcirc$ |  | $\pm$ | $\bigcirc$ |  | \％N | ～ | － |  | ${ }^{\omega}$ |  |  | － | － | － | $\omega$ | － | －w | w | － | ～ | ～ | ～ | $\sim$ | － | $\stackrel{ }{+}$ | － | － | $\square$ | －w | $\omega$ w | ${ }^{\omega}$ | ～ | $\square$ | Heavies |  |  | \％ | － | － | － | － | $\square$ | ～ | $\square$ | $\square$ | － | － | － | － | － | － | － | $\square$ | － | $\square$ | － | － 0 |  |  | $\square$ | － | － | － | － 0 |  |
| $\sim$ | $\approx$ | $\pi$ | $\sim$ | $\approx$ | \％ |  | w | $\underset{\sim}{\sim}$ |  | \％ | $\underline{\square}$ | \％ |  | $\simeq$ |  | F | $=$ | 5 |  | 5 | ＝ | $=0$ | － | $\sim$ | － | － | － | － | － | － | － | － | － | $\sim$ | － | $\checkmark$ | $\sim$ | －${ }^{\circ}$ | $\omega$ Total |  |  | \％ | － | － | －～ | $\sim \sim$ | ～ | ${ }^{\omega}$ | ш | $\omega$ | － | ～ | － | － | － | － | $\bigcirc$ | $\cdots$ | $\circ$ | $\infty$ | $\sigma$ | $\checkmark \sim$ | ＂ | $\cdots$ | $\circ$ | $\circ$ | $\omega$ | $\sim$ | $\sim \sim$ |  |
| － | － | － | － | － | 。 |  | － | － |  | － 0 | － | － |  | － |  |  | － | － |  | －。 | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | Lights |  |  | \％ | － | $\square$ | ～w | $\sim$～ | $\omega$ | ～ | $\square$ | $\square$ | － | － | ＊ | － | － | $\sigma$ | ～ | $\checkmark$ | $\stackrel{\rightharpoonup}{\square}$ | a | \％ | ゅ | $\overleftarrow{5}$ | $\pm$ | $\pm$ | \％ | u | $\checkmark$ | $\because$ |  |
| － | － | － | － | － | 。 |  | － | － |  | － 0 | － | － |  | － |  |  | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － 0 | － | － | －$\circ$ | Heav |  |  | สั | － | $\square$ | $\square \square$ | － | － | ${ }^{\sim}$ | ～ | ～ | － | ～ | ～ | $\omega$ w | ～ | $\square$ | － | － | － | － | － | －N | ～ |  | $\omega$ | － | $u$ | ＂ | の 0 |  |
| － | － | － | － |  | － |  | － | － |  |  |  |  |  |  |  |  |  |  |  |  |  |  | － |  |  |  |  | － |  |  | － | － |  |  |  | － | － | －$\circ$ | Tota |  |  | \％ | ～ | $\sim$ | $\omega^{\circ}$－ | $\sim$ | － | ${ }^{\omega}$ | ${ }^{\omega}$ | $\omega$ | ～ | の | $\sigma$ |  |  | $\checkmark$ | \％ | $\because$ | ゅ | $\sim$ | \％ | 5 | $\simeq$ | \％ | \％ | \％ | \％ | ${ }_{0}$ | ※ |  |
| － | $\stackrel{\square}{-}$ | － | － | － | 。 |  | － | － |  | ＇ | ＊ | － |  | － 0 |  | －N | ～N |  |  | $\cdots$～ | $\sim$ | $\sim$ | － | － | $\stackrel{\sim}{+}$ | － |  | － |  | － | － | － | － | － | － 0 | － | － | － 0 | Lights |  |  | \％ | － | $\checkmark$ | $\square{ }^{-}$ | － | － | － | － | $\square$ | $\square$ | － | ＊ | － | － | $\square$ | － | $\square$ | $\square$ | ～ | ～ | w |  |  | $\infty$ | $\infty$ | $\checkmark$ | － | $\omega$ |  |
| － | － | － | $\square$ | － | － |  | －${ }^{-}$ | － |  | － 0 | $\bigcirc$ | － |  | $\square{ }^{-}$ |  | $\checkmark$ | －${ }^{-}$ | － | － 0 | － 0 | － | $\sim$ | ～ | ～ | $\sim$ | － | － | － | － | － | － | － | － | － | － | － | － | －$\circ$ | －Heavies |  |  | \％ | － | － | －－ | －～ | $\omega$ | $\omega$ | $\omega$ | ～ | ～ | $\omega^{\omega}$ | $\omega$ | $\cdots$ A | －w | － | $\omega^{\omega}$ | － | $\checkmark$ | $\checkmark$ | $\omega$ | $\omega$ | ～ |  | $\checkmark$ | $\sim$ | の | $\infty$ | $\sim$ | ¢ |
| － | $\stackrel{\square}{ }$ | － | － |  | $\square$ |  | －${ }^{-}$ | － |  | $\checkmark$ | $\sim$ |  |  |  |  |  |  |  |  |  |  |  | w |  | $\sim \sim$ |  |  | 。 |  |  | － | － |  |  |  | － |  |  | rotal |  |  | W | － | $\checkmark$ | $\square{ }^{-}$ | ～ | ${ }^{\omega}$ | ${ }^{\omega}$ | ${ }^{\omega}$ | ${ }^{\omega}$ | $\omega$ | $\sim$ | $\checkmark$ | －$\infty$ |  | $\checkmark$ | － | $\checkmark$ | $\sigma$ | $\sim$ | ＂ |  | $\bullet$ |  | む | 5 | $E$ | $\sim$ | $\square$ |  |
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| $10: 15$ to $11: 15$ | 0 | 0 | 0 | 2 | 3 | 5 | 7 | ${ }^{3}$ | 10 | 2 | 0 | 2 | 18 | 5 | ${ }^{23}$ | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10:30 to $11: 30$ | 0 | 0 | 0 | 4 | 4 | 8 | 4 | 2 | 6 | 1 | 0 | 1 | 22 | 3 | 25 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 |
| 10:45 to $11: 45$ | 0 | 0 | 0 | 5 | ${ }^{3}$ | 8 | 6 | 2 | 8 | 0 | 0 | 0 | 24 | ${ }^{3}$ | 27 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:00 to $^{12: 00}$ | 0 | 0 | 0 | 5 | 3 | 8 | 7 | ${ }^{3}$ | 10 | 0 | 0 | 0 | 24 | ${ }^{3}$ | 27 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| $11: 15$ to $12: 15$ | 0 | 0 | 0 | 6 | 3 | 9 | 8 | 3 | 11 | 0 | 0 | 0 | 28 | 3 | ${ }^{31}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 113:30 to $^{12} \mathbf{1 2} 3$ | 0 | 0 | 0 | 7 | 3 | 10 | 10 | 3 | ${ }^{13}$ | 1 | 0 | 1 | 26 | 4 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 to $12: 45$ | 0 | 0 | 0 | ${ }^{6}$ | 2 | 8 | 10 | 4 | 14 | 1 | 0 | 1 | 25 | 4 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| $\begin{array}{llll}12: 00 & \text { to } & 13: 00\end{array}$ | 0 | 0 | 0 | 5 | 1 | 6 | 10 | 5 | 15 | 1 | 0 | 1 | 21 | 5 | 26 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:15 to $^{13} \mathbf{1 3} \mathbf{1 5}$ | 0 | 0 | 0 | 3 | 1 | 4 | 7 | 5 | 12 | 1 | 0 | 1 | ${ }^{14}$ | 5 | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:30 to $13: 30$ | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 4 | 9 | 0 | 0 | 0 | ${ }^{17}$ | 9 | 26 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:45 | 0 | 0 | 0 | 1 | 1 | 2 | ${ }^{3}$ | 6 | 9 | 0 | 0 | 0 | 20 | 8 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 13:00 to 14:00 | 0 | 0 | 0 | 2 | 2 | 4 | 5 | 4 | 9 | 0 | 0 | 0 | 29 | 7 | 36 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 13:15 | 0 | 0 | $\bigcirc$ | 5 | 2 | 7 | 7 | 4 | ${ }^{11}$ | 0 | 0 | - | ${ }^{36}$ | 6 | 42 | 0 | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 |
| 1330 to 14.30 | 0 | 0 | 0 | 6 | 4 | 10 | 6 | 6 | 12 | 0 | 0 | 0 | 40 | 3 | 43 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 13:45 to 14:45 | 0 | 0 | 0 | 5 | ${ }_{4}$ | 9 | 9 | 4 | ${ }^{13}$ | 0 | 0 | 0 | 40 | 6 | 46 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 |
| 14:00 to 15:00 | 0 | 0 | 0 | 6 | 4 | 10 | 6 | 7 | ${ }^{13}$ | 0 | 0 | 0 | ${ }^{37}$ | ${ }^{6}$ | ${ }^{43}$ | 0 | 0 | 0 | 1 | 0 | 1 | - | 0 | 0 |
| 14.15 to $15: 15$ | 0 | 0 | 0 | 4 | 4 | 8 | 10 | 9 | 19 | 0 | 0 | 0 | 33 | 6 | 39 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 |
| 14.30 to 15.30 | 0 | 0 | 0 | 3 | 2 | 5 | ${ }^{13}$ | 7 | 20 | 0 | 0 | 0 | 23 | 6 | 29 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 |
| 14.45 to 15.45 | 0 | 0 | 0 | 5 | 1 | 6 | ${ }^{11}$ | ${ }^{13}$ | 24 | 0 | 0 | 0 | 24 | 5 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - | 0 |
| 15:00 to $16: 00$ | 0 | 0 | 0 | 3 | 0 | 3 | 12 | 14 | 26 | 0 | 0 | 0 | 19 | 5 | 24 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | 0 | 0 | 0 | 2 | 2 | 4 | 15 | 17 | 32 | 0 | 0 | 0 | 19 | 6 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15:30 to $16: 30$ | 0 | 0 | 0 | 3 | 2 | 5 | ${ }^{17}$ | 19 | ${ }^{36}$ | 0 | 0 | 0 | 24 | 5 | 29 | - | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15:45 to 16.45 | 0 | 0 | 0 | 1 | 2 | 3 | 22 | 14 | ${ }^{36}$ | 0 | 0 | 0 | 16 | 8 | 24 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:00 to 17:00 | 0 | 0 | 0 | 2 | 2 | 4 | 24 | ${ }^{12}$ | ${ }^{36}$ | 0 | 0 | 0 | 22 | ${ }^{11}$ | 33 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:15 to $17: 15$ | 0 | 0 | 0 | ${ }^{3}$ | 0 | 3 | ${ }^{18}$ | ${ }^{8}$ | 26 | 0 | 0 | 0 | ${ }^{21}$ | ${ }^{10}$ | ${ }^{31}$ | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 |
| 16:30 to 17730 | 0 | 0 | 0 | 3 | 1 | 4 | 16 | 6 | 22 | 0 | 0 | 0 | 20 | 10 | 30 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 |
| 16:45 to 17:45 | 0 | 0 | 0 | 4 | 1 | 5 | ${ }^{11}$ | 4 | 15 | 0 | 0 | 0 | 23 | 7 | 30 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 |
| 17:00 to $18: 00$ | 0 | 0 | 0 | 4 | 1 | 5 | 12 | 2 | 14 | 0 | 0 | 0 | ${ }^{17}$ | 4 | ${ }^{21}$ | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 |
| $17 / 15$ to $18: 15$ | 0 | 0 | 0 | 4 | 1 | 5 | 12 | 0 | 12 | 0 | 0 | 0 | 17 | 3 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17730 to $18: 30$ | 0 | 0 | 0 | 3 | 0 | 3 | ${ }^{11}$ | 0 | ${ }^{11}$ | 0 | 0 | 0 | ${ }^{12}$ | 2 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:45 | 0 | 0 | 0 | 3 | $\bigcirc$ | 3 | ${ }^{11}$ | 2 | ${ }^{13}$ | 0 | 0 | - | 9 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 18:00 to $19: 00$ | 0 | 0 | $\bigcirc$ | 4 | 0 | 4 | 6 | 2 | 8 | 0 | 0 | 0 | 8 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 18.15 to $19: 15$ | 0 | 0 | 0 | 7 | 1 | 8 | 3 | 2 | 5 | 0 | 0 | 0 | 5 | 0 | 5 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 |
| 18330 to $19: 30$ | 0 | 0 | 0 | 9 | 1 | 10 | 2 | 2 | 4 | 0 | 0 | 0 | 5 | 1 | 6 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 |
| 18:45 to $19: 45$ | 0 | 0 | 0 | ${ }^{11}$ | 1 | 12 | 1 | 1 | 2 | 0 | 0 | 0 | 4 | 1 | 5 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 |
| 19:00 to 20.00 | 0 | 0 | 0 | 9 | 1 | 10 | 2 | 1 | 3 | 0 | 0 | 0 | 2 | 1 | 3 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 |
| $19: 15$ to $20: 15$ | 0 | 0 | 0 | 5 | 0 | 5 | 2 | 1 | 3 | 0 | 0 | 0 | 1 | 1 | 2 | - | 0 | 0 | 1 | 0 | 1 | 0 | - | 0 |
| 19330 to 20.30 | 0 | 0 | 0 | ${ }^{3}$ | 0 | 3 | 2 | 1 | 3 | 0 | 0 | 0 | 0 | $\bigcirc$ | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 |
| 19:45 ${ }^{\text {to }}$ 20:45 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 1 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 20:00 to 21:00 | 0 | 0 | $\bigcirc$ | 0 | 0 | 0 | 3 | 1 | 4 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 20.15 to $21: 15$ | 0 | 0 | 0 | 0 | $\bigcirc$ | 0 | 3 | 1 | 4 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 20:30 to $21: 30$ | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 1 | 5 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 20:45 to 21:45 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 21:00 to $22: 00$ | 0 | 0 | 0 | 0 | $\bigcirc$ | 0 | 4 | 0 | 4 | 0 | 0 | 0 | $\bigcirc$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - | 0 |
| 21.15 to 22.15 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | $\bigcirc$ | 0 | 0 | 0 | 0 | 0 | 0 |
| 21:30 to $22: 30$ | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 21:45 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 0 | 0 | 0 | 2 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 22:00 | 0 | 0 | 0 | 0 | 0 | 0 | ${ }^{3}$ | 0 | 3 | 0 | 0 | 0 | 2 | 1 | ${ }^{3}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 22:15 ${ }^{2}$ to 23.15 | 0 | 0 | 0 | 0 | 0 | 0 | ${ }^{3}$ | 0 | 3 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 22:30 to $23: 30$ | 0 | 0 | 0 | 0 | $\bigcirc$ | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | $\bigcirc$ | 0 | 0 | $\bigcirc$ | 0 | 0 | 0 |
| 22:45 ${ }^{2}$ to 23.45 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 |
| 23:00 to 0.00 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 24hr Totals | 0 | 0 | 0 | 110 | 25 | 135 | 137 | ${ }^{73}$ | 210 | 3 | 1 | 4 | 292 | 79 | ${ }^{371}$ | - | 0 | 0 | ${ }^{11}$ | 6 | 17 | - | 0 | 0 |



Jerrara Rd

|  | 㬰 | 铦 | 勫 | 管 | 管 | 岩 | ｜r | 苞 | 䓂 | 范 | H | （ | （1） |  |  |  | 苞 | 䓂 | 总 | 葡 | 苞 | 呂 | 倉 | 茧 | 促 |  |  | 管 | 笭 | \％ |  | 范 |  |  |  | \％ |  |  | 资 |  | 萢 | \％ | 念 |  | 蔞 |  | 会 | ｜r |  |  |  | ｜r | 苞 | 管 | 茧 | 隿 | 芯 \％ \％ ¢ | 落 | 令 | ｜l｜ | 鴯 |  |  |  |  |
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| － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | T | Total |  |  |
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| 9 | $\check{\square}$ | 2 | \％ | ஃ | $\geq$ | v | $\checkmark$ | の | ๕ | \％ | \％ | ＊ | ¢ | ${ }_{\infty}$ | $\backsim$ | $\check{\square}$ | $\checkmark$ | ू | E | $\pm$ | के | a | $\pm$ | E | $\stackrel{\text { a }}{ }$ | ش | \＆ | ¢ | a | E | ش | ＊ | a | ¢ | \％ | « | $\stackrel{\square}{\square}$ | « | ～ | ¢ | w | \％ | w | \％ | ～ | $\stackrel{\square}{0}$ | $\square$ | ゅ | L | ～ | $\bullet$ | の | $\sim$ | － | N | $\omega$ | の | $\sim$ | $\bullet$ | $\checkmark$ | $\sim$ | To | Total |  |  |
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| － | － | － | － | － | － | － | － | － | － | － | － | － |  |  | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | －${ }^{\text {T }}$ | Total |  |  |
| － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | 。 | 。 | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | L | Lights |  |  |
| － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | H | Heavies |  |  |
| － | － | － | － | － | － | － | － | － | － | － | － | － | － |  | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | T | Total |  |  |
| － | － | － | － | － | － | － | － | － | － | － | － | － | － |  | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － 4 | Lights |  |  |
| － | － | － | － | － | － | － | － | － | － | － | － | － |  |  | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | H | Heavies |  |  |
| － | － | － | － | － | － | － | － | － | － | － | － | － | － |  | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | T | Total |  | $\stackrel{\square}{\square}$ |
| － | － | － | － | － | － | － | － | － | － | － | － |  | － |  | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | Li | Lights |  | O |
| － | － | － | － | － | － | － | － | － | － | － | － |  |  |  | － | － | － | － | － | － | － | － | － | － | － | － | － | － | 。 | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | H | Heavies | \％ |  |
| － | － | － | － | － | － | － | － | － | － | － | － |  |  |  | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | 。 | － | T | Total |  |  |
| － | － | － | － | － | － | － | － | － | － | － | － | － |  |  | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | Li | Lights |  |  |
| － | － | － | － | － | － | － | － | － | － | － | － | － | － |  | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | H | Heavies |  |  |
| － | － | － | － | － | － | － | － | － | － | － | － |  | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | － | T | Total |  |  |


| 15：30 to 16.30 | 0 | 0 | 0 | 0 | 7 | 7 | 48 | ${ }^{14}$ | 62 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15．45 to 16：45 | 0 | 0 | 0 | 1 | 6 | 7 | 30 | 17 | 47 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16：00 to 17700 | 0 | 0 | 0 | 1 | 4 | 5 | 40 | ${ }^{20}$ | 60 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| $16: 15$ to 17：15 | 0 | 0 | 0 | 1 | 2 | 3 | 39 | 19 | 58 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16.30 to 17.30 | 0 | 0 | 0 | ${ }^{3}$ | 2 | 5 | 40 | 19 | 59 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16：45 to 17745 | 0 | 0 | 0 | 3 | 1 | 4 | 45 | ${ }^{14}$ | 59 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17：00 to 18：00 | 0 | 0 | 0 | ${ }^{3}$ | 2 | 5 | ${ }_{3}$ | 9 | ${ }^{41}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17：15 to 18：15 | 0 | 0 | 0 | 3 | 1 | 4 | 33 | 5 | 38 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17：30 to 18.30 | 0 | 0 | 0 | 1 | 1 | 2 | 28 | 4 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17：45 to 18，45 | 0 | 0 | 0 | 0 | 1 | 1 | 22 | 3 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 18.00 to 19.00 | 0 | 0 | 0 | 0 | 0 | 0 | 20 | 4 | 24 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 18.15 to $19: 15$ | 0 | 0 | 0 | 0 | 0 | 0 | ${ }^{11}$ | 5 | ${ }^{16}$ | 0 | 0 | － | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | 0 | 0 | 0 | 0 | 0 | 0 | 10 | ${ }^{6}$ | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 18.45 to 19：45 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 5 | ${ }^{14}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 19：00 to 20.00 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 4 | ${ }^{13}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 19.15 to $20: 15$ | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 5 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 19：30 to 20.30 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 3 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 19：45 to 20.45 | 0 | 0 | 0 | 1 | 0 | 1 | 8 | 4 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | － | 0 | 0 | 0 | 0 | 0 | 0 |
| 20：00 to 21：00 | 0 | 0 | 0 | 1 | 0 | 1 | 7 | 5 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 20：15 to 21：15 | 0 | 0 | 0 | 2 | 0 | 2 | 5 | 4 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 20：30 to $^{21: 30}$ | 0 | 0 | 0 | 2 | 0 | 2 | 4 | 3 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 20．45 to 21：45 | 0 | 0 | 0 | 1 | 0 | 1 | 2 | 2 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | － | 0 | 0 |
| 21：00 to 22：00 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 21：15 to 22：15 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 21：30 to 22：30 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 21：45 to 22：45 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 5 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 22：00 to 23：00 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 4 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 22：15 to 23：15 | 0 | 0 | 0 | 1 | 0 | 1 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 22：30 to 23.30 | 0 | 0 | 0 | 1 | 0 | 1 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 22，45 to 23，45 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 23．00 to 0.00 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 24hr Totals | － | － | 0 | 56 | 110 | 166 | 463 | 269 | 732 | － | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | － | 0 | $\bigcirc$ |


| Approach <br> Direction |  |  | Jerrara Rd |  |  |  |  |  |  |  |  |  |  |  | Hume Hwy Off Ramp |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Direction 7 （Left Turn） |  |  | Direction 8 （Through） |  |  | Direction 9 <br> （Right Turn） |  |  | Direction 9U （U Turn） |  |  | Direction 10 （Left Turn） |  |  | Direction 11 （Through） |  |  | Direction 12 （Right Turn） |  |  | $\begin{aligned} & \text { Direction 12U } \\ & \text { (U Turn) } \end{aligned}$ |  |  |
| Time Period |  |  |  |  |  | $\begin{aligned} & \text { n } \\ & \text { 喜 } \\ & \hline \end{aligned}$ |  | $\stackrel{\text { ® }}{6}$ | $\begin{aligned} & \text { n } \\ & \stackrel{y}{w}{ }^{2} \\ & \hline \end{aligned}$ |  |  | $\begin{aligned} & \text { 㰻 } \\ & \text { 器 } \\ & \hline \end{aligned}$ |  |  | $\begin{aligned} & \text { n } \\ & \substack{\text { an } \\ \hline} \\ & \hline \end{aligned}$ |  |  | $\begin{array}{r} \text { n } \\ \substack{\text { 曼 } \\ \hline} \end{array}$ |  | $\begin{gathered} \bar{\circ} \mathrm{E} \\ \hline \end{gathered}$ | $\begin{aligned} & \text { n } \\ & \substack{\text { In } \\ \hline} \end{aligned}$ |  | 든 | $\begin{aligned} & \text { n} \\ & \substack{\text { ati } \\ \hline} \\ & \hline \end{aligned}$ |  | $\stackrel{\bar{\circ}}{\stackrel{\rightharpoonup}{\circ}}$ |
| 0：00 | to | 1：00 | 3 | 0 | 3 | 5 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 1 | 0 | 0 | 0 |
| 0：15 | to | 1：15 | 3 | 0 | 3 | 6 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 1 | 0 | 1 | 0 | 0 | 0 |
| 0：30 | to | 1：30 | 2 | 0 | 2 | 3 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 1 | 0 | 1 | 0 | 0 | 0 |
| 0：45 | to | 1：45 | 2 | 0 | 2 | 3 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 1 | 0 | 0 | 0 |
| 1：00 | to | 2：00 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 1 | 0 | 0 | 0 |
| 1：15 | to | 2：15 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 |
| 1：30 | to | 2：30 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 |
| 1：45 | to | 2：45 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2：00 | to | 3：00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2：15 | to | 3：15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2：30 | to | 3：30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2：45 | to | 3：45 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3：00 | to | 4：00 | 1 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 1 | 0 | 0 | 0 |
| 3：15 | to | 4：15 | 1 | 0 | 1 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 1 | 0 | 0 | 0 |
| 3：30 | to | 4：30 | 1 | 0 | 1 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 0 | 2 | 0 | 0 | 0 |
| 3：45 | to | 4：45 | 1 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 0 | 0 | 0 | 5 | 0 | 5 | 0 | 0 | 0 |
| 4：00 | to | 5：00 | 1 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 4 | 7 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 0 | 0 |
| 4：15 | to | 5：15 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 6 | 9 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 0 | 0 |
| 4：30 | to | 5：30 | 1 | 4 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 6 | 11 | 0 | 0 | 0 | 7 | 0 | 7 | 0 | 0 | 0 |
| 4：45 | to | 5：45 | 1 | 7 | 8 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 5 | 12 | 0 | 0 | 0 | 9 | 0 | 9 | 0 | 0 | 0 |
| 5：00 | to | 6：00 | 0 | ${ }^{11}$ | 11 | 0 | 3 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 3 | 12 | 0 | 0 | 0 | 16 | 0 | 16 | 0 | 0 | 0 |
| 5：15 | to | 6：15 | 2 | 14 | 16 | 3 | 3 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 18 | 2 | 20 | 0 | 0 | 0 | ${ }^{21}$ | 2 | 23 | 0 | 0 | 0 |
| 5：30 | to | 6：30 | 5 | 11 | 16 | 6 | 3 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 22 | 2 | 24 | 0 | 0 | 0 | 18 | 4 | 22 | 0 | 0 | 0 |
| 5：45 | to | 6：45 | 6 | 11 | 17 | 6 | 2 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 21 | 2 | 23 | 0 | 0 | 0 | 18 | 6 | 24 | 0 | 0 | 0 |
| 6：00 | to | 7：00 | 6 | 8 | 14 | 6 | 1 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 17 | 2 | 19 | 0 | 0 | 0 | 22 | 7 | 29 | 0 | 0 | 0 |
| 6：15 | to | 7：15 | 4 | 8 | 12 | 4 | 1 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 1 | 10 | 0 | 0 | 0 | 28 | 6 | 34 | 0 | 0 | 0 |
| 6：30 | to | 7：30 | 1 | 9 | 10 | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 1 | 4 | 0 | 0 | 0 | 30 | 5 | 35 | 0 | 0 | 0 |
| 6：45 | to | 7：45 | 0 | 12 | 12 | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 0 | 0 | 0 | 29 | 3 | 32 | 0 | 0 | 0 |
| 7：00 | to | 8：00 | 0 | 13 | 13 | 2 | 2 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 18 | 2 | 20 | 0 | 0 | 0 |
| 7：15 | to | 8：15 | 0 | 14 | 14 | 2 | 2 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 1 | 3 | 4 | 9 | 4 | 13 | 0 | 0 | 0 |
| 7：30 | to | 8：30 | 1 | 17 | 18 | 2 | 2 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 2 | 5 | 3 | 3 | 6 | 7 | 5 | 12 | 0 | 0 | 0 |
| 7：45 | to | 8：45 | 1 | 12 | ${ }^{13}$ | ${ }^{2}$ | 3 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 2 | 7 | 3 | 3 | 6 | 4 | 5 | 9 | 0 | 0 | 0 |
| 8：00 | to | 9：00 | 1 | ${ }^{11}$ | 12 | 1 | 3 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 3 | 9 | ${ }^{3}$ | 3 | 6 | 5 | 6 | 11 | 0 | 0 | 0 |
| 8：15 | to | 9：15 | 2 | 8 | 10 | 2 | 3 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | ${ }^{6}$ | 2 | 8 | ${ }^{3}$ | 0 | 3 | ${ }^{3}$ | 5 | 8 | 0 | 0 | 0 |
| 8：30 | to | 9：30 | 1 | 7 | 8 | 2 | 3 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 1 | 5 | 1 | 0 | 1 | 3 | 3 | 6 | 0 | 0 | 0 |
| 8：45 | to | 9：45 | 1 | 7 | 8 | 2 | 3 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 3 | 1 | 0 | 1 | 5 | 3 | 8 | 0 | 0 | 0 |
| 9：00 | to | 10：00 | 2 | 7 | 9 | 2 | 2 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 1 | 0 | 1 | 4 | 4 | 8 | 0 | 0 | 0 |
| 9：15 | to | 10：15 | 1 | 8 | 9 | 2 | 2 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 3 | 0 | 0 | 0 | 6 | 2 | 8 | 0 | 0 | 0 |
| 9：30 | to | 10：30 | 1 | 6 | 7 | 3 | 3 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 2 | 5 | 0 | 0 | 0 | 9 | 3 | 12 | 0 | 0 | 0 |
| 9：45 | to | 10：45 | 1 | 8 | 9 | 3 | 2 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 2 | 6 | 1 | 0 | 1 | 7 | 5 | 12 | 0 | 0 | 0 |
| 10：00 | to | 11：00 | 0 | 11 | 11 | 4 | 1 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 2 | 7 | 1 | 1 | 2 | 8 | 4 | ${ }^{12}$ | 0 | 0 | 0 |


| 10:15 to 11:15 | 0 | 14 | 14 | 2 | 2 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 2 | 6 | 2 | 1 | 3 | 9 | 4 | 13 | 0 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10:30 to 11:30 | 0 | 17 | 17 | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 4 | 2 | 1 | 3 | 8 | 5 | 13 | 0 | 0 | 0 |
| 10:45 to 11:45 | 0 | 14 | 14 | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 3 | 1 | 1 | 2 | 9 | 4 | 13 | 0 | 0 | 0 |
| 11:00 to 12:00 | 1 | 12 | 13 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 11 | 4 | 15 | 0 | 0 | 0 |
| 11:15 to 12:15 | 2 | 9 | ${ }^{11}$ | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 1 | 0 | 1 | 13 | 4 | 17 | 0 | 0 | 0 |
| 11:30 to $12: 30$ | 2 | 7 | 9 | 1 | 3 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 3 | 1 | 0 | 1 | 16 | 3 | 19 | 0 | 0 | 0 |
| 11:45 to 12:45 | 3 | 10 | 13 | 1 | 3 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 3 | 6 | 1 | 0 | 1 | 16 | 3 | 19 | 0 | 0 | 0 |
| 12:00 to 13:00 | 3 | 9 | 12 | 2 | 3 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 4 | 8 | 2 | 0 | 2 | 14 | 3 | 17 | 0 | 0 | 0 |
| 12:15 to 13:15 | 8 | 9 | 17 | 2 | 3 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 3 | 6 | 3 | 0 | 3 | 9 | 3 | 12 | 0 | 0 | 0 |
| 12:30 to $13: 30$ | 10 | 7 | 17 | 1 | 3 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 4 | 8 | 5 | 0 | 5 | 3 | 2 | 5 | 0 | 0 | 0 |
| 12:45 to 13:45 | 9 | 8 | 17 | 1 | 5 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 4 | 8 | 5 | 0 | 5 | 2 | 3 | 5 | 0 | 0 | 0 |
| 13:00 to 14:00 | 9 | 8 | 17 | 2 | 4 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 3 | 7 | 6 | 0 | 6 | 4 | 3 | 7 | 0 | 0 | 0 |
| 13:15 to 14:15 | 4 | 6 | 10 | 3 | 4 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 4 | 9 | 5 | 0 | 5 | 8 | 3 | 11 | 0 | 0 | 0 |
| 13:30 to $14: 30$ | 2 | 6 | 8 | 3 | 5 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 2 | 7 | 5 | 0 | 5 | 9 | 5 | 14 | 0 | 0 | 0 |
| 13:45 to 14:45 | 3 | 3 | 6 | 4 | 3 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 4 | 7 | 5 | 1 | 6 | 10 | 5 | 15 | 0 | 0 | 0 |
| 14:00 to 15:00 | 3 | 4 | 7 | 2 | 6 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 6 | 8 | 3 | 2 | 5 | 10 | 5 | 15 | 0 | 0 | 0 |
| 14:15 to 15:15 | 4 | 6 | 10 | 6 | 9 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 6 | 3 | 2 | 5 | 7 | 5 | 12 | 0 | 0 | 0 |
| 14:30 to 15:30 | 5 | 6 | ${ }^{11}$ | 9 | 7 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 10 | 1 | 2 | 3 | 6 | 3 | 9 | 0 | 0 | 0 |
| 14:45 to 15:45 | 6 | 5 | ${ }^{11}$ | 8 | 12 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 8 | 2 | 1 | 3 | 7 | 3 | 10 | 0 | 0 | 0 |
| 15:00 to 16:00 | 5 | 3 | 8 | 8 | 12 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 8 | 3 | 0 | 3 | 6 | 3 | 9 | 0 | 0 | 0 |
| 15:15 to 16:15 | 9 | 1 | 10 | 11 | 12 | 23 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 10 | 2 | 0 | 2 | 6 | 7 | 13 | 0 | 0 | 0 |
| 15:30 to $16: 30$ | 9 | 1 | 10 | 10 | 14 | 24 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 6 | 7 | 3 | 0 | 3 | 10 | 7 | 17 | 0 | 0 | 0 |
| 15:45 to 16:45 | 7 | 2 | 9 | 14 | 10 | 24 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 5 | 6 | 2 | 0 | 2 | 9 | 6 | 15 | 0 | 0 | 0 |
| 16:00 $\quad$ to 17:00 | 7 | 2 | 9 | 15 | 9 | 24 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 3 | 5 | 2 | 0 | 2 | 11 | 5 | 16 | 0 | 0 | 0 |
| 16:15 to 17:15 | 3 | 4 | 7 | 7 | 6 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 3 | 2 | 0 | 2 | 14 | 2 | 16 | 0 | 0 | 0 |
| 16:30 to 17:30 | 3 | 3 | 6 | 6 | 4 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 3 | 0 | 3 | 12 | 3 | 15 | 0 | 0 | 0 |
| 16:45 to 17:45 | 7 | 2 | 9 | 2 | 3 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 3 | 0 | 3 | 13 | 2 | 15 | 0 | 0 | 0 |
| 17:00 to 18:00 | 9 | 2 | ${ }^{11}$ | 3 | 1 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 4 | 0 | 4 | 12 | 2 | 14 | 0 | 0 | 0 |
| 17:15 $\quad$ to $18: 15$ | 9 | 1 | 10 | 6 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 4 | 0 | 4 | 10 | 1 | 11 | 0 | 0 | 0 |
| 17:30 $\quad$ to $18: 30$ | 10 | 1 | 11 | 6 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 2 | 0 | 2 | 9 | 0 | 9 | 0 | 0 | 0 |
| 17:45 to $18: 45$ | 6 | 1 | 7 | ${ }^{6}$ | 1 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 8 | 1 | 9 | 0 | 0 | 0 |
| 18:00 to 19:00 | 4 | 1 | 5 | 4 | 1 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 1 | 8 | 0 | 0 | 0 |
| 18:15 to 19:15 | 2 | 0 | 2 | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 2 | 11 | 0 | 0 | 0 |
| 18:30 to $19: 30$ | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 2 | 13 | 0 | 0 | 0 |
| 18:45 to 19:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 2 | 14 | 0 | 0 | 0 |
| 19:00 to 20:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 2 | 13 | 0 | 0 | 0 |
| 19:15 to 20:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 1 | 8 | 0 | 0 | 0 |
| 19:30 to 20:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 5 | 1 | 6 | 0 | 0 | 0 |
| 19:45 to 20:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 0 | 0 | 3 | 1 | 4 | 0 | 0 | 0 |
| 20:00 to 21:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 0 | 0 | ${ }^{3}$ | 1 | 4 | 0 | 0 | 0 |
| 20:15 to 21:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 0 | 0 | 3 | 1 | 4 | 0 | 0 | 0 |
| 20:30 to 21:30 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 4 | 1 | 5 | 0 | 0 | 0 |
| 20:45 to 21:45 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 0 | 0 |
| 21:00 to 22:00 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 0 | 0 |
| 21:15 to 22:15 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 0 | 0 |
| 21:30to $22: 30$ <br> 1035  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 2 | 2 | 4 | 0 | 0 | 0 |
| 21:45 to 22:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 3 | 0 | 0 | 0 |
| 22:00to $23: 00$ <br> 20  | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 |
| 22:15 to 23:15 | 1 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 |
| 22:30 to 23:30 | 1 | 0 | 1 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 22:45 to 23:45 | 1 | 0 | 1 | ${ }^{3}$ | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 23:00 to 0:00 | 1 | 0 | 1 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 24hr Totals | 57 | 102 | 159 | 63 | 50 | 113 | 0 | 0 | 0 | 0 | 0 | 0 | 59 | ${ }^{41}$ | 100 | 26 | 10 | 36 | 173 | 54 | 227 | 0 | 0 | 0 |





Annexure B
SIDRA results

## MOVEMENT SUMMARY

## $\nabla$ Site: 001A [Brayton Rd/Ambrose Rd Ex AM (Site Folder: Ex)]

Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{gathered} \text { INP } \\ \text { VOLU } \\ \text { [ Total } \\ \text { veh/h } \end{gathered}$ | JT MES HV] veh/h | $\begin{gathered} \text { DEM } \\ \text { FLC } \\ \text { [ Total } \\ \text { veh/h } \end{gathered}$ | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service | $\begin{aligned} & \text { 95\% BA } \\ & \text { QUE } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | CK OF DE Dist ] | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| SouthEast: Brayton Road (SE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 T1 | 8 | 1 | 8 | 12.5 | 0.009 | 0.1 | LOS A | 0.0 | 0.3 | 0.09 | 0.23 | 0.09 | 75.2 |
| 6 R2 | 5 | 1 | 5 | 20.0 | 0.009 | 7.5 | LOS A | 0.0 | 0.3 | 0.09 | 0.23 | 0.09 | 63.3 |
| Approach | 13 | 2 | 14 | 15.4 | 0.009 | 2.9 | NA | 0.0 | 0.3 | 0.09 | 0.23 | 0.09 | 70.1 |
| NorthEast: Ambrose Road (NE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 7 | 0 | 7 | 0.0 | 0.006 | 7.1 | LOS A | 0.0 | 0.2 | 0.10 | 0.59 | 0.10 | 64.9 |
| 9 R2 | 10 | 8 | 11 | 80.0 | 0.018 | 9.1 | LOSA | 0.1 | 0.8 | 0.19 | 0.58 | 0.19 | 45.5 |
| Approach | 17 | 8 | 18 | 47.1 | 0.018 | 8.3 | LOS A | 0.1 | 0.8 | 0.15 | 0.59 | 0.15 | 51.9 |
| NorthWest: Brayton Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 11 | 8 | 12 | 72.7 | 0.021 | 8.3 | LOS A | 0.0 | 0.0 | 0.00 | 0.22 | 0.00 | 51.2 |
| 11 T1 | 20 | 2 | 21 | 10.0 | 0.021 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.22 | 0.00 | 78.3 |
| Approach | 31 | 10 | 33 | 32.3 | 0.021 | 2.9 | NA | 0.0 | 0.0 | 0.00 | 0.22 | 0.00 | 65.9 |
| All <br> Vehicles | 61 | 20 | 64 | 32.8 | 0.021 | 4.4 | NA | 0.1 | 0.8 | 0.06 | 0.33 | 0.06 | 62.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

$\nabla$ Site: 001B [Brayton Rd/Ambrose Rd Ex PM (Site Folder: Ex)]
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | JT MES HV $]$ veh/h | $\begin{aligned} & \text { DEN } \\ & \text { FLC } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{gathered} \text { AND } \\ \text { WS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. Satn <br> v/c | Aver. Delay $\qquad$ | Level of Service | $\begin{gathered} 95 \% \mathrm{~B} \\ \text { QU } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| SouthEast: Brayton Road (SE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 T1 | 27 | 2 | 28 | 7.4 | 0.020 | 0.0 | LOS A | 0.0 | 0.3 | 0.04 | 0.08 | 0.04 | 78.8 |
| 6 R2 | 4 | 2 | 4 | 50.0 | 0.020 | 8.1 | LOS A | 0.0 | 0.3 | 0.04 | 0.08 | 0.04 | 56.8 |
| Approach | 31 | 4 | 33 | 12.9 | 0.020 | 1.1 | NA | 0.0 | 0.3 | 0.04 | 0.08 | 0.04 | 75.0 |
| NorthEast: Ambrose Road (NE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 2 | 0 | 2 | 0.0 | 0.002 | 7.1 | LOS A | 0.0 | 0.0 | 0.10 | 0.59 | 0.10 | 64.9 |
| 9 R2 | 3 | 3 | 3 | 100.0 | 0.006 | 10.0 | LOSA | 0.0 | 0.3 | 0.25 | 0.58 | 0.25 | 49.4 |
| Approach | 5 | 3 | 5 | 60.0 | 0.006 | 8.8 | LOS A | 0.0 | 0.3 | 0.19 | 0.58 | 0.19 | 54.6 |
| NorthWest: Brayton Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 14 | 4 | 15 | 28.6 | 0.022 | 7.5 | LOS A | 0.0 | 0.0 | 0.00 | 0.26 | 0.00 | 61.0 |
| 11 T1 | 21 | 4 | 22 | 19.0 | 0.022 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.26 | 0.00 | 75.7 |
| Approach | 35 | 8 | 37 | 22.9 | 0.022 | 3.0 | NA | 0.0 | 0.0 | 0.00 | 0.26 | 0.00 | 69.0 |
| All <br> Vehicles | 71 | 15 | 75 | 21.1 | 0.022 | 2.6 | NA | 0.0 | 0.3 | 0.03 | 0.20 | 0.03 | 70.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

## $\nabla$ Site: 002A [Hume Hwy/Red Hills Rd Ex AM (Site Folder: Ex)]

Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | UT MES HV ] veh/h |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay $\qquad$ | Level of Service | $\begin{aligned} & \text { 95\% B/ } \\ & \text { QUł } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| NorthWest: Red Hills Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 9 | 5 | 9 | 55.6 | 0.007 | 6.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.50 | 0.00 | 53.0 |
| Approach | 9 | 5 | 9 | 55.6 | 0.007 | 6.8 | NA | 0.0 | 0.0 | 0.00 | 0.50 | 0.00 | 53.0 |
| SouthWest: Hume Highway (SW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 12 | 9 | 13 | 75.0 | 0.010 | 9.8 | LOSA | 0.0 | 0.0 | 0.00 | 0.67 | 0.00 | 53.9 |
| 2 T1 | 618 | 181 | 651 | 29.3 | 0.199 | 0.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 99.9 |
| Approach | 630 | 190 | 663 | 30.2 | 0.199 | 0.2 | NA | 0.0 | 0.0 | 0.00 | 0.01 | 0.00 | 98.3 |
| All <br> Vehicles | 639 | 195 | 673 | 30.5 | 0.199 | 0.3 | NA | 0.0 | 0.0 | 0.00 | 0.02 | 0.00 | 97.1 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Organisation: EMM CONSULTING | Licence: NETWORK / 1PC | Processed: Thursday, 8 July 2021 4:15:00 PM
Project: T:\Jobs\2019\J190263 - Gunlake Quarry SSD MOD2\Technical studiesITransport|SIDRAINEW SSDISIDRA.sip9

## MOVEMENT SUMMARY

$\nabla$ Site: 002B [Hume Hwy/Red Hills Rd Ex PM (Site Folder: Ex)]
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | UT MES HV ] veh/h |  | $\begin{aligned} & \text { 4ND } \\ & \text { WS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay $\qquad$ | Level of Service | $\begin{aligned} & \text { 95\% B/ } \\ & \text { QUł } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| NorthWest: Red Hills Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 15 | 6 | 16 | 40.0 | 0.011 | 6.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.51 | 0.00 | 53.5 |
| Approach | 15 | 6 | 16 | 40.0 | 0.011 | 6.8 | NA | 0.0 | 0.0 | 0.00 | 0.51 | 0.00 | 53.5 |
| SouthWest: Hume Highway (SW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 7 | 3 | 7 | 42.9 | 0.005 | 9.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.66 | 0.00 | 61.1 |
| 2 T1 | 758 | 131 | 798 | 17.3 | 0.228 | 0.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 99.9 |
| Approach | 765 | 134 | 805 | 17.5 | 0.228 | 0.1 | NA | 0.0 | 0.0 | 0.00 | 0.01 | 0.00 | 99.3 |
| All <br> Vehicles | 780 | 140 | 821 | 17.9 | 0.228 | 0.2 | NA | 0.0 | 0.0 | 0.00 | 0.02 | 0.00 | 97.7 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 005A [George St/Brayton Rd Ex AM (Site Folder: Ex)]
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | JT MES HV ] veh/h |  | $\begin{gathered} \text { AND } \\ \text { WS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. Satn <br> v/c | Aver. Delay $\qquad$ | Level of Service | $\begin{aligned} & \text { 95\% Bf } \\ & \text { QUE } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| SouthEast: Brayton Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 L2 | 51 | 6 | 54 | 11.8 | 0.035 | 4.7 | LOS A | 0.1 | 1.1 | 0.03 | 0.51 | 0.03 | 46.4 |
| 22 T1 | 5 | 0 | 5 | 0.0 | 0.006 | 4.2 | LOS A | 0.0 | 0.2 | 0.28 | 0.46 | 0.28 | 46.7 |
| 23 R2 | 1 | 0 | 1 | 0.0 | 0.006 | 5.5 | LOSA | 0.0 | 0.2 | 0.28 | 0.46 | 0.28 | 46.3 |
| Approach | 57 | 6 | 60 | 10.5 | 0.035 | 4.6 | LOS A | 0.1 | 1.1 | 0.06 | 0.51 | 0.06 | 46.4 |
| NorthEast: George Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 4 | 2 | 4 | 50.0 | 0.003 | 5.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.52 | 0.00 | 45.9 |
| 25 T1 | 4 | 0 | 4 | 0.0 | 0.003 | 0.0 | LOSA | 0.0 | 0.0 | 0.05 | 0.11 | 0.05 | 49.2 |
| 26 R2 | 1 | 0 | 1 | 0.0 | 0.003 | 4.7 | LOSA | 0.0 | 0.0 | 0.05 | 0.11 | 0.05 | 48.5 |
| Approach | 9 | 2 | 9 | 22.2 | 0.003 | 2.8 | NA | 0.0 | 0.0 | 0.03 | 0.29 | 0.03 | 47.6 |
| NorthWest: Brayton Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 2 | 0 | 2 | 0.0 | 0.001 | 4.6 | LOS A | 0.0 | 0.0 | 0.04 | 0.51 | 0.04 | 46.5 |
| 28 T1 | 35 | 3 | 37 | 8.6 | 0.106 | 4.3 | LOS A | 0.4 | 3.2 | 0.32 | 0.55 | 0.32 | 46.2 |
| 29 R2 | 54 | 2 | 57 | 3.7 | 0.106 | 6.1 | LOS A | 0.4 | 3.2 | 0.32 | 0.55 | 0.32 | 45.7 |
| Approach | 91 | 5 | 96 | 5.5 | 0.106 | 5.4 | LOS A | 0.4 | 3.2 | 0.32 | 0.55 | 0.32 | 45.9 |
| SouthWest: George Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 L2 | 35 | 5 | 37 | 14.3 | 0.092 | 4.7 | LOSA | 0.4 | 3.2 | 0.05 | 0.49 | 0.05 | 46.4 |
| 31 T1 | 6 | 1 | 6 | 16.7 | 0.092 | 0.0 | LOS A | 0.4 | 3.2 | 0.05 | 0.49 | 0.05 | 47.1 |
| 32 R 2 | 82 | 14 | 86 | 17.1 | 0.092 | 4.8 | LOS A | 0.4 | 3.2 | 0.05 | 0.49 | 0.05 | 46.2 |
| Approach | 123 | 20 | 129 | 16.3 | 0.092 | 4.5 | NA | 0.4 | 3.2 | 0.05 | 0.49 | 0.05 | 46.3 |
| All Vehicles | 280 | 33 | 295 | 11.8 | 0.106 | 4.8 | NA | 0.4 | 3.2 | 0.14 | 0.51 | 0.14 | 46.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

$\nabla$ Site: 005A [George St/Brayton Rd Ex PM (Site Folder: Ex)]
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | JT MES HV ] veh/h |  | $\begin{gathered} \text { AND } \\ \text { WS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. Satn <br> v/c | Aver. Delay $\qquad$ | Level of Service | $\begin{aligned} & \text { 95\% Bf } \\ & \text { QUE } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| SouthEast: Brayton Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 L2 | 42 | 2 | 44 | 4.8 | 0.028 | 4.6 | LOS A | 0.1 | 0.8 | 0.03 | 0.51 | 0.03 | 46.5 |
| 22 T1 | 32 | 3 | 34 | 9.4 | 0.047 | 4.9 | LOS A | 0.2 | 1.6 | 0.36 | 0.52 | 0.36 | 46.5 |
| 23 R2 | 6 | 4 | 6 | 66.7 | 0.047 | 6.9 | LOSA | 0.2 | 1.6 | 0.36 | 0.52 | 0.36 | 45.2 |
| Approach | 80 | 9 | 84 | 11.3 | 0.047 | 4.9 | LOS A | 0.2 | 1.6 | 0.19 | 0.52 | 0.19 | 46.4 |
| NorthEast: George Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 8 | 2 | 8 | 25.0 | 0.005 | 4.8 | LOSA | 0.0 | 0.0 | 0.00 | 0.52 | 0.00 | 46.3 |
| 25 T1 | 5 | 0 | 5 | 0.0 | 0.003 | 0.1 | LOSA | 0.0 | 0.0 | 0.08 | 0.09 | 0.08 | 49.3 |
| 26 R2 | 1 | 0 | 1 | 0.0 | 0.003 | 4.8 | LOSA | 0.0 | 0.0 | 0.08 | 0.09 | 0.08 | 48.6 |
| Approach | 14 | 2 | 15 | 14.3 | 0.005 | 3.1 | NA | 0.0 | 0.0 | 0.03 | 0.34 | 0.03 | 47.5 |
| NorthWest: Brayton Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 1 | 0 | 1 | 0.0 | 0.001 | 4.6 | LOS A | 0.0 | 0.0 | 0.04 | 0.51 | 0.04 | 46.5 |
| 28 T1 | 19 | 2 | 20 | 10.5 | 0.054 | 4.6 | LOS A | 0.2 | 1.6 | 0.36 | 0.55 | 0.36 | 46.1 |
| 29 R2 | 24 | 1 | 25 | 4.2 | 0.054 | 6.5 | LOS A | 0.2 | 1.6 | 0.36 | 0.55 | 0.36 | 45.5 |
| Approach | 44 | 3 | 46 | 6.8 | 0.054 | 5.6 | LOS A | 0.2 | 1.6 | 0.35 | 0.55 | 0.35 | 45.8 |
| SouthWest: George Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 L2 | 92 | 4 | 97 | 4.3 | 0.128 | 4.6 | LOSA | 0.5 | 4.0 | 0.06 | 0.49 | 0.06 | 46.5 |
| 31 T1 | 8 | 0 | 8 | 0.0 | 0.128 | 0.1 | LOS A | 0.5 | 4.0 | 0.06 | 0.49 | 0.06 | 47.0 |
| 32 R 2 | 90 | 6 | 95 | 6.7 | 0.128 | 4.7 | LOS A | 0.5 | 4.0 | 0.06 | 0.49 | 0.06 | 46.3 |
| Approach | 190 | 10 | 200 | 5.3 | 0.128 | 4.5 | NA | 0.5 | 4.0 | 0.06 | 0.49 | 0.06 | 46.4 |
| All <br> Vehicles | 328 | 24 | 345 | 7.3 | 0.128 | 4.7 | NA | 0.5 | 4.0 | 0.13 | 0.50 | 0.13 | 46.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

B Site: 003A [Hume Hwy Off Ramp/Jerrara Rd/Marulan S Rd Ex AM (Site Folder: Ex)]

마 Network: N101 [Ex AM (Network Folder: General)]

Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | ND VS <br> HV ] \% | ARR FLO [ Tota veh/h | VAL WS HV ] \% | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% <br> [ Veh. veh | $\begin{gathered} \text { K OF } \\ \text { JE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | EffectiveA Stop Rate | ver. No. Cycles | Aver. Speed km/h |
| SouthEast: Marulan South Road (SE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 13 | 8.3 | 13 | 8.3 | 0.016 | 4.3 | LOS A | 0.1 | 0.6 | 0.22 | 0.44 | 0.22 | 54.4 |
| $5 \quad$ T1 | 7 | 0.0 | 7 | 0.0 | 0.016 | 4.3 | LOS A | 0.1 | 0.6 | 0.22 | 0.44 | 0.22 | 51.8 |
| Approach | 20 | 5.3 | 20 | 5.3 | 0.016 | 4.3 | LOS A | 0.1 | 0.6 | 0.22 | 0.44 | 0.22 | 53.8 |
| NorthEast: Hume Highway Off Ramp (NE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 62 | 3.4 | 62 | 3.4 | 0.100 | 4.1 | LOS A | 0.5 | 4.5 | 0.18 | 0.49 | 0.18 | 54.0 |
| 8 T1 | 23 | 63.6 | 23 | 63.6 | 0.100 | 4.9 | LOS A | 0.5 | 4.5 | 0.18 | 0.49 | 0.18 | 53.8 |
| 9 R2 | 29 | 89.3 | 29 | 89.3 | 0.100 | 10.1 | LOS A | 0.5 | 4.5 | 0.18 | 0.49 | 0.18 | 49.8 |
| Approach | 115 | 37.6 | 115 | 37.6 | 0.100 | 5.8 | LOS A | 0.5 | 4.5 | 0.18 | 0.49 | 0.18 | 53.3 |
| NorthWest: Jerrara Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 38 | 2.8 | 38 | 2.8 | 0.030 | 3.4 | LOS A | 0.1 | 1.0 | 0.03 | 0.45 | 0.03 | 54.5 |
| 12 R 2 | 7 | 28.6 | 7 | 28.6 | 0.030 | 8.0 | LOS A | 0.1 | 1.0 | 0.03 | 0.45 | 0.03 | 52.6 |
| Approach | 45 | 7.0 | 45 | 7.0 | 0.030 | 4.2 | LOS A | 0.1 | 1.0 | 0.03 | 0.45 | 0.03 | 54.2 |
| SouthWest: Jerrara Road (SW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 22 | 14.3 | 22 | 14.3 | 0.020 | 4.2 | LOS A | 0.1 | 0.8 | 0.17 | 0.48 | 0.17 | 52.0 |
| 3 R2 | 2 | 50.0 | 2 | 50.0 | 0.020 | 9.5 | LOS A | 0.1 | 0.8 | 0.17 | 0.48 | 0.17 | 53.9 |
| Approach | 24 | 17.4 | 24 | 17.4 | 0.020 | 4.7 | LOS A | 0.1 | 0.8 | 0.17 | 0.48 | 0.17 | 52.3 |
| All Vehicles | 204 | 25.3 | 204 | 25.3 | 0.100 | 5.2 | LOS A | 0.5 | 4.5 | 0.15 | 0.47 | 0.15 | 53.5 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 004A [Hume Hwy On Ramp/Hume Hwy Off Ramp/Jerrara
Network: N101 [Ex AM Road Ex AM (Site Folder: Ex)] (Network Folder: General)]

Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|l\|l} \hline \text { Mov Turn } \\ \text { ID } \end{array}$ |  | $\begin{aligned} & \text { AND } \\ & \text { WS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | ARF FLO [ Tota veh/h | IVAL WS HV] \% | Deg. Satn v/c | Aver. Delay sec | Level of Service | $95 \%$ [ Veh. veh | $\begin{gathered} \text { K OF } \\ \text { JE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | EffectiveA Stop Rate | ver. No. Cycles | Aver. Speed km/h |
| SouthEast: Jerrara Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 T1 | 19 | 88.9 | 19 | 88.9 | 0.044 | 0.1 | LOS A | 0.2 | 1.8 | 0.09 | 0.39 | 0.09 | 52.6 |
| 6 R2 | 36 | 35.3 | 36 | 35.3 | 0.044 | 5.2 | LOSA | 0.2 | 1.8 | 0.09 | 0.39 | 0.09 | 47.0 |
| Approach | 55 | 53.8 | 55 | 53.8 | 0.044 | 3.4 | NA | 0.2 | 1.8 | 0.09 | 0.39 | 0.09 | 48.8 |
| NorthWest: Jerrara Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 13 | 100.0 | 13 | $100 .$ | 0.013 | 6.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.48 | 0.00 | 49.2 |
| 11 T1 | 2 | 50.0 | 2 | 50.0 | 0.013 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.48 | 0.00 | 50.0 |
| Approach | 15 | 92.9 | 15 | 92.9 | 0.013 | 5.7 | NA | 0.0 | 0.0 | 0.00 | 0.48 | 0.00 | 49.3 |
| SouthWest: Hume Highway Off Ramp (SW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 2 | 50.0 | 2 | 50.0 | 0.047 | 6.3 | LOS A | 0.2 | 1.4 | 0.20 | 0.59 | 0.20 | 50.9 |
| 2 T1 | 1 | 0.0 | 1 | 0.0 | 0.047 | 4.8 | LOS A | 0.2 | 1.4 | 0.20 | 0.59 | 0.20 | 53.1 |
| 3 R2 | 34 | 9.4 | 34 | 9.4 | 0.047 | 6.5 | LOSA | 0.2 | 1.4 | 0.20 | 0.59 | 0.20 | 49.7 |
| Approach | 37 | 11.4 | 37 | 11.4 | 0.047 | 6.5 | LOS A | 0.2 | 1.4 | 0.20 | 0.59 | 0.20 | 50.0 |
| All Vehicles | 106 | 44.6 | 106 | 44.6 | 0.047 | 4.8 | NA | 0.2 | 1.8 | 0.11 | 0.47 | 0.11 | 49.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

© Site: 003B [Hume Hwy Off Ramp/Jerrara Rd/Marulan S Rd Ex
Network: N101 [Ex PM
PM (Site Folder: Ex)]

Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | ND NS HV ] \% | ARR FLO [ Tota veh/h | $\begin{aligned} & \text { IVAL } \\ & \text { WS } \\ & 1 \mathrm{HV} \text { ] } \\ & \hline \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% Q <br> [ Veh. veh | $\begin{gathered} \text { K OF } \\ \text { JE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | ver. No. Cycles | Aver. Speed <br> km/h |
| SouthEast: Marulan South Road (SE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 34 | 21.9 | 34 | 21.9 | 0.055 | 4.7 | LOS A | 0.3 | 2.1 | 0.26 | 0.45 | 0.26 | 53.8 |
| $5 \quad \mathrm{~T} 1$ | 29 | 7.1 | 29 | 7.1 | 0.055 | 4.6 | LOS A | 0.3 | 2.1 | 0.26 | 0.45 | 0.26 | 51.5 |
| Approach | 63 | 15.0 | 63 | 15.0 | 0.055 | 4.6 | LOS A | 0.3 | 2.1 | 0.26 | 0.45 | 0.26 | 53.0 |
| NorthEast: Hume Highway Off Ramp (NE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 5 | 20.0 | 5 | 20.0 | 0.054 | 4.3 | LOS A | 0.2 | 2.4 | 0.17 | 0.46 | 0.17 | 53.2 |
| 8 T1 | 37 | 22.9 | 37 | 22.9 | 0.054 | 4.4 | LOS A | 0.2 | 2.4 | 0.17 | 0.46 | 0.17 | 54.7 |
| 9 R2 | 17 | 87.5 | 17 | 87.5 | 0.054 | 10.1 | LOSA | 0.2 | 2.4 | 0.17 | 0.46 | 0.17 | 49.5 |
| Approach | 59 | 41.1 | 59 | 41.1 | 0.054 | 6.0 | LOS A | 0.2 | 2.4 | 0.17 | 0.46 | 0.17 | 53.6 |
| NorthWest: Jerrara Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 4 | 50.0 | 4 | 50.0 | 0.029 | 3.4 | LOS A | 0.1 | 1.4 | 0.02 | 0.61 | 0.02 | 48.9 |
| 12 R 2 | 34 | 53.1 | 34 | 53.1 | 0.029 | 8.0 | LOS A | 0.1 | 1.4 | 0.02 | 0.61 | 0.02 | 47.5 |
| Approach | 38 | 52.8 | 38 | 52.8 | 0.029 | 7.5 | LOS A | 0.1 | 1.4 | 0.02 | 0.61 | 0.02 | 47.6 |
| SouthWest: Jerrara Road (SW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 26 | 24.0 | 26 | 24.0 | 0.024 | 4.4 | LOS A | 0.1 | 0.9 | 0.18 | 0.47 | 0.18 | 51.9 |
| 3 R2 | 1 | 0.0 | 1 | 0.0 | 0.024 | 8.9 | LOS A | 0.1 | 0.9 | 0.18 | 0.47 | 0.18 | 56.0 |
| Approach | 27 | 23.1 | 27 | 23.1 | 0.024 | 4.6 | LOS A | 0.1 | 0.9 | 0.18 | 0.47 | 0.18 | 52.2 |
| All Vehicles | 187 | 32.0 | 187 | 32.0 | 0.055 | 5.6 | LOS A | 0.3 | 2.4 | 0.17 | 0.49 | 0.17 | 52.1 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Project: T:\Jobs\2019\J190263 - Gunlake Quarry SSD MOD2\Technical studies\TransportISIDRAINEW SSDISIDRA.sip9

## MOVEMENT SUMMARY

$\nabla$ Site: 004B [Hume Hwy On Ramp/Hume Hwy Off Ramp/Jerrara Road Ex PM (Site Folder: Ex)]

마 Network: N101 [Ex PM (Network Folder: General)]

Site Category: (None)
Give-Way (Two-Way)


Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

$\nabla$ Site: 001C [Brayton Rd/Ambrose Rd Dev AM (Site Folder:
Dev)]

Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | UT <br> MES HV ] veh/h |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. <br> Satn <br> v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate |  | Aver Speed km/h |
| SouthEast: Brayton Road (SE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 T1 | 10 | 1 | 11 | 10.0 | 0.017 | 0.5 | LOS A | 0.1 | 0.6 | 0.21 | 0.28 | 0.21 | 74.4 |
| 6 R2 | 10 | 5 | 11 | 50.0 | 0.017 | 8.4 | LOSA | 0.1 | 0.6 | 0.21 | 0.28 | 0.21 | 54.5 |
| Approach | 20 | 6 | 21 | 30.0 | 0.017 | 4.5 | NA | 0.1 | 0.6 | 0.21 | 0.28 | 0.21 | 62.9 |
| NorthEast: Ambrose Road (NE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 10 | 1 | 11 | 10.0 | 0.010 | 7.4 | LOS A | 0.0 | 0.3 | 0.16 | 0.58 | 0.16 | 61.4 |
| 9 R2 | 50 | 47 | 53 | 94.0 | 0.104 | 10.6 | LOSA | 0.4 | 5.3 | 0.31 | 0.62 | 0.31 | 42.7 |
| Approach | 60 | 48 | 63 | 80.0 | 0.104 | 10.0 | LOS A | 0.4 | 5.3 | 0.29 | 0.61 | 0.29 | 45.0 |
| NorthWest: Brayton Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 52 | 48 | 55 | 92.3 | 0.062 | 8.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.43 | 0.00 | 47.3 |
| 11 T1 | 24 | 1 | 25 | 4.2 | 0.062 | 0.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.43 | 0.00 | 78.2 |
| Approach | 76 | 49 | 80 | 64.5 | 0.062 | 5.9 | NA | 0.0 | 0.0 | 0.00 | 0.43 | 0.00 | 54.1 |
| All Vehicles | 156 | 103 | 164 | 66.0 | 0.104 | 7.3 | NA | 0.4 | 5.3 | 0.14 | 0.48 | 0.14 | 51.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

$\nabla$ Site: 001D [Brayton Rd/Ambrose Rd Dev PM (Site Folder:
Dev)]

Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  |  |  | $\begin{aligned} & \text { AND } \\ & \text { WS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% <br> [ Veh. veh | CK OF UE Dist ] | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| SouthEast: Brayton Road (SE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 T1 | 36 | 3 | 38 | 8.3 | 0.029 | 0.2 | LOS A | 0.1 | 0.6 | 0.10 | 0.10 | 0.10 | 78.2 |
| 6 R2 | 7 | 4 | 7 | 57.1 | 0.029 | 8.7 | LOSA | 0.1 | 0.6 | 0.10 | 0.10 | 0.10 | 54.7 |
| Approach | 43 | 7 | 45 | 16.3 | 0.029 | 1.6 | NA | 0.1 | 0.6 | 0.10 | 0.10 | 0.10 | 73.0 |
| NorthEast: Ambrose Road (NE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 7 | 4 | 7 | 57.1 | 0.009 | 8.5 | LOS A | 0.0 | 0.3 | 0.19 | 0.58 | 0.19 | 49.7 |
| 9 R2 | 46 | 46 | 48 | 100.0 | 0.105 | 11.5 | LOS A | 0.4 | 5.4 | 0.37 | 0.65 | 0.37 | 48.4 |
| Approach | 53 | 50 | 56 | 94.3 | 0.105 | 11.1 | LOS A | 0.4 | 5.4 | 0.34 | 0.64 | 0.34 | 48.5 |
| NorthWest: Brayton Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 58 | 45 | 61 | 77.6 | 0.066 | 8.4 | LOS A | 0.0 | 0.0 | 0.00 | 0.44 | 0.00 | 49.1 |
| 11 T1 | 26 | 4 | 27 | 15.4 | 0.066 | 0.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.44 | 0.00 | 75.7 |
| Approach | 84 | 49 | 88 | 58.3 | 0.066 | 5.8 | NA | 0.0 | 0.0 | 0.00 | 0.44 | 0.00 | 55.1 |
| All <br> Vehicles | 180 | 106 | 189 | 58.9 | 0.105 | 6.4 | NA | 0.4 | 5.4 | 0.13 | 0.41 | 0.13 | 56.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

$\nabla$ Site: 002C [Hume Hwy/Red Hills Rd Dev AM (Site Folder:
Dev)]

Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | JT MES HV ] veh/h |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate |  | Aver. Speed <br> km/h |
| NorthWest: Red Hills Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 57 | 52 | 60 | 91.2 | 0.053 | 7.4 | LOS A | 0.0 | 0.0 | 0.00 | 0.48 | 0.00 | 51.8 |
| Approach | 57 | 52 | 60 | 91.2 | 0.053 | 7.4 | NA | 0.0 | 0.0 | 0.00 | 0.48 | 0.00 | 51.8 |
| SouthWest: Hume Highway (SW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| L2 | 59 | 56 | 62 | 94.9 | 0.056 | 10.3 | LOS A | 0.0 | 0.0 | 0.00 | 0.67 | 0.00 | 50.2 |
| 2 T1 | 720 | 217 | 758 | 30.1 | 0.232 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 99.9 |
| Approach | 779 | 273 | 820 | 35.0 | 0.232 | 0.8 | NA | 0.0 | 0.0 | 0.00 | 0.05 | 0.00 | 92.9 |
| All Vehicles | 836 | 325 | 880 | 38.9 | 0.232 | 1.3 | NA | 0.0 | 0.0 | 0.00 | 0.08 | 0.00 | 88.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

$\nabla$ Site: 002D [Hume Hwy/Red Hills Rd Dev PM (Site Folder:
Dev)]
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | Tis <br> HV ] veh/h |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay sec | Level of Service | $\begin{gathered} 95 \% \text { B } \\ \text { QU } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | OF JE Dist $]$ m | $\begin{aligned} & \text { Prop. } \\ & \text { Out } \end{aligned}$ | Effective Stop Rate | Aver No. Cycles | Aver. Speed <br> km/h |
| NorthWest: Red Hills Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 65 | 53 | 68 | 81.5 | 0.058 | 7.5 | LOSA | 0.0 | 0.0 | 0.00 | 0.49 | 0.00 | 52.1 |
| Approach | 65 | 53 | 68 | 81.5 | 0.058 | 7.5 | NA | 0.0 | 0.0 | 0.00 | 0.49 | 0.00 | 52.1 |
| SouthWest: Hume Highway (SW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| L2 | 54 | 49 | 57 | 90.7 | 0.050 | 10.2 | LOSA | 0.0 | 0.0 | 0.00 | 0.67 | 0.00 | 50.9 |
| 2 T1 | 895 | 174 | 942 | 19.4 | 0.272 | 0.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 99.8 |
| Approach | 949 | 223 | 999 | 23.5 | 0.272 | 0.6 | NA | 0.0 | 0.0 | 0.00 | 0.04 | 0.00 | 94.6 |
| All Vehicles | 1014 | 276 | 1067 | 27.2 | 0.272 | 1.1 | NA | 0.0 | 0.0 | 0.00 | 0.07 | 0.00 | 89.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

$\nabla$ Site: 005A [George St/Brayton Rd Dev AM (Site Folder: Dev)]
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INF } \\ & \text { VOLL } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | UT MES HV ] veh/h |  | AND NS HV ] \% | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% <br> [ Veh <br> veh | CK OF UE Dist $]$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| SouthEast: Brayton Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 L2 | 67 | 8 | 71 | 11.9 | 0.046 | 4.7 | LOSA | 0.2 | 1.4 | 0.03 | 0.51 | 0.03 | 46.4 |
| 22 T1 | 8 | 1 | 8 | 12.5 | 0.011 | 4.8 | LOSA | 0.0 | 0.3 | 0.36 | 0.48 | 0.36 | 46.4 |
| 23 R2 | 1 | 0 | 1 | 0.0 | 0.011 | 6.0 | LOS A | 0.0 | 0.3 | 0.36 | 0.48 | 0.36 | 46.2 |
| Approach | 76 | 9 | 80 | 11.8 | 0.046 | 4.7 | LOS A | 0.2 | 1.4 | 0.07 | 0.51 | 0.07 | 46.4 |
| NorthEast: George Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 6 | 3 | 6 | 50.0 | 0.005 | 5.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.52 | 0.00 | 45.9 |
| 25 T1 | 5 | 0 | 5 | 0.0 | 0.003 | 0.0 | LOSA | 0.0 | 0.0 | 0.06 | 0.09 | 0.06 | 49.3 |
| 26 R2 | 1 | 0 | 1 | 0.0 | 0.003 | 4.8 | LOSA | 0.0 | 0.0 | 0.06 | 0.09 | 0.06 | 48.6 |
| Approach | 12 | 3 | 13 | 25.0 | 0.005 | 2.9 | NA | 0.0 | 0.0 | 0.03 | 0.30 | 0.03 | 47.5 |
| NorthWest: Brayton Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 3 | 0 | 3 | 0.0 | 0.002 | 4.6 | LOS A | 0.0 | 0.1 | 0.04 | 0.51 | 0.04 | 46.5 |
| 28 T1 | 59 | 17 | 62 | 28.8 | 0.230 | 5.3 | LOS A | 1.0 | 9.0 | 0.44 | 0.63 | 0.44 | 45.3 |
| 29 R2 | 95 | 27 | 100 | 28.4 | 0.230 | 7.8 | LOSA | 1.0 | 9.0 | 0.44 | 0.63 | 0.44 | 44.6 |
| Approach | 157 | 44 | 165 | 28.0 | 0.230 | 6.8 | LOS A | 1.0 | 9.0 | 0.43 | 0.63 | 0.43 | 44.9 |
| SouthWest: George Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 L2 | 55 | 16 | 58 | 29.1 | 0.126 | 4.9 | LOS A | 0.6 | 4.7 | 0.07 | 0.49 | 0.07 | 46.2 |
| 31 T1 | 8 | 1 | 8 | 12.5 | 0.126 | 0.1 | LOS A | 0.6 | 4.7 | 0.07 | 0.49 | 0.07 | 47.0 |
| 32 R 2 | 106 | 18 | 112 | 17.0 | 0.126 | 4.8 | LOS A | 0.6 | 4.7 | 0.07 | 0.49 | 0.07 | 46.2 |
| Approach | 169 | 35 | 178 | 20.7 | 0.126 | 4.6 | NA | 0.6 | 4.7 | 0.07 | 0.49 | 0.07 | 46.2 |
| All <br> Vehicles | 414 | 91 | 436 | 22.0 | 0.230 | 5.4 | NA | 1.0 | 9.0 | 0.21 | 0.54 | 0.21 | 45.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

$\nabla$ Site: 005A [George St/Brayton Rd Dev PM (Site Folder: Dev)]
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INP } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | UT MES HV ] veh/h | $\begin{gathered} \text { DEM } \\ \text { FLC } \\ \text { [ Total } \\ \text { veh/h } \end{gathered}$ | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service | $\begin{gathered} 95 \% \text { B } \\ \text { QL } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | CK OF DE Dist ] | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| SouthEast: Brayton Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 L2 | 55 | 3 | 58 | 5.5 | 0.037 | 4.6 | LOSA | 0.1 | 1.1 | 0.04 | 0.51 | 0.04 | 46.5 |
| 22 T1 | 50 | 12 | 53 | 24.0 | 0.089 | 6.4 | LOS A | 0.4 | 3.2 | 0.46 | 0.61 | 0.46 | 45.6 |
| 23 R2 | 8 | 5 | 8 | 62.5 | 0.089 | 7.6 | LOSA | 0.4 | 3.2 | 0.46 | 0.61 | 0.46 | 44.5 |
| Approach | 113 | 20 | 119 | 17.7 | 0.089 | 5.6 | LOS A | 0.4 | 3.2 | 0.26 | 0.56 | 0.26 | 45.9 |
| NorthEast: George Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 11 | 3 | 12 | 27.3 | 0.007 | 4.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.52 | 0.00 | 46.2 |
| 25 T1 | 7 | 0 | 7 | 0.0 | 0.004 | 0.1 | LOS A | 0.0 | 0.0 | 0.08 | 0.07 | 0.08 | 49.4 |
| 26 R2 | 1 | 0 | 1 | 0.0 | 0.004 | 5.1 | LOS A | 0.0 | 0.0 | 0.08 | 0.07 | 0.08 | 48.7 |
| Approach | 19 | 3 | 20 | 15.8 | 0.007 | 3.1 | NA | 0.0 | 0.0 | 0.03 | 0.33 | 0.03 | 47.5 |
| NorthWest: Brayton Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 1 | 0 | 1 | 0.0 | 0.001 | 4.6 | LOS A | 0.0 | 0.0 | 0.05 | 0.51 | 0.05 | 46.5 |
| 28 T1 | 29 | 7 | 31 | 24.1 | 0.111 | 5.6 | LOS A | 0.4 | 3.8 | 0.47 | 0.64 | 0.47 | 45.1 |
| 29 R2 | 39 | 9 | 41 | 23.1 | 0.111 | 8.5 | LOSA | 0.4 | 3.8 | 0.47 | 0.64 | 0.47 | 44.4 |
| Approach | 69 | 16 | 73 | 23.2 | 0.111 | 7.2 | LOS A | 0.4 | 3.8 | 0.46 | 0.64 | 0.46 | 44.7 |
| SouthWest: George Street |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 L2 | 145 | 31 | 153 | 21.4 | 0.187 | 4.8 | LOS A | 0.8 | 6.1 | 0.07 | 0.48 | 0.07 | 46.3 |
| 31 T1 | 10 | 0 | 11 | 0.0 | 0.187 | 0.1 | LOS A | 0.8 | 6.1 | 0.07 | 0.48 | 0.07 | 47.0 |
| 32 R2 | 117 | 8 | 123 | 6.8 | 0.187 | 4.7 | LOSA | 0.8 | 6.1 | 0.07 | 0.48 | 0.07 | 46.3 |
| Approach | 272 | 39 | 286 | 14.3 | 0.187 | 4.6 | NA | 0.8 | 6.1 | 0.07 | 0.48 | 0.07 | 46.3 |
| All <br> Vehicles | 473 | 78 | 498 | 16.5 | 0.187 | 5.2 | NA | 0.8 | 6.1 | 0.17 | 0.52 | 0.17 | 46.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

$\nabla$ Site: 003C [Hume Hwy Off Ramp/Jerrara Rd/Marulan S Rd
미 Network: N101 [Dev AM
Dev AM (Site Folder: Dev)]

Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | ND WS HV] \% | ARR FLO [ Tota veh/h | IVAL WS [HV ] \% | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% <br> [ Veh. veh | $\begin{gathered} \text { K OF } \\ \text { JE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | EffectiveAv Stop Rate | ver. No. Cycles | Aver. Speed km/h |
| SouthEast: Marulan South Road (SE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 19 | 22.2 | 19 | 22.2 | 0.035 | 4.9 | LOS A | 0.2 | 1.5 | 0.32 | 0.47 | 0.32 | 53.6 |
| $5 \quad$ T1 | 17 | 43.8 | 17 | 43.8 | 0.035 | 5.3 | LOS A | 0.2 | 1.5 | 0.32 | 0.47 | 0.32 | 51.1 |
| Approach | 36 | 32.4 | 36 | 32.4 | 0.035 | 5.1 | LOS A | 0.2 | 1.5 | 0.32 | 0.47 | 0.32 | 52.8 |
| NorthEast: Hume Highway Off Ramp (NE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 77 | 9.6 | 77 | 9.6 | 0.164 | 4.3 | LOS A | 0.8 | 8.5 | 0.24 | 0.51 | 0.24 | 53.6 |
| 8 T1 | 26 | 64.0 | 26 | 64.0 | 0.164 | 5.1 | LOS A | 0.8 | 8.5 | 0.24 | 0.51 | 0.24 | 53.6 |
| 9 R2 | 71 | 95.5 | 71 | 95.5 | 0.164 | 10.4 | LOS A | 0.8 | 8.5 | 0.24 | 0.51 | 0.24 | 49.4 |
| Approach | 174 | 52.7 | 174 | 52.7 | 0.164 | 6.9 | LOS A | 0.8 | 8.5 | 0.24 | 0.51 | 0.24 | 52.6 |
| NorthWest: Jerrara Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 53 | 8.0 | 53 | 8.0 | 0.041 | 3.4 | LOS A | 0.2 | 1.6 | 0.03 | 0.45 | 0.03 | 54.3 |
| 12 R 2 | 11 | 30.0 | 11 | 30.0 | 0.041 | 8.0 | LOS A | 0.2 | 1.6 | 0.03 | 0.45 | 0.03 | 52.5 |
| Approach | 63 | 11.7 | 63 | 11.7 | 0.041 | 4.2 | LOS A | 0.2 | 1.6 | 0.03 | 0.45 | 0.03 | 54.0 |
| SouthWest: Jerrara Road (SW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 29 | 17.9 | 29 | 17.9 | 0.029 | 4.7 | LOS A | 0.1 | 1.1 | 0.28 | 0.49 | 0.28 | 51.4 |
| 3 R2 | 2 | 50.0 | 2 | 50.0 | 0.029 | 10.0 | LOSA | 0.1 | 1.1 | 0.28 | 0.49 | 0.28 | 53.6 |
| Approach | 32 | 20.0 | 32 | 20.0 | 0.029 | 5.0 | LOS A | 0.1 | 1.1 | 0.28 | 0.49 | 0.28 | 51.6 |
| All Vehicles | 304 | 38.4 | 304 | 38.4 | 0.164 | 5.9 | LOS A | 0.8 | 8.5 | 0.21 | 0.49 | 0.21 | 52.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 004C [Hume Hwy On Ramp/Hume Hwy Off Ramp/Jerrara
마 Network: N101 [Dev AM (Network Folder: General)]

Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | AND NS HV] \% | ARR FLO <br> [ Tota veh/h | IVAL WS HV ] \% | Deg. Satn v/c | Aver. Delay sec | Level of Service | $\begin{gathered} 95 \% \text { E } \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | EffectiveA <br> Stop <br> Rate | ver. No. Cycles | Aver. Speed km/h |
| SouthEast: Jerrara Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $5 \quad$ T1 | 25 | 87.5 | 25 | 87.5 | 0.108 | 0.2 | LOS A | 0.5 | 5.4 | 0.13 | 0.45 | 0.13 | 52.5 |
| 6 R2 | 92 | 66.7 | 92 | 66.7 | 0.108 | 5.2 | LOS A | 0.5 | 5.4 | 0.13 | 0.45 | 0.13 | 45.0 |
| Approach | 117 | 71.2 | 117 | 71.2 | 0.108 | 4.1 | NA | 0.5 | 5.4 | 0.13 | 0.45 | 0.13 | 46.4 |
| NorthWest: Jerrara Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 19 | 100.0 |  | $\begin{gathered} 100 . \\ 0 \end{gathered}$ | 0.020 | 6.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.48 | 0.00 | 49.1 |
| 11 T1 | 3 | 66.7 | 3 | 66.7 | 0.020 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.48 | 0.00 | 49.8 |
| Approach | 22 | 95.2 | 22 | 95.2 | 0.020 | 5.7 | NA | 0.0 | 0.0 | 0.00 | 0.48 | 0.00 | 49.1 |
| SouthWest: Hume Highway Off Ramp (SW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 3 | 66.7 | 3 | 66.7 | 0.064 | 6.6 | LOS A | 0.2 | 1.9 | 0.30 | 0.63 | 0.30 | 49.6 |
| 2 T1 | 1 | 0.0 | 1 | 0.0 | 0.064 | 5.8 | LOS A | 0.2 | 1.9 | 0.30 | 0.63 | 0.30 | 52.4 |
| 3 R2 | 39 | 10.8 | 39 | 10.8 | 0.064 | 7.6 | LOS A | 0.2 | 1.9 | 0.30 | 0.63 | 0.30 | 48.4 |
| Approach | 43 | 14.6 | 43 | 14.6 | 0.064 | 7.5 | LOS A | 0.2 | 1.9 | 0.30 | 0.63 | 0.30 | 48.7 |
| All Vehicles | 182 | 60.7 | 182 | 60.7 | 0.108 | 5.1 | NA | 0.5 | 5.4 | 0.15 | 0.50 | 0.15 | 47.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 003D [Hume Hwy Off Ramp/Jerrara Rd/Marulan S Rd
$\square$ Network: N101 [Dev PM
Dev PM (Site Folder: Dev)] (Network Folder: General)]

Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | ND WS HV] \% | ARR FLO [ Tota veh/h | IVAL WS HV ] \% | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% <br> [ Veh. veh | $\begin{gathered} \text { K OF } \\ \text { JE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | EffectiveA Stop Rate | ver. No. Cycles | Aver. Speed km/h |
| SouthEast: Marulan South Road (SE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 43 | 19.5 | 43 | 19.5 | 0.085 | 5.2 | LOS A | 0.4 | 3.4 | 0.38 | 0.50 | 0.38 | 53.4 |
| $5 \quad$ T1 | 44 | 19.0 | 44 | 19.0 | 0.085 | 5.3 | LOS A | 0.4 | 3.4 | 0.38 | 0.50 | 0.38 | 50.7 |
| Approach | 87 | 19.3 | 87 | 19.3 | 0.085 | 5.2 | LOS A | 0.4 | 3.4 | 0.38 | 0.50 | 0.38 | 52.4 |
| NorthEast: Hume Highway Off Ramp (NE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 13 | 58.3 | 13 | 58.3 | 0.124 | 4.9 | LOS A | 0.6 | 6.7 | 0.23 | 0.52 | 0.23 | 51.6 |
| 8 T1 | 42 | 22.5 | 42 | 22.5 | 0.124 | 4.5 | LOS A | 0.6 | 6.7 | 0.23 | 0.52 | 0.23 | 54.4 |
| 9 R2 | 67 | 96.9 | 67 | 96.9 | 0.124 | 10.4 | LOS A | 0.6 | 6.7 | 0.23 | 0.52 | 0.23 | 49.0 |
| Approach | 122 | 67.2 | 122 | 67.2 | 0.124 | 7.8 | LOS A | 0.6 | 6.7 | 0.23 | 0.52 | 0.23 | 52.0 |
| NorthWest: Jerrara Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 8 | 62.5 | 8 | 62.5 | 0.040 | 3.4 | LOS A | 0.2 | 2.0 | 0.02 | 0.60 | 0.02 | 48.5 |
| 12 R 2 | 44 | 52.4 | 44 | 52.4 | 0.040 | 8.0 | LOS A | 0.2 | 2.0 | 0.02 | 0.60 | 0.02 | 47.6 |
| Approach | 53 | 54.0 | 53 | 54.0 | 0.040 | 7.3 | LOS A | 0.2 | 2.0 | 0.02 | 0.60 | 0.02 | 47.7 |
| SouthWest: Jerrara Road (SW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 36 | 26.5 | 36 | 26.5 | 0.035 | 4.9 | LOS A | 0.2 | 1.4 | 0.31 | 0.50 | 0.31 | 51.2 |
| 3 R2 | 1 | 0.0 | 1 | 0.0 | 0.035 | 9.3 | LOS A | 0.2 | 1.4 | 0.31 | 0.50 | 0.31 | 55.6 |
| Approach | 37 | 25.7 | 37 | 25.7 | 0.035 | 5.1 | LOS A | 0.2 | 1.4 | 0.31 | 0.50 | 0.31 | 51.5 |
| All Vehicles | 299 | 45.8 | 299 | 45.8 | 0.124 | 6.6 | LOS A | 0.6 | 6.7 | 0.25 | 0.53 | 0.25 | 51.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 004D [Hume Hwy On Ramp/Hume Hwy Off Ramp/Jerrara
마 Network: N101 [Dev PM (Network Folder: General)]

Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{gathered} \text { DEM } \\ \text { FLO } \\ \text { [ Total } \\ \text { veh/h } \end{gathered}$ | $\begin{aligned} & \text { AND } \\ & \text { WS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | ARR <br> FLO [ Tota veh/h | IVAL WS HV ] \% | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service | $\begin{gathered} 95 \% \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | $\begin{aligned} & \text { CK OF } \\ & \text { UE } \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. Que | EffectiveA Stop Rate | ver. No. Cycles | Aver. Speed km/h |
| SouthEast: Jerrara Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $5 \quad \mathrm{~T} 1$ | 18 | 100.0 | 18 | $\begin{gathered} 100 . \\ 0 \end{gathered}$ | 0.135 | 0.5 | LOS A | 0.6 | 6.2 | 0.21 | 0.50 | 0.21 | 52.9 |
| 6 R2 | 128 | 50.0 | 128 | 50.0 | 0.135 | 5.5 | LOS A | 0.6 | 6.2 | 0.21 | 0.50 | 0.21 | 46.3 |
| Approach | 146 | 56.1 | 146 | 56.1 | 0.135 | 4.9 | NA | 0.6 | 6.2 | 0.21 | 0.50 | 0.21 | 47.1 |
| NorthWest: Jerrara Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 27 | 53.8 | 27 | 53.8 | 0.042 | 6.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.27 | 0.00 | 53.6 |
| 11 T1 | 32 | 53.3 | 32 | 53.3 | 0.042 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.27 | 0.00 | 55.4 |
| Approach | 59 | 53.6 | 59 | 53.6 | 0.042 | 2.9 | NA | 0.0 | 0.0 | 0.00 | 0.27 | 0.00 | 54.3 |
| SouthWest: Hume Highway Off Ramp (SW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 13 | 100.0 | 13 | $\begin{gathered} 100 . \\ 0 \end{gathered}$ | 0.054 | 7.0 | LOS A | 0.2 | 2.2 | 0.16 | 0.58 | 0.16 | 47.7 |
| 2 T1 | 2 | 0.0 | 2 | 0.0 | 0.054 | 6.5 | LOS A | 0.2 | 2.2 | 0.16 | 0.58 | 0.16 | 51.6 |
| 3 R 2 | 16 | 53.3 | 16 | 53.3 | 0.054 | 10.3 | LOS A | 0.2 | 2.2 | 0.16 | 0.58 | 0.16 | 47.1 |
| Approach | 31 | 69.0 | 31 | 69.0 | 0.054 | 8.7 | LOS A | 0.2 | 2.2 | 0.16 | 0.58 | 0.16 | 47.8 |
| All Vehicles | 236 | 57.1 | 236 | 57.1 | 0.135 | 4.9 | NA | 0.6 | 6.2 | 0.15 | 0.45 | 0.15 | 49.1 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Network Data dialog (Network tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.



[^0]:    1 'Overburden': any extracted unsalable material.

[^1]:    2 Network peak refers to the peak across all intersections. For example, if four intersections are surveyed between 6 am and 9 am and the peak hours are between 6.45 am to 7.45 am for three of the intersections, the network peak is considered to be 6.45 am to 7.45 am . This is the peak hour for the road network as a whole, not necessarily for the site.

[^2]:    As the respective peak hours for each key intersection vary (Section 3.4.1i), the weighbridge data for the relevant peak hours are presented, noting that some of the peak hour intervals overlap.

[^3]:    *Assuming peak hour traffic being 10\% of daily traffic.

