17 June 2022

Chris Ritchie
Director, Industry Assessments
Department of Planning and Environment
4 Parramatta Square
12 Darcy Street
Parramatta NSW 2150

Dear Chris,

## RE: Mamre Road Precinct - Request for Additional Information - Traffic Modelling

This letter is written in response to the NSW Department of Planning and Environment's (DPE) request for additional information, dated 7 June 2022 and ongoing discussions with Transport for NSW relating to the precinct-wide modelling and removal of the Southern Link Road in the 2026 scenario.

The Mamre Road Landowner's Group - East (LOG-E) has prepared this response to respond to items pertaining to traffic modelling and traffic warrants. This letter is accompanied by an Ason memo to comprehensively address each of the issues raised.

## 1. Aldington Road - Warrant Assessment

The Intersection Warrant Analysis along Aldington Road: Modelling should take into account options for roundabouts and signals. If the warrants are not met (and signals cannot be supported within the medium and long term) there must be adequate land dedicated for the roundabouts in the interim.

The approval of traffic warrants along Abbotts and Aldington Roads is critical to enable the delivery under the proposed Planning Agreement with Penrith City Council.

The identification of signalised intersections for this important corridor as it was determined through extensive modelling and consultation, which was used to inform the Mamre Road Precinct Development Control Plan (DCP) (refer to Figure 1 below).

Figure 1 Road Network Hierarchy


To proceed with Penrith City Council on a design that reflects the DCP, the signalisation of intersections requires approval from Transport for NSW. The LOG-E has undertaken an assessment against Transport for NSW's Traffic Signal Design - Section 2 - Warrants, which is the guide for installation of traffic signals. It is important to note this document explicitly states it is a guide and traffic signals may be installed outside these criteria from external factors, such as public pressure or administrative direction.

The main criterion used to determine traffic signals is anticipated traffic flows through a corridor. The LOG-E instructed Ason to review the precinct-wide traffic model to determine if the 2026 scenario meets this criterion. The 2026 scenario identified the forecasted traffic flows do not meet the warrants for traffic generation under the guide. However, the 2036 scenario does meet the warrants criteria and satisfies the medium-long term for the Precinct.

While historically this criterion has been the main determinant factor to enable Transport for NSW to approval traffic signals, there are additional criteria to enable an approval outside of traffic generation and volume.

As stated earlier, the installation of signals may occur outside the guideline due to public pressure or an administrative directive. In the case of Abbotts and Aldington Roads intersections, the precinct-
wide DCP should be recognised as an administrative direction as it identifies where signalised intersections are to be located. Further, Penrith City Council has stated their preference in signals due to their desire for the ultimate solution delivery under the planning agreement.

To assist in understanding its qualitative merits, the following table provides an assessment against the guide and its application to the Abbotts and Aldington Road corridor.

Table 1 Assessment against Traffic Warrants Guide
\(\left.$$
\begin{array}{|l|l|}\hline \text { Traffic Warrant Criteria } & \text { Application to Abbotts and Aldington Roads } \\
\hline \text { Traffic Flows } & \begin{array}{l}\text { The } 2026 \text { modelling does not meet the traffic } \\
\text { flows criterion in the guide. However, the 2026 } \\
\text { scenario only assumes development on the } \\
\text { Mamre Road Precinct Landowner Group sites. }\end{array}
$$ <br>
The 2036 modelling of the precinct, which is <br>
the ultimate scenario, does meet the traffic <br>
flow warrant criterion. <br>
Given the current demand and climate for <br>
zoned industrial land, it is noted there are more <br>
development applications along this corridor <br>
other than the Mamre Road Precinct <br>
Landowners Group. These sites will contribute <br>
to overall traffic generation as the Precinct is <br>
delivered. Therefore, it is our opinion requiring <br>
roundabout intersections will quickly result in <br>

redundant works.\end{array}\right\}\)| Further, it does not align with the ultimate, |
| :--- |
| which Council is seeking to deliver in an |
| efficient manner once versus a protracted |
| staged delivery creating significant risks |
| pertaining to cost blowout. |


|  | traffic conflict and enable a pedestrian safe environment along the corridor. |
| :---: | :---: |
| Traffic Accident Statistics | The statistics on traffic accidents is unknown for the upgraded corridor. It is viewed that the delivery of signalised intersections along the corridor will be a preventative measure to minimise risk associated with this criterion. |
| Access to Major Roads | As the precinct road network is delivered, the Abbotts and Aldington Road will become a major thoroughfare connecting Mamre Road to the future Southern Link Road. The precinctwide modelling identifies a significant increase of traffic flows along this corridor once Southern Link Road is delivered, as it provides the most direct link route from Erskine Park to Elizabeth Drive. |
| Cost of Installation | The cost of installation of signals along Abbotts and Aldington Roads is factored into the Mamre Road Precinct Section 7.11 Contribution Plan and will be funded by developer contributions. <br> Future costs and redundant works have no source of funding. <br> The cost to deliver signalised intersection in today's dollars will be significantly cheaper compared to future augmentation. Therefore, it is the Government's best value for money to deliver the signals today versus future as money and levy mechanism is identified and developers are wiling to assist in delivering the ultimate in line with their forecasted delivery programs. This is not guaranteed in the future if signalised intersections are not delivered with the proposed planning agreement with Council. |
| Availability of Funds | The funds to deliver signalised intersections and the upgrade of Abbotts and Aldington Roads are available now via developers (under Section 7.11 contributions and works-in-kind). Further, Penrith City Council has been awarded funding by NSW Government to deliver the ultimate corridor including signalised intersections. This funding has been awarded on the basis the ultimate corridor can be delivered in line with delivery of industrial estates, which is occurring now and not in the future. |

## FIFECAPITAL

Stockland

| Maintenance Costs | Maintenance of signals, in the short term, can <br> be facilitated via developers through either the <br> planning agreement or contribution to ensure <br> no additional costs are incurred in lieu of <br> required traffic flows. |
| :--- | :--- |
| Practicality | The delivery of the ultimate outcome would <br> simplify land acquisition and delivery of <br> infrastructure. It significantly reduces the risk to <br> fund future upgrades and minimises redundant <br> works by developers or Council. |
| Feasibility | Traffic signals have been developed in the <br> concept design and costing of the Section 7.11 <br> contribution plan. |
| This concept design has been endorsed by |  |
| Council and DPE- Strategic Planning teams. It is |  |
| understood a housekeeping amendment is |  |
| currently being drafted based on the ultimate |  |
| alignment. It does not consider any intersection |  |
| treatments outside of signalised intersections |  |
| as per the DCP. |  |

Further to the assessment against Transport for NSW guideline on signalised intersection, the Mainroads Western Australia Guide provides research and guidance on how roads should be designed for large vehicle, such as trucks. In a summary, it notes the following:

> Needs of large vehicles signalised intersections are considered to provide a more convenient treatment for the drivers of large trucks than roundabouts, depending on the characteristics of the intersection. While trucks at times will encounter the inconvenience of coming to a complete stop at a red signal, they are often able to continue through a green signal. This is generally preferred to the inconvenience associated with negotiation a roundabout (Austroads, 2013), where multi-combinational vehicles struggle to "pick a gap" when the circulatory traffic is high due to poor acceleration characteristics. However, it should be noted that signalised intersections the traffic signal timing needs to accommodate the heavy vehicle acceleration characteristics.

Based on the above information, we believe there is sufficient justification and support to approve signals given it is consistent with the medium-long term.

## 2. Mamre Road Precinct 2026 model updated based on reverse brief and discussions on 8 March 2022 <br> This model was requested in order to review SSD applications in the area. The model requires updates as per below: <br> Modelling Input Assumptions

a. Road Network to be modelled (Figure 1): Option testing should be provided to understand the threshold that the intersection will operate at an unacceptable Level of Service
b. Table 2 Road Network Assumption - Mamre Road (south of Erskine Park Road): the lane assumptions are to be consistent with the existing (and approved) lane arrangements.
Scenario modelling was undertaken within the Southern Link Road in year 2026. The modelling shows how the Landowner's Group can unlock GFA in the short-medium term. A breakdown of this analysis is contained in the Ason memo attached.

## 3. Mamre Road Staging Strategy <br> Provide a copy of the traffic model underpinning the Mamre Road Precinct Staging Strategy presentation slides, which were presented to TfNSW and the Department on 13 April 2022.

The Ason memo outlines the proposed staging to ensure road hierarchy is completed as development progresses throughout the Mamre Road Precinct. As development progresses across the Precinct, we believe this staging strategy can be used to deliver the ultimate road network and enable the progressive development of the Precinct.

To assist with the sequencing, the LOG-E has prepared a summary of infrastructure works across the Mamre Road Precinct and the indicative costs for each upgrade. In summary, the landowners group via development applications and planning agreements has the ability to deliver $51 \%$ of the local road infrastructure within the Precinct. We ask the NSW Government to note the significant commitment, which is currently proposed to the LOG, given the 2026 scenario only assumes $75 \%$ of LOG-owned lands.

The remaining $18 \%$ can be delivered by other developers with current development applications within the system. This leaves the remaining $31 \%$ to be delivered by Council via contribution levies as future development is identified (refer to addendum in this letter).

The critical items to require NSW Government attention is the delivery of Mamre Road and Southern Link Road. While proposals are being sought for intersection upgrades along Mamre Road, it is critical for government to identify remaining funding as soon as possible to upgrade and deliver these road corridors. SIC funding has the ability to assist with kickstarting this work. The LOG-E has estimated value of contributions based on existing DAs to be $\$ 83,977,800$.

The LOG-E has invested a significant amount of time, money and resources to develop this staging scenario to assist NSW Government to progress development applications within the Precinct. We believe development can be jointly delivered as infrastructure is invested. This is demonstrated by the LOG-E's intent to deliver the entire Abbotts and Aldington Road corridor with collaboration with Penrith City Council. It is also demonstrated in the overall staging strategy for the entire Precinct.

As you can appreciate, this item is extremely critical and sensitive to development viability in the Precinct. Given the model is owned by the Landowner's Group, we ask to be included on any decision or discussion on this item to ensure the Precinct can be logically delivered in line with the infrastructure and commercial frameworks of both public and private stakeholders.

If you have any questions please do not hesitate to contact us.

Regards,

Mamre Road Precinct Landowners Group - East

## Richard Harris

Senior Development Manager

## FIFECAPITAL

## Craig Lenarduzzi

National Development Manager

## Workplace and Logistics

Stockland

Michael Robinson
Acquisition Manager
FRASERS
PROPERTY

Grace Macdonald
Planning Manager - NSW

## Attachment A: Ason Memo

FIFECAPITAL (B) Stockland

FRASERS PROPERTY

OESR

Breakdown in Section 7.11 Contribution Plan/ Staging


Yellow: To be delivered via Council/ Section 7.11 levies

| To | Landowners Group - East | info@asongroup.com.au |
| :--- | :--- | :--- |
|  | +61290836601 |  |
| FROM | Andrew Johnson (Director); Ason Group | Suite 17.02, Level 17, |
| CC |  | 1 Castlereagh Street, |
| Cydney, NSW 2000 |  |  |

ABN: 81168423872
SUBJECT Mamre Road Precinct - Revised Modelling and Warrants Assessment

Dear Landowners Group - East,

Ason Group have now completed the analysis of the road network conditions assuming the removal of the Southern Link Road (SLR) and the internal road network and demands which form part of the current SSDA applications relating to the broader Land Owners Group (LOG).

The analysis responds to the meeting held with Transport for NSW on the $8^{\text {th }}$ March and subsequent agreed scoping study dated 15 March 2022. The analysis also considers and responds to the Request for information (RFI) received from the Department of Planning and Environment dated 7 June 2022.

## Background

The Mamre Road Precinct Land Owners Group previously submitted Aimsun modelling to TfNSW in June 2021 for 2026 interim modelling and 2036 ultimate road network.

The 2036 modelling was endorsed by TfNSW and informed the adopted Mamre Road DCP Road Network. TfNSW was requested to undertake a sensitivity analysis and remove the inclusion of the Southern Link Road from the 2026 road network assumptions.

A scoping study was issued to TfNSW for review and comment on the $15^{\text {th }}$ March 2022 and generally agreed with the following additions:

- Option testing should be provided to understand the intersection thresholds.
- The $75 \%$ LOG GFA assumptions to be modelled under the revised scenario and adjusted, if required.
- Mamre Road (south of Erskine Park Road) lane assumptions are to be consistent with the existing (and approved) lane arrangements
- An intersection warrant analysis is to be included for the key intersections along Aldington Road


## Modelling Inputs Assumptions

For the purpose of this revised modelling, we adopted the previously agreed inputs documented in the TfNSW Mamre Road Modelling Outcomes memo, which forms the basis of all previous modelling completed for the precinct, including the June 2021 models submitted to TfNSW. A summary of the key input data and assumptions are listed below:

- Trip generation:
- AM Peak: 0.23 trips per $100 \mathrm{~m}^{2}$
- PM Peak: 0.24 trips per $100 \mathrm{~m}^{2}$
- Daily: 2.91 trips per $100 \mathrm{~m}^{2}$
- Model Time Periods:
- AM - 06:00-10:00
- PM - 15:00-19:00
- Traffic Demand and Distribution
- Background Growth per STFM LU19
- Internal Travel Zones (WSEA) per TfNSW approved disaggregation
- Mamre Road Travel Zones per Trip Generation profile based on approved Ason Group LUD Model
- The traffic flows on Compass Drive and SLR diverted to Mamre Road in conjunction with the latest STFM data.

The location of the relevant sites forming part of the Land Owners Group are shown in Figure 1. The figure also demonstrates the extent of the road network (particularly internal road network) that forms part of the relevant applications currently under consideration by the Department of Planning and Environment.


Figure 1: Road network Extents and LOG Ownership

Figure $\mathbf{- 2}$ shows the modelled Aimsun network with all key intersections in the precinct along Mamre Road and Aldington Road. As agreed, the SLR connection was removed between Compass drive and Aldington Road. The road network assumed includes all proposed or approved intersection layouts and the internal road network that can be delivered by the Land Owners Group as part of their current SSDA's.


Figure 2: Aimsun network with key intersections

## Adopted Intersection Layouts

Mamre Road / Bakers Lane
The adopted layout for the intersection of Mamre Road with Bakers Lane is shown in Figure 3 below. The intersection reflects that currently under construction by Altis / Frasers JV as part of the relevant conditions of consent relating to SSDA 9522.


Figure 3: Mamre Road / Bakers Lane Source: Altis

Mamre Road / New Road (Mirvac Access)
The adopted layout for the intersection of Mamre Road with the new connection to the Mirvac Access Road 01 is shown in Figure 4. This layout is consistent with that required as part of approved SSD 10448.


Figure 4: Mamre Road / MIRVAC Source: MIRVAC Drawing No. 2021_19_SKJ0009

## Mamre Road / Altis Left in Left out

The intersection providing access to the Altis development is shown in Figure 5. This access is consistent with the requirements of the recently endorsed DCP Road Network and forms part of the current application SSD 17647189 being assessed by DPE.


Figure 5: Mamre Road / Altis Left in Left Out Source: Altis

## Mamre Road / Abbotts Road

The layout adopted for the Mamre Road with Abbotts Road intersection is consistent with the VPA Letter of Offer and design previously presented to TfNSW.


Figure 6: Mamre Road / Abbotts Road Source: AT\&T Drawing No. 21-843-5KC025

## Aldington Road Corridor

The intersections along Aldington Road have been modelled as signalised intersections consistent with the endorsed DCP Road network. Three signalised junctions were included in the modelling including

- Aldington Road / New Road (north) - providing access to Fife Kemps Creek (North) and Frasers North developments,
- Aldington Road / New Road (south) - similarly providing access to the southern extent of the Fife Kemps Creek (south) development and Frasers South development, and
- Aldington Road / Abbotts Road.

The detailed layout of all intersections is shown in Figure - $\mathbf{8}$ to Figure - 10 .


Figure 7: Intersections along Aldington Road Source: AT\&L Drawing No. 21-843-C502

The detailed layout of each intersection is provided below. All layouts are consistent with the current VPA Offer proposed by the Land Owners Group (East). The layouts have also been generally endorsed by Penrith Council, subject to confirmation through modelling.


Figure 8: Aldington Road / Fife Kemps Creek (north) Source: AT\&L Drawing No. 21-843-C565


Figure 9: Aldington Road / Fife Kemps Creek (south) Source: AT\&L Drawing No. 21-843-C559


Figure 10: Aldington Road / Abbotts Road (Interim Layout)Source: AT\&L Drawing No. 21-843-C554

An initial modelling assumption of $57.5 \%$ of the total GFA was adopted to identify the operation of the network. The scenario included:

- Approximately $990,215 \mathrm{~m}^{2}$ of the total GFA
- The road network as currently proposed. That is, completely consistent with either the current SSDA applications, approved intersection layouts or current VPA offers.
- Internal road network assumed to be delivered by 2026.

The road network and intersection layouts are shown in Figure 11. The local road network, including Aldington Road and Abbotts Road (shown as Purple in the figure), will be delivered by developers and form part of the current SSD application under assessment by the department. For clarity, all purple roads can be delivered by 2026 via estate delivery or Works-in-Kind Agreements..


Figure 11: Precinct Key Intersection under Scenario 1
Table 2 summarises the SIDRA results for Scenario 1 and indicates that the assumed layout in both Mamre Road and Aldington Road corridor complied with the revised TfNSW threshold. A detailed SIDRA summary of all intersections is shown in Attachment 1.

TABLE 21 SCENARIO 1 - SIDRA RESULTS

| ID | Intersection | Control | Approach | AM |  |  | TfNSW Guidelines Compliance | PM |  |  | TfNSW Guidelines Compliance |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | DOS | LOS | Queue |  | DOS | LOS | Queue |  |
| 1 | Mamre Road / Bakers Lane | Signal | S | 0.76 | B | 205 | $\checkmark$ | 0.83 | B | 257 | $\checkmark$ |
|  |  |  | E | 0.78 | F | 38 | x | 0.87 | F | 110 | $\times$ |
|  |  |  | N | 0.72 | E | 54 | x | 0.87 | D | 315 | $\checkmark$ |
|  |  |  | W | 0.86 | C | 26 | $\checkmark$ | 0.66 | E | 75 | x |
|  |  |  | Overall | 0.86 | D | 205 | x | 0.87 | D | 315 | x |
| 2 | Mamre Road / Mirvac Access | Signal | S | 0.48 | B | 129 | $\checkmark$ | 0.75 | B | 133 | $\checkmark$ |
|  |  |  | E | 0.51 | D | 91 | $\checkmark$ | 0.64 | D | 110 | $\checkmark$ |
|  |  |  | N | 0.67 | B | 208 | $\checkmark$ | 0.87 | C | 355 | $\checkmark$ |
|  |  |  | Overall | 0.67 | B | 208 | $\checkmark$ | 0.87 | C | 355 | $\checkmark$ |
| 3 | Mamre Road / Altis Access | Priority (Left In Left Out) | S | 0.66 | A | - | $\checkmark$ | 0.73 | A | - | $\checkmark$ |
|  |  |  | E | 0.09 | A | - | $\checkmark$ | 0.18 | A | - | $\checkmark$ |
|  |  |  | N | 0.59 | A | - | $\checkmark$ | 0.88 | A | - | $\checkmark$ |
|  |  |  | Overall | 0.66 | A | - | $\checkmark$ | 0.88 | A | - | $\checkmark$ |
| 4 | Mamre Road / Abbotts Road | Signal | S | 0.39 | A | 22 | $\checkmark$ | 0.63 | A | 70 | $\checkmark$ |
|  |  |  | E | 0.18 | D | 14 | $\checkmark$ | 0.28 | D | 21 | $\checkmark$ |
|  |  |  | N | 0.34 | A | 37 | $\checkmark$ | 0.60 | A | 94 | $\checkmark$ |
|  |  |  | Overall | 0.39 | A | 37 | $\checkmark$ | 0.63 | A | 94 | $\checkmark$ |
| 5 | Aldington Road Fife Kemps Creek (North) | Signal | S | 0.06 | C | 10 | $\checkmark$ | 0.10 | D | 12 | $\checkmark$ |
|  |  |  | E | 0.13 | C | 21 | $\checkmark$ | 0.15 | B | 30 | $\checkmark$ |
|  |  |  | N | 0.25 | B | 28 | $\checkmark$ | 0.14 | C | 17 | $\checkmark$ |
|  |  |  | W | 0.19 | C | 11 | $\checkmark$ | 0.12 | C | 6 | $\checkmark$ |
|  |  |  | Overall | 0.25 | B | 28 | $\checkmark$ | 0.15 | C | 30 | $\checkmark$ |
| 6 | Aldington Road Fife Kemps Creek (South) | Signal | S | 0.09 | C | 13 | $\checkmark$ | 0.30 | C | 46 | $\checkmark$ |
|  |  |  | E | 0.31 | D | 32 | $\checkmark$ | 0.30 | C | 55 | $\checkmark$ |
|  |  |  | N | 0.03 | C | 5 | $\checkmark$ | 0.10 | D | 14 | $\checkmark$ |
|  |  |  | W | 0.23 | C | 22 | $\checkmark$ | 0.13 | C | 12 | $\checkmark$ |
|  |  |  | Overall | 0.31 | C | 32 | $\checkmark$ | 0.30 | C | 55 | $\checkmark$ |
| 7 | Aldington Road / Abbotts Road | Signal | E | 0.04 | D | 7 | $\checkmark$ | 0.07 | A | 13 | $\checkmark$ |
|  |  |  | N | 0.03 | D | 3 | $\checkmark$ | 0.05 | D | 6 | $\checkmark$ |
|  |  |  | W | 0.13 | A | 27 | $\checkmark$ | 0.30 | B | 56 | $\checkmark$ |
|  |  |  | Overall | 0.13 | B | 27 | $\checkmark$ | 0.30 | B | 56 | $\checkmark$ |
| 8 | Internal Roundabout (Mirvac) | Roundabout | S | 0.19 | A | 7 | $\checkmark$ | 0.22 | A | 12 | $\checkmark$ |
|  |  |  | N | 0.11 | A | 3 | $\checkmark$ | 0.06 | A | 4 | $\checkmark$ |
|  |  |  | W | 0.19 | A | 5 | $\checkmark$ | 0.06 | A | 3 | $\checkmark$ |
|  |  |  | Overall | 0.19 | A | 7 | $\checkmark$ | 0.22 | A | 12 | $\checkmark$ |
| 9 | Internal Roundabout (Altis) | Roundabout | S | 0.14 | A | 6 | $\checkmark$ | 0.22 | A | 7 | $\checkmark$ |
|  |  |  | N | 0.05 | A | 1 | $\checkmark$ | 0.03 | A | 1 | $\checkmark$ |
|  |  |  | W | 0.19 | A | 5 | $\checkmark$ | 0.08 | A | 2 | $\checkmark$ |
|  |  |  | Overall | 0.19 | A | 6 | $\checkmark$ | 0.22 | A | 7 | $\checkmark$ |

The modelling demonstrates that all intersections and movements operate within the thresholds set by TfNSW. All legs of all intersections comply with the original thresholds set by TfNSW in 2020, with the exception of the eastern approach to the Mamre Road / Bakers Lane intersection which operate with LoS of $F$ and with delays of 77.1 and 74.5 sec in the morning and evening peak period respectively. This minor noncompliance is acceptable noting that this intersection will likely be further upgraded in the short to medium term and that its overall LoS still meets the RMS Guide thresholds for signalised intersections.

The modelling demonstrates that subject to the delivery of the nominated infrastructure, including the internal road networks (which from part of the current SSDA's) and the upgrades as proposed to the Mamre Road corridor (including those currently under construction or proposed as part of the relevant VPA Offer), the network can accommodated approximately $990,215 \mathrm{~m}^{2}$ of development.

## Scenario 2

A second modelling scenario assuming $75 \%$ of the total GFA was modelled to identify the additional road network upgrades required. The scenario included:

- $1,291,584 \mathrm{~m}^{2}$ of total GFA within the Precinct
- The road network as adopted for Scenario 1 with the following additional upgrades:
- Widening of Mamre Road to four lanes (2 northbound and 2 southbound) between Bakers Lane and the Mirvac access intersection.
- Upgrade to Mamre Road / Bakers Lane
- North Approach - additional short through lane and dedicated left slip lane
- East Approach - Dedicated left slip lane
- West approach - Dedicated left slip lane
- South approach - additional short through lane, dedicated left slip lane and additional departure lane
Figure 12 below shows the assumed Mamre Road and Aldington Road corridor, the required upgrades are listed below and highlighted blue in the figure.


Figure 12: Additional Upgrades under 75\% GFA Scenario


Figure 13: Precinct Key Intersection under 75\% GFA

The results of the modelling are provided in Table 3 with detailed SIDRA movement/layout summary included at Attachment 2. The modelling demonstrates:

- Generally improved network operation with reduced queues and delays at Bakers Lane with Mamre Road
- All intersections and individual legs operate with delays and degree of saturation within the limits set by TfNSW
- Spare capacity at all intersections to enable further development above the $1,291,584 \mathrm{~m}^{2}$ modelled.

The additional upgrades identified can therefore accommodate at least the $1,291,584 \mathrm{~m}^{2}$ GFA of the relevant Land Owners Group. Additional capacity would also be available for smaller applications within the precinct that would unlikely result in any further degradation below the acceptable thresholds nominated by TfNSW.

It is noted that additional capacity may also be available within the network having consideration to the trip rates required for adoption. The rates, which are significantly higher than those established through surveys or inherent within he RMS Guide to Traffic Generating Developments, in our view overestimate the future transport demands and therefore reflect a worst case analysis.

TABLE 32 SCENARIO 2 - SIDRA RESULTS

| ID | Intersection | Control | Approach | AM |  |  | TfNSW Guidelines Compliance | PM |  |  | TfNSW Guidelines Compliance |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | DOS | LOS | Queue |  | DOS | LOS | Queue |  |
| 1 | Mamre Road / Bakers Lane | Signal | S | 0.90 | D | 310 | $\checkmark$ | 0.89 | C | 332 | $\checkmark$ |
|  |  |  | E | 0.30 | D | 31 | $\checkmark$ | 0.74 | D | 118 | $\checkmark$ |
|  |  |  | N | 0.86 | C | 295 | $\checkmark$ | 0.85 | C | 282 | $\checkmark$ |
|  |  |  | W | 0.29 | C | 40 | $\checkmark$ | 0.48 | D | 90 | $\checkmark$ |
|  |  |  | Overall | 0.90 | C | 310 | $\checkmark$ | 0.89 | C | 332 | $\checkmark$ |
| 2 | Mamre Road / Mirvac Access | Signal | S | 0.73 | B | 142 | $\checkmark$ | 0.88 | B | 171 | $\checkmark$ |
|  |  |  | E | 0.71 | D | 138 | $\checkmark$ | 0.79 | D | 149 | $\checkmark$ |
|  |  |  | N | 0.58 | B | 178 | $\checkmark$ | 0.90 | D | 405 | $\checkmark$ |
|  |  |  | Overall | 0.72 | B | 178 | $\checkmark$ | 0.90 | C | 405 | $\checkmark$ |
| 3 | Mamre Road / Altis Access | Priority (Left In Left Out) | S | 0.67 | A | - | $\checkmark$ | 0.82 | A | - | $\checkmark$ |
|  |  |  | E | 0.11 | A | - | $\checkmark$ | 0.30 | C | - | $\checkmark$ |
|  |  |  | N | 0.57 | A | - | $\checkmark$ | 0.89 | C | - | $\checkmark$ |
|  |  |  | Overall | 0.67 | A | - | $\checkmark$ | 0.89 | C | - | $\checkmark$ |
| 4 | Mamre Road / <br> Abbotts Road | Signal | S | 0.48 | A | 31 | $\checkmark$ | 0.84 | B | 105 | $\checkmark$ |
|  |  |  | E | 0.06 | D | 11 | $\checkmark$ | 0.48 | D | 37 | $\checkmark$ |
|  |  |  | N | 0.35 | A | 51 | $\checkmark$ | 0.64 | A | 109 | $\checkmark$ |
|  |  |  | Overall | 0.48 | A | 51 | $\checkmark$ | 0.84 | B | 109 | $\checkmark$ |
| 5 | Aldington Road / Fife Kemps Creek (North) | Signal | S | 0.05 | B | 9 | $\checkmark$ | 0.21 | C | 34 | $\checkmark$ |
|  |  |  | E | 0.15 | C | 26 | $\checkmark$ | 0.21 | C | 39 | $\checkmark$ |
|  |  |  | N | 0.25 | B | 27 | $\checkmark$ | 0.14 | C | 23 | $\checkmark$ |
|  |  |  | W | 0.20 | C | 7 | $\checkmark$ | 0.19 | C | 10 | $\checkmark$ |
|  |  |  | Overall | 0.25 | B | 27 | $\checkmark$ | 0.21 | C | 39 | $\checkmark$ |
| 6 | Aldington Road / Fife Kemps Creek (South) | Signal | S | 0.20 | C | 35 | $\checkmark$ | 0.41 | D | 69 | $\checkmark$ |
|  |  |  | E | 0.26 | D | 40 | $\checkmark$ | 0.41 | C | 75 | $\checkmark$ |
|  |  |  | N | 0.03 | C | 5 | $\checkmark$ | 0.20 | C | 31 | $\checkmark$ |
|  |  |  | W | 0.19 | C | 18 | $\checkmark$ | 0.30 | C | 31 | $\checkmark$ |
|  |  |  | Overall | 0.26 | C | 40 | $\checkmark$ | 0.41 | C | 75 | $\checkmark$ |
| 7 | Aldington Road / Abbotts Road | Signal | E | 0.21 | B | 24 | $\checkmark$ | 0.10 | A | 18 | $\checkmark$ |
|  |  |  | N | 0.04 | D | 4 | $\checkmark$ | 0.19 | D | 23 | $\checkmark$ |
|  |  |  | W | 0.21 | B | 48 | $\checkmark$ | 0.46 | B | 113 | $\checkmark$ |
|  |  |  | Overall | 0.21 | B | 48 | $\checkmark$ | 0.46 | B | 113 | $\checkmark$ |
| 8 | Internal Roundabout (Mirvac) | Roundabout | S | 0.21 | A | 16 | $\checkmark$ | 0.30 | A | 18 | $\checkmark$ |
|  |  |  | N | 0.07 | A | 4 | $\checkmark$ | 0.10 | A | 4 | $\checkmark$ |
|  |  |  | W | 0.19 | A | 10 | $\checkmark$ | 0.15 | A | 9 | $\checkmark$ |
|  |  |  | Overall | 0.21 | A | 16 | $\checkmark$ | 0.30 | A | 18 | $\checkmark$ |
| 9 | Internal Roundabout (Altis South) | Roundabout | S | 0.14 | A | 10 | $\checkmark$ | 0.28 | A | 16 | $\checkmark$ |
|  |  |  | N | 0.13 | A | 8 | $\checkmark$ | 0.12 | A | 9 | $\checkmark$ |
|  |  |  | W | 0.11 | A | 5 | $\checkmark$ | 0.10 | A | 4 | $\checkmark$ |
|  |  |  | Overall | 0.14 | A | 10 | $\checkmark$ | 0.28 | A | 16 | $\checkmark$ |

Based on the modelling completed for the corridor the following additional works must be considered to release further capacity in the network to enable further development within the precinct:


Figure 13: Additional Road Network Upgrades
The main constraint within the network is the lack of north-south capacity. The logical next stage of works is the delivery of the SLR Stage 1, which would provide a connection between Mamre Road and Compass Drive (including a new connection with Aldington Road). This connection would provide direct access to Lenore Drive, reducing the reliance on Erskine Park Road and Mamre Road and providing an alternate route to the M7 and M4 motorways.

Additional localised capacity can also be achieved through the further widening of Mamre Road, between Mirvac Site Access to Kerrs Road (see Figure 13). This widening would provide additional north-south capacity.

The delivery of SLR combined with regional network upgrades assumed in the Governments Strategic Modelling and Works Programs will support the delivery of the Precinct. These upgrades are to be programmed and coordinated by Transport for NSW.

## Traffic Signal Warrant

At the request of TfNSW a traffic warrant assessment has been completed for the design horizon year of 2026 (Scenario 2) and 2036 under full development of the precinct. It is noted that whilst this assessment has been completed, the need for signals should be considered across multiple criteria and not just the warrants in isolation, particularly for Greenfield developments.

The RMS Traffic Signal Design - Section 2 stipulates:
"traffic signals are sometimes installed due to public pressure or an administrative directive irrespective of the general warrants".

In the case of the Aldington Road intersections the Mamre Road Precinct DCP can be seen as an administrative directive, that identifies where signalised intersections are to be located. The Penrith City Council has also made it clear that they prefer signals in part due to the delivery of what is viewed at the ultimate solution for the intersections, which has cost and delivery implications.

Notwithstanding this, a traffic warrant assessment was conducted in accordance with the guidelines set forth by the RTA in the Traffic Signal Design Section 2 - Warrants, the traffic flow warrants are listed below:

- Traffic Demand:
- The major road flow exceeds 600 vehicles/hour in each direction, and
- The minor road flow exceeds 200 vehicles/hours in one direction.
- Continuous Traffic:
- The major road flow exceeds 900 vehicles/hour in each direction, and
- The minor road flow exceeds 100 vehicles/hour in one direction.

Table 3 below summarizes the traffic signal warrant for intersections along Mamre Road and Aldington Road corridor for the 2026 and 2036 scenarios. A detailed analysis of each movement and approach is also provided in Attachment 3.

TABLE 4 TRAFFIC SIGNAL WARRANT

| \# | Key Intersections | Traffic Signal Warrant Satisfied 2026 (Scenario 2) |  | Traffic Signal Warrant Satisfied 2036 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM | PM | AM | PM |
| 1 | Mamre Road / Bakers Lane | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 2 | Mamre Road / Mirvac Access | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 3 | Mamre Road / Abbotts Road | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| 4 | Aldington Road / Fife Kemps Creek (North) | X | X | $\checkmark$ | $\checkmark$ |
| 5 | Aldington Road / Fife Kemps Creek (south) | X | X | $\checkmark$ | $\checkmark$ |
| 6 | Aldington Road / Abbotts Road | X | X | $\checkmark$ | $\checkmark$ |

The warrant assessment demonstrates compliance with all proposed signalised intersections by 2036.

Whilst technical traffic flow warrants are not met under the 2026 Scenario, further considerations must be considered as noted in the RMS Traffic Signal Design strategic direction. The relevant qualitative merits considered under the Guide are outlined in Table 5.

TABLE 5 CONSIDERATIONS IN SIGNALISATION OF ALDINGTON ROAD

| Factors for Consideration | Application to Aldington Road |
| :--- | :--- |
|  | The 2026 modelling does not meet the traffic flows criterion in the guide. <br> However, the 2026 scenario only assumes development on the Mamre <br> Road Precinct Landowner Group sites. |
| Traffic flows | The 2036 modelling of the precinct, which is the ultimate scenario, does <br> meet the traffic flow warrant criterion. |
| Given the current demand for zoned industrial land, it is noted there are <br> more development applications along this corridor other than the Mamre <br> Road Precinct Landowners Group. These sites will contribute to overall <br> traffic generation as the Precinct is delivered. |  |
| Traffic conflicts | The relationship and interaction between trucks, light vehicles and <br> pedestrians is a significant criterion for assessment of warrants. The <br> strategic planning for Mamre Road Precinct identified the need to create <br> an employment precinct which contributes toward all forms of transport, <br> including cycling and walking. |
| Traffic accident statistics | The delivery of signalised intersections enables safe crossings along the <br> corrider for pedestrians and cyclists. Given the nature of trucks entering <br> and exiting this corridor and their restricted visibility compared to light <br> vehicles, traffic signals are required to minimise traffic conflict and <br> enable a pedestrian safe environment along the corridor. |
| The statistics on traffic accidents is unknown for the upgraded corridor. <br> It is viewed that the delivery of signalised intersections along the corridor <br> will be a preventative measure to minimise risk associated with this <br> criterion |  |
| Pedestrian requirements | Pedestrian access is being encouraged with a requirement for Green <br> Travel Plans, bus routes. Crossing facilities must be provided within the <br> corridor to facilitate safe pedestrian movements |
| Access to major roads | Aldington Road and Abbotts Road are designated as Distributor <br> Industrial roads under the Mamre Road Precinct DCP. |
| As the precinct road network is delivered, Abbotts Road and Aldington |  |
| Road will become a major thoroughfare connecting Mamre Road to the |  |
| future Southern Link Road. The precinct-wide modelling identififes a installation |  |
| significant increase of traffic flows along this corridor once Southern Link |  |
| Road is delivered, as it provides the most direct link route from Erskine |  |
| Park to Elizabeth Drive. |  |


|  | The cost to deliver signalised intersection in today's dollars will be <br> significantly cheaper compared to future augmentation. Therefore, it is <br> the Government's best value for money to deliver the signals today <br> versus future as money and levy mechanism is identified and <br> developers are wiling to assist in delivering the ultimate in line with their <br> forecasted delivery programs. This is not guaranteed in the future if <br> signalised intersections are not delivered with the proposed planning <br> agreement with Council |
| :--- | :--- |
| Availability of funds | The funds to deliver signalised intersections and the upgrade of Abbotts <br> and Aldington Roads are available now via developers (under Section <br> 7.11 contributions and works-in-kind). Further, Penrith City Council has <br> been awarded funding by NSW Government to deliver the ultimate <br> corridor including signalised intersections. This funding has been <br> awarded on the basis the ultimate corridor can be delivered in line with <br> delivery of industrial estates, which is occurring now and not in the <br> future. |
| Maintenance Costs | Maintenance of signals, in the short term, can be facilitated via <br> developers through either the planning agreement or contribution to <br> ensure no additional costs are incurred in lieu of required traffic flows. |
| Practicality | The delivery of the ultimate outcome would simplify land acquisition and <br> delivery of infrastructure. It significantly reduces the risk to fund future <br> upgrades and minimises redundant works by developers or Council. |
| Feasibility | Traffic signals have been developed in the concept design and costing <br> of the Section 7.11 contribution plan. <br> This concept design has been endorsed by Council and DPE- Strategic |
| Planning teams. It is understood a housekeeping amendment is |  |
| currently being drafted based on the ultimate alignment. It does not |  |
| consider any intersection treatments outside of signalised intersections |  |
| as per the DCP. |  |$|$| Signposted speed limit is not |
| :--- |
| more than 80km/hr | | Signposted speed limit expected to be 60km/hr. |
| :--- |

Noting the above, there is sufficient justification for TfNSW to approve signals along Aldington Road, consistent with he recently endorsed Mamre Road DCP. The construction of signals will improve traffic and road user safety with minimal, if any, impact to TfNSW. Furthermore, there is sufficient risk that funding for future signalisation of the subject intersections would not be available in the future.

## Summary

Based on the analysis and set of assumptions outlined above the following conclusion have been reached:

## Scenario 1

- The road network currently proposed or under construction by Land Owners Group members can deliver up to $900,000 \mathrm{~m}^{2}$,
- All intersections along the Mamre Road and Aldington Road corridor complied with the TfNSW threshold for both Delays and practical capacity.


## Scenario 2

- To support the additional GFA (up to $1,291,584 \mathrm{~m}^{2}$ ) some upgrades to the road network would be required to retain the operating thresholds set by TfNSW.
- These upgrades would include:
- Widening of Mamre Road to four lanes (2 northbound and 2 southbound) between Bakers Lane and the Mirvac access intersection.
- Upgrade to Mamre Road / Bakers Lane
- The modelling demonstrates that with the aforementioned upgrades all intersection along Mamre Road and Aldington corridor operates at LoS C or better.


## Ultimate Precinct Delivery

- Additional capacity can be delivered within the precinct through additional road network upgrades.
- These upgrades have not been considered as part of this analysis however would include:
- Delivery of SLR Stage 1
- Duplication of Mamre Road through lanes, south of the Mirvac Access Road
- Regional road network upgrades previously identified by TfNSW and included in the current strategic modelling for WSEA and broader Aerotropolis.


## Traffic Signal Warrant

- Under the modelled scenarios, the traffic signal warrants on Aldington Road are not met in the 2026 scenario. However, the 2036 modelling confirms Aldington Road corridor requires signalised intersection, therefore satisfying the medium-long term requirement.
- Traffic signal warrants are not the only criteria that should be considered in TfNSW's assessment and consideration to all road users and the recently endorsed DCP must also be considered.

Based on the above, we see no impediment to the approval of the current SSDA applications that form the Land Owners Group East. Additionally, the modelling demonstrates that the proposed road network meets all of TfNSW requirements.

Yours sincerely,


## Andrew Johnson

Director
E andrew.johnson@asongroup.com.au

## Attachment 1

## SITE LAYOUT

目 Site: 1 [IID: 1] (AM) Bakers Lane / Mamre Road - AM (Site
Folder: 2026 - AM 60\% GFA)]
Bakers Lane / Mamre Road
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Coordinated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.
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Project: C:IUsers\Arun Mohan\Desktop\Ason Group\P1815-2026 MRP revised modellingISIDRA Files\From SharepointlP1815 2026 SIDRA Models Option 0 (1) (2).sip9

## MOVEMENT SUMMARY

目 Site: 1 [[ID: 1] (AM) Bakers Lane / Mamre Road - AM (Site
Folder: 2026 - AM 60\% GFA)]
Bakers Lane / Mamre Road
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Coordinated Cycle Time $=122$ seconds (Site User-Given Phase Times)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INP } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | MES <br> HV $]$ veh/h |  | AND NS HV ] \% | Deg. <br> Satn <br> V/c | Aver. Delay sec | Level of Service | $\begin{gathered} 95 \% \text { E } \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No Cycles | Aver. Speed km/h |
| South: Mamre Road (1200m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 21 | 15 | 22 | 70.3 | 0.039 | 14.6 | LOS B | 0.3 | 4.7 | 0.44 | 0.68 | 0.44 | 57.1 |
| 2 T1 | 1242 | 245 | 1307 | 19.7 | 0.761 | 14.8 | LOS B | 22.8 | 205.4 | 0.64 | 0.59 | 0.64 | 70.6 |
| 3 R2 | 45 | 7 | 47 | 15.6 | * 0.719 | 77.6 | LOS F | 3.1 | 24.8 | 1.00 | 0.81 | 1.24 | 40.1 |
| Approach | 1308 | 267 | 1377 | 20.4 | 0.761 | 17.0 | LOS B | 22.8 | 205.4 | 0.65 | 0.59 | 0.66 | 69.0 |
| East: Bakers Ln |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 2 | 1 | 2 | 50.0 | 0.018 | 194.5 | LOS F | 0.1 | 1.3 | 0.88 | 0.63 | 0.88 | 48.6 |
| 5 T1 | 1 | 0 | 1 | 0.0 | 0.018 | 44.2 | LOS D | 0.1 | 1.3 | 0.88 | 0.63 | 0.88 | 39.5 |
| 6 R2 | 149 | 9 | 157 | 6.0 | * 0.776 | 75.8 | LOS F | 5.1 | 37.5 | 1.00 | 0.85 | 1.27 | 42.4 |
| Approach | 152 | 10 | 160 | 6.6 | 0.776 | 77.1 | LOS F | 5.1 | 37.5 | 1.00 | 0.84 | 1.26 | 42.4 |
| North: Mamre Road (1250m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 362 | 0 | 381 | 0.0 | 0.237 | 9.3 | LOSA | 4.7 | 33.0 | 0.23 | 0.69 | 0.23 | 70.1 |
| 8 T1 | 1633 | 230 | 1719 | 14.1 | * 0.724 | 74.7 | LOS F | 6.4 | 53.6 | 0.14 | 0.13 | 0.14 | 78.8 |
| 9 R2 | 227 | 34 | 239 | 14.9 | 0.394 | 54.3 | LOS D | 6.3 | 53.2 | 0.92 | 0.79 | 0.92 | 43.7 |
| Approach | 2222 | 264 | 2339 | 11.9 | 0.724 | 62.0 | LOS E | 6.4 | 53.6 | 0.23 | 0.29 | 0.23 | 72.7 |
| West: Bakers Ln |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 101 | 30 | 106 | 29.7 | 0.116 | 12.7 | LOS A | 1.9 | 20.1 | 0.32 | 0.62 | 0.32 | 56.3 |
| 11 T1 | 1 | 0 | 1 | 0.0 | 0.116 | 5.5 | LOS A | 1.9 | 20.1 | 0.32 | 0.62 | 0.32 | 55.2 |
| 12 R 2 | 33 | 10 | 35 | 30.3 | * 0.855 | 82.4 | LOS F | 2.5 | 26.2 | 1.00 | 0.95 | 1.60 | 35.2 |
| Approach | 135 | 40 | 142 | 29.6 | 0.855 | 29.7 | LOS C | 2.5 | 26.2 | 0.49 | 0.70 | 0.64 | 49.2 |
| All <br> Vehicles | 3817 | 581 | 4018 | 15.2 | 0.855 | 46.0 | LOS D | 22.8 | 205.4 | 0.41 | 0.43 | 0.43 | 68.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline \multicolumn{12}{|l|}{Pedestrian Movement Performance} \\
\hline \[
{ }_{\text {ID }}^{\text {Mov }} \text { Crossing }
\] \& \begin{tabular}{l}
Input Vol. \\
ped/h
\end{tabular} \& Dem. Flow ped/h \& Aver. Delay sec \& \multicolumn{3}{|l|}{Level of AVERAGE BACK OF Service QUEUE} \& \multicolumn{2}{|l|}{Prop. Effective
Que
Stop

Rate} \& Travel Time sec \& \begin{tabular}{l}
Travel Dist. <br>
m

 \& 

Aver. <br>
Speed <br>
$\mathrm{m} / \mathrm{sec}$
\end{tabular} <br>

\hline \multicolumn{12}{|l|}{South: Mamre Road (1200m)} <br>
\hline P1 Full \& 10 \& 11 \& 55.2 \& LOS E \& 0.0 \& 0.0 \& 0.95 \& 0.95 \& 229.3 \& 226.4 \& 0.99 <br>
\hline \multicolumn{12}{|l|}{East: Bakers Ln} <br>
\hline P2 Full \& 10 \& 11 \& 55.2 \& LOS E \& 0.0 \& 0.0 \& 0.95 \& 0.95 \& 223.4 \& 218.7 \& 0.98 <br>
\hline
\end{tabular}

West: Bakers Ln

| P4 Full | 10 | 11 | 55.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 223.9 | 219.4 | 0.98 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| All | 30 | 32 | 55.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 225.6 | 221.5 | 0.98 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## MOVEMENT SUMMARY

目 Site: 1 [[ID: 1] Bakers Lane / Mamre Road - PM (Site Folder:
2026 - PM 60\% GFA)]
Bakers Lane / Mamre Road
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Coordinated Cycle Time $=120$ seconds (Site User-Given Cycle Time)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  |  |  | $\begin{aligned} & \text { AND } \\ & \text { WS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% B <br> [ Veh. <br> veh | $\overline{C K}$ OF UE Dist ] | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Mamre Road (1200m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 92 | 18 | 97 | 19.6 | 0.084 | 11.5 | LOS A | 1.5 | 12.8 | 0.28 | 0.68 | 0.28 | 58.9 |
| 2 T1 | 1424 | 209 | 1499 | 14.7 | 0.826 | 18.1 | LOS B | 30.8 | 257.3 | 0.73 | 0.69 | 0.76 | 68.8 |
| 3 R 2 | 5 | 0 | 5 | 0.0 | 0.056 | 68.3 | LOS E | 0.3 | 2.1 | 0.98 | 0.65 | 0.98 | 43.9 |
| Approach | 1521 | 227 | 1601 | 14.9 | 0.826 | 17.9 | LOS B | 30.8 | 257.3 | 0.71 | 0.69 | 0.73 | 68.1 |
| East: Bakers Ln |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 33 | 0 | 35 | 0.0 | 0.132 | 124.7 | LOS F | 1.9 | 13.0 | 0.91 | 0.73 | 0.91 | 47.4 |
| 5 T1 | 1 | 0 | 1 | 0.0 | 0.132 | 52.8 | LOS D | 1.9 | 13.0 | 0.91 | 0.73 | 0.91 | 36.4 |
| 6 R2 | 453 | 9 | 477 | 2.0 | * 0.865 | 70.9 | LOS F | 15.4 | 109.9 | 1.00 | 0.94 | 1.28 | 43.8 |
| Approach | 487 | 9 | 513 | 1.8 | 0.865 | 74.5 | LOS F | 15.4 | 109.9 | 0.99 | 0.92 | 1.25 | 44.0 |
| North: Mamre Road (1250m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 145 | 2 | 153 | 1.6 | 0.107 | 11.2 | LOS A | 2.4 | 16.8 | 0.29 | 0.69 | 0.29 | 68.3 |
| 8 T1 | 1436 | 259 | 1512 | 18.0 | * 0.868 | 57.4 | LOS E | 36.1 | 314.5 | 0.80 | 0.79 | 0.86 | 66.3 |
| 9 R2 | 56 | 39 | 59 | 69.6 | * 0.619 | 77.8 | LOS F | 1.9 | 25.9 | 1.00 | 0.79 | 1.18 | 38.0 |
| Approach | 1637 | 300 | 1723 | 18.3 | 0.868 | 54.0 | LOS D | 36.1 | 314.5 | 0.76 | 0.78 | 0.82 | 65.1 |
| West: Bakers Ln |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 149 | 22 | 157 | 14.8 | 0.659 | 63.1 | LOS E | 9.1 | 75.4 | 0.99 | 0.83 | 1.03 | 41.0 |
| 11 T1 | 1 | 0 | 1 | 0.0 | * 0.659 | 54.1 | LOS D | 9.1 | 75.4 | 0.99 | 0.83 | 1.03 | 35.7 |
| 12 R 2 | 117 | 22 | 123 | 18.8 | 0.559 | 57.4 | LOS E | 6.9 | 61.3 | 0.98 | 0.80 | 0.98 | 40.9 |
| Approach | 267 | 44 | 281 | 16.5 | 0.659 | 60.5 | LOS E | 9.1 | 75.4 | 0.99 | 0.82 | 1.01 | 40.9 |
| All <br> Vehicles | 3912 | 580 | 4118 | 14.8 | 0.868 | 42.9 | LOS D | 36.1 | 314.5 | 0.78 | 0.77 | 0.85 | 61.1 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Input Vol. <br> ped/h | Dem. Flow <br> ped/h | Aver. Delay <br> sec | Level of Service |  | $\begin{aligned} & \text { ACK OF } \\ & \text { IE } \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. Que | ective Stop Rate | Travel Time $\qquad$ sec | Travel Dist. $\qquad$ | Aver. <br> Speed <br> $\mathrm{m} / \mathrm{sec}$ |
| South: Mamre Road (1200m) |  |  |  |  |  |  |  |  |  |  |  |
| P1 Full | 10 | 11 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 228.3 | 226.4 | 0.99 |
| East: Bakers Ln |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 10 | 11 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 222.4 | 218.7 | 0.98 |

West: Bakers Ln

| P4 Full | 10 | 11 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 222.9 | 219.4 | 0.98 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| All | 30 | 32 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 224.6 | 221.5 | 0.99 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## SITE LAYOUT

目 Site: 2 [[ID: 2] (AM) Mamre x Mirvac Access - AM (Site Folder:
2026 - AM 60\% GFA)]
Mamre Road x Mirvac Access
Site Category: Proposed Interim
Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


## MOVEMENT SUMMARY

目 Site: 2 [[ID: 2] (AM) Mamre x Mirvac Access - AM (Site Folder:
2026 - AM 60\% GFA)]
Mamre Road x Mirvac Access
Site Category: Proposed Interim
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=120$ seconds (Site User-Given Phase Times)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | INPUT VOLUMES |  | DEMAND FLOWS |  | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% BACK OF QUEUE |  | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Mamre Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 1062 | 128 | 1118 | 12.1 | 0.475 | 13.6 | LOS A | 16.0 | 129.0 | 0.54 | 0.49 | 0.54 | 57.9 |
| 3 R2 | 37 | 16 | 39 | 43.2 | * 0.262 | 61.5 | LOS E | 2.2 | 25.8 | 0.95 | 0.74 | 0.95 | 29.5 |
| Approach | 1099 | 144 | 1157 | 13.1 | 0.475 | 15.2 | LOS B | 16.0 | 129.0 | 0.55 | 0.50 | 0.55 | 56.1 |
| East: Mirvac Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 22 | 6 | 23 | 27.3 | 0.036 | 15.7 | LOS B | 0.4 | 4.3 | 0.38 | 0.59 | 0.38 | 47.3 |
| 6 R2 | 264 | 135 | 278 | 51.1 | * 0.506 | 53.1 | LOS D | 7.3 | 90.9 | 0.92 | 0.80 | 0.92 | 30.8 |
| Approach | 286 | 141 | 301 | 49.3 | 0.506 | 50.2 | LOS D | 7.3 | 90.9 | 0.88 | 0.79 | 0.88 | 31.7 |
| North: Mamre Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 590 | 137 | 621 | 23.2 | 0.501 | 8.4 | LOS A | 6.1 | 56.4 | 0.27 | 0.66 | 0.27 | 51.8 |
| 8 T1 | 1098 | 129 | 1156 | 11.7 | * 0.670 | 26.7 | LOS B | 25.6 | 207.7 | 0.82 | 0.74 | 0.82 | 47.2 |
| Approach | 1688 | 266 | 1777 | 15.8 | 0.670 | 20.3 | LOS B | 25.6 | 207.7 | 0.63 | 0.71 | 0.63 | 48.7 |
| All Vehicles | 3073 | 551 | 3235 | 17.9 | 0.670 | 21.2 | LOS B | 25.6 | 207.7 | 0.62 | 0.64 | 0.62 | 48.6 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\text { ID }_{\text {Mov }} \text { Crossing }$ | Input Vol. <br> ped/h | Dem. Flow <br> ped/h | Aver. Delay $\qquad$ <br> sec | Level of AVERAGE BACK OF Service QUEUE |  |  | Prop. Effective Que Stop |  | Travel Time $\qquad$ | Travel Aver. Dist. Speed $\mathrm{m} \mathrm{m} / \mathrm{sec}$ |  |
| South: Mamre Rd |  |  |  |  |  |  |  |  |  |  |  |
| P1 Full | 50 | 53 | 50.5 | LOS E | 0.2 | 0.2 | 0.92 | 0.92 | 222.5 | 223.5 | 1.00 |
| East: Mirvac Access |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 50 | 53 | 22.9 | LOS C | 0.1 | 0.1 | 0.62 | 0.62 | 189.8 | 217.0 | 1.14 |
| All Pedestrians | 100 | 105 | 36.7 | LOS D | 0.2 | 0.2 | 0.77 | 0.77 | 206.1 | 220.3 | 1.07 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

## MOVEMENT SUMMARY

Site: 2 [[ID: 2] Mamre x Mirvac Access - PM (Site Folder: 2026 -
PM 60\% GFA)]
Mamre Road x Mirvac Access
Site Category: Proposed Interim
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=120$ seconds (Site User-Given Phase Times)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | UT MES HV ] veh/h | $\begin{aligned} & \text { DEM } \\ & \text { FLO } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { AND } \\ & \text { WS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay sec $\qquad$ | Level of Service | $\begin{gathered} 95 \% \text { B } \\ \text { QU } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Mamre Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 1102 | 114 | 1160 | 10.3 | 0.488 | 16.5 | LOS B | 16.8 | 133.3 | 0.54 | 0.49 | 0.54 | 57.8 |
| 3 R2 | 132 | 24 | 139 | 18.2 | * 0.751 | 67.1 | LOS E | 8.5 | 75.1 | 1.00 | 0.87 | 1.16 | 28.3 |
| Approach | 1234 | 138 | 1299 | 11.2 | 0.751 | 21.9 | LOS B | 16.8 | 133.3 | 0.59 | 0.53 | 0.61 | 52.0 |
| East: Mirvac Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 45 | 5 | 47 | 11.1 | 0.066 | 26.8 | LOS B | 1.2 | 9.8 | 0.52 | 0.64 | 0.52 | 43.2 |
| 6 R2 | 404 | 112 | 425 | 27.7 | * 0.637 | 56.7 | LOS E | 11.5 | 110.1 | 0.96 | 0.83 | 0.96 | 29.6 |
| Approach | 449 | 117 | 473 | 26.1 | 0.637 | 53.7 | LOS D | 11.5 | 110.1 | 0.92 | 0.81 | 0.92 | 30.6 |
| North: Mamre Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 145 | 90 | 153 | 62.1 | 0.161 | 9.4 | LOS A | 1.5 | 19.9 | 0.24 | 0.62 | 0.24 | 50.9 |
| 8 T1 | 1408 | 190 | 1482 | 13.5 | * 0.869 | 40.9 | LOS C | 43.1 | 355.4 | 0.96 | 0.96 | 1.06 | 40.9 |
| Approach | 1553 | 280 | 1635 | 18.0 | 0.869 | 38.0 | LOS C | 43.1 | 355.4 | 0.90 | 0.93 | 0.98 | 41.7 |
| All Vehicles | 3236 | 535 | 3406 | 16.5 | 0.869 | 34.0 | LOS C | 43.1 | 355.4 | 0.78 | 0.76 | 0.83 | 42.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & { }_{\text {ID }} \end{aligned}$ | Input Vol. ped/h | Dem. Flow ped/h | Aver. Delay | Level of AVERAGE BACK OF Service QUEUE |  |  | Prop. EffectiveQueStop <br> Rate |  | Travel Time | Travel Aver. Dist. Speed m m/sec |  |
| South: Mamre Rd |  |  |  |  |  |  |  |  |  |  |  |
| P1 Full | 50 | 53 | 50.5 | LOS E | 0.2 | 0.2 | 0.92 | 0.92 | 222.5 | 223.5 | 1.00 |
| East: Mirvac Access |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 50 | 53 | 22.9 | LOS C | 0.1 | 0.1 | 0.62 | 0.62 | 189.8 | 217.0 | 1.14 |
| All <br> Pedestrians | 100 | 105 | 36.7 | LOS D | 0.2 | 0.2 | 0.77 | 0.77 | 206.1 | 220.3 | 1.07 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

## SITE LAYOUT

目 Site: 4 [[ID: 4] Abbotts Road / Mamre Road - AM (Site Folder:
2026 - AM 60\% GFA)]
Abbotts Road / Mamre Road
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Coordinated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


## MOVEMENT SUMMARY

目 Site: 4 [IID: 4] Abbotts Road / Mamre Road - AM (Site Folder:
2026 - AM 60\% GFA)]
Abbotts Road / Mamre Road
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Coordinated Cycle Time $=120$ seconds (Site User-Given Phase Times)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | INPUT VOLUMES [Total HV ] veh/h veh/h |  | DEMAND FLOWS |  | Deg. Satn $\qquad$ v/c | Aver. Delay <br> sec | Level of Service | 95\% BACK OF QUEUE <br> [ Veh. Dist] <br> veh m |  | Prop. <br> Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| South: Mamre Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 1067 | 131 | 1123 | 12.3 | 0.387 | 1.7 | LOS A | 1.0 | 8.4 | 0.03 | 0.03 | 0.03 | 79.6 |
| 3 R2 | 88 | 35 | 93 | 39.8 | * 0.323 | 46.1 | LOS D | 2.1 | 21.9 | 0.95 | 0.75 | 0.95 | 35.1 |
| Approach | 1155 | 166 | 1216 | 14.4 | 0.387 | 5.1 | LOS A | 2.1 | 21.9 | 0.10 | 0.09 | 0.10 | 74.4 |
| East: Abbotts Road (400m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 20 | 5 | 21 | 25.0 | 0.034 | 38.7 | LOS C | 0.6 | 5.7 | 0.73 | 0.66 | 0.73 | 34.9 |
| 6 R2 | 41 | 19 | 43 | 46.3 | * 0.179 | 62.7 | LOS E | 1.2 | 14.0 | 0.94 | 0.72 | 0.94 | 30.5 |
| Approach | 61 | 24 | 64 | 39.3 | 0.179 | 54.9 | LOS D | 1.2 | 14.0 | 0.87 | 0.70 | 0.87 | 31.5 |
| North: Mamre Road ( 800 m ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $7 \quad$ L2 | 105 | 17 | 111 | 16.2 | 0.112 | 16.8 | LOS B | 2.5 | 21.6 | 0.42 | 0.70 | 0.42 | 55.5 |
| 8 T1 | 997 | 146 | 1049 | 14.6 | * 0.338 | 5.6 | LOSA | 4.4 | 37.1 | 0.23 | 0.21 | 0.23 | 73.5 |
| Approach | 1102 | 163 | 1160 | 14.8 | 0.338 | 6.7 | LOS A | 4.4 | 37.1 | 0.25 | 0.25 | 0.25 | 71.4 |
| All <br> Vehicles | 2318 | 353 | 2440 | 15.2 | 0.387 | 7.2 | LOS A | 4.4 | 37.1 | 0.19 | 0.18 | 0.19 | 70.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }_{\text {ID }}^{\text {Mov }} \text { Crossing }$ | Input Vol. ped/h | Dem. Flow ped/h | Aver. Delay sec | Level of Service | $\begin{gathered} \text { VERAG } \\ \text { Qu } \\ \text { [ Ped } \\ \text { ped } \end{gathered}$ |  | Prop. Que | fective Stop <br> Rate | Travel Time | Travel Dist. <br> m | Aver. Speed <br> $\mathrm{m} / \mathrm{sec}$ |
| South: Mamre Road (500m) |  |  |  |  |  |  |  |  |  |  |  |
| P1 Full | 10 | 11 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 234.8 | 234.8 | 1.00 |
| East: Abbotts Road (400m) |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 10 | 11 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 221.3 | 217.2 | 0.98 |
| P2B Slip/ Bypass | 10 | 11 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 215.3 | 209.4 | 0.97 |
| North: Mamre Road (800m) |  |  |  |  |  |  |  |  |  |  |  |
| P3BSlip/ <br> Bypass | 10 | 11 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 212.0 | 205.2 | 0.97 |
| All Pedestrians | 40 | 42 | 54.2 | LOSE | 0.0 | 0.0 | 0.95 | 0.95 | 220.8 | 216.7 | 0.98 |

[^0]Pedestrian movement LOS values are based on average delay per pedestrian movement.

## MOVEMENT SUMMARY

目 Site: 4 [[ID: 4] Abbotts Road / Mamre Road - PM (Site Folder:
2026 - PM 60\% GFA)]
Abbotts Road / Mamre Road
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Coordinated Cycle Time $=120$ seconds (Site User-Given Phase Times)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | UT MES HV] veh/h |  | AND WS HV ] \% | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% <br> [ Veh. <br> veh | CK OF UE Dist] | Prop. Que | Effective Stop Rate | Aver. No Cycles | Aver. Speed km/h |
| South: Mamre Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 1137 | 122 | 1197 | 10.7 | 0.409 | 2.2 | LOSA | 1.2 | 9.3 | 0.04 | 0.03 | 0.04 | 79.5 |
| 3 R2 | 281 | 35 | 296 | 12.5 | * 0.626 | 61.2 | LOS E | 8.4 | 70.0 | 0.99 | 0.82 | 1.00 | 30.6 |
| Approach | 1418 | 157 | 1493 | 11.1 | 0.626 | 13.9 | LOS A | 8.4 | 70.0 | 0.22 | 0.19 | 0.23 | 64.3 |
| East: Abbotts Road (400m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 69 | 14 | 73 | 20.3 | 0.110 | 42.8 | LOS D | 2.1 | 18.7 | 0.75 | 0.71 | 0.75 | 35.1 |
| 6 R2 | 82 | 12 | 86 | 14.6 | * 0.280 | 63.7 | LOS E | 2.4 | 20.7 | 0.96 | 0.74 | 0.96 | 33.4 |
| Approach | 151 | 26 | 159 | 17.2 | 0.280 | 54.1 | LOS D | 2.4 | 20.7 | 0.87 | 0.73 | 0.87 | 34.1 |
| North: Mamre Road (800m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 22 | 17 | 23 | 77.3 | 0.041 | 17.5 | LOS B | 0.5 | 7.5 | 0.39 | 0.66 | 0.39 | 53.3 |
| 8 T1 | 1799 | 234 | 1894 | 13.0 | * 0.595 | 8.0 | LOSA | 11.5 | 94.0 | 0.34 | 0.31 | 0.34 | 71.9 |
| Approach | 1821 | 251 | 1917 | 13.8 | 0.595 | 8.1 | LOS A | 11.5 | 94.0 | 0.34 | 0.31 | 0.34 | 71.7 |
| All <br> Vehicles | 3390 | 434 | 3568 | 12.8 | 0.626 | 12.6 | LOS A | 11.5 | 94.0 | 0.31 | 0.28 | 0.32 | 65.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov <br> ID Crossing | Input Vol. <br> ped/h | Dem. Flow ped/h | Aver. Delay sec | Level of Service | $\begin{gathered} \text { VERAC } \\ \text { Q } \\ \text { [ Ped } \\ \text { ped } \end{gathered}$ | $\square$ | Prop. Que | Effective Stop Rate | Travel Time sec | Travel Dist. <br> m | Aver. Speed $\mathrm{m} / \mathrm{sec}$ |
| South: Mamre Road ( 500 m ) |  |  |  |  |  |  |  |  |  |  |  |
| P1 Full | 10 | 11 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 234.8 | 234.8 | 1.00 |
| East: Abbotts Road (400m) |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 10 | 11 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 221.3 | 217.2 | 0.98 |
| P2BSlip/ Bypass | 10 | 11 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 215.3 | 209.4 | 0.97 |
| North: Mamre Road (800m) |  |  |  |  |  |  |  |  |  |  |  |
| P3BSlip/ Bypass | 10 | 11 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 212.0 | 205.2 | 0.97 |
| All <br> Pedestrians | 40 | 42 | 54.2 | LOSE | 0.0 | 0.0 | 0.95 | 0.95 | 220.8 | 216.7 | 0.98 |

[^1]Pedestrian movement LOS values are based on average delay per pedestrian movement.

## SITE LAYOUT

$\nabla$ Site: 3 [[ID: [3] (AM) Mamre Rd x Altis Access - AM (Site
Folder: 2026 - AM 60\% GFA)]
Mamre Road x Altis Access
Site Category: (None)
Give-Way (Two-Way)

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings


## MOVEMENT SUMMARY

$\nabla$ Site: 3 [ [ID: [3] (AM) Mamre Rd x Altis Access - AM (Site
Folder: 2026 - AM 60\% GFA)]
Mamre Road x Altis Access
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | JT MES HV ] veh/h | $\begin{aligned} & \text { DEM } \\ & \text { FLO } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. <br> Satn <br> v/c | Aver. Delay <br> sec | Level of Service |  | CK OF <br> UE Dist ] m | Prop. Que | Effective Stop Rate |  | Aver. Speed <br> km/h |
| South: Mamre Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 1098 | 149 | 1156 | 13.6 | 0.664 | 0.4 | LOS A | 0.0 | 0.0 | 0.00 | 0.01 | 0.00 | 78.0 |
| Approach | 1098 | 149 | 1156 | 13.6 | 0.664 | 0.4 | NA | 0.0 | 0.0 | 0.00 | 0.01 | 0.00 | 78.0 |
| East: Altis |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 106 | 44 | 112 | 41.5 | 0.085 | 10.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.51 | 0.00 | 53.2 |
| Approach | 106 | 44 | 112 | 41.5 | 0.085 | 10.7 | NA | 0.0 | 0.0 | 0.00 | 0.51 | 0.00 | 53.2 |
| North: Mamre Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 110 | 15 | 116 | 13.6 | 0.071 | 7.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.63 | 0.00 | 60.2 |
| 8 T1 | 988 | 119 | 1040 | 12.0 | 0.592 | 0.3 | LOSA | 0.0 | 0.0 | 0.00 | 0.01 | 0.00 | 78.3 |
| Approach | 1098 | 134 | 1156 | 12.2 | 0.592 | 1.0 | NA | 0.0 | 0.0 | 0.00 | 0.07 | 0.00 | 76.0 |
| All <br> Vehicles | 2302 | 327 | 2423 | 14.2 | 0.664 | 1.1 | NA | 0.0 | 0.0 | 0.00 | 0.06 | 0.00 | 75.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## SIDRA INTERSECTION 9.0 | Copyright © 2000-2020 Akcelik and Associates Pty Ltd | sidrasolutions.com

Organisation: ASON GROUP PTY LTD | Licence: NETWORK / 1PC | Processed: Wednesday, 15 June 2022 1:03:26 PM
Project: C:IUsers\Arun Mohan\Desktop\Ason GrouplP1815-2026 MRP revised modelling\SIDRA Files\From SharepointlP1815 2026 SIDRA
Models Option 0 (1) (2).sip9

## MOVEMENT SUMMARY

$\nabla$ Site: 101 [[ID: 3] Mamre Rd x Altis Access - PM (Site Folder:
2026 - PM 60\% GFA)]
Mamre Road x Altis Road
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{array}{r} \text { INP } \\ \text { VOLU } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ | DEMAND FLOWS |  | Deg. Satn v/c | Aver. Delay sec | Level of Service | $\begin{gathered} 95 \% \text { E } \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \mathrm{m} \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed |
| South: Mamre Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 1225 | 10.9 | 1289 | 10.9 | 0.726 | 0.5 | LOS A | 0.0 | 0.0 | 0.00 | 0.01 | 0.00 | 77.9 |
| Approach | 1225 | 10.9 | 1289 | 10.9 | 0.726 | 0.5 | NA | 0.0 | 0.0 | 0.00 | 0.01 | 0.00 | 77.9 |
| East: Altis |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 279 | 16.0 | 294 | 16.0 | 0.182 | 13.3 | LOS A | 0.0 | 0.0 | 0.00 | 0.52 | 0.00 | 54.2 |
| Approach | 279 | 16.0 | 294 | 16.0 | 0.182 | 13.3 | NA | 0.0 | 0.0 | 0.00 | 0.52 | 0.00 | 54.2 |
| North: Mamre Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 26 | 50.0 | 27 | 50.0 | 0.021 | 7.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.62 | 0.00 | 50.6 |
| 8 T1 | 1457 | 13.1 | 1534 | 13.1 | 0.878 | 1.6 | LOSA | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 75.5 |
| Approach | 1483 | 13.8 | 1561 | 13.8 | 0.878 | 1.7 | NA | 0.0 | 0.0 | 0.00 | 0.01 | 0.00 | 74.8 |
| All <br> Vehicles | 2987 | 12.8 | 3144 | 12.8 | 0.878 | 2.3 | NA | 0.0 | 0.0 | 0.00 | 0.06 | 0.00 | 73.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Project: C:IUsers\Arun Mohan\Desktop\Ason GrouplP1815-2026 MRP revised modellingISIDRA Files\From SharepointlP1815 2026 SIDRA
Models Option 0 (1) (2).sip9

## SITE LAYOUT

目 Site: 5 [IID: 5] Aldington Road /Bakers Lane / Fife Kemps
Creek (North) - PM (Site Folder: 2026 - PM 60\% GFA)]
Aldington Road /Bakers Lane / Fife Kemps Creek (North)
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.
$Q^{2}$


## MOVEMENT SUMMARY

## 目 Site: 5 [[ID: 5] Aldington Road /Bakers Lane / Fife Kemps <br> Creek (North) - AM (Site Folder: 2026 - AM 60\% GFA)]

Aldington Road /Bakers Lane / Fife Kemps Creek (North)
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=120$ seconds (Site User-Given Cycle Time)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  |  |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay sec | Level of Service |  | CK OF UE Dist ] | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| South: Aldington Road (670m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 7 | 6 | 7 | 85.7 | 0.022 | 27.1 | LOS B | 0.2 | 4.6 | 0.58 | 0.65 | 0.58 | 39.9 |
| 2 T1 | 33 | 0 | 35 | 0.0 | 0.060 | 32.5 | LOS C | 1.4 | 10.1 | 0.75 | 0.56 | 0.75 | 45.3 |
| 3 R2 | 2 | 1 | 2 | 50.0 | 0.015 | 57.6 | LOS E | 0.1 | 1.1 | 0.91 | 0.63 | 0.91 | 31.3 |
| Approach | 42 | 7 | 44 | 16.7 | 0.060 | 32.8 | LOS C | 1.4 | 10.1 | 0.73 | 0.58 | 0.73 | 43.8 |
| East: New Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 1 | 0 | 1 | 0.0 | 0.127 | 37.9 | LOS C | 3.0 | 20.8 | 0.77 | 0.72 | 0.77 | 36.5 |
| 5 T1 | 1 | 0 | 1 | 0.0 | 0.127 | 33.4 | LOS C | 3.0 | 20.8 | 0.77 | 0.72 | 0.77 | 33.0 |
| 6 R2 | 64 | 0 | 67 | 0.0 | 0.127 | 37.9 | LOS C | 3.0 | 20.8 | 0.77 | 0.72 | 0.77 | 39.8 |
| Approach | 66 | 0 | 69 | 0.0 | 0.127 | 37.9 | LOS C | 3.0 | 20.8 | 0.77 | 0.72 | 0.77 | 39.7 |
| North: Aldington Road (980m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $7 \quad$ L2 | 259 | 0 | 273 | 0.0 | * 0.249 | 12.1 | LOS A | 4.0 | 28.3 | 0.52 | 0.72 | 0.52 | 49.6 |
| 8 T1 | 1 | 0 | 1 | 0.0 | 0.002 | 31.4 | LOS C | 0.0 | 0.3 | 0.72 | 0.44 | 0.72 | 45.6 |
| 9 R2 | 31 | 0 | 33 | 0.0 | 0.149 | 57.8 | LOS E | 1.8 | 12.3 | 0.93 | 0.72 | 0.93 | 34.8 |
| Approach | 291 | 0 | 306 | 0.0 | 0.249 | 17.1 | LOS B | 4.0 | 28.3 | 0.56 | 0.72 | 0.56 | 47.4 |
| West: New Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 12 | 3 | 13 | 25.0 | * 0.194 | 33.4 | LOS C | 0.8 | 11.4 | 0.93 | 0.71 | 0.93 | 40.7 |
| 11 T1 | 1 | 0 | 1 | 0.0 | * 0.194 | 28.5 | LOS C | 0.8 | 11.4 | 0.93 | 0.71 | 0.93 | 34.6 |
| 12 R 2 | 11 | 9 | 12 | 81.8 | 0.194 | 34.0 | LOS C | 0.8 | 11.4 | 0.93 | 0.71 | 0.93 | 36.5 |
| Approach | 24 | 12 | 25 | 50.0 | 0.194 | 33.5 | LOS C | 0.8 | 11.4 | 0.93 | 0.71 | 0.93 | 38.7 |
| All <br> Vehicles | 423 | 19 | 445 | 4.5 | 0.249 | 22.8 | LOS B | 4.0 | 28.3 | 0.63 | 0.70 | 0.63 | 45.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID Crossing | Input Vol. ped/h | Dem. Flow ped/h | Aver. Delay $\qquad$ sec | Level of AVERAGE BACK OF Service QUEUE |  |  | Prop. Effective Que Stop Rate |  | Travel Time sec | Travel Dist. $\qquad$ m | Aver. Speed <br> $\mathrm{m} / \mathrm{sec}$ |
| South: Aldington Road (670m) |  |  |  |  |  |  |  |  |  |  |  |
| P1 Full | 50 | 53 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 224.7 | 221.5 | 0.99 |
| East: New Road (500m) |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 50 | 53 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 216.6 | 211.0 | 0.97 |
| All | 0 | 105 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 220.6 | 216.3 | 0.98 |

## MOVEMENT SUMMARY

## 目 Site: 5 [[ID: 5] Aldington Road /Bakers Lane / Fife Kemps <br> Creek (North) - PM (Site Folder: 2026 - PM 60\% GFA)]

Aldington Road /Bakers Lane / Fife Kemps Creek (North)
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=120$ seconds (Site User-Given Cycle Time)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | UT MES HV] veh/h |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. <br> Satn <br> v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver Speed km/h |
| South: Aldington Road (670m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 23 | 6 | 24 | 26.1 | 0.056 | 38.6 | LOS C | 1.0 | 9.2 | 0.75 | 0.70 | 0.75 | 36.5 |
| 2 T1 | 32 | 0 | 34 | 0.0 | 0.103 | 45.8 | LOS D | 1.7 | 11.8 | 0.88 | 0.65 | 0.88 | 41.1 |
| 3 R2 | 3 | 0 | 3 | 0.0 | 0.016 | 57.2 | LOS E | 0.2 | 1.2 | 0.91 | 0.63 | 0.91 | 31.5 |
| Approach | 58 | 6 | 61 | 10.3 | 0.103 | 43.5 | LOS D | 1.7 | 11.8 | 0.83 | 0.67 | 0.83 | 39.0 |
| East: New Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 4 | 3 | 4 | 75.0 | 0.149 | 25.9 | LOS B | 4.1 | 29.8 | 0.62 | 0.70 | 0.62 | 39.1 |
| 5 T1 | 1 | 0 | 1 | 0.0 | * 0.149 | 20.6 | LOS B | 4.1 | 29.8 | 0.62 | 0.70 | 0.62 | 37.2 |
| 6 R2 | 110 | 0 | 116 | 0.0 | 0.149 | 25.1 | LOS B | 4.1 | 29.8 | 0.62 | 0.70 | 0.62 | 43.9 |
| Approach | 115 | 3 | 121 | 2.6 | 0.149 | 25.1 | LOS B | 4.1 | 29.8 | 0.62 | 0.70 | 0.62 | 43.7 |
| North: Aldington Road (980m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $7 \quad$ L2 | 34 | 0 | 36 | 0.0 | 0.031 | 10.4 | LOS A | 0.4 | 3.1 | 0.41 | 0.65 | 0.41 | 50.4 |
| 8 T1 | 43 | 2 | 45 | 4.7 | * 0.144 | 46.3 | LOS D | 2.3 | 16.6 | 0.89 | 0.67 | 0.89 | 41.0 |
| 9 R2 | 4 | 0 | 4 | 0.0 | 0.021 | 57.3 | LOS E | 0.2 | 1.6 | 0.92 | 0.64 | 0.92 | 34.9 |
| Approach | 81 | 2 | 85 | 2.5 | 0.144 | 31.8 | LOS C | 2.3 | 16.6 | 0.69 | 0.66 | 0.69 | 43.9 |
| West: New Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 12 | 0 | 13 | 0.0 | * 0.123 | 35.8 | LOS C | 0.9 | 6.1 | 0.94 | 0.70 | 0.94 | 40.4 |
| 11 T1 | 1 | 0 | 1 | 0.0 | * 0.123 | 31.2 | LOS C | 0.9 | 6.1 | 0.94 | 0.70 | 0.94 | 33.7 |
| 12 R2 | 9 | 0 | 9 | 0.0 | 0.123 | 35.7 | LOS C | 0.9 | 6.1 | 0.94 | 0.70 | 0.94 | 37.4 |
| Approach | 22 | 0 | 23 | 0.0 | 0.123 | 35.6 | LOS C | 0.9 | 6.1 | 0.94 | 0.70 | 0.94 | 39.0 |
| All <br> Vehicles | 276 | 11 | 291 | 4.0 | 0.149 | 31.8 | LOS C | 4.1 | 29.8 | 0.71 | 0.68 | 0.71 | 42.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID Crossing | Input Vol. ped/h | Dem. <br> Flow <br> ped/h | Aver. Delay <br> sec | Level of AVERAGE BACK OF Service QUEUE |  |  | Prop. Effective Que Stop Rate |  | Travel Time <br> sec | Travel Dist. $\qquad$ | Aver. <br> Speed <br> $\mathrm{m} / \mathrm{sec}$ |
| South: Aldington Road (670m) |  |  |  |  |  |  |  |  |  |  |  |
| P1 Full | 50 | 53 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 224.7 | 221.5 | 0.99 |
| East: New Road (500m) |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 50 | 53 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 216.6 | 211.0 | 0.97 |
| All | 0 | 105 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 220.6 | 216.3 | 0.98 |

## SITE LAYOUT

目 Site: 6 [[ID: 6] Aldington Road /Bakers Lane / Fife Kemps
Creek (South) - AM (Site Folder: 2026 - AM 60\% GFA)]
Aldington Road /Bakers Lane / Fife Kemps Creek (South)
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


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Models Option 0 (1) (2).sip9

## MOVEMENT SUMMARY

## Site: 6 [[ID: 6] Aldington Road /Bakers Lane / Fife Kemps

Creek (South) - AM (Site Folder: 2026 - AM 60\% GFA)]
Aldington Road /Bakers Lane / Fife Kemps Creek (South)
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=120$ seconds (Site User-Given Cycle Time)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  |  |  | $\begin{aligned} & \text { AND } \\ & \text { WS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% <br> [ Veh. veh | CK OF UE Dist ] | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Aldington Road (580m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 35 | 17 | 37 | 48.6 | 0.101 | 36.7 | LOS C | 1.5 | 17.1 | 0.73 | 0.72 | 0.73 | 36.9 |
| 2 T1 | 5 | 3 | 5 | 60.0 | * 0.039 | 49.5 | LOS D | 0.3 | 4.2 | 0.89 | 0.60 | 0.89 | 36.4 |
| 3 R 2 | 32 | 11 | 34 | 34.4 | 0.064 | 30.9 | LOS C | 1.2 | 11.2 | 0.66 | 0.69 | 0.66 | 37.9 |
| Approach | 72 | 31 | 76 | 43.1 | 0.101 | 35.0 | LOS C | 1.5 | 17.1 | 0.71 | 0.70 | 0.71 | 37.2 |
| East: New Road (450m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 7 | 0 | 7 | 0.0 | 0.334 | 56.2 | LOS D | 2.8 | 38.8 | 0.94 | 0.73 | 0.94 | 30.6 |
| $5 \quad \mathrm{~T} 1$ | 85 | 61 | 89 | 71.8 | * 0.334 | 52.2 | LOS D | 2.8 | 38.8 | 0.94 | 0.73 | 0.94 | 29.8 |
| 6 R2 | 33 | 0 | 35 | 0.0 | 0.131 | 53.6 | LOS D | 1.8 | 12.6 | 0.91 | 0.72 | 0.91 | 31.8 |
| Approach | 125 | 61 | 132 | 48.8 | 0.334 | 52.8 | LOS D | 2.8 | 38.8 | 0.93 | 0.73 | 0.93 | 30.4 |
| North: Aldington Road (670m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 1 | 0 | 1 | 0.0 | 0.017 | 34.2 | LOS C | 0.1 | 1.4 | 0.86 | 0.59 | 0.86 | 38.3 |
| 8 T1 | 4 | 3 | 4 | 75.0 | 0.020 | 40.5 | LOS C | 0.1 | 2.2 | 0.87 | 0.58 | 0.87 | 38.6 |
| 9 R2 | 7 | 6 | 7 | 85.7 | 0.027 | 31.8 | LOS C | 0.3 | 5.1 | 0.64 | 0.65 | 0.64 | 39.5 |
| Approach | 12 | 9 | 13 | 75.0 | 0.027 | 34.9 | LOS C | 0.3 | 5.1 | 0.74 | 0.62 | 0.74 | 39.1 |
| West: New Road (620m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 7 | 6 | 7 | 85.7 | * 0.258 | 37.7 | LOS C | 1.2 | 20.6 | 0.92 | 0.70 | 0.92 | 36.5 |
| 11 T1 | 51 | 50 | 54 | 98.0 | * 0.258 | 44.0 | LOS D | 1.7 | 26.5 | 0.93 | 0.71 | 0.93 | 31.7 |
| 12 R 2 | 2 | 1 | 2 | 50.0 | 0.013 | 54.2 | LOS D | 0.1 | 1.1 | 0.89 | 0.62 | 0.89 | 31.7 |
| Approach | 60 | 57 | 63 | 95.0 | 0.258 | 43.6 | LOS D | 1.7 | 26.5 | 0.93 | 0.70 | 0.93 | 32.3 |
| All <br> Vehicles | 269 | 158 | 283 | 58.7 | 0.334 | 45.2 | LOS D | 2.8 | 38.8 | 0.86 | 0.71 | 0.86 | 32.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID Crossing | Input Vol. ped/h | Dem. Flow ped/h | Aver. Delay | Level of Service |  | $\begin{aligned} & \text { ACK OF } \\ & \text { E } \\ & \text { Dist ] } \\ & \mathrm{m} \end{aligned}$ | Prop. Que | fective <br> Stop <br> Rate | Travel Time sec | Travel Dist. m | Aver. Speed |
| South: Aldington Road (580m) |  |  |  |  |  |  |  |  |  |  |  |
| P1 Full | 50 | 53 | 26.2 | LOS C | 0.1 | 0.1 | 0.90 | 0.90 | 195.8 | 220.5 | 1.13 |
| East: New Road (450m) |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 50 | 53 | 54.3 | LOSE | 0.2 | 0.2 | 0.95 | 0.95 | 225.0 | 222.0 | 0.99 |
| North: Aldington Road (670m) |  |  |  |  |  |  |  |  |  |  |  |


| P3 Full | 50 | 53 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 223.9 | 220.5 | 0.98 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| West: New Road $(620 \mathrm{~m})$ |  |  |  |  |  |  |  |  |  |  |  |
| P4 Full | 50 | 53 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 224.7 | 221.5 | 0.99 |
| All | 0 | 211 | 47.3 | LOS E | 0.2 | 0.2 | 0.94 | 0.94 | 217.4 | 221.1 | 1.02 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## MOVEMENT SUMMARY

## Site: 6 [[ID: 6] Aldington Road /Bakers Lane / Fife Kemps

Creek (South) - PM (Site Folder: 2026 - PM 60\% GFA)]
Aldington Road /Bakers Lane / Fife Kemps Creek (South)
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=120$ seconds (Site User-Given Cycle Time)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{array}{r} \text { IN } \\ \text { VOL } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | JT MES HV] veh/h |  | $\begin{aligned} & \text { AND } \\ & \text { WS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay $\qquad$ <br> sec | Level of Service |  | $\begin{aligned} & \text { CK OF } \\ & \text { UE } \\ & \text { Dist ] } \\ & \mathrm{m} \\ & \hline \end{aligned}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> $\mathrm{km} / \mathrm{h}$ |
| South: Aldington Road (580m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 116 | 16 | 122 | 13.8 | 0.245 | 37.7 | LOS C | 5.2 | 44.8 | 0.77 | 0.76 | 0.77 | 36.8 |
| 2 T1 | 22 | 2 | 23 | 9.1 | * 0.091 | 48.7 | LOS D | 1.2 | 9.0 | 0.90 | 0.65 | 0.90 | 36.6 |
| 3 R2 | 113 | 12 | 119 | 10.6 | * 0.301 | 46.1 | LOS D | 5.7 | 45.7 | 0.86 | 0.77 | 0.86 | 33.0 |
| Approach | 251 | 30 | 264 | 12.0 | 0.301 | 42.4 | LOS C | 5.7 | 45.7 | 0.82 | 0.76 | 0.82 | 35.1 |
| East: New Road (450m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 12 | 5 | 13 | 41.7 | 0.298 | 40.8 | LOS C | 5.4 | 55.2 | 0.82 | 0.68 | 0.82 | 34.6 |
| 5 T1 | 216 | 65 | 227 | 30.1 | * 0.298 | 36.2 | LOS C | 5.6 | 55.2 | 0.82 | 0.68 | 0.82 | 34.2 |
| 6 R2 | 28 | 0 | 29 | 0.0 | 0.055 | 37.8 | LOS C | 1.2 | 8.7 | 0.76 | 0.69 | 0.76 | 36.3 |
| Approach | 256 | 70 | 269 | 27.3 | 0.298 | 36.6 | LOS C | 5.6 | 55.2 | 0.82 | 0.68 | 0.82 | 34.4 |
| North: Aldington Road (670m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $7 \quad$ L2 | 3 | 2 | 3 | 66.7 | 0.024 | 32.7 | LOS C | 0.2 | 1.9 | 0.84 | 0.62 | 0.84 | 39.2 |
| 8 T1 | 8 | 1 | 8 | 12.5 | 0.029 | 42.6 | LOS D | 0.3 | 2.9 | 0.88 | 0.60 | 0.88 | 38.3 |
| 9 R2 | 41 | 1 | 43 | 2.4 | 0.098 | 43.5 | LOS D | 2.0 | 14.0 | 0.81 | 0.72 | 0.81 | 36.4 |
| Approach | 52 | 4 | 55 | 7.7 | 0.098 | 42.7 | LOS D | 2.0 | 14.0 | 0.82 | 0.70 | 0.82 | 36.8 |
| West: New Road (620m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 9 | 5 | 9 | 55.6 | 0.126 | 31.3 | LOS C | 0.6 | 7.4 | 0.89 | 0.67 | 0.89 | 38.8 |
| 11 T1 | 27 | 26 | 28 | 96.3 | * 0.126 | 41.3 | LOS C | 0.9 | 11.7 | 0.90 | 0.67 | 0.90 | 32.3 |
| 12 R 2 | 1 | 0 | 1 | 0.0 | 0.004 | 52.6 | LOS D | 0.1 | 0.4 | 0.88 | 0.59 | 0.88 | 32.6 |
| Approach | 37 | 31 | 39 | 83.8 | 0.126 | 39.2 | LOS C | 0.9 | 11.7 | 0.90 | 0.66 | 0.90 | 33.9 |
| All <br> Vehicles | 596 | 135 | 627 | 22.7 | 0.301 | 39.7 | LOS C | 5.7 | 55.2 | 0.83 | 0.71 | 0.83 | 34.9 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID Crossing | Input Vol. ped/h | Dem. Flow ped/h | Aver. Delay | Level of Service |  | $\begin{aligned} & \text { ACK OF } \\ & \text { E } \\ & \text { Dist ] } \\ & \mathrm{m} \end{aligned}$ | Prop. Que | fective <br> Stop <br> Rate | Travel Time sec | Travel Dist. m | Aver. Speed |
| South: Aldington Road (580m) |  |  |  |  |  |  |  |  |  |  |  |
| P1 Full | 50 | 53 | 24.4 | LOS C | 0.1 | 0.1 | 0.90 | 0.90 | 194.0 | 220.5 | 1.14 |
| East: New Road (450m) |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 50 | 53 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 225.0 | 222.0 | 0.99 |
| North: Aldington Road (670m) |  |  |  |  |  |  |  |  |  |  |  |


| P3 Full | 50 | 53 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 223.9 | 220.5 | 0.98 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| West: New Road $(620 \mathrm{~m})$ |  |  |  |  |  |  |  |  |  |  |  |
| P4 Full | 50 | 53 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 224.7 | 221.5 | 0.99 |
| All | 0 | 211 | 46.8 | LOS E | 0.2 | 0.2 | 0.94 | 0.94 | 216.9 | 221.1 | 1.02 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## SITE LAYOUT

## 目 Site: 7 [[ID: 7] Aldington Road / Abbotts Road - AM (Site

Folder: 2026 - AM 60\% GFA)]
Aldington Road / Abbotts Road
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


New Road (130m)

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Models Option 0 (1) (2).sip9

## MOVEMENT SUMMARY

## 目 Site: 7 [[ID: 7] Aldington Road / Abbotts Road - AM (Site

Folder: 2026 - AM 60\% GFA)]

## Aldington Road / Abbotts Road

Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=120$ seconds (Site User-Given Phase Times)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | MES HV ] veh/h |  | $\begin{aligned} & \text { AND } \\ & \text { WS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. <br> Satn <br> v/c | Aver. Delay <br> sec | Level of Service |  | CK OF UE Dist] m | Prop. Que | Effective Stop Rate |  | Aver. Speed <br> km/h |
| East: New Road (130m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 T1 | 51 | 21 | 54 | 41.2 | 0.039 | 11.8 | LOS A | 0.7 | 7.2 | 0.42 | 0.32 | 0.42 | 42.6 |
| 6 R2 | 1 | 0 | 1 | 0.0 | * 0.039 | 30.6 | LOS C | 0.7 | 7.2 | 0.67 | 0.50 | 0.67 | 33.9 |
| Approach | 52 | 21 | 55 | 40.4 | 0.039 | 12.2 | LOS A | 0.7 | 7.2 | 0.43 | 0.33 | 0.43 | 42.4 |
| North: Aldington Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 1 | 0 | 1 | 0.0 | 0.028 | 48.3 | LOS D | 0.3 | 3.4 | 0.84 | 0.67 | 0.84 | 26.0 |
| 9 R2 | 11 | 4 | 12 | 36.4 | * 0.028 | 49.3 | LOS D | 0.3 | 3.4 | 0.84 | 0.67 | 0.84 | 30.4 |
| Approach | 12 | 4 | 13 | 33.3 | 0.028 | 49.3 | LOS D | 0.3 | 3.4 | 0.84 | 0.67 | 0.84 | 30.1 |
| West: Abbotts Road (400m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 71 | 30 | 75 | 42.3 | 0.101 | 16.0 | LOS B | 1.8 | 18.6 | 0.43 | 0.67 | 0.43 | 44.1 |
| 11 T1 | 122 | 22 | 128 | 18.0 | * 0.132 | 11.3 | LOSA | 3.1 | 27.0 | 0.44 | 0.48 | 0.44 | 43.1 |
| Approach | 193 | 52 | 203 | 26.9 | 0.132 | 13.0 | LOS A | 3.1 | 27.0 | 0.44 | 0.55 | 0.44 | 43.6 |
| All <br> Vehicles | 257 | 77 | 271 | 30.0 | 0.132 | 14.6 | LOS B | 3.1 | 27.0 | 0.45 | 0.51 | 0.45 | 42.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & { }_{\text {ID }} \end{aligned}$ | Input Vol. <br> ped/h | Dem. Flow ped/h | Aver. Delay sec | Level of AVERAGE BACK OF Service QUEUE |  |  | Prop. Effective Que $\begin{aligned} & \text { Stop } \\ & \text { Rate }\end{aligned}$ |  | Travel Time | Travel Dist. | Aver. Speed <br> $\mathrm{m} / \mathrm{sec}$ |
| East: New Road (130m) |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 50 | 53 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 222.7 | 219.0 | 0.98 |
| All Pedestrians | 0 | 53 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 222.7 | 219.0 | 0.98 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## MOVEMENT SUMMARY

## 目 Site: 7 [[ID: 7] Aldington Road / Abbotts Road - PM (Site

Folder: 2026 - PM 60\% GFA)]

## Aldington Road / Abbotts Road

Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Phase Times)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | JT MES HV] veh/h |  | $\begin{gathered} \text { AND } \\ \text { WS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \mathrm{m} \end{gathered}$ | Prop. Que | Effective Stop Rate |  | Aver. Speed <br> km/h |
| East: New Road (130m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 T1 | 131 | 20 | 138 | 15.3 | 0.066 | 9.0 | LOS A | 1.6 | 13.2 | 0.39 | 0.32 | 0.39 | 45.7 |
| 6 R2 | 1 | 0 | 1 | 0.0 | * 0.066 | 18.8 | LOS B | 1.6 | 13.2 | 0.51 | 0.40 | 0.51 | 41.2 |
| Approach | 132 | 20 | 139 | 15.2 | 0.066 | 9.1 | LOS A | 1.6 | 13.2 | 0.40 | 0.32 | 0.40 | 45.6 |
| North: Aldington Road ( 500 m ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 1 | 0 | 1 | 0.0 | 0.053 | 48.8 | LOS D | 0.6 | 6.4 | 0.84 | 0.69 | 0.84 | 25.9 |
| 9 R2 | 21 | 6 | 22 | 28.6 | * 0.053 | 49.7 | LOS D | 0.6 | 6.4 | 0.85 | 0.69 | 0.85 | 30.4 |
| Approach | 22 | 6 | 23 | 27.3 | 0.053 | 49.7 | LOS D | 0.6 | 6.4 | 0.85 | 0.69 | 0.85 | 30.2 |
| West: Abbotts Road (400m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 248 | 29 | 261 | 11.7 | * 0.265 | 16.9 | LOS B | 6.9 | 56.4 | 0.49 | 0.72 | 0.49 | 44.5 |
| 11 T1 | 65 | 23 | 68 | 35.4 | 0.086 | 11.1 | LOS A | 1.6 | 17.2 | 0.43 | 0.45 | 0.43 | 43.4 |
| Approach | 313 | 52 | 329 | 16.6 | 0.265 | 15.7 | LOS B | 6.9 | 56.4 | 0.48 | 0.66 | 0.48 | 44.3 |
| All Vehicles | 467 | 78 | 492 | 16.7 | 0.265 | 15.4 | LOS B | 6.9 | 56.4 | 0.47 | 0.57 | 0.47 | 43.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline \multicolumn{12}{|l|}{Pedestrian Movement Performance} \\
\hline Mov ID Crossing \& \begin{tabular}{l}
Input Vol. \\
ped/h
\end{tabular} \& Dem. Flow ped/h \& Aver. Delay sec \& \multicolumn{3}{|l|}{Level of AVERAGE BACK OF Service QUEUE} \& \multicolumn{2}{|l|}{Prop. Effective
Que
Stop

Rate} \& Travel Time sec \& Travel Dist. m \& Aver. Speed <br>
\hline \multicolumn{12}{|l|}{East: New Road (130m)} <br>
\hline P2 Full \& 50 \& 53 \& 54.3 \& LOS E \& 0.2 \& 0.2 \& 0.95 \& 0.95 \& 222.7 \& 219.0 \& 0.98 <br>
\hline All Pedestrians \& 0 \& 53 \& 54.3 \& LOS E \& 0.2 \& 0.2 \& 0.95 \& 0.95 \& 222.7 \& 219.0 \& 0.98 <br>
\hline
\end{tabular}

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## SITE LAYOUT

S Site: 8 [[ID: 8] Internal Road Roundabout (Mirvac) - AM (Site
Folder: 2026 - AM 60\% GFA)]
Internal Road Roundabout (Mirvac)
Site Category: (None)
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


## MOVEMENT SUMMARY

$\nabla$ Site: 8 [[ID: 8] Internal Road Roundabout (Mirvac) - AM (Site
Folder: 2026 - AM 60\% GFA)]
Internal Road Roundabout (Mirvac)
Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | UT MES HV ] veh/h |  | $\begin{aligned} & \text { AND } \\ & \text { WS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay $\qquad$ | Level of Service | $\begin{aligned} & 95 \% \text { B/ } \\ & \text { QUt } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \mathrm{m} \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: New Road (620m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 81 | 36 | 85 | 44.4 | 0.078 | 2.7 | LOSA | 0.4 | 4.4 | 0.18 | 0.31 | 0.18 | 48.5 |
| 2 T 1 | 124 | 85 | 131 | 68.5 | 0.122 | 2.1 | LOS A | 0.7 | 9.8 | 0.19 | 0.22 | 0.19 | 50.2 |
| 3 u U | 1 | 0 | 1 | 0.0 | 0.122 | 9.7 | LOSA | 0.7 | 9.8 | 0.19 | 0.22 | 0.19 | 52.4 |
| Approach | 206 | 121 | 217 | 58.7 | 0.122 | 2.4 | LOS A | 0.7 | 9.8 | 0.18 | 0.26 | 0.18 | 49.5 |
| North: New Road (370m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 238 | 77 | 251 | 32.4 | 0.110 | 2.0 | LOSA | 0.6 | 6.3 | 0.20 | 0.25 | 0.20 | 50.1 |
| 9 R 2 | 26 | 13 | 27 | 50.0 | 0.110 | 8.3 | LOSA | 0.6 | 6.4 | 0.21 | 0.31 | 0.21 | 49.9 |
| 9 u U | 1 | 0 | 1 | 0.0 | 0.110 | 9.7 | LOSA | 0.6 | 6.4 | 0.21 | 0.31 | 0.21 | 53.1 |
| Approach | 265 | 90 | 279 | 34.0 | 0.110 | 2.6 | LOSA | 0.6 | 6.4 | 0.20 | 0.26 | 0.20 | 50.1 |
| West: New Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 24 | 10 | 25 | 41.7 | 0.029 | 3.9 | LOS A | 0.1 | 1.5 | 0.41 | 0.41 | 0.41 | 47.3 |
| 12 R 2 | 41 | 6 | 43 | 14.6 | 0.032 | 8.4 | LOSA | 0.2 | 1.5 | 0.36 | 0.55 | 0.36 | 47.4 |
| 12u U | 1 | 0 | 1 | 0.0 | 0.032 | 10.1 | LOSA | 0.2 | 1.5 | 0.36 | 0.55 | 0.36 | 48.8 |
| Approach | 66 | 16 | 69 | 24.2 | 0.032 | 6.8 | LOSA | 0.2 | 1.5 | 0.38 | 0.50 | 0.38 | 47.4 |
| All <br> Vehicles | 537 | 227 | 565 | 42.3 | 0.122 | 3.1 | LOS A | 0.7 | 9.8 | 0.21 | 0.29 | 0.21 | 49.5 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 8 [[ID: 8] Internal Road Roundabout Mirvac - PM (Site
Folder: 2026 - PM 60\% GFA)]

```
Internal Road Roundabout (Mirvac)
Site Category: (None)
Roundabout
```

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{array}{r} \text { INP } \\ \text { VOLU } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | UT MES HV] veh/h |  | $\begin{aligned} & \text { AND } \\ & \text { WS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay sec $\qquad$ | Level of Service | $\begin{aligned} & \text { 95\% BA } \\ & \text { QUE } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> $\mathrm{km} / \mathrm{h}$ |
| South: New Road (620m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 284 | 44 | 299 | 15.5 | 0.190 | 2.5 | LOS A | 1.1 | 9.2 | 0.20 | 0.33 | 0.20 | 48.6 |
| 2 T 1 | 253 | 74 | 266 | 29.2 | 0.221 | 2.1 | LOS A | 1.3 | 12.2 | 0.24 | 0.24 | 0.24 | 50.1 |
| 3 u U | 1 | 0 | 1 | 0.0 | 0.221 | 9.8 | LOSA | 1.3 | 12.2 | 0.24 | 0.24 | 0.24 | 52.3 |
| Approach | 538 | 118 | 566 | 21.9 | 0.221 | 2.4 | LOS A | 1.3 | 12.2 | 0.22 | 0.29 | 0.22 | 49.3 |
| North: New Road (370m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 82 | 58 | 86 | 70.7 | 0.057 | 1.9 | LOS A | 0.3 | 3.2 | 0.06 | 0.27 | 0.06 | 49.8 |
| 9 R2 | 54 | 8 | 57 | 14.8 | 0.057 | 7.6 | LOS A | 0.3 | 3.2 | 0.05 | 0.47 | 0.05 | 48.4 |
| 9 u U | 1 | 0 | 1 | 0.0 | 0.057 | 9.5 | LOSA | 0.3 | 3.2 | 0.05 | 0.47 | 0.05 | 50.4 |
| Approach | 137 | 66 | 144 | 48.2 | 0.057 | 4.2 | LOSA | 0.3 | 4.0 | 0.06 | 0.35 | 0.06 | 49.3 |
| West: New Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 67 | 11 | 71 | 16.4 | 0.058 | 3.6 | LOSA | 0.3 | 2.9 | 0.46 | 0.45 | 0.46 | 47.3 |
| 12 R 2 | 3 | 2 | 3 | 66.7 | 0.005 | 10.4 | LOSA | 0.0 | 0.3 | 0.49 | 0.55 | 0.49 | 46.2 |
| 12 u U | 1 | 0 | 1 | 0.0 | 0.005 | 11.0 | LOSA | 0.0 | 0.3 | 0.49 | 0.55 | 0.49 | 47.8 |
| Approach | 71 | 13 | 75 | 18.3 | 0.058 | 4.0 | LOS A | 0.3 | 2.9 | 0.46 | 0.45 | 0.46 | 47.3 |
| All <br> Vehicles | 746 | 197 | 785 | 26.4 | 0.221 | 2.9 | LOS A | 1.3 | 12.2 | 0.21 | 0.31 | 0.21 | 49.1 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## SITE LAYOUT

© Site: 9 [[ID: 9] Internal Road Roundabout (Altis)- AM (Site Folder: 2026 - AM 60\% GFA)]
Internal Road Roundabout (Altis)
Site Category: (None)
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


## MOVEMENT SUMMARY

$\nabla$ Site: 9 [[ID: 9] Internal Road Roundabout (Altis)- AM (Site
Folder: 2026 - AM 60\% GFA)]
Internal Road Roundabout (Altis)
Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { INF } \\ & \text { VOLI } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | JT MES HV ] veh/h |  | $\begin{aligned} & \text { AND } \\ & \text { WS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay sec $\qquad$ | Level of Service | $\begin{gathered} \text { 95\% B B } \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed $\mathrm{km} / \mathrm{h}$ |
| South: New Road (370m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 150 | 94 | 158 | 62.7 | 0.142 | 3.1 | LOS A | 0.4 | 6.2 | 0.16 | 0.35 | 0.16 | 47.9 |
| 2 T1 | 1 | 0 | 1 | 0.0 | 0.001 | 1.8 | LOSA | 0.0 | 0.0 | 0.13 | 0.20 | 0.13 | 50.5 |
| Approach | 151 | 94 | 159 | 62.3 | 0.142 | 3.1 | LOS A | 0.4 | 6.2 | 0.16 | 0.35 | 0.16 | 48.0 |
| North: New Road (1000m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 26 | 12 | 27 | 46.2 | 0.030 | 2.8 | LOSA | 0.1 | 1.0 | 0.29 | 0.31 | 0.29 | 49.9 |
| 9 R2 | 58 | 23 | 61 | 39.7 | 0.051 | 8.5 | LOSA | 0.2 | 1.7 | 0.27 | 0.57 | 0.27 | 48.1 |
| Approach | 84 | 35 | 88 | 41.7 | 0.051 | 6.7 | LOSA | 0.2 | 1.7 | 0.27 | 0.49 | 0.27 | 48.6 |
| West: New Road (600m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 1 | 0 | 1 | 0.0 | 0.188 | 2.1 | LOS A | 0.4 | 4.5 | 0.01 | 0.55 | 0.01 | 47.5 |
| 12 R 2 | 242 | 78 | 255 | 32.2 | 0.188 | 7.7 | LOS A | 0.4 | 4.5 | 0.01 | 0.55 | 0.01 | 48.0 |
| Approach | 243 | 78 | 256 | 32.1 | 0.188 | 7.7 | LOS A | 0.4 | 4.5 | 0.01 | 0.55 | 0.01 | 48.0 |
| All <br> Vehicles | 478 | 207 | 503 | 43.3 | 0.188 | 6.1 | LOS A | 0.4 | 6.2 | 0.10 | 0.48 | 0.10 | 48.1 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\forall$ Site: 9 [[ID: 9] Internal Road Roundabout Altis - PM (Site

Folder: 2026 - PM 60\% GFA)]
Internal Road Roundabout Altis
Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { INP } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | JT MES HV ] veh/h |  | $\begin{gathered} \text { AND } \\ \text { WS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service | $\begin{aligned} & 95 \% \text { B } \\ & \text { QU } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \mathrm{m} \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: New Road (370m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 325 | 89 | 342 | 27.4 | 0.221 | 2.6 | LOS A | 0.7 | 7.2 | 0.07 | 0.33 | 0.07 | 48.5 |
| 2 T1 | 1 | 0 | 1 | 0.0 | 0.001 | 1.7 | LOSA | 0.0 | 0.0 | 0.06 | 0.19 | 0.06 | 50.8 |
| Approach | 326 | 89 | 343 | 27.3 | 0.221 | 2.6 | LOS A | 0.7 | 7.2 | 0.07 | 0.33 | 0.07 | 48.5 |
| North: New Road (1000m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 52 | 5 | 55 | 9.6 | 0.032 | 1.8 | LOSA | 0.1 | 0.6 | 0.14 | 0.22 | 0.14 | 50.2 |
| 9 R2 | 8 | 8 | 8 | 100.0 | 0.015 | 9.3 | LOSA | 0.0 | 0.9 | 0.22 | 0.48 | 0.22 | 47.2 |
| Approach | 60 | 13 | 63 | 21.7 | 0.032 | 2.8 | LOS A | 0.1 | 0.9 | 0.15 | 0.25 | 0.15 | 49.7 |
| West: New Road (600m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 1 | 0 | 1 | 0.0 | 0.083 | 2.1 | LOS A | 0.2 | 2.3 | 0.01 | 0.52 | 0.01 | 47.5 |
| 12 R 2 | 86 | 62 | 91 | 72.1 | 0.083 | 8.0 | LOSA | 0.2 | 2.3 | 0.01 | 0.52 | 0.01 | 47.6 |
| Approach | 87 | 62 | 92 | 71.3 | 0.083 | 7.9 | LOS A | 0.2 | 2.3 | 0.01 | 0.52 | 0.01 | 47.6 |
| All <br> Vehicles | 473 | 164 | 498 | 34.7 | 0.221 | 3.6 | LOS A | 0.7 | 7.2 | 0.07 | 0.35 | 0.07 | 48.6 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## Attachment 2

## SITE LAYOUT

目 Site: 1 [ID [1]. Mamre Road / Bakers Lane - AM (Site Folder:
2026 - AM - 75\% GFA)]
Mamre Road / Bakers Lane
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Coordinated

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## MOVEMENT SUMMARY

目 Site: 1 [ID [1]. Mamre Road / Bakers Lane - AM (Site Folder:
2026-AM-75\% GFA)]
Mamre Road / Bakers Lane
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Coordinated Cycle Time $=120$ seconds (Site User-Given Phase Times)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INP } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | MES <br> HV $]$ veh/h |  | AND NS HV ] \% | Deg. <br> Satn <br> V/c | Aver. Delay sec | Level of Service | $\begin{gathered} 95 \% \text { B } \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No Cycles | Aver. Speed km/h |
| South: Mamre Road (1200m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 44 | 25 | 46 | 56.8 | 0.896 | 54.2 | LOS D | 21.6 | 209.1 | 0.83 | 0.98 | 1.10 | 45.1 |
| 2 T1 | 1343 | 276 | 1414 | 20.6 | 0.896 | 44.5 | LOS D | 34.1 | 310.4 | 0.92 | 0.97 | 1.11 | 57.3 |
| 3 R2 | 28 | 6 | 29 | 21.4 | * 0.129 | 56.2 | LOS D | 1.5 | 12.6 | 0.90 | 0.73 | 0.90 | 45.2 |
| Approach | 1415 | 307 | 1489 | 21.7 | 0.896 | 45.1 | LOS D | 34.1 | 310.4 | 0.92 | 0.97 | 1.10 | 56.7 |
| East: Bakers Ln |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 7 | 6 | 7 | 85.7 | 0.022 | 26.8 | LOS B | 0.2 | 2.8 | 0.54 | 0.65 | 0.54 | 57.3 |
| 5 T1 | 1 | 0 | 1 | 0.0 | * 0.022 | 19.1 | LOS B | 0.2 | 2.8 | 0.54 | 0.65 | 0.54 | 49.3 |
| 6 R2 | 156 | 4 | 164 | 2.6 | * 0.300 | 57.2 | LOS E | 4.4 | 31.2 | 0.93 | 0.77 | 0.93 | 47.8 |
| Approach | 164 | 10 | 173 | 6.1 | 0.300 | 55.7 | LOS D | 4.4 | 31.2 | 0.91 | 0.76 | 0.91 | 48.1 |
| North: Mamre Road (1250m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 367 | 0 | 386 | 0.0 | 0.859 | 22.9 | LOS B | 22.5 | 174.0 | 0.56 | 0.74 | 0.64 | 63.9 |
| 8 T1 | 1575 | 248 | 1658 | 15.7 | * 0.859 | 26.6 | LOS B | 34.4 | 294.6 | 0.78 | 0.80 | 0.86 | 64.4 |
| 9 R2 | 275 | 39 | 289 | 14.2 | 0.414 | 51.0 | LOS D | 7.3 | 61.6 | 0.90 | 0.80 | 0.90 | 44.7 |
| Approach | 2217 | 287 | 2334 | 12.9 | 0.859 | 29.0 | LOS C | 34.4 | 294.6 | 0.76 | 0.79 | 0.83 | 61.6 |
| West: Bakers Ln |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 106 | 40 | 112 | 37.7 | 0.205 | 23.9 | LOS B | 3.5 | 40.3 | 0.60 | 0.68 | 0.60 | 51.7 |
| 11 T1 | 1 | 0 | 1 | 0.0 | 0.009 | 58.2 | LOS E | 0.1 | 0.4 | 0.96 | 0.56 | 0.96 | 35.9 |
| 12 R 2 | 43 | 21 | 45 | 48.8 | 0.292 | 56.1 | LOS D | 2.5 | 31.4 | 0.93 | 0.75 | 0.93 | 40.1 |
| Approach | 150 | 61 | 158 | 40.7 | 0.292 | 33.4 | LOS C | 3.5 | 40.3 | 0.70 | 0.70 | 0.70 | 47.7 |
| All <br> Vehicles | 3946 | 665 | 4154 | 16.9 | 0.896 | 36.0 | LOS C | 34.4 | 310.4 | 0.82 | 0.85 | 0.93 | 58.6 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID Crossing | Input Vol. ped/h | Dem. Flow ped/h | Aver. Delay sec | Level of Service | $\begin{gathered} \text { VERAG } \\ \text { QL } \\ \text { [ Ped } \\ \text { ped } \end{gathered}$ | $\begin{aligned} & \text { ACK OF } \\ & \text { IE } \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. Que | fective Stop Rate | Travel Time sec | Travel Dist. m | Aver. Speed |
| South: Mamre Road (1200m) |  |  |  |  |  |  |  |  |  |  |  |
| P1 Full | 10 | 11 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 231.0 | 229.9 | 1.00 |
| East: Bakers Ln |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 10 | 11 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 222.4 | 218.7 | 0.98 |

West: Bakers Ln

| P4 Full | 10 | 11 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 222.9 | 219.4 | 0.98 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| All | 30 | 32 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 225.5 | 222.7 | 0.99 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## MOVEMENT SUMMARY

目 Site: 1 [ID [1]. Mamre Road / Bakers Lane - PM (Site Folder:
2026 - PM - 75\% GFA)]
Mamre Road / Bakers Lane
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Coordinated Cycle Time $=120$ seconds (Site User-Given Phase Times)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | JT MES HV ] veh/h |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service |  | CK OF UE Dist] m | Prop. Que | Effective Stop Rate |  | Aver. Speed <br> $\mathrm{km} / \mathrm{h}$ |
| South: Mamre Road (1200m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 150 | 25 | 158 | 16.7 | 0.893 | 43.7 | LOS D | 29.2 | 254.6 | 0.81 | 0.97 | 1.00 | 48.1 |
| 2 T1 | 1614 | 292 | 1699 | 18.1 | * 0.893 | 38.5 | LOS C | 38.2 | 331.8 | 0.89 | 0.94 | 1.03 | 60.3 |
| 3 R2 | 10 | 0 | 11 | 0.0 | 0.067 | 63.3 | LOSE | 0.6 | 4.1 | 0.95 | 0.68 | 0.95 | 45.4 |
| Approach | 1774 | 317 | 1867 | 17.9 | 0.893 | 39.0 | LOS C | 38.2 | 331.8 | 0.88 | 0.94 | 1.03 | 59.2 |
| East: Bakers Ln |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 12 | 0 | 13 | 0.0 | 0.027 | 22.0 | LOS B | 0.4 | 3.1 | 0.56 | 0.66 | 0.56 | 63.7 |
| 5 T1 | 3 | 2 | 3 | 66.7 | * 0.027 | 16.6 | LOS B | 0.4 | 3.1 | 0.56 | 0.66 | 0.56 | 50.1 |
| 6 R2 | 558 | 9 | 587 | 1.6 | * 0.735 | 56.5 | LOSE | 16.6 | 117.7 | 0.99 | 0.86 | 1.04 | 48.0 |
| Approach | 573 | 11 | 603 | 1.9 | 0.735 | 55.6 | LOS D | 16.6 | 117.7 | 0.98 | 0.86 | 1.02 | 48.3 |
| North: Mamre Road (1250m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 187 | 31 | 197 | 16.6 | 0.852 | 29.5 | LOS C | 19.2 | 178.2 | 0.60 | 0.77 | 0.72 | 57.8 |
| 8 T1 | 1454 | 305 | 1531 | 21.0 | 0.852 | 28.9 | LOS C | 31.7 | 282.2 | 0.79 | 0.82 | 0.88 | 63.5 |
| 9 R2 | 62 | 37 | 65 | 59.7 | * 0.376 | 69.1 | LOS E | 2.0 | 23.8 | 0.98 | 0.74 | 0.98 | 40.0 |
| Approach | 1703 | 373 | 1793 | 21.9 | 0.852 | 30.4 | LOS C | 31.7 | 282.2 | 0.78 | 0.81 | 0.87 | 61.9 |
| West: Bakers Ln |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 208 | 46 | 219 | 22.1 | 0.479 | 41.7 | LOS C | 9.7 | 90.4 | 0.83 | 0.80 | 0.83 | 49.1 |
| 11 T1 | 1 | 0 | 1 | 0.0 | 0.008 | 56.9 | LOS E | 0.1 | 0.4 | 0.95 | 0.56 | 0.95 | 36.3 |
| 12 R 2 | 144 | 27 | 152 | 18.8 | 0.474 | 49.7 | LOS D | 7.9 | 69.5 | 0.92 | 0.80 | 0.92 | 42.9 |
| Approach | 353 | 73 | 372 | 20.7 | 0.479 | 45.0 | LOS D | 9.7 | 90.4 | 0.87 | 0.80 | 0.87 | 46.3 |
| All <br> Vehicles | 4403 | 774 | 4635 | 17.6 | 0.893 | 38.3 | LOS C | 38.2 | 331.8 | 0.86 | 0.87 | 0.95 | 57.7 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID Crossing | Input Vol. ped/h | Dem. Flow ped/h | Aver. Delay sec | Level of Service | $\begin{gathered} \text { VERAG } \\ \text { QL } \\ \text { [ Ped } \\ \text { ped } \end{gathered}$ | $\begin{aligned} & \text { ACK OF } \\ & \text { IE } \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. Que | fective Stop Rate | Travel Time sec | Travel Dist. m | Aver. Speed |
| South: Mamre Road (1200m) |  |  |  |  |  |  |  |  |  |  |  |
| P1 Full | 10 | 11 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 231.0 | 229.9 | 1.00 |
| East: Bakers Ln |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 10 | 11 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 222.4 | 218.7 | 0.98 |

West: Bakers Ln

| P4 Full | 10 | 11 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 222.9 | 219.4 | 0.98 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| All | 30 | 32 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 225.5 | 222.7 | 0.99 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## SITE LAYOUT

目 Site: 2 [ID [2]. Mamre Road / Mirvac Access - AM (Site Folder:
2026 - AM - 75\% GFA)]
Mamre Road x Mirvac Access
Site Category: Proposed Interim
Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


## MOVEMENT SUMMARY

目 Site: 2 [ID [2]. Mamre Road / Mirvac Access - AM (Site Folder:
2026-AM - 75\% GFA)]
Mamre Road x Mirvac Access
Site Category: Proposed Interim
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=120$ seconds (Site User-Given Cycle Time)
Variable Sequence Analysis applied. The results are given for the selected output sequence.

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INP } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | JT <br> MES HV ] veh/h |  | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service |  | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate |  | Aver. Speed <br> km/h |
| South: Mamre Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 1053 | 138 | 1108 | 13.1 | 0.499 | 12.5 | LOS A | 17.1 | 142.4 | 0.58 | 0.53 | 0.58 | 56.3 |
| 3 R2 | 48 | 16 | 51 | 33.3 | * 0.726 | 75.5 | LOS F | 3.3 | 34.5 | 1.00 | 0.84 | 1.26 | 26.6 |
| Approach | 1101 | 154 | 1159 | 14.0 | 0.726 | 15.3 | LOS B | 17.1 | 142.4 | 0.60 | 0.54 | 0.61 | 53.7 |
| East: Mirvac Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 34 | 16 | 36 | 47.1 | 0.068 | 14.8 | LOS B | 0.6 | 8.0 | 0.36 | 0.60 | 0.36 | 47.1 |
| 6 R2 | 376 | 175 | 396 | 46.5 | * 0.711 | 54.4 | LOS D | 11.5 | 137.6 | 0.98 | 0.87 | 1.05 | 29.9 |
| Approach | 410 | 191 | 432 | 46.6 | 0.711 | 51.1 | LOS D | 11.5 | 137.6 | 0.92 | 0.85 | 0.99 | 30.8 |
| North: Mamre Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 586 | 95 | 617 | 16.2 | 0.473 | 8.4 | LOS A | 6.2 | 54.0 | 0.27 | 0.66 | 0.27 | 51.8 |
| 8 T1 | 1009 | 145 | 1062 | 14.4 | * 0.582 | 22.0 | LOS B | 21.0 | 177.9 | 0.74 | 0.66 | 0.74 | 49.9 |
| Approach | 1595 | 240 | 1679 | 15.0 | 0.582 | 17.0 | LOS B | 21.0 | 177.9 | 0.56 | 0.66 | 0.56 | 50.6 |
| All <br> Vehicles | 3106 | 585 | 3269 | 18.8 | 0.726 | 20.9 | LOS B | 21.0 | 177.9 | 0.62 | 0.64 | 0.64 | 47.6 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID Crossing | Input Vol. ped/h | Dem. Flow ped/h | Aver. <br> Delay <br> sec | Level of AVERAGE BACK OF Service QUEUE |  |  | Prop. Effective Que Stop Rate |  | Travel Time sec | Travel Aver. Dist. Speed$\qquad$ |  |
| South: Mamre Rd |  |  |  |  |  |  |  |  |  |  |  |
| P1 Full | 50 | 53 | 47.8 | LOS E | 0.2 | 0.2 | 0.89 | 0.89 | 219.7 | 223.5 | 1.02 |
| East: Mirvac Access |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 50 | 53 | 19.9 | LOS B | 0.1 | 0.1 | 0.58 | 0.58 | 186.8 | 217.0 | 1.16 |
| North: Mamre Rd |  |  |  |  |  |  |  |  |  |  |  |
| P3 Full | 50 | 53 | 47.8 | LOS E | 0.2 | 0.2 | 0.89 | 0.89 | 220.1 | 224.0 | 1.02 |
| All Pedestrians | 150 | 158 | 38.5 | LOS D | 0.2 | 0.2 | 0.79 | 0.79 | 208.9 | 221.5 | 1.06 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

## MOVEMENT SUMMARY

目 Site: 2 [ID [2]. Mamre Road / Mirvac Access - PM (Site Folder:
2026 - PM - 75\% GFA)]
Mamre Road x Mirvac Access
Site Category: Proposed Interim
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=120$ seconds (Site User-Given Phase Times)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{array}{r} \text { IN } \\ \mathrm{VOL} \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | JT MES HV] veh/h |  | $\begin{gathered} \text { AND } \\ \text { WS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% BACK OF QUEUE |  | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed |
| South: Mamre Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 1228 | 155 | 1293 | 12.6 | 0.565 | 12.3 | LOS A | 20.6 | 170.6 | 0.60 | 0.55 | 0.60 | 56.4 |
| 3 R2 | 150 | 19 | 158 | 12.7 | * 0.879 | 75.6 | LOS F | 10.5 | 87.6 | 1.00 | 0.97 | 1.38 | 26.6 |
| Approach | 1378 | 174 | 1451 | 12.6 | 0.879 | 19.2 | LOS B | 20.6 | 170.6 | 0.64 | 0.59 | 0.68 | 50.3 |
| East: AIE Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 23 | 6 | 24 | 26.1 | 0.038 | 31.3 | LOS C | 0.7 | 6.7 | 0.53 | 0.63 | 0.53 | 43.2 |
| 6 R2 | 493 | 142 | 519 | 28.8 | * 0.786 | 57.1 | LOS E | 15.7 | 149.3 | 1.00 | 0.91 | 1.12 | 28.2 |
| Approach | 516 | 148 | 543 | 28.7 | 0.786 | 55.9 | LOS D | 15.7 | 149.3 | 0.98 | 0.90 | 1.10 | 28.6 |
| North: Mamre Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 181 | 135 | 191 | 74.6 | 0.209 | 9.6 | LOS A | 2.0 | 27.8 | 0.24 | 0.62 | 0.24 | 50.7 |
| 8 T1 | 1482 | 205 | 1560 | 13.8 | * 0.900 | 47.6 | LOS D | 49.1 | 404.5 | 0.99 | 1.02 | 1.13 | 38.6 |
| Approach | 1663 | 340 | 1751 | 20.4 | 0.900 | 43.5 | LOS D | 49.1 | 404.5 | 0.91 | 0.98 | 1.03 | 39.7 |
| All <br> Vehicles | 3557 | 662 | 3744 | 18.6 | 0.900 | 35.9 | LOS C | 49.1 | 404.5 | 0.81 | 0.82 | 0.91 | 40.7 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov <br> ID Crossing | Input Vol. ped/h | Dem. Flow ped/h | Aver. Delay sec | Level of Service | $\begin{gathered} \text { VERAC } \\ \text { Q } \\ \text { [ Ped } \\ \text { ped } \end{gathered}$ | ACK OF E <br> Dist ] <br> m | Prop. Que | Effective Stop Rate | Travel Time sec | Travel Dist. m | Aver. Speed |
| South: Mamre Rd |  |  |  |  |  |  |  |  |  |  |  |
| P1 Full | 50 | 53 | 47.8 | LOS E | 0.2 | 0.2 | 0.89 | 0.89 | 219.7 | 223.5 | 1.02 |
| East: AIE Access |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 50 | 53 | 22.3 | LOS C | 0.1 | 0.1 | 0.61 | 0.61 | 189.2 | 217.0 | 1.15 |
| North: Mamre Rd |  |  |  |  |  |  |  |  |  |  |  |
| P3 Full | 50 | 53 | 47.8 | LOS E | 0.2 | 0.2 | 0.89 | 0.89 | 220.1 | 224.0 | 1.02 |
| All | 150 | 158 | 39.3 | LOS D | 0.2 | 0.2 | 0.80 | 0.80 | 209.7 | 221.5 | 1.06 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

## SITE LAYOUT

$\nabla$ Site: 3 [ID [3]. Mamre Road / Altis Access - AM (Site Folder:
2026 - AM - 75\% GFA)]
Mamre Road x Altis Access
Site Category: (None)
Give-Way (Two-Way)
Layout pictures are schematic functional drawings reflecting input data. They are not design drawings

## 4N



## MOVEMENT SUMMARY

$\nabla$ Site: 3 [ID [3]. Mamre Road / Altis Access - AM (Site Folder:
2026-AM - 75\% GFA)]
Mamre Road x Altis Access
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | UT MES HV ] veh/h |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service |  | CK OF <br> UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver Speed <br> km/h |
| South: Mamre Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 1098 | 154 | 1156 | 14.0 | 0.670 | 0.4 | LOS A | 0.0 | 0.0 | 0.00 | 0.01 | 0.00 | 77.8 |
| Approach | 1098 | 154 | 1156 | 14.0 | 0.670 | 0.4 | NA | 0.0 | 0.0 | 0.00 | 0.01 | 0.00 | 77.8 |
| East: Altis |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 137 | 53 | 144 | 38.7 | 0.113 | 7.2 | LOSA | 0.0 | 0.0 | 0.00 | 0.51 | 0.00 | 53.2 |
| Approach | 137 | 53 | 144 | 38.7 | 0.113 | 7.2 | NA | 0.0 | 0.0 | 0.00 | 0.51 | 0.00 | 53.2 |
| North: Mamre Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 119 | 21 | 125 | 17.6 | 0.080 | 7.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.63 | 0.00 | 58.6 |
| 8 T1 | 923 | 139 | 972 | 15.1 | 0.571 | 0.4 | LOSA | 0.0 | 0.0 | 0.00 | 0.02 | 0.00 | 77.9 |
| Approach | 1042 | 160 | 1097 | 15.4 | 0.571 | 1.2 | NA | 0.0 | 0.0 | 0.00 | 0.09 | 0.00 | 75.0 |
| All <br> Vehicles | 2277 | 367 | 2397 | 16.1 | 0.670 | 1.2 | NA | 0.0 | 0.0 | 0.00 | 0.08 | 0.00 | 74.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## SIDRA INTERSECTION 9.0 | Copyright © 2000-2020 Akcelik and Associates Pty Ltd | sidrasolutions.com

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Models Option 3 - double RT (2).sip9

## MOVEMENT SUMMARY

$\nabla$ Site: 3 [ID [3]. Mamre Road / Altis Access - PM (Site Folder:
2026 - PM - 75\% GFA)]
Mamre Road x Altis Access
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | INPUT VOLUMES |  | DEMAND FLOWS |  | $\begin{aligned} & \text { Deg. } \\ & \text { Satn } \\ & \text { v/c } \end{aligned}$ | Aver. Delay sec | Level of Service | 95\% BACK OF QUEUE |  | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Mamre Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 1350 | 172 | 1421 | 12.7 | 0.817 | 0.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.01 | 0.00 | 76.6 |
| Approach | 1350 | 172 | 1421 | 12.7 | 0.817 | 0.8 | NA | 0.0 | 0.0 | 0.00 | 0.01 | 0.00 | 76.6 |
| East: Altis |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 468 | 62 | 493 | 13.2 | 0.301 | 37.1 | LOS C | 0.0 | 0.0 | 0.00 | 0.52 | 0.00 | 54.3 |
| Approach | 468 | 62 | 493 | 13.2 | 0.301 | 37.1 | NA | 0.0 | 0.0 | 0.00 | 0.52 | 0.00 | 54.3 |
| North: Mamre Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 31 | 22 | 33 | 71.0 | 0.030 | 7.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.62 | 0.00 | 44.9 |
| 8 T1 | 1479 | 187 | 1557 | 12.6 | 0.887 | 36.5 | LOS C | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 75.3 |
| Approach | 1510 | 209 | 1589 | 13.8 | 0.887 | 35.9 | NA | 0.0 | 0.0 | 0.00 | 0.01 | 0.00 | 74.3 |
| All <br> Vehicles | 3328 | 443 | 3503 | 13.3 | 0.887 | 21.8 | NA | 0.0 | 0.0 | 0.00 | 0.08 | 0.00 | 71.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Project: C:IUsers\Arun Mohan\Desktop\Ason Group\P1815-2026 MRP revised modelling\SIDRA Files\From SharepointlP1815 2026 SIDRA
Models Option 3 - double RT (2).sip9

## SITE LAYOUT

目 Site: 4 [ID [4]. Mamre Road / Abbotts Road - AM (Site Folder:
2026 - AM - 75\% GFA)]
Mamre Road / Abbotts Road
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Coordinated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


## MOVEMENT SUMMARY

目 Site: 4 [ID [4]. Mamre Road / Abbotts Road - AM (Site Folder:
2026 - AM - 75\% GFA)]
Mamre Road / Abbotts Road
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Coordinated Cycle Time $=120$ seconds (Site User-Given Phase Times)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | JT MES HV] veh/h |  | $\begin{aligned} & \text { AND } \\ & \text { WS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay sec | Level of Service |  | CK OF UE Dist ] | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Mamre Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 1076 | 146 | 1133 | 13.6 | * 0.424 | 1.9 | LOS A | 1.1 | 9.2 | 0.04 | 0.03 | 0.04 | 79.4 |
| 3 R2 | 121 | 55 | 127 | 45.5 | 0.475 | 44.0 | LOS D | 2.8 | 30.9 | 0.98 | 0.77 | 0.98 | 35.8 |
| Approach | 1197 | 201 | 1260 | 16.8 | 0.475 | 6.1 | LOS A | 2.8 | 30.9 | 0.13 | 0.11 | 0.13 | 72.9 |
| East: Abbotts Road (400m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 31 | 17 | 33 | 54.8 | 0.061 | 35.2 | LOS C | 0.9 | 11.3 | 0.69 | 0.67 | 0.69 | 33.1 |
| 6 R2 | 23 | 8 | 24 | 34.8 | * 0.063 | 54.6 | LOS D | 0.6 | 6.6 | 0.88 | 0.69 | 0.88 | 33.5 |
| Approach | 54 | 25 | 57 | 46.3 | 0.063 | 43.5 | LOS D | 0.9 | 11.3 | 0.77 | 0.68 | 0.77 | 33.3 |
| North: Mamre Road (800m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 138 | 27 | 145 | 19.6 | 0.170 | 19.9 | LOS B | 3.9 | 36.0 | 0.49 | 0.72 | 0.49 | 53.3 |
| 8 T1 | 918 | 160 | 966 | 17.4 | 0.353 | 8.8 | LOSA | 5.7 | 50.7 | 0.33 | 0.29 | 0.33 | 70.0 |
| Approach | 1056 | 187 | 1112 | 17.7 | 0.353 | 10.3 | LOS A | 5.7 | 50.7 | 0.35 | 0.34 | 0.35 | 67.4 |
| All Vehicles | 2307 | 413 | 2428 | 17.9 | 0.475 | 8.9 | LOS A | 5.7 | 50.7 | 0.25 | 0.23 | 0.25 | 68.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID Crossing | Input Vol. <br> ped/h | Dem. Flow ped/h | Aver. Delay sec | Level of Service | $\begin{aligned} & \text { IVERAG } \\ & \text { Qu } \\ & \text { [ Ped } \\ & \text { ped } \end{aligned}$ | ACK OF <br> Dist ] <br> m | Prop. Que | fective Stop Rate | Travel Time sec | Travel Dist. $\qquad$ | Aver. Speed |
| South: Mamre Road (500m) |  |  |  |  |  |  |  |  |  |  |  |
| P1 Full | 10 | 11 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 234.8 | 234.8 | 1.00 |
| East: Abbotts Road (400m) |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 10 | 11 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 221.3 | 217.2 | 0.98 |
| P2BSlip/ Bypass | 10 | 11 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 215.3 | 209.4 | 0.97 |
| North: Mamre Road (800m) |  |  |  |  |  |  |  |  |  |  |  |
| P3B Slip/ <br> Bypass | 10 | 11 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 212.0 | 205.2 | 0.97 |
| All <br> Pedestrians | 40 | 42 | 54.2 | LOSE | 0.0 | 0.0 | 0.95 | 0.95 | 220.8 | 216.7 | 0.98 |

[^2]Pedestrian movement LOS values are based on average delay per pedestrian movement.

## MOVEMENT SUMMARY

目 Site: 4 [ID [4]. Mamre Road / Abbotts Road - PM (Site Folder:
2026 - PM - 75\% GFA)]
Abbotts Road / Mamre Road
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Coordinated Cycle Time $=120$ seconds (Site User-Given Phase Times)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INP } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | JT HV ] veh/h |  | AND WS HV ] \% | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% <br> [ Veh. <br> veh | CK OF Dist ] <br> m | Prop. Que | Effective Stop Rate | Aver Cycles | Aver. Speed km/h |
| South: Mamre Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 1232 | 131 | 1297 | 10.6 | 0.445 | 3.0 | LOSA | 1.3 | 10.8 | 0.04 | 0.04 | 0.04 | 79.5 |
| 3 R2 | 368 | 51 | 387 | 13.9 | * 0.837 | 70.1 | LOSE | 12.4 | 105.3 | 1.00 | 0.93 | 1.26 | 28.3 |
| Approach | 1600 | 182 | 1684 | 11.4 | 0.837 | 18.4 | LOS B | 12.4 | 105.3 | 0.26 | 0.24 | 0.32 | 60.5 |
| East: Abbotts Road (400m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 126 | 24 | 133 | 19.0 | 0.190 | 45.7 | LOS D | 3.9 | 32.8 | 0.77 | 0.73 | 0.77 | 35.1 |
| 6 R2 | 112 | 36 | 118 | 32.1 | * 0.482 | 67.1 | LOS E | 3.5 | 37.4 | 0.99 | 0.77 | 0.99 | 31.0 |
| Approach | 238 | 60 | 251 | 25.2 | 0.482 | 55.8 | LOS D | 3.9 | 37.4 | 0.87 | 0.75 | 0.87 | 32.8 |
| North: Mamre Road (800m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 30 | 18 | 32 | 60.0 | 0.048 | 17.2 | LOS B | 0.7 | 8.7 | 0.40 | 0.67 | 0.40 | 54.0 |
| 8 T1 | 1943 | 236 | 2045 | 12.1 | * 0.639 | 9.0 | LOSA | 13.4 | 109.1 | 0.36 | 0.33 | 0.36 | 71.6 |
| Approach | 1973 | 254 | 2077 | 12.9 | 0.639 | 9.1 | LOS A | 13.4 | 109.1 | 0.36 | 0.34 | 0.36 | 71.3 |
| All Vehicles | 3811 | 496 | 4012 | 13.0 | 0.837 | 15.9 | LOS B | 13.4 | 109.1 | 0.35 | 0.32 | 0.38 | 62.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID Crossing | Input Vol. <br> ped/h | Dem. Flow ped/h | Aver. Delay sec | Level of Service | $\begin{aligned} & \text { IVERAG } \\ & \text { Qu } \\ & \text { [ Ped } \\ & \text { ped } \end{aligned}$ | ACK OF <br> Dist ] <br> m | Prop. Que | fective Stop Rate | Travel Time sec | Travel Dist. $\qquad$ | Aver. Speed |
| South: Mamre Road (500m) |  |  |  |  |  |  |  |  |  |  |  |
| P1 Full | 10 | 11 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 234.8 | 234.8 | 1.00 |
| East: Abbotts Road (400m) |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 10 | 11 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 221.3 | 217.2 | 0.98 |
| P2BSlip/ Bypass | 10 | 11 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 215.3 | 209.4 | 0.97 |
| North: Mamre Road (800m) |  |  |  |  |  |  |  |  |  |  |  |
| P3B Slip/ <br> Bypass | 10 | 11 | 54.2 | LOS E | 0.0 | 0.0 | 0.95 | 0.95 | 212.0 | 205.2 | 0.97 |
| All <br> Pedestrians | 40 | 42 | 54.2 | LOSE | 0.0 | 0.0 | 0.95 | 0.95 | 220.8 | 216.7 | 0.98 |

[^3]Pedestrian movement LOS values are based on average delay per pedestrian movement.

## SITE LAYOUT

目 Site: 5 [ID [5]. Aldington Road / Fife Kemps Creek North - AM
(Site Folder: 2026-AM - 75\% GFA)]
Aldington Road / Fife Kemps Creek North
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.
$Q^{2}$


## MOVEMENT SUMMARY

目 Site: 5 [ID [5]. Aldington Road / Fife Kemps Creek North - AM
(Site Folder: 2026-AM - 75\% GFA)]
Aldington Road / Fife Kemps Creek North
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=120$ seconds (Site User-Given Cycle Time)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INP } \\ & \text { VOLu } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | JT <br> MES <br> HV ] <br> veh/h |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service |  | CK OF <br> UE Dist ] m | Prop. Que | Effective Stop Rate |  | Aver Speed <br> km/h |
| South: Aldington Road (670m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 6 | 3 | 6 | 50.0 | 0.011 | 25.9 | LOS B | 0.2 | 2.0 | 0.58 | 0.64 | 0.58 | 40.9 |
| 2 T1 | 26 | 2 | 27 | 7.7 | 0.050 | 29.5 | LOS C | 1.1 | 9.1 | 0.71 | 0.53 | 0.71 | 46.3 |
| 3 R2 | 1 | 0 | 1 | 0.0 | 0.007 | 60.1 | LOS E | 0.1 | 0.4 | 0.93 | 0.59 | 0.93 | 30.9 |
| Approach | 33 | 5 | 35 | 15.2 | 0.050 | 29.8 | LOS C | 1.1 | 9.1 | 0.70 | 0.55 | 0.70 | 45.0 |
| East: New Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 1 | 0 | 1 | 0.0 | 0.150 | 35.2 | LOS C | 3.8 | 26.4 | 0.75 | 0.73 | 0.75 | 37.4 |
| 5 T1 | 1 | 0 | 1 | 0.0 | 0.150 | 30.6 | LOS C | 3.8 | 26.4 | 0.75 | 0.73 | 0.75 | 33.8 |
| 6 R2 | 85 | 0 | 89 | 0.0 | 0.150 | 35.2 | LOS C | 3.8 | 26.4 | 0.75 | 0.73 | 0.75 | 40.6 |
| Approach | 87 | 0 | 92 | 0.0 | 0.150 | 35.1 | LOS C | 3.8 | 26.4 | 0.75 | 0.73 | 0.75 | 40.5 |
| North: Aldington Road (980m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $7 \quad$ L2 | 289 | 0 | 304 | 0.0 | * 0.249 | 10.3 | LOS A | 3.9 | 27.2 | 0.45 | 0.70 | 0.45 | 50.5 |
| 8 T1 | 1 | 0 | 1 | 0.0 | 0.002 | 28.5 | LOS B | 0.0 | 0.3 | 0.69 | 0.42 | 0.69 | 46.7 |
| 9 R2 | 28 | 0 | 29 | 0.0 | 0.188 | 62.6 | LOS E | 1.7 | 11.7 | 0.96 | 0.72 | 0.96 | 33.7 |
| Approach | 318 | 0 | 335 | 0.0 | 0.249 | 14.9 | LOS B | 3.9 | 27.2 | 0.49 | 0.70 | 0.49 | 48.3 |
| West: New Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 8 | 0 | 8 | 0.0 | * 0.200 | 36.4 | LOS C | 0.7 | 6.9 | 0.96 | 0.70 | 0.96 | 40.3 |
| 11 T1 | 1 | 0 | 1 | 0.0 | * 0.200 | 31.8 | LOS C | 0.7 | 6.9 | 0.96 | 0.70 | 0.96 | 33.5 |
| 12 R 2 | 12 | 8 | 13 | 66.7 | 0.200 | 37.0 | LOS C | 0.7 | 6.9 | 0.96 | 0.70 | 0.96 | 36.1 |
| Approach | 21 | 8 | 22 | 38.1 | 0.200 | 36.5 | LOS C | 0.7 | 6.9 | 0.96 | 0.70 | 0.96 | 37.7 |
| All Vehicles | 459 | 13 | 483 | 2.8 | 0.249 | 20.8 | LOS B | 3.9 | 27.2 | 0.58 | 0.70 | 0.58 | 45.9 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID Crossing | Input Vol. ped/h | Dem. Flow ped/h | Aver. Delay <br> sec | Level of Service | $\begin{gathered} \text { ERAG } \\ \text { Qu } \\ \text { [ Ped } \\ \text { ped } \end{gathered}$ | CK <br> Dist ] <br> m | Prop. Effective Que Stop Rate |  | Travel Time sec | Travel Dist. <br> m | Aver. Speed <br> $\mathrm{m} / \mathrm{sec}$ |
| South: Aldington Road (670m) |  |  |  |  |  |  |  |  |  |  |  |
| P1 Full | 50 | 53 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 224.7 | 221.5 | 0.99 |
| East: New Road (500m) |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 50 | 53 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 216.6 | 211.0 | 0.97 |
| All | 0 | 105 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 220.6 | 216.3 | 0.98 |

## MOVEMENT SUMMARY

目 Site: 5 [ID [5]. Aldington Road / Fife Kemps Creek North - PM
(Site Folder: 2026-PM - 75\% GFA)]
Aldington Road / Fife Kemps Creek North
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=120$ seconds (Site User-Given Cycle Time)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INP } \\ & \text { VOLu } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | JT <br> MES <br> HV ] <br> veh/h |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service |  | CK OF <br> UE Dist ] m | Prop. Que | Effective Stop Rate |  | Aver. Speed <br> km/h |
| South: Aldington Road (670m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 17 | 6 | 18 | 35.3 | 0.031 | 28.5 | LOS B | 0.6 | 5.6 | 0.62 | 0.67 | 0.62 | 40.0 |
| 2 T1 | 101 | 0 | 106 | 0.0 | * 0.209 | 37.4 | LOS C | 4.9 | 34.0 | 0.82 | 0.66 | 0.82 | 43.7 |
| 3 R2 | 1 | 0 | 1 | 0.0 | 0.006 | 57.8 | LOS E | 0.1 | 0.4 | 0.92 | 0.59 | 0.92 | 31.4 |
| Approach | 119 | 6 | 125 | 5.0 | 0.209 | 36.3 | LOS C | 4.9 | 34.0 | 0.80 | 0.66 | 0.80 | 43.1 |
| East: New Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 1 | 0 | 1 | 0.0 | 0.212 | 34.5 | LOS C | 5.6 | 39.1 | 0.75 | 0.74 | 0.75 | 37.6 |
| 5 T1 | 1 | 0 | 1 | 0.0 | * 0.212 | 29.9 | LOS C | 5.6 | 39.1 | 0.75 | 0.74 | 0.75 | 34.0 |
| 6 R2 | 127 | 0 | 134 | 0.0 | 0.212 | 34.5 | LOS C | 5.6 | 39.1 | 0.75 | 0.74 | 0.75 | 40.8 |
| Approach | 129 | 0 | 136 | 0.0 | 0.212 | 34.4 | LOS C | 5.6 | 39.1 | 0.75 | 0.74 | 0.75 | 40.8 |
| North: Aldington Road (980m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $7 \quad$ L2 | 32 | 0 | 34 | 0.0 | 0.030 | 10.7 | LOS A | 0.4 | 2.8 | 0.42 | 0.65 | 0.42 | 50.2 |
| 8 T1 | 69 | 0 | 73 | 0.0 | 0.143 | 36.7 | LOS C | 3.3 | 22.8 | 0.81 | 0.63 | 0.81 | 43.9 |
| 9 R2 | 1 | 0 | 1 | 0.0 | 0.006 | 57.8 | LOS E | 0.1 | 0.4 | 0.92 | 0.60 | 0.92 | 34.8 |
| Approach | 102 | 0 | 107 | 0.0 | 0.143 | 28.7 | LOS C | 3.3 | 22.8 | 0.69 | 0.64 | 0.69 | 45.5 |
| West: New Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 18 | 0 | 19 | 0.0 | * 0.189 | 33.5 | LOS C | 1.3 | 9.6 | 0.94 | 0.72 | 0.94 | 41.1 |
| 11 T1 | 1 | 0 | 1 | 0.0 | * 0.189 | 28.9 | LOS C | 1.3 | 9.6 | 0.94 | 0.72 | 0.94 | 34.4 |
| 12 R 2 | 20 | 2 | 21 | 10.0 | 0.189 | 33.5 | LOS C | 1.3 | 9.6 | 0.94 | 0.72 | 0.94 | 38.0 |
| Approach | 39 | 2 | 41 | 5.1 | 0.189 | 33.4 | LOS C | 1.3 | 9.6 | 0.94 | 0.72 | 0.94 | 39.5 |
| All Vehicles | 389 | 8 | 409 | 2.1 | 0.212 | 33.4 | LOS C | 5.6 | 39.1 | 0.77 | 0.69 | 0.77 | 42.6 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID Crossing | Input Vol. ped/h | Dem. Flow ped/h | Aver. Delay <br> sec | Level of Service | $\begin{gathered} \text { ERAG } \\ \text { Qu } \\ \text { [ Ped } \\ \text { ped } \end{gathered}$ | CK <br> Dist ] <br> m | Prop. Effective Que Stop Rate |  | Travel Time sec | Travel Dist. <br> m | Aver. Speed <br> $\mathrm{m} / \mathrm{sec}$ |
| South: Aldington Road (670m) |  |  |  |  |  |  |  |  |  |  |  |
| P1 Full | 50 | 53 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 224.7 | 221.5 | 0.99 |
| East: New Road (500m) |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 50 | 53 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 216.6 | 211.0 | 0.97 |
| All | 0 | 105 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 220.6 | 216.3 | 0.98 |

## SITE LAYOUT

目Site: 6 [ID [6]. Aldington Road / Fife Kemps Creek South- AM
(Site Folder: 2026-AM - 75\% GFA)]
Aldington Road / Fife Kemps Creek South
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


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Organisation: ASON GROUP PTY LTD | Licence: NETWORK / 1PC | Created: Wednesday, 15 June 2022 2:28:49 PM
Project: C:IUsers\Arun Mohan\Desktop\Ason Group\P1815-2026 MRP revised modellingISIDRA Files\From SharepointlP1815 2026 SIDRA
Models Option 3 - double RT (2).sip9

## MOVEMENT SUMMARY

## 目 Site: 6 [ID [6]. Aldington Road / Fife Kemps Creek South- AM

(Site Folder: 2026-AM - 75\% GFA)]
Aldington Road / Fife Kemps Creek South
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=120$ seconds (Site User-Given Cycle Time)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INF } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | MES HV] veh/h |  | $\begin{aligned} & \text { AND } \\ & \text { WS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. <br> Satn <br> v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{aligned} & \text { CK OF } \\ & \text { UE } \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. Que | Effective Stop Rate |  | Aver. Speed <br> km/h |
| South: Aldington Road (580m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 62 | 38 | 65 | 61.3 | 0.197 | 38.2 | LOS C | 2.8 | 34.7 | 0.76 | 0.74 | 0.76 | 36.4 |
| 2 T1 | 24 | 2 | 25 | 8.3 | * 0.103 | 49.0 | LOS D | 1.3 | 10.5 | 0.90 | 0.66 | 0.90 | 36.6 |
| 3 R2 | 60 | 30 | 63 | 50.0 | 0.188 | 38.7 | LOS C | 2.7 | 33.2 | 0.76 | 0.74 | 0.76 | 35.0 |
| Approach | 146 | 70 | 154 | 47.9 | 0.197 | 40.2 | LOS C | 2.8 | 34.7 | 0.78 | 0.73 | 0.78 | 35.9 |
| East: New Road (450m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 7 | 6 | 7 | 85.7 | 0.259 | 49.0 | LOS D | 2.7 | 40.1 | 0.87 | 0.69 | 0.87 | 31.5 |
| $5 \quad \mathrm{~T} 1$ | 94 | 63 | 99 | 67.0 | * 0.259 | 43.9 | LOS D | 2.7 | 39.9 | 0.87 | 0.69 | 0.87 | 32.0 |
| 6 R2 | 1 | 0 | 1 | 0.0 | 0.003 | 44.1 | LOS D | 0.0 | 0.3 | 0.81 | 0.59 | 0.81 | 34.4 |
| Approach | 102 | 69 | 107 | 67.6 | 0.259 | 44.3 | LOS D | 2.7 | 40.1 | 0.87 | 0.69 | 0.87 | 32.0 |
| North: Aldington Road (670m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 1 | 0 | 1 | 0.0 | 0.006 | 32.6 | LOS C | 0.1 | 0.5 | 0.85 | 0.58 | 0.85 | 38.8 |
| 8 T1 | 2 | 1 | 2 | 50.0 | 0.008 | 41.0 | LOS C | 0.1 | 0.7 | 0.87 | 0.55 | 0.87 | 38.6 |
| 9 R2 | 8 | 7 | 8 | 87.5 | 0.030 | 37.2 | LOS C | 0.3 | 4.7 | 0.71 | 0.66 | 0.71 | 37.9 |
| Approach | 11 | 8 | 12 | 72.7 | 0.030 | 37.5 | LOS C | 0.3 | 4.7 | 0.75 | 0.63 | 0.75 | 38.1 |
| West: New Road (620m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 5 | 4 | 5 | 80.0 | * 0.185 | 35.2 | LOS C | 0.8 | 12.7 | 0.91 | 0.68 | 0.91 | 37.4 |
| 11 T1 | 38 | 37 | 40 | 97.4 | * 0.185 | 42.4 | LOS C | 1.2 | 18.3 | 0.92 | 0.68 | 0.92 | 32.1 |
| 12 R 2 | 1 | 0 | 1 | 0.0 | 0.004 | 52.6 | LOS D | 0.1 | 0.4 | 0.88 | 0.59 | 0.88 | 32.6 |
| Approach | 44 | 41 | 46 | 93.2 | 0.185 | 41.8 | LOS C | 1.2 | 18.3 | 0.92 | 0.68 | 0.92 | 32.7 |
| All <br> Vehicles | 303 | 188 | 319 | 62.0 | 0.259 | 41.7 | LOS C | 2.8 | 40.1 | 0.83 | 0.70 | 0.83 | 34.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Input Vol. <br> ped/h | Dem. Flow ped/h | Aver. Delay | Level of Service | VERAC <br> [Ped ped | $\square$ | Prop. Que | Effective Stop Rate | Travel Time | Travel Dist. <br> m | Aver. Speed <br> $\mathrm{m} / \mathrm{sec}$ |
| South: Aldington Road (580m) |  |  |  |  |  |  |  |  |  |  |  |
| P1 Full | 50 | 53 | 24.8 | LOS C | 0.1 | 0.1 | 0.90 | 0.90 | 194.4 | 220.5 | 1.13 |
| East: New Road (450m) |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 50 | 53 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 225.0 | 222.0 | 0.99 |
| North: Aldington Road (670m) |  |  |  |  |  |  |  |  |  |  |  |


| P3 Full | 50 | 53 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 223.9 | 220.5 | 0.98 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| West: New Road $(620 \mathrm{~m})$ |  |  |  |  |  |  |  |  |  |  |  |
| P4 Full | 50 | 53 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 224.7 | 221.5 | 0.99 |
| All | 0 | 211 | 46.9 | LOS E | 0.2 | 0.2 | 0.94 | 0.94 | 217.0 | 221.1 | 1.02 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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Organisation: ASON GROUP PTY LTD | Licence: NETWORK / 1PC | Processed: Wednesday, 15 June 2022 2:26:56 PM
Project: C:IUsers\Arun Mohan\Desktop\Ason Group\P1815-2026 MRP revised modellingISIDRA Files\From SharepointlP1815 2026 SIDRA Models Option 3 - double RT (2).sip9

## MOVEMENT SUMMARY

## 目 Site: 6 [ID [6]. Aldington Road / Fife Kemps Creek South- PM

(Site Folder: 2026-PM - 75\% GFA)]
Aldington Road / Fife Kemps Creek South
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=120$ seconds (Site User-Given Cycle Time)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | T HV ] veh/h |  | $\begin{gathered} \text { AND } \\ \text { WS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. <br> Satn <br> v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver Speed km/h |
| South: Aldington Road (580m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 159 | 30 | 167 | 18.9 | 0.358 | 39.3 | LOS C | 7.5 | 68.6 | 0.81 | 0.79 | 0.81 | 36.2 |
| 2 T1 | 21 | 1 | 22 | 4.8 | * 0.083 | 48.6 | LOS D | 1.1 | 8.3 | 0.90 | 0.65 | 0.90 | 36.7 |
| 3 R2 | 159 | 22 | 167 | 13.8 | * 0.405 | 45.1 | LOS D | 8.1 | 68.6 | 0.87 | 0.79 | 0.87 | 33.2 |
| Approach | 339 | 53 | 357 | 15.6 | 0.405 | 42.6 | LOS D | 8.1 | 68.6 | 0.84 | 0.78 | 0.84 | 34.9 |
| East: New Road (450m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 80 | 18 | 84 | 22.5 | 0.406 | 42.7 | LOS D | 8.0 | 74.5 | 0.86 | 0.75 | 0.86 | 33.7 |
| 5 T1 | 225 | 62 | 237 | 27.6 | * 0.406 | 39.4 | LOS C | 8.0 | 74.5 | 0.87 | 0.73 | 0.87 | 33.1 |
| 6 R2 | 17 | 0 | 18 | 0.0 | 0.037 | 39.9 | LOS C | 0.8 | 5.4 | 0.78 | 0.67 | 0.78 | 35.6 |
| Approach | 322 | 80 | 339 | 24.8 | 0.406 | 40.2 | LOS C | 8.0 | 74.5 | 0.86 | 0.74 | 0.86 | 33.4 |
| North: Aldington Road (670m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $7 \quad$ L2 | 1 | 1 | 1 | 100.0 | 0.006 | 23.0 | LOS B | 0.0 | 0.7 | 0.67 | 0.59 | 0.67 | 40.7 |
| 8 T1 | 2 | 0 | 2 | 0.0 | 0.007 | 45.3 | LOS D | 0.1 | 0.7 | 0.87 | 0.55 | 0.87 | 37.5 |
| 9 R2 | 88 | 5 | 93 | 5.7 | 0.196 | 42.3 | LOS C | 4.2 | 30.8 | 0.81 | 0.75 | 0.81 | 36.7 |
| Approach | 91 | 6 | 96 | 6.6 | 0.196 | 42.1 | LOS C | 4.2 | 30.8 | 0.81 | 0.75 | 0.81 | 36.8 |
| West: New Road (620m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 76 | 5 | 80 | 6.6 | 0.295 | 27.5 | LOS B | 2.8 | 24.7 | 0.88 | 0.75 | 0.88 | 40.7 |
| 11 T1 | 49 | 48 | 52 | 98.0 | * 0.295 | 43.1 | LOS D | 2.8 | 24.7 | 0.92 | 0.73 | 0.92 | 31.8 |
| 12 R 2 | 4 | 3 | 4 | 75.0 | 0.041 | 56.5 | LOS D | 0.2 | 3.9 | 0.90 | 0.66 | 0.90 | 30.7 |
| Approach | 129 | 56 | 136 | 43.4 | 0.295 | 34.3 | LOS C | 2.8 | 30.6 | 0.90 | 0.74 | 0.90 | 36.9 |
| All <br> Vehicles | 881 | 195 | 927 | 22.1 | 0.406 | 40.5 | LOS C | 8.1 | 74.5 | 0.86 | 0.75 | 0.86 | 34.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov <br> ID Crossing | Input Vol. ped/h | Dem. <br> Flow <br> ped/h | Aver. Delay sec | Level of Service |  | $\begin{aligned} & \text { ACK OF } \\ & \text { E } \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. Que | Stop <br> Rate | Trave Time sec |  | Aver. Speed |
| South: Aldington Road (580m) |  |  |  |  |  |  |  |  |  |  |  |
| P1 Full | 50 | 53 | 24.4 | LOS C | 0.1 | 0.1 | 0.90 | 0.90 | 194.0 | 220.5 | 1.14 |
| East: New Road (450m) |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 50 | 53 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 225.0 | 222.0 | 0.99 |
| North: Aldington Road (670m) |  |  |  |  |  |  |  |  |  |  |  |


| P3 Full | 50 | 53 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 223.9 | 220.5 | 0.98 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| West: New Road $(620 \mathrm{~m})$ |  |  |  |  |  |  |  |  |  |  |  |
| P4 Full | 50 | 53 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 224.7 | 221.5 | 0.99 |
| All | 0 | 211 | 46.8 | LOS E | 0.2 | 0.2 | 0.94 | 0.94 | 216.9 | 221.1 | 1.02 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## SITE LAYOUT

## 目 Site: 7 [ID [7]. Aldington Road / Abbotts Road - AM (Site

Folder: 2026 - AM - 75\% GFA)]
Aldington Road / Abbotts Road
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


New Road (130m)

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## MOVEMENT SUMMARY

## 目 Site: 7 [ID [7]. Aldington Road / Abbotts Road - AM (Site

Folder: 2026 - AM - 75\% GFA)]
Aldington Road / Abbotts Road
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=120$ seconds (Site User-Given Phase Times)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | JT <br> MES <br> HV ] <br> veh/h |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service |  | CK OF <br> UE Dist ] m | Prop. Que | Effective Stop Rate |  | Aver Speed <br> km/h |
| East: New Road (130m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 T1 | 42 | 17 | 44 | 40.5 | 0.049 | 5.3 | LOS A | 0.7 | 8.5 | 0.31 | 0.24 | 0.31 | 49.9 |
| 6 R2 | 39 | 19 | 41 | 48.7 | * 0.207 | 52.1 | LOS D | 2.1 | 23.7 | 0.89 | 0.74 | 0.89 | 24.1 |
| Approach | 81 | 36 | 85 | 44.4 | 0.207 | 27.8 | LOS B | 2.1 | 23.7 | 0.59 | 0.48 | 0.59 | 31.9 |
| North: Aldington Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $7 \quad \mathrm{~L} 2$ | 1 | 0 | 1 | 0.0 | 0.037 | 48.8 | LOS D | 0.3 | 4.4 | 0.84 | 0.68 | 0.84 | 25.9 |
| 9 R2 | 12 | 7 | 13 | 58.3 | * 0.037 | 50.1 | LOS D | 0.3 | 4.4 | 0.84 | 0.67 | 0.84 | 29.9 |
| Approach | 13 | 7 | 14 | 53.8 | 0.037 | 50.0 | LOS D | 0.3 | 4.4 | 0.84 | 0.67 | 0.84 | 29.6 |
| West: Abbotts Road (400m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 105 | 51 | 111 | 48.6 | 0.208 | 24.8 | LOS B | 3.7 | 43.8 | 0.60 | 0.73 | 0.60 | 39.2 |
| 11 T1 | 155 | 31 | 163 | 20.0 | * 0.214 | 19.6 | LOS B | 5.4 | 47.7 | 0.60 | 0.58 | 0.60 | 36.4 |
| Approach | 260 | 82 | 274 | 31.5 | 0.214 | 21.7 | LOS B | 5.4 | 47.7 | 0.60 | 0.64 | 0.60 | 37.9 |
| All Vehicles | 354 | 125 | 373 | 35.3 | 0.214 | 24.1 | LOS B | 5.4 | 47.7 | 0.61 | 0.61 | 0.61 | 36.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }_{\text {ID }}^{\text {Mov }} \text { Crossing }$ | Input Vol. <br> ped/h | Dem. Flow ped/h | Aver. Delay <br> sec |  | Level of AVERAGE BACK OF Service QUEUE | $\begin{aligned} & \text { ACK OF } \\ & \text { IE } \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. EffectiveQue $\begin{aligned} & \text { Stop } \\ & \\ & \\ & \\ & \text { Rate }\end{aligned}$ |  | Travel Time <br> sec $\qquad$ | Travel Dist. $\qquad$ | Aver. Speed <br> $\mathrm{m} / \mathrm{sec}$ |
| East: New Road (130m) |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 50 | 53 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 222.7 | 219.0 | 0.98 |
| All Pedestrians | 0 | 53 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 222.7 | 219.0 | 0.98 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## MOVEMENT SUMMARY

目 Site: 8v [ID [7]. Aldington Road / Abbotts Road - PM (Site
Folder: 2026 - PM - 75\% GFA)]
Aldington Road / Abbotts Road
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=120$ seconds (Site User-Given Phase Times)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | JT MES HV] veh/h |  | $\begin{aligned} & \text { AND } \\ & \text { WS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% <br> [ Veh. veh | CK OF UE Dist ] | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| East: New Road (130m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 T1 | 142 | 30 | 149 | 21.1 | 0.102 | 12.3 | LOS A | 2.0 | 18.0 | 0.43 | 0.35 | 0.43 | 42.2 |
| 6 R2 | 8 | 0 | 8 | 0.0 | * 0.102 | 41.8 | LOS C | 1.8 | 15.4 | 0.80 | 0.63 | 0.80 | 28.9 |
| Approach | 150 | 30 | 158 | 20.0 | 0.102 | 13.9 | LOS A | 2.0 | 18.0 | 0.45 | 0.36 | 0.45 | 41.0 |
| North: Aldington Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 1 | 0 | 1 | 0.0 | 0.187 | 50.3 | LOS D | 2.3 | 22.5 | 0.88 | 0.75 | 0.88 | 25.4 |
| 9 R2 | 87 | 23 | 92 | 26.4 | * 0.187 | 51.0 | LOS D | 2.3 | 22.5 | 0.88 | 0.75 | 0.88 | 30.1 |
| Approach | 88 | 23 | 93 | 26.1 | 0.187 | 51.0 | LOS D | 2.3 | 22.6 | 0.88 | 0.75 | 0.88 | 30.1 |
| West: Abbotts Road (400m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 324 | 50 | 341 | 15.4 | * 0.459 | 27.2 | LOS B | 13.0 | 112.9 | 0.70 | 0.79 | 0.70 | 38.9 |
| 11 T1 | 84 | 25 | 88 | 29.8 | 0.129 | 18.8 | LOS B | 2.8 | 27.6 | 0.57 | 0.55 | 0.57 | 37.0 |
| Approach | 408 | 75 | 429 | 18.4 | 0.459 | 25.4 | LOS B | 13.0 | 112.9 | 0.68 | 0.74 | 0.68 | 38.7 |
| All Vehicles | 646 | 128 | 680 | 19.8 | 0.459 | 26.2 | LOS B | 13.0 | 112.9 | 0.65 | 0.65 | 0.65 | 37.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \\ & \text { Crossing } \end{aligned}$ | Input Vol. <br> ped/h | Dem. Flow $\mathrm{ped} / \mathrm{h}$ | Aver. Delay sec | Level of Service | VERA <br> [Ped ped | ACK OF E Dist ] m | Prop. E Que | ective <br> Stop <br> Rate | Travel Time sec | Travel Dist. <br> m | Aver. Speed <br> $\mathrm{m} / \mathrm{sec}$ |
| East: New Road (130m) |  |  |  |  |  |  |  |  |  |  |  |
| P2 Full | 50 | 53 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 222.7 | 219.0 | 0.98 |
| All <br> Pedestrians | 0 | 53 | 54.3 | LOS E | 0.2 | 0.2 | 0.95 | 0.95 | 222.7 | 219.0 | 0.98 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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## SITE LAYOUT

© Site: 8 [ID [8]. Internal Road Roundabout (Mirvac) - AM (Site
Folder: 2026-AM - 75\% GFA)]
Internal Road Roundabout (Mirvac)
Site Category: (None)
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


## MOVEMENT SUMMARY

$\nabla$ Site: 8 [ID [8]. Internal Road Roundabout (Mirvac) - AM (Site
Folder: 2026 - AM - 75\% GFA)]
Internal Road Roundabout (Mirvac)
Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { INP } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | UT MES HV] veh/h |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay sec $\qquad$ | Level of Service | $\begin{gathered} \text { 95\% B B } \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | CK OF Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed $\mathrm{km} / \mathrm{h}$ |
| South: New Road (370m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 223 | 121 | 235 | 54.3 | 0.207 | 3.1 | LOS A | 1.2 | 15.6 | 0.31 | 0.37 | 0.31 | 47.8 |
| 2 T 1 | 1 | 0 | 1 | 0.0 | 0.002 | 2.0 | LOS A | 0.0 | 0.1 | 0.25 | 0.45 | 0.25 | 48.5 |
| 3 u U | 1 | 0 | 1 | 0.0 | 0.002 | 9.9 | LOSA | 0.0 | 0.1 | 0.25 | 0.45 | 0.25 | 50.5 |
| Approach | 225 | 121 | 237 | 53.8 | 0.207 | 3.2 | LOS A | 1.2 | 15.6 | 0.31 | 0.37 | 0.31 | 47.8 |
| North: New Road (1000m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 29 | 10 | 31 | 34.5 | 0.044 | 4.7 | LOSA | 0.2 | 2.5 | 0.51 | 0.45 | 0.51 | 49.2 |
| 9 R2 | 68 | 26 | 72 | 38.2 | 0.069 | 9.5 | LOSA | 0.3 | 3.8 | 0.47 | 0.61 | 0.47 | 47.7 |
| $9 \mathrm{u} \quad \mathrm{U}$ | 1 | 0 | 1 | 0.0 | 0.069 | 10.6 | LOS A | 0.3 | 3.8 | 0.47 | 0.61 | 0.47 | 49.2 |
| Approach | 98 | 36 | 103 | 36.7 | 0.069 | 8.1 | LOS A | 0.3 | 3.8 | 0.48 | 0.56 | 0.48 | 48.1 |
| West: New Road (600m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 1 | 0 | 1 | 0.0 | 0.001 | 2.2 | LOS A | 0.0 | 0.0 | 0.03 | 0.31 | 0.03 | 49.4 |
| 12 R 2 | 292 | 76 | 307 | 26.0 | 0.192 | 7.7 | LOS A | 1.1 | 10.1 | 0.03 | 0.55 | 0.03 | 48.0 |
| 12 u U | 1 | 0 | 1 | 0.0 | 0.192 | 9.5 | LOS A | 1.1 | 10.1 | 0.03 | 0.55 | 0.03 | 49.8 |
| Approach | 294 | 76 | 309 | 25.9 | 0.192 | 7.7 | LOS A | 1.1 | 10.1 | 0.03 | 0.55 | 0.03 | 48.0 |
| All <br> Vehicles | 617 | 233 | 649 | 37.8 | 0.207 | 6.1 | LOS A | 1.2 | 15.6 | 0.21 | 0.49 | 0.21 | 48.0 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 8 [ID [8]. Internal North Rounabout (Mirvac)- PM (Site
Folder: 2026 - PM - 75\% GFA)]
Internal Road Roundabout (Mirvac)
Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INP } \\ & \text { VOLu } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | JT <br> MES <br> HV ] <br> veh/h |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service |  | CK OF <br> UE Dist ] m | Prop. Que | Effective Stop Rate |  | Aver Speed <br> km/h |
| South: New Road (370m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 390 | 106 | 411 | 27.2 | 0.297 | 3.0 | LOS A | 1.9 | 18.4 | 0.35 | 0.39 | 0.35 | 47.9 |
| 2 T1 | 1 | 0 | 1 | 0.0 | 0.002 | 2.1 | LOSA | 0.0 | 0.1 | 0.28 | 0.45 | 0.28 | 48.5 |
| 3 u U | 1 | 0 | 1 | 0.0 | 0.002 | 10.0 | LOSA | 0.0 | 0.1 | 0.28 | 0.45 | 0.28 | 50.4 |
| Approach | 392 | 106 | 413 | 27.0 | 0.297 | 3.0 | LOS A | 1.9 | 18.4 | 0.35 | 0.39 | 0.35 | 47.9 |
| North: New Road (1000m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 93 | 18 | 98 | 19.4 | 0.095 | 3.2 | LOS A | 0.5 | 4.2 | 0.43 | 0.37 | 0.43 | 49.5 |
| 9 R2 | 99 | 29 | 104 | 29.3 | 0.082 | 8.8 | LOSA | 0.4 | 3.8 | 0.40 | 0.58 | 0.40 | 48.0 |
| 9 u U | 1 | 0 | 1 | 0.0 | 0.082 | 10.4 | LOSA | 0.4 | 3.8 | 0.40 | 0.58 | 0.40 | 49.3 |
| Approach | 193 | 47 | 203 | 24.4 | 0.095 | 6.1 | LOS A | 0.5 | 4.2 | 0.41 | 0.48 | 0.41 | 48.6 |
| West: New Road (600m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 1 | 0 | 1 | 0.0 | 0.001 | 2.2 | LOS A | 0.0 | 0.0 | 0.03 | 0.31 | 0.03 | 49.4 |
| 12 R2 | 200 | 92 | 211 | 46.0 | 0.150 | 7.8 | LOSA | 0.8 | 9.2 | 0.04 | 0.53 | 0.04 | 47.7 |
| 12u U | 1 | 0 | 1 | 0.0 | 0.150 | 9.5 | LOS A | 0.8 | 9.2 | 0.04 | 0.53 | 0.04 | 49.8 |
| Approach | 202 | 92 | 213 | 45.5 | 0.150 | 7.8 | LOS A | 0.8 | 9.2 | 0.04 | 0.53 | 0.04 | 47.7 |
| All <br> Vehicles | 787 | 245 | 828 | 31.1 | 0.297 | 5.0 | LOS A | 1.9 | 18.4 | 0.28 | 0.45 | 0.28 | 48.1 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Models Option 3 - double RT (2).sip9

## SITE LAYOUT

© Site: 9 [ID [9]. Internal Road Roundabout (AItis ) - AM (Site
Folder: 2026 - AM - 75\% GFA)]
Internal Road Roundabout Altis
Site Category: (None)
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


## MOVEMENT SUMMARY

$\nabla$ Site: 9 [ID [9]. Internal Road Roundabout (Altis ) - AM (Site
Folder: 2026 - AM - 75\% GFA)]
Internal Road Roundabout Altis
Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{array}{r} \text { INP } \\ \text { VOLU } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | UT MES HV] veh/h |  | $\begin{aligned} & \text { AND } \\ & \text { WS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay $\qquad$ sec | Level of Service | $\begin{aligned} & \text { 95\% B B } \\ & \text { QU } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> $\mathrm{km} / \mathrm{h}$ |
| South: New Road (620m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 108 | 46 | 114 | 42.6 | 0.142 | 2.7 | LOS A | 0.8 | 9.7 | 0.18 | 0.28 | 0.18 | 48.6 |
| 2 T1 | 194 | 111 | 204 | 57.2 | 0.142 | 2.2 | LOSA | 0.8 | 9.7 | 0.20 | 0.24 | 0.20 | 50.2 |
| Approach | 302 | 157 | 318 | 52.0 | 0.142 | 2.3 | LOSA | 0.8 | 10.2 | 0.19 | 0.25 | 0.19 | 49.6 |
| North: New Road (370m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 295 | 76 | 311 | 25.8 | 0.129 | 2.0 | LOSA | 0.8 | 7.3 | 0.22 | 0.25 | 0.22 | 50.0 |
| 9 R2 | 28 | 10 | 29 | 35.7 | 0.129 | 8.3 | LOSA | 0.7 | 7.5 | 0.23 | 0.31 | 0.23 | 50.1 |
| Approach | 323 | 86 | 340 | 26.6 | 0.129 | 2.5 | LOSA | 0.8 | 7.5 | 0.22 | 0.26 | 0.22 | 50.0 |
| West: New Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 31 | 15 | 33 | 48.4 | 0.106 | 4.8 | LOS A | 0.5 | 4.8 | 0.45 | 0.60 | 0.45 | 45.1 |
| 12 R 2 | 45 | 9 | 47 | 20.0 | 0.106 | 9.4 | LOSA | 0.5 | 4.8 | 0.45 | 0.60 | 0.45 | 48.1 |
| Approach | 76 | 24 | 80 | 31.6 | 0.106 | 7.5 | LOSA | 0.5 | 4.8 | 0.45 | 0.60 | 0.45 | 47.0 |
| All <br> Vehicles | 701 | 267 | 738 | 38.1 | 0.142 | 3.0 | LOS A | 0.8 | 10.2 | 0.23 | 0.29 | 0.23 | 49.5 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 9 [ID [9]. Internal South Rounabout (Altis ) - PM (Site
Folder: 2026 - PM - 75\% GFA)]

```
Internal Road Roundabout (Altis )
Site Category: (None)
Roundabout
```

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { INP } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | JT MES HV ] veh/h |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay $\qquad$ sec | Level of Service | $\begin{aligned} & \text { 95\% B } \\ & \text { QUt } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: New Road (620m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 300 | 41 | 316 | 13.7 | 0.277 | 3.2 | LOSA | 1.7 | 15.0 | 0.40 | 0.40 | 0.40 | 48.1 |
| 2 T1 | 346 | 99 | 364 | 28.6 | 0.277 | 3.0 | LOSA | 1.7 | 15.0 | 0.43 | 0.37 | 0.43 | 49.3 |
| Approach | 646 | 140 | 680 | 21.7 | 0.277 | 3.1 | LOS A | 1.7 | 15.9 | 0.42 | 0.38 | 0.42 | 48.7 |
| North: New Road (370m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 T1 | 133 | 87 | 140 | 65.4 | 0.122 | 2.0 | LOSA | 0.8 | 6.8 | 0.15 | 0.25 | 0.15 | 49.9 |
| 9 R2 | 162 | 24 | 171 | 14.8 | 0.122 | 7.7 | LOSA | 0.8 | 6.8 | 0.13 | 0.51 | 0.13 | 47.8 |
| Approach | 295 | 111 | 311 | 37.6 | 0.122 | 5.1 | LOS A | 0.8 | 9.4 | 0.14 | 0.39 | 0.14 | 48.8 |
| West: New Road (500m) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 48 | 10 | 51 | 20.8 | 0.096 | 4.6 | LOSA | 0.4 | 4.1 | 0.53 | 0.60 | 0.53 | 46.5 |
| 12 R2 | 18 | 8 | 19 | 44.4 | 0.096 | 10.6 | LOSA | 0.4 | 4.1 | 0.53 | 0.60 | 0.53 | 49.0 |
| Approach | 66 | 18 | 69 | 27.3 | 0.096 | 6.2 | LOSA | 0.4 | 4.1 | 0.53 | 0.60 | 0.53 | 47.3 |
| All <br> Vehicles | 1007 | 269 | 1060 | 26.7 | 0.277 | 3.9 | LOS A | 1.7 | 15.9 | 0.34 | 0.40 | 0.34 | 48.6 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## Attachment 3 - Traffic Signal Warrant Analysis

TABLE 6 TRAFFIC WARRANT FOR 2026 - 1,290,000M² GFA

| ID | Intersection | Warrant A | Major Road $>900$ vph | Minor>100vph | Major>900vph | Minor>100vph | Traffic Flow Warrant Met? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Warrant B | Major Road $>600 \mathrm{vph}$ | Minor>200vph | Major>600vph | Minor>200vph |  |
|  |  | Hour | South (veh) | East (veh) | North (veh) | West (veh) |  |
| 1 | Mamre Road / Bakers Lane | 7-8AM | 1,415 | 164 | 2,217 | 150 | Yes |
|  |  | 8-9AM | 1,525 | 429 | 2,120 | 215 | Yes |
|  |  | 3-4PM | 1,774 | 573 | 1,703 | 355 | Yes |
|  |  | 4-5PM | 1,734 | 497 | 1,502 | 412 | Yes |
| 2 | Mamre Road / Mirvac Access | 7-8AM | 1,101 | 410 | 1,595 | - | Yes |
|  |  | 8-9AM | 1,180 | 509 | 1,561 | - | Yes |
|  |  | 3-4PM | 1,378 | 516 | 1,663 | - | Yes |
|  |  | 4-5PM | 1,381 | 551 | 1,603 | - | Yes |
| 4 | Mamre Road / Abbotts Road | $3-4 \mathrm{PM}$ | 1,600 | 240 | 1,973 | - | Yes |
|  |  | 4-5PM | 1,663 | 295 | 1,906 | - | Yes |
|  |  | 5-6PM | 1,385 | 163 | 1,791 | - | Yes |
|  |  | 6-7PM | 968 | 151 | 1,141 | - | Yes |
| 5 | Aldington Road / Fife Kemps Creek (North) | 7-8AM | 33 | 87 | 318 | 21 | No |
|  |  | 8-9AM | 74 | 103 | 240 | 26 | No |
|  |  | $3-4 \mathrm{PM}$ | 119 | 129 | 102 | 39 | No |
|  |  | 4-5PM | 173 | 209 | 58 | 53 | No |
| 6 | Aldington Road / Fife Kemps Creek (South) | 7-8AM | 146 | 102 | 11 | 44 | No |
|  |  | 8-9AM | 152 | 115 | 10 | 74 | No |
|  |  | 3-4PM | 339 | 322 | 91 | 129 | No |
|  |  | 4-5PM | 382 | 246 | 50 | 247 | No |
| 7 | Aldington Road / Abbotts Road | 7-8AM | - | 81 | 13 | 260 | No |
|  |  | 8-9AM | - | 95 | 21 | 228 | No |
|  |  | 3-4PM | - | 150 | 88 | 408 | No |
|  |  | 4-5PM | - | 157 | 196 | 468 | No |

TABLE 7 TRAFFIC WARRANT FOR 2036 NETWORK - FULL PRECINCT

| ID | Intersection | Warrant A | Major Road $>900 \mathrm{vph}$ | Minor>100vph | Major $>900 \mathrm{vph}$ | Minor $>100 \mathrm{vph}$ | Traffic Flow Warrant Met? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Warrant B | Major Road>600vph | Minor>200vph | Major>600vph | Minor>200vph |  |
|  |  | Hour | South (veh) | East (veh) | North (veh) | West (veh) |  |
| 1 | Mamre Road / Bakers Lane | 7-8AM | 2,137 | 902 | 2,881 | 233 | Yes |
|  |  | 8-9AM | 2,250 | 922 | 2,703 | 312 | Yes |
|  |  | 3-4PM | 2,278 | 875 | 1,703 | 355 | Yes |
|  |  | 4-5PM | 1,584 | 759 | 1,924 | 496 | Yes |
| 2 | Mamre Road / Mirvac Access | 7-8AM | 1,898 | 389 | 2,761 | 245 | Yes |
|  |  | 8-9AM | 2,027 | 259 | 2,952 | 277 | Yes |
|  |  | 3-4PM | 2,094 | 162 | 2,878 | 277 | Yes |
|  |  | 4-5PM | 2,192 | 166 | 1,371 | 752 | Yes |
| 4 | Mamre Road / Abbotts Road | $3-4 \mathrm{PM}$ | 2,505 | 138 | 2,180 | 134 | Yes |
|  |  | 4-5PM | 2,661 | 157 | 2,157 | 174 | Yes |
|  |  | 5-6PM | 2,814 | 138 | 2,013 | 210 | Yes |
|  |  | 6-7PM | 2,000 | 123 | 1,490 | 208 | Yes |
| 5 | Aldington Road / Fife Kemps Creek (North) | 7-8AM | 655 | 201 | 2,111 | 327 | Yes |
|  |  | 8-9AM | 717 | 223 | 2,193 | 224 | Yes |
|  |  | 3-4PM | 839 | 260 | 1,913 | 264 | Yes |
|  |  | 4-5PM | 601 | 416 | 1,454 | 205 | Yes |
| 6 | Aldington Road / Fife Kemps Creek (South) | 7-8AM | 720 | 203 | 1,044 | 211 | Yes |
|  |  | 8-9AM | 798 | 202 | 1,082 | 206 | Yes |
|  |  | 3-4PM | 859 | 210 | 1,045 | 210 | Yes |
|  |  | 4-5PM | 648 | 237 | 1,156 | 203 | Yes |
| 7 | Aldington Road / Abbotts Road | 7-8AM | 119 | 123 | 1,088 | 1,240 | Yes |
|  |  | 8-9AM | 143 | 112 | 1,065 | 1,171 | Yes |
|  |  | 3-4PM | 300 | 108 | 1,552 | 1,021 | Yes |
|  |  | 4-5PM | 202 | 201 | 1,266 | 881 | Yes |



Mamre Road Precinct-Houriy Trip Generation Summany (S.56\%)

| Start Time | All Vehicle | Light vehicle | Heary Vehicle | Rigid | Semitrailer | B-double |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0:00 | 34 | 0 | 34 | 0 | 20 | 14 |
| 1:00 | 161 | 110 | 51 | 0 | 40 | 11 |
| 2:00 | 178 | 110 | 68 | 27 | 30 | 11 |
| 3:00 | 281 | 220 | 61 | 27 | 20 | 14 |
| 4:00 | 905 | 769 | 136 | 81 | 30 | 25 |
| 5:00 | 1,636 | 1,318 | 318 | 188 | 91 | 39 |
| 6:00 | 2,203 | 1,758 | 445 | 295 | 111 | 39 |
| 7:00 | 2,301 | 1,758 | 543 | 349 | 141 | 54 |
| 8:00 | 2,052 | 1,428 | 624 | 429 | 141 | 54 |
| 9:00 | 1,780 | 1,099 | 681 | 483 | 141 | 57 |
| 10:00 | 1,549 | 879 | 670 | 456 | 171 | ${ }^{43}$ |
| 11:00 | 1,659 | 989 | 670 | 456 | 171 | 43 |
| 12:00 | 1,602 | 989 | 613 | 429 | 141 | 43 |
| 13:00 | 1,859 | 1,209 | 650 | 456 | 151 | ${ }^{43}$ |
| 14:00 | 2,197 | 1,648 | 549 | 403 | 111 | ${ }^{36}$ |
| 15:00 | 2,257 | 1,758 | 499 | 349 | 111 | 39 |
| 16:00 | 2,459 | 1,978 | 482 | 349 | 101 | 32 |
| 17:00 | 1,842 | 1,538 | 304 | 215 | 60 | 29 |
| 18:00 | 1,232 | 989 | 243 | 161 | 60 | 21 |
| 19:00 | 651 | 549 | 102 | 54 | 30 | 18 |
| 20:00 | 428 | 330 | 98 | 54 | 30 | 14 |
| 21:00 | 428 | 330 | 98 | 54 | 30 | 14 |
| 22:00 | 295 | 220 | 75 | 27 | 30 | 18 |
| 23:00 | 74 | 0 | 74 | 27 | 40 | 7 |
| Total | 30,062 | 21,973 | 8,089 | 5,367 | 2,004 | 718 |


[^0]:    Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)

[^1]:    Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)

[^2]:    Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)

[^3]:    Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)

