

Appendix D

Air Quality Impact Assessment Report

FINAL REPORT

Woy Woy Waste Management Facility Air Quality Impact Assessment

Prepared for

Gosford City Council

49 Mann St
Gosford NSW 2250

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Executive Summary

URS (Australia) Pty Ltd has been commissioned by Gosford City Council to undertake an air quality impact assessment for the proposed Woy Woy Waste Management Facility, to be located at the Woy Woy Landfill site. Upon development, it is proposed that the Facility will accept 70,000 tonnes per annum of Municipal Solid Waste to an Alternative Waste Technology (AWT) facility. The proposed development will also include an enclosed green waste facility which would accept 30,000 tonnes per annum of green waste and 15,000 tonnes per annum of biosolids. As part of processing of the waste, compost will be created and the Facility will also incorporate a compost maturation and storage area.

The air quality impact assessment of the proposed development has been assessed against the Department of Environment and Climate Change, incorporating the New South Wales Environment Protection Authority (NSW EPA) Impact Assessment Criteria as specified within NSW EPA (2005) *Approved methods for the modelling and assessment of air pollutants within New South Wales* and NSW EPA (2006) *Technical framework: Assessment and management of odour from stationary source in NSW*. Air quality criteria provided within these documents have been set with the aim of protecting public health, and to provide mitigation against nuisance odour.

Due to the nature of the processing on site, the primary air quality impact of concern is odour. The proposed processes at the site have odorous emissions resulting from the decomposition of Municipal Solid Waste, Green Waste and Biosolids. The proposed facility aims to reduce emissions by enclosing the processes, extracting the odorous air from the buildings and passing it through biofilters. Emission estimates of odour have been made for the proposed development based on measurements undertaken for similar activities on other sites both within Australia and internationally.

The dispersion of odorous emissions was modelled using the Calpuff V6.0 dispersion modelling package, which has the capability to address the complex terrain surrounding the site. The nearest Bureau of Meteorology station was located at Narara, north of Gosford (14km north of the site), which due to its remote and sheltered location, was not considered suitable for implementation in modelling applications. On this basis a synthetic meteorological file was generated using the CSIRO's TAPM package, which uses a synoptic weather database with terrain and land use information to calculate hourly three-dimensional weather data. These TAPM results were processed within the meteorological pre-processor CALMET to generate the wind fields within the terrain surrounding the site.

The results from the dispersion modelling show that the peak odour concentration as a result of site activities will be less than 1.7 Odour Units (OU) at the nearest sensitive receptor (99.0 percentile, nose response time) against a 2 OU criteria.

In relation to other atmospheric pollutants, the combustion of fuel including the use of motor vehicles results in the liberation of nitrogen and carbon in all oxidation states as well as particulate matter. Representative background data was examined for 2005, and all combustion and industrial related pollutants were found to be below the limit values with the exception of PM₁₀. In December 2005, the maximum background concentration of PM₁₀ during the month, as measured over 24 hours, was equal to the limit value of 50µgm⁻³. It is likely that this occurred due to a natural particulate event and may be discounted from the record.

Executive Summary

Combustion on site will be limited to site and delivery vehicles. It is predicted that there will be an additional 8 truck deliveries per day to the site as a result of the proposed development. Such a low number of vehicles will not add appreciably to ambient pollutant concentrations, and given the low background levels, this additional activity will not result in an exceedance of the assessment criteria for nitrogen dioxide and carbon monoxide.

The greatest potential for the generation of suspended particulates and PM₁₀ is as a result of site vehicles passing over unsealed roads. An undertaking to seal all site access roads and main internal haul roads will reduce the potential for dust generation. Areas where vehicles pass over unsealed ground will be sprayed with water to mitigate dust emissions. Using these methods, it is considered that the generation of dust will be minimised, and that concentrations at the nearest sensitive receptors will not exceed the assessment thresholds.

The consideration of likely emissions and the results of dispersion modelling therefore indicate that the proposed activities will not adversely impact the air quality at nearby sensitive receptors.

1.1 Introduction

Gosford City Council (Council) is currently in the process of augmenting their Waste Management Facility (WMF) at Woy Woy landfill. The proposed development is to include three primary facilities, namely:

1. An enclosed Alternative Waste Technology (AWT) Treatment Facility. The AWT facility will treat up to 70,000 tonnes of municipal solid wastes (MSW) per year. The type of AWT will be determined through a separate tendering process; however it is likely that Council will only consider fully enclosed systems at the site.
2. An enclosed Greenwaste Processing Facility. This facility will receive, sort and shred garden organics. It is understood an enclosed type composting facility is preferred, with the capacity for up to 30,000 tonnes of source separated municipal greenwaste and 15,000 tonnes of biosolids, per year.
3. Matured greenwaste / biosolids Compost Processing and Storage area.

Prior to this detailed investigation, a preliminary odour assessment was performed by URS. In the NSW odour guidelines, (NSW EPA, 2001), three levels of odour assessment are provided, namely Levels 1, 2 and 3, each successive level being more detailed and refined. A Level 1 assessment uses simple calculations and presumes worst case impacts to assess whether a more refined assessment (Level 2 or 3) is necessary. Levels 2 and 3 are more refined and use atmospheric dispersion modelling which incorporates site specific geographic and meteorological data.

The preliminary assessment comprised a Level 2 assessment and used the dispersion model AUSPLUME V6.0, with generic (non-site specific) meteorological data. The results displayed the potential for an adverse impact at the nearest receptors, justifying the Level 3 assessment documented in this report.

Whilst odour is generally considered the primary air emission from waste and composting type facilities, this report has also investigated the potential for dust and other common air pollutants such as nitrogen dioxide, carbon monoxide and sulphur dioxide to present adverse air quality impacts on air quality. These pollutants were also investigated as part of this assessment and a brief background of the pollutants are discussed in the following sections.

1.2 Odour

An odour is defined as the property of a substance that gives it its characteristic scent or smell. Odours are very subjective, with responses varying greatly from individual to individual. Whether an odour is perceived as being pleasant or unpleasant is often based on personal opinion.

The sensory perception of odour has four major dimensions: concentration, intensity, character, and hedonic tone.

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- **Odour concentration:** otherwise known as the odour threshold, is the concentration of a compound necessary for detection by 50% of the population.
 - **Odour intensity:** this refers to the perceived strength of the odour sensation. Intensity, for most chemicals, increases exponentially with the concentration of the compound.
 - **Odour character:** this is what the substance smells like. A commonly used list of descriptors includes “fishy, hay, nutty, creosote, turpentine, rancid, sewer, and ammonia”.
 - **Hedonic tone:** this is the judgement of the relative pleasantness or unpleasantness of the odour. It is this aspect that primarily dictates whether an odour nuisance occurs.

Obviously, there are many odours, or situations, when a smell does not cause a nuisance. It is the subjective judgement of the hedonic tone that enables the decision to be made as to whether an odour is a nuisance or not. Solid waste and greenwaste odours are generally considered to be unpleasant, however, treatment using odour control technologies, such as biofilters, reduce the concentration and intensity of the odours and normally change the character of the odour, resulting in the odour having a more neutral tone.

1.3 Particulate Matter

Particulate Matter is generally divided into two broad fractions, deposited and suspended. Deposited particulate matter is dust that, because of its aerodynamic diameter and density, rapidly falls from the air. In general terms, deposited particulate has a diameter of greater than about 20 μm . However there is no distinct dividing line between these particles and the smaller particles of suspended matter that fall more slowly out of the air. Because of the size of the particulate matter, most of this material will not enter the body. Hence the effects of deposited particulate are primarily nuisance, and may only affect health via annoyance reactions and the like.

Suspended particulate matter is dust or aerosol that stays suspended in the atmosphere for significant periods. The current nomenclature is to describe fractions of suspended particulate as:

- **PM₁₀:** all particulate effectively less than 10 microns (μm) in diameter;
- **PM_{2.5}:** all particulate effectively less than 2.5 μm in diameter; and
- **TSP:** total suspended particulate, generally less than 50 μm in diameter.

Within the range of suspended particulate, the group of particles which are sized 10 μm or less (PM₁₀) have been associated with health effects including increases in mortality, aggravation of existing respiratory and cardiovascular disease, increased hospital admissions and increased asthma incidents. More recent research however, indicates that it may be the PM_{2.5} fraction that has the greatest impact on human health. Particles that are larger than 10 μm , tend not to be able to penetrate the respiratory tract and do not appear to be significant with respect to potential health effects.

Major natural sources of background particulate levels include forest fires, pollen and wind-blown dust from exposed areas. Anthropogenic sources include stationary and mobile combustion sources, road dust, agriculture, mining, major fires and emissions from industrial processes. Background levels vary widely depending on location, meteorology and proximity of major point or area sources.

1.4 Combustion Products & Other Criteria Pollutants

Combustion products such as oxides of nitrogen (NO_x) and carbon monoxide (CO) as well as industrial related emissions such as sulphur dioxide (SO_2) are unlikely to be emitted from the proposed development in large quantities, however, are ubiquitous in the ambient air and can occur in high concentrations, hence the need for assessment.

1.4.1 Oxides of nitrogen

Oxides of nitrogen (NO_x) is the sum of nitric oxide (NO) and nitrogen dioxide (NO_2) concentrations. NO and NO_2 are linked in a circular reaction with oxidants such as ozone which generates NO_2 from NO and sunlight which breaks NO_2 down to NO. Due to this reaction sequence, the exact amount of NO and NO_2 within emissions is often unknown, and consequently the sum emission of both species is quoted. The ambient concentration of NO_2 near to a NO_x source is dependent on the amount of oxidant and sunlight at the time.

In ambient concentrations usually found within the atmosphere, NO has no impact on either human health or the environment. Conversely, it is known that short term concentrations greater than 200ppb ($411\mu\text{g.m}^{-3}$), people with asthma have an increased response to irritant stimuli. To ensure that these potential sufferers are protected, maximum short term exposure is set within NSW at $246\mu\text{g.m}^{-3}$ (120ppb). The long term effects of NO_2 are less well known although some evidence suggests poor lung function of inhabitants of areas with high NO_2 concentrations. A limit of $62\mu\text{g.m}^{-3}$ has been set by the NSW EPA as an annual mean.

1.4.2 Carbon monoxide

CO binds more readily with red blood cells than oxygen forming carboxyhaemoglobin (COHb) which deprives the human body of the oxygen needed to function. In ambient concentrations found within non-urban environments, carbon monoxide (CO) does not have any impact on human health. In high traffic environments where pollutants become trapped within street canyons, such as in congested urban centres CO concentrations are known to build to concentrations which often result in headaches.

Carbon monoxide (CO) is produced due to the incomplete combustion of any fuel containing carbon, where there is too little oxygen within the mix or the fuel is burnt at too high a temperature. The most common generation of this is in motor vehicles which are driving at low speeds, idling or coasting downhill.

1.4.3 Sulphur dioxide

As SO₂ is released in to the atmosphere it combines with water within the atmosphere to generate acid rain which acidifies lakes, results in the destruction of forest and damages buildings constructed of limestone. The sulphuric acid may also damage the moist parts of the nose, mouth, pharynx and larger bronchiole.

SO₂ is generated through the combustion of sulphur containing fuels such as coal and petrol / diesel. The site has no plans to burn coal and the Federal Clean Fuels Act, 2000 ensures that the sulphur content of automotive fuels will be reduced in the coming years. It is considered, therefore, that sulphur emissions from the site will be minimal and will not result in elevated concentrations in the surrounding area.

2.1 Assessment Criteria

There are three main types of air quality criteria which are generally assessed as part of developments:

Emission Standards – which are maximum allowable pollutant concentrations specified for particular classes of equipment;

Air Impact Assessment Criteria – which are designed for use in air dispersion modelling studies and air quality impact assessments for new or modified emission sources; and

Ambient Air Quality Standards – set standards against which ambient air quality monitoring results may be assessed.

The Emission Standards are primarily used to limit major industrial processes emissions such as oxides of nitrogen and sulphur from power plants. For this development, Emissions Standards are not as relevant as the principal air quality impacts will be from fugitive odour during operation and potentially fugitive dust emission during construction. The Air Impact Assessment Criteria are more relevant to this development.

Air Impact Assessment Criteria are used in evaluating the expected impact of air emissions on local air quality and the effectiveness of plant design and any associated mitigation measures. Another objective of these criteria is to ensure that the resulting local and regional ambient air quality meets the relevant Ambient Air Quality Standards.

The Ambient Air Quality Standards refers to the NEPM guidelines which provide regional guidelines for several key air pollutants and the guidelines and have not been designed to provide guidelines for assessing individual developments, rather for setting broad scale regional limits. They are discussed in Section 2.2.2.

2.1.1 Air Impact Assessment Criteria

Department of Environment and Conservation (incorporating the New South Wales Environment Protection Authority) have published impact assessment criteria to be applied in the design stages of an activity to ensure that there will be no impact on public health or amenity values. These criteria are set on the basis of the toxicity of a chemical or, if more stringent, the odour threshold of a pollutant. DEC impact assessment criteria relevant to the proposed development are given in Table 2-1.

Table 2-1: DEC (NSW EPA) Impact Assessment Criteria

Pollutant	NSW EPA Impact Assessment Criteria ($\mu\text{g}/\text{m}^3$) ^A	Averaging Time
Odour	2 OU (nose response time) ^B	1 hour
PM ₁₀	50 30	24 hours annual
Nitrogen Dioxide	246 62	1 hour annual
Carbon Monoxide	100,000 30,000 10,000	15 minutes 1 hour 8 hours
Sulphur Dioxide	712 570 228 60	10 minutes 1 hour 24 hours annual

^A all criteria listed in $\mu\text{g}/\text{m}^3$, unless otherwise specified.

^B See Table 2-2 for more detail on odour units.

Odour Regulations in New South Wales

The NSW EPA provides odour criteria in NSW EPA (2006a) *Technical framework: Assessment and management of odour from stationary sources in NSW*. The criteria is shown in Table 2-2, and ranges from 2 OU to 7 OU (99.0%, nose response time) and corresponds to an affected population of >2000 (2 OU criteria) to 2 (7 OU criteria).

Table 2-2: Odour Performance Criteria (from Table 3.1, NSW EPA 2006)

Population of affected community	Odour performance criteria (odour units/ m^3)
Urban areas (≥ 2000)	2.0
500 - 2000	3.0
125-500	4.0
30-125	5.0
10-30	6.0
Single residence (≤ 2)	7.0

The nose response time essentially refers to a 1 second averaging time and incorporates “peak to mean ratios”. The peak to mean ratio is defined by NSW EPA (2006a, p55) as “a conversion factor that adjusts mean dispersion model predictions to the peak concentrations perceived by the human nose”. Peak to mean ratios for odorous area and volume sources (likely for this development) are presented in Table 2-3.

Table 2-3: Peak to Mean Ratios (from Table 6.1, NSW EPA 2005)

	Pasquill-Gifford stability class	Near field i_{maz}	Near field x_{max}	Near field P/M_{60}	Far field i	Far field P/M_{60}
Area	D	0.5	500 to 1000	2.5	0.4	2.3
	E,F	0.5	300 to 800	2.3	0.3	1.9
	A,B,C	0.5	500 to 1000	2.5	0.4	2.3
Volume	A-F	0.4	-	2.3	0.4	2.3

Peak to mean ratios can be further explained in the following example. Where a 1-hour averaging time has been used for modelling and an odour concentration at a receptor (resident) is predicted to be 0.5 OU, a peak to mean ratio of 3 would increase the predicted odour concentration to 1.5 OU. During that hour, the dispersion model predicts an average concentration of 0.5 OU at the receptor, however, the odour concentration at the receptor may rise to 1.5 OU and fall to 0.1 OU, but the fluctuations may only last for a matter of seconds. As the nose has a relatively quick response time, namely in the order of seconds, the peak to mean ratio incorporates the quick response time of the human nose when perceiving natural variations (increases) in odour concentration throughout that hour period.

Based on the residential area to the east, the odour performance criterion to be adopted is 2 OU.

2.1.2 Ambient Air Quality Standards

In June 1998, the National Environment Protection Council (NEPC) released a National Environment Protection Measure (NEPM) for Ambient Air Quality, setting out national standards and goals for six common ambient air pollutants (NEPC, 1998).

When reviewing the standards and goals set out in the NEPM for Ambient Air Quality, it should be noted that they are designed for use in assessing regional air quality and are not intended for use as site boundary of atmospheric dispersion modelling criteria. Consequently, proposed facility emissions have not been assessed directly against NEPM guidelines, however, the guidelines provided by the NEPM match the Air Impact Assessment Criteria provided in NSW EPA (2005).

3.1 Proposed Operations

AWT Facility

This will involve the receipt of approximately 70,000 tpa of Municipal Solid Waste (MSW) into an enclosed building which will separate the waste into various fractions. The various operations involved in receiving and sorting the waste will generate strong odours, hence the building air will be vented via an external biofilter to treat the odorous air. In this assessment, allowance for fugitive emissions has also been made.

Greenwaste / Biosolids Processing Facility

The enclosed type composting facility will process up to 30,000 tonnes of source separated municipal greenwaste and 15,000 tonnes of biosolids, per year. The receipt, sorting and shredding facility for greenwaste will generate odours, however the greatest odours are generally associated with exposed surface areas of greenwaste composting. Building air will be ducted to a biofilter, and as in the case of the AWT facility allowance for fugitive emissions has also been made.

Matured Compost Processing and Storage area

This area is not expected to generate significant odour, however these sources have been included in the dispersion modelling for completeness.

Pre-Existing Operations

Whilst the introduction of the AWT facility will reduce the proportion of waste to be directed to landfill, the existing Landfill and Leachate system will continue to operate on the site.

4.1 Climate

The closest Automatic Weather Station (AWS) is located at Narara Research Station, north of Gosford in the foothills of Mount Penang. This data was considered inappropriate for use in dispersion modelling due to the highly specific terrain-induced flows present at the sheltered location, coupled with its distance from the proposed site (14km to the north). However this data was considered generally indicative of the local climate.

A summary of climatological data collected at the Narara Research Station AWS is provided in Table 4-1. The climatological data indicates that the region experiences warm summers and mild winters. The records indicate that average daily temperatures for summer are approximately 27°C but can exceed 40°C in January, February and March. The area experiences a high amount of rainfall for the region. An annual rainfall of 1320mm over an average of 116 rain days per year is reported. In comparison, Sydney's mean annual rainfall is 1094mm. The wettest months are between January and June.

Mean wind speeds are lightest in the months between March and August. Afternoon winds show more seasonal variability than the morning winds, which may be attributed to coastal sea breezes. The morning winds remain consistently light until August to November where the monthly mean wind speed increases.

A discussion of site representative meteorology, as used in the dispersion modelling, is provided in Appendix A.

4.2 Background air quality

Odour

For the majority of air quality assessments, background concentrations of pollutants are added to the concentrations predicted to occur from the plant emissions in order to obtain a cumulative, or total concentration. In relation to odour assessments, it is generally accepted practice to assume a zero background odour concentrations unless there are significant odour sources in the vicinity of the development.

The only potential odour source identified in the vicinity of the development is the Woy Woy Sewage Treatment Plant (STP), located in the base of the valley to the north of the site. The STP is isolated from the proposed facility by a distance of approximately 2km, and by strong terrain features with a difference in elevation of greater than 120m along the path, between the two sites. The STP has been excluded from the assessment as a potential odour source, as explained in the following sections.

The Council has not received odour complaints from the Woy Woy STP for the past 25 years, suggesting the odour from the STP is confined to the site. This is consistent with a field odour assessment conducted by URS on the eastern boundary of the STP on 8 May 2007, which did not detect sewage type odours.

Furthermore, the meteorological conditions of northerly breezes and/or surface layer convection, in which air is potentially transported from the STP, to the region of the proposed site are not synonymous with worst case odour conditions, as significant amounts of turbulence (mechanical and/or convective) would be an inherent part of these transport mechanisms. These atmospheric conditions are in contrast to stable, low wind conditions, which are conducive to poor dispersion and adverse odour impacts. Consequently atmospheric conditions likely to transport odour from the STP to the area surrounding the proposed development are conditions where low odour impacts are expected from the development.

In addition, the relative alignment of the STP, the proposed development and the sensitive receptors nearest to the proposed site also prevents the STP from forming a source of background odour during worst case conditions i.e. westerly breezes. During westerly breezes, the emissions from the proposed facility would be transported towards receptors to the east of the proposed facility. These conditions suggest that the odours from the proposed facility would be travelling in parallel to the STP odours, thus the cumulative odour impact on the residential area to the east of the proposed development would be negligible.

Furthermore, the modelling conducted, which is discussed in subsequent sections, predicts the likely odour impact from the proposed development in the vicinity of STP. The results show that the odour concentration from the proposed development at the STP is approximately 0.1 OU (nose response time).

Given that the closest receptors to the STP are to the north east of the STP and further away from the proposed development, it follows that the added odour impact at the nearest receptors to the STP would be less than 0.1 OU (nose response time), which is considered negligible.

On this basis, the STP is unlikely to add to the predicted odour from the proposed development to cause a cumulative odour impact in exceedance of guidelines at sensitive receptors. Thus the STP has been excluded from this assessment as a significant odour source.

Table 4-1: Climate Data from Narara Research Station Automatic Weather Station (BoM, 2006)

	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	ANN	No. Years
Mean Daily Max Temp (deg C)	27.5	27.1	26	23.7	20.2	17.8	17.4	18.8	21.1	23.6	24.9	26.9	22.9	23.6
Mean no. Days, Max $\geq$ 40 deg C	0.4	0.2	0.1	0	0	0	0	0	0	0	0	0.2	1	20.7
Highest Max Temp (deg C)	42.8	43	40.1	32.8	28	25	25.5	29.3	36.1	36.5	39.9	43	43	20.8
Mean Daily Min Temp (deg C)	16.6	17.1	15.4	11.9	8.3	6.4	4.5	5.4	7.6	10.6	12.7	15.2	10.9	23.9
Mean no. Days, Min $\leq$ 0 deg C	0	0	0	0	0	0.5	2.1	0.7	0	0	0	0	3.3	20.9
Lowest Min Temp (deg C)	7.5	9.7	5.8	3.1	0.1	-1.1	-4.2	-1.1	-0.6	1.1	3.9	6	-4.2	21
Mean 9am Air Temp (deg C)	22.9	22.4	20.9	18.4	14.2	11.6	10.3	12.7	16.1	19.1	20.4	22.4	17.6	23.9
Mean 9am Wind Speed (km/hr)	8.3	7.2	7	6.8	6.9	7.3	7.2	9	10.1	10.8	9.6	8.5	8.2	20.3
Mean 3pm Air Temp (deg C)	26.8	26	24.4	21.7	18.7	16.3	15.8	17.6	19.7	21.9	22.8	25	21	8.3
Mean 3pm Wind Speed (km/hr)	13.7	11.7	11.2	9.1	7.9	7.6	8.4	10.2	12.4	11.5	12.8	13.4	10.8	8.6
Mean Rainfall (mm)	139	148.1	149.8	136.2	119.1	127.6	79	75.9	68.6	82.9	92.4	102.2	1320.8	81.6
Highest Monthly Rainfall (mm)	517.5	597.7	500.3	661.9	634	664	455.6	426.2	232.1	344.1	361.5	417.1	-	81.6
Lowest Monthly Rainfall (mm)	4.3	0	6	4.6	6.1	1.9	0	0	2	1	4.1	6	-	81.6
Highest Recorded Daily Rain (mm)	210.8	191.8	205.5	218.4	177.3	170.7	194.8	119.2	106.9	129.3	155.2	155.2	218.4	75.9
Mean No. Raindays ¹	11.1	10.8	11.1	10.6	9.2	9.7	8	8.1	8.4	9	9.8	10.1	115.8	67.3
Mean no. of Clear Days	6.7	8	7.3	9.3	7.3	6.6	9.8	12.4	6.2	9.8	5.8	6.8	96	4.3
Mean no. of Cloudy Days	11.3	7.7	8	5	10	6.8	6.4	5	8	6.2	7.2	5.6	87.2	4.3
Maximum Wind Gust (km/hr)	53.6	51.8	50	57.2	48.2	77.8	50	57.2	51.8	64.8	53.6	50	77.8	3.9

¹ A rainday is a day where more than 0.2mm of precipitation was recorded.

Particulate Matter and Criteria Pollutants

Background concentrations of pollutants within the immediate locale are an important consideration when undertaking an air quality assessment. Background concentrations provide an indication of existing air quality prior to development. Background monitoring stations only monitor the air quality for the location in which they are placed, and provide only an indication of existing air quality in other areas. When using data from an air quality monitor in one area as representative of another area, both areas should have similar topography and surrounding land use. Within New South Wales (NSW), monitoring is undertaken by the DEC in multiple locations and also by specific industries, where it is considered relevant by the DEC. Data from industrial monitoring is not publicly available, and therefore cannot be considered within this assessment. The DEC has monitors throughout NSW, and within the area surrounding the site, four were primarily considered, these were:

1. Lindfield – approximately 35km south-west of the site;
2. Beresfield – approximately 85km north-east of the site;
3. Newcastle – approximately 75km north-east of the site; and
4. Wallsend – approximately 75km north of the site;

Of the four monitors considered, the Wallsend site was considered most representative of the site as it was located on the edge of a moderately sized urban area, with a large forested area to the west and south-west of the monitoring location. Whilst urbanisation exists closer to the monitoring location than is the case at the proposed site, there are no major roads indicating that this would be a typical background location, and would be representative of the expected background concentrations at site.

Data collected at the Wallsend monitoring site for the most recent complete monitoring cycle (2005) was compared to the impact assessment criteria identified within the DEC, 2005. The impact assessment criteria within NSW have been drawn from a number of Australian and International sources and represent limit values at which ambient concentrations are not considered harmful to human health or the environment. Figure 4-1 shows the annual mean concentrations of NO₂, PM₁₀ and SO₂ in comparison to the NSW impact assessment criteria, it may be seen, that in 2005 background concentrations were significantly below the assessment criteria for these pollutants.

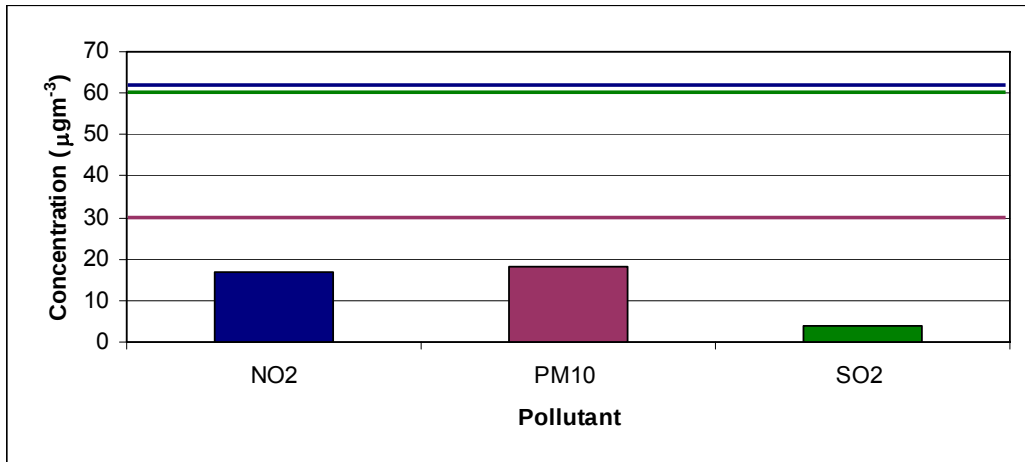


Figure 4-1: Annual mean background concentration compared with DEC impact assessment criteria, measured at Wallsend in 2005

The NSW impact assessment criteria also require comparison of certain pollutants against concentrations measured over shorter averaging periods than the annual mean due to the acute impact of elevated short-term concentrations.

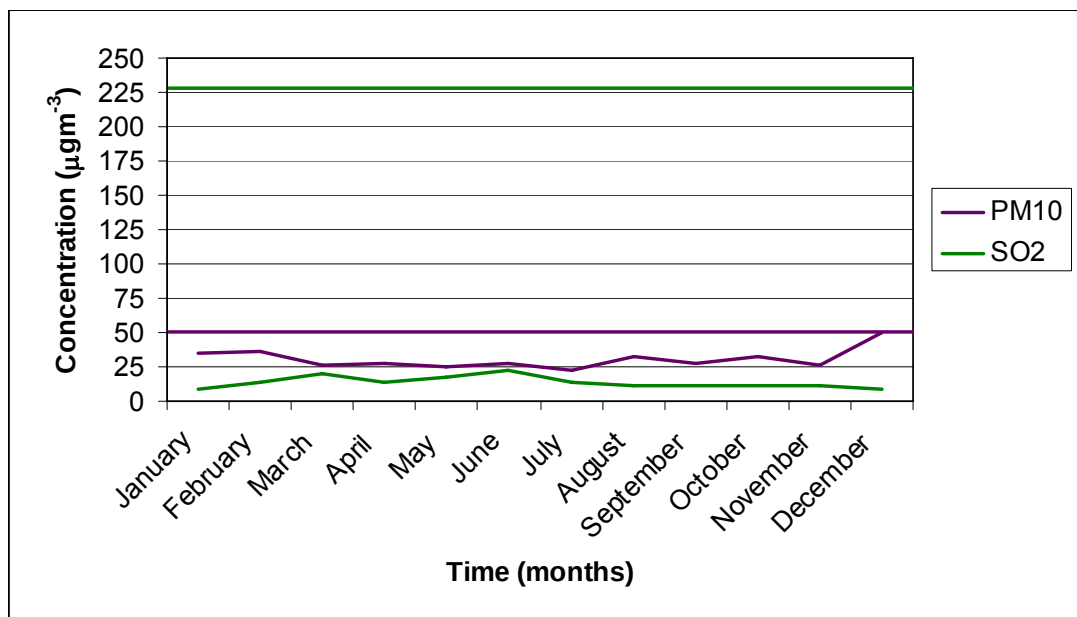


Figure 4-2: Maximum 24-hour mean concentration for PM₁₀ and SO₂ measured at Wallsend in 2005

Figure 4-2 shows the maximum twenty-four hour mean concentration for each month in 2005 as measured at the Wallsend monitoring station in comparison to the impact assessment criteria. As would be expected in a suburban environment away from industrial sources, 24-hour mean concentrations of SO₂ are significantly below the assessment criteria. Background concentrations of PM₁₀ are closer to the assessment criteria, and in December 2005 ambient concentrations measured over 24-hours were equal to

the assessment criteria. It is thought that this is the result of a naturally occurring wind-blown dust, or a bush fire in the surrounding area.

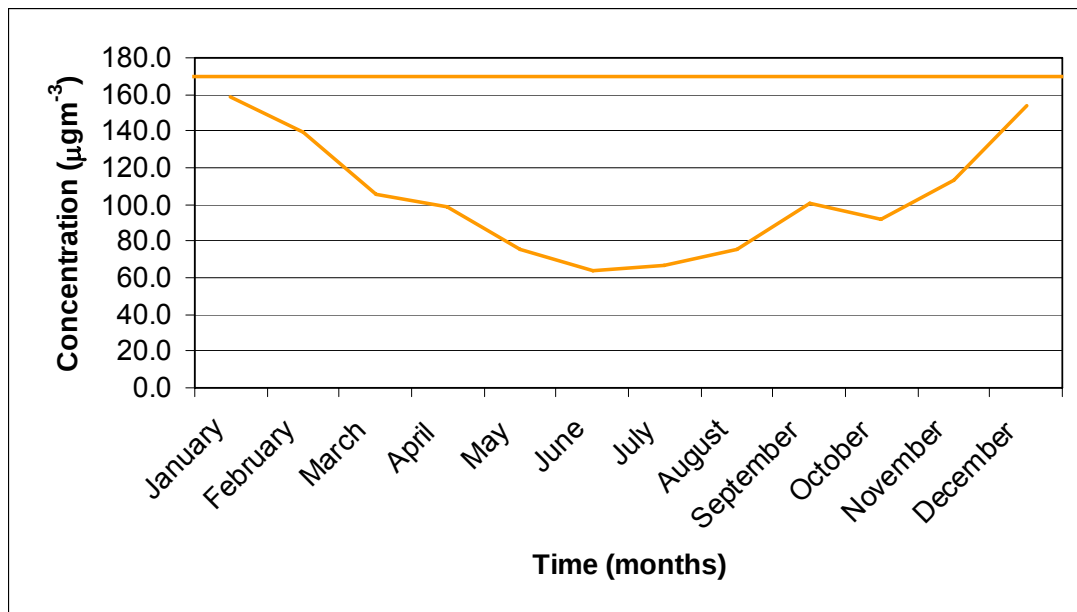


Figure 4-3: Maximum 4-hour mean concentration of O_3 measured at Wallsend in 2005

Figure 4-3 shows the maximum 4-hour mean concentration of ozone which is commonly used as a representative indication of photochemical oxidants within a study area. Photochemical oxidants are important as they oxidise nitric oxide into nitrogen dioxide and are needed in the formation of peroxyacetyl nitrates (PAN), or photochemical smog. Concentrations of these pollutants were below the assessment criteria for the measurement period.

Figure 4-4 shows the maximum 1-hour mean concentrations for ozone (O_3), NO_2 and SO_2 measured at Wallsend for each month in 2005. Concentrations of these pollutants did not exceed the assessment criteria at any point throughout the year.

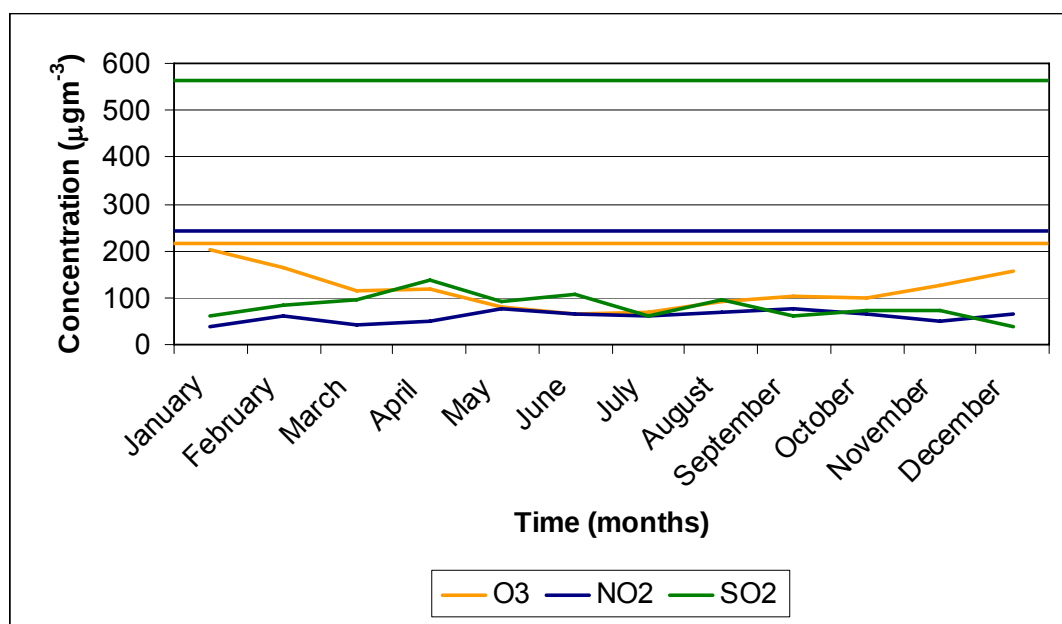


Figure 4-4: Maximum 1-hour concentrations of O₃, NO₂ and SO₂ measured at Wallsend in 2005

4.3 Summary

Emissions of ozone (O₃), nitrogen dioxide (NO₂), particulate matter (PM₁₀) and sulphur dioxide (SO₂) from the site will be negligible. Anthropogenic creation of O₃ within the troposphere is not the result of direct emission; rather it is the result of chemical reactions of oxides of nitrogen (NO_x) and volatile organic compounds (VOCs) with other natural atmospheric constituents and isolation.

Anthropogenic generation of O₃ in large quantities requires large volumes of traffic and insolation. It would not be expected that the site would provide sufficient additional traffic to generate added O₃, and has therefore not been considered further in this assessment. NO_x emissions from the site will also be minimal due to the low number of site vehicles and other on site combustion sources, and it would not be expected that the additional site traffic would result in an exceedance of the assessment criteria.

PM₁₀ emissions are likely to be generated from site vehicles passing over unsealed roads. The majority of roads on site will be sealed reducing PM₁₀ emissions to the maximum extent achievable. Only machinery within the cells will pass over unsealed roads; emissions of PM₁₀ will be kept to a minimum within these areas by control techniques. It is not anticipated that site activities will significantly add to background concentrations of PM₁₀, and these have therefore not been considered further within this assessment.

Finally emissions of SO₂ will be limited to those generated through the use of sulphur containing fuels on site. The amount of sulphur in fuels is controlled in Australia by the Fuel Quality Standards Act, 2000, which limits sulphur in diesel to 50ppm as from 1 January 2006 and to 10ppm from the 1st January 2009. The low sulphur fuels will ensure that site sulphur emissions are minimal and that site contribution to ambient concentrations will not result in exceedance of the assessment criteria over any averaging period.

Carbon monoxide was not measured at the Wallsend site, however, background concentrations are likely to be low and site emission sources, namely vehicle emissions, are derived from relatively few sources and are not expected to add significant concentrations to background concentrations. Hence, carbon monoxide is not considered to be a significant pollutant in relation to this assessment.

Background concentrations for the pollutants considered within this section over all averaging periods combined with the expected emissions would not be expected to exceed the assessment criteria specified by the DEC. The only significant pollutant likely to arise from the proposed development is additional odour, which is further assessed in the following sections.

5.1 Proposed Operations

The two major sources of air emissions related to this project include dust emissions during the construction phase and odour emissions during the operational phase. As dust generated during construction will be temporary and can be effectively controlled using mitigation measures, this report will focus on the assessment of odour during the operational phase of the project.

5.2 Odour Emission Rates

The final design selection of the AWT and composting facility to be employed at the Woy Woy facility is yet to be made. Thus Odour Emission Rates (OERs) have been calculated based on the proposed tonnage of material to be processed, in accordance with emission rates from existing facilities which employ similar processes to those proposed for the Woy Woy facility. The OERs calculated, include significant margin for safety, in order to be consistent with the conservative nature of this assessment. Where a range of OERs have been available, the most conservative rates have generally been selected.

5.2.1 AWT Facility

OERs for the AWT facility have been estimated from a proposed Municipal Solid Waste Facility at South Windsor (Thiess Services, 2003). The odour emission data presented in Thiess Services (2003) was based on empirical odour data collected from waste at a plant with similar operations, hence the data is considered suitable for use in this assessment.

The proposed AWT facility is to consist of a waste receival hall where municipal solid waste is delivered by trucks and unloaded inside the building. The waste is then to be conveyed to adjoining rooms for processing using a rotating drum. An extraction system captures air from the primary processing areas which is then vented to a biofilter. The estimation of odorous emissions from the facility have also included a large quantity of fugitive emissions from the building, however, it is expected that the odours will primarily be treated by the biofilter.

The OERs for the Woy Woy AWT facility are based on this work, as the process proposed for the Woy Woy AWT is similar to that investigated at South Windsor. Thiess (2003) calculated a fugitive odour emission rate of 5100 OU.s⁻¹ based on a throughput of 155,000 tonnes per annum with the odour control technology being a biofilter, which was designed to have a surface area of 100m², with a total emission rate 556 OU.s⁻¹.

The OERs for the proposed Woy Woy AWT were scaled linearly to the throughput of 70,000 tonnes per annum for the AWT (as shown below in Equation 5-1), which resulted in an OER of 2303 OU.s⁻¹ for the AWT facility and an OER of 250 OU.s⁻¹ for the biofilter.

$$OER_D = OER_T \times \frac{Throughput_D}{Throughput_T} \quad \dots \text{Equation 5-1}$$

Where:

OER_D and OER_T are the Odour Emission Rates proposed for Woy Woy and South Windsor respectively.

Throughput_D and Throughput_T are the proposed development throughputs for Woy Woy (70,000 Tpa) and South Windsor respectively (155,000Tpa)

It should be noted that all wastewater generate as part of this facility will be contained within storage tanks, hence this source does not warrant inclusion in the odour modelling.

5.2.2 Green Waste / Biosolids Composting Facility

The composting facility will comprise an enclosed building where the majority of processing is to occur. In a manner similar to the AWT facility, air from within the building will be ducted to a biofilter, whilst a large allowance for fugitive emissions has been made.

Based on the likely throughput of approximately 45,000 Tonnes of material annually, and given 20,000 tonnes would generally comprise 8 windrows operating continuously, 18 windrows were assumed to be situated within the building. Each windrow used in the modelling assumed dimensions shown in Figure 5-1, with a height of 3m.

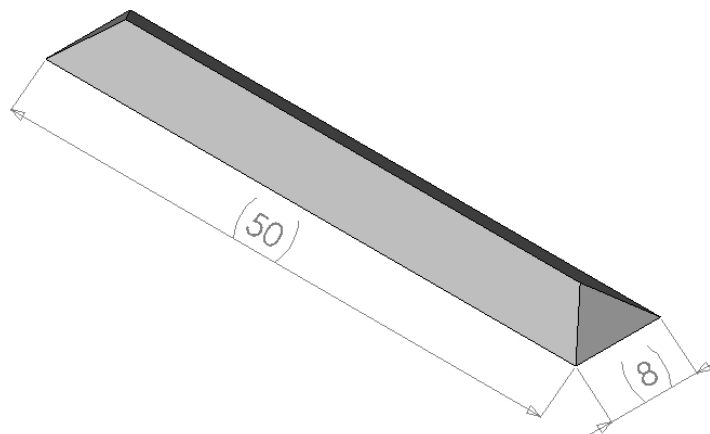


Figure 5-1: Windrow dimensions (in metres) used in emission calculations.

The surface area of each cell was calculated by assuming that each cell occupied 50 x 8m of ground, and formed a triangular prism. Each end was angled at 40 degrees from horizontal which gave a total exposed surface area of approximately 571 m² per cell. This area allows the Odour Emission Rate (OER) for a single windrow to be calculated from the Surface Odour Emission Rate (SOER).

Work undertaken by Kühner *et al.* 1999 has shown that for a Gore covered windrow, such as those proposed, have an SOER of 1.25 OU.m⁻².s⁻¹, resulting in an average odour emission rate of 714 OU.s⁻¹ per windrow. On the basis that 18 windrows are contained within the Composting Facility, and that 50% of the odorous air is either treated using a biofilter or retained by the enclosure, the odours produced by the windrows that escape the building as fugitive emissions, is estimated to be 6,424 OU.s⁻¹. Whilst it is known that odour emissions from the windrows are increased during turning, the biofilter and enclosure will act to contain those peak emissions.

The composting facility is proposed to have a biofilter which is used to treat the extracted air from the building. GHD (2006) indicated that a 440 m² biofilter attached to a similar green waste facility (30,000 tpa) generated an SOER of 2.8 OU.m⁻².s⁻¹. Similar to the method used to calculate the biofilter area of the AWT facility, the area of the proposed biofilter has been designed to be 660m², based on 45,000 tpa of biosolids and greenwaste combined. This will produce a net emission rate of 1848 OU.s⁻¹ from the biofilter.

It should be noted that all wastewater generate as part of this facility will be contained within storage tanks, hence this source does not warrant inclusion in the odour modelling.

5.2.3 Green Waste Maturation Windrows

It is known that greenwaste processing can generate significant odorous emissions, however, it is generally during the initial weeks where the majority of the odours are released. After 12 weeks of processing within the enclosed composting facility, significant odour emissions are unlikely to be generated when the windrows are moved outside for further drying.

Mature windrows, such as these, have been shown to have an SOER of approximately 0.46 OU.m⁻².s⁻¹. The value of 0.46 OU.m⁻².s⁻¹ was calculated from other mature compost odour emission rates, as shown in Table 5.1. It should be noted, in Table 5-1, that URS considers the inclusion of the Mature Product, with an SOER of 4.5 OU.m⁻².s⁻¹ as being overly conservative, and it is the experience of URS that SOERs for this type of source would generally be significantly less than shown. Consequently, the geometric average was used to reduce the skew which resulted from the inclusion of this datum.

Table 5-1: Literature review of SOER from Mature Compost Product

Odour Emission Source	SOER (OU.m ⁻² .s ⁻¹)	Geometric Average ^A (OU.m ⁻² .s ⁻¹)	Sampling Method	Reference
Finished Product – Fine	0.83	0.46	Flux Hood	AWT (2001)
Finished Product – Coarse	0.18		Flux Hood	AWT (2001)
Unscreened Finished Compost	0.08		Flux Hood	AWT (2001)
Mature Product	4.5		Wind Tunnel	Kühner & Kischer (1999)
Final Product	0.4		Unknown	Haug (1993)

It has been assumed that 12 windrows of material, each having a surface area of 571 m², will be stored in the maturation area at any one time. The net emission rate from the external windrows will therefore be 3152 OU.s⁻¹.

5.2.4 Existing Tip Face

The existing tip face will remain operational to accept the fraction of waste which the AWT is unable to treat or use elsewhere. Emission rates incorporated into this assessment are for tip faces which accept putrescible Municipal Solid Waste. Table 5.2 gives a range of emission rates for active tip faces including emission rates measured Woy Woy in 2003. The site specific data has not been included as there is more conservative data available. The dispersion modelling has assumed an odour emission rate of $2.7 \text{ OU.m}^{-2}.\text{s}^{-1}$, which was sourced from GHD, 2006².

Table 5-2: SOERs for Putrescible Solid Waste Landfill Tip Faces

Odour Emission Source	SOER ($\text{OU.m}^{-2}.\text{s}^{-1}$)	Sampling Method	Reference
Kincumber Landfill	0.146	Flux Hood	Bowly (2003)
Woy Woy Landfill	0.110	Flux Hood	Bowly (2003)
Buttonderry Landfill	0.335	Flux Hood	Bowly (2003)
Jacks Gully WMC	2.71	Flux Hood	GHD (2006)

¹ This incorporates a scaling factor of two in order to account for cooler weather during sampling (GHD,2006)

Given that the tip face will move around the site as the landfill takes on new material, the tip face has been assumed to be located at the southern-most point of the landfilling area. This allows for the emissions of the AWT and tip face to consolidate, hence ensuring the most conservative location has been assessed. The tip face was assumed to be $30 \times 30 \text{ m}^2$, a total of 900 square metres. This results in a source emission rate of 2,430 OU/s. As an added level of conservativeness, the tipface emissions were assumed to emit continuously, even though the tipface is generally covered by soil during night times.

5.2.5 Leachate Pond

The leachate pond on the site will remain operational in order to process the leachate produced by the existing landfill. Table 5.3 gives a range of emission rates for leachate ponds.

² Contained in Table 10 of Appendix 7.

Table 5-3: SOERs for Leachate Ponds

Odour Emission Source	SOER (OU.m ⁻² .s ⁻¹)	Sampling Method	Reference
Buttonderry Landfill	0.833	Flux Hood (converted)	Bowly (2003)
Jacks Gully WRC	0.108	Flux Hood	URS(2004)
Jacks Gully WRC	0.054	Flux Hood	URS(2004)

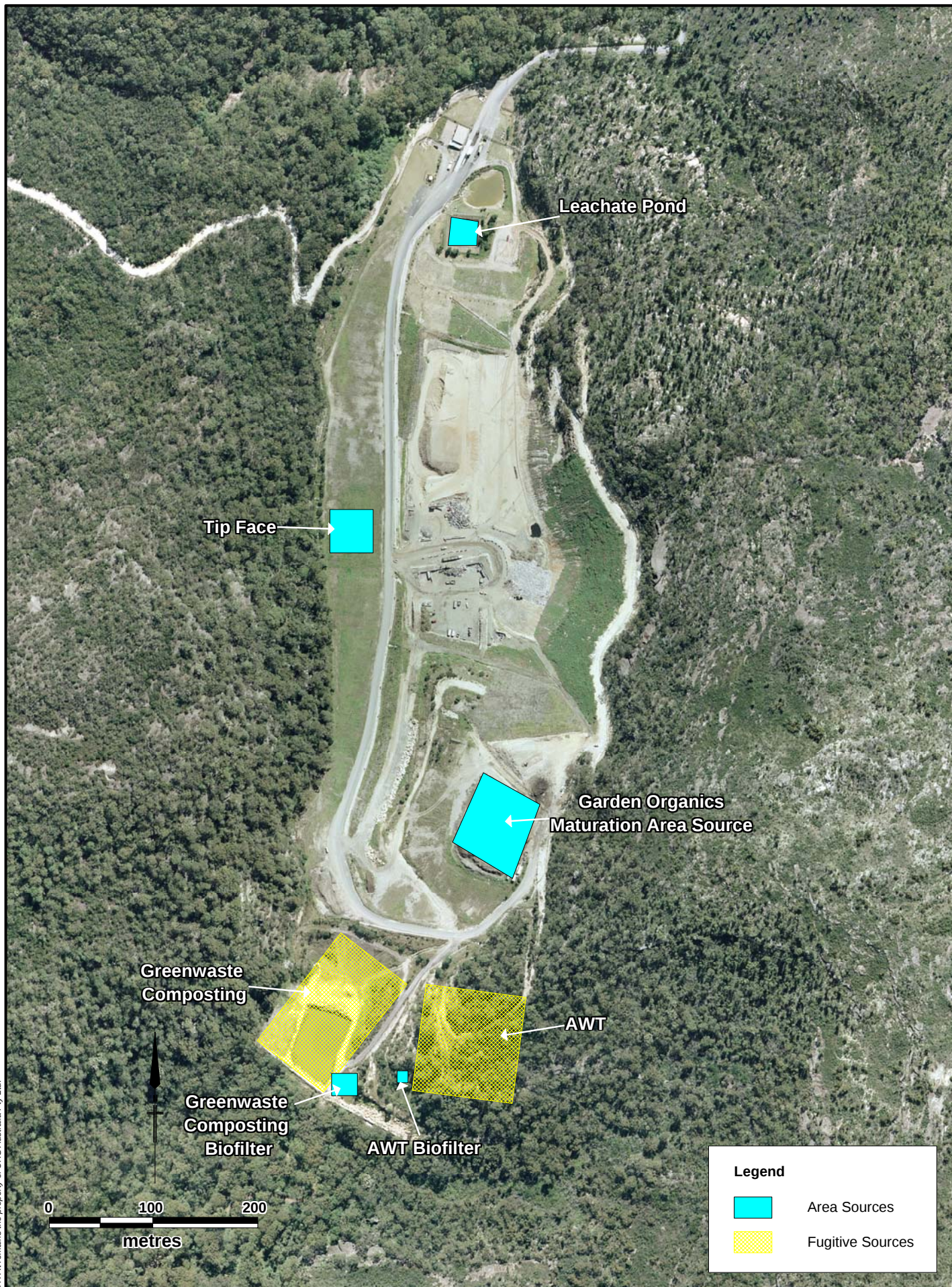
The existing leachate pond is approximately 23 x 23m² in size, totalling 529 square metres. Taking the most conservative SOER from Table 5-3, this constitutes a total of 441 OU/s being emitted from the leachate pond for every hour of the year.

5.3 Odour emission rate summary

The odour emission rates used in the modelling are provided in Table 5-2, and have been derived from various studies of other similar facilities both internationally and within Australia as described above. These emission rates do not incorporate a peak to mean ratio, as a peak to mean ratio of 2.5 has been incorporated in the post processing of the model results. The locations of the sources are shown in Figure 5.2 on the following page.

Table 5-4: Odour Emission Rates

Odour Source	Source Type	Surface Odour Emission Rate (OU.m ⁻² .s ⁻¹)	Odour Emission Rate (OU.s ⁻¹)
AWT Treatment Facility	Fugitive	-	2,303
AWT Treatment Facility (Biofilter)	Area	2.5	250
Green waste Treatment Facility	Fugitive	-	6,424
Green waste Treatment Facility (Biofilter)	Area	2.8	1,848
Green waste Maturation Area	Area	0.46	3,152
Tip Face	Area	2.7	2,430
Leachate Pond	Area	0.833	441
TOTAL			16,848



Client GOSFORD CITY COUNCIL	Project WOY WOY WASTE MANAGEMENT FACILITY			Title SOURCE TYPE AND LOCATIONS AS USED IN DISPERSION MODELLING	
	Drawn: AJW	Approved: DRAFT	Date: 27/06/2007	Figure: 5-2	
	Job No: 43177409		File No: 43177409-006.wor		

5.4 Modelling Methodology & Parameters

A discussion of the modelling, performed using CALPUFF, including processing of meteorological data is provided in Appendix A and example of the CALPUFF files are provided in Appendix B. The modelling domain and an example of a wind field over the domain is provided in Figure 5.3, which shows the lower wind speeds in the valleys and higher wind speeds atop the ridges. Generation of suitable wind speeds is necessary, as adverse odour impacts generally occur under light wind and stable atmospheric conditions.

In addition to the modelling discussion in Appendix A, the following sections discuss some of the key points in relation to dispersion modelling.

Sensitive Receptors

Sensitive receptors are locations close to the development where people or organisms could be adversely affected by the emissions from the development. For this development, the location of sensitive receptors, such as residences, are located approximately 1000m to the east of the development.

Frequency

The frequency of the modelling is the amount of time it spends at or below a given concentration. For example, modelled contours at a 99% frequency indicate that the concentration of a species will lie within the area shown by the contours for 99% of the year. Following on, for 1% of the year, there exists a potential that the species will exist at a concentration higher than that shown by the contours.

For the odour dispersion modelling performed, a frequency of 99% was used, as recommended in NSW EPA (2006).

Averaging Times

The hourly concentration output from a dispersion model is a representation of what is in the real world a constantly fluctuating quantity. The concentration of a species is constantly changing in time depending on the proximity and nature of the plume at any one instant. Thus a user-defined averaging time is input into the model, to specify the period over which the concentration will be averaged.

The averaging time used will vary from seconds to hours or even months, and is generally dependent on the nature of the receptor's sensitivity to a species. For example, in a situation where an odour nuisance is to be assessed, one is able to detect the odorous air within seconds, thus short averaging times will be used, ensuring that the extremities of the fluctuations are represented in the results.

Whilst on the other hand, for pollutants that have chronic or cumulative effects on the receptor, a longer averaging time is used. Here the amount of fluctuation of concentration is not as critical as the total average exposure.

Using a lower averaging time will give a higher concentration in the model output, as higher concentrations (which may only exist for short periods) are represented in the top ranking results. Alternatively, higher averaging times will give a lower result, as the variations in concentration are averaged out over a longer period.

For the odour dispersion modelling performed, an averaging time of 1 hour was used, as recommended in DEC, 2006a.

Peak to Mean Ratios

As recommended by NSW EPA (2006), appropriate peak to mean ratios should be applied in these modelling situations to account for fluctuation in odour concentration. The peak to mean ratios are provided in Table 6.1 of NSW EPA (2005). This table gives a specific range of values between 2.3 and 2.5 for area and volume odour sources. As all sources were considered to be area or volume sources, the more conservative peak to mean ratio of 2.5 was applied to the modelled concentrations.

Building and Biofilter Information

The dimensions of the buildings, as used in the dispersion modelling, are provided in Table 5-3.

Table 5-2: Building dimensions

Building	Length (m)	Width (m)	Height (m) ^A
AWT	100	100	10
AWT Biofilter	10	10	1
Greenwaste Composting	130	80	10
Greenwaste Composting Biofilter	33	20	1

A: height in metres above ground level.

It should be noted that the biofilters were regarded as separate units for the purposes of consistency with previous assessments, however the option to combine the two biofilters into one larger unit, as proposed in the main report, will not significantly affect the outcome of this assessment. In addition, slight changes to the location of the buildings and biofilter may occur upon finalisation of the layout of the facility. Again, slight modifications to the location of the facility are not considered to significantly affect the outcomes of this assessment.

6.1 Odour

On the basis that 2 OU (nose response time) represents the odour performance criteria, Figure 6.1 shows that the modelling has predicted an odour concentration contour 2OU approximately 900m to the east of the proposed development, located within the Brisbane Waters National Park. Thus, the predicted odour concentration at the residential area to the east of the site is below the criteria of 2 OU (nose response time).

To confirm the impact of odour on sensitive receptors close to the site, four receptor locations were chosen to be examined. Figure 6-2 shows the three closest residential receptor locations close to the proposed site. The odour concentration predicted at these locations, as shown in Table 6-1, were below 2 OU, confirming odour impact at sensitive receptors to be meet regulatory guidelines.

Table 6-1: Odour concentrations at sensitive receptors

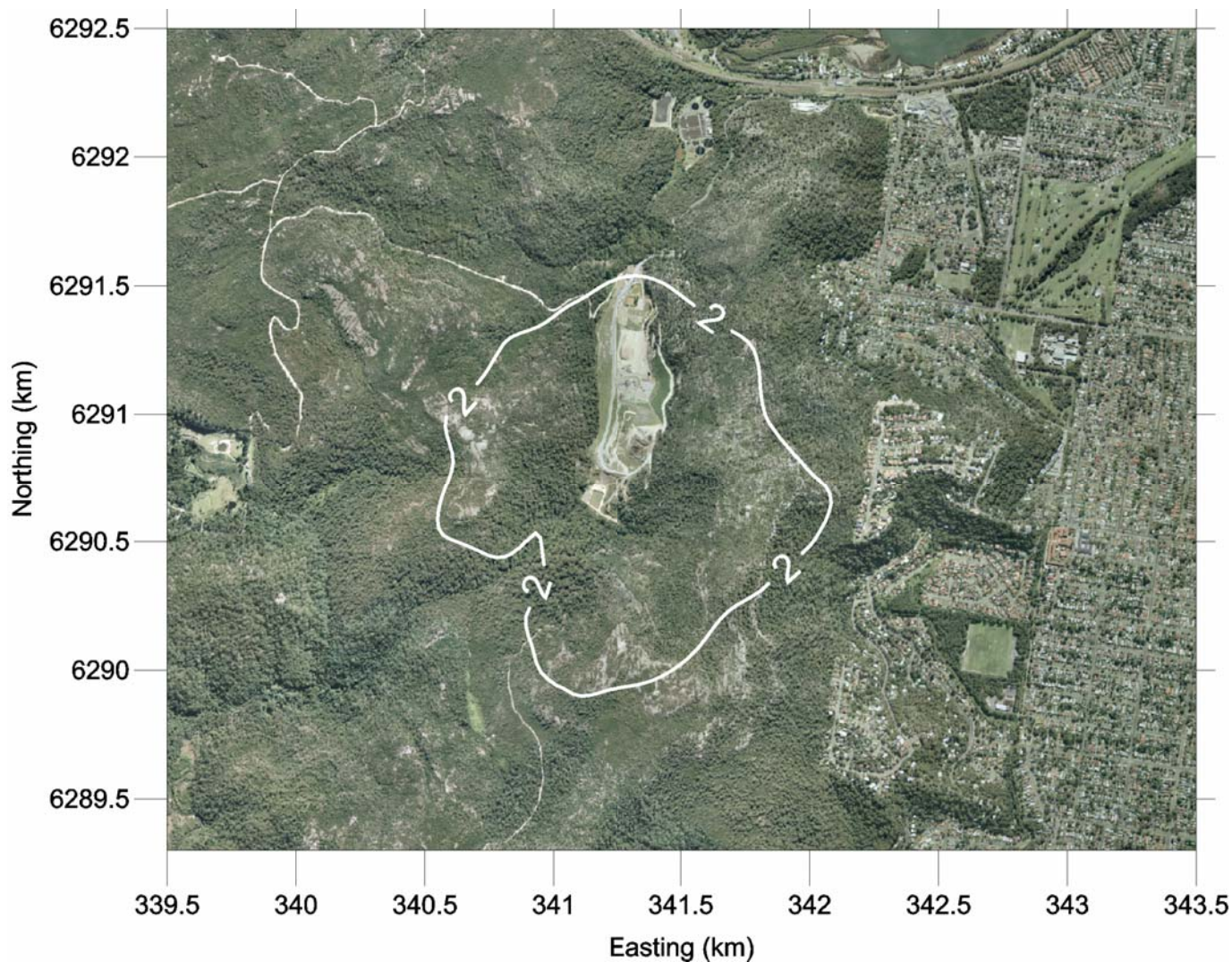
Location	Odour concentration (OU)
	(99.0%ile, Peak to Mean Ratio of 2.5)
Sensitive receptor location 1	1.1
Sensitive receptor location 2	1.7
Sensitive receptor location 3	0.7
Woy Woy STP	0.1

To further demonstrate the influence of terrain on the odorous emissions, Figure 6.3 shows the odour impacts lessening down the valleys to the north and south-west of the site, whilst ridges to the east and west of the site show increased odour impacts.

6.2 Particulate Matter

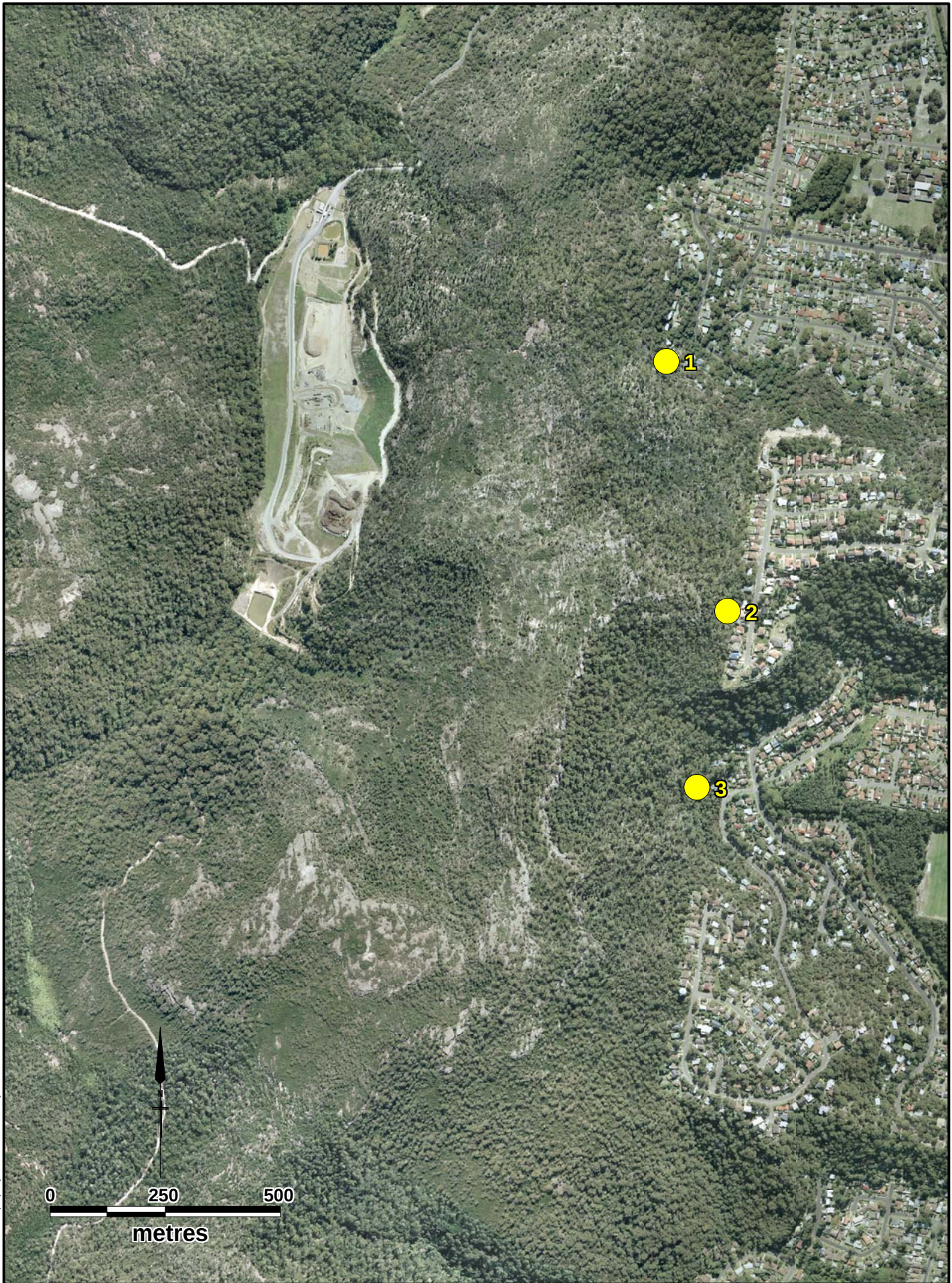
Particulate emissions generated during construction will be temporary and can be controlled using known and effective dust mitigation measures.

During operation, PM₁₀ emissions are likely to be generated from site vehicles passing over unsealed roads, however, the majority of roads on site will be sealed, limiting the adverse impacts of PM₁₀. Other site activities, such as those being performed within enclosed buildings are not anticipated to significantly add to background concentrations of PM₁₀, and therefore PM₁₀ is not considered to have a significantly adverse impact on local air quality.

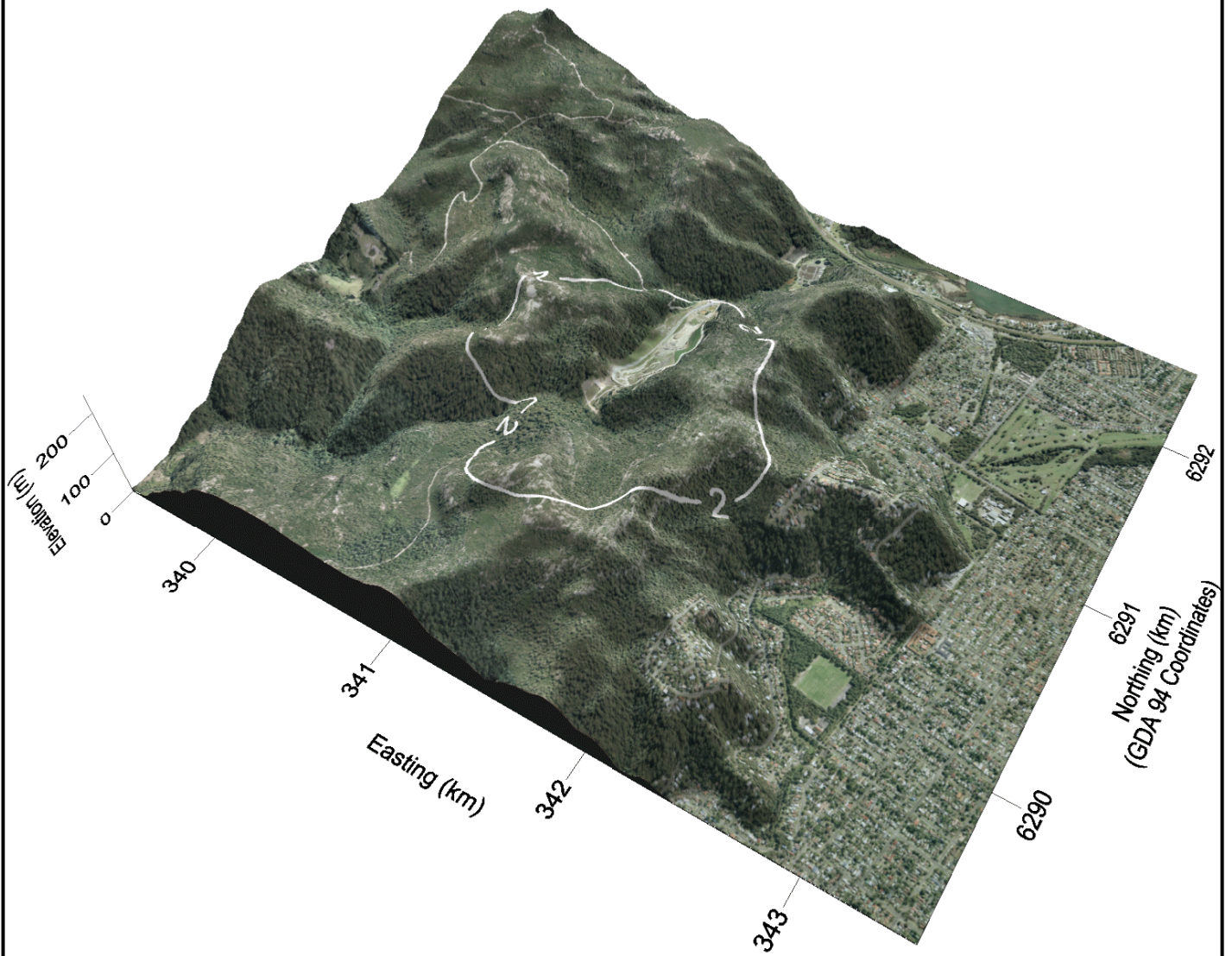


GDA94 Coordinates

Client	Project			Title
GOSFORD CITY COUNCIL	Environmental Assessment of Proposed Alternative Waste Technology and Composting Facilities at Woy Woy WMF			OPERATING FACILITY 20U CONCENTRATION CONTOUR (99.0% NOSE RESPONSE TIME)
	Drawn: AJW	Approved: FINAL	Date: 25/06/2007	Figure: 6-1
	Job No: 43177409		File No: 43177409-008.wor	



Client GOSFORD CITY COUNCIL	Project WOY WOY WASTE MANAGEMENT FACILITY			Title DISCRETE RECEPTORS
URS	Drawn: AJW	Approved: DRAFT	Date: 30/10/2006	Figure: 6-2
	Job No: 43177409		File No: 43177409-010.wor	



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Client GOSFORD CITY COUNCIL	Project WOY WOY WASTE MANAGEMENT FACILITY	Title 3D VIEW OF OPERATING FACILITY 200 CONCENTRATION CONTOUR (99.0% NOSE RESPONSE TIME)
URS	Drawn: AJW Approved: DRAFT Date: 25/06/2007 Job No: 43177409 File No: 43177409-007.wor	Figure: 6-3

6.3 Oxides of Nitrogen

NO_x is generated through the combustion of nitrogen containing fuels, and also in high temperature environments, such as a combustion engine, where nitrogen and oxygen within the air become combined to form NO and NO₂ in approximately a 9:1 ratio. When the proposed facilities are operating at peak capacity the site will have an increase of 57 trucks of per day on current levels, as well as a small number of site vehicles. There is currently planned to be no other on combustion sources on site. Due to the relatively low number of site and delivery vehicles and the lack of other combustion sources, it is considered that site contribution to ambient NO₂ concentrations will not be significant. Furthermore, it is known that NO_x generated by transport sources will disperse to background concentrations within 200m of generation (Highways, 2003). The nearest sensitive receptors to site are 1000m from the site access roads or workings.

6.4 Oxides of Sulphur

Emission of sulphur dioxide from the site will be limited to the combustion of fuels such as petrol and diesel which contain sulphur. The amount of sulphur within petrol and diesel is controlled by the Clean Fuels Act, 2000, which will continue to reduce the amount of sulphur within fuels. As a result of this legislation, high concentrations of sulphur dioxide are not associated with high traffic densities, and it is therefore considered that the site will not contribute significant amounts of sulphur dioxide to the surrounding environment.

6.5 Carbon monoxide

High CO levels are only expected where there is a high concentration of vehicles to generate the pollutant. Due to the low number of site and delivery vehicles, it would be expected that the site would not generate a high concentration of CO.

6.6 Summary

Impact of odour on the surrounding area was shown to minimal, with the highest concentration shown to be less than 2 OU at the nearest receptor. Thus odour impacts on sensitive receptors adhere to NSW odour regulations of 2 OU (nose response time) and the odour impacts are expected to be minimal.

As discussed, emissions of CO, NO_x and SO₂ are considered to be minimal from the proposed development. When these minimal emissions are dispersed in to the wider environment, it would not be expected that ambient concentrations of these pollutants would change and regional air quality would therefore be protected.

Dust generation on site will be minimised by the sealing of all site haul roads and site access roads with the exception of work within the cells. Within the unpaved areas, dust generation will be minimised through the use of water sprays in very dry weather where work is undertaken. The reduction in area for

potential dust generation combined with dust suppression techniques on remaining areas will ensure that the site impact on regional dust levels will be minimal. When dispersion is also considered with the high surface roughness of the land use surrounding the site, dust concentrations at a regional level will not be increased significantly from current levels.

7.1 During the Design Phase

The atmospheric dispersion modelling study undertaken as part of this assessment has been based on preliminary design information and covers a number of possible design options. As part of the detailed design of the development, the assumptions and emission estimates used in this assessment will be reviewed despite the conservative nature of emissions estimates used, should the expected emission rates increase over values used, the modelling will be revised to ensure that they are compliant with NSW EPA air quality standards and goals.

In addition, throughout the design process, opportunities to minimise emissions to air will be investigated and implemented wherever possible to ensure that off-site impacts are minimised.

7.2 During Construction

Environmental safeguards that would be implemented during the construction phases of the expansion are listed below. Any emissions of particulates (dust) would be specifically controlled through the implementation of these mitigation measures, which would be incorporated into a Construction Environment Management Plan (CEMP) for the works.

- Before works begin, a CEMP will be prepared which addresses air monitoring and management issues.
- In dry, windy conditions, water sprays will be used to dampen down soils prior to excavation and handling. Exposed surfaces and stockpiles will also be watered, sprayed or covered where required.
- Where practical, demolition activities or particularly dusty works will be scheduled under favourable meteorological conditions only. Earth-moving activities will be stopped when wind speeds exceed 30 km/hr.
- Vehicles will only be loaded to less than the height of the side and tailboards and loads of contaminated fill will be covered during transport. Any soil adhering to the undercarriage and wheels of trucks will be removed prior to departure from the site.
- Any long-term stockpiles will be stabilised using fast-seeding grass or synthetic cover spray.
- All major access roads will be sealed and vehicle speeds on unsealed areas will be controlled to minimise dust.

The air quality impact assessment of the proposed Woy Woy AWT Facility has been assessed against the DECC (NSW EPA) Impact Assessment Criteria as specified within DEC (2005) *Approved methods for the modelling and assessment of air pollutants within New South Wales* and NSW EPA (2006) *Technical Framework: Assessment and management of odour from stationary sources in NSW*. Limit values provided within these documents have been set with the aim of protecting public health, and in the case of odour, mitigating against public annoyance.

The air quality species assessed as part of this investigation included the following:

- Odour;
- Particulate matter (dust);
- Oxides of nitrogen;
- Sulphur dioxide; and
- Carbon monoxide.

As the primary air quality issue relating to waste processing and composting facilities is odour, this investigation focused on the generation and dispersion of odour. The odour emissions were modelled using the Calpuff dispersion modelling package, based on TAPM generated meteorological data.

Due to the highly exposed nature of the areas around the proposed site and despite conservative odour emission estimates, the proposed facility was found to have no adverse odour impacts at the nearest sensitive receptors. The predicted results showed the odour concentration to be present at a maximum concentration of 1.7 OU, at the nearest sensitive receptors, falling below the NSW odour performance criteria of 2 OU (nose response time).

The majority of site generated total suspended particulates and PM₁₀ will occur as a result of site vehicles passing over unmade roads. An undertaking to seal all site access roads and main internal haul roads will reduce the potential for dust generation. Areas where vehicles pass over unmade ground will be sprayed with water to reduce dust emissions. Using these mitigation methods, it is considered that the generation of dust will be minimised, and that concentrations at the nearest sensitive receptors will not exceed the assessment thresholds.

In relation to other atmospheric pollutants, namely oxides of nitrogen, sulphur dioxide and carbon monoxide the combustion of fossil fuel including the use of motor vehicles results in the liberation of nitrogen and carbon in all oxidation states as well as particulate matter.

Representative background data for these species was examined for the year 2005, and all combustion and industrial related pollutants were found to be below the limit values with the exception of PM₁₀. It is likely that this is due to a naturally occurring dust event and may be discounted from the record.

Such a low number of additional vehicles will not add appreciably to ambient pollutant concentrations, and given the low background levels will not result in an exceedance of the assessment criteria for nitrogen dioxide and carbon monoxide.

In conclusion, the findings of this report indicate that the proposed activities will not present an adverse impact the air quality in the area.

URS Australia Pty Ltd (URS) has prepared this report in accordance with the usual care and thoroughness of the consulting profession for the use of Gosford City Council and only those third parties who have been authorised in writing by URS to rely on the report. It is based on generally accepted practices and standards at the time it was prepared. No other warranty, expressed or implied, is made as to the professional advice included in this report. It is prepared in accordance with the scope of work and for the purpose outlined in the Proposal dated April 2006.

The methodology adopted and sources of information used by URS are outlined in this report. URS has made no independent verification of this information beyond the agreed scope of works and URS assumes no responsibility for any inaccuracies or omissions. No indications were found during our investigations that information contained in this report as provided to URS was false.

This report was prepared between October 2006 and August 2007 and is based on the conditions encountered and information reviewed at the time of preparation. URS disclaims responsibility for any changes that may have occurred after this time.

This report should be read in full. No responsibility is accepted for use of any part of this report in any other context or for any other purpose or by third parties. This report does not purport to give legal advice. Legal advice can only be given by qualified legal practitioners.

AWT (2001) *Odour Evaluation of the Glenlee Composting Operation for Camden Soil Mix Pty Ltd*. March 2001

BoM (2006) http://www.bom.gov.au/climate/averages/tables/cw_061087.shtml

Bowly (2003) Masters Thesis, *New Approaches to Landfill Odour Impact Assessment*, Macquarie University

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Highways (2003) <http://www.standardsforhighways.co.uk/dmrb/vol11/section3/11s3p01.pdf>

Kühner M, Fischer IK, (1999) Composting with Covers as an alternative to conventional (traditional) decomposting of organic matter in 75th *Colloquium of Waste* – Practical Report 25.03.1999.

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NSW EPA 2006b *Technical notes: Assessment and management of odour from stationary source in NSW*. Department of Environment & Climate Change. NSW Government.

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Appendix A

Meteorological Data Discussion

Contents

Appendix A Meteorological Data Discussion

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Appendix A

Meteorological Data Discussion

A1.1 Assessment of Meteorological Data – 2000 to 2005

The meteorological data needed for dispersion modelling is required to be site representative. The closest weather station to the Woy Woy Landfill site is located at Narara Research Station, approximately 14km north-northeast (GDA94 344592mE, 6303685mN) of the proposed site.

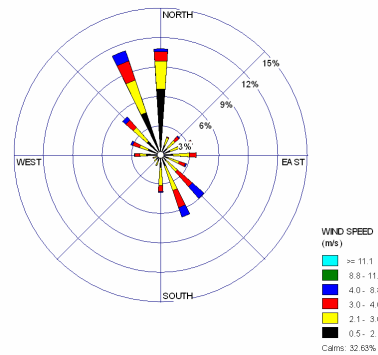
Due to its location in the foothills of Mt Penang, the Narara meteorological station was considered to be affected by localised terrain-induced flows, therefore not suitable for inclusion in the meteorological modelling for the Woy Woy site. However, the data was considered an indicator of the regional climate. Thus, URS examined six years from 2000 through to 2005 as recommended by DEC (2005) *Approved Methods for the Modelling and Assessment of Air Pollutants in New South Wales*.

The Narara Research Station windroses for 2000 – 2005 are shown in Figure A.1. The examination of the six years showed extremely low wind speeds at the Narara AWS, and the high occurrence of calms in the vicinity of 30%. The average wind speed showed little difference from year to year, with a range between 1.49 m/s to 1.59m/s, the average being 1.53 m/s. The year 2004 appears to be consistent with other years, does not show any anomalous characteristics. Where possible, the most recent meteorological data is used in the assessments, however, 2005 was shown to have a low average wind speed, when compared to other years, consequently the year 2004 was considered suitable for use within this assessment.

The generation and assessment of site specific meteorological data is discussed in the following sections.

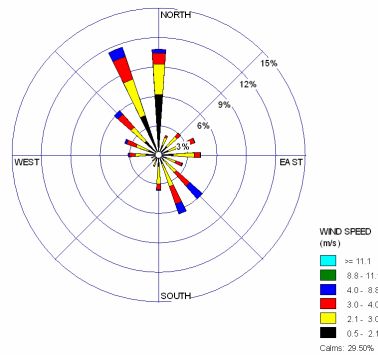
Appendix A

Meteorological Data Discussion



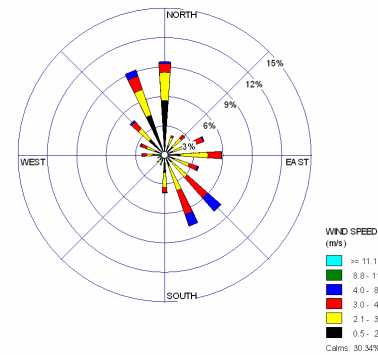
2000

Average wind speed: 1.49 m/s



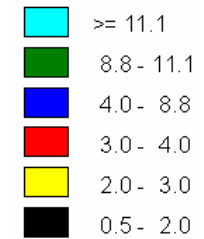
2001

Average wind speed: 1.59 m/s

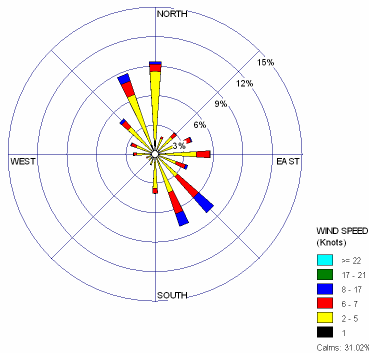


2002

Average wind speed: 1.55 m/s

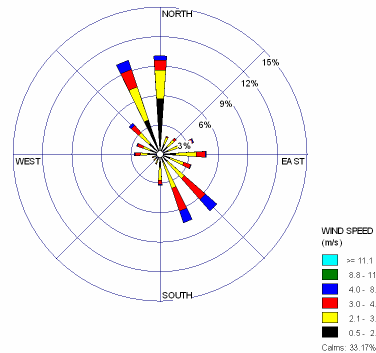


Wind Speed Legend (m/s)



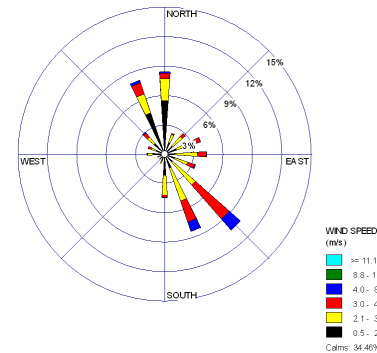
2003

Average wind speed: 1.55 m/s



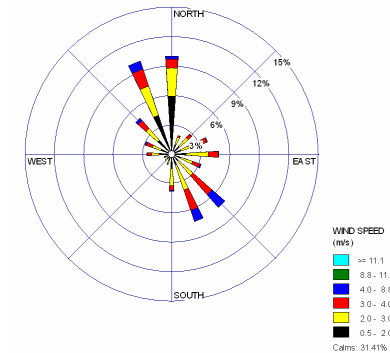
2004

Average wind speed: 1.51 m/s



2005

Average wind speed: 1.39 m/s



All years

Average wind speed: 1.53 m/s

Figure A.1: Narara Research station wind roses 2000-2004

Appendix A

Meteorological Data Discussion

A1.2 Meteorological Data Generation Using TAPM

Where site specific meteorological data does not exist, the DEC (2005) *Approved Methods for the Modelling and Assessment of Air Pollutants in New South Wales* suggests the use of CSIRO's The Air Pollution Model (TAPM) to predict site specific meteorology, which is based on regional meteorological observations.

TAPM was run to calculate meteorological fields for the modelling domain. Through a number of verification studies (e.g. CSIRO 2005), TAPM has been identified as a suitable model of choice to simulate meteorological fields in a number of situations¹.

TAPM is an incompressible, non-hydrostatic, primitive equation model with a terrain-following vertical co-ordinate for three-dimensional simulations. It includes parameterisations for cloud/rain micro-physical processes, turbulence closure, urban/vegetative canopy and soil, and radiative fluxes.

Whilst the Narara AWS was located within the TAPM modelling domain for the first three nests, the wind information was not included for assimilation in the TAPM Meteorological modelling, as the small radius of influence used for the Narara data would limit it from affecting meteorology at or nearby the Woy Woy site.

TAPM was configured as detailed below:

- Grid centre coordinates $-33^{\circ}30.5'$ latitude, $151^{\circ}17.5'$ longitude (GDA 341326mE, 6291051mN);
- Four nested grid domains with 25 x 25 points at the following resolution: 10km, 3km, 1km, 300m
- Twenty-five vertical grid levels from 10 to 8000m;
- Terrain, vegetation and soil type data at a 250m grid spacing from the US Geological Survey, Earth Resources Observation System (EROS) Data Centre Distributed Active Archive Centre (EDC DAAC);
- Sea surface temperature data at 100km grid intervals from the US National Centre for Atmospheric Research (NCAR); and
- Six hourly synoptic scale meteorology on a 75 to 100 km grid: this data is derived from the Bureau of Meteorology's Limited Area Prediction System (LAPS).

Upon completion, the TAPM meteorological data was further processed in Calmet, which was needed for incorporation into the dispersion model, Calpuff.

¹ CSIRO, 2005. *The Air Pollution Model (TAPM) Version 3. Part 2: Summary of Some Verification Studies*. CSIRO Atmospheric Research Technical Paper 72, 2005.

Appendix A

Meteorological Data Discussion

A1.3 Dispersion Meteorology Generation Using Calmet

Calmet was run with the following parameters and options:

- 49 x 49 Grid Points at 150m resolution (Total grid dimensions of 7.2 x 7.2km) using high resolution terrain and land use data.
- TAPM Generated Surface and Upper air meteorological stations for a point 1 kilometre northwest of the site (339826mE 6292551mN) site for the year 2004.
- CSUMM formatted TAPM output for use in the 'initial guess' stage of wind field generation.
- 9 vertical levels ranging from 10 to 1500m (cell centers).

An example of the Calmet generated wind fields can be seen in Figure 5.3. This figure of the full 7.2 x 7.2km Calmet domain shows Calmet's ability to produce flow vector fields that reflect the localised terrain and land use.

Upon completion, the meteorological data was used as input data in the dispersion model for the assessment, namely Calpuff.

A1.4 Assessment of Meteorological data 2004

A1.4.1 Wind Speed and Direction

The Calmet produced wind roses are presented in Figure A.2 and show the dominance of high wind speed in the area surrounding the site. Westerly winds are seen to be dominant throughout the year, with the exception of summer where regional northerly winds coupled with afternoon sea breezes result in a north-easterly trend to wind patterns.

TAPM has predicted calm conditions (wind speeds less than 0.5m/s) for 0.4% of the year, on an hourly averaged basis. This is as would be expected for an elevated (170m) coastal location that is so openly exposed from all directions. This is also consistent with wind frequency distributions for locations of this type in the region, where annual calms of less than 1% are experienced.

Appendix A

Meteorological Data Discussion

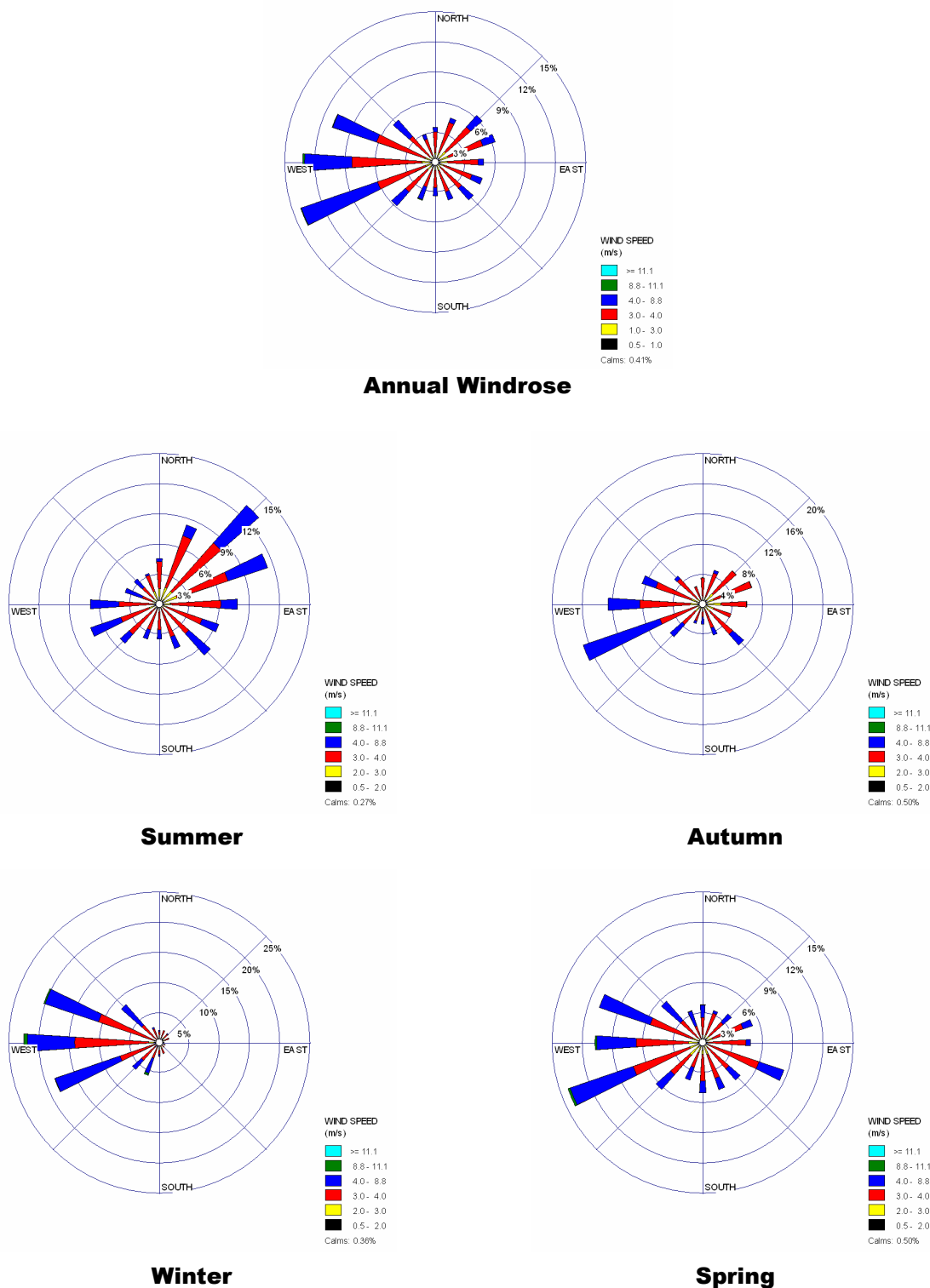


Figure A.2: TAPM/Calmet generated Windroses for Woy Woy Landfill (2004)

Appendix A

Meteorological Data Discussion

The presence of east to north-easterly sea breezes is indicated in the wind rose for summer afternoons (3-6pm) shown below, in Figure A.3.

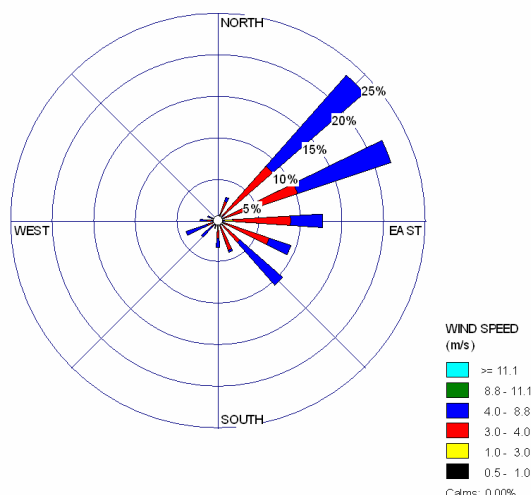


Figure A.3 – Summer afternoon sea breezes

A1.4.2 Atmospheric Stability

Stability class is used as an indicator of atmospheric dispersion for use in dispersion models. Gaussian Atmospheric dispersion calculation is generally based on the Pasquill-Gifford-Turner scheme where six categories are used (A to F) which represent atmospheric stability from extremely unstable to moderately stable conditions. The stability class of the atmosphere is based on two main characteristics, these being:

- Static Stability/Convective turbulence (vertical temperature profiles as dictated by radiative heating of the ground);and
- Mechanical turbulence (as a function of wind speed and surface roughness).

The Pasquill Gifford Stability classes are provided in Table A.1.

The relative frequency of stability classes for the site have been extracted from the Calmet generated meteorological file and are shown in Table A.1.

Appendix A

Meteorological Data Discussion

Table A.1: Modified Pasquill-Gifford Stability Classes (adapted from Turner, 1994)

Surface Wind Speed at 10m (m/s)	Insolation			Night-time cloud (Oktas)	
	Strong	Moderate	Slight	Thinly overcast of > 4/8 low cloud	< 3/8 Cloud
≤ 2	A	A-B	B	-	-
2 - 3	A-B	B	C	E	F
3 - 5	B	B-C	C	D	E
5 - 6	C	C-D	D	D	D
> 6	C	D	D	D	D

The Pasquill Gifford Stability Classes, shown in Table A.2 show neutral atmospheric conditions (Stability Class D) is the most prevalent Stability Class of the area, with the extreme stability classes, namely Extremely Unstable (Stability Class A) being the least prevalent

Table A.2: Site Representative Pasquill-Gifford Stability Classes

Stability Class	% of year
A	0.8%
B	10.9%
C	18.6%
D	29.4%
E	23.2%
F	17.0%

In addition to their composition, Calmet predicted Stability Classes are also presented as a function of time of day, as shown in Figure A.4. The Stability Classes in Figure A.4 are labelled 1 through 6 and refer to Stability Classes A (Extremely Unstable) through F (Very Stable) respectively. As expected, there is a tendency for the unstable classes (Stability Classes A, B and C) to occur during daytime, whilst the more stable conditions (Stability Classes D, E and F) are shown to occur primarily during night time.

Appendix A

Meteorological Data Discussion

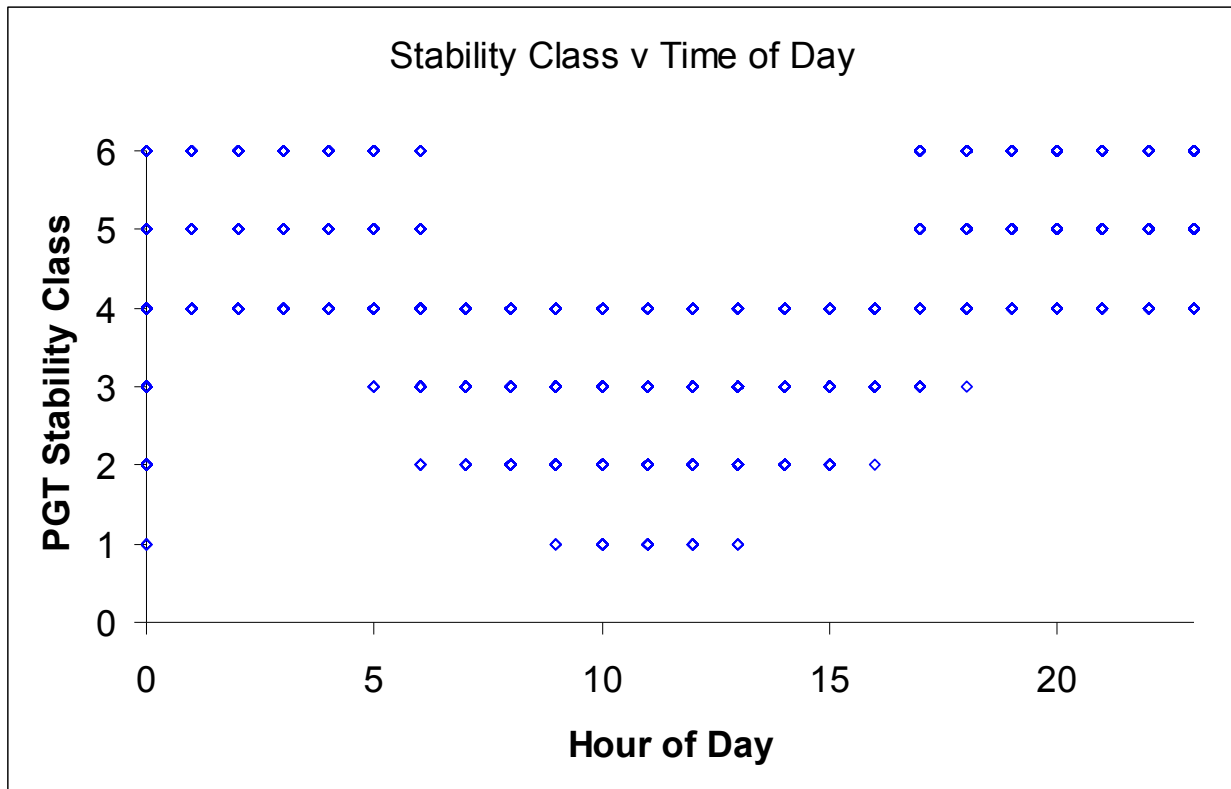


Figure A.4: Stability Class vs Time of Day, as generated by Calmet/TAPM at Woy Woy Landfill, 2004

In Figure A.5 stability Classes are shown against wind speed,. The Stability Classes in Figure A.5 are labelled 1 through 6 and refer to Stability Classes A through F respectively. As expected, the highest wind speeds are associated with stable or neutral stability classes (Stability Classes C and D). The more unstable conditions (Stability Classes A and B) are associated with situations where there are lower wind speeds present, coupled with radiative heating of the ground. When this occurs convective turbulence leads to strong vertical mixing (assisting dispersion). The more stable conditions (Stability Classes E and F) also are also associated with lower wind speeds, but in the absence of radiative heating (i.e. night). Here the absence of both mechanical and convective turbulence acts to minimise dispersion. The data are consistent with the values contained in Table A.1.

Appendix A

Meteorological Data Discussion

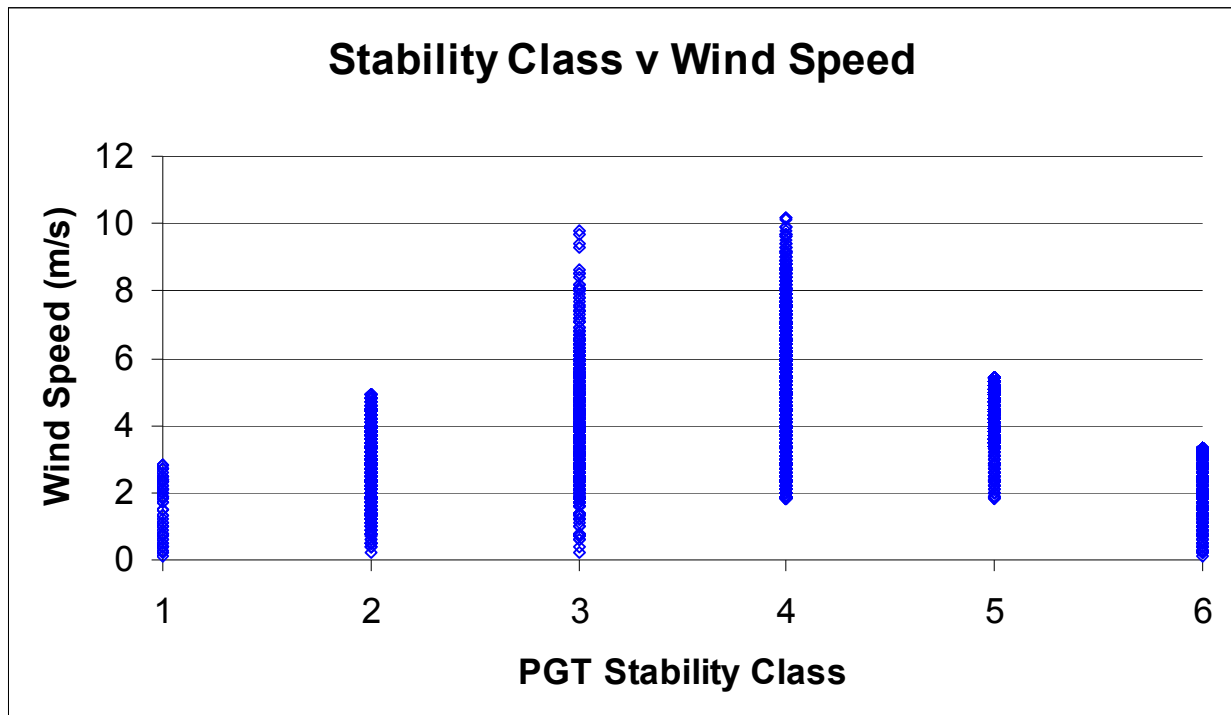


Figure A.5: Stability Class vs Wind Speed – as generated by Calmet/TAPM at Woy Woy Landfill, 2004

A1.5 Conclusion

Where site specific meteorological data does not exist, as is the case for the Woy Woy Landfill site, the predicted meteorological data used in the dispersion modelling is required to be representative of the surrounding area. It is an accepted standard Australian practice, that in situations where adequate site-specific meteorological data does not exist, TAPM is used to synthetically generate meteorological data. TAPM is a sophisticated, 3D meteorological model that has been extensively validated.

The assessment of the predicted meteorology at the Woy Woy Landfill site was discussed and was shown to be consistent with general atmospheric parameters. It is therefore considered that the meteorological data used in dispersion modelling is appropriate.

Appendix B

Dispersion Modelling Files

Appendix B
Dispersion Modelling Files
CALPUFF List File

```

WWCP5.LST                                     10/06/2007
***** CALPUFF Version: 6.113 Lev *****

Clock time: 16:10:54
Date: 06-10-2007

Internal Coordinate Transformations by --- COORDLIB Version: 1.96 Level: 05

Run Title:
Woy Woy MSW/Greenwaste Facility Odour Modelling

-----
INPUT GROUP: 1 -- General run control parameters
-----
Option to run all periods found
in the met. file (METRUN) Default: 0 ! METRUN = 0 !

METRUN = 0 - Run period explicitly defined below
METRUN = 1 - Run all periods in met. file

Starting date: Year (IBYR) -- No default ! IBYR = 2004 !
               Month (IBMO) -- No default ! IBMO = 1 !
               Day (IBDY) -- No default ! IDY = 1 !
Starting time: Hour (IBHR) -- No default ! IBHR = 0 !
               Minute (IBMIN) -- No default ! IBMIN = 0 !
               Second (IBSEC) -- No default ! IBSEC = 0 !

Ending date: Year (IEYR) -- No default ! IEYR = 2004 !
              Month (IEMO) -- No default ! IEMO = 12 !
              Day (IEDY) -- No default ! IEDY = 31 !
Ending time: Hour (IEHR) -- No default ! IEHR = 23 !
              Minute (IEMIN) -- No default ! IEMIN = 0 !
              Second (IESEC) -- No default ! IESEC = 0 !

(These are only used if METRUN = 0)

Base time zone (XBTZ) -- No default ! XBTZ= -10.0 !
The zone is the number of hours that must be
ADDED to the time to obtain UTC (or GMT)
Examples: PST = 8., MST = 7.
          CST = 6., EST = 5.

Length of modeling time-step (seconds)
Equal to update period in the primary
meteorological data files, or an
integer fraction of it (1/2, 1/3 ...)
Must be no larger than 1 hour
(NSECDT) Default: 3600 ! NSECDT = 3600 !
Units: seconds

Number of chemical species (NSPEC)
Default: 5 ! NSPEC = 1 !

Number of chemical species
to be emitted (NSE) Default: 3 ! NSE = 1 !

Flag to stop run after
SETUP phase (ITEST) Default: 2 ! ITEST = 2 !
(Used to allow checking
of the model inputs, files, etc.)
ITEST = 1 - STOPS program after SETUP phase
ITEST = 2 - Continues with execution of program

1

```

```

WWCP5.LST                                     10/06/2007
after SETUP

Restart Configuration:

Control flag (MRESTART) Default: 0 ! MRESTART = 0 !

0 = Do not read or write a restart file
1 = Read a restart file at the beginning of
the run
2 = Write a restart file during run
3 = Read a restart file at beginning of run
and write a restart file during run

Number of periods in Restart
output cycle (NRESPD) Default: 0 ! NRESPD = 0 !

0 = File written only at last period
>0 = File updated every NRESPD periods

Meteorological Data Format (METFM)
Default: 1 ! METFM = 1 !

METFM = 1 - CALMET binary file (CALMET.MET)
METFM = 2 - ISC ASCII file (ISCMET.MET)
METFM = 3 - AUSPLUME ASCII file (PLMMET.MET)
METFM = 4 - CTDm plus tower file (PROFILE.DAT) and
surface parameters file (SURFACE.DAT)
METFM = 5 - AERMET tower file (PROFILE.DAT) and
surface parameters file (SURFACE.DAT)

Meteorological Profile Data Format (MPRFFM)
(used only for METFM = 1, 2, 3)
Default: 1 ! MPRFFM = 1 !

MPRFFM = 1 - CTDm plus tower file (PROFILE.DAT)
MPRFFM = 2 - AERMET tower file (PROFILE.DAT)

PG sigma-y is adjusted by the factor (AVET/PGTIME)**0.2
Averaging Time (minutes) (AVET) Default: 60.0 ! AVET = 60. !
PG Averaging Time (minutes) (PGTIME) Default: 60.0 ! PGTIME = 60. !

!END!

-----
NOTICE: Starting year in control file sets the
expected century for the simulation. All
YY years are converted to YYYY years in
the range: 1954 2053
-----

INPUT GROUP: 2 -- Technical options
-----

Vertical distribution used in the
near field (MGAUSS) Default: 1 ! MGAUSS = 1 !
0 = uniform
1 = Gaussian

Terrain adjustment method
(MCTADJ) Default: 3 ! MCTADJ = 3 !
0 = no adjustment
1 = ISC-type of terrain adjustment
2 = simple, CALPUFF-type of terrain
adjustment
3 = partial plume path adjustment

2

```

```

WWCP5.LST                                     10/06/2007

Subgrid-scale complex terrain
flag (MCTSG) Default: 0 ! MCTSG = 0 !
0 = not modeled
1 = modeled

Near-field puffs modeled as
elongated slugs? (MSLUG) Default: 0 ! MSLUG = 0 !
0 = no
1 = yes (slug model used)

Transitional plume rise modeled?
(MTRANS) Default: 1 ! MTRANS = 0 !
0 = no (i.e., final rise only)
1 = yes (i.e., transitional rise computed)

Stack tip downwash? (MTIP) Default: 1 ! MTIP = 0 !
0 = no (i.e., no stack tip downwash)
1 = yes (i.e., use stack tip downwash)

Method used to simulate building
downwash? (MBDW) Default: 1 ! MBDW = 1 !
1 = ISC method
2 = PRIME method

Vertical wind shear modeled above
stack top? (MSHEAR) Default: 0 ! MSHEAR = 0 !
0 = no (i.e., vertical wind shear not modeled)
1 = yes (i.e., vertical wind shear modeled)

Puff splitting allowed? (MSPLIT) Default: 0 ! MSPLIT = 0 !
0 = no (i.e., puffs not split)
1 = yes (i.e., puffs are split)

Chemical mechanism flag (MCHEM) Default: 1 ! MCHEM = 0 !
0 = chemical transformation not
modeled
1 = transformation rates computed
internally (MESOPUFF II scheme)
2 = user-specified transformation
rates used
3 = transformation rates computed
internally (RIVAD/ARM3 scheme)
4 = secondary organic aerosol formation
computed (MESOPUFF II scheme for OH)

Aqueous phase transformation flag (MAQCHEM)
(Used only if MCHEM = 1, or 3) Default: 0 ! MAQCHEM = 0 !
0 = aqueous phase transformation
not modeled
1 = transformation rates adjusted
for aqueous phase reactions

Wet removal modeled? (MWET) Default: 1 ! MWET = 0 !
0 = no
1 = yes

Dry deposition modeled? (MDRY) Default: 1 ! MDRY = 0 !
0 = no
1 = yes
(dry deposition method specified
for each species in Input Group 3)

Gravitational settling (plume tilt)
modeled? (MTILT) Default: 0 ! MTILT = 0 !
0 = no
1 = yes
(puff center falls at the gravitational
settling velocity for 1 particle species)

Restrictions:
- MDRY = 1

3

```

```

WWCP5.LST                                     10/06/2007

- NSPEC = 1 (must be particle species as well)
- sg = 0 GEOMETRIC STANDARD DEVIATION in Group 8 is
set to zero for a single particle diameter

Method used to compute dispersion
coefficients (MDISP) Default: 3 ! MDISP = 3 !

1 = dispersion coefficients computed from measured values
of turbulence, sigma v, sigma w
2 = dispersion coefficients from internally calculated
sigma v, sigma w using micrometeorological variables
(u*, w*, L, etc.)
3 = PG dispersion coefficients for RURAL areas (computed using
the ISCST multi-segment approximation) and MP coefficients in
urban areas
4 = same as 3 except PG coefficients computed using
the MESOPUFF II eqns.
5 = CTDm sigmas used for stable and neutral conditions.
For unstable conditions, sigmas are computed as in
MDISP = 3, described above. MDISP = 5 assumes that
measured values are read

Sigma-v/sigma-theta, sigma-w measurements used? (MTURBVW)
(Used only if MDISP = 1 or 5) Default: 3 ! MTURBVW = 3 !
1 = use sigma-v or sigma-theta measurements
from PROFILE.DAT to compute sigma-y
(valid for METFM = 1, 2, 3, 4, 5)
2 = use sigma-w measurements
from PROFILE.DAT to compute sigma-z
(valid for METFM = 1, 2, 3, 4, 5)
3 = use both sigma-(v/theta) and sigma-w
from PROFILE.DAT to compute sigma-y and sigma-z
(valid for METFM = 1, 2, 3, 4, 5)
4 = use sigma-theta measurements
from PLMMET.DAT to compute sigma-y
(valid only if METFM = 3)

Back-up method used to compute dispersion
when measured turbulence data are
missing (MDISP2) Default: 3 ! MDISP2 = 3 !
(used only if MDISP = 1 or 5)
2 = dispersion coefficients from internally calculated
sigma v, sigma w using micrometeorological variables
(u*, w*, L, etc.)
3 = PG dispersion coefficients for RURAL areas (computed using
the ISCST multi-segment approximation) and MP coefficients in
urban areas
4 = same as 3 except PG coefficients computed using
the MESOPUFF II eqns.

[DIAGNOSTIC FEATURE]
Method used for Lagrangian timescale for Sigma-y
(used only if MDISP=1,2 or MDISP2=1,2)
(MTAULY) Default: 0 ! MTAULY = 0 !
0 = Draxler default 617,284 (s)
1 = Computed as Lag. Length / (.75 q) -- after SCIPUFF
10 < Direct user input (s) -- e.g., 306.9

[DIAGNOSTIC FEATURE]
Method used for Advective-Decay timescale for Turbulence
(used only if MDISP=2 or MDISP2=2)
(MTAUADV) Default: 0 ! MTAUADV = 0 !
0 = No turbulence advection
1 = Computed (OPTION NOT IMPLEMENTED)
10 < Direct user input (s) -- e.g., 300

Method used to compute turbulence sigma-v &
sigma-w using micrometeorological variables
(Used only if MDISP = 2 or MDISP2 = 2)
(MCTURB) Default: 1 ! MCTURB = 1 !
1 = Standard CALPUFF subroutines

4

```

WWCP5.LST 10/06/2007

2 = AERMOD subroutines

PG sigma-y,z adj. for roughness? Default: 0 ! MROUGH = 0 !
(MROUGH)
0 = no
1 = yes

Partial plume penetration of Default: 1 ! MPARTL = 0 !
elevated inversion? (MPARTL)
0 = no
1 = yes

Strength of temperature inversion Default: 0 ! MTINV = 0 !
provided in PROFILE.DAT extended records? (MTINV)
0 = no (computed from measured/default gradients)
1 = yes

PDF used for dispersion under convective conditions? Default: 0 ! MPDF = 0 !
(MPDF)
0 = no
1 = yes

Sub-Grid TIBL module used for shore line? Default: 0 ! MSGTIBL = 0 !
(MSGTIBL)
0 = no
1 = yes

Boundary conditions (concentration) modeled? Default: 0 ! MBCON = 0 !
(MBCON)
0 = no
1 = yes, using formatted BCON.DAT file
2 = yes, using unformatted CONC.DAT file

Note: MBCON > 0 requires that the last species modeled be 'BCON'. Mass is placed in species BCON when generating boundary condition puffs so that clean air entering the modeling domain can be simulated in the same way as polluted air. Specify zero emission of species BCON for all regular sources.

Individual source contributions saved? Default: 0 ! MSOURCE = 0 !
(MSOURCE)
0 = no
1 = yes

Analyses of fogging and icing impacts due to emissions from arrays of mechanically-forced cooling towers can be performed using CALPUFF in conjunction with a cooling tower emissions processor (CTEMISS) and its associated postprocessors. Hourly emissions of water vapor and temperature from each cooling tower cell are computed for the current cell configuration and ambient conditions by CTEMISS. CALPUFF models the dispersion of these emissions and provides cloud information in a specialized format for further analysis. Output to FOG.DAT is provided in either 'plume mode' or 'receptor mode' format.

Configure for FOG Model output? Default: 0 ! MFOG = 0 !
(MFOG)
0 = no
1 = yes - report results in PLUME Mode format
2 = yes - report results in RECEPTOR Mode format

Test options specified to see if they conform to regulatory

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values? (MREG) Default: 1 ! MREG = 0 !

0 = NO checks are made
1 = Technical options must conform to USEPA Long Range Transport (LRT) guidance

METFM 1 or 2
AVET 60. (min)
PGTIME 60. (min)
MGAUSS 1
MCTADJ 3
MTRANS 1
MTIP 1
MCHM 1 or 3 (if modeling SOx, NOx)
MMET 1
MDRY 1
MDISP 2 or 3
MPDF 0 if MDISP=3
1 if MDISP=2
MROUGH 0
MPARTL 1
SYTDEF 550. (m)
MHFTSZ 0

!END!

INPUT GROUP: 3a, 3b -- Species list

Subgroup (3a)

The following species are modeled:

! CSPEC = ODOR ! !END!

SPECIES NAME (Limit: 12 Characters in length)	MODELED (0=NO, 1=YES)	EMITTED (0=NO, 1=YES)	Dry DEPOSITED (0=NO, 1=COMPUTED-GAS 2=COMPUTED-PARTICLE 3=USER-SPECIFIED)	OUTPUT NUMB (0=NON 1=1st 2=2nd 3= etc
! ODOR =	1,	1,	0,	0 !

!END!

Note: The last species in (3a) must be 'BCON' when using the boundary condition option (MBCON > 0). Species BCON should typically be modeled as inert (no chem transformation or removal).

Subgroup (3b)

The following names are used for Species-Groups in which results for certain species are combined (added) prior to output. The CGRUP name will be used as the species name in output files. Use this feature to model specific particle-size distributions by treating each size-range as a separate species. Order must be consistent with 3(a) above.

INPUT GROUP: 4 -- Map Projection and Grid control parameters

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Projection for all (X,Y):

Map projection (PMAP) Default: UTM ! PMAP = UTM !

UTM : Universal Transverse Mercator
TMM : Tangential Transverse Mercator
LCC : Lambert Conformal Conic
PS : Polar Stereographic
EM : Equatorial Mercator
LAZA : Lambert Azimuthal Equal Area

False Easting and Northing (km) at the projection origin
(Used only if PMAP= TTM, LCC, or LAZA)
(FEAST) Default=0.0 ! FEAST = 0.000 !
(FNORTH) Default=0.0 ! FNORTH = 0.000 !

UTM zone (1 to 60)
(Used only if PMAP=UTM)
(UTMZN) No Default ! IUTMZN = 56 !

Hemisphere for UTM projection?
(Used only if PMAP=UTM)
(UTMHM) Default: N ! UTMHEM = S !
N : Northern hemisphere projection
S : Southern hemisphere projection

Latitude and Longitude (decimal degrees) of projection origin
(Used only if PMAP= TTM, LCC, PS, EM, or LAZA)
(RLATO) No Default ! RLATO = 0N !
(RLONO) No Default ! RLONO = 0E !

TTM : RLONO identifies central (true N/S) meridian of projection
RLATO selected for convenience
LCC : RLONO identifies central (true N/S) meridian of projection
RLATO selected for convenience
PS : RLONO identifies central (grid N/S) meridian of projection
RLATO selected for convenience
EM : RLONO identifies central meridian of projection
RLATO is REPLACED by 0.0N (Equator)
LAZA: RLONO identifies longitude of tangent-point of mapping plane
RLATO identifies latitude of tangent-point of mapping plane

Matching parallel(s) of latitude (decimal degrees) for projection
(Used only if PMAP= LCC or PS)
(XLAT1) No Default ! XLAT1 = 0N !
(XLAT2) No Default ! XLAT2 = 0N !

LCC : Projection cone slices through Earth's surface at XLAT1 and XLAT2
PS : Projection plane slices through Earth at XLAT1
(XLAT2 is not used)

Note: Latitudes and longitudes should be positive, and include a letter N,S,E, or W indicating north or south latitude, and east or west longitude. For example,
35.9 N Latitude = 35.9N
118.7 E Longitude = 118.7E

Datum-region

The Datum-Region for the coordinates is identified by a character string. Many mapping products currently available use the model of the Earth known as the World Geodetic System 1984 (WGS-84). Other local models may be in use, and their selection in CALMET will make its output consistent with local mapping products. The list of Datum-Regions with official transformation parameters is provided by the National Imagery and Mapping Agency (NIMA).

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NIMA Datum - Regions(Examples)

WGS-84 WGS-84 Reference Ellipsoid and Geoid, Global coverage (WGS84)
NAS-C NORTH AMERICAN 1927 Clarke 1866 Spheroid, MEAN FOR CONUS (NAD27)
NAR-C NORTH AMERICAN 1983 GRS 80 Spheroid, MEAN FOR CONUS (NAD83)
NWS-84 NWS 6370KM Radius, Sphere
ESR-S ESR1 REFERENCE 6371KM Radius, Sphere

Datum-region for output coordinates
(DATUM) Default: WGS-84 ! DATUM = WGS-84 !

METEOROLOGICAL Grid:

Rectangular grid defined for projection PMAP, with X the Easting and Y the Northing coordinate

No. X grid cells (NX)	No default	! NX = 49 !
No. Y grid cells (NY)	No default	! NY = 49 !
No. vertical layers (NZ)	No default	! NZ = 9 !
Grid spacing (DGRIDKM)	No default	! DGRIDKM = .15 !
Units: km		
Cell face heights (ZFACE(nz+1))	No defaults	
Units: m		
! ZFACE = .0, 20.0, 40.0, 60.0, 90.0, 150.0, 250.0, 500.0, 1000.0, 2000.0 !		
Reference Coordinates of SOUTHWEST corner of grid cell(1, 1):		
X coordinate (XORIGKM)	No default	! XORIGKM = 337.717 !
Y coordinate (YORIGKM)	No default	! YORIGKM = 6287.453 !
Units: km		

COMPUTATIONAL Grid:

The computational grid is identical to or a subset of the MET. grid. The lower left (LL) corner of the computational grid is at grid point (IBCOMP, JBCOMP) of the MET. grid. The upper right (UR) corner of the computational grid is at grid point (IECOMP, JECOMP) of the MET. grid. The grid spacing of the computational grid is the same as the MET. grid.

X index of LL corner (IBCOMP) (1 <= IBCOMP <= NX)	No default	! IBCOMP = 11 !
Y index of LL corner (JBCOMP) (1 <= JBCOMP <= NY)	No default	! JBCOMP = 11 !
X index of UR corner (IECOMP) (1 <= IECOMP <= NX)	No default	! IECOMP = 39 !
Y index of UR corner (JECOMP) (1 <= JECOMP <= NY)	No default	! JECOMP = 39 !

SAMPLING Grid (GRIDDED RECEPTORS):

The lower left (LL) corner of the sampling grid is at grid point (IBSAMP, JBSAMP) of the MET. grid. The upper right (UR) corner of the sampling grid is at grid point (IESAMP, JESAMP) of the MET. grid. The sampling grid must be identical to or a subset of the computational grid. It may be a nested grid inside the computational grid. The grid spacing of the sampling grid is DGRIDKM/MESHDM.

Logical flag indicating if gridded receptors are used (LSAMP) Default: T ! LSAMP = T !

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```

(T=yes, F=no)

X index of LL corner (IBSAMP)      No default      ! IBSAMP = 11 !
(BCOMP <= IBSAMP <= IECOMP)

Y index of LL corner (JBSAMP)      No default      ! JBSAMP = 11 !
(JBCOMP <= JBSAMP <= JECOMP)

X index of UR corner (IESAMP)      No default      ! IESAMP = 39 !
(BCOMP <= IESAMP <= IECOMP)

Y index of UR corner (JESAMP)      No default      ! JESAMP = 39 !
(JBCOMP <= JESAMP <= JECOMP)

Nesting factor of the sampling
grid (MESHDN)                      Default: 1      ! MESHDN = 1 !
(MESHDN is an integer >= 1)

!END!

```

INPUT GROUP: 5 -- Output Options

FILE	DEFAULT VALUE	VALUE THIS RUN
Concentrations (ICON)	1	! ICON = 1 !
Dry Fluxes (IDRY)	1	! IDRY = 0 !
Wet Fluxes (IWET)	1	! IWET = 0 !
2D Temperature (IT2D)	0	! IT2D = 0 !
2D Density (IRHO)	0	! IRHO = 0 !
Relative Humidity (IVIS)	1	! IVIS = 0 !
(relative humidity file is required for visibility analysis)		
Use data compression option in output file? (LCOMPRS)	Default: T	! LCOMPRS = T !

*
0 = Do not create file, 1 = create file

QA PLOT FILE OUTPUT OPTION:
Create a standard series of output files (e.g. locations of sources, receptors, grids ...) suitable for plotting?
(IQAPLOT) Default: 1 ! IQAPLOT = 1 !
0 = no
1 = yes

DIAGNOSTIC MASS FLUX OUTPUT OPTIONS:
Mass flux across specified boundaries for selected species reported? (IMFLX) Default: 0 ! IMFLX = 0 !
0 = no
1 = yes (FLUXBDY.DAT and MASSFLX.DAT filenames are specified in Input Group 0)

Mass balance for each species reported? (IMBAL) Default: 0 ! IMBAL = 0 !
0 = no
1 = yes (MASSBAL.DAT filename is specified in Input Group 0)

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LINE PRINTER OUTPUT OPTIONS:

	Default:	
Print concentrations (ICPRT)	0	! ICPRT = 0 !
Print dry fluxes (IDPRT)	0	! IDPRT = 0 !
Print wet fluxes (IWPRT)	0	! IWPRT = 0 !
(0 = Do not print, 1 = Print)		
Concentration print interval (ICFRQ) in timesteps	1	! ICFRQ = 1 !
Dry flux print interval (IDFRQ) in timesteps	1	! IDFRQ = 1 !
Wet flux print interval (IWFRQ) in timesteps	1	! IWFRQ = 1 !
Units for Line Printer Output (IPRTU)	1	! IPRTU = 1 !
for Concentration	g/m**3	Deposition g/m**2/s
1 =	mg/m**3	mg/m**2/s
2 =	ug/m**3	ug/m**2/s
3 =	ng/m**3	ng/m**2/s
4 =	Odour Units	
5 =		

Messages tracking progress of run written to the screen ? (IMESG) Default: 2 ! IMESG = 2 !
0 = no
1 = yes (advection step, puff ID)
2 = yes (YYYYJJJHH, # old puffs, # emitted puffs)

SPECIES (or GROUP for combined species) LIST FOR OUTPUT OPTIONS

SPECIES /GROUP	PRINTED?	SAVED ON DISK?	PRINTED?	SAVED ON DISK?	PRINTED?
ODOR =	0,	1,	0,	0,	0,

Note: Species BCON (for MBCON > 0) does not need to be saved on disk.

OPTIONS FOR PRINTING "DEBUG" QUANTITIES (much output)

	Default:	
Logical for debug output (LDEBUG)	F	! LDEBUG = F !
First puff to track (IPFDEB)	1	! IPFDEB = 1 !
Number of puffs to track (NPFDEB)	1	! NPFDEB = 1 !
Met. period to start output (NN1)	1	! NN1 = 1 !
Met. period to end output (NN2)	10	! NN2 = 10 !

!END!

INPUT GROUP: 6a, 6b, & 6c -- Subgrid scale complex terrain inputs

Subgroup (6a)

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Number of terrain features (NHILL) Default: 0 ! NHILL = 0 !

Number of special complex terrain receptors (NCTREC) Default: 0 ! NCTREC = 0 !

Terrain and CTSG Receptor data for CTSG hills input in CTD format ? (MHILL) No Default ! MHILL = 2 !
1 = Hill and Receptor data created by CTD processors & read from HILL.DAT and HILLRCT.DAT files
2 = Hill data created by OPTHILL & input below in Subgroup (6b); Receptor data in Subgroup (6c)

Factor to convert horizontal dimensions to meters (MHILL=1) Default: 1.0 ! XHILL2M = 1.0 !

Factor to convert vertical dimensions to meters (MHILL=1) Default: 1.0 ! ZHILL2M = 1.0 !

X-origin of CTD system relative to CALPUFF coordinate system, in Kilometers (MHILL=1) No Default ! XCTDMKM = 0 !

Y-origin of CTD system relative to CALPUFF coordinate system, in Kilometers (MHILL=1) No Default ! YCTDMKM = 0 !

! END !

Subgroup (6b)

HILL information 1 **

HILL NO.	XC (km)	YC (km)	THETAH (deg.)	ZGRID (m)	RELIEF (m)	EXPO 1 (m)	EXPO 2 (m)	SCA (

Subgroup (6c)

COMPLEX TERRAIN RECEPTOR INFORMATION

XRCT (km)	YRCT (km)	ZRCT (m)	XHH

1 Description of Complex Terrain Variables:
XC, YC = Coordinates of center of hill
THETAH = Orientation of major axis of hill (clockwise from North)
ZGRID = Height of the 0 of the grid above mean sea level
RELIEF = Height of the crest of the hill above the grid elevation
EXPO 1 = Hill-shape exponent for the major axis
EXPO 2 = Hill-shape exponent for the minor axis
SCALE 1 = Horizontal length scale along the major axis
SCALE 2 = Horizontal length scale along the minor axis
AMAX = Maximum allowed axis length for the major axis
BMAX = Maximum allowed axis length for the minor axis

XRCT, YRCT = Coordinates of the complex terrain receptors
ZRCT = Height of the ground (MSL) at the complex terrain Receptor
XHH = Hill number associated with each complex terrain receptor (NOTE: MUST BE ENTERED AS A REAL NUMBER)

** NOTE: DATA for each hill and CTSG receptor are treated as a separate input subgroup and therefore must end with an input group terminator.

INPUT GROUP: 7 -- Chemical parameters for dry deposition of gases

SPECIES NAME	DIFFUSIVITY (cm**2/s)	ALPHA STAR	REACTIVITY	MESOPHYLL RESIST (s/cm)

!END!

INPUT GROUP: 8 -- Size parameters for dry deposition of particles

For SINGLE SPECIES, the mean and standard deviation are used to compute a deposition velocity for NINT (see group 9) size-ranges, and these are then averaged to obtain a mean deposition velocity.

For GROUPED SPECIES, the size distribution should be explicitly specified (by the 'species' in the group), and the standard deviation for each should be entered as 0. The model will then use the deposition velocity for the stated mean diameter.

SPECIES NAME	GEOMETRIC MASS MEAN DIAMETER (microns)	GEOMETRIC STANDARD DEVIATION (microns)

!END!

INPUT GROUP: 9 -- Miscellaneous dry deposition parameters

	Default:	
Reference cuticle resistance (s/cm) (RCUTR)	30	! RCUTR = 30.0 !
Reference ground resistance (s/cm) (RGR)	10	! RGR = 10.0 !
Reference pollutant reactivity (REACTR)	8	! REACTR = 8.0 !
Number of particle-size intervals used to evaluate effective particle deposition velocity (NINT)	9	! NINT = 9 !
Vegetation state in unirrigated areas (IVEG)	1	! IVEG = 1 !
IVEG=1 for active and unstressed vegetation IVEG=2 for active and stressed vegetation IVEG=3 for inactive vegetation		

!END!

INPUT GROUP: 10 -- Wet Deposition Parameters

Scavenging Coefficient -- Units: (sec)**(-1)

Pollutant	Liquid Precip.	Frozen Precip.
!END!		

INPUT GROUP: 11 -- Chemistry Parameters

Ozone data input option (MOZ) Default: 1 ! MOZ = 0 !
 (Used only if MCHM = 1, 3, or 4)
 0 = use a monthly background ozone value
 1 = read hourly ozone concentrations from the OZONE.DAT data file

Monthly ozone concentrations
 (Used only if MCHM = 1, 3, or 4 and
 MOZ = 0 or MOZ = 1 and all hourly O3 data missing)
 (BCKO3) in ppb Default: 12*80.
 ! BCKO3 = 80.00, 80.00, 80.00, 80.00, 80.00, 80.00, 80.00, 80.00, 80.00, 80.00

Monthly ammonia concentrations
 (Used only if MCHM = 1, or 3)
 (BCKNH3) in ppb Default: 12*10.
 ! BCKNH3 = 10.00, 10.00, 10.00, 10.00, 10.00, 10.00, 10.00, 10.00, 10.00, 10.00, 1

Nighttime SO2 loss rate (RNITE1)
 in percent/hour Default: 0.2 ! RNITE1 = .2 !

Nighttime NOx loss rate (RNITE2)
 in percent/hour Default: 2.0 ! RNITE2 = 2.0 !

Nighttime HNO3 formation rate (RNITE3)
 in percent/hour Default: 2.0 ! RNITE3 = 2.0 !

H2O2 data input option (MH2O2) Default: 1 ! MH2O2 = 1 !
 (Used only if MQACHEM = 1)
 0 = use a monthly background H2O2 value
 1 = read hourly H2O2 concentrations from the H2O2.DAT data file

Monthly H2O2 concentrations
 (Used only if MQACHEM = 1 and
 MH2O2 = 0 or MH2O2 = 1 and all hourly H2O2 data missing)
 (BCKH2O2) in ppb Default: 12*1.
 ! BCKH2O2 = 1.00, 1.00, 1.00, 1.00, 1.00, 1.00, 1.00, 1.00, 1.00, 1.00, 1.0

--- Data for SECONDARY ORGANIC AEROSOL (SOA) Option
 (used only if MCHM = 4)

The SOA module uses monthly values of:
 Fine particulate concentration in ug/m³ (BCKPMF)
 Organic fraction of fine particulate (OFRAC)
 VOC / NOX ratio (after reaction) (VCNX)
 to characterize the air mass when computing
 the formation of SOA from VOC emissions.
 Typical values for several distinct air mass types are:

Month	1	2	3	4	5	6	7	8	9	10	11	12
	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Clean Continental												
BCKPMF	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.	1.
OFRAC	.15	.15	.20	.20	.20	.20	.20	.20	.20	.20	.20	.15
VCNX	50.	50.	50.	50.	50.	50.	50.	50.	50.	50.	50.	50.

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Clean Marine (surface)

BCKPMF	.5	.5	.5	.5	.5	.5	.5	.5	.5	.5	.5	.5
OFRAC	.25	.25	.30	.30	.30	.30	.30	.30	.30	.30	.30	.25
VCNX	50.	50.	50.	50.	50.	50.	50.	50.	50.	50.	50.	50.

Urban - low biogenic (controls present)

BCKPMF	30.	30.	30.	30.	30.	30.	30.	30.	30.	30.	30.	30.
OFRAC	.20	.20	.25	.25	.25	.25	.25	.25	.20	.20	.20	.20
VCNX	4.	4.	4.	4.	4.	4.	4.	4.	4.	4.	4.	4.

Urban - high biogenic (controls present)

BCKPMF	60.	60.	60.	60.	60.	60.	60.	60.	60.	60.	60.	60.
OFRAC	.25	.25	.30	.30	.30	.30	.30	.30	.20	.20	.20	.25
VCNX	15.	15.	15.	15.	15.	15.	15.	15.	15.	15.	15.	15.

Regional Plume

BCKPMF	20.	20.	20.	20.	20.	20.	20.	20.	20.	20.	20.	20.
OFRAC	.20	.20	.25	.25	.25	.25	.25	.25	.20	.20	.20	.20
VCNX	15.	15.	15.	15.	15.	15.	15.	15.	15.	15.	15.	15.

Urban - no controls present

BCKPMF	100.	100.	100.	100.	100.	100.	100.	100.	100.	100.	100.	100.
OFRAC	.30	.30	.35	.35	.35	.35	.35	.35	.20	.20	.20	.30
VCNX	2.	2.	2.	2.	2.	2.	2.	2.	2.	2.	2.	2.

Default: Clean Continental

BCKPMF	1.00,	1.00,	1.00,	1.00,	1.00,	1.00,	1.00,	1.00,	1.00,	1.00,	1.00,	1.00
OFRAC	0.15,	0.15,	0.20,	0.20,	0.20,	0.20,	0.20,	0.20,	0.20,	0.20,	0.20,	0.20
VCNX	50.00,	50.00,	50.00,	50.00,	50.00,	50.00,	50.00,	50.00,	50.00,	50.00,	50.00,	50.00

!END!

INPUT GROUP: 12 -- Misc. Dispersion and Computational Parameters

Horizontal size of puff (m) beyond which
 time-dependent dispersion equations (Heffter)
 are used to determine sigma-y and
 sigma-z (SYTDEP) Default: 550. ! SYTDEP = 5.5E02

Switch for using Heffter equation for sigma z
 as above (0 = Not use Heffter; 1 = use Heffter
 (MHFTSZ) Default: 0 ! MHFTSZ = 0 !

Stability class used to determine plume
 growth rates for puffs above the boundary
 layer (JSUP) Default: 5 ! JSUP = 5 !

Vertical dispersion constant for stable
 conditions (k1 in Eqn. 2.7-3) (CONK1) Default: 0.01 ! CONK1 = .01 !

Vertical dispersion constant for neutral/
 unstable conditions (k2 in Eqn. 2.7-4)
 (CONK2) Default: 0.1 ! CONK2 = .1 !

Factor for determining Transition-point from
 Schulman-Scire to Huber-Snyder Building Downwash
 scheme (SS used for Hs < Hb + TBD * HL)
 (TBD) Default: 0.5 ! TBD = .5 !

TBD < 0 ==> always use Huber-Snyder
 TBD = 1.5 ==> always use Schulman-Scire
 TBD = 0.5 ==> ISC Transition-point

Range of land use categories for which
 urban dispersion is assumed
 (IURB1, IURB2) Default: 10 ! IURB1 = 10 !
 19 ! IURB2 = 10 !

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Site characterization parameters for single-point Met data files -----
 (needed for METFM = 2,3,4,5)

Land use category for modeling domain
 (ILANDUIN) Default: 20 ! ILANDUIN = 20

Roughness length (m) for modeling domain
 (Z0IN) Default: 0.25 ! Z0IN = .25 !

Leaf area index for modeling domain
 (XLAIIN) Default: 3.0 ! XLAIIN = 3.0 !

Elevation above sea level (m)
 (ELEVIN) Default: 0.0 ! ELEVIN = .0 !

Latitude (degrees) for met location
 (XLATIN) Default: -999. ! XLATIN = -999.0

Longitude (degrees) for met location
 (XLONIN) Default: -999. ! XLONIN = -999.0

Specialized information for interpreting single-point Met data files ----

Anemometer height (m) (Used only if METFM = 2,3)
 (ANEMHT) Default: 10. ! ANEMHT = 10.0 !

Form of lateral turbulence data in PROFILE.DAT file
 (Used only if METFM = 4,5 or MTURBVW = 1 or 3)
 (ISIGMAV) Default: 1 ! ISIGMAV = 1 !
 0 = read sigma-theta
 1 = read sigma-v

Choice of mixing heights (Used only if METFM = 4)
 (IMIXCTDM) Default: 0 ! IMIXCTDM = 0
 0 = read PREDICTED mixing heights
 1 = read OBSERVED mixing heights

Maximum length of a slug (met. grid units)
 (MXMLEN) Default: 1.0 ! MXMLEN = 1.0 !

Maximum travel distance of a puff/slug (in
 grid units) during one sampling step
 (XSAMLEN) Default: 1.0 ! XSAMLEN = 1.0 !

Maximum Number of slugs/puffs release from
 one source during one time step
 (MXNEW) Default: 99 ! MXNEW = 99 !

Maximum Number of sampling steps for
 one puff/slug during one time step
 (MXSAM) Default: 99 ! MXSAM = 99 !

Number of iterations used when computing
 the transport wind for a sampling step
 that includes gradual rise (for CALMET
 and PROFILE winds)
 (NCOUNT) Default: 2 ! NCOUNT = 2 !

Minimum sigma y for a new puff/slug (m)
 (SYMIN) Default: 1.0 ! SYMIN = 1.0 !

Minimum sigma z for a new puff/slug (m)
 (SZMIN) Default: 1.0 ! SZMIN = 1.0 !

Default minimum turbulence velocities sigma-v and sigma-w
 for each stability class over land and over water (m/s)
 (SVMIN(12) and SWMIN(12))

Stab Class :	LAND						WATER					
	A	B	C	D	E	F	A	B	C	D	E	
Default SVMIN :	.50	.50	.50	.50	.50	.50	.37	.37	.37	.37	.37	.37

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Default SWMIN : .20, .12, .08, .06, .03, .016, .20, .12, .08, .06, .03,
 ! SVMIN = 0.500, 0.500, 0.500, 0.500, 0.500, 0.500, 0.370, 0.370, 0.37
 ! SWMIN = 0.200, 0.120, 0.080, 0.060, 0.030, 0.016, 0.200, 0.120, 0.08

Divergence criterion for dw/dz across puff
 used to initiate adjustment for horizontal
 convergence (1/s)
 Partial adjustment starts at CDIV(1), and
 full adjustment is reached at CDIV(2)
 (CDIV(2)) Default: 0.0,0.0 ! CDIV = .0, .0

Minimum wind speed (m/s) allowed for
 non-calm conditions. Also used as minimum
 speed returned when using power-law
 extrapolation toward surface
 (WSCALM) Default: 0.5 ! WSCALM = .5 !

Maximum mixing height (m)
 (XMAXZI) Default: 3000. ! XMAXZI = 3000.0

Minimum mixing height (m)
 (XMINZI) Default: 50. ! XMINZI = 50.0 !

Default wind speed classes --
 5 upper bounds (m/s) are entered;
 the 6th class has no upper limit
 (WSCAT(5)) Default :
 ISC RURAL : 1.54, 3.09, 5.14, 8.23, 10.8 (10
 Wind Speed Class : 1 2 3 4 5
 ! WSCAT = 1.54, 3.09, 5.14, 8.23, 10.80 !

Default wind speed profile power-law
 exponents for stabilities 1-6
 (PLX0(6)) Default : ISC RURAL values
 ISC RURAL : .07, .07, .10, .15, .35, .55
 ISC URBAN : .15, .15, .20, .25, .30, .30

Stability Class : A B C D E F
 ! PLX0 = 0.07, 0.07, 0.10, 0.15, 0.35, 0.

Default potential temperature gradient
 for stable classes E, F (degK/m)
 (PTG0(2)) Default: 0.020, 0.035
 ! PTG0 = 0.020, 0.035 !

Default plume path coefficients for
 each stability class (used when option
 for partial plume height terrain adjustment
 is selected -- MCTADJ=3)
 (PPC(6)) Stability Class : A B C D E F
 Default PPC : .50, .50, .50, .50, .35, .3
 ! PPC = 0.50, 0.50, 0.50, 0.50, 0.35, 0.

Slug-to-puff transition criterion factor
 equal to sigma-y/length of slug
 (SL2PF) Default: 10. ! SL2PF = 10.0 !

Puff-splitting control variables -----

VERTICAL SPLIT

Number of puffs that result every time a puff
 is split - nsplit=2 means that 1 puff splits
 into 2 (NSPLIT) Default: 3 ! NSPLIT = 3 !

Time(s) of a day when split puffs are eligible to

16

```

per day, around sunset before nocturnal shear develops.
24 values: 0 is midnight (00:00) and 23 is 11 PM (23:00)
Odo not re-split      l=eligible for re-split
(IRESPPLIT(24))           Default: Hour 17 = 1
! IRESPPLIT = 0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0 !

Split is allowed only if last hour's mixing
height (m) exceeds a minimum value
(ZISPLITH)                   Default: 100.          ! ZISPLITH = 100.0

Split is allowed only if ratio of last hour's
mixing ht to the maximum mixing ht experienced
by the puff is less than a maximum value (this
postpones a split until a nocturnal layer develops)
(ROLDMAX)                   Default: 0.25          ! ROLDMAX = 0.25 !

HORIZONTAL SPLIT
-----

Number of puffs that result every time a puff
is split - nsplith=5 means that 1 puff splits
into 5
(NSPLITH)                   Default: 5              ! NSPLITH = 5 !

Minimum sigma-y (Grid Cells Units) of puff
before it may be split
(SYSPLITH)                  Default: 1.0            ! SYSPLITH = 1.0 !

Minimum puff elongation rate (SYSPLITH/hr) due to
wind shear, before it may be split
(SHSPLITH)                  Default: 2.             ! SHSPLITH = 2.0 !

Minimum concentration (g/m^3) of each
species in puff before it may be split
Enter array of NSPEC values; if a single value is
entered, it will be used for ALL species
(CNSPLITH)                  Default: 1.0E-07         ! CNSPLITH = 1.0E-
                                07

Integration control variables -----

Fractional convergence criterion for numerical SLUG
sampling integration
(EFSSLUG)                   Default: 1.0e-04       ! EFSSLUG = 1.0E-0
                                4

Fractional convergence criterion for numerical AREA
source integration
(EPSAREA)                   Default: 1.0e-06       ! EPSAREA = 1.0E-0
                                6

Trajectory step-length (m) used for numerical rise
integration
(DSRISE)                    Default: 1.0            ! DSRISE = 1.0 !

Boundary Condition (BC) Puff control variables -----

Minimum height (m) to which BC puffs are mixed as they are emitted
(MBCON=2 ONLY). Actual height is reset to the current mixing height
at the release point if greater than this minimum.
(HTMINBC)                   Default: 500.          ! HTMINBC = 500.0

Search radius (km) about a receptor for sampling nearest BC puff.
BC puffs are typically emitted with a spacing of one grid cell
length, so the search radius should be greater than DGRIDKM.
(RSAMPCB)                   Default: 10.           ! RSAMPCB = 10.0 !

Near-Surface depletion adjustment to concentration profile used when
sampling BC puffs?
(MDEPBC)                    Default: 1              ! MDEPBC = 1 !
0 = Concentration is NOT adjusted for depletion
1 = Adjust Concentration for depletion

```

```

INPUT GROUPS: 13a, 13b, 13c, 13d -- Point source parameters
-----
Subgroup (13a)
-----
Number of point sources with
parameters provided below      (NPT1)  No default  !  NPT1 =  0  !

Units used for point source
emissions below                (IPTU)  Default: 1  !  IPTU =  1  !
1 =      g/s
2 =      kg/hr
3 =      lb/hr
4 =      tons/yr
5 =      Odour Unit * m**3/s  (vol. flux of odour compound)
6 =      Odour Unit * m**3/min
7 =      metric tons/yr

Number of source-species
combinations with variable
emissions scaling factors
provided below in (13d)        (NSPT1) Default: 0  !  NSPT1 =  0  !

Number of point sources with
variable emission parameters
provided in external file      (NPT2)  No default  !  NPT2 =  0  !

(If NPT2 > 0, these point
source emissions are read from
the file: PTEMARB.DAT)

!END!

```

Subgroup (13b)									a
POINT SOURCE: CONSTANT DATA									
Source No.	X Coordinate (km)	Y Coordinate (km)	Stack Height (m)	Base Elevation (m)	Stack Diameter (m)	Exit Vel. (m/s)	Exit Temp. (deg. K)	Bldg Wash	
a Data for each source are treated as a separate input subgroup and therefore must end with an input group terminator. SRCNAM is a 12-character name for a source (No default) X is an array holding the source data listed by the column headings (No default) SIGYZI is an array holding the initial sigma-y and sigma-z (m) (Default: 0.0,.) FMFAC is a vertical momentum flux factor (0. or 1.0) used to represent the effect of rain-caps or other physical configurations that reduce momentum rise associated with the actual exit velocity. (Default: 1.0 -- full momentum used) ZPLTFM is the platform height (m) for sources influenced by an isolated structure that has a significant open area between the surface and the bulk of the structure, such as an offshore oil platform. The Base Elevation is that of the surface (ground or ocean), and the Stack Height is the release height above the Base (not									

above the platform). Building heights entered in Subgroup 13c must be those of the buildings on the platform, measured from the platform deck. ZPLTFM is used only with MBDW=1 (ISC downwash method) for sources with building downwash. (Default: 0.0)

b

- 0. = No building downwash modeled
- 1. = Downwash modeled for buildings resting on the surface
- 2. = Downwash modeled for buildings raised above the surface (ZPLTFM > 0.)

NOTE: must be entered as a REAL number (i.e., with decimal point)

^c An emission rate must be entered for every pollutant modeled. Enter emission rate of zero for secondary pollutants that are modeled, but not emitted. Units are specified by IPTU (e.g. 1 for g/s).

Subgroup (13c)

BUILDING DIMENSION DATA FOR SOURCES SUBJECT TO DOWNWASH

Source No.	a
	Effective building height, width, length and X/Y offset (in meters) every 10 degrees. LENGTH, XBADJ, and YBADJ are only needed for MBDW=2 (PRIME downwash option)

a Building height, width, length, and X/Y offset from the source are treated as a separate input subgroup for each source and therefore must end with an input group terminator. The X/Y offset is the position, relative to the stack, of the center of the upwind face of the projected building, with the x-axis pointing along the flow direction.

Subgroup (13d)

Use this subgroup to describe temporal variations in the emission rates given in 13b. Factors entered multiply the rates in 13b. Skip sources here that have constant emissions. For more elaborate variation in source parameters, use PTEMARB.DAT and NPT2 > 0.

IVARY determines the type of variation, and is source-specific:
(IVARY) Default: 0

0	=	Constant	
1	=	Diurnal cycle	(24 scaling factors: hours 1-24)
2	=	Monthly cycle	(12 scaling factors: months 1-12)
3	=	Hour & Season	(4 groups of 24 hourly scaling factors, where first group is DEC-JAN-FEB)
4	=	Speed & Stab.	(6 groups of 6 scaling factors, where first group is Stability Class A, and the speed classes have upper bounds (m/s) defined in Group 12
5	=	Temperature	(12 scaling factors, where temperature classes have upper bounds (C) of: 0, 5, 10, 15, 20, 25, 30, 35, 40, 45, 50, 50+)

^a Data for each species are treated as a separate input subgroup

and therefore must end with an input group terminator.

INPUT GROUPS: 14a, 14b, 14c, 14d -- Area source parameters

```

Subgroup (14a)
-----

Number of polygon area sources with
parameters specified below (NAR1)           No default ! NAR1 = 5 !

Units used for area source
emissions below (IARU)                     Default: 1 ! IARU = 5 !
1 =      g/m**2/s
2 =      kg/m**2/hr
3 =      lb/m**2/hr
4 =      tons/m**2/yr
5 =      Odour Unit * m/s (vol. flux/m**2 of odour compound)
6 =      Odour Unit * m/min
7 =      metric tons/m**2/yr

Number of source-species
combinations with variable
emissions scaling factors
provided below in (14d)                     (NSAR1) Default: 0 ! NSAR1 = 0 !

Number of buoyant polygon area sources
with variable location and emission
parameters (NAR2)                           No default ! NAR2 = 0 !
(If NAR2 > 0, ALL parameter data for
these sources are read from the file: BAEMARB.DAT)

'END'

```

Subgroup (14b)

AREA SOURCE: CONSTANT DATA

Source No.	Effect. Height (m)	Base Elevation (m)	Initial Sigma z (m)	Emission Rates
1: SRCNAM = GOBF !				
1: X = 1.0,	115.0,	1.5,	2.8E00 !	!END!
2: SRCNAM = AWTBF !				
2: X = 1.0,	115.0,	1.0,	2.5E00 !	!END!
3: SRCNAM = MGWOR !				
3: X = 0.0,	140.0,	2.0,	4.6E-01 !	!END!
4: SRCNAM = LEACH !				
4: X = 0.0,	68.0,	1.0,	8.33E-01 !	!END!
5: SRCNAM = TIPFF !				
5: X = 0.0,	100.0,	2.0,	2.7E00 !	!END!

a
Data for each source are treated as a separate input subgroup
and therefore must end with an input group terminator.

b An emission rate must be entered for every pollutant modeled. Enter emission rate of zero for secondary pollutants that are modeled, but not emitted. Units are specified by IARU (e.g. 1 for $g/m^2/s$).

Subgroup (14c)

COORDINATES (km) FOR EACH VERTEX(4) OF EACH POLYGON

Source No. Ordered list of X followed by list of Y, grouped by source

1 ! SRCNAM = GOBF !
1 ! XVERT = 341.18, 341.213, 341.213, 341.18!
1 ! YVERT = 6290.63, 6290.63, 6290.61, 6290.61!
!END!
2 ! SRCNAM = AWTBF !
2 ! XVERT = 341.24, 341.25, 341.25, 341.24!
2 ! YVERT = 6290.633, 6290.633, 6290.623, 6290.623!
!END!
3 ! SRCNAM = MGOWR !
3 ! XVERT = 341.295, 341.376, 341.35, 341.266!
3 ! YVERT = 6290.934, 6290.888, 6290.819, 6290.869!
!END!
4 ! SRCNAM = LEACHT !
4 ! XVERT = 341.295, 341.318, 341.318, 341.295!
4 ! YVERT = 6291.453, 6291.453, 6291.43, 6291.43!
!END!
5 ! SRCNAM = TIFPAC !
5 ! XVERT = 341.17, 341.2, 341.2, 341.17!
5 ! YVERT = 6291.18, 6291.18, 6291.15, 6291.15!
!END!

a
Data for each source are treated as a separate input subgroup
and therefore must end with an input group terminator.

Subgroup (14d)

AREA SOURCE: VARIABLE EMISSIONS DATA

Use this subgroup to describe temporal variations in the emission rates given in 14b. Factors entered multiply the rates in 14b. Skip sources here that have constant emissions. For more elaborate variation in source parameters, use BAEMARB.DAT and NAR2 > 0.

IVARY determines the type of variation, and is source-specific:
(IVARY) Default: 0
0 = Constant
1 = Diurnal cycle (24 scaling factors: hours 1-24)
2 = Monthly cycle (12 scaling factors: months 1-12)
3 = Hour & Season (4 groups of 24 hourly scaling factors, where first group is DEC-JAN-FEB)
4 = Speed & Stab. (6 groups of 6 scaling factors, where first group is Stability Class A, and the speed classes have upper bounds (m/s) defined in Group 12
5 = Temperature (12 scaling factors, where temperature classes have upper bounds (C) of: 0, 5, 10, 15, 20, 25, 30, 35, 40, 45, 50, 50+)

a
Data for each species are treated as a separate input subgroup
and therefore must end with an input group terminator.

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INPUT GROUPS: 15a, 15b, 15c -- Line source parameters

Subgroup (15a)

Number of buoyant line sources with variable location and emission parameters (NLN2) No default ! NLN2 = 0 !
(if NLN2 > 0, ALL parameter data for these sources are read from the file: LNMARB.DAT)
Number of buoyant line sources (NLINES) No default ! NLINES = 0 !
Units used for line source emissions below (ILNU) Default: 1 ! ILNU = 1 !
1 = g/s
2 = kg/hr
3 = lb/hr
4 = tons/yr
5 = Odour Unit * m**3/s (vol. flux of odour compound)
6 = Odour Unit * m**3/min
7 = metric tons/yr
Number of source-species combinations with variable emissions scaling factors provided below in (15c) (NSLN1) Default: 0 ! NSLN1 = 0 !
Maximum number of segments used to model each line (MXNSEG) Default: 7 ! MXNSEG = 7 !
The following variables are required only if NLINES > 0. They are used in the buoyant line source plume rise calculations.
Number of distances at which transitional rise is computed Default: 6 ! NLRISE = 6 !
Average building length (XL) No default ! XL = .0 ! (in meters)
Average building height (HBL) No default ! HBL = .0 ! (in meters)
Average building width (WBL) No default ! WBL = .0 ! (in meters)
Average line source width (WML) No default ! WML = .0 ! (in meters)
Average separation between buildings (DXL) No default ! DXL = .0 ! (in meters)
Average buoyancy parameter (FPRIMEL) No default ! FPRIMEL = .0 ! (in m**4/s**3)
!END!

Subgroup (15b)

BUOYANT LINE SOURCE: CONSTANT DATA

Source No.	Beg. X Coordinate (km)	Beg. Y Coordinate (km)	End. X Coordinate (km)	End. Y Coordinate (km)	Release Height (m)	Base Elevation (m)	Em
------------	------------------------	------------------------	------------------------	------------------------	--------------------	--------------------	----

22

a
Data for each source are treated as a separate input subgroup
and therefore must end with an input group terminator.

b
An emission rate must be entered for every pollutant modeled. Enter emission rate of zero for secondary pollutants that are modeled, but not emitted. Units are specified by ILNTU (e.g. 1 for g/s).

Subgroup (15c)

BUOYANT LINE SOURCE: VARIABLE EMISSIONS DATA

Use this subgroup to describe temporal variations in the emission rates given in 15b. Factors entered multiply the rates in 15b. Skip sources here that have constant emissions.

IVARY determines the type of variation, and is source-specific:
(IVARY) Default: 0
0 = Constant
1 = Diurnal cycle (24 scaling factors: hours 1-24)
2 = Monthly cycle (12 scaling factors: months 1-12)
3 = Hour & Season (4 groups of 24 hourly scaling factors, where first group is DEC-JAN-FEB)
4 = Speed & Stab. (6 groups of 6 scaling factors, where first group is Stability Class A, and the speed classes have upper bounds (m/s) defined in Group 12
5 = Temperature (12 scaling factors, where temperature classes have upper bounds (C) of: 0, 5, 10, 15, 20, 25, 30, 35, 40, 45, 50, 50+)

a
Data for each species are treated as a separate input subgroup
and therefore must end with an input group terminator.

INPUT GROUPS: 16a, 16b, 16c -- Volume source parameters

Subgroup (16a)

Number of volume sources with parameters provided in 16b,c (NVL1) No default ! NVL1 = 4 !
Units used for volume source emissions below in 16b (IVLU) Default: 1 ! IVLU = 5 !
1 = g/s
2 = kg/hr
3 = lb/hr
4 = tons/yr
5 = Odour Unit * m**3/s (vol. flux of odour compound)
6 = Odour Unit * m**3/min
7 = metric tons/yr
Number of source-species combinations with variable emissions scaling factors

23

provided below in (16c) (NSVL1) Default: 0 ! NSVL1 = 0 !

Number of volume sources with variable location and emission parameters (NVL2) No default ! NVL2 = 0 !

(if NVL2 > 0, ALL parameter data for these sources are read from the VOLEMARB.DAT file(s))

!END!

Subgroup (16b)

VOLUME SOURCE: CONSTANT DATA

X Coordinate (km)	Y Coordinate (km)	Effect. Height (m)	Base Elevation (m)	Initial Sigma y (m)	Initial Sigma z (m)	Emission Rates
1! SRCNAM = GOBLD1 ! ! X = 341.214, 6290.711,		5.0,	115.0,	12.5,	2.5,3.213E03 !	!E
2! SRCNAM = GOBLD2 ! ! X = 341.174, 6290.644,		5.0,	115.0,	12.5,	2.5,3.213E03 !	!E
3! SRCNAM = AWTBL1 ! ! X = 341.337, 6290.69,		5.0,	115.0,	12.5,	2.5,1.152E03 !	!E
4! SRCNAM = AWTBL2 ! ! X = 341.33, 6290.639,		5.0,	115.0,	12.5,	2.5,1.152E03 !	!E

a
Data for each source are treated as a separate input subgroup
and therefore must end with an input group terminator.

b
An emission rate must be entered for every pollutant modeled. Enter emission rate of zero for secondary pollutants that are modeled, but not emitted. Units are specified by IVLU (e.g. 1 for g/s).

Subgroup (16c)

VOLUME SOURCE: VARIABLE EMISSIONS DATA

Use this subgroup to describe temporal variations in the emission rates given in 16b. Factors entered multiply the rates in 16b. Skip sources here that have constant emissions. For more elaborate variation in source parameters, use VOLEMARB.DAT and NVL2 > 0.

IVARY determines the type of variation, and is source-specific:
(IVARY) Default: 0
0 = Constant
1 = Diurnal cycle (24 scaling factors: hours 1-24)
2 = Monthly cycle (12 scaling factors: months 1-12)
3 = Hour & Season (4 groups of 24 hourly scaling factors, where first group is DEC-JAN-FEB)
4 = Speed & Stab. (6 groups of 6 scaling factors, where first group is Stability Class A, and the speed classes have upper bounds (m/s) defined in Group 12
5 = Temperature (12 scaling factors, where temperature classes have upper bounds (C) of: 0, 5, 10, 15, 20, 25, 30, 35, 40, 45, 50, 50+)

24

a
Data for each species are treated as a separate input subgroup
and therefore must end with an input group terminator.

INPUT GROUPS: 17a & 17b -- Non-gridded (discrete) receptor information

Subgroup (17a)

```
Number of non-gridded receptors (NREC) No default ! NREC = 3 !
```

! END !

Subgroup (17b)

NON-GRIDDED (DISCRETE) RECEPTOR DATA ^a

Receptor No.	X Coordinate (km)	Y Coordinate (km)	Ground Elevation (m)	Height Above Ground (m)	b
1 ! X =	342.046,	6291.203,	120.000,	2.000!	!END!
2 ! X =	342.18,	6290.668,	125.000,	2.000!	!END!
3 ! X =	342.112,	6290.283,	90.000,	2.000!	!END!

INPUT FILES

Default Name	Unit No.	File Name and Path
CALPUFF.INP	1	C:\CALPUFF\WOYWOY\WWCP5.INP
CALMET.DAT	7	C:\CALPUFF\WOYWOY\WWCMJJ.DAT
(----	7	C:\CALPUFF\WOYWOY\WWCMJD.DAT

OUTPUT FILES

Default Name	Unit No.	File Name and Path
CALPUFF.LST	2	C:\CALPUFF\WOYWOY\WWCP5.LST
CONC.DAT	8	C:\CALPUFF\WOYWOY\WWCP5.DAT

CALMET Control file information:

CALMET.DAT	2.1	No-Obs file structure with embedded control file
------------	-----	--

Produced by CALMET Version: 6.212 Level: 060519
Internal Coordinate Transformations --- COORDLIB Version: 1.96 Level: 0510
CALMET.INP 2.1 Hour Start and End Times with Seconds
woy woy calmet JJ

```
-- Data begin at:
```

IBYR	=	2004
IBMO	=	1
IBDY	=	1
IBHR	=	0
IBSEC	=	0

```
-- Data end at:
IEYR      = 2004
IEMO      = 7
IEDY      = 1
IEHR      = 0
IESEC     = 0
```

```

XBXTM      = -10.0000000
IRLG       = 4368
IRTYPE     = 1
LCALGRD    = 1
PMAP       = 1
DATUM      = WGS-84
NIMADATE   = 02-21-2003
FEASTIM    = 0.000000000E+00
FNCRTHM    = 0.000000000E+00
IUTZM      = 36
UTMHEM     = S
NXM         = 49
NYM         = 49
NZM        = 9
XGRIDIM    = 150.000000
XORIGIM     = 337717.000
YORIGIM     = 6287453.00
IUTZCOD     = 1
NSTSTA     = 1
NUSTA      = 1
NPSTA      = 0
NOWSTA     = 0
NLU        = 14
IWAT1      = 55
IWAT2      = 55

```

Met Station Locations (Met Grid meters)

Met	Station	Locations
XSSTA	=	2108.98877
YSSTA	=	5097.78125
XUSTA	=	2108.98877
YUSTA	=	5097.78125

Surface roughness lengths (m) 20

Multiply all values by 10 ** -3

[illegible][illegible]

Surface roughness lengths (m) 20

[illegible]

WWCP5.LST														10/06/2007											
37	I	1250	1300	1150	860	100	400	1200	1100	900	640	100	10												
36	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
35	I	1060	1000	900	600	180	40	750	900	700	600	600	460	10											
34	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
33	I	1400	1300	1100	860	400	100	40	10	10	10	0	0												
32	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
31	I	1470	1450	1240	800	300	60	100	110	110	100	80	40	1											
30	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
29	I	1350	1560	1200	840	340	30	100	630	400	450	300	80	2											
28	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
27	I	1180	1480	1100	700	650	100	300	700	950	940	500	100	2											
26	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
25	I	1030	1250	1160	900	350	350	700	1100	1350	950	400	20	1											
24	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
23	I	950	900	860	500	200	600	1000	1280	1000	700	250	10	1											
22	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
21	I	1000	880	700	600	720	960	900	1210	1000	340	50	20	2											
20	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
19	I	1250	1000	950	740	820	1200	1100	1400	1200	700	130	60	6											
18	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
17	I	1300	1150	1300	850	900	1500	1500	1600	1200	600	100	200	12											
16	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
15	I	1500	1600	1600	970	1000	1400	1700	1680	1400	1100	600	700	40											
14	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
13	I	1630	1460	1630	1100	1040	1600	1710	1700	1400	1120	1000	1030	105											
12	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
11	I	1570	1350	1400	1250	1300	1540	1540	1640	1530	1300	1270	1200	120											
10	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
9	I	1500	1160	1070	1080	1300	1260	1400	1610	1400	1300	1170	600	55											
8	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
7	I	1200	920	1240	1240	1190	1220	1430	1590	1200	900	700	160	1											
6	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
5	I	660	900	1230	1450	1400	1360	1530	1650	1100	750	70	30	3											
4	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
3	I	850	1050	1140	1560	1640	1480	1520	1600	1170	750	200	100	7											
2	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
1	I	900	1100	1550	1830	1880	1800	1700	1700	1200	1000	900	200	7											
0	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
0	I	950	1200	1530	1660	1700	1850	1700	1700	1330	1330	1000	650	23											
0	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
0	I	1060	1120	1260	1480	1640	1550	1460	1500	1100	1050	1200	1100	43											
0	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
0	I	1190	1160	1240	1460	1560	1150	1100	1240	1160	710	970	800	43											
0	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
0	I	1280	1230	1350	1550	1100	900	900	980	900	700	420	350	5											
0	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
0	I	1430	1400	1630	1400	910	640	600	880	800	250	100	20	1											
0	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
0	I	1540	1430	1650	1660	1200	900	500	200	650	300	60	10	1											
0	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
0	I	1500	1170	1350	1500	1200	1000	850	270	200	140	50	10	1											
0	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
0	I	1570	1240	1130	1100	1100	900	500	300	10	90	80	60	4											
0	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
0	I	1530	1360	1100	1050	1080	1000	770	650	20	60	80	90	6											
0	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
0	I	1640	1500	1100	1040	970	950	900	900	700	200	70	70	6											
0	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
0	I	1760	1540	1240	1050	1050	1160	1250	1100	450	70	70	50	10											
0	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
0	I	1750	1630	1400	1260	1130	1350	1000	700	350	200	130	250	60											
0	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
0	I	1780	1720	1610	1500	1270	1140	970	930	800	830	560	750	63											
0	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
0	I	1790	1800	1630	1490	1240	1220	1190	1160	1170	1070	870	930	76											
0	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
0	I	1680	1660	1600	1580	1500	1400	1370	1370	1340	1240	960	600	12											
0	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
0	I	1400	1300	1300	1300	1400	1460	1250	1100	1100	1100	1020	900	30											
0	I	+	+	+	+	+	+	+	+	+	+	+	+	+											
0	I	1450	1170	1050	1000	1080	1300	1250	770	720	770	760	850	50											

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														I	+	+	+	+	+	+	+	+	+	+	+	+	+	+
														21	22	23	24	25	26	27	28	29	30	31	32	3		
Terrain heights (m)														ELEV														
Multiply all values by 10 ** -1																												
49	I	640	930	600	20	0	0	0	0	0	0	0	0															
48	I	650	200	10	0	10	0	30	0	0	0	0	0															
47	I	580	50	0	0	10	0	20	10	0	0	0	0															
46	I	0	60	0	0	10	10	0	10	20	0	0	0															
45	I	0	0	0	0	20	10	0	0	20	0	0	0															
44	I	0	0	0	0	10	0	10	0	0	0	0	0															
43	I	0	0	0	0	20	20	20	10	0	0	0	0															
42	I	20	0	0	0	20	10	10	10	20	0	0	0															
41	I	0	0	10	30	20	10	10	10	10	10	10	10															
40	I	0	20	30	30	20	20	10	10	10	10	10	10															
39	I	20	30	30	30	20	20	10	10	10	10	10	10															
38	I	20	10	20	30	20	20	10	10	20	0	0	0															
37	I	20	20	30	30	20	20	10	10	20	0	0	0															
36	I	20	30	30	30	20	20	10	10	20	0	0	0															
35	I	20	30	30	30	20	20	10	10	10	10	10	10															
34	I	30	30	30	20	20	10	10	10	0	0	0	0															
33	I	30	30	30	20	20	10	10	20	0	0	0	0															
32	I	40	40	30	30	20	20	30	20	0	0	0	0															
31	I	50	50	40	30	20	30	30	30	30	0	0	0															
30	I	50	50	40	30	30	30	40	40	30	0	0	0															
29	I	60	60	50	40	30	40	50	40	60	0	0	0															
28	I	60	60	60	50	50	40	20	40	0	0	0	0															
27	I	60	60	60	60	50	40	10	20	0	0	0	0															
26	I	50	60	60	60	50	40	30	10	10	0	0	0															
25	I	40	50	60	60	50	40	30	10	10	0	0	0															
24	I	40	50	60	60	50	50	30	20	10	0	0	0															
23	I	30	50	60	60	60	50	40	30	30	0	0	0															
22	I	30	50	50	60	60	60	50	50	40	0	0	0															
21	I	30	40	50	60	60	60	50	40	0	0	0	0															
20	I	30	40	50	60	60	60	50	40	0	0	0	0															
19	I	30	40	50	60	60	60	50	30	0	0	0	0															
18	I	30	40	50	60	60	60	50	40	20	0	0	0															
17	I	30	40	40	50	50	50	40	30	20	0	0	0															

[illegible]

WCP5.LST													10/06/2007		
12	I	7000	7000	7000	7000	7000	7000	7000	7000	7000	7000	200	200	20	
11	I	+	+	+	+	+	+	+	+	+	+	+	+	20	
10	I	7000	7000	7000	7000	7000	7000	7000	7000	7000	7000	200	200	20	
9	I	7000	7000	7000	7000	7000	7000	7000	7000	7000	7000	200	200	20	
8	I	+	+	+	+	+	+	+	+	+	+	+	+	20	
7	I	7000	7000	7000	7000	7000	7000	7000	7000	7000	7000	200	200	20	
6	I	+	+	+	+	+	+	+	+	+	+	+	+	20	
5	I	7000	7000	7000	7000	7000	7000	7000	7000	7000	7000	7000	7000	700	
4	I	+	+	+	+	+	+	+	+	+	+	+	+	700	
3	I	7000	7000	7000	7000	7000	7000	7000	7000	7000	7000	7000	7000	700	
2	I	+	+	+	+	+	+	+	+	+	+	+	+	700	
1	I	7000	7000	7000	7000	7000	7000	7000	7000	7000	7000	7000	7000	700	
	I	+	+	+	+	+	+	+	+	+	+	+	+		
		21	22	23	24	25	26	27	28	29	30	31	32	3	
Leaf area index													XLAI		
Multiply all values by 10 ** -3															
49	I	7000	7000	7000	7000	0	0	0	0	0					
48	I	+	+	+	+	0	200	0	200	0	0				
47	I	7000	7000	0	0	200	0	200	200	0					
46	I	+	+	+	+	200	+	+	+	+					
45	I	7000	0	0	200	200	0	200	200	0					
44	I	+	+	+	+	+	+	+	+	+					
43	I	0	0	0	0	200	200	200	200	0					
42	I	+	+	+	+	+	+	+	+	+					
41	I	7000	0	0	0	200	200	200	200	200					
40	I	+	+	+	+	+	+	+	+	+					
39	I	0	200	200	200	200	200	200	200	200					
38	I	+	+	+	+	+	+	+	+	+					
37	I	200	200	200	200	200	200	200	200	200					
36	I	+	+	+	+	+	+	+	+	+					
35	I	200	200	200	200	200	200	200	200	200					
34	I	+	+	+	+	+	+	+	+	+					
33	I	200	200	200	200	200	200	200	200	200					
32	I	+	+	+	+	+	+	+	+	+					
31	I	200	200	200	200	200	200	200	200	200					
30	I	+	+	+	+	+	+	+	+	+					
29	I	200	200	200	200	200	200	200	200	200					
	I	+	+	+	+	+	+	+	+	+					

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[illegible][illegible]

[illegible]

14	I	+	+	+	+	+	+	+	+	+	+	+
13	I	+	+	+	+	+	+	+	+	+	+	+
12	I	+	+	+	+	+	+	+	+	+	+	+
11	I	+	+	+	+	+	+	+	+	+	+	+
10	I	+	+	+	+	+	+	+	+	+	+	+
9	I	+	+	+	+	+	+	+	+	+	+	+
8	I	+	+	+	+	+	+	+	+	+	+	+
7	I	+	+	+	+	+	+	+	+	+	+	+
6	I	+	+	+	+	+	+	+	+	+	+	+
5	I	+	+	+	+	+	+	+	+	+	+	+
4	I	+	+	+	+	+	+	+	+	+	+	+
3	I	+	+	+	+	+	+	+	+	+	+	+
2	I	+	+	+	+	+	+	+	+	+	+	+
1	I	+	+	+	+	+	+	+	+	+	+	+
		21	22	23	24	25	26	27	28	29	30	31

```

WCPC5.LST
10/06/2007

 3 I 1000 1000 1000 1000 1000 1000 1000 1000 1000
  I   +      +      +      +      +      +      +      +
 2 I 1000 + 1000 + 1000 + 1000 + 1000 + 1000 + 1000 +
  I   +      +      +      +      +      +      +      +
 1 I 1000 1000 1000 1000 1000 1000 1000 1000 1000
  I   +      +      +      +      +      +      +      +
      -----
      41      42      43      44      45      46      47      48      49

LAST PERIOD PROCESSED ENDS AT:
Year: 2004 Month: 12 Day: 31 Julian day: 366 Hour: 23 Second: 0

End of run -- Clock time: 18:58:44
Date: 06-10-2007

Elapsed Clock Time: 10070.0 (seconds)

CPU Time: 10070.0 (seconds)

```


Appendix B

Dispersion Modelling Files

CALPOST List File

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***** CALPOST Version 6.132 Level *****

Internal Coordinate Transformations by --- COORDLIB Version: 1.96 Level: 05

Run Title:

INPUT GROUP: 1 -- General run control parameters

Option to run all periods found in the met. file(s) (METRUN) Default: 0 ! METRUN = 1 !

METRUN = 0 - Run period explicitly defined below
METRUN = 1 - Run all periods in CALPUFF data file(s)

Starting date: Year (ISYR) -- No default ! ISYR = 2004 !
Month (ISMO) -- No default ! ISMO = 0 !
Day (ISDY) -- No default ! ISDY = 0 !
Starting time: Hour (ISHR) -- No default ! ISHR = 0 !
Minute (ISMIN) -- No default ! ISMIN = 0 !
Second (ISSEC) -- No default ! ISSEC = 0 !

Ending date: Year (IEYR) -- No default ! IEYR = 0 !
Month (IEMO) -- No default ! IEMO = 0 !
Day (IEDY) -- No default ! IEDY = 0 !
Ending time: Hour (IEHR) -- No default ! IEHR = 0 !
Minute (IEMIN) -- No default ! IEMIN = 0 !
Second (IESEC) -- No default ! IESec = 0 !

(These are only used if METRUN = 0)

All times are in the base time zone of the CALPUFF simulation. CALPUFF Dataset Version 2.1 contains the zone, but earlier versions do not, and the zone must be specified here. The zone is the number of hours that must be ADDED to the time to obtain UTC (or GMT). Identify the Base Time Zone for the CALPUFF simulation (BTZONE) -- No default ! BTZONE = -10.0 !

Process every period of data? (NREP) -- Default: 1 ! NREP = 1 !
(1 = every period processed,
2 = every 2nd period processed,
5 = every 5th period processed, etc.)

Species & Concentration/Deposition Information

Species to process (ASPEC) -- No default ! ASPEC = ODOR !
(ASPEC = VISIB for visibility processing)

Layer/deposition code (ILAYER) -- Default: 1 ! ILAYER = 1 !
'1' for CALPUFF concentrations,
'-1' for dry deposition fluxes,
'-2' for wet deposition fluxes,
'-3' for wet-dry deposition fluxes.

Scaling factors of the form: -- Defaults: ! A = 2.5 !
X(new) = X(old) * A + B A = 0.0 ! B = 0.0 !
(NOT applied if A = B = 0.0) B = 0.0

Add Hourly Background Concentrations/Fluxes?

1

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(LBACK) -- Default: F ! LBACK = F !

Source information

Option to process source contributions:
0 = Process only total reported contributions
1 = Sum all individual source contributions and process
2 = Run in TRACEBACK mode to identify source contributions at a SINGLE receptor (MSOURCE) -- Default: 0 ! MSOURCE = 0 !

Receptor information

Gridded receptors processed? (LG) -- Default: F ! LG = T !
Discrete receptors processed? (LD) -- Default: F ! LD = T !
CTSG Complex terrain receptors processed? (LCT) -- Default: F ! LCT = F !

--Report results by DISCRETE receptor RING? (only used when LD = T) (LDRING) -- Default: F ! LDRING = F !

--Select range of DISCRETE receptors (only used when LD = T):

Select ALL DISCRETE receptors by setting NDRECP flag to -1;
OR
Select SPECIFIC DISCRETE receptors by entering a flag (0,1) for each
0 = discrete receptor not processed
1 = discrete receptor processed
using repeated value notation to select blocks of receptors:
23*1, 15*0, 12*1
Flag for all receptors after the last one assigned is set to 0 (NDRECP) -- Default: -1 ! NDRECP = -1 !

--Select range of GRIDDED receptors (only used when LG = T):

X index of LL corner (IBGRID) -- Default: -1 ! IBGRID = -1 !
(-1 OR 1 <= IBGRID <= NX)

Y index of LL corner (JBGRID) -- Default: -1 ! JBGRID = -1 !
(-1 OR 1 <= JBGRID <= NY)

X index of UR corner (IEGRID) -- Default: -1 ! IEGRID = -1 !
(-1 OR 1 <= IEGRID <= NX)

Y index of UR corner (JEGRID) -- Default: -1 ! JEGRID = -1 !
(-1 OR 1 <= JEGRID <= NY)

Note: Entire grid is processed if IBGRID=JBGRID=IEGRID=JEGRID=-1

--Specific gridded receptors can also be excluded from CALPOST processing by filling a processing grid array with 0s and 1s. If the processing flag for receptor index (i,j) is 1 (ON), that receptor will be processed if it lies within the range delineated by IBGRID, JBGRID, IEGRID, and JEGRID. If it is 0 (OFF), it will not be processed in the run. By default, all array values are set to 1 (ON).

Number of gridded receptor rows provided in Subgroup (1a) to identify specific gridded receptors to process (NGONOFF) -- Default: 0 ! NGONOFF = 0 !

!END!

Subgroup (1a) -- Specific gridded receptors included/excluded

Specific gridded receptors are excluded from CALPOST processing

2

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by filling a processing grid array with 0s and 1s. A total of NGONOFF lines are read here. Each line corresponds to one 'row' in the sampling grid, starting with the NORTHERNMOST row that contains receptors that you wish to exclude, and finishing with row 1 to the SOUTH (no intervening rows may be skipped). Within a row, each receptor position is assigned either a 0 or 1, starting with the westernmost receptor.
0 = gridded receptor not processed
1 = gridded receptor processed

Repeated value notation may be used to select blocks of receptors:
23*1, 15*0, 12*1

Because all values are initially set to 1, any receptors north of the first row entered, or east of the last value provided in a row, remain ON.

(NGXRECP) -- Default: 1

INPUT GROUP: 2 -- Visibility Parameters (ASPEC = VISIB)

Particle growth curve f(RH) for hygroscopic species (MFRH) -- Default: 2 ! MFRH = 2 !

1 = IWAQM (1998) f(RH) curve (originally used with MVISBK=1)
2 = FLAG (2000) f(RH) tabulation
3 = EPA (2003) f(RH) tabulation

Maximum relative humidity (%) used in particle growth curve (RHMAX) -- Default: 98 ! RHMAX = 98.0 !

Modeled species to be included in computing the light extinction

Include SULFATE? (LVS04) -- Default: T ! LVS04 = T !
Include NITRATE? (LVNO3) -- Default: T ! LVNO3 = T !
Include ORGANIC CARBON? (LVOC) -- Default: T ! LVOC = T !
Include COARSE PARTICLES? (LVPMC) -- Default: T ! LVPMC = T !
Include FINE PARTICLES? (LVPMF) -- Default: T ! LVPMF = T !
Include ELEMENTAL CARBON? (LVEC) -- Default: T ! LVEC = T !

And, when ranking for TOP-N, TOP-50, and Exceedance tables, Include BACKGROUND? (LVBK) -- Default: T ! LVBK = T !

Species name used for particulates in MODEL.DAT file
COARSE (SPECPMC) -- Default: PMC ! SPECPMC = PMC !
FINE (SPECPMF) -- Default: PMF ! SPECPMF = PMF !

Extinction Efficiency (1/Mm per ug/m**3)

MODELED particulate species:
PM COARSE (EPPMC) -- Default: 0.6 ! EPPMC = 0.6 !
PM FINE (EPPMF) -- Default: 1.0 ! EPPMF = 1.0 !

BACKGROUND particulate species:
PM COARSE (EPPMCBK) -- Default: 0.6 ! EPPMCBK = 0.6 !

Other species:
AMMONIUM SULFATE (EES04) -- Default: 3.0 ! EES04 = 3.0 !
AMMONIUM NITRATE (EEN03) -- Default: 3.0 ! EEN03 = 3.0 !
ORGANIC CARBON (EEOC) -- Default: 4.0 ! EEOC = 4.0 !
SOIL (EESOIL) -- Default: 1.0 ! EESOIL = 1.0 !
ELEMENTAL CARBON (EEEC) -- Default: 10. ! EEEC = 10.0 !

Background Extinction Computation

Method used for the 24h-average of percent change of light extinction: Hourly ratio of source light extinction / background light extinction is averaged? (LAVER) -- Default: F ! LAVER = F !

Method used for background light extinction

3

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(MVISBK) -- Default: 2 ! MVISBK = 2 !

1 = Supply single light extinction and hygroscopic fraction - Hourly F(RH) adjustment applied to hygroscopic background and modeled sulfate and nitrate

2 = Compute extinction from speciated PM measurements (A) - Hourly F(RH) adjustment applied to observed and modeled sulfate and nitrate
- F(RH) factor is capped at F(RHMAX)

3 = Compute extinction from speciated PM measurements (B) - Hourly F(RH) adjustment applied to observed and modeled sulfate and nitrate
- Receptor-hour excluded if RH>RHMAX
- Receptor-day excluded if fewer than 6 valid receptor-hours

4 = Read hourly transmission background extinction measurements - Hourly F(RH) adjustment applied to modeled sulfate and nitrate
- Hour excluded if measurement invalid (missing, interference, or large RH)
- Receptor-hour excluded if RH>RHMAX
- Receptor-day excluded if fewer than 6 valid receptor-hours

5 = Read hourly nephelometer background extinction measurements - Rayleigh extinction value (BEXTRAY) added to measurement
- Hourly F(RH) adjustment applied to modeled sulfate and nitrate
- Hour excluded if measurement invalid (missing, interference, or large RH)
- Receptor-hour excluded if RH>RHMAX
- Receptor-day excluded if fewer than 6 valid receptor-hours

6 = Compute extinction from speciated PM measurements - FLAG monthly RH adjustment factor applied to observed and modeled sulfate and nitrate

7 = Use observed weather or prognostic weather information for background extinction during weather events; otherwise, use Method - Hourly F(RH) adjustment applied to modeled sulfate and nitrate
- F(RH) factor is capped at F(RHMAX)
- During observed weather events, compute Bext from visual range if using an observed weather data file, or
- During prognostic weather events, use Bext from the prognostic weather file
- Use Method 2 for hours without a weather event

Additional inputs used for MVISBK = 1:

Background light extinction (1/Mm) (BEXTBK) -- No default ! BEXTBK = 0.0 !
Percentage of particles affected by relative humidity (RHFRAC) -- No default ! RHFRAC = 0.0 !

Additional inputs used for MVISBK = 6:

Extinction coefficients for hygroscopic species (modeled and background) are computed using a monthly RH adjustment factor in place of an hourly RH factor (VISB.DAT file is NOT needed). Enter the 12 monthly factors here (RHFAC). Month 1 is January.

(RHFAC) -- No default ! RHFAC = 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0 !

Additional inputs used for MVISBK = 7:

The weather data file (DATSAV abbreviated space-delimited) that is identified as VSRN.DAT may contain data for more than one station. Identify the stations that are needed in the order in which they will be used to obtain valid weather and visual range. The first station that contains valid data for an hour will be used. Enter up to MXNSTA (set in PARAMS file) integer station IDs up to 6 digits each as variable IDWSTA, and enter the corresponding time zone for each, as variable TZONE (= UTC-LST).

A prognostic weather data file with Bext for weather events may be used in place of the observed weather file. Identify this as the VSRN.DAT file and use a station ID of IDWSTA = 999999, and TZONE = 0.

4

NOTE: TZONE identifies the time zone used in the dataset. The DATSAV abbreviated space-delimited data usually are prepared with UTC time rather than local time, so TZONE is typically set to zero.

(IDWSTA) -- No default
! IDWSTA = 999999 !
(TZONE) -- No default
! TZONE = 0.0 !

Additional inputs used for MVISBK = 2,3,6,7:

Background extinction coefficients are computed from monthly CONCENTRATIONS of ammonium sulfate (BKS04), ammonium nitrate (BKNO3), coarse particulates (BKPMC), organic carbon (BKOC), soil (BKSOIL), and elemental carbon (BKEC). Month 1 is January.
(ug/m**3)

(BKS04) -- No default ! BKS04 = 0.0, 0.0, 0.0, 0.0,
0.0, 0.0, 0.0, 0.0,
0.0, 0.0, 0.0, 0.0 !
(BKNO3) -- No default ! BKNO3 = 0.0, 0.0, 0.0, 0.0,
0.0, 0.0, 0.0, 0.0,
0.0, 0.0, 0.0, 0.0 !
(BKPMC) -- No default ! BKPMC = 0.0, 0.0, 0.0, 0.0,
0.0, 0.0, 0.0, 0.0,
0.0, 0.0, 0.0, 0.0 !
(BKOC) -- No default ! BKOC = 0.0, 0.0, 0.0, 0.0,
0.0, 0.0, 0.0, 0.0,
0.0, 0.0, 0.0, 0.0 !
(BKSOIL) -- No default ! BKSOIL = 0.0, 0.0, 0.0, 0.0,
0.0, 0.0, 0.0, 0.0,
0.0, 0.0, 0.0, 0.0 !
(BKEC) -- No default ! BKEC = 0.0, 0.0, 0.0, 0.0,
0.0, 0.0, 0.0, 0.0,
0.0, 0.0, 0.0, 0.0 !

Additional inputs used for MVISBK = 2,3,5,6,7:

Extinction due to Rayleigh scattering is added (1/Mm)
(BEXTRAY) -- Default: 10.0 ! BEXTRAY = 10.0 !

!END!

INPUT GROUP: 3 -- Output options

Documentation

Documentation records contained in the header of the CALPUFF output file may be written to the list file.
Print documentation image? (LDOC) -- Default: F ! LDOC = F !

Output Units

Units for All Output (IPRTU) -- Default: 1 ! IPRTU = 5 !
for
Concentration Deposition
1 = g/m**3 g/m**2/s
2 = mg/m**3 mg/m**2/s
3 = ug/m**3 ug/m**2/s
4 = ng/m**3 ng/m**2/s
5 = Odour Units

Visibility: extinction expressed in 1/Mega-meters (IPRTU is ignored)

Averaging time(s) reported

5

1-pd averages (L1PD) -- Default: T ! L1PD = T !
(pd = averaging period of model output)

1-hr averages (L1HR) -- Default: T ! L1HR = T !

3-hr averages (L3HR) -- Default: T ! L3HR = F !

24-hr averages (L24HR) -- Default: T ! L24HR = F !

Run-length averages (LRUNL) -- Default: T ! LRUNL = F !

User-specified averaging time in hours, minutes, seconds
- results for this averaging time are reported if it is not zero

(NAVGH) -- Default: 0 ! NAVGH = 0 !
(NAVGM) -- Default: 0 ! NAVGM = 0 !
(NAVGS) -- Default: 0 ! NAVGS = 0 !

Types of tabulations reported

1) Visibility: daily visibility tabulations are always reported for the selected receptors when ASPEC = VISIB.
In addition, any of the other tabulations listed below may be chosen to characterize the light extinction coefficients.
[List file or Plot/Analysis File]

2) Top 50 table for each averaging time selected
[List file only]
(LT50) -- Default: T ! LT50 = T !

3) Top 'N' table for each averaging time selected
[List file or Plot file]
(LTOPN) -- Default: F ! LTOPN = T !
-- Number of 'Top-N' values at each receptor selected (NTOP must be <= 4)
(NTOP) -- Default: 4 ! NTOP = 1 !
-- Specific ranks of 'Top-N' values reported (NTOP values must be entered)
(ITOP(4) array) -- Default: ! ITOP = 88 !
1,2,3,4

4) Threshold exceedance counts for each receptor and each averaging time selected
[List file or Plot file]
(LEXCD) -- Default: F ! LEXCD = F !
-- Identify the threshold for each averaging time by assigning a non-negative value (output units).
-- Default: -1.0
Threshold for 1-hr averages (THRESH1) ! THRESH1 = -1.0 !
Threshold for 3-hr averages (THRESH3) ! THRESH3 = -1.0 !
Threshold for 24-hr averages (THRESH24) ! THRESH24 = -1.0 !
Threshold for NAVG-hr averages (THRESHN) ! THRESHN = -1.0 !

-- Counts for the shortest averaging period selected can be tallied daily, and receptors that experience more than NCOUNT counts over any NDAY period will be reported. This type of exceedance violation output is triggered only if NDAY > 0.

Accumulation period(Days)
(NDAY) -- Default: 0 ! NDAY = 0 !
Number of exceedances allowed
(NCOUNT) -- Default: 1 ! NCOUNT = 1 !

6

5) Selected day table(s)

Echo Option -- Many records are written each averaging period selected and output is grouped by day
[List file or Plot file]
(LECHO) -- Default: F ! LECHO = F !

Timeseries Option -- Averages at all selected receptors for each selected averaging period are written to timeseries files. Each file contains one averaging period, and all receptors are written to a single record each averaging time.
[TSERIES_ASPEC_tTHR_CONC_TSUNAM.DAT files]
(LTIME) -- Default: F ! LTIME = F !

Peak Value Option -- Averages at all selected receptors for each selected averaging period are screened and the peak value each period is written to timeseries files.
Each file contains one averaging period.
[PEAKVAL_ASPEC_tTHR_CONC_TSUNAM.DAT files]
(LPEAK) -- Default: F ! LPEAK = F !

-- Days selected for output
(IECHO(366)) -- Default: 366*0
! IECHO = 366*0 !
(366 values must be entered)

Plot output options

Plot files can be created for the Top-N, Exceedance, and Echo tables selected above. Two formats for these files are available, DATA and GRID. In the DATA format, results at all receptors are listed along with the receptor location [x,y,vall,val2,...]. In the GRID format, results at only gridded receptors are written, using a compact representation. The gridded values are written in rows (x varies), starting with the most southern row of the grid. The GRID format is given the .GRD extension, and includes headers compatible with the SURFER(R) plotting software.

A plotting and analysis file can also be created for the daily peak visibility summary output, in DATA format only.

Generate Plot file output in addition to writing tables to list file?
(LPLT) -- Default: F ! LPLT = T !

Use GRID format rather than DATA format, when available?
(LGRD) -- Default: F ! LGRD = T !

Auxiliary Output Files (for subsequent analyses)

Visibility

A separate output file may be requested that contains the change in visibility at each selected receptor when ASPEC = VISIB. This file can be processed to construct visibility measures that are not available in CALPOST.

Output file with the visibility change at each receptor?
(MDVIS) -- Default: 0 ! MDVIS = 0 !

0 = Do Not create file
1 = Create file of DAILY (24 hour) Delta-Deciview
2 = Create file of DAILY (24 hour) Extinction Change (%)
3 = Create file of HOURLY Delta-Deciview
4 = Create file of HOURLY Extinction Change (%)

Additional Debug Output

7

Output selected information to List file for debugging?
(LDEBUG) -- Default: F ! LDEBUG = F !

Output hourly extinction information to REPORT.HRV?
(Visibility Method 7)
(LVEXTHR) -- Default: F ! LVEXTHR = F !

!END!

NOTICE: Starting year in control file sets the expected century for the simulation. All YY years are converted to YYYY years in the range: 1954 2053

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CALPOST Control File Input Summary -----

Replace run data with data in Puff file 1-Y: 1
Run starting date -- year: 2004
month: 0
day: 0
Time at start of run - Julian day: 0
- hour(0-23): 0
- minute: 0
- second: 0
Run ending date -- year: 0
month: 0
day: 0
Time at end of run - Julian day: 0
- hour(0-23): 0
- minute: 0
- second: 0
Base time zone (Group 1): -10.0
Every period of data processed -- NREP = 1

Species & Concentration/Deposition Information

Species: ODOR
Layer of processed data: 1
(>0=conc, -1=dry flux, -2=wet flux, -3=wet & dry flux)
Multiplicative scaling factor: 2.5000E+00
Additive scaling factor: 0.0000E+00
Hourly background values used?: F

SAMPLER option

Processing method: 0
0 = SAMPLER option not used
1 = Report total modeled impact (list file)
2 = TRACEBACK mode (DAT files)
3 = TRACEBACK mode with sampling factor (DAT files)

Source information

Source contribution processing: 0
0 = No source contributions
1 = Contributions are summed

8

***** NOTICE *****
Gridded receptor range reset to NGX by NGY

OUTPUT FILES		
Default Name	Unit No.	File Name and Path
CALPOST.LST	8	C:\CALPUFF\WOYWOY\WWCPST5.LST
(TOPN)	11	RANK()_SPECIES_tTHR_CONC_RUN1.GRD*****

 CALPOST Version 6.132 Level

	ODOR	1
DATE OF TEST	08-07-2019	
TESTER'S NAME	MARCO ANTONIO DE OLIVEIRA	
LABORATORY	INSTITUTO AGROPECUARIO DO PARANÁ	
ADDRESS	RUA CARLOS KOPPEL, 160 - JARDIM BOA VISTA - FLORESTAL - PR - CEP: 81250-970	
PHONE	(41) 3333-3333	
E-MAIL	marcoantonio@institutoagropecuario.org.br	
SIGNATURE	[Signature]	
STAMP	[Stamp]	

[illegible]

2004	54	0000	(13, 11)	G	8.3145E+01	341.092	6290.5
2004	308	2200	(14, 11)	G	7.6380E+01	341.242	6290.5
2004	174	1800	(14, 12)	G	6.2907E+01	341.092	6290.5
2004	184	1900	(13, 11)	G	6.3326E+01	341.092	6290.5
2004	359	0200	(14, 11)	G	6.2557E+01	341.242	6290.5
2004	79	0300	(14, 11)	G	6.0127E+01	341.242	6290.5
2004	174	1700	(14, 11)	G	5.9191E+01	341.242	6290.5
2004	105	0000	(14, 11)	G	5.5598E+01	341.242	6290.5
2004	264	2100	(14, 15)	G	5.2407E+01	341.242	6291.1
2004	184	2000	(14, 11)	G	5.1575E+01	341.242	6290.5
2004	264	2100	(14, 11)	G	5.1365E+01	341.242	6290.5
2004	121	1100	(14, 13)	G	5.1292E+01	341.242	6290.5
2004	220	1700	(14, 12)	G	5.0481E+01	341.392	6290.6
2004	64	0100	(14, 11)	G	4.9045E+01	341.242	6290.5
2004	33	0200	(13, 11)	G	4.8663E+01	341.092	6290.5
2004	130	0200	(13, 13)	G	4.7470E+01	341.092	6290.8
2004	79	1900	(14, 11)	G	4.6799E+01	341.092	6290.5
2004	232	1700	(14, 13)	G	4.6665E+01	341.242	6290.8
2004	249	1800	(14, 11)	G	4.6576E+01	341.242	6290.5
2004	352	0300	(14, 15)	G	4.6378E+01	341.242	6291.1
2004	335	0100	(15, 11)	G	4.5184E+01	341.392	6290.6
2004	28	0200	(14, 11)	G	4.5218E+01	341.242	6290.5
2004	102	1900	(15, 12)	G	4.4835E+01	341.392	6290.6
2004	297	2200	(13, 11)	G	4.4753E+01	341.092	6290.5
2004	118	0200	(15, 12)	G	4.4672E+01	341.392	6290.6
2004	102	1100	(13, 13)	G	4.4292E+01	341.242	6290.5
2004	120	0500	(13, 13)	G	4.3184E+01	341.092	6290.8
2004	297	2300	(15, 12)	G	4.2667E+01	341.392	6290.6
2004	63	2300	(13, 11)	G	4.2244E+01	341.092	6290.5
2004	120	0300	(13, 16)	G	4.1873E+01	341.092	6291.2
2004	248	1800	(14, 11)	G	4.1722E+01	341.242	6290.5
2004	264	2000	(14, 13)	G	4.1638E+01	341.242	6290.8
2004	109	2300	(15, 12)	G	4.0553E+01	341.392	6290.6
2004	232	1800	(14, 11)	G	4.0322E+01	341.242	6290.5
2004	241	2000	(13, 12)	G	3.9236E+01	341.092	6290.8
2004	327	0300	(15, 12)	G	3.9202E+01	341.392	6290.6
2004	157	1900	(13, 11)	G	3.8715E+01	341.092	6290.5

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2004	138	1900	(14, 13)	G	3.5163E+01	341.242	6290.8
------	-----	------	-----------	---	------------	---------	--------

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	ODOR	1
--	------	---

1 RANKED 1 HOUR AVERAGE CONCENTRATION VALUES AT EACH GRIDDED RECEPTOR (YE

RECEPTOR	COORDINATES (km)	88 RANK
----------	------------------	---------

1,	2	339.292	6289.178	2.6140E-01	(2004,094,1800)
----	---	---------	----------	------------	-----------------

1.	4	339.292	6289.478	2.7171E-01	(2004.016.0400)
----	---	---------	----------	------------	-----------------

1	5	339.292	6289.628	2.7391E-01	(2004, 043, 2300)
1	6	339.292	6289.778	2.8662E-01	(2004, 358, 2100)

1,	7	339.292	6289.928	2.7686E-01	(2004,130,0000)
----	---	---------	----------	------------	-----------------

```
1, 9      339.292  6290.228   3.1748E-01 (2004,338,0500)
```

1, 10	339.292	6290.528	2.0902E-01	(2001, 250, 2100)
1, 11	339.292	6290.528	3.0719E-01	(2004, 315, 1800)

1, 12	339.292	6290.678	2.9263E-01	(2004, 262, 1700)
1, 13	330.303	6200.838	3.5356E-01	(2004, 033, 1800)

1, 14	339.292	6290.978	4.0691E-01	(2004, 050, 2100)
-------	---------	----------	------------	-------------------

1, 16	339.292	6291.278	3.3591E-01	(2004,073,2000)
-------	---------	----------	------------	-----------------

1. 18	339.292	6291.578	2.8170E-01	(2004.014.2000)
-------	---------	----------	------------	-----------------

1, 19	339.292	6291.728	2.4857E-01	(2004, 350, 1900)
1, 20	339.292	6291.878	1.9447E-01	(2004, 263, 2200)

1,	21	339.292	6292.028	1.7381E-01	(2004,045,0000)
1,	22	339.292	6292.028	1.7381E-01	(2004,045,0000)

1, 23	339.292	6292.328	1.5853E-01	(2004,078,1300)
-------	---------	----------	------------	-----------------

1. 25	339.292	6292.628	1.1360E-01	(2004.081.0600)
-------	---------	----------	------------	-----------------

1, 26	339.292	6292.778	1.2368E-01	(2004, 283, 1700)
1, 27	339.292	6292.928	1.1557E-01	(2004, 267, 1700)

1,	28	339.292	6293.078	1.0704E-01	(2004,082,1900)
1,	28	339.292	6293.078	0.1633E+00	(2004,017,0000)

2, 1 339.442 6289.028 5.7533E-02 (2004,028,1900)

2.	3	339.442	6289.328	2.9002E-01	(2004.320,2200)
----	---	---------	----------	------------	-----------------

2,	4	339.442	6289.478	1.7774E-01	(2004, 049, 2100)
2,	5	339.442	6289.628	1.5247E-01	(2004, 353, 0500)

2,	6	339.442	6289.778	3.3027E-01	(2004,100,1600)
----	---	---------	----------	------------	-----------------

2, 8 339.442 6290.078 3.7243E-01 (2004,335,0000)

2.	10	339.442	6290.378	3.5694E-01	(2004.129,2300)
----	----	---------	----------	------------	-----------------

2, 11	339.442	6290.528	3.6364E-01	(2004, 297, 1700)
2, 12	339.442	6290.678	3.5585E-01	(2004, 291, 0400)

2, 13	339.442	6290.828	3.7713E-01	(2004, 048, 0600)
-------	---------	----------	------------	-------------------

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```
29, 9 343.492 6290.228 8.3918E-02 (2004,128,0100)
29, 10 343.492 6290.378 8.5863E-02 (2004,238,0400)
29, 11 343.492 6290.528 8.1059E-02 (2004,198,0600)
29, 12 343.492 6290.678 8.1580E-02 (2004,225,0300)
29, 13 343.492 6290.828 8.0275E-02 (2004,199,0000)
29, 14 343.492 6290.978 8.1560E-02 (2004,092,1900)
29, 15 343.492 6291.128 8.3937E-02 (2004,151,2300)
29, 16 343.492 6291.278 8.4045E-02 (2004,194,1900)
29, 17 343.492 6291.428 7.9098E-02 (2004,030,2200)
29, 18 343.492 6291.578 7.4660E-02 (2004,263,0600)
29, 19 343.492 6291.728 7.0343E-02 (2004,135,2200)
29, 20 343.492 6291.878 6.6621E-02 (2004,203,0600)
29, 21 343.492 6292.028 6.1588E-02 (2004,241,0500)
29, 22 343.492 6292.178 5.5920E-02 (2004,135,2000)
29, 23 343.492 6292.328 5.4635E-02 (2004,288,2100)
29, 24 343.492 6292.478 4.8211E-02 (2004,093,0400)
29, 25 343.492 6292.628 4.3844E-02 (2004,268,0300)
29, 26 343.492 6292.778 4.5085E-02 (2004,163,2100)
29, 27 343.492 6292.928 3.8594E-02 (2004,054,0200)
29, 28 343.492 6293.078 3.4822E-02 (2004,208,1800)
29, 29 343.492 6293.228 3.0030E-02 (2004,151,1500)
```

88 - RANK HIGHEST VALUES FOR PERIOD

Multiply all values by 10 ** -2

```
29 I 8 11 11 13 14 13 14 14 14 15 16 14 1
I + + + + + + + + + + + +
28 I 11 14 16 16 19 18 18 20 17 19 21 19 1
I + + + + + + + + + + + +
27 I 12 15 17 19 19 22 21 22 21 22 22 23 2
I + + + + + + + + + + + +
26 I 12 15 18 21 23 25 26 25 26 22 24 22 2
I + + + + + + + + + + + +
25 I 11 15 18 21 25 27 28 31 32 27 29 28 2
I + + + + + + + + + + + +
24 I 14 16 19 22 27 30 33 36 36 34 35 37 3
I + + + + + + + + + + + +
23 I 16 20 20 23 27 31 36 40 46 46 41 45 3
I + + + + + + + + + + + +
22 I 17 22 23 24 28 36 37 48 50 52 52 52 4
I + + + + + + + + + + + +
21 I 17 22 26 29 31 37 42 50 60 65 67 62 5
I + + + + + + + + + + + +
20 I 19 24 27 32 36 42 48 51 63 72 78 86 8
I + + + + + + + + + + + +
19 I 25 28 29 34 41 44 52 58 54 62 71 80 8
I + + + + + + + + + + + +
18 I 28 31 33 37 42 51 57 66 79 89 86 99 7
I + + + + + + + + + + + +
17 I 32 32 34 43 49 58 69 85 85 116 135 141 21
I + + + + + + + + + + + +
16 I 34 36 31 35 47 63 75 98 131 147 195 244 49
I + + + + + + + + + + + +
15 I 36 41 44 42 34 47 84 104 134 173 230 380 116
I + + + + + + + + + + + +
14 I 41 44 46 54 36 51 97 89 146 238 327 417 74
I + + + + + + + + + + + +
13 I 35 38 36 27 32 44 41 40 116 224 395 496 83
I + + + + + + + + + + + +
12 I 29 36 42 35 29 22 29 72 155 244 404 645 48
I + + + + + + + + + + + +
11 I 31 36 41 39 52 47 25 105 150 250 420 169 168
I + + + + + + + + + + + +
10 I 29 36 45 54 65 73 22 110 64 41 56 120 72
I + + + + + + + + + + + +
9 I 32 45 43 41 45 35 16 42 23 69 92 245 36
I + + + + + + + + + + + +
8 I 31 37 35 14 26 14 15 17 23 101 100 218 28
I + + + + + + + + + + + +
7 I 28 35 13 10 10 11 12 15 36 117 107 180 21
I + + + + + + + + + + + +
6 I 29 33 12 10 17 22 21 35 101 129 116 131 15
```

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```
I + + + + + + + + + + + +
5 I 27 15 9 21 51 59 64 72 90 108 121 117 12
I + + + + + + + + + + + +
4 I 27 18 8 8 41 59 64 70 87 96 99 103 10
I + + + + + + + + + + + +
3 I 28 29 7 14 32 49 54 66 75 83 81 86 8
I + + + + + + + + + + + +
2 I 26 17 7 6 20 41 52 58 60 70 66 72 6
I + + + + + + + + + + + +
1 I 8 6 6 9 26 35 45 45 53 53 56 55 5
I + + + + + + + + + + + +
```

1 2 3 4 5 6 7 8 9 10 11 12 1

88 - RANK HIGHEST VALUES FOR PERIOD

Multiply all values by 10 ** -2

```
29 I 10 7 6 9 7 5 5 4 3
I + + + + + + + + +
28 I 7 9 6 10 11 6 6 5 3
I + + + + + + + + +
27 I 7 6 5 5 6 6 6 5 4
I + + + + + + + + +
26 I 14 11 6 6 6 7 6 6 5
I + + + + + + + + +
25 I 6 6 6 6 7 7 6 6 4
I + + + + + + + + +
24 I 6 6 6 7 8 7 6 6 5
I + + + + + + + + +
23 I 7 6 7 7 8 7 7 6 5
I + + + + + + + + +
22 I 9 7 7 8 7 8 7 7 6
I + + + + + + + + +
21 I 14 8 8 7 8 8 8 7 6
I + + + + + + + + +
20 I 12 8 8 8 9 8 8 8 7
I + + + + + + + + +
19 I 11 9 9 9 9 9 9 9 8 7
I + + + + + + + + +
18 I 11 9 9 9 9 9 9 9 7
I + + + + + + + + +
17 I 13 10 10 9 9 10 9 9 8
I + + + + + + + + +
16 I 13 14 12 11 9 10 10 10 8
I + + + + + + + + +
15 I 27 37 17 21 12 10 11 10 8
I + + + + + + + + +
14 I 84 78 71 58 28 10 11 10 8
I + + + + + + + + +
13 I 117 95 81 61 22 10 10 10 8
I + + + + + + + + +
12 I 134 26 22 34 17 10 11 10 8
I + + + + + + + + +
11 I 41 15 11 10 12 11 10 10 8
I + + + + + + + + +
10 I 14 12 11 12 12 12 11 11 9
I + + + + + + + + +
9 I 15 12 11 11 11 11 11 10 8
I + + + + + + + + +
8 I 51 13 10 10 10 10 10 10 8
I + + + + + + + + +
7 I 53 23 11 9 10 10 10 9 7
I + + + + + + + + +
6 I 55 45 15 8 9 9 9 9 7
I + + + + + + + + +
5 I 39 28 13 10 8 9 9 8 7
I + + + + + + + + +
4 I 12 11 7 8 8 9 8 8 6
I + + + + + + + + +
3 I 7 7 7 7 7 8 8 8 6
I + + + + + + + + +
2 I 7 7 7 8 7 7 7 7 6
```

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WWCPST5.LST

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```
I + + + + + + + + +
1 I 6 6 7 6 6 6 5 5
I + + + + + + + + +
-----
21 22 23 24 25 26 27 28 29
ODOR 1
```

1 RANKED 1 HOUR AVERAGE CONCENTRATION VALUES AT EACH DISCRETE RECEPTOR (Y

```
RECEPTOR COORDINATES (km) 88 RANK
1 342.046 6291.203 1.1101E+00 (2004,169,1700)
2 342.180 6290.668 1.7150E+00 (2004,111,0400)
3 342.112 6290.283 6.8161E-01 (2004,207,2200)
```

```
*****
CALPOST Version 6.132 Level
*****
```

SUMMARY SECTION

ODOR 1

(Odour Units)

RECEPTOR	COORDINATES (km)	TYPE	PEAK (YEAR, DAY, START TIME)	FOR RA
13, 11	341.092 6290.528	GRIDDED	1.6828E+01 (2004,094,0100)	RANK
2	342.180 6290.668	DISCRETE	1.7150E+00 (2004,111,0400)	RANK
13, 11	341.092 6290.528	GRIDDED	1.6828E+01 (2004,094,0100)	RANK
2	342.180 6290.668	DISCRETE	1.7150E+00 (2004,111,0400)	RANK