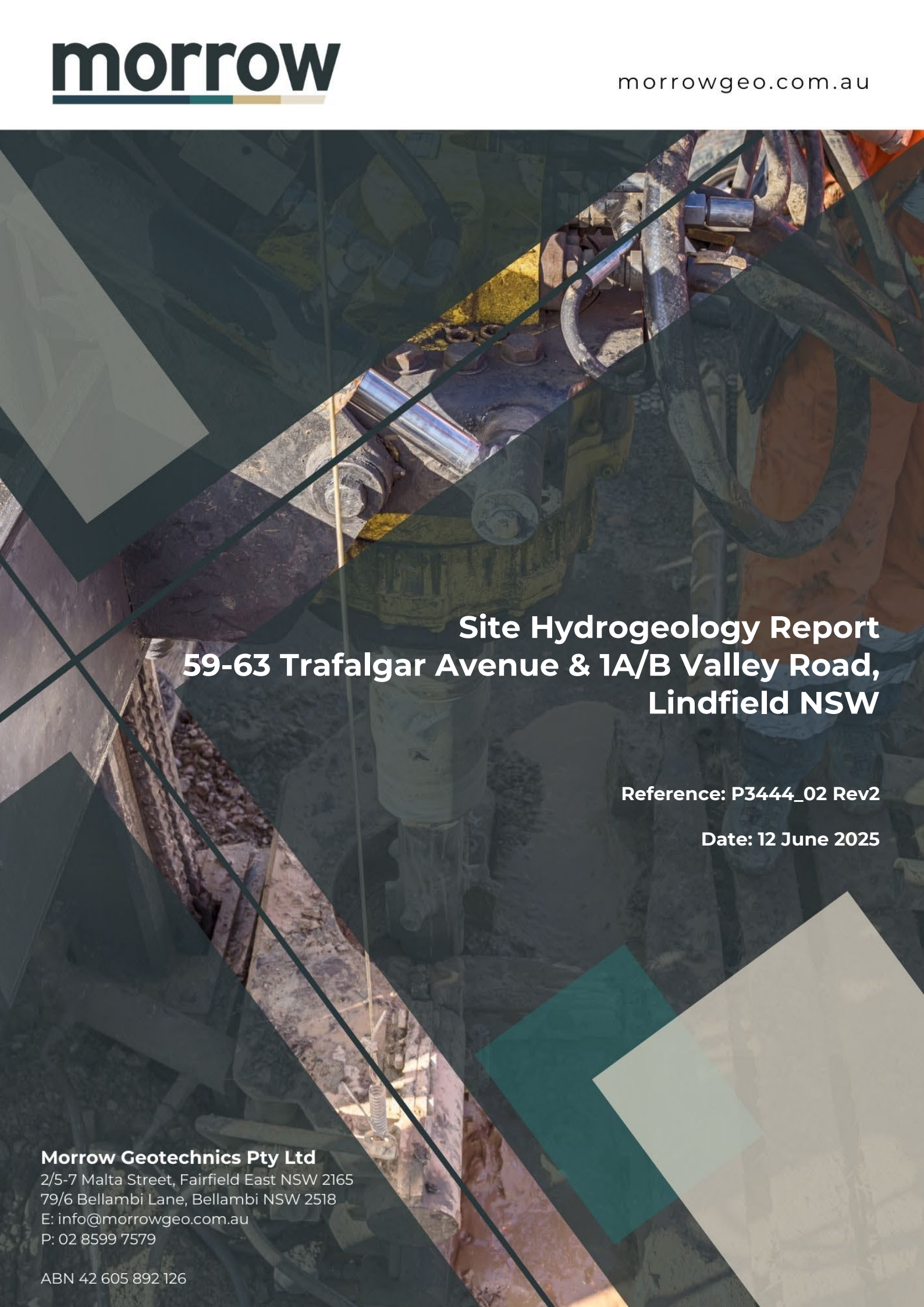


The background of the report cover is a photograph of industrial machinery, likely a drilling rig, with various pipes, bolts, and mechanical components visible. The image is overlaid with a dark, semi-transparent geometric pattern consisting of several overlapping triangles and quadrilaterals in shades of grey, teal, and yellow.

## Site Hydrogeology Report 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW

Reference: P3444\_02 Rev2

Date: 12 June 2025

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|          | Full Name & Title                                           | Signature                                                                             |
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## 1. Introduction

### 1.1 Overview

Morrow Geotechnics Pty Ltd has carried out a Groundwater Study and prepared a Site Hydrogeology Report for the proposed development at 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW (the site) also known as Lot 30 in DP 4215, Lot 71 in DP 4665, Lot 7 in DP 17373, Lot B in DP 344051 and Lot 1 in DP 127411.

The following geotechnical reports have been prepared for the site:

- Morrow Geotechnics Pty Ltd, Geotechnical Investigation Report, 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW, referenced P3444\_01 Rev1, and dated 17 April 2025 (MG 2025).

The geotechnical report presents the results of site investigations for the proposed development and geotechnical recommendations for design and construction.

### 1.2 Proposed Development

Preliminary architectural drawings for the proposed development have been prepared by DKO Architecture for project number 13688 and dated 17 April 2025. From the drawings provided morrow geotechnics understands the proposed involves the construction of a nine storey mixed use development over two levels of basement carpark. Excavation for the basement is expected to extend to a depth of approximately 15.5 m below existing ground level (mBGL) to RL 75.80 mAHD. The basement area is approximately 3228 m<sup>2</sup> with a 300 m perimeter.

### 1.3 Proposed Dewatering Schedule

Given the relatively low permeability of the sandstone profile encountered in the geotechnical investigation it is proposed to construct the basement as a drained soldier pile wall. Dewatering through spear points and pumping is not proposed for the construction period, rather any groundwater seepage will be allowed to drain through strip drainage installed behind shotcrete panels and collected by sump pits within the basement.

The excavation program for the proposed basement is expected to take up to 6 months. Temporary construction dewatering is expected to occur for construction seepage inflows during this 6 month period.

### 1.4 Objectives

The objective of this Site Hydrogeology Report is to provide results on the presence of water at the site and comment on whether there is an aquifer present at the site in accordance with the definition of aquifer as laid out in the NSW DPI Office of Water Aquifer Interference Policy. Section 1.2 of the policy defines an aquifer as

“the term ‘aquifer’ is commonly understood to mean a groundwater system that is sufficiently permeable to allow water to move within it, and which can yield productive volumes of groundwater”

Further, this report provides analysis of the permeability of soils encountered within boreholes at the site and geotechnical advice and recommendations on the management of groundwater in the design and construction of the proposed development.



## 2. Geological Model

### 2.1 Published Geological Mapping

Information on regional sub-surface conditions, referenced from the Department of Mineral Resources Geological Map Sydney 1:100,000 (Geological Series Sheet 9130) indicate that the site is located on the boundary of (Rwa) Ashfield Shale of the Wianamatta Group, which is typically comprised of black to dark-grey shale and laminate, and (Rh) Hawkesbury Sandstone, which is typically comprised of medium to coarse-grained quartz sandstone, with very minor shale and laminite lenses.

### 2.2 Soil Landscapes

The Soil Conservation Service of NSW Sydney 1:100,000 Soil Landscapes Series Sheet 9130 (4th Edition) indicates that the erosional landscape at the site likely comprises Glenorie Landscape. Generally, comprises gently undulating to rolling low hills on Wianamatta Group shales with inclined slopes of typically 5-20%. Soils of Glenorie landscape generally comprises shallow to moderately deep (<1000cm) red and brown podzolic soil in the upper slopes. These soils are noted moderately reactive.

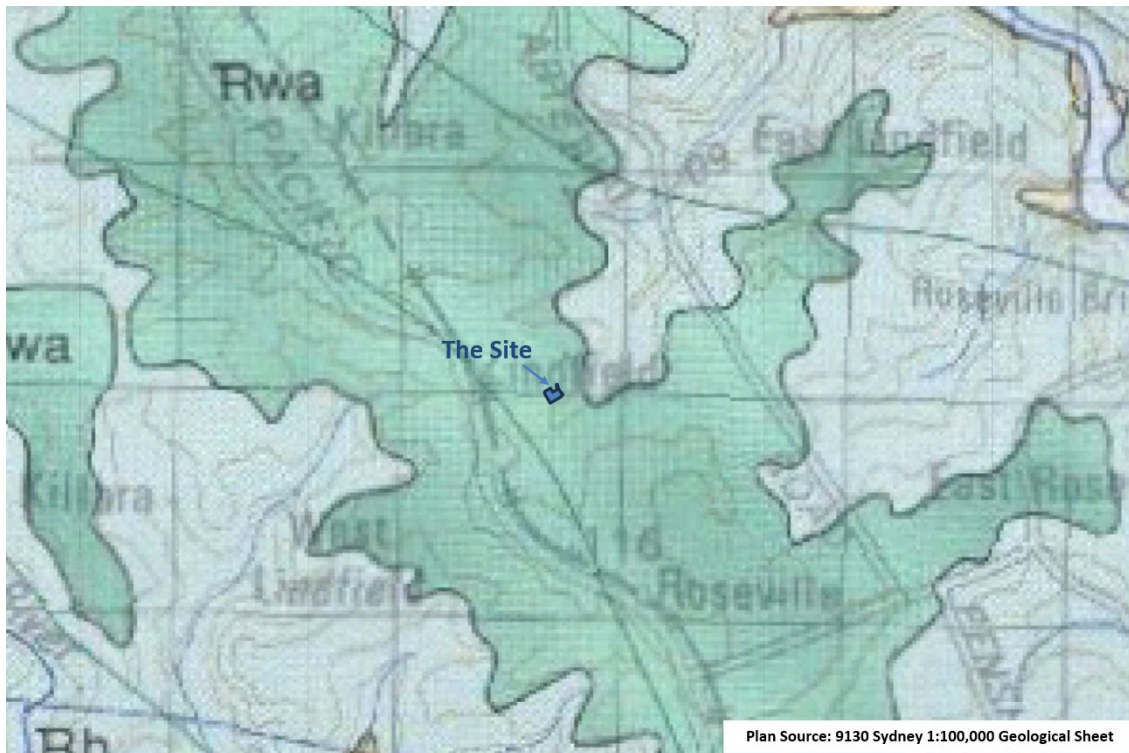
### 2.3 Site Description

During the Geotechnical and Hydrogeological Investigations, the site was occupied by five residential lots.

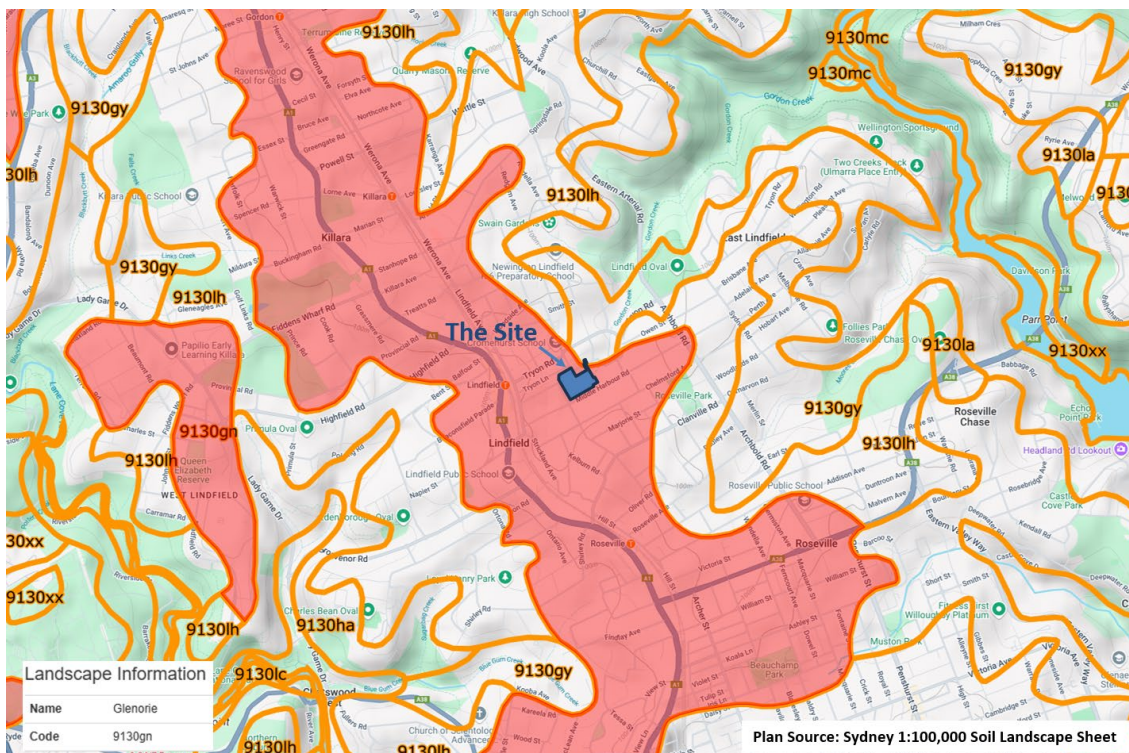
**Table 1 Site Description**

| Address                    | Lot/DP          | Comments                                                                         |
|----------------------------|-----------------|----------------------------------------------------------------------------------|
| <b>1A Valley Road</b>      | <b>B/34401</b>  | Occupied by a two storey brick residence with an in-ground pool and tennis court |
| <b>1B Valley Road</b>      | <b>7/17373</b>  | Occupied by a two storey brick residence with an in-ground pool                  |
| <b>59 Trafalgar Avenue</b> | <b>71/4665</b>  | Occupied by a two storey brick residence with an in-ground pool                  |
| <b>61 Trafalgar Avenue</b> | <b>30/4215</b>  | Occupied by a two storey brick residence with an in-ground pool                  |
| <b>63 Trafalgar Avenue</b> | <b>1/127411</b> | Occupied by a two storey brick residence with an in-ground pool and tennis court |

The site covers approximately 6672 m<sup>2</sup>. The site topography slopes moderately towards the south, with elevations ranging from RL 91.35 mAHD in the north west corner to RL 81.3 mAHD in the south west corner of the site. The site is bordered to the north, east, south and west by residential properties.



**Figure 1:** Regional Geology taken from 9130 Sydney 1:100,000 Geological Sheet



**Figure 2:** Soil Landscapes taken from Sydney 1:100,000 Soil Landscape Sheet

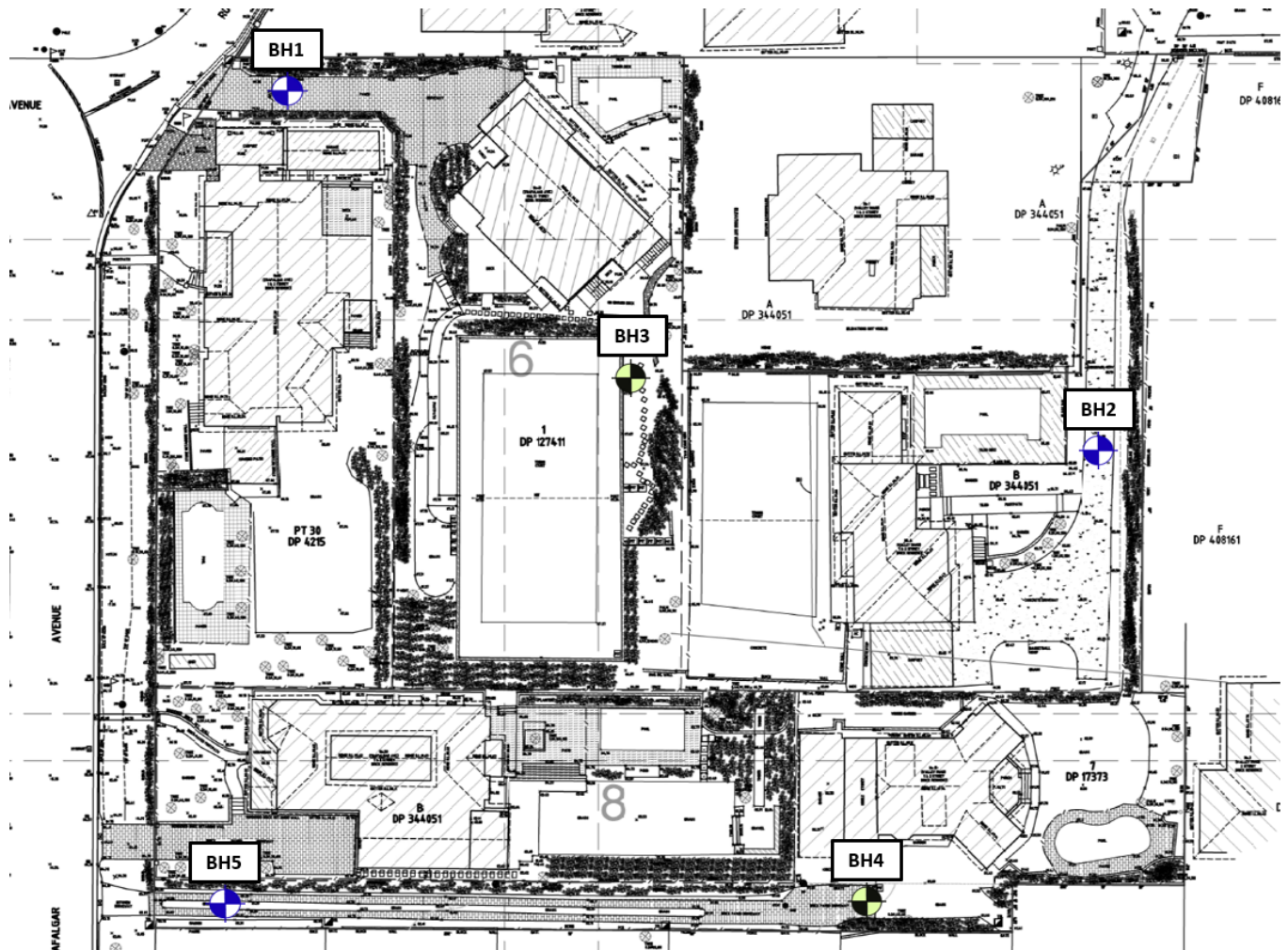
## 2.4 Stratigraphic Model

Five boreholes were drilled in total (BH1, BH2, BH3, BH4 and BH5). Boreholes BH1, BH2, BH4 and BH5 were drilled by a track-mounted drill rig using solid flight augers equipped with a tungsten-carbide bit (TC bit). BH3 was drilled by a man-portable drilling rig. The boreholes were extended



beyond TC bit refusal by NMLC coring techniques to depths of between 18.0 m and 35.75 m below ground level (mBGL).

Borehole locations are shown on **Figure 3** below:



**Figure 3:** Borehole Location Plan

The subsurface conditions encountered during the previous investigations indicate that the site is underlain by fill/topsoil and residual soil overlying sandstone bedrock. A summary of the subsurface conditions across the site, interpreted from the investigation results, is presented in **Table 2** and **Table 3**. Borehole Locations are shown on the plan attached to this report.

**Table 2 Summary of Inferred Subsurface Conditions**

| Unit | Material            | Generalised Description                                                                                                                                                                                          |
|------|---------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| 1    | Fill/Topsoil        | FILL: Silty to gravelly SAND, loose, fine grained, fine to coarse sized gravel. Unit 1 is inferred to be uncontrolled and poorly compacted.                                                                      |
| 2    | Residual Clay       | Residual Silty to gravelly CLAY, firm to stiff, medium to high plasticity, fine to coarse sized gravel, subangular to subrounded ironstone gravel, less than or equal to plastic limit.                          |
| 3    | Class V Sandstone   | Extremely to highly weathered Sandstone, extremely low to very low strength, fine grained, with extremely weathered seams and ironstone bands, 5° laminations.                                                   |
| 4    | Class IV Sandstone  | Moderately to Slightly weathered Sandstone, very low to low strength, fine grained. Defects consist of Extremely weathered and crushed seams as well as partings between 1° and 5° and Joints between 20° – 90°. |
| 5    | Class III Sandstone | Fresh Sandstone, medium strength, fine grained. Generally massive with some carbonaceous laminations.                                                                                                            |
| 6    | Class II Sandstone  | Fresh Sandstone, high strength, fine grained. Generally massive with some carbonaceous laminations. A medium strength shale band was encountered within Unit 6 in BH1 at between 34.65 and 35.43 mBGL.           |

**Table 3 Encountered Geotechnical Conditions**

| Unit | Material            | Approx. Depth Range of Unit <sup>1</sup> mBGL (RL mAHD) |                               |                               |                               |                               |
|------|---------------------|---------------------------------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|
|      |                     | BH1                                                     | BH2                           | BH3                           | BH4                           | BH5                           |
| 1    | Fill/Topsoil        | 0.0 to 0.2<br>(91.3 to 91.1)                            | 0.0 to 0.7<br>(85.4 to 84.7)  | 0.0 to 0.3<br>(87.5 to 87.2)  | 0.0 to 0.5<br>(81.7 to 81.2)  | 0.0 to 0.4<br>(83.8 to 83.4)  |
| 2    | Residual Clay       | 0.2 to 1.0<br>(90.9 to 90.1)                            | 0.7 to 1.0<br>(84.7 to 84.4)  | 0.3 to 0.5<br>(87.2 to 87.0)  | 0.5 to 2.5<br>(81.2 to 79.2)  | 0.4 to 1.5<br>(83.4 to 82.3)  |
| 3    | Class V Sandstone   | 1.0 to 2.0<br>(90.1 to 89.1)                            | 1.0 to 4.8<br>(84.4 to 80.6)  | 0.5 to 2.4<br>(87.0 to 85.1)  | 2.5 to 3.0<br>(79.2 to 78.7)  | 1.5 to 2.5<br>(82.3 to 81.3)  |
| 4    | Class IV Sandstone  | 2.0 to 6.4<br>(89.1 to 84.9)                            | 4.8 to 6.0<br>(80.6 to 79.4)  | 2.4 to 4.7<br>(85.1 to 82.8)  | 3.0 to 3.6<br>(78.7 to 78.1)  | 2.5 to 3.6<br>(81.3 to 80.2)  |
| 5    | Class III Sandstone | 6.4 to 7.7<br>(84.9 to 83.6)                            | 6.0 to 8.0<br>(79.4 to 77.4)  | 4.7 to 9.3<br>(82.8 to 78.2)  | 3.6 to 7.2<br>(78.1 to 74.5)  | 3.6 to 6.6<br>(80.2 to 77.2)  |
| 6    | Class II Sandstone  | 7.7 to 35.7<br>(83.6 to 55.6)                           | 8.0 to 20.5<br>(77.4 to 64.9) | 9.3 to 20.4<br>(78.2 to 67.1) | 7.2 to 18.0<br>(74.5 to 63.7) | 6.6 to 18.0<br>(77.2 to 65.8) |

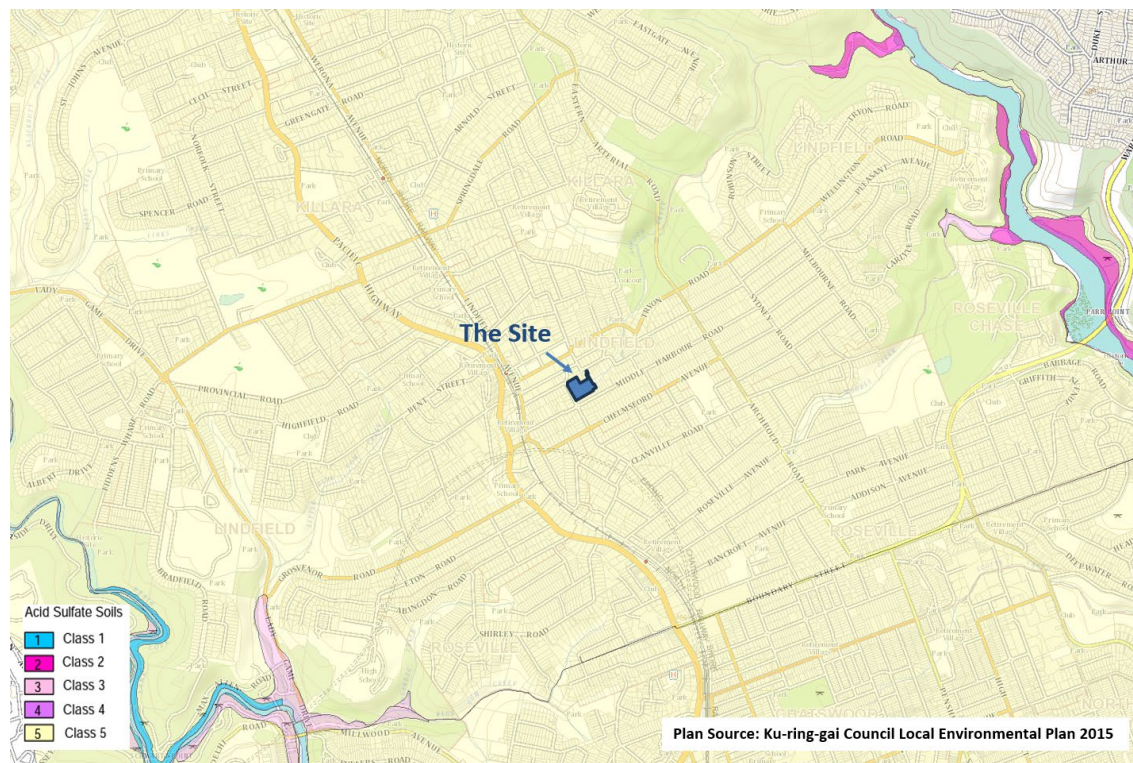
**Notes:**

<sup>1</sup> Depths shown are based on material observed within test locations and will vary across the site.



## 2.5 Acid Sulfate Soils

According to the Ku-ring-gai Council Local Environmental Plan 2015 the site is located in a Class 5 area of Acid Sulfate Soils (see location in **Figure 4** below). Class 5 areas are within 500 m of areas mapped as Class 4 to 1, however Acid Sulphate Soils are not expected within Class 5 Areas.



**Figure 4:** Acid Sulfate Soils Map with site location

## 2.6 Groundwater Dependent Ecosystems

Groundwater Dependent Ecosystems (GDEs) are ecosystems that rely on groundwater to fulfill all or part of their water needs, ensuring the survival of their plant and animal communities, as well as their ecological processes and services (NSW DPE 2023). The reliance of GDEs on groundwater can be seasonal, continual, or episodic (Howe et al. 2007). These ecosystems vary widely in size, ranging from just a few meters to several square kilometres. GDEs can be categorized into three main types (Eamus et al. 2006; Richardson et al. 2011):

- **Groundwater Dependent Vegetation (Terrestrial GDEs):** These ecosystems depend on the subsurface presence of groundwater, often accessed through the capillary fringe or vadose zone (the unsaturated subsurface area just above the water table) (Naumburg et al. 2005; Eamus et al. 2006a). Within these communities, plant species may exhibit varying degrees of groundwater dependency, from complete reliance on groundwater to partial or infrequent dependency (Hatton and Evans 1998; Zencich et al. 2002; Eamus et al. 2006; Froend and Drake 2006).
- **Aquatic GDEs:** These environments occur where groundwater surfaces, such as in rivers, wetlands, and springs. Aquatic GDEs are considered dependent on groundwater if groundwater is essential to the biota and ecological processes at any stage of the ecosystem's life span (Howe et al. 2007).
- **Subterranean GDEs:** These ecosystems exist within the saturated zones of aquifers, including water-filled spaces in various geological matrices such as karst (caves), fractured

rock, and alluvial systems. They also encompass hyporheic ecosystems, which occur within the sediments of surface waters, acting as a transitional zone between surface and groundwater ecosystems (Hose et al. 2022).

GDEs include a wide range of environments like aquifers, lakes, streams, springs, cave systems, swamps, and wetlands. They rely on groundwater to meet their water requirements, which is crucial for maintaining their flora and fauna. The level of groundwater dependence and the nature of this reliance affect how GDEs respond to changes in groundwater quality and quantity. Groundwater extraction can negatively impact these ecosystems.

According to New South Wales Government mapping (see location in **Figure 5** below), areas of low to medium probability GDEs surround the site with High Ecological Value Aquatic Ecosystems (HEVAE) identified at Gordon Creek 500m to the north east of site and Roseville park 550m to the east of the site.



**Figure 5:** Groundwater Dependent Ecosystems with site location

## 2.7 Groundwater Monitoring Bores

According to the Bureau of Meteorology (BOM) Australian Groundwater Explorer no water supply bores are located with 500m of the site, bore locations are shown on **Figure 6** below.



**Figure 6:** Bores with site location

## 3. Hydrogeological Model

### 3.1 Groundwater Observations

Standpipe piezometer wells were installed the boreholes (BH1, BH2 and BH5) as part of the geotechnical & environmental investigations. Monitoring well construction details are found in **Table 4** below. Before the installation of the piezometers, drill cuttings and water in the boreholes were flushed out. The monitoring wells were constructed using 50 mm diameter screw threaded PVC casing, sections of which were machine slotted. The annulus between the casing and boreholes was backfilled using 2 mm filter gravel pack to above the top of the screen. A bentonite plug with a minimum thickness of 0.5m was then installed above the gravel pack, the remaining annulus was backfilled with drill cuttings. The wells were each finished with a cement plug and a gatic cover.

Groundwater levels within the three piezometer wells have been monitored by Morrow Geotechnics between 28 February 2025 and 4 June 2025.



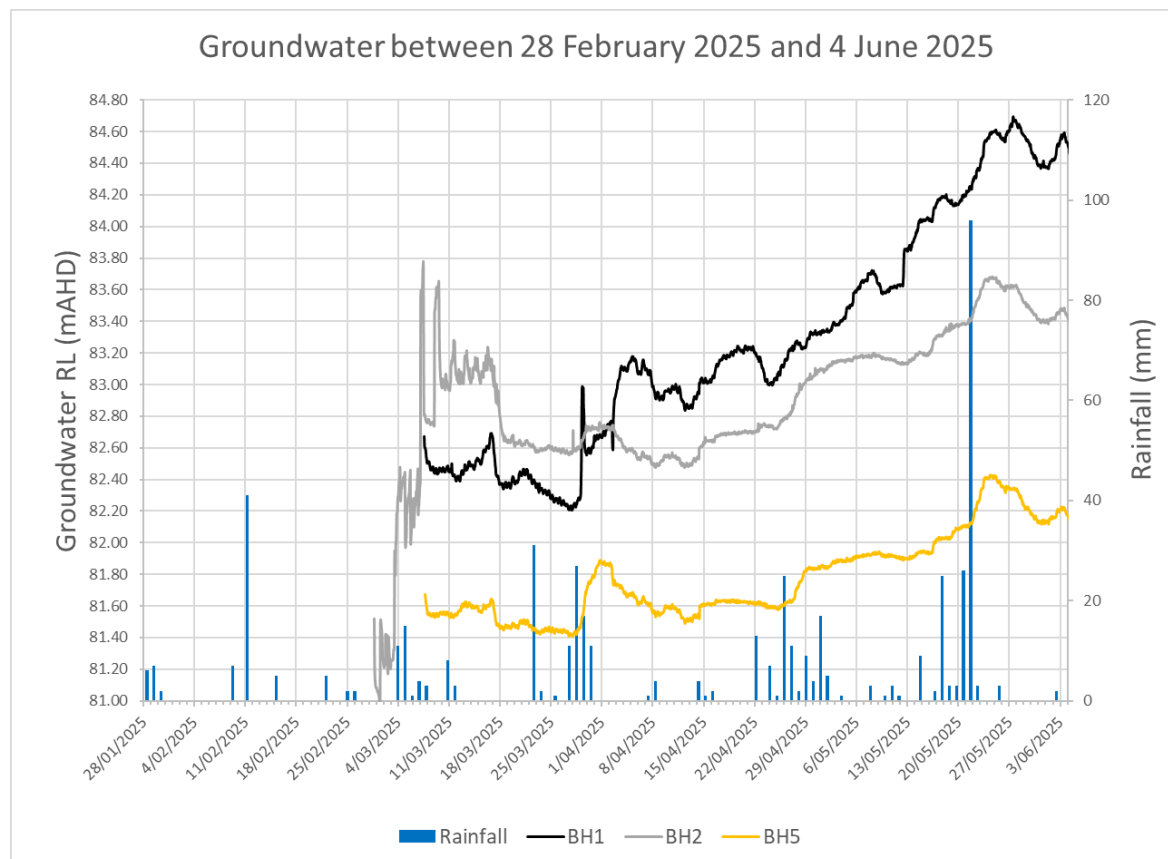
**Table 4 Piezometer Details**

| Piezometer                          | BH1         | BH2         | BH5         |
|-------------------------------------|-------------|-------------|-------------|
| Top of Piezometer approx. RL (mAHD) | 91.3        | 85.4        | 83.8        |
| Piezometer Depth mBGL               | 35.0        | 20.4        | 18.0        |
| Bentonite Plug Depth mBGL           | 0.0 to 1.5  | 2.5 to 5.0  | 1.0 to 3.0  |
| Screen Depth mBGL                   | 1.5 to 35.0 | 5.5 to 20.4 | 3.0 to 18.0 |
| Well Development Date               | 28/02/2025  | 28/02/2025  | 28/02/2025  |

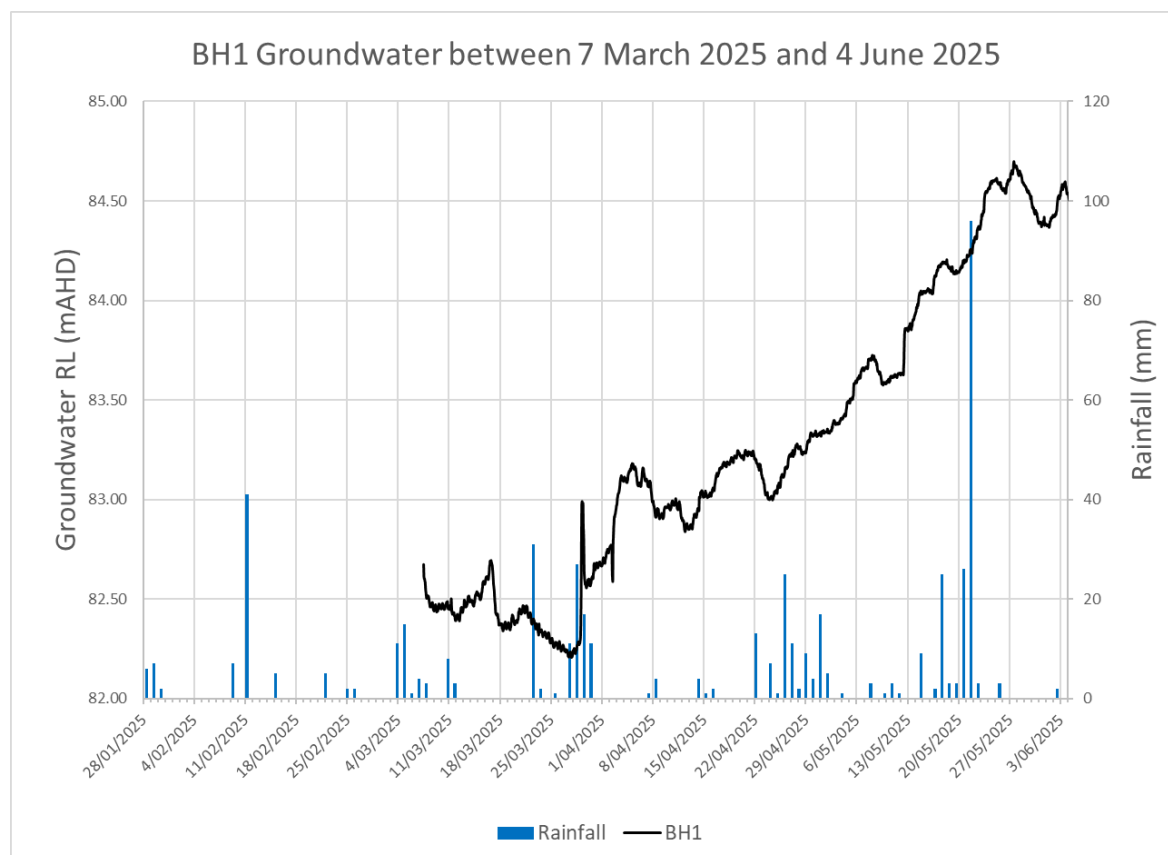
**Table 5 Water Levels from Manual Readings**

| Monitoring Date  | Piezometer Groundwater Level mBGL (RL mAHD) |                      |                      |
|------------------|---------------------------------------------|----------------------|----------------------|
|                  | BH1                                         | BH2                  | BH5                  |
| <b>7/03/2025</b> | 8.80<br>(82.50 mAHD)                        | 3.13<br>(82.27 mAHD) | 2.28<br>(81.52 mAHD) |
| <b>2/04/2025</b> | 8.55<br>(82.75 mAHD)                        | 2.60<br>(82.80 mAHD) | 1.95<br>(81.85 mAHD) |
| <b>4/06/2025</b> | 6.90<br>(84.40 mAHD)                        | 2.03<br>(83.37 mAHD) | 1.65<br>(82.15 mAHD) |

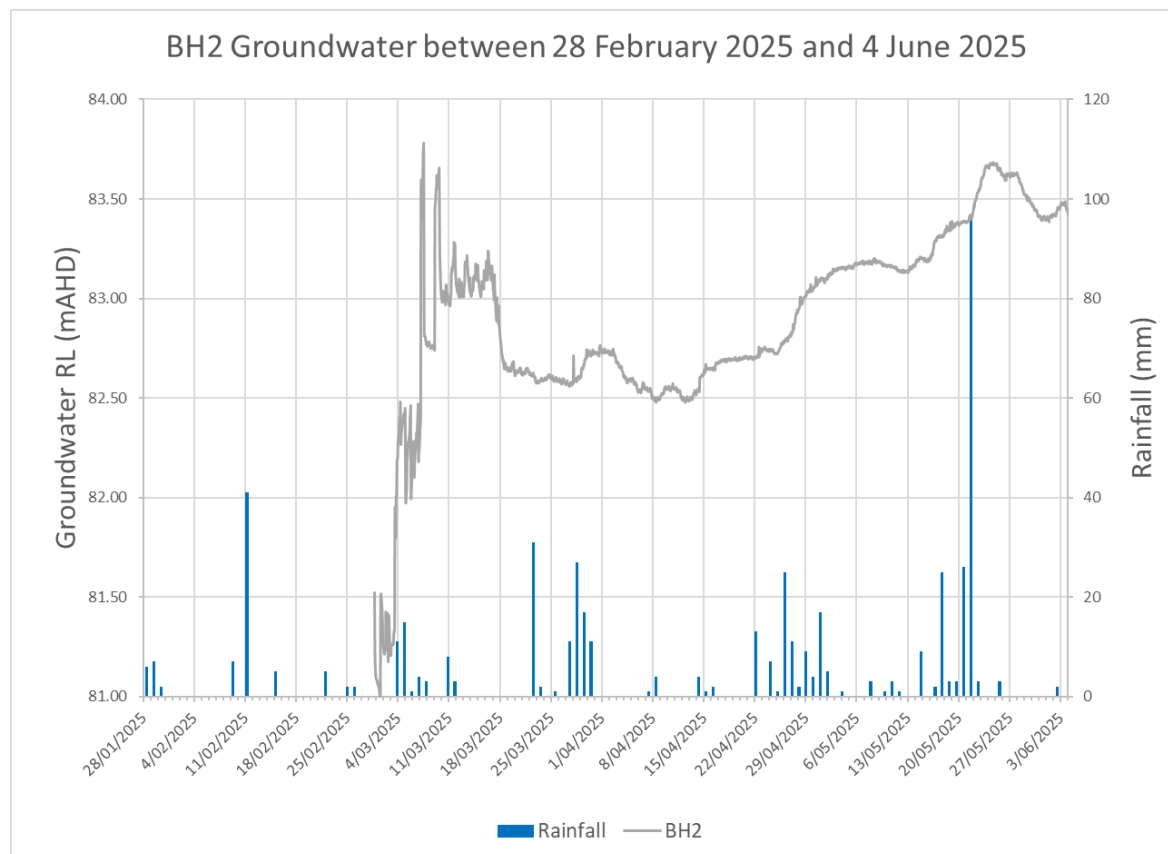
Automatic dataloggers were installed within BH1, BH2 and BH5 in order to provide long term groundwater measurements. Dataloggers were installed between 28 February 2025 and 4 June 2025. The data loggers were set to measure groundwater levels at one hour intervals. Graphs of water level measurements taken by the automatic dataloggers are displayed in **Figure 7** to **Figure 10** below. Daily rainfall totals taken from Bureau of Meteorology North Ryde Golf Club AWS {station 66213} for the monitoring period are displayed alongside water level measurements.



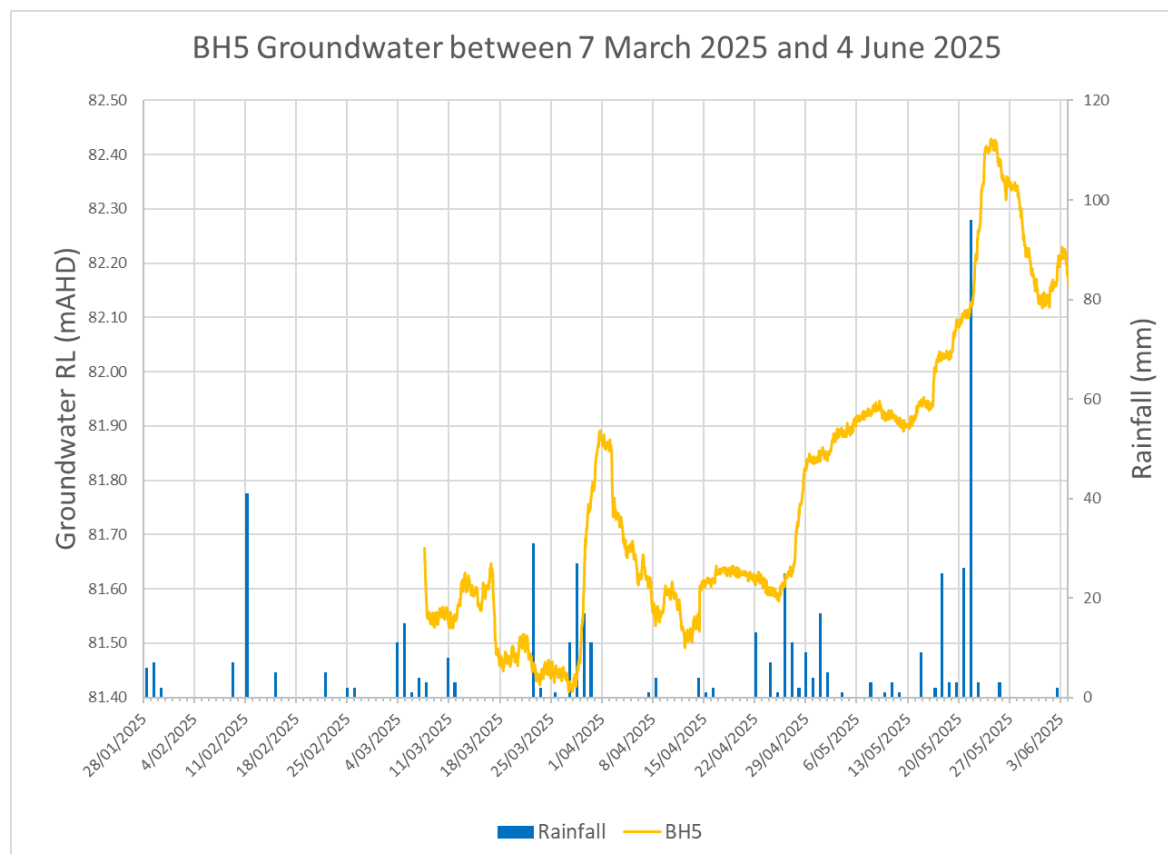
**Figure 7:** Data Logger Measurements and Daily Rainfall



**Figure 8:** BH1 Data Logger Measurements and Daily Rainfall



**Figure 9:** BH2 Data Logger Measurements and Daily Rainfall



**Figure 10:** BH5 Data Logger Measurements and Daily Rainfall



A summary of the groundwater observations within the three wells is provided below:

**Table 6      Groundwater Observation Summary**

| Monitoring Date            | Piezometer Groundwater Level mBGL (RL mAHD) |                           |                           |
|----------------------------|---------------------------------------------|---------------------------|---------------------------|
|                            | BH1                                         | BH2                       | BH5                       |
| <b>Maximum Water Level</b> | 6.60 mBGL<br>(84.69 mAHD)                   | 1.62 mBGL<br>(83.77 mAHD) | 1.37 mBGL<br>(82.42 mAHD) |
| <b>Minimum Water Level</b> | 9.09 mBGL<br>(82.20 mAHD)                   | 4.40 mBGL<br>(80.99 mAHD) | 2.39 mBGL<br>(81.41 mAHD) |
| <b>Average Water Level</b> | 8.01 mBGL<br>(83.28 mAHD)                   | 2.50 mBGL<br>(82.89 mAHD) | 2.01 mBGL<br>(81.78 mAHD) |
| <b>Median Water Level</b>  | 8.13 mBGL<br>(83.16 mAHD)                   | 2.57 mBGL<br>(82.82 mAHD) | 2.13 mBGL<br>(81.66 mAHD) |

Average groundwater levels at the three piezometers fall within the following lithologies;

- BH1 - Unit 6 Class II Sandstone;
- BH2 - Unit 3 Class V Sandstone; and
- BH5 - Unit 3 Class V Sandstone.

Water levels within the borehole BH1 and BH5 were moderately responsive to rainfall events during the monitoring period. This is inferred to result from surface water infiltration following rainfall recharging the groundwater.

The results of the water level monitoring show a stable hydraulic gradient across the site between RL 83.3 mAHD and RL 81.8 mAHD. On the basis of ongoing groundwater monitoring at the site it is recommended that a design groundwater level for site is taken at the following depths;

- BH1 – RL 85.00 mAHD;
- BH2 - RL 83.80 mAHD; and
- BH5 - RL 82.50 mAHD.

### 3.2      Hydraulic Conductivity Testing

Rising head permeability tests were carried out on BH1, BH2 and BH5 to give an indication of in-situ permeability of the material at the site. Permeability values were calculated on the basis of the testing in accordance with the formulas provided in British Standard BS5930 -1999 Code of Practice for Site Investigations, Section 21.4.6. Calculation sheets for permeability testing are provided as an attachment to this letter as **Appendix C**. Permeability tests were repeated three times to ensure reliability of results.

Permeability values which were adopted from the testing for the assessment of groundwater seepage volumes are shown in **Table 7** below.

**Table 7      Borehole Permeability Values**

| Borehole          | Permeability Based on In-situ Measurement |                       |
|-------------------|-------------------------------------------|-----------------------|
|                   | (m/s)                                     | (m/day)               |
| <b>BH1 Test 1</b> | $2.75 \times 10^{-8}$                     | $2.37 \times 10^{-3}$ |
| <b>BH1 Test 2</b> | $2.00 \times 10^{-8}$                     | $1.72 \times 10^{-3}$ |
| <b>BH1 Test 3</b> | $2.50 \times 10^{-8}$                     | $2.16 \times 10^{-3}$ |
| <b>BH1 Test 4</b> | $3.90 \times 10^{-8}$                     | $3.36 \times 10^{-3}$ |
| <b>BH2 Test 1</b> | $4.70 \times 10^{-7}$                     | 0.0406                |
| <b>BH2 Test 2</b> | $6.59 \times 10^{-7}$                     | 0.0569                |
| <b>BH2 Test 3</b> | $7.12 \times 10^{-7}$                     | 0.0615                |
| <b>BH2 Test 4</b> | $1.93 \times 10^{-7}$                     | 0.0166                |
| <b>BH5 Test 1</b> | $2.00 \times 10^{-7}$                     | 0.0172                |
| <b>BH5 Test 2</b> | $1.94 \times 10^{-7}$                     | 0.0167                |
| <b>BH5 Test 3</b> | $2.15 \times 10^{-7}$                     | 0.0185                |

On the basis of the testing results presented above, the following permeability values may be adopted for design and analysis of the excavation:

- Class V to Class IV Sandstone –  $3.8 \times 10^{-7}$  m/s - interpreted from BH2 and BH5 testing; and
- Class III to Class II Sandstone –  $2.8 \times 10^{-8}$  m/s - interpreted from BH1 testing.

### 3.3 Local Groundwater Regime

On the basis of ongoing groundwater monitoring at the site it is recommended that a design groundwater level for the water table is taken at the following depths;

- BH1 – RL 85.00 mAHD;
- BH2 - RL 83.80 mAHD; and
- BH5 - RL 82.50 mAHD.

Based on the geotechnical investigation and ongoing monitoring it is possible to conclude that the hydrogeological conditions at the site are typical of a generally low to moderate permeability rock mass.

### 3.4 Water Quality Observations

Field testing of the groundwater was carried out on 2 April 2025. The results of which are presented in **Table 8**.

**Table 8      Field Testing Results**

| Measured Concentration in Water Sample |             |                   |            |      |                  |                       |                                           |
|----------------------------------------|-------------|-------------------|------------|------|------------------|-----------------------|-------------------------------------------|
| BH                                     | Test Number | Date & Time       | Redox (mV) | pH   | Dissolved Oxygen | Conductivity (µS/cm.) | Appearance (Colour, Turbidity, Odour etc) |
| BH1                                    | 1           | 02/4/2025 9:45am  | 79         | 6.24 | 3.58             | 2047                  | Slightly Cloudy                           |
|                                        | 2           | 02/4/2025 10:00am | 78.9       | 6.25 | 3.52             | 2190                  | Slightly Cloudy                           |
|                                        | 3           | 02/4/2025 10:10am | 72.9       | 6.36 | 3.54             | 2270                  | Slightly Cloudy                           |
| BH2                                    | 1           | 02/4/2025 10:50am | 44.8       | 6.86 | 4.08             | 554                   | Natural gas odour, slightly cloudy        |
|                                        | 2           | 02/4/2025 11:05am | 99.5       | 5.88 | 3.76             | 1019                  | Natural gas odour, slightly cloudy        |
|                                        | 3           | 02/4/2025 11:15am | 101.1      | 5.86 | 3.54             | 1148                  | Natural gas odour, slightly cloudy        |
| BH5                                    | 1           | 02/4/2025 11:30am | 141.6      | 5.15 | 3.67             | 1580                  | Sulphur odour, cloudy                     |
|                                        | 2           | 02/4/2025 11:45am | 148.7      | 5.01 | 3.58             | 1652                  | Sulphur odour, cloudy                     |
|                                        | 3           | 02/4/2025 11:55am | 144.0      | 5.10 | 3.54             | 1540                  | Sulphur odour, cloudy                     |

A sample of the water to be discharged was taken on 2 April 2025 and sent to a NATA accredited laboratory for testing against the ANZG (2018) and Australia and New Zealand Environment Conservation Council ANZECC (2000) guidelines for 95% protection of marine ecosystems (in the absence of guidelines the criteria for fresh waters was used) and National Environment Protection (Assessment of Site Contamination) Measure (NEPM, 2013). Relevant water quality results are presented in **Table 9** to **Table 13**, lab results are attached in **Appendix B**.

The groundwater samples were taken from BH1, BH2 and BH5 using an electric powered pump with a length of ¼ inch low-density polyethylene (LDPE) tubing. The groundwater sample was collected from the outflow tube and stored in containers proved by SGS laboratory. The containers were immediately placed in an esky with ice packs to maintain a cool temperature and delivered to SGS laboratory same day. Disposable nitrile gloves were used for sample collection to minimize potential contamination.

**Table 9 Water Quality Results - Physical Parameters**

| Analytes                                           | Measured Concentration in Water Sample |     |      | KRG Council | ANZECC (2000) Fresh Water Threshold | ANZECC (2000) Marine Water Threshold | ANZG (2018) Fresh Water (95% Species Protection) | ANZG (2018) Marine (95% Species Protection) |
|----------------------------------------------------|----------------------------------------|-----|------|-------------|-------------------------------------|--------------------------------------|--------------------------------------------------|---------------------------------------------|
|                                                    | BH1                                    | BH2 | BH5  |             |                                     |                                      |                                                  |                                             |
| Bicarbonate Alkalinity as CaCO <sub>3</sub> (mg/L) | 69                                     | 86  | <5   | -           | -                                   | -                                    | -                                                | -                                           |
| Carbonate Alkalinity as CaCO <sub>3</sub> (mg/L)   | <1                                     | <1  | <1   | -           | -                                   | -                                    | -                                                | -                                           |
| Hydroxide Alkalinity as CaCO <sub>3</sub> (mg/L)   | <5                                     | <5  | <5   | -           | -                                   | -                                    | -                                                | -                                           |
| Total Alkalinity as CaCO <sub>3</sub> (mg/L)       | 69                                     | 86  | <5   | -           | -                                   | -                                    | -                                                | -                                           |
| pH                                                 | 5.9                                    | 6.3 | 4.7  | -           | -                                   | -                                    | -                                                | -                                           |
| Electrical Conductivity (µS/cm)                    | 1300                                   | 440 | 1200 | -           | -                                   | -                                    | -                                                | -                                           |
| Redox Potential (Eh) (mV)                          | 282                                    | -   | -    | -           | -                                   | -                                    | -                                                | -                                           |
| Total Dissolved Solids (TDS) (mg/L)                | 800                                    | 270 | 750  | -           | -                                   | -                                    | -                                                | -                                           |
| Total Hardness (mg/L)                              | 170                                    | -   | -    | -           | -                                   | -                                    | -                                                | -                                           |
| Dissolved Oxygen (DO) (mg/L)                       | 4.3                                    | -   | -    | -           | -                                   | -                                    | -                                                | -                                           |
| Turbidity (NTU)                                    | 150                                    | -   | -    | -           | -                                   | -                                    | -                                                | -                                           |
| Total Suspended Solids (TSS) (mg/L)                | 280                                    | 240 | 950  | -           | -                                   | -                                    | -                                                | -                                           |
| Total Organic Carbon (TOC) (mg/L)                  | 4.0                                    | -   | -    | -           | -                                   | -                                    | -                                                | -                                           |
| Sodium Absorption Ration (SAR)                     | 8.4                                    | -   | -    | -           | -                                   | -                                    | -                                                | -                                           |



**Table 10      Water Quality Results - Major Anions & Major Cations**

| Analytes      | Measured Concentration in Water Sample |      |     | KRG Council | ANZECC (2000) Fresh Water Threshold | ANZECC (2000) Marine Water Threshold | ANZG (2018) Fresh Water (95% Species Protection) | ANZG (2018) Marine (95% Species Protection) |
|---------------|----------------------------------------|------|-----|-------------|-------------------------------------|--------------------------------------|--------------------------------------------------|---------------------------------------------|
|               | BH1                                    | BH2  | BH5 |             |                                     |                                      |                                                  |                                             |
| Major Anions  | Sulfate (SO <sub>4</sub> ) (mg/L)      | 200  | 72  | 94          | -                                   | -                                    | -                                                | -                                           |
|               | Chloride (mg/L)                        | 380  | 110 | 470         | -                                   | -                                    | -                                                | -                                           |
|               | Bromide (Br) (mg/L)                    | 1.9  | -   | -           | -                                   | -                                    | -                                                | -                                           |
|               | Fluoride (F) (mg/L)                    | 0.48 | -   | -           | -                                   | -                                    | -                                                | -                                           |
|               | Calcium (Ca) (mg/L)                    | 19   | 23  | 7.8         | -                                   | -                                    | -                                                | -                                           |
| Major Cations | Magnesium (Mg) (mg/L)                  | 30   | 3.7 | 27          | -                                   | -                                    | -                                                | -                                           |
|               | Sodium (Na) (mg/L)                     | 250  | 72  | 230         | -                                   | -                                    | -                                                | -                                           |
|               | Potassium (K) (mg/L)                   | 7.7  | 3.3 | 4.5         | -                                   | -                                    | -                                                | -                                           |
|               | Cation/Anion Balance (%)               | <0   | -   | -           | -                                   | -                                    | -                                                | -                                           |

**Table 11 Water Quality Results - Dissolved Inorganics and Dissolved Heavy Metals**

| Analytes                       | Measured Concentration in Water Sample |         |         | KRG Council | ANZECC (2000) Fresh Water Threshold | ANZECC (2000) Marine Water Threshold | ANZG (2018) Fresh Water (95% Species Protection) | ANZG (2018) Marine (95% Species Protection) |
|--------------------------------|----------------------------------------|---------|---------|-------------|-------------------------------------|--------------------------------------|--------------------------------------------------|---------------------------------------------|
|                                | BH1                                    | BH2     | BH5     |             |                                     |                                      |                                                  |                                             |
| Aluminium (Al) (µg/L)          | 67                                     | -       | -       | -           | -                                   | -                                    | 0.8 (pH<6.5)*<br>55 (pH>6.5)*                    | -                                           |
| Antimony (Sb) (µg/L)           | <1                                     | -       | -       | -           | -                                   | -                                    | 91*                                              | -                                           |
| Arsenic (As) (µg/L)            | <1                                     | <1      | 3       | -           | 24                                  | -                                    | 24                                               | -                                           |
| Barium (Ba)                    | 29                                     | -       | -       | -           | -                                   | -                                    | -                                                | -                                           |
| Beryllium (Be)                 | 1                                      | -       | -       | -           | -                                   | -                                    | -                                                | -                                           |
| Boron (B) (µg/L)               | 120                                    | -       | -       | -           | -                                   | -                                    | 940                                              | -                                           |
| Cadmium (Cd) (µg/L)            | 0.2                                    | <0.1    | <0.1    | -           | 0.2                                 | 0.7                                  | 0.2                                              | 5.5                                         |
| Chromium (Cr) (µg/L)           | <1                                     | <1      | <1      | -           | 1                                   | 4.4                                  | -                                                | -                                           |
| Cobalt (Co) (µg/L)             | 34                                     | -       | -       | -           | -                                   | -                                    | 1.4*                                             | 1                                           |
| Copper (Cu) (µg/L)             | 4                                      | <1      | 2       | -           | 1.4                                 | 1.3                                  | 1.4                                              | 1.3                                         |
| Iron (Fe)                      | 6                                      | -       | -       | -           | -                                   | -                                    | -                                                | -                                           |
| Lead (Pb) (µg/L)               | <1                                     | <1      | <1      | -           | 3.4                                 | 4.4                                  | 3.4                                              | 4.4                                         |
| Lithium (Li) (mg/L)            | 0.042                                  | -       | -       | -           | -                                   | -                                    | -                                                | -                                           |
| Manganese (Mn) (µg/L)          | 2600                                   | -       | -       | -           | -                                   | -                                    | 1900                                             | -                                           |
| Mercury (Hg) (mg/L)            | <0.0001                                | <0.0001 | <0.0001 | -           | 0.06                                | 0.1                                  | 0.6                                              | 0.4                                         |
| Molybdenum (Mo) (µg/L)         | <1                                     | -       | -       | -           | -                                   | -                                    | 34*                                              | -                                           |
| Nickel (Ni) (µg/L)             | 28                                     | 2       | 71      | -           | 11                                  | 7                                    | 11                                               | 70                                          |
| Selenium (Se) (µg/L)           | <1                                     | -       | -       | -           | -                                   | -                                    | 11                                               | -                                           |
| Silica (dissolved SiO2) (mg/L) | 51                                     | -       | -       | -           | -                                   | -                                    | -                                                | -                                           |
| Silver (Ag) (µg/L)             | <1                                     | -       | -       | -           | -                                   | -                                    | 0.05                                             | 1.4                                         |
| Strontium (Sr) (µg/L)          | 130                                    | -       | -       | -           | -                                   | -                                    | -                                                | -                                           |
| Uranium (U) (µg/L)             | <1                                     | -       | -       | -           | -                                   | -                                    | 0.5*                                             | -                                           |
| Vanadium (V) (µg/L)            | <1                                     | -       | -       | -           | -                                   | -                                    | 6*                                               | 100                                         |
| Zinc (Zn) (µg/L)               | 180                                    | 17      | 240     | -           | 8                                   | 15                                   | 8                                                | 8                                           |

**Table 12      Water Quality Results – Nutrients & Microbiological Organisms**

| Analytes                  |                                 | Measured Concentration in Water Sample |     |     | KRG Council | ANZECC (2000) Fresh Water Threshold | ANZECC (2000) Marine Water Threshold | ANZG (2018) Fresh Water (95% Species Protection) | ANZG (2018) Marine (95% Species Protection) |
|---------------------------|---------------------------------|----------------------------------------|-----|-----|-------------|-------------------------------------|--------------------------------------|--------------------------------------------------|---------------------------------------------|
|                           |                                 | BH1                                    | BH2 | BH5 |             |                                     |                                      |                                                  |                                             |
| Nutrients                 | Ammonia (NH3) (mg/L)            | 0.17                                   | -   | -   |             | -                                   | -                                    | 900                                              | 910                                         |
|                           | Nitrate (NO3) (mg/L)            | <0.005                                 | -   | -   |             | -                                   | -                                    | -                                                | -                                           |
|                           | Total Nitrogen (N) (mg/L)       | 0.53                                   | -   | -   |             | -                                   | -                                    | -                                                | -                                           |
|                           | Oxidised Nitrogen (N) (mg/L)    | <0.005                                 | -   | -   |             | -                                   | -                                    | -                                                | -                                           |
|                           | Total Phosphorus (P) (mg/L)     | 0.10                                   | -   | -   |             | -                                   | -                                    | -                                                | -                                           |
|                           | Reactive Phosphorus (P) (mg/L)  | <0.005                                 | -   | -   |             | -                                   | -                                    | -                                                | -                                           |
| Microbiological Organisms | Faecal Coliforms (MPN/100mL)    | 5                                      | -   | -   |             | -                                   | -                                    | -                                                | -                                           |
|                           | Faecal Streptococci (CFU/100mL) | 130                                    | -   | -   |             | -                                   | -                                    | -                                                | -                                           |
|                           | Escherichia Coli (CFU/100mL)    | 10                                     | -   | -   |             | -                                   | -                                    | -                                                | -                                           |

**Table 13 Water Quality Results - Organics**

| Analytes                                                   | Measured Concentration in Water Sample |      |      | KRG Council | ANZECC (2000) Fresh Water Threshold | ANZECC (2000) Marine Water Threshold | ANZG (2018) Fresh Water (95% Species Protection) | ANZG (2018) Marine (95% Species Protection) |
|------------------------------------------------------------|----------------------------------------|------|------|-------------|-------------------------------------|--------------------------------------|--------------------------------------------------|---------------------------------------------|
|                                                            | BH1                                    | BH2  | BH5  |             |                                     |                                      |                                                  |                                             |
| Benzene (µg/L)                                             | <0.5                                   | <0.5 | <0.5 |             | 950                                 | 500                                  | 950                                              | 700                                         |
| Toluene (µg/L)                                             | <0.5                                   | 0.5  | <0.5 |             | -                                   | -                                    | 180                                              | 180                                         |
| Ethylbenzene (µg/L)                                        | <0.5                                   | <0.5 | <0.5 |             | -                                   | -                                    | 80                                               | 80                                          |
| O-Xylene (µg/L)                                            | <0.5                                   | <0.5 | <0.5 |             | 350                                 | -                                    | 350                                              | -                                           |
| M/P-Xylene (µg/L)                                          | <1                                     | <1   | <1   |             | 200                                 | -                                    | -                                                | -                                           |
| Naphthalene (VOC) (µg/L)                                   | <0.5                                   | <0.5 | <0.5 |             | 16                                  | 50                                   | 16                                               | 70                                          |
| Benzene<br>Toluene<br>Ethylbenzene<br>Xylene (BTEX) (µg/L) | <3                                     | <3   | <3   |             | -                                   | -                                    | -                                                | -                                           |
| Total Recoverable Hydrocarbons (TRHs) C6-C10 (µg/L)        | <50                                    | <50  | <50  |             | -                                   | -                                    | -                                                | -                                           |
| Total Recoverable Hydrocarbons (TRHs) C6-C9 (µg/L)         | <40                                    | <40  | <40  |             | -                                   | -                                    | -                                                | -                                           |
| Polycyclic Aromatic Hydrocarbons (PAHs) (µg/L)             | <1                                     | <1   | <1   |             | -                                   | -                                    | -                                                | -                                           |

Concentrations of **Copper**, **Manganese**, **Nickel** and **Zinc** are above the ANZG Freshwater guidelines for the water sample tested at the site.

#### 4. Statement of Limitations

The advice and parameters presented in this Groundwater Management Plan are for assessment of the expected groundwater seepage based upon the proposed development and encountered site conditions at the investigation locations.

We draw your attention to the document “Important Information”, which is attached to this letter. The statements presented in this document are intended to advise you of what your realistic expectations of this report should be. The document is not intended to reduce the level of responsibility accepted by Morrow Geotechnics, but rather to ensure that all parties who may rely on this report are aware of the responsibilities each assumes in so doing.





|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                                |                     |              |
|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------|---------------------|--------------|
| <div><div></div><div><div><div>02 8599 7579</div></div><div><div>Sydney Gadigal Land,<br/>2/5-7 Malta Steet, Fairfield East<br/>NSW 2155</div></div><div><div>info@morrowgeo.com.au</div></div></div></div> |                                |                     |              |
| Sydney Gadigal Land: 2/5-7<br>Malta Steet, Fairfield East<br>NSW 2155                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  |                                | P: 02 8599 7579     |              |
| P3444 Borehole Location Plan                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |                                |                     |              |
| Client No:                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             |                                | Job No: P3444       |              |
| Client: Landmark Group Construction Australia Pty Ltd                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  |                                |                     |              |
| Project: Lindfield                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |                                |                     |              |
| Address: 59-63 Trafalgar Avenue & 1A/B Valley Road,<br>Lindfield NSW                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   |                                |                     |              |
| Legend:                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |                                |                     |              |
| <div> Borehole Locations</div> <div> Groundwater Monitoring Well Locations</div>                                                                                                                                                                                                                                                                                                 |                                |                     |              |
| Image Source: NearMap                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  |                                | Viewed: 2025-03-06  |              |
| Drawn By:<br>R. McKeon                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 | Checked By:<br>Ozzie<br>Baskan | Date:<br>2025-03-06 | Figure:<br>1 |

**APPENDIX A**

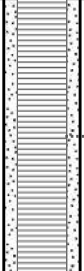
**BOREHOLE LOGS, EXPLANATORY NOTES AND SITE  
PHOTOS**



|                       |                                   |                                                                     |
|-----------------------|-----------------------------------|---------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : GEO205 - Comacchio  | Job Number : P3444                                                  |
| Easting : 330797,48   | Driller Supplier : GEOSENSE       | Client : Landmark Group Construction Australia Pty Ltd              |
| Northing : 6261245,34 | Logged By : Ozzie Baskan          | Project : Lindfield                                                 |
| RL : 91.30(m)         | Reviewed By : Mahmoud Jangidaryan | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth : 35.75 m | Date : 26/02/2025                 | Loc Comment : Driveway of 63 Trafalgar Avenue , near the gate.      |

| Drilling Method | Water   | Well Diagram | Testing | Elevation | Graphic Log | Material Type | Classification Code | Material Description                                                                                                                        | Depth (m) | Consistency | Weathering | Moisture |
|-----------------|---------|--------------|---------|-----------|-------------|---------------|---------------------|---------------------------------------------------------------------------------------------------------------------------------------------|-----------|-------------|------------|----------|
|                 |         |              |         | Depth (m) |             |               |                     |                                                                                                                                             |           |             |            |          |
| ADT             | 2. GWNE |              |         | 91.1      |             | Non-Soil      | PAV                 | Non-Soil - Pavers                                                                                                                           | 0.15      |             |            |          |
|                 |         |              |         | 0.15      |             |               |                     | Residual Silty CLAY stiff to very stiff, medium to high plasticity, pale brown brown pale grey, trace fine to medium sized gravel, w < pl.  |           |             |            |          |
|                 |         |              |         | 90.3      |             | Residual      | CI-CH               |                                                                                                                                             |           | St-VSt      |            | w < PL   |
|                 |         |              |         | 1         |             |               |                     | Extremely weathered Sandstone, Silty CLAY hard, low to medium plasticity, pale grey mottled brown, with ironstone and sandstone bands.      | 1         |             |            |          |
|                 |         |              |         | 89.3      |             | Rock          | SLT                 |                                                                                                                                             |           | H           | XW         |          |
|                 |         |              |         | 2         |             |               |                     | Rock SANDSTONE: highly weathered, very low to low strength, pale brown pale grey mottled red, fine to medium grained, with ironstone bands. | 2         |             |            |          |
|                 |         |              |         |           |             | Rock          | SST                 |                                                                                                                                             |           | VLS-LS      | HW         |          |
|                 |         |              |         |           |             |               |                     |                                                                                                                                             | 3         |             |            |          |

|                       |                                   |                                                                     |
|-----------------------|-----------------------------------|---------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : GEO205 - Comacchio  | Job Number : P3444                                                  |
| Easting : 330797.48   | Driller Supplier : GEOSENSE       | Client : Landmark Group Construction Australia Pty Ltd              |
| Northing : 6261245.34 | Logged By : Ozzie Baskan          | Project : Lindfield                                                 |
| RL : 91.30(m)         | Reviewed By : Mahmoud Jangidaryan | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth : 35.75 m | Date : 26/02/2025                 | Loc Comment : Driveway of 63 Trafalgar Avenue , near the gate.      |

| Drilling Method                                                                                                                                                                                                                                                                                           | Water | Well Diagram                                                                      | Testing | Elevation | Graphic Log                                                                       | Material Type | Classification Code | Material Description                                                                                                                        | Depth (m) | Consistency | Weathering | Moisture |
|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------|-----------------------------------------------------------------------------------|---------|-----------|-----------------------------------------------------------------------------------|---------------|---------------------|---------------------------------------------------------------------------------------------------------------------------------------------|-----------|-------------|------------|----------|
|                                                                                                                                                                                                                                                                                                           |       |                                                                                   |         | Depth (m) |                                                                                   |               |                     |                                                                                                                                             |           |             |            |          |
| <div style="text-align: center;"> <div style="width: 100%; height: 100%; border: 1px solid black; position: relative;"> <div style="position: absolute; left: 0; top: 0; bottom: 0; width: 2px; background: linear-gradient(to bottom, black 49%, white 49%, white 51%, black 51%);"></div> </div> </div> |       |  |         | 86.6      |  | Rock          | SST                 | Rock SANDSTONE: highly weathered, very low to low strength, pale brown pale grey mottled red, fine to medium grained, with ironstone bands. | 4.7       | VLS-LS      | HW         |          |
|                                                                                                                                                                                                                                                                                                           |       |                                                                                   |         | 4.7       |                                                                                   |               |                     |                                                                                                                                             |           |             |            |          |
|                                                                                                                                                                                                                                                                                                           |       |                                                                                   |         |           |                                                                                   |               |                     | Commenced Coring at 4.7m                                                                                                                    |           |             |            |          |

|                       |                                   |                                                                     |
|-----------------------|-----------------------------------|---------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : GEO205 - Comacchio  | Job Number : P3444                                                  |
| Easting : 330797.48   | Driller Supplier : GEOSENSE       | Client : Landmark Group Construction Australia Pty Ltd              |
| Northing : 6261245.34 | Logged By : Ozzie Baskan          | Project : Lindfield                                                 |
| RL : 91.30(m)         | Reviewed By : Mahmoud Jangidaryan | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth : 35.75 m | Date : 26/02/2025                 | Loc Comment : Driveway of 63 Trafalgar Avenue , near the gate.      |

| Drilling Method | Water | Well Diagram | Elevation | Graphic Log | Classification Code | Material Description                                                                                                                 | Depth (m) | Weathering | Testing          | Estimated Strength | RQD% and TCR%              | Defect Spacing (mm) | Defect Description                                                                                                                                                                 |
|-----------------|-------|--------------|-----------|-------------|---------------------|--------------------------------------------------------------------------------------------------------------------------------------|-----------|------------|------------------|--------------------|----------------------------|---------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
|                 |       |              | Depth (m) |             |                     |                                                                                                                                      |           |            | Is(50)           |                    |                            |                     |                                                                                                                                                                                    |
|                 |       |              |           |             |                     | Commenced Coring at 4.7m                                                                                                             |           |            |                  |                    |                            |                     |                                                                                                                                                                                    |
|                 |       |              | 86.2      | X           | SST                 | Rock SANDSTONE: highly to moderately weathered, medium strength, red pale grey, fine grained, ..                                     | 5         | HW-MW      | d:0.10 ; a:0.40  |                    | RQD = 27.78%<br>TCR = 100% |                     | 4.73, P, 5°, UN, RO, STN, OP,<br>4.75, P, 10°, UN, RO, STN, C,<br>4.79, P, 5°, IR, RO, CL, OP, (X2),<br>4.87, P, 5°, UN, RO, STN, OP, (X2),<br>4.95, P, 5°, PL, RO, STN, OP, (X2), |
|                 |       |              | 5.06      |             | CRL                 | Coreloss                                                                                                                             | 5.06      |            |                  |                    |                            |                     | 5.05, P, 5°, UN, RO, CL, OP, (X2),<br>5.06-5.24, CORELOSS,                                                                                                                         |
|                 |       |              | 86.1      | X           | SST                 | Rock SANDSTONE: highly to moderately weathered, low strength, pale grey pale brown, fine to medium grained, with ironstone beddings. | 5.24      | HW-MW      |                  |                    |                            |                     | 5.24-5.45, CRF, 5°, IR, RO, STN, OP,                                                                                                                                               |
|                 |       |              | 5.24      |             |                     |                                                                                                                                      |           |            |                  |                    |                            |                     | 5.43-5.52, XWS,                                                                                                                                                                    |
|                 |       |              | 85.8      | X           | SST                 | Rock SANDSTONE: moderately weathered, medium strength, pale grey, fine to medium grained, carbonaceous beddings.                     | 5.53      | MW         | d:0.24 ; a:0.98  |                    | RQD = 63.16%<br>TCR = 100% |                     | 5.61, P, 5°, IR, RO, CL, OP,<br>5.64, P, 5°, IR, RO, CL, OP,                                                                                                                       |
|                 |       |              | 5.53      |             |                     |                                                                                                                                      |           |            |                  |                    |                            |                     | 5.81, XWS, 5mm,<br>5.83-5.84, XWS, 10mm,                                                                                                                                           |
|                 |       |              | 85.5      | X           | SST                 | As above, but pale grey pale brown.                                                                                                  | 5.85      | MW         |                  |                    |                            |                     | 6.03, P, 5°, UN, RO, CL, OP, (X2),                                                                                                                                                 |
|                 |       |              | 5.85      |             |                     |                                                                                                                                      |           |            |                  |                    |                            |                     | 6.2-6.37, CORELOSS,                                                                                                                                                                |
|                 |       |              | 85.1      | X           | CRL                 | Coreloss                                                                                                                             | 6.2       |            |                  |                    |                            |                     | 6.46, P, 5°, UN, RO, CL, OP,                                                                                                                                                       |
|                 |       |              | 6.2       |             |                     |                                                                                                                                      |           |            |                  |                    |                            |                     | 6.61, P, 5°, UN, RO, CL, OP,                                                                                                                                                       |
|                 |       |              | 84.9      | X           | SST                 | Rock SANDSTONE: moderately to slightly weathered, medium to high strength, pale grey, fine to medium grained, ..                     | 6.37      | MW-SW      | d:0.25 ; a:1.36  |                    |                            |                     | 6.81, P, 5°, PL, RO, CL, OP, (X2),                                                                                                                                                 |
|                 |       |              | 6.37      |             |                     |                                                                                                                                      |           |            |                  |                    |                            |                     | 7.02, P, 5°, UN, RO, CL, OP, (X2),                                                                                                                                                 |
|                 |       |              | 84.5      | X           | SST                 | As above, but moderately weathered, low to medium strength, pale grey, with siltstone bands.                                         | 6.8       | MW         | d:0.09 ; a:0.38  |                    |                            |                     | 7.16, P, 5°, PL, RO, CL, OP,                                                                                                                                                       |
|                 |       |              | 6.8       |             |                     |                                                                                                                                      |           |            |                  |                    |                            |                     | 7.25, P, PL, RO, CL, OP, (X2),                                                                                                                                                     |
|                 |       |              | 84.3      | X           | SST                 | Rock SANDSTONE: slightly weathered, high strength, pale grey, fine grained, ..                                                       | 7.2       | SW         | d:0.142 ; a:1.30 |                    | RQD = 94.38%<br>TCR = 100% |                     | 7.43, P, 5°, UN, RO, CL, OP, (2X),                                                                                                                                                 |
|                 |       |              | 7         |             |                     |                                                                                                                                      |           |            |                  |                    |                            |                     | 7.61-7.67, CRF, 5°,<br>7.7, P, 5°, PL, RO, CL, OP,                                                                                                                                 |



|                       |                                   |                                                                     |
|-----------------------|-----------------------------------|---------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : GEO205 - Comacchio  | Job Number : P3444                                                  |
| Easting : 330797.48   | Driller Supplier : GEOSENSE       | Client : Landmark Group Construction Australia Pty Ltd              |
| Northing : 6261245.34 | Logged By : Ozzie Baskan          | Project : Lindfield                                                 |
| RL : 91.30(m)         | Reviewed By : Mahmoud Jangidaryan | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth : 35.75 m | Date : 26/02/2025                 | Loc Comment : Driveway of 63 Trafalgar Avenue , near the gate.      |

| Drilling Method | Water                | Well Diagram     | Elevation | Graphic Log | Classification Code | Material Description                                                                                        | Depth (m) | Weathering | Testing         | Estimated Strength | RQD% and TCR%              | Defect Spacing (mm) | Defect Description                                                 |
|-----------------|----------------------|------------------|-----------|-------------|---------------------|-------------------------------------------------------------------------------------------------------------|-----------|------------|-----------------|--------------------|----------------------------|---------------------|--------------------------------------------------------------------|
|                 |                      |                  | Depth (m) |             |                     |                                                                                                             |           |            | Is(50)          |                    |                            |                     |                                                                    |
| NMLC Coring     | Loss - 0% Water Loss | 50mm PVC Slotted | 83.3      |             | SST                 | Rock SANDSTONE: slightly weathered, high strength, pale grey, fine to medium grained, with siltstone bands. | 8         | SW         |                 |                    | RQD = 94.38%<br>TCR = 100% |                     | 8.27, P, 5°, PL, RO, CL, OP,<br><br>8.61, P, 10°, UN, RO, CL, OP,  |
|                 |                      |                  |           |             |                     |                                                                                                             |           |            | d:1.07 ; a:1.68 |                    |                            |                     |                                                                    |
|                 |                      |                  | 82.3      |             |                     |                                                                                                             | 9         |            | d:1.46 ; a:2.17 |                    |                            |                     |                                                                    |
|                 |                      |                  |           |             |                     |                                                                                                             |           |            |                 |                    |                            |                     |                                                                    |
| NMLC Coring     | Loss - 0% Water Loss | 50mm PVC Slotted |           |             | SST                 | As above, but pale grey.                                                                                    |           | SW         |                 |                    | RQD = 100%<br>TCR = 100%   |                     | 9.81, P, 5°, UN, RO, CL, OP,<br><br>10.64, P, 30°, PL, RO, CL, OP, |
|                 |                      |                  |           |             |                     |                                                                                                             |           |            | d:1.69 ; a:2.03 |                    |                            |                     |                                                                    |
|                 |                      |                  |           |             |                     |                                                                                                             |           |            |                 |                    |                            |                     |                                                                    |
|                 |                      |                  |           |             |                     |                                                                                                             |           |            |                 |                    |                            |                     |                                                                    |
| NMLC Coring     | Loss - 0% Water Loss | 50mm PVC Slotted | 80.1      |             | SST                 | As above, but moderately weathered, medium to high strength.                                                | 11.2      | MW         |                 |                    | RQD = 100%<br>TCR = 100%   |                     | 11.64, P, 5°, PL, RO, CL, OP,                                      |
|                 |                      |                  |           |             |                     |                                                                                                             |           |            | d:0.79 ; a:1.75 |                    |                            |                     |                                                                    |
|                 |                      |                  |           |             |                     |                                                                                                             |           |            |                 |                    |                            |                     |                                                                    |
|                 |                      |                  |           |             |                     |                                                                                                             |           |            |                 |                    |                            |                     |                                                                    |

|             |              |                  |                       |             |                                                            |
|-------------|--------------|------------------|-----------------------|-------------|------------------------------------------------------------|
| UTM         | : 56S        | Driller Rig      | : GEO205 - Comacchio  | Job Number  | : P3444                                                    |
| Easting     | : 330797.48  | Driller Supplier | : GEOSENSE            | Client      | : Landmark Group Construction Australia Pty Ltd            |
| Northing    | : 6261245.34 | Logged By        | : Ozzie Baskan        | Project     | : Lindfield                                                |
| RL          | : 91.30(m)   | Reviewed By      | : Mahmoud Jangidaryan | Location    | : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth | : 35.75 m    | Date             | : 26/02/2025          | Loc Comment | : Driveway of 63 Trafalgar Avenue , near the gate.         |

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|                       |                                   |                                                                     |
|-----------------------|-----------------------------------|---------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : GEO205 - Comacchio  | Job Number : P3444                                                  |
| Easting : 330797.48   | Driller Supplier : GEOSENSE       | Client : Landmark Group Construction Australia Pty Ltd              |
| Northing : 6261245.34 | Logged By : Ozzie Baskan          | Project : Lindfield                                                 |
| RL : 91.30(m)         | Reviewed By : Mahmoud Jangidaryan | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth : 35.75 m | Date : 26/02/2025                 | Loc Comment : Driveway of 63 Trafalgar Avenue , near the gate.      |

| Drilling Method | Water                | Well Diagram     | Elevation | Graphic Log | Classification Code | Material Description                                                                  | Depth (m) | Weathering | Testing         | Estimated Strength | RQD% and TCR% | Defect Spacing (mm) | Defect Description |
|-----------------|----------------------|------------------|-----------|-------------|---------------------|---------------------------------------------------------------------------------------|-----------|------------|-----------------|--------------------|---------------|---------------------|--------------------|
|                 |                      |                  | Depth (m) |             |                     |                                                                                       |           |            | Is(50)          |                    |               |                     |                    |
| NMLC Coring     | Loss - 0% Water Loss | 50mm PVC Slotted |           | SST         |                     | As above, but fine to coarse grained.                                                 |           |            |                 |                    |               |                     |                    |
|                 |                      |                  |           |             |                     |                                                                                       |           |            | d:1.23 ; a:1.31 |                    |               |                     |                    |
|                 |                      |                  |           |             |                     |                                                                                       | 17        | SW         |                 |                    |               |                     |                    |
|                 |                      |                  |           |             |                     |                                                                                       |           |            | d:1.36 ; a:1.23 |                    |               |                     |                    |
|                 |                      |                  |           |             |                     |                                                                                       | 18        |            |                 |                    |               |                     |                    |
|                 |                      |                  | 72.6      | CRL         |                     |                                                                                       | 18.7      |            |                 |                    |               |                     |                    |
|                 |                      |                  | 18.7      |             |                     | Coreloss                                                                              |           |            |                 |                    |               |                     |                    |
|                 |                      |                  | 72.5      |             |                     |                                                                                       | 18.8      |            |                 |                    |               |                     |                    |
|                 |                      |                  | 18.8      |             |                     | Rock SANDSTONE: slightly weathered, high strength, pale grey, fine to coarse grained. |           |            | d:1.28 ; a:1.09 |                    |               |                     |                    |
|                 |                      |                  |           |             |                     |                                                                                       | 19        | SW         |                 |                    |               |                     |                    |
|                 | Loss - 0% Water Loss |                  |           | SST         |                     |                                                                                       |           |            |                 |                    |               |                     |                    |
|                 |                      |                  |           |             |                     |                                                                                       |           |            | d:1.18 ; a:1.10 |                    |               |                     |                    |
|                 |                      |                  |           |             |                     |                                                                                       |           |            |                 |                    |               |                     |                    |

|             |              |                  |                       |             |                                                            |
|-------------|--------------|------------------|-----------------------|-------------|------------------------------------------------------------|
| UTM         | : 56S        | Driller Rig      | : GEO205 - Comacchio  | Job Number  | : P3444                                                    |
| Easting     | : 330797.48  | Driller Supplier | : GEOSENSE            | Client      | : Landmark Group Construction Australia Pty Ltd            |
| Northing    | : 6261245.34 | Logged By        | : Ozzie Baskan        | Project     | : Lindfield                                                |
| RL          | : 91.30(m)   | Reviewed By      | : Mahmoud Jangidaryan | Location    | : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth | : 35.75 m    | Date             | : 26/02/2025          | Loc Comment | : Driveway of 63 Trafalgar Avenue , near the gate.         |

| Drilling Method | Water                           | Well Diagram                  | Elevation | Graphic Log | Classification Code | Material Description                                                                  | Depth (m)     | Weathering | Testing |                 | Estimated Strength                                         | RQD% and TCR%                | Defect Spacing (mm)                             | Defect Description                   |
|-----------------|---------------------------------|-------------------------------|-----------|-------------|---------------------|---------------------------------------------------------------------------------------|---------------|------------|---------|-----------------|------------------------------------------------------------|------------------------------|-------------------------------------------------|--------------------------------------|
|                 |                                 |                               | Depth (m) |             |                     |                                                                                       |               |            | Is(50)  |                 |                                                            |                              |                                                 |                                      |
| NMLC Coring     | <div>Loss - 0% Water Loss</div> | <div>50mm PVC Slotted</div>   |           | <div></div> | SST                 | Rock SANDSTONE: slightly weathered, high strength, pale grey, fine to coarse grained. | <div>21</div> | SW         |         | d:1.68 ; a:1.03 | <div>VLS<br/>LS<br/>LS<br/>MS<br/>HS<br/>VHS<br/>EHS</div> | RQD = 96.67%<br>TCR = 96.67% | <div>30<br/>100<br/>300<br/>1000<br/>3000</div> | 20.03, J, 30°, PL, RO, CT, OP, (X2), |
|                 |                                 |                               |           |             |                     |                                                                                       |               |            |         |                 |                                                            |                              |                                                 | 20.35, P, 5°, PL, RO, CT, OP,        |
|                 |                                 |                               |           |             |                     |                                                                                       |               |            |         |                 |                                                            |                              |                                                 | 20.68, P, 5°, PL, RO, CL, OP, (X2),  |
|                 |                                 |                               |           |             |                     |                                                                                       |               |            |         |                 |                                                            |                              |                                                 | 21.62, P, 20°, PL, RO, VN, OP,       |
|                 |                                 |                               |           |             |                     |                                                                                       |               |            |         | d:1.23 ; a:1.28 |                                                            |                              |                                                 | 22.75, J, 70°, UN, RO, CL, OP,       |
|                 |                                 |                               |           |             |                     |                                                                                       |               |            |         | d:0.75 ; a:1.53 |                                                            |                              |                                                 | 23.13, P, 5°, PL, RO, CL, OP, (X2),  |
|                 | d:1.03 ; a:1.09                 | 23.45, P, 5°, PL, RO, CT, OP, |           |             |                     |                                                                                       |               |            |         |                 |                                                            |                              |                                                 |                                      |

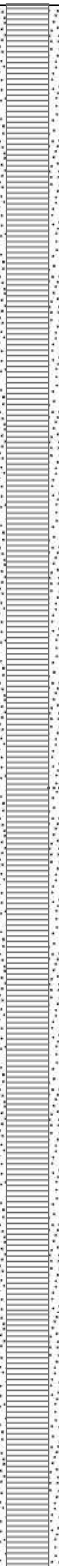
|                       |                                   |                                                                     |
|-----------------------|-----------------------------------|---------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : GEO205 - Comacchio  | Job Number : P3444                                                  |
| Easting : 330797.48   | Driller Supplier : GEONSENSE      | Client : Landmark Group Construction Australia Pty Ltd              |
| Northing : 6261245.34 | Logged By : Ozzie Baskan          | Project : Lindfield                                                 |
| RL : 91.30(m)         | Reviewed By : Mahmoud Jangidaryan | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth : 35.75 m | Date : 26/02/2025                 | Loc Comment : Driveway of 63 Trafalgar Avenue , near the gate.      |

| Drilling Method | Water                | Well Diagram     | Elevation    | Graphic Log | Classification Code | Material Description                                                                                                        | Depth (m) | Weathering | Testing         | Estimated Strength | RQD% and TCR%            | Defect Spacing (mm) | Defect Description            |
|-----------------|----------------------|------------------|--------------|-------------|---------------------|-----------------------------------------------------------------------------------------------------------------------------|-----------|------------|-----------------|--------------------|--------------------------|---------------------|-------------------------------|
|                 |                      |                  | Depth (m)    |             |                     |                                                                                                                             |           |            | Is(50)          |                    |                          |                     |                               |
| NMLC Coring     | Loss - 0% Water Loss | 50mm PVC Slotted |              | SST         | SST                 | Rock SANDSTONE: slightly weathered, high strength, pale grey, fine to coarse grained.                                       |           | SW         |                 |                    | RQD = 100%<br>TCR = 100% |                     | 24.6, P, 5°, UN, RO, CL, OP,  |
|                 |                      |                  |              |             |                     |                                                                                                                             | 25        |            | d:1.28 ; a:1.50 |                    |                          |                     |                               |
|                 |                      |                  |              |             |                     |                                                                                                                             | 26        |            | d:1.45 ; a:1.30 |                    |                          |                     |                               |
|                 |                      |                  |              |             |                     |                                                                                                                             | 26.6      |            | d:0.72 ; a:1.15 |                    | RQD = 100%<br>TCR = 100% |                     |                               |
|                 |                      |                  | 64.7<br>26.6 |             |                     | Rock SANDSTONE: slightly weathered, high strength, grey mottled dark grey, fine to coarse grained, laminations at 0° to 5°. | 26.6      |            |                 |                    |                          |                     |                               |
|                 |                      |                  |              | SST         | SST                 |                                                                                                                             | 27        | SW         | d:0.71 ; a:1.82 |                    |                          |                     | 27.33, P, 5°, PL, RO, CL, OP, |
|                 |                      |                  |              |             |                     |                                                                                                                             |           |            | d:0.43 ; a:1.32 |                    | RQD = 100%<br>TCR = 100% |                     |                               |
|                 | Loss - 0% Water Loss |                  |              |             |                     |                                                                                                                             |           |            |                 |                    |                          |                     | 27.98, P, 5°, PL, RO, CL, OP, |

Loss



|                       |                                   |                                                                     |
|-----------------------|-----------------------------------|---------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : GEO205 - Comacchio  | Job Number : P3444                                                  |
| Easting : 330797.48   | Driller Supplier : GEOSENSE       | Client : Landmark Group Construction Australia Pty Ltd              |
| Northing : 6261245.34 | Logged By : Ozzie Baskan          | Project : Lindfield                                                 |
| RL : 91.30(m)         | Reviewed By : Mahmoud Jangidaryan | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth : 35.75 m | Date : 26/02/2025                 | Loc Comment : Driveway of 63 Trafalgar Avenue , near the gate.      |

| Drilling Method | Water                | Well Diagram                                                                       | Elevation | Graphic Log                                                                        | Classification Code | Material Description                                                                                                 | Depth (m) | Weathering | Testing         |                                               | Estimated Strength       | RQD% and TCR%                                                                        | Defect Spacing (mm)           | Defect Description |
|-----------------|----------------------|------------------------------------------------------------------------------------|-----------|------------------------------------------------------------------------------------|---------------------|----------------------------------------------------------------------------------------------------------------------|-----------|------------|-----------------|-----------------------------------------------|--------------------------|--------------------------------------------------------------------------------------|-------------------------------|--------------------|
|                 |                      |                                                                                    | Depth (m) |                                                                                    |                     |                                                                                                                      |           |            | Is(50)          |                                               |                          |                                                                                      |                               |                    |
|                 |                      |                                                                                    |           |                                                                                    |                     |                                                                                                                      |           |            |                 |                                               |                          |                                                                                      |                               |                    |
| NMLC Coring     | Loss - 0% Water Loss |  | 63.3      |  | SST                 | Rock SANDSTONE: slightly weathered, high strength, grey dark grey, fine to coarse grained, laminations at 5° to 10°. | 28        | SW         |                 | VLS 0.1<br>LS 0.3<br>MS 1.0<br>HS 3<br>EPS 10 | RQD = 100%<br>TCR = 100% |  |                               |                    |
|                 |                      |                                                                                    | 28        |                                                                                    |                     |                                                                                                                      |           |            | d:0.90 ; a:1.05 |                                               |                          |                                                                                      |                               |                    |
|                 |                      |                                                                                    | 62.7      |                                                                                    |                     | As above, but pale grey.                                                                                             | 28.64     |            |                 |                                               | RQD = 100%<br>TCR = 100% |                                                                                      | 28.62, P, 5°, UN, RO, VN, OP, |                    |
|                 |                      |                                                                                    | 28.64     |                                                                                    | SST                 |                                                                                                                      |           |            | d:0.72 ; a:1.30 |                                               |                          |                                                                                      |                               |                    |
|                 |                      |                                                                                    |           |                                                                                    |                     |                                                                                                                      | 29        |            |                 |                                               |                          |                                                                                      |                               |                    |
|                 |                      |                                                                                    |           |                                                                                    |                     |                                                                                                                      | 30        | SW         |                 | d:1.19 ; a:1.37                               |                          |                                                                                      |                               |                    |
|                 |                      |                                                                                    |           |                                                                                    |                     |                                                                                                                      |           |            |                 | d:1.13 ; a:1.22                               |                          |                                                                                      |                               |                    |
|                 |                      |                                                                                    |           |                                                                                    |                     |                                                                                                                      | 31        |            |                 |                                               |                          |                                                                                      |                               |                    |
|                 | Loss - 0% Water      |                                                                                    |           |                                                                                    |                     |                                                                                                                      |           |            | d:1.90 ; a:2.39 |                                               |                          |                                                                                      |                               |                    |

Loss

|                       |                                   |                                                                     |
|-----------------------|-----------------------------------|---------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : GEO205 - Comacchio  | Job Number : P3444                                                  |
| Easting : 330797.48   | Driller Supplier : GEOSENSE       | Client : Landmark Group Construction Australia Pty Ltd              |
| Northing : 6261245.34 | Logged By : Ozzie Baskan          | Project : Lindfield                                                 |
| RL : 91.30(m)         | Reviewed By : Mahmoud Jangidaryan | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth : 35.75 m | Date : 26/02/2025                 | Loc Comment : Driveway of 63 Trafalgar Avenue , near the gate.      |

| Drilling Method            | Water                           | Well Diagram                | Elevation | Graphic Log | Classification Code                                                                   | Material Description               | Depth (m) | Weathering | Testing |                                        | Estimated Strength                                                                                                                                                                                                       | RQD% and TCR%            | Defect Spacing (mm)                             | Defect Description |
|----------------------------|---------------------------------|-----------------------------|-----------|-------------|---------------------------------------------------------------------------------------|------------------------------------|-----------|------------|---------|----------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------|-------------------------------------------------|--------------------|
|                            |                                 |                             | Depth (m) |             |                                                                                       |                                    |           |            | Is(50)  |                                        |                                                                                                                                                                                                                          |                          |                                                 |                    |
| <div>↑ NMLC Coring ↓</div> | <div>Loss - 0% Water Loss</div> | <div>50mm PVC Slotted</div> |           | <div></div> | SST                                                                                   | As above, but pale grey.           |           | SW         |         |                                        | <div>YLS 0.1<br/>LS 0.3<br/>MS 1.0<br/>HS 3<br/>EHS 10</div>                                                                                                                                                             | RQD = 100%<br>TCR = 100% | <div>30<br/>100<br/>300<br/>1000<br/>3000</div> |                    |
|                            |                                 |                             |           |             |                                                                                       |                                    |           |            |         |                                        |                                                                                                                                                                                                                          |                          |                                                 |                    |
|                            |                                 |                             |           |             |                                                                                       |                                    |           |            |         |                                        |                                                                                                                                                                                                                          |                          |                                                 |                    |
|                            |                                 |                             |           |             |                                                                                       |                                    |           |            |         |                                        |                                                                                                                                                                                                                          |                          |                                                 |                    |
|                            |                                 |                             |           |             |                                                                                       |                                    |           |            |         |                                        |                                                                                                                                                                                                                          |                          |                                                 |                    |
|                            |                                 |                             |           |             |                                                                                       |                                    |           |            |         |                                        |                                                                                                                                                                                                                          |                          |                                                 |                    |
|                            |                                 |                             |           |             |                                                                                       |                                    |           |            |         |                                        |                                                                                                                                                                                                                          |                          |                                                 |                    |
|                            |                                 |                             |           |             |                                                                                       |                                    |           |            |         |                                        |                                                                                                                                                                                                                          |                          |                                                 |                    |
|                            |                                 |                             |           |             |                                                                                       |                                    |           |            |         |                                        |                                                                                                                                                                                                                          |                          |                                                 |                    |
|                            |                                 |                             |           |             |                                                                                       |                                    |           |            |         |                                        |                                                                                                                                                                                                                          |                          |                                                 |                    |
|                            |                                 |                             |           |             |                                                                                       |                                    |           |            |         |                                        |                                                                                                                                                                                                                          |                          |                                                 |                    |
|                            |                                 | 56.6<br>34.65               |           | SHA         | Rock SHALE: moderately weathered, medium strength, dark grey, fine grained.           | 34.65                              | MW        |            |         | <div>RQD = 96.84%<br/>TCR = 100%</div> | <div>34.29-34.32, CRF, 5°,<br/><br/>34.77-34.8, CRF, 5°,<br/><br/>34.91, J, 40°, UN, SO, CL, OP,<br/><br/>35.2, P, 30°, PL, SO, CL, OP,<br/><br/>35.43, P, 10°, PL, RO, CL, OP,<br/>35.49, P, 20°, PL, RO, CL, OP,</div> |                          |                                                 |                    |
|                            |                                 |                             |           |             |                                                                                       |                                    |           |            |         |                                        |                                                                                                                                                                                                                          |                          |                                                 |                    |
|                            |                                 |                             |           |             |                                                                                       |                                    |           |            |         |                                        |                                                                                                                                                                                                                          |                          |                                                 |                    |
|                            |                                 |                             |           |             |                                                                                       |                                    |           |            |         |                                        |                                                                                                                                                                                                                          |                          |                                                 |                    |
|                            |                                 |                             |           |             |                                                                                       |                                    |           |            |         |                                        |                                                                                                                                                                                                                          |                          |                                                 |                    |
|                            |                                 |                             |           |             |                                                                                       |                                    |           |            |         |                                        |                                                                                                                                                                                                                          |                          |                                                 |                    |
|                            |                                 |                             |           |             |                                                                                       |                                    |           |            |         |                                        |                                                                                                                                                                                                                          |                          |                                                 |                    |
|                            |                                 |                             |           |             |                                                                                       |                                    |           |            |         |                                        |                                                                                                                                                                                                                          |                          |                                                 |                    |
|                            |                                 |                             |           |             |                                                                                       |                                    |           |            |         |                                        |                                                                                                                                                                                                                          |                          |                                                 |                    |
|                            |                                 |                             |           |             |                                                                                       |                                    |           |            |         |                                        |                                                                                                                                                                                                                          |                          |                                                 |                    |
|                            |                                 |                             |           |             |                                                                                       |                                    |           |            |         |                                        |                                                                                                                                                                                                                          |                          |                                                 |                    |
|                            |                                 | 55.9<br>35.43               |           | SST         | Rock SANDSTONE: slightly weathered, high strength, pale grey, fine to coarse grained. | 35.43                              | SW        |            |         |                                        |                                                                                                                                                                                                                          |                          |                                                 |                    |
|                            |                                 |                             |           |             |                                                                                       |                                    |           |            |         |                                        |                                                                                                                                                                                                                          |                          |                                                 |                    |
|                            |                                 |                             |           |             |                                                                                       | BH1 Reached Target Depth at 35.75m |           |            |         |                                        |                                                                                                                                                                                                                          |                          |                                                 |                    |

# morrow

CLIENT NAME: LANDMARK

PROJECT:

LOCATION: 63 Trafalgar Ave, Lindfield

JOB NUMBER: P3444

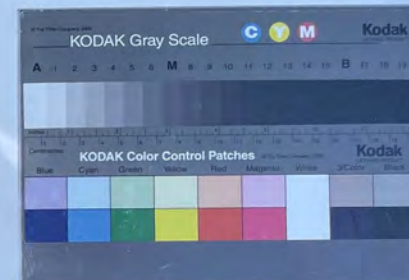
LOGGED BY: Ozzie B.

BOREHOLE ID: BH1

DEPTH: 4.7m to 9.0m

CORE TRAY NO: 1 of 7

DATE: 26/02/2025



# morrow



02 8599 7579



Sydney Gadigal Land,  
2/5-7 Malta Street, Fairfield  
East NSW 2155



info@morrowgeo.com.au

## Photo description

Box 1 of 7

|              |                                                          |          |              |
|--------------|----------------------------------------------------------|----------|--------------|
| Client       | Landmark Group Construction Australia Pty Ltd            |          |              |
| Location     | 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |          |              |
| Project name | Lindfield                                                |          |              |
| Project No   | P3444                                                    | Scale    | Not to Scale |
| BH No        | BH1                                                      | BH Depth | CorePhoto    |



# morrow

CLIENT NAME: LANDMARK

PROJECT:

LOCATION: 63 Trafalgar Ave, Lindfield

JOB NUMBER: P3444

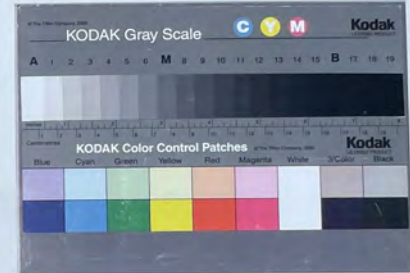
LOGGED BY: Ozzie B.

BOREHOLE ID: BH1

DEPTH: 3.0m to 14.0m

CORE TRAY NO: 2 of 7

DATE: 27/02/2025



# morrow



02 8599 7579



Sydney Gadigal Land,  
2/5-7 Malta Street, Fairfield  
East NSW 2155



info@morrowgeo.com.au

## Photo description

Box 2 of 7

## Client

Landmark Group Construction Australia Pty Ltd

## Location

59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW

## Project name

Lindfield

## Project No

P3444

## Scale

Not to Scale

## BH No

BH1

## BH Depth

CorePhoto

# morrow

CLIENT NAME: LANDMARK

PROJECT:

LOCATION: 63 Trafalgar Ave, Lindfield

JOB NUMBER: P3444

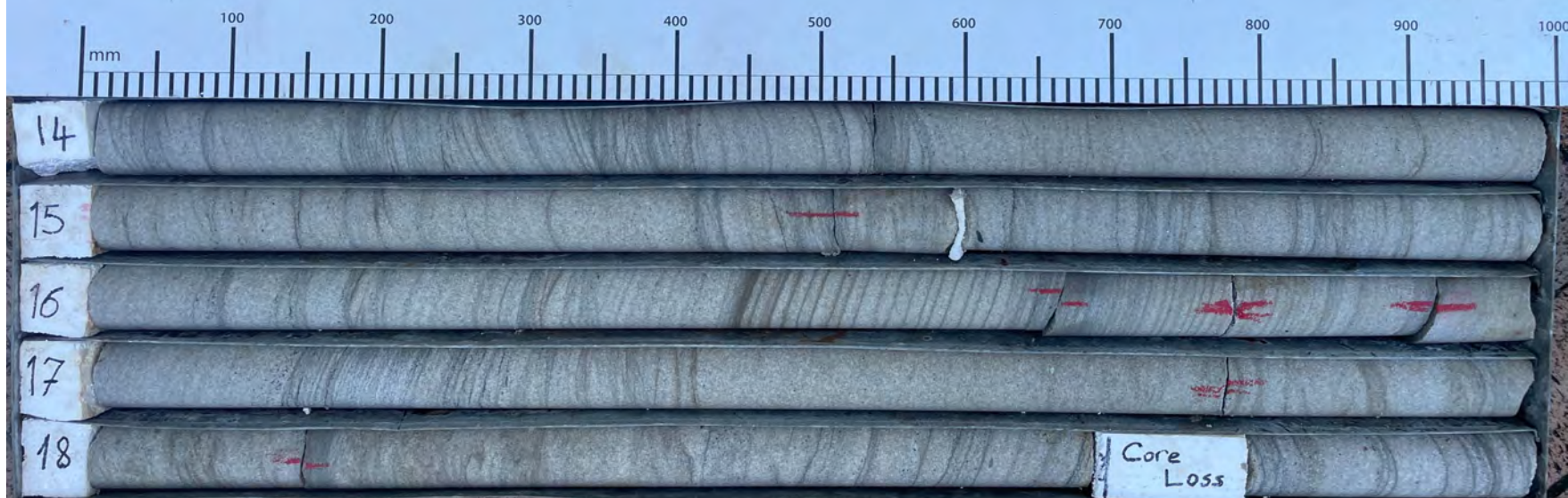
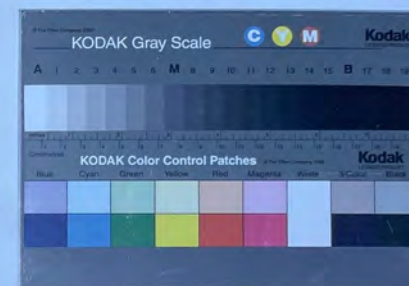
LOGGED BY: Ozzie B.

BOREHOLE ID: BH1

DEPTH: 14.0m to 19.0m

CORE TRAY NO: 3 of 7

DATE: 27/02/2025



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Sydney Gadigal Land,  
2/5-7 Malta Street, Fairfield  
East NSW 2155



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## Photo description

Box 3 of 7

## Client

Landmark Group Construction Australia Pty Ltd

## Location

59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW

## Project name

Lindfield

## Project No

P3444

## Scale

Not to Scale

## BH No

BH1

## BH Depth

CorePhoto



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CLIENT NAME: LANDMARK

PROJECT:

LOCATION: 63 Trafalgar Ave, Lindfield

JOB NUMBER: P3444

LOGGED BY: Ozzie B.

BOREHOLE ID: BH1

DEPTH: 13m to 24m

CORE TRAY N 4 of 7

DATE: 27/02/2025



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Sydney Gadigal Land,  
2/5-7 Malta Street, Fairfield  
East NSW 2155



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## Photo description

Box 4 of 7

## Client

Landmark Group Construction Australia Pty Ltd

## Location

59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW

## Project name

Lindfield

## Project No

P3444

## Scale

Not to Scale

## BH No

BH1

## BH Depth

CorePhoto

# morrow

CLIENT NAME: LANDMARK

PROJECT:

LOCATION: 63 Trafalgar Ave, Lindfield

JOB NUMBER: P3444

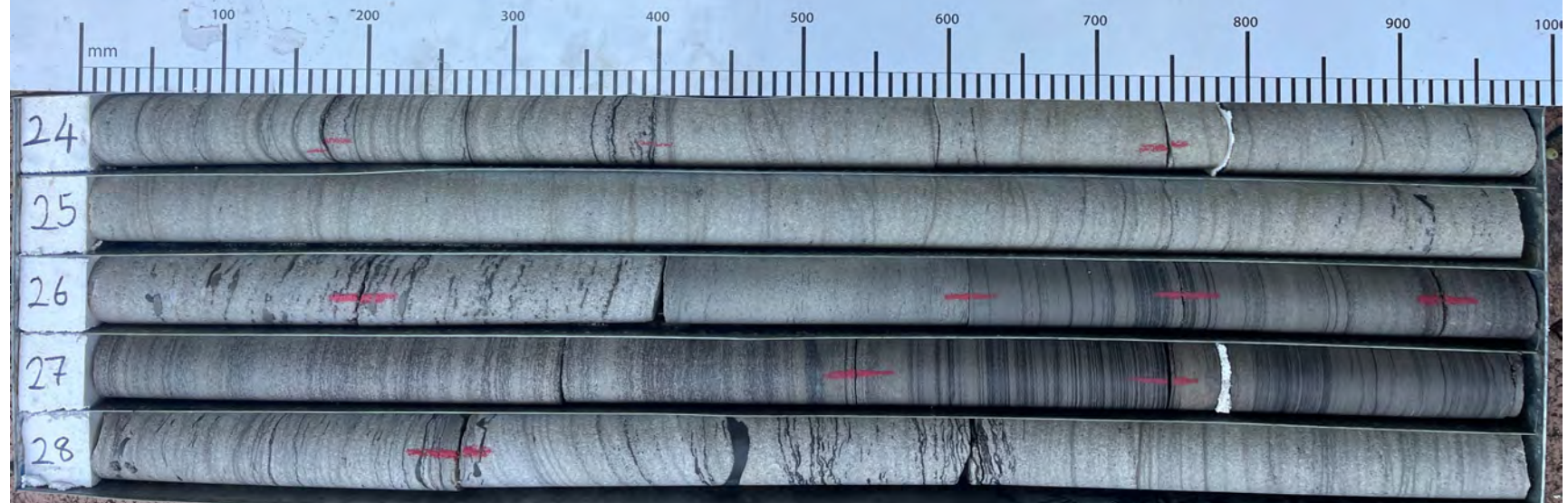
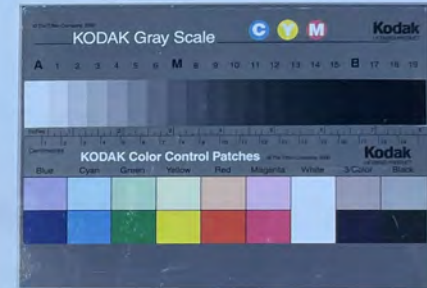
LOGGED BY: Ozzie B.

BOREHOLE ID: BH1

DEPTH: 24m to 29m

CORE TRAY N° 5 of 7

DATE: 27/02/2025



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Sydney Gadigal Land,  
2/5-7 Malta Street, Fairfield  
East NSW 2155



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## Photo description

Box 5 of 7

## Client

Landmark Group Construction Australia Pty Ltd

## Location

59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW

## Project name

Lindfield

## Project No

P3444

## Scale

Not to Scale

## BH No

BH1

## BH Depth

CorePhoto



# morrow

CLIENT NAME: LANDMARK

PROJECT:

LOCATION: 63 Trafalgar Ave, Lindfield

JOB NUMBER: P3444

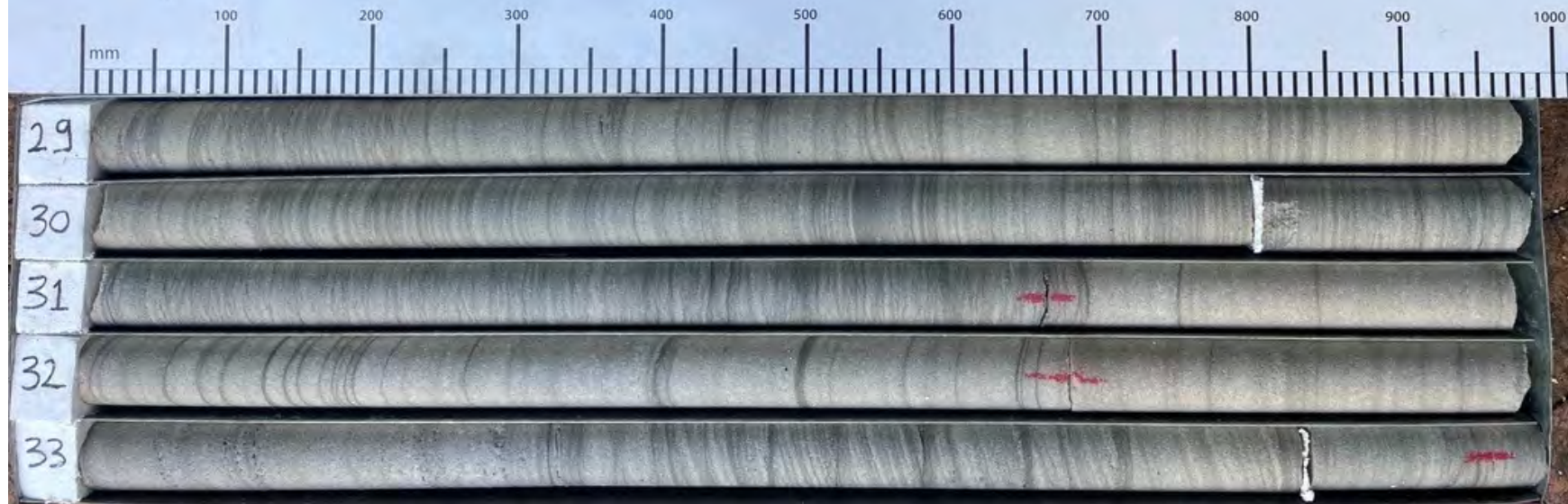
LOGGED BY: Ozzie B.

BOREHOLE ID: BH1

DEPTH: 29m to 34m

CORE TRAY NO: 6 of 7

DATE: 27/02/2025



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Sydney Gadigal Land,  
2/5-7 Malta Street, Fairfield  
East NSW 2155



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## Photo description

Box 6 of 7

## Client

Landmark Group Construction Australia Pty Ltd

## Location

59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW

## Project name

Lindfield

## Project No

P3444

## Scale

Not to Scale

## BH No

BH1

## BH Depth

CorePhoto

# morrow

CLIENT NAME: LANDMARK

PROJECT:

LOCATION: 63 Trafalgar Ave, Lindfield

JOB NUMBER: P3444

LOGGED BY: Ozzie B.

BOREHOLE ID: BH1

DEPTH: 34m to 35.75m

CORE TRAY N 7 of 7

DATE: 27/02/2025



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Sydney Gadigal Land,  
2/5-7 Malta Street, Fairfield  
East NSW 2155



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## Photo description

Box 7 of 7

## Client

Landmark Group Construction Australia Pty Ltd

## Location

59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW

## Project name

Lindfield

## Project No

P3444

## Scale

Not to Scale

## BH No

BH1

## BH Depth

CorePhoto

|                                                                                                                                       |                                                                                                                                                                                          |                                                                                                                                                                                                                                                                                  |
|---------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| <b>UTM</b> : 56S<br><b>Easting</b> : 330881,21<br><b>Northing</b> : 6261255,66<br><b>RL</b> : 85,40(m)<br><b>Total Depth</b> : 20,5 m | <b>Driller Rig</b> : GEO205 - Comacchio<br><b>Driller Supplier</b> : GEOSENSE<br><b>Logged By</b> : Mahmoud Jangidaryan<br><b>Reviewed By</b> : Ozzie Baskan<br><b>Date</b> : 14/02/2025 | <b>Job Number</b> : P3444<br><b>Client</b> : Landmark Group Construction Australia Pty Ltd<br><b>Project</b> : Lindfield<br><b>Location</b> : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW<br><b>Loc Comment</b> : Driveway of 1A Valley Road, across from the pool. |
|---------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|

| Drilling Method    | Water   | Well Diagram | Testing            | Elevation<br>Depth (m) | Graphic Log | Material Type | Classification Code | Material Description                                                                                                                                                             | Depth (m) | Consistency | Weathering | Moisture |
|--------------------|---------|--------------|--------------------|------------------------|-------------|---------------|---------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------|-------------|------------|----------|
|                    |         |              | SPT                |                        |             |               |                     |                                                                                                                                                                                  |           |             |            |          |
| Diatube<br>↑ ADT ↓ | 1, GWNE |              |                    | 85.3                   |             | Non-Soil      | CCT                 | Concrete                                                                                                                                                                         | 0.13      |             |            |          |
|                    |         |              |                    | 0.13                   |             | FILL          | SP                  | FILL Gravelly SAND loose, dark grey, fine grained, fine to medium sized gravel, moist.                                                                                           |           | L           |            | M        |
|                    |         |              | 3,3,3<br>(N=6)     | 84.7<br>0.7            |             | Residual      | CI                  | Residual Gravelly to sandy CLAY firm to stiff, medium plasticity, fine sized gravel, inorganic, ironstone gravels.                                                               | 0.7       | F-St        |            |          |
|                    |         |              |                    | 84.4<br>1              |             | Rock          | SST                 | Extremely weathered Sandstone, Gravelly SAND very dense, pale grey with orange, fine grained, fine to medium sized gravel, trace low plasticity clay, trace low plasticity silt. | 1         | VD-WC       | XW         | D        |
|                    |         |              | 0mm,0/mm<br>(N=23) | 83.7<br>1.75           |             |               |                     |                                                                                                                                                                                  | 1.75      |             |            |          |
|                    |         |              |                    |                        |             |               |                     | Commenced Coring at 1.75m                                                                                                                                                        |           |             |            |          |



|                       |                                  |                                                                     |
|-----------------------|----------------------------------|---------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : GEO205 - Comacchio | Job Number : P3444                                                  |
| Easting : 330881.21   | Driller Supplier : GEOSENSE      | Client : Landmark Group Construction Australia Pty Ltd              |
| Northing : 6261255.66 | Logged By : Mahmoud Jangidaryan  | Project : Lindfield                                                 |
| RL : 85.40(m)         | Reviewed By : Ozzie Baskan       | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth : 20.5 m  | Date : 14/02/2025                | Loc Comment : Driveway of 1A Valley Road, across from the pool.     |

| Drilling Method | Water | Well Diagram | Elevation    | Graphic Log | Classification Code | Material Description                                                                                      | Depth (m) | Weathering | Testing | Estimated Strength                                       | RQD% and TCR%             | Defect Spacing (mm)              | Defect Description                                                                                                    |
|-----------------|-------|--------------|--------------|-------------|---------------------|-----------------------------------------------------------------------------------------------------------|-----------|------------|---------|----------------------------------------------------------|---------------------------|----------------------------------|-----------------------------------------------------------------------------------------------------------------------|
|                 |       |              | Depth (m)    |             |                     |                                                                                                           |           |            | Is(50)  |                                                          |                           |                                  |                                                                                                                       |
|                 |       | A            |              |             |                     |                                                                                                           |           |            |         | VLS 0.03<br>LS 0.1<br>MS 0.3<br>HS 0.5<br>FHS 1<br>FHS 3 |                           | 90<br>100<br>300<br>1000<br>3000 |                                                                                                                       |
|                 |       |              |              |             |                     | Commenced Coring at 1.75m                                                                                 |           |            |         |                                                          |                           |                                  |                                                                                                                       |
|                 |       |              |              |             |                     | Coreloss                                                                                                  |           |            |         |                                                          |                           |                                  | 1.75-2.38, CORELOSS,                                                                                                  |
|                 |       |              |              |             | CRL                 |                                                                                                           | 2         |            |         |                                                          |                           |                                  |                                                                                                                       |
|                 |       |              | 83.0<br>2.4  |             |                     | Rock SANDSTONE: highly weathered, very low strength, pale grey orange red, fine grained, ironstone bands. | 2.4       |            |         |                                                          | RQD = 0%<br>TCR = 53.33%  |                                  | 2.38-3.1, XWS,                                                                                                        |
|                 |       |              |              |             | SST                 |                                                                                                           | 3         |            |         |                                                          |                           |                                  | 3.13, P, 5°, PL, RO,<br>3.16, P, 5°, PL, RO,<br>3.24, P, 5°, PL, RO,<br>3.42, P, 5°, PL, SO,<br>3.51, P, 25°, PL, SO, |
|                 |       |              | 81.6<br>3.77 |             |                     |                                                                                                           | 3.77      |            |         |                                                          | RQD = 15%<br>TCR = 59.17% |                                  | 3.77-4.45, CORELOSS,                                                                                                  |
|                 |       |              |              |             | CRL                 | Coreloss                                                                                                  |           |            |         |                                                          |                           |                                  |                                                                                                                       |

|                       |                                  |                                                                     |
|-----------------------|----------------------------------|---------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : GEO205 - Comacchio | Job Number : P3444                                                  |
| Easting : 330881.21   | Driller Supplier : GEOSENSE      | Client : Landmark Group Construction Australia Pty Ltd              |
| Northing : 6261255.66 | Logged By : Mahmoud Jangidaryan  | Project : Lindfield                                                 |
| RL : 85.40(m)         | Reviewed By : Ozzie Baskan       | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth : 20.5 m  | Date : 14/02/2025                | Loc Comment : Driveway of 1A Valley Road, across from the pool.     |

| Drilling Method | Water                 | Well Diagram     | Elevation | Graphic Log | Classification Code | Material Description                                                                                                                        | Depth (m) | Weathering | Testing         | Estimated Strength | RQD% and TCR%             | Defect Spacing (mm) | Defect Description                                                                 |
|-----------------|-----------------------|------------------|-----------|-------------|---------------------|---------------------------------------------------------------------------------------------------------------------------------------------|-----------|------------|-----------------|--------------------|---------------------------|---------------------|------------------------------------------------------------------------------------|
|                 |                       |                  | Depth (m) |             |                     |                                                                                                                                             |           |            | Is(50)          |                    |                           |                     |                                                                                    |
| NMLC Coring     | Loss - 20% Water Loss | 50mm PVC Solid   | 81.0      |             | CRL                 | Coreloss                                                                                                                                    | 4.45      | HW         |                 |                    | RQD = 15%<br>TCR = 59.17% |                     | 4.45-4.8, XWS,                                                                     |
|                 |                       |                  | 4.45      |             |                     | Rock SANDSTONE: highly weathered, very low strength, pale grey orange red, fine grained.                                                    | 5         |            | d:0.06 ; a:0.04 |                    |                           |                     | 5.05-5.15, J, 80°, PL, RO,                                                         |
| NMLC Coring     | Loss - 20% Water Loss | 50mm PVC Slotted | 80.3      |             | SST                 | Rock SANDSTONE: highly weathered, very low to low strength, pale grey with red, very fine grained.                                          | 5.1       | HW         | d:0.27 ; a:1.12 |                    | RQD = 74%<br>TCR = 100%   |                     | 5.28, P, 10°, CV, RO,<br>5.32-5.63, CRF, RO,                                       |
|                 |                       |                  | 79.4      |             |                     | Rock SANDSTONE: moderately to slightly weathered, medium strength, pale grey with grey and brown, very fine grained, carbonaceous beddings. | 6         |            | d:0.04 ; a:0.47 |                    |                           |                     | 5.86, P, 10°, RO,<br>5.91-5.95, CS,                                                |
| NMLC Coring     | Loss - 20% Water Loss | 50mm PVC Slotted | 79.4      |             | SST                 | Rock SANDSTONE: moderately to slightly weathered, medium strength, pale grey with grey and brown, very fine grained, carbonaceous beddings. | 6         | MW-SW      | d:0.64 ; a:1.41 |                    | RQD = 74%<br>TCR = 100%   |                     | 6.15, P, 15°, IR, VR,<br>6.26, P, 20°, PL, RO, CL, ,<br>6.3, P, 20°, PL, RO, CL, , |
|                 |                       |                  | 7         |             |                     |                                                                                                                                             | 7         |            | d:0.81 ; a:0.93 |                    |                           |                     | 6.66, J, 50°, PL, RO,<br>6.73, J, 50°, PL, RO,<br>6.77, J, 50°, PL, RO,            |
| NMLC Coring     | Loss - 20% Water Loss | 50mm PVC Slotted | 7         |             | SST                 |                                                                                                                                             | 7         | MW-SW      | d:1.39 ; a:1.09 |                    | RQD = 74%<br>TCR = 100%   |                     | 7.72, P, 20°, IR, RO, CL, ,<br>7.77, P, 5°, PL, RO,                                |
|                 |                       |                  |           |             |                     |                                                                                                                                             |           |            |                 |                    |                           |                     | 7.93, P, 5°, PL, RO,                                                               |

|                       |                                  |                                                                     |
|-----------------------|----------------------------------|---------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : GEO205 - Comacchio | Job Number : P3444                                                  |
| Easting : 330881.21   | Driller Supplier : GEOSENSE      | Client : Landmark Group Construction Australia Pty Ltd              |
| Northing : 6261255.66 | Logged By : Mahmoud Jangidaryan  | Project : Lindfield                                                 |
| RL : 85.40(m)         | Reviewed By : Ozzie Baskan       | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth : 20.5 m  | Date : 14/02/2025                | Loc Comment : Driveway of 1A Valley Road, across from the pool.     |

| Drilling Method | Water | Well Diagram | Elevation | Graphic Log | Classification Code | Material Description                                                                                                                        | Depth (m) | Weathering | Testing         | Estimated Strength                                       | RQD% and TCR%                                       | Defect Spacing (mm)              | Defect Description     |
|-----------------|-------|--------------|-----------|-------------|---------------------|---------------------------------------------------------------------------------------------------------------------------------------------|-----------|------------|-----------------|----------------------------------------------------------|-----------------------------------------------------|----------------------------------|------------------------|
|                 |       |              | Depth (m) |             |                     |                                                                                                                                             |           |            | Is(50)          |                                                          |                                                     |                                  |                        |
|                 |       |              | 76.4      |             | SST                 | Rock SANDSTONE: moderately to slightly weathered, medium strength, pale grey with grey and brown, very fine grained, carbonaceous beddings. | 9.9       | MW-SW      | d:0.60 ; a:0.85 | VLS 0.03<br>LS 0.1<br>MS 0.3<br>HS 0.3<br>EPS 1<br>EPS 3 | RQD = 74%<br>TCR = 100%<br>RQD = 100%<br>TCR = 100% | 30<br>100<br>300<br>1000<br>3000 |                        |
|                 |       |              | 9         |             | SST                 | Rock SANDSTONE: fresh weathered, high strength, pale grey grey, fine grained, with carbonaceous beddings..                                  | 10        | F          | d:1.26 ; a:1.47 |                                                          |                                                     |                                  | 9.53, P, 10°, PL, RO,  |
|                 |       |              |           |             |                     |                                                                                                                                             | 11        |            | d:1.12 ; a:0.90 |                                                          |                                                     |                                  | 9.76, P, 10°, PL, RO,  |
|                 |       |              |           |             |                     |                                                                                                                                             |           |            | d:1.10 ; a:1.04 |                                                          |                                                     |                                  | 9.89, P, 10°, PL, RO,  |
|                 |       |              |           |             |                     |                                                                                                                                             |           |            |                 |                                                          | RQD = 100%<br>TCR = 100%                            |                                  | 11.07, P, 10°, PL, RO, |

|                       |                                  |                                                                     |
|-----------------------|----------------------------------|---------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : GEO205 - Comacchio | Job Number : P3444                                                  |
| Easting : 330881.21   | Driller Supplier : GEOSENSE      | Client : Landmark Group Construction Australia Pty Ltd              |
| Northing : 6261255.66 | Logged By : Mahmoud Jangidaryan  | Project : Lindfield                                                 |
| RL : 85.40(m)         | Reviewed By : Ozzie Baskan       | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth : 20.5 m  | Date : 14/02/2025                | Loc Comment : Driveway of 1A Valley Road, across from the pool.     |

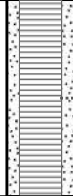
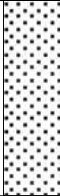
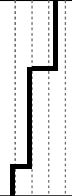
| Drilling Method | Water                 | Well Diagram     | Elevation | Graphic Log | Classification Code | Material Description                                                                                       | Depth (m) | Weathering | Testing         | Estimated Strength                                       | RQD% and TCR%            | Defect Spacing (mm)              | Defect Description                                                                                |
|-----------------|-----------------------|------------------|-----------|-------------|---------------------|------------------------------------------------------------------------------------------------------------|-----------|------------|-----------------|----------------------------------------------------------|--------------------------|----------------------------------|---------------------------------------------------------------------------------------------------|
|                 |                       |                  | Depth (m) |             |                     |                                                                                                            |           |            | Is(50)          |                                                          |                          |                                  |                                                                                                   |
| NMLC Coring     | Loss - 10% Water Loss | 50mm PVC Slotted |           |             | SST                 | Rock SANDSTONE: fresh weathered, high strength, pale grey grey, fine grained, with carbonaceous beddings.. | 13        | F          | d:0.92; a:1.60  | VLS 0.03<br>LS 0.1<br>MS 0.1<br>HS 0.3<br>EPS 1<br>EPS 3 | RQD = 100%<br>TCR = 100% | 30<br>100<br>300<br>1000<br>3000 | 12.63, P, 20°, PL, RO,                                                                            |
|                 |                       |                  |           |             |                     |                                                                                                            |           |            | d:1.47 ; a:1.50 |                                                          |                          |                                  |                                                                                                   |
|                 |                       |                  |           |             |                     |                                                                                                            | 14        |            | d:1.99 ; a:1.72 |                                                          |                          |                                  |                                                                                                   |
|                 |                       |                  |           |             |                     |                                                                                                            |           |            | d:1.54 ; a:1.80 |                                                          |                          |                                  |                                                                                                   |
|                 |                       |                  |           |             |                     |                                                                                                            | 15        |            | d:1.93 ; a:2.38 |                                                          |                          |                                  | 15.62, P, 10°, UN, RO,<br>15.67, P, 5°, PL, RO,<br>15.71, P, 5°, PL, RO,<br>15.81, P, 5°, PL, RO, |
|                 |                       |                  |           |             |                     |                                                                                                            |           |            |                 |                                                          |                          |                                  |                                                                                                   |



|                       |                                  |                                                                     |
|-----------------------|----------------------------------|---------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : GEO205 - Comacchio | Job Number : P3444                                                  |
| Easting : 330881.21   | Driller Supplier : GEOSENSE      | Client : Landmark Group Construction Australia Pty Ltd              |
| Northing : 6261255.66 | Logged By : Mahmoud Jangidaryan  | Project : Lindfield                                                 |
| RL : 85.40(m)         | Reviewed By : Ozzie Baskan       | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth : 20.5 m  | Date : 14/02/2025                | Loc Comment : Driveway of 1A Valley Road, across from the pool.     |

| Drilling Method | Water                 | Well Diagram     | Elevation<br>Depth (m) | Graphic Log | Classification Code | Material Description                                                                                       | Depth (m) | Weathering | Testing         |                                                          | Estimated Strength | RQD% and TCR% | Defect Spacing (mm) | Defect Description                              |
|-----------------|-----------------------|------------------|------------------------|-------------|---------------------|------------------------------------------------------------------------------------------------------------|-----------|------------|-----------------|----------------------------------------------------------|--------------------|---------------|---------------------|-------------------------------------------------|
|                 |                       |                  |                        |             |                     |                                                                                                            |           |            | Is(50)          |                                                          |                    |               |                     |                                                 |
| NMLC Coring     | Loss - 10% Water Loss | 50mm PVC Slotted |                        |             | SST                 | Rock SANDSTONE: fresh weathered, high strength, pale grey grey, fine grained, with carbonaceous beddings.. | 17        | F          | d:2.10 ; a:2.36 | VLS 0.03<br>LS 0.1<br>MS 0.3<br>HS 0.3<br>EPS 1<br>EPS 3 |                    |               |                     | 16.9, J, 30°, PL, RO,                           |
|                 |                       |                  |                        |             |                     |                                                                                                            |           |            | d:1.88 ; a:1.61 |                                                          |                    |               |                     |                                                 |
|                 |                       |                  |                        |             |                     |                                                                                                            | 18        |            | d:2.13 ; a:1.78 |                                                          |                    |               |                     | 17.9, P, PL, VR,                                |
|                 |                       |                  |                        |             |                     |                                                                                                            |           |            | d:1.61 ; a:1.35 |                                                          |                    |               |                     |                                                 |
|                 |                       |                  |                        |             |                     |                                                                                                            | 19        |            |                 |                                                          |                    |               |                     | 18.52, P, 5°, PL, VR,<br>18.61, P, 10°, PL, VR, |
|                 |                       |                  |                        |             |                     |                                                                                                            |           |            |                 |                                                          |                    |               |                     |                                                 |

|                       |                                  |                                                                     |
|-----------------------|----------------------------------|---------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : GEO205 - Comacchio | Job Number : P3444                                                  |
| Easting : 330881.21   | Driller Supplier : GEOSENSE      | Client : Landmark Group Construction Australia Pty Ltd              |
| Northing : 6261255.66 | Logged By : Mahmoud Jangidaryan  | Project : Lindfield                                                 |
| RL : 85.40(m)         | Reviewed By : Ozzie Baskan       | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth : 20.5 m  | Date : 14/02/2025                | Loc Comment : Driveway of 1A Valley Road, across from the pool.     |

| Drilling Method                   | Water | Well Diagram                                                                      | Elevation | Graphic Log                                                                       | Classification Code | Material Description                                                                                       | Depth (m) | Weathering | Testing         |  | Estimated Strength                                                                  | RQD% and TCR% | Defect Spacing (mm)                                                                 | Defect Description                                  |
|-----------------------------------|-------|-----------------------------------------------------------------------------------|-----------|-----------------------------------------------------------------------------------|---------------------|------------------------------------------------------------------------------------------------------------|-----------|------------|-----------------|--|-------------------------------------------------------------------------------------|---------------|-------------------------------------------------------------------------------------|-----------------------------------------------------|
|                                   |       |                                                                                   | Depth (m) |                                                                                   |                     |                                                                                                            |           |            | Is(50)          |  |                                                                                     |               |                                                                                     |                                                     |
| NMLC Coring                       |       |  |           |  | SST                 | Rock SANDSTONE: fresh weathered, high strength, pale grey grey, fine grained, with carbonaceous beddings.. |           | F          |                 |  |  |               |  | 20.17, P, 10°, UN, VR,<br><br>20.42, P, 5°, PL, RO, |
|                                   |       |                                                                                   |           |                                                                                   |                     |                                                                                                            |           |            | d:1.34 ; a:1.71 |  |                                                                                     |               |                                                                                     |                                                     |
| BH2 Reached Target Depth at 20.5m |       |                                                                                   |           |                                                                                   |                     |                                                                                                            |           |            |                 |  |                                                                                     |               |                                                                                     |                                                     |

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CLIENT NAME: Landmark Group

PROJECT: Lindfield

LOCATION: 1A Valley Road

JOB NUMBER: P3444

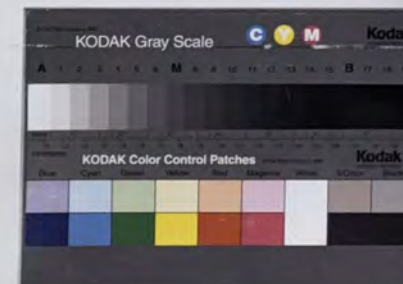
LOGGED BY: MJ

BOREHOLE ID: BH2

DEPTH: 1.75 to 6.0 m

CORE TRAY NO: Box 1 of 4

DATE: 14,2,2025



# morrow



02 8599 7579



Sydney Gadigal Land,  
2/5-7 Malta Street, Fairfield  
East NSW 2155



info@morrowgeo.com.au

## Photo description

Box 1 of 4

## Client

Landmark Group Construction Australia Pty Ltd

## Location

59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW

## Project name

Lindfield

## Project No

P3444

## Scale

Not to Scale

## BH No

BH2

## BH Depth

CorePhoto



# morrow

CLIENT NAME: Landmark Group

PROJECT: Lindfield

LOCATION: 1A Valley Road

JOB NUMBER: P3444

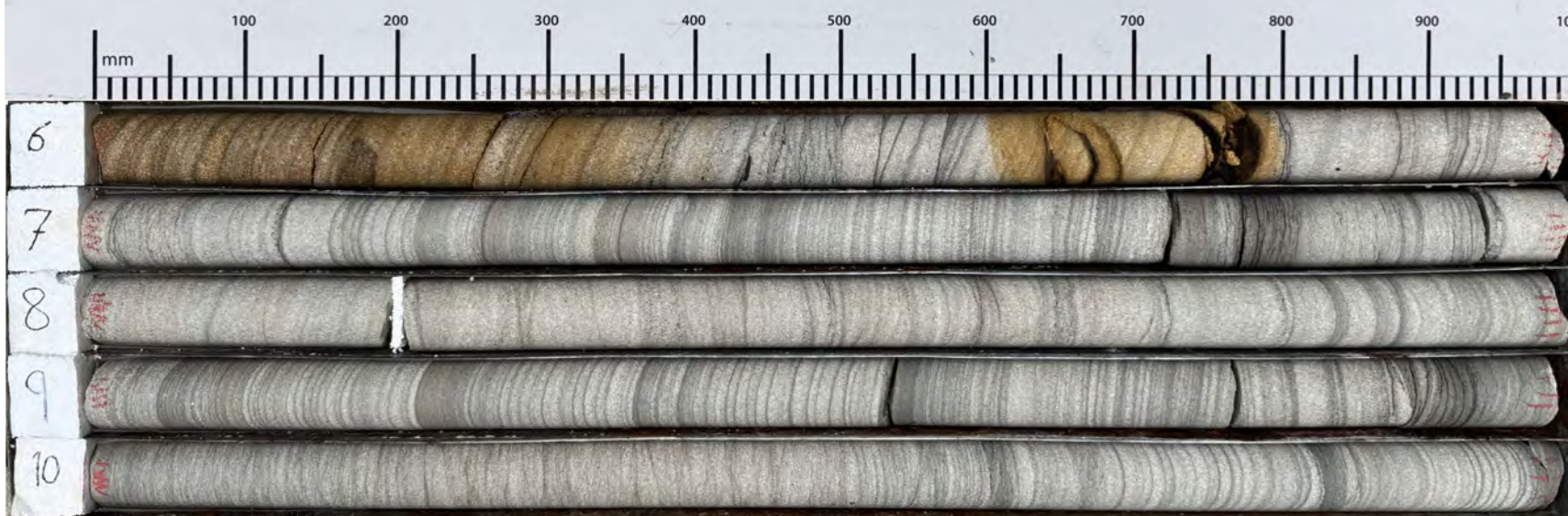
LOGGED BY: MJ

BOREHOLE ID: BH2

DEPTH: 6.0 to 11.0 m

CORE TRAY NO: Box 2 of 4

DATE: 14, 2, 2025



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Sydney Gadigal Land,  
2/5-7 Malta Street, Fairfield  
East NSW 2155



info@morrowgeo.com.au

## Photo description

Box 2 of 4

|              |                                                          |          |              |
|--------------|----------------------------------------------------------|----------|--------------|
| Client       | Landmark Group Construction Australia Pty Ltd            |          |              |
| Location     | 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |          |              |
| Project name | Lindfield                                                |          |              |
| Project No   | P3444                                                    | Scale    | Not to Scale |
| BH No        | BH2                                                      | BH Depth | CorePhoto    |

# morrow

CLIENT NAME: Landmark Group

PROJECT: Lindfield

LOCATION: 1A Valley Road

JOB NUMBER: P3444

LOGGED BY: MJ

BOREHOLE ID: BH2

DEPTH: 11.0 to 16.0 m

CORE TRAY NO: Box 3 of 4

DATE: 14,2,2025



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Sydney Gadigal Land,  
2/5-7 Malta Street, Fairfield  
East NSW 2155



info@morrowgeo.com.au

## Photo description

Box 3 of 4

## Client

Landmark Group Construction Australia Pty Ltd

## Location

59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW

## Project name

Lindfield

## Project No

P3444

## Scale

Not to Scale

## BH No

BH2

## BH Depth

CorePhoto





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02 8599 7579



Sydney Gadigal Land,  
2/5-7 Malta Street, Fairfield  
East NSW 2155



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#### Photo description

Box 4 of 4

#### Client

Landmark Group Construction Australia Pty Ltd

#### Location

59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW

#### Project name

Lindfield

#### Project No

P3444

#### Scale

Not to Scale

#### BH No

BH2

#### BH Depth

CorePhoto

|                       |                                 |                                                                                |
|-----------------------|---------------------------------|--------------------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : Man Portable      | Job Number : P3444                                                             |
| Easting : 330840,02   | Driller Supplier : TIGHT Site   | Client : Landmark Group Construction Australia Pty Ltd                         |
| Northing : 6261235,97 | Logged By : Mahmoud Jangidaryan | Project : Lindfield                                                            |
| RL : 87.50(m)         | Reviewed By : Ozzie Baskan      | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW            |
| Total Depth : 20.4 m  | Date : 11/02/2025               | Loc Comment : North-eastern corner of the tennis court at 63 Trafalgar Avenue. |

| Drilling Method | Water | Testing | Elevation<br>Depth (m) | Material Type | Graphic Log                                                                       | Classification Code | Material Description                                                                                                                                                            | Depth (m)   | Consistency | Weathering | Moisture |
|-----------------|-------|---------|------------------------|---------------|-----------------------------------------------------------------------------------|---------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------|-------------|------------|----------|
| Hand Auger      |       |         | 87.4<br>0.08           | Non-Soil      |  | CCT                 | Concrete                                                                                                                                                                        | 0.08        |             |            |          |
|                 |       |         | 87.2<br>0.3            | FILL          |  | CL                  | FILL Gravelly to sandy CLAY low plasticity, stiff, orange pale grey, fine to medium sized gravel, fine grained sand, trace low plasticity silt, inorganic, w < pl.              | 0.3         | St          |            | w < PL   |
|                 |       |         | 87.0<br>0.45           | Residual      |  | CH                  | Residual Silty CLAY stiff to very stiff, high plasticity, pale grey with red, inorganic, trace of ironstone gravels.                                                            | 0.45        | St-VSt      |            |          |
|                 |       |         | 86.9<br>0.6            | Rock          |  | SST                 | Extremely weathered Sandstone, Gravelly SAND very dense, pale grey orange red, fine to medium grained, fine sized gravel, trace low plasticity clay, trace low plasticity silt. | 0.50<br>0.6 | VD-PC-MC    | XW         | M        |
|                 |       |         |                        |               |                                                                                   |                     | Commenced Coring at 0.6m                                                                                                                                                        |             |             |            |          |

| Drilling Method | Water         | Depth (m)                        | Elevation (m) | Graphic Log | Classification Code                                                                                                                                   | Material Description        | Depth (m) | Weathering      | Testing                | Estimated Strength | RQD% and TCR% | Defect Spacing (mm) | Defect Description<br>type, inclination, planarity, roughness, coating, thickness |
|-----------------|---------------|----------------------------------|---------------|-------------|-------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------|-----------|-----------------|------------------------|--------------------|---------------|---------------------|-----------------------------------------------------------------------------------|
|                 |               |                                  |               |             |                                                                                                                                                       |                             |           |                 | Is(50)                 |                    |               |                     |                                                                                   |
|                 |               |                                  |               |             |                                                                                                                                                       |                             |           |                 |                        |                    |               |                     |                                                                                   |
|                 |               |                                  | 88            |             |                                                                                                                                                       |                             |           |                 |                        |                    |               |                     |                                                                                   |
|                 |               | 0.50                             | 87            |             |                                                                                                                                                       | Commenced Coring at 0.6m    | 0.50      |                 |                        |                    |               |                     |                                                                                   |
| NMLC Coring     | No Water Loss | 1                                |               | SST         | Rock SANDSTONE: highly weathered, very low strength, pale grey dark grey pale brown, very fine grained, with siltstone laminations and iron staining. | 1                           | HW        | d:1.67 ; a:1.93 | RQD = 0%<br>TCR = 100% | 0.6-0.85, CRF,     |               |                     |                                                                                   |
|                 |               | 1.50                             | 1.50          |             |                                                                                                                                                       | d:0.02 ; a:0.85             |           | 1.06-1.09, XWS, |                        |                    |               |                     |                                                                                   |
|                 |               | 2                                | 2             |             |                                                                                                                                                       | 1.19, P, 5°, PL, RO,        |           |                 |                        |                    |               |                     |                                                                                   |
|                 |               | 2.35                             | 2.35          |             |                                                                                                                                                       | 1.52, P, 5°, PL, RO,        |           |                 |                        |                    |               |                     |                                                                                   |
|                 |               | 2.50                             | 2.50          |             |                                                                                                                                                       | 1.87, P, 20°, PL, RO,       |           |                 |                        |                    |               |                     |                                                                                   |
|                 |               | 2.64                             | 2.64          |             |                                                                                                                                                       | 1.9, P, 10°, PL, RO,        |           |                 |                        |                    |               |                     |                                                                                   |
|                 |               | 3                                | 3             |             |                                                                                                                                                       | 2.04, P, 10°, PL, RO, CL, , |           |                 |                        |                    |               |                     |                                                                                   |
|                 |               | 3.26                             | 3.26          |             |                                                                                                                                                       | 2.15, P, 10°, PL, RO, CL, , |           |                 |                        |                    |               |                     |                                                                                   |
|                 |               | 3.32                             | 3.32          |             |                                                                                                                                                       | 2.24, P, 5°, PL, RO, CL, ,  |           |                 |                        |                    |               |                     |                                                                                   |
|                 |               | 3.36-3.45                        | 3.36-3.45     |             |                                                                                                                                                       | 2.26, P, 5°, PL, RO, CL, ,  |           |                 |                        |                    |               |                     |                                                                                   |
| 3.48            | 3.48          | 2.3, P, 5°, PL, RO, CL, ,        |               |             |                                                                                                                                                       |                             |           |                 |                        |                    |               |                     |                                                                                   |
| 3.56            | 3.56          | 2.35-2.36, CORELOSS,             |               |             |                                                                                                                                                       |                             |           |                 |                        |                    |               |                     |                                                                                   |
| 3.65            | 3.65          | 2.42, P, 5°, PL, SO, CL, ,       |               |             |                                                                                                                                                       |                             |           |                 |                        |                    |               |                     |                                                                                   |
| 3.72            | 3.72          | 2.64, P, 5°, PL, RO, CL, , (X2), |               |             |                                                                                                                                                       |                             |           |                 |                        |                    |               |                     |                                                                                   |
| 3.82            | 3.82          | 2.9, P, 10°, PL, RO, CL, ,       |               |             |                                                                                                                                                       |                             |           |                 |                        |                    |               |                     |                                                                                   |
| 3.92            | 3.92          | 3.26, P, 10°, PL, RO, CL, ,      |               |             |                                                                                                                                                       |                             |           |                 |                        |                    |               |                     |                                                                                   |
| 3.92            | 3.92          | 3.32, P, 10°, PL, RO,            |               |             |                                                                                                                                                       |                             |           |                 |                        |                    |               |                     |                                                                                   |
| 3.92            | 3.92          | 3.36-3.45, J, 60°, PL, RO,       |               |             |                                                                                                                                                       |                             |           |                 |                        |                    |               |                     |                                                                                   |
| 3.92            | 3.92          | 3.48, P, 5°, PL, RO,             |               |             |                                                                                                                                                       |                             |           |                 |                        |                    |               |                     |                                                                                   |
| 3.92            | 3.92          | 3.56, P, 5°, PL, RO,             |               |             |                                                                                                                                                       |                             |           |                 |                        |                    |               |                     |                                                                                   |
| 3.92            | 3.92          | 3.65, P, 10°, PL, RO, (X2),      |               |             |                                                                                                                                                       |                             |           |                 |                        |                    |               |                     |                                                                                   |
| 3.92            | 3.92          | 3.72, P, 10°, PL, RO,            |               |             |                                                                                                                                                       |                             |           |                 |                        |                    |               |                     |                                                                                   |
| 3.92            | 3.92          | 3.82, P, 10°, PL, RO, (X2),      |               |             |                                                                                                                                                       |                             |           |                 |                        |                    |               |                     |                                                                                   |
| 3.92            | 3.92          | 3.92, P, 10°, PL, RO, (X2),      |               |             |                                                                                                                                                       |                             |           |                 |                        |                    |               |                     |                                                                                   |

|                       |                                 |                                                                                |
|-----------------------|---------------------------------|--------------------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : Man Portable      | Job Number : P3444                                                             |
| Easting : 330840.02   | Driller Supplier : TIGHT Site   | Client : Landmark Group Construction Australia Pty Ltd                         |
| Northing : 6261235.97 | Logged By : Mahmoud Jangidaryan | Project : Lindfield                                                            |
| RL : 87.50(m)         | Reviewed By : Ozzie Baskan      | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW            |
| Total Depth : 20.4 m  | Date : 11/02/2025               | Loc Comment : North-eastern corner of the tennis court at 63 Trafalgar Avenue. |

| Drilling Method | Water         | Depth (m) | Elevation (m) | Graphic Log | Classification Code | Material Description                                                                                                                          | Depth (m) | Weathering | Testing         |                    | RQD% and TCR%              | Defect Spacing (mm) | Defect Description<br><small>type, inclination, planarity, roughness, coating, thickness</small>                                                                                                                                                                                                |
|-----------------|---------------|-----------|---------------|-------------|---------------------|-----------------------------------------------------------------------------------------------------------------------------------------------|-----------|------------|-----------------|--------------------|----------------------------|---------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
|                 |               |           |               |             |                     |                                                                                                                                               |           |            | Is(50)          | Estimated Strength |                            |                     |                                                                                                                                                                                                                                                                                                 |
| NMLC Coring     | No Water Loss |           | 84            |             | SST                 | Rock SANDSTONE: highly weathered, medium strength, pale grey dark grey pale brown, fine grained, with siltstone lamination and iron staining. | 4.31      | HW         |                 |                    | RQD = 0%<br>TCR = 88.73%   |                     | 4.07-4.17, J, 75°, PL, RO, STN, OP,<br>4.19, P, 10°, PL, RO,<br>4.25-4.3, CS,<br>4.31-4.39, CORELOSS,                                                                                                                                                                                           |
|                 |               |           |               |             | CRL                 | Coreloss                                                                                                                                      | 4.39      |            |                 |                    |                            |                     |                                                                                                                                                                                                                                                                                                 |
|                 |               | 4.50      | 83            |             | SST                 | Rock SANDSTONE: highly weathered, high strength, pale grey dark grey pale brown, fine grained, with siltstone lamination and iron staining.   | 4.50      | HW         | d:0.78 ; a:1.12 |                    | RQD = 98.74%<br>TCR = 100% |                     | 4.41, P, 10°, PL, RO, CL, ,<br>4.57, P, 10°, PL, RO,<br>4.63-4.67, J, 40°, PL, RO, (X2),<br>4.73-4.79, J, 40°, PL, RO,<br>4.9, P, 10°, PL, RO, CL, OP,<br>5.18, P, 10°, PL, RO, CL, OP,                                                                                                         |
|                 |               |           |               |             |                     |                                                                                                                                               | 4.7       |            |                 |                    |                            |                     |                                                                                                                                                                                                                                                                                                 |
|                 |               | 5.50      | 82            |             |                     | Rock SANDSTONE: moderately weathered, high strength, pale grey with pale brown, fine grained.                                                 | 5.50      |            | d:0.72 ; a:1.04 |                    |                            |                     |                                                                                                                                                                                                                                                                                                 |
|                 |               |           |               |             |                     |                                                                                                                                               |           |            |                 |                    |                            |                     |                                                                                                                                                                                                                                                                                                 |
|                 |               | 6         |               |             |                     |                                                                                                                                               | 6         |            |                 |                    | RQD = 77.22%<br>TCR = 100% |                     | 5.58, P, 10°, UN, VR, CL, OP,<br>5.92, P, 5°, PL, RO, CL, OP,<br>6.02, P, 5°, CV, RO, CL, OP,<br>6.1, P, 15°, PL, RO, CL, OP,<br>6.14, P, 15°, PL, RO, CL, OP,<br>6.19, P, 20°, IR, VR, CL, OP,<br>6.27, 10°, CV, RO, CL, OP,<br>6.33, P, 20°, PL, RO, CL, OP,<br>6.34, P, 20°, PL, RO, CL, OP, |
|                 |               |           |               |             | SST                 |                                                                                                                                               | 6.50      |            | d:1.23 ; a:1.50 |                    |                            |                     |                                                                                                                                                                                                                                                                                                 |
|                 |               | 7         |               |             |                     |                                                                                                                                               | 7         |            |                 |                    |                            |                     |                                                                                                                                                                                                                                                                                                 |
|                 |               |           |               |             |                     |                                                                                                                                               |           |            |                 |                    |                            |                     |                                                                                                                                                                                                                                                                                                 |
|                 |               | 7.50      | 80            |             |                     |                                                                                                                                               | 7.50      |            | d:1.30 ; a:1.70 |                    | RQD = 71.95%<br>TCR = 100% |                     | 7.04, P, PL, SO, CL, OP,<br>7.23, P, PL, SO, CL, OP,<br>7.44, P, UN, RO, CL, OP,<br>7.69, P, 5°, PL, RO,<br>7.78, P, 5°, PL, RO,<br>7.83, P, 5°, PL, RO,                                                                                                                                        |
|                 |               |           |               |             |                     |                                                                                                                                               |           |            |                 |                    |                            |                     |                                                                                                                                                                                                                                                                                                 |



|                       |                                 |                                                                                |
|-----------------------|---------------------------------|--------------------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : Man Portable      | Job Number : P3444                                                             |
| Easting : 330840.02   | Driller Supplier : TIGHT Site   | Client : Landmark Group Construction Australia Pty Ltd                         |
| Northing : 6261235.97 | Logged By : Mahmoud Jangidaryan | Project : Lindfield                                                            |
| RL : 87.50(m)         | Reviewed By : Ozzie Baskan      | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW            |
| Total Depth : 20.4 m  | Date : 11/02/2025               | Loc Comment : North-eastern corner of the tennis court at 63 Trafalgar Avenue. |

| Drilling Method | Water         | Depth (m) | Elevation (m) | Graphic Log | Classification Code | Material Description                                                                                                        | Depth (m) | Weathering | Testing         | Estimated Strength | RQD% and TCR% | Defect Spacing (mm)                                      | Defect Description<br><small>type, inclination, planarity, roughness, coating, thickness</small> |
|-----------------|---------------|-----------|---------------|-------------|---------------------|-----------------------------------------------------------------------------------------------------------------------------|-----------|------------|-----------------|--------------------|---------------|----------------------------------------------------------|--------------------------------------------------------------------------------------------------|
|                 |               |           |               |             |                     |                                                                                                                             |           |            | Is(50)          |                    |               |                                                          |                                                                                                  |
| NMLC Coring     | No Water Loss |           | 80            |             | SST                 | Rock SANDSTONE: moderately weathered, high strength, pale grey with pale brown, fine grained.                               |           | MW         |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             | 8.3                 |                                                                                                                             |           |            |                 |                    |               |                                                          | 8.19, P, 5°, PL, RO,                                                                             |
|                 |               | 8.50      | 79            |             |                     | Rock SANDSTONE: slightly to fresh weathered, medium to high strength, pale grey, fine grained, with carbonaceous beddings.. |           |            | d:0.32 ; a:0.83 |                    |               | 8.31, P, 10°, PL, VR,<br>8.36, P, 10°, PL, VR,           |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               | 8.5, P, 2°, PL, SO,                                      |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               | 8.66-8.73, CORELOSS,                                     |                                                                                                  |
|                 |               | 9         |               |             |                     |                                                                                                                             |           |            |                 |                    |               | 9, P, 20°, PL, RO, CL, OP,<br>9.02-9.06, J, 40°, PL, RO, |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               | 9.06, P, 10°, PL, RO,                                    |                                                                                                  |
|                 |               | 9.50      | 78            |             |                     |                                                                                                                             |           |            |                 | d:1.16 ; a:1.32    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               | 10        |               |             |                     |                                                                                                                             | SST       |            | SW-F            |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                 |                    |               |                                                          |                                                                                                  |

|                       |                                 |                                                                                |
|-----------------------|---------------------------------|--------------------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : Man Portable      | Job Number : P3444                                                             |
| Easting : 330840.02   | Driller Supplier : TIGHT Site   | Client : Landmark Group Construction Australia Pty Ltd                         |
| Northing : 6261235.97 | Logged By : Mahmoud Jangidaryan | Project : Lindfield                                                            |
| RL : 87.50(m)         | Reviewed By : Ozzie Baskan      | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW            |
| Total Depth : 20.4 m  | Date : 11/02/2025               | Loc Comment : North-eastern corner of the tennis court at 63 Trafalgar Avenue. |

| Drilling Method | Water         | Depth (m) | Elevation (m) | Graphic Log | Classification Code | Material Description                                                                                                        | Depth (m) | Weathering | Testing           |  | Estimated Strength                                                                                            | RQD% and TCR%              | Defect Spacing (mm)                                                                | Defect Description<br><small>type, inclination, planarity, roughness, coating, thickness</small> |
|-----------------|---------------|-----------|---------------|-------------|---------------------|-----------------------------------------------------------------------------------------------------------------------------|-----------|------------|-------------------|--|---------------------------------------------------------------------------------------------------------------|----------------------------|------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------|
|                 |               |           |               |             |                     |                                                                                                                             |           |            | Is(50)            |  |                                                                                                               |                            |                                                                                    |                                                                                                  |
| NMLC Coring     | No Water Loss |           | 76            |             | SST                 | Rock SANDSTONE: slightly to fresh weathered, medium to high strength, pale grey, fine grained, with carbonaceous beddings.. |           | SW-F       |                   |  | <div><div>MLS 0.1</div><div>LS 0.3</div><div>MS 1.0</div><div>HS 3</div><div>VHS 10</div><div>EHS</div></div> | RQD = 96.86%<br>TCR = 100% | <div><div>30</div><div>100</div><div>300</div><div>1000</div><div>3000</div></div> |                                                                                                  |
|                 |               | 12.50     | 75            |             |                     |                                                                                                                             | 12.50     |            | d:0.97 ; a:0.82   |  |                                                                                                               |                            |                                                                                    |                                                                                                  |
|                 |               | 13        |               |             |                     |                                                                                                                             | 13        |            |                   |  |                                                                                                               |                            |                                                                                    |                                                                                                  |
|                 |               | 13.50     | 74            |             |                     |                                                                                                                             | 13.50     |            | d:0.63 ; a:0.94   |  |                                                                                                               |                            |                                                                                    |                                                                                                  |
|                 |               | 14        |               |             |                     |                                                                                                                             | 14        |            |                   |  |                                                                                                               |                            |                                                                                    |                                                                                                  |
|                 |               | 14.50     | 73            |             |                     |                                                                                                                             | 14.50     |            | d:0.78 ; a:0.1.05 |  |                                                                                                               |                            |                                                                                    |                                                                                                  |
|                 |               | 15        |               |             |                     |                                                                                                                             | 15        |            |                   |  |                                                                                                               |                            |                                                                                    |                                                                                                  |
|                 |               | 15.50     | 72            |             |                     |                                                                                                                             | 15.50     |            | d:0.57 ; a:1.68   |  |                                                                                                               |                            |                                                                                    |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                   |  |                                                                                                               |                            |                                                                                    |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             |           |            |                   |  |                                                                                                               |                            |                                                                                    |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             | 14.66     |            |                   |  | RQD = 100% TCR = 100%                                                                                         |                            | 14.66, P, 45°, PL, RO, CL, OP,                                                     |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             | 14.75     |            |                   |  |                                                                                                               |                            | 14.75, P, PL, RO, CL, OP,                                                          |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             | 15.59     |            |                   |  | RQD = 100% TCR = 100%                                                                                         |                            | 15.59, P, 5°, PL, RO, CL, OP,                                                      |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                                             | 15.97     |            |                   |  | RQD = 100% TCR = 100%                                                                                         |                            | 15.97, P, 25°, PL, RO, CL, OP,                                                     |                                                                                                  |

|                       |                                 |                                                                                |
|-----------------------|---------------------------------|--------------------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : Man Portable      | Job Number : P3444                                                             |
| Easting : 330840.02   | Driller Supplier : TIGHT Site   | Client : Landmark Group Construction Australia Pty Ltd                         |
| Northing : 6261235.97 | Logged By : Mahmoud Jangidaryan | Project : Lindfield                                                            |
| RL : 87.50(m)         | Reviewed By : Ozzie Baskan      | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW            |
| Total Depth : 20.4 m  | Date : 11/02/2025               | Loc Comment : North-eastern corner of the tennis court at 63 Trafalgar Avenue. |

| Drilling Method | Water         | Depth (m) | Elevation (m) | Graphic Log | Classification Code | Material Description                                                                                 | Depth (m) | Weathering | Testing         |                                                                                                | RQD% and TCR%         | Defect Spacing (mm) | Defect Description<br><small>type, inclination, planarity, roughness, coating, thickness</small> |
|-----------------|---------------|-----------|---------------|-------------|---------------------|------------------------------------------------------------------------------------------------------|-----------|------------|-----------------|------------------------------------------------------------------------------------------------|-----------------------|---------------------|--------------------------------------------------------------------------------------------------|
|                 |               |           |               |             |                     |                                                                                                      |           |            | Is(50)          | Estimated Strength<br><small>MLS 0.1<br/>LS 0.3<br/>MS 1.0<br/>HS 3<br/>VHS 10<br/>EHS</small> |                       |                     |                                                                                                  |
|                 | No Water Loss |           | 72            |             | SST                 | Rock SANDSTONE: fresh weathered, high strength, pale grey, fine grained, with carbonaceous beddings. |           | F          |                 |                                                                                                | RQD = 100% TCR = 100% |                     | 16.13, P, PL, VR, CL, OP,                                                                        |
|                 |               | 16.50     | 71            |             |                     |                                                                                                      | 16.50     |            | d:1.39 ; a:2.12 |                                                                                                |                       |                     | 16.8, P, 5°, PL, RO, CL, OP,                                                                     |
|                 |               | 17        |               |             |                     |                                                                                                      | 17        |            |                 |                                                                                                |                       |                     | 17.08, P, 5°, PL, VR, CL, OP,                                                                    |
|                 |               | 17.50     | 70            |             |                     |                                                                                                      | 17.50     |            | d:0.84 ; a:1.22 |                                                                                                |                       |                     | 17.19, P, 20°, PL, RO, CL, OP,                                                                   |
|                 |               | 18        |               |             |                     |                                                                                                      | 18        |            |                 |                                                                                                |                       |                     | 17.98, P, 30°, PL, VR, CL, OP,                                                                   |
|                 |               | 18.50     | 69            |             |                     |                                                                                                      | 18.50     |            | d:1.68 ; a:1.64 |                                                                                                |                       |                     | 18.38, P, PL, RO, CL, OP,                                                                        |
|                 |               | 19        |               |             |                     |                                                                                                      | 19        |            |                 |                                                                                                |                       |                     | 18.91, P, 10°, PL, RO, CL, OP,                                                                   |
|                 |               | 19.50     | 68            |             |                     |                                                                                                      | 19.50     |            | d:1.56 ; a:2.21 |                                                                                                |                       |                     |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                      |           |            |                 |                                                                                                |                       |                     |                                                                                                  |
|                 |               |           |               |             |                     |                                                                                                      |           |            |                 |                                                                                                |                       |                     |                                                                                                  |

|                       |                                 |                                                                                |
|-----------------------|---------------------------------|--------------------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : Man Portable      | Job Number : P3444                                                             |
| Easting : 330840.02   | Driller Supplier : TIGHT Site   | Client : Landmark Group Construction Australia Pty Ltd                         |
| Northing : 6261235.97 | Logged By : Mahmoud Jangidaryan | Project : Lindfield                                                            |
| RL : 87.50(m)         | Reviewed By : Ozzie Baskan      | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW            |
| Total Depth : 20.4 m  | Date : 11/02/2025               | Loc Comment : North-eastern corner of the tennis court at 63 Trafalgar Avenue. |

| Drilling Method    | Water | Depth (m) | Elevation (m) | Graphic Log                                                                       | Classification Code | Material Description                                                                                 | Depth (m) | Weathering      | Testing |                                                                                                | RQD% and TCR%            | Defect Spacing (mm)                                                                 | Defect Description<br><small>type, inclination, planarity, roughness, coating, thickness</small> |
|--------------------|-------|-----------|---------------|-----------------------------------------------------------------------------------|---------------------|------------------------------------------------------------------------------------------------------|-----------|-----------------|---------|------------------------------------------------------------------------------------------------|--------------------------|-------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------|
|                    |       |           |               |                                                                                   |                     |                                                                                                      |           |                 | Is(50)  | Estimated Strength<br><small>MLS 0.1<br/>LS 0.3<br/>MS 1.0<br/>HS 3<br/>VHS 10<br/>EHS</small> |                          |                                                                                     |                                                                                                  |
| ↑ NMLC Coring<br>↓ |       |           | 68            |  | SST                 | Rock SANDSTONE: fresh weathered, high strength, pale grey, fine grained, with carbonaceous beddings. |           | F               |         |                                                                                                | RQD = 100%<br>TCR = 100% |  |                                                                                                  |
|                    |       |           |               |                                                                                   |                     |                                                                                                      |           | d:2.27 ; a:0.88 |         |                                                                                                |                          |                                                                                     |                                                                                                  |
|                    |       |           |               |                                                                                   |                     | BH3 Reached Target Depth at 20.4m                                                                    |           |                 |         |                                                                                                |                          |                                                                                     |                                                                                                  |

# morrow

CLIENT NAME: Landmark Group

PROJECT: Lindfield

LOCATION: 63 Trafalgar Ave

JOB NUMBER: P3444

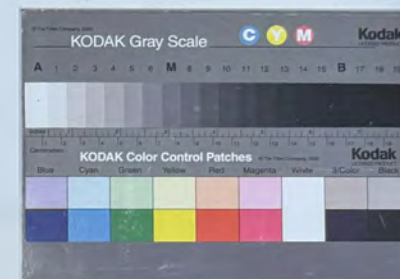
LOGGED BY: MS

BOREHOLE ID: BH3

DEPTH: 0.6 to 5.0m

CORE TRAY NO: Box 1 of 4

DATE: 11, 2, 25



# morrow



02 8599 7579



Sydney Gadigal Land,  
2/5-7 Malta Street, Fairfield  
East NSW 2155



info@morrowgeo.com.au

## Photo description

BH3 - Box 1 of 4

## Client

Landmark Group Construction Australia Pty Ltd

## Location

59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW

## Project name

Lindfield

## Project No

P3444

## Scale

Not to Scale

## BH No

BH3

## BH Depth

CorePhoto



# morrow

CLIENT NAME: Landmark Group

PROJECT: Lindfield

LOCATION: 63 Trafalgar Ave

JOB NUMBER: P3444

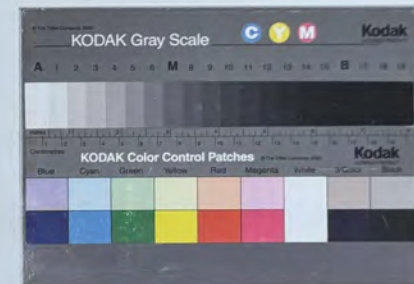
LOGGED BY: MJ

BOREHOLE ID: BH3

DEPTH: 5.0 to 10.0m

CORE TRAY N: Box 2 of 4

DATE: 11, 2, 25



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02 8599 7579



Sydney Gadigal Land,  
2/5-7 Malta Street, Fairfield  
East NSW 2155



info@morrowgeo.com.au

## Photo description

BH3 - Box 2 of 4

## Client

Landmark Group Construction Australia Pty Ltd

## Location

59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW

## Project name

Lindfield

## Project No

P3444

## Scale

Not to Scale

## BH No

BH3

## BH Depth

CorePhoto

# morrow

CLIENT NAME: Landmark Group

PROJECT: Lindfield

LOCATION: 63 Trafalgar Ave

JOB NUMBER: P3444

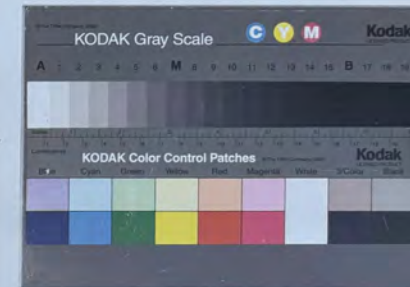
LOGGED BY: MS

BOREHOLE ID: BH3

DEPTH: 10.0 to 15.0m

CORE TRAY N: Box 3 of 4

DATE: 11, 2, 25



# morrow



02 8599 7579



Sydney Gadigal Land,  
2/5-7 Malta Street, Fairfield  
East NSW 2155



info@morrowgeo.com.au

## Photo description

BH3 - Box 3 of 4

## Client

Landmark Group Construction Australia Pty Ltd

## Location

59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW

## Project name

Lindfield

## Project No

P3444

## Scale

Not to Scale

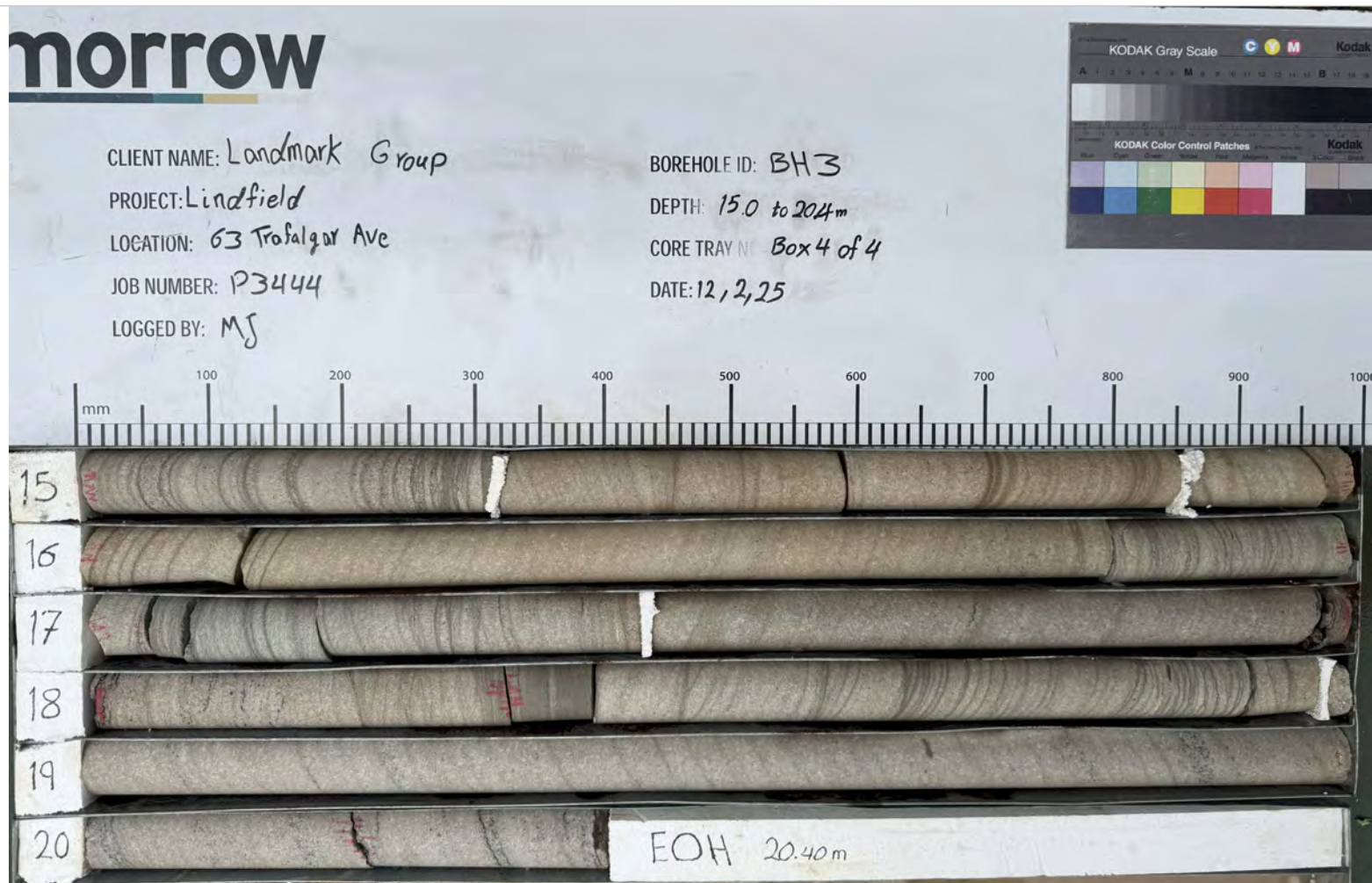
## BH No

BH3

## BH Depth

CorePhoto





**morrow**



02 8599 7579



Sydney Gadigal Land,  
2/5-7 Malta Street, Fairfield  
East NSW 2155



info@morrowgeo.com.au

#### Photo description

BH3 - Box 4 of 4

#### Client

Landmark Group Construction Australia Pty Ltd

#### Location

59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW

#### Project name

Lindfield

#### Project No

P3444

#### Scale

Not to Scale

#### BH No

BH3

#### BH Depth

CorePhoto

|                       |                                   |                                                                     |
|-----------------------|-----------------------------------|---------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : GEO205 - Comacchio  | Job Number : P3444                                                  |
| Easting : 330887,16   | Driller Supplier : GEOSENSE       | Client : Landmark Group Construction Australia Pty Ltd              |
| Northing : 6261205,27 | Logged By : Ozzie Baskan          | Project : Lindfield                                                 |
| RL : 81.70(m)         | Reviewed By : Mahmoud Jangidaryan | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth : 18 m    | Date : 03/03/2025                 | Loc Comment : End of the driveway of 1B Valley Road.                |

| Drilling Method | Water   | Testing        | Depth (m) | Elevation (m) | Material Type | Graphic Log | Classification Code | Material Description                                                                                                                   | Elevation    | Consistency/Density | Moisture |
|-----------------|---------|----------------|-----------|---------------|---------------|-------------|---------------------|----------------------------------------------------------------------------------------------------------------------------------------|--------------|---------------------|----------|
|                 |         | SPT            |           |               |               |             |                     |                                                                                                                                        | Depth (m)    |                     |          |
|                 | 2. GWNE |                |           | 82            | TOPSOIL       |             | SM                  | Topsoil Silty SAND very loose to loose, dark grey, fine grained, dry.                                                                  |              | VL-L                | D        |
|                 |         |                |           |               | FILL          |             | CL                  | FILL Silty CLAY low plasticity, soft to firm, dark grey, w < pl.                                                                       | 81.5<br>0.2  | S-F                 | w < PL   |
|                 |         | 2,2,3<br>(N=5) |           |               | Residual      |             | CI-CH               | Residual Silty CLAY firm to stiff, medium to high plasticity, pale brown, w > pl, with organic matter (roots).                         | 81.2<br>0.5  | F-St                | w > PL   |
|                 |         |                | 1         | 81            |               |             |                     |                                                                                                                                        |              |                     |          |
|                 |         | 8,5,3<br>(N=8) |           |               | Residual      |             | CI-CH               | Residual Silty CLAY firm to stiff, medium to high plasticity, grey white mottled red, w > pl, with organic matter (roots).             | 80.2<br>1.5  | F-St                | w > PL   |
|                 |         |                | 2         | 80            |               |             |                     |                                                                                                                                        |              |                     |          |
|                 |         |                |           |               | Rock          |             | SST                 | Extremely weathered Sandstone, Silty CLAY hard, low to medium plasticity, pale grey mottled brown, with ironstone and sandstone bands. | 79.2<br>2.5  | VLS                 |          |
|                 |         |                |           |               | Rock          |             | SST                 | Rock SANDSTONE: highly weathered, very low to low strength, white grey red, fine to medium grained.                                    | 78.7<br>3    | VLS-LS              |          |
|                 |         |                |           |               |               |             |                     |                                                                                                                                        | 78.1<br>3.62 |                     |          |
|                 |         |                |           |               |               |             |                     | Commenced Coring at 3.62m                                                                                                              |              |                     |          |

|                       |                                   |                                                                     |
|-----------------------|-----------------------------------|---------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : GEO205 - Comacchio  | Job Number : P3444                                                  |
| Easting : 330887.16   | Driller Supplier : GEOSENSE       | Client : Landmark Group Construction Australia Pty Ltd              |
| Northing : 6261205.27 | Logged By : Ozzie Baskan          | Project : Lindfield                                                 |
| RL : 81.70(m)         | Reviewed By : Mahmoud Jangidaryan | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth : 18 m    | Date : 03/03/2025                 | Loc Comment : End of the driveway of 1B Valley Road.                |

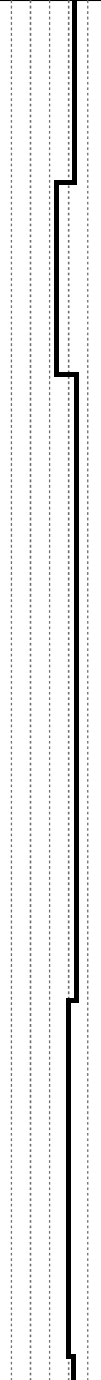
| Drilling Method | Water | Depth (m) | Elevation (m) | Graphic Log | Classification Code | Material Description                                                                                                  | Depth (m) | Weathering | Testing        |  | Estimated Strength | RQD% and TCR%         | Defect Spacing (mm) | Defect Description<br><small>type, inclination, planarity, roughness, coating, thickness</small> |
|-----------------|-------|-----------|---------------|-------------|---------------------|-----------------------------------------------------------------------------------------------------------------------|-----------|------------|----------------|--|--------------------|-----------------------|---------------------|--------------------------------------------------------------------------------------------------|
|                 |       |           |               |             |                     |                                                                                                                       |           |            | Is(50)         |  |                    |                       |                     |                                                                                                  |
|                 |       |           | 82            |             |                     |                                                                                                                       |           |            |                |  |                    |                       |                     |                                                                                                  |
|                 |       | 0.50      | 81            |             |                     |                                                                                                                       | 0.50      |            |                |  |                    |                       |                     |                                                                                                  |
|                 |       | 1         |               |             |                     |                                                                                                                       | 1         |            |                |  |                    |                       |                     |                                                                                                  |
|                 |       | 1.50      | 80            |             |                     |                                                                                                                       | 1.50      |            |                |  |                    |                       |                     |                                                                                                  |
|                 |       | 2         |               |             |                     |                                                                                                                       | 2         |            |                |  |                    |                       |                     |                                                                                                  |
|                 |       | 2.50      | 79            |             |                     |                                                                                                                       | 2.50      |            |                |  |                    |                       |                     |                                                                                                  |
|                 |       | 3         |               |             |                     |                                                                                                                       | 3         |            |                |  |                    |                       |                     |                                                                                                  |
|                 |       | 3.50      | 78            |             |                     |                                                                                                                       | 3.50      |            |                |  |                    |                       |                     |                                                                                                  |
|                 |       |           |               |             |                     | Commenced Coring at 3.62m                                                                                             |           |            |                |  |                    |                       |                     |                                                                                                  |
| NMLC Coring     |       |           |               |             | SST                 | Rock SANDSTONE: moderately weathered, high strength, red grey pale brown, fine to medium grained, with iron staining. |           | MW         | d:0.86; a:1.82 |  |                    | RQD = 100% TCR = 100% |                     | 3.62, P, PL, RO, CL, OP,                                                                         |
|                 |       |           |               |             |                     |                                                                                                                       |           |            |                |  |                    |                       |                     |                                                                                                  |
|                 |       |           |               |             |                     |                                                                                                                       |           |            |                |  |                    |                       |                     |                                                                                                  |



|                       |                                   |                                                                     |
|-----------------------|-----------------------------------|---------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : GEO205 - Comacchio  | Job Number : P3444                                                  |
| Easting : 330887.16   | Driller Supplier : GEOSENSE       | Client : Landmark Group Construction Australia Pty Ltd              |
| Northing : 6261205.27 | Logged By : Ozzie Baskan          | Project : Lindfield                                                 |
| RL : 81.70(m)         | Reviewed By : Mahmoud Jangidaryan | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth : 18 m    | Date : 03/03/2025                 | Loc Comment : End of the driveway of 1B Valley Road.                |

| Drilling Method | Water               | Depth (m) | Elevation (m) | Graphic Log | Classification Code | Material Description                                                                                                      | Depth (m) | Weathering | Testing        |  | Estimated Strength                                   | RQD% and TCR% | Defect Spacing (mm) | Defect Description<br><small>type, inclination, planarity, roughness, coating, thickness</small> |
|-----------------|---------------------|-----------|---------------|-------------|---------------------|---------------------------------------------------------------------------------------------------------------------------|-----------|------------|----------------|--|------------------------------------------------------|---------------|---------------------|--------------------------------------------------------------------------------------------------|
|                 |                     |           |               |             |                     |                                                                                                                           |           |            | Is(50)         |  |                                                      |               |                     |                                                                                                  |
| NMLC Coring     | Loss 10% Water Loss |           | 78            |             | SST                 | Rock SANDSTONE: moderately weathered, high strength, red grey pale brown, fine to medium grained, with iron staining.     |           | MW         |                |  | VLS 0.1<br>LS 0.3<br>MS 1.0<br>HS 3<br>VHS 10<br>EHS |               |                     | 4.06, P, 30°, PL, RO, CL, OP,                                                                    |
|                 |                     | 4.50      | 77            |             |                     |                                                                                                                           | 4.50      |            |                |  |                                                      |               |                     |                                                                                                  |
|                 |                     |           |               |             | SST                 | Rock SANDSTONE: moderately weathered, medium strength, fine to medium grained, laminations at 5° to 10°.                  | 4.68      |            | d:0.38, a:0.46 |  |                                                      |               |                     | 4.67, J, 5°, PL, RO, CT, OP,                                                                     |
|                 |                     | 5         |               |             |                     |                                                                                                                           | 5         | MW         |                |  |                                                      |               |                     |                                                                                                  |
|                 |                     |           |               |             |                     |                                                                                                                           | 5.4       |            |                |  |                                                      |               |                     |                                                                                                  |
|                 |                     | 5.50      | 76            |             | SST                 | Rock SANDSTONE: moderately weathered, medium strength, orange pale grey, fine to medium grained, with ironstone staining. | 5.50      | MW         | d:0.87, a:0.68 |  |                                                      |               |                     | 5.2, 5°, PL, RO, CL, OP,                                                                         |
|                 |                     | 6         |               |             |                     |                                                                                                                           | 6         |            |                |  |                                                      |               |                     |                                                                                                  |
|                 |                     |           |               |             |                     | As above, but pale grey.                                                                                                  | 6.16      |            |                |  |                                                      |               |                     |                                                                                                  |
|                 |                     | 6.50      | 75            |             | SST                 |                                                                                                                           | 6.50      | MW         | d:0.59, a:0.88 |  |                                                      |               |                     | 6.68, P, 30°, PL, RO, VN, OP,                                                                    |
|                 |                     | 7         |               |             |                     |                                                                                                                           | 7         |            |                |  |                                                      |               |                     | 6.88, J, 5°, PL, RO, STN, OP, (X2),                                                              |
|                 | Loss 0% Water Loss  |           |               |             |                     |                                                                                                                           | 7.2       |            | d:0.8, a:1.21  |  |                                                      |               |                     | 7.05, P, 5°, PL, RO, STN, OP, (X2),                                                              |
|                 |                     | 7.50      | 74            |             | SST                 | Rock SANDSTONE: slightly weathered, medium to high strength, pale grey, fine to medium grained.                           | 7.50      | SW         |                |  |                                                      |               |                     |                                                                                                  |

|                       |                                   |                                                                     |
|-----------------------|-----------------------------------|---------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : GEO205 - Comacchio  | Job Number : P3444                                                  |
| Easting : 330887.16   | Driller Supplier : GEOSENSE       | Client : Landmark Group Construction Australia Pty Ltd              |
| Northing : 6261205.27 | Logged By : Ozzie Baskan          | Project : Lindfield                                                 |
| RL : 81.70(m)         | Reviewed By : Mahmoud Jangidaryan | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth : 18 m    | Date : 03/03/2025                 | Loc Comment : End of the driveway of 1B Valley Road.                |

| Drilling Method | Water              | Depth (m) | Elevation (m) | Graphic Log                                                                        | Classification Code | Material Description                                                                            | Depth (m) | Weathering | Testing | Estimated Strength                                   | RQD% and TCR%         | Defect Spacing (mm)                                                                  | Defect Description<br><small>type, inclination, planarity, roughness, coating, thickness</small>                                                            |  |  |  |  |  |
|-----------------|--------------------|-----------|---------------|------------------------------------------------------------------------------------|---------------------|-------------------------------------------------------------------------------------------------|-----------|------------|---------|------------------------------------------------------|-----------------------|--------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------|--|--|--|--|--|
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            | Is(50)  |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
| NMLC Coring     |                    |           | 74            |  | SST                 | Rock SANDSTONE: slightly weathered, medium to high strength, pale grey, fine to medium grained. |           |            |         | VLS 0.1<br>LS 0.3<br>MS 1.0<br>HS 3<br>VHS 10<br>EHS | RQD = 100% TCR = 100% |  | 8.46, P, 30°, PL, RO, CL, OP,<br><br>8.95, P, 5°, PL, RO, CL, OP,<br><br><br><br>10.55, P, 5°, PL, RO, VN, OP,<br><br><br><br>11.46, P, 5°, IR, RO, CL, OP, |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    | 8.50      | 73            |                                                                                    |                     |                                                                                                 |           | 8.50       |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 | Loss 0% Water Loss |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    | 9         |               |                                                                                    |                     |                                                                                                 |           | 9          |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    | 9.50      | 72            |                                                                                    |                     |                                                                                                 |           | 9.50       |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    | 10        |               |                                                                                    |                     |                                                                                                 |           | 10         | SW      |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    |           |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |
|                 |                    | </        |               |                                                                                    |                     |                                                                                                 |           |            |         |                                                      |                       |                                                                                      |                                                                                                                                                             |  |  |  |  |  |

**Job Number : P3444**  
**Client : Landmark Group Construction Australia Pty Ltd**  
**Project : Lindfield**  
**Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW**  
**Loc Comment : End of the driveway of 1B Valley Road.**

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|                       |                                   |                                                                     |
|-----------------------|-----------------------------------|---------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : GEO205 - Comacchio  | Job Number : P3444                                                  |
| Easting : 330887,16   | Driller Supplier : GEONSENSE      | Client : Landmark Group Construction Australia Pty Ltd              |
| Northing : 6261205,27 | Logged By : Ozzie Baskan          | Project : Lindfield                                                 |
| RL : 81.70(m)         | Reviewed By : Mahmoud Jangidaryan | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth : 18 m    | Date : 03/03/2025                 | Loc Comment : End of the driveway of 1B Valley Road.                |

| Drilling Method                                                                                                 | Water | Depth (m) | Elevation (m) | Graphic Log | Classification Code | Material Description                                                                     | Depth (m) | Weathering | Testing        | Estimated Strength | RQD% and TCR%            | Defect Spacing (mm) | Defect Description<br><small>type, inclination, planarity, roughness, coating, thickness</small> |
|-----------------------------------------------------------------------------------------------------------------|-------|-----------|---------------|-------------|---------------------|------------------------------------------------------------------------------------------|-----------|------------|----------------|--------------------|--------------------------|---------------------|--------------------------------------------------------------------------------------------------|
|                                                                                                                 |       |           |               |             |                     |                                                                                          |           |            | Is(50)         |                    |                          |                     |                                                                                                  |
| <div> <div>NMLC Coring</div> <div> <div>Loss</div> <div>0%</div> <div>Water</div> <div>Loss</div> </div> </div> |       |           | 66            |             |                     | Rock SANDSTONE: slightly weathered, high strength, pale grey, fine to medium grained, ,. |           |            |                |                    |                          |                     |                                                                                                  |
|                                                                                                                 |       | 16.50     | 65            |             |                     |                                                                                          | 16.50     |            | d:0.76, a:1.85 |                    |                          |                     |                                                                                                  |
|                                                                                                                 |       | 17        |               |             | SST                 |                                                                                          | 17        | SW         |                |                    | RQD = 100%<br>TCR = 100% |                     |                                                                                                  |
|                                                                                                                 |       | 17.50     | 64            |             |                     |                                                                                          | 17.50     |            | d:0.89, a 1.08 |                    |                          |                     |                                                                                                  |
|                                                                                                                 |       |           |               |             |                     | BH4 Reached Target Depth at 18m                                                          |           |            |                |                    |                          |                     |                                                                                                  |

# morrow

CLIENT NAME: LANDMARK

PROJECT:

LOCATION: 63 Trafalgar Ave., Lindfield

JOB NUMBER: P3444

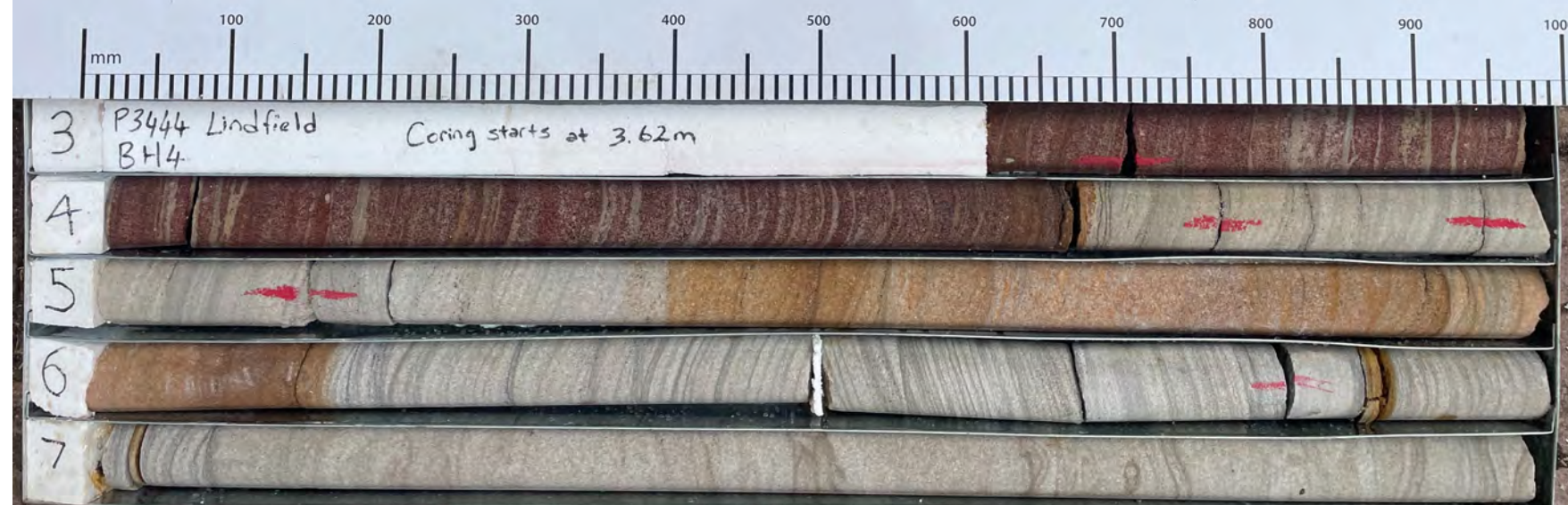
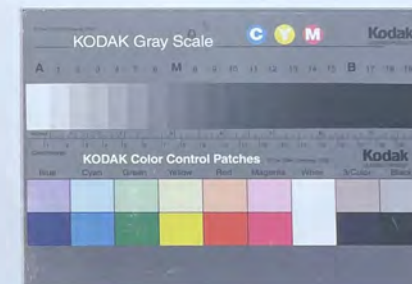
LOGGED BY: Ozzie B.

BOREHOLE ID: BH4

DEPTH: 3.62m to 8.0m

CORE TRAY: 1 of 3

DATE: 3/13/2025



# morrow



02 8599 7579



Sydney Gadigal Land,  
2/5-7 Malta Street, Fairfield  
East NSW 2155



info@morrowgeo.com.au

## Photo description

BH4 - Box 1 of 3

## Client

Landmark Group Construction Australia Pty Ltd

## Location

59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW

## Project name

Lindfield

## Project No

P3444

## Scale

Not to Scale

## BH No

BH4

## BH Depth

CorePhoto



# morrow

CLIENT NAME: LANDMARK

PROJECT:

LOCATION: 63 Trafalgar Ave, Lindfield

JOB NUMBER: P3444

LOGGED BY: Ozzie B.

BOREHOLE ID: BH4

DEPTH: 80m to 130m

CORE TRAY: 2 of 3

DATE: 3/3/2025



# morrow



02 8599 7579



Sydney Gadigal Land,  
2/5-7 Malta Street, Fairfield  
East NSW 2155



info@morrowgeo.com.au

## Photo description

BH4 - Box 2 of 3

## Client

Landmark Group Construction Australia Pty Ltd

## Location

59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW

## Project name

Lindfield

## Project No

P3444

## Scale

Not to Scale

## BH No

BH4

## BH Depth

CorePhoto

# morrow

CLIENT NAME: LANDMARK

PROJECT:

LOCATION: 63 Trafalgar Ave, Lindfield

JOB NUMBER: P3444

LOGGED BY: Ozzie B.

BOREHOLE ID: BH4

DEPTH: 13.0m to 18.0m

CORE TRAY: 3 of 3

DATE: 3/13/2025



# morrow



02 8599 7579



Sydney Gadigal Land,  
2/5-7 Malta Street, Fairfield  
East NSW 2155



info@morrowgeo.com.au

## Photo description

BH4 - Box 3 of 3

## Client

Landmark Group Construction Australia Pty Ltd

## Location

59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW

## Project name

Lindfield

## Project No

P3444

## Scale

Not to Scale

## BH No

BH4

## BH Depth

CorePhoto

|                       |                                   |                                                                     |
|-----------------------|-----------------------------------|---------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : GEO205 - Comacchio  | Job Number : P3444                                                  |
| Easting : 330828,69   | Driller Supplier : GEOSENSE       | Client : Landmark Group Construction Australia Pty Ltd              |
| Northing : 6261173,80 | Logged By : Ozzie Baskan          | Project : Lindfield                                                 |
| RL : 83.80(m)         | Reviewed By : Mahmoud Jangidaryan | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth : 18 m    | Date : 28/02/2025                 | Loc Comment : Driveway of 1B Valley road.                           |

| Drilling Method | Water | Well Diagram | Testing | Elevation   | Graphic Log | Material Type | Classification Code | Material Description                                                                                                                           | Depth (m) | Consistency | Weathering | Moisture |
|-----------------|-------|--------------|---------|-------------|-------------|---------------|---------------------|------------------------------------------------------------------------------------------------------------------------------------------------|-----------|-------------|------------|----------|
|                 |       |              |         | Depth (m)   |             |               |                     |                                                                                                                                                |           |             |            |          |
|                 |       |              |         |             |             | TOPSOIL       | CL-CI               | Topsoil Silty CLAY low to medium plasticity, dark grey, with fine to medium sized gravel, with fine grained sand, w < pl.                      | 0.4       |             |            | w < PL   |
|                 |       |              |         | 83.4<br>0.4 |             |               |                     | Residual Sandy CLAY stiff to very stiff, low to medium plasticity, pale brown white, with fine sized gravel, with low plasticity silt, w < pl. | 1         | St-VSt      |            | w < PL   |
|                 |       |              |         | 82.3<br>1.5 |             | Rock          | SST                 | Extremely weathered Sandstone, Silty CLAY hard, low to medium plasticity, pale grey mottled brown, with ironstone and sandstone bands.         | 2         | VLS         | XW         |          |
|                 |       |              |         | 81.3<br>2.5 |             |               |                     | Rock SANDSTONE: highly weathered, very low strength, pale brown white pale grey red, fine grained, with ironstone bands.                       | 3         | VLS         | HW         |          |
|                 |       |              |         |             |             |               |                     | Commenced Coring at 3.3m                                                                                                                       | 3.3       |             |            |          |

|                       |                                   |                                                                     |
|-----------------------|-----------------------------------|---------------------------------------------------------------------|
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| Easting : 330828,69   | Driller Supplier : GEOSENSE       | Client : Landmark Group Construction Australia Pty Ltd              |
| Northing : 6261173,80 | Logged By : Ozzie Baskan          | Project : Lindfield                                                 |
| RL : 83.80(m)         | Reviewed By : Mahmoud Jangidaryan | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth : 18 m    | Date : 28/02/2025                 | Loc Comment : Driveway of 1B Valley road.                           |

| Drilling Method                      | Water | Well Diagram | Elevation | Graphic Log | Classification Code | Material Description                                                                                                     | Depth (m) | Weathering | Testing         | Estimated Strength                            | RQD% and TCR%             | Defect Spacing (mm)              | Defect Description             |
|--------------------------------------|-------|--------------|-----------|-------------|---------------------|--------------------------------------------------------------------------------------------------------------------------|-----------|------------|-----------------|-----------------------------------------------|---------------------------|----------------------------------|--------------------------------|
|                                      |       |              | Depth (m) |             |                     |                                                                                                                          |           |            | Is(50)          |                                               |                           |                                  |                                |
|                                      |       | C            |           |             |                     |                                                                                                                          |           |            |                 | VLS 0.1<br>LS 0.3<br>MS 1.0<br>HS 3<br>EPS 10 |                           | 30<br>100<br>300<br>1000<br>3000 |                                |
|                                      |       |              |           |             |                     |                                                                                                                          | 1         |            |                 |                                               |                           |                                  |                                |
|                                      |       |              |           |             |                     |                                                                                                                          | 2         |            |                 |                                               |                           |                                  |                                |
|                                      |       |              |           |             |                     |                                                                                                                          | 3         |            |                 |                                               |                           |                                  |                                |
|                                      |       |              |           |             |                     | Commenced Coring at 3.3m                                                                                                 |           |            |                 |                                               |                           |                                  |                                |
| NMLC Coring<br>Loss - 20% Water Loss |       |              | 80.3      |             | SST                 | Rock SANDSTONE: highly weathered, very low strength, pale brown white pale grey red, fine grained, with ironstone bands. | 3.55      | MW         | d:0.02 ; a:0.02 |                                               | RQD = 84.52%<br>TCR = 95% |                                  | 3.3-3.5, XWS, 5°,              |
|                                      |       |              | 3.55      |             | SST                 | Rock SANDSTONE: moderately weathered, medium strength, red mottled white, fine to medium grained, iron staining.         |           |            | d:0.73 ; a:0.77 |                                               |                           |                                  | 3.7-3.78, XWS,                 |
|                                      |       |              |           |             |                     |                                                                                                                          |           |            |                 |                                               |                           |                                  | 3.92, J, 30°, PL, RO, STN, OP, |

|                       |                                   |                                                                     |
|-----------------------|-----------------------------------|---------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : GEO205 - Comacchio  | Job Number : P3444                                                  |
| Easting : 330828,69   | Driller Supplier : GEOSENSE       | Client : Landmark Group Construction Australia Pty Ltd              |
| Northing : 6261173,80 | Logged By : Ozzie Baskan          | Project : Lindfield                                                 |
| RL : 83.80(m)         | Reviewed By : Mahmoud Jangidaryan | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth : 18 m    | Date : 28/02/2025                 | Loc Comment : Driveway of 1B Valley road.                           |

| Drilling Method | Water                            | Well Diagram                | Elevation    | Graphic Log | Classification Code | Material Description                                                                                                          | Depth (m) | Weathering | Testing         | Estimated Strength                           | RQD% and TCR%             | Defect Spacing (mm)                             | Defect Description                                                                                                                                                                                          |
|-----------------|----------------------------------|-----------------------------|--------------|-------------|---------------------|-------------------------------------------------------------------------------------------------------------------------------|-----------|------------|-----------------|----------------------------------------------|---------------------------|-------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
|                 |                                  |                             | Depth (m)    |             |                     |                                                                                                                               |           |            | Is(50)          |                                              |                           |                                                 |                                                                                                                                                                                                             |
|                 |                                  |                             |              |             |                     |                                                                                                                               |           |            |                 |                                              |                           |                                                 |                                                                                                                                                                                                             |
| NMLC Coring     | <div>Loss - 10% Water Loss</div> | <div>50mm PVC Slotted</div> |              |             | SST                 | Rock SANDSTONE: moderately weathered, medium strength, red mottled white, fine to medium grained, iron staining.              |           | MW         |                 | VS 0.1<br>VS 0.3<br>HS 1.0<br>VS 3<br>EHS 10 | RQD = 84.52%<br>TCR = 95% | <div>30<br/>100<br/>300<br/>1000<br/>3000</div> | 4.09, P, 5°, IR, RO, STN, OP,<br>4.18-4.23, XWS,<br><br><br><br><br><br>4.85, P, 5°, UN, RO, STN, OP,<br>5.02-5.05, XWS,<br><br><br><br>5.77-5.79, XWS,<br>5.89-5.9, XWS,<br>6.02, J, 10°, IR, RO, STN, OP, |
|                 |                                  |                             | 78.7<br>5.06 |             | SST                 | Rock SANDSTONE: moderately weathered, medium strength, pale grey mottled red, fine to medium grained, iron staining.          | 5<br>5.06 | MW         | d:0.44 ; a:0.38 |                                              |                           |                                                 |                                                                                                                                                                                                             |
|                 |                                  |                             | 78.4<br>5.4  |             | SST                 | Rock SANDSTONE: moderately weathered, medium strength, pale red mottled white, fine to medium grained, iron staining.         | 5.4       | MW         |                 |                                              |                           |                                                 |                                                                                                                                                                                                             |
|                 |                                  |                             | 77.8<br>6.03 |             | SST                 | Rock SANDSTONE: moderately weathered, medium strength, pale grey, fine to medium grained, ..                                  | 6.03      | MW         | d:0.76 ; a:0.76 |                                              |                           |                                                 |                                                                                                                                                                                                             |
|                 |                                  |                             | 77.4<br>6.4  |             | CRL                 | Core loss                                                                                                                     | 6.4       |            |                 |                                              |                           |                                                 |                                                                                                                                                                                                             |
|                 |                                  |                             | 77.3<br>6.55 |             | SST                 | Rock SANDSTONE: slightly to fresh weathered, high strength, pale grey, fine to medium grained, with carbonaceous laminations. | 6.55      | SW-F       | d:0.71 ; a:1.04 |                                              |                           |                                                 |                                                                                                                                                                                                             |
|                 |                                  |                             |              |             |                     |                                                                                                                               | 7         |            |                 |                                              |                           |                                                 |                                                                                                                                                                                                             |
|                 |                                  |                             |              |             |                     |                                                                                                                               |           |            |                 |                                              |                           |                                                 |                                                                                                                                                                                                             |
|                 |                                  |                             |              |             |                     |                                                                                                                               |           |            |                 |                                              |                           |                                                 |                                                                                                                                                                                                             |
|                 |                                  |                             |              |             |                     |                                                                                                                               |           |            |                 |                                              |                           |                                                 |                                                                                                                                                                                                             |
|                 |                                  |                             |              |             |                     |                                                                                                                               |           |            |                 |                                              |                           |                                                 |                                                                                                                                                                                                             |



|                       |                                   |                                                                     |
|-----------------------|-----------------------------------|---------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : GEO205 - Comacchio  | Job Number : P3444                                                  |
| Easting : 330828,69   | Driller Supplier : GEOSENSE       | Client : Landmark Group Construction Australia Pty Ltd              |
| Northing : 6261173,80 | Logged By : Ozzie Baskan          | Project : Lindfield                                                 |
| RL : 83.80(m)         | Reviewed By : Mahmoud Jangidaryan | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth : 18 m    | Date : 28/02/2025                 | Loc Comment : Driveway of 1B Valley road.                           |

| Drilling Method | Water                    | Well Diagram         | Elevation | Graphic Log | Classification Code | Material Description                                                                                                          | Depth (m) | Weathering | Testing         | Estimated Strength                            | RQD% and TCR%            | Defect Spacing (mm)                                                     | Defect Description             |
|-----------------|--------------------------|----------------------|-----------|-------------|---------------------|-------------------------------------------------------------------------------------------------------------------------------|-----------|------------|-----------------|-----------------------------------------------|--------------------------|-------------------------------------------------------------------------|--------------------------------|
|                 |                          |                      | Depth (m) |             |                     |                                                                                                                               |           |            | Is(50)          |                                               |                          |                                                                         |                                |
| <br>NMLC Coring | <br>Loss - 0% Water Loss | <br>50mm PVC Slotted |           | <br>SST     |                     | Rock SANDSTONE: slightly to fresh weathered, high strength, pale grey, fine to medium grained, with carbonaceous laminations. |           | SW-F       |                 | VLS 0.1<br>LS 0.3<br>MS 1.0<br>HS 3<br>EPS 10 | RQD = 95%<br>TCR = 95%   | <br>8.13, P, 10°, PL, RO, CL, OP, (X2),<br>8.36, P, 5°, PL, RO, CT, OP, |                                |
|                 |                          |                      |           |             |                     |                                                                                                                               |           |            | d:1.52 ; a:1.74 |                                               |                          |                                                                         |                                |
|                 |                          |                      |           |             |                     |                                                                                                                               | 9         |            |                 |                                               |                          |                                                                         |                                |
|                 |                          |                      |           |             |                     |                                                                                                                               | 10        |            | d:1.43 ; a:1.60 |                                               |                          |                                                                         |                                |
|                 |                          |                      |           |             |                     |                                                                                                                               | 11        |            | d:1.38 ; a:1.38 |                                               |                          |                                                                         |                                |
|                 |                          |                      |           |             |                     |                                                                                                                               |           |            | d:1.5 ; a:1.67  |                                               | RQD = 100%<br>TCR = 100% |                                                                         | 10.48, J, 30°, PL, SO, VN, OP, |
|                 |                          |                      |           |             |                     |                                                                                                                               |           |            |                 |                                               |                          |                                                                         | 11.89, P, 5°, IR, RO, CT, OP,  |

|                       |                                   |                                                                     |
|-----------------------|-----------------------------------|---------------------------------------------------------------------|
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| Easting : 330828,69   | Driller Supplier : GEOSENSE       | Client : Landmark Group Construction Australia Pty Ltd              |
| Northing : 6261173,80 | Logged By : Ozzie Baskan          | Project : Lindfield                                                 |
| RL : 83.80(m)         | Reviewed By : Mahmoud Jangidaryan | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth : 18 m    | Date : 28/02/2025                 | Loc Comment : Driveway of 1B Valley road.                           |

| Drilling Method            | Water                           | Well Diagram                | Elevation | Graphic Log | Classification Code | Material Description                                                                                                          | Depth (m)       | Weathering | Testing                  |                                                              | Estimated Strength       | RQD% and TCR%                                   | Defect Spacing (mm)            | Defect Description                  |
|----------------------------|---------------------------------|-----------------------------|-----------|-------------|---------------------|-------------------------------------------------------------------------------------------------------------------------------|-----------------|------------|--------------------------|--------------------------------------------------------------|--------------------------|-------------------------------------------------|--------------------------------|-------------------------------------|
|                            |                                 |                             | Depth (m) |             |                     |                                                                                                                               |                 |            | Is(50)                   |                                                              |                          |                                                 |                                |                                     |
|                            |                                 |                             |           |             |                     |                                                                                                                               |                 |            |                          |                                                              |                          |                                                 |                                |                                     |
| <div>↑ NMLC Coring ↓</div> | <div>Loss - 0% Water Loss</div> | <div>50mm PVC Slotted</div> |           | <div></div> | SST                 | Rock SANDSTONE: slightly to fresh weathered, high strength, pale grey, fine to medium grained, with carbonaceous laminations. | 13              | SW-F       | d:1.39 ; a:2.30          | <div>VLS 0.1<br/>LS 0.3<br/>MS 1.0<br/>HS 3<br/>EHS 10</div> | RQD = 100%<br>TCR = 100% | <div>30<br/>100<br/>300<br/>1000<br/>3000</div> | 13.11, J, 10°, PL, RO, VN, OP, |                                     |
|                            |                                 |                             | 14        |             |                     |                                                                                                                               | d:1.51 ; a:1.63 |            | RQD = 100%<br>TCR = 100% |                                                              |                          |                                                 |                                | 13.65, J, 5°, IR, RO, CT, OP, (X2), |
|                            |                                 |                             | 15        |             |                     |                                                                                                                               | d:1.58 ; a:2.09 |            |                          |                                                              |                          |                                                 |                                |                                     |
|                            |                                 |                             |           |             |                     |                                                                                                                               |                 |            | d:1.69 ; a:1.93          |                                                              |                          |                                                 |                                | RQD = 100%<br>TCR = 100%            |

|                       |                                   |                                                                     |
|-----------------------|-----------------------------------|---------------------------------------------------------------------|
| UTM : 56S             | Driller Rig : GEO205 - Comacchio  | Job Number : P3444                                                  |
| Easting : 330828,69   | Driller Supplier : GEOSENSE       | Client : Landmark Group Construction Australia Pty Ltd              |
| Northing : 6261173,80 | Logged By : Ozzie Baskan          | Project : Lindfield                                                 |
| RL : 83.80(m)         | Reviewed By : Mahmoud Jangidaryan | Location : 59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW |
| Total Depth : 18 m    | Date : 28/02/2025                 | Loc Comment : Driveway of 1B Valley road.                           |

| Drilling Method | Water | Well Diagram | Elevation | Graphic Log | Classification Code | Material Description                                                                                                          | Depth (m) | Weathering | Testing         | Estimated Strength | RQD% and TCR%            | Defect Spacing (mm) | Defect Description             |
|-----------------|-------|--------------|-----------|-------------|---------------------|-------------------------------------------------------------------------------------------------------------------------------|-----------|------------|-----------------|--------------------|--------------------------|---------------------|--------------------------------|
|                 |       |              | Depth (m) |             |                     |                                                                                                                               |           |            | Is(50)          |                    |                          |                     |                                |
|                 |       |              |           |             |                     | Rock SANDSTONE: slightly to fresh weathered, high strength, pale grey, fine to medium grained, with carbonaceous laminations. | 17        | SW-F       | d:1.70 ; a:1.73 |                    | RQD = 100%<br>TCR = 100% |                     | 17.33, P, 30°, PL, RO, CL, OP, |
|                 |       |              |           |             |                     |                                                                                                                               |           |            | d:2.17 ; a:2.32 |                    |                          |                     |                                |
|                 |       |              |           |             |                     | BH5 Reached Target Depth at 18m                                                                                               |           |            |                 |                    |                          |                     |                                |

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CLIENT NAME: LANDMARK

PROJECT:

LOCATION: 63 Trafalgar Ave, Lindfield

JOB NUMBER: P3444

LOGGED BY: Ozzie B.

BOREHOLE ID: BH5

DEPTH: 3.3m to 8.0m

CORE TRAY: 1 of 3

DATE: 28/03/2025



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02 8599 7579



Sydney Gadigal Land,  
2/5-7 Malta Street, Fairfield  
East NSW 2155



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## Photo description

BH5 - Box 1 of 3

## Client

Landmark Group Construction Australia Pty Ltd

## Location

59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW

## Project name

Lindfield

## Project No

P3444

## Scale

Not to Scale

## BH No

BH5

## BH Depth

CorePhoto



# morrow

CLIENT NAME: LANDMARK

PROJECT:

LOCATION: 63 Trafalgar Ave, Lindfield

JOB NUMBER: P3444

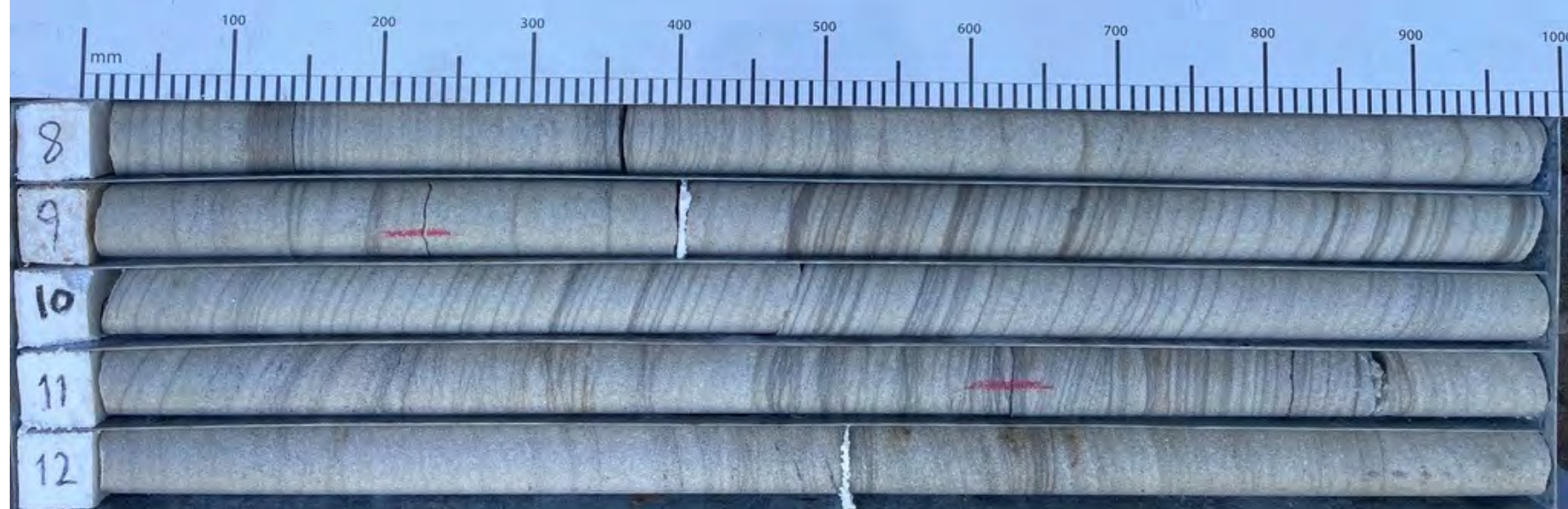
LOGGED BY: Ozzie B.

BOREHOLE ID: BH5

DEPTH: 8m to 13m

CORE TRAY: 2 of 3

DATE: 28/02/2025



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02 8599 7579



Sydney Gadigal Land,  
2/5-7 Malta Street, Fairfield  
East NSW 2155



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## Photo description

BH5 - Box 2 of 3

## Client

Landmark Group Construction Australia Pty Ltd

## Location

59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW

## Project name

Lindfield

## Project No

P3444

## Scale

Not to Scale

## BH No

BH5

## BH Depth

CorePhoto



# morrow

CLIENT NAME: LANDMARK

PROJECT:

LOCATION: 63 Trafalgar Ave, Lindfield

JOB NUMBER: P3444

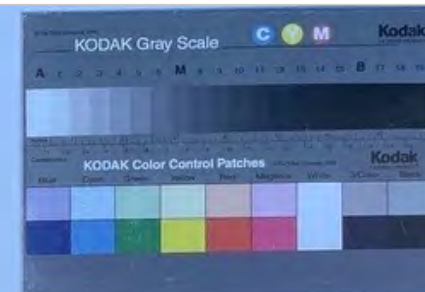
LOGGED BY: Ozzie B.

BOREHOLE ID: BH5

DEPTH: 13m to 18m

CORE TRAY: 3 of 3

DATE: 28/03/2025



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Sydney Gadigal Land,  
2/5-7 Malta Street, Fairfield  
East NSW 2155



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## Photo description

BH5 - Box 3 of 3

## Client

Landmark Group Construction Australia Pty Ltd

## Location

59-63 Trafalgar Avenue & 1A/B Valley Road, Lindfield NSW

## Project name

Lindfield

## Project No

P3444

## Scale

Not to Scale

## BH No

BH5

## BH Depth

CorePhoto

## GENERAL

Information obtained from site investigations is recorded on log sheets. The "Cored Drill Hole Log" presents data from an operation where a core barrel has been used to recover material - commonly rock. The "Non-Core Drill Hole - Geological Log" presents data from an operation where coring has not been used and information is based on a combination of regular sampling and insitu testing. The material penetrated in non-core drilling is commonly soil but may include rock. The "Excavation - Geological Log" presents data and drawings from exposures of soil and rock resulting from excavation of pits, trenches, etc.

The heading of the log sheets contains information on Project Identification, Hole or Pit Identification, Location and Elevation. The main section of the logs contains information on methods and conditions, material substance description and structure presented as a series of columns in relation to depth below the ground surface which is plotted on the left side of the log sheet. The common depth scale is 8m per drill log sheet and about 3-5m for excavation logs sheets.

As far as is practicable the data contained on the log sheets is factual. Some interpretation is inevitable in the identification of material boundaries in areas of partial sampling, the location of areas of core loss, description and classification of material, estimation of strength and identification of drilling induced fractures. Material description and classifications are based on SAA Site Investigation Code AS 1726 - 1993 with some modifications as defined below.

These notes contain an explanation of the terms and abbreviations commonly used on the log sheets.

## DRILLING

### Drilling & Casing

|      |                            |
|------|----------------------------|
| ADV  | Auger Drilling with V-Bit  |
| ADT  | Auger Drilling with TC Bit |
| WB   | Wash-bore drilling         |
| RR   | Rock Roller                |
| NMLC | NMLC core barrel           |
| NQ   | NQ core barrel             |
| HMLC | HMLC core barrel           |
| HQ   | HQ core barrel             |

### Drilling Fluid/Water

The drilling fluid used is identified and loss of return to the surface estimated as a percentage.

### Drilling Penetration/Drill Depth

Core lifts are identified by a line and depth with core loss per run as a percentage. Ease of penetration in non-core drilling is abbreviated as follows:

|    |           |
|----|-----------|
| VE | Very Easy |
| E  | Easy      |
| M  | Medium    |
| H  | High      |
| VH | Very High |

## Groundwater Levels

Date of measurement is shown.

Standing water level measured in completed boreholeLevel taken during or immediately after drilling

|     |                              |
|-----|------------------------------|
| D   | Disturbed                    |
| B   | Bulk                         |
| U   | Undisturbed                  |
| SPT | Standard Penetration Test    |
| N   | Result of SPT (sample taken) |
| PBT | Plate Bearing Test           |
| PZ  | Piezometer Installation      |
| HP  | Hand Penetrometer Test       |

## EXCAVATION LOGS

Explanatory notes are provided at the bottom of drill log sheets. Information about the origin, geology and pedology may be entered in the "Structure and other Observations" column. The depth of the base of excavation (for the logged section) at the appropriate depth in the "Material Description" column. Refusal of excavation plant is noted should it occur. A sketch of the exposure may be added.

## MATERIAL DESCRIPTION – SOIL

Classification Symbol - In accordance with the Unified Classification System (AS 1726-1993, Appendix A, Table A1)

Material Description - In accordance with AS 1726-1993, Appendix A2.3

### Moisture Condition

|   |                                    |
|---|------------------------------------|
| D | Dry, looks and feels dry           |
| M | Moist, No free water on remoulding |
| W | Wet, free water on remoulding      |

Consistency - In accordance with AS 1726-1993, Appendix A2.5

|     |            |               |
|-----|------------|---------------|
| VS  | Very Soft  | < 12.5 kPa    |
| S   | Soft       | 12.5 – 25 kPa |
| F   | Firm       | 25 – 50 kPa   |
| St  | Stiff      | 50 – 100 kPa  |
| VSt | Very Stiff | 100 – 200 kPa |
| H   | Hard       | > 200 kPa     |

Strength figures quoted are the approximate range of undrained shear strength for each class.

Density Index. (%) is estimated or is based on SPT results.

|    |              |           |
|----|--------------|-----------|
| VL | Very Loose   | < 15 %    |
| L  | Loose        | 15 – 35 % |
| MD | Medium Dense | 35 – 65 % |
| D  | Dense        | 65 – 85 % |
| VD | Very Dense   | > 85 %    |

## MATERIAL DESCRIPTION -ROCK

### Material Description

Identification of rock type, composition and texture based on visual features in accordance with AS 1726-1993, Appendix A3.1-A3.3 and Tables A6a, A6b and A7.

## Core Loss

Is shown at the bottom of the run unless otherwise indicated.

## Bedding

|                     |            |
|---------------------|------------|
| Thinly Laminated    | < 6 mm     |
| Laminated           | 6 - 20     |
| Very Thinly Bedded  | 20 - 60    |
| Thinly Bedded       | 60 - 200   |
| Medium Bedded       | 200 - 600  |
| Thickly Bedded      | 600 - 2000 |
| Very Thickly Bedded | > 2000     |

**Weathering** - No distinction is made between weathering and alteration. Weathering classification assists in identification but does not imply engineering properties.

|                           |                                                                                                     |
|---------------------------|-----------------------------------------------------------------------------------------------------|
| Fresh (F)                 | Rock substance unaffected by weathering                                                             |
| Slightly Weathered (SW)   | Rock substance partly stained or discoloured. Colour and texture of fresh rock recognisable.        |
| Moderately Weathered (MW) | Staining or discolouration extends throughout rock substance. Fresh rock colour not recognisable.   |
| Highly Weathered (HW)     | Stained or discoloured throughout. Signs of chemical or physical alteration. Rock texture retained. |
| Extremely Weathered (EW)  | Rock texture evident but material has soil properties and can be remoulded.                         |

**Strength** - The following terms are used to described rock strength:

| Rock Strength Class | Abbreviation | Point Load Strength Index, Is(50) (MPa) |
|---------------------|--------------|-----------------------------------------|
| Extremely Low       | EL           | < 0.03                                  |
| Very Low            | VL           | 0.03 to 0.1                             |
| Low                 | L            | 0.1 to 0.3                              |
| Medium              | M            | 0.3 to 1                                |
| High                | H            | 1 to 3                                  |
| Very High           | VH           | 3 to 10                                 |
| Extremely High      | EH           | ≥ 10                                    |

Strengths are estimated and where possible supported by Point Load Index Testing of representative samples. Test results are plotted on the graphical estimated strength by using:

Diametral Point Load Test

Axial Point Load Test

Where the estimated strength log covers more than one range it indicates the rock strength varies between the limits shown.

## MATERIALS STRUCTURE/FRACTURES

### ROCK

Natural Fracture Spacing - A plot of average fracture spacing excluding defects known or suspected to be due to drilling, core boxing or testing. Closed or cemented joints, drilling breaks and handling breaks are not included in the Natural Fracture Spacing.

Visual Log - A diagrammatic plot of defects showing type, spacing and orientation in relation to core axis.

| Defects |                                                                                                                                                                                                                                              | Defects open in-situ or clay sealed<br>Defects closed in-situ<br>Breaks through rock substance |
|---------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------|
|         | <div style="border-bottom: 1px solid black; width: 50px; margin-bottom: 2px;"></div> <div style="border-bottom: 1px dashed black; width: 50px; margin-bottom: 2px;"></div> <div style="border-bottom: 1px dotted black; width: 50px;"></div> |                                                                                                |

Additional Data - Description of individual defects by type, orientation, in-filling, shape and roughness in accordance with AS 1726-1993, Appendix A Table A10, notes and Figure A2.

Orientation - angle relative to the plane normal to the core axis.

| Type      | BP<br>JT<br>SM<br>FZ<br>SZ<br>VN<br>FL<br>CL<br>DL<br>HB<br>DB | Bedding Parting<br>Joint<br>Seam<br>Fracture Zone<br>Shear Zone<br>Vein<br>Foliation<br>Cleavage<br>Drill Lift<br>Handling Break<br>Drilling Break |
|-----------|----------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------|
| Infilling | CN<br>X<br>Clay<br>KT<br>CA<br>Fe<br>Qz<br>MS<br>MU            | Clean<br>Carbonaceous<br>Clay<br>Chlorite<br>Calcite<br>Iron Oxide<br>Quartz<br>Secondary Mineral<br>Unidentified Mineral                          |
| Shape     | PR<br>CU<br>UN<br>ST<br>IR<br>DIS                              | Planar<br>Curved<br>Undulose<br>Stepped<br>Irregular<br>Discontinuous                                                                              |
| Roughness | POL<br>SL<br>S<br>RF<br>VR                                     | Polished<br>Slicksided<br>Smooth<br>Rough<br>Very Rough                                                                                            |

### SOIL

Structures - Fissuring and other defects are described in accordance with AS 1726-1993, Appendix A2.6, using the terminology for rock defects.

Origin - Where practicable an assessment is provided of the probable origin of the soil, eg fill, topsoil, alluvium, colluvium, residual soil

## **APPENDIX B**

# **WATER QUALITY LABORATORY TESTING CERTIFICATES**

## CLIENT DETAILS

Contact **Andrew Butel**  
 Client **MORROW GEOTECHNICS PTY LTD**  
 Address **79/6 Bellambi Lane  
 Bellambi  
 NSW 2518**

Telephone (Not specified)  
 Facsimile (Not specified)  
 Email **andy@morrowgeo.com.au**

Project **P3444 Lindfield**  
 Order Number **P3444**  
 Samples **3**

## LABORATORY DETAILS

Manager **Shane McDermott**  
 Laboratory **SGS Alexandria Environmental**  
 Address **Unit 16, 33 Maddox St  
 Alexandria NSW 2015**

Telephone **+61 2 8594 0400**  
 Facsimile **+61 2 8594 0499**  
 Email **au.environmental.sydney@sgs.com**

SGS Reference **SE280753 R0**  
 Date Received **2/4/2025**  
 Date Reported **9/4/2025**

## COMMENTS

Accredited for compliance with ISO/IEC 17025 - Testing. NATA accredited laboratory 2562(4354).

## SIGNATORIES



**Akheeqar BENIAMEEN**  
 Chemist



**Dong LIANG**  
 Metals/Inorganics Team Leader



**Ly Kim HA**  
 Organic Section Head



**Shane MCDERMOTT**  
 Laboratory Manager



VOCs in Water [AN433]    Tested: 7/4/2025

| PARAMETER          | UOM  | LOR | BH1                                        | BH2                                        | BH5                                        |
|--------------------|------|-----|--------------------------------------------|--------------------------------------------|--------------------------------------------|
|                    |      |     | WATER<br>-<br>2/4/25 11:00<br>SE280753.001 | WATER<br>-<br>2/4/25 11:00<br>SE280753.002 | WATER<br>-<br>2/4/25 11:00<br>SE280753.003 |
| Benzene            | µg/L | 0.5 | <0.5                                       | <0.5                                       | <0.5                                       |
| Toluene            | µg/L | 0.5 | <0.5                                       | <b>0.5</b>                                 | <0.5                                       |
| Ethylbenzene       | µg/L | 0.5 | <0.5                                       | <0.5                                       | <0.5                                       |
| m/p-xylene         | µg/L | 1   | <1                                         | <1                                         | <1                                         |
| o-xylene           | µg/L | 0.5 | <0.5                                       | <0.5                                       | <0.5                                       |
| Total Xylenes      | µg/L | 1.5 | <1.5                                       | <1.5                                       | <1.5                                       |
| Total BTEX         | µg/L | 3   | <3                                         | <3                                         | <3                                         |
| Naphthalene (VOC)* | µg/L | 0.5 | <0.5                                       | <0.5                                       | <0.5                                       |

Volatile Petroleum Hydrocarbons in Water [AN433]    Tested: 7/4/2025

| PARAMETER                  | UOM  | LOR | BH1                          | BH2                          | BH5                          |
|----------------------------|------|-----|------------------------------|------------------------------|------------------------------|
|                            |      |     | WATER                        | WATER                        | WATER                        |
|                            |      |     | -                            | -                            | -                            |
|                            |      |     | 2/4/25 11:00<br>SE280753.001 | 2/4/25 11:00<br>SE280753.002 | 2/4/25 11:00<br>SE280753.003 |
| TRH C6-C9                  | µg/L | 40  | <40                          | <40                          | <40                          |
| Benzene (F0)               | µg/L | 0.5 | <0.5                         | <0.5                         | <0.5                         |
| TRH C6-C10                 | µg/L | 50  | <50                          | <50                          | <50                          |
| TRH C6-C10 minus BTEX (F1) | µg/L | 50  | <50                          | <50                          | <50                          |

TRH (Total Recoverable Hydrocarbons) in Water [AN403]    Tested: 7/4/2025

| PARAMETER                       | UOM  | LOR | BH1                                        | BH2                                        | BH5                                        |
|---------------------------------|------|-----|--------------------------------------------|--------------------------------------------|--------------------------------------------|
|                                 |      |     | WATER<br>-<br>2/4/25 11:00<br>SE280753.001 | WATER<br>-<br>2/4/25 11:00<br>SE280753.002 | WATER<br>-<br>2/4/25 11:00<br>SE280753.003 |
| TRH C10-C14                     | µg/L | 50  | <b>57</b>                                  | <50                                        | <50                                        |
| TRH C15-C28                     | µg/L | 200 | <200                                       | <b>470</b>                                 | <200                                       |
| TRH C29-C36                     | µg/L | 200 | <200                                       | <b>470</b>                                 | <200                                       |
| TRH C37-C40                     | µg/L | 200 | <200                                       | <200                                       | <200                                       |
| TRH >C10-C16                    | µg/L | 60  | <b>67</b>                                  | <60                                        | <60                                        |
| TRH >C10-C16 - Naphthalene (F2) | µg/L | 60  | <b>67</b>                                  | <60                                        | <60                                        |
| TRH >C16-C34 (F3)               | µg/L | 500 | <500                                       | <b>790</b>                                 | <500                                       |
| TRH >C34-C40 (F4)               | µg/L | 500 | <500                                       | <500                                       | <500                                       |
| TRH C10-C40                     | µg/L | 320 | <320                                       | <b>1100</b>                                | <320                                       |

## PAH (Polynuclear Aromatic Hydrocarbons) in Water [AN420]    Tested: 7/4/2025

| PARAMETER              | UOM  | LOR | BH1                                        | BH2                                        | BH5                                        |
|------------------------|------|-----|--------------------------------------------|--------------------------------------------|--------------------------------------------|
|                        |      |     | WATER<br>-<br>2/4/25 11:00<br>SE280753.001 | WATER<br>-<br>2/4/25 11:00<br>SE280753.002 | WATER<br>-<br>2/4/25 11:00<br>SE280753.003 |
| Naphthalene            | µg/L | 0.1 | <0.1                                       | <0.1                                       | <0.1                                       |
| 2-methylnaphthalene    | µg/L | 0.1 | <0.1                                       | <0.1                                       | <0.1                                       |
| 1-methylnaphthalene    | µg/L | 0.1 | <0.1                                       | <0.1                                       | <0.1                                       |
| Acenaphthylene         | µg/L | 0.1 | <0.1                                       | <0.1                                       | <0.1                                       |
| Acenaphthene           | µg/L | 0.1 | <0.1                                       | <0.1                                       | <0.1                                       |
| Fluorene               | µg/L | 0.1 | <0.1                                       | <0.1                                       | <0.1                                       |
| Phenanthrene           | µg/L | 0.1 | <0.1                                       | <0.1                                       | <0.1                                       |
| Anthracene             | µg/L | 0.1 | <0.1                                       | <0.1                                       | <0.1                                       |
| Fluoranthene           | µg/L | 0.1 | <0.1                                       | <0.1                                       | <0.1                                       |
| Pyrene                 | µg/L | 0.1 | <0.1                                       | <0.1                                       | <0.1                                       |
| Benzo(a)anthracene     | µg/L | 0.1 | <0.1                                       | <0.1                                       | <0.1                                       |
| Chrysene               | µg/L | 0.1 | <0.1                                       | <0.1                                       | <0.1                                       |
| Benzo(b&j)fluoranthene | µg/L | 0.1 | <0.1                                       | <0.1                                       | <0.1                                       |
| Benzo(k)fluoranthene   | µg/L | 0.1 | <0.1                                       | <0.1                                       | <0.1                                       |
| Benzo(a)pyrene         | µg/L | 0.1 | <0.1                                       | <0.1                                       | <0.1                                       |
| Indeno(1,2,3-cd)pyrene | µg/L | 0.1 | <0.1                                       | <0.1                                       | <0.1                                       |
| Dibenzo(ah)anthracene  | µg/L | 0.1 | <0.1                                       | <0.1                                       | <0.1                                       |
| Benzo(ghi)perylene     | µg/L | 0.1 | <0.1                                       | <0.1                                       | <0.1                                       |
| Total PAH (18)         | µg/L | 1   | <1                                         | <1                                         | <1                                         |

Anions by Ion Chromatography in Water [AN245]    Tested: 4/4/2025

| PARAMETER               | UOM  | LOR   | BH1                          | BH2                          | BH5                          |
|-------------------------|------|-------|------------------------------|------------------------------|------------------------------|
|                         |      |       | WATER                        | WATER                        | WATER                        |
|                         |      |       | -                            | -                            | -                            |
|                         |      |       | 2/4/25 11:00<br>SE280753.001 | 2/4/25 11:00<br>SE280753.002 | 2/4/25 11:00<br>SE280753.003 |
| Chloride                | mg/L | 1     | <b>380</b>                   | <b>110</b>                   | <b>470</b>                   |
| Sulfate, SO4            | mg/L | 1     | <b>200</b>                   | <b>72</b>                    | <b>94</b>                    |
| Nitrate Nitrogen, NO3-N | mg/L | 0.005 | <0.005                       | -                            | -                            |
| Fluoride                | mg/L | 0.1   | <b>0.48</b>                  | -                            | -                            |
| Bromide                 | mg/L | 0.05  | <b>1.9</b>                   | -                            | -                            |





ANALYTICAL RESULTS

SE280753 R0

pH in water [AN101]    Tested: 2/4/2025

|           |         |     | BH1          | BH2          | BH5          |
|-----------|---------|-----|--------------|--------------|--------------|
|           |         |     | WATER        | WATER        | WATER        |
|           |         |     | -            | -            | -            |
|           |         |     | 2/4/25 11:00 | 2/4/25 11:00 | 2/4/25 11:00 |
|           |         |     | SE280753.001 | SE280753.002 | SE280753.003 |
| PARAMETER | UOM     | LOR |              |              |              |
| pH**      | No unit | -   | 5.9          | 6.3          | 4.7          |



ANALYTICAL RESULTS

SE280753 R0

Conductivity and TDS by Calculation - Water [AN106]    Tested: 2/4/2025

|                                         |       |     | BH1          | BH2          | BH5          |
|-----------------------------------------|-------|-----|--------------|--------------|--------------|
|                                         |       |     | WATER        | WATER        | WATER        |
|                                         |       |     | -            | -            | -            |
|                                         |       |     | 2/4/25 11:00 | 2/4/25 11:00 | 2/4/25 11:00 |
|                                         |       |     | SE280753.001 | SE280753.002 | SE280753.003 |
| PARAMETER                               | UOM   | LOR |              |              |              |
| Conductivity @ 25 C                     | µS/cm | 2   | 1300         | 440          | 1200         |
| Total Dissolved Solids (by calculation) | mg/L  | 2   | 800          | 270          | 750          |

Alkalinity [AN135] Tested: 7/4/2025

| PARAMETER                                          | UOM   | LOR  | BH1                          | BH2                          | BH5                          |
|----------------------------------------------------|-------|------|------------------------------|------------------------------|------------------------------|
|                                                    |       |      | WATER                        | WATER                        | WATER                        |
|                                                    |       |      | -                            | -                            | -                            |
|                                                    |       |      | 2/4/25 11:00<br>SE280753.001 | 2/4/25 11:00<br>SE280753.002 | 2/4/25 11:00<br>SE280753.003 |
| Bicarbonate Alkalinity as CaCO <sub>3</sub>        | mg/L  | 5    | <b>69</b>                    | <b>86</b>                    | <5                           |
| Carbonate Alkalinity as CaCO <sub>3</sub>          | mg/L  | 1    | <1                           | <1                           | <1                           |
| Hydroxide Alkalinity as CaCO <sub>3</sub>          | mg/L  | 5    | <5                           | <5                           | <5                           |
| Phenolphthalein Alkalinity as CaCO <sub>3</sub> *  | mg/L  | 5    | <5                           | <5                           | <5                           |
| Total Alkalinity as CaCO <sub>3</sub>              | mg/L  | 5    | <b>69</b>                    | <b>86</b>                    | <5                           |
| Hydroxide Alkalinity as OH (meq/L)                 | meq/L | 0.06 | <0.06                        | <0.06                        | <0.06                        |
| Bicarbonate Alkalinity as HCO <sub>3</sub> (meq/L) | meq/L | 0.03 | <b>1.4</b>                   | <b>1.7</b>                   | <0.03                        |
| Carbonate Alkalinity as CO <sub>3</sub> (meq/L)    | meq/L | 0.03 | <0.03                        | <0.03                        | <0.03                        |



ANALYTICAL RESULTS

SE280753 R0

Acidity and Free CO2 [AN140]    Tested: 8/4/2025

|                   |            |     | BH2          | BH5          |
|-------------------|------------|-----|--------------|--------------|
|                   |            |     | WATER        | WATER        |
|                   |            |     | -            | -            |
|                   |            |     | 2/4/25 11:00 | 2/4/25 11:00 |
|                   |            |     | SE280753.002 | SE280753.003 |
| PARAMETER         | UOM        | LOR |              |              |
| Acidity to pH 8.3 | mg CaCO3/L | 5   | 91           | 110          |



ANALYTICAL RESULTS

SE280753 R0

Nitrite in Water [AN277]    Tested: 2/4/2025

|                                |      |       | BH1          |
|--------------------------------|------|-------|--------------|
|                                |      |       | WATER        |
|                                |      |       | -            |
|                                |      |       | 2/4/25 11:00 |
| PARAMETER                      | UOM  | LOR   | SE280753.001 |
| Nitrite Nitrogen, NO2 as N     | mg/L | 0.005 | <0.005       |
| Total Oxidised Nitrogen, NOx-N | mg/L | 0.005 | <0.005       |





ANALYTICAL RESULTS

SE280753 R0

TKN Kjeldahl Digestion by Discrete Analyser [AN292]    Tested: 8/4/2025

|                         |      |      | BH1          |
|-------------------------|------|------|--------------|
|                         |      |      | WATER        |
|                         |      |      | -            |
|                         |      |      | 2/4/25 11:00 |
|                         |      |      | SE280753.001 |
| PARAMETER               | UOM  | LOR  |              |
| Total Kjeldahl Nitrogen | mg/L | 0.05 | 0.52         |
| Total Nitrogen (calc)   | mg/L | 0.05 | 0.53         |



ANALYTICAL RESULTS

SE280753 R0

Ammonia Nitrogen by Discrete Analyser [AN291]    Tested: 2/4/2025

|                                        |      |      | BH1          |
|----------------------------------------|------|------|--------------|
|                                        |      |      | WATER        |
|                                        |      |      | -            |
|                                        |      |      | 2/4/25 11:00 |
|                                        |      |      | SE280753.001 |
| PARAMETER                              | UOM  | LOR  |              |
| Ammonia Nitrogen, NH <sub>3</sub> as N | mg/L | 0.01 | <b>0.17</b>  |



ANALYTICAL RESULTS

SE280753 R0

Calculation of Anion-Cation Balance (SAR Calc) [AN121]    Tested: 9/4/2025

|                                 |       |     | BH1          |
|---------------------------------|-------|-----|--------------|
|                                 |       |     | WATER        |
|                                 |       |     | -            |
|                                 |       |     | 2/4/25 11:00 |
|                                 |       |     | SE280753.001 |
| PARAMETER                       | UOM   | LOR |              |
| Sum of Cation Milliequivalents* | meq/L | -   | <b>14</b>    |
| Sum of Anion Milliequivalents*  | meq/L | -   | <b>16</b>    |
| Sum of Ions*                    | mg/L  | -   | <b>958</b>   |
| Anion-Cation Balance            | %     | -   | <0           |



ANALYTICAL RESULTS

SE280753 R0

Total Phosphorus by Kjeldahl Digestion DA in Water [AN279/AN293(Sydney only)]    Tested: 8/4/2025

|                                            |      |      | BH1          |
|--------------------------------------------|------|------|--------------|
|                                            |      |      | WATER        |
|                                            |      |      | -            |
|                                            |      |      | 2/4/25 11:00 |
| PARAMETER                                  | UOM  | LOR  | SE280753.001 |
| Total Phosphorus (Kjeldahl Digestion) as P | mg/L | 0.02 | 0.10         |



ANALYTICAL RESULTS

SE280753 R0

Filterable Reactive Phosphorus (FRP) [AN278]    Tested: 2/4/2025

|                                     |      |       | BH1          |
|-------------------------------------|------|-------|--------------|
|                                     |      |       | WATER        |
|                                     |      |       | -            |
|                                     |      |       | 2/4/25 11:00 |
|                                     |      |       | SE280753.001 |
| PARAMETER                           | UOM  | LOR   |              |
| Filterable Reactive Phosphorus as P | mg/L | 0.005 | <0.005       |





ANALYTICAL RESULTS

SE280753 R0

Total Dissolved Solids (TDS) in water [AN113]    Tested: 3/4/2025

|                                           |      |     | BH1          | BH2          | BH5          |
|-------------------------------------------|------|-----|--------------|--------------|--------------|
|                                           |      |     | WATER        | WATER        | WATER        |
|                                           |      |     | -            | -            | -            |
|                                           |      |     | 2/4/25 11:00 | 2/4/25 11:00 | 2/4/25 11:00 |
|                                           |      |     | SE280753.001 | SE280753.002 | SE280753.003 |
| PARAMETER                                 | UOM  | LOR |              |              |              |
| Total Dissolved Solids Dried at 175-185°C | mg/L | 10  | 990          | 390          | 960          |



ANALYTICAL RESULTS

SE280753 R0

Turbidity [AN119]    Tested: 2/4/2025

|           |     |     |              |
|-----------|-----|-----|--------------|
|           |     |     | BH1          |
|           |     |     | WATER        |
|           |     |     | -            |
|           |     |     | 2/4/25 11:00 |
| PARAMETER | UOM | LOR | SE280753.001 |
| Turbidity | NTU | 0.5 | 150          |



ANALYTICAL RESULTS

SE280753 R0

Dissolved Oxygen by Membrane Electrode [AN176]    Tested: 2/4/2025

|                                         |      |     | BH1          |
|-----------------------------------------|------|-----|--------------|
|                                         |      |     | WATER        |
|                                         |      |     | -            |
|                                         |      |     | 2/4/25 11:00 |
| PARAMETER                               | UOM  | LOR | SE280753.001 |
| Temperature*                            | °C   | -   | 18.3         |
| Dissolved Oxygen**                      | mg/L | 0.5 | 4.3          |
| Dissolved Oxygen (percent saturation)** | %    | 1   | 45.6         |



ANALYTICAL RESULTS

SE280753 R0

Total and Volatile Suspended Solids (TSS / VSS) [AN114]    Tested: 4/4/2025

|                                           |      |     | BH1          | BH2          | BH5          |
|-------------------------------------------|------|-----|--------------|--------------|--------------|
|                                           |      |     | WATER        | WATER        | WATER        |
|                                           |      |     | -            | -            | -            |
|                                           |      |     | 2/4/25 11:00 | 2/4/25 11:00 | 2/4/25 11:00 |
|                                           |      |     | SE280753.001 | SE280753.002 | SE280753.003 |
| PARAMETER                                 | UOM  | LOR |              |              |              |
| Total Suspended Solids Dried at 103-105°C | mg/L | 5   | 280          | 240          | 950          |



ANALYTICAL RESULTS

SE280753 R0

Forms of Carbon [AN190]    Tested: 3/4/2025

|                              |      |     | BH1          |
|------------------------------|------|-----|--------------|
|                              |      |     | WATER        |
|                              |      |     | -            |
|                              |      |     | 2/4/25 11:00 |
| PARAMETER                    | UOM  | LOR | SE280753.001 |
| Total Organic Carbon as NPOC | mg/L | 0.2 | 4.0          |





ANALYTICAL RESULTS

SE280753 R0

Redox Potential (Eh) in water [AN240]    Tested: 2/4/2025

|                                                   |     |      | BH1          |
|---------------------------------------------------|-----|------|--------------|
|                                                   |     |      | WATER        |
|                                                   |     |      | -            |
|                                                   |     |      | 2/4/25 11:00 |
|                                                   |     |      | SE280753.001 |
| PARAMETER                                         | UOM | LOR  |              |
| Eh of Sample Relative to Standard H+ Electrode*** | mV  | -500 | <b>282</b>   |
| Temperature of Sample*                            | °C  | 0.1  | <b>22.6</b>  |



ANALYTICAL RESULTS

SE280753 R0

Enterococci in Water [AN705]    Tested: 3/4/2025

|                         |           |     | BH1              |
|-------------------------|-----------|-----|------------------|
|                         |           |     | WATER            |
|                         |           |     | -                |
|                         |           |     | 2/4/25 11:00     |
|                         |           |     | SE280753.001     |
| PARAMETER               | UOM       | LOR |                  |
| Date & Time Processed*  | No unit   | -   | 2025-04-02 20:32 |
| Intestinal Enterococci* | CFU/100mL | 1   | 5                |
| Notes*                  | No unit   | -   | -                |



ANALYTICAL RESULTS

SE280753 R0

E. coli and Thermotolerant coliforms in Water (CFU) [AN703]    Tested: 3/4/2025

|                          |           |     | BH1              |
|--------------------------|-----------|-----|------------------|
|                          |           |     | WATER            |
|                          |           |     | -                |
|                          |           |     | 2/4/25 11:00     |
|                          |           |     | SE280753.001     |
| PARAMETER                | UOM       | LOR |                  |
| Date & Time Processed*   | No unit   | -   | 2025-04-02 20:32 |
| E. coli                  | CFU/100mL | 1   | <b>10</b>        |
| Thermotolerant Coliforms | CFU/100mL | 1   | <b>130</b>       |

Trace Metals (Dissolved) in Water by ICPMS [AN318]    Tested: 8/4/2025

| PARAMETER  | UOM  | LOR | BH1                                        | BH2                                        | BH5                                        |
|------------|------|-----|--------------------------------------------|--------------------------------------------|--------------------------------------------|
|            |      |     | WATER<br>-<br>2/4/25 11:00<br>SE280753.001 | WATER<br>-<br>2/4/25 11:00<br>SE280753.002 | WATER<br>-<br>2/4/25 11:00<br>SE280753.003 |
| Arsenic    | µg/L | 1   | <1                                         | <1                                         | <b>3</b>                                   |
| Cadmium    | µg/L | 0.1 | <b>0.2</b>                                 | <0.1                                       | <0.1                                       |
| Chromium   | µg/L | 1   | <1                                         | <1                                         | <1                                         |
| Copper     | µg/L | 1   | <b>4</b>                                   | <1                                         | <b>2</b>                                   |
| Lead       | µg/L | 1   | <1                                         | <1                                         | <1                                         |
| Nickel     | µg/L | 1   | <b>28</b>                                  | <b>2</b>                                   | <b>71</b>                                  |
| Zinc       | µg/L | 5   | <b>180</b>                                 | <b>17</b>                                  | <b>240</b>                                 |
| Silver     | µg/L | 1   | <1                                         | -                                          | -                                          |
| Aluminium  | µg/L | 5   | <b>67</b>                                  | -                                          | -                                          |
| Antimony   | µg/L | 1   | <1                                         | -                                          | -                                          |
| Barium     | µg/L | 1   | <b>29</b>                                  | -                                          | -                                          |
| Beryllium  | µg/L | 1   | <b>1</b>                                   | -                                          | -                                          |
| Boron      | µg/L | 5   | <b>120</b>                                 | -                                          | -                                          |
| Cobalt     | µg/L | 1   | <b>34</b>                                  | -                                          | -                                          |
| Iron       | µg/L | 5   | <b>6</b>                                   | -                                          | -                                          |
| Manganese  | µg/L | 1   | <b>2600</b>                                | -                                          | -                                          |
| Molybdenum | µg/L | 1   | <1                                         | -                                          | -                                          |
| Selenium   | µg/L | 1   | <1                                         | -                                          | -                                          |
| Strontium  | µg/L | 1   | <b>130</b>                                 | -                                          | -                                          |
| Uranium    | µg/L | 1   | <1                                         | -                                          | -                                          |
| Vanadium   | µg/L | 1   | <1                                         | -                                          | -                                          |

Metals in Water (Dissolved) by ICPOES [AN320] Tested: 8/4/2025

| PARAMETER                        | UOM        | LOR   | BH1                               | BH2                               | BH5                               |
|----------------------------------|------------|-------|-----------------------------------|-----------------------------------|-----------------------------------|
|                                  |            |       | WATER                             | WATER                             | WATER                             |
|                                  |            |       | -<br>2/4/25 11:00<br>SE280753.001 | -<br>2/4/25 11:00<br>SE280753.002 | -<br>2/4/25 11:00<br>SE280753.003 |
| Calcium, Ca                      | mg/L       | 0.1   | <b>19</b>                         | <b>23</b>                         | <b>7.8</b>                        |
| Magnesium, Mg                    | mg/L       | 0.1   | <b>30</b>                         | <b>3.7</b>                        | <b>27</b>                         |
| Sodium, Na                       | mg/L       | 0.1   | <b>250</b>                        | <b>72</b>                         | <b>230</b>                        |
| Potassium, K                     | mg/L       | 0.2   | <b>7.7</b>                        | <b>3.3</b>                        | <b>4.5</b>                        |
| Iron, Fe                         | mg/L       | 0.02  | <0.02                             | -                                 | -                                 |
| Total Hardness by Calculation    | mg CaCO3/L | 1     | <b>170</b>                        | -                                 | -                                 |
| Sodium Adsorption Ratio          | No unit    | 0.2   | <b>8.4</b>                        | -                                 | -                                 |
| Lithium, Li                      | mg/L       | 0.005 | <b>0.042</b>                      | -                                 | -                                 |
| Silicon, Si*                     | mg/L       | 0.05  | <b>24</b>                         | -                                 | -                                 |
| Soluble Silicon as Silica, SiO2* | mg/L       | 0.1   | <b>51</b>                         | -                                 | -                                 |



ANALYTICAL RESULTS

SE280753 R0

Mercury (dissolved) in Water [AN311(Perth)/AN312]    Tested: 3/4/2025

|           |      |        | BH1          | BH2          | BH5          |
|-----------|------|--------|--------------|--------------|--------------|
|           |      |        | WATER        | WATER        | WATER        |
|           |      |        | -            | -            | -            |
|           |      |        | 2/4/25 11:00 | 2/4/25 11:00 | 2/4/25 11:00 |
| PARAMETER | UOM  | LOR    | SE280753.001 | SE280753.002 | SE280753.003 |
| Mercury   | mg/L | 0.0001 | <0.0001      | <0.0001      | <0.0001      |



## METHOD

## METHODOLOGY SUMMARY

|       |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               |
|-------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| AN020 | Unpreserved water sample is filtered through a 0.45µm membrane filter and acidified with nitric acid similar to APHA3030B.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    |
| AN101 | pH in Soil Sludge Sediment and Water: pH is measured electrometrically using a combination electrode (glass plus reference electrode) and is calibrated against 3 buffers purchased commercially. For soils, an extract with water is made at a ratio of 1:5 and the pH determined and reported on the extract. Reference APHA 4500-H+.                                                                                                                                                                                                                                                                                                                       |
| AN106 | Conductivity and TDS by Calculation: Conductivity is measured by meter with temperature compensation and is calibrated against a standard solution of potassium chloride. Conductivity is generally reported as µmhos/cm or µS/cm @ 25°C. For soils, an extract with water is made at a ratio of 1:5 and the EC determined and reported on the extract, or calculated back to the as-received sample. Total Dissolved Salts can be estimated from conductivity using a conversion factor, which for natural waters, is in the range 0.55 to 0.75. SGS use 0.6. Reference APHA 2510 B.                                                                         |
| AN106 | Salinity may be calculated in terms of NaCl from the sample conductivity. This assumes all soluble salts present, measured by the conductivity, are present as NaCl.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |
| AN113 | Total Dissolved Solids: A well-mixed filtered sample of known volume is evaporated to dryness at 180°C and the residue weighed. Approximate methods for correlating chemical analysis with dissolved solids are available. Reference APHA 2540 C.                                                                                                                                                                                                                                                                                                                                                                                                             |
| AN113 | The Total Dissolved Solids residue may also be ignited at 550 C and volatile TDS (Organic TDS) and non-volatile TDS (Inorganic) can be determined.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            |
| AN114 | Total Suspended and Volatile Suspended Solids: The sample is homogenised by shaking and a known volume is filtered through a pre-weighed GF/C filter paper and washed well with deionised water. The filter paper is dried and reweighed. The TSS is the residue retained by the filter per unit volume of sample. Reference APHA 2540 D. Internal Reference AN114                                                                                                                                                                                                                                                                                            |
| AN119 | Turbidity by Nephelometry: Small particles in a light beam scatter light at a range of angles. A turbidimeter measures this scatter and reports results compared to turbidity standards, in NTU. This procedure is not suitable for very dark coloured liquids or samples with high solids because light absorption causes artificially low light scatter and low turbidity. Reference APHA 2130B.                                                                                                                                                                                                                                                            |
| AN121 | This method is used to calculate the balance of major Anions and Cations in water samples and converts major ion concentration to milliequivalents and then summed. Anions sum and Cation sum is calculated as a difference and expressed as a percentage.                                                                                                                                                                                                                                                                                                                                                                                                    |
| AN135 | Alkalinity (and forms of) by Titration: The sample is titrated with standard acid to pH 8.3 (P titre) and pH 4.5 (T titre) and permanent and/or total alkalinity calculated. The results are expressed as equivalents of calcium carbonate or recalculated as bicarbonate, carbonate and hydroxide. Reference APHA 2320. Internal Reference AN135                                                                                                                                                                                                                                                                                                             |
| AN140 | Acidity by Titration: The water sample is titrated with sodium hydroxide to designated pH end point. In a sample containing only carbon dioxide, bicarbonates and carbonates, titration to pH 8.3 at 25°C corresponds to stoichiometric neutralisation of carbonic acid to bicarbonate. Method reference APHA 2310 B.                                                                                                                                                                                                                                                                                                                                         |
| AN176 | Dissolved Oxygen: DO can also be measured directly using an oxygen permeable membrane electrode and meter. Under steady state conditions the current is directly proportional to the DO conc. DO can also be measured via Luminescent dissolved oxygen probes (LDO) which also operates using an oxygen permeable membrane with an oxygen sensitive luminescent dye making up the second probe layer. The presence of oxygen causes changes in the lifetime and intensity of luminescence, which are then quantified. Zero headspace is required for sample analysis, if headspace is observed report comment will be recorded. Reference APHA 4500-C, G & O. |
| AN190 | TOC and DOC in Water: A homogenised micro portion of sample is injected into a heated reaction chamber packed with an oxidative catalyst that converts organic carbon to carbon dioxide. The CO <sub>2</sub> is measured using a non-dispersive infrared detector. The process is fully automated in a commercially available analyser. If required a sugar value can be calculated from the TOC result. Reference APHA 5310 B.                                                                                                                                                                                                                               |
| AN190 | Chemical oxygen demand can be calculated/estimated based on the O <sub>2</sub> /C relation as 2.67*NPOC (TOC). This is an estimate only and the factor will vary with sample matrix so results should be interpreted with caution.                                                                                                                                                                                                                                                                                                                                                                                                                            |
| AN240 | Oxidation-Reduction Potential (Eh): Electrometric measurements are made by potentiometric determination of electron activity (or intensity) with an inert indicator electrode and a suitable reference electrode. At redox equilibrium, the potential difference between the two electrodes equals the redox potential of the system. This measurement is then corrected for the difference between the potential of the reference electrode and that of the standard hydrogen electrode.                                                                                                                                                                     |
| AN245 | Anions by Ion Chromatography: A water sample is injected into an eluent stream that passes through the ion chromatographic system where the anions of interest ie Br, Cl, NO <sub>2</sub> , NO <sub>3</sub> and SO <sub>4</sub> are separated on their relative affinities for the active sites on the column packing material. Changes to the conductivity and the UV-visible absorbance of the eluent enable identification and quantitation of the anions based on their retention time and peak height or area. APHA 4110 B                                                                                                                               |
| AN277 | Nitrite ions, when reacted with a reagent containing sulphanilamide and N-(1-naphthyl)-ethylenediamine dihydrochloride produce a highly coloured azo dye that is measured photometrically at 540nm.                                                                                                                                                                                                                                                                                                                                                                                                                                                           |

|                     |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |
|---------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| AN278               | Filterable Reactive Phosphorus by DA (determined on filtered sample): Orthophosphate reacts with ammonium molybdate (Mo VI) and potassium antimonyl tartrate (Sb III) in acid medium to form an antimony-phosphomolybdate complex. This complex is subsequently reduced with ascorbic acid to form a blue colour and the absorbance is read at 880 nm. The sensitivity of the automated method is 10-20 times that of the macro method. Reference APHA 4500-P F                                                                                                                                                                |
| AN279/AN293(Sydney) | The sample is digested with Sulphuric acid, K <sub>2</sub> SO <sub>4</sub> and CuSO <sub>4</sub> . All forms of phosphorus are converted into orthophosphate. The digest is cooled and placed on the discrete analyser for colorimetric analysis.                                                                                                                                                                                                                                                                                                                                                                              |
| AN281               | An unfiltered water or soil sample is first digested in a block digester with sulfuric acid, K <sub>2</sub> SO <sub>4</sub> and CuSO <sub>4</sub> . The ammonia produced following digestion is then measured colourimetrically using the Discrete Analyser. A portion of the digested sample is buffered to an alkaline pH, and interfering cations are complexed. The ammonia then reacts with salicylate and hypochlorite to give a blue colour whose absorbance is measured at 660nm and compared with calibration standards. This is proportional to the concentration of Total Kjeldahl Nitrogen in the original sample. |
| AN291               | Ammonia in solution reacts with hypochlorite ions from Sodium Dichloroisocyanate, and salicylate in the presence of Sodium Nitroprusside to form indophenol blue and measured at 660 nm by Discrete Analyser.                                                                                                                                                                                                                                                                                                                                                                                                                  |
| AN311(Perth)/AN312  | Mercury by Cold Vapour AAS in Waters: Mercury ions are reduced by stannous chloride reagent in acidic solution to elemental mercury. This mercury vapour is purged by nitrogen into a cold cell in an atomic absorption spectrometer or mercury analyser. Quantification is made by comparing absorbances to those of the calibration standards. Reference APHA 3112/3500.                                                                                                                                                                                                                                                     |
| AN318               | Determination of elements at trace level in waters by ICP-MS technique,, referenced to USEPA 6020B and USEPA 200.8 (5.4).                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      |
| AN320               | Metals by ICP-OES: Samples are preserved with 10% nitric acid for a wide range of metals and some non-metals. This solution is measured by Inductively Coupled Plasma. Solutions are aspirated into an argon plasma at 8000-10000K and emit characteristic energy or light as a result of electron transitions through unique energy levels. The emitted light is focused onto a diffraction grating where it is separated into components .                                                                                                                                                                                   |
| AN320               | Photomultipliers or CCDs are used to measure the light intensity at specific wavelengths. This intensity is directly proportional to concentration. Corrections are required to compensate for spectral overlap between elements . Reference APHA 3120 B.                                                                                                                                                                                                                                                                                                                                                                      |
| AN403               | Total Recoverable Hydrocarbons: Determination of Hydrocarbons by gas chromatography after a solvent extraction. Detection is by flame ionisation detector (FID) that produces an electronic signal in proportion to the combustible matter passing through it. Total Recoverable Hydrocarbons (TRH) are routinely reported as four alkane groupings based on the carbon chain length of the compounds: C6-C9, C10-C14, C15-C28 and C29-C36 and in recognition of the NEPM 1999 (2013), >C10-C16 (F2), >C16-C34 (F3) and >C34-C40 (F4). Where F2 is corrected for Naphthalene, the VOC data for Naphthalene is used.            |
| AN403               | Additionally, the volatile C6-C9/C6-C10 fractions may be determined by a purge and trap technique and GC/MS because of the potential for volatiles loss. Total Recoverable Hydrocarbons - Silica (TRH-Silica) follows the same method of analysis after silica gel cleanup of the solvent extract. Aliphatic/Aromatic Speciation follows the same method of analysis after fractionation of the solvent extract over silica with differential polarity of the eluent solvents.                                                                                                                                                 |
| AN403               | The GC/FID method is not well suited to the analysis of refined high boiling point materials (ie lubricating oils or greases) but is particularly suited for measuring diesel, kerosene and petrol if care to control volatility is taken. This method will detect naturally occurring hydrocarbons, lipids, animal fats, phenols and PAHs if they are present at sufficient levels, dependent on the use of specific cleanup/fractionation techniques. Reference USEPA 3510B, 8015B.                                                                                                                                          |
| AN420               | (SVOCs) including OC, OP, PCB, Herbicides, PAH, Phthalates and Speciated Phenols (etc) in soils, sediments and waters are determined by GCMS/ECD technique following appropriate solvent extraction process (Based on USEPA 3500C and 8270D).<br>Total PAH calculated from individual analyte detections at or above the limit of reporting .                                                                                                                                                                                                                                                                                  |
| AN433               | VOCs and C6-C9 Hydrocarbons by GC-MS P&T: VOC's are volatile organic compounds. The sample is presented to a gas chromatograph via a purge and trap (P&T) concentrator and autosampler and is detected with a Mass Spectrometer (MSD). Solid samples are initially extracted with methanol whilst liquid samples are processed directly. References: USEPA 5030B, 8020A, 8260.                                                                                                                                                                                                                                                 |
| AN703               | A known volume of water is passed through a membrane of known pore size. The membrane is placed on a selective agar plate and incubated. The volume of sample filtered depends upon the expected count. Referenced to AS4276.5.                                                                                                                                                                                                                                                                                                                                                                                                |
| AN705               | A known volume of water is passed through a membrane of known pore size. The membrane is placed on a selective agar plate and incubated. The volume of sample filtered depends upon the expected count. Referenced to AS/NZS4276.9 (ISO 7899-2:2000 MOD).                                                                                                                                                                                                                                                                                                                                                                      |
| Calculation         | Free and Total Carbon Dioxide may be calculated using alkalinity forms only when the samples TDS is <500mg/L. If TDS is >500mg/L free or total carbon dioxide cannot be reported . APHA4500CO2 D.                                                                                                                                                                                                                                                                                                                                                                                                                              |

FOOTNOTES

|     |                                                                    |     |                                   |     |                                    |
|-----|--------------------------------------------------------------------|-----|-----------------------------------|-----|------------------------------------|
| *   | NATA accreditation does not cover the performance of this service. | -   | Not analysed.                     | UOM | Unit of Measure.                   |
| **  | Indicative data, theoretical holding time exceeded.                | NVL | Not validated.                    | LOR | Limit of Reporting.                |
| *** | Indicates that both * and ** apply.                                | IS  | Insufficient sample for analysis. | ↑↓  | Raised/lowered Limit of Reporting. |
|     |                                                                    | LNR | Sample listed, but not received.  |     |                                    |

Unless it is reported that sampling has been performed by SGS, the samples have been analysed as received.  
Solid samples expressed on a dry weight basis.

Where "Total" analyte groups are reported (for example, Total PAHs, Total OC Pesticides) the total will be calculated as the sum of the individual analytes, with those analytes that are reported as <LOR being assumed to be zero. The summed (Total) limit of reporting is calculated by summing the individual analyte LORs and dividing by two. For example, where 16 individual analytes are being summed and each has an LOR of 0.1 mg/kg, the "Totals" LOR will be 1.6 / 2 (0.8 mg/kg). Where only 2 analytes are being summed, the "Total" LOR will be the sum of those two LORs.

Some totals may not appear to add up because the total is rounded after adding up the raw values.

If reported, measurement uncertainty follow the ± sign after the analytical result and is expressed as the expanded uncertainty calculated using a coverage factor of 2, providing a level of confidence of approximately 95%, unless stated otherwise in the comments section of this report.

Results reported for samples tested under test methods with codes starting with ARS-SOP, radionuclide or gross radioactivity concentrations are expressed in becquerel (Bq) per unit of mass or volume or per wipe as stated on the report. Becquerel is the SI unit for activity and equals one nuclear transformation per second.

Note that in terms of units of radioactivity:

- 1 Bq is equivalent to 27 pCi
- 37 MBq is equivalent to 1 mCi

For results reported for samples tested under test methods with codes starting with ARS-SOP, less than (<) values indicate the detection limit for each radionuclide or parameter for the measurement system used. The respective detection limits have been calculated in accordance with ISO 11929.

The QC and MU criteria are subject to internal review according to the SGS QAQC plan and may be provided on request or alternatively can be found here: [www.sgs.com.au/en-gb/environment-health-and-safety](http://www.sgs.com.au/en-gb/environment-health-and-safety).

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## **APPENDIX C**

# **BOREHOLE PERMEABILITY TESTING**

# Rising Head Permeability Results

**morrow**

79/6 Bellambi Lane, Bellambi NSW 2518  
P: 0405 843 933 | E: info@morrowgeo.com.au

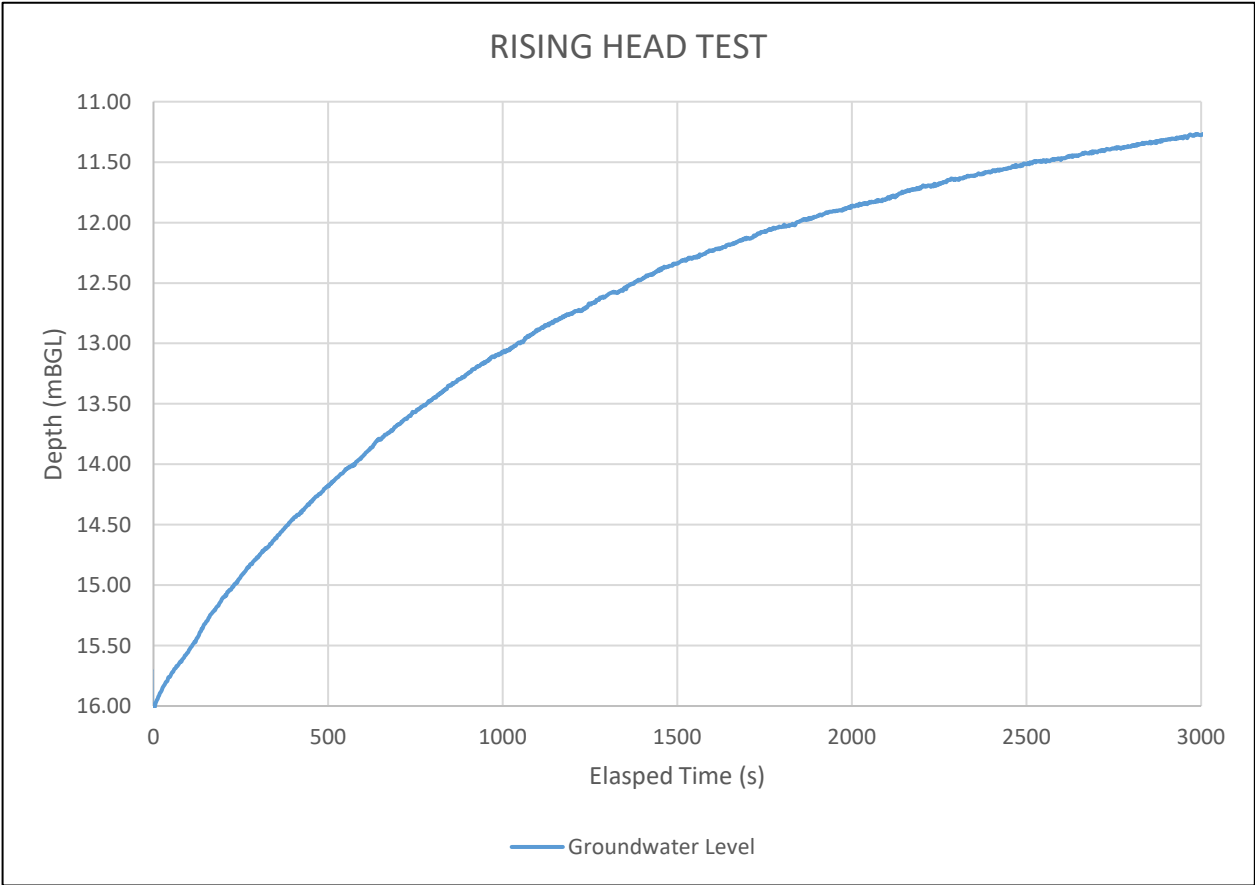
|                 |                                        |
|-----------------|----------------------------------------|
| Project Number  | P3444 - Lindfield                      |
| Address         | 59-63 Trafalgar Ave & 1A/B Valley Road |
| Borehole        | BH1 Test 1                             |
| Monitoring Date | 28/02/2025                             |

|                                            |       |
|--------------------------------------------|-------|
| Static water level (mBGL)                  | 8.55  |
| Internal Diameter (D) (m)                  | 0.07  |
| Length of Standpipe below Ground Level (m) | 35.00 |
| Height of Water above Ground Level (m)     | 0.00  |
| Length of Standpipe above Ground Level (m) | 0.00  |
| Water level at start of test (mBGL)        | 8.55  |
| Top of Response Zone (mBGL)                | 8.55  |
| Bottom of Response Zone (mBGL)             | 35.00 |

|               |      |
|---------------|------|
| Time (t1) (s) | 4    |
| Time (t2) (s) | 1400 |

|                             |        |
|-----------------------------|--------|
| Initial Head (H1) at (t1)   | 16.00  |
| Final Head (H2) at (t2)     | 12.47  |
| Length of Response Zone (L) | 26.45  |
| Cross Sectional Area (A)    | 0.0038 |

Stratigraphy Description: Fill overlying residual clay and sandstone bedrock



Intake Factor (F) Case D  $\frac{2pL}{\log_e [(L/D) + \sqrt{1 + (L/D)^2}]}$  =  $\frac{166.19}{6.63}$  = 25.08

Permeability (k)  $\frac{A}{F(t_2 - t_1)} \log_e \frac{H_1}{H_2}$  = 2.75E-08 m/s

Rising Head Test Method 1 (after Hvorslev)  
Formulae for borehole permeability tests(21.4.6) BS5930 : 1981

Calculation by: AB      Checked by: AM      Date: 14/04/2025

# Rising Head Permeability Results

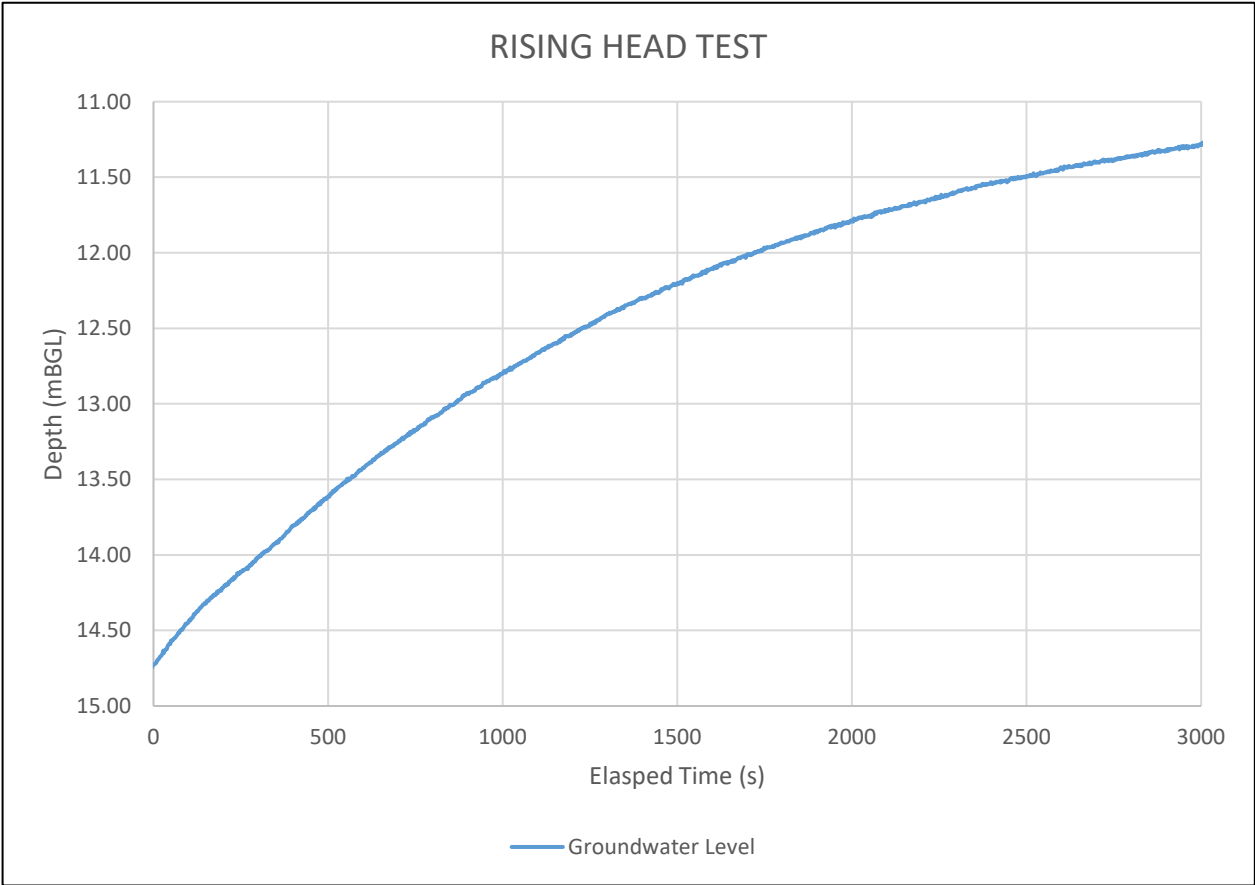
**morrow**

79/6 Bellambi Lane, Bellambi NSW 2518  
P: 0405 843 933 | E: info@morrowgeo.com.au

|                 |                                        |
|-----------------|----------------------------------------|
| Project Number  | P3444 - Lindfield                      |
| Address         | 59-63 Trafalgar Ave & 1A/B Valley Road |
| Borehole        | BH1 Test 2                             |
| Monitoring Date | 28/02/2025                             |

|                                            |       |                             |        |
|--------------------------------------------|-------|-----------------------------|--------|
| Static water level (mBGL)                  | 8.55  | Time (t1) (s)               | 12     |
| Internal Diameter (D) (m)                  | 0.07  | Time (t2) (s)               | 1330   |
| Length of Standpipe below Ground Level (m) | 35.00 |                             |        |
| Height of Water above Ground Level (m)     | 0.00  | Initial Head (H1) at (t1)   | 14.69  |
| Length of Standpipe above Ground Level (m) | 0.00  | Final Head (H2) at (t2)     | 12.38  |
| Water level at start of test (mBGL)        | 8.55  | Length of Response Zone (L) | 26.45  |
| Top of Response Zone (mBGL)                | 8.55  | Cross Sectional Area (A)    | 0.0038 |
| Bottom of Response Zone (mBGL)             | 35.00 |                             |        |

Stratigraphy Description: Fill overlying residual clay and sandstone bedrock



Intake Factor (F) Case D  $\frac{2pL}{\log_e [(L/D) + \ddot{O}(1 + (L/D)^2)]}$  =  $\frac{166.19}{6.63}$  = 25.08

Permeability (k)  $\frac{A}{F(t_2-t_1)} \log_e \frac{H_1}{H_2}$  = 2.00E-08 m/s

Rising Head Test Method 1 (after Hvorslev)  
Formulae for borehole permeability tests(21.4.6) BS5930 : 1981

Calculation by: AB      Checked by: AM      Date: 14/04/2025



# Rising Head Permeability Results

**morrow**

79/6 Bellambi Lane, Bellambi NSW 2518  
P: 0405 843 933 | E: info@morrowgeo.com.au

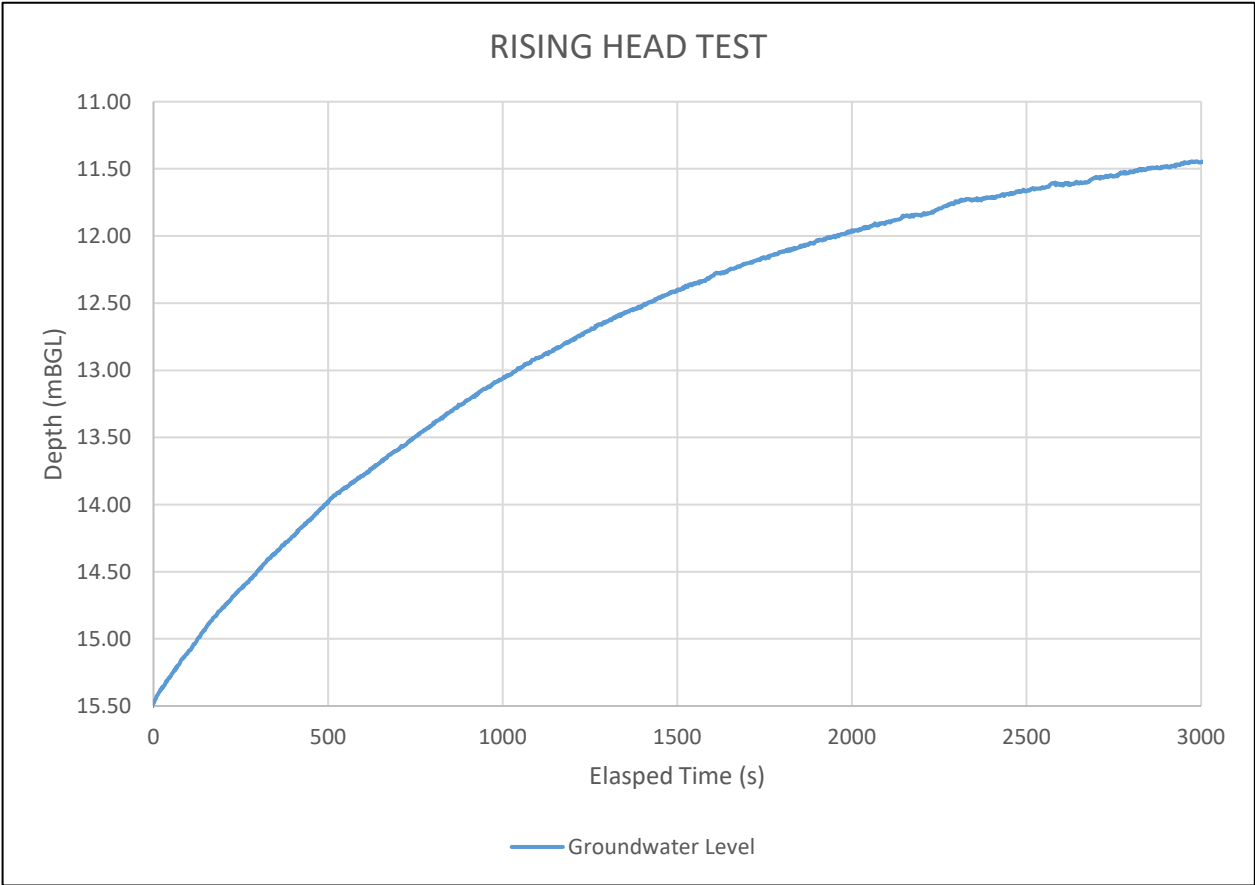
|                 |                                        |
|-----------------|----------------------------------------|
| Project Number  | P3444 - Lindfield                      |
| Address         | 59-63 Trafalgar Ave & 1A/B Valley Road |
| Borehole        | BH1 Test 3                             |
| Monitoring Date | 28/02/2025                             |

|                                            |       |
|--------------------------------------------|-------|
| Static water level (mBGL)                  | 8.55  |
| Internal Diameter (D) (m)                  | 0.07  |
| Length of Standpipe below Ground Level (m) | 35.00 |
| Height of Water above Ground Level (m)     | 0.00  |
| Length of Standpipe above Ground Level (m) | 0.00  |
| Water level at start of test (mBGL)        | 8.55  |
| Top of Response Zone (mBGL)                | 8.55  |
| Bottom of Response Zone (mBGL)             | 35.00 |

|               |      |
|---------------|------|
| Time (t1) (s) | 26   |
| Time (t2) (s) | 1074 |

|                             |        |
|-----------------------------|--------|
| Initial Head (H1) at (t1)   | 15.37  |
| Final Head (H2) at (t2)     | 12.95  |
| Length of Response Zone (L) | 26.45  |
| Cross Sectional Area (A)    | 0.0038 |

Stratigraphy Description: Fill overlying residual clay and sandstone bedrock



Intake Factor (F) Case D 
$$\frac{2pL}{\log_e \left[ \frac{L}{D} + \sqrt{1 + \left( \frac{L}{D} \right)^2} \right]} = \frac{166.19}{6.63} = 25.08$$

Permeability (k) 
$$\frac{A}{F(t_2 - t_1)} \log_e \frac{H_1}{H_2} = 2.50E-08 \text{ m/s}$$

Rising Head Test Method 1 (after Hvorslev)  
Formulae for borehole permeability tests(21.4.6) BS5930 : 1981

Calculation by: **AB**      Checked by: **AM**      Date: **14/04/2025**

# Rising Head Permeability Results

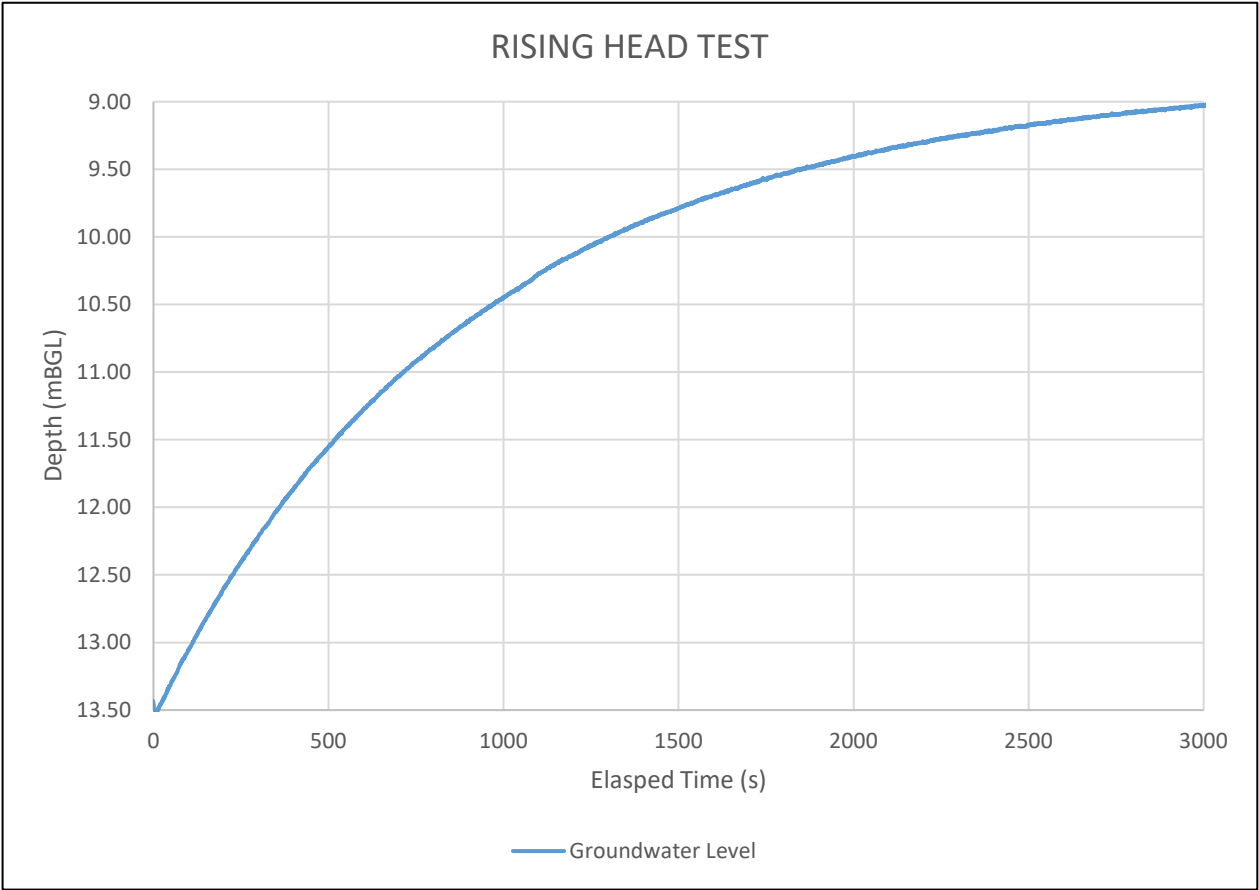
**morrow**

79/6 Bellambi Lane, Bellambi NSW 2518  
P: 0405 843 933 | E: info@morrowgeo.com.au

|                 |                                        |
|-----------------|----------------------------------------|
| Project Number  | P3444 - Lindfield                      |
| Address         | 59-63 Trafalgar Ave & 1A/B Valley Road |
| Borehole        | BH1 Test 4                             |
| Monitoring Date | 2/04/2025                              |

|                                            |       |                             |        |
|--------------------------------------------|-------|-----------------------------|--------|
| Static water level (mBGL)                  | 8.55  | Time (t1) (s)               | 13     |
| Internal Diameter (D) (m)                  | 0.07  | Time (t2) (s)               | 1042   |
| Length of Standpipe below Ground Level (m) | 35.00 |                             |        |
| Height of Water above Ground Level (m)     | 0.00  | Initial Head (H1) at (t1)   | 13.50  |
| Length of Standpipe above Ground Level (m) | 0.00  | Final Head (H2) at (t2)     | 10.39  |
| Water level at start of test (mBGL)        | 8.55  | Length of Response Zone (L) | 26.45  |
| Top of Response Zone (mBGL)                | 8.55  | Cross Sectional Area (A)    | 0.0038 |
| Bottom of Response Zone (mBGL)             | 35.00 |                             |        |

Stratigraphy Description: Fill and residual clay over sandstone bedrock



Intake Factor (F) Case D  $\frac{2pL}{\log_e [(L/D) + \sqrt{1 + (L/D)^2}]}$  =  $\frac{166.19}{6.63}$  = 25.08

Permeability (k)  $\frac{A}{F (t_2 - t_1)} \log_e \frac{H_1}{H_2}$  = 3.90E-08 m/s

Rising Head Test Method 1 (after Hvorslev)  
Formulae for borehole permeability tests(21.4.6) BS5930 : 1981

Calculation by: AB      Checked by: AM      Date: 14/04/2025

# Rising Head Permeability Results

morrow

79/6 Bellambi Lane, Bellambi NSW 2518  
P: 0405 843 933 | E: info@morrowgeo.com.au

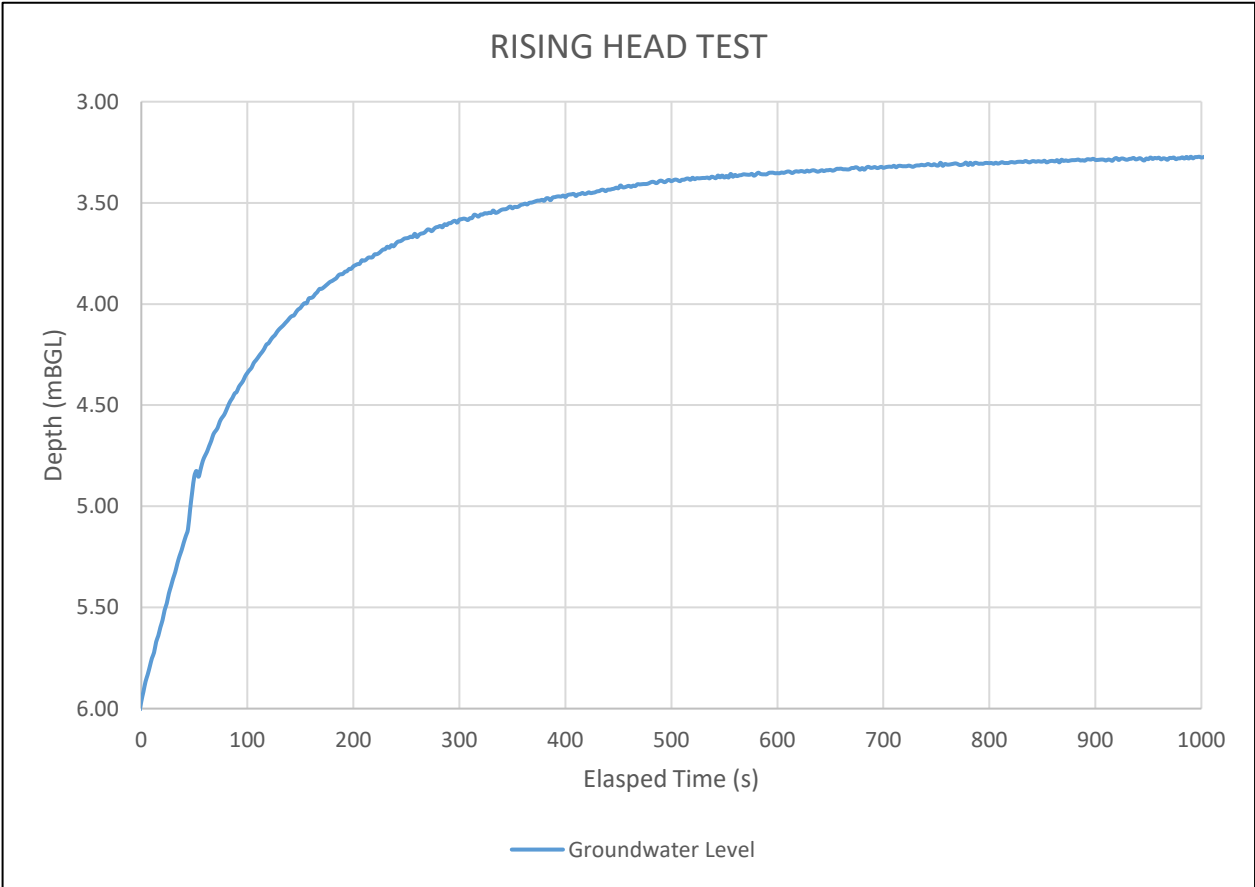
|                 |                                        |
|-----------------|----------------------------------------|
| Project Number  | P3444 - Lindfield                      |
| Address         | 59-63 Trafalgar Ave & 1A/B Valley Road |
| Borehole        | BH2 Test 1                             |
| Monitoring Date | 28/02/2025                             |

|                                            |       |
|--------------------------------------------|-------|
| Static water level (mBGL)                  | 3.13  |
| Internal Diameter (D) (m)                  | 0.07  |
| Length of Standpipe below Ground Level (m) | 19.92 |
| Height of Water above Ground Level (m)     | 0.00  |
| Length of Standpipe above Ground Level (m) | 0.00  |
| Water level at start of test (mBGL)        | 3.13  |
| Top of Response Zone (mBGL)                | 3.13  |
| Bottom of Response Zone (mBGL)             | 19.92 |

|               |     |
|---------------|-----|
| Time (t1) (s) | 2   |
| Time (t2) (s) | 218 |

|                             |        |
|-----------------------------|--------|
| Initial Head (H1) at (t1)   | 5.92   |
| Final Head (H2) at (t2)     | 3.77   |
| Length of Response Zone (L) | 16.79  |
| Cross Sectional Area (A)    | 0.0038 |

Stratigraphy Description: Fill overlying residual clay and sandstone bedrock



Intake Factor (F) Case D  $\frac{2pL}{\log_e [(L/D) + \ddot{O}(1 + (L/D)^2)]}$  =  $\frac{105.49}{6.17}$  = 17.09

Permeability (k)  $\frac{A}{F(t_2 - t_1)} \log_e \frac{H_1}{H_2}$  = 4.70E-07 m/s

Rising Head Test Method 1 (after Hvorslev)  
Formulae for borehole permeability tests(21.4.6) BS5930 : 1981

Calculation by: AB      Checked by: AM      Date: 14/04/2025

# Rising Head Permeability Results

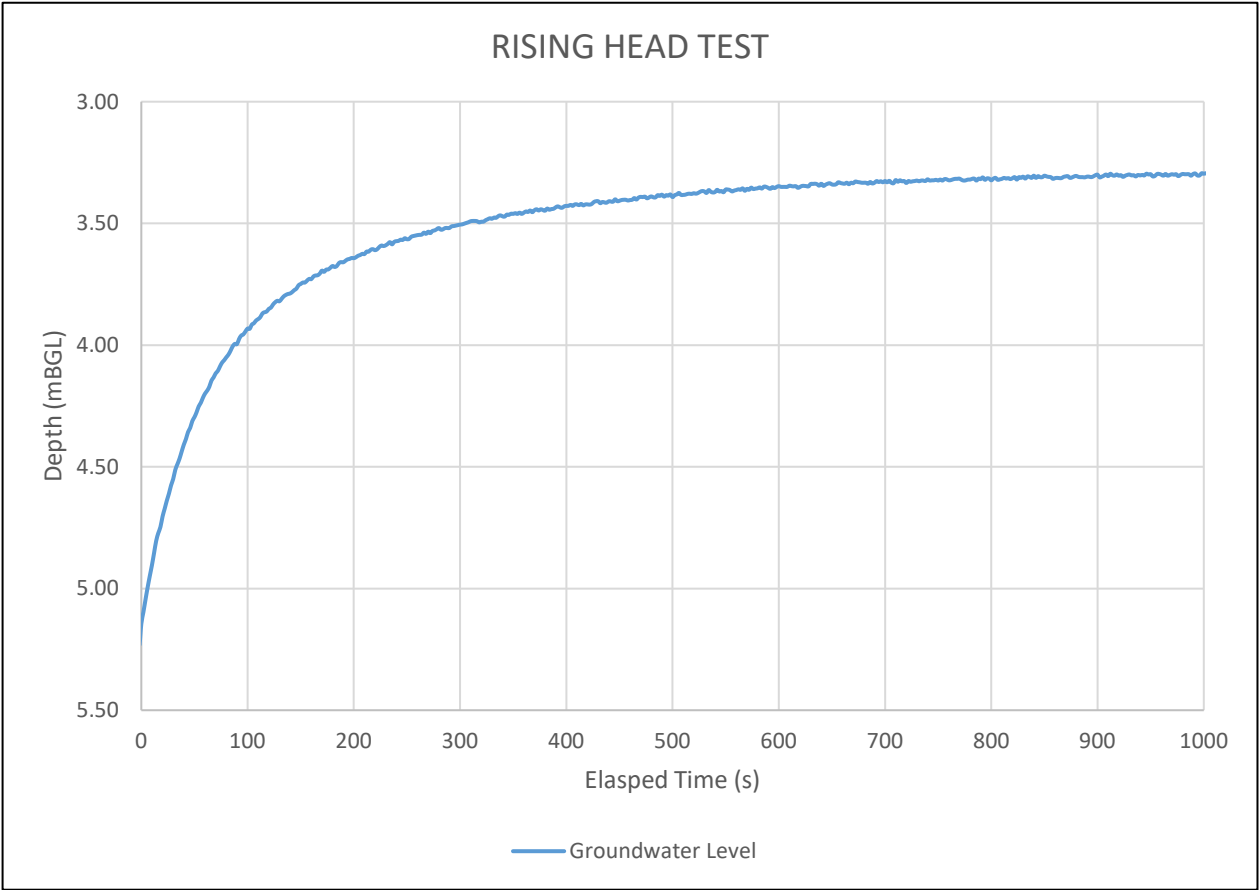
**morrow**

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P: 0405 843 933 | E: info@morrowgeo.com.au

|                 |                                        |
|-----------------|----------------------------------------|
| Project Number  | P3444 - Lindfield                      |
| Address         | 59-63 Trafalgar Ave & 1A/B Valley Road |
| Borehole        | BH2 Test 2                             |
| Monitoring Date | 28/02/2025                             |

|                                            |       |                             |        |
|--------------------------------------------|-------|-----------------------------|--------|
| Static water level (mBGL)                  | 3.13  | Time (t1) (s)               | 4      |
| Internal Diameter (D) (m)                  | 0.07  | Time (t2) (s)               | 78     |
| Length of Standpipe below Ground Level (m) | 19.92 |                             |        |
| Height of Water above Ground Level (m)     | 0.00  | Initial Head (H1) at (t1)   | 5.04   |
| Length of Standpipe above Ground Level (m) | 0.00  | Final Head (H2) at (t2)     | 4.06   |
| Water level at start of test (mBGL)        | 3.13  | Length of Response Zone (L) | 16.79  |
| Top of Response Zone (mBGL)                | 3.13  | Cross Sectional Area (A)    | 0.0038 |
| Bottom of Response Zone (mBGL)             | 19.92 |                             |        |

Stratigraphy Description: Fill overlying residual clay and sandstone bedrock



Intake Factor (F) Case D  $\frac{2pL}{\log_e [(L/D) + \ddot{O}(1 + (L/D)^2)]}$  =  $\frac{105.49}{6.17}$  = 17.09

Permeability (k)  $\frac{A}{F(t_2-t_1)} \log_e \frac{H_1}{H_2}$  = 6.59E-07 m/s

Rising Head Test Method 1 (after Hvorslev)  
Formulae for borehole permeability tests(21.4.6) BS5930 : 1981

Calculation by: AB      Checked by: AM      Date: 14/04/2025

# Rising Head Permeability Results

**morrow**

79/6 Bellambi Lane, Bellambi NSW 2518  
P: 0405 843 933 | E: info@morrowgeo.com.au

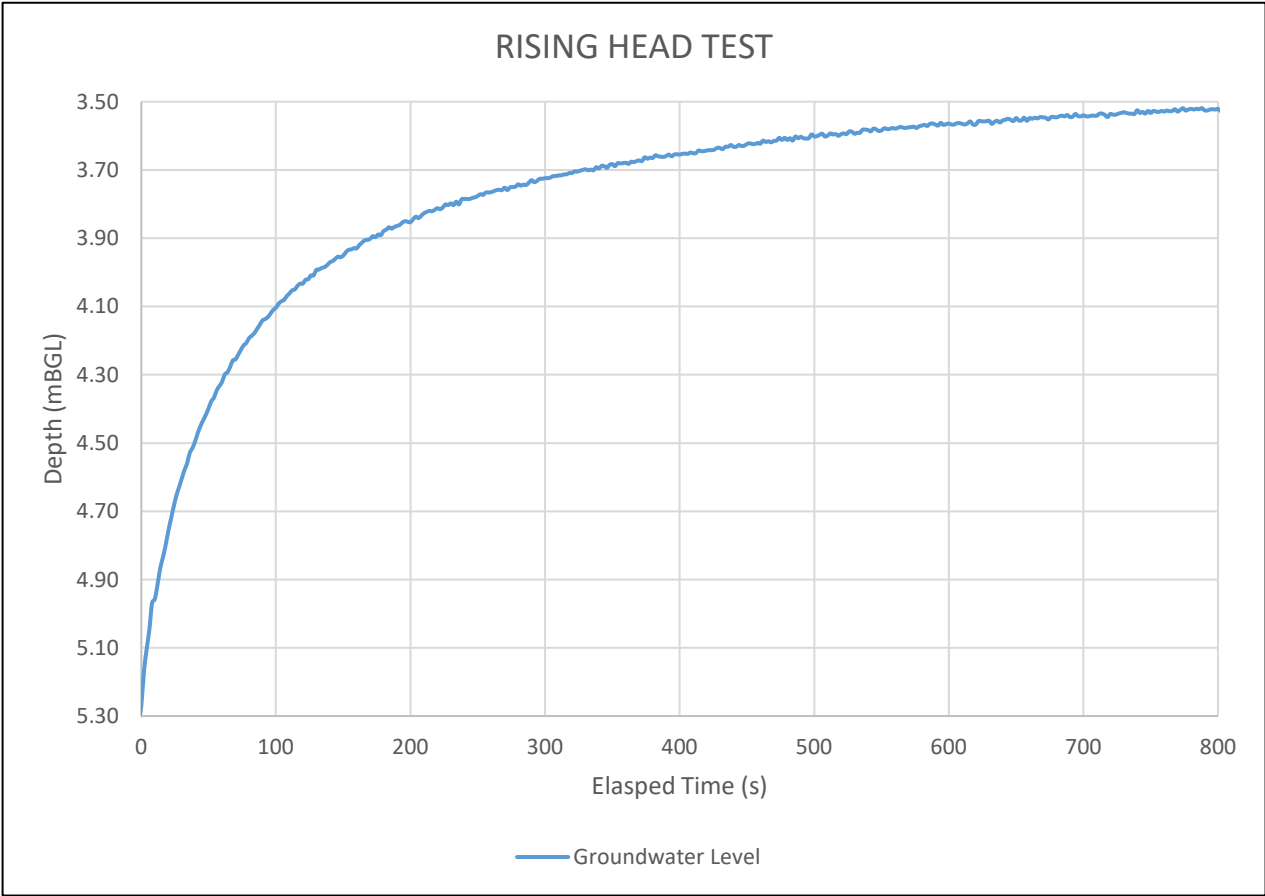
|                 |                                        |
|-----------------|----------------------------------------|
| Project Number  | P3444 - Lindfield                      |
| Address         | 59-63 Trafalgar Ave & 1A/B Valley Road |
| Borehole        | BH2 Test 3                             |
| Monitoring Date | 28/02/2025                             |

|                                            |       |
|--------------------------------------------|-------|
| Static water level (mBGL)                  | 3.13  |
| Internal Diameter (D) (m)                  | 0.07  |
| Length of Standpipe below Ground Level (m) | 19.92 |
| Height of Water above Ground Level (m)     | 0.00  |
| Length of Standpipe above Ground Level (m) | 0.00  |
| Water level at start of test (mBGL)        | 3.13  |
| Top of Response Zone (mBGL)                | 3.13  |
| Bottom of Response Zone (mBGL)             | 19.92 |

|               |    |
|---------------|----|
| Time (t1) (s) | 0  |
| Time (t2) (s) | 66 |

|                             |        |
|-----------------------------|--------|
| Initial Head (H1) at (t1)   | 5.27   |
| Final Head (H2) at (t2)     | 4.28   |
| Length of Response Zone (L) | 16.79  |
| Cross Sectional Area (A)    | 0.0038 |

Stratigraphy Description: Fill overlying residual clay and sandstone bedrock



Intake Factor (F) Case D 
$$\frac{2pL}{\log_e [(L/D) + \ddot{O}(1 + (L/D)^2)]} = \frac{105.49}{6.17} = 17.09$$

Permeability (k) 
$$\frac{A}{F(t_2 - t_1)} \log_e \frac{H_1}{H_2} = 7.12E-07 \text{ m/s}$$

Rising Head Test Method 1 (after Hvorslev)  
Formulae for borehole permeability tests(21.4.6) BS5930 : 1981

Calculation by: AB      Checked by: AM      Date: 14/04/2025

# Rising Head Permeability Results

morrow

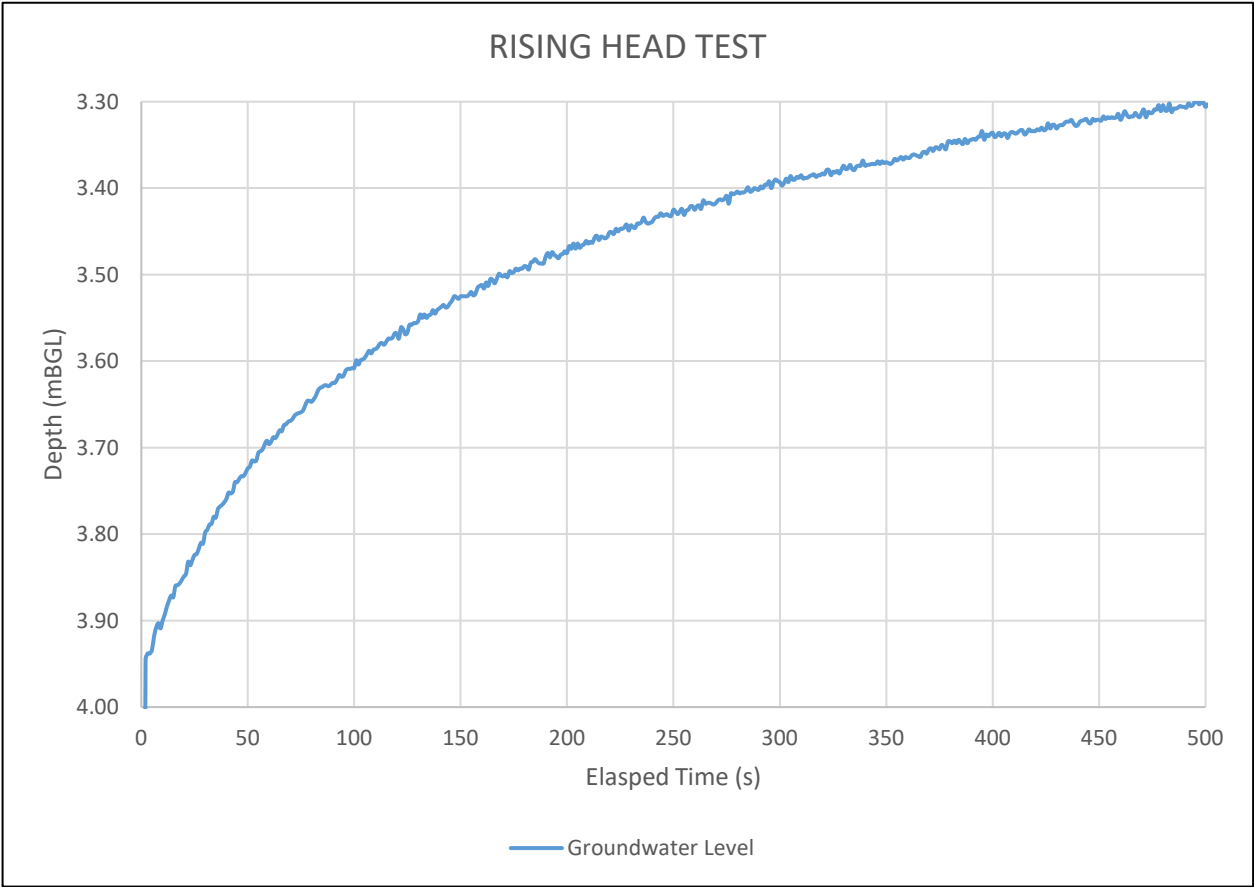
79/6 Bellambi Lane, Bellambi NSW 2518  
P: 0405 843 933 | E: info@morrowgeo.com.au

|                 |                                        |
|-----------------|----------------------------------------|
| Project Number  | P3444 - Lindfield                      |
| Address         | 59-63 Trafalgar Ave & 1A/B Valley Road |
| Borehole        | BH2 Test 4                             |
| Monitoring Date | 2/04/2025                              |

|                                            |       |
|--------------------------------------------|-------|
| Static water level (mBGL)                  | 2.60  |
| Internal Diameter (D) (m)                  | 0.07  |
| Length of Standpipe below Ground Level (m) | 19.92 |
| Height of Water above Ground Level (m)     | 0.00  |
| Length of Standpipe above Ground Level (m) | 0.00  |
| Water level at start of test (mBGL)        | 2.60  |
| Top of Response Zone (mBGL)                | 2.60  |
| Bottom of Response Zone (mBGL)             | 19.92 |

|                             |        |
|-----------------------------|--------|
| Time (t1) (s)               | 2      |
| Time (t2) (s)               | 111    |
| Initial Head (H1) at (t1)   | 3.95   |
| Final Head (H2) at (t2)     | 3.58   |
| Length of Response Zone (L) | 17.32  |
| Cross Sectional Area (A)    | 0.0038 |

Stratigraphy Description: Fill overlying residual clay and sandstone bedrock



Intake Factor (F) Case D 
$$\frac{2pL}{\log_e [(L/D) + \ddot{O}(1 + (L/D)^2)]} = \frac{108.82}{6.20} = 17.54$$

Permeability (k) 
$$\frac{A}{F(t_2 - t_1)} \log_e \frac{H_1}{H_2} = 1.93\text{E-}07 \text{ m/s}$$

Rising Head Test Method 1 (after Hvorslev)  
Formulae for borehole permeability tests(21.4.6) BS5930 : 1981

Calculation by: AB      Checked by: AM      Date: 14/04/2025



# Rising Head Permeability Results

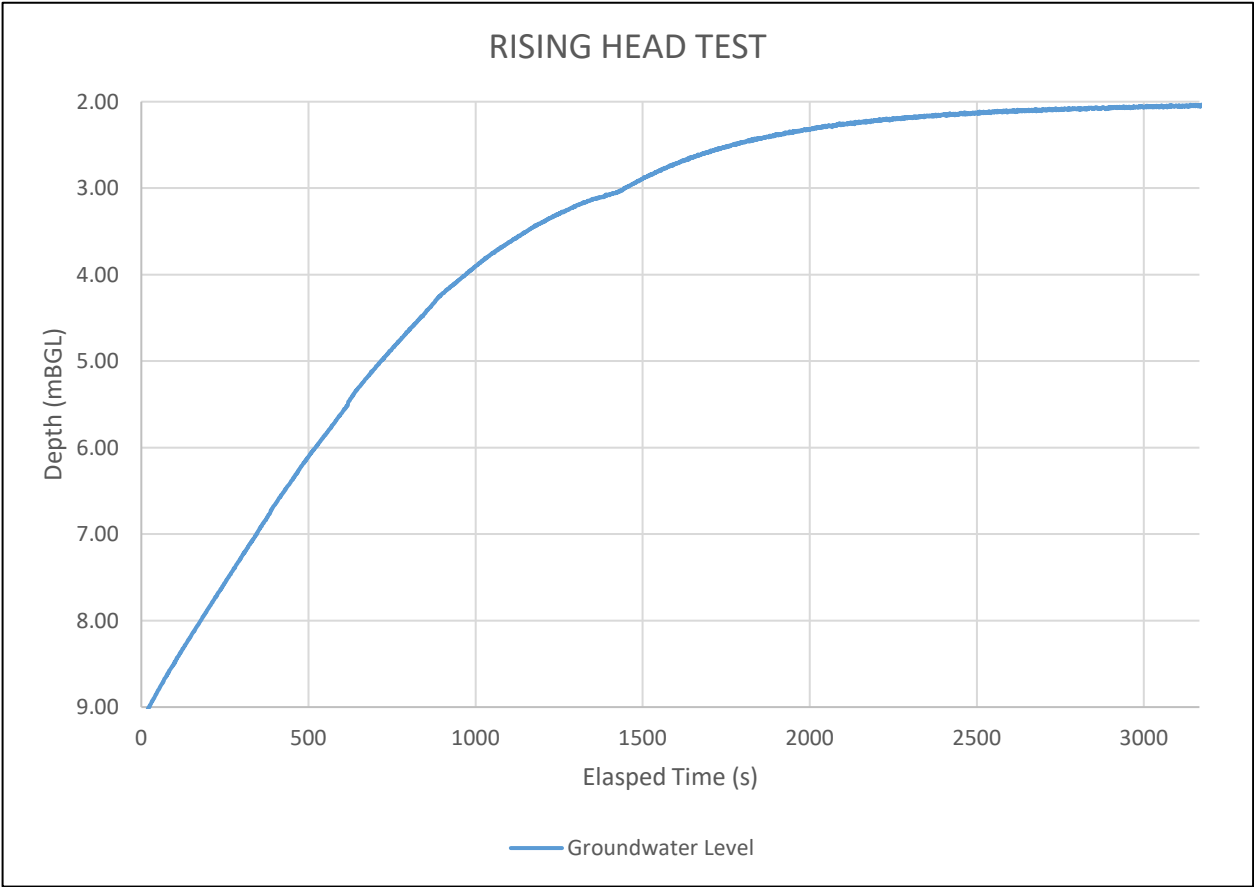
**morrow**

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P: 0405 843 933 | E: info@morrowgeo.com.au

|                 |                                        |
|-----------------|----------------------------------------|
| Project Number  | P3444 - Lindfield                      |
| Address         | 59-63 Trafalgar Ave & 1A/B Valley Road |
| Borehole        | BH5 Test 1                             |
| Monitoring Date | 2/04/2025                              |

|                                            |       |                             |        |
|--------------------------------------------|-------|-----------------------------|--------|
| Static water level (mBGL)                  | 1.95  | Time (t1) (s)               | 53     |
| Internal Diameter (D) (m)                  | 0.07  | Time (t2) (s)               | 993    |
| Length of Standpipe below Ground Level (m) | 18.00 |                             |        |
| Height of Water above Ground Level (m)     | 0.00  | Initial Head (H1) at (t1)   | 8.79   |
| Length of Standpipe above Ground Level (m) | 0.00  | Final Head (H2) at (t2)     | 3.93   |
| Water level at start of test (mBGL)        | 1.95  | Length of Response Zone (L) | 16.05  |
| Top of Response Zone (mBGL)                | 1.95  | Cross Sectional Area (A)    | 0.0038 |
| Bottom of Response Zone (mBGL)             | 18.00 |                             |        |

Stratigraphy Description: Fill overlying residual clay and sandstone bedrock



Intake Factor (F) Case D  $\frac{2pL}{\log_e [(L/D) + \sqrt{1 + (L/D)^2}]}$  =  $\frac{100.85}{6.13}$  = 16.46

Permeability (k)  $\frac{A}{F (t_2 - t_1)} \log_e \frac{H_1}{H_2}$  = 2.00E-07 m/s

Rising Head Test Method 1 (after Hvorslev)  
Formulae for borehole permeability tests(21.4.6) BS5930 : 1981

Calculation by: AB      Checked by: AM      Date: 14/04/2025

# Rising Head Permeability Results

**morrow**

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P: 0405 843 933 | E: info@morrowgeo.com.au

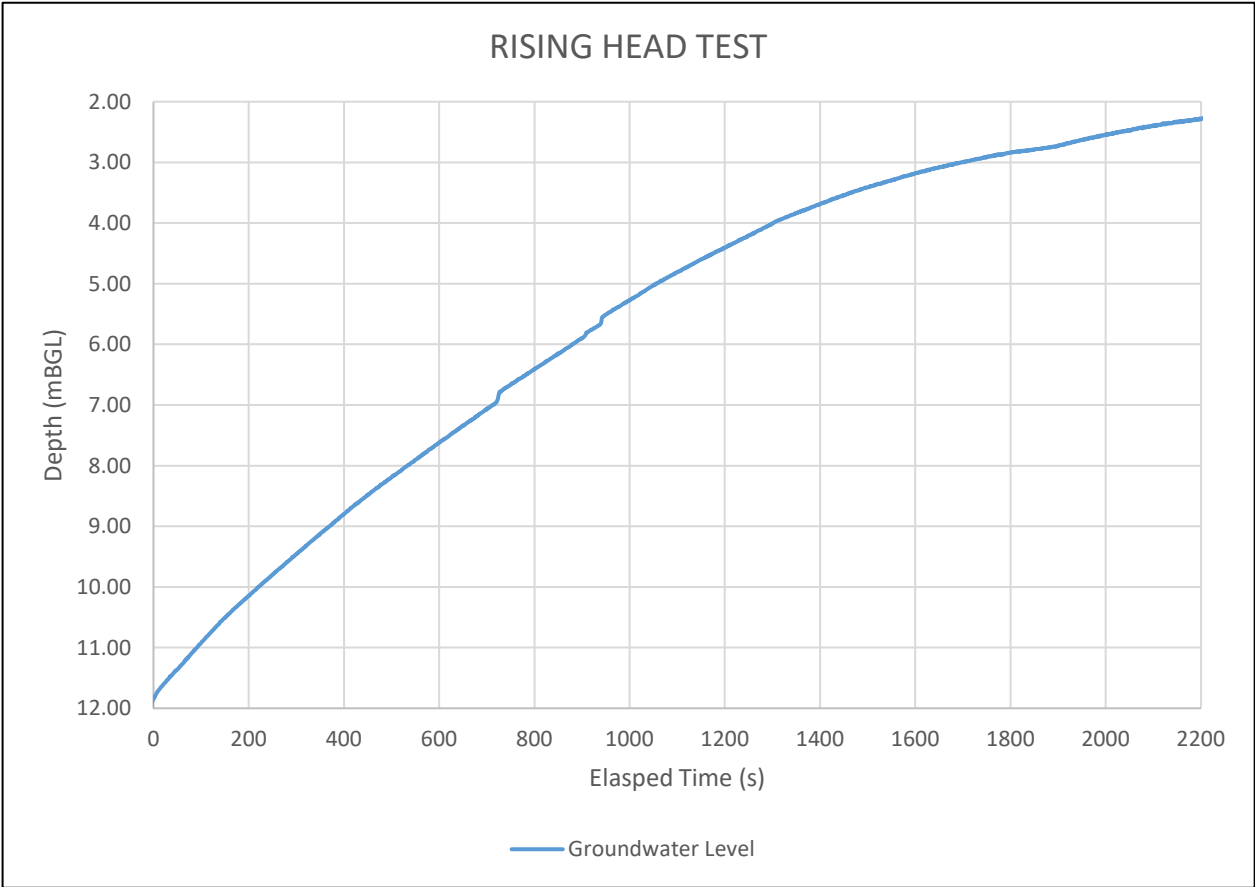
|                 |                                        |
|-----------------|----------------------------------------|
| Project Number  | P3444 - Lindfield                      |
| Address         | 59-63 Trafalgar Ave & 1A/B Valley Road |
| Borehole        | BH5 Test 2                             |
| Monitoring Date | 2/04/2025                              |

|                                            |       |
|--------------------------------------------|-------|
| Static water level (mBGL)                  | 1.95  |
| Internal Diameter (D) (m)                  | 0.07  |
| Length of Standpipe below Ground Level (m) | 18.00 |
| Height of Water above Ground Level (m)     | 0.00  |
| Length of Standpipe above Ground Level (m) | 0.00  |
| Water level at start of test (mBGL)        | 1.95  |
| Top of Response Zone (mBGL)                | 1.95  |
| Bottom of Response Zone (mBGL)             | 18.00 |

|               |      |
|---------------|------|
| Time (t1) (s) | 37   |
| Time (t2) (s) | 1336 |

|                             |        |
|-----------------------------|--------|
| Initial Head (H1) at (t1)   | 11.46  |
| Final Head (H2) at (t2)     | 3.91   |
| Length of Response Zone (L) | 16.05  |
| Cross Sectional Area (A)    | 0.0038 |

Stratigraphy Description: Fill overlying residual clay and sandstone bedrock



Intake Factor (F) Case D  $\frac{2pL}{\log_e [(L/D) + \sqrt{1 + (L/D)^2}]}$  =  $\frac{100.85}{6.13}$  = 16.46

Permeability (k)  $\frac{A}{F(t_2 - t_1)} \log_e \frac{H_1}{H_2}$  = 1.94E-07 m/s

Rising Head Test Method 1 (after Hvorslev)  
Formulae for borehole permeability tests(21.4.6) BS5930 : 1981

Calculation by: **AB**      Checked by: **AM**      Date: **14/04/2025**

# Rising Head Permeability Results

**morrow**

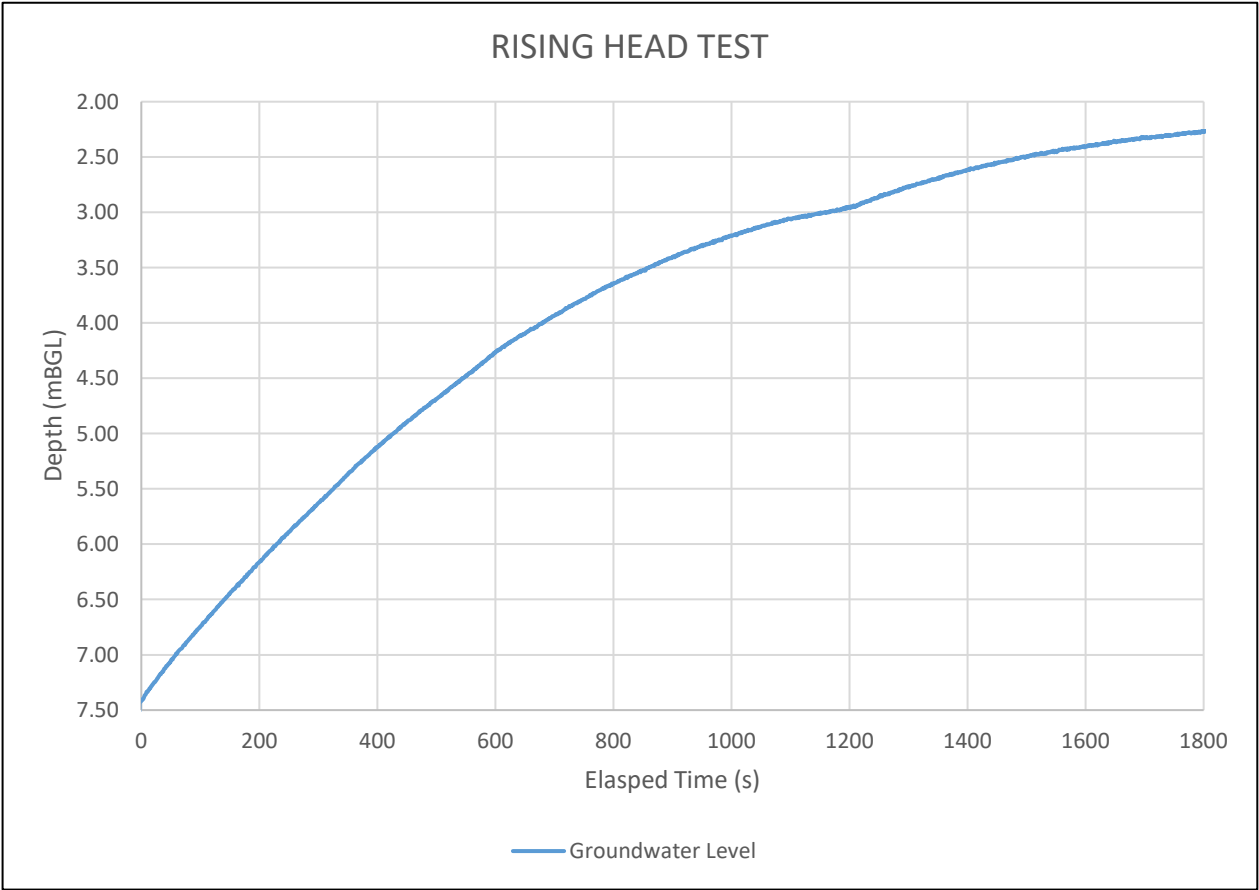
79/6 Bellambi Lane, Bellambi NSW 2518  
P: 0405 843 933 | E: info@morrowgeo.com.au

|                 |                                        |
|-----------------|----------------------------------------|
| Project Number  | P3444 - Lindfield                      |
| Address         | 59-63 Trafalgar Ave & 1A/B Valley Road |
| Borehole        | BH5 Test 3                             |
| Monitoring Date | 2/04/2025                              |

|                                            |       |
|--------------------------------------------|-------|
| Static water level (mBGL)                  | 1.95  |
| Internal Diameter (D) (m)                  | 0.07  |
| Length of Standpipe below Ground Level (m) | 18.00 |
| Height of Water above Ground Level (m)     | 0.00  |
| Length of Standpipe above Ground Level (m) | 0.00  |
| Water level at start of test (mBGL)        | 1.95  |
| Top of Response Zone (mBGL)                | 1.95  |
| Bottom of Response Zone (mBGL)             | 18.00 |

|                             |        |
|-----------------------------|--------|
| Time (t1) (s)               | 1      |
| Time (t2) (s)               | 613    |
| Initial Head (H1) at (t1)   | 7.40   |
| Final Head (H2) at (t2)     | 4.22   |
| Length of Response Zone (L) | 16.05  |
| Cross Sectional Area (A)    | 0.0038 |

Stratigraphy Description: Fill overlying residual clay and sandstone bedrock



Intake Factor (F) Case D  $\frac{2pL}{\log_e [(L/D) + \ddot{O}(1 + (L/D)^2)]}$  =  $\frac{100.85}{6.13}$  = 16.46

Permeability (k)  $\frac{A}{F(t_2-t_1)} \log_e \frac{H_1}{H_2}$  = 2.15E-07 m/s

Rising Head Test Method 1 (after Hvorslev)  
Formulae for borehole permeability tests(21.4.6) BS5930 : 1981

Calculation by: AB      Checked by: AM      Date: 14/04/2025

## **APPENDIX D**

# **IMPORTANT INFORMATION**

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