TRANSPORT AND ACCESSIBILITY **IMPACT ASSESSMENT** 

TAFE NSW Construction Centre of Excellence Nepean Kingswood Campus – 2-44 O'Connell Street, Kingswood

 Reference:
 20.456r02v08

 Date:
 May 2021



Suite 2.08, 50 Holt St Surry Hills, NSW 2010

t: (02) 8324 8700 w: www.traffix.com.au



## DOCUMENT VERIFICATION

| Job Number | 20.456  |               |            |   |
|------------|---|---------------|------------|---|
| Project    | TAFENSW Construction Centre of ExcellenceNepean Kingswood Campus – 2-44 O'Connell Street, Kingswood |               |            |   |
| Address    |   |               |            |   |
| Client     | Client TAFE NSW   |               |            |   |
| Revision   | Date  | Prepared By   | Checked By | Signed  |
| v08        | 19/05/2021  | Justin Pindar | Vince Doan | de la companya de la |

## CONTENTS

| 1. | Response to Submissions  | 1  |
|----|--|----|
|    | 1.1 Transport for New South Wales                              | 1  |
|    | 1.2 Planning, Industry and Environment Response to Submissions | 6  |
|    | 1.3 Council's Response to Submissions                          | 8  |
| 2. | Introduction   | 10 |
| 3. | Location and Site  | 11 |
| 4. | Existing Traffic Conditions                                    | 14 |
|    | 4.1 Road Network   | 14 |
|    | 4.2 Key Intersections  | 17 |
|    | 4.3 Public Transport   | 20 |
|    | 4.4 Sustainable Transport                                      | 24 |
|    | 4.5 Existing Modal Splits                                      | 25 |
| 5. | Description of Proposed Development                            | 27 |
| 6. | Parking Requirements   | 29 |
|    | 6.1 Car Parking  | 29 |
|    | 6.2 Accessible Parking   | 33 |
|    | 6.3 Bicycle Parking  | 33 |
|    | 6.4 Shuttle Bus  | 34 |
|    | 6.5 Refuse Collection and Servicing                            | 34 |
|    | 6.6 Emergency Vehicle Access                                   | 35 |
|    | 6.7 Pick up and Drop Off Arrangements                          | 35 |
| 7. | Traffic and Transport Impacts                                  | 36 |
|    | 7.1 Assumptions from Surveys                                   | 36 |
|    | 7.2 Data Analysis  | 36 |
|    | 7.3 Existing Site Generation                                   | 37 |
|    | 7.4 Growth Rates   | 37 |
|    | 7.5 Development Trip Generation                                | 38 |
|    | 7.6 Assessed Network   | 40 |
|    | 7.7 Traffic Distributions                                      | 40 |
|    | 7.8 Modelling Methodology                                      | 44 |
|    | 7.9 Network Performance  | 34 |
| 8. | Access and Internal Design Aspects                             | 38 |

0

|     | 8.1 | Site Vehicular Access       | 38 |
|-----|-----|-----------------------------|----|
|     | 8.2 | Internal Design             | 38 |
|     | 8.3 | Summary                     | 39 |
| 9.  | Su  | mmary of Responses to SEARS | 40 |
| 10. | Сс  | onclusions                  | 46 |

## Appendices

| Appendix A: | Photographic Record                     |
|-------------|---|
| Appendix B: | Reduced Plans                           |
| Appendix C: | 2021 Weekly Survey Results              |
| Appendix D: | Swept Path Analysis                     |
| Appendix E: | TfNSW Correspondence                    |
| Appendix F: | SIDRA Modelling Outputs                 |
| Appendix G: | Wayfinding, Signage & Line Marking Plan |
| Appendix H: | SEARS Requirements                      |

## 1. RESPONSE TO SUBMISSIONS

### 1.1 Transport for New South Wales

#### Green Travel Plan

#### 1. Comments: Green Star Rating

The Green Travel Plan states:

This GTP is subject to review once the targets outlined in the green star rating have been provided. As such, it is recommended that this GTP, TAG and associated targets be revisited at a later stage, once the green star rating document is available for review.

#### Whereas the EIS states:

The proposed development targets the following: 5 Star Green Star Design & As Built v1.3 rating, considered Australian 'Best Practice'.

#### Recommendation:

The applicant should be able to determine any required mode shift target changes to achieve the 5-Star rating by referring to the Design & As Built V1.3 released by Green Building Council Australia. If the applicant does not consider this possible, a specific revision date should be provided rather than saying "at a later stage". This revision should be undertaken in consultation with TfNSW.

**TRAFFIX Response:** Reference should be made to the Green Travel Plan (GTP) which achieves a Green Star Rating of five (5) points. In addition, the EIS has been updated to be consistent with the GTP.

#### 2. Comments:

a. Sustainable Transport Options -

The GTP has not identified existing cycling infrastructure connecting to the site which staff and students currently use in their journey to the site. Promoting these routes will be important in achieving the proposed 2% mode share shift to cycling.

**TRAFFIX Response:** The GTP now identifies the existing and future cycling infrastructure. Reference should be made to the Sustainable Transport Options - Pedestrian and Bicycle



Facilities (page 5) of the GTP and Strategies and Transport Initiatives -Bicycle Facilities (page 13) of the GTP.

b. Existing Travel Modes –

The GTP has not stated how many responses were received to the interview questionnaire survey that was used to establish the existing travel mode splits. A high response rate would provide an accurate base case scenario.

**TRAFFIX Response:** The Sustainable Transport Calculator has now been used as the reference travel mode which assumes the travel characteristics for the 'reference project', being for 'education' based in the Kingswood – Werrington SA2 zone and data collected from the 2011 census. This provides consistency with the Green Star Sustainable Transport Calculator as the base case scenario. Nevertheless, the Transport and Accessibility Impact Assessment (Section 4.5 of this report) discuss the interview questionnaire survey results with 291 students and staff participating.

c. Strategies and Transport Initiatives –

The GTP has not provided clear actions with timeframes for how each initiative would be implemented to achieve mode shift targets

**TRAFFIX Response:** Reference should be made to Table 3 (page 11) of the revised GTP which provides timeframes and the Strategies and Transport Initiatives (page 12) of the GTP.

d. Green Travel Plan Maintenance –

Travel mode targets should not be revised in favour for private car use. Targets should only be revised in favour for the other travel modes including public transport, walking, cycling. Additional actions should be considered by the applicant to ensure mode shift targets are achieved. The applicant should provide Transport for NSW with the name and contact details of the Travel Plan Coordinator once appointed.

**TRAFFIX Response:** The 'Green Travel Plan Maintenance' (page 14) of the GTP states 'Regular review of the success measures outlined in this plan should be undertaken intermittently to determine whether alternative or supplementary measures are necessary, noting that any revised travel mode targets should favour alternate travel modes (i.e. not private car use).'



e. Summary of the GTP –

The GTP states the long-term targets should be achieved by 2030. It is unclear when the applicant considers the short-term targets should be achieved. If dependant on each stage of construction, indicative milestones could be provided as to ensure mode shift targets are on track to being achieved.

**TRAFFIX Response:** The 'Proposed Travel Modes' (page 11) of the GTP outlines short-term and long-term targets. It is recommended that a survey of staff and students be conducted annually by the Travel Plan Coordinator to monitor the progress of these targets, noting that these targets are primarily indicative and will require on-going evaluation and fine-tuning.

#### <u>Recommendation</u>

TfNSW requests the abovementioned information be addressed and the GTP be updated to reflect the outcomes.

**TRAFFIX Response:** All the above mentioned information has been addressed within the updated GTP. Please refer to the respective sections of the GTP and TIA described above.

#### Transport Assessment

#### 3. Comment

a) It is noted that the cycle times at Great Western Highway (GWH)/O'Connell & French streets are all over the place, they vary from 120s in the existing to 90s in 2026 to 100s in 2026+development. For major arterial roads like GWH, 120s to 140s cycle time is recommended. The modelling should be updated to reflect a consistent cycle time of 120s.

**TRAFFIX Response:** SIDRA Intersection 9 modelling has been updated to incorporate a cycle time of 120 seconds – 140 seconds for all signalised intersections. Reference should be made to the intersection modelling outputs presented in **Appendix E.** 

b. The existing right turn bay on the western approach is currently at around 80% capacity, once the model is updated to reflect the correct cycle times it is likely that the queue length will exceed the length of the bay. Should the queuing exceed the length of the bay, mitigation measures should be investigated and may be required for this movement.

TRAFFIX Response: Reference should be made to Section 7.9.1.



c. From the information presented in the traffic report the number of trips should be about 30% higher than what was concluded in section 6.5, the applicant is to clarify how they arrived at the numbers they present in section 6.5.

**TRAFIX Response:** The vehicle trips are based on survey data and future staff/student population data provided by TAFE NSW. Reference should be made to **Section 7.1** and **Section 7.5**. Traffic volumes of the vehicle trips are highly conservative as noted within **Section 7.9.1**.

d. Table 6 - The intersection performance of GWH/O'Connell St intersection is worsens to LOS D in the 2030 + Dev scenario (PM Peak). Applicant to propose mitigation measures may be required to improve LOS to an acceptable level. TfNSW advises to have all movements at each approach to have LOS C or better if possible.

**TRAFFIX Response:** Reference should be made to **Section 7.9** of this report, noting that whilst queuing lengths do exceed the length of right turn bay lengths on individual movements, the overall intersection operates at a level of service D with a practical cycle time of 120 seconds for this intersection under the 2036 + Development scenario. Intersection performance is not measured based on the performance of individual movements for signalized intersections as per Section 4.2.2 of the *RMS Guide to Traffic Generating Developments (2002)* publication. Rather, RMS Guidelines acknowledge that "The best indicator of the level of service at an intersection is the average delay experienced by vehicles at the intersection. For traffic signals, the average delay over all movements should be taken". Therefore, the operation of this intersection of GWH/O'Connell Street is considered acceptable and is indicative of a worst-case scenario in any case. Reference should also be made to **Section 7.9.1** for further discussion.

e. It is unclear if the swept paths can be achieved without crossing the centreline of O'Connell St and other internal roads involved. To determine if the swept paths of the largest vehicle are able to be achieved without crossing the centreline the swept path analysis shall include details of lane lines, kerb, gutter and median/centreline.

**TRAFFIX Response:** Reference should be made to **Section 8.1** of this report and the swept path analysis presented in **Appendix C** showing the largest vehicle requiring access to the subject site does not cross the centreline. However, it should also be noted that a 12.5m

long HRV is permitted to turn left out of the driveway and take up most of the public road in accordance with Figure 3.1 (Note 1) of AS2890.2 (2018).

f. The reports claim to encourage active transport, however there has been no attempt to entice active transport to the site apart from providing additional bicycling parking at the proposed development. Great Western Highway has a shared path this however reduces to a 900mm path along O'Connell with no bicycle facilities at the entrance. A shaded path along O'Connell should be provided to encourage active transport to the site, the verge back of kerb to property line is 3.5m. In addition, it is noted that the footpaths provided on site are inadequate to be used as shared paths.

**TRAFFIX Response:** Reference should be made to the updated GTP provided separately. TAFE NSW to address item.

g. Connection from the site to the shared path on GWH should be considered along the eastern boundary to the site.

**TRAFFIX Response:** The connection from the site to the shared path on GWH has been considered and is proposed. Reference should be made to the GTP and the updated Architectural Plans (reduced plans provided in **Appendix B**) which now include shared pathway connection from the building to the GWH.

h. The intersection of GWH/Western Sydney University has not been assessed. Should there be access between the TAFE and University, students can rat run to access the parking closer to the development. In this regard the intersection of GWH/Western Sydney University should be considered in the model.

**TRAFFIX Response:** It is noted that rat running will not be possible to access the TAFE site as there is no vehicular access between TAFE and University car parks. In addition, WSU provides paid parking whereas TAFE parking is free. As a result, TAFE staff and students would park their vehicles within the TAFE car park with access via O'Connell Street. Therefore, the intersection of GWH / WSU is not considered a critical intersection and not required to be modelled.



#### Recommendation:

TfNSW requests the abovementioned information be addressed and the TIA be updated to reflect the outcomes.

#### Construction Traffic Management Plan (CTMP)

#### 4. Comment

a. Section 5.1.2: The truck routes will be using the GWH/Western Sydney University intersection. Modelling of this intersection is required to show the results of the intersection performance on each stage of work.

**TRAFFIX Response:** SIDRA 9 Intersection modelling has been conducted for the worst-case scenario of construction being bulk excavation noting that there are only minor changes to intersection delays with level of service A. As such, the development construction is considered supportable from a traffic planning perspective with no external improvements to the network required. Reference should be made to Section 6.2 of the updated Preliminary CTPMP provided separately.

b. Appendix C Loading Zone Swept Paths: Traffic Controller is recommended to ensure there is no conflict between construction trucks and vehicles / pedestrians using the carpark.

**TRAFFIX Response:** Appendix C Loading Zone swept path has been updated to include a traffic controller. It is noted that this is a Preliminary CTPMP and further details of traffic controllers will be provided within the detailed CTPMP and final TCPs.

### 1.2 Planning, Industry and Environment Response to Submissions

Concerns are raised regarding the traffic including the appropriateness of the traffic model used to inform the Traffic Impact Assessment and of the proposal's impact on the performance of the Great Western Highway (GWH) / O'Connell Street intersection. The Department requires you to address these concerns, including but not limited to the provision of:

• an updated traffic model to reflect a consistent cycle time of 120s at the GWH / O'Connell and French Street intersection.



- detailed mitigation measures should queuing exceed the length of the right turn bay GWH / O'Connell Street, and any mitigation measures required to improve LOS to an acceptable level.
- modelling of the GWH / Western Sydney University intersection, demonstrating the results of the intersection performance during each stage of construction work.

**TRAFFIX Response:** SIDRA Intersection 9 modelling has been updated to incorporate a cycle time of 120 seconds – 140 seconds for all signalised intersections as per TfNSW requirements. Reference should be made to the intersection modelling outputs presented in **Appendix E**. Reference should also be made to **Section 7.9.1** of this report in relation to the intersection performance for Great Western Highway, French Street and O'Connell Street in the 2030 + development scenario.

• additional evidence to demonstrate that the swept paths of construction vehicles can be achieved without crossing the centreline of O'Connell Street and other internal roads.

**TRAFFIX Response:** Construction vehicles are not to access O'Connell Street. Access for construction vehicles will be via the intersection of GWH with WUS access. However, it should also be noted that a HRV is permitted to turn left out of the driveway and take up most of the public road in accordance with Figure 3.1 (Note 1) of AS2890.2 (2018).

The Department also notes Council's concerns that the proposal does not provide sufficient on-site car parking when existing parking rates are applied to the proposal, compounded by TfNSW's comments regarding a lack of adequate information provided within the Green Travel Plan (GTP).

**TRAFFIX Response:** Updated parking surveys have been conducted over a typical week on each weekday from Monday 19<sup>th</sup> April 2021 – Friday 23<sup>rd</sup> April 2021 to understand onsite parking demand during a typical semester over a week. Reference should be made to **Section 6.1** of this report.

Please provide the following:

- further justification and details regarding the target driver modal split of 70 per cent for the 2030 scenario.
- a revised GTP to provide clear actions with timeframes for how each initiative would be implemented to achieve mode shift targets.
- consideration of additional actions to ensure the mode shift targets are achieved.



 additional information regarding the capacity/usage of the existing north/central campus carpark (west of the pond), and proposed methods of improving connections between the carpark and the proposed building site, if any. Note: this carpark appeared to be somewhat under-utilised during a Department officer visit to the site.

**TRAFFIX Response:** Reference should be made to the Green Travel Plan for discussion regarding driver model split targets, actions and timeframes. Updated parking surveys have been conducted over a typical week. Discussion in relation to parking can be found in **Section 6.1**.

### 1.3 Council's Response to Submissions

The proposal has been considered having regard to traffic management and car parking considerations and the following aspects are identified for further address:

The proposal currently does not provide sufficient on-site parking to cater for the proposed development when existing car parking demand rates are applied to the proposal. The submitted traffic report states that 84% of students and staff currently drive to the TAFE campus however in suggesting a reduced parking rate, the report assumes that the percentage of students and staff driving to the site will reduce down to 70% by 2030. There does not appear to be a strong basis for this assumption, noting specifically that there is no station proposed to be constructed at this campus or WSU as part of the Metro works. Further clarification and justification is sought from the applicant on the reasoning and rationale for the suggested parking reduction as there does not appear to be sufficient basis for the parking supply proposed. This justification should be based on projected modelling post Metro construction and any other information or modelling associated with similar facilities that has informed the proposed reduced parking rate as now proposed.

**TRAFIX Response:** Reference should be made to **Section 6.1** of this report. All parking demands are readily accommodated onsite with a safety margin of more than 60 parking spaces in the 2030 development scenario, assuming no changes to parking demand from implementation the proposed Green Travel Plan. The adopted parking strategy and target modal splits are strongly supported and will deliver a sustainable planning outcome that is in the public interest. However, it is considered of importance that the current travel behaviour is not replicated in 2030, to drive a more sustainable planning outcome as a matter of good policy.



The traffic report outlines that key intersections surrounding the development will be reduced to a level of service D which indicates that mitigation measures should be investigated for implementation as part of the development.

**TRAFIX Response:** Reference should be made to **Section 7.9** of this report, noting that whilst queuing lengths do exceed the length of right turn bay lengths on individual movements, the overall intersection operates at a level of service D with a practical cycle time of 120 seconds for the intersection of GWH/O'Connell Street under the 2036 + Development scenario. Intersection performance is not measured based on the performance of individual movements for signalized intersections as per RMS Guidelines. Rather, Section 4.2.2 of the RMS Guide to Traffic Generating Developments (2002) publication acknowledge that "The best indicator of the level of service at an intersection is the average delay experienced by vehicles at the intersection. For traffic signals, the average delay over all movements should be taken". Therefore, the operation of this intersection of GWH/O'Connell Street is considered acceptable and is indicative of a worst-case scenario in any case. Reference should also be made to **Section 7.9.1** for further discussion.

The provided swept paths in the traffic report appear to show the service vehicle taking up the majority of the width of the circulation roadways and driveway. This is not appropriate, is unsafe and the driveway and circulation roadways should be widened to accommodate passing of the service vehicle and a passenger vehicle.

**TRAFFIX Response:** Appropriate passing opportunities have been provided within the onsite carpark and TRAFFIX confirms that internal traffic will be managed safely and efficiently in accordance with AS2890.1 (2004) and AS2890.2 (2018). Reference should be made to **Section 8.2** of this report. In addition, a loading dock management plan can be provided at a later stage during construction certificate.



## 2. INTRODUCTION

TRAFFIX has been commissioned by Cadence Australia Pty Ltd on behalf of TAFE NSW to prepare a Transport and Accessibility Impact Assessment report in relation to the proposed TAFE NSW Construction Centre of Excellence at the Nepean Kingswood campus at 2-44 O'Connell Street, Kingswood. The development will be assessed by the Department of Planning, Industry and Environment for determination.

The student and staff populations are projected to increase over a 7-year period following construction of the proposed development. This report assesses the impacts associated with the expansion of the existing TAFE campus having regard for two forecast population scenarios over time: 2023 and 2030. The development is a State Significant Development (SSD) and therefore is required to respond to the Secretary's Environmental Assessment Requirements (SEARs) as provided by the Department of Planning and Environment.

This report documents the findings of our investigations and should be read in the context of the Statement of Environmental Effects (SEE) prepared separately. Reference should also be made to the SEARs (Application Number SSD-8571481).

The report is structured as follows:

- ) Section 2: Describes the site and its location
- ) Section 3: Documents existing traffic conditions
- ) Section 4: Describes the proposed development
- ) Section 5: Assesses the parking requirements
- ) Section 6: Assesses traffic impacts
- ) Section 7: Discusses access and internal design aspects
- ) Section 8: Addresses the SEARs
- ) Section 9: Presents the overall study conclusion



## 3. LOCATION AND SITE

The subject site is located within the TAFE NSW Nepean Kingswood campus at 2-44 O'Connell Street, Kingswood (Lot 1 in DP866081). More specifically, it is situated along the eastern boundary of the campus, north of 'Building T' and adjacent 'Building BA' of the Western Sydney University (WSU) Werrington South campus.

The site is rectangular in configuration with a total site area of approximately 2.1 hectares. It has a northern boundary to recreational area and a southern boundary to Building T of the TAFE that measure approximately 100 metres. The remaining eastern and western boundaries measure approximately 210 metres to the internal road/Building BA of WSU and recreational area of the TAFE, respectively.

Vehicular access to the wider TAFE site is currently provided via the following vehicular crossings which provide access to two separate carparking areas:

- ) Gate 1 Access: O'Connell Street (northern access); and
- ) Gate 2 Access: O'Connell Street (southern access).

Vehicular access to the subject site is proposed via the Gate 2 O'Connell Street access driveway.

A Location Plan is presented in **Figure 1**, with a Site Plan presented in **Figure 2**. Reference should also be made to the photographic record presented in **Appendix A**, which provides an appreciation of the general character of roads and other key attributes in proximity to the site.

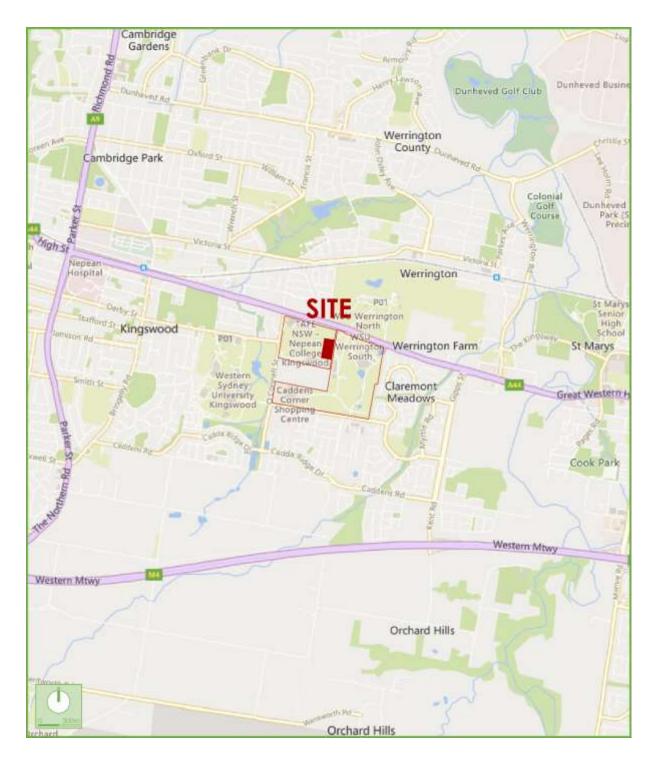


Figure 1: Location Plan



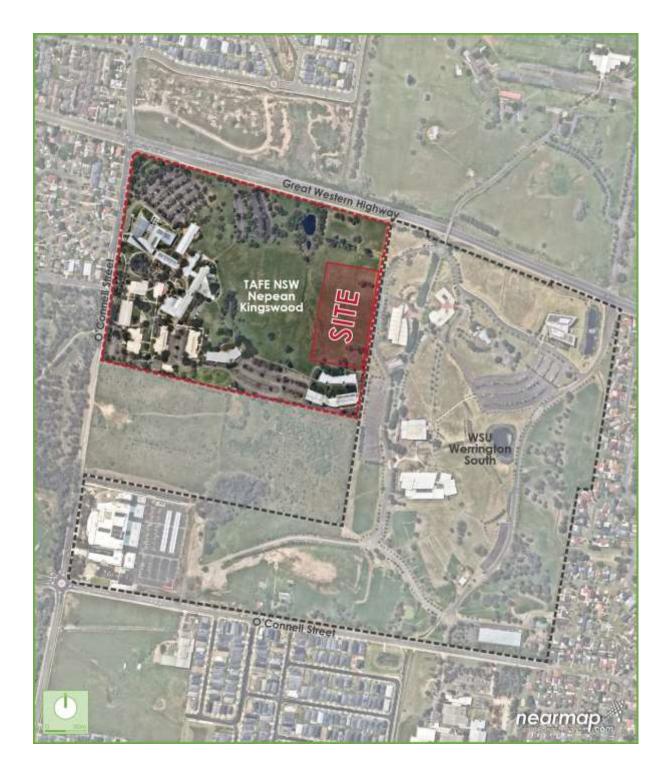


Figure 2: Site Plan



## 4. EXISTING TRAFFIC CONDITIONS

### 4.1 Road Network

The road hierarchy in the vicinity of the site is shown in **Figure 3** with the following roads of particular interest:

| ) | Great Western Highway: | an RMS highway (HW5) that traverses east-west between<br>Sydney in the east and Bathurst in the west. Within the<br>vicinity of the site, it is generally subject to 80km/h speed<br>zoning (60km/h within proximity of the O'Connell Street<br>intersection) and accommodates 2-3 lanes of traffic in<br>each direction. Great Western Highway does not permit<br>on-street parking and has been identified by the RMS as an<br>approved 26.0m B-Double route. |
|---|------------------------|---|
| ) | Gipps Street:          | a local road that traverses north-south between the Great<br>Western Highway (HW5) in the north and Kent Road in the<br>south. It is subject to 80km/h speed zoning and<br>accommodates two (2) lanes of traffic in each direction.<br>Gipps Street does not permit on-street parking along both<br>sides of the road.  |
| ) | O'Connell Street:      | a local road that traverses north-east between the Great<br>Western Highway (HW5) in the north and Sunflower Drive in<br>the east. It is generally subject to 50-60km/h speed zoning<br>and accommodates a single lane of traffic in each<br>direction. O'Connell Street permits on-street parking along<br>both sides of the road.   |
| ) | Bringelly Road:        | a local collector road that traverses north-south between<br>the Great Western Highway (HW5) in the north and The<br>Northern Road / Parker Street in the south. It is subject to<br>50km/h speed zoning and accommodates a single lane of<br>traffic in each direction within an undivided carriageway.<br>Parallel parking is generally permitted along both kerbside   |

of Bringelly Road.

- ) Caddens Road: a local collector road that traverses east-west forming a cul-de-sac in the east and connecting to Bringelly Road in the west. It is noted that Caddens Road is not a continuous road and provides sections of road break. It is subject to 50km/h speed zoning and accommodates a single lane of traffic in each direction within an undivided carriageway. On-street parking is generally not permitted west of Ulm Road.
- ) Kent Road: a local collector road that traverses north-south between Caddens Road in the north and Landsdowne Road in the south. It is subject to 80km/h speed zoning and accommodates two (2) lanes of traffic in each direction within a divided carriageway in the vicinity of its intersection with Caddens Road. On-street parking is not permitted along its length in either direction.

It can be seen from **Figure 3** that the site is conveniently located with respect to the main arterial road network serving the region being the Great Western Highway. As such, traffic can effectively be distributed onto the wider road network, minimising traffic impacts.



Figure 3: Road Hierarchy



## 4.2 Key Intersections

The key intersections in the vicinity of the site are shown below and provide an understanding of the existing road geometry and alignment in the locality.



#### 4.2.1 Great Western Highway, O'Connell Street and French Street

#### Figure 4: Intersection of Great Western Highway, O'Connell Street and French Street

It can be seen from **Figure 4** that the intersection of Great Western Highway, O'Connell Street and French Street is a four-legged signalised intersection, with the east and west legs providing signalised pedestrian crossings. The main attributes of each approach are outlined below.

- ) Great Western Highway (east-west)
  - The eastern approach provides two (2) through lanes, one (1) through lane from which left turns can be made and one (1) right-turn only lane.
  - The western approach provides two (2) through lanes, one (1) through lane from which left turns can be made and one (1) right-turn only lane.
- ) O'Connell Street (south)
  - The southern approach provides one (1) through lane from which left turns can be made and one (1) through lane from which right turns can be made.



- ) French Street (north)
  - The northern approach provides one (1) through lane from which through, left and right turns can be made.

#### 4.2.2 Great Western Highway and Bringelly Road



#### Figure 5: Intersection of Great Western Highway and Bringelly Road

It can be seen from **Figure 5** that the intersection of Great Western Highway and Bringelly Road is a three-legged signalised T-intersection, with signalised pedestrian crossings provided along all legs. The main attributes of each approach are outlined below.

- ) Great Western Highway (east-west)
  - The eastern approach provides two (2) through lanes and one (1) through lane from which left turns can be made.
  - The western approach provides three (3) through lanes, and one (1) right turn only lane.
- ) Bringelly Road (south)
  - The southern approach provides one (1) left turn lane and one (1) right turn lane.





Figure 6: Intersection of Gipps Street, Kent Road and Caddens Road

It can be seen from **Figure 6** that the intersection of Caddens Road, Gipps Street and Kent Road is a four-legged signalised intersection, with signalised pedestrian crossings provided along all legs. The main attributes of each approach are outlined below.

- ) Caddens Road (east-west)
  - The eastern approach provides one (1) right turn only lane and one (1) shared through lane from which left turns can be made
  - The western approach provides one (1) right turn only lane and one (1) shared through lane from which let turns can be made.
- ) Kent Road (south)
  - The southern approach provides one (1) through lane, one (1) shared through lane from which left turns can be made and one (1) right turn only lane.
- ) Kent Road (south)
  - The southern approach provides one (1) through lane, one (1) shared through lane from which left turns can be made and one (1) right turn only lane.

- ) Gipps Street (north)
  - The northern approach provides one (1) through lane, one (1) shared through lane from which left turns can be made and one (1) right turn only lane.

The assessment of the existing performance of the above key intersections during the critical morning and evening network peaks is discussed in Section 6.

### 4.3 Public Transport

#### 4.3.1 Bus Services

The subject site is within optimal walking distance (400 metres) of several bus services operating along O'Connell Street and the Great Western Highway. These bus services are presented in **Figure 7**, with the service frequencies during peak periods outlined in **Table 1** below.

| D       | us No. | Route                                    | Service Frequency   |                  |
|---------|--------|--|---------------------|------------------|
| DUS NO. |        | KOUIE                                    | Weekdays            | Saturdays        |
|         | 770    | Mount Druitt to Penrith via St Marys     | Every 20-30 minutes | Every 60 minutes |
|         | 775    | Mount Druitt to Penrith via Erskine Park | Every 30 minutes    | Every 60 minutes |
|         | 776    | Mount Druitt to Penrith via St Clair     | Every 20-30 minutes | Every 60 minutes |
|         | 835    | UWS to Prairiewood                       | Every 30 minutes    | -                |

#### Table 1: Bus Routes and Service Frequencies

Furthermore, these above bus services provide regular services to Penrith, St Marys and Mount Druitt railway stations, which provide railway services along the following lines:

- ) T1 North Shore and Western Line
- ) T5 Cumberland Line
- ) BML Blue Mountains Line
- ) Regional Western NSW Line



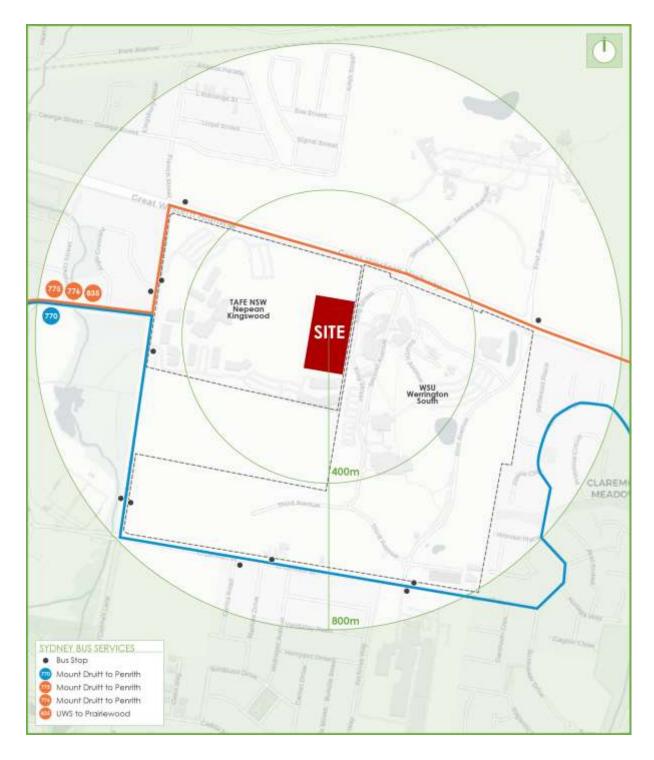


Figure 7: Bus Services

#### 4.3.2 Metro Services

It is likely that St Mary's Train Station will be extended under the South West Rail Link Extension to connect the existing passenger rail line from St Mary's to the Aerotropolis which is now part of the Sydney Metro Greater West – Nancy Bird Walton International Airport project.

In future, students and staff who may live in other suburbs can take advantage of the metro service to get to the site and services will be frequent (approximately every 5-10 minutes, in line with other Sydney Metro projects). This is presented in **Figure 8** below and will significantly alter current modal splits, which are heavily weighted to private car travel.

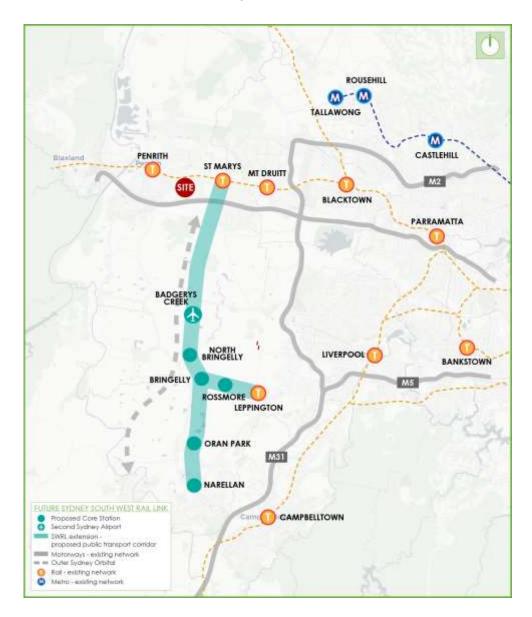


Figure 8: Metro Services



#### 4.3.3 Shuttle Bus Services

The existing WSU campus provides a private shuttle bus service for existing WSU students and staff between Kingswood Railway Station and the WSU Werrington and Kingswood campus. A proposal is in place to provide a shared shuttle bus service for WSU and TAFE students and staff with regular services between Kingswood Station in the west and the TAFE / WSU in the east. The shuttle bus would pick up and drop off students via the existing internal roadway access via the WSU vehicular access to Great Western Highway. The pick-up and drop off area are to be DDA compliant thereby ensuring ease of access to mobility impaired passengers. It is noted that the estimated time between services is 30 minutes operating from 7:00am to 7:00pm Monday to Friday with the following bus stops:

- ) Kingswood Station (Great Western Highway, slightly East of the entrance to the Station)
- ) Kingswood Campus (Kingswood Campus Student Plaza)
- ) Werrington South Campus (buildings BA, BD)
- ) Werrington Corporate Park
- ) Kingswood Campus (Student Residential College, Library and Building F)

The indictive proposed shuttle bus route and internal pick up and drop off for the TAFE students is shown in **Figure 9** below.

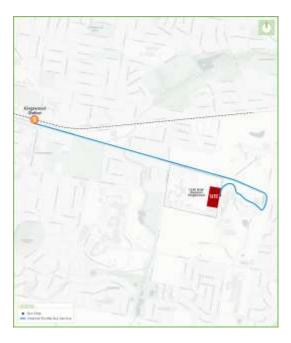


Figure 9: Shuttle Bus Route



## 4.4 Sustainable Transport

The area surrounding the subject site is well developed with established road and pedestrian footpath networks connecting the site with nearby public transport infrastructure as well as neighbouring residential developments. In addition, the bicycle network in the locality is shown in **Figure 10** below.

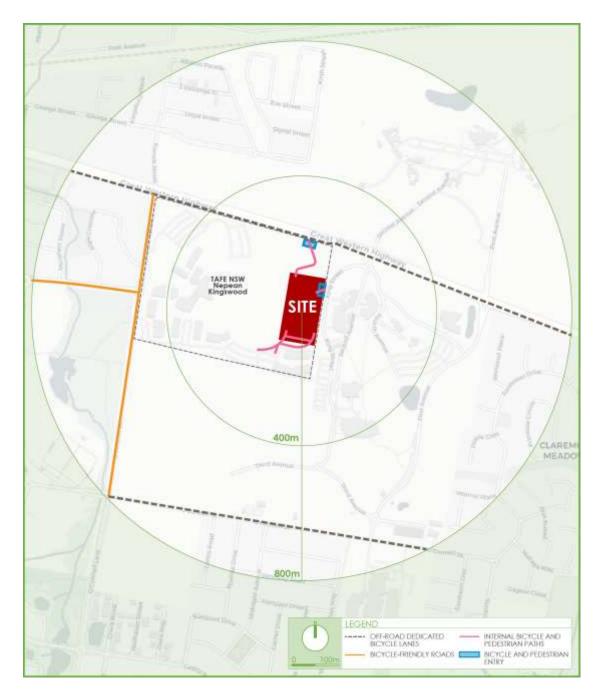


Figure 10: Cycleways



The TAFE proposes to retain the following accesses to the site, comprising:

- ) 1 x main pedestrian and vehicular access via O'Connell Street (northern access)
- ) 1 x vehicular access via O'Connell Street (southern access).

Finally, a new shared path is proposed connecting the new Construction Centre of Excellence Building in the eastern sector of the site with the existing TAFE building in the western sector of the site, thereby encouraging more sustainable modes of transport.

### 4.5 Existing Modal Splits

Existing travel modal splits has been determined based on interview questionnaire survey responses which were distributed to existing staff and students. The results from 291 students and staff participating are summarised in **Table 2** as follows:

| Travel Mode                | Travel Percentage |
|----------------------------|-------------------|
| Car Driver <sup>1</sup>    | 84%               |
| Car Passenger <sup>2</sup> | 6%                |
| Train                      | 4%                |
| Bus                        | 4%                |
| Bicycle                    | 2%                |
| Walk                       | 0%                |
| Train & Shuttle Bus        | 0%                |

#### Table 3: Existing Travel Modal Splits

1 - Car driver includes motorcyclists.

2 - Includes car passenger dropped off and car passenger's carpooling with other students or staff.

It can be seen from **Table 3** above that the vast majority of staff and students (84%) drove and parked whilst only 10% of arrivals were by other modes of transport (public transport, cycle or walk). It should be noted the above travel modal splits between private vehicles and other travel modal splits were obtained from questionnaire surveys and are slightly different from the reference travel modal splits outlines in the Green Travel Plan which were derived from the Green Star Sustainable Transport Calculator provided to TRAFFIX and cannot be altered. However, it is noted the travel modal splits obtained from the surveys are similar to the reference

travel modal splits provided in the Green Star Sustainable Transport Calculator and are therefore aligned.



## 5. DESCRIPTION OF PROPOSED DEVELOPMENT

The subject development involves construction of a new Construction Centre of Excellence (CCoE) Building within the northeast corner of the existing TAFE NSW Nepean Kingswood Campus. The development is proposed to be completed by 2023 with student and staff populations projected to grow over a 7-year period. This report focuses on the traffic impacts associated with projected student and staff populations in the following years:

- ) Existing (2020) 6,000 students enrolments annually
- 2023 an additional 1,750 projected students from CCoE
   Projected TAFE NSW Kingswood Campus annual student population of 7,750
- 2030 an additional 3,500 projected students over existing (2020) from CCoE
   Projected TAFE NSW Kingswood Campus annual student population of 9,500

The above related to student enrolments through the year. However, these enrolments are dispersed throughout the week and daytime activity relating to the number of staff and students on a typical peak weekday between 7.30am - 5.00pm are summarised in **Table 4**.

| Year | Staff | Students | Total |
|------|-------|----------|-------|
| 2020 | 39    | 998      | 1037  |
| 2023 | 61    | 1185     | 1246  |
| 2030 | 78    | 1439     | 1517  |

#### **Table 4: On Site Peak Attendances**

It can be seen from Table 4 that at full development, the site will need to accommodate an additional 480 persons daily over the 7-year forecast population growth timeframe. It is important to note that not all of these staff and students will be on site at one time over this period. In addition, the development will incorporate:

- ) New carparking comprising 16 car parking spaces for students and staff;
- ) Loading area south of the proposed Construction Centre of Excellence Building;
- ) New shared path connecting the existing TAFE buildings to the west of the site with the proposed Construction Centre of Excellence Building.

Reference should be made to the plans submitted separately to Council which are presented at reduced scale in **Appendix B**.

# 6. PARKING REQUIREMENTS

### 6.1 Car Parking

#### 6.1.1 Council Controls & RMS Guidance

Penrith City Council's Development Control Plan (DCP) and the RMS Guide to Traffic Generating Developments 2002 have been reviewed; however, neither of these guidelines assess the tertiary educational uses proposed by the subject development. it is noted that the Penrith City Council DCP 2014 Section C10 (Transport Access & Parking) states as follows:

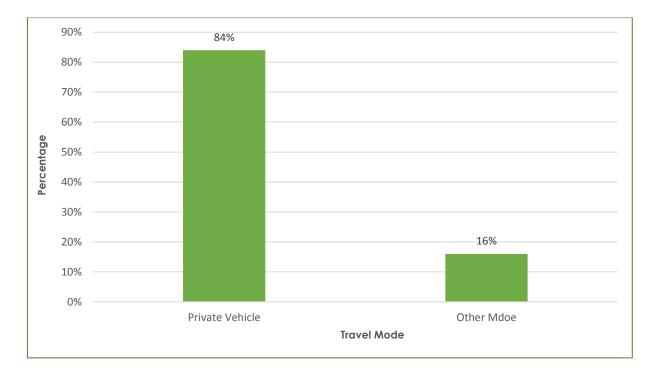
"(f)) In the absence of specific requirements relevant to particular developments, the parking requirements in the RTA's "Guide to Traffic Generating Developments" (as updated) and Australian Standard AS 2890.1 and 2 - 2004 should be referred to as a guide. In the absence of all data, the applicant should revert to the use of first principles."

A superior methodology is a 'survey based' assessment and this has been undertaken to determine the future parking demand and corresponding on-site parking requirement associated with the proposed development, which is the preferred methodology based on RMS Guidelines and appropriate where the expansion of an existing facility is proposed.

#### 6.1.2 Survey Based Assessment

Online interview/questionnaire surveys were undertaken of staff and students at the existing TAFE campus, between 27<sup>th</sup> November and 15<sup>th</sup> December 2020. These surveys were designed to establish existing modal splits and travel behaviour of staff and students. A total of 291 interview questionnaire surveys were returned, comprising 191 student responses and 100 staff responses.

The results are shown in **Chart 1** below for the combined TAFE population, noting that the results for staff and students were similar.



#### Chart 1: Student and Staff Modal Choice to and From Campus

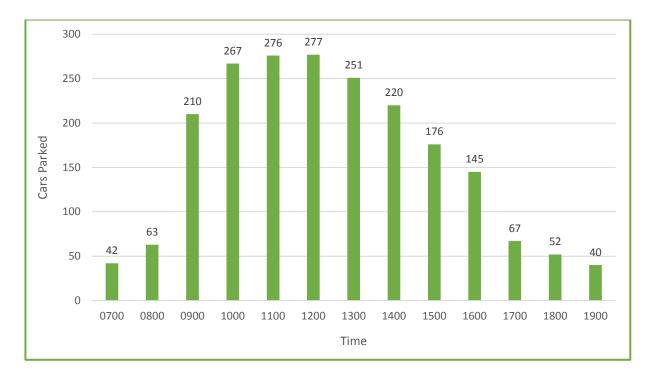
It can be seen from Chart 1 that the following is evident:

- ) 84% of students and staff drove and parked within the subject site.
- ) These drivers arrived prior to 9:30am;
- ) The balance of 16% of arrivals occurred after 9:30am; and
- ) 36% of departures occurred prior to 4:00pm, outside the on-street commuter peak.

Therefore, the peak parking demand occurred after 9:30am, was sustained until about 1:00pm and decreased progressively after that time.

#### 6.1.3 2020 On-site Parking Survey

The peak parking demand timeframe (after 9:30am) has been validated by undertaking separate parking surveys of the internal campus carparks. These surveys were undertaken on Thursday 26<sup>th</sup> November 2020 between 7:00am and 7:00pm. The results are summarised in **Chart 2** below.



#### Chart 2: Weekday On-Site Parking Occupancy

It is evident from **Chart 2** that the parking demand at 9:30am is approximately 238 spaces. This is 86% of the peak demand that occurs at midday, which is very close to the 84% of arrivals prior to 9:30am based on the questionnaire surveys. It is noted that the existing TAFE Nepean Kingswood campus provides a total of 907 car parking spaces. It is emphasised that the above results reflect conditions during COVID restrictions, which therefore reflects a lower attendance level. However, the spread of activity (demand profile) across the day is expected to be similar to that shown in **Chart 2**. Accordingly, additional surveys were conducted in 2021 when the TAFE was fully operational with no COVID restrictions. This is discussed in detailed below.

#### 6.1.4 2021 (Existing) Onsite Parking Demand

Additional on-site parking surveys were conducted over a typical week on each weekday from Monday 19<sup>th</sup> April 2021 – Friday 23<sup>rd</sup> April 2021 to understand onsite parking demand during a typical semester over a week. The day with the highest parking demand, (thereby representing a worst-case scenario) was Wednesday 21<sup>st</sup> April. A summary of the parking demand profile across this day is presented in **Chart 3** below with survey result for the week provided in **Appendix C**.

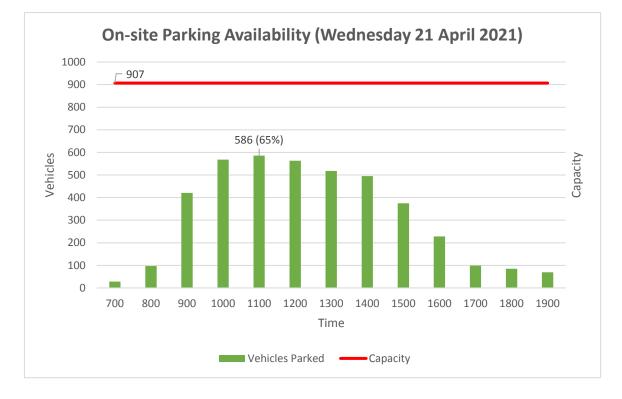


Chart 3: Weekday On-Site Parking Availability (Wednesday 21st April 2021)

It can be seen from **Chart 3** above that parking demand peaked at 11:00am when 586 out of 907 (65%) parking spaces were occupied, which is equivalent to 1 space per 1.8 daily persons in attendance (1037). Therefore, a surplus of 321 (35%) parking spaces were available at 11:00am when parking demand peaked. This represents a worst-case scenario and the impact of the subject development on available parking provision for the 2023 and 2030 development scenarios is discussed in Sections 6.1.5 and 6.1.6 below.

#### 6.1.5 2023 Development Scenario Parking Demand

The 2023 development scenario is projected to relate to an additional 210 staff and students, from 1037 to 1247. Based on the existing demand profile of 1 space per 1.8 daily persons in attendance (derived above), this would result in a net additional 117 car spaces. This can be readily accommodated by the existing parking surplus of 321 spaces.

Nevertheless, it is highly noteworthy that this assumes no change in current travel behaviour. In addition, the Green Travel Plan accompanying this report, together with other factors, is expected to reduce parking demand and hence deliver a higher parking surplus in the year 2023.



2030 Development Scenario Parking DemandThe 2030 development scenario is projected to relate to an additional 480 staff and students, from 1037 to 1517 over the base case scenario (year 2020). Based on the existing demand profile of 1 space per 1.8 daily persons in attendance (derived previously), this would result in a net additional 267 spaces. This can be readily accommodated by the existing parking surplus of 321 spaces with 54 spare spaces.

Nevertheless, it is highly noteworthy that this assumes no change in current travel behaviour. The Green Travel Plan accompanying this report, together with other factors, is expected to reduce travel behaviour and parking demand and hence deliver a higher parking surplus in the year 2030.

In addition, the development proposes to construct an additional 16 spaces, which will increase the parking supply from 907 spaces to 923 spaces. This is more than the expected peak demand of 857 spaces (267 + 586) in the 2030 development scenario and will provide a safety margin.

In summary, all parking demands are readily accommodated onsite with a safety margin of more than 60 parking spaces in the 2030 development scenario, assuming no changes to parking demand from implementation the proposed Green Travel Plan, prepared separately. The adopted parking strategy and target modal splits are strongly supported and will deliver a sustainable planning outcome that is in the public interest. However, it is considered of importance that the current travel behaviour is not replicated in 2030, to drive a more sustainable planning outcome as a matter of good policy.

## 6.2 Accessible Parking

The proposed development will provide an additional accessible parking space within the new carpark adjacent to the new Construction Centre of Excellence Building.

## 6.3 Bicycle Parking

The Penrith City Council DCP defers to the Planning Guidelines for Walking and Cycling' (NSW Government 2004) to determine minimum bicycle parking requirements. The Planning Guidelines provide the following bicycle parking rates for tertiary education establishments, universities and TAFE's:

) Staff: 3-5% of staff,

- ) Students: 5-10% of fulltime students.
- ) Visitors: 5-10% of staff.

At this stage, the number of fulltime student enrolments is unknown. However, application of the above bicycle parking rates to the maximum number of students and staff onsite at any one time for the 2030 development scenario (441 additional students and 39 additional staff) results in the requirement for approximately 26-48 bicycle spaces (2 x staff spaces, 22-44 student spaces and 2 visitor spaces).

Application of the long-term bicycle travel mode target for staff and students (4.7%) to the 2030 development scenario staff and student population increase results in a requirement for 23 bicycle parking spaces.

Therefore, provision of 26 bicycle parking spaces is considered adequate to satisfy Council's DCP requirement and long-term bicycle travel mode targets for staff and students. In response, a minimum of 26 bicycle parking spaces and end of trip facilities are to be provided on the lower ground floor. These future bicycle facilities are to be detailed at CC Stage. However, it is envisaged that additional bicycle parking spaces could be provided in response to demand throughout the lifecycle of the subject development, as required.

## 6.4 Shuttle Bus

The development proposes to utilise WSU existing shuttle bus services to Kingswood Railway Station. A shuttle bus stop is proposed via the USW internal road network which runs adjacent (to the east) of the subject development. This is discussed in more detail in the Green Travel Plan prepared separately.

## 6.5 Refuse Collection and Servicing

The proposed loading bay to the south of the proposed Construction Centre of Excellence building can accommodate vehicles up to a 12.5m heavy rigid vehicle (HRV) and will readily accommodate any standard waste collection vehicle. Reference should be made to the swept path analysis provided in **Appendix D**.



## 6.6 Emergency Vehicle Access

The proposed internal road network and loading bay to the south of the proposed Construction Centre of Excellence building can readily accommodate all emergency service vehicles, thereby ensuring all emergency vehicles are able to access the site when required.

## 6.7 Pick up and Drop Off Arrangements

Questionnaire survey results demonstrated that only 6% of staff and students were car passengers which includes car passenger dropped off and car passenger's carpooling with other staff and students. For a conservative assessment, say all 6% were dropped off /picked up and application of this modal split was applied to the 2030 development scenario, approximately 29 staff and students would be dropped off and picked up. Importantly, pick ups and drop offs will be spread throughout the day and it is envisaged that all pickup/drop arrivals can be accommodated safely within an available parking space or within the circulation aisle of the proposed carpark, accordingly. This arrangement is considered supportable.



# 7. TRAFFIC AND TRANSPORT IMPACTS

## 7.1 Assumptions from Surveys

For consistency across the assessed intersections the following assumptions were made based on the travel mode surveys and intersection surveys:

- ) The network peak hour used for this assessment was based on the combined peak hourly traffic volume at all assessed intersections. This was determined as 7:45am to 8:45am in the morning (AM) peak and 4:45pm to 5:45pm in the evening (PM) peak.
- ) The travel mode survey of the students was used to determine the percentage of students arriving/departing during the peak periods. As the question for arrivals and departures was based on 30-minute intervals, the two highest percentages of the three overlapping intervals were summed to determine the percentage of vehicles in the peak period. During the AM peak 54% vehicles arrived or departed during the peak hour and 28% during the PM peak hour.

## 7.2 Data Analysis

Due to uncertainty regarding the reliability of traffic volumes during the time intersection surveys were undertaken due to potential COVID-19 impacts, it was necessary to compare traffic data from 2019 (without COVID-19 impacts) with 2020 traffic data (with COVID-19 impacts) during both morning and afternoon peak periods. TRAFFIX received SCATS data from TfNSW for the intersection of Great Western Highway and O'Connell Street for the following dates:

- ) Tuesday 26<sup>th</sup> November 2019
- ) Tuesday 24<sup>th</sup> November 2020

SCATS data revealed there was a slight increase in traffic volumes at the intersection of Great Western Highway and O'Connell Street from 2019 to 2020 during peak morning (7:45am-8:45am) and afternoon (4:45pm-5:45pm) times as summarised below:

- ) Morning peak hour: + 103 vehicles
- ) Afternoon peak hour: +75 vehicles.



As a result, existing traffic volumes were not required to be factored to account for COVID-19 impacts. TRAFFIX consulted with TfNSW to confirm the validity of the above methodology and reference should be made to **Appendix E** in this regard.

## 7.3 Existing Site Generation

The subject site currently accommodates the existing TAFE development. Accordingly, TRAFFIX has undertaken a site inspection on Thursday 3<sup>rd</sup> December 2020 between 8:30am to 9:30am and 4:30pm to 5:30pm noting the following traffic generations:

- ) 235 vehicle trips per hour in the morning peak period (189 in, 46 out); and
- ) 107 vehicle trips per hour in the afternoon peak period (35 in, 72 out).

It should be noted that this traffic generation of the existing development is captured within the existing survey data and traffic modelling.

## 7.4 Growth Rates

A growth rate of 2% per annum compounding has been assumed for the background traffic in the 2026 and 2030 scenarios. This is considered a conservative 'worst-case' scenario for the following reasons:

- ) The traffic counting station on the Great Western Highway has shown the traffic volumes decreasing each year since 2017. Therefore, the 2% background growth is considered unlikely to occur in the foreseeable future.
- ) A cumulative assessment of the development potential of the Quarter Precinct Masterplan and Western Sydney University Redevelopment Plan is not considered feasible due to a lack of publicly available information to assess these developments. However, the 2% growth rate is considered more than sufficient to account for the development potential of these developments with current background traffic in decline.

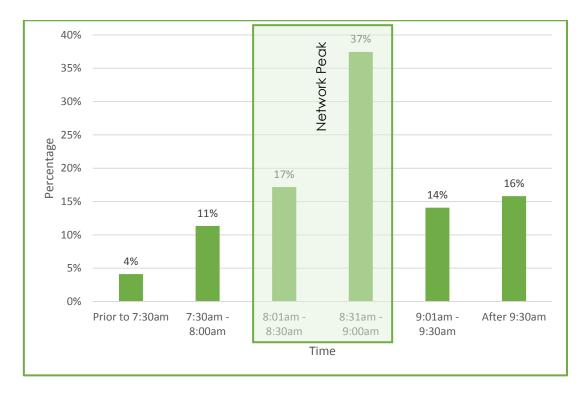
The SEARs requests 2031 and 2036 scenarios to be assessed however as the development will be fully operational by 2030 this is considered sufficient to determine the impact of the proposed development. Any assessment of years beyond will be assessing the background growth rather than the development based on a conservative growth rate, which is not considered necessary for a development of this size or scale.



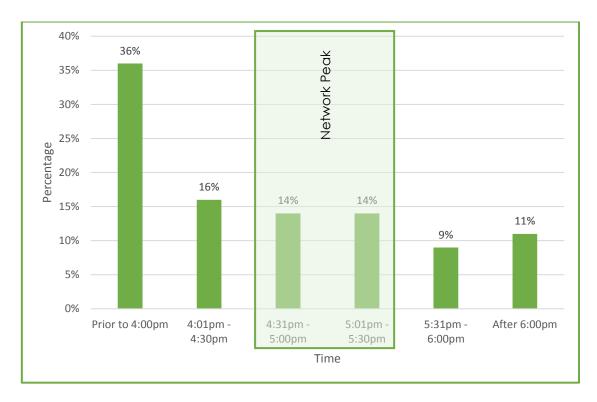
## 7.5 Development Trip Generation

The impacts of the proposed development on the external road network have been assessed having regard for the projected student and staff population data provided by TAFE in conjunction with the interview questionnaire survey results based on the existing staff and student population. These relate as close as possible to the Year Scenarios 2026, 2031 and 2036 as required under the SEARS.

Based on the travel mode survey results in **Table 3** from Section 4.5, 84% of students/staff currently drive to the existing development. However, the arrival and departure of students/staff does not occur within a single hour as shown in **Chart 4** and **Chart 5**. The network peak periods (discussed within Section 7.1) sees 54% of vehicles arrive/depart in the morning network peak hour and 28% of vehicles arrive/depart in the afternoon network peak hour. This data has been used for the future year scenarios.



#### Chart 4: Morning Peak Distribution



#### Chart 5: Afternoon/Evening Distribution

#### 7.5.1 2026 Development Scenario

Student and staff population data provided by TAFE demonstrates that 209 additional students and staff per day are projected to attend campus in the 2023 development scenario which will also be relevant to the 2026 scenario as indicated by SEARS.

This equates to:

- ) +96 vehicle trips (77 arrivals and 19 departures) during the morning network peak hour period (7:45am-8:45am), and:
- ) +49 vehicle trips (15 arrivals and 34 departures) during the afternoon network peak hour period (4:45pm-5:45pm).

### 7.5.2 2030 Development Scenario

Student and staff population data provided by TAFE demonstrates that 480 additional students and staff per day are projected to attend campus in the 2030 development scenario.



This equates to:

- ) +218 vehicle trips (174 arrivals and 44 departures) during the morning network peak hour period (7:45am-8:45am), and:
- ) +113 vehicle trips (33 arrivals and 80 departures) during the afternoon network peak hour period (4:45pm-5:45pm).

### 7.5.3 2036 Development Scenario

Based on the building population projections provided by TAFE NSW, it is forecasted that the development will reach its capacity by 2030. As such, no additional trips relating to the subject development will be added after 2030. Therefore, any increase in trips will be the result of background traffic growth not attributed to the subject development.

## 7.6 Assessed Network

In order to determine the impact of these additional trips on the surrounding road network, the below critical intersections have been assessed based on the SEARs, noting that there are no other intersections considered of interest:

- ) Great Western Highway / French Street / O'Connell Street
- ) Great Western Highway / Bringelly Road
- ) Caddens Road / Gipps Street

Impacts to the above key intersections as a result of the proposed development are discussed below.

## 7.7 Traffic Distributions

The distribution of the traffic generation has been based the travel mode survey where students/staff identified the suburb they live. The route to and from their suburb was allocated to the following routes listed in **Table 5**. The table includes the route, suburbs allocated to the route and percentage of students/staff.

#### Table 5: Traffic Distributions

| Route                   | Suburbs   | Percentage |
|-------------------------|---|------------|
| Great Western Highway   | Emerton, Hebersham, Mount Druitt, St Clair, St  | 6.1%       |
| East via O'Connell      | Marys,  |            |
|                         | Cambridge Park, Castlereagh, Cranebrook,        |            |
|                         | East Kurrajong, Ebenezer, Glossodia, Grose      |            |
| Great Western Highway   | Vale, Kurrajong Hills, Londonderry, Mount       | 22.1%      |
| West via O'Connell      | Riverview, North Richmond, Penrith,             |            |
|                         | Werrington, Werrington County, Werrington       |            |
|                         | Downs, Wilberforce, Windsor                     |            |
| Second Avenue via       | Kingswood                                       | 6.1%       |
| O'Connell               | Kiigswood                                       | 0.176      |
|                         | Baulkham Hills, Blacktown, Burwood, Casula,     |            |
|                         | Claremont Meadows, Doonside, Girraween,         |            |
| The Northern Road via   | Greenacre, Greenwich, Kellyville, Marayong,     |            |
| Bringelly Road, Caddens | Middleton Grange, Mount Annan, Mount            | 28.3%      |
| Road, Cadda Ridge Road  | Vernon, Northmead Padstow, Parramatta,          | 20.076     |
| and O'Connell Street    | Pendle Hill, Plumpton Quakers Hill, Riverstone, |            |
|                         | Schofields, Seven Hills, Springwood, Stanhope   |            |
|                         | Gardens, The Ponds, Wentworthville, Wilmot      |            |
|                         | Belimbla Park, Blaxland, Camden, Emu            |            |
| M4 East via Gipps Road, | Heights, Emu Plains, Faulconbridge,             |            |
| Bringelly Road, Caddens | Glenbrook, Glenmore Park, Hazelbrook,           |            |
| Road, Cadda Ridge Road  | Katoomba, Lapstone, Lawson, Leonay,             | 37.4%      |
| and O'Connell Street    | Linden, Narellan Vale, Oran Park, Silverdale,   |            |
|                         | South Penrith, Wallacia, Warrimoo, Wentworth    |            |
|                         | Falls, Winmalee, Woodford                       |            |

The above distributions have been used to create the following distribution diagrams in **Figure 11 and Figure 12**, which were then inputted into the SIDRA Intersection modelling to determine the impact of the traffic on the surrounding road network.

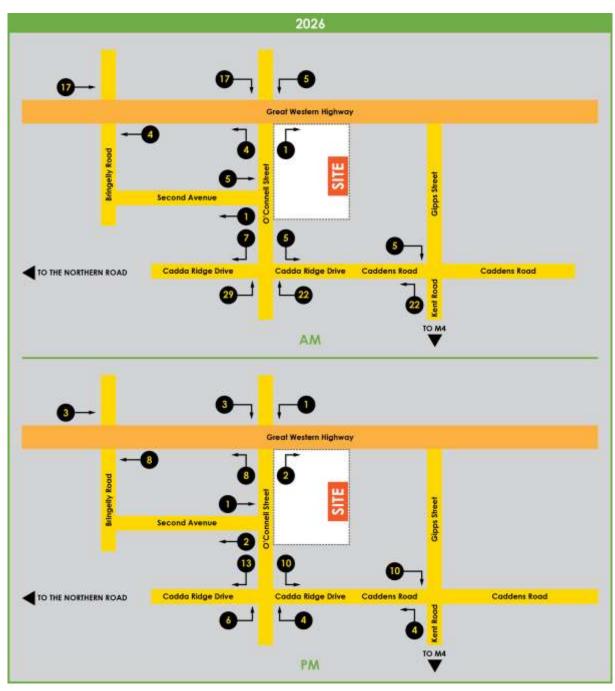


Figure 11: 2026 Trip Distribution

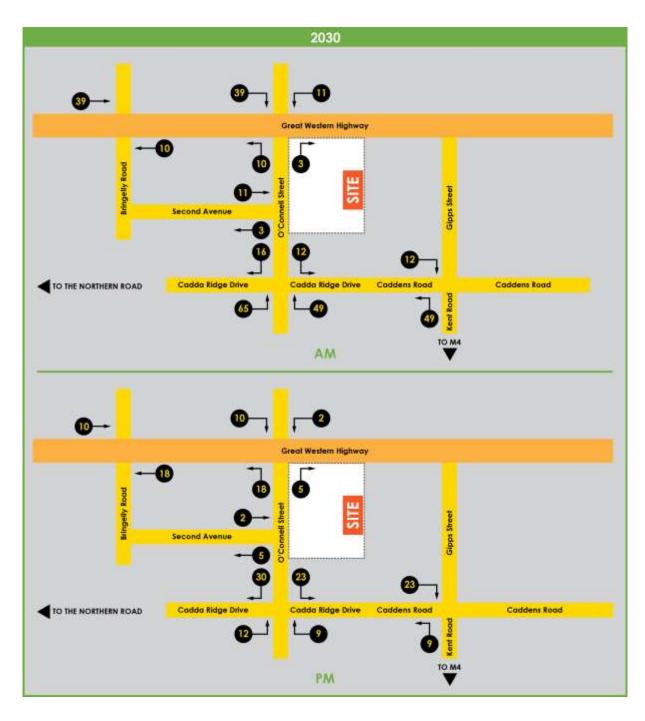


Figure 12: 2030 Trip Distribution



## 7.8 Modelling Methodology

In order to assess the potential traffic impacts of the proposed development, the following modelling was undertaken:

) Existing 2020;

) Future 2030 growth only;

) Future 2026 growth only;

) Future 2030 + Development.

) Future 2026 + Development;

Traffic surveys were undertaken of the intersections mentioned above, which are considered to be most critical in relation to the site and are the required intersection to be assessed in accordance with SEAR's. These counts were undertaken on Tuesday 17<sup>th</sup> November and Thursday 19<sup>th</sup> November 2020 between 7:30am-9:30am and 4:00am-6:00pm. The traffic volumes in these surveys formed the base case volumes for software modelling undertaken to assess intersection performance characteristics under existing traffic conditions. The SIDRA Intersection 9 model produces a range of outputs, the most useful of which are the Degree of Saturation (DoS) and Average Vehicle Delay per vehicle (AVD). The AVD is in turn related to a level of service (LoS) criteria. These performance measures can be interpreted using the following explanations as summarised in **Table 6** below:

- **DoS** the DoS is a measure of the operational performance of individual intersections. As both queue length and delay increase rapidly as DoS approaches 1, it is usual to attempt to keep DoS to less than 0.9. When DoS exceeds 0.9 residual queues can be anticipated, as occurs at many major intersections throughout the metropolitan area during peak periods. In this regard, a practical limit at 1.1 can be assumed. For intersections controlled by roundabout or give way/stop control, satisfactory intersection operation is generally indicated by a DoS of 0.8 or less.
- **AVD** the AVD for individual intersections provides a measure of the operational performance of an intersection. In general, levels of acceptability of AVD for individual intersections depend on the time of day (motorists generally accept higher delays during peak commuter periods) and the road system being modelled (motorists are more likely to accept longer delays on side streets than on the main road system).
- **LoS** this is a comparative measure which provides an indication of the operating performance of an intersection.

| Level of<br>Service | Average Delay per<br>Vehicle (secs/veh) | Traffic Signals, Roundabout  |
|---------------------|---|--|
| А                   | Less than 14                            | Good operation   |
| В                   | 15 to 28                                | Good with acceptable delays and spare capacity   |
| С                   | 29 to 42                                | Satisfactory   |
| D                   | 43 to 56                                | Operating near capacity  |
| E                   | 57 to 70                                | At capacity; at signals incidents will cause excessive delays.<br>Roundabouts require other control mode |
| F                   | More than 70                            | Unsatisfactory and requires additional capacity  |

#### Table 6: Intersection Performance Indicators (RMS)

### 7.9 Network Performance

The traffic impacts arising from the proposed development during the morning and afternoon peak periods in the existing and future scenarios have been assessed by loading the distributed traffic volumes into the SIDRA Intersection model. The results of this software modelling for the base case, future and base case plus development traffic is summarised in **Table 7**, **Table 8** and **Table 9** below. The detailed outputs are provided in **Appendix F**.

#### 7.9.1 Intersection of Great Western Highway, French Street and O'Connell Street

| Intersection   | Control | Period | Scenario   | Degree of<br>Saturation<br>(DoS) | Average<br>Delay | Level of<br>Service |
|--|---------|--------|------------|----------------------------------|------------------|---------------------|
|  | Signal  | АМ     | 2020 Base  | 0.725                            | 23.5             | В                   |
|  |         |        | 2026       | 0.913                            | 24.5             | В                   |
|  |         |        | 2026+ Dev  | 0.923                            | 26.7             | В                   |
| Great Western Highway /<br>French Street / O'Connell |         |        | 2030       | 0.985                            | 33.8             | С                   |
| Street   |         |        | 2030 + Dev | 1.052                            | 44.4             | D                   |
|  |         |        | 2020 Base  | 0.737                            | 25.7             | В                   |
|  |         | РМ     | 2026       | 0.828                            | 28.9             | С                   |
|  |         |        | 2026+ Dev  | 0.830                            | 29.1             | С                   |

## Table 7: Base and Proposed Intersection Performance for Great Western Highway, French Street and O'Connell Street

| Intersection | Control | Period | Scenario   | Degree of<br>Saturation<br>(DoS) | Average<br>Delay | Level of<br>Service |
|--------------|---------|--------|------------|----------------------------------|------------------|---------------------|
|              |         |        | 2030       | 0.902                            | 36.2             | С                   |
|              |         |        | 2030 + Dev | 0.915                            | 42.2             | С                   |

It can be seen from **Table 7** above that GWH/French Street/O'Connell Street operates at a level of service (LoS) D with an average delay of 44.4 seconds in the 2030 + development scenario during the peak morning period (worst case scenario) and is operating near capacity with an increase of 10.6 seconds in delay from the 2030 scenario. In addition, the 95<sup>th</sup> percentile queue length of 81.9<sup>m</sup> for the right turn bay on the western approach extends 10 metres beyond the current lane. However, this is considered acceptable for the following reasons:

- ) The model has assumed the current travel modes for the trip distributions including the 84% of students/staff driving to TAFE. However, the Green Travel Plan has established a car driver target of 69.3% by 2030 through the use of a number of strategies to encourage alterative transport modes. Therefore, the model is overestimating the traffic generation of the development in 2030 as the reduction in the number of car drivers has not been taken into account. It is emphasised that the model split changes will apply to the entire campus population, current and future, resulting in significant traffic demand suppression.
- ) The 95<sup>th</sup> percentile is the maximum queue length and as such unlikely to be occurring frequently.
- ) The model has assumed a 2% growth rate along the Great Western Highway, however volumes along the Great Western Highway has declined over the past few years since 2017 in accordance with daily traffic count volumes obtained from TfNSW Traffic Volume Viewer Station ID 7123-PR located on the Great Western Highway, and therefore the model is a conservative assessment of the future intersection performance.
- ) The intersection with an average delay of 44.4 seconds during the 2030 + development scenario is only marginally within the LoS D range of 43 to 56 seconds.

As such, for the above reasons, the future intersection performance is considered acceptable and likely to operate at a LoS C (being satisfactory). In addition, it is unlikely that the right turn bay on GWH would exceed the length of the bay.

#### 7.9.2 Intersection of Great Western Highway/Bringelly Road

| Intersection            | Control | Period | Scenario   | Degree of<br>Saturation<br>(DoS) | Average<br>Delay | Level of<br>Service |
|-------------------------|---------|--------|------------|----------------------------------|------------------|---------------------|
|                         | Signal  |        | 2020 Base  | 0.674                            | 23.7             | В                   |
|                         |         |        | 2026       | 0.760                            | 25.0             | В                   |
|                         |         | AM     | 2026 + Dev | 0.749                            | 33.1             | В                   |
|                         |         |        | 2030       | 0.826                            | 26.9             | В                   |
| Great Western Highway / |         |        | 2030 + Dev | 0.826                            | 27.0             | В                   |
| Bringelly Road          |         | РМ     | 2020 Base  | 0.652                            | 24.7             | В                   |
|                         |         |        | 2026       | 0.739                            | 26.0             | В                   |
|                         |         |        | 2026 + Dev | 0.759                            | 26.3             | В                   |
|                         |         |        | 2030       | 0.829                            | 29.1             | С                   |
|                         |         |        | 2030 + Dev | 0.858                            | 30.6             | С                   |

#### Table 8: Base and Proposed Intersection Performance for Great Western Highway/Bringelly Road

As **Table 8** shows, the intersection of Great Western Highway and Bringelly Road operates at a LoS C and an average delay of 30.6 seconds in the 2030 + development scenario during the peak evening period. This is a 1.5 second increase of the expected 2030 during the evening peak and therefore the impact proposed development has minimal impact upon this intersection.

### 7.9.3 Intersection of Caddens Road / Gipps Road / Kent Road

| Intersection         | Control | Period | Scenario   | Degree of<br>Saturation<br>(DoS) | Average<br>Delay | Level of<br>Service |
|----------------------|---------|--------|------------|----------------------------------|------------------|---------------------|
|                      | Signal  |        | 2020 Base  | 0.748                            | 31.7             | С                   |
|                      |         |        | 2026       | 0.798                            | 34.2             | С                   |
|                      |         | AM     | 2026 + Dev | 0.812                            | 34.8             | С                   |
|                      |         |        | 2030       | 0.859                            | 41.3             | С                   |
| Caddens Road / Gipps |         |        | 2030 + Dev | 0.888                            | 45.3             | D                   |
| Street / Kent Road   |         | РМ     | 2020 Base  | 0.691                            | 31.4             | С                   |
|                      |         |        | 2026       | 0.756                            | 33.1             | С                   |
|                      |         |        | 2026 + Dev | 0.770                            | 33.8             | С                   |
|                      |         |        | 2030       | 0.822                            | 36.1             | С                   |
|                      |         |        | 2030 + Dev | 0.849                            | 39.1             | С                   |

## Table 9: Base and Proposed Intersection Performance for Caddens Road / Gipps Road / Kent Road

It is evident from **Table 9** that the intersection of Caddens Road / Gipps Road / Kent Road operates at a LoS D with an average delay of 45.3 seconds in the 2030 + development scenario during the peak morning period and is operating near capacity however considered acceptable with an increase of 4.0 second increase in delay from the 2030 scenario.

### 7.9.4 Summary

Therefore, all future traffic impacts resulting from the proposed development are considered manageable and no external road upgrades or improvements are considered necessary at any of the key intersections analysed under future scenarios as required under SEARs. This result is a consequence of the adopted parking strategy and target modal splits aimed at delivering a sustainable planning outcome that is in the public interest.



# 8. ACCESS AND INTERNAL DESIGN ASPECTS

## 8.1 Site Vehicular Access

No changes are proposed to the O'Connell Street Gate 1 access driveway as a result of the subject development.

The O'Connell Street Gate 2 access driveway will provide vehicular access to the proposed development with an additional 16 car parking spaces. AS 2890.1 requires access driveway widths to be designed in accordance with the number of car parking spaces effectively served by that access. As a result, the addition of 16 spaces is considered minor and therefore, the existing vehicular access is satisfactory. It is noted however minor works to remove the median is proposed to accommodate service vehicles up to a 12.5m long heavy rigid vehicle accessing the site. This is considered acceptable as service vehicles will only access the site out of operating hours and schedule times only. In addition, it is proposed that the roadway near the vehicular access within the development is to be widened slightly to accommodate a passing opportunity in the unlikely event that a truck and a car is required to pass.

In summary, the vehicular accesses for the TAFE will operate satisfactory and is designed in accordance with AS 2890.1 and AS 2890.2. Reference should be made to the swept path analysis presented in **Appendix D**.

## 8.2 Internal Design

The internal car park complies with the requirements of AS 2890.1 (2004), AS2890.2 (2002), AS 2890.3 (2015) and AS 2890.6 (2009), and the following characteristics are noteworthy:

### 8.2.1 Parking Modules

- ) All car parking spaces are to be designed in accordance with a User Class 2. These spaces are provided with a minimum space length of 5.4m, a minimum width of 2.5m and a minimum aisle width of 5.8m.
- ) All spaces located adjacent to obstructions of greater than 150mm in height are to be provided with an additional width of 300mm.
- ) Dead-end aisles are to be provided with the required 1.0m aisle extension in accordance with Figure 2.3 of AS2890.1 (2004) and turning bays when exceeding six spaces.



 All accessible parking spaces are to be designed in accordance with AS2890.6 (2009), being
 2.4m wide, 5.4m long and situated immediately adjacent to a dedicated shared area or the circulating aisle.

#### 8.2.2 Bicycle Parking

) All bicycle parking facilities are to be provided on the ground floor for ease of access. All bicycle parking facilities are to be designed in accordance with the minimum requirements of AS2890.3 (2015) and this can be dealt with during CC Stage.

#### 8.2.3 Service Area Design

) The internal design of the service area is to be undertaken in accordance with the requirements of AS2890.2 for the maximum length vehicle permissible on-site being a 12.5m long HRV.

#### 8.2.4 Wayfinding, Signage & Line Marking

) Internal vehicle movements, pedestrians and cyclists are to be managed safety and efficiently within the subject site in accordance with AS2890, Austroads Guidelines and standard traffic engineering principles. Reference should be made to the signage and wayfinding plan presented in **Appendix G** which provides a guide, to be finalised at Construction Certification Stage.

### 8.3 Summary

In summary, the internal configuration of the car park has been designed in accordance with AS2890.1 (2004), AS2890.2 (2002), AS 2890.3 (2015) and AS2890.6 (2009). It is however envisaged that a condition of consent would be imposed requiring compliance with these standards and as such any minor amendments considered necessary (if any) can be dealt with prior to the release of a Construction Certificate.



# 9. SUMMARY OF RESPONSES TO SEARS

A response to each relevant requirement of the Secretary's Environmental Assessment Requirements (SEARs) is provided below, including references to sections of this report where applicable. Reference should also be made to the full copy of the SEARs provided in **Appendix H** and the below matters relate specifically to Item 7:

#### 7. Transport and Accessibility

Include a transport and accessibility impact assessment, which details, but not limited to the following:

Accurate details of the current daily and peak hour vehicle, existing and future public transport networks and pedestrian and cycle movement provided on the road network located adjacent to the proposed development;

#### ) TRAFFIX Response:

Reference should be made to Section 4 which provides an overview of the existing pedestrian and cycle infrastructure available within the vicinity of the subject site, including linkages to pedestrian and cycle infrastructure within the proposed development. Section 7.3 provides an overview of existing traffic volumes on the external road network within the vicinity of the subject site.

Details of estimated total daily and peak hour trips generated by the proposal, including vehicle, public transport, pedestrian and bicycle trips based on surveys of the existing TAFE NSW Nepean Kingswood Campus facilities and similar education facilities within the local area;

### ) TRAFFIX Response:

Reference should be made to Section 7 for future trips generated by the subject development and impacts to the surrounding external road network.

Cumulative impacts of all trips generated by the development and the existing TAFE NSW Nepean Kingswood Campus, as well as the development potential identified in the Quarter Precinct Master Plan and Western Sydney University Redevelopment Plan;



#### ) TRAFFIX Response:

Reference should be made to Section 7.4

Existing car parking capacity and utilisation on streets within a 400 metre radius from the site on a typical weekday covering at least one hour before and after the proposed hours of operation (including night classes);

#### ) TRAFFIX Response:

All parking is accommodated onsite and no reliance on on-street parking is proposed. Therefore, there will be no impact to existing on-street parking availability within the vicinity of the site. Reference should be made to Section 6 with weekday on-site parking survey shown in Chart 2 and Chart 3.

The adequacy of existing public transport or any future public transport infrastructure and services within the vicinity of the site, pedestrian and bicycle networks and associated infrastructure to meet the likely future demand of the proposed development;

#### ) TRAFFIX Response:

Reference should be made to Section 4 which provides an assessment of the existing and future public transport infrastructure and services within the vicinity of the subject site.

#### Measures to integrate the development with the existing/future public transport network.

#### ) TRAFFIX Response:

Reference should be made to Section 4.

Impact of trips generated by the development on the area-wide network, with consideration of the cumulative impacts of the development on the surrounding roads and intersections in the context of any other approved planning proposals and developments in the precinct and surrounds, should be considered. Including the impact of nearby intersections and the need/associated funding for upgrading or road improvement works, if required;

#### ) TRAFFIX Response:

Impacts to surrounding road networks as a result of the proposed development are considered negligible with no improvements or upgrades to existing surrounding road



infrastructure considered necessary. Reference should be made to Section 7 for a detailed analysis. In addition, a conservative growth rate of 2% per annum compounding has been assumed for the background traffic to account for future growth as discussed in Section 7.4.

An assessment of the forecast impacts on traffic volume generated on road safety and capacity of road network including consideration of cumulative impacts at key intersections using SIDRA or similar traffic model as prescribed by Transport for New South Wales (TfNSW). The traffic modelling should consider the scenarios of year 2026, 2031, 2036 and the year until the facility ceases operation. These should include, but not be limited to:

- Great Western Highway/O'Connell Street/French Street
- Great Western Highway/Bringelly Road
- Gipps Street (Werrington Arterial)/Caddens Road

#### ) TRAFFIX Response:

Reference should be made to Section 7.4 with modelling results provided in Section 7.9.

The identification of infrastructure required to ameliorate any impacts on traffic efficiency and road safety impacts associated with the proposed development, including details on improvements required to affected intersections, additional bus routes along bus capable roads (i.e. minimum 3.5 m wide travel lanes), additional bus stops or bus bays;

#### ) TRAFFIX Response:

No infrastructure upgrades are considered necessary. References should be made to Section 7.9.

Details of travel demand management measures to minimise the impact on general traffic and bus operations, including details of a location-specific sustainable travel plan (Green Travel Plan and specific Workplace travel plan) and the provision of facilities to increase the non-car mode share for travel to and from the site;

#### ) TRAFFIX Response:

Reference should be made to the Green Travel Plan prepared separately by TRAFFIX.



The proposed walking and cycling access arrangements and connections to public transport services;

#### ) TRAFFIX Response:

Reference should be made to Section 4.

The design of the proposed cycle and pedestrian entry connecting to the Great Western Highway shared path should ensure that there are clear sight lines between the cyclists from the development and the faster moving cyclists on the Great Western Highway;

#### ) TRAFFIX Response:

Cyclist and pedestrian access is provided using existing (approved) vehicular and pedestrian access locations via O'Connell Street. In addition, a cycle and pedestrian entry connecting to the GWH shared path is proposed.

The proposed access arrangements, including car and bus pick-up/drop-off facilities, and measures to mitigate any associated traffic impacts and impacts on public transport, pedestrian and bicycle networks, including pedestrian crossings and refuges and speed control devices and zones;

#### ) TRAFFIX Response:

Reference should be made to the reduced plans presented in Appendix B.

Proposed bicycle parking provision, including end of trip facilities, in secure, convenient, accessible areas close to main entries incorporating lighting and passive surveillance;

#### ) TRAFFIX Response:

All bicycle parking demands are able to be readily accommodated onsite. Reference should be made to Section 6.3.

Details of vehicle circulation, proposed number of on-site car parking spaces for staff, students and visitors and corresponding compliance with appropriate parking codes and justification for the level of car parking provided on-site;



#### ) TRAFFIX Response:

Reference should be made to the internal design aspects discussed in Section 8 and the parking assessment presented in Section 6.

Any short term reduction of existing car spaces for staff, students and visitors due to the proposed construction works (if any), and the proposed location, operational and functional characteristics of the re-allocated staff, students and visitors car parking (if applicable);

#### ) TRAFFIX Response:

Not applicable.

Details of the proposed site access and the parking provisions associated with the proposed development including compliance with the requirements of the relevant Australian Standards (i.e. turn paths, sight distance requirements, aisle widths, etc.);

#### ) TRAFFIX Response:

Reference should be made to the internal design aspects discussed in Section 8.

An assessment of the cumulative on-street parking impacts of cars and bus pick-up/drop-off, staff parking and any other parking demands associated with the development and provide any associated recommendations to ameliorate any such impacts;

#### ) TRAFFIX Response:

Not applicable. All parking drop off and pick up requirements are to be accommodated without reliance on the public road network.

# An assessment of road and pedestrian safety adjacent to the proposed development and the details of required road safety measures and personal safety in line with CPTED;

#### ) TRAFFIX Response:

Not applicable.

Emergency vehicle access, service vehicle access, delivery and loading arrangements and estimated service vehicle movements (including vehicle type and the likely arrival and departure times);



#### ) TRAFFIX Response:

Refer to Section 6.6: Emergency vehicle access is provided throughout the subject site.

The preparation of a preliminary Construction Traffic and Pedestrian Management Plan to demonstrate the proposed management of the impact in relation to construction traffic addressing the following:

- Assessment of cumulative impacts associated with other construction activities (if any);
- An assessment of road safety at key intersections and locations subject to heavy vehicle construction traffic movements and high pedestrian activity;
- Details of construction program detailing the anticipated construction duration and highlighting significant and milestone stages and events during the construction process;
- Details of anticipated peak hour and daily construction vehicle movements to and from the site;
- Details of on-site car parking and access arrangements of construction vehicles, construction workers to and from the site, emergency vehicles and service vehicles; and
- Details of temporary cycling and pedestrian access during construction.

#### ) TRAFFIX Response:

Reference should be made to the Preliminary CTPMP Report, prepared separately by TRAFFIX.

Alternate methods for gaining the most accurate traffic analysis data may be agreed with TfNSW, if required.

#### ) TRAFFIX Response:

Reference should be made to Section 7.2.

# 10. CONCLUSIONS

In summary:

- ) The State Significant Development (SSD) application to which this report relates, seeks approval for the expansion of the existing TAFE Nepean Kingswood Campus located at 2-44 O'Connell Street, Kingswood. The expansion includes the construction of a new building known as the NSW Construction Centre of Excellence facility located in the eastern sector of the overall TAFE campus.
- ) TAFE NSW seeks approval to expand the existing campus to accommodate 1,750 additional students per semester by 2023 and an additional 3,500 students per semester by 2030 (over and above the existing 3,000 students per semester.
- ) The assessment relies upon enrolment data provided by TAFE, which has provided the context for this assessment.
- ) There are presently a total of 907 spaces within the existing campus, demonstrating that existing peak parking demands are readily accommodated on-site, with a surplus of 321 spaces. This demand profile is not expected to continue into the future with opportunities to change modal splits and spread on-site activity across the day.

The 2023 development scenario is projected to relate to an additional maximum of 210 staff and students onsite at any one time, from 1037 to 1247. Based on the existing demand profile of 1 space per 1.8 daily persons in attendance, this would result in a net additional 117 car spaces. This can be readily accommodated by the existing parking surplus of 321 spaces in addition to the future 16 additional spaces proposed.

The 2030 development scenario would result in a net additional 267 car spaces (over existing 2020). This can be readily accommodated by the existing parking surplus of 321 spaces in addition to the future 16 additional spaces proposed.

However, a reduced parking demand profile will result due to the factors discussed in Section 6.1.6, including the provision of a shared shuttle service with UWS to Kingswood Railway Station, so that adoption of a 'target' car driver modal split of 69.3% (17.3% reduction from existing in accordance with the GTP) for the entire campus is considered achievable. The adopted parking strategy and target modal splits are strongly supported and will deliver a sustainable planning outcome that is in the public interest. This may be

contrasted with a 'no intervention' approach where current travel behaviour remains unchanged in 2030, failing to drive a sustainable planning outcome as a matter of good policy; and wasting Government resources.

- ) The subject development proposes to construct an additional 16 spaces, which will increase the parking supply from 907 spaces to 923 spaces. This is more than the expected demand of 900 spaces and will provide a buffer of more than 60 spaces.
- ) TfNSW has requested that the assessment consider peak traffic conditions in 2026, 2031 and 2036. This has however been undertaken for 2020, 2026 and 2030, at which time the development is fully populated. That is, any increase in trips after 2030 will be the result of background traffic growth only with no development impacts beyond 2030 when the development is fully populated. There is no nexus between the development and increased network traffic beyond 2030.
- ) A growth rate of 2% per annum compounding has been assumed for the background traffic in the 2026 and 2030 scenarios. This is considered a conservative 'worst-case' scenario for the reasons discussed in Section 7.4.
- ) The Future Years Scenarios have been examined under 'Base Case' (without development) and 'Future' (base case year + development) for each year, in order to compare the relative impact of the proposed development with conditions that will occur in any event, absent the development. The assessment has taken account of growth in background traffic.. It is emphasised that the modal split changes will apply to the entire campus population, current and future, resulting in significant traffic demand suppression, which is sound policy.
- ) The 2026 Development Scenario equates to a net additional 96 vehicle trips (77 arrivals and 19 departures) during the morning network weekday peak (7:45am-8:45am), and 49 vehicle trips (15 arrivals and 34 departures) during the weekday afternoon network peak (4:45pm-5:45pm). These can be readily accommodated on the road network.
- ) The 2030 Development Scenario equates to a net additional 218 vehicle trips (174 arrivals and 44 departures) during the morning network peak hour period (7:45am-8:45am), and 113 vehicle trips (34 arrivals and 79 departures) during the afternoon network peak hour period (4:45pm-5:45pm). These increases can be similarly accommodated.
- ) Specifically, all intersections operate with a Level of Service D or better under all future scenarios, even based on a conservative 2% background traffic growth rate. Therefore, all



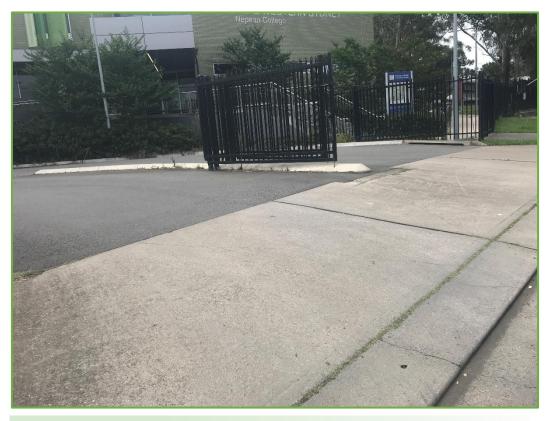
future traffic impacts resulting from the proposed development are considered manageable and no external road upgrades are considered necessary at any of the key intersections analysed under future scenarios identified in the SEARs.

- ) The design of accesses and parking areas will be appropriately located and have been assessed to comply with AS2890.1 (2004), AS2890.2 (2002) and AS2890.6 (2009).
- ) Each individual SEAR's requirement has been addressed as summarised in Section 9.
- ) The application is supported by a Draft Green Travel Plan in response to SEAR's requirements.
- ) The application is supported by a Preliminary Construction Traffic Management Plan prepared separately in response to SEAR's requirements.

This Transport and Accessibility Impact Assessment therefore demonstrates that the subject application is supportable on transport planning grounds. TRAFFIX anticipates an ongoing involvement during the development approval process.

# APPENDIX A

Photographic Record



View looking southwest at the access driveway of Gate 1



View looking northeast at the access driveway of Gate 1



View looking west at the pedestrian refuge island outside of Gate 1



View looking south at the access driveway of Gate 2



View looking north at the access driveway of Gate 2



View looking west at the pedestrian refuge island near Gate 2

# APPENDIX B

Reduced Plans

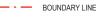


#### LEGEND

EXISTING PEDESTRIAN ACCESS



EXISTING VEHICULAR



EXISTING BUILDING NAME

A \_\_\_\_\_ RECONFIGURATION

PROPOSED VEHICULAR ROUTE CARPARK



PROPOSED PEDESTRIAN PROPC

EXTENT OF SSD SCOPE

PROPOSED CONSTRUCTION HUB



PROPOSED ROADS WALKWAYS AND RECONFIGURED CARPARK

EXISTING ROADS, WALKWAYS AND CARPARKS

## **GRAY PUKSAND**

#### DISCLAIMER

e secure, may be corrupted in transmission or due to id/or may be amended or altered by third parties after

NSW N nated Architects Scott Movian 7147 Craig Saltmarsh 656

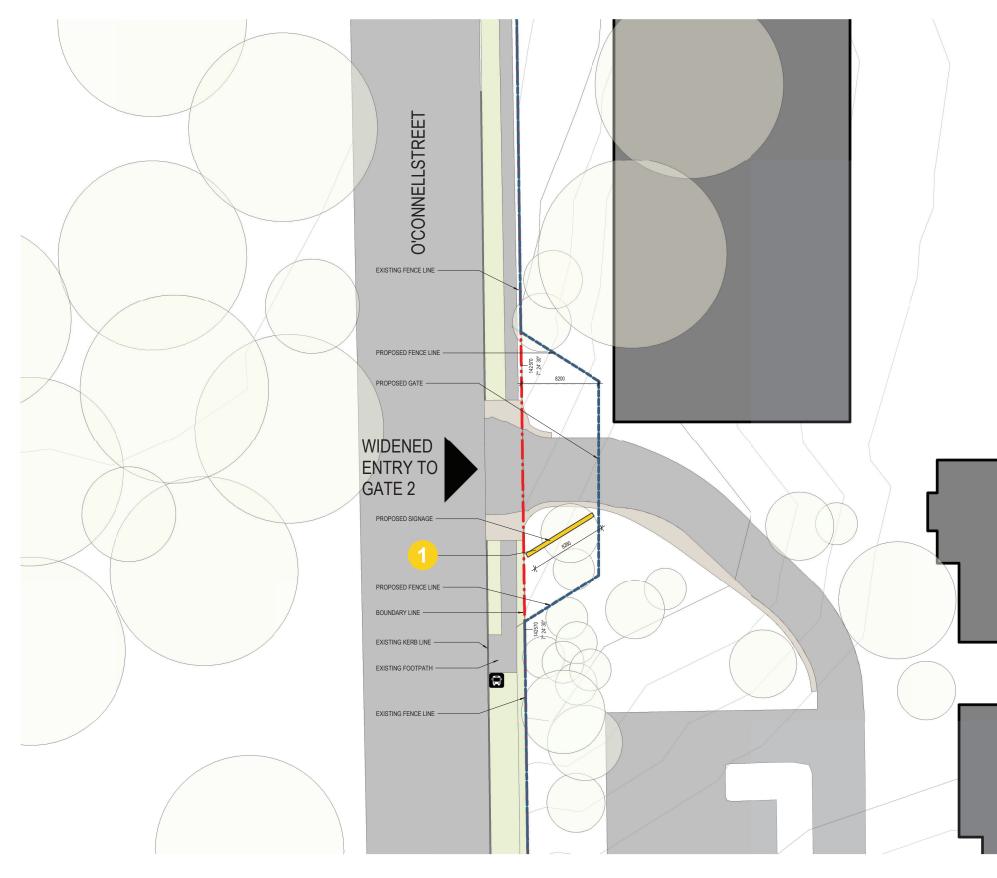
| REV    | DESCRIPTI    | ON              | DATE          |
|--------|--------------|-----------------|---------------|
| A      | Test of Adeo | uacy Submission | 10-02-21      |
| В      | Issued for S | SDA             | 04-03-21      |
| C<br>D | Issued for S |                 | 11-03-21      |
| D      | Issued for S | SDA             | 12-05-21      |
|        |              |                 |               |
|        |              |                 |               |
|        |              |                 |               |
|        |              |                 |               |
|        |              |                 |               |
|        |              |                 |               |
| PROJ   | IECT NO      | 220090          |               |
| DRAV   | VN           | PW              | $( \uparrow)$ |
| CHEC   | CKED         | SS              | 9             |
| APPF   | ROVED        | вн              | 0             |
|        |              |                 |               |

Insitute of Applied **Technology for Construction** 12-44 O'Connell St, Kingswood NSW 2747

#### SSDA

#### SITE PLAN - PROPOSED

| DWG #      | DA0103       | REV | D |
|------------|--------------|-----|---|
| SCALE @ A1 | As indicated |     |   |

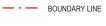


#### LEGEND





EXISTING VEHICULAR ACCESS





EXISTING BUILDING NAME



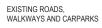
PROPOSED PEDESTRIAN PATH



EXTENT OF SSD SCOPE

PROPOSED CONSTRUCTION HUB

PROPOSED ROADS WALKWAYS AND RECONFIGURED CARPARK



SIGN TYPE 1

## **GRAY PUKSAND**

#### DISCLAIMER

e secure, may be corrupted in transmission or due to d/or may be amended or altered by third parties after

e over Scale diatley referre utory Authori

NSW Nominated Architects Scott Moylan 7147 Craig Saltmarsh 6569

| REV  | DESCRIPTI     | ON               | DATE      |
|------|---------------|------------------|-----------|
| P1   | Issued for In |                  | 04-03-21  |
|      |               |                  |           |
|      |               |                  |           |
|      |               |                  |           |
|      |               |                  |           |
|      |               |                  |           |
|      |               |                  |           |
|      |               |                  |           |
|      |               |                  |           |
|      |               |                  |           |
|      |               |                  |           |
|      |               |                  |           |
|      |               |                  |           |
|      |               |                  |           |
|      |               |                  |           |
| PRO. | JECT NO       | 220090           |           |
| PRO. |               | 220090<br>Author | $\square$ |
| DRA  |               |                  |           |

TAFE NSW Construction Centre of Excellence 12-44 O'connell St, Kingswood NSW 2747

#### PROPOSED ENTRY

| DWG#       | DA0110       | REV | P1 |
|------------|--------------|-----|----|
| SCALE @ A1 | As indicated |     |    |



2021 Weekly Survey Results

R.O.A.R. DATA *Reliable, Original & Authentic Results* Ph. Mob.0418-239019



Client Job No / Name Day/Date

: Traffix : 7515 KINGSWOOD Parking Surveys 2 : Mon 19th to Fri 23rd April 2021







| Zone | On Street                     | Сар | 0700  | 0800 | 0900  | 1000  | 1100  | 1200  | 1300  | 1400  | 1500  | 1600  | 1700  | 1800 | 1900  |
|------|-------------------------------|-----|-------|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|-------|
| Α    | O'Connell St East / Side      | 23  | 4     | 2    | 6     | 4     | 3     | 4     | 3     | 4     | 4     | 5     | 5     | 2    | 1     |
| В    | O'Connell St East / Side      | 10  | 0     | 0    | 0     | 0     | 0     | 0     | 0     | 0     | 0     | 0     | 0     | 0    | 0     |
| С    | O'Connell St West / Side      | 18  | 1     | 1    | 4     | 3     | 3     | 2     | 2     | 3     | 3     | 2     | 3     | 1    | 1     |
| D    | O'Connell St West / Side      | 12  | 4     | 2    | 2     | 4     | 4     | 3     | 3     | 1     | 2     | 1     | 2     | 3    | 5     |
|      | D O'Connell St West / Side 12 |     |       |      |       |       |       |       |       |       |       |       |       |      |       |
|      | Total of Vehicles Parked 63   |     |       | 5    | 12    | 11    | 10    | 9     | 8     | 8     | 9     | 8     | 10    | 6    | 7     |
|      | Number of Vacant Spaces       |     | 54    | 58   | 51    | 52    | 53    | 54    | 55    | 55    | 54    | 55    | 53    | 57   | 56    |
|      | % of Capacity Used            |     | 14.3% | 7.9% | 19.0% | 17.5% | 15.9% | 14.3% | 12.7% | 12.7% | 14.3% | 12.7% | 15.9% | 9.5% | 11.1% |

| Area | Car Parks                    | Сар | 0700 | 0800 | 0900  | 1000  | 1100  | 1200  | 1300  | 1400  | 1500  | 1600  | 1700  | 1800 | 1900 |
|------|------------------------------|-----|------|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|------|
| 1    | North Eastern                | 180 | 0    | 2    | 15    | 18    | 19    | 20    | 15    | 15    | 14    | 7     | 4     | 2    | 0    |
| 2    | North Western                | 313 | 2    | 35   | 244   | 266   | 264   | 273   | 256   | 223   | 169   | 77    | 41    | 23   | 20   |
| 3    | Southern                     | 414 | 31   | 41   | 178   | 236   | 235   | 235   | 236   | 219   | 167   | 139   | 59    | 62   | 55   |
|      |                              |     |      |      |       |       |       |       |       |       |       |       |       |      |      |
|      |                              |     |      |      |       |       |       |       |       |       |       |       |       |      |      |
|      |                              |     |      |      |       |       |       |       |       |       |       |       |       |      |      |
| -    | Total of Vehicles Parked 907 |     |      | 78   | 437   | 520   | 518   | 528   | 507   | 457   | 350   | 223   | 104   | 87   | 75   |
|      | Number of Vacant Spaces      |     | 874  | 829  | 470   | 387   | 389   | 379   | 400   | 450   | 557   | 684   | 803   | 820  | 832  |
|      | % of Capacity Used           |     | 3.6% | 8.6% | 48.2% | 57.3% | 57.1% | 58.2% | 55.9% | 50.4% | 38.6% | 24.6% | 11.5% | 9.6% | 8.3% |







| Zone | On Street                | Сар | 0700 | 0800 | 0900  | 1000  | 1100  | 1200  | 1300  | 1400  | 1500  | 1600  | 1700 | 1800 | 1900 |
|------|--------------------------|-----|------|------|-------|-------|-------|-------|-------|-------|-------|-------|------|------|------|
| Α    | O'Connell St East / Side | 23  | 1    | 1    | 3     | 4     | 4     | 4     | 3     | 2     | 2     | 2     | 0    | 0    | 0    |
| В    | O'Connell St East / Side | 10  | 0    | 0    | 0     | 0     | 0     | 0     | 0     | 0     | 0     | 0     | 1    | 1    | 0    |
| С    | O'Connell St West / Side | 18  | 1    | 1    | 4     | 9     | 10    | 9     | 9     | 7     | 5     | 3     | 2    | 1    | 1    |
| D    | O'Connell St West / Side | 12  | 4    | 2    | 3     | 2     | 1     | 1     | 0     | 1     | 1     | 2     | 3    | 1    | 1    |
|      |                          |     |      |      |       |       |       |       |       |       |       |       |      |      |      |
| 1    | Total of Vehicles Parked | 63  | 6    | 4    | 10    | 15    | 15    | 14    | 12    | 10    | 8     | 7     | 6    | 3    | 2    |
|      | Number of Vacant Spaces  |     | 57   | 59   | 53    | 48    | 48    | 49    | 51    | 53    | 55    | 56    | 57   | 60   | 61   |
|      | % of Capacity Used       |     | 9.5% | 6.3% | 15.9% | 23.8% | 23.8% | 22.2% | 19.0% | 15.9% | 12.7% | 11.1% | 9.5% | 4.8% | 3.2% |

| Area | Car Parks                | Сар | 0700 | 0800  | 0900  | 1000  | 1100  | 1200  | 1300  | 1400  | 1500  | 1600  | 1700  | 1800  | 1900 |
|------|--------------------------|-----|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|
| 1    | North Eastern            | 180 | 0    | 3     | 19    | 22    | 22    | 21    | 19    | 18    | 17    | 9     | 6     | 0     | 0    |
| 2    | North Western            | 313 | 2    | 28    | 226   | 244   | 253   | 254   | 251   | 227   | 167   | 90    | 45    | 14    | 3    |
| 3    | Southern                 | 414 | 32   | 70    | 180   | 282   | 287   | 290   | 276   | 266   | 231   | 172   | 68    | 81    | 73   |
|      |                          |     |      |       |       |       |       |       |       |       |       |       |       |       |      |
|      |                          |     |      |       |       |       |       |       |       |       |       |       |       |       |      |
|      |                          |     |      |       |       |       |       |       |       |       |       |       |       |       |      |
|      | Total of Vehicles Parked | 907 | 34   | 101   | 425   | 548   | 562   | 565   | 546   | 511   | 415   | 271   | 119   | 95    | 76   |
|      | Number of Vacant Spaces  |     | 873  | 806   | 482   | 359   | 345   | 342   | 361   | 396   | 492   | 636   | 788   | 812   | 831  |
|      | % of Capacity Used       |     | 3.7% | 11.1% | 46.9% | 60.4% | 62.0% | 62.3% | 60.2% | 56.3% | 45.8% | 29.9% | 13.1% | 10.5% | 8.4% |





| Zone | On Street                | Сар | 0700  | 0800 | 0900  | 1000  | 1100  | 1200  | 1300  | 1400  | 1500 | 1600 | 1700 | 1800 | 1900 |
|------|--------------------------|-----|-------|------|-------|-------|-------|-------|-------|-------|------|------|------|------|------|
| Α    | O'Connell St East / Side | 23  | 2     | 2    | 5     | 6     | 4     | 2     | 0     | 0     | 0    | 0    | 0    | 0    | 0    |
| В    | O'Connell St East / Side | 10  | 1     | 0    | 0     | 0     | 0     | 0     | 0     | 0     | 0    | 0    | 0    | 0    | 0    |
| С    | O'Connell St West / Side | 18  | 1     | 1    | 4     | 8     | 10    | 8     | 8     | 5     | 2    | 2    | 1    | 1    | 1    |
| D    | O'Connell St West / Side | 12  | 4     | 2    | 1     | 1     | 1     | 2     | 2     | 2     | 1    | 0    | 1    | 1    | 2    |
|      |                          |     |       |      |       |       |       |       |       |       |      |      |      |      |      |
| -    | Total of Vehicles Parked | 63  | 8     | 5    | 10    | 15    | 15    | 12    | 10    | 7     | 3    | 2    | 2    | 2    | 3    |
|      | Number of Vacant Spaces  |     | 55    | 58   | 53    | 48    | 48    | 51    | 53    | 56    | 60   | 61   | 61   | 61   | 60   |
|      | % of Capacity Used       |     | 12.7% | 7.9% | 15.9% | 23.8% | 23.8% | 19.0% | 15.9% | 11.1% | 4.8% | 3.2% | 3.2% | 3.2% | 4.8% |

| Area | Car Parks                | Сар | 0700 | 0800  | 0900  | 1000  | 1100         | 1200  | 1300  | 1400  | 1500  | 1600  | 1700  | 1800 | 1900 |
|------|--------------------------|-----|------|-------|-------|-------|--------------|-------|-------|-------|-------|-------|-------|------|------|
| 1    | North Eastern            | 180 | 0    | 5     | 37    | 40    | 40           | 38    | 29    | 29    | 28    | 11    | 3     | 2    | 0    |
| 2    | North Western            | 313 | 0    | 24    | 219   | 267   | 282          | 274   | 249   | 239   | 168   | 86    | 41    | 28   | 19   |
| 3    | Southern                 | 414 | 28   | 68    | 165   | 261   | 249          | 251   | 240   | 227   | 179   | 131   | 55    | 55   | 50   |
|      |                          |     |      |       |       |       |              |       |       |       |       |       |       |      |      |
|      |                          |     |      |       |       |       |              |       |       |       |       |       |       |      |      |
|      |                          |     |      |       |       |       |              |       |       |       |       |       |       |      |      |
|      | Total of Vehicles Parked | 907 | 28   | 97    | 421   | 568   | 571          | 563   | 518   | 495   | 375   | 228   | 99    | 85   | 69   |
|      | Number of Vacant Spaces  |     | 879  | 810   | 486   | 339   | 336          | 344   | 389   | 412   | 532   | 679   | 808   | 822  | 838  |
|      | % of Capacity Used       |     | 3.1% | 10.7% | 46.4% | 62.6% | <b>63.0%</b> | 62.1% | 57.1% | 54.6% | 41.3% | 25.1% | 10.9% | 9.4% | 7.6% |





| Zone | On Street                   | Сар | 0700 | 0800 | 0900  | 1000  | 1100 | 1200 | 1300 | 1400 | 1500 | 1600 | 1700 | 1800 | 1900 |
|------|-----------------------------|-----|------|------|-------|-------|------|------|------|------|------|------|------|------|------|
| Α    | O'Connell St East / Side    | 23  | 0    | 0    | 3     | 3     | 3    | 1    | 0    | 0    | 0    | 1    | 1    | 0    | 0    |
| В    | O'Connell St East / Side    | 10  | 1    | 0    | 0     | 0     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| С    | O'Connell St West / Side    | 18  | 1    | 1    | 2     | 2     | 2    | 2    | 1    | 2    | 2    | 1    | 0    | 0    | 0    |
| D    | O'Connell St West / Side    | 12  | 2    | 4    | 3     | 3     | 0    | 1    | 2    | 1    | 1    | 0    | 0    | 1    | 1    |
|      |                             |     |      |      |       |       |      |      |      |      |      |      |      |      |      |
|      | Total of Vehicles Parked 63 |     |      | 5    | 8     | 8     | 5    | 4    | 3    | 3    | 3    | 2    | 1    | 1    | 1    |
|      | Number of Vacant Spaces     |     |      | 58   | 55    | 55    | 58   | 59   | 60   | 60   | 60   | 61   | 62   | 62   | 62   |
|      | % of Capacity Used          |     | 6.3% | 7.9% | 12.7% | 12.7% | 7.9% | 6.3% | 4.8% | 4.8% | 4.8% | 3.2% | 1.6% | 1.6% | 1.6% |

| Area | Car Parks                    | Сар | 0700 | 0800 | 0900  | 1000  | 1100  | 1200  | 1300  | 1400  | 1500  | 1600  | 1700 | 1800 | 1900 |
|------|------------------------------|-----|------|------|-------|-------|-------|-------|-------|-------|-------|-------|------|------|------|
| 1    | North Eastern                | 180 | 0    | 1    | 23    | 27    | 29    | 27    | 25    | 21    | 19    | 8     | 5    | 1    | 0    |
| 2    | North Western                | 313 | 3    | 11   | 188   | 206   | 204   | 213   | 193   | 158   | 113   | 41    | 23   | 3    | 1    |
| 3    | Southern                     | 414 | 32   | 54   | 151   | 243   | 248   | 246   | 210   | 194   | 140   | 110   | 50   | 86   | 80   |
|      |                              |     |      |      |       |       |       |       |       |       |       |       |      |      |      |
|      |                              |     |      |      |       |       |       |       |       |       |       |       |      |      |      |
|      |                              |     |      |      |       |       |       |       |       |       |       |       |      |      |      |
| 1    | Total of Vehicles Parked 907 |     |      | 66   | 362   | 476   | 481   | 486   | 428   | 373   | 272   | 159   | 78   | 90   | 81   |
|      | Number of Vacant Spaces      |     | 872  | 841  | 545   | 431   | 426   | 421   | 479   | 534   | 635   | 748   | 829  | 817  | 826  |
|      | % of Capacity Used           |     | 3.9% | 7.3% | 39.9% | 52.5% | 53.0% | 53.6% | 47.2% | 41.1% | 30.0% | 17.5% | 8.6% | 9.9% | 8.9% |





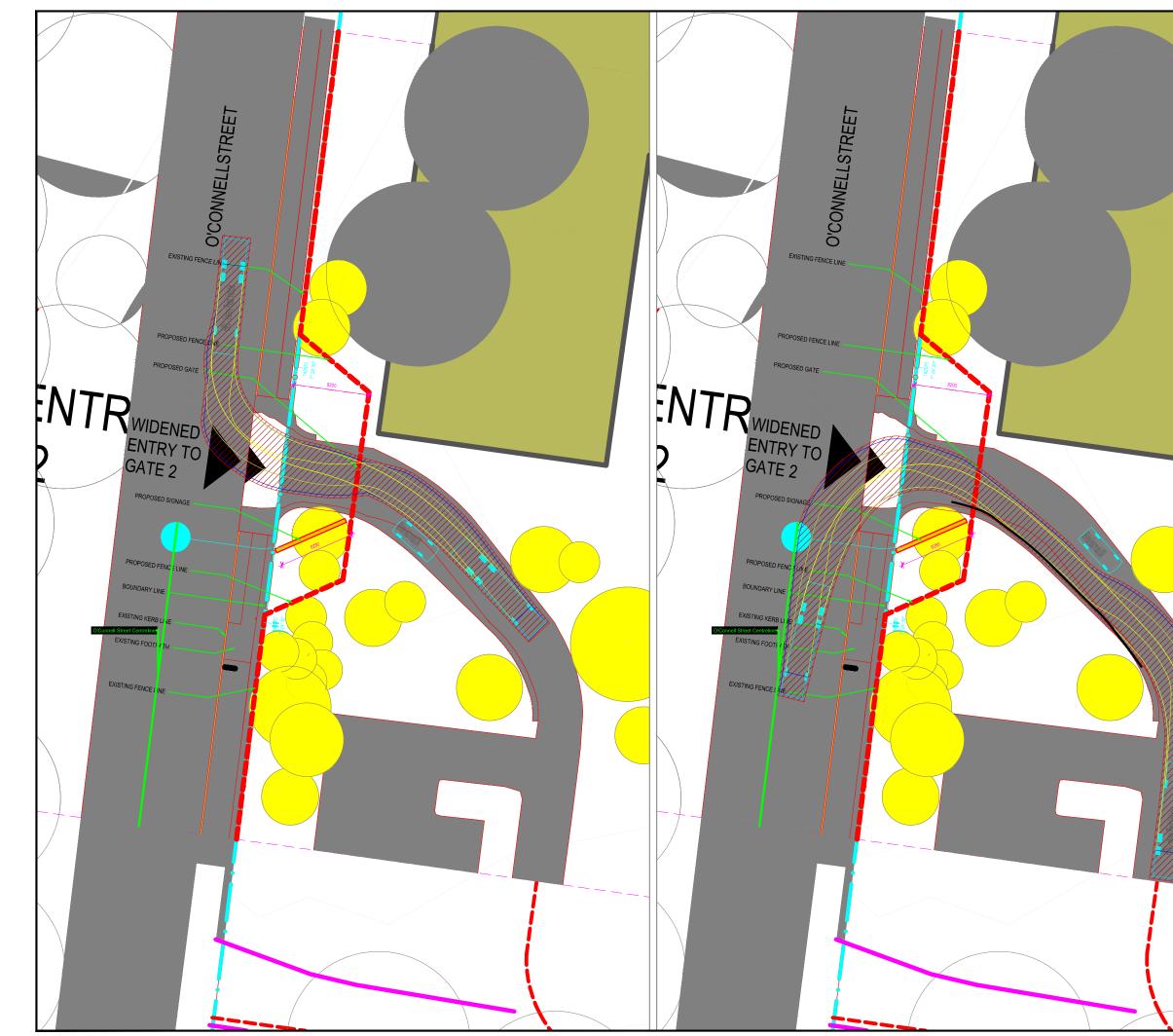
Client : Traffix Job No / Name : 7515 KINGSWOOD Parking Surveys 2 Day/Date : Friday 23rd April 2021

| Zone | On Street                | Сар | 0700 | 0800 | 0900 | 1000 | 1100        | 1200 | 1300 | 1400 | 1500 | 1600 | 1700 | 1800 | 1900 |
|------|--------------------------|-----|------|------|------|------|-------------|------|------|------|------|------|------|------|------|
| Α    | O'Connell St East / Side | 23  | 0    | 0    | 1    | 0    | 0           | 0    | 0    | 0    | 0    | 0    | 0    | 1    | 0    |
| В    | O'Connell St East / Side | 10  | 0    | 0    | 0    | 0    | 0           | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| С    | O'Connell St West / Side | 18  | 1    | 1    | 1    | 1    | 1           | 1    | 1    | 2    | 2    | 1    | 1    | 1    | 1    |
| D    | O'Connell St West / Side | 12  | 2    | 2    | 2    | 3    | 4           | 4    | 3    | 2    | 2    | 2    | 1    | 1    | 1    |
|      |                          |     |      |      |      |      |             |      |      |      |      |      |      |      |      |
| -    | Total of Vehicles Parked | 63  | 3    | 3    | 4    | 4    | 5           | 5    | 4    | 4    | 4    | 3    | 2    | 3    | 2    |
|      | Number of Vacant Spaces  |     | 60   | 60   | 59   | 59   | 58          | 58   | 59   | 59   | 59   | 60   | 61   | 60   | 61   |
|      | % of Capacity Used       |     | 4.8% | 4.8% | 6.3% | 6.3% | <b>7.9%</b> | 7.9% | 6.3% | 6.3% | 6.3% | 4.8% | 3.2% | 4.8% | 3.2% |

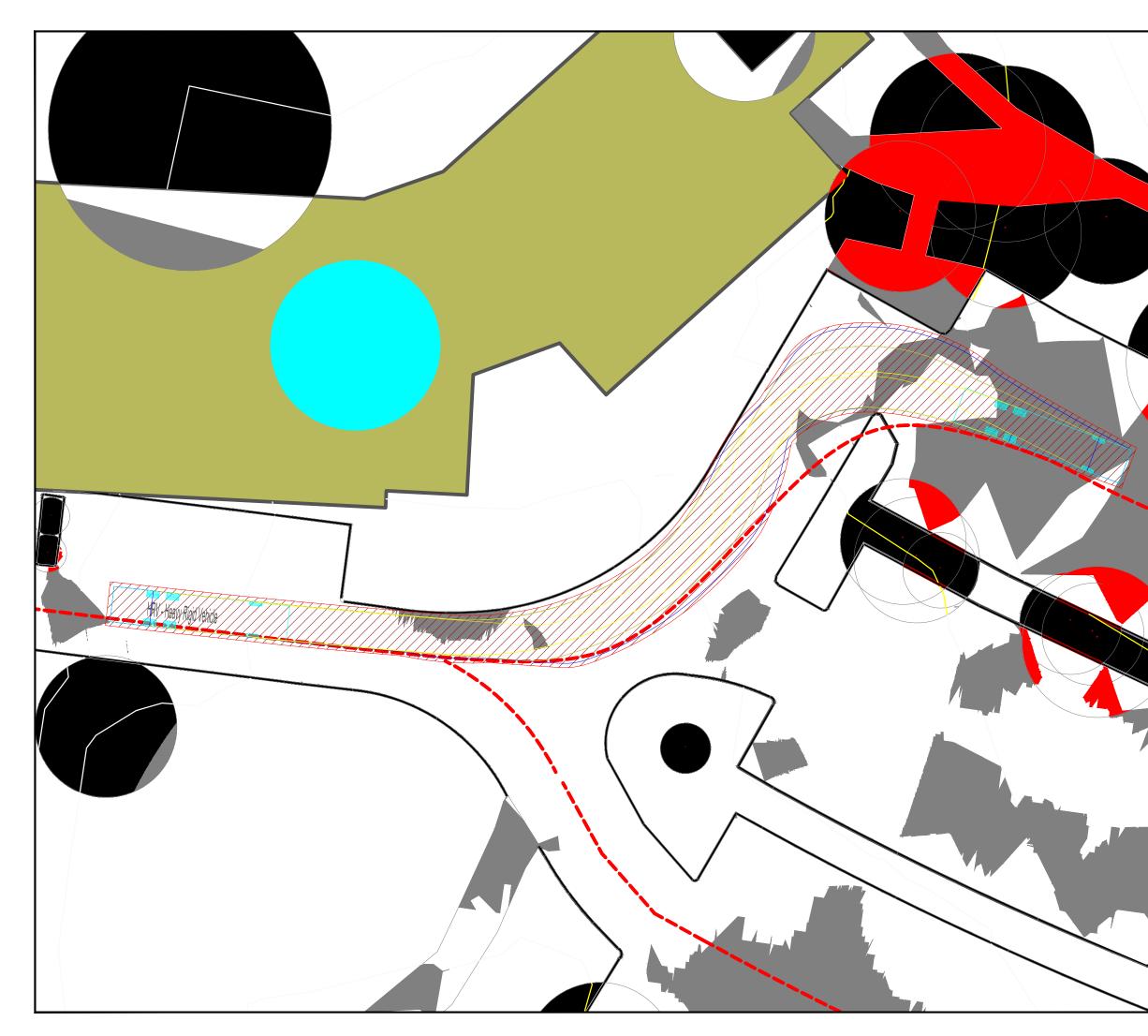
| Area | Car Parks                | Сар | 0700 | 0800 | 0900  | 1000  | 1100  | 1200  | 1300  | 1400  | 1500  | 1600 | 1700 | 1800 | 1900 |
|------|--------------------------|-----|------|------|-------|-------|-------|-------|-------|-------|-------|------|------|------|------|
| 1    | North Eastern            | 180 | 0    | 0    | 7     | 9     | 10    | 7     | 8     | 9     | 8     | 5    | 2    | 0    | 0    |
| 2    | North Western            | 313 | 2    | 18   | 170   | 181   | 184   | 180   | 173   | 158   | 113   | 35   | 12   | 1    | 1    |
| 3    | Southern                 | 414 | 27   | 41   | 77    | 119   | 121   | 114   | 103   | 113   | 68    | 50   | 11   | 5    | 1    |
|      |                          |     |      |      |       |       |       |       |       |       |       |      |      |      |      |
|      |                          |     |      |      |       |       |       |       |       |       |       |      |      |      |      |
|      |                          |     |      |      |       |       |       |       |       |       |       |      |      |      |      |
| 7    | Total of Vehicles Parked | 907 | 29   | 59   | 254   | 309   | 315   | 301   | 284   | 280   | 189   | 90   | 25   | 6    | 2    |
|      | Number of Vacant Spaces  |     | 878  | 848  | 653   | 598   | 592   | 606   | 623   | 627   | 718   | 817  | 882  | 901  | 905  |
|      | % of Capacity Used       |     | 3.2% | 6.5% | 28.0% | 34.1% | 34.7% | 33.2% | 31.3% | 30.9% | 20.8% | 9.9% | 2.8% | 0.7% | 0.2% |

# APPENDIX D

Swept Path Analysis



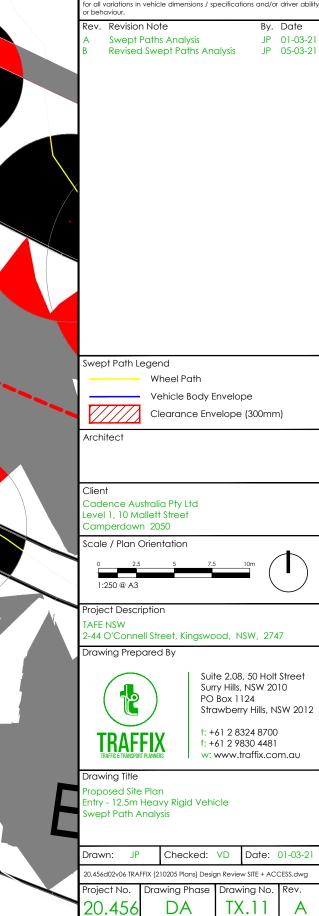
| Notes:<br>This drawing is pre   | pared for inform   | ation p   | urposes only  | It is no  | ot to be used   |
|---|--|---|---|---|---|
| for construction.   |  |   |   |   |   |
| Mark-ups only. Bas  | e drawing prepc  | red by  | others.   |   | -   |
| venicie swept p<br>turning path softw<br>data based upo<br>Parking facilities -<br>facilities - Off-str<br>embody a degre<br>these standards re<br>for all variations in<br>or behaviour. | rare and associa<br>n relevant Aust<br>Off-street car p<br>eet commercia<br>e of tolerance,<br>epresent a suitab | ated C.<br>ralian<br>Darking<br>I vehic<br>howeve | AD drawing<br>Standards (/<br>, and/or AS2<br>cle facilities)<br>er the vehicl<br>gn vehicle ar | platfor<br>AS/NZS<br>2890.2:<br>. Thes<br>e chai<br>nd do | ms. Vehicle<br>2890.1:2004<br>2002 Parking<br>e standards<br>racteristics in<br>not account |
| Rev. Revision   |  |   |   | '   | Date  |
| B Swept<br>C Revised  | vept Paths A<br>Paths Analys<br>I Swept Path<br>I Swept Path   | is<br>Is And                                      | alysis  | JP<br>JP<br>JP  | 21-01-21<br>08-02-21<br>01-03-21<br>05-03-21  |
|   |  |   |   |   |   |
| Swept Path L  | egend  |   |   |   |   |
|   | Wheel Pa   |   |   |   |   |
| V/////  | Vehicle Bo<br>Clearance  |   |   | 0mm   | 1)  |
| Architect   |  |   |   |   | '/  |
| Archileer   |  |   |   |   |   |
| Client<br>Cadence Au<br>Level 1, 10 Ma<br>Camperdown  | allett Street  | d   |   |   |   |
| Scale / Plan (  | Drientation  |   |   |   | <b></b>   |
| 0 4<br>1:400 @ A3   | 8  | 12  | 16m   |   |   |
| Project Descr<br>TAFE NSW<br>2-44 O'Conne   |  | gswo  | od, NSW,  | , 274   | 7   |
| Drawing Prep  | ared By  |   |   |   |   |
|   |  | Surr<br>PO  | e 2.08, 50<br>y Hills, NS<br>Box 1124<br>iwberry Hi   | W 20  | 10  |
| TRAFFIC & TRANSPOR  | FIX  | f: +a   | 61 2 8324<br>61 2 9830<br>www.traff   | 4481  |   |
| Drawing Title<br>O'Connell Stra<br>Swept Path A<br>12.5m HRV - S<br>Left: Entry Mo<br>Right: Exit Ma  | nalysis<br>ite Access 8<br>noeuvre   |   |   | ortuni  | ty  |
| Drawn: JP   | Check  | ed:   | VD Da   | ite:  | 08-02-21  |
| 20.456d02v06 TRA  |  |   |   |   | -   |
| Project No. <b>20.456</b>   | Drawing Ph   | use   | TX.1  |   | Rev.<br>A   |

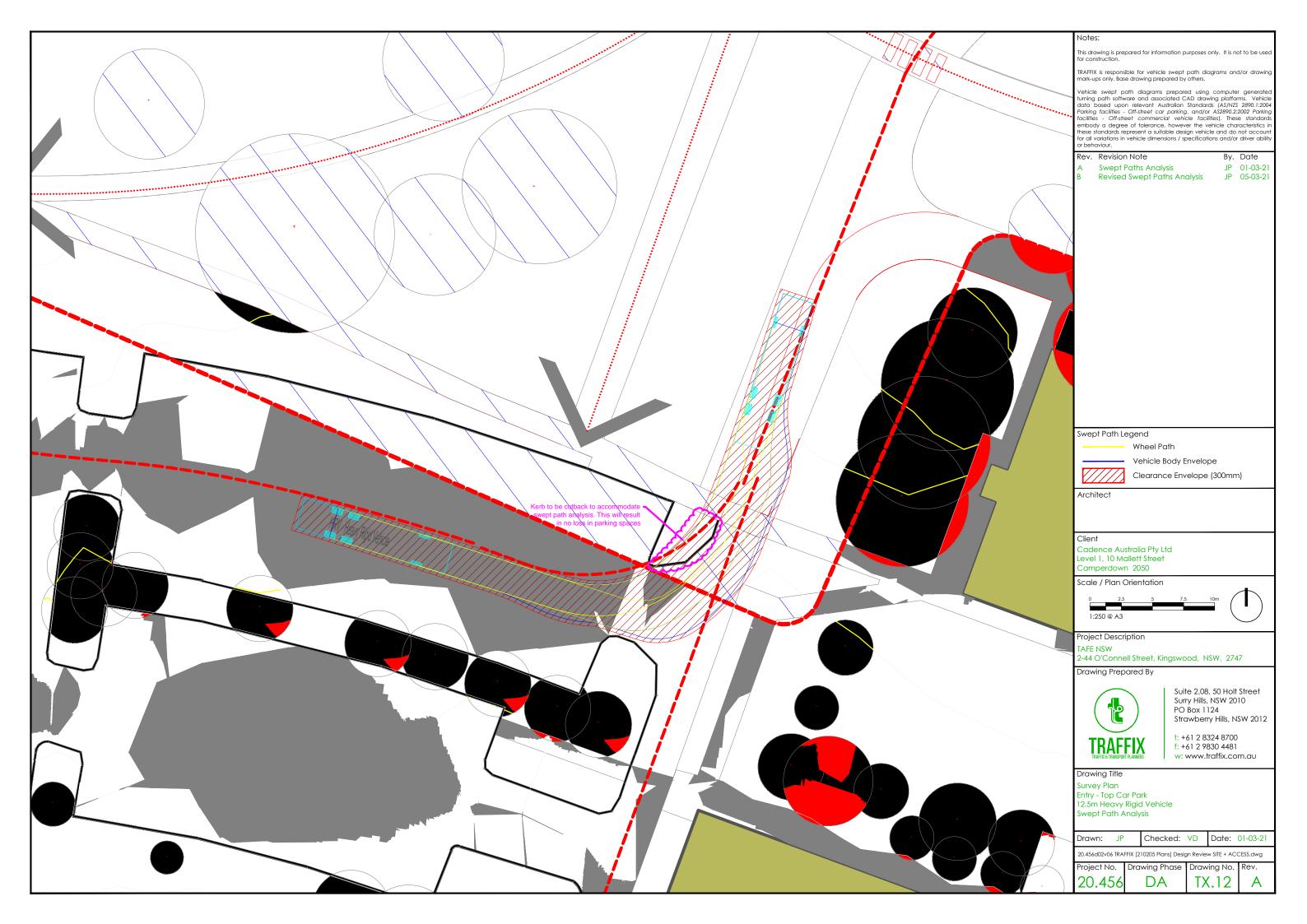


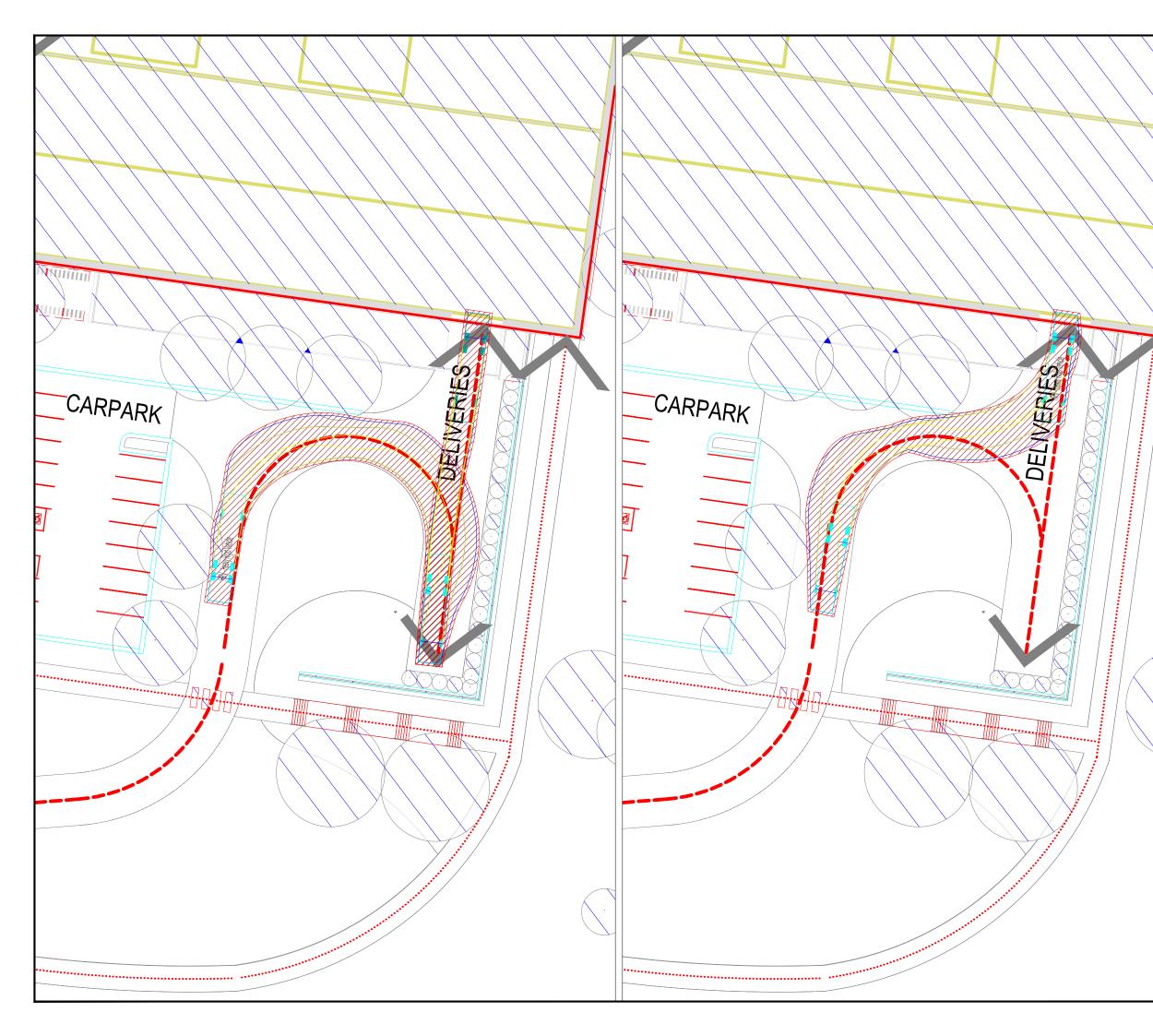
This drawing is prepared for information purposes only. It is not to be used for construction.

TRAFFIX is responsible for vehicle swept path diagrams and/or drawing mark-ups only. Base drawing prepared by others.

Vehicle swept path diagrams prepared using computer generated turning path software and associated CAD drawing platforms. Vehicle data based upon relevant Australian Standards (AS/N/XS 2890.1:2004 Parking facilities - Off-street car parking, and/or AS2890.2:2002 Parking facilities - Off-street commercial vehicle facilities). These standards embody a degree of tolerance, however the vehicle characteristics in these standards represent a suitable design vehicle and do na cacount for all variations in vehicle dimensions / specifications and/or driver ability or behaviour.



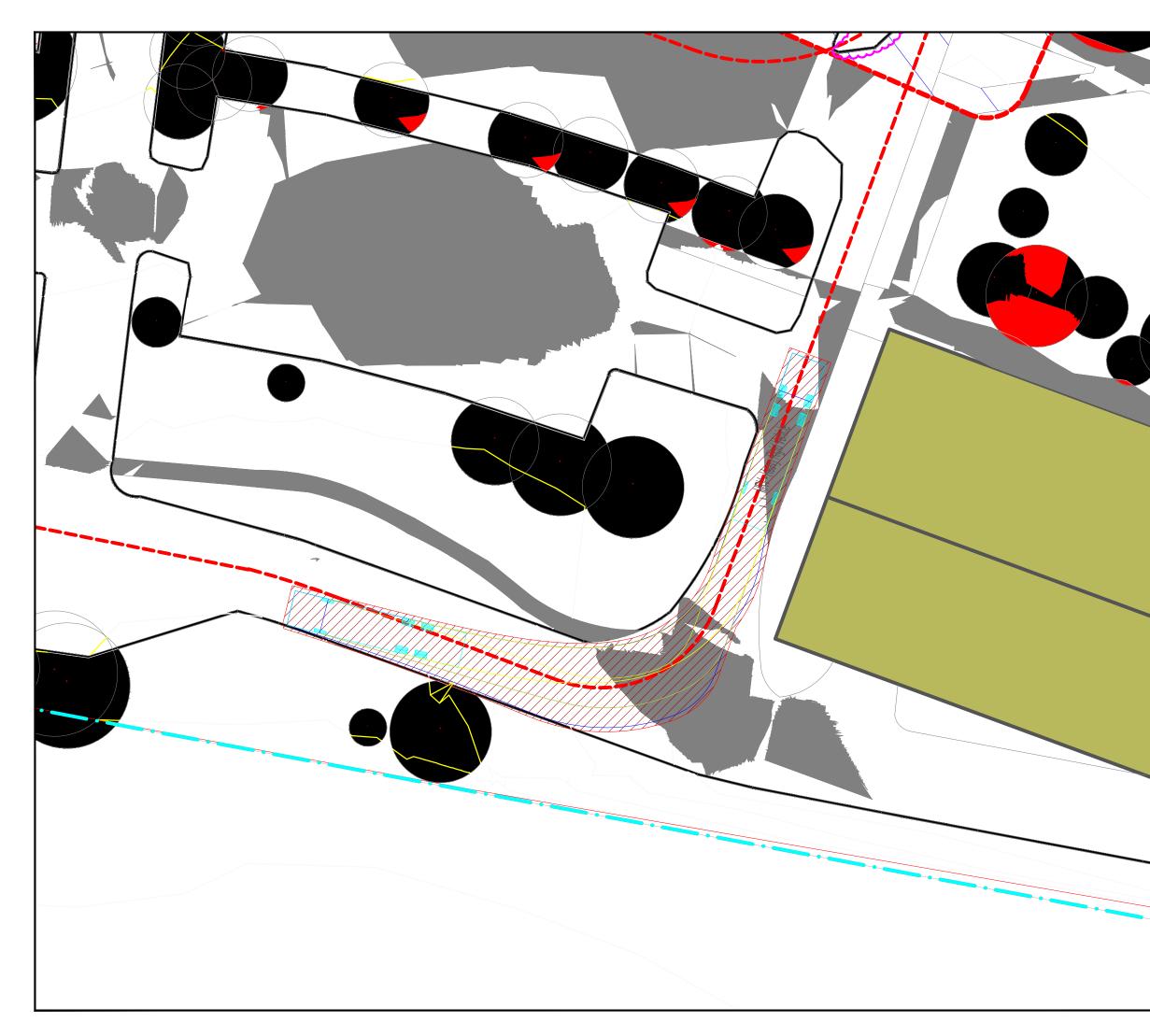




This drawing is prepared for information purposes only. It is not to be use for construction.

RAFFIX is responsible for vehicle swept path diagrams and/or drawin

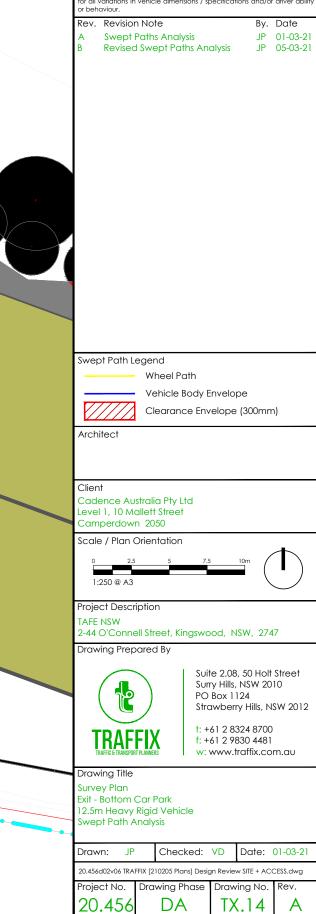
nark-ups only. Base drawing prepared by others. Vehicle swept path diagrams prepared using computer generated turning path software and associated CAD drawing platforms. Vehicle data based upon relevant Australian Standards (AS/NZS 2890.1:2004 Parking facilities - Off-street car parking, and/or AS2890.2:2002 Parking facilities - Off-street commercial vehicle facilities). These standards embody a degree of tolerance, however the vehicle characteristics in these standards represent a suitable design vehicle and do not account for all variations in vehicle dimensions / specifications and/or driver ability or behaviour. Rev. Revision Note By. Date Swept Paths Analysis JP 01-03-21 Revised Swept Paths Analysis JP 05-03-21 Swept Path Legend Wheel Path Vehicle Body Envelope Clearance Envelope (300mm) Architect Client Cadence Australia Pty Ltd Level 1, 10 Mallett Street Camperdown 2050 Scale / Plan Orientation 1:400 @ A3 Project Description TAFE NSW 2-44 O'Connell Street, Kingswood, NSW, 2747 Drawing Prepared By Suite 2.08, 50 Holt Street Surry Hills, NSW 2010 ł PO Box 1124 Strawberry Hills, NSW 2012 t: +61 2 8324 8700 TRAFFIX f: +61 2 9830 4481 w: www.traffix.com.au Drawing Title Proposed Site Plan Delivery Bay 2.5m Heavy Rigid Vehicle - Swept Path Analysis eft: Reverse Entry Manoeuvre Right: Forward Exit Manoeuvre Checked: VD Date: 01-03-21 Drawn: IP 20.456d02v06 TRAFFIX [210205 Plans] Design Review SITE + ACCESS.dwg Project No. Drawing Phase Drawing No. Rev. 20.456 DA TX.13 Α

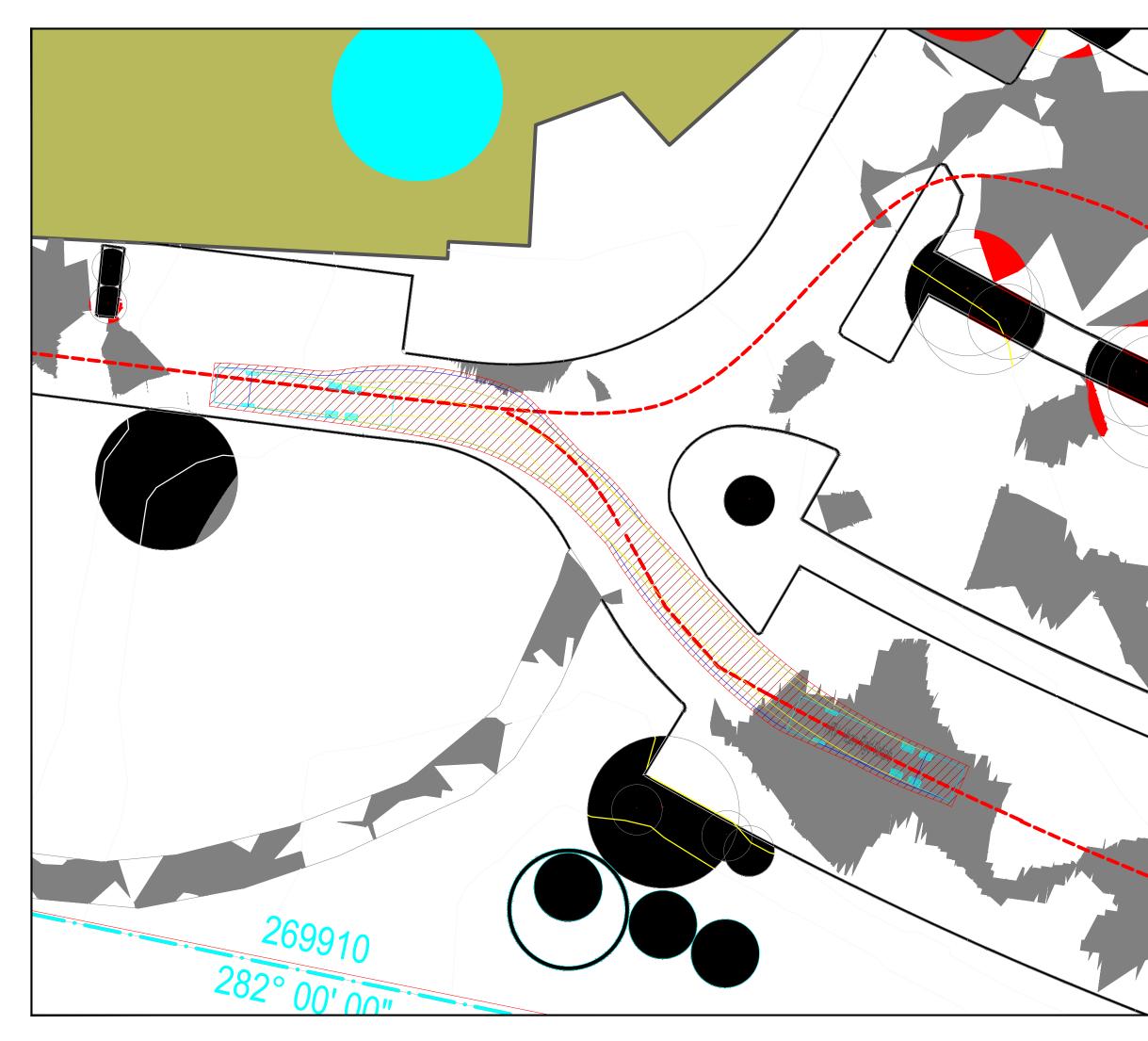


This drawing is prepared for information purposes only. It is not to be used for construction.

 $\ensuremath{\mathsf{TRAFFIX}}$  is responsible for vehicle swept path diagrams and/or drawing mark-ups only. Base drawing prepared by others.

Vehicle swept path diagrams prepared using computer generated turning path software and associated CAD drawing platforms. Vehicle data based upon relevant Australian Standards (AS/NZS 2890.1:2004 Parking facilities - Off-street car parking, and/or AS2890.2:2002 Parking facilities - Off-street commercial vehicle facilities]. These standards embody a degree of tolerance, however the vehicle characteristics in these standards represent a suitable design vehicle and do not account for all variations in vehicle dimensions / specifications and/or driver ability or behaviour.

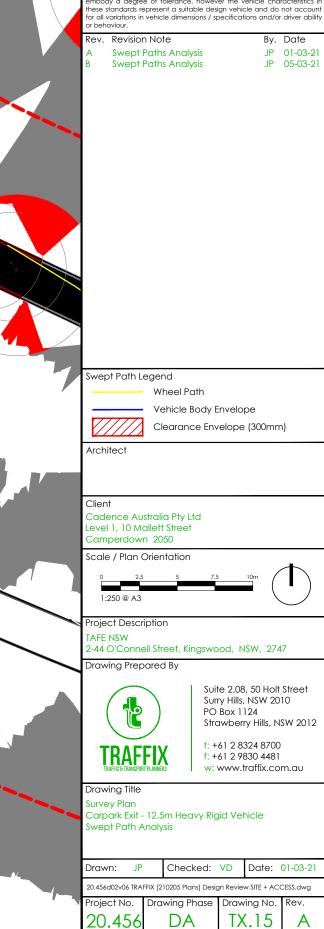




This drawing is prepared for information purposes only. It is not to be used for construction.

TRAFFIX is responsible for vehicle swept path diagrams and/or drawing mark-ups only. Base drawing prepared by others.

Vehicle swept path diagrams prepared using computer generated turning path software and associated CAD drawing platforms. Vehicle data based upon relevant Australian Standards (AS/NZS 2890.1:2004 Parking facilities - Off-street car parking, and/or AS2890.2:2002 Parking facilities - Off-street commercial vehicle facilities]. These standards embody a degree of tolerance, however the vehicle characteristics in these standards represent a suitable design vehicle and do not account for all variations in vehicle dimensions / specifications and/or driver ability or behaviour.



# APPENDIX E

TfNSW Correspondence

### Vince Doan

### Subject:

FW: [20.456] TAFE NSW Nepean Kingswood: 2-44 O'Connell Street, Kingswood

From: Vince Doan
Sent: Friday, 4 December 2020 4:37 PM
To: Laura Van putten
Cc: Justin Pindar
Subject: RE: [20.456] TAFE NSW Nepean Kingswood: 2-44 O'Connell Street, Kingswood

Hi Laura,

Thank you for the chat on Thursday (26/11/2020). We have now requested and received SCATS data. As discussed, the following will be our modelling methodology:

- Compare the intersection volume from this year and last year
- If last year volumes were greater than this year, we will use the SCATS data and the turning counts will be based on this years turning counts percentage on each approach
- If this year surveys are greater, we will use the surveys.

Please let me know if you have any other comments however, I do assume that is this the general approach for traffic modelling during this period (COVID-19).

Regards,

### Vince Doan Executive Engineer

### TRAFFIX



This email is confidential. If you are not the intended recipient, you must not disclose or use the information contained in it. If you have received this email in error, please notify us immediately by return email and delete the email and any attachments. TRAFFIX does not warrant the information in this e-mail or any attachment as being free from virus or any other defect or error. No liability is accepted for any resulting loss. Any views or opinions presented in this email are solely those of the author and do not necessarily represent those of the company.

From: Laura Van putten
Sent: Wednesday, 25 November 2020 9:44 AM
To: Vince Doan
Subject: RE: [20.456] TAFE NSW Nepean Kingswood: 2-44 O'Connell Street, Kingswood

### Hi Vince

Happy to discuss – I will be available to chat in the morning tomorrow please feel free to contact me my details are below.

If for whatever reason I may be away from the phone just flick me a quick email and I will call you back.

### Kind regards,

Laura van Putten

From: Vince Doan
Sent: Wednesday, 25 November 2020 8:27 AM
To: Laura Van putten
Cc: Development Sydney; Justin Pindar
Subject: RE: [20.456] TAFE NSW Nepean Kingswood: 2-44 O'Connell Street, Kingswood

Hi Laura,

Will you be free Thursday before 3pm or Friday (anytime) to have a quick chat either via the phone or teams?

Just wanted to have a quick discussion about the methodology of the proposal.

Regards,

Vince Doan Executive Engineer

TRAFFIX

This email is confidential. If you are not the intended recipient, you must not disclose or use the information contained in it. If you have received this email in error, please notify us immediately by return email and delete the email and any attachments. TRAFFIX does not warrant the information in this e-mail or any attachment as being free from virus or any other defect or error. No liability is accepted for any resulting loss. Any views or opinions presented in this email are solely those of the author and do not necessarily represent those of the company.

From: Sharon Verhoeven On Behalf Of Development Sydney
Sent: Friday, 20 November 2020 12:40 PM
To: Vince Doan
Cc: Laura Van putten
Subject: RE: [20.456] TAFE NSW Nepean Kingswood: 2-44 O'Connell Street, Kingswood

Hi Vince

It will be Laura Van Putten looking after this referral.

Kind regards Sharon

From: Vince Doan
Sent: Friday, 20 November 2020 12:18 PM
To: Development Sydney
Cc: Justin Pindar
Subject: RE: [20.456] TAFE NSW Nepean Kingswood: 2-44 O'Connell Street, Kingswood
Importance: High

Hi,

Yet to receive anything. Could you please advise who is the best contact?

Regards,

Vince Doan Executive Engineer

TRAFFIX

This email is confidential. If you are not the intended recipient, you must not disclose or use the information contained in it. If you have received this email in error, please notify us immediately by return email and delete the email and any attachments. TRAFFIX does not warrant the information in this e-mail or any attachment as being free from virus or any other defect or error. No liability is accepted for any resulting loss. Any views or opinions presented in this email are solely those of the author and do not necessarily represent those of the company.

From: Vince Doan
Sent: Wednesday, 11 November 2020 4:33 PM
To: Development Sydney
Cc: Justin Pindar
Subject: [20.456] TAFE NSW Nepean Kingswood: 2-44 O'Connell Street, Kingswood

To whom it may concern,

We have been engaged by TAFE NSW as the traffic engineers for works on the TAFE Nepean Kingswood Campus. The proposal is an SSD (SSD-8571481 attached).

Could you please advise who is the best contact moving forward? In addition, I would like to arrange a quick telephone chat sometime next week to just discuss the methodology.

Please contact me should you have any queries.

Regards,

Vince Doan Executive Engineer

TRAFFIX

This email is confidential. If you are not the intended recipient, you must not disclose or use the information contained in it. If you have received this email in error, please notify us immediately by return email and delete the email and any attachments. TRAFFIX does not warrant the information in this e-mail or any attachment as being free from virus or any other defect or error. No liability is accepted for any resulting loss. Any views or opinions presented in this email are solely those of the author and do not necessarily represent those of the company.



### Before printing, please consider the environment

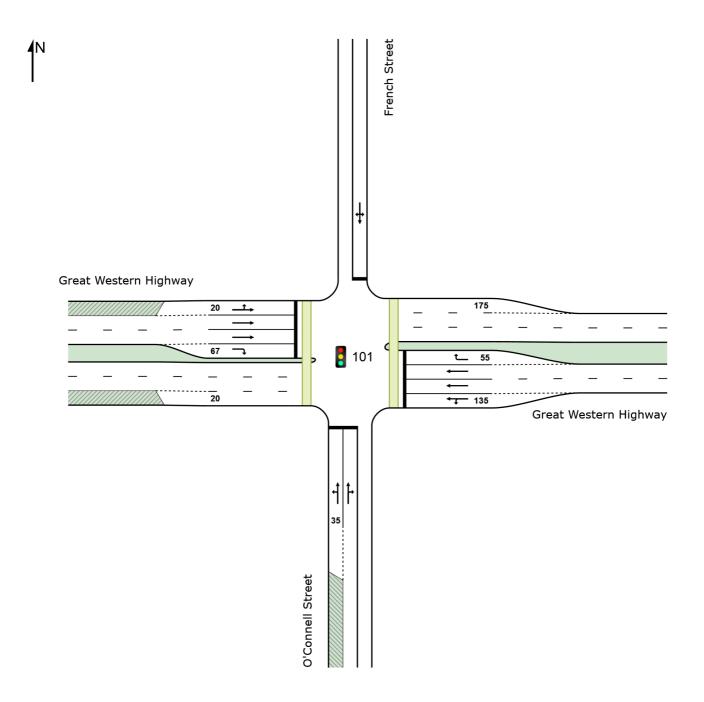
IMPORTANT NOTICE: This email and any attachment to it are intended only to be read or used by the named addressee. It is confidential and may contain legally privileged information. No confidentiality or privilege is waived or lost by any mistaken transmission to you. Roads and Maritime Services is not responsible for any unauthorised alterations to this email or attachment to it. Views expressed in this message are those of the individual sender, and are not necessarily the views of Roads and Maritime Services. If you receive this email in error, please immediately delete it from your system and notify the sender. You must not disclose, copy or use any part of this email if you are not the intended recipient.

This email is intended only for the addressee and may contain confidential information. If you receive this email in error please delete it and any attachments and notify the sender immediately by reply email. Transport for NSW takes all care to ensure that attachments are free from viruses or other defects. Transport for NSW assume no liability for any loss, damage or other consequences which may arise from opening or using an attachment.

Consider the environment. Please don't print this e-mail unless really necessary.

# APPENDIX F-1

SIDRA Modelling Outputs Great Western Highway, French Street and O'Connell Street



## **USER REPORT FOR SITE**

### **All Movement Classes**

Project: 20.456m01v03 TRAFFIX

## Site: 101 [Great Western Highway x O'Connell Street x French Street Existing AM (Site Folder: Exisitng (2020))]

New Site

Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site Optimum Cycle Time - Minimum Delay) Variable Sequence Analysis applied. The results are given for the selected output sequence.

Timings based on settings in the Site Phasing & Timing dialog Phase Times determined by the program Phase Sequence: TCS Reference Phase: Phase A Input Phase Sequence: A, B\*, C\*, D, E, E1\*, E2\* Output Phase Sequence: A, D, E (\* Variable Phase)

| Vehi         | cle M   | ovemen                          | t Perfor | mance                           |     |                     |      |                     |      |                             |                |                           |                        |                        |
|--------------|---------|---------------------------------|----------|---------------------------------|-----|---------------------|------|---------------------|------|-----------------------------|----------------|---------------------------|------------------------|------------------------|
| Mov<br>ID    | Turn    | INF<br>VOLU<br>[ Total<br>veh/h |          | DEM/<br>FLO<br>[ Total<br>veh/h |     | Deg.<br>Satn<br>v/c |      | Level of<br>Service |      | ACK OF<br>EUE<br>Dist]<br>m | Prop. E<br>Que | Effective<br>Stop<br>Rate | Aver.<br>No.<br>Cycles | Aver.<br>Speed<br>km/h |
| Sout         | h: O'Co | onnell Str                      | eet      |                                 |     |                     |      |                     |      |                             |                |                           |                        |                        |
| 1            | L2      | 44                              | 1        | 46                              | 2.3 | 0.130               | 44.0 | LOS D               | 2.6  | 18.6                        | 0.81           | 0.71                      | 0.81                   | 30.4                   |
| 2            | T1      | 11                              | 0        | 12                              | 0.0 | 0.130               | 37.5 | LOS C               | 2.6  | 18.6                        | 0.81           | 0.71                      | 0.81                   | 29.1                   |
| 3            | R2      | 169                             | 9        | 178                             | 5.3 | *0.725              | 58.3 | LOS E               | 10.4 | 76.2                        | 0.99           | 0.87                      | 1.09                   | 25.8                   |
| Appr         | oach    | 224                             | 10       | 236                             | 4.5 | 0.725               | 54.5 | LOS D               | 10.4 | 76.2                        | 0.95           | 0.83                      | 1.02                   | 26.7                   |
| East         | Great   | Western                         | Highway  | ý                               |     |                     |      |                     |      |                             |                |                           |                        |                        |
| 4            | L2      | 204                             | 10       | 215                             | 4.9 | 0.211               | 19.1 | LOS B               | 6.1  | 44.3                        | 0.52           | 0.72                      | 0.52                   | 40.3                   |
| 5            | T1      | 1458                            | 45       | 1535                            | 3.1 | <b>*</b> 0.718      | 20.0 | LOS B               | 32.7 | 234.9                       | 0.78           | 0.72                      | 0.78                   | 45.2                   |
| 6            | R2      | 23                              | 0        | 24                              | 0.0 | 0.174               | 63.8 | LOS E               | 1.4  | 9.7                         | 0.97           | 0.71                      | 0.97                   | 27.8                   |
| Appr         | oach    | 1685                            | 55       | 1774                            | 3.3 | 0.718               | 20.5 | LOS B               | 32.7 | 234.9                       | 0.76           | 0.72                      | 0.76                   | 44.3                   |
| North        | n: Fren | ch Street                       |          |                                 |     |                     |      |                     |      |                             |                |                           |                        |                        |
| 7            | L2      | 49                              | 0        | 52                              | 0.0 | 0.438               | 50.9 | LOS D               | 7.4  | 51.6                        | 0.92           | 0.79                      | 0.92                   | 31.1                   |
| 8            | T1      | 24                              | 0        | 25                              | 0.0 | 0.438               | 45.3 | LOS D               | 7.4  | 51.6                        | 0.92           | 0.79                      | 0.92                   | 26.9                   |
| 9            | R2      | 62                              | 0        | 65                              | 0.0 | 0.438               | 49.9 | LOS D               | 7.4  | 51.6                        | 0.92           | 0.79                      | 0.92                   | 31.2                   |
| Appr         | oach    | 135                             | 0        | 142                             | 0.0 | 0.438               | 49.4 | LOS D               | 7.4  | 51.6                        | 0.92           | 0.79                      | 0.92                   | 30.4                   |
| West         | : Grea  | t Westerr                       | n Highwa | y                               |     |                     |      |                     |      |                             |                |                           |                        |                        |
| 10           | L2      | 8                               | 0        | 8                               | 0.0 | 0.558               | 20.1 | LOS B               | 10.7 | 77.0                        | 0.57           | 0.50                      | 0.57                   | 44.4                   |
| 11           | T1      | 1254                            | 43       | 1320                            | 3.4 | 0.598               | 16.1 | LOS B               | 20.5 | 147.4                       | 0.62           | 0.55                      | 0.62                   | 47.6                   |
| 12           | R2      | 90                              | 7        | 95                              | 7.8 | <b>*</b> 0.718      | 69.2 | LOS E               | 5.9  | 43.8                        | 1.00           | 0.84                      | 1.16                   | 23.7                   |
| Appr         | oach    | 1352                            | 50       | 1423                            | 3.7 | 0.718               | 19.6 | LOS B               | 20.5 | 147.4                       | 0.64           | 0.57                      | 0.65                   | 45.2                   |
| All<br>Vehic | cles    | 3396                            | 115      | 3575                            | 3.4 | 0.725               | 23.5 | LOS B               | 32.7 | 234.9                       | 0.73           | 0.67                      | 0.74                   | 42.3                   |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## Site: 301 [Great Western Highway x O'Connell Street x French Street 2026 AM (Site Folder: Future - 2026)]

New Site

Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time) Variable Sequence Analysis applied. The results are given for the selected output sequence. Design Life Analysis (Final Year): Results for 6 years

#### Timings based on settings in the Site Phasing & Timing dialog (Demand & Sensitivity Analysis overrides) Phase Times determined by the program Phase Sequence: TCS Reference Phase: Phase A Input Phase Sequence: A, B\*, C\*, D, E, E1\*, E2\* Output Phase Sequence: A, D, E, E2\* (\* Variable Phase)

| Vehi         | cle M   | ovemen                          | t Perfoi | rmance                          |     |                     |      |                     |      |                             |                |                           |                        |                        |
|--------------|---------|---------------------------------|----------|---------------------------------|-----|---------------------|------|---------------------|------|-----------------------------|----------------|---------------------------|------------------------|------------------------|
| Mov<br>ID    | Turn    | INP<br>VOLU<br>[ Total<br>veh/h |          | DEM/<br>FLO<br>[ Total<br>veh/h |     | Deg.<br>Satn<br>v/c |      | Level of<br>Service |      | ACK OF<br>EUE<br>Dist]<br>m | Prop. I<br>Que | Effective<br>Stop<br>Rate | Aver.<br>No.<br>Cycles | Aver.<br>Speed<br>km/h |
| South        | n: O'C  | onnell Str                      | eet      |                                 |     |                     |      |                     |      |                             |                |                           |                        |                        |
| 1            | L2      | 44                              | 1        | 52                              | 2.3 | 0.152               | 45.5 | LOS D               | 3.0  | 21.4                        | 0.82           | 0.72                      | 0.82                   | 30.0                   |
| 2            | T1      | 11                              | 0        | 13                              | 0.0 | 0.152               | 38.5 | LOS C               | 3.0  | 21.4                        | 0.82           | 0.72                      | 0.82                   | 28.8                   |
| 3            | R2      | 169                             | 9        | 200                             | 5.3 | <b>*</b> 0.913      | 76.8 | LOS F <sup>11</sup> | 14.0 | 102.8                       | 1.00           | 1.06                      | 1.45                   | 22.1                   |
| Appro        | oach    | 224                             | 10       | 266                             | 4.5 | 0.913               | 68.8 | LOS E <sup>11</sup> | 14.0 | 102.8                       | 0.96           | 0.98                      | 1.30                   | 23.6                   |
| East:        | Great   | Western                         | Highwa   | y                               |     |                     |      |                     |      |                             |                |                           |                        |                        |
| 4            | L2      | 204                             | 10       | 242                             | 4.9 | 0.234               | 18.8 | LOS B               | 6.8  | 49.8                        | 0.52           | 0.72                      | 0.52                   | 40.5                   |
| 5            | T1      | 1458                            | 45       | 1728                            | 3.1 | <b>*</b> 0.817      | 21.1 | LOS B               | 39.7 | 284.9                       | 0.84           | 0.78                      | 0.84                   | 44.5                   |
| 6            | R2      | 23                              | 0        | 27                              | 0.0 | 0.294               | 68.7 | LOS E <sup>11</sup> | 1.6  | 11.5                        | 1.00           | 0.71                      | 1.00                   | 26.8                   |
| Appro        | oach    | 1685                            | 55       | 1997                            | 3.3 | 0.817               | 21.5 | LOS B               | 39.7 | 284.9                       | 0.81           | 0.77                      | 0.81                   | 43.7                   |
| North        | n: Fren | ch Street                       |          |                                 |     |                     |      |                     |      |                             |                |                           |                        |                        |
| 7            | L2      | 49                              | 0        | 58                              | 0.0 | 0.520               | 53.0 | LOS D               | 8.5  | 59.8                        | 0.94           | 0.80                      | 0.94                   | 30.6                   |
| 8            | T1      | 24                              | 0        | 28                              | 0.0 | 0.520               | 47.1 | LOS D               | 8.5  | 59.8                        | 0.94           | 0.80                      | 0.94                   | 26.5                   |
| 9            | R2      | 62                              | 0        | 73                              | 0.0 | 0.520               | 51.7 | LOS D               | 8.5  | 59.8                        | 0.94           | 0.80                      | 0.94                   | 30.7                   |
| Appro        | oach    | 135                             | 0        | 160                             | 0.0 | 0.520               | 51.3 | LOS D               | 8.5  | 59.8                        | 0.94           | 0.80                      | 0.94                   | 30.0                   |
| West         | : Grea  | t Westerr                       | n Highwa | ıy                              |     |                     |      |                     |      |                             |                |                           |                        |                        |
| 10           | L2      | 8                               | 0        | 9                               | 0.0 | 0.601               | 18.3 | LOS B               | 11.2 | 80.8                        | 0.54           | 0.48                      | 0.54                   | 45.4                   |
| 11           | T1      | 1254                            | 43       | 1487                            | 3.4 | 0.643               | 14.4 | LOS A               | 22.8 | 164.4                       | 0.60           | 0.53                      | 0.60                   | 48.7                   |
| 12           | R2      | 90                              | 7        | 107                             | 7.8 | *0.808              | 72.0 | LOS F <sup>11</sup> | 6.8  | 50.9                        | 1.00           | 0.91                      | 1.29                   | 23.1                   |
| Appro        | oach    | 1352                            | 50       | 1603                            | 3.7 | 0.808               | 18.3 | LOS B               | 22.8 | 164.4                       | 0.63           | 0.56                      | 0.64                   | 46.0                   |
| All<br>Vehic | cles    | 3396                            | 115      | 4026                            | 3.4 | 0.913               | 24.5 | LOS B               | 39.7 | 284.9                       | 0.75           | 0.70                      | 0.78                   | 41.9                   |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

11 Level of Service is worse than the Level of Service Target specified in the Parameter Settings dialog.

## Site: 501 [Great Western Highway x O'Connell Street x French Street 2026+DEV AM (Site Folder: Future - 2026 + DEV)]

New Site

Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time) Variable Sequence Analysis applied. The results are given for the selected output sequence. Design Life Analysis (Final Year): Results for 6 years

#### Timings based on settings in the Site Phasing & Timing dialog (Demand & Sensitivity Analysis overrides) Phase Times determined by the program Phase Sequence: TCS Reference Phase: Phase A Input Phase Sequence: A, B\*, C\*, D, E, E1\*, E2\* Output Phase Sequence: A, D, E (\* Variable Phase)

| Vehi         | cle M   | ovemen                          | t Perfor | mance                           |     |                     |      |                     |      |                             |              |                           |                        |                        |
|--------------|---------|---------------------------------|----------|---------------------------------|-----|---------------------|------|---------------------|------|-----------------------------|--------------|---------------------------|------------------------|------------------------|
| Mov<br>ID    | Turn    | INP<br>VOLL<br>[ Total<br>veh/h |          | DEM/<br>FLO<br>[ Total<br>veh/h |     | Deg.<br>Satn<br>v/c |      | Level of<br>Service |      | ACK OF<br>EUE<br>Dist]<br>m | Prop.<br>Que | Effective<br>Stop<br>Rate | Aver.<br>No.<br>Cycles | Aver.<br>Speed<br>km/h |
| South        | n: O'C  | onnell Str                      |          |                                 |     |                     |      |                     |      |                             |              |                           |                        |                        |
| 1            | L2      | 48                              | 1        | 56                              | 2.1 | 0.168               | 46.6 | LOS D               | 3.2  | 23.1                        | 0.84         | 0.72                      | 0.84                   | 29.7                   |
| 2            | T1      | 11                              | 0        | 13                              | 0.0 | 0.168               | 39.6 | LOS C               | 3.2  | 23.1                        | 0.84         | 0.72                      | 0.84                   | 28.5                   |
| 3            | R2      | 170                             | 9        | 201                             | 5.3 | *0.923              | 79.1 | LOS F <sup>11</sup> | 14.4 | 105.1                       | 1.00         | 1.08                      | 1.48                   | 21.7                   |
| Appro        | oach    | 229                             | 10       | 271                             | 4.4 | 0.923               | 70.4 | LOS E <sup>11</sup> | 14.4 | 105.1                       | 0.96         | 0.99                      | 1.32                   | 23.3                   |
| East:        | Great   | Western                         | Highway  | ý                               |     |                     |      |                     |      |                             |              |                           |                        |                        |
| 4            | L2      | 209                             | 10       | 247                             | 4.8 | 0.243               | 19.4 | LOS B               | 7.1  | 52.0                        | 0.54         | 0.73                      | 0.54                   | 40.2                   |
| 5            | T1      | 1458                            | 45       | 1728                            | 3.1 | <b>*</b> 0.831      | 23.2 | LOS B               | 41.6 | 298.9                       | 0.86         | 0.80                      | 0.87                   | 43.4                   |
| 6            | R2      | 23                              | 0        | 27                              | 0.0 | 0.176               | 62.6 | LOS E <sup>11</sup> | 1.5  | 10.8                        | 0.96         | 0.72                      | 0.96                   | 28.1                   |
| Appro        | oach    | 1690                            | 55       | 2003                            | 3.3 | 0.831               | 23.3 | LOS B               | 41.6 | 298.9                       | 0.82         | 0.79                      | 0.83                   | 42.8                   |
| North        | n: Fren | ch Street                       |          |                                 |     |                     |      |                     |      |                             |              |                           |                        |                        |
| 7            | L2      | 49                              | 0        | 58                              | 0.0 | 0.524               | 53.1 | LOS D               | 8.6  | 59.9                        | 0.94         | 0.80                      | 0.94                   | 30.6                   |
| 8            | T1      | 24                              | 0        | 28                              | 0.0 | 0.524               | 47.2 | LOS D               | 8.6  | 59.9                        | 0.94         | 0.80                      | 0.94                   | 26.5                   |
| 9            | R2      | 62                              | 0        | 73                              | 0.0 | 0.524               | 51.7 | LOS D               | 8.6  | 59.9                        | 0.94         | 0.80                      | 0.94                   | 30.7                   |
| Appro        | oach    | 135                             | 0        | 160                             | 0.0 | 0.524               | 51.4 | LOS D               | 8.6  | 59.9                        | 0.94         | 0.80                      | 0.94                   | 30.0                   |
| West         | : Grea  | t Westerr                       | n Highwa | y                               |     |                     |      |                     |      |                             |              |                           |                        |                        |
| 10           | L2      | 8                               | 0        | 9                               | 0.0 | 0.645               | 20.5 | LOS B               | 12.0 | 86.3                        | 0.58         | 0.51                      | 0.58                   | 44.2                   |
| 11           | T1      | 1254                            | 43       | 1487                            | 3.4 | 0.691               | 16.9 | LOS B               | 24.8 | 178.5                       | 0.65         | 0.58                      | 0.65                   | 47.1                   |
| 12           | R2      | 107                             | 7        | 125                             | 6.7 | <b>*</b> 0.843      | 73.0 | LOS F <sup>11</sup> | 8.1  | 59.8                        | 1.00         | 0.94                      | 1.33                   | 23.0                   |
| Appro        | oach    | 1369                            | 50       | 1621                            | 3.7 | 0.843               | 21.2 | LOS B               | 24.8 | 178.5                       | 0.68         | 0.61                      | 0.70                   | 44.3                   |
| All<br>Vehic | les     | 3423                            | 115      | 4054                            | 3.4 | 0.923               | 26.7 | LOS B               | 41.6 | 298.9                       | 0.78         | 0.73                      | 0.82                   | 40.8                   |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

11 Level of Service is worse than the Level of Service Target specified in the Parameter Settings dialog.

## Site: 701 [Great Western Highway x O'Connell Street x French Street 2030 AM (Site Folder: Future - 2030)]

New Site

Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 130 seconds (Site Practical Cycle Time) Variable Sequence Analysis applied. The results are given for the selected output sequence. Design Life Analysis (Final Year): Results for 10 years

#### Timings based on settings in the Site Phasing & Timing dialog (Demand & Sensitivity Analysis overrides) Phase Times determined by the program Phase Sequence: TCS Reference Phase: Phase A Input Phase Sequence: A, B\*, C\*, D, E, E1\*, E2\* Output Phase Sequence: A, D, E (\* Variable Phase)

| Vehi         | icle M  | ovemen                          | t Perfoi | rmance                          |     |                     |       |                     |      |                             |                |                          |                        |                        |
|--------------|---------|---------------------------------|----------|---------------------------------|-----|---------------------|-------|---------------------|------|-----------------------------|----------------|--------------------------|------------------------|------------------------|
| Mov<br>ID    | Turn    | INP<br>VOLU<br>[ Total<br>veh/h |          | DEM/<br>FLO<br>[ Total<br>veh/h |     | Deg.<br>Satn<br>v/c |       | Level of<br>Service |      | ACK OF<br>EUE<br>Dist]<br>m | Prop. E<br>Que | ffective<br>Stop<br>Rate | Aver.<br>No.<br>Cycles | Aver.<br>Speed<br>km/h |
| Sout         | h: O'C  | onnell Str                      | eet      |                                 |     |                     |       |                     |      |                             |                |                          |                        |                        |
| 1            | L2      | 44                              | 1        | 56                              | 2.3 | 0.160               | 48.4  | LOS D               | 3.5  | 24.9                        | 0.82           | 0.72                     | 0.82                   | 29.2                   |
| 2            | T1      | 11                              | 0        | 14                              | 0.0 | 0.160               | 41.2  | LOS C               | 3.5  | 24.9                        | 0.82           | 0.72                     | 0.82                   | 28.0                   |
| 3            | R2      | 169                             | 9        | 217                             | 5.3 | *0.985              | 106.5 | LOS F <sup>11</sup> | 19.0 | 139.3                       | 1.00           | 1.17                     | 1.65                   | 18.0                   |
| Appr         | oach    | 224                             | 10       | 287                             | 4.5 | 0.985               | 91.9  | LOS F <sup>11</sup> | 19.0 | 139.3                       | 0.96           | 1.06                     | 1.45                   | 19.8                   |
| East         | Great   | Western                         | Highwa   | у                               |     |                     |       |                     |      |                             |                |                          |                        |                        |
| 4            | L2      | 204                             | 10       | 262                             | 4.9 | 0.253               | 20.0  | LOS B               | 8.1  | 58.7                        | 0.53           | 0.73                     | 0.53                   | 39.8                   |
| 5            | T1      | 1458                            | 45       | 1871                            | 3.1 | *0.903              | 34.9  | LOS C               | 60.0 | 430.8                       | 0.90           | 0.91                     | 1.00                   | 38.1                   |
| 6            | R2      | 23                              | 0        | 30                              | 0.0 | 0.207               | 68.4  | LOS E <sup>11</sup> | 1.8  | 12.7                        | 0.97           | 0.72                     | 0.97                   | 26.9                   |
| Appr         | oach    | 1685                            | 55       | 2162                            | 3.3 | 0.903               | 33.5  | LOS C               | 60.0 | 430.8                       | 0.86           | 0.89                     | 0.94                   | 38.1                   |
| North        | n: Fren | ch Street                       |          |                                 |     |                     |       |                     |      |                             |                |                          |                        |                        |
| 7            | L2      | 49                              | 0        | 63                              | 0.0 | 0.542               | 57.2  | LOS E <sup>11</sup> | 10.0 | 70.2                        | 0.95           | 0.81                     | 0.95                   | 29.6                   |
| 8            | T1      | 24                              | 0        | 31                              | 0.0 | 0.542               | 51.1  | LOS D               | 10.0 | 70.2                        | 0.95           | 0.81                     | 0.95                   | 25.5                   |
| 9            | R2      | 62                              | 0        | 80                              | 0.0 | 0.542               | 55.6  | LOS D               | 10.0 | 70.2                        | 0.95           | 0.81                     | 0.95                   | 29.7                   |
| Appr         | oach    | 135                             | 0        | 173                             | 0.0 | 0.542               | 55.4  | LOS D               | 10.0 | 70.2                        | 0.95           | 0.81                     | 0.95                   | 29.0                   |
| West         | t: Grea | t Westerr                       | n Highwa | iy                              |     |                     |       |                     |      |                             |                |                          |                        |                        |
| 10           | L2      | 8                               | 0        | 10                              | 0.0 | 0.691               | 21.1  | LOS B               | 13.3 | 95.8                        | 0.58           | 0.51                     | 0.58                   | 43.9                   |
| 11           | T1      | 1254                            | 43       | 1609                            | 3.4 | 0.740               | 18.2  | LOS B               | 30.7 | 220.9                       | 0.66           | 0.59                     | 0.66                   | 46.4                   |
| 12           | R2      | 90                              | 7        | 115                             | 7.8 | <b>*</b> 0.853      | 79.3  | LOS F <sup>11</sup> | 8.1  | 60.7                        | 1.00           | 0.94                     | 1.35                   | 21.8                   |
| Appr         | oach    | 1352                            | 50       | 1735                            | 3.7 | 0.853               | 22.2  | LOS B               | 30.7 | 220.9                       | 0.68           | 0.62                     | 0.71                   | 43.8                   |
| All<br>Vehio | cles    | 3396                            | 115      | 4358                            | 3.4 | 0.985               | 33.8  | LOS C               | 60.0 | 430.8                       | 0.80           | 0.79                     | 0.88                   | 37.7                   |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

11 Level of Service is worse than the Level of Service Target specified in the Parameter Settings dialog.

## Site: 901 [Great Western Highway x O'Connell Street x French Street 2030+DEV AM (Site Folder: Future - 2030 +DEV)]

New Site

Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 130 seconds (Site User-Given Cycle Time) Design Life Analysis (Final Year): Results for 10 years

Timings based on settings in the Site Phasing & Timing dialog (Demand & Sensitivity Analysis overrides) Phase Times determined by the program Phase Sequence: TCS - Existing Reference Phase: Phase A Input Phase Sequence: A, D, E Output Phase Sequence: A, D, E

| Vehi         | cle M   | ovemen                          | t Perfoi | mance                           |     |                     |       |                     |      |                             |                |                          |                        |                        |
|--------------|---------|---------------------------------|----------|---------------------------------|-----|---------------------|-------|---------------------|------|-----------------------------|----------------|--------------------------|------------------------|------------------------|
| Mov<br>ID    | Turn    | INP<br>VOLL<br>[ Total<br>veh/h |          | DEM/<br>FLO<br>[ Total<br>veh/h |     | Deg.<br>Satn<br>v/c |       | Level of<br>Service |      | ACK OF<br>EUE<br>Dist]<br>m | Prop. E<br>Que | ffective<br>Stop<br>Rate | Aver.<br>No.<br>Cycles | Aver.<br>Speed<br>km/h |
| South        | h: O'C  | onnell Str                      | eet      |                                 |     |                     |       |                     |      |                             |                |                          |                        |                        |
| 1            | L2      | 54                              | 1        | 67                              | 1.9 | 0.177               | 47.9  | LOS D               | 4.0  | 28.4                        | 0.82           | 0.73                     | 0.82                   | 29.5                   |
| 2            | T1      | 11                              | 0        | 14                              | 0.0 | 0.177               | 40.6  | LOS C               | 4.0  | 28.4                        | 0.82           | 0.73                     | 0.82                   | 28.2                   |
| 3            | R2      | 172                             | 9        | 220                             | 5.2 | <b>*</b> 1.052      | 145.4 | LOS F <sup>11</sup> | 23.1 | 169.0                       | 1.00           | 1.30                     | 1.92                   | 14.2                   |
| Appro        | oach    | 237                             | 10       | 301                             | 4.3 | 1.052               | 118.8 | LOS F <sup>11</sup> | 23.1 | 169.0                       | 0.95           | 1.15                     | 1.62                   | 16.5                   |
| East:        | Great   | Western                         | Highwa   | y                               |     |                     |       |                     |      |                             |                |                          |                        |                        |
| 4            | L2      | 215                             | 10       | 273                             | 4.7 | 0.275               | 21.7  | LOS B               | 8.9  | 65.1                        | 0.56           | 0.74                     | 0.56                   | 38.9                   |
| 5            | T1      | 1458                            | 45       | 1871                            | 3.1 | <b>*</b> 0.947      | 51.7  | LOS D               | 72.2 | 519.1                       | 0.95           | 1.05                     | 1.17                   | 32.4                   |
| 6            | R2      | 23                              | 0        | 30                              | 0.0 | 0.159               | 64.5  | LOS E <sup>11</sup> | 1.8  | 12.3                        | 0.95           | 0.72                     | 0.95                   | 27.7                   |
| Appro        | oach    | 1696                            | 55       | 2174                            | 3.2 | 0.947               | 48.1  | LOS D               | 72.2 | 519.1                       | 0.90           | 1.01                     | 1.09                   | 32.9                   |
| North        | n: Fren | ch Street                       |          |                                 |     |                     |       |                     |      |                             |                |                          |                        |                        |
| 7            | L2      | 49                              | 0        | 63                              | 0.0 | 0.569               | 56.9  | LOS E <sup>11</sup> | 10.5 | 73.3                        | 0.95           | 0.81                     | 0.95                   | 29.8                   |
| 8            | T1      | 31                              | 0        | 38                              | 0.0 | 0.569               | 50.7  | LOS D               | 10.5 | 73.3                        | 0.95           | 0.81                     | 0.95                   | 25.9                   |
| 9            | R2      | 62                              | 0        | 80                              | 0.0 | 0.569               | 55.2  | LOS D               | 10.5 | 73.3                        | 0.95           | 0.81                     | 0.95                   | 29.9                   |
| Appro        | oach    | 142                             | 0        | 181                             | 0.0 | 0.569               | 54.8  | LOS D               | 10.5 | 73.3                        | 0.95           | 0.81                     | 0.95                   | 29.1                   |
| West         | : Grea  | t Westerr                       | n Highwa | ıy                              |     |                     |       |                     |      |                             |                |                          |                        |                        |
| 10           | L2      | 8                               | 0        | 10                              | 0.0 | 0.736               | 23.3  | LOS B               | 14.3 | 103.1                       | 0.61           | 0.54                     | 0.61                   | 42.7                   |
| 11           | T1      | 1254                            | 43       | 1609                            | 3.4 | 0.788               | 21.0  | LOS B               | 31.6 | 228.0                       | 0.69           | 0.63                     | 0.71                   | 44.8                   |
| 12           | R2      | 129                             | 7        | 157                             | 5.7 | <b>*</b> 0.877      | 79.3  | LOS F <sup>11</sup> | 11.1 | 81.9                        | 1.00           | 0.96                     | 1.35                   | 22.0                   |
| Appro        | oach    | 1391                            | 50       | 1776                            | 3.6 | 0.877               | 26.2  | LOS B               | 31.6 | 228.0                       | 0.72           | 0.66                     | 0.76                   | 41.7                   |
| All<br>Vehic | cles    | 3466                            | 115      | 4431                            | 3.3 | 1.052               | 44.4  | LOS D               | 72.2 | 519.1                       | 0.84           | 0.87                     | 0.99                   | 33.8                   |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

11 Level of Service is worse than the Level of Service Target specified in the Parameter Settings dialog.

## Site: 201 [Great Western Highway x O'Connell Street x French Street Existing PM (Site Folder: Exisitng (2020))]

New Site Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site Optimum Cycle Time - Minimum Delay) Variable Sequence Analysis applied. The results are given for the selected output sequence.

Timings based on settings in the Site Phasing & Timing dialog Phase Times determined by the program Phase Sequence: TCS Reference Phase: Phase A Input Phase Sequence: A, B\*, C\*, D, E, E1\*, E2\* Output Phase Sequence: A, D, E (\* Variable Phase)

| Vehi         | cle M    | ovemen                          | t Perfo  | rmance                          |            |                     |              |                     |                                |                             |                |                           |                        |                        |
|--------------|----------|---------------------------------|----------|---------------------------------|------------|---------------------|--------------|---------------------|--------------------------------|-----------------------------|----------------|---------------------------|------------------------|------------------------|
| Mov<br>ID    | Turn     | INP<br>VOLU<br>[ Total<br>veh/h |          | DEM/<br>FLO<br>[ Total<br>veh/h |            | Deg.<br>Satn<br>v/c |              | Level of<br>Service | 95% BA<br>QUE<br>[ Veh.<br>veh | ACK OF<br>EUE<br>Dist]<br>m | Prop. I<br>Que | Effective<br>Stop<br>Rate | Aver.<br>No.<br>Cycles | Aver.<br>Speed<br>km/h |
| South        | n: O'C   | onnell Str                      | reet     |                                 |            |                     |              |                     |                                |                             |                |                           |                        |                        |
| 1<br>2       | L2<br>T1 | 55<br>17                        | 4<br>0   | 58<br>18                        | 7.3<br>0.0 | 0.144<br>0.722      | 40.6<br>37.8 | LOS C<br>LOS C      | 3.1<br>12.0                    | 22.9<br>86.9                | 0.78<br>0.83   | 0.71<br>0.75              | 0.78<br>0.84           | 31.3<br>28.9           |
| 3            | R2       | 198                             | 8        | 208                             | 4.0        | *0.722              | 53.3         | LOS D               | 12.0                           | 86.9                        | 0.97           | 0.87                      | 1.04                   | 27.0                   |
| Appro        | oach     | 270                             | 12       | 284                             | 4.4        | 0.722               | 49.8         | LOS D               | 12.0                           | 86.9                        | 0.92           | 0.83                      | 0.98                   | 27.9                   |
| East:        | Great    | Western                         | Highwa   | у                               |            |                     |              |                     |                                |                             |                |                           |                        |                        |
| 4<br>5       | L2<br>T1 | 216<br>1220                     | 9<br>25  | 227<br>1284                     | 4.2<br>2.0 | 0.236<br>0.655      | 21.4<br>20.8 | LOS B<br>LOS B      | 7.0<br>27.8                    | 50.6<br>198.2               | 0.57<br>0.76   | 0.73<br>0.68              | 0.57<br>0.76           | 39.0<br>44.7           |
| 6            | R2       | 73                              | 0        | 77                              | 0.0        | 0.552               | 66.4         | LOSE                | 4.6                            | 32.1                        | 1.00           | 0.77                      | 1.01                   | 27.3                   |
| Appro        |          | 1509                            | 34       | 1588                            | 2.3        | 0.655               | 23.1         | LOS B               | 27.8                           | 198.2                       | 0.74           | 0.70                      | 0.74                   | 42.6                   |
| North        | : Fren   | ch Street                       |          |                                 |            |                     |              |                     |                                |                             |                |                           |                        |                        |
| 7            | L2       | 40                              | 1        | 42                              | 2.5        | 0.338               | 46.8         | LOS D               | 6.0                            | 42.5                        | 0.87           | 0.77                      | 0.87                   | 32.2                   |
| 8            | T1       | 18                              | 0        | 19                              | 0.0        | 0.338               | 40.9         | LOS C               | 6.0                            | 42.5                        | 0.87           | 0.77                      | 0.87                   | 28.0                   |
| 9            | R2       | 58                              | 1        | 61                              | 1.7        | 0.338               | 45.5         | LOS D               | 6.0                            | 42.5                        | 0.87           | 0.77                      | 0.87                   | 32.3                   |
| Appro        | bach     | 116                             | 2        | 122                             | 1.7        | 0.338               | 45.2         | LOS D               | 6.0                            | 42.5                        | 0.87           | 0.77                      | 0.87                   | 31.7                   |
| West         | : Grea   | t Westerr                       | n Highwa | iy                              |            |                     |              |                     |                                |                             |                |                           |                        |                        |
| 10           | L2       | 19                              | 1        | 20                              | 5.3        | 0.688               | 22.9         | LOS B               | 12.9                           | 91.4                        | 0.62           | 0.55                      | 0.62                   | 42.8                   |
| 11           | T1       | 1441                            | 24       | 1517                            | 1.7        | <b>*</b> 0.737      | 19.9         | LOS B               | 29.0                           | 205.9                       | 0.71           | 0.63                      | 0.71                   | 45.4                   |
| 12           | R2       | 85                              | 4        | 89                              | 4.7        | <b>*</b> 0.664      | 68.0         | LOS E               | 5.5                            | 39.8                        | 1.00           | 0.82                      | 1.10                   | 23.9                   |
| Appro        | oach     | 1545                            | 29       | 1626                            | 1.9        | 0.737               | 22.5         | LOS B               | 29.0                           | 205.9                       | 0.72           | 0.64                      | 0.73                   | 43.6                   |
| All<br>Vehic | les      | 3440                            | 77       | 3621                            | 2.2        | 0.737               | 25.7         | LOS B               | 29.0                           | 205.9                       | 0.75           | 0.68                      | 0.76                   | 41.2                   |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## Site: 401 [Great Western Highway x O'Connell Street x French Street 2026 PM (Site Folder: Future - 2026)]

New Site

Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time) Variable Sequence Analysis applied. The results are given for the selected output sequence. Design Life Analysis (Final Year): Results for 6 years

#### Timings based on settings in the Site Phasing & Timing dialog (Demand & Sensitivity Analysis overrides) Phase Times determined by the program Phase Sequence: TCS Reference Phase: Phase A Input Phase Sequence: A, B\*, C\*, D, E, E1\*, E2\* Output Phase Sequence: A, D, E, E2\* (\* Variable Phase)

| Vehi         | cle M    | ovemen                          | t Perfor | rmance                          |            |                     |              |                              |             |                             |                |                           |                        |                        |
|--------------|----------|---------------------------------|----------|---------------------------------|------------|---------------------|--------------|------------------------------|-------------|-----------------------------|----------------|---------------------------|------------------------|------------------------|
| Mov<br>ID    | Turn     | INP<br>VOLU<br>[ Total<br>veh/h |          | DEM/<br>FLO<br>[ Total<br>veh/h |            | Deg.<br>Satn<br>v/c |              | Level of<br>Service          |             | ACK OF<br>EUE<br>Dist]<br>m | Prop. I<br>Que | Effective<br>Stop<br>Rate | Aver.<br>No.<br>Cycles | Aver.<br>Speed<br>km/h |
| Sout         | n: O'C   | onnell Str                      | eet      |                                 |            |                     |              |                              |             |                             |                |                           |                        |                        |
| 1<br>2       | L2<br>T1 | 55<br>17                        | 4<br>0   | 65<br>20                        | 7.3<br>0.0 | 0.161<br>0.807      | 40.3<br>37.2 | LOS C<br>LOS C               | 3.5<br>14.3 | 26.1<br>103.9               | 0.78<br>0.82   | 0.71<br>0.75              | 0.78<br>0.85           | 31.5<br>29.1           |
| 3            | R2       | 198                             | 8        | 235                             | 4.0        | * 0.807             | 57.2<br>57.6 | LOS C<br>LOS E <sup>11</sup> | 14.3        | 103.9                       | 0.82           | 0.75                      | 1.16                   | 29.1                   |
| Appr         | oach     | 270                             | 12       | 320                             | 4.4        | 0.807               | 52.8         | LOS D                        | 14.3        | 103.9                       | 0.93           | 0.88                      | 1.06                   | 27.1                   |
| East:        | Great    | Western                         | Highway  | y                               |            |                     |              |                              |             |                             |                |                           |                        |                        |
| 4<br>5       | L2<br>T1 | 216<br>1220                     | 9<br>25  | 256<br>1446                     | 4.2<br>2.0 | 0.270<br>0.754      | 22.3<br>23.1 | LOS B<br>LOS B               | 8.2<br>33.9 | 59.2<br>241.2               | 0.59<br>0.82   | 0.74<br>0.75              | 0.59<br>0.82           | 38.6<br>43.5           |
| 6            | R2       | 73                              | 0        | 87                              | 0.0        | <b>*</b> 0.799      | 73.1         | LOS F <sup>11</sup>          | 5.6         | 38.9                        | 1.00           | 0.89                      | 1.29                   | 26.0                   |
| Appr         | oach     | 1509                            | 34       | 1789                            | 2.3        | 0.799               | 25.4         | LOS B                        | 33.9        | 241.2                       | 0.80           | 0.76                      | 0.81                   | 41.5                   |
| North        | n: Fren  | ch Street                       |          |                                 |            |                     |              |                              |             |                             |                |                           |                        |                        |
| 7            | L2       | 40                              | 1        | 47                              | 2.5        | 0.370               | 47.5         | LOS D                        | 6.8         | 48.2                        | 0.88           | 0.77                      | 0.88                   | 32.1                   |
| 8            | T1       | 18                              | 0        | 21                              | 0.0        | 0.370               | 41.3         | LOS C                        | 6.8         | 48.2                        | 0.88           | 0.77                      | 0.88                   | 28.0                   |
| 9            | R2       | 58                              | 1        | 69                              | 1.7        | 0.370               | 45.8         | LOS D                        | 6.8         | 48.2                        | 0.88           | 0.77                      | 0.88                   | 32.2                   |
| Appr         | oach     | 116                             | 2        | 138                             | 1.7        | 0.370               | 45.7         | LOS D                        | 6.8         | 48.2                        | 0.88           | 0.77                      | 0.88                   | 31.6                   |
| West         | : Grea   | t Westerr                       | n Highwa | ıy                              |            |                     |              |                              |             |                             |                |                           |                        |                        |
| 10           | L2       | 19                              | 1        | 23                              | 5.3        | 0.773               | 26.1         | LOS B                        | 15.5        | 109.9                       | 0.63           | 0.60                      | 0.68                   | 41.3                   |
| 11           | T1       | 1441                            | 24       | 1708                            | 1.7        | *0.828              | 24.3         | LOS B                        | 36.8        | 261.3                       | 0.74           | 0.71                      | 0.79                   | 43.0                   |
| 12           | R2       | 85                              | 4        | 101                             | 4.7        | 0.748               | 69.8         | LOS E <sup>11</sup>          | 6.3         | 45.8                        | 1.00           | 0.86                      | 1.19                   | 23.6                   |
| Appro        | oach     | 1545                            | 29       | 1831                            | 1.9        | 0.828               | 26.8         | LOS B                        | 36.8        | 261.3                       | 0.75           | 0.72                      | 0.81                   | 41.5                   |
| All<br>Vehic | les      | 3440                            | 77       | 4078                            | 2.2        | 0.828               | 28.9         | LOS C                        | 36.8        | 261.3                       | 0.79           | 0.75                      | 0.84                   | 39.7                   |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

11 Level of Service is worse than the Level of Service Target specified in the Parameter Settings dialog.

## Site: 601 [Great Western Highway x O'Connell Street x French Street 2026+DEV PM (Site Folder: Future - 2026 + DEV)]

New Site

Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time) Variable Sequence Analysis applied. The results are given for the selected output sequence. Design Life Analysis (Final Year): Results for 6 years

#### Timings based on settings in the Site Phasing & Timing dialog (Demand & Sensitivity Analysis overrides) Phase Times determined by the program Phase Sequence: TCS Reference Phase: Phase A Input Phase Sequence: A, B\*, C\*, D, E, E1\*, E2\* Output Phase Sequence: A, D, E, E2\* (\* Variable Phase)

| Vehi         | cle M   | ovemen                          | t Perfor | mance                           |     |                     |      |                     |      |                             |              |                           |                        |                        |
|--------------|---------|---------------------------------|----------|---------------------------------|-----|---------------------|------|---------------------|------|-----------------------------|--------------|---------------------------|------------------------|------------------------|
| Mov<br>ID    | Turn    | INP<br>VOLU<br>[ Total<br>veh/h |          | DEM/<br>FLO<br>[ Total<br>veh/h |     | Deg.<br>Satn<br>v/c |      | Level of<br>Service |      | ACK OF<br>EUE<br>Dist]<br>m | Prop.<br>Que | Effective<br>Stop<br>Rate | Aver.<br>No.<br>Cycles | Aver.<br>Speed<br>km/h |
| South        | n: O'C  | onnell Str                      |          |                                 |     |                     |      |                     |      |                             |              |                           |                        |                        |
| 1            | L2      | 63                              | 4        | 74                              | 6.4 | 0.166               | 39.8 | LOS C               | 3.7  | 27.4                        | 0.77         | 0.72                      | 0.77                   | 31.8                   |
| 2            | T1      | 17                              | 0        | 20                              | 0.0 | 0.830               | 40.2 | LOS C               | 15.0 | 108.7                       | 0.84         | 0.79                      | 0.91                   | 28.2                   |
| 3            | R2      | 200                             | 8        | 237                             | 4.0 | *0.830              | 59.7 | LOS E <sup>11</sup> | 15.0 | 108.7                       | 0.99         | 0.95                      | 1.20                   | 25.5                   |
| Appro        | oach    | 280                             | 12       | 331                             | 4.3 | 0.830               | 54.1 | LOS D               | 15.0 | 108.7                       | 0.93         | 0.89                      | 1.09                   | 26.8                   |
| East:        | Great   | Western                         | Highway  | ý                               |     |                     |      |                     |      |                             |              |                           |                        |                        |
| 4            | L2      | 217                             | 9        | 257                             | 4.1 | 0.271               | 22.3 | LOS B               | 8.2  | 59.5                        | 0.59         | 0.74                      | 0.59                   | 38.6                   |
| 5            | T1      | 1220                            | 25       | 1446                            | 2.0 | 0.753               | 23.1 | LOS B               | 33.9 | 241.5                       | 0.82         | 0.75                      | 0.82                   | 43.5                   |
| 6            | R2      | 73                              | 0        | 87                              | 0.0 | <b>*</b> 0.799      | 73.1 | LOS F <sup>11</sup> | 5.6  | 38.9                        | 1.00         | 0.89                      | 1.29                   | 26.0                   |
| Appro        | oach    | 1510                            | 34       | 1790                            | 2.3 | 0.799               | 25.4 | LOS B               | 33.9 | 241.5                       | 0.80         | 0.76                      | 0.81                   | 41.5                   |
| North        | n: Fren | ch Street                       |          |                                 |     |                     |      |                     |      |                             |              |                           |                        |                        |
| 7            | L2      | 41                              | 1        | 48                              | 2.4 | 0.374               | 47.6 | LOS D               | 6.8  | 48.6                        | 0.88         | 0.77                      | 0.88                   | 32.1                   |
| 8            | T1      | 18                              | 0        | 21                              | 0.0 | 0.374               | 41.3 | LOS C               | 6.8  | 48.6                        | 0.88         | 0.77                      | 0.88                   | 28.0                   |
| 9            | R2      | 58                              | 1        | 69                              | 1.7 | 0.374               | 45.9 | LOS D               | 6.8  | 48.6                        | 0.88         | 0.77                      | 0.88                   | 32.2                   |
| Appro        | oach    | 117                             | 2        | 139                             | 1.7 | 0.374               | 45.8 | LOS D               | 6.8  | 48.6                        | 0.88         | 0.77                      | 0.88                   | 31.6                   |
| West         | : Grea  | t Westerr                       | n Highwa | у                               |     |                     |      |                     |      |                             |              |                           |                        |                        |
| 10           | L2      | 19                              | 1        | 23                              | 5.3 | 0.774               | 26.2 | LOS B               | 15.6 | 111.0                       | 0.63         | 0.60                      | 0.68                   | 41.2                   |
| 11           | T1      | 1441                            | 24       | 1708                            | 1.7 | *0.829              | 24.4 | LOS B               | 36.8 | 261.5                       | 0.74         | 0.71                      | 0.79                   | 43.0                   |
| 12           | R2      | 88                              | 4        | 104                             | 4.6 | 0.770               | 70.4 | LOS E <sup>11</sup> | 6.5  | 47.5                        | 1.00         | 0.88                      | 1.22                   | 23.5                   |
| Appro        | oach    | 1548                            | 29       | 1835                            | 1.9 | 0.829               | 27.0 | LOS B               | 36.8 | 261.5                       | 0.75         | 0.72                      | 0.82                   | 41.4                   |
| All<br>Vehic | les     | 3455                            | 77       | 4094                            | 2.2 | 0.830               | 29.1 | LOS C               | 36.8 | 261.5                       | 0.79         | 0.75                      | 0.84                   | 39.6                   |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

11 Level of Service is worse than the Level of Service Target specified in the Parameter Settings dialog.

## Site: 801 [Great Western Highway x O'Connell Street x French Street 2030 PM (Site Folder: Future - 2030)]

New Site

Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 140 seconds (Site User-Given Cycle Time) Variable Sequence Analysis applied. The results are given for the selected output sequence. Design Life Analysis (Final Year): Results for 10 years

#### Timings based on settings in the Site Phasing & Timing dialog (Demand & Sensitivity Analysis overrides) Phase Times determined by the program Phase Sequence: TCS Reference Phase: Phase A Input Phase Sequence: A, B\*, C\*, D, E, E1\*, E2\* Output Phase Sequence: A, D, E, E2\* (\* Variable Phase)

| Vehi         | cle M   | ovemen                          | t Perfor | rmance                          |     |                     |      |                     |      |                             |                |                           |                        |                        |
|--------------|---------|---------------------------------|----------|---------------------------------|-----|---------------------|------|---------------------|------|-----------------------------|----------------|---------------------------|------------------------|------------------------|
| Mov<br>ID    | Turn    | INP<br>VOLU<br>[ Total<br>veh/h |          | DEM/<br>FLO<br>[ Total<br>veh/h |     | Deg.<br>Satn<br>v/c |      | Level of<br>Service |      | ACK OF<br>EUE<br>Dist]<br>m | Prop.  <br>Que | Effective<br>Stop<br>Rate | Aver.<br>No.<br>Cycles | Aver.<br>Speed<br>km/h |
| Sout         | n: O'C  | onnell Str                      | eet      |                                 |     |                     |      |                     |      |                             |                |                           |                        |                        |
| 1            | L2      | 55                              | 4        | 71                              | 7.3 | 0.180               | 46.8 | LOS D               | 4.7  | 34.3                        | 0.79           | 0.72                      | 0.79                   | 29.5                   |
| 2            | T1      | 17                              | 0        | 22                              | 0.0 | *0.902              | 41.4 | LOS C               | 20.0 | 144.7                       | 0.80           | 0.73                      | 0.81                   | 28.0                   |
| 3            | R2      | 198                             | 8        | 254                             | 4.0 | 0.902               | 78.9 | LOS F <sup>11</sup> | 20.0 | 144.7                       | 1.00           | 1.02                      | 1.33                   | 21.7                   |
| Appr         | oach    | 270                             | 12       | 346                             | 4.4 | 0.902               | 70.0 | LOS E <sup>11</sup> | 20.0 | 144.7                       | 0.95           | 0.94                      | 1.19                   | 23.3                   |
| East:        | Great   | Western                         | Highway  | y                               |     |                     |      |                     |      |                             |                |                           |                        |                        |
| 4            | L2      | 216                             | 9        | 277                             | 4.2 | 0.283               | 23.8 | LOS B               | 10.0 | 72.6                        | 0.58           | 0.74                      | 0.58                   | 37.8                   |
| 5            | T1      | 1220                            | 25       | 1565                            | 2.0 | 0.820               | 26.1 | LOS B               | 40.7 | 289.7                       | 0.84           | 0.77                      | 0.84                   | 42.0                   |
| 6            | R2      | 73                              | 0        | 94                              | 0.0 | <b>*</b> 0.883      | 88.3 | LOS F <sup>11</sup> | 7.2  | 50.5                        | 1.00           | 0.95                      | 1.42                   | 23.5                   |
| Appr         | oach    | 1509                            | 34       | 1936                            | 2.3 | 0.883               | 28.8 | LOS C               | 40.7 | 289.7                       | 0.81           | 0.77                      | 0.83                   | 39.9                   |
| North        | n: Fren | ch Street                       |          |                                 |     |                     |      |                     |      |                             |                |                           |                        |                        |
| 7            | L2      | 40                              | 1        | 51                              | 2.5 | 0.396               | 53.9 | LOS D               | 8.5  | 60.5                        | 0.88           | 0.78                      | 0.88                   | 30.5                   |
| 8            | T1      | 18                              | 0        | 23                              | 0.0 | 0.396               | 47.3 | LOS D               | 8.5  | 60.5                        | 0.88           | 0.78                      | 0.88                   | 26.4                   |
| 9            | R2      | 58                              | 1        | 74                              | 1.7 | 0.396               | 51.9 | LOS D               | 8.5  | 60.5                        | 0.88           | 0.78                      | 0.88                   | 30.6                   |
| Appr         | oach    | 116                             | 2        | 149                             | 1.7 | 0.396               | 51.9 | LOS D               | 8.5  | 60.5                        | 0.88           | 0.78                      | 0.88                   | 30.0                   |
| West         | : Grea  | t Westerr                       | n Highwa | ıy                              |     |                     |      |                     |      |                             |                |                           |                        |                        |
| 10           | L2      | 19                              | 1        | 24                              | 5.3 | 0.827               | 33.2 | LOS C               | 19.6 | 139.4                       | 0.61           | 0.63                      | 0.71                   | 38.2                   |
| 11           | T1      | 1441                            | 24       | 1849                            | 1.7 | *0.886              | 33.6 | LOS C               | 51.8 | 368.1                       | 0.76           | 0.76                      | 0.85                   | 38.8                   |
| 12           | R2      | 85                              | 4        | 109                             | 4.7 | 0.850               | 84.5 | LOS F <sup>11</sup> | 8.2  | 59.7                        | 1.00           | 0.93                      | 1.33                   | 21.0                   |
| Appr         | oach    | 1545                            | 29       | 1982                            | 1.9 | 0.886               | 36.4 | LOS C               | 51.8 | 368.1                       | 0.77           | 0.77                      | 0.88                   | 37.4                   |
| All<br>Vehic | les     | 3440                            | 77       | 4414                            | 2.2 | 0.902               | 36.2 | LOS C               | 51.8 | 368.1                       | 0.80           | 0.79                      | 0.88                   | 36.7                   |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

11 Level of Service is worse than the Level of Service Target specified in the Parameter Settings dialog.

## Site: 1001 [Great Western Highway x O'Connell Street x French Street 2030+DEV PM (Site Folder: Future - 2030 +DEV)]

New Site

Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 140 seconds (Site User-Given Cycle Time) Variable Sequence Analysis applied. The results are given for the selected output sequence. Design Life Analysis (Final Year): Results for 10 years

#### Timings based on settings in the Site Phasing & Timing dialog (Demand & Sensitivity Analysis overrides) Phase Times determined by the program Phase Sequence: TCS Reference Phase: Phase A Input Phase Sequence: A, B\*, C\*, D, E, E1\*, E2\* Output Phase Sequence: A, D, E, E2\* (\* Variable Phase)

| Vehi         | cle M   | ovemen                          | t Perfor | mance                           |     |                     |      |                     |      |                             |              |                           |                        |                        |
|--------------|---------|---------------------------------|----------|---------------------------------|-----|---------------------|------|---------------------|------|-----------------------------|--------------|---------------------------|------------------------|------------------------|
| Mov<br>ID    | Turn    | INP<br>VOLL<br>[ Total<br>veh/h |          | DEM/<br>FLO<br>[ Total<br>veh/h |     | Deg.<br>Satn<br>v/c |      | Level of<br>Service |      | ACK OF<br>EUE<br>Dist]<br>m | Prop.<br>Que | Effective<br>Stop<br>Rate | Aver.<br>No.<br>Cycles | Aver.<br>Speed<br>km/h |
| Sout         | n: O'C  | onnell Str                      |          |                                 |     |                     |      |                     |      |                             |              |                           |                        |                        |
| 1            | L2      | 73                              | 4        | 90                              | 5.7 | 0.181               | 42.6 | LOS D               | 5.0  | 36.4                        | 0.75         | 0.72                      | 0.75                   | 31.0                   |
| 2            | T1      | 17                              | 0        | 22                              | 0.0 | *0.905              | 49.5 | LOS D               | 21.0 | 151.6                       | 0.84         | 0.83                      | 0.96                   | 25.9                   |
| 3            | R2      | 203                             | 8        | 259                             | 4.0 | 0.905               | 78.6 | LOS F <sup>11</sup> | 21.0 | 151.6                       | 0.99         | 1.03                      | 1.33                   | 21.8                   |
| Appr         | oach    | 293                             | 12       | 371                             | 4.2 | 0.905               | 68.2 | LOS E <sup>11</sup> | 21.0 | 151.6                       | 0.93         | 0.94                      | 1.17                   | 23.7                   |
| East:        | Great   | Western                         | Highway  | Ý                               |     |                     |      |                     |      |                             |              |                           |                        |                        |
| 4            | L2      | 218                             | 9        | 279                             | 4.1 | 0.297               | 25.6 | LOS B               | 10.6 | 76.7                        | 0.61         | 0.75                      | 0.61                   | 36.9                   |
| 5            | T1      | 1220                            | 25       | 1565                            | 2.0 | 0.859               | 32.8 | LOS C               | 45.6 | 324.8                       | 0.87         | 0.83                      | 0.92                   | 39.0                   |
| 6            | R2      | 73                              | 0        | 94                              | 0.0 | <b>*</b> 0.883      | 88.3 | LOS F <sup>11</sup> | 7.2  | 50.5                        | 1.00         | 0.95                      | 1.42                   | 23.5                   |
| Appr         | oach    | 1511                            | 34       | 1938                            | 2.3 | 0.883               | 34.4 | LOS C               | 45.6 | 324.8                       | 0.84         | 0.83                      | 0.90                   | 37.5                   |
| North        | n: Fren | ch Street                       |          |                                 |     |                     |      |                     |      |                             |              |                           |                        |                        |
| 7            | L2      | 40                              | 1        | 51                              | 2.5 | 0.383               | 52.1 | LOS D               | 8.4  | 59.8                        | 0.87         | 0.78                      | 0.87                   | 31.0                   |
| 8            | T1      | 19                              | 0        | 24                              | 0.0 | 0.383               | 45.6 | LOS D               | 8.4  | 59.8                        | 0.87         | 0.78                      | 0.87                   | 26.9                   |
| 9            | R2      | 58                              | 1        | 74                              | 1.7 | 0.383               | 50.1 | LOS D               | 8.4  | 59.8                        | 0.87         | 0.78                      | 0.87                   | 31.1                   |
| Appr         | oach    | 117                             | 2        | 150                             | 1.7 | 0.383               | 50.1 | LOS D               | 8.4  | 59.8                        | 0.87         | 0.78                      | 0.87                   | 30.4                   |
| West         | : Grea  | t Westerr                       | n Highwa | у                               |     |                     |      |                     |      |                             |              |                           |                        |                        |
| 10           | L2      | 19                              | 1        | 24                              | 5.3 | 0.854               | 38.9 | LOS C               | 22.0 | 156.3                       | 0.64         | 0.68                      | 0.78                   | 36.0                   |
| 11           | T1      | 1441                            | 24       | 1849                            | 1.7 | *0.915              | 41.8 | LOS C               | 57.5 | 408.1                       | 0.78         | 0.83                      | 0.93                   | 35.7                   |
| 12           | R2      | 95                              | 4        | 120                             | 4.3 | 0.845               | 83.4 | LOS F <sup>11</sup> | 8.9  | 64.9                        | 1.00         | 0.92                      | 1.30                   | 21.2                   |
| Appr         | oach    | 1555                            | 29       | 1993                            | 1.9 | 0.915               | 44.3 | LOS D               | 57.5 | 408.1                       | 0.79         | 0.83                      | 0.95                   | 34.6                   |
| All<br>Vehic | les     | 3476                            | 77       | 4452                            | 2.2 | 0.915               | 42.2 | LOS C               | 57.5 | 408.1                       | 0.83         | 0.84                      | 0.94                   | 34.5                   |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

11 Level of Service is worse than the Level of Service Target specified in the Parameter Settings dialog.

# APPENDIX F-2

SIDRA Modelling Outputs Great Western Highway/Bringelly Road

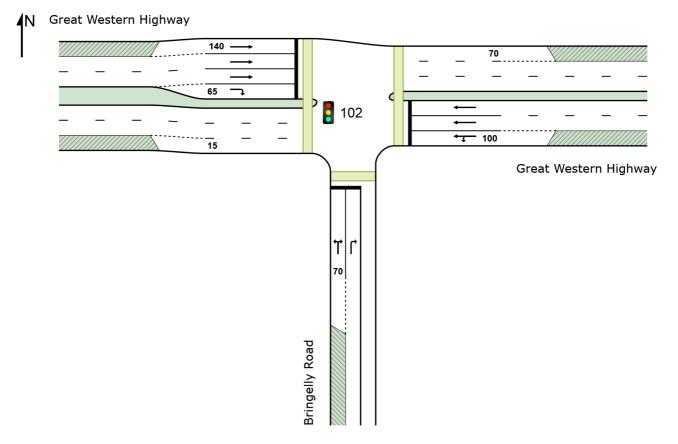
### Site: 102 [Great Western Highway x Bringelly Road Exsting AM (Site Folder: Exisitng (2020))]

New Site Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Timings based on settings in the Site Phasing & Timing dialog Phase Times determined by the program Phase Sequence: Leading Right Turn Reference Phase: Phase A Input Phase Sequence: A, B, C Output Phase Sequence: A, B, C

### Site Layout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



### Site: 102 [Great Western Highway x Bringelly Road Exsting AM (Site Folder: Exisitng (2020))]

New Site Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing & Timing dialog Phase Times determined by the program Phase Sequence: Leading Right Turn Reference Phase: Phase A Input Phase Sequence: A, B, C Output Phase Sequence: A, B, C

| Vehi         | cle M    | ovemen           | t Perfor      | mance            |           |                |      |                     |               |               |                |                   |              |                |
|--------------|----------|------------------|---------------|------------------|-----------|----------------|------|---------------------|---------------|---------------|----------------|-------------------|--------------|----------------|
| Mov<br>ID    | Turn     | INP<br>VOLL      |               | DEM.<br>FLO      |           | Deg.<br>Satn   |      | Level of<br>Service |               | ACK OF<br>EUE | Prop.  <br>Que | Effective<br>Stop | Aver.<br>No. | Aver.<br>Speed |
|              |          | [ Total<br>veh/h | HV ]<br>veh/h | [ Total<br>veh/h | HV ]<br>% | v/c            | sec  |                     | [ Veh.<br>veh | Dist ]<br>m   |                | Rate              | Cycles       | km/h           |
| Sout         | n: Bring | gelly Roa        | d             |                  |           |                |      |                     |               |               |                |                   |              |                |
| 1            | L2       | 177              | 10            | 186              | 5.6       | 0.661          | 52.5 | LOS D               | 14.6          | 106.1         | 0.96           | 0.84              | 0.96         | 31.8           |
| 3            | R2       | 299              | 9             | 315              | 3.0       | <b>*</b> 0.661 | 53.8 | LOS D               | 14.6          | 106.1         | 0.98           | 0.83              | 0.98         | 26.0           |
| Appr         | oach     | 476              | 19            | 501              | 4.0       | 0.661          | 53.3 | LOS D               | 14.6          | 106.1         | 0.97           | 0.83              | 0.97         | 28.3           |
| East:        | Great    | Western          | Highway       | /                |           |                |      |                     |               |               |                |                   |              |                |
| 4            | L2       | 167              | 4             | 176              | 2.4       | 0.199          | 24.3 | LOS B               | 5.8           | 41.3          | 0.61           | 0.73              | 0.61         | 37.0           |
| 5            | T1       | 1163             | 40            | 1224             | 3.4       | <b>*</b> 0.674 | 25.1 | LOS B               | 27.6          | 198.6         | 0.82           | 0.74              | 0.82         | 45.4           |
| Appr         | oach     | 1330             | 44            | 1400             | 3.3       | 0.674          | 25.0 | LOS B               | 27.6          | 198.6         | 0.79           | 0.74              | 0.79         | 44.7           |
| West         | : Grea   | t Westerr        | n Highwa      | у                |           |                |      |                     |               |               |                |                   |              |                |
| 11           | T1       | 1151             | 47            | 1212             | 4.1       | 0.375          | 7.3  | LOS A               | 11.5          | 83.2          | 0.42           | 0.37              | 0.42         | 55.0           |
| 12           | R2       | 185              | 10            | 195              | 5.4       | <b>*</b> 0.459 | 40.6 | LOS C               | 9.8           | 71.6          | 0.91           | 0.92              | 0.91         | 35.1           |
| Appr         | oach     | 1336             | 57            | 1406             | 4.3       | 0.459          | 11.9 | LOS A               | 11.5          | 83.2          | 0.48           | 0.45              | 0.48         | 51.8           |
| All<br>Vehic | cles     | 3142             | 120           | 3307             | 3.8       | 0.674          | 23.7 | LOS B               | 27.6          | 198.6         | 0.69           | 0.63              | 0.69         | 44.8           |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

### Site: 302 [Great Western Highway x Bringelly Road 2026 AM (Site Folder: Future - 2026)]

New Site

Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time) Design Life Analysis (Final Year): Results for 6 years

Timings based on settings in the Site Phasing & Timing dialog (Demand & Sensitivity Analysis overrides) Phase Times determined by the program Phase Sequence: Leading Right Turn Reference Phase: Phase A Input Phase Sequence: A, B, C Output Phase Sequence: A, B, C

| Vehi         | cle M    | ovemen           | t Perfor      | mance            |           |                |      |                     |               |               |                |                  |              |                |
|--------------|----------|------------------|---------------|------------------|-----------|----------------|------|---------------------|---------------|---------------|----------------|------------------|--------------|----------------|
| Mov<br>ID    | Turn     | INP<br>VOLL      |               | DEM<br>FLO       |           | Deg.<br>Satn   |      | Level of<br>Service |               | ACK OF<br>EUE | Prop. E<br>Que | ffective<br>Stop | Aver.<br>No. | Aver.<br>Speed |
|              |          | [ Total<br>veh/h | HV ]<br>veh/h | [ Total<br>veh/h | HV ]<br>% | v/c            | sec  |                     | [ Veh.<br>veh | Dist ]<br>m   |                | Rate             | Cycles       | km/h           |
| Sout         | h: Bring | gelly Roa        | d             |                  |           |                |      |                     |               |               |                |                  |              |                |
| 1            | L2       | 177              | 10            | 210              | 5.6       | 0.744          | 55.5 | LOS D               | 17.2          | 125.6         | 0.99           | 0.87             | 1.04         | 31.0           |
| 3            | R2       | 299              | 9             | 354              | 3.0       | *0.744         | 56.5 | LOS E <sup>11</sup> | 17.2          | 125.6         | 1.00           | 0.87             | 1.06         | 25.3           |
| Appr         | oach     | 476              | 19            | 564              | 4.0       | 0.744          | 56.1 | LOS D               | 17.2          | 125.6         | 0.99           | 0.87             | 1.05         | 27.6           |
| East:        | Great    | Western          | Highway       | /                |           |                |      |                     |               |               |                |                  |              |                |
| 4            | L2       | 167              | 4             | 198              | 2.4       | 0.221          | 24.0 | LOS B               | 6.5           | 46.4          | 0.61           | 0.74             | 0.61         | 37.2           |
| 5            | T1       | 1163             | 40            | 1379             | 3.4       | <b>*</b> 0.760 | 25.9 | LOS B               | 33.5          | 241.7         | 0.86           | 0.78             | 0.86         | 45.1           |
| Appr         | oach     | 1330             | 44            | 1577             | 3.3       | 0.760          | 25.6 | LOS B               | 33.5          | 241.7         | 0.83           | 0.78             | 0.83         | 44.4           |
| West         | : Grea   | t Westerr        | n Highwa      | у                |           |                |      |                     |               |               |                |                  |              |                |
| 11           | T1       | 1151             | 47            | 1364             | 4.1       | 0.423          | 7.7  | LOS A               | 13.6          | 98.3          | 0.43           | 0.39             | 0.43         | 54.8           |
| 12           | R2       | 185              | 10            | 219              | 5.4       | <b>*</b> 0.563 | 48.7 | LOS D               | 11.3          | 83.0          | 0.95           | 0.98             | 0.95         | 32.5           |
| Appr         | oach     | 1336             | 57            | 1584             | 4.3       | 0.563          | 13.4 | LOS A               | 13.6          | 98.3          | 0.50           | 0.47             | 0.50         | 51.0           |
| All<br>Vehic | cles     | 3142             | 120           | 3725             | 3.8       | 0.760          | 25.0 | LOS B               | 33.5          | 241.7         | 0.72           | 0.66             | 0.73         | 44.2           |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

11 Level of Service is worse than the Level of Service Target specified in the Parameter Settings dialog.

# Site: 502 [Great Western Highway x Bringelly Road 2026+DEV AM (Site Folder: Future - 2026 + DEV)]

New Site

Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time) Design Life Analysis (Final Year): Results for 6 years

Timings based on settings in the Site Phasing & Timing dialog (Demand & Sensitivity Analysis overrides) Phase Times determined by the program Phase Sequence: Leading Right Turn Reference Phase: Phase A Input Phase Sequence: A, B, C Output Phase Sequence: A, B, C

| Vehi         | cle M    | ovemen           | t Perfor      | mance            |           |                |      |                     |               |               |                |                   |        |                |
|--------------|----------|------------------|---------------|------------------|-----------|----------------|------|---------------------|---------------|---------------|----------------|-------------------|--------|----------------|
| Mov<br>ID    | Turn     | INF<br>VOLL      | JMES          | DEM.<br>FLO      | WS        | Deg.<br>Satn   |      | Level of<br>Service | QU            | ACK OF<br>EUE | Prop. E<br>Que | Effective<br>Stop |        | Aver.<br>Speed |
|              |          | [ Total<br>veh/h | HV ]<br>veh/h | [ Total<br>veh/h | HV ]<br>% | v/c            | sec  |                     | [ Veh.<br>veh | Dist ]<br>m   |                | Rate              | Cycles | km/h           |
| South        | n: Bring | gelly Roa        | d             |                  |           |                |      |                     |               |               |                |                   |        |                |
| 1            | L2       | 177              | 10            | 210              | 5.6       | 0.744          | 55.5 | LOS D               | 17.2          | 125.6         | 0.99           | 0.87              | 1.04   | 31.0           |
| 3            | R2       | 299              | 9             | 354              | 3.0       | *0.744         | 56.5 | LOS E <sup>11</sup> | 17.2          | 125.6         | 1.00           | 0.87              | 1.06   | 25.3           |
| Appro        | oach     | 476              | 19            | 564              | 4.0       | 0.744          | 56.2 | LOS D               | 17.2          | 125.6         | 0.99           | 0.87              | 1.05   | 27.6           |
| East:        | Great    | Western          | Highway       | Y                |           |                |      |                     |               |               |                |                   |        |                |
| 4            | L2       | 167              | 4             | 198              | 2.4       | 0.217          | 23.4 | LOS B               | 6.4           | 45.6          | 0.60           | 0.74              | 0.60   | 37.6           |
| 5            | T1       | 1167             | 40            | 1383             | 3.4       | <b>*</b> 0.749 | 25.1 | LOS B               | 33.1          | 238.2         | 0.85           | 0.77              | 0.85   | 45.4           |
| Appro        | oach     | 1334             | 44            | 1581             | 3.3       | 0.749          | 24.8 | LOS B               | 33.1          | 238.2         | 0.82           | 0.77              | 0.82   | 44.8           |
| West         | : Grea   | t Westerr        | n Highwa      | у                |           |                |      |                     |               |               |                |                   |        |                |
| 11           | T1       | 1168             | 47            | 1382             | 4.0       | 0.428          | 7.7  | LOS A               | 13.8          | 100.1         | 0.44           | 0.39              | 0.44   | 54.8           |
| 12           | R2       | 185              | 10            | 219              | 5.4       | <b>*</b> 0.583 | 49.0 | LOS D               | 11.4          | 83.8          | 0.96           | 0.98              | 0.96   | 32.4           |
| Appro        | oach     | 1353             | 57            | 1602             | 4.2       | 0.583          | 13.4 | LOS A               | 13.8          | 100.1         | 0.51           | 0.47              | 0.51   | 51.0           |
| All<br>Vehic | les      | 3163             | 120           | 3747             | 3.8       | 0.749          | 24.7 | LOS B               | 33.1          | 238.2         | 0.71           | 0.66              | 0.72   | 44.4           |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

11 Level of Service is worse than the Level of Service Target specified in the Parameter Settings dialog.

### Site: 702 [Great Western Highway x Bringelly Road 2030 AM (Site Folder: Future - 2030)]

New Site

Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time) Design Life Analysis (Final Year): Results for 10 years

Timings based on settings in the Site Phasing & Timing dialog (Demand & Sensitivity Analysis overrides) Phase Times determined by the program Phase Sequence: Leading Right Turn Reference Phase: Phase A Input Phase Sequence: A, B, C Output Phase Sequence: A, B, C

| Vehicle Movement Performance |                             |                  |               |                  |           |                |                                 |                     |                      |             |                             |      |              |                |
|------------------------------|-----------------------------|------------------|---------------|------------------|-----------|----------------|---------------------------------|---------------------|----------------------|-------------|-----------------------------|------|--------------|----------------|
| Mov<br>ID                    | Turn                        | INPUT<br>VOLUMES |               | DEMAND<br>FLOWS  |           | Deg.<br>Satn   | Aver. Level of<br>Delay Service |                     | 95% BACK OF<br>QUEUE |             | Prop. Effective<br>Que Stop |      | Aver.<br>No. | Aver.<br>Speed |
|                              |                             | [ Total<br>veh/h | HV ]<br>veh/h | [ Total<br>veh/h | HV ]<br>% | v/c            | sec                             |                     | [ Veh.<br>veh        | Dist ]<br>m |                             | Rate | Cycles       | km/h           |
| South: Bringelly Road        |                             |                  |               |                  |           |                |                                 |                     |                      |             |                             |      |              |                |
| 1                            | L2                          | 177              | 10            | 227              | 5.6       | 0.826          | 60.5                            | LOS E <sup>11</sup> | 19.5                 | 141.9       | 1.00                        | 0.92 | 1.15         | 29.8           |
| 3                            | R2                          | 299              | 9             | 384              | 3.0       | *0.826         | 61.3                            | LOS E <sup>11</sup> | 19.5                 | 141.9       | 1.00                        | 0.92 | 1.17         | 24.1           |
| Appr                         | oach                        | 476              | 19            | 611              | 4.0       | 0.826          | 61.0                            | LOS E <sup>11</sup> | 19.5                 | 141.9       | 1.00                        | 0.92 | 1.16         | 26.4           |
| East                         | East: Great Western Highway |                  |               |                  |           |                |                                 |                     |                      |             |                             |      |              |                |
| 4                            | L2                          | 167              | 4             | 214              | 2.4       | 0.235          | 23.6                            | LOS B               | 7.0                  | 49.9        | 0.60                        | 0.74 | 0.60         | 37.4           |
| 5                            | T1                          | 1163             | 40            | 1492             | 3.4       | <b>*</b> 0.819 | 28.0                            | LOS B               | 39.2                 | 282.3       | 0.89                        | 0.83 | 0.91         | 44.2           |
| Appr                         | oach                        | 1330             | 44            | 1707             | 3.3       | 0.819          | 27.4                            | LOS B               | 39.2                 | 282.3       | 0.85                        | 0.82 | 0.87         | 43.6           |
| West                         | : Grea                      | t Westerr        | n Highwa      | у                |           |                |                                 |                     |                      |             |                             |      |              |                |
| 11                           | T1                          | 1151             | 47            | 1477             | 4.1       | 0.458          | 8.0                             | LOS A               | 15.2                 | 110.3       | 0.45                        | 0.40 | 0.45         | 54.6           |
| 12                           | R2                          | 185              | 10            | 237              | 5.4       | <b>*</b> 0.652 | 53.5                            | LOS D               | 12.5                 | 91.8        | 0.97                        | 1.00 | 0.97         | 31.2           |
| Appr                         | oach                        | 1336             | 57            | 1714             | 4.3       | 0.652          | 14.3                            | LOS A               | 15.2                 | 110.3       | 0.52                        | 0.49 | 0.52         | 50.5           |
| All<br>Vehio                 | cles                        | 3142             | 120           | 4032             | 3.8       | 0.826          | 26.9                            | LOS B               | 39.2                 | 282.3       | 0.73                        | 0.69 | 0.77         | 43.4           |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

11 Level of Service is worse than the Level of Service Target specified in the Parameter Settings dialog.

# Site: 902 [Great Western Highway x Bringelly Road 2030+DEV AM (Site Folder: Future - 2030 +DEV)]

New Site

Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time) Design Life Analysis (Final Year): Results for 10 years

Timings based on settings in the Site Phasing & Timing dialog (Demand & Sensitivity Analysis overrides) Phase Times determined by the program Phase Sequence: Leading Right Turn Reference Phase: Phase A Input Phase Sequence: A, B, C Output Phase Sequence: A, B, C

| Vehicle Movement Performance |        |                  |               |                  |           |                |                                 |                     |                      |             |                             |      |              |                |
|------------------------------|--------|------------------|---------------|------------------|-----------|----------------|---------------------------------|---------------------|----------------------|-------------|-----------------------------|------|--------------|----------------|
| Mov<br>ID                    | Turn   | INPUT<br>VOLUMES |               | DEMAND<br>FLOWS  |           | Deg.<br>Satn   | Aver. Level of<br>Delay Service |                     | 95% BACK OF<br>QUEUE |             | Prop. Effective<br>Que Stop |      | Aver.<br>No. | Aver.<br>Speed |
|                              |        | [ Total<br>veh/h | HV ]<br>veh/h | [ Total<br>veh/h | HV ]<br>% | v/c            | sec                             |                     | [ Veh.<br>veh        | Dist ]<br>m |                             | Rate | Cycles       | km/h           |
| South: Bringelly Road        |        |                  |               |                  |           |                |                                 |                     |                      |             |                             |      |              |                |
| 1                            | L2     | 177              | 10            | 227              | 5.6       | 0.826          | 60.5                            | LOS E <sup>11</sup> | 19.5                 | 141.9       | 1.00                        | 0.92 | 1.15         | 29.8           |
| 3                            | R2     | 299              | 9             | 384              | 3.0       | *0.826         | 61.2                            | LOS E <sup>11</sup> | 19.5                 | 141.9       | 1.00                        | 0.92 | 1.17         | 24.1           |
| Appro                        | bach   | 476              | 19            | 611              | 4.0       | 0.826          | 61.0                            | LOS E <sup>11</sup> | 19.5                 | 141.9       | 1.00                        | 0.92 | 1.16         | 26.4           |
| East:                        | Great  | Western          | Highway       | /                |           |                |                                 |                     |                      |             |                             |      |              |                |
| 4                            | L2     | 167              | 4             | 214              | 2.4       | 0.235          | 23.6                            | LOS B               | 7.0                  | 49.9        | 0.60                        | 0.74 | 0.60         | 37.4           |
| 5                            | T1     | 1173             | 40            | 1503             | 3.4       | <b>*</b> 0.825 | 28.6                            | LOS C               | 40.0                 | 288.2       | 0.89                        | 0.84 | 0.92         | 43.9           |
| Appro                        | bach   | 1340             | 44            | 1717             | 3.3       | 0.825          | 28.0                            | LOS B               | 40.0                 | 288.2       | 0.86                        | 0.83 | 0.88         | 43.4           |
| West                         | : Grea | t Westerr        | n Highwa      | у                |           |                |                                 |                     |                      |             |                             |      |              |                |
| 11                           | T1     | 1190             | 47            | 1518             | 4.0       | 0.480          | 8.1                             | LOS A               | 16.4                 | 118.4       | 0.45                        | 0.41 | 0.45         | 54.6           |
| 12                           | R2     | 185              | 10            | 237              | 5.4       | <b>*</b> 0.654 | 53.8                            | LOS D               | 12.5                 | 91.8        | 0.98                        | 1.00 | 0.98         | 31.1           |
| Appro                        | bach   | 1375             | 57            | 1755             | 4.2       | 0.654          | 14.3                            | LOS A               | 16.4                 | 118.4       | 0.52                        | 0.49 | 0.52         | 50.5           |
| All<br>Vehic                 | les    | 3191             | 120           | 4083             | 3.8       | 0.826          | 27.0                            | LOS B               | 40.0                 | 288.2       | 0.74                        | 0.70 | 0.77         | 43.3           |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

11 Level of Service is worse than the Level of Service Target specified in the Parameter Settings dialog.

### Site: 202 [Great Western Highway x Bringelly Road Exsting PM (Site Folder: Exisitng (2020))]

New Site Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing & Timing dialog Phase Times determined by the program Phase Sequence: Leading Right Turn Reference Phase: Phase A Input Phase Sequence: A, B, C Output Phase Sequence: A, B, C

| Vehicle Movement Performance |          |                  |               |                  |           |              |                                 |       |                      |             |                |                   |              |                |
|------------------------------|----------|------------------|---------------|------------------|-----------|--------------|---------------------------------|-------|----------------------|-------------|----------------|-------------------|--------------|----------------|
| Mov<br>ID                    | Turn     | INPUT<br>VOLUMES |               | DEMAND<br>FLOWS  |           | Deg.<br>Satn | Aver. Level of<br>Delay Service |       | 95% BACK OF<br>QUEUE |             | Prop. I<br>Que | Effective<br>Stop | Aver.<br>No. | Aver.<br>Speed |
|                              |          | [ Total<br>veh/h | HV ]<br>veh/h | [ Total<br>veh/h | HV ]<br>% | v/c          | sec                             |       | [ Veh.<br>veh        | Dist ]<br>m |                | Rate              | Cycles       | km/h           |
| Sout                         | h: Bring | gelly Roa        | d             |                  |           |              |                                 |       |                      |             |                |                   |              |                |
| 1                            | L2       | 165              | 5             | 174              | 3.0       | 0.639        | 49.8                            | LOS D | 15.7                 | 111.9       | 0.95           | 0.84              | 0.95         | 32.6           |
| 3                            | R2       | 379              | 6             | 399              | 1.6       | *0.639       | 50.0                            | LOS D | 15.7                 | 111.9       | 0.95           | 0.84              | 0.95         | 27.0           |
| Appr                         | oach     | 544              | 11            | 573              | 2.0       | 0.639        | 49.9                            | LOS D | 15.7                 | 111.9       | 0.95           | 0.84              | 0.95         | 28.9           |
| East:                        | Great    | Western          | Highway       | ý                |           |              |                                 |       |                      |             |                |                   |              |                |
| 4                            | L2       | 197              | 1             | 207              | 0.5       | 0.240        | 25.9                            | LOS B | 7.2                  | 50.5        | 0.64           | 0.75              | 0.64         | 36.3           |
| 5                            | T1       | 1098             | 30            | 1156             | 2.7       | *0.652       | 26.0                            | LOS B | 25.9                 | 185.4       | 0.82           | 0.74              | 0.82         | 45.0           |
| Appr                         | oach     | 1295             | 31            | 1363             | 2.4       | 0.652        | 26.0                            | LOS B | 25.9                 | 185.4       | 0.79           | 0.74              | 0.79         | 44.1           |
| West                         | : Grea   | t Westerr        | n Highwa      | y                |           |              |                                 |       |                      |             |                |                   |              |                |
| 11                           | T1       | 1181             | 22            | 1243             | 1.9       | 0.404        | 9.6                             | LOS A | 13.5                 | 96.3        | 0.48           | 0.42              | 0.48         | 53.6           |
| 12                           | R2       | 166              | 3             | 175              | 1.8       | *0.442       | 40.1                            | LOS C | 9.0                  | 63.8        | 0.92           | 0.88              | 0.92         | 35.4           |
| Appr                         | oach     | 1347             | 25            | 1418             | 1.9       | 0.442        | 13.4                            | LOS A | 13.5                 | 96.3        | 0.53           | 0.48              | 0.53         | 51.1           |
| All<br>Vehic                 | cles     | 3186             | 67            | 3354             | 2.1       | 0.652        | 24.7                            | LOS B | 25.9                 | 185.4       | 0.71           | 0.65              | 0.71         | 44.2           |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

### Site: 402 [Great Western Highway x Bringelly Road 2026 PM (Site Folder: Future - 2026)]

New Site

Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time) Design Life Analysis (Final Year): Results for 6 years

Timings based on settings in the Site Phasing & Timing dialog (Demand & Sensitivity Analysis overrides) Phase Times determined by the program Phase Sequence: Leading Right Turn Reference Phase: Phase A Input Phase Sequence: A, B, C Output Phase Sequence: A, B, C

| Vehi         | icle M  | ovemen           | t Perfor      | rmance           |           |                |      |                     |               |               |                |                  |              |                |
|--------------|---------|------------------|---------------|------------------|-----------|----------------|------|---------------------|---------------|---------------|----------------|------------------|--------------|----------------|
| Mov<br>ID    | Turn    |                  | PUT<br>JMES   | DEM.<br>FLO      |           | Deg.<br>Satn   |      | Level of<br>Service |               | ACK OF<br>EUE | Prop. E<br>Que | ffective<br>Stop | Aver.<br>No. | Aver.<br>Speed |
|              |         | [ Total<br>veh/h | HV ]<br>veh/h | [ Total<br>veh/h | HV ]<br>% | v/c            | sec  |                     | [ Veh.<br>veh | Dist ]<br>m   |                | Rate             | Cycles       | km/h           |
| Sout         | h: Brin | gelly Roa        | ıd            |                  |           |                |      |                     |               |               |                |                  |              |                |
| 1            | L2      | 165              | 5             | 196              | 3.0       | 0.730          | 52.0 | LOS D               | 18.1          | 129.3         | 0.97           | 0.86             | 1.00         | 32.0           |
| 3            | R2      | 379              | 6             | 449              | 1.6       | <b>*</b> 0.730 | 52.1 | LOS D               | 18.1          | 129.3         | 0.98           | 0.86             | 1.01         | 26.4           |
| Appr         | oach    | 544              | 11            | 645              | 2.0       | 0.730          | 52.1 | LOS D               | 18.1          | 129.3         | 0.98           | 0.86             | 1.01         | 28.3           |
| East         | : Great | Western          | Highway       | y                |           |                |      |                     |               |               |                |                  |              |                |
| 4            | L2      | 197              | 1             | 234              | 0.5       | 0.266          | 25.6 | LOS B               | 8.1           | 56.9          | 0.64           | 0.75             | 0.64         | 36.4           |
| 5            | T1      | 1098             | 30            | 1302             | 2.7       | <b>*</b> 0.739 | 26.7 | LOS B               | 31.5          | 225.8         | 0.86           | 0.78             | 0.86         | 44.7           |
| Appr         | oach    | 1295             | 31            | 1535             | 2.4       | 0.739          | 26.5 | LOS B               | 31.5          | 225.8         | 0.83           | 0.77             | 0.83         | 43.8           |
| West         | t: Grea | t Westerr        | n Highwa      | ıy               |           |                |      |                     |               |               |                |                  |              |                |
| 11           | T1      | 1181             | 22            | 1400             | 1.9       | 0.454          | 10.1 | LOS A               | 16.0          | 113.8         | 0.50           | 0.45             | 0.50         | 53.4           |
| 12           | R2      | 166              | 3             | 197              | 1.8       | <b>*</b> 0.551 | 49.2 | LOS D               | 10.4          | 73.9          | 0.96           | 0.96             | 0.96         | 32.5           |
| Appr         | oach    | 1347             | 25            | 1597             | 1.9       | 0.551          | 14.9 | LOS B               | 16.0          | 113.8         | 0.55           | 0.51             | 0.55         | 50.2           |
| All<br>Vehic | cles    | 3186             | 67            | 3777             | 2.1       | 0.739          | 26.0 | LOS B               | 31.5          | 225.8         | 0.74           | 0.68             | 0.74         | 43.6           |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

# Site: 602 [Great Western Highway x Bringelly Road 2026+DEV PM (Site Folder: Future - 2026 + DEV)]

New Site

Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time) Design Life Analysis (Final Year): Results for 6 years

Timings based on settings in the Site Phasing & Timing dialog (Demand & Sensitivity Analysis overrides) Phase Times determined by the program Phase Sequence: Leading Right Turn Reference Phase: Phase A Input Phase Sequence: A, B, C Output Phase Sequence: A, B, C

| Vehi         | cle M    | ovemen           | t Perfor      | mance            |           |                |      |                     |               |               |                |                   |              |                |
|--------------|----------|------------------|---------------|------------------|-----------|----------------|------|---------------------|---------------|---------------|----------------|-------------------|--------------|----------------|
| Mov<br>ID    | Turn     | INF<br>VOLL      |               | DEM.<br>FLO      |           | Deg.<br>Satn   |      | Level of<br>Service |               | ACK OF<br>EUE | Prop. E<br>Que | Effective<br>Stop | Aver.<br>No. | Aver.<br>Speed |
|              |          | [ Total<br>veh/h | HV ]<br>veh/h | [ Total<br>veh/h | HV ]<br>% | v/c            | sec  |                     | [ Veh.<br>veh | Dist ]<br>m   |                | Rate              | Cycles       | km/h           |
| South        | n: Bring | gelly Roa        | d             |                  |           |                |      |                     |               |               |                |                   |              |                |
| 1            | L2       | 165              | 5             | 196              | 3.0       | 0.728          | 51.9 | LOS D               | 18.1          | 129.5         | 0.97           | 0.86              | 1.00         | 32.0           |
| 3            | R2       | 379              | 6             | 449              | 1.6       | *0.728         | 52.1 | LOS D               | 18.1          | 129.5         | 0.98           | 0.86              | 1.01         | 26.5           |
| Appro        | bach     | 544              | 11            | 645              | 2.0       | 0.728          | 52.0 | LOS D               | 18.1          | 129.5         | 0.97           | 0.86              | 1.01         | 28.3           |
| East:        | Great    | Western          | Highway       | ý                |           |                |      |                     |               |               |                |                   |              |                |
| 4            | L2       | 197              | 1             | 234              | 0.5       | 0.270          | 26.3 | LOS B               | 8.2           | 57.8          | 0.65           | 0.75              | 0.65         | 36.1           |
| 5            | T1       | 1106             | 30            | 1310             | 2.7       | <b>*</b> 0.759 | 27.7 | LOS B               | 32.5          | 232.9         | 0.88           | 0.79              | 0.88         | 44.3           |
| Appro        | bach     | 1303             | 31            | 1544             | 2.4       | 0.759          | 27.5 | LOS B               | 32.5          | 232.9         | 0.84           | 0.78              | 0.84         | 43.4           |
| West         | : Grea   | t Westerr        | n Highwa      | y                |           |                |      |                     |               |               |                |                   |              |                |
| 11           | T1       | 1184             | 22            | 1403             | 1.9       | 0.455          | 10.1 | LOS A               | 16.1          | 114.2         | 0.50           | 0.45              | 0.50         | 53.4           |
| 12           | R2       | 166              | 3             | 197              | 1.8       | <b>*</b> 0.534 | 49.3 | LOS D               | 10.3          | 73.3          | 0.95           | 0.95              | 0.95         | 32.4           |
| Appro        | bach     | 1350             | 25            | 1600             | 1.9       | 0.534          | 14.9 | LOS B               | 16.1          | 114.2         | 0.55           | 0.51              | 0.55         | 50.2           |
| All<br>Vehic | les      | 3197             | 67            | 3788             | 2.1       | 0.759          | 26.3 | LOS B               | 32.5          | 232.9         | 0.74           | 0.68              | 0.75         | 43.4           |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

### Site: 802 [Great Western Highway x Bringelly Road 2030 PM (Site Folder: Future - 2030)]

New Site

Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time) Design Life Analysis (Final Year): Results for 10 years

Timings based on settings in the Site Phasing & Timing dialog (Demand & Sensitivity Analysis overrides) Phase Times determined by the program Phase Sequence: Leading Right Turn Reference Phase: Phase A Input Phase Sequence: A, B, C Output Phase Sequence: A, B, C

| Vehi         | cle M   | ovemen           | t Perfor      | mance            |           |                |                  |                    |               |               |                |                   |              |                |
|--------------|---------|------------------|---------------|------------------|-----------|----------------|------------------|--------------------|---------------|---------------|----------------|-------------------|--------------|----------------|
| Mov<br>ID    | Turn    |                  | PUT<br>JMES   | DEM.<br>FLO      |           | Deg.<br>Satn   | Aver. L<br>Delay | evel of<br>Service |               | ACK OF<br>EUE | Prop. E<br>Que | Effective<br>Stop | Aver.<br>No. | Aver.<br>Speed |
|              |         | [ Total<br>veh/h | HV ]<br>veh/h | [ Total<br>veh/h | HV ]<br>% | v/c            | sec              |                    | [ Veh.<br>veh | Dist ]<br>m   |                | Rate              | Cycles       | km/h           |
| Sout         | h: Brin | gelly Roa        | ıd            |                  |           |                |                  |                    |               |               |                |                   |              |                |
| 1            | L2      | 165              | 5             | 212              | 3.0       | 0.821          | 55.4             | LOS D              | 19.2          | 137.0         | 0.95           | 0.90              | 1.09         | 31.1           |
| 3            | R2      | 379              | 6             | 486              | 1.6       | <b>*</b> 0.821 | 56.4             | LOS D              | 21.8          | 155.0         | 0.99           | 0.91              | 1.12         | 25.3           |
| Appr         | oach    | 544              | 11            | 698              | 2.0       | 0.821          | 56.1             | LOS D              | 21.8          | 155.0         | 0.98           | 0.91              | 1.11         | 27.2           |
| East:        | Great   | Western          | Highway       | Ý                |           |                |                  |                    |               |               |                |                   |              |                |
| 4            | L2      | 197              | 1             | 253              | 0.5       | 0.293          | 26.5             | LOS B              | 9.0           | 63.4          | 0.66           | 0.76              | 0.66         | 36.0           |
| 5            | T1      | 1098             | 30            | 1409             | 2.7       | *0.829         | 31.9             | LOS C              | 39.1          | 279.9         | 0.91           | 0.86              | 0.96         | 42.6           |
| Appr         | oach    | 1295             | 31            | 1662             | 2.4       | 0.829          | 31.1             | LOS C              | 39.1          | 279.9         | 0.87           | 0.85              | 0.91         | 41.9           |
| West         | : Grea  | t Westerr        | n Highwa      | у                |           |                |                  |                    |               |               |                |                   |              |                |
| 11           | T1      | 1181             | 22            | 1515             | 1.9       | 0.498          | 11.0             | LOS A              | 18.4          | 131.1         | 0.53           | 0.48              | 0.53         | 52.9           |
| 12           | R2      | 166              | 3             | 213              | 1.8       | *0.624         | 54.6             | LOS D              | 11.4          | 81.1          | 0.98           | 0.98              | 0.98         | 31.0           |
| Appr         | oach    | 1347             | 25            | 1728             | 1.9       | 0.624          | 16.3             | LOS B              | 18.4          | 131.1         | 0.58           | 0.54              | 0.58         | 49.5           |
| All<br>Vehic | cles    | 3186             | 67            | 4088             | 2.1       | 0.829          | 29.1             | LOS C              | 39.1          | 279.9         | 0.77           | 0.73              | 0.81         | 42.2           |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## Site: 1002 [Great Western Highway x Bringelly Road 2030+DEV PM (Site Folder: Future - 2030 +DEV)]

New Site

Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time) Design Life Analysis (Final Year): Results for 10 years

Timings based on settings in the Site Phasing & Timing dialog (Demand & Sensitivity Analysis overrides) Phase Times determined by the program Phase Sequence: Leading Right Turn Reference Phase: Phase A Input Phase Sequence: A, B, C Output Phase Sequence: A, B, C

| Vehi         | cle M   | ovemen                 | t Perfor | rmance                |     |              |      |                     |      |                         |                |                           |                        |                |
|--------------|---------|------------------------|----------|-----------------------|-----|--------------|------|---------------------|------|-------------------------|----------------|---------------------------|------------------------|----------------|
| Mov<br>ID    | Turn    | INP<br>VOLU<br>[ Total |          | DEM<br>FLO<br>[ Total |     | Deg.<br>Satn |      | Level of<br>Service |      | ACK OF<br>EUE<br>Dist ] | Prop. E<br>Que | Effective<br>Stop<br>Rate | Aver.<br>No.<br>Cycles | Aver.<br>Speed |
|              |         | veh/h                  | veh/h    | veh/h                 | %   | v/c          | sec  |                     | veh  | m                       |                |                           |                        | km/h           |
| Sout         | h: Brin | gelly Roa              | ld       |                       |     |              |      |                     |      |                         |                |                           |                        |                |
| 1            | L2      | 165                    | 5        | 212                   | 3.0 | 0.816        | 56.3 | LOS D               | 21.2 | 151.8                   | 0.98           | 0.91                      | 1.10                   | 30.9           |
| 3            | R2      | 379                    | 6        | 486                   | 1.6 | *0.816       | 55.9 | LOS D               | 21.2 | 151.8                   | 0.99           | 0.91                      | 1.12                   | 25.4           |
| Appr         | oach    | 544                    | 11       | 698                   | 2.0 | 0.816        | 56.0 | LOS D               | 21.2 | 151.8                   | 0.98           | 0.91                      | 1.11                   | 27.3           |
| East:        | Great   | Western                | Highway  | y                     |     |              |      |                     |      |                         |                |                           |                        |                |
| 4            | L2      | 197                    | 1        | 253                   | 0.5 | 0.298        | 27.2 | LOS B               | 9.2  | 64.4                    | 0.67           | 0.76                      | 0.67                   | 35.6           |
| 5            | T1      | 1116                   | 30       | 1428                  | 2.7 | *0.858       | 36.2 | LOS C               | 42.6 | 305.1                   | 0.94           | 0.91                      | 1.02                   | 41.0           |
| Appr         | oach    | 1313                   | 31       | 1681                  | 2.4 | 0.858        | 34.8 | LOS C               | 42.6 | 305.1                   | 0.90           | 0.89                      | 0.96                   | 40.5           |
| West         | : Grea  | t Westerr              | n Highwa | ıy                    |     |              |      |                     |      |                         |                |                           |                        |                |
| 11           | T1      | 1191                   | 22       | 1526                  | 1.8 | 0.502        | 11.0 | LOS A               | 18.6 | 132.4                   | 0.53           | 0.48                      | 0.53                   | 52.8           |
| 12           | R2      | 166                    | 3        | 213                   | 1.8 | *0.604       | 54.7 | LOS D               | 11.3 | 80.4                    | 0.97           | 0.98                      | 0.97                   | 30.9           |
| Appr         | oach    | 1357                   | 25       | 1739                  | 1.8 | 0.604        | 16.4 | LOS B               | 18.6 | 132.4                   | 0.58           | 0.54                      | 0.58                   | 49.5           |
| All<br>Vehic | cles    | 3214                   | 67       | 4118                  | 2.1 | 0.858        | 30.6 | LOS C               | 42.6 | 305.1                   | 0.78           | 0.75                      | 0.83                   | 41.6           |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

# **APPENDIX F-3**

SIDRA Modelling Outputs Caddens Road / Gipps Road / Kent Road

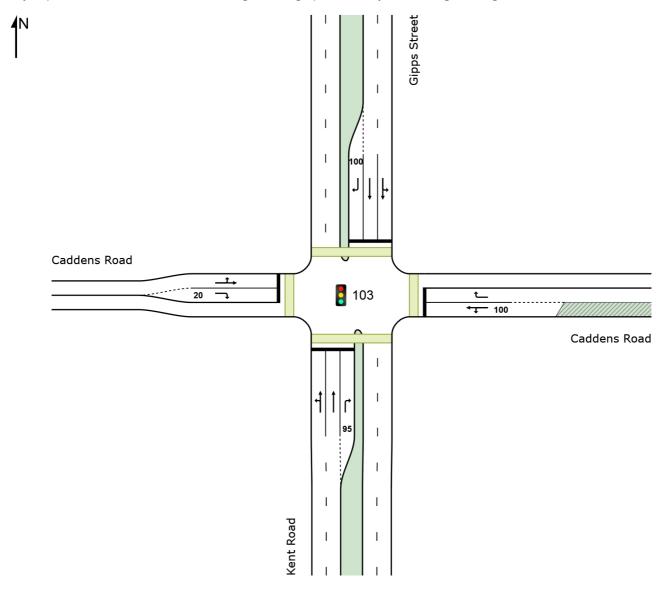
### Site: 103 [Caddens Road x Gipps Street x Kent Road Existing AM (Site Folder: Exisitng (2020))]

New Site Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Timings based on settings in the Site Phasing & Timing dialog Phase Times determined by the program Phase Sequence: TCS Reference Phase: Phase A Input Phase Sequence: A, B\*, C\*, D, E, E1\*, E2\* Output Phase Sequence: A, D, E (\* Variable Phase)

#### Site Layout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



SIDRA INTERSECTION 9.0 | Copyright © 2000-2020 Akcelik and Associates Pty Ltd | sidrasolutions.com Organisation: TRAFFIX PTY LTD | Licence: NETWORK / 1PC | Created: Thursday, 6 May 2021 3:54:50 PM Project: T:\Synergy\Projects\20\20.456\Modelling\20.456m01v03 TRAFFIX.sip9

### Site: 103 [Caddens Road x Gipps Street x Kent Road Existing AM (Site Folder: Exisitng (2020))]

New Site Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site Optimum Cycle Time - Minimum Delay) Variable Sequence Analysis applied. The results are given for the selected output sequence.

Timings based on settings in the Site Phasing & Timing dialog Phase Times determined by the program Phase Sequence: TCS Reference Phase: Phase A Input Phase Sequence: A, B\*, C\*, D, E, E1\*, E2\* Output Phase Sequence: A, D, E (\* Variable Phase)

Vehicle Movement Performance Deg. Satn 95% BACK OF Mov Turn INPUT DEMAND Aver. Level of Prop. Effective Aver Aver VOLUMES FLOWS Delay Service Stop QUEUE Speed Que HV ] [ Total HV] Dist ] Rate [ Total [Veh. Cycles veh/h km/h veh/h veh/h South: Kent Road 1 L2 0.83 194 204 2.1 0.748 36.2 LOS C 30.2 219.8 0.89 0.89 43.4 4 2 Τ1 991 59 1043 6.0 \*0.748 29.1 LOS C 30.2 219.8 0.89 0.81 0.89 47.2 66.5 LOS E 3 R2 20 0.98 0.71 0.98 30.0 0 21 0.0 0.170 12 8.5 1268 30.8 LOS C 30.2 0.89 Approach 1205 63 5.2 0.748 219.8 0.89 0.81 46.0 East: Caddens Road 4 L2 61 0 64 0.0 0.143 31.6 LOS C 3.7 26.7 0.70 0.67 0.70 40.5 T1 5 31 2 33 6.5 0.143 27.0 LOS B 3.7 26.7 0.70 0.67 0.70 38.0 R2 68 3 72 0.202 40.2 LOS C 23.4 0.80 6 4.4 3.2 0.80 0.74 32.8 Approach 160 5 168 3.1 0.202 34.3 LOS C 3.7 26.7 0.74 0.70 0.74 36.7 North: Gipps Street L2 7 28 1 29 3.6 0.542 32.6 LOS C 19.4 141.0 0.78 0.70 0.78 40.1 8 T1 849 37 894 4.4 0.542 25.6 LOS B 19.5 141.5 0.78 0.69 0.78 50.1 9 R2 2 81 2.6 \*0.667 70.5 LOS E 5.0 35.7 0.80 26.9 77 1.00 1.11 Approach 954 40 1004 4.2 0.667 29.4 LOS C 19.5 141.5 0.80 0.70 0.81 46.7 West: Caddens Road L2 3 0.323 30.1 LOS C 43.9 0.69 0.73 0.69 10 137 144 22 6.1 39.7 11 T1 18 1 19 5.6 0.323 25.7 LOS B 6.1 43.9 0.69 0.73 0.69 37.9 12 R2 212 8 223 3.8 \*0.728 46.7 LOS D 11.6 84.1 0.89 0.85 0.97 36.1 Approach 367 12 386 3.3 0.728 39.5 LOS C 11.6 84.1 0.81 0.80 0.85 37.3 All 4.5 30.2 0.77 2686 120 2827 0.748 31.7 LOS C 219.8 0.84 0.85 44.1 Vehicles

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

### Site: 303 [Caddens Road x Gipps Street x Kent Road 2026 AM (Site Folder: Future - 2026)]

New Site

Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time) Variable Sequence Analysis applied. The results are given for the selected output sequence. Design Life Analysis (Final Year): Results for 6 years

#### Timings based on settings in the Site Phasing & Timing dialog (Demand & Sensitivity Analysis overrides) Phase Times determined by the program Phase Sequence: TCS Reference Phase: Phase A Input Phase Sequence: A, B\*, C\*, D, E, E1\*, E2\*

Output Phase Sequence: A, B\*, D, E, E2\*

(\* Variable Phase)

| Vehi         | cle M   | ovemen          | t Perfoi     | rmance         |           |                |       |                     |       |               |      |              |               |       |
|--------------|---------|-----------------|--------------|----------------|-----------|----------------|-------|---------------------|-------|---------------|------|--------------|---------------|-------|
| -            | Turn    |                 | TUT          | DEM            |           | Deg.           |       | _evel of            |       | ACK OF        |      | Effective    | Aver.         | Aver. |
| ID           |         | VOLL<br>[ Total | IMES<br>HV 1 | FLO<br>[ Total | WS<br>HV] | Satn           | Delay | Service             | [Veh. | EUE<br>Dist ] | Que  | Stop<br>Rate | NO.<br>Cycles | Speed |
|              |         | veh/h           | veh/h        | veh/h          | %         | v/c            | sec   |                     | veh   | m             |      | Trate        | Cycles        | km/h  |
| Sout         | h: Ken  | t Road          |              |                |           |                |       |                     |       |               |      |              |               |       |
| 1            | L2      | 194             | 4            | 230            | 2.1       | 0.798          | 36.0  | LOS C               | 35.1  | 255.3         | 0.91 | 0.85         | 0.92          | 39.1  |
| 2            | T1      | 991             | 59           | 1175           | 6.0       | *0.798         | 28.9  | LOS C               | 35.1  | 255.3         | 0.91 | 0.84         | 0.92          | 42.4  |
| 3            | R2      | 20              | 0            | 24             | 0.0       | 0.128          | 35.4  | LOS C               | 0.7   | 5.2           | 0.94 | 0.70         | 0.94          | 35.2  |
| Appr         | oach    | 1205            | 63           | 1428           | 5.2       | 0.798          | 30.1  | LOS C               | 35.1  | 255.3         | 0.91 | 0.84         | 0.92          | 41.6  |
| East:        | Cadd    | ens Road        | ł            |                |           |                |       |                     |       |               |      |              |               |       |
| 4            | L2      | 61              | 0            | 72             | 0.0       | 0.160          | 31.1  | LOS C               | 4.2   | 29.9          | 0.70 | 0.67         | 0.70          | 36.4  |
| 5            | T1      | 31              | 2            | 37             | 6.5       | 0.160          | 26.5  | LOS B               | 4.2   | 29.9          | 0.70 | 0.67         | 0.70          | 38.2  |
| 6            | R2      | 68              | 3            | 81             | 4.4       | 0.263          | 44.9  | LOS D               | 3.9   | 28.2          | 0.85 | 0.76         | 0.85          | 31.3  |
| Appr         | oach    | 160             | 5            | 190            | 3.1       | 0.263          | 36.1  | LOS C               | 4.2   | 29.9          | 0.76 | 0.71         | 0.76          | 34.4  |
| North        | n: Gipp | s Street        |              |                |           |                |       |                     |       |               |      |              |               |       |
| 7            | L2      | 28              | 1            | 33             | 3.6       | 0.723          | 40.2  | LOS C               | 26.5  | 192.1         | 0.91 | 0.82         | 0.91          | 36.6  |
| 8            | T1      | 849             | 37           | 1006           | 4.4       | 0.723          | 32.8  | LOS C               | 26.5  | 192.1         | 0.90 | 0.80         | 0.90          | 40.4  |
| 9            | R2      | 77              | 2            | 91             | 2.6       | <b>*</b> 0.751 | 72.2  | LOS F <sup>11</sup> | 5.7   | 41.0          | 1.00 | 0.84         | 1.21          | 26.6  |
| Appr         | oach    | 954             | 40           | 1131           | 4.2       | 0.751          | 36.2  | LOS C               | 26.5  | 192.1         | 0.91 | 0.80         | 0.93          | 38.4  |
| West         | : Cadd  | lens Roa        | d            |                |           |                |       |                     |       |               |      |              |               |       |
| 10           | L2      | 137             | 3            | 162            | 2.2       | 0.442          | 32.6  | LOS C               | 7.3   | 52.3          | 0.73 | 0.75         | 0.73          | 38.5  |
| 11           | T1      | 18              | 1            | 21             | 5.6       | 0.442          | 28.2  | LOS B               | 7.3   | 52.3          | 0.73 | 0.75         | 0.73          | 36.9  |
| 12           | R2      | 212             | 8            | 251            | 3.8       | *0.779         | 48.7  | LOS D               | 13.6  | 97.9          | 0.89 | 0.87         | 1.02          | 31.4  |
| Appr         | oach    | 367             | 12           | 435            | 3.3       | 0.779          | 41.7  | LOS C               | 13.6  | 97.9          | 0.82 | 0.82         | 0.90          | 34.1  |
| All<br>Vehic | cles    | 2686            | 120          | 3184           | 4.5       | 0.798          | 34.2  | LOS C               | 35.1  | 255.3         | 0.89 | 0.82         | 0.91          | 38.6  |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

11 Level of Service is worse than the Level of Service Target specified in the Parameter Settings dialog.

## Site: 503 [Caddens Road x Gipps Street x Kent Road 2026+DEV AM (Site Folder: Future - 2026 + DEV)]

New Site

Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time) Variable Sequence Analysis applied. The results are given for the selected output sequence. Design Life Analysis (Final Year): Results for 6 years

#### Timings based on settings in the Site Phasing & Timing dialog (Demand & Sensitivity Analysis overrides) Phase Times determined by the program Phase Sequence: TCS Reference Phase: Phase A Input Phase Sequence: A, B\*, C\*, D, E, E1\*, E2\* Output Phase Sequence: A, B\*, D, E, E2\* (\* Variable Phase)

| Vehi                                    | cle M                  | ovemen                            | t Perfo                  | mance                           |                                 |   |                                      |  |                                    |   |                                      |                                      |                                      |                                      |
|---|------------------------|-----------------------------------|--------------------------|---------------------------------|---------------------------------|---|--------------------------------------|--|------------------------------------|---|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|
| Mov<br>ID                               | Turn                   | INP<br>VOLU<br>[ Total<br>veh/h   |                          | DEM/<br>FLO<br>[ Total<br>veh/h |                                 | Deg.<br>Satn<br>v/c                         |                                      | Level of<br>Service                            | 95% BA<br>QUI<br>[ Veh.<br>veh     | ACK OF<br>EUE<br>Dist]<br>m             | Prop. I<br>Que                       | Effective<br>Stop<br>Rate            | Aver.<br>No.<br>Cycles               | Aver.<br>Speed<br>km/h               |
| South                                   | n: Ken                 | t Road                            |                          |                                 |                                 |   |                                      |  |                                    |   |                                      |                                      |                                      |                                      |
| 1<br>2<br>3                             | L2<br>T1<br>R2         | 216<br>991<br>20                  | 4<br>59<br>0             | 253<br>1175<br>24               | 1.9<br>6.0<br>0.0               | 0.812<br>* 0.812<br>0.128                   | 37.0<br>30.0<br>35.4                 | LOS C<br>LOS C<br>LOS C                        | 36.5<br>36.5<br>0.7                | 265.5<br>265.5<br>5.2                   | 0.92<br>0.92<br>0.94                 | 0.87<br>0.86<br>0.70                 | 0.94<br>0.94<br>0.94                 | 38.4<br>41.6<br>35.2                 |
| Appro                                   | bach                   | 1227                              | 63                       | 1452                            | 5.1                             | 0.812                                       | 31.3                                 | LOS C  | 36.5                               | 265.5                                   | 0.92                                 | 0.86                                 | 0.94                                 | 40.8                                 |
| East:                                   | Cadd                   | ens Road                          |                          |                                 |                                 |   |                                      |  |                                    |   |                                      |                                      |                                      |                                      |
| 4<br>5<br>6<br>Appro                    | ı: Gipp                | 61<br>31<br>68<br>160<br>s Street | 0<br>2<br>3<br>5         | 72<br>37<br>81<br>190           | 0.0<br>6.5<br>4.4<br>3.1        | 0.160<br>0.160<br>0.263<br>0.263            | 31.1<br>26.5<br>44.9<br>36.1         | LOS C<br>LOS B<br>LOS D<br>LOS C               | 4.2<br>4.2<br>3.9<br>4.2           | 29.9<br>29.9<br>28.2<br>29.9            | 0.70<br>0.70<br>0.85<br>0.76         | 0.67<br>0.67<br>0.76<br>0.71         | 0.70<br>0.70<br>0.85<br>0.76         | 36.4<br>38.2<br>31.3<br>34.4         |
| 7<br>8<br>9<br>Appre                    | L2<br>T1<br>R2<br>pach | 28<br>849<br>77<br>954            | 1<br>37<br>2<br>40       | 33<br>1006<br>91<br>1131        | 3.6<br>4.4<br>2.6<br>4.2        | 0.722<br>0.722<br>* 0.751<br>0.751          | 40.2<br>32.8<br>72.2<br>36.2         | LOS C<br>LOS C<br>LOS F <sup>11</sup><br>LOS C | 26.4<br>26.4<br>5.7<br>26.4        | 191.9<br>191.9<br>41.0<br>191.9         | 0.91<br>0.90<br>1.00<br>0.91         | 0.81<br>0.80<br>0.84<br>0.80         | 0.91<br>0.90<br>1.21<br>0.93         | 36.6<br>40.4<br>26.6<br>38.4         |
| West                                    | : Cado                 | lens Road                         | d                        |                                 |                                 |   |                                      |  |                                    |   |                                      |                                      |                                      |                                      |
| 10<br>11<br>12<br>Appro<br>All<br>Vehic |                        | 137<br>18<br>217<br>372<br>2713   | 3<br>1<br>8<br>12<br>120 | 162<br>21<br>257<br>440<br>3212 | 2.2<br>5.6<br>3.7<br>3.2<br>4.4 | 0.446<br>0.446<br>* 0.793<br>0.793<br>0.812 | 32.6<br>28.2<br>49.9<br>42.5<br>34.8 | LOS C<br>LOS D<br>LOS C<br>LOS C               | 7.3<br>7.3<br>14.1<br>14.1<br>36.5 | 52.3<br>52.3<br>101.7<br>101.7<br>265.5 | 0.73<br>0.73<br>0.90<br>0.83<br>0.89 | 0.75<br>0.75<br>0.88<br>0.83<br>0.83 | 0.73<br>0.73<br>1.05<br>0.91<br>0.92 | 38.5<br>36.9<br>31.0<br>33.8<br>38.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

11 Level of Service is worse than the Level of Service Target specified in the Parameter Settings dialog.

### Site: 703 [Caddens Road x Gipps Street x Kent Road 2030 AM (Site Folder: Future - 2030)]

New Site

Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 140 seconds (Site User-Given Cycle Time) Variable Sequence Analysis applied. The results are given for the selected output sequence. Design Life Analysis (Final Year): Results for 10 years

#### Timings based on settings in the Site Phasing & Timing dialog (Demand & Sensitivity Analysis overrides) Phase Times determined by the program Phase Sequence: TCS Reference Phase: Phase A Input Phase Sequence: A, B\*, C\*, D, E, E1\*, E2\*

Output Phase Sequence: A, B\*, D, E, E2\*

(\* Variable Phase)

| Vehi         | cle M   | ovemen          | t Perfor     | rmance         |           |                |       |                     |              |               |      |              |               |       |
|--------------|---------|-----------------|--------------|----------------|-----------|----------------|-------|---------------------|--------------|---------------|------|--------------|---------------|-------|
|              | Turn    | INF             |              | DEM            |           | Deg.           |       | Level of            |              | ACK OF        |      | Effective    | Aver.         | Aver. |
| ID           |         | VOLL<br>[ Total | IMES<br>HV 1 | FLO<br>[ Total | WS<br>HV] | Satn           | Delay | Service             | QUI<br>[Veh. | EUE<br>Dist ] | Que  | Stop<br>Rate | No.<br>Cycles | Speed |
|              |         | veh/h           | veh/h        | veh/h          | %         | v/c            | sec   |                     | veh          | m             |      | Nate         | Cycles        | km/h  |
| Sout         | h: Ken  | t Road          |              |                |           |                |       |                     |              |               |      |              |               |       |
| 1            | L2      | 194             | 4            | 249            | 2.1       | 0.859          | 45.4  | LOS D               | 48.4         | 352.6         | 0.96 | 0.92         | 1.00          | 35.0  |
| 2            | T1      | 991             | 59           | 1272           | 6.0       | <b>*</b> 0.859 | 38.2  | LOS C               | 48.4         | 352.6         | 0.95 | 0.91         | 1.00          | 37.0  |
| 3            | R2      | 20              | 0            | 26             | 0.0       | 0.161          | 41.3  | LOS C               | 0.9          | 6.6           | 0.96 | 0.71         | 0.96          | 33.0  |
| Appr         | oach    | 1205            | 63           | 1546           | 5.2       | 0.859          | 39.4  | LOS C               | 48.4         | 352.6         | 0.95 | 0.91         | 1.00          | 36.5  |
| East         | Cadd    | ens Road        | ł            |                |           |                |       |                     |              |               |      |              |               |       |
| 4            | L2      | 61              | 0            | 78             | 0.0       | 0.167          | 34.4  | LOS C               | 5.2          | 37.1          | 0.69 | 0.68         | 0.69          | 35.0  |
| 5            | T1      | 31              | 2            | 40             | 6.5       | 0.167          | 29.9  | LOS C               | 5.2          | 37.1          | 0.69 | 0.68         | 0.69          | 36.9  |
| 6            | R2      | 68              | 3            | 87             | 4.4       | 0.278          | 49.9  | LOS D               | 4.8          | 35.0          | 0.84 | 0.76         | 0.84          | 29.9  |
| Appr         | oach    | 160             | 5            | 205            | 3.1       | 0.278          | 40.1  | LOS C               | 5.2          | 37.1          | 0.76 | 0.71         | 0.76          | 33.0  |
| North        | n: Gipp | s Street        |              |                |           |                |       |                     |              |               |      |              |               |       |
| 7            | L2      | 28              | 1            | 36             | 3.6       | 0.750          | 44.1  | LOS D               | 33.8         | 245.0         | 0.92 | 0.83         | 0.92          | 35.1  |
| 8            | T1      | 849             | 37           | 1089           | 4.4       | 0.750          | 36.4  | LOS C               | 33.8         | 245.0         | 0.90 | 0.81         | 0.90          | 38.3  |
| 9            | R2      | 77              | 2            | 99             | 2.6       | *0.843         | 86.1  | LOS F <sup>11</sup> | 7.4          | 53.1          | 1.00 | 0.88         | 1.33          | 23.8  |
| Appr         | oach    | 954             | 40           | 1224           | 4.2       | 0.843          | 40.6  | LOS C               | 33.8         | 245.0         | 0.91 | 0.81         | 0.93          | 36.1  |
| West         | : Cadd  | lens Roa        | d            |                |           |                |       |                     |              |               |      |              |               |       |
| 10           | L2      | 137             | 3            | 176            | 2.2       | 0.530          | 35.6  | LOS C               | 9.0          | 64.6          | 0.72 | 0.75         | 0.72          | 37.2  |
| 11           | T1      | 18              | 1            | 23             | 5.6       | 0.530          | 31.2  | LOS C               | 9.0          | 64.6          | 0.72 | 0.75         | 0.72          | 35.8  |
| 12           | R2      | 212             | 8            | 272            | 3.8       | *0.846         | 60.9  | LOS E <sup>11</sup> | 18.2         | 131.4         | 0.90 | 0.91         | 1.10          | 28.0  |
| Appr         | oach    | 367             | 12           | 471            | 3.3       | 0.846          | 50.0  | LOS D               | 18.2         | 131.4         | 0.82 | 0.84         | 0.94          | 31.3  |
| All<br>Vehic | cles    | 2686            | 120          | 3447           | 4.5       | 0.859          | 41.3  | LOS C               | 48.4         | 352.6         | 0.91 | 0.85         | 0.95          | 35.2  |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

11 Level of Service is worse than the Level of Service Target specified in the Parameter Settings dialog.

## Site: 903 [Caddens Road x Gipps Street x Kent Road 2030+DEV AM (Site Folder: Future - 2030 +DEV)]

New Site Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 140 seconds (Site User-Given Cycle Time) Variable Sequence Analysis applied. The results are given for the selected output sequence. Design Life Analysis (Final Year): Results for 10 years

#### Timings based on settings in the Site Phasing & Timing dialog (Demand & Sensitivity Analysis overrides) Phase Times determined by the program Phase Sequence: TCS Reference Phase: Phase A Input Phase Sequence: A, B\*, C\*, D, E, E1\*, E2\* Output Phase Sequence: A, B\*, D, E (\* Variable Phase)

| Vehi                                    | cle M                  | ovemen                          | t Perfoi                 | mance                           |                                 |   |                                      |   |                                    |   |                                      |                                      |                                      |                                      |
|---|------------------------|---------------------------------|--------------------------|---------------------------------|---------------------------------|---|--------------------------------------|---|------------------------------------|---|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|
| Mov<br>ID                               | Turn                   | INP<br>VOLU<br>[ Total<br>veh/h |                          | DEM/<br>FLO<br>[ Total<br>veh/h |                                 | Deg.<br>Satn<br>v/c                         |                                      | Level of<br>Service   | 95% BA<br>QUI<br>[ Veh.<br>veh     | ACK OF<br>EUE<br>Dist]<br>m             | Prop. I<br>Que                       | Effective<br>Stop<br>Rate            | Aver.<br>No.<br>Cycles               | Aver.<br>Speed<br>km/h               |
| South                                   | n: Kent                | t Road                          |                          |                                 |                                 |   |                                      |   |                                    |   |                                      |                                      |                                      |                                      |
| 1<br>2<br>3                             | L2<br>T1<br>R2         | 243<br>991<br>20                | 4<br>59<br>0             | 301<br>1272<br>26               | 1.7<br>6.0<br>0.0               | 0.888<br>* 0.888<br>0.129                   | 50.3<br>43.3<br>39.3                 | LOS D<br>LOS D<br>LOS C                                     | 53.8<br>53.8<br>0.9                | 390.6<br>390.6<br>6.4                   | 0.98<br>0.97<br>0.94                 | 0.96<br>0.96<br>0.71                 | 1.07<br>1.06<br>0.94                 | 32.9<br>34.5<br>33.7                 |
| Appro                                   | oach                   | 1254                            | 63                       | 1598                            | 5.1                             | 0.888                                       | 44.5                                 | LOS D   | 53.8                               | 390.6                                   | 0.97                                 | 0.95                                 | 1.06                                 | 34.1                                 |
| East:                                   | Cadd                   | ens Road                        | I                        |                                 |                                 |   |                                      |   |                                    |   |                                      |                                      |                                      |                                      |
| 4<br>5<br>6<br>Appro                    | L2<br>T1<br>R2<br>Dach | 61<br>31<br>68<br>160           | 0<br>2<br>3<br>5         | 78<br>40<br>87<br>205           | 0.0<br>6.5<br>4.4<br>3.1        | 0.167<br>0.167<br>0.278<br>0.278            | 34.4<br>29.9<br>49.9<br>40.1         | LOS C<br>LOS C<br>LOS D<br>LOS C                            | 5.2<br>5.2<br>4.8<br>5.2           | 37.1<br>37.1<br>35.0<br>37.1            | 0.69<br>0.69<br>0.84<br>0.76         | 0.67<br>0.67<br>0.76<br>0.71         | 0.69<br>0.69<br>0.84<br>0.76         | 35.0<br>36.9<br>29.9<br>33.0         |
| North                                   | : Gipp                 | s Street                        |                          |                                 |                                 |   |                                      |   |                                    |   |                                      |                                      |                                      |                                      |
| 7<br>8<br>9<br>Appro                    | L2<br>T1<br>R2<br>Dach | 28<br>849<br>77<br>954          | 1<br>37<br>2<br>40       | 36<br>1089<br>99<br>1224        | 3.6<br>4.4<br>2.6<br>4.2        | 0.790<br>0.790<br>* 0.843<br>0.843          | 47.2<br>39.8<br>86.1<br>43.7         | LOS D<br>LOS C<br><mark>LOS F</mark> <sup>11</sup><br>LOS D | 35.1<br>35.1<br>7.4<br>35.1        | 254.7<br>254.7<br>53.1<br>254.7         | 0.95<br>0.93<br>1.00<br>0.94         | 0.86<br>0.84<br>0.88<br>0.84         | 0.95<br>0.94<br>1.33<br>0.97         | 33.9<br>36.6<br>23.8<br>34.7         |
| West                                    | : Cado                 | lens Roa                        | b                        |                                 |                                 |   |                                      |   |                                    |   |                                      |                                      |                                      |                                      |
| 10<br>11<br>12<br>Appro<br>All<br>Vehic |                        | 137<br>18<br>224<br>379<br>2747 | 3<br>1<br>8<br>12<br>120 | 176<br>23<br>285<br>484<br>3511 | 2.2<br>5.6<br>3.6<br>3.2<br>4.4 | 0.543<br>0.543<br>* 0.879<br>0.879<br>0.888 | 35.6<br>31.2<br>66.8<br>53.8<br>45.3 | LOS C<br>LOS C<br>LOS E <sup>11</sup><br>LOS D              | 9.0<br>9.0<br>20.2<br>20.2<br>53.8 | 64.6<br>64.6<br>145.6<br>145.6<br>390.6 | 0.72<br>0.72<br>0.91<br>0.83<br>0.93 | 0.75<br>0.75<br>0.94<br>0.86<br>0.89 | 0.72<br>0.72<br>1.17<br>0.98<br>1.00 | 37.2<br>35.8<br>26.5<br>30.2<br>33.6 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

11 Level of Service is worse than the Level of Service Target specified in the Parameter Settings dialog.

## Site: 203 [Caddens Road x Gipps Street x Kent Road Existing PM (Site Folder: Exisitng (2020))]

New Site

Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site Optimum Cycle Time - Minimum Delay)

Variable Sequence Analysis applied. The results are given for the selected output sequence.

Timings based on settings in the Site Phasing & Timing dialog Phase Times determined by the program Phase Sequence: TCS Reference Phase: Phase A Input Phase Sequence: A, B\*, C\*, D, E, E1\*, E2\* Output Phase Sequence: A, D, E (\* Variable Phase)

| Vehi         | icle M  | ovemen          | t Perfor | mance          |           |                |       |          |        |               |         |              |               |       |
|--------------|---------|-----------------|----------|----------------|-----------|----------------|-------|----------|--------|---------------|---------|--------------|---------------|-------|
|              | Turn    | INP             |          | DEM            |           | Deg.           |       | Level of |        |               | Prop. E |              | Aver.         | Aver. |
| ID           |         | VOLL<br>[ Total | HV 1     | FLO<br>[ Total | WS<br>HV] | Satn           | Delay | Service  | [ Veh. | EUE<br>Dist ] | Que     | Stop<br>Rate | No.<br>Cycles | Speed |
|              |         | veh/h           | veh/h    | veh/h          | пvј<br>%  | v/c            | sec   |          | veh    | m             |         | Rale         | Cycles        | km/h  |
| Sout         | h: Ken  | t Road          |          |                |           |                |       |          |        |               |         |              |               |       |
| 1            | L2      | 230             | 8        | 242            | 3.5       | 0.687          | 33.8  | LOS C    | 27.3   | 196.3         | 0.85    | 0.80         | 0.85          | 44.3  |
| 2            | T1      | 897             | 25       | 944            | 2.8       | <b>*</b> 0.687 | 26.4  | LOS B    | 27.3   | 196.3         | 0.84    | 0.76         | 0.84          | 48.9  |
| 3            | R2      | 48              | 0        | 51             | 0.0       | 0.297          | 63.8  | LOS E    | 2.9    | 20.1          | 0.97    | 0.75         | 0.97          | 30.6  |
| Appr         | oach    | 1175            | 33       | 1237           | 2.8       | 0.687          | 29.4  | LOS C    | 27.3   | 196.3         | 0.84    | 0.77         | 0.84          | 46.6  |
| East         | Cadd    | ens Roac        | I        |                |           |                |       |          |        |               |         |              |               |       |
| 4            | L2      | 38              | 1        | 40             | 2.6       | 0.095          | 33.9  | LOS C    | 2.3    | 16.6          | 0.72    | 0.67         | 0.72          | 39.1  |
| 5            | T1      | 16              | 2        | 17             | 12.5      | 0.095          | 29.3  | LOS C    | 2.3    | 16.6          | 0.72    | 0.67         | 0.72          | 37.0  |
| 6            | R2      | 59              | 3        | 62             | 5.1       | 0.176          | 42.1  | LOS C    | 2.8    | 20.8          | 0.81    | 0.74         | 0.81          | 32.1  |
| Appr         | oach    | 113             | 6        | 119            | 5.3       | 0.176          | 37.5  | LOS C    | 2.8    | 20.8          | 0.77    | 0.70         | 0.77          | 35.1  |
| North        | n: Gipp | s Street        |          |                |           |                |       |          |        |               |         |              |               |       |
| 7            | L2      | 82              | 2        | 86             | 2.4       | 0.593          | 32.1  | LOS C    | 22.6   | 160.7         | 0.79    | 0.73         | 0.79          | 40.0  |
| 8            | T1      | 927             | 17       | 976            | 1.8       | 0.593          | 25.1  | LOS B    | 22.8   | 161.9         | 0.79    | 0.72         | 0.79          | 50.2  |
| 9            | R2      | 111             | 1        | 117            | 0.9       | <b>*</b> 0.691 | 67.7  | LOS E    | 7.1    | 49.8          | 1.00    | 0.82         | 1.10          | 27.6  |
| Appr         | oach    | 1120            | 20       | 1179           | 1.8       | 0.691          | 29.8  | LOS C    | 22.8   | 161.9         | 0.81    | 0.73         | 0.82          | 45.8  |
| West         | t: Cado | lens Roa        | d        |                |           |                |       |          |        |               |         |              |               |       |
| 10           | L2      | 63              | 0        | 66             | 0.0       | 0.144          | 34.7  | LOS C    | 3.6    | 25.6          | 0.73    | 0.71         | 0.73          | 38.1  |
| 11           | T1      | 22              | 2        | 23             | 9.1       | 0.144          | 30.3  | LOS C    | 3.6    | 25.6          | 0.73    | 0.71         | 0.73          | 36.4  |
| 12           | R2      | 209             | 2        | 220            | 1.0       | *0.672         | 47.0  | LOS D    | 11.4   | 80.2          | 0.91    | 0.83         | 0.93          | 36.3  |
| Appr         | oach    | 294             | 4        | 309            | 1.4       | 0.672          | 43.1  | LOS D    | 11.4   | 80.2          | 0.86    | 0.80         | 0.87          | 36.6  |
| All<br>Vehie | cles    | 2702            | 63       | 2844           | 2.3       | 0.691          | 31.4  | LOS C    | 27.3   | 196.3         | 0.83    | 0.75         | 0.84          | 44.3  |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

### Site: 403 [Caddens Road x Gipps Street x Kent Road 2026 PM (Site Folder: Future - 2026)]

New Site

Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time) Variable Sequence Analysis applied. The results are given for the selected output sequence. Design Life Analysis (Final Year): Results for 6 years

#### Timings based on settings in the Site Phasing & Timing dialog (Demand & Sensitivity Analysis overrides) Phase Times determined by the program Phase Sequence: TCS Reference Phase: Phase A Input Phase Sequence: A, B<sup>\*</sup>, C<sup>\*</sup>, D, E, E1<sup>\*</sup>, E2<sup>\*</sup>

Output Phase Sequence: A, B\*, D, E, E2\*

(\* Variable Phase)

| Vehi         | cle M   | ovemen           | t Perfoi      | rmance           |           |                |      |                     |               |             |              |                   |        |                |
|--------------|---------|------------------|---------------|------------------|-----------|----------------|------|---------------------|---------------|-------------|--------------|-------------------|--------|----------------|
| Mov<br>ID    | Turn    | INP<br>VOLL      | JMES          | DEM,<br>FLO      | WS        | Deg.<br>Satn   |      | Level of<br>Service | QUI           | ACK OF      | Prop.<br>Que | Effective<br>Stop |        | Aver.<br>Speed |
|              |         | [ Total<br>veh/h | HV ]<br>veh/h | [ Total<br>veh/h | HV ]<br>% | v/c            | sec  |                     | [ Veh.<br>veh | Dist ]<br>m |              | Rate              | Cycles | km/h           |
| Sout         | h: Ken  | t Road           |               |                  |           |                |      |                     |               |             |              |                   |        |                |
| 1            | L2      | 230              | 8             | 273              | 3.5       | 0.747          | 33.7 | LOS C               | 31.7          | 227.9       | 0.87         | 0.83              | 0.87   | 40.0           |
| 2            | T1      | 897              | 25            | 1063             | 2.8       | 0.747          | 26.3 | LOS B               | 31.7          | 227.9       | 0.86         | 0.79              | 0.86   | 44.2           |
| 3            | R2      | 48               | 0             | 57               | 0.0       | *0.306         | 37.0 | LOS C               | 2.0           | 13.8        | 0.96         | 0.74              | 0.96   | 34.5           |
| Appr         | oach    | 1175             | 33            | 1393             | 2.8       | 0.747          | 28.2 | LOS B               | 31.7          | 227.9       | 0.87         | 0.79              | 0.87   | 42.6           |
| East         | Cadd    | ens Roac         | ł             |                  |           |                |      |                     |               |             |              |                   |        |                |
| 4            | L2      | 38               | 1             | 45               | 2.6       | 0.105          | 32.6 | LOS C               | 2.5           | 18.3        | 0.71         | 0.66              | 0.71   | 35.4           |
| 5            | T1      | 16               | 2             | 19               | 12.5      | 0.105          | 28.0 | LOS B               | 2.5           | 18.3        | 0.71         | 0.66              | 0.71   | 37.5           |
| 6            | R2      | 59               | 3             | 70               | 5.1       | 0.224          | 45.3 | LOS D               | 3.4           | 24.6        | 0.85         | 0.75              | 0.85   | 31.2           |
| Appr         | oach    | 113              | 6             | 134              | 5.3       | 0.224          | 38.5 | LOS C               | 3.4           | 24.6        | 0.78         | 0.71              | 0.78   | 33.4           |
| North        | n: Gipp | s Street         |               |                  |           |                |      |                     |               |             |              |                   |        |                |
| 7            | L2      | 82               | 2             | 97               | 2.4       | 0.756          | 37.6 | LOS C               | 30.6          | 218.0       | 0.91         | 0.83              | 0.91   | 37.4           |
| 8            | T1      | 927              | 17            | 1099             | 1.8       | <b>*</b> 0.756 | 29.9 | LOS C               | 30.6          | 218.0       | 0.89         | 0.80              | 0.89   | 42.1           |
| 9            | R2      | 111              | 1             | 132              | 0.9       | 0.713          | 67.2 | LOS E <sup>11</sup> | 8.0           | 56.1        | 1.00         | 0.83              | 1.11   | 27.7           |
| Appr         | oach    | 1120             | 20            | 1328             | 1.8       | 0.756          | 34.1 | LOS C               | 30.6          | 218.0       | 0.90         | 0.80              | 0.91   | 39.3           |
| West         | : Cado  | lens Roa         | d             |                  |           |                |      |                     |               |             |              |                   |        |                |
| 10           | L2      | 63               | 0             | 75               | 0.0       | 0.175          | 37.2 | LOS C               | 4.2           | 30.3        | 0.76         | 0.73              | 0.76   | 37.0           |
| 11           | T1      | 22               | 2             | 26               | 9.1       | 0.175          | 32.9 | LOS C               | 4.2           | 30.3        | 0.76         | 0.73              | 0.76   | 35.5           |
| 12           | R2      | 209              | 2             | 248              | 1.0       | *0.752         | 50.8 | LOS D               | 13.6          | 95.9        | 0.93         | 0.87              | 1.03   | 30.9           |
| Appr         | oach    | 294              | 4             | 349              | 1.4       | 0.752          | 46.6 | LOS D               | 13.6          | 95.9        | 0.88         | 0.83              | 0.95   | 32.4           |
| All<br>Vehic | cles    | 2702             | 63            | 3203             | 2.3       | 0.756          | 33.1 | LOS C               | 31.7          | 227.9       | 0.88         | 0.80              | 0.89   | 39.3           |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

11 Level of Service is worse than the Level of Service Target specified in the Parameter Settings dialog.

## Site: 603 [Caddens Road x Gipps Street x Kent Road 2026+DEV AM (Site Folder: Future - 2026 + DEV)]

New Site

Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time) Variable Sequence Analysis applied. The results are given for the selected output sequence. Design Life Analysis (Final Year): Results for 6 years

#### Timings based on settings in the Site Phasing & Timing dialog (Demand & Sensitivity Analysis overrides) Phase Times determined by the program Phase Sequence: TCS Reference Phase: Phase A Input Phase Sequence: A, B\*, C\*, D, E, E1\*, E2\* Output Phase Sequence: A, B\*, D, E, E2\* (\* Variable Phase)

| Vehi                 | cle M          | ovemen                          | t Perfo            | rmance                          |                          |                                    |                              |  |                             |                                 |                              |                              |                                     |                              |
|----------------------|----------------|---------------------------------|--------------------|---------------------------------|--------------------------|------------------------------------|------------------------------|--|-----------------------------|---------------------------------|------------------------------|------------------------------|-------------------------------------|------------------------------|
| Mov<br>ID            | Turn           | INP<br>VOLU<br>[ Total<br>veh/h |                    | DEM/<br>FLO<br>[ Total<br>veh/h |                          | Deg.<br>Satn<br>v/c                |                              | Level of<br>Service                            |                             | ACK OF<br>EUE<br>Dist]<br>m     | Prop.  <br>Que               | Effective<br>Stop<br>Rate    | Aver.<br>No.<br>Cycles              | Aver.<br>Speed<br>km/h       |
| South                | h: Ken         | t Road                          |                    |                                 |                          |                                    |                              |  |                             |                                 |                              |                              |                                     |                              |
| 1<br>2<br>3          | L2<br>T1<br>R2 | 234<br>897<br>48                | 8<br>25<br>0       | 277<br>1063<br>57               | 3.4<br>2.8<br>0.0        | 0.763<br>0.763<br>* 0.306          | 34.6<br>27.2<br>36.8         | LOS C<br>LOS B<br>LOS C                        | 32.4<br>32.4<br>1.9         | 232.6<br>232.6<br>13.6          | 0.89<br>0.87<br>0.96         | 0.84<br>0.80<br>0.74         | 0.89<br>0.87<br>0.96                | 39.5<br>43.5<br>34.6         |
| Appro                | oach           | 1179                            | 33                 | 1397                            | 2.8                      | 0.763                              | 29.1                         | LOS C  | 32.4                        | 232.6                           | 0.88                         | 0.81                         | 0.88                                | 42.1                         |
| East:                | Cadd           | ens Roac                        | I                  |                                 |                          |                                    |                              |  |                             |                                 |                              |                              |                                     |                              |
| 4<br>5<br>6          | L2<br>T1<br>R2 | 38<br>16<br>59                  | 1<br>2<br>3        | 45<br>19<br>70                  | 2.6<br>12.5<br>5.1       | 0.102<br>0.102<br>0.217            | 31.8<br>27.3<br>44.3         | LOS C<br>LOS B<br>LOS D                        | 2.5<br>2.5<br>3.3           | 18.1<br>18.1<br>24.3            | 0.70<br>0.70<br>0.84         | 0.66<br>0.66<br>0.75         | 0.70<br>0.70<br>0.84                | 35.7<br>37.8<br>31.5         |
| Appro                |                | 113                             | 6                  | 134                             | 5.3                      | 0.217                              | 37.7                         | LOS C  | 3.3                         | 24.3                            | 0.77                         | 0.71                         | 0.77                                | 33.6                         |
|                      |                | s Street                        | •                  |                                 | . <i>.</i>               |                                    |                              |  |                             |                                 |                              |                              |                                     |                              |
| 7<br>8<br>9<br>Appre | L2<br>T1<br>R2 | 82<br>927<br>111<br>1120        | 2<br>17<br>1<br>20 | 97<br>1099<br>132<br>1328       | 2.4<br>1.8<br>0.9<br>1.8 | 0.770<br>* 0.770<br>0.713<br>0.770 | 38.5<br>31.0<br>67.2<br>35.1 | LOS C<br>LOS C<br>LOS E <sup>11</sup><br>LOS C | 31.1<br>31.1<br>8.0<br>31.1 | 220.9<br>220.9<br>56.1<br>220.9 | 0.92<br>0.90<br>1.00<br>0.91 | 0.84<br>0.81<br>0.83<br>0.82 | 0.92<br>0.90<br><u>1.11</u><br>0.93 | 37.1<br>41.3<br>27.7<br>38.8 |
|                      |                | lens Roa                        |                    | 1020                            | 1.0                      | 0.110                              | 00.1                         | 2000   | 01.1                        | 220.0                           | 0.01                         | 0.02                         | 0.00                                | 00.0                         |
| 10                   | L2             | 63                              | 0                  | 75                              | 0.0                      | 0.171                              | 36.4                         | LOS C  | 4.2                         | 29.9                            | 0.75                         | 0.72                         | 0.75                                | 37.3                         |
| 11                   | T1             | 22                              | 2                  | 26                              | 9.1                      | 0.171                              | 32.1                         | LOS C  | 4.2                         | 29.9                            | 0.75                         | 0.72                         | 0.75                                | 35.7                         |
| 12                   | R2             | 219                             | 2                  | 258                             | 0.9                      | * 0.759                            | 50.5                         | LOS D  | 14.2                        | 100.0                           | 0.93                         | 0.87                         | 1.03                                | 31.0                         |
| Appro                | oach           | 304                             | 4                  | 359                             | 1.3                      | 0.759                              | 46.2                         | LOS D  | 14.2                        | 100.0                           | 0.88                         | 0.83                         | 0.95                                | 32.5                         |
| All<br>Vehic         | cles           | 2716                            | 63                 | 3218                            | 2.3                      | 0.770                              | 33.8                         | LOS C  | 32.4                        | 232.6                           | 0.89                         | 0.81                         | 0.90                                | 38.8                         |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

11 Level of Service is worse than the Level of Service Target specified in the Parameter Settings dialog.

### Site: 803 [Caddens Road x Gipps Street x Kent Road 2030 PM (Site Folder: Future - 2030)]

New Site

Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time) Variable Sequence Analysis applied. The results are given for the selected output sequence. Design Life Analysis (Final Year): Results for 10 years

#### Timings based on settings in the Site Phasing & Timing dialog (Demand & Sensitivity Analysis overrides) Phase Times determined by the program Phase Sequence: TCS **Reference Phase: Phase A** Input Phase Sequence: A, B\*, C\*, D, E, E1\*, E2\* Output Phase Sequence: A, B\*, D, E, E2\*

(\* Variable Phase)

| Vehi         | cle M   | ovemen           | t Perfor      | mance            |           |              |      |                     |               |               |              |                   |              |                |
|--------------|---------|------------------|---------------|------------------|-----------|--------------|------|---------------------|---------------|---------------|--------------|-------------------|--------------|----------------|
| Mov<br>ID    | Turn    | INF<br>VOLL      | JMES          | DEM.<br>FLO      | WS        | Deg.<br>Satn |      | Level of<br>Service | QUI           | ACK OF<br>EUE | Prop.<br>Que | Effective<br>Stop | Aver.<br>No. | Aver.<br>Speed |
|              |         | [ Total<br>veh/h | HV ]<br>veh/h | [ Total<br>veh/h | HV ]<br>% | v/c          | sec  |                     | [ Veh.<br>veh | Dist ]<br>m   |              | Rate              | Cycles       | km/h           |
| Sout         | h: Ken  | t Road           |               |                  |           |              |      |                     |               |               |              |                   |              |                |
| 1            | L2      | 230              | 8             | 295              | 3.5       | 0.809        | 36.1 | LOS C               | 36.7          | 264.0         | 0.92         | 0.87              | 0.93         | 38.8           |
| 2            | T1      | 897              | 25            | 1151             | 2.8       | 0.809        | 28.7 | LOS C               | 36.7          | 264.0         | 0.90         | 0.84              | 0.92         | 42.5           |
| 3            | R2      | 48               | 0             | 62               | 0.0       | *0.332       | 37.1 | LOS C               | 2.1           | 15.0          | 0.97         | 0.75              | 0.97         | 34.5           |
| Appr         | oach    | 1175             | 33            | 1508             | 2.8       | 0.809        | 30.5 | LOS C               | 36.7          | 264.0         | 0.91         | 0.84              | 0.92         | 41.2           |
| East         | Cadd    | ens Road         | ł             |                  |           |              |      |                     |               |               |              |                   |              |                |
| 4            | L2      | 38               | 1             | 49               | 2.6       | 0.114        | 32.7 | LOS C               | 2.7           | 19.9          | 0.71         | 0.67              | 0.71         | 35.4           |
| 5            | T1      | 16               | 2             | 21               | 12.5      | 0.114        | 28.1 | LOS B               | 2.7           | 19.9          | 0.71         | 0.67              | 0.71         | 37.5           |
| 6            | R2      | 59               | 3             | 76               | 5.1       | 0.248        | 46.4 | LOS D               | 3.7           | 27.0          | 0.86         | 0.76              | 0.86         | 30.8           |
| Appr         | oach    | 113              | 6             | 145              | 5.3       | 0.248        | 39.2 | LOS C               | 3.7           | 27.0          | 0.79         | 0.71              | 0.79         | 33.1           |
| North        | n: Gipp | s Street         |               |                  |           |              |      |                     |               |               |              |                   |              |                |
| 7            | L2      | 82               | 2             | 105              | 2.4       | 0.818        | 41.2 | LOS C               | 36.0          | 255.9         | 0.95         | 0.89              | 0.98         | 36.0           |
| 8            | T1      | 927              | 17            | 1189             | 1.8       | *0.818       | 33.8 | LOS C               | 36.0          | 255.9         | 0.92         | 0.86              | 0.96         | 39.6           |
| 9            | R2      | 111              | 1             | 142              | 0.9       | 0.772        | 68.9 | LOS E <sup>11</sup> | 8.8           | 62.1          | 1.00         | 0.86              | 1.18         | 27.3           |
| Appr         | oach    | 1120             | 20            | 1437             | 1.8       | 0.818        | 37.8 | LOS C               | 36.0          | 255.9         | 0.93         | 0.86              | 0.99         | 37.4           |
| West         | : Cadd  | lens Roa         | d             |                  |           |              |      |                     |               |               |              |                   |              |                |
| 10           | L2      | 63               | 0             | 81               | 0.0       | 0.190        | 37.4 | LOS C               | 4.6           | 32.9          | 0.77         | 0.73              | 0.77         | 36.9           |
| 11           | T1      | 22               | 2             | 28               | 9.1       | 0.190        | 33.1 | LOS C               | 4.6           | 32.9          | 0.77         | 0.73              | 0.77         | 35.4           |
| 12           | R2      | 209              | 2             | 268              | 1.0       | *0.822       | 56.1 | LOS D               | 15.8          | 111.6         | 0.95         | 0.91              | 1.14         | 29.4           |
| Appr         | oach    | 294              | 4             | 377              | 1.4       | 0.822        | 50.4 | LOS D               | 15.8          | 111.6         | 0.90         | 0.86              | 1.03         | 31.2           |
| All<br>Vehic | cles    | 2702             | 63            | 3467             | 2.3       | 0.822        | 36.1 | LOS C               | 36.7          | 264.0         | 0.91         | 0.85              | 0.96         | 37.7           |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

11 Level of Service is worse than the Level of Service Target specified in the Parameter Settings dialog.

## Site: 1003 [Caddens Road x Gipps Street x Kent Road 2030+DEV PM (Site Folder: Future - 2030 +DEV)]

New Site

Site Category: (None) Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site User-Given Cycle Time) Variable Sequence Analysis applied. The results are given for the selected output sequence. Design Life Analysis (Final Year): Results for 10 years

#### Timings based on settings in the Site Phasing & Timing dialog (Demand & Sensitivity Analysis overrides) Phase Times determined by the program Phase Sequence: TCS Reference Phase: Phase A Input Phase Sequence: A, B\*, C\*, D, E, E1\*, E2\* Output Phase Sequence: A, B\*, D, E, E2\* (\* Variable Phase)

| Vehicle Movement Performance            |                        |                                 |                        |                                 |                                 |   |                                      |  |                                    |   |                                      |                                      |                                      |                                      |
|---|------------------------|---------------------------------|------------------------|---------------------------------|---------------------------------|---|--------------------------------------|--|------------------------------------|---|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|
| Mov<br>ID                               | Turn                   | INP<br>VOLL<br>[ Total<br>veh/h |                        | DEM/<br>FLO<br>[ Total<br>veh/h |                                 | Deg.<br>Satn<br>v/c                         |                                      | Level of<br>Service                            |                                    | ACK OF<br>EUE<br>Dist]<br>m             | Prop.<br>Que                         | Effective<br>Stop<br>Rate            | Aver.<br>No.<br>Cycles               | Aver.<br>Speed<br>km/h               |
| South                                   | n: Kent                | t Road                          |                        |                                 |                                 |   |                                      |  |                                    |   |                                      |                                      |                                      |                                      |
| 1<br>2<br>3                             | L2<br>T1<br>R2         | 239<br>897<br>48                | 8<br>25<br>0           | 305<br>1151<br>62               | 3.4<br>2.8<br>0.0               | 0.828<br>0.828<br>* 0.332                   | 38.6<br>31.3<br>36.8                 | LOS C<br>LOS C<br>LOS C                        | 38.7<br>38.7<br>2.1                | 278.0<br>278.0<br>14.6                  | 0.94<br>0.92<br>0.97                 | 0.89<br>0.87<br>0.75                 | 0.97<br>0.96<br>0.97                 | 37.6<br>40.8<br>34.6                 |
| Appro                                   | bach                   | 1184                            | 33                     | 1517                            | 2.8                             | 0.828                                       | 33.0                                 | LOS C  | 38.7                               | 278.0                                   | 0.92                                 | 0.87                                 | 0.96                                 | 39.7                                 |
| East:                                   | Cadde                  | ens Roac                        | ł                      |                                 |                                 |   |                                      |  |                                    |   |                                      |                                      |                                      |                                      |
| 4<br>5<br>6<br>Appro                    |                        | 38<br>16<br>59<br>113           | 1<br>2<br>3<br>6       | 49<br>21<br>76<br>145           | 2.6<br>12.5<br>5.1<br>5.3       | 0.108<br>0.108<br>0.232<br>0.232            | 31.2<br>26.6<br>44.5<br>37.5         | LOS C<br>LOS B<br>LOS D<br>LOS C               | 2.6<br>2.6<br>3.6<br>3.6           | 19.4<br>19.4<br>26.4<br>26.4            | 0.69<br>0.69<br>0.84<br>0.77         | 0.66<br>0.66<br>0.75<br>0.71         | 0.69<br>0.69<br>0.84<br>0.77         | 36.0<br>38.0<br>31.4<br>33.7         |
| North                                   | : Gipp                 | s Street                        |                        |                                 |                                 |   |                                      |  |                                    |   |                                      |                                      |                                      |                                      |
| 7<br>8<br>9<br>Appro                    | L2<br>T1<br>R2<br>bach | 82<br>927<br>111<br>1120        | 2<br>17<br>1<br>20     | 105<br>1189<br>142<br>1437      | 2.4<br>1.8<br>0.9<br>1.8        | 0.849<br>* 0.849<br>0.842<br>0.849          | 45.9<br>38.6<br>73.2<br>42.6         | LOS D<br>LOS C<br>LOS F <sup>11</sup><br>LOS D | 38.5<br>38.5<br>9.2<br>38.5        | 273.7<br>273.7<br>64.7<br>273.7         | 0.97<br>0.95<br>1.00<br>0.96         | 0.94<br>0.91<br>0.90<br>0.91         | 1.05<br>1.03<br>1.31<br>1.06         | 34.1<br>37.0<br>26.4<br>35.1         |
| West                                    | Cadd                   | lens Roa                        | d                      |                                 |                                 |   |                                      |  |                                    |   |                                      |                                      |                                      |                                      |
| 10<br>11<br>12<br>Appro<br>All<br>Vehic |                        | 63<br>22<br>232<br>317<br>2734  | 0<br>2<br>2<br>4<br>63 | 81<br>28<br>292<br>401<br>3501  | 0.0<br>9.1<br>0.9<br>1.3<br>2.3 | 0.180<br>0.180<br>* 0.840<br>0.840<br>0.849 | 35.8<br>31.5<br>56.7<br>50.7<br>39.1 | LOS C<br>LOS C<br>LOS E <sup>11</sup><br>LOS D | 4.5<br>4.5<br>17.5<br>17.5<br>38.7 | 32.1<br>32.1<br>123.7<br>123.7<br>278.0 | 0.75<br>0.75<br>0.95<br>0.90<br>0.93 | 0.73<br>0.73<br>0.93<br>0.87<br>0.88 | 0.75<br>0.75<br>1.16<br>1.04<br>1.00 | 37.6<br>36.0<br>29.1<br>31.0<br>36.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Geometric Delay is included).

Queue Model: SIDRA Standard.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

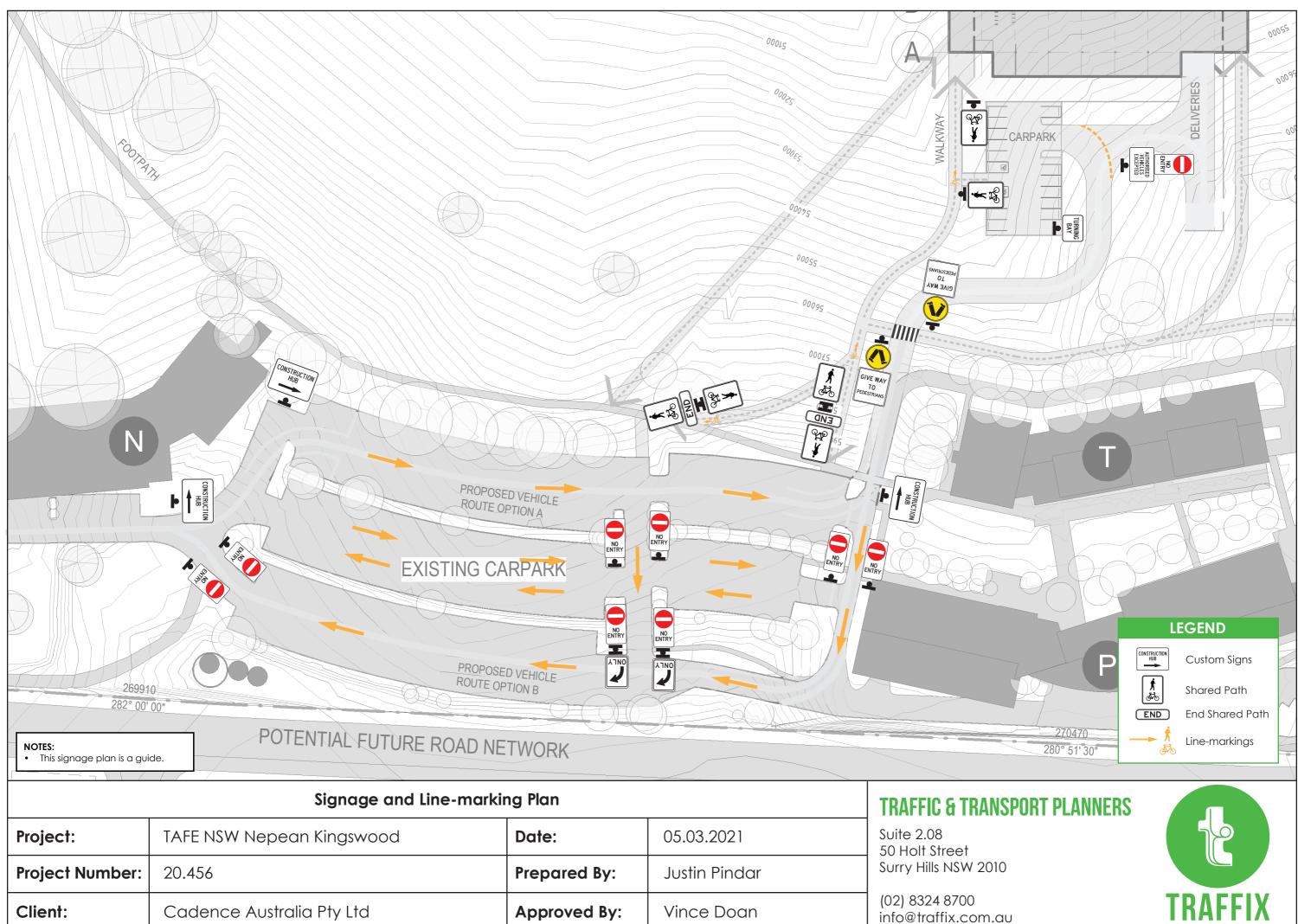
11 Level of Service is worse than the Level of Service Target specified in the Parameter Settings dialog.

\* Critical Movement (Signal Timing)

SIDRA INTERSECTION 9.0 | Copyright © 2000-2020 Akcelik and Associates Pty Ltd | sidrasolutions.com Organisation: TRAFFIX PTY LTD | Licence: NETWORK / 1PC | Created: Thursday, 6 May 2021 3:52:30 PM Project: T:\Synergy\Projects\20\20.456\Modelling\20.456m01v03 TRAFFIX.sip9

# APPENDIX G

Wayfinding, Signage & Line Marking Plan



| Signage and Line-marking Plan |                           |              |               |                                       |  |  |
|-------------------------------|---------------------------|--------------|---------------|---------------------------------------|--|--|
| Project:                      | TAFE NSW Nepean Kingswood | Date:        | 05.03.2021    | Suite 2.08<br>50 Holt Street          |  |  |
| Project Number:               | 20.456                    | Prepared By: | Justin Pindar | Surry Hills NSW 2010                  |  |  |
| Client:                       | Cadence Australia Pty Ltd | Approved By: | Vince Doan    | (02) 8324 8700<br>info@traffix.com.au |  |  |

au



SEAR's Requirements

## Planning Secretary's Environmental Assessment Requirements

## Section 4.12(8) of the *Environmental Planning and Assessment Act* 1979 Schedule 2 of the Environmental Planning and Assessment Regulation 2000

| Application Number   | SSD-8571481  |
|----------------------|--|
| Proposal Name        | TAFE NSW Western Sydney Construction Hub   |
| Location             | TAFE NSW Nepean Kingswood campus, 2-44 O'Connell Street, Kingswood   |
| Applicant            | TAFE NSW   |
| Date of Issue        | DRAFT  |
| General Requirements | <ul> <li>The Environmental Impact Statement (EIS) must be prepared in accordance with and meet the minimum requirements of clauses 6 and 7 of Schedule 2 the Environmental Planning and Assessment Regulation 2000 (the Regulation).</li> <li>Notwithstanding the key issues specified below, the EIS must include an environmental risk assessment to identify the potential environmental impacts associated with the development.</li> <li>Where relevant, the assessment of the key issues below, and any other significant issues identified in the risk assessment, must include: <ul> <li>adequate baseline data</li> <li>consideration of potential cumulative impacts due to other development in the vicinity (completed, underway or proposed)</li> <li>measures to avoid, minimise and if necessary, offset the predicted impacts, including detailed contingency plans for managing any significant risks to the environment.</li> </ul> </li> <li>The EIS must be accompanied by a report from a qualified quantity surveyor providing: <ul> <li>a detailed calculation of the capital investment value (CIV) (as defined in clause 3 of the Regulation) of the proposal, including details of all assumptions and components from which the CIV calculation is derived</li> <li>an estimate of the jobs that will be created by the future development during the construction and operational phases of the development</li> </ul> </li> </ul> |
| Key Issues           | The EIS must address the following specific matters:   |
|                      | <ul> <li><b>1. Statutory and Strategic Context</b></li> <li>Address the statutory provisions contained in all relevant environmental planning instruments, including: <ul> <li>Biodiversity Conservation Act 2016;</li> <li>State Environmental Planning Policy (State &amp; Regional Development) 2011;</li> <li>State Environmental Planning Policy (Infrastructure 2007);</li> <li>State Environmental Planning Policy (Educational Establishments and Child Care Facilities) 2017;</li> <li>State Environmental Planning Policy No. 64 – Advertising and Signage;</li> <li>State Environmental Planning Policy No. 55 – Remediation of Land;</li> <li>Draft State Environmental Planning Policy (Environment); and</li> <li>Penrith Local Environmental Plan 2010</li> </ul> </li> </ul>   |

Detail the nature and extent of any prohibitions that apply to the development.

#### **Development Standards**

Identify compliance with the development standards applying to the site and provide justification for any contravention of the development standards.

#### Provisions

Adequately demonstrate and document in the EIS how each of the provisions in the listed instruments are addressed, including reference to necessary technical documents.

#### 2. Policies

Address the relevant planning provisions, goals and strategic planning objectives in the following:

- NSW State Priorities;
- The Greater Sydney Regional Plan, A Metropolis of three cities
- Future Transport Strategy 2056 and supporting plans;
- · State Infrastructure Strategy 2018 2038 Building the Momentum;
- Sydney's Cycling Future 2013;
- Sydney's Walking Future 2013;
- Sydney's Bus Future 2013;
- · Crime Prevention Through Environmental Design (CPTED) Principles

Better Placed: An integrated design policy for the built environment of New South Wales (Government Architect NSW (GANSW), 2017);

- · Healthy Urban Development Checklist (NSW Health, 2009);
- · Draft Greener Places Design Guide;
- Western Sydney District Plan; and
- · Penrith Development Control Plan 2014.

#### 3. Operation

Provide details of the existing and proposed operations, including staff and student numbers, and hours of operation.

Provide a detailed justification of suitability of the site to accommodate the proposal.

#### 4. Built Form and Urban Design

Address the height, density, bulk and scale, setbacks and interface of the proposal in relation to the surrounding development, topography, streetscape and any public open spaces.

Address design quality and built form, with specific consideration of the overall site layout, streetscape, open spaces, façade, rooftop, massing, setbacks, building articulation, materials and colours.

Provide details of any digital signage boards, including size, location and finishes.

• Detail how services, including but not limited to waste management, loading zones, and mechanical plant are integrated into the design of the development.

- Provide detailed site and context analysis to justify the proposed site planning and design approach including massing options and preferred strategy for future development.
- Provide a detailed site-wide landscape strategy, including consideration of integration with built form, security, shade, topography and existing vegetation.
- Provide a visual impact assessment that identifies any potential impacts on the surrounding built environment and landscape including views to and from the site and any adjoining heritage items.
- · Address CPTED Principles.
  - Provide details of integration with the wider campus site and the adjoining

Western Sydney University site (if relevant), including contextual integration and spatial arrangements, vehicle and pedestrian connections, landscaping, and consideration of significant view corridors & preservation of significant views and features, where relevant.

#### 5. Environmental Amenity

- Assess amenity impacts on the surrounding locality, including solar access, visual privacy, visual amenity, overshadowing, wind impacts and acoustic impacts. A high level of environmental amenity for any surrounding residential land uses must be demonstrated.
- Conduct a view analysis to the site from key vantage points and streetscape locations (photomontages or perspectives should be provided showing the building and likely future development).
- Include a lighting strategy and measures to reduce spill into the surrounding sensitive receivers.

#### 6. Staging

Provide details regarding the staging of the proposed development (if any).

#### 7. Transport and Accessibility

Include a transport and accessibility impact assessment, which details, but not limited to the following:

- accurate details of the current daily and peak hour vehicle, existing and future public transport networks and pedestrian and cycle movement provided on the road network located adjacent to the proposed development;
- details of estimated total daily and peak hour trips generated by the proposal, including vehicle, public transport, pedestrian and bicycle trips based on surveys of the existing TAFE NSW Nepean Kingswood Campus facilities and similar education facilities within the local area;
- cumulative impacts of all trips generated by the development and the existing TAFE NSW Nepean Kingswood Campus, as well as the development potential identified in the Quarter Precinct Master Plan and Western Sydney University Redevelopment Plan;
- existing car parking capacity and utilisation on streets within a 400 metre radius from the site on a typical weekday covering at least one hour before and after the proposed hours of operation (including night classes);
- the adequacy of existing public transport or any future public transport infrastructure and services within the vicinity of the site, pedestrian and bicycle networks and associated infrastructure to meet the likely future demand of the proposed development;
- measures to integrate the development with the existing/future public transport network;
- impact of trips generated by the development on the area-wide network, with consideration of the cumulative impacts of the development on the surrounding roads and intersections in the context of any other approved planning proposals and developments in the precinct and surrounds, should be considered. Including the impact of nearby intersections and the need/associated funding for upgrading or road improvement works, if required;
  - an assessment of the forecast impacts on traffic volume generated on road safety and capacity of road network including consideration of cumulative impacts at key intersections using SIDRA or similar traffic model as prescribed by Transport for New South Wales (TfNSW). The traffic modelling should consider the scenarios of year 2026, 2031, 2036 and the year until the facility ceases operation. These should include, but not be limited to:
    - o Great Western Highway/O'Connell Street/French Street
    - o Great Western Highway/Bringelly Road

- o Gipps Street (Werrington Arterial)/Caddens Road;
- the identification of infrastructure required to ameliorate any impacts on traffic efficiency and road safety impacts associated with the proposed development, including details on improvements required to affected intersections, additional bus routes along bus capable roads (i.e. minimum 3.5 m wide travel lanes), additional bus stops or bus bays;
- details of travel demand management measures to minimise the impact on general traffic and bus operations, including details of a location-specific sustainable travel plan (Green Travel Plan and specific Workplace travel plan) and the provision of facilities to increase the non-car mode share for travel to and from the site;
- the proposed walking and cycling access arrangements and connections to public transport services;
- the design of the proposed cycle and pedestrian entry connecting to the Great Western Highway shared path should ensure that there are clear sight lines between the cyclists from the development and the faster moving cyclists on the Great Western Highway;
- the proposed access arrangements, including car and bus pick-up/drop-off facilities, and measures to mitigate any associated traffic impacts and impacts on public transport, pedestrian and bicycle networks, including pedestrian crossings and refuges and speed control devices and zones;
- proposed bicycle parking provision, including end of trip facilities, in secure, convenient, accessible areas close to main entries incorporating lighting and passive surveillance;
- details of vehicle circulation, proposed number of on-site car parking spaces for staff, students and visitors and corresponding compliance with appropriate parking codes and justification for the level of car parking provided on-site;
- any short term reduction of existing car spaces for staff, students and visitors due to the proposed construction works (if any), and the proposed location, operational and functional characteristics of the re-allocated staff, students and visitors car parking (if applicable);
- details of the proposed site access and the parking provisions associated with the proposed development including compliance with the requirements of the relevant Australian Standards (i.e. turn paths, sight distance requirements, aisle widths, etc.);
- an assessment of the cumulative on-street parking impacts of cars and bus pick-up/drop-off, staff parking and any other parking demands associated with the development and provide any associated recommendations to ameliorate any such impacts;
- an assessment of road and pedestrian safety adjacent to the proposed development and the details of required road safety measures and personal safety in line with CPTED;
- emergency vehicle access, service vehicle access, delivery and loading arrangements and estimated service vehicle movements (including vehicle type and the likely arrival and departure times);
  - the preparation of a preliminary Construction Traffic and Pedestrian Management Plan to demonstrate the proposed management of the impact in relation to construction traffic addressing the following:
  - assessment of cumulative impacts associated with other construction activities (if any);
  - o an assessment of road safety at key intersections and locations subject to heavy vehicle construction traffic movements and high pedestrian activity;
  - details of construction program detailing the anticipated construction duration and highlighting significant and milestone stages and events during the construction process;
  - o details of anticipated peak hour and daily construction vehicle movements to

and from the site;

- details of on-site car parking and access arrangements of construction vehicles, construction workers to and from the site, emergency vehicles and service vehicles; and
- o details of temporary cycling and pedestrian access during construction. Alternate methods for gaining the most accurate traffic analysis data may be agreed with TfNSW, if required.

### Relevant Policies and Guidelines:

- Guide to Traffic Generating Developments (Roads and Maritime Services, 2002)
   EIS Guidelines Road and Related Facilities (Department of Urban Affairs and Planning (DUAP), 1996)
- · Cycling Aspects of Austroads Guides
- NSW Planning Guidelines for Walking and Cycling (Department of Infrastructure, Planning and Natural Resources (DIPNR), 2004)
- Austroads Guide to Traffic Management Part 12: Traffic Impacts of Development Standards Australia AS2890.1 (Off-Street car parking)
- Standards Australia AS2890.2 (Parking Facilities Off-street commercial vehicle facilities)
- · Standards Australia AS2890.3 (Bicycle Parking Facilities)
- Standards Australia AS2890.5 (On-street parking)
- Standards Australia AS2890.6 (Off-street parking for people with disabilities)
- Werrington Enterprise Living + Learning Precinct Strategy
- Penrith Health & Education Precinct Strategic Vision

#### 8. Ecologically Sustainable Development (ESD)

- Detail how ESD principles (as defined in clause 7(4) of Schedule 2 of the Regulation) will be incorporated in the design and ongoing operation phases of the development;
- Include a framework for how the future development will be designed to consider and reflect national best practice sustainable building principles to improve environmental performance and reduce ecological impact. This should be based on a materiality assessment and include waste reduction design measures, future proofing, use of sustainable and low-carbon materials, energy and water efficient design (including water sensitive urban design) and technology and use of renewable energy;
- Include preliminary consideration of building performance and mitigation of climate change, including consideration of Green Star Performance;
- Include an assessment against an accredited ESD rating system or an equivalent program of ESD performance. This should include a minimum rating scheme target level; and
- Provide a statement regarding how the design of the future development is responsive to the CSIRO projected impacts of climate change, specifically:
  - o hotter days and more frequent heatwave events
  - o extended drought periods
  - o more extreme rainfall events
  - o gustier wind conditions
  - how these will inform landscape design, material selection and social equity aspects (respite/shelter areas).

### **Relevant Policies and Guidelines:**

- NSW and ACT Government Regional Climate Modelling (NARCliM) climate change projections.
- 9. Heritage
  - Provide a statement of significance and an assessment of the impact on the

heritage significance of the heritage items on the site in accordance with the guidelines in the NSW Heritage Manual (Heritage Office and DUAP, 1996); and Address any archaeological potential and significance on the site and the impacts the development may have on this significance.

#### 10. Aboriginal Heritage

- Identify and describe the Aboriginal cultural heritage values that exist across the site and document these in an Aboriginal Cultural Heritage Assessment Report (ACHAR). This may include the need for surface survey and test excavation;
- Identify and address the Aboriginal cultural heritage values in accordance with the Guide to investigating, assessing and reporting on Aboriginal Cultural Heritage in NSW (Office of Environment and Heritage (OEH), 2011) and Code of Practice for Archaeological Investigations of Aboriginal Objects in NSW (OEH, 2010), and in consultation with Heritage NSW;
- Document consultation with Aboriginal people in accordance with Aboriginal Cultural Heritage Consultation Requirements for Proponents 2010 (Department of Environment, Climate Change and Water) (DECCW). The significance of cultural heritage values of Aboriginal people who have a cultural association with the land are to be documented in the ACHAR;
- Identify, assess and document all impacts on the Aboriginal cultural heritage values in the ACHAR;
- Demonstrate attempts to avoid any impact upon cultural heritage values and identify any conservation outcomes. Where impacts are unavoidable, the ACHAR and EIS must outline measures proposed to mitigate impacts. Any objects recorded as part of the assessment must be documented and notified to Heritage NSW and the Environment, Energy and Science Group of the Department of Planning, Industry and Environment; and
- Outline procedures to be followed if Aboriginal objects are found at any stage of the life of the project to formulate appropriate measures to manage unforeseen impacts.

#### 11. Social Impacts

Include an assessment of the social consequences of the building's relative location and decanting activities if proposed.

#### 12. Noise and Vibration

- Identify and provide a quantitative assessment of the main noise and vibration generating sources during demolition, site preparation, bulk excavation, construction. Outline measures to minimise and mitigate the potential noise impacts on surrounding occupiers of land.
- Identify and assess operational noise, including consideration of any public-address system, workshop activities, mechanical services (e.g. air conditioning plant), use of site facilities for events, and any out of hours community use of facilities, and outline measures to minimise and mitigate the potential noise impacts on surrounding occupiers of land.

#### **Relevant Policies and Guidelines:**

- NSW Noise Policy for Industry 2017 (NSW Environment Protection Authority (EPA)
- Interim Construction Noise Guideline (Department of Environment and Climate Change, 2009)
- Assessing Vibration: A Technical Guideline 2006 (Department of Environment and Conservation, 2006)
- Development Near Rail Corridors and Busy Roads Interim Guideline (Department of Planning, 2008)
  - NSW Road Noise Policy (DECCW, 2011)

Australian Standard 2363:1999 Acoustics - Measurement of noise from helicopter operations.

### 13. Contamination

Assess and quantify any soil and groundwater contamination and demonstrate that the site is suitable for the proposed use in accordance with SEPP 55.

### Relevant Policies and Guidelines:

- Managing Land Contamination: Planning Guidelines SEPP 55 Remediation of Land (DUAP, 1998)
- Sampling Design Guidelines (EPA, 1995)
- Consultants reporting on contaminated land: Contaminated Land Guidelines (EPA, 2020)
  - National Environment Protection (Assessment of Site Contamination) Measure (National Environment Protection Council, as amended 2013)

#### 14. Utilities

Prepare an Infrastructure Management Plan in consultation with relevant agencies, detailing information on the existing capacity and any augmentation and easement requirements of the development for the provision of utilities including staging of infrastructure;

 Detail impacts of any existing infrastructure assets of utility stakeholders from demolition/construction and any proposed mitigation/protection measures; and

Prepare an Integrated Water Management Plan detailing any proposed alternative water supplies, proposed end uses of potable and non-potable water, and water sensitive urban design.

#### 15. Water Quality

- Demonstrate that all practical measures to avoid or minimise water pollution and protect human health and the environment from harm are investigated and implemented; and
- Identify sensitive receiving environments and develop a strategy to avoid or minimise impacts on these environments.

#### **Relevant Policies and Guidelines:**

- ANZECC Guidelines and Water Quality Objectives in NSW (DEC, 2006)
- Australian and New Zealand Guidelines for Fresh and Marine Water Quality (ANZG, 2018)
- Approved Methods for the Sampling and Analysis of Water Pollutants in NSW (DECC, 2008)

Managing Urban Stormwater, Soils and Construction Volume 1 (Landcom 2004) and Volume 2 (A. Installation of Services; B. Waste Landfills; C. Unsealed Roads; D. Main Roads; E. Mines and Quarries) (DECC, 2008) NSW Water Quality and River Flow Objectives at

http://www.environment.nsw.gov.au/ieo/index.htm

### 16. Water-related Infrastructure Requirements

Determine service demands following servicing investigations and demonstrate that satisfactory arrangements for drinking water, wastewater, and if required, recycled water services have been made.

Obtain endorsement and/or approval from Sydney Water to ensure that the proposed development does not adversely impact on any existing water, wastewater or stormwater main, or any other Sydney Water asset, including any easement of property.

17. Integrated Water Cycle Management

Detail any sustainability initiatives that will minimise/reduce the demand for drinking water, including any alternative water supply and end uses of drinking and non-drinking water that may be proposed, and demonstrate water sensitive urban design (principles are used), and any water conservation measures that are likely to be proposed.

#### 18. Stormwater Management

Detail any steps/measures to be taken to protect existing stormwater assets, such as avoiding over and/or adjacent to stormwater assets and building bridges over stormwater assets, if required. Outline measures to minimise or eliminate flooding, degradation of water quality, and avoid adverse impacts on any heritage items, and create pipeline easements where required.

Detail how the design of the proposal would ensure that post-development stormwater flows match pre-development flows. Provide, where applicable, a preliminary stormwater management plan for the development that:

- is prepared by a suitably qualified person in consultation with Council and any other relevant drainage authority;
- details of proposed drainage design for the site including on-site detention facilities, water quality measures and the nominated discharge point;
- demonstrates compliance with Council or other drainage authority requirements; and
- stormwater plans detailing the proposed methods of drainage without impacting on the downstream properties.

#### **Relevant Policies and Guidelines:**

- Guidelines for developments adjoining land managed by the Office of Environment and Heritage (OEH, 2013).
- Stormwater Drainage Specification for Building Developments (Penrith City Council, 2018)
- Water Sensitive Urban Design Policy (Penrith City Council, 2013) and Technical Guidelines (Penrith City Council, 2015).

#### **19. Contributions**

Address Council's 'Section 7.11 Werrington Enterprise Living and Learning (WELL) Precinct Development Contributions Plan' and/or details of any Voluntary Planning Agreement which may be required to be amended because of the proposed development.

#### 20. Drainage

Detail measures to minimise operational water quality impacts on surface waters and groundwater.

#### **Relevant Policies and Guidelines:**

Guidelines for developments adjoining land managed by the Office of Environment and Heritage (OEH, 2013).

### 21. Flooding

Identify flood risk on-site (detailing the most recent flood studies for the project area) and consideration of any relevant provisions of the NSW Floodplain Development Manual (DIPNR, 2005) and Council flood studies, including the potential effects of climate change, sea level rise and an increase in rainfall intensity. If there is a material flood risk, include design solutions for mitigation.

#### 22. Bushfire

Prepare a Bush Fire Assessment Report that addresses the requirements for Special Fire Protection Purpose as detailed in Planning for Bush Fire Protection 2019 (NSW RFS) (PBP-2019). The report must address the extent to which the proposed development conforms with or deviates from the specifications set out in PBP-2019, including a classification of the vegetation on and surrounding the development (out to a distance of 140 metres from the boundaries of the site).

 Address the bush fire risk posed by existing grassland surrounds or areas subject to revegetation and demonstrate that the asset protections zones can comply with Table A1.12.1 of PBP-2019.

### 23. Biodiversity Assessment

Provide a Biodiversity Development Assessment Report (BDAR) that assesses the biodiversity impacts of the proposed development in accordance with the requirements of the Biodiversity Conservation Act 2016, Biodiversity Conservation Regulation 2017 and Biodiversity Assessment Method, except where a BDAR waiver has been issued in relation to the development or the development is located on biodiversity certified land.

Where a BDAR is not required because a BDAR waiver has been issued in relation to the development, provide:

- a copy of the BDAR waiver and demonstrate that the proposed development is consistent with that covered in the BDAR waiver; and
- an assessment of flora and fauna impacts where significant vegetation or flora and fauna values would be affected by the proposed development.

### 24. Water and Soils

- · Provide:
  - o an assessment of potential impacts on surface and groundwater (quality and quantity), soil, related infrastructure and watercourse(s) where relevant;
  - details of measures and procedures to minimise and manage the generation and off-site transmission of sediment, dust and fine particles; and
  - o an assessment of salinity and acid sulphate soil impacts, including a Salinity Management Plan and/or Acid Sulphate Soils Management Plan, where relevant.

#### Relevant Policies and Guidelines:

- Managing Urban Stormwater Soils & Construction Volume 1 2004 (Landcom)
   Approved Methods for the Modelling and Assessment of Air Pollutants in NSW (EPA)
- Guidelines for development adjoining land managed by the Office of Environment and Heritage (OEH, 2013)

#### 25. Waste

Identify, quantify and classify the likely waste streams to be generated during construction and operation and describe the measures to be implemented to manage, reuse, recycle and safely dispose of this waste. Identify appropriate servicing arrangements (including but not limited to, waste management, loading zones, mechanical plant) for the site.

#### Relevant Policies and Guidelines:

Waste Classification Guidelines (EPA, 2014)

#### 26. Construction Hours

 Identify proposed construction hours and provide details of the instances where it is expected that works will be required to be carried out outside the standard construction hours.

Plans and Documents The EIS must include all relevant plans, architectural drawings, diagrams and relevant documentation required under Schedule 1 of the Regulation. Provide these

| as part | of the EIS rather than as separate documents.   |
|---------|---|
| · As    | tion, the EIS must include the following:<br>section 10.7(2) and (5) Planning Certificates (previously Section 149(2) and (5  |
| · Are   | anning Certificate)<br>chitectural drawings showing key dimensions, RLs, scale bar and north point,   |
| o<br>O  | Huding:<br>plans, sections and elevation of the proposal at no less than 1:200;<br>illustrated materials schedule including physical or digital samples board<br>with correct proportional representation of materials, nominated colours and               |
| 0<br>0  | finishes;<br>details of proposed signage, including size, location and finishes;<br>detailed annotated wall sections at 1:20 scale that demonstrate typical<br>cladding, window and floor details, including materials and general<br>construction quality; |
|         | site plans and operations statement;<br>e Survey Plan, showing existing levels, location and height of existing and   |
| -       | acent structures / buildings and site boundaries;<br>e Analysis and Context Plans, including:   |
| 0       | site and context plans that demonstrate principles for future development<br>and expansion, built form character and open space network;  |
| 0       | precinct scale plan showing relationship of the proposal to any proposed development on surrounding land;   |
| 0       | active transport linkages with existing, proposed and potential footpaths and bicycle paths and public transport links; and   |
| 0       | site and context plans that demonstrate principles for future network, active transport linkages with existing, proposed and potential footpaths and  |
|         | bicycle paths and public transport links.<br>diment and Erosion Control Plan;   |
|         | adow Diagrams;<br>w analysis, photomontages and architectural renders, including from those   |
|         | m public vantage points;<br>ndscape architectural drawings showing key dimensions, RLs, scale bar and   |
| no      | rth point, including:   |
| 0<br>0  | integrated landscape plans at appropriate scale, with detail of new and retained planting, shade structures, materials and finishes; plan identifying significant trees, trees to be removed and trees to be  |
|         | retained or transplanted;   |
|         | sign report to demonstrate how design quality will be achieved in accordance<br>h the above Key Issues including:   |
| 0<br>0  | architectural design statement;<br>diagrams, structure plan, illustrations and drawings to clarify the design<br>intent of the proposal;  |
| 0<br>0  | detailed site and context analysis;<br>analysis of options considered to justify the proposed site planning and<br>design approach;   |
| 0       | visual impact assessment identifying potential impacts on the surrounding<br>built environment and adjoining heritage items;  |
| 0       | summary of feedback provided by GANSW and NSW State Design Review Panel (SDRP) and responses to this advice;  |
| 0       | summary report of consultation with the community and response to any feedback provided; and  |
| 0       | how Aboriginal culture and heritage has been considered and incorporated into the design;   |
|         | otechnical and Structural Report;<br>cessibility Report;  |

|   | <ul> <li>Arborist Report;</li> <li>Salinity Investigation Report (where required);</li> <li>Noise and Vibration Assessment;</li> <li>Contamination Assessment;</li> <li>Acid Sulphate Soils Management Plan (where required); and</li> <li>Schedule of materials and finishes.</li> </ul>   |
|---|---|
| Consultation                            | During the preparation of the EIS, you must consult with the relevant local, State or<br>Commonwealth Government authorities, service providers, community groups,<br>special interest groups, including local Aboriginal land councils and registered<br>Aboriginal stakeholders, and affected landowners. In particular, you must consult<br>with:<br>· Penrith City Council;<br>· Government Architect NSW (through the NSW SDRP process) (GANSW);<br>· Transport for NSW (TfNSW);<br>· Transport for NSW (Roads and Maritime Services) (TfNSW RMS).<br>Consultation with GANSW, TfNSW and TfNSW (RMS) should commence as soon as<br>practicable to agree the scope of investigation.<br>The EIS must outline and describe the consultation process undertaken and the<br>issues raised, and identify where the design of the development has been amended<br>in response to these issues. Where amendments have not been made to address an<br>issue, a short explanation must be provided. |
| Further consultation<br>after two years | If you do not lodge a development application and EIS for the development within two years of the issue date of these SEARs, you must consult further with the Planning Secretary in relation to the preparation of the EIS.  |
| References                              | The assessment of the key issues listed above must consider relevant guidelines, policies, and plans as identified.   |