# Design for a better future / 

HUNT ARCHITECTS
ALLIED PINNACLE FLOUR AND MAIZE MILL PROPOSED MODIFICATION (DA-318-12-2004)

# APPENDIX K 

TRAFFIC AND TRANSPORT MEMORANDUM

| TO: | Mark Maund |
| :--- | :--- |
| FROM: | Sam McCormick <br> Chris Chun |
| SUBJECT: | Allied Pinnacle Traffic and Transport Memorandum |
| OUR REF: | PS124818-P\&M-MEM-001-RevA |
| DATE: | $\mathbf{6}$ October 2021 |

This memorandum addresses the traffic and transport impacts associated with the proposed upgrades to the Allied Pinnacle site development located at Picton Road in Maldon NSW, shown in Figure 1.1 below.


Source: nearmap
Figure 1.1 Allied Pinnacle site

Within the Wollondilly Shire Council, the site is located in an industrial zone with adjacent residential and rural areas around Picton, Douglas Park and Wilton. Proposed upgrades to the site include an external expansion to the northwest corner of the existing building

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The WSP team was unable to attend a site visit based on the current state-wide lockdown preventing non-essential travel. Additionally, traffic surveys were originally scoped although deemed not suitable as they would likely show an inaccurate measure of very low traffic volumes with the state in lockdown. Therefore, historical traffic survey data from Tuesday 10 March 2020 has been provided by Trans Traffic Survey (TTS) from before the COVID pandemic. This survey was conducted at the Picton Road / Menangle Road intersection upstream of the site and has been reviewed to assess the impact of the proposed development. This data enabled an investigation into the worst-case scenario for traffic and helped to inform potential impacts to the surrounding network. Detailed surveys are available in Appendix A.

Based on these traffic surveys, peak hours for the site are:

- AM peak 7:30 am - 8:30 am
- PM peak 4:15 pm - 5:15 pm

For this assessment, a $1 \%$ growth per annum (p.a.) has been applied as a conservative measure to estimate the future background volumes for 2030 scenarios. The following scenarios have been modelled to assess the impacts of the expanded site:

- 2020 Existing - existing layout and arrangement using 2020 survey data (TTS).
- 2020 with Development - existing layout and arrangement using 2020 survey data (TTS) plus development generated traffic.
- 2030 Future Base - existing layout and arrangement using 2020 survey data (TTS) with $1 \%$ p.a. growth rate to 2030 .
- 2030 with Development - existing layout and arrangement using 2020 survey data (TTS) with $1 \%$ p.a. growth rate to 2030 plus development generated traffic.

A previous development application report, Report on the Assessment Development Application No DA-318-12-2004-I (Department of Infrastructure, Planning and Natrual Resources, July 2005) ("2004 DA Report"), has been reviewed with regards to the traffic and transport impacts section (Section 6.4). Some of the information has been brought through in this assessment including assumptions around the original development's traffic generation numbers for both staff and visitors. Similarly, the directional splits of this traffic have been brought through in this investigation with the assumption that these traffic movements have not changed.

## 1. TRAFFIC GENERATION AND DISTRIBUTION

## TRAFFIC GENERATION

The site's expansion is relatively small compared to the existing development. Likely additional traffic generated by the site has been provided by the client including to following employee numbers:

- 5 trucks (heavy vehicles, HV) per day
- 10 passenger vehicles (light vehicles, LV) per day

The expansions size and purpose as a combined warehouse extension and engineering area indicate it is for employees only and thus no additional visitor numbers have been included.

It is assumed that the generated vehicle numbers all enter the site during the AM peak and all exit during the PM peak, shown in Table 1.1.

Table 1.1 Peak distribution

|  | IN | OUT |
| :--- | :--- | :--- |
| AM | $100 \%$ | $0 \%$ |
| PM | $0 \%$ | $100 \%$ |

## TRAFFIC DISTRIBUTION

The 2004 DA Report assumes 28 ( $52 \%$ ) of the generated 54 employee light vehicles access the site from the west, with $26(48 \%)$ light vehicles accessing from the east. All heavy vehicles are assumed to access the site from the east via the Hume Highway only.

Similarly, the 2004 DA Report assumes all construction vehicles originate from Metropolitan Sydney and therefore access the site by using the Hume Highway. This means all entering construction vehicles to site enter turning left in from Picton Road and exit right out onto Picton Road.

These directional splits are shown in Figure 1.1 where light vehicle and heavy vehicles volumes are represented by green and red numbers respectively.


## Figure 1.1 Directional splits

As the site has not changed in size since 2004, it is assumed that the development's traffic generation has not changed. Considering this, Table 1.2 shows existing traffic generation and Figure 1.2 displays their movements in and out of the site.

Table 1.2 Existing site traffic generation

|  | EMPLOYEES | VISITORS | TOTAL |
| :--- | :--- | :--- | :--- |
| Light Vehicles (LV) | 54 | 21 | $\mathbf{7 5}$ |
| Heavy Vehicles (HV) | 33 | 2 | $\mathbf{3 5}$ |



Figure 1.2 Distributed existing site traffic generation
Based on these assumptions above, additional traffic to be generated by the increased development is distributed as shown in Figure 1.3.


Figure 1.3 Additional development traffic generation
The total generation of the development, including existing and proposed based on the proposed upgrades, will therefore be $\mathbf{8 5}$ light vehicles and $\mathbf{4 0}$ heavy vehicles with an assumption that all of these enter the site during the AM peak all exit during the PM peak to represent a worst-case scenario.

## 2. OPERATIONAL IMPACTS

### 2.1 INTERSECTION OPERATION

The operation of the site access intersection has been assessed using the SIDRA Intersection modelling software, adopting the estimated 2020 base traffic volumes and the site generated traffic volumes for a typical weekday. An aerial image of the intersection is provided in Figure 2.1, with the SIDRA layout provided in Figure 2.2.


Source: Nearmap
Figure 2.1 Intersection of Picton Road and site access (aerial)


Source: SIDRA Intersection
Figure 2.2 Intersection of Picton Road and site access (SIDRA layout)
The Traffic Modelling Guidelines (Transport for NSW - formerly Roads and Maritime Services, 2013) specifies that intersection operation is generally measured by degree of saturation, Level of Service and 95th percentile base of queue distance.

SIDRA Intersection measures these elements, with the intersection level of service being a measure of the average delay at the intersection, as defined by the criteria set out in Table 2.1.

Table 2.1 SIDRA Intersection Level of Service criteria

| Level <br> of <br> service | Average delay <br> (seconds per <br> vehicle) | Criteria for traffic signals | Criteria for give way and stop <br> signs |
| :---: | :---: | :--- | :--- |
| A | $<14$ | Good operation | Good operation |
| B | 15 to 28 | Good operation with acceptable <br> delays and spare capacity | Good operation with acceptable <br> delays and spare capacity |
| C | 29 to 42 | Satisfactory | Satisfactory, but accident study <br> required |
| D | 43 to 56 | Near capacity | Near capacity and accident study <br> required |
| E | 57 to 70 | At capacity, at signals, incidents |  |
| will cause excessive delays | At capacity, requires other <br> control mode |  |  |
| F | $>70$ | Extra capacity required | At capacity, requires other <br> control mode |
| Source: | Adopted from Guide to Traffic Generating Developments (Roads and Maritime Services, <br> 2002 ) |  |  |

Table 2.2 presents a summary of the site access intersection operation during the weekday AM and PM peak hours, adopting the traffic generation. The full modelling results are presented in Appendix B.

It should be noted that the critical movement for the level of service at a priority-controlled intersection is the movement with the worst delay and therefore, this has been reported in Table 2.2.

Table 2.2 Site access intersection operation

| Year | Scenario | Volume | Degree of <br> Saturation | Average <br> delay <br> (seconds) | $95^{\text {th }}$ percentile <br> queue (metres) |  | Level of <br> South | East | West |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

### 2.2 RESULTS SUMMARY

Table 2.2 shows that the existing (2020 Existing Scenario) site access intersection should generally operate well during the AM peak hour, with Level of Service A, and with diminished yet acceptable performance during the PM Peak hour, at Level of Service C. This is due largely to the delay and queues experienced by right turning vehicles out of the site access and across opposing westbound through traffic volumes of up to 782 vehicles. 2020 With Development scenarios show a similar trend with the AM and PM peaks performing at Level of Service A and C respectively with no distinguishable change in the AM Peak, and a two seconds increase in delay and additional queuing in the PM Peak.

The future 2030 Scenarios show negligible increases under one second in delay for the AM Peaks. This is due to the background growth of $1 \%$ per annum, expected to operate with a maintained Level of Service A and negligible increases in delay and queueing.

The PM peak shows worsened performance with 45.3 seconds delay and 21 metre queues for the 2030 Existing PM and 49.3 seconds delay and 26 metre queues for the 2030 With Development PM scenario. This is likely due to heavy vehicle movements out of the site given the opposing westbound through traffic volumes of up to 908 vehicles. Overall, this remains an acceptable operational performance at Level of Service D given the main movements at this intersection are east-west through movements that are not impacted by the development's traffic.

### 2.3 OPERATIONAL IMPACTS

Key operational impacts are listed below:

- Minor increase in delay for right turn movements into the site access during both the AM and PM peaks between 2020 and 2030 scenarios due to slight increase in development traffic.
- Key impact is during the PM peak hour with right turning vehicles exiting site having to compete with opposing westbound through traffic of up to 782 vehicles in 2020 and 902 vehicles in 2030.
- 2020 and 2030 PM peak diminished performance is largely due to background traffic growth along Picton Road with additional growth potentially requiring intersection treatments to address worsening conditions for site access.


## 3. CONSTRUCTION IMPACTS

### 3.1 CONSTRUCTION WORKFORCE

Construction workforce will include a maximum of 15 to 25 staff per day, at an average of 10 to 15 . The construction plant required for works include:

- 5 tonne excavator
- Bobcat
- Tip truck
- 2.5 tonne forklift

The above equipment represents the likely construction vehicles on site to a maximum of 25 light vehicle and five heavy vehicle inbound movements during the AM peak and outbound during the PM peak.

### 3.2 CONSTRUCTION IMPACTS

Given that the total proposed construction traffic volumes ( $25 \mathrm{LV}, 5 \mathrm{HV}$ ) is less than that proposed to be generated by the development with upgrades ( $85 \mathrm{LV}, 40 \mathrm{HV}$ ), quantitative traffic assessment has not been undertaken for the construction period. The impacts of construction traffic would not eclipse those noted within the 2020 With Development scenario.

With all construction vehicles proposed to access the site via the Hume Highway, however the likely impacts are minimal based on low volumes of the generated construction traffic.

- Construction vehicles exiting during the PM peak turning right out of the site across the opposing westbound traffic flows of up to 782 vehicles may experience some increased delays.
- Potential delays or congestion at the Hume Highway's western ramps as vehicles exit the highway during the AM peak, merging with westbound traffic along Picton Road. Similarly, potential worsening performance of the southbound on-ramp with additional construction vehicles at this location mixing with existing vehicles.


## 4. MITIGATION MEASURES

### 4.1 OPERATIONAL IMPACT MITIGATION

The operational impacts are largely due to background traffic growth along Picton Road and the need for vehicles entering and exiting the site to cross the westbound through movement. Potential intersection treatments such as a formalised basic left turn lane with a longer lane length should be implemented to increase storage capacity on the southern leg (Allied Mills Access). However, it won't be required until 2030. Such treatments to address greater background growth up to and beyond 2030 (noting $1 \%$ p.a. has been assumed for this assessment) would require further investigation.

APPENDIX A HISTORICAL TRAFFIC SURVEYS

## TRANS TRAFFIC SURVEY <br> TURNING MOVEMENT SURVEY <br> $\overline{\text { ONV.GL }}$ $\overline{\overline{\text { ONVGL }}}$

Intersection of Picton Rd and Menangle Rd, Razorback

| GPS -34.193092, 150.644081 |  | North: | Menangle Rd | Survey Period | AM: | 6:00 AM-10:00 AM |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Date: | Tue 10/03/20 |  |  |  |  |  |
| Weather: | Overcast | East: | Picton Rd |  | PM: | 3:00 PM-7:00 PM |
| Suburban: | Razorback | South: | N/A | Traffic | AM: | 7:30 AM-8:30 AM |
| Customer: | McLaren | West: | Picton Rd | Peak | PM: | 4:15 PM-5:15 PM |


| Time |  | North Approach Menangle Rd |  |  | East Approach Picton Rd |  |  | West Approach Picton Rd |  |  | Hourly Total |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Period Start | Period End | U | R | L | U | R | WB | $u$ | EB | L | Hour | Peak |
| 6:00 | 6:15 | 0 | 2 | 17 | 0 | 6 | 41 | 0 | 141 | 13 | 1099 |  |
| 6:15 | 6:30 | 0 | 4 | 27 | 0 | 7 | 65 | 0 | 165 | 16 | 1161 |  |
| 6:30 | 6:45 | 0 | 10 | 22 | 0 | 20 | 87 | 0 | 141 | 21 | 1184 |  |
| 6:45 | 7:00 | 0 | 16 | 24 | 0 | 14 | 80 | 0 | 147 | 13 | 1258 |  |
| 7:00 | 7:15 | 0 | 8 | 27 | 0 | 21 | 68 | 0 | 140 | 18 | 1303 |  |
| 7:15 | 7:30 | 0 | 4 | 39 | 0 | 26 | 75 | 0 | 145 | 18 | 1323 |  |
| 7:30 | 7:45 | 0 | 13 | 52 | 0 | 39 | 68 | 0 | 166 | 37 | 1346 | Peak |
| 7:45 | 8:00 | 0 | 22 | 29 | 0 | 34 | 94 | 0 | 123 | 37 | 1292 |  |
| 8:00 | 8:15 | 0 | 10 | 27 | 0 | 54 | 89 | 0 | 95 | 27 | 1259 |  |
| 8:15 | 8:30 | 0 | 12 | 35 | 0 | 34 | 94 | 0 | 127 | 28 | 1252 |  |
| 8:30 | 8:45 | 0 | 15 | 32 | 0 | 45 | 88 | 0 | 105 | 36 | 1189 |  |
| 8:45 | 9:00 | 0 | 20 | 33 | 0 | 46 | 103 | 0 | 84 | 20 | 1103 |  |
| 9:00 | 9:15 | 0 | 18 | 24 | 0 | 38 | 85 | 0 | 100 | 30 | 1019 |  |
| 9:15 | 9:30 | 0 | 13 | 24 | 0 | 24 | 100 | 0 | 88 | 18 |  |  |
| 9:30 | 9:45 | 0 | 12 | 18 | 0 | 20 | 80 | 0 | 75 | 30 |  |  |
| 9:45 | 10:00 | 0 | 10 | 13 | 0 | 25 | 90 | 0 | 64 | 20 |  |  |
| 15:00 | 15:15 | 0 | 19 | 14 | 0 | 25 | 96 | 0 | 91 | 9 | 1150 |  |
| 15:15 | 15:30 | 0 | 17 | 30 | 0 | 29 | 90 | 0 | 93 | 16 | 1212 |  |
| 15:30 | 15:45 | 0 | 31 | 28 | 0 | 20 | 97 | 0 | 100 | 26 | 1319 |  |
| 15:45 | 16:00 | 0 | 21 | 17 | 0 | 40 | 131 | 0 | 104 | 6 | 1357 |  |
| 16:00 | 16:15 | 0 | 18 | 12 | 0 | 36 | 134 | 0 | 99 | 17 | 1415 |  |
| 16:15 | 16:30 | 0 | 26 | 24 | 0 | 36 | 190 | 0 | 86 | 20 | 1448 | Peak |
| 16:30 | 16:45 | 0 | 34 | 22 | 0 | 39 | 142 | 0 | 86 | 17 | 1442 |  |
| 16:45 | 17:00 | 0 | 33 | 19 | 0 | 29 | 183 | 0 | 97 | 16 | 1425 |  |
| 17:00 | 17:15 | 0 | 25 | 21 | 0 | 41 | 161 | 0 | 90 | 11 | 1413 |  |
| 17:15 | 17:30 | 0 | 28 | 20 | 0 | 38 | 172 | 0 | 103 | 15 | 1373 |  |
| 17:30 | 17:45 | 0 | 33 | 26 | 0 | 25 | 149 | 0 | 78 | 12 | 1281 |  |
| 17:45 | 18:00 | 0 | 32 | 20 | 0 | 24 | 182 | 0 | 93 | 14 | 1200 |  |
| 18:00 | 18:15 | 0 | 35 | 19 | 0 | 20 | 168 | 0 | 57 | 10 | 1025 |  |
| 18:15 | 18:30 | 0 | 29 | 9 | 0 | 20 | 123 | 0 | 87 | 16 |  |  |
| 18:30 | 18:45 | 0 | 16 | 9 | 0 | 17 | 124 | 0 | 66 | 10 |  |  |
| 18:45 | 19:00 | 0 | 12 | 11 | 0 | 11 | 81 | 0 | 64 | 11 |  |  |


| Peak Time | North Approach Menangle Rd |  |  | East Approach Picton Rd |  |  |  | West Approach Picton Rd |  |  | Peak <br> total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Period Start | Period End | U | R | L | U | R | WB | U | EB | L |  |
| $7: 30$ | $8: 30$ | 0 | 57 | 143 | 0 | 161 | 345 | 0 | 511 | 129 | 1346 |
| $16: 15$ | $17: 15$ | 0 | 118 | 86 | 0 | 145 | 676 | 0 | 359 | 64 | 1448 |

Note: Site sketch is for illustrating traffic flows. Direction is indicative only, drawing is not to scale and not an exact streets configuration.

a


| Time |  | North Approach Menangle Rd |  |  | East Approach Picton Rd |  |  | West Approach Picton Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Period Start | Period End | U | R | L | U | R | WB | U | EB | L |
| 6：00 | 6：15 | 0 | 1 | 13 | 0 | 5 | 29 | 0 | 124 | 13 |
| 6：15 | 6：30 | 0 | 4 | 25 | 0 | 5 | 53 | 0 | 152 | 15 |
| 6：30 | 6：45 | 0 | 9 | 18 | 0 | 20 | 79 | 0 | 121 | 21 |
| 6：45 | 7：00 | 0 | 16 | 22 | 0 | 14 | 70 | 0 | 136 | 13 |
| 7：00 | 7：15 | 0 | 6 | 25 | 0 | 21 | 52 | 0 | 125 | 18 |
| 7：15 | 7：30 | 0 | 4 | 39 | 0 | 25 | 62 | 0 | 132 | 17 |
| 7：30 | 7：45 | 0 | 13 | 46 | 0 | 37 | 56 | 0 | 156 | 32 |
| 7：45 | 8：00 | 0 | 22 | 27 | 0 | 33 | 81 | 0 | 115 | 37 |
| 8：00 | 8：15 | 0 | 9 | 25 | 0 | 52 | 75 | 0 | 85 | 27 |
| 8：15 | 8：30 | 0 | 10 | 35 | 0 | 31 | 86 | 0 | 108 | 27 |
| 8：30 | 8：45 | 0 | 15 | 30 | 0 | 45 | 75 | 0 | 89 | 36 |
| 8：45 | 9：00 | 0 | 18 | 33 | 0 | 41 | 95 | 0 | 71 | 19 |
| 9：00 | 9：15 | 0 | 15 | 24 | 0 | 36 | 73 | 0 | 86 | 30 |
| 9：15 | 9：30 | 0 | 12 | 24 | 0 | 24 | 86 | 0 | 78 | 18 |
| 9：30 | 9：45 | 0 | 12 | 17 | 0 | 18 | 70 | 0 | 68 | 30 |
| 9：45 | 10：00 | 0 | 9 | 13 | 0 | 24 | 77 | 0 | 51 | 19 |
| 15：00 | 15：15 | 0 | 18 | 14 | 0 | 23 | 84 | 0 | 80 | 9 |
| 15：15 | 15：30 | 0 | 17 | 29 | 0 | 28 | 78 | 0 | 81 | 16 |
| 15：30 | 15：45 | 0 | 29 | 27 | 0 | 18 | 84 | 0 | 94 | 26 |
| 15：45 | 16：00 | 0 | 20 | 11 | 0 | 40 | 121 | 0 | 95 | 6 |
| 16：00 | 16：15 | 0 | 17 | 10 | 0 | 33 | 124 | 0 | 88 | 16 |
| 16：15 | 16：30 | 0 | 24 | 21 | 0 | 35 | 178 | 0 | 83 | 19 |
| 16：30 | 16：45 | 0 | 34 | 21 | 0 | 35 | 135 | 0 | 81 | 17 |
| 16：45 | 17：00 | 0 | 33 | 19 | 0 | 27 | 171 | 0 | 88 | 16 |
| 17：00 | 17：15 | 0 | 25 | 20 | 0 | 38 | 151 | 0 | 84 | 11 |
| 17：15 | 17：30 | 0 | 27 | 19 | 0 | 38 | 170 | 0 | 95 | 15 |
| 17：30 | 17：45 | 0 | 33 | 26 | 0 | 23 | 144 | 0 | 75 | 12 |
| 17：45 | 18：00 | 0 | 32 | 17 | 0 | 22 | 173 | 0 | 91 | 14 |
| 18：00 | 18：15 | 0 | 35 | 19 | 0 | 20 | 162 | 0 | 55 | 10 |
| 18：15 | 18：30 | 0 | 29 | 9 | 0 | 20 | 121 | 0 | 85 | 15 |
| 18：30 | 18：45 | 0 | 16 | 8 | 0 | 17 | 121 | 0 | 61 | 10 |
| 18：45 | 19：00 | 0 | 12 | 10 | 0 | 11 | 78 | 0 | 61 | 11 |


| Peak Time | North Approach Menangle Rd |  |  |  | East Approach Picton Rd |  |  |  | West Approach Picton Rd |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Period Start Period End | U | R | L | U | Peak <br> total |  |  |  |  |  |  |
| $7: 30$ | $8: 30$ | 0 | 54 | 133 | 0 | 153 | WB | U | EB | L |  |
| $16: 15$ | $17: 15$ | 0 | 116 | 81 | 0 | 135 | 635 | 0 | 464 | 123 | 1225 |

Heavy Vehicles

| Time |  | North Approach Menangle Rd |  | East Approach Picton Rd |  |  | West Approach Picton Rd |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Period Start Period End | $U$ | R | L | U | R | WB | U | EB | L |  |
| $6: 00$ | $6: 15$ | 0 | 1 | 4 | 0 | 1 | 12 | 0 | 17 | 0 |
| $6: 15$ | $6: 30$ | 0 | 0 | 2 | 0 | 2 | 12 | 0 | 13 | 1 |
| $6: 30$ | $6: 45$ | 0 | 1 | 4 | 0 | 0 | 8 | 0 | 20 | 0 |
| $6: 45$ | $7: 00$ | 0 | 0 | 2 | 0 | 0 | 10 | 0 | 11 |  |
| $7: 00$ | $7: 15$ | 0 | 2 | 2 | 0 | 0 | 16 | 0 | 15 | 0 |
| $7: 15$ | $7: 30$ | 0 | 0 | 0 | 0 | 1 | 13 | 0 | 13 |  |
| $7: 30$ | $7: 45$ | 0 | 0 | 6 | 0 | 2 | 12 | 0 | 10 | 1 |
| $7: 45$ | $8: 00$ | 0 | 0 | 2 | 0 | 1 | 13 | 0 | 8 |  |
| $8: 00$ | $8: 15$ | 0 | 1 | 2 | 0 | 2 | 14 | 0 | 10 |  |
| $8: 15$ | $8: 30$ | 0 | 2 | 0 | 0 | 3 | 8 | 0 | 0 | 19 |


| 8:30 | 8:45 | 0 | 0 | 2 | 0 | 0 | 13 | 0 | 16 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 8:45 | 9:00 | 0 | 2 | 0 | 0 | 5 | 8 | 0 | 13 | 1 |
| 9:00 | 9:15 | 0 | 3 | 0 | 0 | 2 | 12 | 0 | 14 | 0 |
| 9:15 | 9:30 | 0 | 1 | 0 | 0 | 0 | 14 | 0 | 10 | 0 |
| 9:30 | 9:45 | 0 | 0 | 1 | 0 | 2 | 10 | 0 | 7 | 0 |
| 9:45 | 10:00 | 0 | 1 | 0 | 0 | 1 | 13 | 0 | 13 | 1 |
| 15:00 | 15:15 | 0 | 1 | 0 | 0 | 2 | 12 | 0 | 11 | 0 |
| 15:15 | 15:30 | 0 | 0 | 1 | 0 | 1 | 12 | 0 | 12 | 0 |
| 15:30 | 15:45 | 0 | 2 | 1 | 0 | 2 | 13 | 0 | 6 | 0 |
| 15:45 | 16:00 | 0 | 1 | 6 | 0 | 0 | 10 | 0 | 9 | 0 |
| 16:00 | 16:15 | 0 | 1 | 2 | 0 | 3 | 10 | 0 | 11 | 1 |
| 16:15 | 16:30 | 0 | 2 | 3 | 0 | 1 | 12 | 0 | 3 | 1 |
| 16:30 | 16:45 | 0 | 0 | 1 | 0 | 4 | 7 | 0 | 5 | 0 |
| 16:45 | 17:00 | 0 | 0 | 0 | 0 | 2 | 12 | 0 | 9 | 0 |
| 17:00 | 17:15 | 0 | 0 | 1 | 0 | 3 | 10 | 0 | 6 | 0 |
| 17:15 | 17:30 | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 8 | 0 |
| 17:30 | 17:45 | 0 | 0 | 0 | 0 | 2 | 5 | 0 | 3 | 0 |
| 17:45 | 18:00 | 0 | 0 | 3 | 0 | 2 | 9 | 0 | 2 | 0 |
| 18:00 | 18:15 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 2 | 0 |
| 18:15 | 18:30 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 1 |
| 18:30 | 18:45 | 0 | 0 | 1 | 0 | 0 | 3 | 0 | 5 | 0 |
| 18:45 | 19:00 | 0 | 0 | 1 | 0 | 0 | 3 | 0 | 3 | 0 |


| Peak Time |  | North Approach Menangle Rd |  |  | East Approach Picton Rd |  |  | West Approach Picton Rd |  |  | Peak total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Period Start | Period End | U | R | L | U | R | WB | U | EB | L |  |
| 7:30 | 8:30 | 0 | 3 | 10 | 0 | 8 | 47 | 0 | 47 | 6 | 121 |
| 16:15 | 17:15 | 0 | 2 | 5 | 0 | 10 | 41 | 0 | 23 | 1 | 82 |

APPENDIX B SIDRA MOVEMENT SUMMARIES

## MOVEMENT SUMMARY

$\nabla$ Site: 101 [2020 AM Picton Road / Allied Mills Access (Site
Folder: 2020)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INP } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | UT HV ] veh/h |  | AND WS HV ] \% | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% <br> [ Veh. <br> veh | CK OF Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| South: Allied Mills Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 1 | 0 | 1 | 0.0 | 0.001 | 8.3 | LOSA | 0.0 | 0.0 | 0.49 | 0.59 | 0.49 | 56.2 |
| 3 R2 | 1 | 0 | 1 | 0.0 | 0.002 | 11.7 | LOSA | 0.0 | 0.1 | 0.57 | 0.63 | 0.57 | 54.4 |
| Approach | 2 | 0 | 2 | 0.0 | 0.002 | 10.0 | LOS A | 0.0 | 0.1 | 0.53 | 0.61 | 0.53 | 55.3 |
| East: Picton Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 71 | 35 | 75 | 49.3 | 0.054 | 7.9 | LOSA | 0.0 | 0.0 | 0.00 | 0.63 | 0.00 | 51.9 |
| 5 T1 | 506 | 55 | 533 | 10.9 | 0.292 | 0.1 | LOSA | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 79.8 |
| Approach | 577 | 90 | 607 | 15.6 | 0.292 | 1.0 | NA | 0.0 | 0.0 | 0.00 | 0.08 | 0.00 | 74.8 |
| West: Picton Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 615 | 57 | 647 | 9.3 | 0.355 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 79.7 |
| 12 R 2 | 39 | 0 | 41 | 0.0 | 0.060 | 10.5 | LOS A | 0.2 | 1.5 | 0.56 | 0.78 | 0.56 | 55.6 |
| Approach | 654 | 57 | 688 | 8.7 | 0.355 | 0.7 | NA | 0.2 | 1.5 | 0.03 | 0.05 | 0.03 | 77.7 |
| All <br> Vehicles | 1233 | 147 | 1298 | 11.9 | 0.355 | 0.9 | NA | 0.2 | 1.5 | 0.02 | 0.06 | 0.02 | 76.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

$\nabla$ Site: 101 [2020 wDev AM Picton Road / Allied Mills Access
(Site Folder: 2020)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | JT MES HV] veh/h |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay $\qquad$ | Level of Service | $\begin{aligned} & 95 \% \text { B } \\ & \text { QU } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed $\mathrm{km} / \mathrm{h}$ |
| South: Allied Mills Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 1 | 0 | 1 | 0.0 | 0.001 | 8.3 | LOSA | 0.0 | 0.0 | 0.49 | 0.59 | 0.49 | 56.2 |
| 3 R2 | 1 | 0 | 1 | 0.0 | 0.002 | 11.8 | LOSA | 0.0 | 0.1 | 0.58 | 0.64 | 0.58 | 54.3 |
| Approach | 2 | 0 | 2 | 0.0 | 0.002 | 10.1 | LOS A | 0.0 | 0.1 | 0.54 | 0.62 | 0.54 | 55.2 |
| East: Picton Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 81 | 40 | 85 | 49.4 | 0.062 | 7.9 | LOSA | 0.0 | 0.0 | 0.00 | 0.63 | 0.00 | 51.9 |
| 5 T1 | 506 | 55 | 533 | 10.9 | 0.292 | 0.1 | LOSA | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 79.8 |
| Approach | 587 | 95 | 618 | 16.2 | 0.292 | 1.1 | NA | 0.0 | 0.0 | 0.00 | 0.09 | 0.00 | 74.3 |
| West: Picton Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 615 | 57 | 647 | 9.3 | 0.355 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 79.7 |
| 12 R 2 | 44 | 0 | 46 | 0.0 | 0.069 | 10.6 | LOSA | 0.3 | 1.8 | 0.57 | 0.80 | 0.57 | 55.5 |
| Approach | 659 | 57 | 694 | 8.6 | 0.355 | 0.8 | NA | 0.3 | 1.8 | 0.04 | 0.05 | 0.04 | 77.5 |
| All <br> Vehicles | 1248 | 152 | 1314 | 12.2 | 0.355 | 1.0 | NA | 0.3 | 1.8 | 0.02 | 0.07 | 0.02 | 75.9 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

$\nabla$ Site: 101 [2020 PM Picton Road / Allied Mills Access (Site
Folder: 2020)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INP } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | UT HV ] veh/h |  | AND WS HV ] \% | Deg. Satn v/c | Aver. Delay sec | Level of Service |  | CK OF Dist ] m | Prop. Que | Effective Stop Rate | Aver Cycles | Aver. Speed km/h |
| South: Allied Mills Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 39 | 0 | 41 | 0.0 | 0.095 | 12.3 | LOS A | 0.3 | 2.1 | 0.70 | 0.87 | 0.70 | 53.0 |
| 3 R2 | 71 | 35 | 75 | 49.3 | 0.409 | 32.4 | LOS C | 1.6 | 16.0 | 0.88 | 1.03 | 1.14 | 35.6 |
| Approach | 110 | 35 | 116 | 31.8 | 0.409 | 25.3 | LOS B | 1.6 | 16.0 | 0.81 | 0.97 | 0.98 | 40.3 |
| East: Picton Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 1 | 0 | 1 | 0.0 | 0.001 | 6.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.63 | 0.00 | 65.4 |
| 5 T1 | 782 | 51 | 823 | 6.5 | 0.440 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 79.6 |
| Approach | 783 | 51 | 824 | 6.5 | 0.440 | 0.1 | NA | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 79.6 |
| West: Picton Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 445 | 28 | 468 | 6.3 | 0.250 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 79.8 |
| 12 R 2 | 1 | 0 | 1 | 0.0 | 0.002 | 12.8 | LOSA | 0.0 | 0.1 | 0.68 | 0.71 | 0.68 | 53.7 |
| Approach | 446 | 28 | 469 | 6.3 | 0.250 | 0.1 | NA | 0.0 | 0.1 | 0.00 | 0.00 | 0.00 | 79.7 |
| All Vehicles | 1339 | 114 | 1409 | 8.5 | 0.440 | 2.2 | NA | 1.6 | 16.0 | 0.07 | 0.08 | 0.08 | 73.7 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

$\nabla$ Site: 101 [2020wDev PM Picton Road / Allied Mills Access
(Site Folder: 2020)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|l\|} \hline \text { Mov Turn } \\ \text { ID } \end{array}$ |  | UT HV ] veh/h |  | ND VS HV ] \% | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% <br> QU <br> [ Veh veh | CK OF UE Dist $]$ m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| South: Allied Mills Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 44 | 0 | 46 | 0.0 | 0.107 | 12.4 | LOS A | 0.3 | 2.4 | 0.70 | 0.87 | 0.70 | 52.9 |
| 3 R2 | 81 | 40 | 85 | 49.4 | 0.467 | 34.1 | LOS C | 1.9 | 19.1 | 0.89 | 1.05 | 1.22 | 35.0 |
| Approach | 125 | 40 | 132 | 32.0 | 0.467 | 26.5 | LOS B | 1.9 | 19.1 | 0.82 | 0.99 | 1.04 | 39.8 |
| East: Picton Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 1 | 0 | 1 | 0.0 | 0.001 | 6.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.63 | 0.00 | 65.4 |
| $5 \quad \mathrm{~T} 1$ | 782 | 51 | 823 | 6.5 | 0.440 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 79.6 |
| Approach | 783 | 51 | 824 | 6.5 | 0.440 | 0.1 | NA | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 79.6 |
| West: Picton Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 445 | 28 | 468 | 6.3 | 0.250 | 0.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 79.8 |
| 12 R 2 | 1 | 0 | 1 | 0.0 | 0.002 | 12.8 | LOSA | 0.0 | 0.1 | 0.68 | 0.71 | 0.68 | 53.7 |
| Approach | 446 | 28 | 469 | 6.3 | 0.250 | 0.1 | NA | 0.0 | 0.1 | 0.00 | 0.00 | 0.00 | 79.7 |
| All Vehicles | 1354 | 119 | 1425 | 8.8 | 0.467 | 2.5 | NA | 1.9 | 19.1 | 0.08 | 0.09 | 0.10 | 72.9 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

$\nabla$ Site: 101 [2030 AM Picton Road / Allied Mills Access (Site
Folder: 2030)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INP } \\ & \text { vOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | UT MES <br> HV ] veh/h |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay sec | Level of Service |  | $\begin{aligned} & \text { CK OF } \\ & \text { UE } \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. Que | Effective <br> Stop <br> Rate | Aver. No. Cycles | Aver. Speed km/h |
| South: Allied Mills Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 1 | 0 | 1 | 0.0 | 0.002 | 8.8 | LOS A | 0.0 | 0.0 | 0.52 | 0.61 | 0.52 | 55.8 |
| 3 R2 | 1 | 0 | 1 | 0.0 | 0.002 | 12.8 | LOS A | 0.0 | 0.1 | 0.62 | 0.65 | 0.62 | 53.7 |
| Approach | 2 | 0 | 2 | 0.0 | 0.002 | 10.8 | LOS A | 0.0 | 0.1 | 0.57 | 0.63 | 0.57 | 54.7 |
| East: Picton Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 71 | 35 | 75 | 49.3 | 0.054 | 7.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.63 | 0.00 | 51.9 |
| 5 T1 | 559 | 61 | 588 | 10.9 | 0.323 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 79.8 |
| Approach | 630 | 96 | 663 | 15.2 | 0.323 | 0.9 | NA | 0.0 | 0.0 | 0.00 | 0.07 | 0.00 | 75.2 |
| West: Picton Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 679 | 63 | 715 | 9.3 | 0.392 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 79.7 |
| 12 R 2 | 39 | 0 | 41 | 0.0 | 0.066 | 11.1 | LOS A | 0.2 | 1.7 | 0.58 | 0.81 | 0.58 | 55.1 |
| Approach | 718 | 63 | 756 | 8.8 | 0.392 | 0.7 | NA | 0.2 | 1.7 | 0.03 | 0.04 | 0.03 | 77.8 |
| All <br> Vehicles | 1350 | 159 | 1421 | 11.8 | 0.392 | 0.8 | NA | 0.2 | 1.7 | 0.02 | 0.06 | 0.02 | 76.5 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

$\nabla$ Site: 101 [2030 wDev AM Picton Road / Allied Mills Access
(Site Folder: 2030)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { INP } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | JT MES HV ] veh/h |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service | $\begin{gathered} 95 \% \text { B } \\ \text { QU } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver No. Cycles | Aver. Speed <br> km/h |
| South: Allied Mills Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 1 | 0 | 1 | 0.0 | 0.002 | 8.8 | LOSA | 0.0 | 0.0 | 0.52 | 0.61 | 0.52 | 55.8 |
| 3 R2 | 1 | 0 | 1 | 0.0 | 0.002 | 12.9 | LOSA | 0.0 | 0.1 | 0.62 | 0.66 | 0.62 | 53.6 |
| Approach | 2 | 0 | 2 | 0.0 | 0.002 | 10.9 | LOS A | 0.0 | 0.1 | 0.57 | 0.63 | 0.57 | 54.7 |
| East: Picton Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 81 | 40 | 85 | 49.4 | 0.062 | 7.9 | LOSA | 0.0 | 0.0 | 0.00 | 0.63 | 0.00 | 51.9 |
| 5 T1 | 559 | 61 | 588 | 10.9 | 0.323 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 79.8 |
| Approach | 640 | 101 | 674 | 15.8 | 0.323 | 1.1 | NA | 0.0 | 0.0 | 0.00 | 0.08 | 0.00 | 74.7 |
| West: Picton Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 679 | 63 | 715 | 9.3 | 0.392 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 79.7 |
| 12 R 2 | 44 | 0 | 46 | 0.0 | 0.075 | 11.3 | LOS A | 0.3 | 1.9 | 0.59 | 0.83 | 0.59 | 55.0 |
| Approach | 723 | 63 | 761 | 8.7 | 0.392 | 0.8 | NA | 0.3 | 1.9 | 0.04 | 0.05 | 0.04 | 77.5 |
| All <br> Vehicles | 1365 | 164 | 1437 | 12.0 | 0.392 | 0.9 | NA | 0.3 | 1.9 | 0.02 | 0.06 | 0.02 | 76.1 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

$\nabla$ Site: 101 [2030 PM Picton Road / Allied Mills Access (Site
Folder: 2030)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | UT <br> MES HV ] veh/h |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. <br> Satn <br> v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate |  | Aver Speed km/h |
| South: Allied Mills Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 39 | 0 | 41 | 0.0 | 0.114 | 14.2 | LOS A | 0.4 | 2.5 | 0.75 | 0.90 | 0.75 | 51.6 |
| 3 R2 | 71 | 35 | 75 | 49.3 | 0.532 | 45.3 | LOS D | 2.1 | 21.1 | 0.93 | 1.08 | 1.32 | 31.7 |
| Approach | 110 | 35 | 116 | 31.8 | 0.532 | 34.2 | LOS C | 2.1 | 21.1 | 0.86 | 1.02 | 1.12 | 36.7 |
| East: Picton Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 1 | 0 | 1 | 0.0 | 0.001 | 6.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.63 | 0.00 | 65.4 |
| 5 T1 | 863 | 56 | 908 | 6.5 | 0.486 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 79.5 |
| Approach | 864 | 56 | 909 | 6.5 | 0.486 | 0.1 | NA | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 79.5 |
| West: Picton Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 492 | 31 | 518 | 6.3 | 0.276 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 79.8 |
| 12 R2 | 1 | 0 | 1 | 0.0 | 0.003 | 14.5 | LOSA | 0.0 | 0.1 | 0.73 | 0.74 | 0.73 | 52.4 |
| Approach | 493 | 31 | 519 | 6.3 | 0.276 | 0.1 | NA | 0.0 | 0.1 | 0.00 | 0.00 | 0.00 | 79.7 |
| All Vehicles | 1467 | 122 | 1544 | 8.3 | 0.532 | 2.7 | NA | 2.1 | 21.1 | 0.07 | 0.08 | 0.08 | 73.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

$\nabla$ Site: 101 [2030 wDev PM Picton Road / Allied Mills Access
(Site Folder: 2030)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | JT MES HV] veh/h |  | $\begin{aligned} & \text { WD } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \end{gathered}$ | Prop. Que | Effective Stop Rate | $\begin{aligned} & \text { Aver. } \\ & \text { No. } \\ & \text { Cycles } \end{aligned}$ | Aver. Speed <br> km/h |
| South: Allied Mills Access |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 44 | 0 | 46 | 0.0 | 0.129 | 14.2 | LOS A | 0.4 | 2.8 | 0.76 | 0.90 | 0.76 | 51.5 |
| 3 R 2 | 81 | 40 | 85 | 49.4 | 0.608 | 49.3 | LOS D | 2.6 | 25.6 | 0.94 | 1.12 | 1.45 | 30.6 |
| Approach | 125 | 40 | 132 | 32.0 | 0.608 | 36.9 | LOS C | 2.6 | 25.6 | 0.87 | 1.04 | 1.21 | 35.7 |
| East: Picton Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 1 | 0 | 1 | 0.0 | 0.001 | 6.9 | LOSA | 0.0 | 0.0 | 0.00 | 0.63 | 0.00 | 65.4 |
| 5 T1 | 863 | 56 | 908 | 6.5 | 0.486 | 0.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 79.5 |
| Approach | 864 | 56 | 909 | 6.5 | 0.486 | 0.1 | NA | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 79.5 |
| West: Picton Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 492 | 31 | 518 | 6.3 | 0.276 | 0.1 | LOSA | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 79.8 |
| 12 R2 | 1 | 0 | 1 | 0.0 | 0.003 | 14.5 | LOSA | 0.0 | 0.1 | 0.73 | 0.74 | 0.73 | 52.4 |
| Approach | 493 | 31 | 519 | 6.3 | 0.276 | 0.1 | NA | 0.0 | 0.1 | 0.00 | 0.00 | 0.00 | 79.7 |
| All <br> Vehicles | 1482 | 127 | 1560 | 8.6 | 0.608 | 3.2 | NA | 2.6 | 25.6 | 0.07 | 0.09 | 0.10 | 72.1 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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